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## Midterm 2

1. a)

$$\frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{G^*} - V_{Tn})^2 = \frac{1}{2} \mu_p C_{ox} \frac{W}{L} (V_{DD} - V_{G^*} - V_{Tp})^2$$

$$V_{G^*} - 0.3 = 0.9 - V_{G^*} - 0.4$$

$$\boxed{V_{G^*} = 0.4 V}$$

b)  $g_{m_n} = \mu_n C_{ox} \frac{W}{L} (V_{G^*} - V_{Tn})$

$$= 0.5 \times 200 \times 0.1 \text{ mS}$$

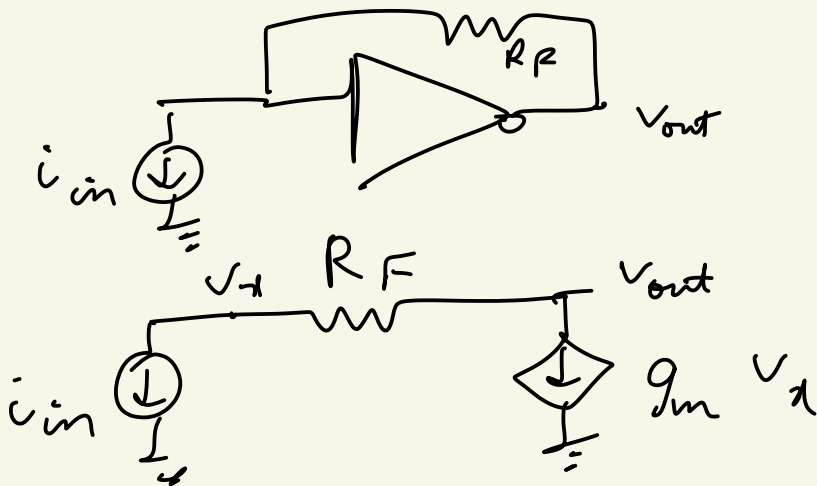
$$= 10 \text{ mS}$$

$$g_{m_p} = \mu_p C_{ox} \frac{W}{L} (V_{DD} - V_{G^*} - V_{Tp})$$

$$= 0.4 \times 250 \times 0.1 \text{ mS}$$

$$= 10 \text{ mS}$$

$$g_m = g_{m_n} + g_{m_p} = 20 \text{ mS}$$



$$v_d = -\frac{i_{in}}{g_m}$$

$$\begin{aligned} V_{out} &= v_d + i_{in} R_F \\ &= -\frac{i_{in}}{g_m} + i_{in} R_F \end{aligned}$$

$$\frac{V_{out}}{i_{in}} = R_F - \frac{1}{g_m}$$

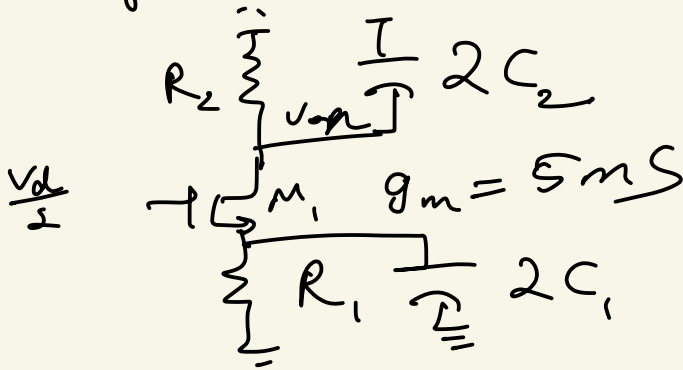
$$R_F = 1.05k\Omega$$

$$g_m = 20mS \quad \frac{1}{g_m} = 50\Omega$$

$$\boxed{\frac{V_{out}}{i_{in}} = 1k\Omega}$$

$$c) \frac{v_{out}}{i_{in}} = 0 \Rightarrow R_F = \frac{1}{g_m} = \boxed{50 \Omega}$$

2. a) DM Half-ckt.

