

Section 3 Universe/Earth/Atmospheric Properties

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Section 3 Recurring Nomenclature

H_p = pressure altitude. The pressure associate with geopotential altitude on a standard day.

T = absolute temperature (Rankin or Kelvin)

T_R = absolute temperature, Rankin scale

T_o = standard day seal level absolute temperature

P = ambient pressure

P_o = standard day seal level ambient pressure

ρ = ambient density

ρ_o = standard day seal level ambient density

$\delta = P/P_o$ = atmospheric pressure/std day sea level pressure

$\theta = T/T_o$ = atmospheric absolute temp / std day sea level absolute temp

$\sigma = \rho/\rho_o$ = atmospheric density/std day sea level density

g = acceleration due to gravity

g_o = standard earth acceleration due to gravity

a_o = speed of sound at std day sea level temperature

Section 3.1 Universal Constants (reference 3.1)

| | | |
|--|---------------------------|----------------------------------|
| Avogadro's number, N_o | 6.022169×10^{23} | molecules/mole |
| Boltzmann constant, k | 1.380×10^{-23} | J/°K |
| electron charge, e | $1,602 \times 10^{-19}$ | coulomb |
| electron mass, m_e | 9.109×10^{-31} | kg |
| gas constant, R | 8.31434 J/°K | mole |
| gravitational constant, G | 6.673×10^{-11} | Nm ² /kg ² |
| neutron mass, m_n | 1.674×10^{-27} | kg |
| Planck constant, h | 6.625×10^{-34} | J sec |
| proton mass, m_p | 1.672×10^{-27} | kg |
| speed of light in a vacuum, c | 2.998×10^8 | m/sec |
| unified atomic mass constant, m_u | 1.660×10^{-27} | kg |
| volume of ideal gas (std temp & press) | 2.241×10 | m ³ /mol |

Newtonian Gravity

The gravitational field (g) near any mass can be calculated as

$$g = \frac{GM}{(R_A)^2}$$

where G is the universal gravitational constant and R_A is the absolute distance from the center of mass M

Section 3.2 Earth Properties (references 3.9.2, 3.9.3)

Std Earth gravitational acceleration, $g_0 = 9.8066 \text{ m/s}^2 = 32.174 \text{ ft/s}^2$

mass = $5.9722 \times 10^{24} \text{ kg} = 13.22 \times 10^{24} \text{ lb}$

rotation rate, $\omega = 7.292115 \times 10^{-5} \text{ rad/sec}$

average density = $5.522 \text{ g/cm}^3 = 344.7 \text{ lb/ft}^3$

radius average, $R_{avg} = 6,367,444 \text{ m} = 3956.538 \text{ st. miles} = 20,890,522 \text{ ft}$

radius at the equator (R_e) is $6,378,137 \text{ m} (\pm 2)$

radius at the poles $R_p = 6,356,752 \text{ [m]}$

radius as a function of latitude, ϕ (assumes perfect ellipsoid):

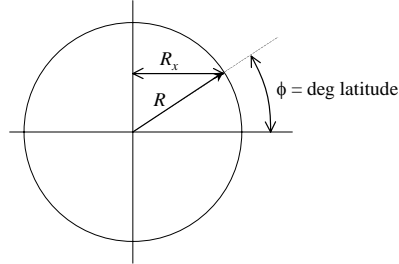
$$R = \left[\left(\frac{\cos \phi}{R_e} \right)^2 + \left(\frac{\sin \phi}{R_p} \right)^2 \right]^{-\frac{1}{2}}$$

Centrifugal Relief from Gravity

The earth's "normal" gravity field includes both the Newtonian Law and a correction for the centrifugal force caused by the earth's rotation. The centrifugal relief correction is

$$\Delta CR = -\frac{V^2}{R_x} = -\frac{(R_x \omega)^2}{R_x} = R_x \omega^2$$

where ω is the earth's rotation rate and R_x is the perpendicular distance from the earth's axis to the surface and can be calculated as $R_x = R \cos \phi$ (see figure below).



For any centrifugal relief calculations associated with aircraft performance, it is sufficiently exact ($g \pm 0.00004 \text{ m/s}^2$) to use the average earth radius. An aircraft flying eastward contributes to centrifugal relief while a west-bound aircraft diminishes it.

The International Association of Geodesy publishes the following equation (accurate to 0.005%) to calculate local sea level gravity including the effects of centrifugal relief for any point fixed to the earth's surface

$$g_{sl} = 9.780327 \left(1 + 0.00530224 \sin^2 \phi - 0.000058 \sin^2 2\phi \right) \left[\frac{m}{s^2} \right]$$

The above equation is tabulated below for quick reference.

| Latitude (deg) | Normal g_{local} | |
|-------------------|--------------------|--------------|
| | (m/s^2) | (ft/s^2) |
| 0 | 9.780327 | 32.088 |
| 15 | 9.783659 | 32.098 |
| 30 | 9.792866 | 32.188 |
| 45 | 9.805689 | 32.171 |
| 60 | 9.818795 | 32.214 |
| 75 | 9.828569 | 32.249 |
| 90 | 9.832185 | 32.258 |

The standard acceleration (g_o) corresponds to a latitude of 46.0625° . g_{sl} at the equator and the poles varies $\pm 0.27\%$ from g_o .

Altitude Effect on Gravitational Acceleration

R_A is the sum of the earth's local radius and the geometric distance (h_G) above the surface: $R_A = R + h_G$

Gravitational acceleration at any geometric altitude:

| h_G (1000 ft) | $\frac{g_{alt}}{g_{sl}}$ |
|--------------------|--------------------------|
| 0 | 1 |
| 10 | 0.99904 |
| 20 | 0.99809 |
| 40 | 0.99618 |
| 60 | 0.99428 |
| 80 | 0.99238 |
| 100 | 0.99049 |

$$g_{alt} = g_{sl} \left(\frac{R}{R + h_G} \right)^2$$

Actual Gravitational Pull on an Aircraft

Adding a centrifugal relief correction due to the aircraft's velocity, a complete calculation for its gravitational acceleration is

$$g_{A/C} = \left[g_{isl} + \omega^2 R \cos \phi \right] \left[\frac{R}{R + h_G} \right]^2 - \left(\omega + \frac{V_G \sin \sigma}{R + h_G} \right)^2 (R + h_G) \cos \phi$$

where V_G = ground speed and σ = ground track angle (0° = true North, 90° = East, etc.).

Gravity Influence on Aircraft Cruise Performance

Even at the same altitude, changes in gravity due to latitude or centrifugal relief directly alter the required lift, drag, and fuel flow. For example, with sufficiently precise instrumentation, data collected heading West could show about 0.5% more drag and fuel flow than data collected heading East (centrifugal relief effect). After determining test and standard (or mission) values for g , flight test values for C_L , C_D , drag, and fuel flow can be corrected to standard as follows:

$$C_{L_{std}} = C_{L_t} \frac{N_{z_{std}}}{N_{z_{eq}}} \left[\frac{g_{std}}{g_{A/C}} \right]$$

$$C_{D_{std}} = \frac{(C_{L_{std}})^2}{\pi A R e}$$

$$\Delta D = D_{std} - D_t = qS [C_{D_{std}} - C_{D_t}]$$

$$\dot{W}_{f_{std}} = \dot{W}_{f_t} + \Delta D \cdot TSFC$$

where N_z = normal load factor,

C_L = lift coefficient, C_D = drag coefficient,

AR = aspect ratio, e = Oswald efficiency factor,

ΔD change in drag force,

$TSFC$ = thrust specific fuel consumption, and

$\dot{W}_{f_{std}}$ = standard day fuel flow

Section 3.3 General Properties of Air (reference 3.9.1)

$$\begin{aligned}\text{Gas constant, } R &= 53.35 \text{ ft lb/R lbm} = 287.074 \text{ J/kg K} \\ &= 1716 \text{ lb(ft)/slgs(R)} = 3089.7 \text{ lb(ft)/slgs(K)}\end{aligned}$$

$$\begin{aligned}\text{Speed of sound} &= a_o(\theta)^{1/2} \\ &= 49.02 (T_R)^{1/2} \text{ ft/sec} \\ &= 33.42 (T_R)^{1/2} \text{ miles/hr} \\ &= 29.04 (T_R)^{1/2} \text{ knots} \\ &= 20.05 (T_R)^{1/2} \text{ m/sec}\end{aligned}$$

$$\text{Density, } \rho = .0023769 \text{ slug/ft}^3 = 1.225 \text{ kg/m}^3 \text{ (at } 15^\circ \text{ C)}$$

$$\text{Specific weight, } g_\rho = .07647 \text{ sec}^2/\text{ft}^4$$

Specific heat capacity at 59°F ($=T_o$)

$$\text{at constant pressure, } c_p = .240 \text{ BTU/lb R} = 1004.76 \text{ J/kg K}$$

$$\text{at constant volume, } c_v = .1715 \text{ BTU/lb R} = 717.986 \text{ J/kg K}$$

$$\text{specific heat ratio, } \gamma = \{c_p / c_v\} = 1.4$$

Normal Composition of clean, dry atmospheric air near sea level

| | |
|------------------------|--------------------|
| Nitrogen, N_2 | 78.084 % by volume |
| Oxygen, O_2 | 20.948 % |
| Argon, A | 0.934 % |
| Carbon Dioxide, CO_2 | 0.031 % |
| Neon, Ne | <u>0.002 %</u> |
| total | 99.9988 % |

plus traces of helium, krypton, xenon, hydrogen, methane, nitrous oxide, ozone, sulfur dioxide, nitrogen dioxide, ammonia, carbon monoxide, and iodine.

