

## Homework assignment 7

**Hand-out time:** Monday, November 11, 2013, at 12:00

**Hand-in deadline:** Friday, November 22, 2013, at 12:00

The problems should be solved by hand, but feel free to use MATLAB to verify your results.

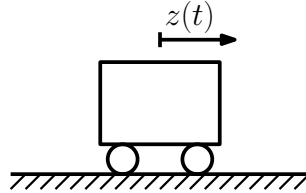
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### Problem 1: Linear quadratic regulation and minimum-energy estimation

Consider a cart for which the equation of motion is given by

$$\ddot{z}(t) - 2\dot{z}(t) = 2u(t) + d(t),$$

where  $z(t)$  is the distance of the cart,  $u(t)$  is an input force and  $d(t)$  is a disturbance force. We are interested in controlling the velocity  $\dot{z}(t)$  of the cart.



- a) Write the equation of motion in the following form

$$\dot{x}(t) = Ax(t) + Bu(t) + \bar{B}d(t), \quad (1)$$

with state  $x(t) = \dot{z}(t)$ .

- b) Is the system (1) controllable? Motivate your answer.

For the moment, we assume that  $d(t) = 0$ . We will design a feedback controller of the form

$$u(t) = -Kx(t). \quad (2)$$

- c) For which values of  $K$  is the closed-loop system (1)-(2) marginally stable? Motivate your answer.
- d) For which values of  $K$  is the closed-loop system (1)-(2) exponentially stable? Motivate your answer.

We select the gain  $K$  such that the control input (2) minimizes the cost function

$$J_{LQR} = \int_0^\infty [Qx^2(t) + Ru^2(t)] dt$$

of the linear quadratic regulation problem, with constants  $Q, R > 0$ . The gain  $K$  is given by

$$K = \frac{BP}{R},$$

where  $P$  is the positive definite solution of the Riccati equation

$$-\frac{B^2}{R}P^2 + 2AP + Q = 0.$$

- e) Compute  $K$  as a function of  $Q$  and  $R$ .
- f) From your answers of d) and e), determine for which values of  $Q > 0$  and  $R > 0$  the closed-loop system (1)-(2) is exponentially stable. Motivate your answer.
- g) Let  $Q = 6$ . Determine the value for  $R > 0$  such that  $K = 3$ .

We assume that the state  $x(t)$  is unknown and can only be measured. The difference between the measured state  $y(t)$  and the actual state  $x(t)$  is given by  $n(t)$ , i.e.

$$n(t) = y(t) - x(t). \quad (3)$$

Note that  $n(t)$  can be considered as measurement noise. Instead of the actual state  $x(t)$ , the controller in (2) uses the measured state  $y(t)$ , which leads to

$$u(t) = -Ky(t). \quad (4)$$

- h) Write the equation (3) as

$$y(t) = Cx(t) + n(t), \quad (5)$$

and determine the constant  $C$ .

The system (1), (4) and (5) is depicted in Fig. 1.

- i) Determine the transfer function from the disturbance  $d(t)$  to the state  $x(t)$  of the system (1), (4) and (5) as a function of  $K$ , i.e. determine  $\frac{x(s)}{d(s)}$  as a function of  $K$ .
- j) Determine the transfer function from the disturbance  $n(t)$  to the state  $x(t)$  of the system (1), (4) and (5) as a function of  $K$ , i.e. determine  $\frac{x(s)}{n(s)}$  as a function of  $K$ .

We assume that  $d(t)$  is a low-frequency signal, and that  $n(t)$  is a high-frequency signal.

- k) Calculate  $\lim_{s \rightarrow 0} \frac{x(s)}{d(s)}$  as a function of  $K$ .
- l) How should the value of  $K$  be chosen such that the effect of the disturbance  $d(t)$  on the state  $x(t)$  is small? Motivate your answer.
- m) Calculate  $\lim_{s \rightarrow \infty} \frac{x(s)}{n(s)}$  as a function of  $K$ .
- n) How should the value of  $K$  be chosen such that the effect of the disturbance  $n(t)$  on the state  $x(t)$  is small? Motivate your answer.

