

MAE 259B Group 2 Progress Report

Siyuan Chen, Xiangzhou Kong, Long Chen

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What we did - Starting point

Start from the homework code

Adapted from the MATLAB sample code, translated into Python, with minor changes and optimizations.

Build utilities

Command line interface, 3D visualization tool, code snapshot tool, etc..



hw-render.mp4



hw-nodes.mp4

Not all PDF viewers can play videos. If not playable here, the videos can be found at
<https://github.com/kmxz/mae259b-project/tree/master/mid-presentation/video>.

What we did - Performance optimization

Profiling shows 90% of time is spent on calculating F and J .

```
def gradEbAndHessEb(xkml, ykml, xk, yk, xkpl, ykpl, φk0):
```

```
    itm1 = 2 * tan(0.5 * φk0)
    itm2 = ((-xk + xkpl) * (xk - xkml) + (-yk + ykpl) * (yk - ykml))
    itm3 = ((-xk + xkpl) * (yk - ykml) - (xk - xkml) * (-yk + ykpl))
    itm4 = itm3 / itm2 ** 2
    itm5 = tan(0.5 * atan(itm3 / itm2))
    itm6 = (1 + itm3 ** 2 / itm2 ** 2)
    itm7 = ((ykml - ykpl) / itm2 + itm3 * (2 * xk - xkml - xkpl) / itm2 ** 2)
    itm8 = ((-xkml + xkpl) / itm2 + itm3 * (2 * yk - ykml - ykpl) / itm2 ** 2)
    itm9 = ((-xk + xkml) / itm2 + (-yk + ykml) * itm4)
    itm10 = ((-xk + xkml) * itm4 + (yk - ykml) / itm2)
    itm11 = (-itm1 + 2 * itm5) * (itm5 ** 2 + 1) * itm5 / itm6 ** 2
    itm12 = (-itm1 + 2 * itm5) * (itm5 ** 2 + 1) / itm6
    itm13 = itm12 / itm6
    itm14 = itm3 ** 2 / itm2 ** 3
```

```
F = np.empty(6)
```

```
F[0] = 2 * ((-xk + xkpl) * itm4 + (-yk + ykpl) / itm2) * itm12
F[1] = 2 * ((xk - xkpl) / itm2 + (-yk + ykpl) * itm4) * itm12
F[2] = 2 * itm7 * itm12
F[3] = 2 * itm8 * itm12
F[4] = 2 * itm10 * itm12
F[5] = 2 * itm9 * itm12
```

```
Jl1 = 2 * ((-2 * xk + 2 * xkpl) * (-xk + xkpl) * itm3 / itm2 ** 3 + 2 * (-xk + xkpl) * (-yk + ykpl) / itm2 ** 2) * itm12 + 2 * ((-2 * xk + 2 * xkpl) * itm14 - (-2 * yk + 2 * ykpl) * itm4) * ((-xk + xkpl) * itm4 + (-yk + ykpl) / itm2) * itm13 + 2 * ((-xk + xkpl) * itm4 + (-yk + ykpl) / itm2) ** 2 * itm11 + 2 * ((-xk + xkpl) * itm4 + (-yk + ykpl) / itm2) ** 2 * (itm5 ** 2 + 1) ** 2 / itm6 ** 2
```

```
Jl2 = 2 * (-itm1 + 2 * itm5) * (itm5 ** 2 + 1) * ((-xk + xkpl) * (xk - xkpl) / itm2 ** 2 + (-xk + xkpl) * (-2 * yk + 2 * ykpl) * itm3 / itm2 ** 3 + (-yk + ykpl) ** 2 / itm2 ** 2) / itm6 + 2 * ((xk - xkpl) / itm2 + (-yk + ykpl) * itm4) * ((-xk + xkpl) * itm4 + (-yk + ykpl) / itm2) * itm11 + 2 * ((xk - xkpl) / itm2 + (-yk + ykpl) * itm4) * ((-xk + xkpl) * itm4 + (-yk + ykpl) / itm2) * (itm5 ** 2 + 1) ** 2 / itm6 ** 2 + 2 * ((-xk + xkpl) * itm4 + (-yk + ykpl) / itm2) * (-2 * xk - 2 * xkpl) * itm4 - (-2 * yk + 2 * ykpl) * itm14) * itm13
```

```
Jl3 = 2 * (-itm1 + 2 * itm5) * (itm5 ** 2 + 1) * ((-xk + xkpl) * (ykml - ykpl) / itm2 ** 2 + (-xk + xkpl) * itm3 * (4 * xk - 2 * xkml - 2 * xkpl) / itm2 ** 3 + (-yk + ykpl) * (2 * xk - xkml - xkpl) / itm2 ** 2 - itm4) / itm6 + 2 * itm7 * ((-xk + xkpl) * itm4 + (-yk + ykpl) / itm2) *
```

30.6 s



7.6 s

4× faster

What we did - Natural curvature

When calculating bending energy, replace $\frac{1}{2}EI(\phi_k)^2$ with $\frac{1}{2}EI(\phi_k - \phi_{k0})^2$.

