

# Nondimensional Longitudinal Stability Derivatives

Table 5.1

Summary—Longitudinal Derivatives

	$C_x$	$C_z$	$C_m$
$\hat{u}^\dagger$	$M_0 \left( \frac{\partial C_T}{\partial M} - \frac{\partial C_D}{\partial M} \right) - \rho u_0^2 \frac{\partial C_D}{\partial p_d} + C_{T_u} \left( 1 - \frac{\partial C_D}{\partial C_T} \right)$	$-M_0 \frac{\partial C_L}{\partial M} - \rho u_0^2 \frac{\partial C_L}{\partial p_d} - C_{T_u} \frac{\partial C_L}{\partial C_T}$	$M_0 \frac{\partial C_m}{\partial M} + \rho u_0^2 \frac{\partial C_m}{\partial p_d} + C_{T_u} \frac{\partial C_m}{\partial C_T}$
$\alpha$	$C_{l_0} - C_{D_\alpha}$	$-(C_{L_\alpha} + C_{D_0})$	$-a(h_n - h)$
$\dot{\alpha}$	Neg.	$* -2a_l V_H \frac{\partial \epsilon}{\partial \alpha}$	$* -2a_l V_H \frac{l_t}{c} \frac{\partial \epsilon}{\partial \alpha}$
$\dot{q}$	Neg.	$* -2a_l V_H$	$* -2a_l V_H \frac{l_t}{c}$

Neg. means usually negligible.

\*means contribution of the tail only, formula for wing-body not available.

$$\dagger C_{T_u} = \frac{(\partial T / \partial u)_0}{\frac{1}{2} \rho u_0 S} - 2C_{T_0}; C_{T_0} = C_{D_0} + C_{w_0} \sin \theta_0$$

## α derivatives

$$C_{m_\alpha} = C_{L_\alpha} (h - h_N)$$

$$C_{z_\alpha}$$

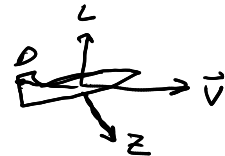
$$Z = -L \cos \alpha - D \sin \alpha$$

$$C_Z = -(C_L \cos \alpha + C_D \sin \alpha)$$

$$= -(C_L + C_D \alpha)$$

$$C_{Z_\alpha} \equiv \left. \frac{\partial C_Z}{\partial \alpha} \right|_0 = -(C_{L_\alpha} + C_{D_0} + \alpha \frac{\partial C_D}{\partial \alpha})$$

$$C_{Z_\alpha} = -(C_{L_\alpha} + C_{D_0})$$



## u derivatives

3 important factors:

- Compressibility: Mach Number
- Dynamic Pressure:  $p_d = \frac{1}{2} \rho V^2$
- Thrust

$$M \equiv \frac{V}{a} \leftarrow \text{speed of sound}$$

- Different from the dynamic pressure in nondimensionalization  
Changes in  $C_L, C_D$ , etc. due to changes in dynamic pressure

$$C_{x_u} \equiv \left. \frac{\partial C_x}{\partial \hat{u}} \right|_0$$

$* \in \{x, z, m\}$

$$C_{*u} = \left. \frac{\partial C_*}{\partial M} \right|_0 \frac{\partial M}{\partial \hat{u}} \Big|_0 + \left. \frac{\partial C_*}{\partial p_d} \right|_0 \frac{\partial p_d}{\partial \hat{u}} \Big|_0 + \left. \frac{\partial C_*}{\partial C_T} \right|_0 \frac{\partial C_T}{\partial \hat{u}} \Big|_0$$

$$\rightarrow \left. \frac{\partial M}{\partial \hat{u}} \right|_0 = u_0 \left. \frac{\partial M}{\partial u} \right|_0 = \frac{u_0}{a} \left. \frac{\partial V}{\partial u} \right|_0 = M_0$$

$$\left. \frac{\partial p_d}{\partial u} \right|_0 = u_0 \left. \frac{\partial p_d}{\partial u} \right|_0 = u_0 \frac{1}{2} \rho \frac{\partial V^2}{\partial u} \Big|_0 = u_0 \rho u_0 = \rho u_0^2$$

$$C_T = \frac{T}{\frac{1}{2} \rho V^2 S}$$

$$\left. \frac{\partial C_T}{\partial u} \right|_0 = u_0 \left. \frac{\partial C_T}{\partial u} \right|_0 = u_0 \left( \frac{\partial T / \partial u}{\frac{1}{2} \rho V^2 S} - \frac{2T}{\frac{1}{2} \rho V^3 S} \right) \Big|_0 = \left. \frac{\partial T / \partial u}{\frac{1}{2} \rho u_0 S} \right|_0 - 2 C_{T_0}$$

