

# Collisions: Non-linearities without the use of iterative solvers

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## 1 Introduction

This document shows several examples of non-linearities in physical modelling based on a method recently published by Michele Ducceschi in [2].

## 2 Preabmble: Mass-barrier collision

The simplest collision case is a mass colliding with a rigid barrier. Imagine a mass at location  $u = u(t)$  colliding with a barrier at location  $b$ . If the barrier is placed above<sup>1</sup> the mass, the force it exerts on the mass will be negative and its system would be described as

$$Mu_{tt} = -K[\eta]_+^\alpha, \quad (1)$$

with mass  $M$  (in kg), collision stiffness  $K \geq 0$  (in N/m [???](#)) and non-linearity  $\alpha \geq 1$  and  $\eta = u - b$  describes the relative displacement between the two colliding bodies (in m).

$$[\eta]_+ = \frac{\eta + |\eta|}{2} \quad (2)$$

describes the positive part of  $\eta$  (see Figure 1). This can be interpreted as that  $\eta$  will only be non-zero when the two colliding bodies are in contact.

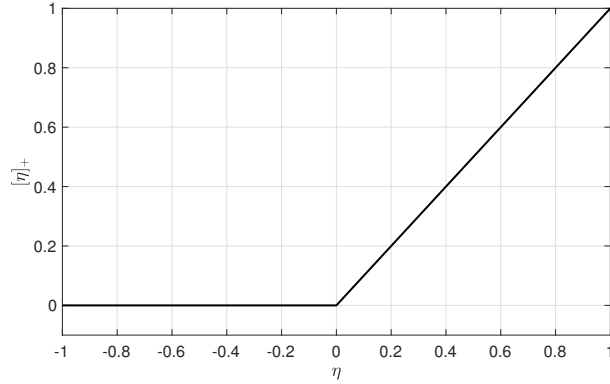


Figure 1: A plot of  $[\eta]_+$ .

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<sup>1</sup>When talking about an element being ‘above’ or ‘below’ another in this context, what is meant is a more positive or negative displacement, i.e., a mass with a displacement of 0.01 will be ‘above’ a barrier with a displacement of -0.05. Along these lines, a positive force acting on an element will accelerate it upwards and a negative force will accelerate it downwards.

The second term can be rewritten to

$$\phi'(\eta) = \frac{d\phi(\eta)}{d\eta} \xrightarrow{\text{chain rule}} \frac{d\phi}{dt} \frac{dt}{d\eta} = \frac{\left(\frac{d\phi}{dt}\right)}{\left(\frac{d\eta}{dt}\right)} = \frac{\dot{\phi}(\eta)}{\dot{\eta}} = K[\eta]_+^\alpha \quad (3)$$

where

$$\phi(\eta) = \frac{K}{\alpha + 1} [\eta]_+^{\alpha+1}, \quad (4)$$

describes the potential energy of the system. Equation (1) can then be rewritten to

$$Mu_{tt} = -\phi'(\eta). \quad (5)$$

According to Ducceschi in [2], this potential has been used before in the literature, but when discretised, results in an implicit system for which an iterative solver (such as Newton-Raphson's method) must be employed. In his work, he proposes to rewrite the potential in Eq. (3) as

$$\psi\psi' \quad \text{where} \quad \psi = \sqrt{2\phi} \quad \text{and} \quad \psi' = \frac{\dot{\psi}}{\dot{\eta}}, \quad (6)$$

yielding

$$Mu_{tt} = -\psi\psi'. \quad (7)$$

See Appendix A for a proof that  $\phi'$  is equivalent to  $\psi\psi'$ .

## 2.1 Discrete time

For the discrete time definition of  $\psi'$  we can use

$$g^n = \frac{\delta_{t+}\psi^{n-1/2}}{\delta_t.\eta^n}, \quad (8)$$

where  $\psi$  at interleaved grid point  $n - 1/2$  is defined as

$$\psi^{n-1/2} = \mu_{t-}\psi^n, \quad (9)$$

and is proven useful as [it requires less memory...](#) Equation (7) can then be discretised to the following system.<sup>2</sup>

$$\begin{cases} M\delta_{tt}u^n & = -(\mu_{t+}\psi^{n-1/2})g^n & (10a) \\ \delta_{t+}\psi^{n-1/2} & = g^n\delta_t.\eta^n & (10b) \\ \eta^n & = u^n - b & (10c) \end{cases}$$

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<sup>2</sup>It is important to realise whether the mass is placed above or below the barrier as this will affect the following two things in (10):

1. The direction of the force (the sign of the term right-hand side in (10a)): if the barrier is placed above the mass this will exert a downwards (negative) force on the mass, when below, the opposite applies. Of course, the sign used here is determined by the system described in (1) where the force-term is negative.
2. The definition of eta (what is subtracted from what?): imagine that the collision happens when  $\eta$  is positive, so when the barrier is placed above the mass,  $u^n - b$  will be positive on collision. Remember:  $\eta$  is defined as the element above subtracted from the element below.

## 2.2 Implementation

### Step 1: Calculate $g^n$

The first step is to calculate  $g^n$  using its analytic derivative

$$g^n = \psi' \Big|_{\eta=\eta^n} = \frac{\phi'}{\sqrt{2\phi}} \Big|_{\eta=\eta^n} \quad (11)$$

which, using (3) and (4), can conveniently be rewritten to

$$g^n = \frac{K[\eta^n]_+^\alpha}{\sqrt{\frac{2K}{\alpha+1}[\eta^n]_+^{\alpha+1}}} = K \sqrt{\frac{\alpha+1}{2K}} [\eta^n]_+^\alpha [\eta^n]_+^{-\frac{(\alpha+1)}{2}} = \sqrt{\frac{K(\alpha+1)}{2}} [\eta^n]_+^{\frac{\alpha-1}{2}}. \quad (12)$$

### Step 2: Substitution of identity for $\mu_{t+}\psi^{n-1/2}$

Using the following identity

$$\mu_{t+}\psi^{n-1/2} = \frac{k}{2}\delta_{t+}\psi^{n-1/2} + \psi^{n-1/2}, \quad (13)$$

inserting (10b) into this

$$\mu_{t+}\psi^{n-1/2} = \frac{k}{2}g^n\delta_t.\eta^n + \psi^{n-1/2},$$

and inserting this into (10a) yields

$$M\delta_{tt}u^n = -\left(\frac{k}{2}g^n\delta_t.\eta^n + \psi^{n-1/2}\right)g^n. \quad (14)$$

### Step 3: Solving the system for $u^{n+1}$

As in this case, the position of barrier  $b$  is static, the following is true:

$$\frac{d\eta}{dt} = \frac{d}{dt}(u - b) \Rightarrow \delta_t.\eta^n = \delta_t.u^n, \quad (15)$$

i.e., the time derivative of  $\eta$  equals the time derivative of  $u$ .<sup>3</sup> Now we can solve (14) explicitly as  $u^{n+1}$  is the only unknown

$$\left(\frac{M}{k^2} + \frac{(g^n)^2}{4}\right)u^{n+1} = \frac{M}{k^2}(2u^n - u^{n-1}) + \frac{(g^n)^2}{4}u^{n-1} - \psi^{n-1/2}g^n, \quad (16)$$

and can be solved by a simple division.

