

# Lateral / Directional Dynamics

More Accurate  
Fewer Assumption

## Big Picture

$$\begin{aligned}\dot{\vec{p}} &= \mathbf{R}_B^E \vec{V}_B^E \\ \dot{\vec{\theta}} &= \dots \\ \vec{V}_B^E &= \\ \dot{\vec{\omega}}_B &= \end{aligned}$$

Nonlinear Rigid Body EOM

Trim  
Linearization

Stability Derivatives  
Control Derivatives

$A_{lon}, B_{lon}$

$A_{lat}, B_{lat}$

S.P. mode

Phugoid mode

$$C_{L_{trim}} = C_{L_{\alpha}} \alpha_{trim} + C_{L_{\delta_e}} \delta_{e_{trim}}$$

$$C_{m_{trim}} = C_{m_0} + C_{m_{\alpha}} \alpha_{trim} + C_{m_{\delta_e}} \delta_{e_{trim}}$$

More Assumptions  
Easier to Analyze

$$\rightarrow \Delta \dot{\phi} = \Delta p + \Delta r \tan \theta_0$$

$$\rightarrow \Delta \dot{\theta} = \Delta q$$

$$\rightarrow \Delta \dot{u} = -g \cos \theta_0 \Delta \theta + \frac{\Delta X}{m}$$

$$\rightarrow \Delta \dot{v} = -u_0 \Delta r + g \cos \theta_0 \Delta \phi + \frac{\Delta Y}{m}$$

$$\rightarrow \Delta \dot{w} = u_0 \Delta q - g \sin \theta_0 \Delta \theta + \frac{\Delta Z}{m}$$

$$\rightarrow \Delta \dot{p} = \Gamma_3 \Delta L + \Gamma_4 \Delta N$$

$$\rightarrow \Delta \dot{q} = \frac{\Delta M}{I_y}$$

$$\rightarrow \Delta \dot{r} = \Gamma_4 \Delta L + \Gamma_8 \Delta N$$

$$Y = \frac{1}{2} \rho V^2 S C_Y(\beta, p, r, \delta_a, \delta_r)$$

$$L = \frac{1}{2} \rho V^2 S b C_\ell(\beta, p, r, \delta_a, \delta_r)$$

$$N = \frac{1}{2} \rho V^2 S b C_n(\beta, p, r, \delta_a, \delta_r)$$

$$\hat{p} = \frac{\rho b}{2u_0}$$

$$Y \approx \frac{1}{2} \rho V_a^2 S \left[ C_{Y_0} + C_{Y_\beta} \beta + C_{Y_p} \frac{b}{2V_a} p + C_{Y_r} \frac{b}{2V_a} r + C_{Y_{\delta_a}} \delta_a + C_{Y_{\delta_r}} \delta_r \right]$$

$$L \approx \frac{1}{2} \rho V_a^2 S b \left[ C_{l_0} + C_{l_\beta} \beta + C_{l_p} \frac{b}{2V_a} p + C_{l_r} \frac{b}{2V_a} r + C_{l_{\delta_a}} \delta_a + C_{l_{\delta_r}} \delta_r \right]$$

$$N \approx \frac{1}{2} \rho V_a^2 S b \left[ C_{n_0} + C_{n_\beta} \beta + C_{n_p} \frac{b}{2V_a} p + C_{n_r} \frac{b}{2V_a} r + C_{n_{\delta_a}} \delta_a + C_{n_{\delta_r}} \delta_r \right]$$

For symmetric aircraft,  $C_{Y_0} = C_{l_0} = C_{n_0} = 0$

$$\dot{\mathbf{x}}_{lat} = \mathbf{A}_{lat} \mathbf{x}_{lat} + \mathbf{c}_{lat}$$

$$\mathbf{x}_{lat} = \begin{pmatrix} \Delta v \\ \Delta p \\ \Delta r \\ \Delta \phi \end{pmatrix} \quad \mathbf{c}_{lat} = \begin{pmatrix} \frac{\Delta Y_c}{m} \\ \Gamma_3 \Delta L_c + \Gamma_4 \Delta N_c \\ \Gamma_4 \Delta L_c + \Gamma_8 \Delta N_c \\ 0 \end{pmatrix}$$

$$\mathbf{A}_{lat} = \begin{pmatrix} \frac{Y_v}{m} & \frac{Y_p}{m} & \left( \frac{Y_r}{m} - u_0 \right) & g \cos \theta_0 \\ \Gamma_3 L_v + \Gamma_4 N_v & \Gamma_3 L_p + \Gamma_4 N_p & \Gamma_3 L_r + \Gamma_4 N_r & 0 \\ \Gamma_4 L_v + \Gamma_8 N_v & \Gamma_4 L_p + \Gamma_8 N_p & \Gamma_4 L_r + \Gamma_8 N_r & 0 \\ 0 & 1 & \tan \theta_0 & 0 \end{pmatrix}$$