The formulas for calculating F and J need to be changed (do differentiation again).

To verify the result:

- Expect same result as previous code when $\phi_0 = 0$;
- Expect a straight beam to recover natural curvature when no external force applied.

```
from sympy import symbols, diff, tan, atan

def  $\phi_k(x_{km}, x_k, x_{kp}, y_{km}, y_k, y_{kp})$ :
    return atan(((xkp - xk) * (yk - ykm)
    - (xk - xkm) * (ykp - yk)) / ((xkp -
    xk) * (xk - xkm) + (ykp - yk) * (yk -
    ykm)))

def Eb( $x_{km}, x_k, x_{kp}, y_{km}, y_k, y_{kp}, \phi_{k0}$ ):
    return (2 * tan( $\phi_k(x_{km}, x_k, x_{kp}, y_{km}, y_k, y_{kp})$  / 2.0) - 2 * tan( $\phi_{k0}$  /
    2.0)) ** 2

xkm, xk, xkp, ykm, yk, ykp,  $\phi_{k0}$  =
    symbols('xkm1 xk xkp1 ykm1 yk ykp1  $\phi_{k0}$ 1')

Eb = Eb( $x_{km}, x_k, x_{kp}, y_{km}, y_k, y_{kp}, \phi_{k0}$ )

F1 = diff(Eb, xkm)
F2 = diff(Eb, ykm)
F3 = diff(Eb, xk)
F4 = diff(Eb, yk)
F5 = diff(Eb, xkp)
F6 = diff(Eb, ykp)

J11 = diff(F1, xkm)
J12 = diff(F1, ykm)
J13 = diff(F1, xk)
J14 = diff(F1, yk)
J15 = diff(F1, xkp)
```

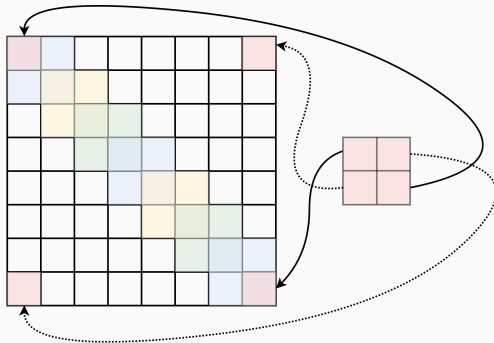
What we did - Circular structure

Instead of $nv - 1$ edges, we have nv edges.

For bending, instead of $nv - 2$ components, we have nv components.

For stretching, instead of $nv - 1$ components, we have nv components.


When assembling the Jacobians, new components added to connect two ends together:



What we did - Circular structure

Verify our code by running the “hanging circle”:

$$\gamma = 10^6 \text{ Pa}$$

 1e6.mp4

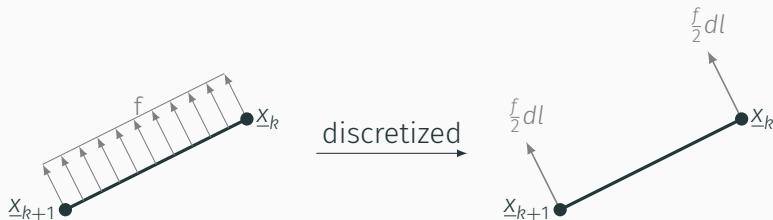
$$\gamma = 10^7 \text{ Pa}$$

 1e7.mp4

$$\gamma = 10^8 \text{ Pa}$$

 1e8.mp4

What we did - Inflation pressure



With \underline{x}_k and \underline{x}_{k+1} , we can easily calculate force exerted on those two points.

As force is dependent on actual positions of nodes, we need to add the variation into the Jacobian matrix. We simply take derivatives on the forces.

What we did - Surface contact

Predictor-corrector method is used.