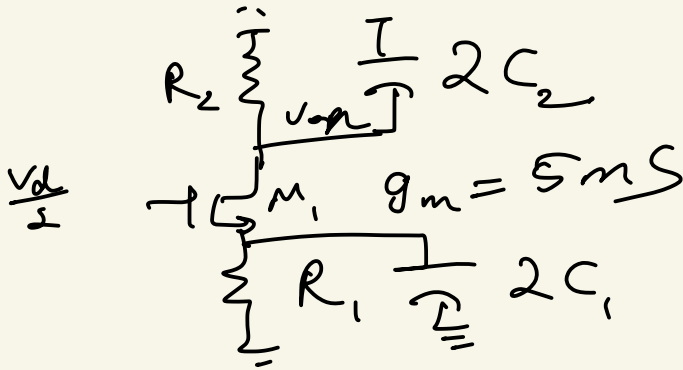


$$v_{on} = - \frac{g_m R_2}{1 + g_m R_1} \cdot \frac{v_d}{2}$$

$$v_{op} = \frac{+g_m R_2}{1 + g_m R_1} \cdot \frac{v_d}{2}$$

$$\begin{aligned} \frac{v_{op} - v_{on}}{v_d} &= \frac{g_m R_2}{1 + g_m R_1} \\ &= \frac{5 \times 0.5}{5} = \boxed{0.5} \end{aligned}$$

b)



$$\frac{V_{op}}{\frac{V_d}{2}} = - \frac{g_m R_2}{1 + g_m R_1} \cdot \frac{1 + s(2R_1 C_1)}{1 + s \left( \frac{R_1 C_1}{1 + g_m R_1} \right)^{1 + s(2C_1 R_1)}} \cdot 1$$

$$\frac{V_{op}}{\frac{V_d}{2}} = + \frac{g_m R_2}{1 + g_m R_1} \cdot \frac{1 + s(2R_1 C_1)}{1 + s \left( \frac{R_1 C_1}{1 + g_m R_1} \right)^{1 + s(2C_1 R_1)}} \cdot 1$$

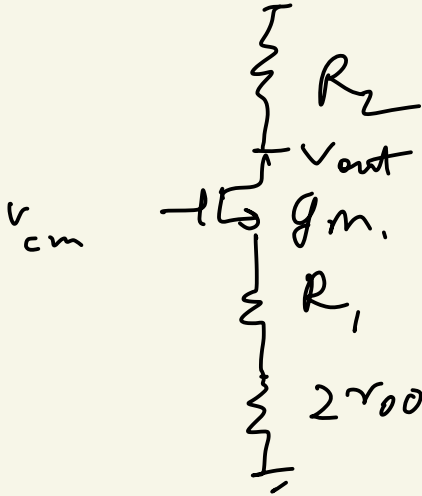
$$\frac{V_{op} - V_{on}}{V_d} = \frac{g_m R_2}{1 + g_m R_1} \cdot \frac{1 + s(2R_1 C_1)}{\left( \frac{1 + s(2R_1 C_1)}{1 + g_m R_1} \right) \left( \frac{1}{1 + s(2C_1 R_1)} \right)}$$

2 poles, 1 zero

Zero at 1.25 GHz

Poles at 6.25 GHz, 50 GHz

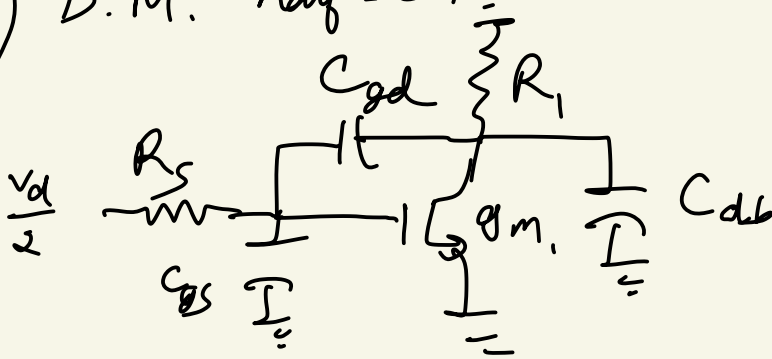
c) CM. half-circuit,



$$\frac{v_{op}}{v_{cm}} = \frac{v_{out}}{v_{cm}}$$

$$= \frac{-g_m R_2}{1 + g_m(R_1 + 2r_{oo})}$$

3. a) D.M. half-circuit



Exact transfer fn.