$$\frac{\partial}{\partial x} \left( \frac{f(x)}{g(x)} \right) = \frac{g'(x)f(x) - f(x)g'(x)}{g(x)^2}$$

$$C_{T_0} = C_{D_0} + C_{W_0} \sin \theta$$

3 cases

Gliding case:  $C_{T_u} = 0$

Constant Thrust (Jet):  $C_{T_u} = -2 C_{T_0}$

Constant Power (Prop):  $C_{T_u} = -3 C_{T_0}$

$TV = \text{constant}$

$$\left. \frac{\partial T}{\partial u} \right|_0 = - \frac{T_0}{u_0}$$

$C_{x_u}$

$$C_x \approx C_T - C_D$$

$$\left. \frac{\partial C_x}{\partial M} \right|_0 = \left. \frac{\partial C_T}{\partial M} \right|_0 - \left. \frac{\partial C_D}{\partial M} \right|_0$$

$$\left. \frac{\partial C_x}{\partial p_d} \right|_0 = \left. \frac{\partial C_T}{\partial p_d} \right|_0 - \left. \frac{\partial C_D}{\partial p_d} \right|_0$$

$$\left. \frac{\partial C_x}{\partial C_T} \right|_0 = 1 - \left. \frac{\partial C_D}{\partial C_T} \right|_0$$

$$C_{x_u} = M_0 \left( \left. \frac{\partial C_T}{\partial M} \right|_0 - \left. \frac{\partial C_D}{\partial M} \right|_0 \right) - \rho u_0^2 \left. \frac{\partial C_D}{\partial p_d} \right|_0 + C_{T_u} \left( 1 - \left. \frac{\partial C_D}{\partial C_T} \right|_0 \right)$$

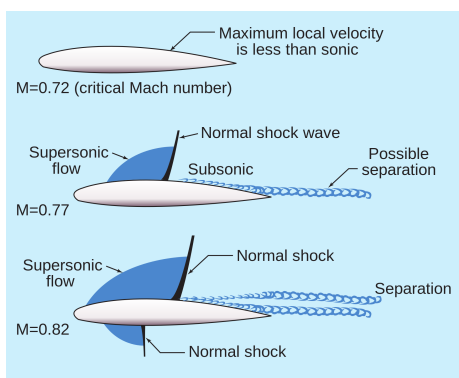
$C_{z_u}$

Assume  $C_z = -C_L$

$$C_{z_u} = -M_0 \underbrace{\left. \frac{\partial C_L}{\partial M} \right|_0}_{\text{small except transonic}} - \rho u_0^2 \left. \frac{\partial C_L}{\partial p_d} \right|_0 - C_{T_u} \left. \frac{\partial C_L}{\partial C_T} \right|_0$$

$C_{m_u}$

$$C_{m_u} = \underbrace{M_0 \left. \frac{\partial C_m}{\partial M} \right|_0}_{\text{Mach Tuck}} + \rho u_0^2 \left. \frac{\partial C_m}{\partial p_d} \right|_0 + C_{T_u} \left. \frac{\partial C_m}{\partial C_T} \right|_0$$



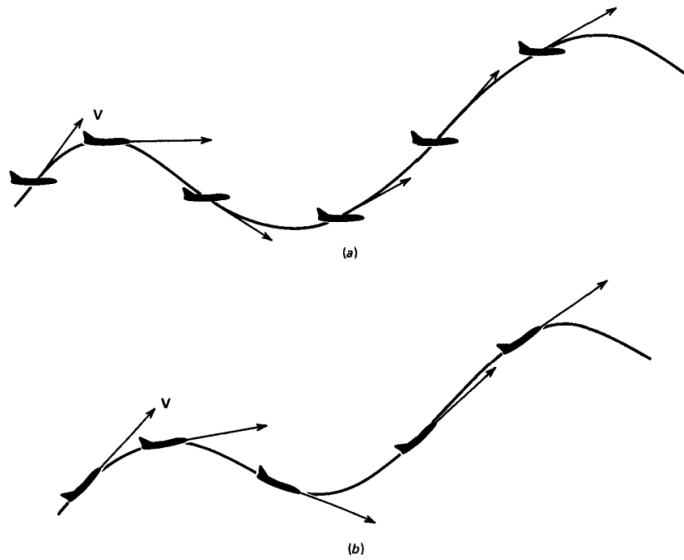
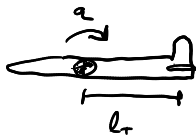


Figure 5.2 (a) Motion with zero  $q$ , but varying  $\alpha_r$ . (b) Motion with zero  $\alpha_r$  but varying  $q$ .

