

Internship Program Report

By

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In association with



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Introduction

Internship program arranged by GUDLAVALLERU ENGINEERING COLLEGE in association with Smart Internz, Hyderabad for the benefit of 3rd year EEE batch 2018-2022 on Electrical Detailed design Engineering for Oil& Gas, Power and Utility industrial sectors.

Program organiser

Smart Bridge, Hyderabad.

Pioneer in organising Internships, knowledge workshops, debates, hackathons, Technical sessions and Industrial Automation projects.



Courtesy

Dr. Sri B. Dasu – HOD – EEE, GEC

Dr.G.Srinivasa Rao-Coordinator

Mr. Ramesh V - Mentor

Mr. Vinay Kumar - System Support

Mr. Harikanth – Softwar/Technical Support

Program details

Smart Internz program schedule: 4 weeks starting from 3rd May 2021

Daily schedule time shall be 4PM to 6.30PM

Mode of Classes: Online through ZOOM

Presenter: Mr Ramesh V

Internship program

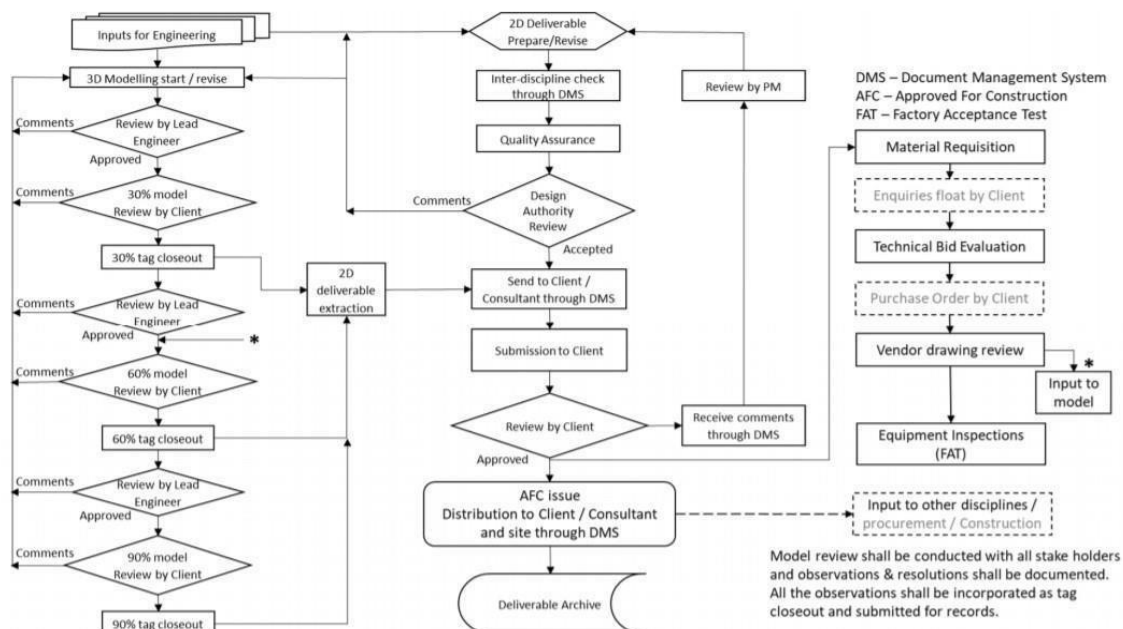
We have been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

3rd May2021: Introduction to EPC Industry

1	EPC Industry & Electrical Detailed Engineering	EPC Industry Engineering Procurement Construction	Introduction Types of Engineering Engineering role in procurement Engineering role during construction
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Topic details:

1C. ELECTRICAL DESIGN & DETAILED ENGINEERING - PROCESS

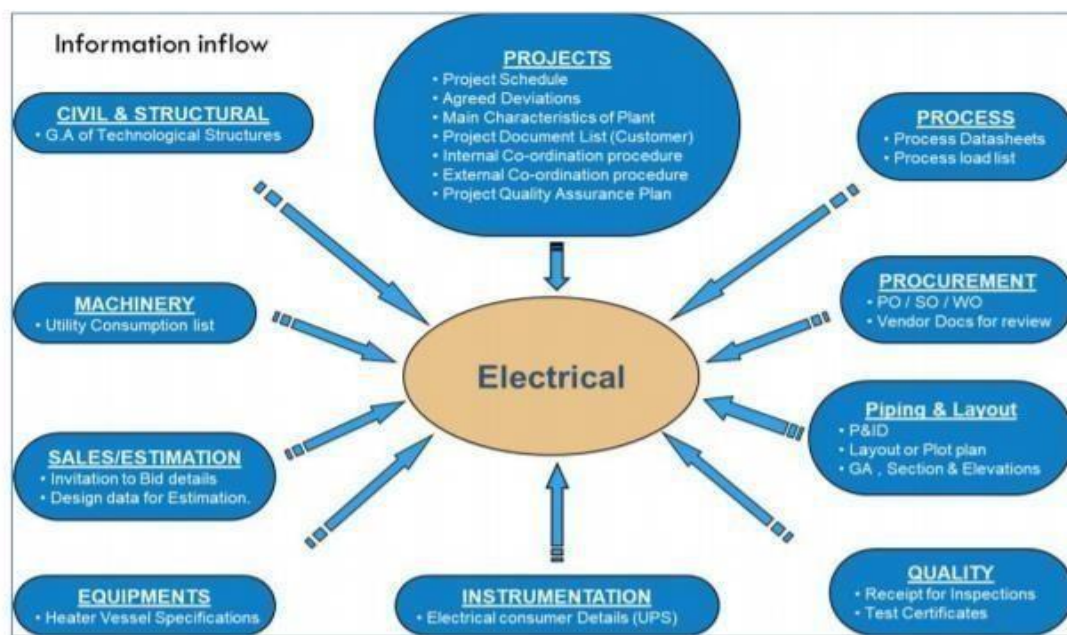


Engineering phases, Engineering deliverables (drawings & documents) list, Design Engineer role at various phases of project.

4th May2021: Engineering documentation for EPC projects

2	Electrical Design Documentation	Engineering Deliverables list Detailed Engineering work flow Document transmission Deliverables types	Sequence of deliverables Detailed engineering process Document submission and info exchange Different types of deliverables
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Topic details:



On this day I have learned the Deliverable list of details and work flow in electrical design. And after sequence of deliverables, Detailed engineering process, Document submission and exchange process, and at last I learned about different types of deliverables.

5th May2021: Engineering documentation for commands and formulae

3	Electrical Design Documentation	Ms word commands Ms excel formulae Auto cad basic commands
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Topic details:

MS Word,Excel and Auto cad COMMANDS.

3C. AUTOCAD BASIC COMMANDS

AUTOCAD BASIC KEYS							
STANDARD		DRAW		MODIFY		FORMAT	
NEW	Ctrl+N	LINE	L	ERASE	E	PROPERTIES	MO
OPEN	Ctrl+O	RAY	RAY	COPY	CO	SELECT COLOR	COL
SAVE	Ctrl+S	PLINE	PL	MIRROR	MI	LAYER	LA
PLOT	Ctrl+P	3DPOLY	3P	OFFSET	O	LINETYPE	LT
PLOT PREVIEW	PRE	POLIGONE	POL	ARRAY	AR	LINEWEIGHTS	LW
CUT	Ctrl+X	RECTANGLE	REC	MOVE	M	LT SCALE	LTS
COPY	Ctrl+C	ARC	A	ROTATE	RO	LIST	LI
PASTE	Ctrl+V	CIRCLE	C	SCALE	SC	DIMEN. STYLE	D
MATCH PROPE.	MA	SPLINE	SPL	STRECH	S	RENAME	REN
CLOSE	Ctrl+F4	ELLIPSE	EL	TRIM	TR	OPTION	OP
EXIT	Ctrl+Q	BLOCK	B	EXTENDED	EX		
		POINT	PO	BRAKE	BR		
		HATCH	H	CHAMFER	CHA		
		GRADIENT	GD	FILLET	F		
		REGION	REG	EXPLODE	X		
		BOUNDARY	BO				
		DONUT	DO				

EXTRA				DRAFTING		PAPER SIZE
UNIT	UN	UCS	UCS	ORTHO	F8, Ctrl+L	A4=210*297
LIMITS	LIMITS	SINGLE TEXT	DT	OSNAP	F3, Ctrl+F	A3=297*420
(0,0; 1000,1000)		MULTILINE TEXT	MT	POLAR	F10, Ctrl+U	A2=420*594
ZOOM	Z	EDIT TEXT	ED	GRID	F7, Ctrl+G	A1=594*841
ALL	A	OBJECT SNAP	OB	OTRACK	F11	A0=841*1189
PAN	P	DIMENTION	DIM	SNAP	F9	
CLEAN SCREEN	Ctrl+0	HORIZONTAL	HOR			
COMMAND WIN	Ctrl+9	VERTICAL	VER			