### Step 4: Calculate $\eta^{n+1}$ and $\phi^{n+1/2}$

From this,  $\eta^{n+1}$  can be calculated using (10c):

$$\eta^{n+1} = u^{n+1} - b, \quad (17)$$

and can be used to calculate  $\psi^{n+1/2}$  by expanding and rewriting (10b) to

$$\psi^{n+1/2} = \psi^{n-1/2} + \frac{\eta^{n+1} - \eta^{n-1}}{2}. \quad (18)$$

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<sup>3</sup>Note that if the barrier was placed underneath the mass, making (10c)  $\eta^n = b - u^n$ , this would result in  $\delta_t.\eta^n = -\delta_t.u^n$ .

### 3 Mass-spring - Rigid barrier collision

If the mass described in the previous section (Eq. (7)) is given a restoring force, the following equation emerges

$$Mu_{tt} = -M\omega_0^2 u - \psi\psi'. \quad (19)$$

where  $\omega_0 = 2\pi f_0$  is the angular frequency of the mass-spring system (in  $\text{s}^{-1}$ ) with fundamental frequency  $f_0$  (in Hz). This system can be discretised to the following system (similar to (10))

$$\begin{cases} M\delta_{tt}u^n &= -M\omega_0^2 u^n - (\mu_{t+}\psi^{n-1/2})g^n, \\ \delta_{t+}\psi^{n-1/2} &= g^n\delta_t\eta^n \\ \eta^n &= u^n - b \end{cases} \quad (20a)$$

$$(20b)$$

$$(20c)$$

where  $g^n$  is again computed according to (12). The system can, similarly to the one in the previous section, be discretised to

$$\left(\frac{M}{k^2} + \frac{(g^n)^2}{4}\right)u^{n+1} = \frac{M}{k^2}(2u^n - u^{n-1}) - M\omega_0^2 u^n + \frac{(g^n)^2}{4}u^{n-1} - \psi^{n-1/2}g^n, \quad (21)$$

after which  $\eta^{n+1}$  using (17) and  $\psi^{n+1/2}$  using (18) can be calculated.

### 4 Mass-spring - Mass-spring Collision

The initial idea for this implementation was to make the barrier in the previous section able to move sinusoidally. However, as the barrier would be unaffected by the mass, the energy balance would be incorrect. Imagine a baseball bat hitting a ping-pong ball. Even though the bat would not seem to be affected by the ping-pong ball, it will as some energy of the ball will be transferred into the bat. To model this behaviour, we can implement two colliding masses, one of which has a very high mass relative to the other, and to make it more interesting, we can add a restoring force to both. Assuming a mass with displacement  $u = u(t)$  to be placed above a mass with displacement  $w = w(t)$ , the (continuous) system will look like this

$$\begin{cases} M_1u_{tt} &= -M_1\omega_1^2 u + \psi\psi' \\ M_2w_{tt} &= -M_2\omega_2^2 w - \psi\psi' \end{cases} \quad (22a)$$

$$(22b)$$

which, when discretised yields

$$\begin{cases} M_1\delta_{tt}u^n &= -M_1\omega_1^2 u^n + (\mu_{t+}\psi^{n-1/2})g^n \\ M_2\delta_{tt}w^n &= -M_2\omega_2^2 w^n - (\mu_{t+}\psi^{n-1/2})g^n \\ \delta_{t+}\psi^{n-1/2} &= g^n\delta_t\eta^n \\ \eta^n &= w^n - u^n \end{cases} \quad (23a)$$

$$(23b)$$

$$(23c)$$

$$(23d)$$

Note that the term denoting the collision will have a positive effect on  $u$  and a negative effect on  $w$  as  $u$  is placed above  $w$ .

As we are now working with two moving objects colliding, (15) is not valid anymore. The main challenge here, is to solve the system for two unknowns:  $u^{n+1}$  and  $w^{n+1}$ . Rewriting (23a) and (23b) in terms of these two unknowns yields

$$\mathbf{A} \begin{bmatrix} u^{n+1} \\ w^{n+1} \end{bmatrix} = \mathbf{v} \quad \Rightarrow \quad \begin{bmatrix} u^{n+1} \\ w^{n+1} \end{bmatrix} = \mathbf{A}^{-1}\mathbf{v} \quad (24)$$

where

$$\mathbf{A} = \begin{bmatrix} \frac{M_1}{k^2} + \frac{(g^n)^2}{4} & -\frac{(g^n)^2}{4} \\ -\frac{(g^n)^2}{4} & \frac{M_2}{k^2} + \frac{(g^n)^2}{4} \end{bmatrix} \quad \text{and} \quad \mathbf{v} = \begin{bmatrix} \frac{M_1}{k^2} (2u^n - u^{n-1}) - M_1 \omega_1 u^n - \frac{(g^n)^2}{4} \eta^{n-1} + \psi^{n-1/2} g^n \\ \frac{M_2}{k^2} (2w^n - w^{n-1}) - M_2 \omega_2 w^n + \frac{(g^n)^2}{4} \eta^{n-1} - \psi^{n-1/2} g^n \end{bmatrix}$$

See Appendix B for the derivation of this. The relative displacement  $\eta^{n+1}$  can then be calculated using (23d).

## 5 String - String Collision

Moving to a string - string collision, we can define states  $u = u(x, t)$  and  $w = w(x, t)$  which are now distributed or defined over spatial coordinate  $0 \leq x \leq L$  where  $L$  is the length of the respective string. Using the definitions of the stiff string defined in, fx., [1], the continuous system is defined as

$$\begin{cases} \rho_1 A_1 u_{tt} & = T_1 u_{xx} - E_1 I_1 u_{xxxx} + \psi \psi' \\ \rho_2 A_2 w_{tt} & = T_2 w_{xx} - E_2 I_2 w_{xxxx} - \psi \psi' \end{cases} \quad (25a)$$

$$(25b)$$

with material density  $\rho$  (in  $\text{kg}\cdot\text{m}^{-3}$ ), cross-sectional area  $A = \pi r^2$  (in  $\text{m}^2$ ) with radius  $r$  (in m), tension  $T$  (in N), Young's modulus  $E$  (in Pa) and area moment of inertia  $I = \pi r^4/4$  (in  $\text{m}^4$ ) of string 1 with displacement  $u$  and string 2 with displacement  $w$  respectively. When discretising this,  $x = lh$  for grid point  $l \in [0, \dots, N]$  and grid spacing  $h$ , yields