Viscosities of Air

$$\text{Coefficient of Viscosity, } \mu_c = \frac{7.3025 \times 10^{-7} (T_R)^{3/2}}{T_R + 198.72} \text{ lb/ft sec}$$

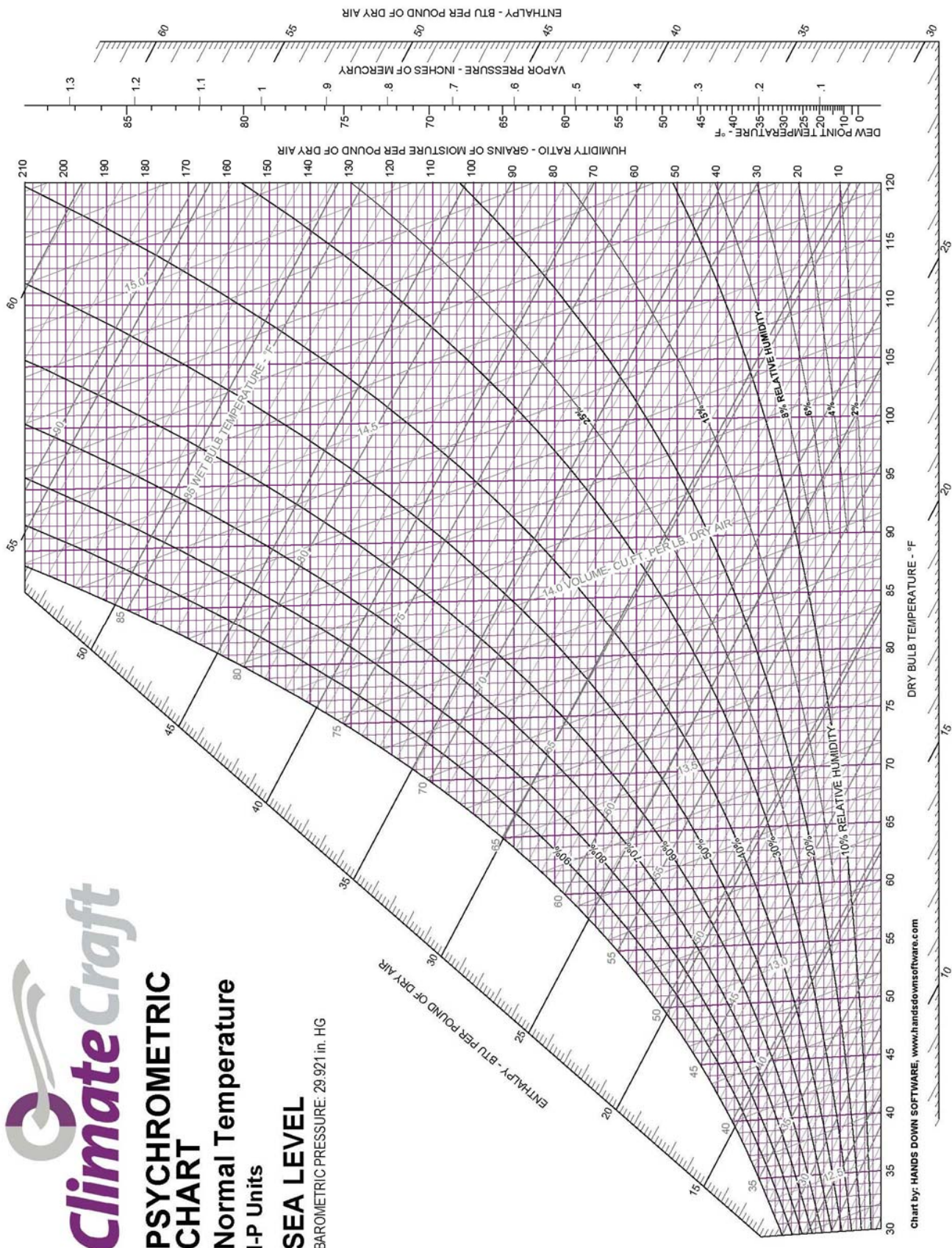
Kinematic viscosity, $\nu = \frac{\mu_c}{g\rho}$ ft²/sec

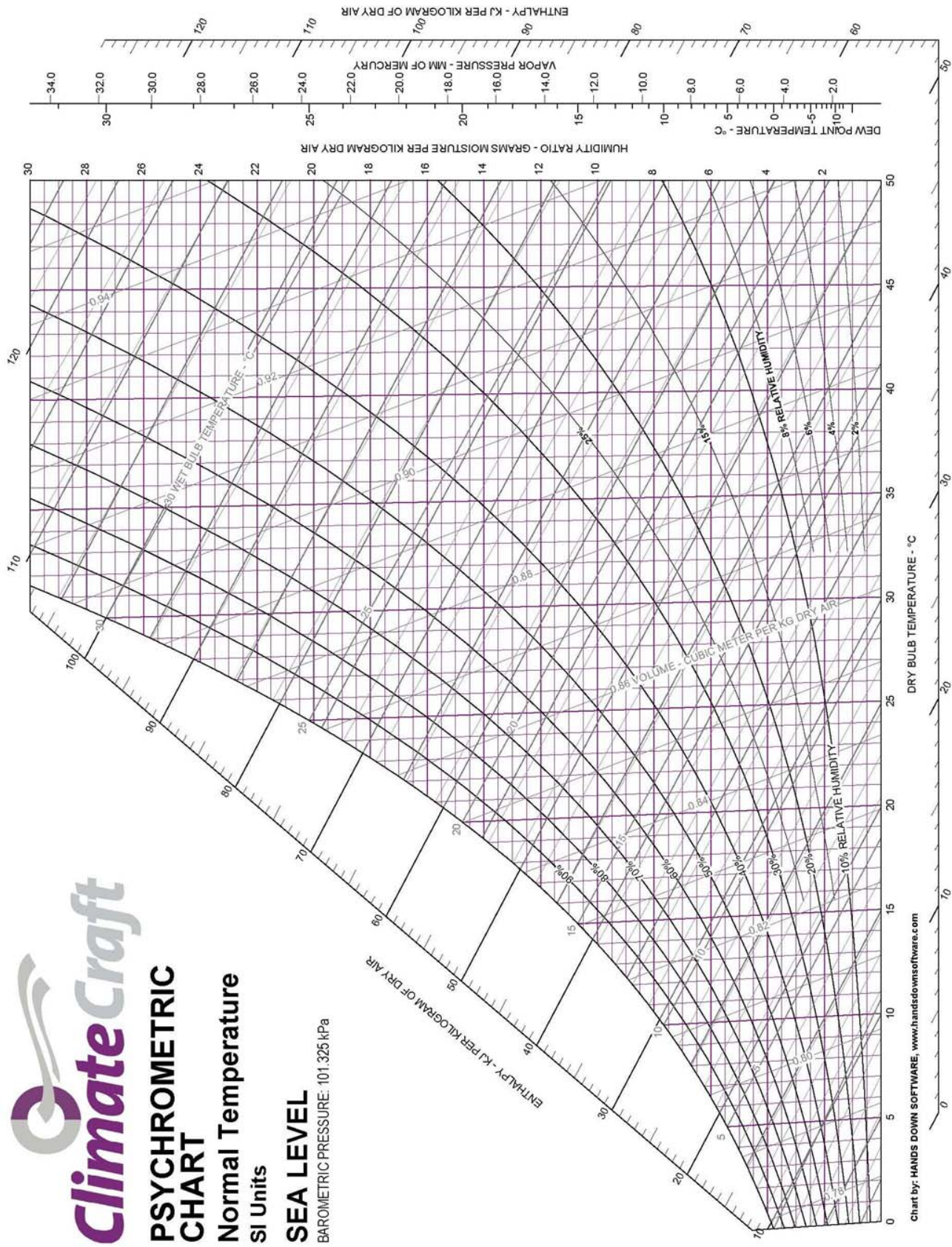
Absolute Viscosity, lb $\mu = \rho\nu = \left[.317(T_R)^{3/2} \left(\frac{734.7}{T_R + 216} \right) \right] \times 10^{-10}$ sec/ft²

Atmospheric Viscosity (U.S. Standard Atmosphere)

| Pressure Altitude <i>ft</i> | Kinematic Viscosity ν (<i>ft²/sec</i>) | Absolute Viscosity μ (<i>lb sec/ft²</i>) |
|--------------------------------|--|--|
| 0 | 1.572 x 10 ⁻⁴ | 3.737 x 10 ⁻⁷ |
| 5,000 | 1.776 | 3.638 |
| 10,000 | 2.013 | 3.538 |
| 15,000 | 2.293 | 3.435 |
| 20,000 | 2.625 | 3.330 |
| 25,000 | 3.019 | 3.224 |
| 30,000 | 3.493 | 3.115 |
| 35,000 | 4.065 | 3.004 |
| 40,000 | 5.074 | 2.981 |
| 45,000 | 6.453 | 2.982 |
| 50,000 | 8.206 | 2.983 |
| 55,000 | 10.44 | 2.985 |
| 60,000 | 13.27 | 2.986 |
| 70,000 | 21.69 | 3.005 |
| 80,000 | 35.75 | 3.043 |
| 90,000 | 58.53 | 3.080 |
| 100,000 | 95.19 | 3.118 |
| 150,000 | 1066 | 3.572 |
| 200,000 | 6880 | 3.435 |

