

Section 3 Universe/Earth/Atmospheric Properties

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Section 3 Recurring Nomenclature

H_p = pressure altitude. The pressure associate with geopotential altitude on a standard day.

T = absolute temperature (Rankin or Kelvin)

T_R = absolute temperature, Rankin scale

T_o = standard day seal level absolute temperature

P = ambient pressure

P_o = standard day seal level ambient pressure

ρ = ambient density

ρ_o = standard day seal level ambient density

$\delta = P/P_o$ = atmospheric pressure/std day sea level pressure

$\theta = T/T_o$ = atmospheric absolute temp / std day sea level absolute temp

$\sigma = \rho/\rho_o$ = atmospheric density/std day sea level density

g = acceleration due to gravity

g_o = standard earth acceleration due to gravity

a_o = speed of sound at std day sea level temperature

Section 3.1 Universal Constants (reference 3.1)

Avogadro's number, N_o	6.022169×10^{23}	molecules/mole
Boltzmann constant, k	1.380×10^{-23}	J/°K
electron charge, e	$1,602 \times 10^{-19}$	coulomb
electron mass, m_e	9.109×10^{-31}	kg
gas constant, R	8.31434 J/°K	mole
gravitational constant, G	6.673×10^{-11}	Nm ² /kg ²
neutron mass, m_n	1.674×10^{-27}	kg
Planck constant, h	6.625×10^{-34}	J sec
proton mass, m_p	1.672×10^{-27}	kg
speed of light in a vacuum, c	2.998×10^8	m/sec
unified atomic mass constant, m_u	1.660×10^{-27}	kg
volume of ideal gas (std temp & press)	2.241×10	m ³ /mol

Newtonian Gravity

The gravitational field (g) near any mass can be calculated as

$$g = \frac{GM}{(R_A)^2}$$

where G is the universal gravitational constant and R_A is the absolute distance from the center of mass M

Section 3.2 Earth Properties (references 3.9.2, 3.9.3)

Std Earth gravitational acceleration, $g_o = 9.8066 \text{ m/s}^2 = 32.174 \text{ ft/s}^2$

mass = $5.98333 \times 10^{24} \text{ kg} = 13.22 \times 10^{24} \text{ lb}$

rotation rate, $\omega = 7.292115 \times 10^{-5} \text{ rad/sec}$

average density = $5.522 \text{ g/cm}^3 = 344.7 \text{ lb/ft}^3$

radius average, $R_{avg} = 6,367,444 \text{ m} = 3956.538 \text{ st. miles} = 20,890,522 \text{ ft}$

radius at the equator (R_e) is $6,378,137 \text{ m} (\pm 2)$

radius at the poles $R_p = 6,356,752 \text{ [m]}$

radius as a function of latitude, ϕ (assumes perfect ellipsoid):

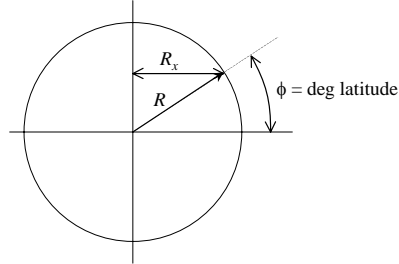
$$R = \left[\left(\frac{\cos \phi}{R_e} \right)^2 + \left(\frac{\sin \phi}{R_p} \right)^2 \right]^{-\frac{1}{2}}$$

Centrifugal Relief from Gravity

The earth's "normal" gravity field includes both the Newtonian Law and a correction for the centrifugal force caused by the earth's rotation. The centrifugal relief correction is

$$\Delta CR = -\frac{V^2}{R_x} = -\frac{(R_x \omega)^2}{R_x} = R_x \omega^2$$

where ω is the earth's rotation rate and R_x is the perpendicular distance from the earth's axis to the surface and can be calculated as $R_x = R \cos \phi$ (see figure below).



For any centrifugal relief calculations associated with aircraft performance, it is sufficiently exact ($g \pm 0.00004 \text{ m/s}^2$) to use the average earth radius. An aircraft flying eastward contributes to centrifugal relief while a west-bound aircraft diminishes it.

The International Association of Geodesy publishes the following equation (accurate to 0.005%) to calculate local sea level gravity including the effects of centrifugal relief for any point fixed to the earth's surface

$$g_{sl} = 9.780327 \left(1 + 0.00530224 \sin^2 \phi - 0.000058 \sin^2 2\phi \right) \left[\frac{m}{s^2} \right]$$

The above equation is tabulated below for quick reference.