$$\begin{cases} \rho_1 A_1 \delta_{tt} u_l^n & = T_1 \delta_{xx} u_l^n - E_1 I_1 \delta_{xxxx} u_l^n + (\mu_{t+} \psi_l^{n-1/2}) g_l^n \end{cases} \quad (26a)$$

$$\begin{cases} \rho_2 A_2 \delta_{tt} w_l^n & = T_2 \delta_{xx} w_l^n - E_2 I_2 \delta_{xxxx} w_l^n - (\mu_{t+} \psi_l^{n-1/2}) g_l^n \end{cases} \quad (26b)$$

$$\begin{cases} \delta_{t+} \psi_l^{n-1/2} & = g_l^n \delta_t \eta_l^n \end{cases} \quad (26c)$$

$$\begin{cases} \eta_l^n & = w_l^n - u_l^n \end{cases} \quad (26d)$$

Note that  $\psi$ ,  $g$  and  $\eta$  are now also distributed, i.e., defined separately for every grid point on the string separately. Also, it is assumed that both strings have the same grid spacing  $h$  and number of points  $N$  and are located right above/below each other. We can solve this system similarly to (23) and solve for every individual grid point  $l$ :

$$\begin{bmatrix} u_l^{n+1} \\ w_l^{n+1} \end{bmatrix} = \mathbf{A}_l^{-1} \mathbf{v}_l \quad (27)$$

where

$$\mathbf{A}_l = \begin{bmatrix} \frac{\rho_1 A_1}{k^2} + \frac{(g_l^n)^2}{4} & -\frac{(g_l^n)^2}{4} \\ -\frac{(g_l^n)^2}{4} & \frac{\rho_2 A_2}{k^2} + \frac{(g_l^n)^2}{4} \end{bmatrix} \quad \text{and} \quad \mathbf{v}_l = \begin{bmatrix} \frac{\rho_1 A_1}{k^2} (2u_l^n - u_l^{n-1}) + T_1 \delta_{xx} u_l^n - E_1 I_1 \delta_{xxxx} u_l^n - \frac{(g_l^n)^2}{4} \eta_l^{n-1} + \psi_l^{n-1/2} g_l^n \\ \frac{\rho_2 A_2}{k^2} (2w_l^n - w_l^{n-1}) + T_2 \delta_{xx} w_l^n - E_2 I_2 \delta_{xxxx} w_l^n + \frac{(g_l^n)^2}{4} \eta_l^{n-1} - \psi_l^{n-1/2} g_l^n \end{bmatrix}$$

For brevity, the spatial-derivative operators  $\delta_{xx}$  and  $\delta_{xxxx}$  have not been expanded.

## 6 Mass-spring - String Collision

The mass-spring - string collision is a bit trickier as we are now working with two different systems. We will denote the string with state  $u = u(x, t)$  and the mass with state  $w = w(t)$ . When placing the

string above the mass, the following system emerges:

$$\begin{cases} \rho A \delta_{tt} u_l^n &= T \delta_{xx} u_l^n - EI \delta_{xxxx} u_l^n + J(l_m) (\mu_{t+} \psi_1^{n-1/2}) g^n & (28a) \\ M \delta_{tt} w^n &= -M \omega_0^2 w^n - (\mu_{t+} \psi^{n-1/2}) g^n & (28b) \\ \delta_{t+} \psi^{n-1/2} &= g^n \delta_t \eta^n & (28c) \\ \eta^n &= w^n - u_{l_m}^n & (28d) \end{cases}$$

where  $0 \leq l_m \leq N$  is the location (in grid points) of the mass along the string. It is important to note that the mass only interacts with one grid point, meaning that the mass (in kg) of the string that it interacts with is only  $\rho A h$ , i.e., the mass of one grid point. This is where the spreading operator  $J$  comes in:

$$J(l_m) = \begin{cases} 1/h, & l = l_m \\ 0, & \text{otherwise} \end{cases} \quad (29)$$

and, as can be seen in (28a), locates the collision term at  $l_m$  and scales it by  $1/h$  at that location. As the collision happens at only one point, i.e., is not distributed as in Section 5, we solve the following system at the point  $l_m$  along the string:

$$\begin{bmatrix} u_{l_m}^{n+1} \\ w^{n+1} \end{bmatrix} = \mathbf{A}^{-1} \mathbf{v} \quad (30)$$

where

$$\mathbf{A} = \begin{bmatrix} \frac{\rho A}{k^2} + \frac{(g^n)^2}{4h} & -\frac{(g^n)^2}{4h} \\ -\frac{(g^n)^2}{4} & \frac{M}{k^2} + \frac{(g^n)^2}{k^2} \end{bmatrix} \quad \text{and} \\ \mathbf{v} = \begin{bmatrix} \frac{\rho A}{k^2} (2u_{l_m}^n - u_{l_m}^{n-1}) + T \delta_{xx} u_{l_m}^n - EI \delta_{xxxx} u_{l_m}^n + \left( -\frac{(g^n)^2}{4} \eta^{n-1} + \psi^{n-1/2} g^n \right) / h \\ \frac{M}{k^2} (2w^n - w^{n-1}) - M \omega_0^2 w^n + \frac{(g^n)^2}{4} \eta^{n-1} - \psi^{n-1/2} g^n \end{bmatrix}$$

Once  $\eta^{n+1}$  is then calculated from this, it can be applied to the string in a common finite-difference scheme for calculating  $u^{n+1}$

$$\frac{\rho A}{k^2} u_l^{n+1} = \frac{\rho A}{k^2} (2u_l^n - u_l^{n-1}) + T \delta_{xx} u_l^n - EI \delta_{xxxx} u_l^n + J(l_m) \left( \frac{(g^n)^2}{4} (\eta^{n+1} - \eta^{n-1}) + \psi^{n-1/2} g^n \right). \quad (31)$$

## 7 Tromba Marina

The tromba marina is a bowed string instrument with a rattling bridge. The bridge has a pivot-point right below where the string rests on the bridge and moves according to the movement of the string. The system we will be looking will contain a string, a mass simulating the bridge and a plate simulating the body of the instrument (see Figure 2).

$$\begin{cases} \rho_s A \delta_{tt} u_l^n &= T \delta_{xx} u_l^n - EI \delta_{xxxx} u_l^n - J_s(l_{br}) F_\alpha & (32a) \\ M \delta_{tt} w^n &= -M \omega_0^2 w^n + (\mu_{t+} \psi^{n-1/2}) g^n + F_\alpha & (32b) \\ \rho_p H \delta_{tt} v_{(l,m)}^n &= -D \delta_{\Delta\Box} \delta_{\Delta\Box} v_{(l,m)}^n - J_p(l_{br}, m_{br}) (\mu_{t+} \psi^{n-1/2}) g^n & (32c) \\ \delta_{t+} \psi^{n-1/2} &= g^n \delta_t \eta_c^n & (32d) \\ \eta_c^n &= v_{(l_{br}, m_{br})}^n - w^n & (32e) \\ F_\alpha &= K_1 \mu_{tt} \eta_s^n + K_3 (\eta_s^n)^2 \mu_t \eta_s^n & (32f) \\ \eta_s^n &= u_{l_{br}}^n - w^n & (32g) \end{cases}$$

where  $D = \frac{EH^3}{12(1-\nu^2)}$ . The subscripts s and p for  $\rho$  denote that it either belongs to the string or the plate. The subscripts s and c for  $\eta$  denote that it either belongs to the non-linear spring or the collision.

