# **Section 1 General Information**

### 1.1 Unit Conversions

**Prefix Multipliers** 

Angles

Angular Acceleration

Angular Velocity

Area

Density

**Electrical Quantities** 

Energy / Work

Force

Illumination

Inertia

Length

Linear Acceleration

Mass

Power

Pressure

Temperature

Time

Torque

Velocity

Viscosity

Volume

- 1.2 Greek Alphabet
- 1.3 Greek Symbols used for Aircraft
- 1.4 Common Subscripts
- 1.5 Common Abbreviations
- 1.6 Sign Conventions
- 1.7 Thermodynamic Relations
- 1.8 Mechanics Relations

### 1.1 Unit Conversions

(references 1.1, 1.2)

Prefix Multipliers				
	$10^{18}$	exa	E	
	$10^{15}$	peta	P	
	$10^{12}$	tera	T	
	$10^{9}$	giga	G	
	$10^{6}$	mega	M	

 $\begin{array}{ccc} 10^3 & kilo & k \\ 10^2 & hecto & h \\ 10 & deka & da \end{array}$ 

10<sup>-1</sup> deci d 10<sup>-2</sup> centi c 10<sup>-3</sup> milli m

 $10^{-6}$  micro  $\mu$   $10^{-9}$  nano n

<u>Multiply</u> <u>by</u> <u>To Obtain</u>

### (Common FTE conversions in boldface)

	(00		
Angles circl	circles	1	circumferences
	circles	12	signs
	circles	21,600	minutes
	circles	$2\pi$	radians
		2.60	

circles 360 degrees quadrants degrees .01111 degrees 3600 seconds degrees 60 minutes mils (Army) .05625 degrees degrees mils (Navy) .05729 quadrants 90 degrees degrees radians 57.2958 revolutions 360 degrees  $4\pi$ steradians# sphere

#solid angle measurement

 $\begin{array}{lll} \textbf{Angular} & \text{rev/min}^2 & 0.001745 & \text{rad/sec}^2 \\ \textbf{Acceleration} & & & \end{array}$ 

Angular cycles/sec 6.2814 rads/sec Velocity rads/sec 0.1592 rev/sec (cycles/sec)

 rads/sec
 9.549
 rpm

 rad/sec
 57.296
 deg/sec

 rpm
 0.01667
 rev/sec

	<u>Multiply</u>	<u>by</u>	<u>To Obtain</u>
Area	acres	43,560	$\mathrm{ft}^2$
	ares	100	$m^2$
	barn	$10^{-28}$	$m^2$
	centares	1	$m^2$
	circular mils	$7.854 \times 10^{-7}$	$in^2$
	cm <sup>2</sup>	100	$mm^2$
	$\mathbf{ft}^2$	144	in <sup>2</sup>
	$ft^2$	0.09290304	$m^2$
	$in^2$	6.452	$cm^2$
	$in^2$	$10^{6}$	$mils^2$
	$m^2$	10.76	$ft^2$
	section	2,589,988.1	$m^2$
	st. mile <sup>2</sup>	27,780,000	$ft^2$
	st. mile <sup>2</sup>	2.590	$km^2$
	township	93,239,572	$m^2$
	$yd^2$	9	$ft^2$
	$yd^2$	0.8361	$m^2$
Density	grams/cm <sup>3</sup>	0.03613	pounds/in <sup>3</sup> *
	grams/cm <sup>3</sup>	62.43	pounds/ft <sup>3</sup> *
	kg/m <sup>3</sup>	16.018463	pounds/ft <sup>3</sup> *
	slugs/ft <sup>3</sup>	515.4	kg/m <sup>3</sup>
	pounds/in <sup>3</sup> *	1728	pounds/ft <sup>3</sup> *
	slugs/ft <sup>3</sup>	1.94	grams/cm <sup>3</sup>

<sup>\*</sup> conversion from kg mass to kg force assumes  $g = 32.174 \text{ ft/s}^2$ 

Electrical	amperes	0.1	abamperes
Quantities	amperes	$1.0365 \times 10^{-5}$	faradays/sec
	amperes	$2.998 \times 10^9$	statamperes
	amperes.cicmil	$1.973 \times 10^5$	amperes/cm <sup>2</sup>
	ampere-hours	3,600	coulombs
	ampere-hours	$1.079 \times 10^{13}$	statcoulombs
	ampere turn/cm	1.257	gilberts/cm
	ampere turn/cm	1.257	oersteds
	coulombs	0.1	abcoulombs
	coulombs	$6.243 \times 10^{18}$	electronic charges
	coulombs	$1.037 \times 10^{-5}$	faradays
	coulombs	$2.998 \times 10^9$	statcoulombs
	faradays	26.8	apmere-hours
	farads	10-9	abfarads
	farads	$10^{6}$	microfarads
	farads	$8.986 \times 10^{11}$	statfarads
	gausses	1	maxwells/cm <sup>2</sup>

	<u>Multiply</u>	<u>by</u>	<u>To Obtain</u>
Electrical Quantities Cont.	gausses gilberts henries henries maxwells oersteds ohms ohms ohm-cm volts	6.452 0.7958 10 <sup>9</sup> 1.113x10 <sup>-12</sup> 1 2.998x10 <sup>10</sup> 10 <sup>9</sup> 1.113x10 <sup>12</sup> 6.015x10 <sup>6</sup> 10 <sup>8</sup> 0.003336	lines/in <sup>2</sup> ampere turns abhenries stathenries lines statoersteds abohms statohms circ mil-ohms/ft abvolts statvolts
Energy / Work	Btu Btu Btu Btu Btu Btu calories calories electron volt ergs ergs foot-pounds foot-pounds hp-hours hp-hours Joules Joules Joules Joules Willowatt-hours thermies watt-second	1.055x10 <sup>10</sup> 1055.1 2.9302x10 <sup>-4</sup> 251.99 778.03 4.1868 3.088 1.519x10 <sup>-22</sup> 1 7.376x10 <sup>8</sup> 1.3558 3.766x10 <sup>-7</sup> 5.051x10 <sup>-7</sup> 0.7457 2546.1 0.23889 1 1 10 <sup>7</sup> 3.6x10 <sup>6</sup> 4.1868x10 <sup>6</sup> 0.73756	ergs Joules (N-m) kilowatt-hours calories (gram) foot-pounds watt-seconds foot-pounds Btu dyne-centimeters foot-pounds Joules (N-m) kilowatt-hours horsepower-hours kilowatt-hours Btu calories Newton-meters watt-seconds ergs Joules Joules foot-pounds
Force	dynes kilogram force kilopond force kip Newtons Newtons ounce ounces (troy)	3.597x10 <sup>-5</sup> <b>9.80665</b> 9.80665 4,448.221 <b>0.224808931</b> 100,000 20 480	ounces Newtons Newtons Newtons pounds dynes pennyweights grains

	<u>Multiply</u>	<u>by</u>	<u>To Obtain</u>
Force	pennyweights	24	grains
Cont.	pound	12	ounces
	pounds	32.174	poundals
	pounds	4.4482216	Newtons
	pounds	5760	grains
	quintals (long)	112	pounds
	quintals (met.)	100	kilograms
	stones	14	pounds
	tons (long)	2,240	pounds
	tons (metric)*	1.102	tons (short)
	tons (short)	2000	pounds
Fuel	gal	5.8	lbs (U.S. AV gas)
	gal	7.5	lbs (U.S. oil)
	Liter (jet A)	0.812	kilograms
	Liter (jet A)	1.794	pounds

## Note: Fuel densities are temperature dependent

Illumination	candles	1	lumens/steradian
	candles/cm <sup>2</sup>	π	lamberts
	candlepower	12.566	lumens
	foot-candles	1	lumens/ft <sup>2</sup>
	foot-candles	10.764	lux
	foot-lamberts	1	lumen/ft <sup>2</sup>
	lamberts	295.72	candles/ft <sup>2</sup>
	lamberts	929.03	lumens/ft <sup>2</sup>
	lumens	0.001496	watts
	lumens/in <sup>2</sup>	1	fots
	lumens/m <sup>2</sup>	1	lux
	lux	1	meter-candles
	lux	0.0001	fots
	meter-candles	1	lumens/m <sup>2</sup>
	millilamberts	0.2957	candles/ft <sup>2</sup>
	millilamberts	0.929	foot-lamberts
	milliphots	0.929	foot-candles
	milliphots	0.929	lumens/ft <sup>2</sup>
	milliphots	10	meter-candles

	<u>Multiply</u>	<u>by</u>	To Obtain
Length	angstroms	10 <sup>-10</sup>	meters
8	•	$1.496 \times 10^{11}$	meters
	cable lengths	120	fathoms
	caliber	0.01	inches
	cubit	0.4572	meters
	fermi	$10^{-15}$	meters
	fathoms	6	feet
	feet	12	inches
	furlongs	40	rods
	hands	4	inches
	inches	2.54	cm
	kilometers	3281	feet
	kilometers	0.53996	nautical miles
	leagues (U.S.)	3	nautical miles
	light years	$5.88 \times 10^{12}$	statute miles
	links (engnr's)	12	inches
	links (srvyr's)	7.92	inches
	meters	3.28084	feet
	meters	39.370079	inches
	microns	$0.1^{6}$	meters
	mils	0.001	inches
	nautical miles	1.15078	statute miles
	nautical miles	1,852	meters
	nautical miles	6,076.115486	feet
	paces	0.762	meters
	parsec	$1.9163 \times 10^{13}$	statute miles
	perch	5.0292	meters
	pica (printers)	0.0042175176	meters
	point (printers)	0.0003514598	meters
	pole (=rod)	5.0292	meters
	skein	109.728	meters
	statute miles	5,280	feet
	statute miles	1.609344	kilometers
	statute miles	8	furlongs
	yards	3	feet