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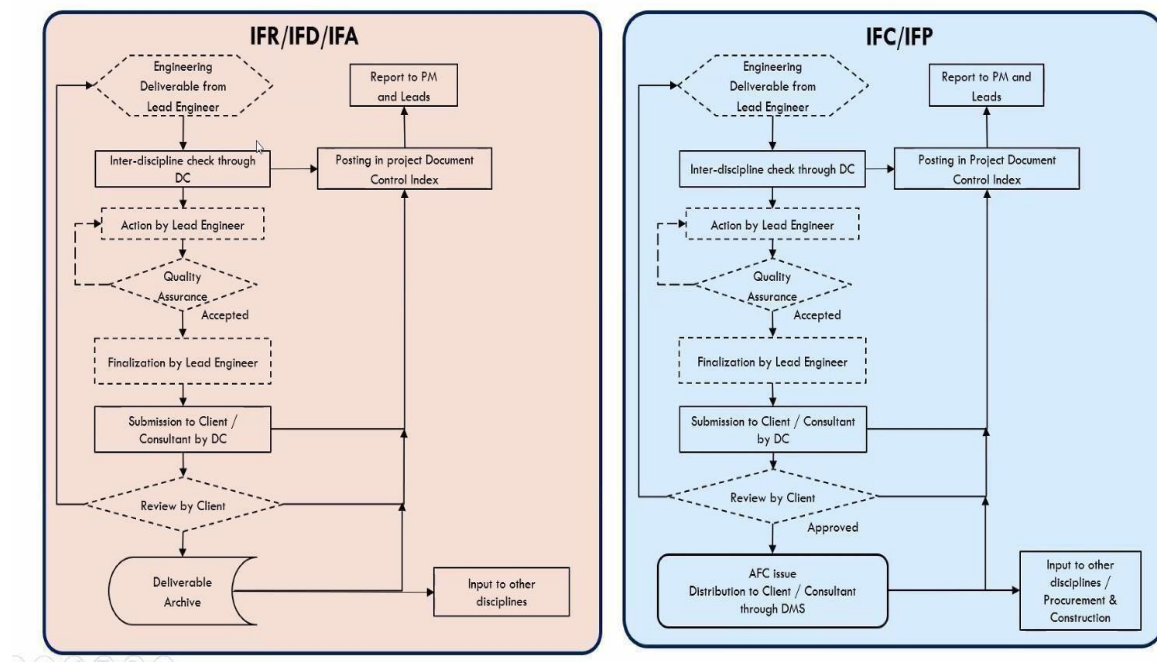
7th May2021: Engineering documentation for Electrical system design

4	Electrical system design for a small small project	Overall plant description Sequence of approach Approach to detailed design
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Topic details: Overall plant description ,approach to detailed design.



1C. DETAILED ENGINEERING



Here we observed that how to do a project and Sequence of approach, Approach to detail design and Overall plant distribution system.

10th May2021: Engineering documentation for Typical diagrams5 Electrical system
design for typical
diagramsLoad lists shedule
Single line diagramPower flow diagram
Typical schematic diagram

Topic details: Typical diagrams and Load calculations.

S No	Equipment No.	Description	Supply by	Type	Status	Non essential	Reinstating	Absorbed load	Equipment rating	Load factor at 100% H or P	Efficiency at load factor C	Power factor at load factor C	kW = A/D		Consumed Load		kW = (100%) x J		Remarks	Revision	
													Continuous	Intermittent and spares	Standby	Total	kW	kVA			
																					No.
PROCESS LOADS																					
1	PD 3431	Portable MEG Injection Pump Package	LEWA	x				27.00	37.00	0.73	0.91	0.83				1	29.67	19.94	Portable Skid (Please refer Note-d)	0	
2	34-PM8401A	Liquid Return Pump Motor	LEWA	x				25.45	31.00	0.82	0.93	0.81				1	27.37	19.81		0	
3	34-PM8401B	Liquid Return Pump Motor	LEWA	x				25.45	31.00	0.82	0.93	0.81						1	27.37	19.81	0
4	34-PM8402A	Booster Pump Motor (LRP Package)	LEWA	x				1.40	2.20	0.84	0.78	0.84				1	1.79	1.16		0	
5	34-PM8402B	Booster Pump Motor (LRP Package)	LEWA	x				1.40	2.20	0.84	0.78	0.84						1	1.79	1.16	0
6	34-PM7902A	Corrosion Inhibitor Injection Pump Motor	LEWA	x				6.45	11.00	0.59	0.90	0.77	1	7.17	5.94					0	
7	34-PM7902B	Corrosion Inhibitor Injection Pump Motor	LEWA	x				6.45	11.00	0.59	0.90	0.77	1	7.17	5.94					0	
8	34-PM7903A	Batch Corrosion Inhibitor Injection Pump Motor	RAM	x				133.50	160.00	0.83	0.96	0.80						1	136.06	104.30	0
9	34-PM7903B	Batch Corrosion Inhibitor Injection Pump Motor	RAM	x				133.50	160.00	0.83	0.96	0.80						1	136.06	104.30	0
10	34-PM7904A	KH Inhibitor Injection Pump Motor	LEWA	x				6.45	11.00	0.59	0.90	0.77	1	7.17	5.94					0	
11	34-PM7904B	KH Inhibitor Injection Pump Motor	LEWA	x				6.45	11.00	0.59	0.90	0.77	1	7.17	5.94					0	
12	34-PM7905A	Scale Inhibitor Injection Pump Motor	FUTURE	x				3.00	4.00	0.75	0.85	0.81	1	3.53	2.56					0	
13	34-PM7905B	Scale Inhibitor Injection Pump Motor	FUTURE	x				3.00	4.00	0.75	0.85	0.81	1	3.53	2.56					0	
14	34-KM6602A	Nitrogen Compressor Motor	GENERON	x				30.00	37.50	0.80	0.90	0.80	1	33.33	25.00					0	
15	34-KM6602B	Nitrogen Compressor Motor	GENERON	x				30.00	37.50	0.80	0.90	0.80	1	33.33	25.00					0	
16	34-KM6602C	Nitrogen Compressor Motor	GENERON	x				30.00	37.50	0.80	0.90	0.80	1	33.33	25.00					0	
17	34-EM6602A	Aftercooler for Nitrogen Compressor	GENERON	x				1.15	2.50	0.46	0.78	0.80	1	1.47	1.11					0	
18	34-EM6602B	Aftercooler for Nitrogen Compressor	GENERON	x				1.15	2.50	0.46	0.78	0.80	1	1.47	1.11					0	
19	34-EM6602C	Aftercooler for Nitrogen Compressor	GENERON	x				1.15	2.50	0.46	0.78	0.80	1	1.44	1.08					0	
20	34-H6602	Nitrogen Heater		x				6.20	1.00	0.20	0.90	1.00								0	
21	34-PM8701A	Hydraulic Fluid Pump - Wellhead HPU - Very High Pressure	FRAMES	x				0.19	0.55	0.35	0.80	0.70	1	0.24	0.24					0	
22	34-PM8701B	Hydraulic Fluid Pump - Wellhead HPU - Very High Pressure	FRAMES	x				0.19	0.55	0.35	0.80	0.70	1	0.24	0.24					0	
23	34-PM8702A	Hydraulic Fluid Pump - Wellhead HPU - Medium High Pressure	FRAMES	x				5.80	7.50	0.77	0.80	0.98	1	7.25	4.30					0	
24	34-PM8702B	Hydraulic Fluid Pump - Wellhead HPU - Medium High Pressure	FRAMES	x				5.80	7.50	0.77	0.80	0.98	1	7.25	4.30					0	
25	34-A0704A	Hydraulic Fluid Pump - ICPPS Valves HPU	LEDEEN	x				5.42	5.50	0.99	0.80	0.86	1	6.78	4.02					0	
26	34-A0704B	Hydraulic Fluid Pump - ICPPS Valves HPU	LEDEEN	x				5.42	5.50	0.99	0.80	0.86	1	6.78	4.02					0	
27	34-PM8705A	Hydraulic Fluid Pump - ESD's HPU	LEDEEN	x				5.42	5.50	0.99	0.80	0.86	1	6.78	4.02					0	
28	34-PM8705B	Hydraulic Fluid Pump - ESD's HPU	LEDEEN	x				5.42	5.50	0.99	0.80	0.86	1	6.78	4.02					0	
29	AC 3435	Crane motor	LIEBHERR	x				112.00	140.00	0.80	0.95	0.90	1	117.89	57.10					0	
30	34-K26303	Lifeboat Recovery Starter Panel	SCHAL HARDING	x				6.74	9.35	0.53	0.81	0.82	1	8.89	18.83			1	9.60	6.70	0
31	CP34302	Flare Knock Out Drum Heater Control Panel	CHROMALOX	x				35.00	35.00	1.00	0.90	0.90	1	38.89	18.83					0	
HVAC LOADS																					
32	34-YH4201ACCU01	Air Cooled Condensing Unit - 01	CCTC	x				37.25	42.80	0.87	0.82	0.80	1	45.43	34.07					0	
33	34-YH4201ACCU02	Air Cooled Condensing Unit - 02	CCTC	x				37.25	42.80	0.87	0.82	0.80	1	45.43	34.07					0	
34	34-YH4201AHU01	Air Handling Unit - 01	CCTC	x				8.85	10.00	0.89	0.80	0.80	1	11.06	8.30					0	
35	34-YH4201AHU02	Air Handling Unit - 02	CCTC	x				8.85	10.00	0.89	0.80	0.80	1	11.06	8.30					0	
36	34-YH4201FF01	Fresh Air Fan - 01	CCTC	x				8.00	8.00	1.00	0.90	0.80	1	8.89	6.67					0	
37	34-YH4201FF02	Fresh Air Fan - 02	CCTC	x				8.00	8.00	1.00	0.90	0.80	1	8.89	6.67					0	
38	34-YH4201EF01	Exhaust Fan - Toilet	CCTC	x				1.00	1.00	1.00	0.90	0.80	1	1.11	0.83					0	
39	34-YH4201EDH01	Duct heater - 01	CCTC	x				8.78	9.78	1.00	1.00	1.00	1	9.78	0.00					0	
40	34-YH4201EDH02	Duct heater - 02	CCTC	x				4.69	4.69	1.00	1.00	1.00	1	4.69	0.00					0	
41	34-YH4201EDH03	Duct heater - 03	CCTC	x				0.90	0.90	1.00	1.00	1.00	1	0.90	0.00					0	
42	34-YH4201EDH04	Duct heater - 04	CCTC	x				4.98	4.98	1.00	1.00	1.00	1	4.98	0.00					0	
ELECTRICAL LOADS																					
43	AC 3431	Power Distribution Board	MASSERA	x				41.00	51.50	0.80	0.98	0.90	1	41.84	31.38					0	
44	UPS-3442/3443	UPS - Main/Bypass	GLTOR	x				24.00	24.00	1.00	0.82	0.80	1	29.27	21.95					0	
45	EC 3442	Switchgear 24 V DC UPS	SAFT	x				1.20	1.20	1.00	0.80	0.80	1	1.50	1.13					0	
46	ELTR 3431	Lighting Transformer for LP 3431	SCHNEIDER	x				27.00	27.00	1.00	0.98	0.90	1	27.55	13.34					0	
47	ELTR 3431	Lighting Transformer for ELP 3431	SCHNEIDER	x				27.00	27.00	1.00	0.98	0.90	1	27.55	13.34					0	
48	WD 3431A	Welding Socket Outlet 1 - Upper Deck	STAHL	x				33.00	33.00	1.00	0.98	0.80	1	33.67	25.26					0	
49	WD 3431B	Welding Socket Outlet 2 - Upper Deck	STAHL	x				33.00	33.00	1.00	0.98	0.80	1	33.67	25.26					0	
50	WD 3432A	Welding Socket Outlet 1 - Lower Deck	STAHL	x				33.00	33.00	1.00	0.98	0.80	1	33.67	25.26					0	
51	WD 3432B	Welding Socket Outlet 2 - Lower Deck	STAHL	x				33.00	33.00	1.00	0.98	0.80	1	33.67	25.26					0	
52	WD 3433A	Welding Socket Outlet 1 - Mezz Deck	STAHL	x				33.00	33.00	1.00	0.98	0.80	1	33.67	25.26					0	
53	WD 3433B	Welding Socket Outlet 2 - Mezz Deck	STAHL	x				33.00	33.00	1.00	0.98	0.80	1	33.67	25.26					0	
54	WD 3434	Welding Socket Outlet - Cellar Deck	STAHL	x				33.00	33.00	1.00	0.98	0.80	1	33.67	25.26					0	
Max. of normal running plant load:								303	kW	332	kVA		TOTAL		278	195	282	128	671	803	Power factor without compensation (Can be 0.85)
(Est. x 1.05 + x 1.05 + x 1.05)								420	kW	382	kVA		339		282	128	638			Power factor with compensation (Can be 0.9)	
Peak load:								420	kW	382	kVA		339		282	128	638			Read capacity at 1.44 = 1.44 x 1.05 + 1.05 + 1.05	kVA
(Est. x 1.05 + x 1.05 + x 1.05)																					
Notes:																					
a) Load classification/starting:																					
For definitions of "Vital", "Essential" and "Non - Essential", services and application of "Restarting", see DEP 33.64.10.10 - Gen. Electrical engineering guidelines.																					
d) The Panel shall feed injection pumps P7901A/B.																					
e) Batch injection pump considered as standby load during normal running condition based on operating philosophy.																					
b) Absorbed loads:																					
- for pumps, shaft load on duty point.																					
- for instrumentation, computers, communication, & air conditioning, the required load during full operation of plant.																					
- for lighting, during dark hours.																					
- for workshops, the average total load in normal full operation.																					
c) Consumed loads:																					
E - "Continuous", all loads that may continuously be required for normal operation including lighting during full operation.																					
F - "Intermittent and spares", the loads required for intermediate pumping, storage, loading, etc. and all electrical spares of electrically driven units.																					
G - "Stand-by" loads: loads required in emergencies only, such as fire water pumps or those of not normally running electrically driven units & electrical stand-by for normally running steam - driven ones (e.g. charge pumps, boiler feed pumps)																					
QATAR GAS 384 OFFSHORE FACILITIES PROJECT WELHEAD PLATFORM 7																					
MCC																					
APPROVED FOR CONSTRUCTION																					
APPROVED FOR CONSTRUCTION WITH HOLD																					
ISSUED FOR COMPANY REVIEW																					
ISSUED FOR IDC																					
REVISIONS:																					
01	24-Jun-07	AK																			
02	20-Aug-07	PJ																			
A	18-Jul-07	PJ																			
B	26-Oct-06	JG																			