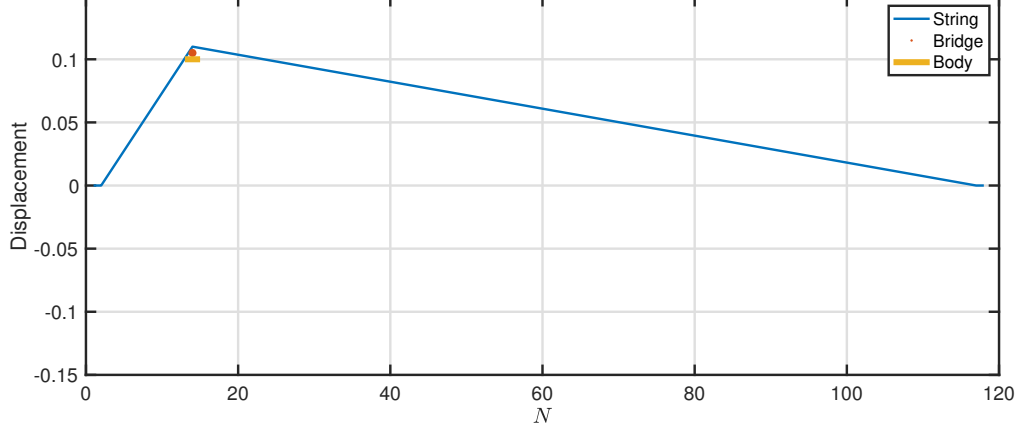


Figure 2: The tromba marina system: a string, a bridge (mass) and body (rigid barrier).

As done in Section 6, the spreading operator  $J_s$  is used to apply the effect of the mass only to grid point  $l_{br}$  on the string. We now also use the 2D spreading operator  $J_p$  to apply the effect of the mass to grid point  $(l_{br}, m_{br})$

$$J_p(l_{br}, m_{br}) = \begin{cases} 1/h_p^2, & l = l_{br} \wedge m = m_{br} \\ 0, & \text{otherwise} \end{cases} \quad (33)$$

Expanding the operators of (32f) and rewriting for  $\eta_s$  yields:

$$\eta_s^{n+1} = \frac{F_\alpha}{\Phi} - \frac{K_1 \eta_s^n}{2\Phi} - \eta_s^{n-1}, \quad (34)$$

where

$$\Phi = \frac{K_1}{4} + \frac{K_3(\eta_s^n)^2}{2}. \quad (35)$$

We can define intermediate states (at the bridge) for the connected components, i.e.,  $u_{br}^I$  and  $w^I$  (where the subscript br is short for  $l_{br}$ ) that exclude the effects of spring and collision forces:

$$u_{br}^I = 2u_{br}^n - u_{br}^{n-1} + \frac{Tk^2}{\rho_s A} \delta_{xx} u_{br}^n - \frac{EI k^2}{\rho_s A} \delta_{xxx} u_{br}^n \quad (36a)$$

$$w^I = 2w^n - w^{n-1} - k^2 \omega_0^2 w^n \quad (36b)$$

Then, looking at the full system in (71) we get that

$$u_{br}^{n+1} = u_{br}^I - \frac{F_\alpha k^2}{h_s \rho_s A} \quad (37a)$$

$$w^{n+1} = w^I + \frac{k^2}{M} ((\mu_{t+} \psi^{n-1/2}) g^n + F_\alpha) \quad (37b)$$

$$(37c)$$

As the  $(\mu_{t+}\psi^{n-1/2})$ -term in (37b) also contains  $w^{n+1}$  we need to solve for this

$$\begin{aligned}
\frac{M}{k^2}w^{n+1} &= \frac{M}{k^2}w^I + \frac{(g^n)^2}{4}(\eta_c^{n+1} - \eta_c^{n-1}) + \psi^{n-1/2}g^n + F_\alpha \\
\frac{M}{k^2}w^{n+1} &= \frac{M}{k^2}w^I + \frac{(g^n)^2}{4}((v_{\text{br}}^{n+1} - w^{n+1}) - \eta_c^{n-1}) + \psi^{n-1/2}g^n + F_\alpha \\
\left(\frac{M}{k^2} + \frac{(g^n)^2}{4}\right)w^{n+1} &= \frac{M}{k^2}w^I + \frac{(g^n)^2}{4}(v_{\text{br}}^{n+1} - \eta_c^{n-1}) + \psi^{n-1/2}g^n + F_\alpha \\
w^{n+1} &= \frac{\frac{M}{k^2}w^I + \frac{(g^n)^2}{4}(v_{\text{br}}^{n+1} - \eta_c^{n-1}) + \psi^{n-1/2}g^n + F_\alpha}{\frac{M}{k^2} + \frac{(g^n)^2}{4}}
\end{aligned} \tag{38}$$

Then writing out (71g) for  $\eta_s^{n+1}$  gives

$$\eta_s^{n+1} = u_{\text{br}}^I - \frac{F_\alpha k^2}{h_s \rho_s A} - \frac{\frac{M}{k^2}w^I + \frac{(g^n)^2}{4}(v_{\text{br}}^{n+1} - \eta_c^{n-1}) + \psi^{n-1/2}g^n + F_\alpha}{\frac{M}{k^2} + \frac{(g^n)^2}{4}}. \tag{39}$$

Setting Equations (34) and (39) equal to each other, we can solve for  $F_\alpha$

$$\begin{aligned}
\frac{F_\alpha}{\Phi} - \frac{K_1 \eta_s^n}{2\Phi} - \eta_s^{n-1} &= u_{\text{br}}^I - \frac{F_\alpha k^2}{h_s \rho_s A} - \frac{\frac{M}{k^2}w^I + \frac{(g^n)^2}{4}(v_{\text{br}}^{n+1} - \eta_c^{n-1}) + \psi^{n-1/2}g^n + F_\alpha}{\frac{M}{k^2} + \frac{(g^n)^2}{4}} \\
\Psi F_\alpha &= \frac{K_1 \eta_s^n}{2\Phi} + \eta_s^{n-1} + u_{\text{br}}^I - \frac{\frac{M}{k^2}w^I + \frac{(g^n)^2}{4}(v_{\text{br}}^{n+1} - \eta_c^{n-1}) + \psi^{n-1/2}g^n}{\frac{M}{k^2} + \frac{(g^n)^2}{4}}
\end{aligned} \tag{40}$$

where

$$\Psi = \frac{1}{\Phi} + \frac{k^2}{h_s \rho_s A} + \frac{1}{\frac{M}{k^2} + \frac{(g^n)^2}{4}}. \tag{41}$$