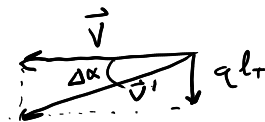
q-derivatives

Wing-body || Tail

Tail



velocity observed by tail



$$\Delta C_{L_r} = a_+ \Delta \alpha = a_+ \tan^{-1} \frac{q l_r}{u_0} \approx a_+ \frac{q l_r}{u_0}$$

$(C_{z_q})_{tail}$

$$C_{z_q} = \frac{\partial C_z}{\partial \hat{q}} \Big|_0 = \frac{z_{u_0}}{\bar{c}} \frac{\partial C_z}{\partial q} \Big|_0 = - \frac{z_{u_0}}{\bar{c}} \frac{\partial C_{L_r}}{\partial q} \Big|_0$$

$$(C_{z_q})_{tail} = - \frac{z_{u_0}}{\bar{c}} a_+ \frac{S_+ l_r}{S u_0} = \boxed{- 2 a_+ V_H}$$

$$\Delta C_L = \frac{S_+}{S} \Delta C_{L_r} = \frac{S_+}{S} a_+ \frac{q l_r}{u_0}$$

$$V_H = \frac{S_+ l_r}{S \bar{c}}$$

$(C_{m_q})_{tail}$

$$C_{m_q} = \frac{\partial C_m}{\partial \hat{q}} \Big|_0 = \frac{z_{u_0}}{\bar{c}} \frac{\partial C_m}{\partial q} \Big|_0$$

$$\boxed{(C_{m_q})_{tail} = - 2 a_+ V_H \frac{l_r}{\bar{c}}}$$

$$\Delta C_m = - V_H \Delta C_{L_r} = a_+ V_H \frac{q l_r}{u_0}$$

Wing-Body

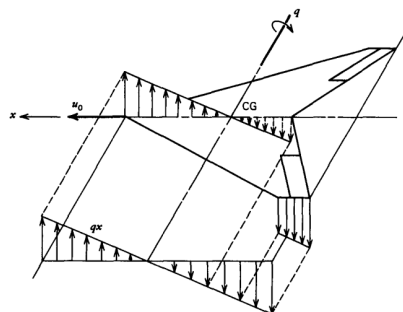


Figure 5.4 Wing velocity distribution due to pitching.

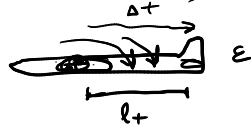
## $\dot{\alpha}$ derivatives

Unsteady effects

**Wing-Body**  $\rightarrow$  Determined by initial response  
or oscillation of wing in wind tunnel  
or flight test

**Tail**

Downwash Lag



$$\Delta \varepsilon = -\frac{\partial \varepsilon}{\partial \alpha} \dot{\alpha} \Delta t = -\frac{\partial \varepsilon}{\partial \alpha} \dot{\alpha} \frac{l_t}{u_0} \\ = -\Delta \alpha_t$$

$(C_{z_{\dot{\alpha}}})_{tail}$

$$\Delta C_{L_t} = a_t \Delta \alpha_t = a_t \dot{\alpha} \frac{l_t}{u_0} \frac{\partial \varepsilon}{\partial \alpha}$$

$$\rightarrow \Delta C_L = a_t \dot{\alpha} \frac{l_t S_t}{u_0 S} \frac{\partial \varepsilon}{\partial \alpha}$$

$$C_{z_{\dot{\alpha}}} = \left. \frac{\partial C_z}{\partial \frac{\dot{\alpha} \varepsilon}{2 u_0}} \right|_0 = \frac{2 u_0}{\bar{c}} \frac{\partial C_z}{\partial \dot{\alpha}} = -2 a_t \frac{l_t S_t}{\bar{c} S} \frac{\partial \varepsilon}{\partial \alpha}$$

$$(C_{z_{\dot{\alpha}}})_{tail} = -2 a_t V_H \frac{\partial \varepsilon}{\partial \alpha}$$

$$(C_{m_{\dot{\alpha}}})_{tail} = -2 a_t V_H \frac{l_t}{\bar{c}} \frac{\partial \varepsilon}{\partial \alpha}$$