$$\frac{v_{o1}}{\frac{v_d}{2}} = \frac{-g_{m1} R \left( 1 - s \frac{C_{gd}}{g_{m1}} \right)}{1 + s \left[ R_S \left[ C_{gs} + C_{gd} (1 + g_{m1} R_L) \right] + R_L [C_{db} + C_{gd}] \right] + s^2 R_S R_L [C_{gs} C_{gd} + C_{gd} C_{db} + C_{gs} C_{db}]}$$

$$\approx \frac{-g_{m1} R \left( 1 - s \frac{C_{gd}}{g_{m1}} \right)}{1 + s \left[ R_S \left[ C_{gs} + C_{gd} (1 + g_{m1} R_L) \right] + R_L [C_{db} + C_{gd}] \right]}$$

3-dB BW

$$g_m R_1 = 9$$

$$\approx \frac{1}{2\pi R_s [C_{gs} + C_{gd}(1 + g_m R_1)] + R_1 [C_{gd} + C_{db}]}$$

$$+ R_1 [C_{gd} + C_{db}]$$

$$= \frac{1}{2\pi \times 2 \text{ k}\Omega [200 \text{ fF} + 200 \text{ fF} \times 10] + 200 \times [200 \text{ fF} + 200 \text{ fF}]}$$

$$= 205 \text{ MHz}$$

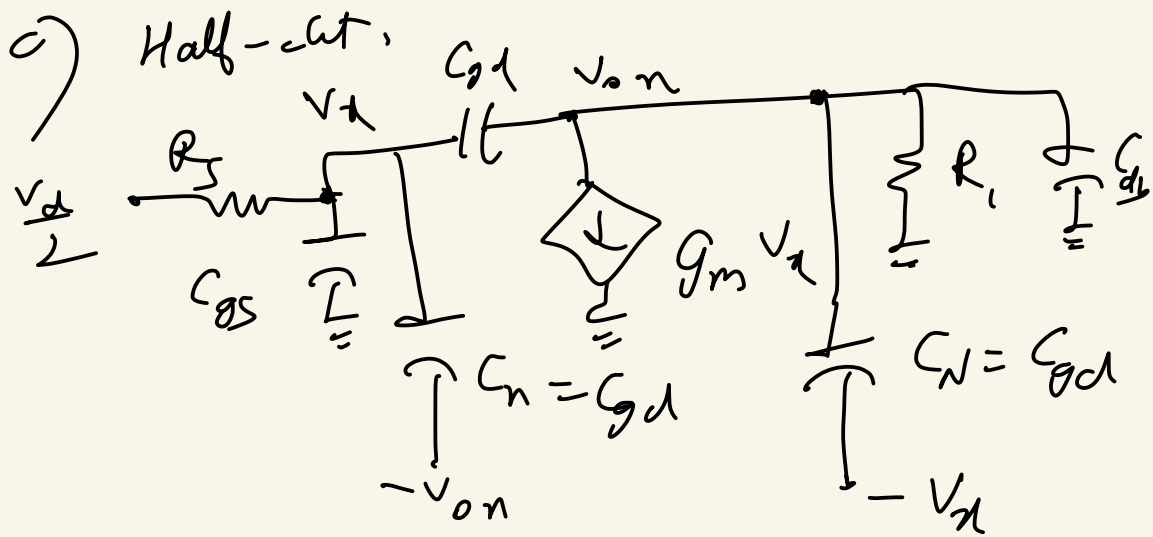
b) zero frequency =,  $g_m$ .

$$2\pi \cdot C_{gd}$$

$$= \frac{45 \text{ nS}}{200 \text{ fF}}$$

$$= 225 \text{ GHz}$$





To find zero freq.,  
consider current from  $v_{on}$   
which depends on  $v_d$ .

$$g_m v_d + (v_{on} - v_d) \cdot s C_{GD} + (v_{on} + v_d) \cdot s C_N$$

$C_N = C_{GD}$

$$= g_m v_d + 2 v_{on} \cdot s C_{GD}$$

$\Rightarrow$  No freq. at which  
current = 0

$\Rightarrow$  No zero

d) Time constant for node  $v_1$

$$\begin{aligned} & R_s \left[ C_{gs} + C_{gd} \left( 1 + g_m R_L \right) \right. \\ & \quad \left. + C_N \left( 1 - g_m R_L \right) \right] \\ &= R_s [C_{gs} + C_{gd} + C_{gd}] \\ &= R_s [C_{gs} + 2C_{gd}] \end{aligned}$$

Time constant for node  $v_{on}$

$$\begin{aligned} &= R_1 \left[ C_{db} + C_{gd} \left( 1 + \frac{1}{g_m R_L} \right) \right. \\ & \quad \left. + C_N \left( 1 - \frac{1}{g_m R_L} \right) \right] \\ &= R_1 [C_{db} + 2C_{gd}] \end{aligned}$$