If we factor out the effect of unknown  $v_{\text{br}}^{n+1}$  we get

$$\begin{aligned}
F_\alpha &= F'_\alpha - \Theta v_{\text{br}}^{n+1} \quad \text{where} \\
F'_\alpha &= \left( \frac{K_1 \eta_s^n}{2\Phi} + \eta_s^{n-1} + u_{\text{br}}^I - \frac{\frac{M}{k^2}w^I - \frac{(g^n)^2}{4}\eta_c^{n-1} + \psi^{n-1/2}g^n}{\frac{M}{k^2} + \frac{(g^n)^2}{4}} \right) / \Psi \\
\text{and } \Theta &= \frac{\frac{(g^n)^2}{4}}{\Psi \left( \frac{M}{k^2} + \frac{(g^n)^2}{4} \right)}
\end{aligned}$$

The complete system can then be solved for the bridge by

$$\begin{bmatrix} u_{\text{br}}^{n+1} \\ w^{n+1} \\ v_{(l_{\text{br}}, m_{\text{br}})}^{n+1} \end{bmatrix} = \mathbf{A}^{-1} \mathbf{v} \tag{42}$$

where

$$\begin{aligned}
\mathbf{A} &= \begin{bmatrix} \frac{\rho_s A}{k^2} & 0 & -\frac{\Theta}{h_s} \\ 0 & \frac{M}{k^2} + \frac{(g^n)^2}{4} & \Theta - \frac{(g^n)^2}{4} \\ 0 & -\frac{(g^n)^2}{4h_p^2} & \frac{\rho_p H}{k^2} + \frac{(g^n)^2}{4h_p^2} \end{bmatrix} \quad \text{and} \\
\mathbf{v} &= \begin{bmatrix} \frac{\rho_s A}{k^2}(2u_{\text{br}}^n - u_{\text{br}}^{n-1}) + T\delta_{xx}u_{\text{br}}^n - EI\delta_{xxxx}u_{\text{br}}^n - F'_\alpha/h_s \\ \frac{M}{k^2}(2w^n - w^{n-1}) - M\omega_0^2 w^n - \frac{(g^n)^2}{4}\eta_c^{n-1} + \psi^{n-1/2}g^n + F'_\alpha \\ \frac{\rho_p H}{k^2}(2v_{\text{br}}^n - v_{\text{br}}^{n-1}) - D\delta_{\Delta\Box}\delta_{\Delta\Box}v_{\text{br}}^n + \left( \frac{(g^n)^2}{4}\eta_c^{n-1} - \psi^{n-1/2}g^n \right) / h_p^2 \end{bmatrix}
\end{aligned}$$



## 7.1 Adding damping

Damping can be added to the string, mass and plate. This results in the following system:

$$\left\{ \begin{array}{l} \rho_s A \delta_{tt} u_l^n \\ M \delta_{tt} w^n \end{array} \right. = \begin{array}{l} T \delta_{xx} u_l^n - EI \delta_{xxx} u_l^n - 2\sigma_{0,s} \delta_t u_l^n + 2\sigma_{1,s} \delta_{t-} \delta_{xx} u_l^n - J_s(l_{br}) F_\alpha \\ -M\omega_0^2 w^n - R \delta_t w^n + (\mu_{t+} \psi^{n-1/2}) g^n + F_\alpha \end{array} \quad (43a)$$

$$\left\{ \begin{array}{l} \rho_p H \delta_{tt} v_{(l,m)}^n \end{array} \right. = \begin{array}{l} -D \delta_{\Delta\Box} \delta_{\Delta\Box} v_{(l,m)}^n - 2\sigma_{0,p} \delta_t v_{(l,m)}^n + 2\sigma_{1,p} \delta_{t-} \delta_{\Delta\Box} v_{(l,m)}^n \\ -J_p(l_{br}, m_{br}) (\mu_{t+} \psi^{n-1/2}) g^n \end{array} \quad (43b)$$

$$\left\{ \begin{array}{l} \delta_{t+} \psi^{n-1/2} \end{array} \right. = g^n \delta_t \eta_c^n \quad (43c)$$

$$\left\{ \begin{array}{l} \eta_c^n \end{array} \right. = v_{(l_{br}, m_{br})}^n - w^n \quad (43d)$$

$$\left\{ \begin{array}{l} F_\alpha \end{array} \right. = K_1 \mu_{tt} \eta_s^n + K_3 (\eta_s^n)^2 \mu_t \eta_s^n + 2\sigma_\times \delta_t \eta_s^n \quad (43e)$$

$$\left\{ \begin{array}{l} \eta_s^n \end{array} \right. = u_{l_{br}}^n - w^n \quad (43f)$$

$$\left\{ \begin{array}{l} \eta_s^n \end{array} \right. = u_{l_{br}}^n - w^n \quad (43g)$$

where  $\sigma_0$  and  $\sigma_1$  are frequency independent and frequency dependent damping coefficients and  $R$  is a damping coefficient for the bridge (mass). If we, like in (34), solve for  $\eta_s^{n+1}$ , this gives

$$\eta_s^{n+1} = \frac{F_\alpha - K_1 \eta_s^n / 2 - \Phi_- \eta_s^{n-1}}{\Phi_+} \quad (44)$$

where

$$\Phi_+ = \frac{K_1}{4} + \frac{K_3 (\eta_s^n)^2}{2} + \frac{\sigma_\times}{k} \quad \text{and} \quad \Phi_- = \frac{K_1}{4} + \frac{K_3 (\eta_s^n)^2}{2} - \frac{\sigma_\times}{k}. \quad (45)$$