11th May 2021: Classification of Transformers and Generators

6	Classification of Transformers and Generators	Different types of Transformers	Different types of Generators
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Topic Details: Classification of Transformers and Generators.



1 Ph. Pad mounted 3 Ph Pole mounted Commercial/ 3 Ph Oil filled (ONAN) Distribution Residential lighting Residential/ street lighting type for industrial & commercial.



415V Diesel generator sets for standby / 240V 1 ph diesel generator set for lighting and & small power only Emergency power supply.

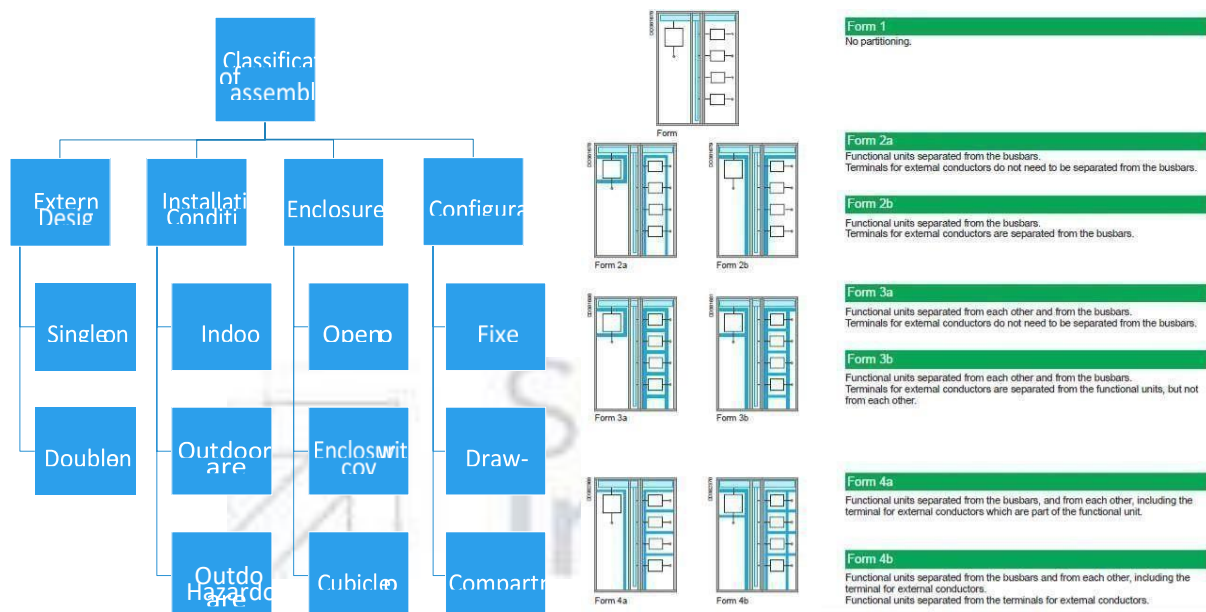
Transformer shall include a primary disconnect on the incoming power source. The disconnect means shall be either a breaker or a load break primary switch that is fused. Transformers are sized to carry the peak running load of all busses connected to them. In addition, feeders to and from power transformers shall be rated to carry full current at the maximum rating.

The packaged combination of a diesel engine, an alternator and various ancillary devices such as base, canopy, sound attenuation, control systems, circuit breakers, jacket water heaters, starting systems etc., is referred to as a Diesel Generating Set or a DG Set in short.

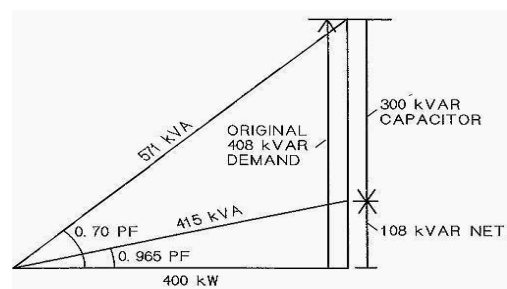
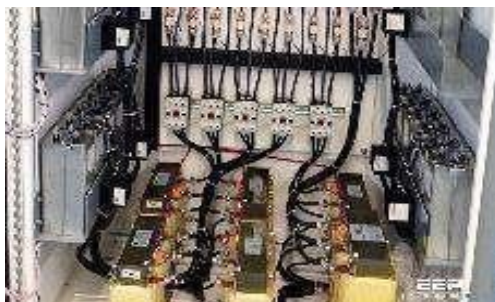
12th May2021: Classification of Switchgear construction and power factor improvement

7	Classification of Switchgear construction and power factor improvement	Different types of Switchgear assemblies	Power factor improvement
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Topic details: Classifiacton of Switchgear contruction and Power Factor Improvement.



Switchgear includes switching & protecting devices like fuses, switches, CTs, VTs, relays, circuit breakers, etc. This device allows operating devices like electrical equipment, generators, distributors, transmission lines, etc.



Power factor defined as the ratio of real power to volt-amperes and is the cosine of the phase angle between the voltage and current in an AC circuit.

17th May2021: Detailing about UPS system and Busducts.

8	Detailing about UPS system and Busducts	Uninterruptible power supply system	Busducts of the system
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Topic details: Power distribution of UPS system and Busducts.

UPS systems are designed to provide continuous power to a load, even with an interruption or loss of utility supply power. UPS generally involves a balance of cost Vs need.



110V or 220V DC
UPS System

110V or 230V
AC UPS System

Busducts are classified into various types depending on its application viz phase separated Busducts, segregated phase busducts, non-segregated phase busducts.



18th May2021: Detailing about Motor Starters and Sizing of motors.