	<u>Multiply</u>	<u>by</u>	<u>To Obtain</u>
Linear	feet/sec <sup>2</sup>	1.09728	kilometers/hr/sec
Acceleration	feet/sec <sup>2</sup>	0.3048	meters/sec <sup>2</sup>
	feet/sec <sup>2</sup>	0.6818	mph/sec
	g	32.174049	feet/sec <sup>2</sup>
	g	9.80665	meters/sec <sup>2</sup>
	gals (Galileo)	0.01	meters/sec <sup>2</sup>
	knots/sec	1.6878	feet/sec <sup>2</sup>
	meters/sec <sup>2</sup>	3.6	kilometers/hr/sec
	mph/sec	0.447	meters/sec <sup>2</sup>
	mph/sec	1.609	kilometers/hr/sec
Mass	carats	200	milligrams
	grams	0.035274	ounces*
	grains	6.479891x10 <sup>-5</sup>	kilograms
	hndrdwght long	50.80 234544	kilograms
	hndrdwght shrt	45.359237	kilograms
	kilograms	0.06852	slugs
	kilograms	6.024x1026	atomic mass units
	kilograms	2.2046	pounds*
	ounces (avd)*	28.349523125	grams
	ounces (troy)*	31.1034768	grams
	pounds (mass)	1	pounds (force)*
	pounds (mass)	0.45359237	kilograms
	pounds (mass)	0.031081	slugs
	scuples (apoth)	0.0012959782	kilograms
	slugs	32.174	pounds *
	slugs	14.594	kilograms
	tons (long)	1016.047	kilograms
	tons (assay)	0.02916	kilograms
	tons (metric)	1000	kilograms
	tons (short)	907.1847	kilograms

<sup>\*</sup> conversion from pounds force to pounds mass assumes  $g = 32.174 \text{ ft/s}^2$ 

	<u>Multiply</u>	<u>by</u>	<u>To Obtain</u>
Moments	gram-cm <sup>2</sup>	$0.737 \times 10^{-7}$	slug-ft <sup>2</sup>
of Inertia	pound-ft <sup>2</sup> * slug-in <sup>2</sup>	0.031081 0.0069444	slug-ft <sup>2</sup> slug-ft <sup>2</sup>
	slug-ft <sup>2</sup>	1.3546	kg-m <sup>2</sup>
	<b>slug-ft<sup>2</sup></b> slug-ft <sup>2</sup>	<b>32.174</b> 12.00	<b>pound-ft<sup>2</sup></b> * pound-inch-sec <sup>2</sup> *
	slug-ft <sup>2</sup>	192.00	ounce-inch-sec <sup>2</sup> *

<sup>\*</sup> conversion from force to mass assumes  $g = 32.174 \text{ ft/s}^2$ 

Power	btu/min	0.01758	kilowatts
	calories(kg)/mir	n 3087.46	foot-pounds/min
	ergs/sec	$7.376 \times 10^{-8}$	foot-pounds/sec
	ft(lbs)/min	$2.260 \times 10^{-5}$	kilowatts
	ft(lbs)/sec	0.07712	btu/min
	ft(lbs)/sec	1.356	watts
	hp	550	ft(lb)/sec
	hp	33,000	ft(lbs)/min
	hp	10.69	calories (kg)/min
	hp	745.7	watts [J/sec]
	hp (metric)	735.5	watts
	hp	1.1014	horsepower (metric)
	kilowatts	1.341	horsepower
	watts	$10^{7}$	ergs/sec
	watts	1	Joules/sec
Pressure	atmospheres	14.696	pounds/in <sup>2</sup>
	atmospheres	29.92	inches of Hg
	atmospheres	76	cm of Hg
	bars	1,000,000	dynes/cm <sup>2</sup>
	bars	29.52	inches of Hg
	barye	0.1	Newtons/m <sup>2</sup>
	dynes/cm <sup>2</sup>	10	Newtons/m <sup>2</sup>
	inches of H <sub>2</sub> O	5.20237	pound/ft <sup>2</sup>
	inches of Hg	70.72619	pounds/ft <sup>2</sup>
	inches of Hg	0.491154	pounds/in <sup>2</sup>
	inches of Hg	13.595	inches of H <sub>2</sub> O
	kiloPascals	100	bars
	pounds/ft <sup>2</sup>	47.88	Pa
	pounds/in <sup>2</sup>	6894.72	Pa
	hectoPascals	1	millibars
	millibars	0.02953	inches of Hg
	mm of Hg	0.019337	pounds/in <sup>2</sup>
	-		_

	<u>Multiply</u>	<u>by</u>	<u>To Obtain</u>
Pressure	mm of Hg	133.32	Newtons/m <sup>2</sup>
Cont.	Pascals	1	Newton/m <sup>2</sup>
	pieze	1000	Newtons/m <sup>2</sup>
	pounds/ft <sup>2</sup>	0.01414	inches of Hg
	pounds/ft <sup>2</sup>	47.88	Newtons/m <sup>2</sup>
	pounds/in <sup>2</sup>	2.036	inches of Hg
	pounds/in <sup>2</sup>	27.681	inches of H <sub>2</sub> O
	pounds/in <sup>2</sup>	.3325	Pa
	torrs	133.32	Newtons/m <sup>2</sup>
Temperature	$Kelvin = {}^{o}C + 27$		
	Rankin = ${}^{\circ}F$ +		
	°Centigrade =		
	°Fahrenheit = (9	$(9/5)^{\circ}C + 32$	
Time	days (solar)	24	hours
	days (sidereal)	23.934	hours
	days (solar)	1.0027	days (sidereal)
	hours	60	minutes
	minutes	60	seconds
	months (sdrl)	27d + 7hr +43n	
	months (lunar)	29d +12hr +44h	
	year	365.24219879	days
Torque	foot-pounds	1.3558	Newton-meters
	foot-pounds	0.1383	kilogram-meters*
	ounce-inches	72.008	gram-centimeters*
	pound-inches	1129800	dyne-centimeters

<sup>\*</sup> conversion from kg mass to kg force assumes  $g = 32.174 \text{ ft/s}^2$ 

Velocity	inches/sec	0.0254	meters/sec
	knots	1.68781	feet/sec
	km/hr	0.621371	mph
	km/hr	0.9113	feet/sec
	Knots (kts)	1.15078	mph
	Knots (kts)	1.852	km/hr
	Knots (kts)	0.51444	meters/sec
	meters/sec	3.281	ft/sec
	meters/sec	3.6	km/hr
	meters/sec	196,85	feet/min
	mph	1.466667	feet/sec

	<u>Multiply</u>	<u>by</u>	To Obtain
Viscosity	centistokes	10 <sup>-6</sup>	m <sup>2</sup> /sec
Viscosity	ft <sup>2</sup> /sec	0.0929	m <sup>2</sup> /sec
	pound sec/ ft <sup>2</sup>	47.880258	Newton secs/ m <sup>2</sup>
	poise	0.1	Newton secs/ m <sup>2</sup>
	rhe	10	m <sup>2</sup> /Newton second
Volume	acre-feet	43,560	ft <sup>3</sup>
	acre-feet	1,233	$m^3$
	acre-feet	$3.259 \times 10^5$	gals (U.S.)
	barrels	31.5	gals (U.S.)
	board-feet	144	$in^3$
	bushels	1.244	ft <sup>3</sup>
	bushels	32	quarts (dry)
	bushels	4	pecks
	cm <sup>3</sup>	0.001	liters
	cm <sup>3</sup>	0.03381	fluid ounces
	cm <sup>3</sup>	0.06102	in <sup>3</sup>
	cord-feet	4x4x1	ft <sup>3</sup>
	cords	128	ft <sup>3</sup>
	cups	0.5	pints (liquid)
	dram (fluid)	3.69669x10 <sup>-6</sup>	$m^3$
	ft <sup>3</sup>	0.0283167	m <sup>3</sup>
	ft <sup>3</sup>	1728	in <sup>3</sup>
	ft <sup>3</sup>	28.32	liters
	ft <sup>3</sup>	7.481	gals (U.S.)
	gals (Imperial)		gals (U.S.)
	gals (Imperial)		$in^3$
	gals (U.K.)	4546.1	cm <sup>3</sup>
	gals (U.S.)	231	in <sup>3</sup>
	gals (U.S.)	0.003785	$m^3$
	gals (U.S.)	3.785	liters
	gals (U.S.)	4	quarts (liquid)
	gals (U.S.)	0.0238095	barrels (U.S.)
	gils	7.219	in <sup>3</sup>
	hogshead	2	barrels
	in <sup>3</sup>	16.39	cm <sup>3</sup>
	liters	0.02838	bushels
	liters	0.9081	quarts (dry)
	liters	1.057	quarts (liquid)
	liters	1000	cm <sup>3</sup>
	liters	61.03	$in^3$
	$m^3$	1.308	$yd^3$
			J