In the remaining part of the exercise, we set  $K = 3$ . To balance the effect of the disturbances  $d(t)$  and  $n(t)$ , we will design a state estimator of the following form:

$$\dot{\hat{x}}(t) = A\hat{x}(t) + Bu(t) + L(y(t) - C\hat{x}(t)), \quad (6)$$

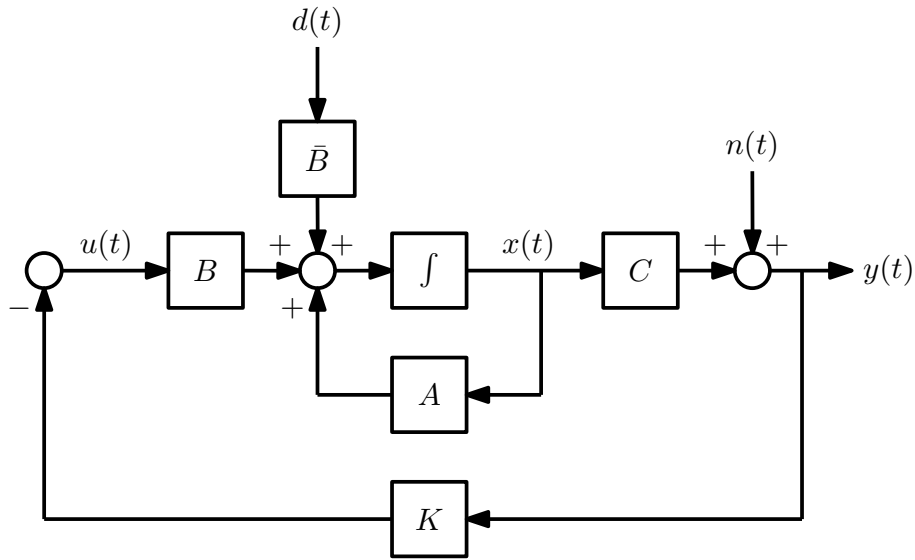


Fig. 1: System (1), (4) and (5).

with estimator gain  $L$ . We will use the estimated state  $\hat{x}(t)$  as an input for the feedback controller in (2), which leads to

$$u(t) = -K\hat{x}(t). \quad (7)$$

- o) Similar to Fig. 1, draw a block diagram of the system with controller and state estimator, which is given by the equations (1), (5), (6) and (7).
- p) We define the estimation error  $e(t) = x(t) - \hat{x}(t)$ . Show that the system (1), (5), (6) and (7) can be written in the form

$$\begin{bmatrix} \dot{x}(t) \\ \dot{e}(t) \end{bmatrix} = \begin{bmatrix} A - BK & BK \\ 0 & A - LC \end{bmatrix} \begin{bmatrix} x(t) \\ e(t) \end{bmatrix} + \begin{bmatrix} \bar{B} & 0 \\ \bar{B} & -L \end{bmatrix} \begin{bmatrix} d(t) \\ n(t) \end{bmatrix}$$

$$y(t) = [C \ 0] \begin{bmatrix} x(t) \\ e(t) \end{bmatrix} + [0 \ 1] \begin{bmatrix} d(t) \\ n(t) \end{bmatrix}.$$

- q) For which values of  $L$  is the system (1), (5), (6) and (7) BIBO stable (bounded-input bounded-output stable)? Motivate your answer.

We select the gain  $L$  such that the state estimator (6) minimizes the cost function

$$J_{MEE} = \int_{-\infty}^t [S(y(t) - C\hat{x}(t))^2 + T\dot{d}^2(t)] dt$$

of the minimum-energy estimation problem, with constants  $S, T > 0$ . The gain  $L$  is given by

$$L = WCS,$$

where  $W$  is the positive definite solution of the Riccati equation

$$-C^2SW^2 + 2AW + \frac{\bar{B}^2}{T} = 0.$$

- r) Compute  $L$  as a function of  $S$  and  $T$ .
- s) From your answers of q) and r), determine for which values of  $S > 0$  and  $T > 0$  the system (1), (5), (6) and (7) is BIBO stable. Motivate your answer.
- t) Determine the transfer function from the disturbance  $d(t)$  to the state  $x(t)$  of the system (1), (5), (6) and (7) as a function of  $L$ .
- u) Determine the transfer function from the disturbance  $n(t)$  to the state  $x(t)$  of the system (1), (5), (6) and (7) as a function of  $L$ .

Again, we assume that  $d(t)$  is a low-frequency signal, and that  $n(t)$  is a high-frequency signal.

- v) How should the value of  $L$  be chosen such that the effect of the disturbance  $d(t)$  on the state  $x(t)$  is small? Motivate your answer.
- w) How should the value of  $L$  be chosen such that the effect of the disturbance  $n(t)$  on the state  $x(t)$  is small? Motivate your answer.

We compare the system with output feedback in (1), (4) and (5) with the system with state-estimated feedback in (1), (5), (6) and (7).

- x) Using  $K = 3$  and  $L = 12$ , is the effect of the low-frequency disturbance  $d(t)$  on the state  $x(t)$  smaller or larger with output feedback than with state-estimated feedback? Motivate your answer.
- y) Using  $K = 3$  and  $L = 12$ , is the effect of the high-frequency disturbance  $n(t)$  on the state  $x(t)$  smaller or larger with output feedback than with state-estimated feedback? Motivate your answer.