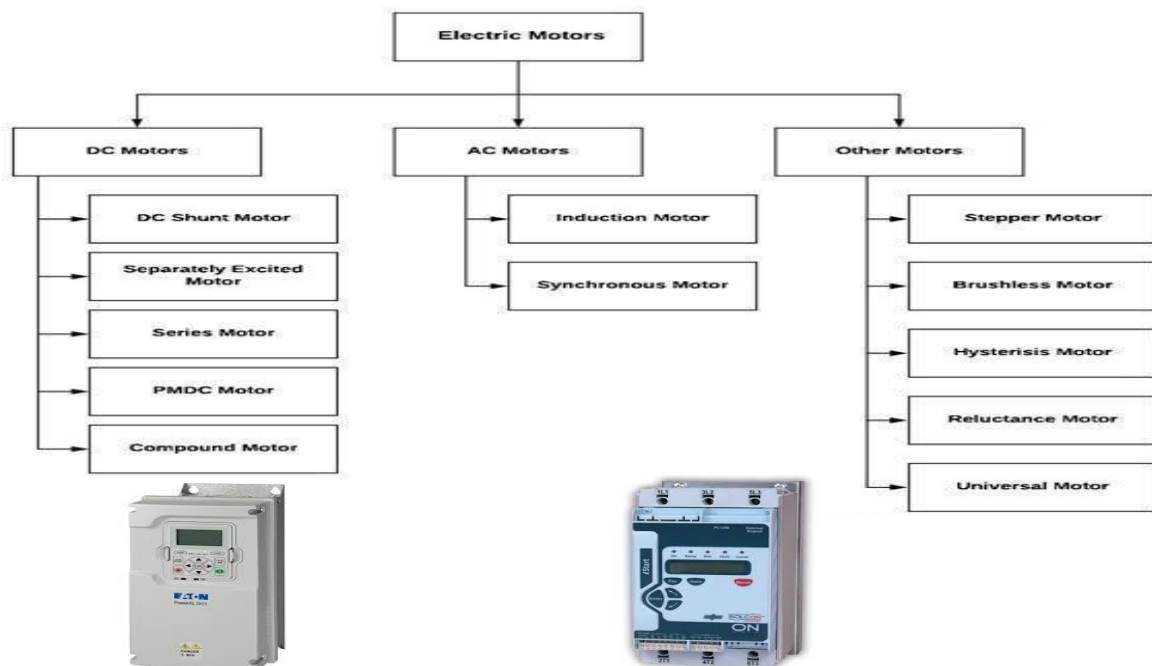
9	Detailing about Motor Starters and Sizing of motors	Motor starters and drives	Sizing and selection of motors
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Topic details: Detailing about Motor Starter and Sizing of motors and their selection.

The principal function of a motor starter is to start and stop the respective motor connected with specially designed electromechanical switches which are similar in some ways to relays. The main difference between a relay and a starter is that a starter has overload protection for the motor that is missing in a relay.

Different types of motor starters are as follows:

- Direct-On-Line Starter
- Rotor Resistance Starter
- Stator Resistance Starter
- Auto Transformer Starter
- Star Delta Starter



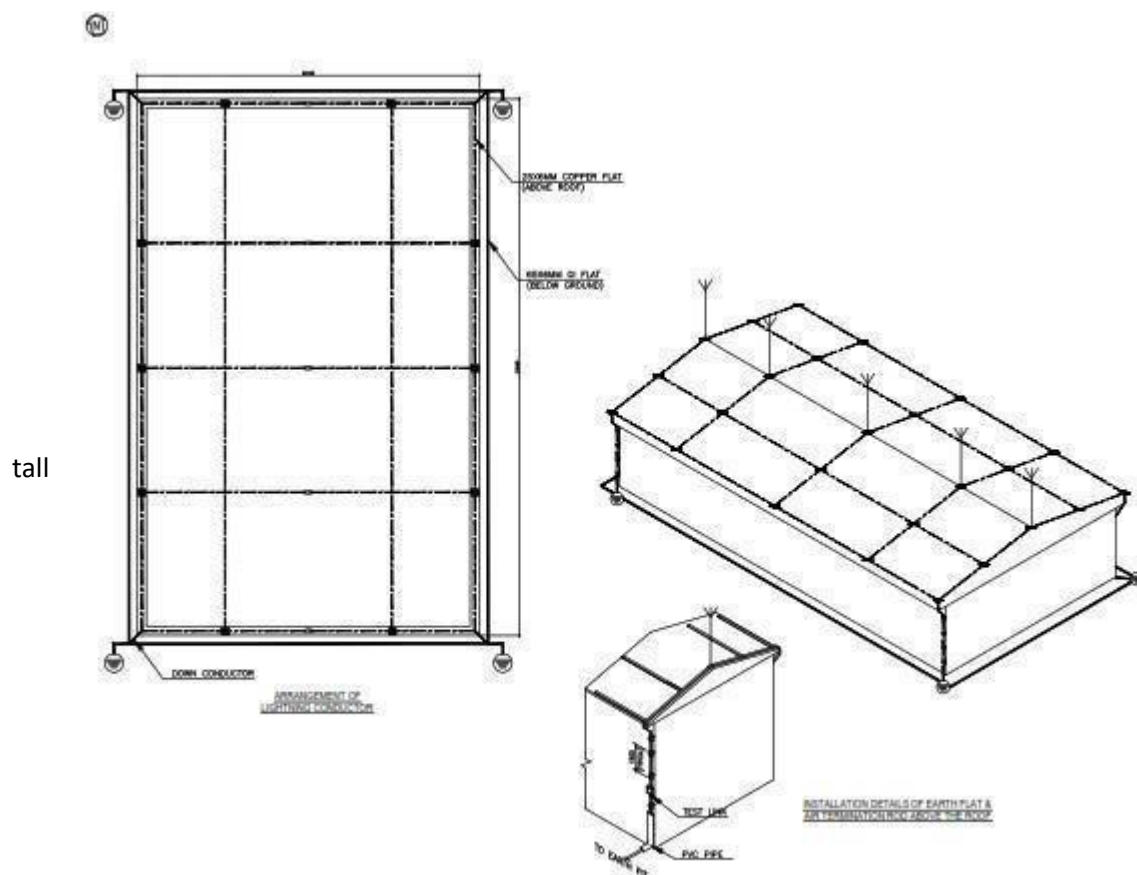
- Starting method – soft starter, Auto transformer, Star/Delta
- Speed variation – Constant speed, variable speed for VFD
 - Frame Size – 56 to 280
- Insulation class & Temp rise – A, E, B, F & H
- Protection – Protection based on voltage & KW rating
- Cable entry, size & termination – Cable sizing based on starting/running voltage drop and short circuit current Vibration – monitoring based on KW rating.

19th May2021: Discribing about Earthing system and Lighting Protection.

10	Discribing about Earthing system and Lighting Protection.	Plant Earthing system	Lighting Protection materials
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Topic details: Discribing about Earthing system and Lighting Protection.

The purpose of earthing is to prevent damage to people and prevent or limit plant damage. Various earthing systems are provided with each earthing system is isolated from the other.



Lightning protection required for high rise structures and important buildings against lightning currents during thunder storms. Primarily Lightning protection system calculations are done based on soil resistivity, conductor material, coverage structure / Building to determine whether lightning protection is required or not.

20th May2021: Lighting or illumination systems and calculations.

11 Lighting or Illumination systems and Calculations

Lighting or illumination systems

Lighting calculations

Topic details: Lighting or Illumination systems and Calculations.

All outdoor lighting fittings shall be connected with armoured PVC cable of suitable no. of cores and size. Necessary type and no. of junction boxes shall be provided for branch connections. Indoor light fittings shall be connected with FRLS PVC wires laid in cable trunks or conduits.



Inputs required: Equipment and cable routing layouts, lighting calculations, Design basis for type of light fittings to be used, required lux levels

Lighting calculations software: Dialux, Chalmrite, Calculux, Relux, Luxicon, CG Lux

Applicable Standards: IS 6665: Code of practice for industrial lighting, IS 3646: Code of practice for interior illumination, IEC 60598: Luminaires, IEC 62493: Assessment of lighting equipment related to human exposure to electromagnetic field

Deliverables: Indoor Lighting layouts, socket outlet layouts, Street lighting and area lighting layouts. BOQ.

Types of light fittings: Industrial, flame proof type (EX d), increased safety type (Ex e).

21th May2021: Lighting or illumination systems using DIALUX software.

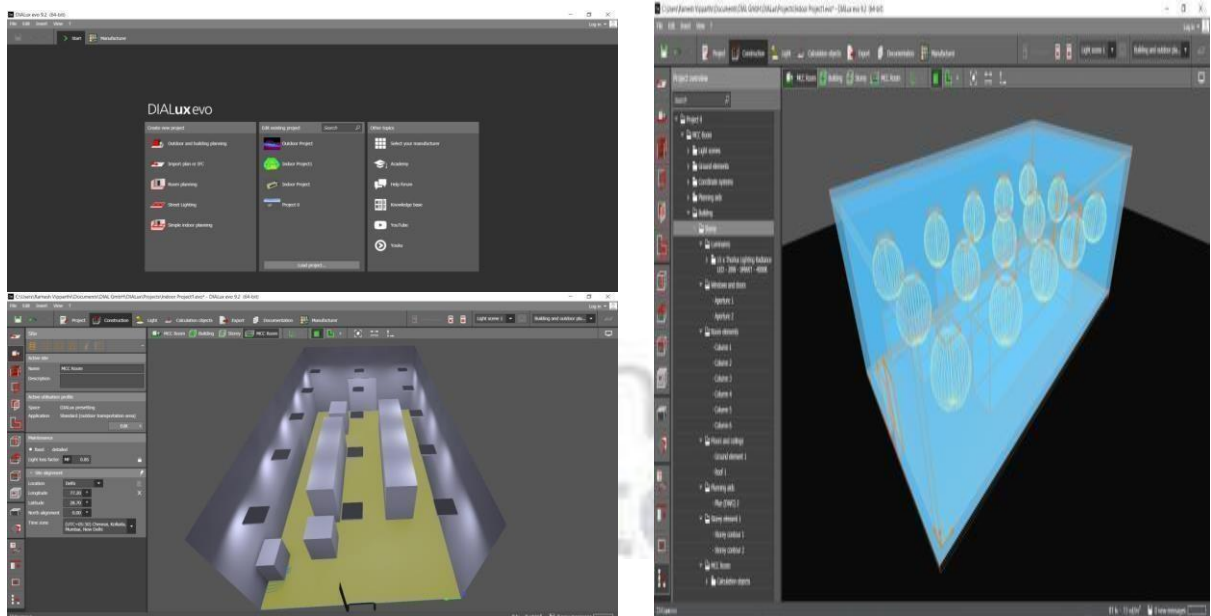
12 Lighting or Illumination using DIALUX software

Lighting or illumination systems

Operation of dialux software

Topic details: Lighting or Illumination Calculations using DIALUX software.