$$\Gamma_1 = \frac{I_{xz} (I_x - I_y + I_z)}{\Gamma}$$

$$\Gamma_2 = \frac{I_z (I_z - I_y) + I_{xz}^2}{\Gamma}$$

$$\Gamma_3 = \frac{I_z}{\Gamma}$$

$$\Gamma_4 = \frac{I_{xz}}{\Gamma}$$

$$\Gamma_5 = \frac{I_z - I_x}{I_y}$$

$$\Gamma_6 = \frac{I_{xz}}{I_y}$$

$$\Gamma_7 = \frac{I_x (I_x - I_y) + I_{xz}^2}{\Gamma}$$

$$\Gamma_8 = \frac{I_x}{\Gamma}$$

$$\Gamma = I_x I_z - I_{xz}^2$$

Sideslip:  $\beta$

$+\beta \Rightarrow$  wind coming from right



$$\beta = \sin^{-1} \frac{\Delta v}{V}$$

$$\beta \approx \frac{\Delta v}{u_0} = \hat{v}$$

$$L = \frac{1}{2} \rho V^2 S b C_l$$

$$L_v \equiv \left. \frac{\partial L}{\partial v} \right|_0 = \frac{1}{2} \rho u_0^2 S b \left. \frac{\partial C_l}{\partial v} \right|_0$$

$$= \frac{1}{2} \rho u_0^2 b S \left. \frac{\partial C_l}{\partial \beta} \right|_0 \left. \frac{\partial \beta}{\partial v} \right|_0$$

$$\boxed{L_v = \frac{1}{2} \rho u_0 b S C_{l_\beta}}$$

$$C_{l_\beta} \equiv \frac{\partial C_l}{\partial \beta}$$

$$\beta = \hat{v} = \frac{\Delta v}{u_0}$$

$$\frac{\partial \beta}{\partial v} = \frac{1}{u_0}$$

$$L_p \equiv \left. \frac{\partial L}{\partial p} \right|_0 = \frac{1}{2} \rho u_0^2 b S \left. \frac{\partial C_l}{\partial p} \right|_0$$

$$= \frac{1}{2} \rho u_0^2 b S \left. \frac{\partial C_l}{\partial \hat{p}} \right|_0 \left. \frac{\partial \hat{p}}{\partial p} \right|_0$$

$$\boxed{L_p = \frac{1}{4} \rho u_0 b^2 S C_{l_p}}$$

$$C_{l_p} \equiv \frac{\partial C_l}{\partial \hat{p}}$$

$$\hat{p} = \frac{b p}{2 u_0}$$

Table 4.5

Lateral Dimensional Derivatives

	Y	L	N
$v$	$\frac{1}{2} \rho u_0 S C_{y_\beta}$	$\frac{1}{2} \rho u_0 b S C_{l_\beta}$	$\frac{1}{2} \rho u_0 b S C_{n_\beta}$
$p$	$\frac{1}{4} \rho u_0 b S C_{y_p}$	$\frac{1}{4} \rho u_0 b^2 S C_{l_p}$	$\frac{1}{4} \rho u_0 b^2 S C_{n_p}$
$r$	$\frac{1}{4} \rho u_0 b S C_{y_r}$	$\frac{1}{4} \rho u_0 b^2 S C_{l_r}$	$\frac{1}{4} \rho u_0 b^2 S C_{n_r}$

Table 5.2

Summary—Lateral Derivatives

	$C_y$	$C_l$	$C_n$
$\beta$	$* -a_F \frac{S_F}{S} \left( 1 - \frac{\partial \sigma}{\partial \beta} \right)$	N.A.	$* a_F V_v \left( 1 - \frac{\partial \sigma}{\partial \beta} \right)$
$\hat{p}$	$* -a_F \frac{S_F}{S} \left( 2 \frac{z_F}{b} - \frac{\partial \sigma}{\partial \hat{p}} \right)$	N.A.	$* a_F V_v \left( 2 \frac{z_F}{b} - \frac{\partial \sigma}{\partial \hat{p}} \right)$
$\hat{r}$	$* a_F \frac{S_F}{S} \left( 2 \frac{l_F}{b} + \frac{\partial \sigma}{\partial \hat{r}} \right)$	$* a_F \frac{S_F}{S} \frac{z_F}{b} \left( 2 \frac{l_F}{b} + \frac{\partial \sigma}{\partial \hat{r}} \right)$	$* -a_F V_v \left( 2 \frac{l_F}{b} + \frac{\partial \sigma}{\partial \hat{r}} \right)$

\*means contribution of the tail only, formula for wing-body not available;  $V_F/V = 1$ .