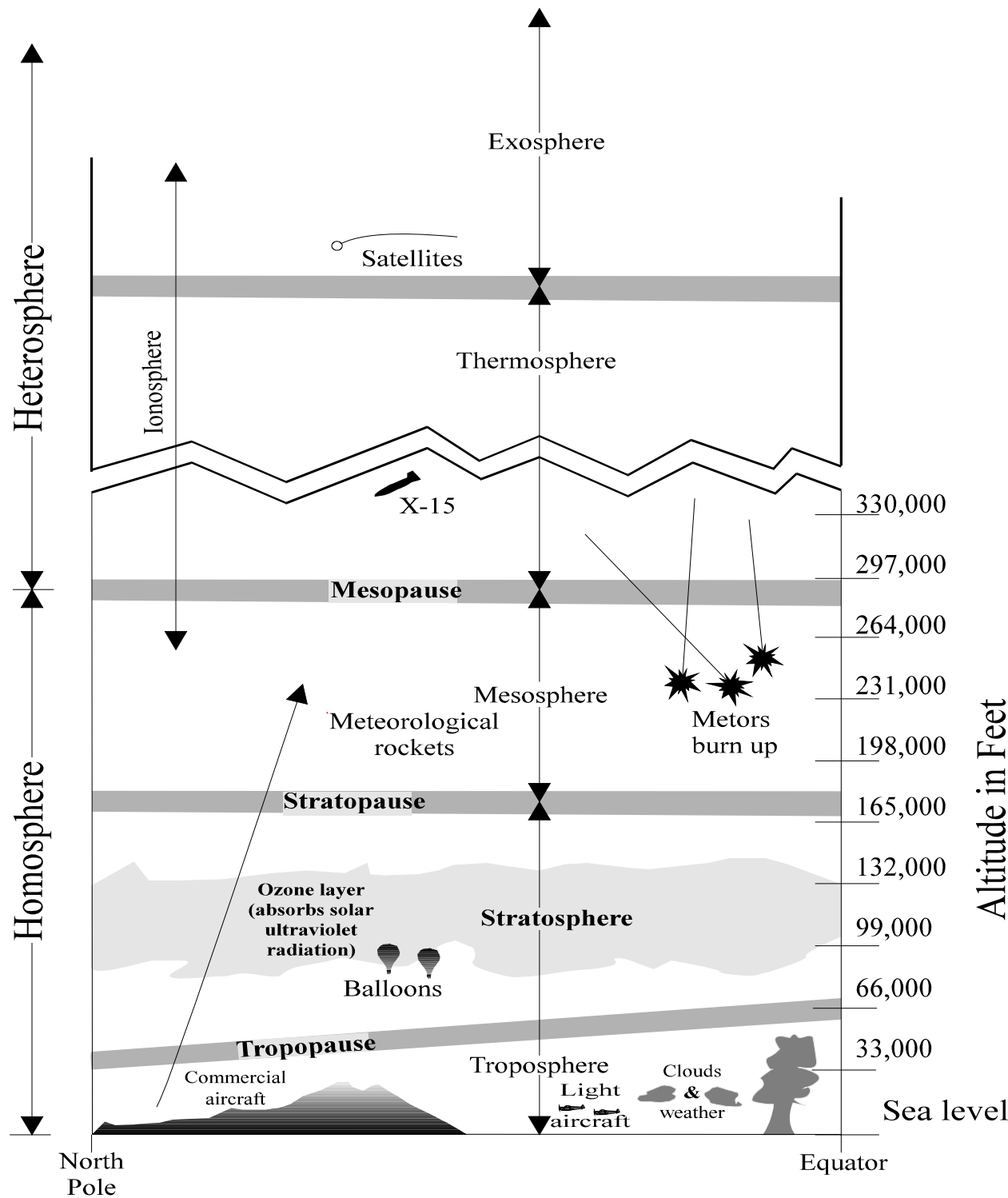
Psychrometric Chart for Seal Level Barometric Pressure





Section 3.4 Standard Atmosphere

Divisions of the Atmosphere



Constantly changing atmospheric conditions cannot be duplicated at will to provide the exact environment in which a flight takes place. A standard atmosphere provides a common basis to relate all flight test, wind tunnel results, aircraft design and general performance. Several models of “standard atmosphere” exist with minor differences based on mathematical constants used in the calculations.

Geometric altitude, h_G , is defined as the height of an aircraft above sea level (also called **tapeline** altitude)

Absolute altitude, h_a , is defined as the height of an aircraft above the center of the earth: (geometric altitude + radius of the earth).

Geopotential altitude, h , is required because g changes with height. If potential energy is calculated using sea level weight ($W_{SL} = mg_o$) instead of actual weight ($W = mg$), then the altitude must be lower.

$$W h_G = W_{SL} h$$

Pressure altitude, H_p is the altitude, on a standard day, at which the test day pressure would be found

Density altitude is the altitude, on a standard day, at which the test day density would be found

Temperature altitude is the altitude, on a standard day, at which the test day temperature would be found

Assumptions on which the standard atmosphere is built

1. The air is dry (only 0.4% per volume of water vapor)
2. The air is a perfect gas and obeys the equation of state,

$$P = \rho g R T$$

where $R = 53.35 \text{ ft lb/}^\circ\text{R lbm}$
3. The gravitational field decreases with altitude
4. Hydrostatic equilibrium exists ($\Delta p = -\rho g_o \Delta h$)

Standard Day Sea Level Atmospheric Conditions

$$P_o = 2116.22 \text{ lb/ft}^2 = 14.696 \text{ lb/in}^2 = 29.921 \text{ in Hg} \\ = 1013.25 \text{ HPa (mb)} = 101325 \text{ Pa}$$

$$T_o = 288.15 \text{ K} = 518.67 \text{ R} = 59^\circ \text{F} = 15^\circ \text{C}$$

$$\rho_o = 0.0023769 \text{ slugs/ft}^3 = 0.07647 \text{ lbm/in}^3 = 1.255 \text{ kg/m}^3 \text{ (at } 15^\circ \text{ C)}$$

$$a_o = 1116.45 \text{ ft/sec} = 661.478 \text{ KTAS} = 761.14 \text{ mph} = 340.294 \text{ m/sec}$$

$$g_o = 32.174 \text{ ft/sec}^2 = 9.80665 \text{ m/sec}^2$$

$$L = \text{standard temperature lapse rate} = 0.0019812 \text{ K /ft}$$

1976 U.S Standard Atmosphere Equations

Troposphere - below 36,089 ft (11,000 m) < 22636 Pa

$$\theta = 1 - (L/T_o) h = 1 - (6.8755856 \times 10^{-6}) h$$

$$\sigma = \theta^{n-1}$$

$$\delta = \theta^n$$

where $n = 5.255876$, h = geopotential altitude (ft)

Stratosphere- between 36,089 ft and 65,616 ft (20,000 m) the standard day temperature is a constant 216.65 K, therefore:

$$\theta = 0.751865$$

$$\sigma = .297076 e^{-0.000048063 [h-36,089]}$$

$$\delta = .223361 e^{-0.000048063 [h-36,089]}$$

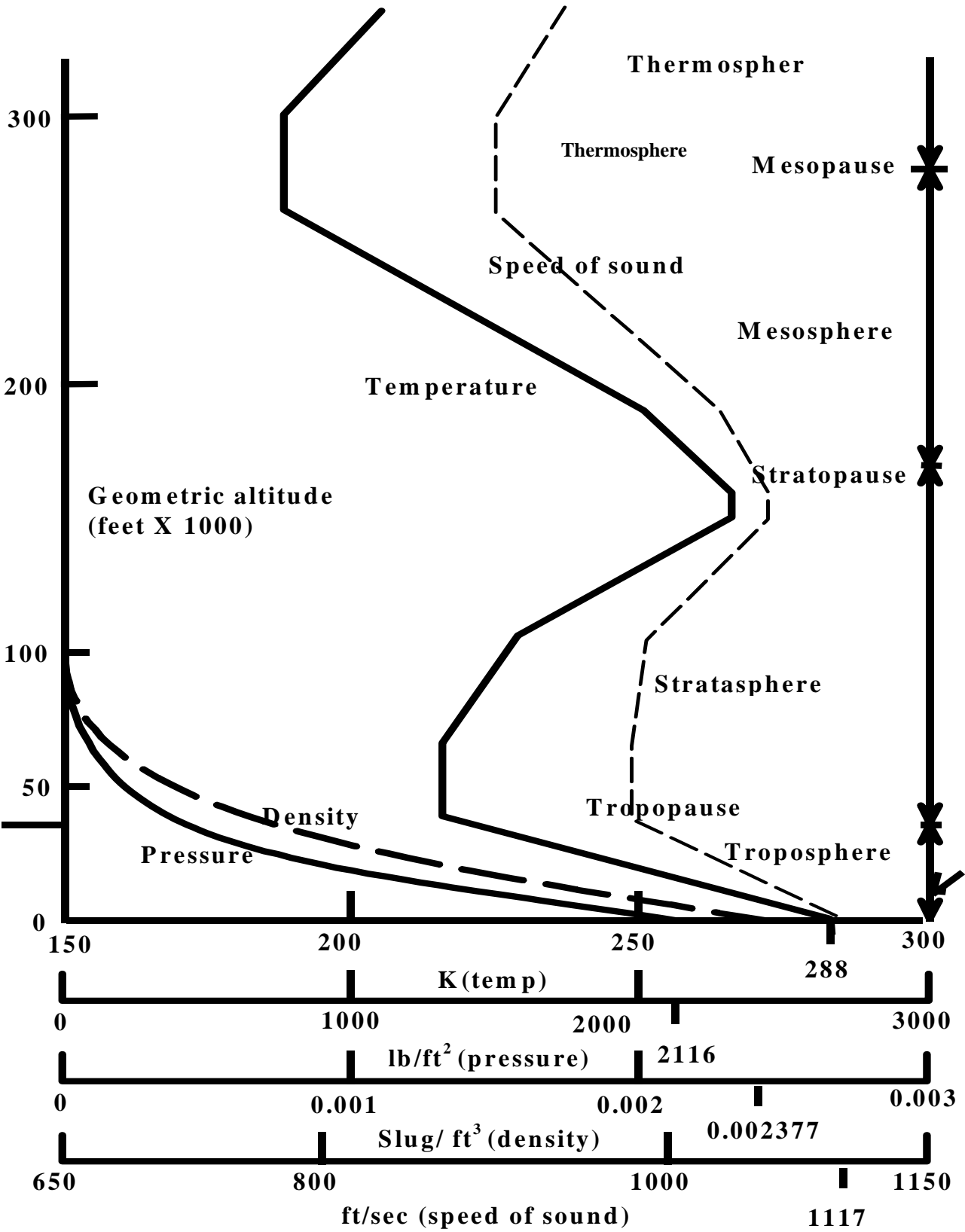
The above relations characterize the standard atmosphere table in this handbook. They may be re-written to solve for pressure altitude (H_p) for any ambient pressure. Below the tropopause (ambient pressure greater than 472.683 psf or 22632 Pa)