As some of the added terms include the state (of a grid point) at the next sample ( $n+1$ ), we add the terms to and slightly rewrite (36) to yield

$$u_{br}^I = \frac{\frac{\rho_s A}{k^2} (2u_{br}^n - u_{br}^{n-1}) + T \delta_{xx} u_{br}^n - EI \delta_{xxx} u_{br}^n + \frac{\sigma_{0,s}}{k} u_{br}^{n-1} + 2\sigma_{1,s} \delta_{t-} \delta_{xx} u_{br}^n}{\frac{\rho_s A}{k^2} + \frac{\sigma_{0,s}}{k}} \quad (46a)$$

$$w^I = \frac{\frac{M}{k^2} (2w^n - w^{n-1}) - M\omega_0^2 w^n + \frac{R}{2k} w^{n-1}}{\frac{M}{k^2} + \frac{R}{2k}} \quad (46b)$$

$$v_{br}^I = \frac{\frac{\rho_p H}{k^2} (2v_{br}^n - v_{br}^{n-1}) - D \delta_{\Delta\Box} \delta_{\Delta\Box} v_{br}^n + \frac{\sigma_{0,p}}{k} v_{br}^{n-1} + 2\sigma_{1,p} \delta_{t-} \delta_{xx} v_{br}^n}{\frac{\rho_p H}{k^2} + \frac{\sigma_{0,p}}{k}} \quad (46c)$$

**$\Leftarrow$  probably don't include the divisions here as that will already happen when doing the matrix division**

and similarly to (37) we can rewrite the individual connected parts of the system at  $n+1$  as

$$u_{br}^{n+1} = u_{br}^I - \frac{F_\alpha}{h_s (\frac{\rho_s A}{k^2} + \frac{\sigma_{0,s}}{k})} \quad (47a)$$

$$w^{n+1} = w^I + \frac{(\mu_{t+} \psi^{n-1/2}) g^n + F_\alpha}{\frac{M}{k^2} + \frac{R}{2k}} \quad (47b)$$

and in a similar fashion as (38), we solve (47b) for  $w^{n+1}$ :

$$w^{n+1} = \frac{(\frac{M}{k^2} + \frac{R}{2k}) w^I - \frac{(g^n)^2}{4} \eta_c^{n-1} + \psi^{n-1/2} g^n + F_\alpha}{\frac{M}{k^2} + \frac{R}{2k} + \frac{(g^n)^2}{4}} \quad (48)$$

Setting (43g) (at  $n+1$ ) and (44) equal to each other and solving for  $F_\alpha$  yields

$$F_\alpha = F'_\alpha - \Theta v_{\text{br}}^{n+1} \quad \text{where} \quad (49)$$

$$F'_\alpha = \left( \frac{K_1 \eta_s^n}{2\Phi_+} + \frac{\Phi_-}{\Phi_+} \eta_s^{n-1} + u_{\text{br}}^{\text{I}} - \frac{\left( \frac{M}{k^2} + \frac{R}{2k} \right) w^{\text{I}} - \frac{(g^n)^2}{4} \eta_c^{n-1} + \psi^{n-1/2} g^n}{\frac{M}{k^2} + \frac{R}{2k} + \frac{(g^n)^2}{4}} \right) / \Psi \quad (50)$$

$$\text{and} \quad \Theta = \frac{\frac{(g^n)^2}{4}}{\Psi \left( \frac{M}{k^2} + \frac{R}{2k} + \frac{(g^n)^2}{4} \right)} = \frac{(g^n)^2 k^2}{\Psi (4M + 2Rk + (g^n)^2 k^2)}, \quad (51)$$

where

$$\Psi = \frac{1}{\Phi_+} + \frac{1}{h_s \left( \frac{\rho_s A}{k^2} + \frac{\sigma_0}{k} \right)} + \frac{1}{\frac{M}{k^2} + \frac{R}{2k} + \frac{(g^n)^2}{4}}. \quad (52)$$

The force excluding the effect of unknown  $v_{\text{br}}^{n+1}$ , and defining the following unchanging (and thus pre-computable) variables

$$\theta_s = h_s(\rho_s A + \sigma_{0,s} k), \quad (53)$$

$$\theta_b = 4M + 2Rk \quad (54)$$

$F'_\alpha$ , can be rewritten to a formula with only one division:

$$F'_\alpha = \frac{(\theta_b + (g^n)^2 k^2)(2kK_1 \eta_s^n + \phi_- \eta_s^{n-1} + \phi_+ u_{\text{br}}^{\text{I}}) - \phi_+ \left( \theta_b w^{\text{I}} - (g^n)^2 k^2 \eta_c^{n-1} + 4k^2 \psi^{n-1/2} g^n \right)}{\phi_+ \Psi (\theta_b + (g^n)^2 k^2)} \quad (55)$$

$$= \frac{\left\{ \begin{aligned} &\phi_+ \theta_s (\theta_b + (g^n)^2 k^2) \left[ (\theta_b + (g^n)^2 k^2)(2kK_1 \eta_s^n + \phi_- \eta_s^{n-1} + \phi_+ u_{\text{br}}^{\text{I}}) \right] \\ &- \phi_+ \left( \theta_b w^{\text{I}} - (g^n)^2 k^2 \eta_c^{n-1} + 4k^2 \psi^{n-1/2} g^n \right) \end{aligned} \right\}}{\phi_+ (\theta_b + (g^n)^2 k^2) \left( \phi_+ k^2 (\theta_b + (g^n)^2 k^2 + 4\theta_s) + 4k\theta_s (\theta_b + (g^n)^2 k^2) \right)} \quad (56)$$

where

$$\phi_+ = k(K_1 + 2K_3(\eta_s)^2) + 4\sigma_\times \quad \text{and} \quad \phi_- = k(K_1 + 2K_3(\eta_s)^2) - 4\sigma_\times \quad (57)$$

and

$$\Theta = \frac{(\phi_+ \theta_s g^2 k^2)}{\phi_+ k^2 (\theta_b + g^2 k^2 + 4\theta_s) + 4k\theta_s (\theta_b + g^2 k^2)} \quad (58)$$

The complete system can then be solved for the bridge by

$$\begin{bmatrix} u_{\text{br}}^{n+1} \\ w_{\text{br}}^{n+1} \\ v_{(l_{\text{br}}, m_{\text{br}})}^{n+1} \end{bmatrix} = \mathbf{A}^{-1} \mathbf{v} \quad (59)$$

where

$$\mathbf{A} = \begin{bmatrix} \frac{\rho_s A}{k^2} + \frac{\sigma_{0,s}}{k} & 0 & -\frac{\Theta}{h_s} \\ 0 & \frac{M}{k^2} + \frac{R}{2k} + \frac{(g^n)^2}{4} & \Theta - \frac{(g^n)^2}{4} \\ 0 & -\frac{(g^n)^2}{4h_p^2} & \frac{\rho_p H}{k^2} + \frac{\sigma_{0,p}}{k} + \frac{(g^n)^2}{4h_p^2} \end{bmatrix} \quad \text{and}$$

$$\mathbf{v} = \begin{bmatrix} \frac{\rho_s A}{k^2} (2u_{\text{br}}^n - u_{\text{br}}^{n-1}) + T\delta_{xx} u_{\text{br}}^n - EI\delta_{xxxx} u_{\text{br}}^n + \frac{\sigma_{0,s}}{k} u_{\text{br}}^{n-1} + 2\sigma_{1,s} \delta_t - \delta_{xx} u_{\text{br}}^n - \frac{F'_\alpha}{h_s} \\ \frac{M}{k^2} (2w_{\text{br}}^n - w_{\text{br}}^{n-1}) - M\omega_0^2 w_{\text{br}}^n + \frac{R}{2k} w_{\text{br}}^{n-1} - \frac{(g^n)^2}{4} \eta^{n-1} + \psi^{n-1/2} g^n + F'_\alpha \\ \frac{\rho_p H}{k^2} (2v_{\text{br}}^n - v_{\text{br}}^{n-1}) - D\delta_{\Delta\Delta} \delta_{\Delta\Delta} v_{\text{br}}^n + \frac{\sigma_{0,p}}{k} v_{\text{br}}^{n-1} + 2\sigma_{1,p} \delta_t - \delta_{\Delta\Delta} v_{\text{br}}^n + \left( \frac{(g^n)^2}{4} \eta^{n-1} - \psi^{n-1/2} g^n \right) / h_p^2 \end{bmatrix}$$