N.A. means no formula available.

# $C_{l\beta}$ : Dihedral Effect

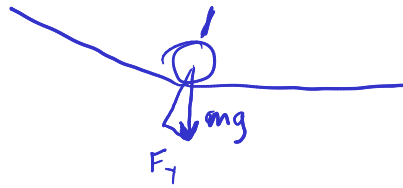
sign: negative

(looking from back)

①



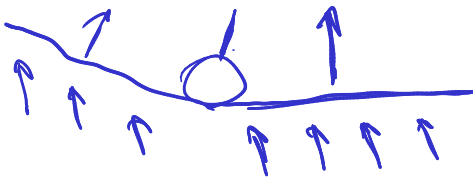
②



③



④



⑤



⑥

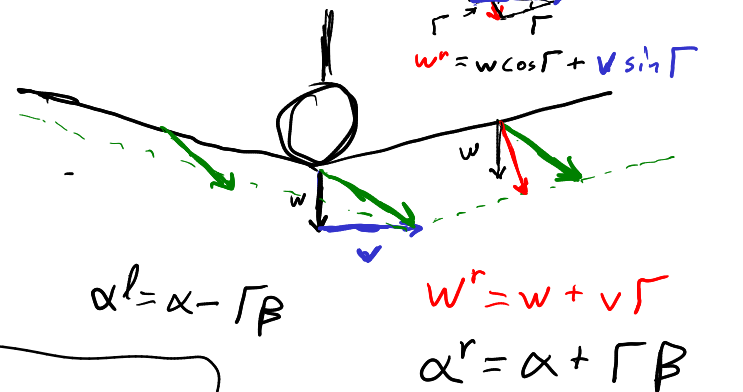
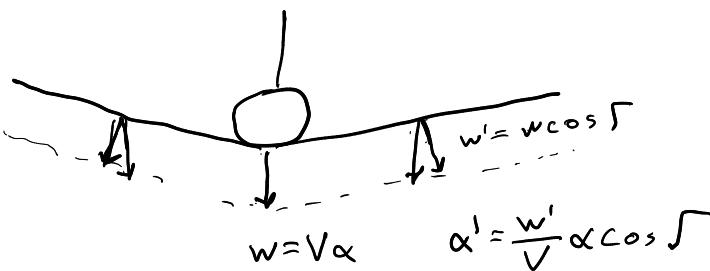


4 significant factors

1. Dihedral Angle
2. Wing Height
3. Wing Sweep
4. Vertical Tail

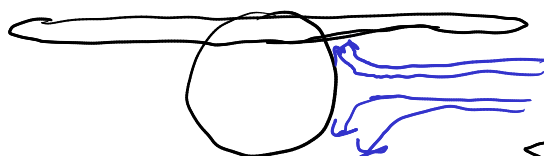
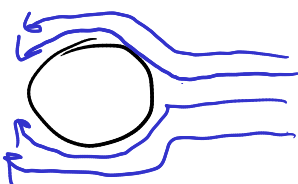


1. Dihedral Angle



$$C_{l\beta}^r \propto \Gamma$$

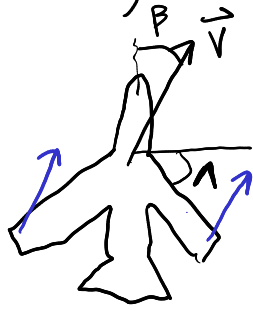
2. Wing Height



high wing  $\Rightarrow -C_{l\beta}$   
low wing  $\Rightarrow +C_{l\beta}$

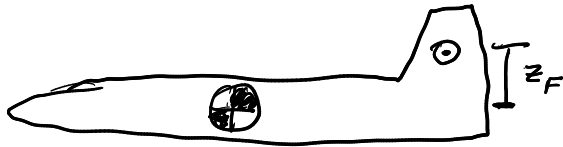


### 3. Wing Sweep



$$C_{l\beta}^1 \propto 2C_L V^2 \sin 2\Lambda$$

### 4. Tail



$$\Delta C_L^F = C_{LF} \frac{S_F z_F}{S_b} = a_F (-\beta + \sigma) \frac{S_F z_F}{S_b}$$

$$C_{l\beta}^F = -a_F \left(1 - \frac{\partial \sigma}{\partial \beta}\right) \frac{S_F z_F}{S_b} \left(\frac{V_F}{V}\right)^2$$