	<u>Multiply</u>	<u>by</u>	<u>To Obtain</u>
Volume	$m^3$	1000	liters
Cont.	$m^3$	264.2	gals (U.S.)
	$m^3$	35.314667	ft <sup>3</sup>
	mil-feet (circ.)	0.0001545	cm <sup>3</sup>
	ounces (U.K.)	28.413	cm <sup>3</sup>
	ounces (U.S.)	29.574	cm <sup>3</sup>
	pecks	8	quarts (dry)
	pecks	8.81	liters
	perches	0.7008	$m^3$
	perches	24.75	ft <sup>3</sup>
	pints (dry)	33.60	$in^3$
	pints (liquid)	28.88	$in^3$
	pints (liquid)	4	gals
	quarts (dry)	1.164	quarts (liquid)
	quarts	2	pints
	register tons	100	$ft^3$
	shipping ton (U	.S.) 40	$ft^3$
	shipping ton (B	*	ft <sup>3</sup>
	steres	1000	liters
	tablespoons	0.0625	cups
	teaspoons	0.3333	tablespoons
	-		-

## 1.2 Greek Alphabet

- $A \quad \alpha \quad Alpha$
- B β Beta
- $\Gamma$   $\gamma$  Gamma
- $\Delta \quad \delta \quad Delta$
- E ε Epsilon
- Z ζ Zeta
- H  $\eta$  Eta
- $\Theta$   $\theta$  Theta
- I ι Iota
- К к Карра
- $\Lambda$   $\lambda$  Lambda
- $M \mu Mu$
- $N \quad \nu \quad Nu$
- $\Xi$   $\xi$  Xi
- O o Omicron
- $\Pi \quad \pi \quad Pi$
- $p \quad \rho \quad Rho$
- Σ σ Sigma
- $T \quad \tau \quad Tau$
- Y υ Upsilon
- $\Phi \quad \phi \quad Phi$
- $X \quad \chi \quad Chi$
- $\Psi \quad \psi \quad Psi$
- $\Omega \quad \omega \quad Omega$

### 1.3 Greek Symbols Used for Aircraft

- $\alpha$  angle of attack (degrees or radians)  $\alpha_{\tau}$  tail angle of attack
- $\beta$  angle of sideslip (degrees)
- γ flight path angle relative to horizontal
- γ specific heat ratio (1.4 for air)
- δ relative pressure ratio  $(P_a/P_o)$
- $\delta_a$  aileron deflection angle
- $\delta_{\rm r}$  rudder deflection angle
- $\delta_e$  elevator deflection angle
- ε downwash angle at tail (degrees)
- $\zeta$  damping ratio  $\eta$  efficiency
- θ body axis/pitch angle
- $\theta$  relative temperature ratio,  $T_a/T_o$
- t angle of incidence
- $t_F$  thrust angle of incidence
- $t_T$  horizontal tail angle of incidence
- $\lambda$  pressure lag constant
- $\Lambda$  wing sweep angle
- $\mu$  coefficient of absolute viscosity =  $\rho v$
- μ Mach cone angle
- v kinematic viscosity =  $\mu/g$
- $\pi$  nondimensional parameter
- ρ density
- $\rho_a$  ambient air density
- $\rho_o$  standard atmospheric density (slugs/ft3)
- $\sigma$  air density ratio ( $\rho_\alpha / \rho_o$ )
- $\sigma_{cr}$  critical density
- τ shear stress (pounds per square inch) psi
- $\tau_R$  Roll Mode Time Constant (sec)
- φ bank angle (degrees)
- ψ aircraft heading (degrees)
- ω frequency
- ω rotational velocity (radians per second)
- $\omega_d$  damped natural frequency
- $\omega_n$  natural undamped frequency

## 1.4 Common Subscripts

- a aileron
- a ambient
- alt at test altitude
- avg average
- c calibrated
- e elevator
- e equivalent
- E endurance leg of mission
- F final
- I initial
- *i* inbound leg of mission
- *i* indicated
- ic instrument corrected
- l subscript for coefficient of rolling moment
- *m* mission conditions
- m pitching moment
- *n* yawing moment
- O outbound leg of mission
- o sea-level standard day
- o sea level
- r reserve leg of mission
- r rudder
- S standard day
- s standard day at altitude
- SL sea level
- True
- t test day

### 1.5 Common Abbreviations

a lift curve slope

a linear acceleration (ft/sec<sup>2</sup> or m/sec<sup>2</sup>)

a speed of sound A/A air-to-air a/c aircraft

AAA anti aircraft artillery
AC aerodynamic center
ac alternating current
ACM air combat maneuvering

A/D analog to digital ADC air data computer

ADC analog-to-digital converter ADF automatic direction finder ADI attitude direction indicator AFMC Air Force Materiel Command

AFOTEC Air Force Operational Test and Evaluation Center

A/G air-to-ground AGL above ground level

AHRS attitude heading reference system

AM amplitude modulation
AOA angle of attack
AOED age of ephemeris data
APU auxiliary power unit
AR air refuel (mode of flight)

AR aspect ratio =  $b^2 / S$ 

ARDP advanced radar data processor ARSP advanced radar signal processor ASPJ airborne self protection jammer

ATC air traffic control

avg average

ax longitudinal acceleration ay lateral acceleration

AZ azimuth

b span of wing (feet) B/N bombadier/navigator

bbl barrel

*BHP* brake horsepower

BICOMS bistatic coherent measurement system

BID bus interface device

BIT built-in test

*BSFC* brake specific fuel consumption

Btu British thermal unit

BW bandwidth

oC degrees centigrade...see *T* c aerodynamic chord of a wing

c brake specific fuel consumption (BSFC)

c

c speed of light in a vacuum

(186,282 miles/sec = 299,792,500 [m/s]) mean aerodynamic chord (MAC) of a wing

C/A coarse acquisition
C/N<sub>o</sub> carrier to noise ratio
CADC central air data computer

CARD cost analysis requirement document

 $C_D$  coefficient of drag  $C_{D\,\mathrm{i}}$  induced drag coefficient  $C_{D\,\mathrm{o}}$  zero lift drag coefficient

(also parasitic drag coefficient for symmetric

wing)

CDI course deviation indicator CDMA code division multiplex access

CDR critical design review

CDRL contracts data requirement list

CDU control display unit CEA circular error average CEP circular error probable  $C_f$  coefficient of friction

CFE contractor furnished equipment

CFT conformal fuel tank

cg center of gravity (normally in % MAC)

C<sub>H</sub> hinge moment coefficient

cine cinetheodolite

 $C_L$ 

 $C_l$  rolling moment coefficient, airfoil section lift co

efficient lift coefficient

CLHQ closed loop handling qualities  $C_{lp}$  roll damping coefficient

 $C_{lr}$  roll moment due to yaw rate coefficient

 $C_m$  pitching moment coefficient

 $C_M$  moment coefficient

cm centimeters cos cosine cot cotangent

 $C_{l\beta}$  (dihedral) rolling moment due to sideslip

 $C_{l\delta a}$  aileron power coefficient  $Cm_q$  pitch damping coefficient

 $Cm_{\alpha}$  longitudinal static stability coefficient

 $Cm_{\delta e}$  elevator power coefficient Cn yawing moment coefficient  $Cn_r$  yaw damping coefficient

cnst constant

 $Cn_{\beta}$  directional stability coefficient

 $Cn_{\delta a}$  adverse yaw coefficient  $Cn_{\delta r}$  rudder power coefficient COTS commercial, off-the-shelf

CP center of pressure

 $C_P$  propeller power coefficient CPU central processing unit  $c_r$  wing root chord

CRM crew resource management

c<sub>t</sub> wing tip chord CTF combined test force CY calendar year

 $C_Y$  side force coefficient

 $CY_{\beta}$  side force due to sideslip coefficient  $CY_{\delta r}$  side force due to rudder coefficient

D diameter D drag

D/A digital/analog

DAC digital to analog converter

DAPS data acquisition and processing system

DARPA Defense Advanced Research Projects Agency

db decibel
DC direct current
deg degrees

DG directional gyro DGPS differential GPS

DMA Defense Mapping Agency
DME distance measuring equipment
DoD Department of Defense
DOP dilution of precision

DSN defense switched network

DT development test
DTC data transfer cartridge

DTIC Defense Technical Information Center

e Oswald efficiency factor

e natural mathematical constant = 2.718281828459

E energy

E lift-to-drag ratio ( $C_L/C_D$ , L/D)

EAS equivalent airspeed EC electronic combat

ECCM electronic counter countermeasures

ECM electronic countermeasures
ECP engineering change proposal
ECS environmental control system
EGT exhaust gas temperature

EL elevation

ELINT electronic intelligence ELV expendable launch vehicle

EM electromagnetic

 $E_{\rm max}$  maximum lift-to-drag ratio EMC electromagnetic compatibility EMI electromagnetic interference

EMP electromagnetic pulse

EO electro optical EOM equations of motion EPR engine pressure ratio

EPROM electrically programmable read only memory

Es specific energy

ESA European Space Agency
ESD Electronic Systems Division
ESHP equivalent shaft horsepower
ETA estimate time of arrival
ETE estimate time en-route