$$H_p [\text{ft}] = [1 - (P_a/P_o)^{0.1902632}] / [6.8755856 \times 10^{-6}]$$

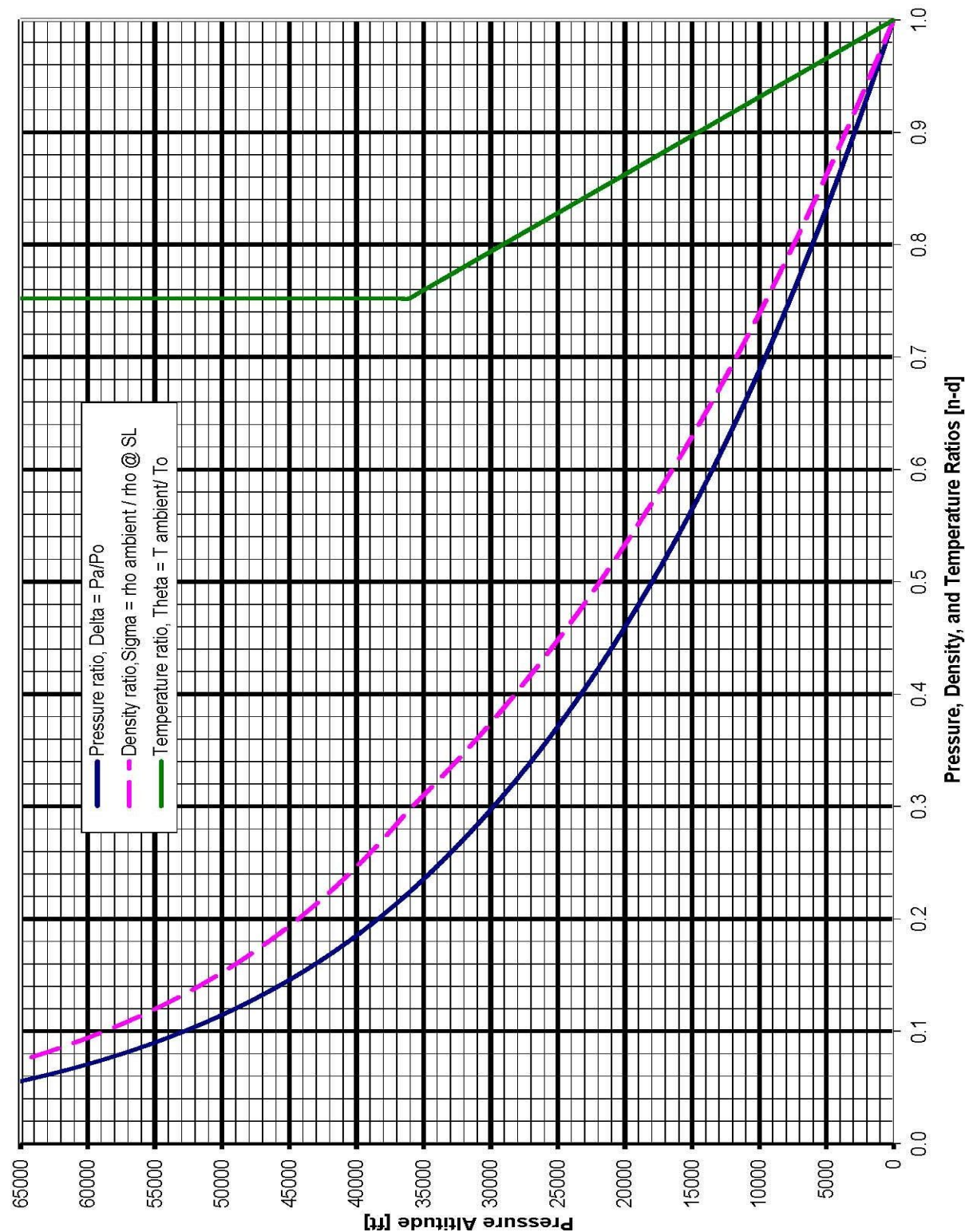
In the troposphere (ambient pressure between 114.347 and 472.683 psf or between 5475 and 22632.1 Pascal)