Here we are using this Dialux evo 5.9.2 software windows to construct the power plant and we can perform the operation from this software.



We have the indoor calculations and outdoor calculations too.

Results

	Symbol	Calculated	Target	Check	Index
Workplane	$E_{\text{perpendicular}}$	264 lx	$\geq 500 \text{ lx}$	✗	□
	ρ_v	0.077	-	-	□
Consumption values	Consumption	1300 kWh/a	max. 3400 kWh/a	✓	
Lighting power density	Room	4.82 W/m ²	-	-	
		1.83 W/m ² /100 lx	-	-	

Utilisation profile: DIALux presetting: Standard (office)

Luminaire list

pcs.	Manufacturer	Article No.	Article name	P	Φ	Luminous efficacy
15	THORLUX	RAD16401	Radiance LED - 28W - SMART - 4000K	31.0 W	4130 lm	133.2 lm/W

Indoor calculation

Piperack

Luminaire list

Φ_{total}	P _{total}	Luminous efficacy
15850 lm	360.0 W	44.0 lm/W

5	CEAG	122658811	eLLK 92018/18 CG-S	72.0 W	3170 lm	44.0 lm/W
		03				

outdoor calculations

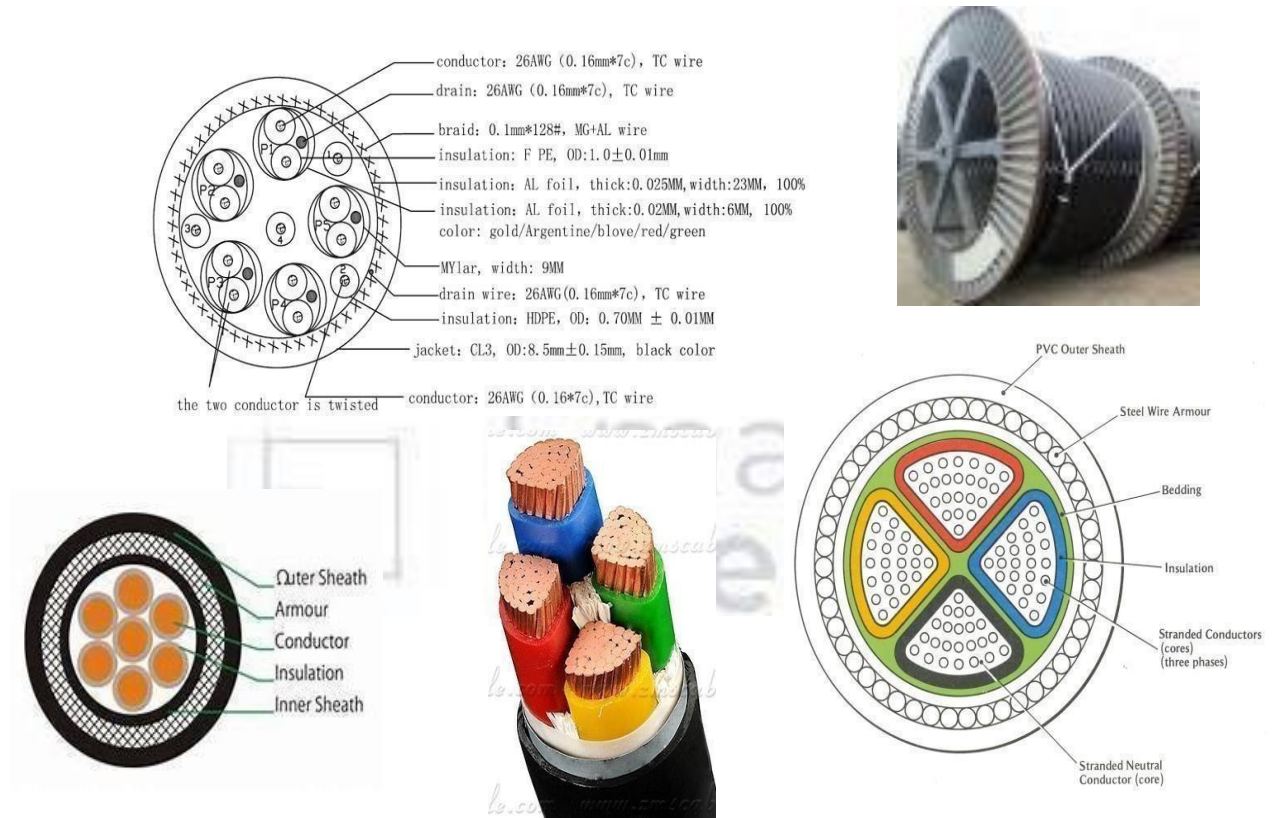
24th May2021: Cabling and their calculations and types.

13 Cabling and their
types and
calculations

Cabling calculations

Types of cabling materials

Topic details: Cabling and their types and calculations .



Electrical cables must be properly supported to relieve mechanical stresses on the conductors, and protected from harsh conditions such as abrasion which might degrade the insulation.

Cables generally laid in the cable trays above ground, direct buried underground and in metallic or PVC conduits. Derating factors may be applicable for each type of cable laying conditions.

Cable trays shall be generally loaded 60 to 70% leaving space for future use. Underground cabling shall be done in concrete cable trenches with cable trays in paved areas and directly buried with mandatory gap of 300mm between different systems of cables.

25th May2021: Cabling calculations and Cable gland selection.

14 Cabling
calculations and
cable gland
selection

Cabling calculations

Cable gland selection

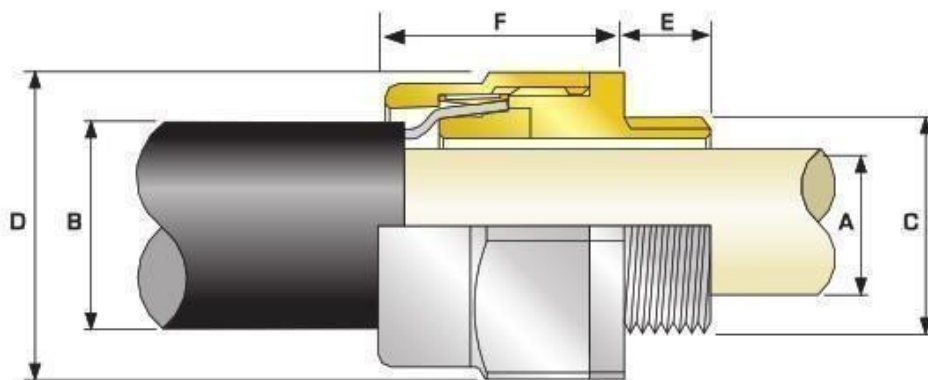
Topic details: Cable sizing calculation and cable gland selection.

Inputs required: Load List, Design basis, Electrical equipment layout, cable schedule, vendor catalogues for cable tray.

Cable tray sizing shall be performed for each branch of cable tray routing up to the load point.

Results shall be checked with specified limits mentioned in design basis.

Cable gland:



Cable Gland Selection Table

Refer to illustration at the top of the page.

Cable Gland Size	Available Entry Threads "C" (Alternate Metric Thread Lengths Available)		Cable Bedding Diameter "A"	Overall Cable Diameter "B"	Armour Range		Across Flats "D"	Across Corners "D"	Protrusion Length "F"
	Metric	Thread Length (Metric) "E"	Max	Max	Min	Max	Max	Max	
20S16	M20	10.0	8.7	13.2	0.8	1.25	24.0	26.4	35.2
20S	M20	10.0	11.7	15.9	0.8	1.25	24.0	26.4	32.2
20	M20	10.0	14.0	20.9	0.8	1.25	30.5	33.6	30.6
25	M25	10.0	20.0	26.2	1.25	1.6	36.0	39.6	36.4
32	M32	10.0	26.3	33.9	1.6	2.0	46.0	50.6	32.6
40	M40	15.0	32.2	40.4	1.6	2.0	55.0	60.5	36.6
50S	M50	15.0	38.2	46.7	2.0	2.5	60.0	66.0	39.6
50	M50	15.0	44.1	53.1	2.0	2.5	70.1	77.1	39.1
63S	M63	15.0	50.0	59.4	2.0	2.5	75.0	82.5	52.0
63	M63	15.0	56.0	65.9	2.0	2.5	80.0	88.0	49.8
75S	M75	15.0	62.0	72.1	2.0	2.5	90.0	99.0	63.7
75	M75	15.0	68.0	78.5	2.5	3.0	100.0	110.0	57.3
90	M90	24.0	80.0	90.4	3.15	4.0	114.3	125.7	66.6

28 th May2021: Load calculations and Transformer sizing calculations

15 Load calculations
and TR
calculations

Load calculations

TR calculations

Topic details:

List of electrical load calculations.