EW early warning
EW electronic warfare
°F degrees Fahrenheit

f frequency...hertz (originally cycles per second)

F.S. fuselage station  $F_a$  aileron force

 $\begin{array}{lll} \text{FAA} & \text{Federal Aviation Administration} \\ \text{FAR} & \text{Federal Aviation Regulation} \\ \text{FCF} & \text{functional check flight} \\ \text{FDC} & \text{flight data computer} \\ F_e & \text{elevator force} \\ F_{ex} & \text{excess thrust} \\ F_g & \text{gross thrust} \\ \end{array}$ 

flight level

Flip flight information publication
FLIR forward-looking infra red
FM frequency modulation
FMC fully mission capable
FMS flight management system
FMS foreign military sales

Fn net thrust

FL

 $Fn/\delta$  corrected thrust parameter

FOM figure of merit

FOT&E follow-on test & evaluation

FOUO for official use only

FOV field of view fpm feet per minute fps feet per second

FQT formal qualification test

Fr rudder force

FRD functional requirements document

FRL fuselage reference line
FRL force, rudder, left
FRR force, rudder, right
FRR flight readiness review
FSD full scale development
FSI full scale integration

ft feet

ft-lb English unit of work...foot-pound...

forward fwd FY fiscal year acceleration due to gravity at altitude g Ggravitational constant =  $6.6732 \times 10^{-11}$  [N m<sup>2</sup>/kg<sup>2</sup>] Government Accounting Office GAO GCA ground control approach ground controlled intercept GCI **GDOP** geometric dilution of precision **GMT** Greenwich mean time standard acceleration due to gravity  $g_o$ (sea level, 46 deg latitude) **GPS** global positioning system GS ground speed glide slope indicator GSI h % MAC Н altitude **HARM** high-speed anti-radiation missile  $H_c$ calibrated altitude (assumed to be pressure altitude in flight test)  $H_D$ density altitude HDDR high density digital recorder **HDOP** horizontal dilution of precision HF high frequency Hg mercury indicated altitude  $H_i$ stick-fixed maneuver point (%MAC)  $h_m$ stick-free maneuver point (%MAC)  $h_{m}$ stick-fixed neutral point (%MAC)  $h_n$ stick-free neutral point (%MAC)  $h_{n}$ hp horsepower hr hour hrs hours horizontal situation indicator HSI head-up display HUD HVhost vehicle Hzhertz I/O input/output indicated airspeed **IAS** 

ICAO International Civilian Aviation Organization

ICU interface computer unit

ICBM intercontinental ballistic missile
IFF identification friend or foe
IFR instrument flight rules
ILS instrument landing system

in accordance with

IMC instrument meteorological conditions

IMN indicated Mach number IMU inertial measuring unit

in inch

IAW

**INS** inertial navigation system INU inertial navigation unit **IOC** initial operational capability IOT&E

initial operational test & evaluation

IUGG International Union of Geodesy and Geographics

moments of inertia  $I_x$ ,  $I_x$ ,  $I_z$  $I_{xy}$ ,  $I_{xz}$ ,  $I_{yz}$ products of inertia

joules energy, (Newton-Meter)

Jpropeller advance ratio J&S jamming and spoofing Joint Chiefs of Staff JCS

K Kelvin (absolute temperature) temperature probe recovery factor K

K. k1 constants

**KCAS** knots calibrated airspeed **KEAS** knots equivalent airspeed kilogram, metric unit of mass kg knots indicated airspeed **KIAS KISS** keep it simple, stupid

kilometer km

KTAS knots true airspeed

kts knots LLift (lbs) length l

Lrolling moment L/D Lift-to-drag ratio L/Dlift-to-drag ratio

low altitude navigation and targeting IR for night LANTIRN

lateral lat lb pound

 $lb_{f}$ English unit of force, often just lb (pound) English unit of mass, often just lb (slug)  $lb_{m}$ 

life cycle cost LCC LCD liquid crystal display LED light emitting diode LLH latitude, longitude, height natural log, log to the base e ln

low observables LO

common log, to the base 10 Log

LOS line of sight

 $l_{\rm t}$ distance from cg to tail's aerodynamic cent rolling moment due to aileron deflection  $L_{\delta a}$ 

moment (ft-lbs) MMMach number

mass m

meter (length) m pitching moment M

MAG magnetic

MAP manifold pressure mb millibar

MCA minimum crossing altitude  $M_{cr}$  critical Mach number

 $M_d$  drag divergence Mach number

 $\begin{array}{ll} M_{ac} & \text{mean aerodynamic cord} \\ M_{GC} & \text{mean geometric chord} \end{array}$ 

MHz megahertz mHZ millihertz

*M<sub>ic</sub>* instrument-corrected Mach number

MilSpec military specification

MIL-STD military standard (publication)

min minute (time) Mm millimeters

MOA memorandum of agreement
MOE measure of effectiveness
MOP measures of performance
MOU memorandum of understanding

MP manifold pressure MSL mean sea level

MTBF mean time between failures

MTTR mean time to repair

MX maintenance N newton (force)

N rotational speed (RPM)

n load factor (g's)N yawing moment

 $N_1$  low pressure compressor speed  $N_2$  high pressure compressor speed

NACA National Advisory Committee for Aeronautics

NADC Naval Air Development Center

NASA National Aeronautics and Space Administration

NAV navigation

NED North, East, Down NM, nm nautical mile (6080 feet)

NOE nap-of-the-earth

NOFORN not releasable to foreign nationals

NOTAM notice to airmen

NRC National Research Council (Canada)

NWCNaval Weapons Center $N_x$ longitudinal load factor (g's) $N_y$ lateral load factor (g's) $N_z$ normal load factor (g's)OAToutside air temperature

OAT on aircraft test

OEI One engine inoperative

OPR Office of Primary Responsibility
OSD Office of the Secretary of Defense
OT&E operational test & evaluation
p aircraft roll rate (degrees/sec)

pressure (N/m<sup>2</sup>, pounds per square inch) P Pa ambient pressure pulse code modulation **PCM** P-code precision code PD pulse Doppler **PDM** pulse duration modulation precision guided munitions **PGM** PIO pilot induced oscillations total thrust horsepower required  $P_{iw}$ probability of kill Pk PLF power for level flight standard atmospheric pressure (2116.22 lb/ft<sup>2</sup>)  $P_{o}$ POC point of contact pitot pressure  $P_p$ parts per million ppm propeller Prop  $P_{s}$ static pressure PS pulse search psf pounds per square foot pounds per square inch psi total pressure  $P_T$ PW pulse width dynamic pressure =  $0.5 \rho V^2$ Q or qaircraft pitch rate q engine torque Q impact pressure  $(P_t - P_a)$  $q_c$  $^{\circ}R$ degrees Rankine =  ${}^{\circ}F + 459.67$ perfect gas constant = 8314.34 [J/kmol K] R aircraft yaw rate (degrees/sec) r R earth radius R range R&D research and development reliability and maintainability R&M R/Crate of climb rad radians Radar radio detection and ranging **RAF** resultant aerodynamic force radar absorbing material **RAM RAT** ram air turbine RCS radar cross section Reynolds number (dimensionless) Re range error probable **REP** RF range factor **RLG** ring laser gyro root mean square rms RNG range

Page 01-22

revolutions per minute (a.k.a. N)

required obstacle clearance

rate of climb

ROC

**ROC RPM**  R/T receiver/transmitter RTO refused takeoff RTO rejected takeoff

RTO responsible test organization

S wing area ( $ft^2$  or  $m^2$ )

S<sub>a</sub> horizontal distance between liftoff and specified height or between specified height and touch

down.

SA selective availability
SA situational awareness
SE specific endurance
sec seconds (time or angle)
SFC specific fuel consumption
S<sub>g</sub> ground roll distance
SHP shaft horsepower

SI international system of units

SIGINT signal intelligence

sin sine SL sea level

SLAM standoff land attack missile

SLR side-looking radar
S/N serial number
S/N signal -to-noise ratio
SOF special operations forces

SOW stand-off weapon SR specific range SRB safety review board

 $S_T$  tail area std standard

 $S_T$  total takeoff or landing distance  $(S_a + S_g)$ 

STOL short takeoff and landing

STOVL short takeoff and vertical landing

T period of oscillation

T temperature t thickness T, t time (sec)

t/c thickness-to-chord ratio
T<sub>a</sub> ambient temperature
TACAN tactical air navigation

tan tangent

T<sub>as</sub> standard temperature at altitude

TAS true airspeed
TBD to be determined
TD touchdown

TED trailing edge down TEL trailing edge left

TEMP test and evaluation master plan

TER trailing edge right TEU trailing edge up

TF terrain following
THP Thrust Horsepower

 $\begin{array}{ll} THP_{alt} & horsepower available at altitude \\ THP_{max} & maximum horsepower available \\ THP_{min} & minimum horsepower required \\ THP_{SL} & horsepower required at sea level \\ \end{array}$ 

TIT turbine inlet temperature

TM telemetry

TMN true Mach number

T/O takeoff

T<sub>o</sub> standard sea level temperature (59.0 °F, 15 °C)