## 7.2 Writing for C++

An essential aspect of real-time sound synthesis is to reduce the number of operations as much as possible.

- Precalculating time-invariant variables
- Group changing variables together

The following equations are identical to the ones found in (46) but with the grid variables ( $u_l^n$ ) factored out (rewritten to have the least amount of operations). Using the following short hand notations

$$\lambda^2 \triangleq \frac{Tk^2}{\rho_s Ah^2}, \quad \mu_s^2 \triangleq \frac{EIk^2}{\rho_s Ah^4}, \quad \mu_p^2 \triangleq \frac{Dk^2}{\rho_s Hh^4} \quad (60)$$

and for the plate grid functions

$$\begin{aligned} v_{br}^n &\triangleq v_{l_{br}, m_{br}}^n \\ v_{br\pm 1}^n &\triangleq (v_{l_{br}+1, m_{br}}^n + v_{l_{br}, m_{br}+1}^n + v_{l_{br}-1, m_{br}}^n + v_{l_{br}, m_{br}-1}^n) \\ v_{br\pm 2}^n &\triangleq (v_{l_{br}+2, m_{br}}^n + v_{l_{br}, m_{br}+2}^n + v_{l_{br}-2, m_{br}}^n + v_{l_{br}, m_{br}-2}^n) \\ v_{l_{br}\pm 1, m_{br}\pm 1}^n &\triangleq (v_{l_{br}+1, m_{br}+1}^n + v_{l_{br}+1, m_{br}-1}^n + v_{l_{br}-1, m_{br}+1}^n + v_{l_{br}-1, m_{br}-1}^n) \end{aligned} \quad (61)$$

and using  $\sigma_{0,s} = \sigma_{0,s}/\rho_s A$ ,  $\sigma_{1,s} = \sigma_{1,s}/\rho_s A$ ,  $\sigma_{0,p} = \sigma_{0,p}/\rho_p H$  and  $\sigma_{2,p} = \sigma_{2,p}/\rho_p H$  we get

$$\begin{aligned} u_{br}^I &= \left[ (2 - 2\lambda^2 - \mu_s^2 - \frac{4\sigma_{1,s}k}{h^2})u_l^n + (\lambda^2 + 4\mu_s^2 + \frac{2\sigma_{1,s}k}{h^2})(u_{br+1}^n + u_{br-1}^n) \right. \\ &\quad \left. + (-\mu_s^2)(u_{br+2}^n + u_{br-2}^n) + (-1 + \sigma_{0,s}k + \frac{4\sigma_{1,s}k}{h^2})u_l^{n-1} + (-\frac{2\sigma_{1,s}k}{h^2})(u_{br+1}^{n-1} + u_{br-1}^{n-1}) \right] \\ &\quad / [1 + \sigma_{0,s}k] \end{aligned} \quad (62a)$$

$$w^I = \frac{(2 - \omega_0^2 k^2)w^n + (-1 + \frac{Rk}{2M})w^{n-1}}{1 + \frac{Rk}{2M}} \quad (62b)$$

$$\begin{aligned} v_{br}^I &= \left[ (2 - 20\mu_p^2 - \frac{8\sigma_{1,p}k}{h^2})v_{br}^n + (8\mu_p^2 + \frac{2\sigma_{1,p}k}{h^2})v_{br\pm 1}^n + (-2\mu_p^2)v_{l_{br}\pm 1, m_{br}\pm 1}^n + (-\mu_p^2)v_{br\pm 2}^n \right. \\ &\quad \left. + (-1 + \frac{8\sigma_{1,p}k}{h^2})v_{br}^{n-1} + (-\frac{2\sigma_{1,p}k}{h^2})v_{br\pm 1}^{n-1} \right] / [1 + \sigma_{0,p}k] \end{aligned} \quad (62c)$$

Again, as done in (37) the individual components at  $n+1$  are **I DO INCLUDE THE PLATE HERE**

$$u_{br}^{n+1} = u_{br}^I - \frac{F_\alpha k^2}{h_s \rho_s A (1 + \sigma_{0,s}k)} \quad (63a)$$

$$w^{n+1} = w^I + \frac{((\mu_t + \psi^{n-1/2})g^n + F_\alpha)k^2}{M(1 + \frac{Rk}{2M})} \quad (63b)$$

$$v_{br}^{n+1} = v_{br}^I - \frac{(\mu_t + \psi^{n-1/2})g^n k^2}{h_p^2 \rho_p H (1 + \sigma_{0,p}k)} \quad (63c)$$

and as in (38) we solve for  $w^{n+1}$

$$w^{n+1} = \frac{M(1 + \frac{Rk}{2M})w^I + k^2 \left( \frac{(g^n)^2}{4} (v_{br}^{n+1} - \eta_c^{n-1}) + \psi^{n-1/2} g^n + F_\alpha \right)}{M(1 + \frac{Rk}{2M}) + \frac{(g^n)^2 k^2}{4}}. \quad (64)$$

We can use this to solve for  $F_\alpha$  which can be shown to be identical to (55).