3-dB BW

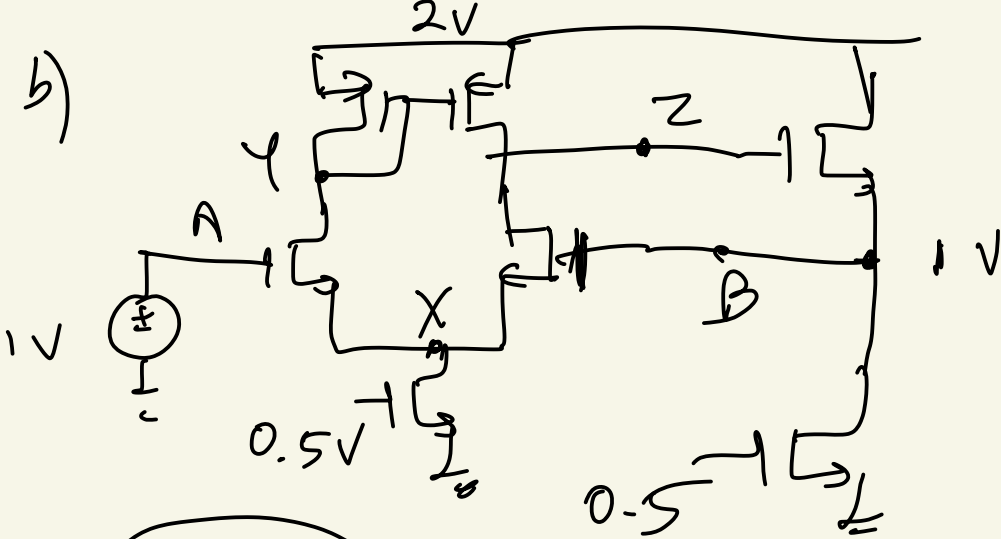
$$\begin{aligned} &\approx \frac{1}{2\pi \left[ R_s [C_{gs} + 2C_{gd}] \right.} \\ & \quad \left. + R_1 [C_{db} + 2C_{gd}] \right] \\ &= \underline{581 \text{ MHz}} \end{aligned}$$

You can actually show that  
full transfer functions

$$\frac{V_{op} - V_{on}}{V_d}(s) = \frac{-g_m R_1}{\left(1 + s R_s [C_{gs} + 2C_{gd}]\right) \left(1 + s R_1 [C_{d2} + 2C_{gd}]\right)}$$

4. a) Terminal B for  
negative feedback

b)



$A = 1V$   
 $B = 1V$  (by negative feedback)

$$Y = V_{DD} - V_{T_p} - \Delta V$$

$$I_0 = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{G_s} - V_{T_n})^2$$

$$= 200 \mu A$$

$$I_3 = \frac{1}{2} \times I_0 = 100 \mu A$$

$$\Rightarrow \Delta V_s = 0.2V$$

$$Y = 2 - 0.4 - 0.2$$

$$Y = 1.4V$$

$$V_{GS_1} = V_{GS_2} = V_1 + \Delta V \big|_{100\mu A}$$

$$\approx 0.3 + 0.2$$

$$\approx 0.5 V$$

$$V_A = V_B = 1 V$$

$$X = 1 V - 0.5 V$$

$$X \approx 0.5 V$$

$$\textcircled{2} \quad V_{GS_6} = \Delta V \big|_{100\mu A, \left(\frac{40}{1}\right)} + V_{T_n}$$