Latitude (deg)	Normal g_{local}	
	(m/s^2)	(ft/s^2)
0	9.780327	32.088
15	9.783659	32.098
30	9.792866	32.188
45	9.805689	32.171
60	9.818795	32.214
75	9.828569	32.249
90	9.832185	32.258

The standard acceleration (g_o) corresponds to a latitude of 46.0625° . g_{sl} at the equator and the poles varies $\pm 0.27\%$ from g_o .

Altitude Effect on Gravitational Acceleration

R_A is the sum of the earth's local radius and the geometric distance (h_G) above the surface: $R_A = R + h_G$

Gravitational acceleration at any geometric altitude:

h_G (1000 ft)	$\frac{g_{alt}}{g_{sl}}$
0	1
10	0.99904
20	0.99809
40	0.99618
60	0.99428
80	0.99238
100	0.99049

$$g_{alt} = g_{sl} \left(\frac{R}{R + h_G} \right)^2$$

Actual Gravitational Pull on an Aircraft

Adding a centrifugal relief correction due to the aircraft's velocity, a complete calculation for its gravitational acceleration is

$$g_{A/C} = \left[g_{isl} + \omega^2 R \cos \phi \right] \left[\frac{R}{R + h_G} \right]^2 - \left(\omega + \frac{V_G \sin \sigma}{R + h_G} \right)^2 (R + h_G) \cos \phi$$

where V_G = ground speed and σ = ground track angle (0° = true North, 90° = East, etc.).

Gravity Influence on Aircraft Cruise Performance

Even at the same altitude, changes in gravity due to latitude or centrifugal relief directly alter the required lift, drag, and fuel flow. For example, with sufficiently precise instrumentation, data collected heading West could show about 0.5% more drag and fuel flow than data collected heading East (centrifugal relief effect). After determining test and standard (or mission) values for g , flight test values for C_L , C_D , drag, and fuel flow can be corrected to standard as follows:

$$C_{L_{std}} = C_{L_t} \frac{N_{z_{std}}}{N_{z_{eq}}} \left[\frac{g_{std}}{g_{A/C}} \right]$$

$$C_{D_{std}} = \frac{(C_{L_{std}})^2}{\pi A R e}$$

$$\Delta D = D_{std} - D_t = qS [C_{D_{std}} - C_{D_t}]$$

$$\dot{W}_{f_{std}} = \dot{W}_{f_t} + \Delta D \cdot TSFC$$

where N_z = normal load factor,

C_L = lift coefficient, C_D = drag coefficient,

AR = aspect ratio, e = Oswald efficiency factor,

ΔD change in drag force,

$TSFC$ = thrust specific fuel consumption, and

$\dot{W}_{f_{std}}$ = standard day fuel flow

Section 3.3 General Properties of Air (reference 3.9.1)

$$\begin{aligned}\text{Gas constant, } R &= 53.35 \text{ ft lb/R lbm} = 287.074 \text{ J/kg K} \\ &= 1716 \text{ lb(ft)/slgs(R)} = 3089.7 \text{ lb(ft)/slgs(K)}\end{aligned}$$

$$\begin{aligned}\text{Speed of sound} &= a_o(\theta)^{1/2} \\ &= 49.02 (T_R)^{1/2} \text{ ft/sec} \\ &= 33.42 (T_R)^{1/2} \text{ miles/hr} \\ &= 29.04 (T_R)^{1/2} \text{ knots} \\ &= 20.05 (T_R)^{1/2} \text{ m/sec}\end{aligned}$$

$$\text{Density, } \rho = .0023769 \text{ slug/ft}^3 = 1.225 \text{ kg/m}^3 \text{ (at } 15^\circ \text{ C)}$$

$$\text{Specific weight, } g_\rho = .07647 \text{ sec}^2/\text{ft}^4$$

Specific heat capacity at 59°F ($=T_o$)

$$\text{at constant pressure, } c_p = .240 \text{ BTU/lb R} = 1004.76 \text{ J/kg K}$$

$$\text{at constant volume, } c_v = .1715 \text{ BTU/lb R} = 717.986 \text{ J/kg K}$$

$$\text{specific heat ratio, } \gamma = \{c_p / c_v\} = 1.4$$

Normal Composition of clean, dry atmospheric air near sea level

Nitrogen, N_2	78.084 % by volume
Oxygen, O_2	20.948 %
Argon, A	0.934 %
Carbon Dioxide, CO_2	0.031 %
Neon, Ne	<u>0.002 %</u>
total	99.9988 %

plus traces of helium, krypton, xenon, hydrogen, methane, nitrous oxide, ozone, sulfur dioxide, nitrogen dioxide, ammonia, carbon monoxide, and iodine.