$$H_p [\text{ft}] = 36089 + [\ln(P_a/P_o) + 1.498966] / 0.000048063$$

1976 U.S. Standard Atmosphere Graph



1976 U.S. Standard Atmosphere



1976 U.S. Standard Atmosphere - Below Tropopause [<11 Km]

| Hp [ft] | | Ambient Air Pressure (P _a) | | | | | P _o = 14.696 | | P _o = 2116.22807 | | P _o = 101325 | | P _o = 29.92126 | | ρ _o = .0023769 | | ρ _o = 1.225 | | Ambient Air Temperature (T _a) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---------|--|--|----------|-----------|-----------|----------|-------------------------|-----------|-----------------------------|---------|-------------------------|--------|---------------------------|--------|---------------------------|--|------------------------|--------|---|--|--|---------|--|--|--|--|---------------------------------------|--|--|--|--|------------------------|--|--|--|--|----------------------|--|--|--|--|-------------------------|--|--|--|--|-----|--|--|--|--|---------|--|--|--|--|-----|--|--|--|--|---------|--|--|--|--|
| | | δ (=Pa/Po) | | | | | [psi] | | | | | [psf] | | | | | [Pa] | | | | | [in Hg] | | | | | σ (= ρ _a /ρ _o) | | | | | [slg/ft ³] | | | | | [kg/m ³] | | | | | θ (=Ta/T _o) | | | | | [K] | | | | | [deg C] | | | | | [R] | | | | | [deg F] | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| -1000 | | 1.036670 | 15.23490 | 2193.8300 | 105040.58 | 31.01847 | 1.029591 | 0.0024472 | 1.261249 | 1.00688 | 290.131 | 16.98 | 522.24 | 62.57 | 288.15 | | 15.00 | 518.67 | 59.00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0 | | 1.000000 | 14.69600 | 2116.2281 | 101325.00 | 29.92126 | 1.000000 | 0.0023769 | 1.225000 | 1.00000 | 288.150 | 15.00 | 518.67 | 59.00 | 288.15 | | 15.00 | 518.67 | 59.00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1000 | | 0.964388 | 14.17264 | 2040.8640 | 97716.57 | 28.85569 | 0.971064 | 0.0023081 | 1.189554 | 0.99312 | 286.169 | 13.02 | 515.10 | 55.43 | 286.169 | | 13.02 | 515.10 | 55.43 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2000 | | 0.929809 | 13.66447 | 1967.6881 | 94212.91 | 27.82106 | 0.942773 | 0.0022409 | 1.154897 | 0.98625 | 284.188 | 11.04 | 511.54 | 51.87 | 284.188 | | 11.04 | 511.54 | 51.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3000 | | 0.896241 | 13.17116 | 1896.6514 | 90811.67 | 26.81668 | 0.915117 | 0.0021751 | 1.121019 | 0.97937 | 282.206 | 9.06 | 507.97 | 48.30 | 282.206 | | 9.06 | 507.97 | 48.30 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4000 | | 0.863662 | 12.69238 | 1827.7057 | 87510.55 | 25.84185 | 0.888086 | 0.0021109 | 1.087906 | 0.97250 | 280.225 | 7.08 | 504.41 | 44.74 | 280.225 | | 7.08 | 504.41 | 44.74 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5000 | | 0.832048 | 12.22778 | 1760.8036 | 84307.27 | 24.89593 | 0.861671 | 0.0020481 | 1.055546 | 0.96562 | 278.244 | 5.09 | 500.84 | 41.17 | 278.244 | | 5.09 | 500.84 | 41.17 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6000 | | 0.801378 | 11.77705 | 1695.8984 | 81199.62 | 23.97824 | 0.835860 | 0.0019868 | 1.023929 | 0.95875 | 276.263 | 3.11 | 497.27 | 37.60 | 276.263 | | 3.11 | 497.27 | 37.60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7000 | | 0.771630 | 11.33987 | 1632.9442 | 78185.37 | 23.08813 | 0.810645 | 0.0019268 | 0.993040 | 0.95187 | 274.282 | 1.13 | 493.71 | 34.04 | 274.282 | | 1.13 | 493.71 | 34.04 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 8000 | | 0.742782 | 10.91592 | 1571.8959 | 75262.38 | 22.22497 | 0.786016 | 0.0018683 | 0.962870 | 0.94500 | 272.300 | -0.85 | 490.14 | 30.47 | 272.300 | | -0.85 | 490.14 | 30.47 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 9000 | | 0.714814 | 10.50490 | 1512.7089 | 72428.50 | 21.38813 | 0.761964 | 0.0018111 | 0.933406 | 0.93812 | 270.319 | -2.83 | 486.57 | 26.90 | 270.319 | | -2.83 | 486.57 | 26.90 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10000 | | 0.687705 | 10.10651 | 1455.3396 | 69681.66 | 20.57699 | 0.738479 | 0.0017553 | 0.904637 | 0.93124 | 268.338 | -4.81 | 483.01 | 23.34 | 268.338 | | -4.81 | 483.01 | 23.34 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 11000 | | 0.661434 | 9.72043 | 1399.7449 | 67019.78 | 19.79093 | 0.715552 | 0.0017008 | 0.876551 | 0.92437 | 266.357 | -6.79 | 479.44 | 19.77 | 266.357 | | -6.79 | 479.44 | 19.77 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 12000 | | 0.635982 | 9.34639 | 1345.8825 | 64440.85 | 19.02938 | 0.693173 | 0.0016476 | 0.849137 | 0.91749 | 264.376 | -8.77 | 475.88 | 16.21 | 264.376 | | -8.77 | 475.88 | 16.21 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 13000 | | 0.611329 | 8.98409 | 1293.7108 | 61942.87 | 18.29172 | 0.671334 | 0.0015957 | 0.822384 | 0.91062 | 262.394 | -10.76 | 472.31 | 12.64 | 262.394 | | -10.76 | 472.31 | 12.64 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14000 | | 0.587455 | 8.63324 | 1243.1889 | 59523.88 | 17.57740 | 0.650025 | 0.0015450 | 0.796281 | 0.90374 | 260.413 | -12.74 | 468.74 | 9.07 | 260.413 | | -12.74 | 468.74 | 9.07 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15000 | | 0.564342 | 8.29357 | 1194.2766 | 57181.96 | 16.88583 | 0.629238 | 0.0014956 | 0.770816 | 0.89687 | 258.432 | -14.72 | 465.18 | 5.51 | 258.432 | | -14.72 | 465.18 | 5.51 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 16000 | | 0.541971 | 7.96481 | 1146.9344 | 54915.22 | 16.21646 | 0.608963 | 0.0014474 | 0.745979 | 0.88999 | 256.451 | -16.70 | 461.61 | 1.94 | 256.451 | | -16.70 | 461.61 | 1.94 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 17000 | | 0.520324 | 7.64668 | 1101.1234 | 52721.79 | 15.56874 | 0.589191 | 0.0014004 | 0.721759 | 0.88312 | 254.470 | -18.68 | 458.05 | -1.62 | 254.470 | | -18.68 | 458.05 | -1.62 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 18000 | | 0.499382 | 7.33891 | 1056.8054 | 50599.84 | 14.94213 | 0.569915 | 0.0013546 | 0.698145 | 0.87624 | 252.488 | -20.66 | 454.48 | -5.19 | 252.488 | | -20.66 | 454.48 | -5.19 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 19000 | | 0.479427 | 7.04126 | 1013.9430 | 48547.59 | 14.33610 | 0.551124 | 0.0013100 | 0.675127 | 0.86936 | 250.507 | -22.64 | 450.91 | -8.76 | 250.507 | | -22.64 | 450.91 | -8.76 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 20000 | | 0.459544 | 6.75345 | 972.4992 | 46563.26 | 13.75013 | 0.532812 | 0.0012664 | 0.652694 | 0.86249 | 248.526 | -24.62 | 447.35 | -12.32 | 248.526 | | -24.62 | 447.35 | -12.32 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 21000 | | 0.440613 | 6.47525 | 932.4379 | 44645.13 | 13.18370 | 0.514968 | 0.0012240 | 0.630836 | 0.85561 | 246.545 | -26.61 | 443.78 | -15.89 | 246.545 | | -26.61 | 443.78 | -15.89 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 22000 | | 0.422319 | 6.20640 | 893.7235 | 42791.48 | 12.63632 | 0.497585 | 0.0011827 | 0.609542 | 0.84874 | 244.564 | -28.59 | 440.21 | -19.46 | 244.564 | | -28.59 | 440.21 | -19.46 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 23000 | | 0.404645 | 5.94666 | 856.3211 | 41000.65 | 12.10749 | 0.480655 | 0.0011425 | 0.588802 | 0.84186 | 242.582 | -30.57 | 436.65 | -23.02 | 242.582 | | -30.57 | 436.65 | -23.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 24000 | | 0.387575 | 5.69580 | 820.1964 | 39271.00 | 11.59672 | 0.464169 | 0.0011033 | 0.568607 | 0.83499 | 240.601 | -32.55 | 433.08 | -26.59 | 240.601 | | -32.55 | 433.08 | -26.59 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 25000 | | 0.371092 | 5.45357 | 785.3157 | 37600.92 | 11.10355 | 0.448119 | 0.0010651 | 0.548946 | 0.82811 | 238.620 | -34.53 | 429.52 | -30.15 | 238.620 | | -34.53 | 429.52 | -30.15 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 26000 | | 0.355182 | 5.21975 | 751.6460 | 35988.81 | 10.62749 | 0.432497 | 0.0010280 | 0.529809 | 0.82123 | 236.639 | -36.51 | 425.95 | -33.72 | 236.639 | | -36.51 | 425.95 | -33.72 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 27000 | | 0.339829 | 4.99412 | 719.1548 | 34433.13 | 10.16810 | 0.417296 | 0.0009919 | 0.511187 | 0.81436 | 234.658 | -38.49 | 422.38 | -37.29 | 234.658 | | -38.49 | 422.38 | -37.29 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 28000 | | 0.325017 | 4.77645 | 687.8104 | 32932.36 | 9.72492 | 0.402506 | 0.0009567 | 0.493070 | 0.80748 | 232.676 | -40.47 | 418.82 | -40.85 | 232.676 | | -40.47 | 418.82 | -40.85 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 29000 | | 0.310733 | 4.56653 | 657.5815 | 31485.00 | 9.29752 | 0.388121 | 0.0009225 | 0.475448 | 0.80061 | 230.695 | -42.45 | 415.25 | -44.42 | 230.695 | | -42.45 | 415.25 | -44.42 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 30000 | | 0.296961 | 4.36414 | 628.4375 | 30089.59 | 8.88545 | 0.374133 | 0.0008893 | 0.458312 | 0.79373 | 228.714 | -44.44 | 411.69 | -47.98 | 228.714 | | -44.44 | 411.69 | -47.98 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

1976 U.S. Standard Atmosphere - Below Tropopause [<11 Km][illegible]

Standard Atmosphere Calculator Website Link
<http://www.digitaldutch.com/atmoscalc/>