$$= 0.1 V + 0.3 V$$

$$= 0.4 V$$

$$V_{S_6} = V_B = 1 V$$

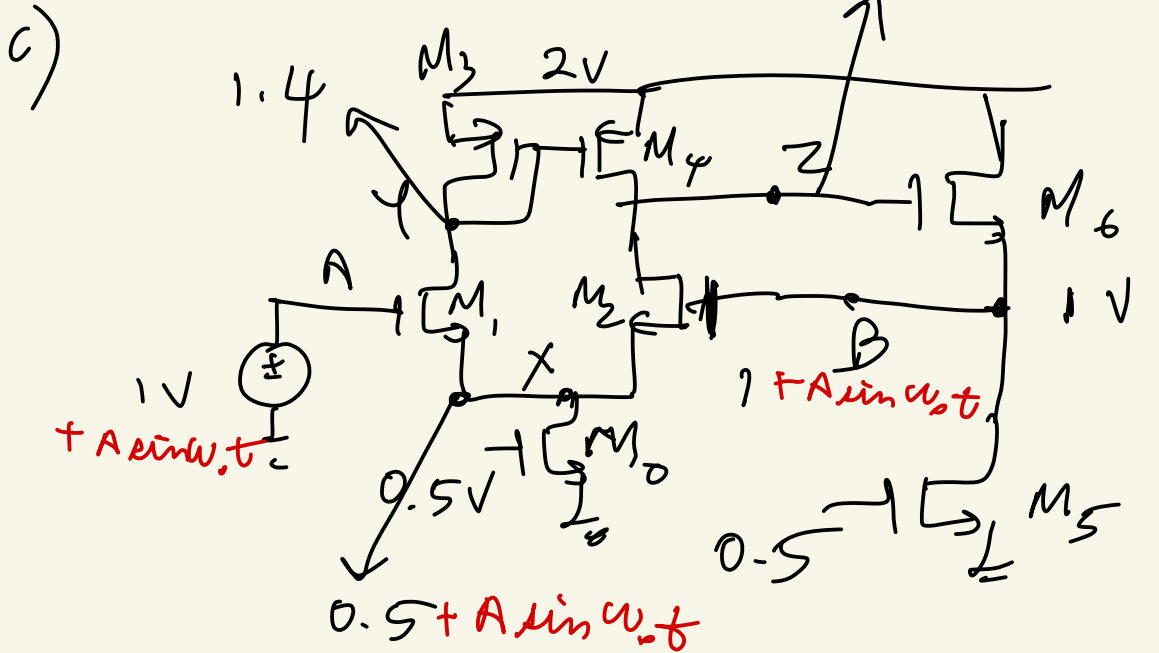
$$V_{G_6} = 1.4 V$$

$$Z = 1.4 V$$

$$\begin{aligned} A, B &= 1V \\ Y, Z &= 1.4V \\ X &= 0.5V \end{aligned}$$

$$\begin{aligned} A, B &= 1V \\ Y, Z &= 1.4V \\ X &= 0.5V \end{aligned}$$

$$\begin{aligned} A, B &= 1V \\ Y, Z &= 1.4V \\ X &= 0.5V \end{aligned}$$



$M_2$  can't get into triode  
(drain & gate swing by same amount)

M<sub>1</sub>

$$V_{G, \max} \approx 1 + A$$

$$V_{G, \max} \approx 1 + A$$

$$V_D = V_{G, \max} - V_T$$

$$A.4 = 1 + A - 0.3$$

$$A = 0.7 \checkmark$$

M0

$$V_{D, \min} = 0.5 - A$$

$$V_G = 0.5$$

$$V_{D, \min} = V_G - V_T$$

$$0.5 - A = 0.5 - 0.3$$

$$A_{\max} = 0.3V$$

M3

never gets to triode

M4

$$V_G = 1.4V$$

$$V_{D, \max} = 1.4 + A$$

$$V_{D, \max} = V_G + V_{T1}$$

$$1.4 + A = 1.4 + 0.4$$

$$A_{\max} = 0.4V$$

M5

$$V_{D, \min} = 1 - A$$

$$V_G = 0.5V$$

$$V_{D, \min} = V_G - V_T$$

$$1 - A = 0.5 - 0.3$$

$$A = 0.8V$$

M6

$$V_{G, \max} = 1.4 + A$$

$$V_D = 2V$$

$$A_{\max} = 0.9V$$

$$A_{max} = 0.3V$$

$M_0$  in cut-off

d)

$$A(s) = \frac{A_0}{1 + \frac{s}{\omega_0}}$$

$$A_0 = g_{m1} (r_{o2} || r_{o4})$$

$$\omega_0 = \frac{1}{(r_{o2} || r_{o4}) \cdot C_L}$$

In unity gain feedback,  
the CLF has a 3-dB BW

of  $A_0 \omega_0$

$$\begin{aligned} \frac{1}{2\pi} \frac{g_{m1}}{C_L} &= \frac{1}{2\pi} \frac{1 \text{ mS}}{\frac{1}{2\pi} \text{ pF}} \\ &= \boxed{1 \text{ kHz}} \end{aligned}$$