TO technical order

TRB technical review board

TRD technical requirements document

TRP technical resources plan

TSFC thrust specific fuel consumption TSPI time, space, position information

T<sub>t</sub> total temperature

TV television

T/W thrust to weight ratio TWT track while scan TWT traveling wave tube

u velocity along aircraft's x-axisUAV uninhabited aerial vehicleUHF ultra high frequency

UPT undergraduate pilot training

USA US Army
USAF US Air Force
USCG US Coast Guard
USMC US Marine Corps

USN US Navy
UT universal time
UV ultraviolet

 $\begin{array}{lll} v & & \text{velocity along aircraft's lateral axis} \\ V_H & & \text{horizontal tail volume coefficient} \\ V_V & & \text{vertical tail volume coefficient} \end{array}$ 

V<sub>1</sub> takeoff decision speed
 V<sub>2</sub> takeoff safety speed
 V<sub>A</sub> design maneuvering speed

VAC volts AC V<sub>b</sub> buffet airspeed

V<sub>B</sub> design speed for max gust intensity

 $\begin{array}{ll} V_{br} & \text{velocity for best range} \\ V_{c} & \text{calibrated airspeed} \\ V_{D} & \text{design diving speed} \end{array}$ 

VDC volts DC

VDOP vertical dilution of precision

V<sub>e</sub> equivalent velocity

V<sub>FE</sub> maximum flap extended speed

 $\begin{array}{lll} V_{FR} & & visual \ flight \ rules \\ V_g & & ground \ speed \\ VHF & very \ high \ frequency \\ V_i & & indicated \ airspeed \end{array}$ 

 $\begin{array}{lll} V_{ic} & & \text{indicated airspeed corrected for instrument error} \\ V_{iw} & & \text{velocity at sea level std day and std weight} \\ VLE & & \text{max speed with landing gear extended} \\ V_{LO} & & \text{max speed while operating landing gear} \\ \end{array}$ 

V<sub>LOF</sub> lift off speed

VLSIC very large scale integrated circuit  $V_{mc}$  minimum directional control speed VMC visual meteorological conditions

 $V_{mca}$  minimum directional control speed in the air  $V_{mcg}$  minimum directional control speed on the

ground

 $V_{mo}/M_{mo}$  maximum operating limit speed

 $V_{mu}$  minimum unstick speed  $V_{NE}$  never exceed velocity

V<sub>no</sub> max structural cruising speed

V<sub>opt</sub> optimum velocity for endurance flight

VOR VHF omni-directional range

VORTAC VHF omni-directional range Tactical Air Navi

gation

V<sub>Pmin</sub> velocity for minimum power

 $V_{Pmin,SL}$  velocity for minimum power at sea level

 $egin{array}{ll} V_R & & \text{rotation speed} \\ V_S & & \text{stall speed} \\ \end{array}$ 

 $V_{S0}$  stall speed in landing configuration  $V_{S1}$  stall speed in some defined configuration

VSTOL vertical/short takeoff and landing

V<sub>T</sub> true airspeed

VTOL vertical takeoff & landing VVI vertical velocity indicator

V<sub>w</sub> wind velocity

 $egin{array}{ll} V_X & ext{speed for best angle of climb} \ V_Y & ext{speed for best rate of climb} \ \end{array}$ 

W weight

w component of velocity along aircraft's Z-axis

WDL weapon data link W/ $\delta$  weight-to-pressure ratio

W<sub>f</sub> fuel weight

WGS-84 World Geodetic System, 1984

WI watch item
WOD word of day
WOW weight on wheels

WPT waypoint wrt with respect to

$\frac{\dot{W}_{f}}{\delta \sqrt{q}}$ ,	corrected fuel flow parameter
W/S	wing loading
$W_{\mathrm{f}}$	fuel flow (lb/hr)
X	aircraft longitudinal axis,
Α	a line running through the nose & tail
$X_{ac}$	distance from leading edge to aerodynamic cen
	ter
Xlink	cross link
y	aircraft lateral axis, a line running the wingtips
Y	force along y-axis
Y-code	encrypted P-code
Z	aircraft vertical or yaw axis,
	a line perpendicular to the longitudinal and lat
	eral axes
$\Delta H_{ic}$	altimeter instrument correction
$\Delta H_{pc}$	altimeter position error correction
$\Delta \mathrm{P}_{\mathrm{p}}$	pitot pressure error
$\Delta P_{\rm s}$	static pressure error
$\Delta { m V}_{ m c}$	scale attitude correction to airspeed
$\Delta  m V_{ic}$	instrument correction to airspeed indicator
$\Delta  m V_{pc}$	correction for airspeed position error
$\infty$	infinity, or freestream conditions

## **1.6 Sign Conventions**

(reference 1.8)

Editor's note There is near unanimous agreement on most sign conventions except for pilot inputs and control surface deflections. Although individual organizations generally are consistent in-house, confusion often arises when trying to mathematically translate inputs & deflections from one organization to another. This section documents the generally accepted "body axes" sign conventions then discusses the rationale for several viewpoints addressing the "inputs & deflections" debate. Below is the SFTE sign convention.

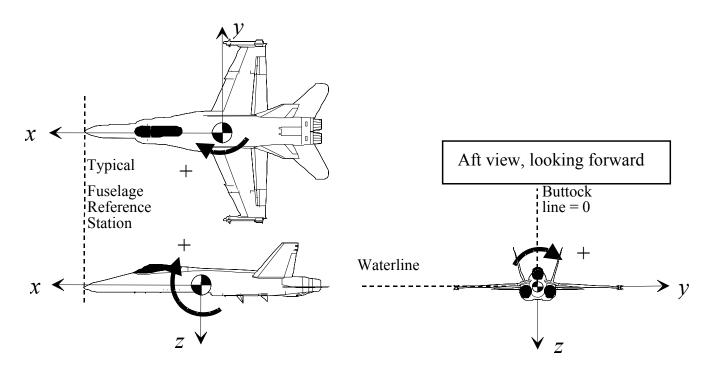
### Wind Axes Sign Convention

Winds are listed according to the direction they are coming from. Airports refer winds to magnetic North while winds at altitude are typically referred to true North. Headwind is true airspeed minus ground speed.  $(V_w = V_T - V_g)$ .

### **Body Axes Sign Convention**

The generally accepted body axes sign convention is based on the establishment of a three-dimensional axis system with the following properties:

- 1. It is right-handed orthogonal
- 2. Its origin is at the vehicle's reference center of gravity (defined by builder).
- 3. The axis system moves with the airframe.



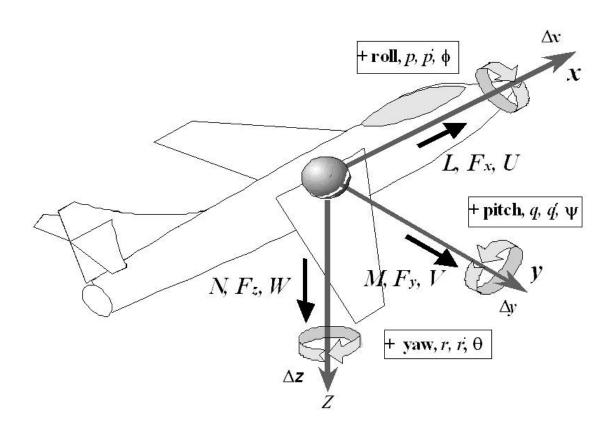
Translational displacements, rates, accelerations, & forces are positive along the positive body axes directions. In spite of the simplicity of this logic, it is important to recognize that lift and normal load factor are positive in the *negative z* direction and the drag is positive in the *negative x* direction.

Angular displacements, rates, accelerations & moments, are positive according to the "right hand rule" (a clockwise rotation while looking in the direction of the positive axis) as shown in the figure.

The body axes, forces & translations along them, and moments & rotations about them are shown with arrows indicating the positive direction.

Angular displacements, rates, accelerations & moments, are positive according to the "right hand rule" (a clockwise rotation while looking in the direction of the positive axis) as shown in the figure.

The body axes, forces & translations along them, and moments & rotations about them are shown with arrows indicating the positive direction.



Angle of attack is positive clockwise from the projection of the velocity vector on the xz plane to the reference x body axis. The angle of sideslip is positive clockwise from the xz plane to the velocity vector (wind in the pilot's right ear).

Aircraft *true* heading is the angle between *true* North and the projection of the x-body axis onto the horizontal plane. Mag. heading refers to mag North

The velocity vector is measured relative to the air mass while the flightpath is measured relative to the ground. They are equivalent only when winds are zero.

Flightpath heading angle (ground track heading)  $\sigma_g$ , is the horizontal angle between true North and the projection of the flightpath on the horizontal plane. Positive rotation is from north to east.

Flightpath elevation angle;  $\gamma$ , is the vertical angle between the flightpath and the horizontal plane. Positive rotation is up. During a descent, this parameter is commonly known as glide path angle.

Flightpath bank angle;  $\mu$ , is the angle between the plane formed by the velocity vector and the lift vector and the vertical plane containing the velocity vector. Positive rotation is clockwise about the velocity vector, looking forward.

Fuselage reference station (FRS), Water line (WL), and Buttock line (BL) are reference coordinates established by the design group.