Assume a surface at $y = 0$, When doing time-marching, on each time step :

1. Compute $\underline{q}(t)$ as before;
2. Check if there exists any node whose $y < 0$. If there is any, set it as a temporarily constrained DOF with $y = 0$, and recompute current frame;
3. Check if there exists any temporarily constrained DOF, such that the normal *force* between the surface and the node is negative. Remove such temporary constraint, and recompute current frame.

```
Fb, Jb = getFb(qCurrentIterate, EI, nv, voronoiRefLen, -2 * pi / nv, isCircular=True)
Fs, Js = getFs(qCurrentIterate, EA, nv, refLen, isCircular=True)
Fg = m * garr
Fp, Jp = getFp(qCurrentIterate, nv, refLen, InflationPressure)

Forces = Fb + Fs + Fg + Fp

# Equation of motion
f = m * (qCurrentIterate - q0) / dt ** 2 - m * u / dt - Forces
fUncons = dofHelper.unconstrained_v(f)
```


What we did - Surface contact

In each frame:

```
qNew, reactionForces = objfun(q0)

# inspect reactionForces to see if any one is negative, which should be UNCONSTRAINED
needToFree = [unconsInd for unconsInd in dofHelper._constrained if (reactionForces[
unconsInd] < 0)]
if needToFree:
    dofHelper.unconstraint(needToFree)
    print('Contact condition updated. Remove constraints and recompute')
    qNew, reactionForces = objfun(q0)

# inspect qNew to see if any one falls below ground, which should be CONSTRAINED
while True:
    q0Effective = None
    for c in range(nv):
        index = 2 * c + 1
        if qNew[index] < 0: # y < 0: bad!
            if q0Effective is None:
                q0Effective = q0.copy()
                q0Effective[index] = 0
                dofHelper.constraint([index])
            if q0Effective is None:
                break
    else:
        print('Contact condition violated. Add constraints and recompute')
        qNew, reactionForces = objfun(q0Effective)
```

Objective completed!

Low pressure

 l-pressure.mp4

High pressure

 h-pressure.mp4

What we did - Damping

Without damping, we have oscillations.

Naïve damping $\underline{F}_{d,k} \propto -\underline{v}_k$ ruins bulk motion (as our bulk velocity is high)

So we use velocity relative to center of mass:

$$\underline{F}_{d,k} \propto -(\underline{v}_k - \underline{v}_{cm})$$

No damping

 no-damp.mp4


Naïve damping

 bad-damp.mp4

CM-Relative damping

 good-damp.mp4

Problem: Shape Jitter

 `jitter.mp4` `jitter-slow.mp4`

- Step size too large, everything bashed to ground before reacting
- No self-intersection detection

Problem: Shape Jitter - Observations

Damping does not really help.

Reducing time-step size helps. For the previous setup:

$$dt = 4 \times 10^{-4} \text{ s}$$

 4e-4.mp4

$$dt = 2.5 \times 10^{-4} \text{ s}$$

 2.5e-4.mp4

Compared to initial time step size $5 \times 10^{-3} \text{ s}$. This takes $20\times$ more computational time! Almost unacceptable.

Adaptive Time Stepping

“Adaptive Time Stepping” in the assigned reading gave us some inspiration.

When the time step is found too large by some criteria. We reduce the step size and try again. When appropriate, step size is increased again.

Δv -based adaptive time stepping

They use a Δx threshold as criteria for deciding time steps. As our bulk velocity is high, we use the Δv threshold instead.

Not very effective: Only saves 20% steps. The oscillation also gives rapidly changing local velocity, we cannot distinguish the “bashing”.

Contact-based adaptive time stepping

Use small step when in contact with the surface. Otherwise use large step.

Not very effective: Not flexible enough (only two step sizes); step size is small even when resting on the surface.

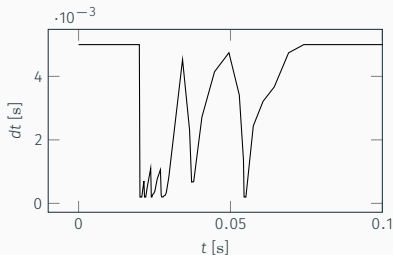
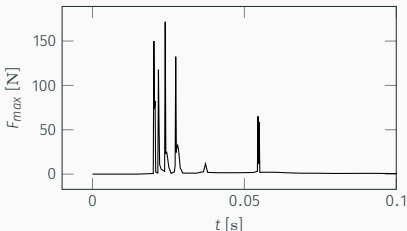
Adaptive Time Stepping

Reaction force-based adaptive time stepping

Step size should be inverse proportional to the maximum nodal reaction force from the ground.

We use $F_{max}dt \leq 0.008 \text{ N} \cdot \text{s}$ as the threshold for previous setup.

Instead of “decreasing by half, increasing by doubling” (as used in the paper), we examine $\frac{F_{max}dt}{0.008 \text{ N} \cdot \text{s}}$ to decide how much we should increase/decrease.



Adaptive Time Stepping

For a 2 s simulation, only 487 steps attempted, resulting in 437 valid steps.

Compared to 400 steps (uniform dt which results in shape jitter), we only need $\sim 20\%$ more steps, instead of $\sim 2000\%$.

Project on GitHub now!

All code, results (and these slides) uploaded to

<https://github.com/kmxz/mae259b-project>