Sl. No.	Equipment No.	Equipment Description	Breaker Rating	Breaker Type	Breaker No. of Poles	FLCB Rating	Absorbed Load	Motor Load Rating	Load Factor (A) / (B)	Efficiency at Load Factor (C)	Power Factor at Load Factor (C)	kVA = (A) / (D)		Consumed Load		kVAR = kVA x tan φ	
							(A)	(B)	(C)	(D)	cos φ	kW	kVAR	kW	kVAR	kW	kVAR
1.	PU235	Silo filter load pump					12.47	15.00	0.83	0.85	0.73	14.67	13.74				
2.	PU 234-A	Absorbent/Neutral oil pump (W)					3.62	4.70	0.77	0.85	0.73	4.3	4.0				
3.	PU 234-B	Absorbent/Neutral oil pump (S)					3.11	3.70	0.84	0.85	0.73					3.7	3.4
4.	PU2305	Feed Pump (Superheater)					12.56	15.00	0.84	0.85	0.73	14.6	13.9				
5.	MX2305	MXER (W)					12.68	15.00	0.85	0.85	0.73	14.9	14.0				
6.	MX 2308	MXER (S)					12.68	15.00	0.85	0.85	0.73					14.9	14.0
7.	RV2313	Boiler					5.45	7.50	0.73	0.85	0.73	6.4	6.0				
8.	Rotary valve	TK 2313B (I)					0.53	0.78	0.71	0.85	0.73			0.6	0.6		
9.	SC234	Screw conveyor (I)					1.23	1.50	0.82	0.85	0.73			1.45	1.35		
10.	AG 2324A	Crisic acid tank agitator (W)					0.91	1.10	0.83	0.85	0.73	1.07	1.00				
11.	AG 2324B	Crisic acid tank agitator (S)					0.91	1.10	0.83	0.85	0.73					1.1	1.0
12.	AG 2305	Crisic oil reaction vessel agitator					3.34	3.70	0.90	0.85	0.73	3.33	3.66				
13.	AG 2309	Lye oil reaction vessel agitator					1.21	1.50	0.81	0.85	0.73	1.42	1.33				
14.	AG 2310	Lye oil reaction vessel agitator					1.21	1.50	0.81	0.85	0.73	1.42	1.33				
15.	AG 234	Screw Absorbent Tank Agitator					2.12	3.00	0.71	0.85	0.73	2.49	2.34				
Maximum of normal running plant load: (Est. x0.5E + y0.5G)			66.0 kVA			61.6 kVAR	sqrt (kW ² + kVAR ²) =		80.4 kVA		TOTAL	65.40	61.23	2.07	1.94	19.65	18.39
Peak Load: (Est. x0.5E + y0.5F + z0.5G)			68.0 kVA			63.7 kVAR	sqrt (kW ² + kVAR ²) =		93.1 kVA		kVA	69.53		2.84		26.91	
Assumptions 1) Load factor, Efficiency and Power factor: Load Rating (kW) ≤ 20 > 20 - ≤ 45 > 45 - ≤ 750 > 750						Efficiency 0.95 0.91 0.93 0.94	Power factor 0.85 0.78 0.82 0.91										

TR sizing calculations:

Calculation for Transformer Capacity

1.0 Example of calculation for Transformer Capacity

1.1 Calculation for consumed load

Consumed loads used for this example are as follows:

	kW	kVar	kVA	
a. Continuous load	125.69	106.5	164.74	--- (i)
b. Intermittent load / Diversity Factor	4.15	3.9	5.69	--- (ii)
c. Stand-by load required as consumed load	37.57	31.4	48.95	--- (iii)

Max. Consumed load = [(i) + 30% (ii) + 10% (iii)] =

Future expansion load (20% capacity)

Total Load =

1.2 Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	171.3 kVA
Spare capacity	=	34.3 kVA
Required capacity	=	205.6 kVA
Transformer rated capacity	=	120 kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW), while all the other loads running, the voltage regulation is as follows:

$P_T = 220 \text{ kVA}$ $(\%Z) = 4.37$ $\& \text{Base } \times \%R = 3.4$
 Hence, $\%R = 1.133\%$
 $\%X = 4.00\%$
 $P_H = 30 \text{ kW}$ having $(K = 6)$ & $C = 1$ & $\cos \theta = 0.78$ & $\text{Eff.} = 0.91$ & $\cos \theta_s = 0.25$
 $P_s = 253.59 \text{ kVA}$
 $\cos \theta_s = 0.25$, Corresponding to Angle $\theta_s = 75.522$ Degrees for which $\sin \theta_s = 0.97$
 $P_s = 126.28 \text{ kVA}$ & P_B in kW is 107.33 & P_s in kVar = 65.66 & $\cos \theta_s = 0.850$
 $\cos \theta_s = 0.85$, Corresponding to Angle $\theta_s = 31.795$ Degrees, for which $\sin \theta_s = 0.53$
 $P_{cp} = 170.73 \text{ kW}$
 $P_{ca} = 311.2 \text{ kVAR}$
 $P_c = 354.96 \text{ kVA}$
 $\cos \theta_c = 0.481$, where as $\sin \theta_c = 0.877$

Voltage Regulation = 6.6 %

Result During starting of max. capacity motor, while all other loads are running, the voltage regulation at Transformer secondary terminals is approx. 6.60%

1.4 Selection of rated capacity
120 kVA transformer selected.

29th May2021: DG set calculations.

16 DG set
calculations

Topic details:

Transformer and DG set calculations,types ,sizing or selections

DG SIZING CALCULATIONS		
Design Data		
Rated Voltage	415	KV
Power factor (Cos ϕ)	0.74	Avg
Efficiency	0.86	Avg
Total operating load on DG set in kVA at 0.74 power factor	166.4	
Largest motor to start in the sequence - load in KW	30	KW
Running kVA of last motor (Cos ϕ = 0.91)	47	KVA
Starting current ratio of motor	6	(Considering starting method as Soft starter)
Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	283	KVA
Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	119	KVA
A Continuous operation under load -P1		
Capacity of DG set based on continuous operation under load P1	119	KVA
B Transient Voltage dip during starting of Last motor P2		
Total momentary load in KVA	402	KVA
(Starting KVA of the last motor+Base load of DG set in KVA)		
Subtransient Reactance of Generator (X_d'')	7.91%	(Assumed)
Transient Reactance of Generator (X_d')	10.065%	(Assumed)
$X_d''' = (X_d'' + X_d')/2$	0.089875	
Transient Voltage Dip	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor (Transient	205	KVA
C Overload capacity P3		
Capacity of DG set required considering overload capacity		
Total momentary load in KVA	402	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) = $\frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	268	KVA

2nd june2021: Caluculations of Earthing and Lighting protection.

17 Calculation of
Earthing and
Lighting protection
calculations

Earthing calculations

Lighting protection calculation

Topic details:

Calculation of Earthing and Lighting protection calculations

Location	7				
Building	Udaipur				
Type of Building	Concrete. Hospital				
Building Length (L)	Flat Roofs (a)				
Building breadth (W)	12				
Building Height (H)	7				
	9				
Risk Factor Calculation					
1 Collection Area (A _c)		=	(L*W) + (2*L*H) + (2*W*H) + (3.14*H*H)		
			805.34		
2 Probability of Being Struck (P)		=	A _c * N _a = 10 ⁻⁶		
			0.001530146		
3 Overall weighing factor		=			
a) Use of structure (A)		=	1.7		
b) Type of construction (B)		=	0.4		
c) Contents or consequential effects (C)		=	1.7		
d) Degree of isolation (D)		=	1.0		
e) Type of country (E)		=	0.3		
W _o - Overall weighing factor		=	A * B * C * D * E		
			0.347		
4 Overall Risk Factor		=	P * W _o		
			0.000530655		
			10 ⁻⁶		
As per clause no. 9.7 of BS- 6651, suggested acceptable risk factor (P _o) has been taken as 10 ⁻⁶					
Since P _o > P _a lightning protection required.					
5 Air Terminations					
Perimeter of the building		=	2(L+W)		
			48	Mts.	
6 Down Conductors					
Perimeter of building		=	48	Mts.	
No. of down conductors based on perimeter		=	2	Nos.	
Hence 2 nos. of Down conductors have been selected.					
Size of Down conductor		=	20 X 2.5 mm Galvanized Steel Strip		
(As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size of Down conductors - 20mm X 2.5 mm Galvanized Steel Strip)					

Earthing calculations:

Maximum line-to-ground fault in kA for 1 sec	13	
Earthing material (Earth rod & earth strip)	GI	
Depth of earth flat burial in meter	0.5	
Average depth / length of Earth rod in meters	4	
Soil resistivity Ω-meter	8.5	
Ambient temperature in deg C	50	
Plot dimensions (earth grid) L x B in meters	70	130
Number of earth rods in nos.	6	
Earth electrode sizing:		
Ac - Required conductor cross section in sq.mm		
$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$		
α _r - Thermal co-efficient of resistivity, at 20 oC	0.0032	
ρ _r - Resistivity of ground conductor at 20 oC	20.10	
T _a - Ambient Temperature is °C	50	
I _{lg} - RMS fault current in kA = 50 KA	14	
t _c - Short circuit current duration sec	1	
Thermal capacity factor, TCAP J/(cm3.oC)	3.93	
T _m - Maximum allowable temperature for copper conductor, in oC	419	
K ₀ - Factor at oC	293	
The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:		
	14 = Ac *	0.123
Ac - Required conductor cross section in sq.mm		114
Earth rod dia in mm		12
Earth rod dia (including 25% corrosion allowance) in mm		15

5th june 2021: Cable sizing and cable tray sizing calculations.

18 Cable sizing and cable tray sizing calculations

Cable sizing calculations

Cable tray calculation

Topic details: Cable sizing and cable tray sizing calculations for LV cables and MV/HV cables.