## **Summary of Generally Accepted Body Axes Sign Convention**

Parameter Name	Symbol	<b>Positive Direction</b>
Ti	ranslational Measuren	nents
Longitudinal axis	X	from ref cg towards nose
Lateral axis	y	from reference cg towards right wing tip
Vertical axis	Z	from reference <i>cg</i> towards vehicle bottom (body axis)
Longitudinal velocity	u	along +x axis
Lateral velocity	v	along +y axis
Vertical velocity	W	along +z axis
Long. acceleration	$a_{x}$	along + x axis
Lateral acceleration	$a_{y}$	along +y axis
Vertical acceleration	$a_z$	along +z axis
Longitudinal load factor	$N_x$	along +x axis
Lateral load factor	$N_y$	along +y-axis
Normal load factor	$N_z$	along –z axis
Longitudinal force	$F_x$	along the +x axis
Lateral force	$F_y$	along the +y axis
Normal force	$F_z$	along the + z axis
Drag force	D	along the –x axis
Side force	Y	along the + y axis
Lift Force	L	along the -z axis

#### **Summary of Generally Accepted Body Axes Sign Convention**

Parameter Name	Symbol	<b>Positive Direction</b>
	Angular Measurements	
Bank angle	$\phi$	right wing down
Pitch angle	$\theta$	nose-up
Heading	Ψ	0 North, +Eastward
Angle of attack	α	normal flight attitude
Angle of sideslip	β	"wind in the right ear"
Roll rate	p	right wing down
Pitch rate	q	nose up
Yaw rate	r	nose right
Roll moment	L	right wing down
Pitch moment	M	nose up
Yaw moment	N	nose right
Flightpath bank angle	$\mu$	right wing down
Flightpath elevation	γ	climb
Flightpath heading	$\sigma_{\!g}$	0 true North, + Eastward

#### **Discussion of "Input & Deflection" Conventions**

The debate regarding proper inputs and deflections stems from the user's viewpoint. From the body axis convention above, flight testers recognize that a climbing right turn generates positive angular measurements. Logically then, pull, right roll and right yaw pilot inputs and subsequent surface deflections should also be positive. The traditional flight tester's convention follows as "All input forces & displacements, surface deflections, and motions that cause a climbing right turn are positive."

Due to differential nature of aileron deflections, they require more discussion. The flight tester's logic implies (but does not dictate) positive deflections are right aileron up and left aileron down. It is, however, equally acceptable to assign downward (or upward) deflection as positive for <u>both</u> ailerons and calculate the difference between the two as a measure of rolling moment.

The rationale within the wind tunnel community is also logical: any control surface deflection that increases lift is positive. From this, positive deflections are trailing edge down (TED) for each: trailing edge flap, stabilizer, elevator, stabilator, rollervator, ruddervator, canard, aileron, flaperon, and all their tabs. Leading edge flap down is also positive. Similarly, since side force is positive to the right, then positive rudder and rudder tab deflections are trailing left (TEL). The only exception to this straightforward logic is for spoilers and speed brakes that extend only in one direction: this deflection is positive even though it might decrease the lift.

Since the above rationale defines downward deflection as positive for both ailerons, a measurement of rolling moments requires calculation of the differential aileron deflection. This rationale does not, however, specifically dictate whether a "positive" differential deflection should generate right wing down (RWD) or left wing down (LWD) moments. Differential aileron can be calculated as either.

$$\delta_a = \frac{\delta_{aR} - \delta_{aL}}{2}$$
 or  $\delta_a = \frac{\delta_{aL} - \delta_{aR}}{2}$ 

Selection of the RWD convention is obvious from the flight tester's viewpoint since deflections that generate right rolls are positive. An alternative interpretation is that a positive differential aileron deflection is one that lifts the positive (right) wing lifts more than the left (LWD).

Another common convention for ailerons is one that gives the same sign to both ailerons for any input. The "right hand screw" convention is opposite to the flight tester's convention, but may be more common:

$$\delta_{aR} = +\text{TED}, \ \delta_{aL} = +\text{TEU}.$$

The above wind tunnel rationale dictates only the polarity for individual control surface deflections, and leaves open the sign convention debate about controller (inceptor) input forces & displacements. One approach is that positive inputs should generate positive *motions* while an alternate approach is that positive inputs generate positive *surface deflections*. Only the flight tester's convention states that positive inputs yield positive motions *and* deflections. All approaches are mathematically connected to the hinge moment sign convention discussed below.

The simplest control surface hinge moment convention is that *all* positive hinge moments (generated by the pilot and the aerodynamics) move the surface in a positive direction, i.e., positive input forces yield positive deflections. This has different implications for the different sign conventions:

- According to the above flight tester's sign convention, a positive pull force is required to generate a positive (TEU) elevator deflection (positive stick force generates a climb).
- According to wind tunnel sign convention, a positive *push* force is required to generate a positive (*TED*) elevator deflection (positive stick force generates a *dive*).

The alternate viewpoint defines a positive inceptor hinge moment as one that *opposes* the aerodynamic moments. In other words, a positive inceptor hinge moment moves the surface to a position which generates positive aerodynamic hinge moments or "positive input forces & displacements generate negative surface deflections."

Based on the above background, the SFTE technical council proposes the following standard convention for inceptor & surface forces & deflections:

- Due to its widespread use and its simple & robust nature, use the wind tunnel convention for control surface deflections.
- Due to widespread test pilot & FTE familiarity and logical nature, use the flight tester's convention that positive inceptor forces & displacements generate a climbing right turn.
- A fallout from these conventions is that positive inceptor hinge moments generate positive aerodynamic hinge moments (negative surface deflections).
- Consistent use of the above logic requires that the calculated value for aileron deflection be negative for right wing down moments. Similarly, differential ruddervator deflections generating nose right yawing moments should have negative values.

#### **Conventions for Positive Control Surface Deflections**

Parameter	Symbol	Flight Test	SFTE/ Wind Tunnel
Horizontal Stabilizer	$\delta_i$	TEU TED	
Elevator	$\delta_e$	TEU	TED
Elev. Tab	$\delta_{et}$	TED	
Stabilators or Rollerva-	$\delta_{eL}$ , $\delta_{eR}$	TEU	TED
tors, average:	$\delta_e$	$= (\delta_{eR} + \delta_{eL})/2$	
differential:	$\Delta\delta_e$	$= (\delta_{eR} - \delta_{eL})/2$	
T.	$\delta_{vL}$ , $\delta_{vR}$	TEU	TED
Elevons average: differential	$\delta_{v}$	$= (\delta_{vR} + \delta_{vL})/2$	
unicientiai	$\Delta\delta_{ u}$	$=(\delta_{vR}-\delta_{vL})/2$	
Flaperons or trailing	$\delta_{fR}$ , $\delta_{fL}$	TED	
edge flap average: differential:	$\delta_f$	$=(\delta_{fR}+\delta_{fL})/2$	
	$\Delta\delta_f$	$= - (\delta_{fR} - \delta_{fL})/2$	$= (\delta_{fR} - \delta_{fL})/2$

Conventions for Positive Control Surface Deflections (Cont'd)					
Parameter	Symbol	Flight Test	SFTE/ Wind Tunnel		
Canards	$\delta_{cL}$ , $\delta_{cR}$	TED			
average:	$\delta_c$	$=(\delta_{cR}$	$+\delta_{cL})/2$		
differential	$\Delta\delta_c$	$= - (\delta_{cR} - \delta_{cL})/2$	$= (\delta_{cR} - \delta_{cL})/2$		
Leading edge flap	$\delta_{\mathit{lefL}}$ , $\delta_{\mathit{lefR}}$	TED			
Average:	$\delta_{\mathit{lef}}$	$=(\delta_{cR}$	$+\delta_{cL})/2$		
Differential:	$\Delta\delta_{\mathit{lef}}$	$= - (\delta_{cR} - \delta_{cL})/2$	$= - (\delta_{cR} - \delta_{cL})/2$		
Duddomatora	$\delta_{rvL}$ , $\delta_{rvR}$	TEU	TED		
Ruddervators Average:	$\delta_{rv}$	$=(\delta_{rvR}$	$+\delta_{rvL})/2$		
Differential:	$\Delta\delta_{rv}$	$=$ - $(\delta_{rvR})$	- δ <sub>rvL</sub> )/2		
Ailerons	$\delta_{aL}$ , $\delta_{aR}$	$\delta_{aR}$ TEU, $\delta_{aL}$ TEDor { $\delta_{aR}$ , $\delta_{aL}$ TED}	$\delta_{aR,}  \delta_{aL}  TED$		
Aileron Tab Average:	$\delta_{at}$	$= (\delta_{aR} + \delta_{aL})/2$	$\delta_{at}$ TED		
Average.	$\delta_a$	$= - (\delta_{aR} - \delta_{aL})/2\}$	$= (\delta_{aR} - \delta_{aL})/2 *$		
	$\delta_{\scriptscriptstyle SL}$ , $\delta_{\scriptscriptstyle SR}$	Extended			
Spoilers average: Differential:	$\delta_{\!\scriptscriptstyle S}$	$= (\delta_{sR} + \delta_{sL})/2$			
	$\Delta d_s$	$= (\delta_{sR} - \delta_{sL})/2$	$= - (\delta_{sR} - \delta_{sL})/2$		
Rudders	$\delta_{rR}$ , $\delta_{rL}$	TER	TEL		
Average:	$\delta_r$	$= (\delta_{rR} + \delta_{rL})/2$			
Rudder tab	$\delta_{rt}$	TI	EL		
Speed brake	$\delta_{sb}$	Exte	Extended		
Conv	Conventions for Positive Inputs and Hinge Moments				
Parameter	Symbol	Flight Test	SFTE/ Wind Tunnel		
Stick/Wheel Long Force	F <sub>e</sub>	Pull			
Stick/Wheel Lateral Force	Fa	Rig	Right		
Pedal Force	$F_{r}$	Right pe	Right pedal push		
Stick/Wheel Long. deflectn	$\delta s_e$	Aft			

### **Conventions for Positive Inputs and Hinge Moments (Cont'd)**

Parameter	Symbol	Flight Test	SFTE <sup>#</sup>
Stick/wheel Lat. deflection	$\delta s_a$	Right	
Pedal deflection	$\delta_{pR,}\delta_{pL}$	Right pedal push	
Aerodynamic Hinge Moments	$C_{h\delta} \ C_{hlpha} \ C_{h\delta} \ C_{h\delta o} \ C_{h\delta tab}$	positive moments generate positive deflections	
Inceptor Hinge Moments	$egin{array}{c} C_{hFe} \ C_{hFa} \ C_{hFr} \end{array}$	+ moments generate + deflections	+ moments generate    - deflections

<sup>\*</sup>The wind tunnel rationale does not inherently define the polarity for control surface differential deflections.