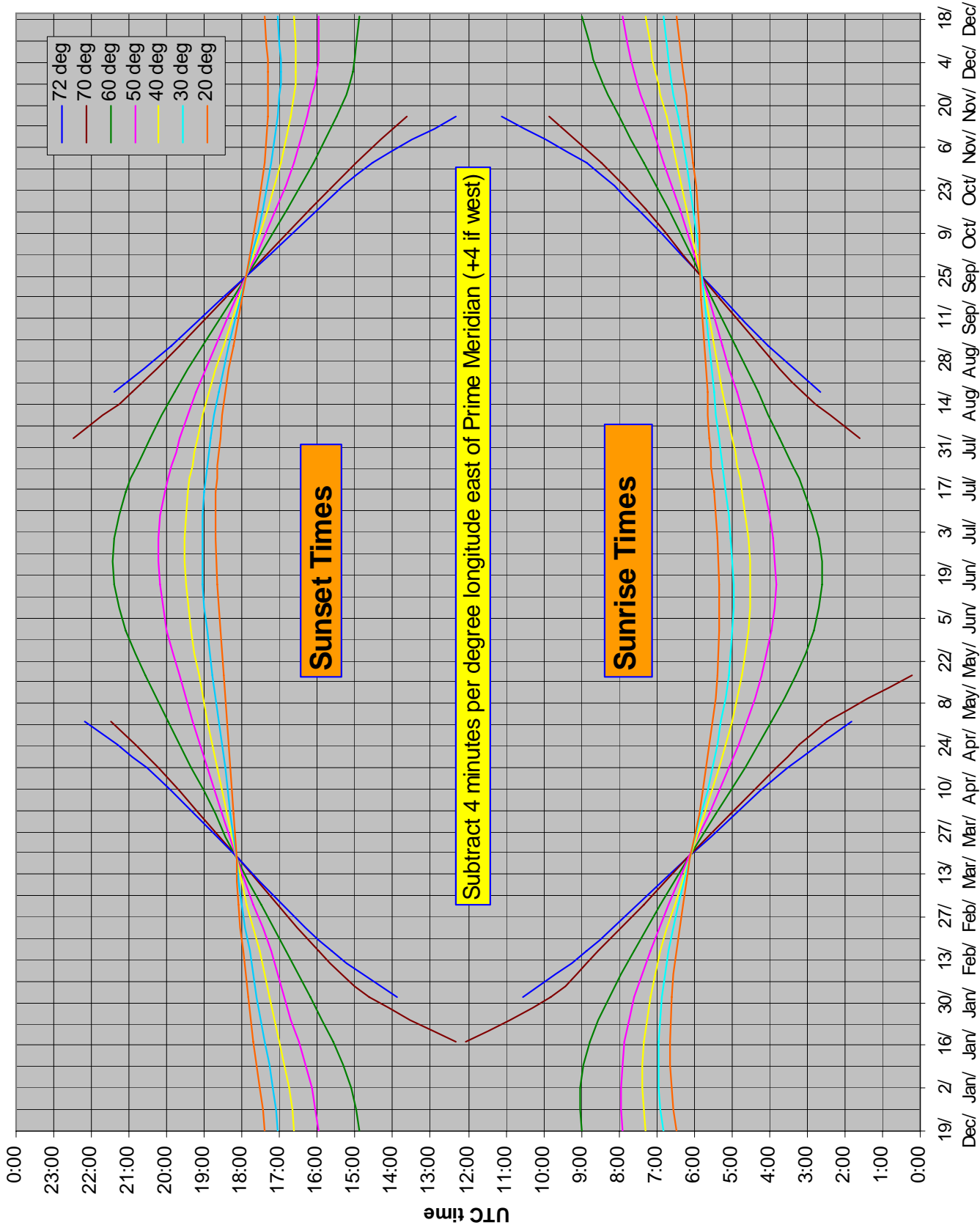
1976 U.S. Standard Atmosphere - Troposphere [11-20 Km]

| Ambient Air Pressure (Pa) | | | | | Amb. Air Density (ρ _a) | | | | Ambient Air Temperature (T _a) | | | | |
|---------------------------|--------------------------------------|---------|---------|---------|------------------------------------|---------------------------------------|------------------------|----------------------|---|---------|---------|--------|---------|
| Hp [ft] | δ (=P _a /P ₀) | [psi] | [psf] | [Pa] | [in Hg] | σ (= ρ _a /ρ ₀) | [slg/ft ³] | [kg/m ³] | θ (=T _a /T ₀) | [K] | [deg C] | [R] | [deg F] |
| 36089 | 0.223361 | 3.28251 | 472.683 | 22632.1 | 6.68324 | 0.297076 | 0.0007061 | 0.363918 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 37000 | 0.213795 | 3.14192 | 452.438 | 21662.7 | 6.39700 | 0.284352 | 0.0006759 | 0.348332 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 38000 | 0.203762 | 2.99449 | 431.207 | 20646.2 | 6.09681 | 0.271009 | 0.0006442 | 0.331986 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 39000 | 0.194200 | 2.85397 | 410.972 | 19677.3 | 5.81071 | 0.258291 | 0.0006139 | 0.316407 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 40000 | 0.185087 | 2.72004 | 391.686 | 18753.9 | 5.53804 | 0.246171 | 0.0005851 | 0.301559 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 41000 | 0.176402 | 2.59240 | 373.306 | 17873.9 | 5.27816 | 0.234619 | 0.0005577 | 0.287408 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 42000 | 0.168124 | 2.47075 | 355.788 | 17035.1 | 5.03048 | 0.223609 | 0.0005315 | 0.273921 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 43000 | 0.160234 | 2.35480 | 339.092 | 16235.7 | 4.79441 | 0.213116 | 0.0005066 | 0.261067 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 44000 | 0.152715 | 2.24430 | 323.180 | 15473.9 | 4.56943 | 0.203115 | 0.0004828 | 0.248816 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 45000 | 0.145549 | 2.13899 | 308.014 | 14747.7 | 4.35500 | 0.193584 | 0.0004601 | 0.237140 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 46000 | 0.138719 | 2.03861 | 293.560 | 14055.7 | 4.15064 | 0.184500 | 0.0004385 | 0.226012 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 47000 | 0.132209 | 1.94295 | 279.785 | 13396.1 | 3.95587 | 0.175842 | 0.0004180 | 0.215406 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 48000 | 0.126005 | 1.85177 | 266.656 | 12767.5 | 3.77023 | 0.167590 | 0.0003983 | 0.205298 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 49000 | 0.120092 | 1.76487 | 254.142 | 12168.3 | 3.59331 | 0.159726 | 0.0003797 | 0.195664 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 50000 | 0.114457 | 1.68206 | 242.216 | 11597.3 | 3.42469 | 0.152230 | 0.0003618 | 0.186482 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 51000 | 0.109086 | 1.60312 | 230.850 | 11053.1 | 3.26398 | 0.145087 | 0.0003449 | 0.177731 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 52000 | 0.103967 | 1.52789 | 220.017 | 10534.4 | 3.11081 | 0.138278 | 0.0003287 | 0.169391 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 53000 | 0.099088 | 1.45620 | 209.693 | 10040.1 | 2.96484 | 0.131790 | 0.0003133 | 0.161442 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 54000 | 0.094438 | 1.38786 | 199.853 | 9568.9 | 2.82571 | 0.125605 | 0.0002986 | 0.153866 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 55000 | 0.090006 | 1.32273 | 190.474 | 9119.9 | 2.69311 | 0.119711 | 0.0002845 | 0.146646 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 56000 | 0.085783 | 1.26066 | 181.536 | 8691.9 | 2.56673 | 0.114093 | 0.0002712 | 0.139764 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 57000 | 0.081757 | 1.20151 | 173.017 | 8284.1 | 2.44628 | 0.108739 | 0.0002585 | 0.133206 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 58000 | 0.077921 | 1.14512 | 164.898 | 7895.3 | 2.33149 | 0.103637 | 0.0002463 | 0.126955 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 59000 | 0.074264 | 1.09139 | 157.160 | 7524.8 | 2.22208 | 0.098773 | 0.0002348 | 0.120997 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 60000 | 0.070779 | 1.04017 | 149.785 | 7171.7 | 2.11781 | 0.094138 | 0.0002238 | 0.115319 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 61000 | 0.067458 | 0.99136 | 142.756 | 6835.2 | 2.01842 | 0.089721 | 0.0002133 | 0.109908 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 62000 | 0.064292 | 0.94484 | 136.057 | 6514.4 | 1.92371 | 0.085510 | 0.0002032 | 0.104750 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 63000 | 0.061275 | 0.90050 | 129.673 | 6208.7 | 1.83344 | 0.081498 | 0.0001937 | 0.099835 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 64000 | 0.058400 | 0.85825 | 123.588 | 5917.4 | 1.74740 | 0.077673 | 0.0001846 | 0.095150 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 65000 | 0.055659 | 0.81797 | 117.788 | 5639.7 | 1.66540 | 0.074028 | 0.0001760 | 0.090685 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |
| 65617 | 0.054034 | 0.79408 | 114.347 | 5475.0 | 1.61675 | 0.071866 | 0.0001708 | 0.088036 | 0.751865 | 216.650 | -56.50 | 389.97 | -69.70 |