Description	Consumed Load KW	Load Rating KW	Voltage (V)	No. of ph	Full Load Current (A)	Starting Current (A)	Load P.F.	SIN φ Running	Motor P.F.	SIN φ Starting	Type	No. of Runs	No. of Cores	Size (mm ²)	Current Rating (A)	Derating factor k1	Derating factor k2	Derating factor k3	Derating factor k4	Overall Derating factor k	Derated Current (A)	Cable Length (M)	Cable Resistance (Ohms/km)	Cable Reactance (Ohms/km)	Voltage drop (Running) (V)	Voltage drop (Running) (%)	Voltage drop (Starting) (V)	Voltage drop (Starting) (%)	Cable size result
230V MCC	10.47	10.47	415	3	217	130.12	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882	58.2	95	2.9400	0.0852	6.86	1.65	40.99	9.88	OK
230V MCC	3.12	3.12	415	3	6.3	37.77	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	95	9.4800	0.1007	7.32	1.91	47.45	11.43	OK
230V MCC	3.12	3.12	415	3	5.4	32.45	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	60	9.4800	0.1007	4.30	1.04	25.75	6.20	OK
230V MCC	16.58	16.58	415	3	219	131.26	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	85	3.9400	0.0902	10.33	2.49	61.78	14.89	OK
230V MCC	16.58	16.58	415	3	221	132.31	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	9.18	2.21	54.95	13.24	OK
230V MCC	16.58	16.58	415	3	221	132.31	0.8	0.6	0.8	0.5	2	1	4.0	10	66	0.98	0.9	1	1	0.882	58.2	105	2.9400	0.0852	7.71	1.86	45.07	11.10	OK
230V MCC	5.45	5.45	415	3	9.5	56.87	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	100	3.9400	0.0902	5.26	1.27	31.49	7.93	OK
230V MCC	0.53	0.53	415	3	0.9	5.53	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	100	3.9400	0.0902	0.51	0.12	3.06	0.74	OK
230V MCC	1.32	1.32	415	3	2.1	12.83	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	0.89	0.21	5.33	1.28	OK
230V MCC	1.99	1.99	415	3	1.6	9.50	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	110	9.4800	0.1007	2.30	0.56	13.61	3.33	OK
230V MCC	1.99	1.99	415	3	1.6	9.50	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	75	3.9400	0.0902	0.66	0.16	3.94	0.95	OK
230V MCC	3.34	3.34	415	3	5.8	34.85	0.8	0.6	0.8	0.5	2	1	4.0	6	51	0.98	0.9	1	1	0.882	45.0	105	3.9400	0.0902	3.39	0.82	20.26	4.88	OK
230V MCC	1.24	1.24	415	3	2.1	12.83	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	85	9.4800	0.1007	2.37	0.57	14.19	3.42	OK
230V MCC	1.24	1.24	415	3	2.1	12.83	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	95	9.4800	0.1007	2.65	0.64	15.86	3.82	OK
230V MCC	2.12	2.12	415	3	3.7	22.12	0.8	0.6	0.8	0.5	2	1	4.0	2.5	28	0.98	0.9	1	1	0.882	24.7	65	9.4800	0.1007	3.17	0.76	19.01	4.58	OK

Cable Tray calculations:

Sr. No.	Cable Route (From-To)	Type & Cable Size	Size of Cable (mm ²)	No. of Cable	Overall Diameter of each Cable (mm)	Sum of Cable OD (mm)	Self Weight of Cable (Kg/Mt)	Total Weight of Cable (Kg/Mt)	Remarks
1	LV MCC	4	10	1	18	18	3.95	0.9	
2	PU2315- VFD	4	10	1	18	18	0.37	0.9	
3	PU2315- VFD	5	15	1	15	15	3.95	0.4	
4	LV MCC	4	2.5	1	16	16	0.37	0.5	
5	LV MCC	5	1.5	1	15	15	3.95	0.4	
6	LV MCC	4	2.5	1	16	16	0.37	0.5	
7	PU 2314 -B- VFD	4	2.5	1	16	16	0.9	0.5	
8	PU 2314 -B- VFD	5	1.5	1	15	15	0.9	0.4	
9	LV MCC	4	6	1	18	18	2.9	0.7	
10	PU2305- VFD	4	6	1	18	18	1.2	0.7	
11	PU2305- VFD	5	15	1	15	15	1.2	0.4	
12	LV MCC	4	6	1	18	18	1.2	0.7	
13	LV MCC	5	1.5	1	15	15	1.45	0.4	
14	LV MCC	4	10	1	18	18	2	0.9	
15	LV MCC	5	1.5	1	15	15	2.4	0.4	
16	LV MCC	4	6	1	18	18	2.4	0.7	
17	BW2313- VFD	4	6	1	18	18	0.85	0.7	
18	BW2313- VFD	5	1.5	1	15	15	0.85	0.4	
19	LV MCC	4	6	1	18	18	0.85	0.7	
20	LV MCC	5	1.5	1	15	15	1	0.4	
21	LV MCC	4	6	1	18	18	0.85	0.7	
Total				21		348	33.91	12.3	
Calculation					Result				
Maximum Cable Diameter:			18	mm	Selected Cable Tray width:				
Consider Spare Capacity of Cable Tray:			30%		Selected Cable Tray Depth:				
Distance between each Cable:			0	mm	Selected Cable Tray Weight:				
Calculated Width of Cable Tray:			452	mm	Selected Cable Tray Size:				
Calculated Area of Cable Tray:			8143	Sq.mm	Including Spare Capacity				
No of Layer of Cables in Cable Tray:			2		Including Spare Capacity				
Selected No of Cable Tray:			1	Nos.	Required Cable Tray Size:				
Selected Cable Tray Width:			300	mm	Required Nos of Cable Tray:				
Selected Cable Tray Depth:			50	mm	Required Cable Tray Weight:				
Selected Cable Tray Weight Capacity:			150	Kg/Meter	Type of Cable Tray:				
Type of Cable Tray:			Ladder		Cable Tray Width Area Reman				
Total Area of Cable Tray:			15000	Sq.mm	Cable Tray Area Remaning:				

Conclusion:

We have been taught many aspects of engineering activities during the EPC stages for all electrical and related other disciplines also.

Feedback:

Smart Bridge

They conduct summer internships, work shops, debates, hackthons, technical sessions.

Method of conducting program

Online virtual program with presentation slides and explanation on the topic and practical usage of topic and with some examples.

Program highlights

It is for the detailed design of any industrial sectors.

Material

The material was good .

Benefits

It has been given the opportunity to learn and interact with industry experienced engineering specialist to learn the Electrical detailed design engineering for various industrial sectors.

ELECTRICAL LOAD CALCULATIONS LV MCC

[illegible]

Assignment - 2

Calculation for Transformer Capacity

Example of calculation for Transformer Capacity

Calculation for consumed load

Consumed loads used for this example are as follows :

	kW	kVar	kVA	
a. Continuous load	125.69	106.5	164.74	--- (i)
b. Intermittent load / Diversity Factor	4.15	3.9	5.69	--- (ii)
c. Stand-by load required as consumed load	37.57	31.4	48.98	--- (iii)
Max. Consumed load = ((i) + 30% (ii) + 10% (iii)) =	130.7	110.8	171.34	
Future expansion load (20% capacity)	26.1	22.2	34.27	
Total Load =	156.8	133.0	205.61	

Calculation for 3.3kV / 0.433 kV transformer capacity

Max. Consumed load	=	171.3 kVA
Spare capacity	=	34.3 kVA
Required capacity	=	205.6 kVA
Transformer rated capacity	=	120 kVA

1.3 Voltage regulation check

During starting or reacceleration of max. capacity motor (3400 kW) , while all the other loads running , the voltage regulation is as follows :

$$P_T = 220 \text{ KVA} \quad (\%Z) = 4.17 \quad \& \text{ Ratio X/R} = 3.4$$

$$\text{Hence, } \%R = 1.193 \%$$

$$\%X = 4.00 \%$$

$$P_M = 30 \text{ KW having } (K = 6 \& C = 1 \& \cos \theta = 0.78 \& \text{Eff.h} = 0.91 \& \cos \theta_s = 0.25$$

$$P_s = 253.593 \text{ KVA}$$

$$\cos \theta_s = 0.25, \text{Corresponding to Angle } \theta_s = 75.5225 \text{ Degrees for which } \sin \theta_s = 0.97$$

$$P_B = 126.28 \text{ KVA} \& \text{PB in KW is } 107.33 \& \text{P}_B \text{ in Kvar} = 65.66 \setminus \cos \theta_B = 0.850$$

$$\cos \theta_B = 0.85, \text{Corresponding to Angle } \theta_s = 31.7952 \text{ Degrees, for which } \sin \theta_s = 0.53$$

$$P_{CP} = 170.728 \text{ KW}$$

$$P_{CQ} = 311.2 \text{ KVAR}$$

$$P_C = 354.956 \text{ KVA}$$

$$\cos \theta_c = 0.48098, \text{ where as } \sin \theta_c = 0.877$$

$$\text{Voltage Regulation } e = 6.6 \%$$

Result: During starting of max. capacity motor, while all other loads are running , the voltage regulation at Transformer secondary terminals is approx.... 6.60%

Selection of rated capacity

120 kVA transformer selected.