#The wind tunnel rationale does not specify a convention for positive inputs or hinge moments. Historically, Dutch, U.S. and some British aircraft use a climbing right turn, while it is a diving left turn for Canadian, Australian, and some British aircraft.

The SFTE Technical Council recognizes that several combinations of the above possibilities are currently in use around the world, and invites comments, additions, or corrections to the above summary and proposal. Although SFTE does not expect all organizations to adopt this standard, it still **provides a cornerstone for reference purposes** 

### 1.7 Thermodynamics Relations (references 1.3, 1.4, 1.5, 1.6)

A **Process** is an event with a redistribution of energy within a system.

A **Reversible** process is one that can be reversed such that the system returns to its original state (form, location & amount).

An **Irreversible** process cannot return to its original state due to heat flow from higher to lower temperatures, fluid turbulence, friction, or inelastic deformation. The change in entropy is non-zero.

An **Isothermal** process is one in which the temperature of the fluid is constant.

An **Adiabatic** process is one in which heat is not transferred to or from the fluid.

Work is the energy transfer by way of changing mechanical energy.

**Heat** is the energy *transfer* from one body to another by virtue of a temperature difference between them.

An **Isentropic** process has constant entropy.

**Conduction** is the energy transfer from a warmer body by tangible contact (transfer of some internal molecular kinetic energy).

**Convection** is the repositioning the energy of a fluid without state changes or energy transformations (e.g. heated air moving from one room to another room).

**Radiation** is the energy transmission through space.

A = area

C = compressibility factor

C =speed of sound

E = u = specific internal energy (e.g. Btu /lb)

 $H = \text{specific enthalpy} \equiv E + PV \text{ (e.g. Btu/lb)}$ 

J = Joule's equivalent  $10^7$  ergs = 778 ft-lb/Btu

Q = energy supplied to a system or region as heat (e.g. Btu/lb)

 $P = absolute pressure (e.g. lbs/ft^2)$ 

 $V = \text{specific volume (e.g. } \text{ft}^3/\text{lb})$ 

W = work (+ if entering)

 $\overline{V}$  = velocity

 $\Delta$  = change (final – initial value)

Z = altitude

S = specific entropy  $\equiv \int \frac{dE + PdV}{T}$  for a reversible process

R = gas constant for each gas (for air =  $287 \text{ J/[kg K]} = 53.35 \text{ ft-lb/lb}_{m}\text{R}$ )

 $\overline{R} = R[M] = universal gas constant$ 

= 8.314 kJ/[kmol K] = 1545 ft lb/[lbmol R]

M = molar mass (for air = 28.97 kg/kmol)

N = number of moles

 $\rho$  = density

The **First Law of Thermodynamics** shows that the net amount of energy added to a system equals the net change in energy within the system (Principle of Conservation of Energy):  $W + Q = (E_2 - E_1)$ 

The **Second Law of Thermodynamics** states that entropy increases during any irreversible process:  $S_2 > S_1$ 

**Ideal Gas Equation of State** (a.k.a. Perfect gas law):

$$PV=RT$$
,  $P = \rho RT$ ,  $PV = mRT$ ,  $PV = nRT$ 

$$\delta = \sigma \theta$$
 where  $\delta P_a/P_o$ ,  $\sigma = \rho_a/\rho_o$ ,  $\theta = T_a/T_o$ 

**Boyle's Law** states that when the temperature of a given mass of gas is held constant, then the volume and pressure vary inversely.

**Charle's Law** states that when a volume of a given mass is held constant, then the change in pressure of the gas is proportional to the change in temperature.

**Real Gas** Relation: PV = CRT

for reversible processes

$$W = -\int P dV$$

$$Q = \int T dS$$

for reversible adiabatic process

$$\frac{P_1}{P_2} = \left[ \frac{V_2}{V_1} \right]^{\gamma}$$

$$\frac{T_1}{T_2} = \left\lceil \frac{V_2}{V_1} \right\rceil^{\gamma - 1}$$

$$\frac{T_1}{T_2} = \left\lceil \frac{P_1}{P_2} \right\rceil^{\frac{\gamma - 1}{\gamma}}$$

$$\frac{P_1}{P_2} = \left[ \frac{\rho_1}{\rho_2} \right]^{\gamma}$$

Steady Flow Energy Equation

$$Q+H_1+\frac{\overline{V}_1^2}{2g}+Z_1=W+H_2+\frac{\overline{V}_2^2}{2g}+Z_2$$

Bernoulli Equation:

$$\frac{\Delta P}{\rho g} + \frac{\overline{V}_2^2 - \overline{V}_1^2}{2g} + \Delta Z = 0$$

Flow per Unit Area:

$$\frac{W}{A} = \sqrt{\frac{\gamma}{R} \frac{P}{\sqrt{T}} \frac{M}{\left(1 + \frac{\gamma - 1}{2} M^2\right) \frac{\gamma + 1}{2(\gamma - 1)}}}$$

Velocity of sound in a perfect gas:

$$c = \sqrt{\gamma gRT}$$

## Development of Specific Heat Relations

$$c_p \equiv \frac{\partial H}{\partial T}\Big|_{P}$$
 specific heat at constant pressure (for air = 1004.76 J/[kg °K])

$$c_v = \frac{\partial u}{\partial T} \Big|_{v}$$
 specific heat at constant volume (for air = 717.986 J/[kg °K])

$$\kappa = \gamma \equiv \frac{c_p}{c_v}$$
 = ratio of specific heats

Enthalpy equation in differential form is: dH = du + d(PV)Substituting definitions and ideal gas law gives  $c_p dT = c_v dT + Rdt$  or  $c_p = c_v + R$ 

Rearranging gives 
$$c_p = R \frac{\kappa}{\kappa - 1}$$
 and  $c_v = \frac{R}{\kappa - 1}$ 

#### Development of **Poisson's Equation**:

- 1) From the 1st law:  $W+Q = E_2-E_1$
- 2) Substitution for each term gives T dS P dV = du
- 3) Divide through by T: dS = du/T + P dV/T
- 4) Recall  $du = c_v dT$  and PV = RT
- 5) Substitution gives  $dS = c_v dT/T + R dV/V$
- 6) Assume constant specific heat and integrate:

$$s_2 - s_1 = c_v \ln \frac{T_2}{T_1} + R \ln \frac{V_2}{V_1}$$

7) Assuming a reversible adiabatic process

$$c_v \ln \frac{T_2}{T_1} = -R \ln \frac{V_2}{V_1}$$

8) Substitute 
$$C_v = \frac{R}{\kappa - 1}$$
 to get:  $\frac{T_2}{T_1} = \left(\frac{V_1}{V_2}\right)^{\kappa - 1}$ 

- 9) Differentiate H: dH = du + P dV + V dP
- 10) Substitution into step #2: T dS = dH-V dP

11) Integrate: 
$$s_2 - s_1 = c_p \ln \frac{T_2}{T_1} + R \ln \frac{P_2}{P_1}$$

12) Assuming a reversible adiabatic process:  $c_p \ln \frac{T_2}{T_1} = -R \ln \frac{P_2}{P_1}$ 

13) Substitute 
$$c_p = R \frac{\kappa}{\kappa - 1}$$
 to get:  $\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{\frac{\kappa - 1}{\kappa}}$ 

14) Combine steps #8, #13 to  $\frac{P_2}{P_1} = \left(\frac{V_1}{V_2}\right)^{\kappa}$  get: or PV<sup> $\kappa$ </sup> = const.