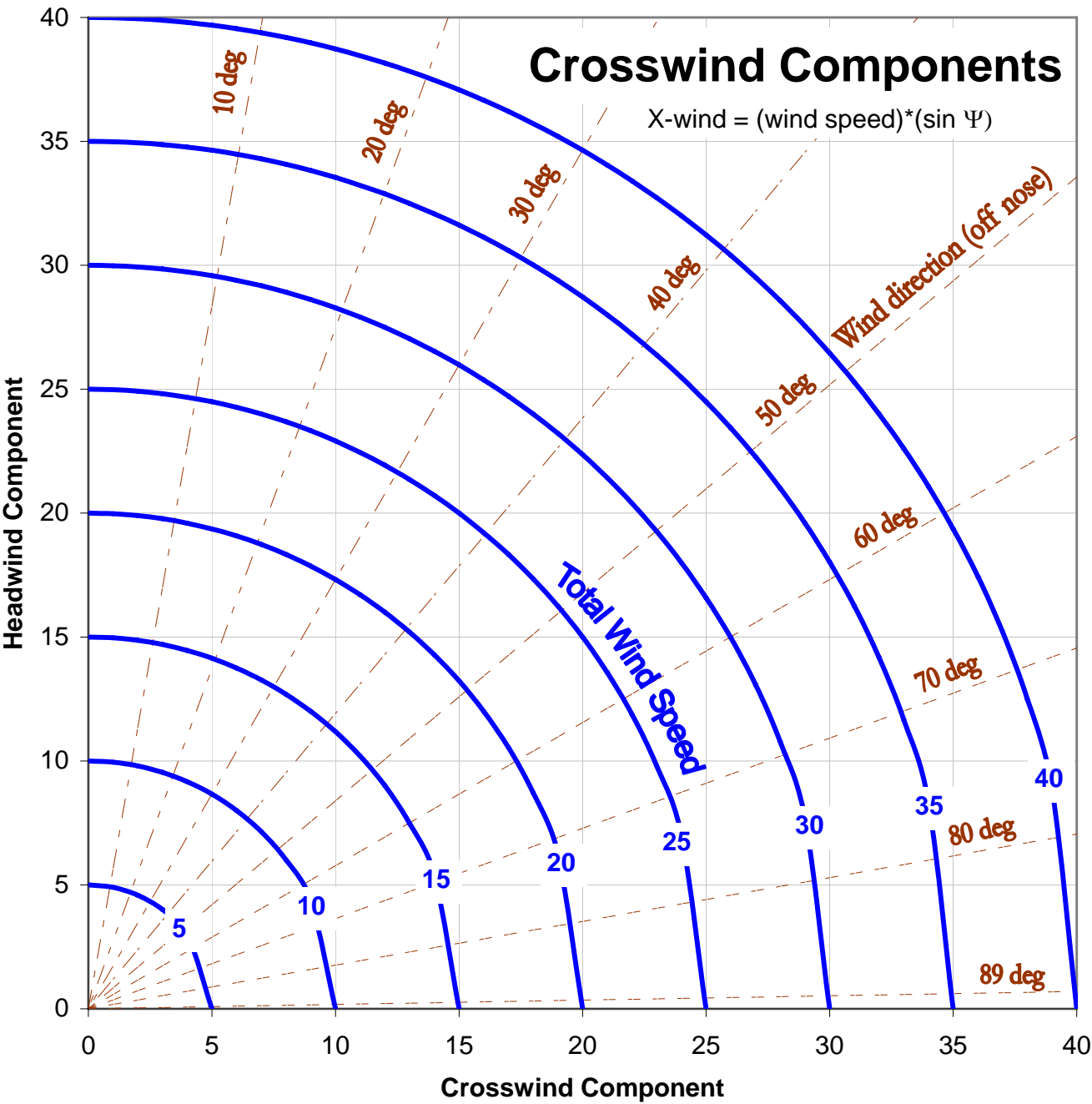
Section 3.5 Sea States(ref 3.3) Sea State
International Swell Scale

| Code | Sea | Wave Height, Crest to Trough (ft) |
|------|--|--------------------------------------|
| 0 | Calm | 0 |
| 1 | Smooth | Less than 1 |
| 2 | Slight | 1-3 |
| 3 | Moderate | 3-5 |
| 4 | Rough | 5-8 |
| 5 | Very rough | 8-12 |
| 6 | High | 12-20 |
| 7 | Very high | 20-40 |
| 8 | Mountainous | 40+ |
| 9 | Confused, Used as additional description 1-8 | |
| Code | Swell | In Open Sea |
| 0 | None | low |
| 1 | Short or average | |
| 2 | Long | |
| 3 | Short | Moderate height |
| 4 | Average | |
| 5 | Long | |
| 6 | Short | heavy |
| 7 | Average | |
| 8 | Long | |
| 9 | Confused, Used as additional description 1-8 | |

Section 3.6 Sunrise Sunset Times



Section 3.7 Crosswind Components



Section 3.8 Geodetic Measurements

Acronyms, Abbreviations and Symbols

DGPS Differential Global Positioning System

ECEF Earth Centered Earth Fixed coordinate system

GPS Global Positioning System

INS Inertial Navigation System

WGS84 World Geodetic System 1984

a Earth's semi-major axis radius

b Earth's semi-minor axis radius

D Great circle distance between two points

e eccentricity of the Earth square

f Earth's flatness factor

h geodetic height

N radius of curvature in prime vertical

P radius of curvature in prime vertical

\vec{r} Vector from earth center extending to coordinates

r Earth's radius

X ECEF x coordinate

Y ECEF y coordinate

Z ECEF z coordinate

ϕ Geodetic latitude

φ Angle between the two vectors originating at the Earth's center and extending to their respective coordinates at the start and end points.

λ Geodetic longitude

ψ Runway heading with \vec{r} respect to true North.

Earth Modeling

The Geodetic System (i.e. latitude, longitude and height) commonly defines the location of any point relative to the earth (Figure 3.8-1, point P). Longitude and latitude are expressed in degrees, minutes, seconds. Longitude lines extend ± 180 degrees from the Prime Meridian, run north to south, and converge at the poles. Latitude lines are parallel to the equator and extend $\pm 90^\circ$.

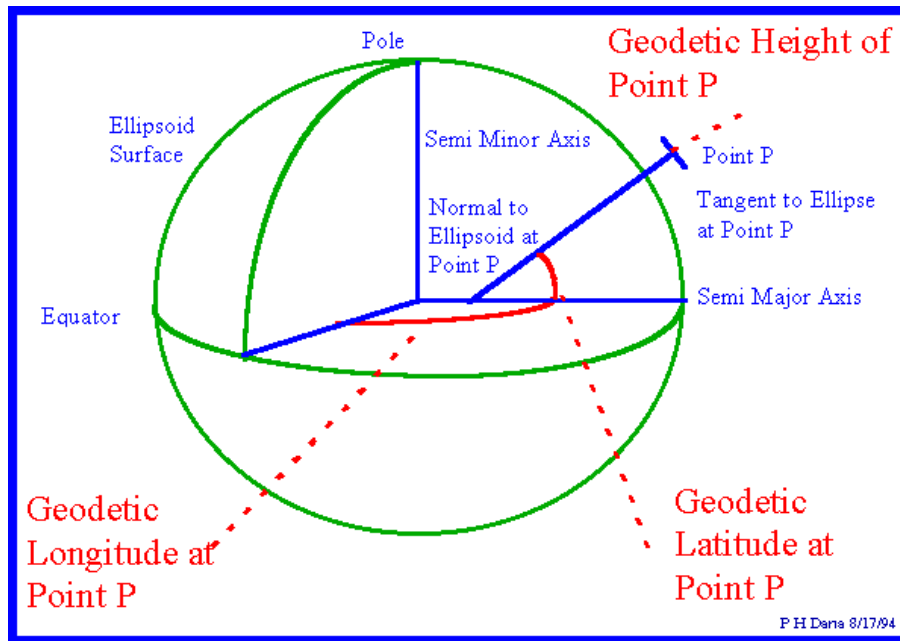


Figure 3.8-1 Geodetic Coordinate System

The 1984 world geodetic system, WGS84, models the earth's surface as an oblate spheroid - an ellipsoid rotated about its semi-minor axis. In this model (used by GPS systems), the earth's semi-major axis, a is 6,378,137.0 meters and the semi-minor axis, b is 6,356,752.314 meters.

The flatness factor (f) is defined as:

$$f = \frac{a - b}{a}$$

For the WGS84 model, $f=1/298.257223563$

Any plane passing through the center of a spheroid traces a great circle around the perimeter of that spheroid. The shortest distance between two points on the surface is that portion of the great circle arc encompassing both points (Figure 3.8-2).

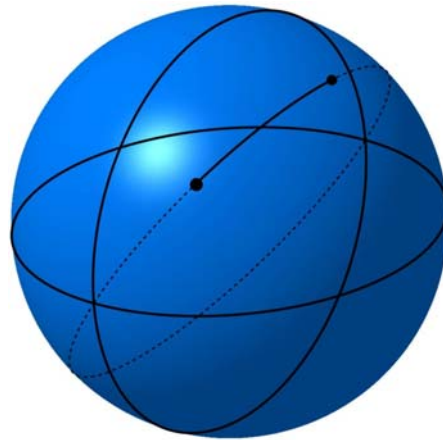


Figure 3.8-2 Great Circle Arc

Note: navigating along a great circle route has the disadvantage of not intercepting longitude lines at the same angle (except when flying along the equator); in other words, the heading changes along the route.

For the purpose of performance, navigation, or noise analysis, flight testers may require distances between two points (the shortest being along the great circle arc) and the average heading of that arc. Calculating these from typical Geodetic System Lat/Long inputs requires conversion to the Earth Centered Earth Fixed (ECEF) coordinate system as shown in Figure 3.8-3.

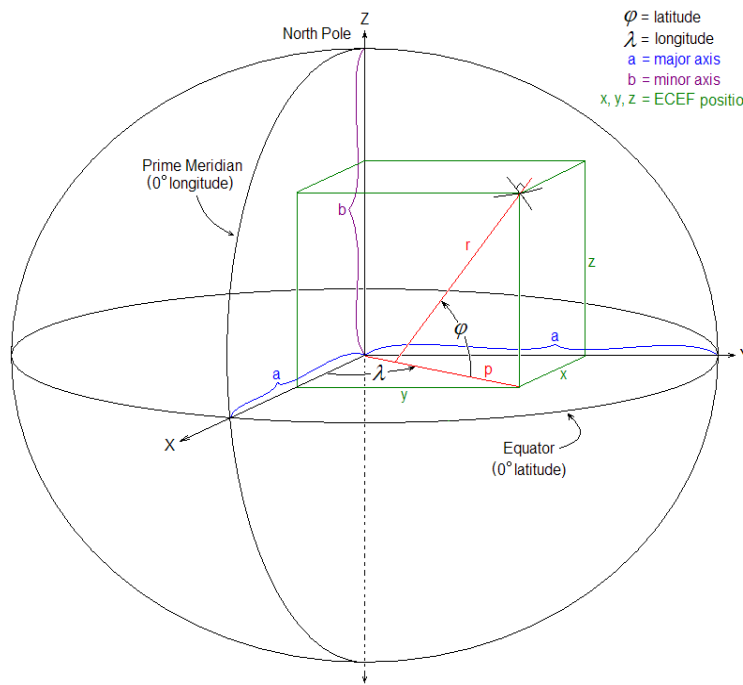


Figure 3.8-3 Earth Centered Earth Fixed Coordinate System

The ECEF coordinate system is a Cartesian system with the origin at the earth's center. In this system, the X-axis is defined by the intersection of the Prime Meridian and equatorial planes. The Z-axis goes through the North Pole. The Y-axis completes a right-handed orthogonal system by a plane 90 degrees east of the X-axis and its intersection with the equator. Geodetic System (lat/long/height) data converts to ECEF as follows:

$$x = (N + h) \cdot \cos(\phi) \cdot \cos(\lambda)$$

$$y = (N + h) \cdot \cos(\phi) \cdot \sin(\lambda)$$

$$z = (N(1 - e^2) + h) \cdot \sin(\phi)$$

where,

x = ECEF coordinate parallel to the X-axis

y = ECEF coordinate parallel to the Y-axis

z = ECEF coordinate parallel to the Z-axis

ϕ = geodetic latitude

λ = geodetic longitude

h = height above geodetic surface

N = Normal radius; distance from earth center to any point on the modeled surface at that latitude

$$N = \frac{a}{\sqrt{1 - e^2 \cdot \sin^2(\phi)}}$$

where,

a = semi-major axis radius

e^2 = eccentricity squared; $e^2 = 1 - \left(\frac{b}{a}\right)^2 = 2 \cdot f - f^2 = 0.00669438002290$ (Earth, per WGS84)

Great Circle Distance

The great circle distance (D) between points (subscripts 1 and 2) can be calculated as

$$P_1 = \sqrt{x_1^2 + y_1^2 + z_1^2} \quad P_2 = \sqrt{x_2^2 + y_2^2 + z_2^2}$$

$$\vec{P_1} \cdot \vec{P_2} = P_1 \cdot P_2 \cos \varphi = x_1 \cdot x_2 + y_1 \cdot y_2 + z_1 \cdot z_2$$

$$\varphi = \arccos \left(\frac{x_1 \cdot x_2 + y_1 \cdot y_2 + z_1 \cdot z_2}{P_1 \cdot P_2} \right)$$

$$D = N(\phi_{avg}) \cdot \varphi$$

where

P = distance from earth center to any point (including height above the spheroid surface).

\vec{P} = Vector from the Earth's center to point P.

φ = Angle between the two \vec{P} vectors

$N(\phi_{avg})$ = Normal radius using average latitude of points 1 and 2

For shorter distances typical of local flight testing, the Great Circle model approximates a two dimensional model.

Distance North-South (Northing): $dy = N(\phi) \cdot \sin(\Delta\phi)$

Earth's radius East-West: $r = N(\phi) \cdot \cos(\phi)$

Distance East-West (Easting): $dx = r \sin(\Delta\lambda)$

Distance between two points: $D = \sqrt{dx^2 + dy^2}$

Heading between two points (relative to true north) $\psi = \arctan(dy/dx)$

Runway Distance Transformation

Data from a runway survey provides a reference point for determining the distance to key locations (e.g. brake release, liftoff, microphone array). From runway survey data, a local coordinate system can be established that uses any point on the runway as the origin, and can either

- keep the same X, Y and Z axes or
- set height as the Z-axis, direction along the runway heading as the X-axis, and direction normal to the runway centerline as the Y-axis (Figure 3.8-4).

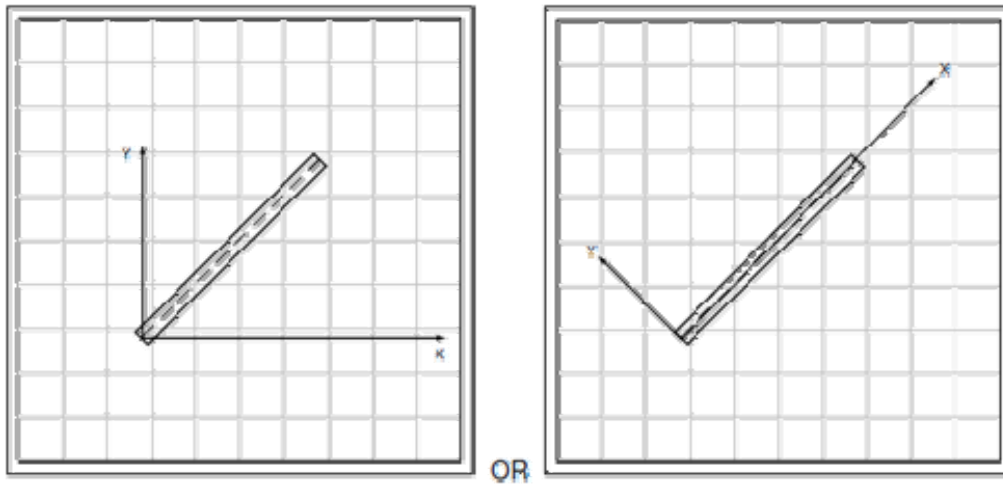


Figure 3.8-4 Local Coordinate System

For the second option above, distance along and normal to the runway can be calculated using the following geometry definitions and equations (Figures 3.8-5 and 3.8-6):

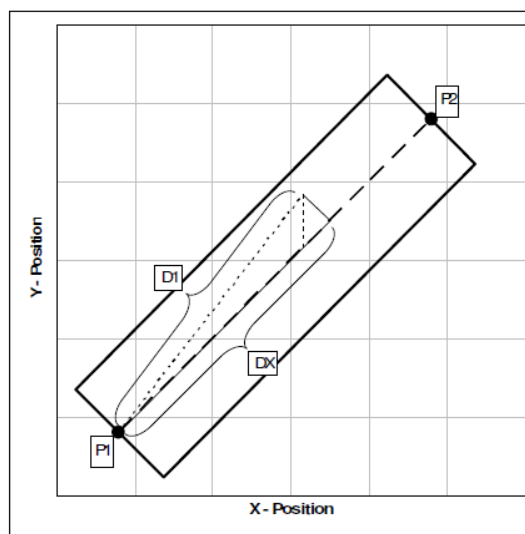


Figure 3.8-5 Local Geometry 1

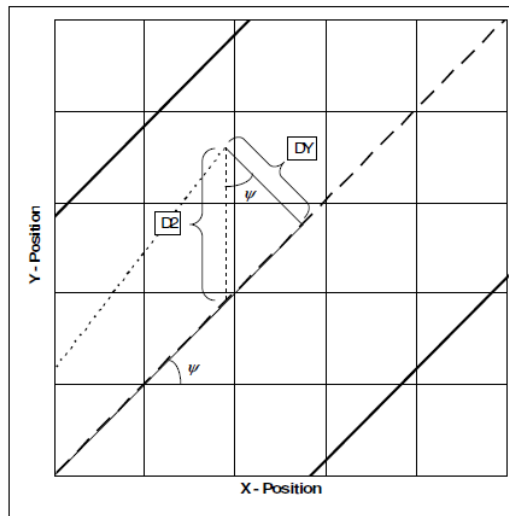


Figure 3.8-6 Local Geometry 2

P1= Main reference point along runway centerline (subscript 1 in the following equations)

P2= 2nd point defining runway centerline (subscript 2 in the following equations)

ψ = runway centerline heading with respect to true north.

$D1$ = total distance from reference point to current position.

$D2$ = distance from current position to runway along the same X position (i.a.w. ECEF coordinates)

DX = distance along runway centerline from reference point to current position.

DY = normal distance between runway centerline and current position.

m = slope of runway centerline equation.

b = intercept of runway centerline equation.

$$\psi = \arctan\left(\frac{y_2 - y_1}{x_2 - x_1}\right)$$

$$D1 = \sqrt{(x - x_1)^2 + (y - y_1)^2}$$

$$y = mx + b, \quad m = \frac{y_2 - y_1}{x_2 - x_1}, \quad b = \frac{x_2 y_1 - x_1 y_2}{x_2 - x_1}$$

$$\cos\psi = \frac{DY}{D2} = \frac{DY}{y - (mx + b)} = \frac{x_2 - x_1}{\sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2}} = \frac{1}{\sqrt{m^2 + 1}}$$

$$DY = \frac{|y - mx - b|}{\sqrt{m^2 + 1}}$$

$$DX = \sqrt{D1^2 - DY^2}$$

Note: the above heading equation applies between any two points and may be useful for navigation analysis in a local environment.

Section 3.9 References

- 3.1 Anon., “Aeronautical Vestpocket Handbook” ,Part No. P&W 079500, United Technologies Pratt & Whitney, Canada, 1990.
- 3.2 Lawless, Alan. R. et al, “Aerodynamics for Flight Testers”, National Test Pilot School, P.O. Box 658, Mojave CA, 93501, 1999.
- 3.3 Denno, Richard R., et al “AIAA Aerospace Design Engineers Guide” ISBN 0-930403-21-5, AIAA, 1987.
- 3.4 Global Positioning System Overview, Peter H. Dana, Department of Geography, University of Texas at Austin, 1994. (www.colorado.edu/geography/gcraft/notes/gps/gps_f.html)
- 3.5 Charles D Ghilani, Penn State College of Engineering, 2008 (<http://surveying.wb.psu.edu/sur351/georef/Ellip4.htm>)
- 3.6 Standard Atmosphere Calculator Website Link <http://www.digitaldutch.com/atmoscalc/>.

NOTES