Assignment - 3

DG SIZING CALCULATIONS

Design Data

Rated Voltage	415	KV
Power factor (Cos ϕ)	0.74	Avg
Efficiency	0.86	Avg
Total operating load on DG set in kVA at 0.74 power factor	166.4	
Largest motor to start in the sequence - load in KW	30	KW
Running kVA of last motor (Cos ϕ = 0.91)	47	KVA
Starting current ratio of motor	6	(Considering starting method as Soft starter)
Starting KVA of the largest motor (Running kVA of last motor X Starting current ratio of motor)	283	KVA
Base load of DG set in KVA (Total operating load in kVA – Running kVA of last motor)	119	KVA

A Continuous operation under load -P1

Capacity of DG set based on continuous operation under load P1	119	KVA
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B Transient Voltage dip during starting of Last motor P2

Total momentary load in KVA (Starting KVA of the last motor+Base load of DG set in KVA)	402	KVA
Subtransient Reactance of Generator (Xd'')	7.91%	(Assumed)
Transient Reactance of Generator (Xd')	10.065%	(Assumed)
$X_d''' = (X_d'' + X_d')/2$	0.089875	
Transient Voltage Dip	15%	(Max)
Transient Voltage dip during Soft starter starting of Last motor $P2 = \text{Total momentary load in KVA} \times X_d''' \times \frac{(1 - \text{Transient Voltage Dip})}{(\text{Transient Voltage Dip})}$	205	KVA

C Overload capacity P3

Capacity of DG set required considering overload capacity		
Total momentary load in KVA	402	KVA
overcurrent capacity of DG (K) (Ref: IS/IEC 60034-1, Clause 9.3.2)	150%	
Capacity of DG set required considering overload capacity (P3) = $\frac{\text{Total momentary load in KVA}}{\text{overcurrent capacity of DG (K)}}$	268	KVA

Considering the last value amongst P1, P2 and P3

Continuous operation under load -P1	119	KVA
Transient Voltage dip during Soft starter starting of Last motor P2	205	KVA
Overload capacity P3	268	KVA
Considering the last value amongst P1, P2 and P3	268	KVA

Hence, Existing Generator 268 KVA is adequate to cater the loads as per re-scheduled loads

NOTE:VOLTAGE DIP CONSIDERED - 15%

Assignment - 4

Lightning Calculations

	7
Location	Udaipur
Building	Concrete, Hospital
Type of Building	Flat Roofs (a)
Building Length (L)	17
Building breadth (W)	7
Building Height (H)	9

Risk Factor Calculation

1 Collection Area (A_c)

$$A_c = (L*W) + (2*L*H) + (2*W*H) + (3.14*H*H) = 805.34$$

2 Probability of Being Struck (P)

$$P = A_c * N_g * 10^{-6} = 0.001530146$$

3 Overall weighing factor

a) Use of structure (A)	=	1.7
b) Type of construction (B)	=	0.4
c) Contents or consequential effects (C)	=	1.7
d) Degree of isolation (D)	=	1.0
e) Type of country (E)	=	0.3
Wo - Overall weighing factor	=	$A * B * C * D * E$
	=	0.347

4 Overall Risk Factor

Po	=	$P * Wo$
Po	=	0.000530655
Pa		10^{-5}

As per clause no. 9.7 of BS- 6651, suggested acceptable risk factor (Po) has been taken as 10^{-5}
 Since Po > Pa lightning protection required.

5 Air Terminations

Perimeter of the building	=	$2(L+W)$
	=	48 Mts.

6 Down Conductors

Perimeter of building	=	48 Mts.
No. of down conductors based on perimeter	=	2 Nos.

Hence 2 nos. of Down conductors have been selected.

Size of Down conductor	=	20 X 2.5 mm Galvanized Steel Strip
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(As per BS6651, lightning currents have very short duration, therefore thermal factors are of little consequence in deciding the cross-section of the conductor. The minimum size of Down conductors - 20mm X 2.5 mm Galvanized Steel Strip)

CABLE SIZING

[illegible]

Assignment – 6

CABLE TRAY

LT CABLES									
CABLE TRAY: FROM		LT-4		TO	LT-5				
Sr. No.	Cable Route (From-To)	Type & Cable Size	Size of Cable (mm2)	No. of Cable	Overall Diameter of each Cable (mm)	Sum of Cable OD (mm)	Self Weight of Cable (Kg/M t)	Total Weight of Cable (Kg/M t)	Remarks
1	LV MCC	4	16	1	21	21	3.95	1	
2	PU2315- VFD	4	16	1	21	21	0.37	1	
3	PU2315- VFD	5	1.5	1	15	15	3.95	0.4	
4	LV MCC	4	6	1	18	18	0.37	0.9	
5	LV MCC	5	1.5	1	15	15	3.95	0.4	
6	LV MCC	4	2.5	1	16	16	0.37	0.5	
7	PU 2314 -B- VFD	4	2.5	1	16	16	0.9	0.5	
8	PU 2314 -B- VFD	5	1.5	1	15	15	0.9	0.4	
9	LV MCC	4	16	1	21	21	2.9	1	
10	PU2305- VFD	4	16	1	21	21	1.2	1	
11	PU2305- VFD	5	1.5	1	15	15	1.2	0.4	
12	LV MCC	4	16	1	21	21	1.2	1	
13	LV MCC	5	1.5	1	15	15	1.45	0.4	
14	LV MCC	4	16	1	21	21	2	1	
15	LV MCC	5	1.5	1	15	15	2.4	0.4	
16	LV MCC	4	16	1	21	21	2.4	1	
17	BW2313- VFD	4	16	1	21	21	0.85	1	
18	BW2313- VFD	5	1.5	1	15	15	0.85	0.4	
19	LV MCC	4	6	1	18	18	0.85	0.9	
20	LV MCC	5	1.5	1	15	15	1	0.4	
21	LV MCC	4	6	1	18	18	0.85	0.9	
Total				21		374	33.91	14.9	
Calculation				Result					
Maximum Cable Diameter:				21	mm	Selected Cable Tray width:			
Consider Spare Capacity of Cable Tray:				30%		Selected Cable Tray Depth:			
Distance between each Cable:				0	mm	Selected Cable Tray Weight:			
Calculated Width of Cable Tray:				486	mm	Selected Cable Tray Size:			
Calculated Area of Cable Tray:					Sq.mm	O.K			
No of Layer of Cables in Cable Tray:						300 x 50			
Selected No of Cable Tray:					Nos.	1			
Selected Cable Tray Width:					mm	150.00			
Selected Cable Tray Depth:					mm	Ladder			
Selected Cable Tray Weight Capacity:					Kg/Meter				
Type of Cable Tray:				Ladder		Cable Tray Width Area Remaning			
Total Area of Cable Tray:				15000	Sq.mm	Cable Tray Area Remaning:			
						19%			
						32%			
</									

Assignment - 7

IEEE
Std 80-2000

IEEE GUIDE FOR SAFETY

Earthing calculations Input

Maximum line-to-ground fault in kA for 1 sec	2	
Earthing material (Earth rod & earth strip)	13	
Depth of earth flat burial in meter	G1	
Average depth / length of Earth rod in meters	0.5	
Soil resistivity Q-meter	4	
Ambient temperature in deg C	8.5	
Plot dimensions (earth grid) L x B in meters	50	
Number of earth rods in nos.	70	130
	6	

Earth electrode sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$$

α_r - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρ_r - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
I _{lg} - RMS fault current in kA = 50 KA	14
t _c - Short circuit current duration sec	1
Thermal capacity factor, TCAP J/(cm ³ .oC)	3.93
T _m - Maximum allowable temperature for copper conductor, in oC	419
K ₀ - Factor at oC	293

The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:

14 = Ac *	0.123
Ac - Required conductor cross section in sq.mm	114
Earth rod dia in mm	12
Earth rod dia (including 25% corrosion allowance) in mm	15

Earth flat sizing:

Ac - Required conductor cross section in sq.mm

$$I_{lg} = A_c \times \sqrt{\left[\frac{TCAP \times 10^{-4}}{t_c \times \alpha_r \times \rho_r} \right] \times \ln \left[\frac{K_0 + T_m}{K_0 + T_a} \right]}$$

α_r - Thermal co-efficient of resistivity, at 20 oC	0.0032
ρ_r - Resistivity of ground conductor at 20 oC	20.10
Ta - Ambient Temperature is °C	50
I _{lg} - RMS fault current in kA = 50 KA	14
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Thermal capacity factor, TCAP J/(cm ³ .oC)	3.93
T _m - Maximum allowable temperature for copper conductor, in oC	419
K ₀ - Factor at oC	293

The data taken from IEEE 80-2000, Clause 11.3, Table-1 for clad steel rod:

14 = Ac *	0.123
Ac - Required conductor cross section in sq.mm	114
Earth flat area in mm	12
Earth flat area (including 25% corrosion allowance) in mm	15
Selected flat size W * Thk in sq mm	20

Table 1—Material constants

Description	Material conductivity (%)	α_r factor at 20 °C (1/°C)	K_0 at 0 °C (0 °C)	Fusing* temperature T_m (°C)	ρ_r , 20 °C ($\mu\Omega\cdot\text{cm}$)	TCAP thermal capacity ($\text{J}/(\text{cm}^3\cdot\text{C})$)
Copper, annealed soft-drawn	100.0	0.00393	234	1083	1.72	3.42
Copper, commercial hard-drawn	97.0	0.00381	242	1084	1.78	3.42
Copper-clad steel wire	40.0	0.00378	245	1084	4.40	3.85
Copper-clad steel wire	30.0	0.00378	245	1084	5.86	3.85
Copper-clad steel rod ^b	20.0	0.00378	245	1084	8.62	3.85
Aluminum, EC grade	61.0	0.00403	228	657	2.86	2.56
Aluminum, 5005 alloy	53.5	0.00353	263	652	3.22	2.60
Aluminum, 6201 alloy	52.5	0.00347	268	654	3.28	2.60
Aluminum-clad steel wire	20.3	0.00360	258	657	8.48	3.58
Steel, 1020	10.8	0.00160	605	1510	15.90	3.28
Stainless-clad steel rod ^c	9.8	0.00160	605	1400	17.50	4.44
Zinc-coated steel rod	8.6	0.00320	293	419	20.10	3.93
Stainless steel, 304	2.4	0.00130	749	1400	72.00	4.03

*From ASTM standards.

^bCopper-clad steel rods based on 0.254 mm (0.010 in) copper thickness.

^cStainless-clad steel rod based on 0.508 mm (0.020 in) No. 304 stainless steel thickness over No. 1020 steel core.