#### 1.8 Mechanics Relations

#### **Abbreviations**

```
a = linear acceleration = dV/dt
a_r = centripetal (radial) acceleration
a_T = tangential acceleration
F = force
g = acceleration due to gravity (32.174 \text{ ft/s}^2 = 9.80 \text{ meters/s}^2)
G = moment
H = angular momentum = Iw
H = height
Hp = horsepower (Hp = 550ft-lbs/sec)
I = rotational moment of inertia (see section 10)
J = impulse = change in momentum
k = radius of gyration
m = mass
N_r = radial load factor = a_r/g
P = power = dW/dt
L = linear momentum = mV
Q = moment (a.k.a. torque)
r = radius
S = distance, displacement
s = seconds
t = time
V = true inertial velocity
V_o = initial inertial velocity
W = work = FS = \frac{1}{2} m [V^2 - V_o^2]
q = angular displacement
Vol = volume
\omega = angular velocity (radians/second)
\dot{\omega} = angular acceleration
```

#### **Newtons Laws**

# 1<sup>st</sup> law (law of inertia):

"Every body persists in its state of rest or uniform motion in a straight line unless it is compelled to change that state by forces impressed on it.

## 2<sup>nd</sup> Law:

"The change in motion is proportional to the motive force impressed and is made in the direction of the straight line in which that force is impressed" (motion defined as velocity *x* quantity of matter or linear momentum, mV).

$$dF = dmV/dt = (dm/dt) + (dV/dt)$$

For constant mass in rectilinear motion: F = ma

For constant mass distribution in curvilinear motion:  $G = \dot{\omega} I$ 

## 3<sup>rd</sup> Law:

"Every action has an equal and opposite reaction; or, the mutual attraction of two bodies upon each other are always equal and directed to contrary parts.[opposite directions]"

# Planar Kinetics, Work, Power and Energy

Rectilinear motion		Curvilinear motion	,
displacement	S	angular displacement	θ
velocity	V = dS/dt	angular velocity	$\omega = d\theta/dt$
acceleration	a = dV/dt	angular acceleration	$= \dot{\omega} d\omega/dt$
inertia	m	rotational inertia	$I = \int r^2 dm$
momentum	L = mV	angular momentum	$H = I \dot{\omega} \omega$
force	F = ma	torque	Q = I
work	$W = \int F dS$	work	$W = \int Q d\theta$
power kinetic energy potential energ		power kinetic energy n/a	$P = Q \omega$ <sup>1</sup> / <sub>2</sub> I $\omega$ <sup>2</sup>

#### **Planar Kinematics at Constant Acceleration**

#### Rectilinear motion Curvilinear motion

$$\begin{aligned}
\nabla &= V_0 + at & \omega &= \omega_0 + t \\
V^2 &= V_0^2 + 2aS & \omega^2 &= \omega_0^2 + 2 & \omega \\
S &= V_0 t + \frac{1}{2} at^2 & \theta &= \omega_0 t + \frac{1}{2} & \omega t^2
\end{aligned}$$

$$S &= \frac{1}{2}(V + V_0)t & \theta &= \frac{1}{2}(\omega + \omega_0)t \\
S &= (V^2 - V_0^2)/2a & \theta &= (\omega^2 - \omega_0^2)/2\dot{\omega} \\
t &= \frac{-V_0 + \sqrt{V_0^2 + 2aS}}{a} & t &= \frac{-\omega_0 + \sqrt{\omega_0^2 - 2\dot{\omega}\theta}}{\dot{\omega}} \\
a &= \frac{2(S - V_0 t)}{t^2} & \dot{\omega} &= \frac{2(\theta - \omega_0 t)}{t^2}
\end{aligned}$$

### Curvilinear motion with constant acceleration and radius:

$$r = V^{2}/gN_{r}$$

$$V = \omega r$$

$$N_{R} = a_{r}/g$$

$$\omega = gN_{r}/V$$

$$\dot{\omega} = \dot{V}/R$$

$$a_{r} = r\omega^{2} = V^{2}/r$$

$$a_{r} = \dot{\omega} r$$

#### Aircraft in level turn:

$$N_{zw}$$
 = load factor normal to flight path
$$r = \text{turn radius}$$

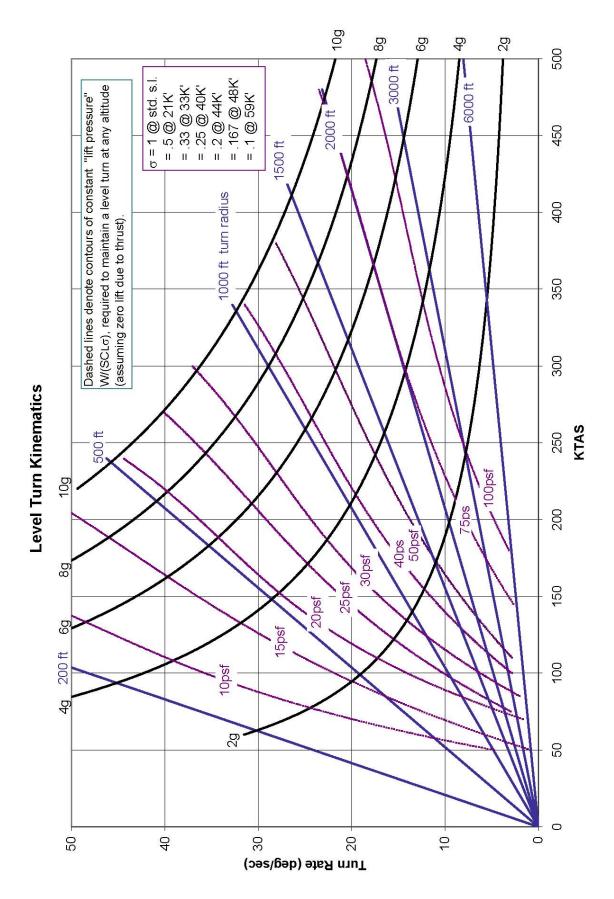
$$\Omega = \text{turn rate (rad/sec)}$$

$$r = \frac{V^2}{g\sqrt{(N_{zw})^2 - 1}}$$

$$\omega = \frac{g\sqrt{(N_{zw})^2 - 1}}{V}$$

$$N_{zw} = \sqrt{\left(\frac{\omega V}{g}\right)^2 + 1}$$

V= inertial velocity



Page 01-44

# **Gyroscopic Motion**

(reference 1.7)

for bodies spinning about an axisymmetric axis

 $\dot{\Psi}$  = spin rate

 $\phi$  = precession rate

 $\dot{\theta}$  = nutation rate

 $I_z$  = moment of inertia about spin axis

 $I_t$  = transverse moment of inertia about the spin point

(perpendicular to spin axis)

 $I_{cg}$  = moment of inertia about the cg (perpendicular to spin axis)

 $M_x$  = moment about spin point (acting along plane that defines  $\theta$ )

For steady precession (constant  $\theta$ ,  $\phi$ ,  $\psi$ )

$$\sum M_x = -I_t \dot{\phi}^2 \sin \theta \cos \theta + I_z \dot{\phi} \sin \theta \left( \dot{\phi} \cos \theta + \dot{\psi} \right)$$

For torque free motion (gravity is only external force)

$$\dot{\psi} = \frac{I_{cg} - I_z}{I_z} \dot{\phi} \cos \theta$$

note that  $I_{cg} > I_z$  yields regular precession while  $I_{cg} < I_z$  yields retrograde precession

# **Section 1.9 International Phonetic Alphabet and Morse Code**

A	Alpha	•—
В	Bravo	-•••
C	Charlie	<b></b> ·
D	Delta	<b>_··</b>
E	Echo	•
F	Foxtrot	••-•
G	Golf	•
Н	Hotel	• • • •
I	India	• •
J	Juliet	•
K	Kilo	<b>-·-</b>
L L	Lima	••
L M	Mike	
N	November	<b>_·</b>
O	Oscar	
P		••
	Papa	
Q	Quebec	••
R	Romeo	• • •
S T	Sierra Tango	_
U	Uniform	••-
V	Victor	•••
W	Whiskey	•
X	X-ray	<b>-··-</b>
Y	Yankee	
Z	Zulu	
1	One	•
2	Two	••
3	Three	•••-
4	Four	••••
5	Five	• • • •
6	Six	<b></b>
7	Seven	
8	Eight	•
9	Niner	
0	Zero	

#### **Section 1 References**

- 1.1 Anon., "Weight Engineers Handbook", Society of Weight Engineers, P.O.Box 60024 Los Angeles, CA 90060,1976.
- 1.2 Anon., "Aeronautical Vestpocket Handbook", United Technologies Pratt & Whitney Canada, 1000 Marie Victorin Blvd. E. P.O.B. 10 Longueuil, Quebec Canada J4K 4X9.
- 1.3 Jones, J. P., Hawkins, G.A., "Engineering Thermodynamics" John Wiley & Sons, 1960.
- 1.4 Esbach, Ovid W., "Handbook of Engineering Fundamentals", John Wiley and Sons Inc., 1963.
- 1.5 Potter, M.C., Somerton, C.W., "Engineering Thermodynamics" Shaum's Outline Series, McGraw-Hill, Inc.,1993.
- 1.6 Abbott, M. M., Van Ness, H. C., "Thermodynamics", Shaum's Outline Series, McGraw-Hill, Inc., 1989.
- 1.7 Halliday, D., Resnick, R., "Fundamentals of Physics", John Wiley & Sons, New York, 1981.
- 1.8 Roberts, S.C., *Chapter 3 Aircraft Control Sytems*, "Aircraft Flying Qualities Testing", National Test Pilot School, 1997. P.O.B. 658, Mojave, CA, 93501.

## **NOTES**