Then, the complete rewritten system can then be solved for the bridge by

$$\begin{bmatrix} u_{l_{\text{br}}}^{n+1} \\ w^{n+1} \\ v_{(l_{\text{br}}, m_{\text{br}})}^{n+1} \end{bmatrix} = \mathbf{A}^{-1} \mathbf{v} \quad (65)$$

where

$$\mathbf{A} = \begin{bmatrix} 1 + \sigma_{0,s}k & 0 & -\frac{\Theta}{\rho_s A h_s^2 k^2} \\ 0 & M(1 + \frac{Rk}{2M}) + \frac{(g^n)^2 k^2}{4} & \Theta - \frac{(g^n)^2 k^2}{4} \\ 0 & -\frac{(g^n)^2 k^2}{4h_p^2} & \rho_p H(1 + \sigma_{0,p}k) + \frac{(g^n)^2 k^2}{4h_p^2} \end{bmatrix} \quad \text{and}$$

$$\mathbf{v} = \begin{bmatrix} (1 + \sigma_{0,s}k)u_{\text{br}}^{\text{I}} - \frac{F'_\alpha k^2}{h_s \rho_s A} \\ M(1 + \frac{Rk}{2M})w^{\text{I}} + k^2 \left( -\frac{(g^n)^2}{4} \eta^{n-1} + \psi^{n-1/2} g^n + F'_\alpha \right) \\ \rho_p H(1 + \sigma_{0,p}k)v_{\text{br}}^{\text{I}} + \frac{k^2}{h_p^2} \left( \frac{(g^n)^2}{4} \eta^{n-1} - \psi^{n-1/2} g^n \right) \end{bmatrix}$$

### 7.3 Energy Analysis

## 8 Conclusion

Using the tools described in this chapter, you can build any system of elements (strings, masses, barriers) and let them collide.

### 8.1 Implementation

Equation (2) can be implemented using Matlab's `subplus` function.

## References

- [1] S. Bilbao. *Numerical Sound Synthesis*. John Wiley & Sons, 2009.
- [2] Michele Ducceschi. Non-iterative solvers for nonlinear problems: The case of collisions. *DAFx-19*, 2019.

## A Proof that $\psi\psi' = \phi'$

In this appendix, I will prove an equality that Ducceschi presents in [2] which is crucial to his method:

$$\psi\psi' = \phi' \Rightarrow \psi \frac{\dot{\psi}}{\dot{\eta}} = \frac{\dot{\phi}}{\dot{\eta}} \quad \text{where} \quad \psi = \sqrt{2\phi}. \quad (66)$$

In discrete time, (66) becomes

$$(\mu_{t+\psi^{n-1/2}}) \frac{\delta_{t+\psi^{n-1/2}}}{\delta_t \eta^n} = \frac{\delta_{t+\phi^{n-1/2}}}{\delta_t \eta^n}. \quad (67)$$

Multiplying both sides by  $\delta_t \eta^n$  and continuing with the left hand side of (67), we can expand its operators:

$$\begin{aligned}
& \frac{1}{2}(\psi^{n+1/2} + \psi^{n-1/2}) \frac{1}{k}(\psi^{n+1/2} - \psi^{n-1/2}) \\
&= \frac{1}{2k} \left( (\psi^{n+1/2})^2 - (\psi^{n-1/2})^2 \right) \\
&= \frac{1}{2k} \left( \left( \sqrt{2\phi^{n+1/2}} \right)^2 - \left( \sqrt{2\phi^{n-1/2}} \right)^2 \right) \\
&= \frac{1}{k} \left( \phi^{n+1/2} - \phi^{n-1/2} \right) \\
&= \delta_{t+} \phi^{n-1/2}
\end{aligned}$$

which, when divided by  $\delta_t \eta^n$  again satisfies (67). Knowing that  $\sqrt{2\phi} = \psi$

$$\begin{aligned}
\psi \psi' &= \phi' \\
\sqrt{2\phi} \frac{d}{dt} [(2\phi)^{1/2}] &= \phi' \\
\sqrt{2\phi} \left( \sqrt{2} \frac{\phi'}{2\sqrt{\phi}} \right) &= \phi' \\
\sqrt{2\phi} \frac{\phi'}{\sqrt{2\phi}} &= \phi' \\
\phi' &= \phi'
\end{aligned} \tag{68}$$

## B Colliding Mass-springs deriviation

$$\begin{aligned}
\frac{M_1}{k^2} u^{n+1} &= \frac{M_1}{k^2} (2u^n - u^{n-1}) - M_1 \omega_1 u^n + \left( \frac{g^n}{4} (\eta^{n+1} - \eta^{n-1}) + \psi^{n-1/2} \right) g^n \\
\frac{M_1}{k^2} u^{n+1} &= \frac{M_1}{k^2} (2u^n - u^{n-1}) - M_1 \omega_1 u^n + \frac{(g^n)^2}{4} (w^{n+1} - u^{n+1} - \eta^{n-1}) + \psi^{n-1/2} g^n \\
\left( \frac{M_1}{k^2} + \frac{(g^n)^2}{4} \right) u^{n+1} - \frac{(g^n)^2}{4} w^{n+1} &= \frac{M_1}{k^2} (2u^n - u^{n-1}) - M_1 \omega_1 u^n - \frac{(g^n)^2}{4} \eta^{n-1} + \psi^{n-1/2} g^n \tag{69}
\end{aligned}$$

$$\begin{aligned}
\frac{M_2}{k^2} w^{n+1} &= \frac{M_2}{k^2} (2w^n - w^{n-1}) - M_2 \omega_2 w^n - \left( \frac{g^n}{4} (\eta^{n+1} - \eta^{n-1}) + \psi^{n-1/2} \right) g^n \\
\frac{M_2}{k^2} w^{n+1} &= \frac{M_2}{k^2} (2w^n - w^{n-1}) - M_2 \omega_2 w^n - \frac{(g^n)^2}{4} (w^{n+1} - u^{n+1} - \eta^{n-1}) - \psi^{n-1/2} g^n \\
-\frac{(g^n)^2}{4} u^{n+1} + \left( \frac{M_2}{k^2} + \frac{(g^n)^2}{4} \right) w^{n+1} &= \frac{M_2}{k^2} (2w^n - w^{n-1}) - M_2 \omega_2 w^n + \frac{(g^n)^2}{4} \eta^{n-1} - \psi^{n-1/2} g^n \tag{70}
\end{aligned}$$

Weird collision case:

$$\begin{cases}
\rho A \delta_{tt} u_l^n &= T \delta_{xx} u_l^n - E I \delta_{xxx} u_l^n - 2\sigma_0 \delta_t \cdot u_l^n + 2\sigma_1 \delta_t \cdot \delta_{xx} u_l^n & (71a) \\
&+ J_s(l_m)(\mu_{t+} \psi_{ms}^{n-1/2}) g_{ms}^n & (71b) \\
M \delta_{tt} w^n &= -M \omega_0^2 w^n - (\mu_{t+} \psi_{ms}^{n-1/2}) g_{ms}^n + (\mu_{t+} \psi_{mb}^{n-1/2}) g_{mb}^n & (71c) \\
\delta_{t+} \psi_{ms}^{n-1/2} &= g_{ms}^n \delta_t \cdot \eta_{ms}^n & (71d) \\
\delta_{t+} \psi_{mb}^{n-1/2} &= g_{mb}^n \delta_t \cdot \eta_{mb}^n & (71e) \\
\eta_{ms}^n &= w^n - u_{ms}^n & (71f) \\
\eta_{mb}^n &= b - w^n & (71g)
\end{cases}$$