Viscosities of Air

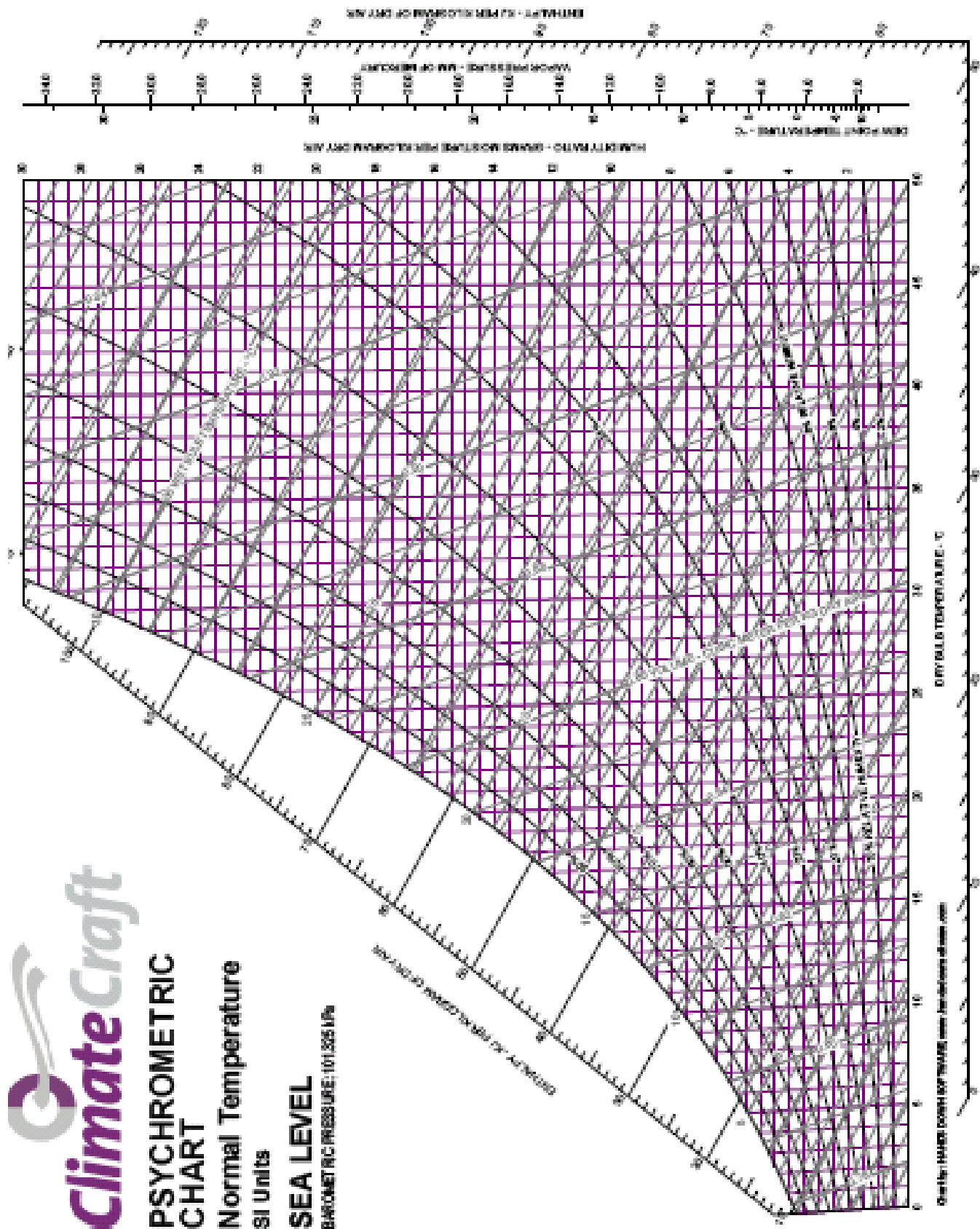
$$\text{Coefficient of Viscosity, } \mu_c = \frac{7.3025 \times 10^{-7} (T_R)^{3/2}}{T_R + 198.72} \text{ lb/ft sec}$$

Kinematic viscosity, $\nu = \frac{\mu_c}{g\rho}$ ft²/sec

Absolute Viscosity, lb $\mu = \rho\nu = \left[.317(T_R)^{3/2} \left(\frac{734.7}{T_R + 216} \right) \right] \times 10^{-10}$ sec/ft²

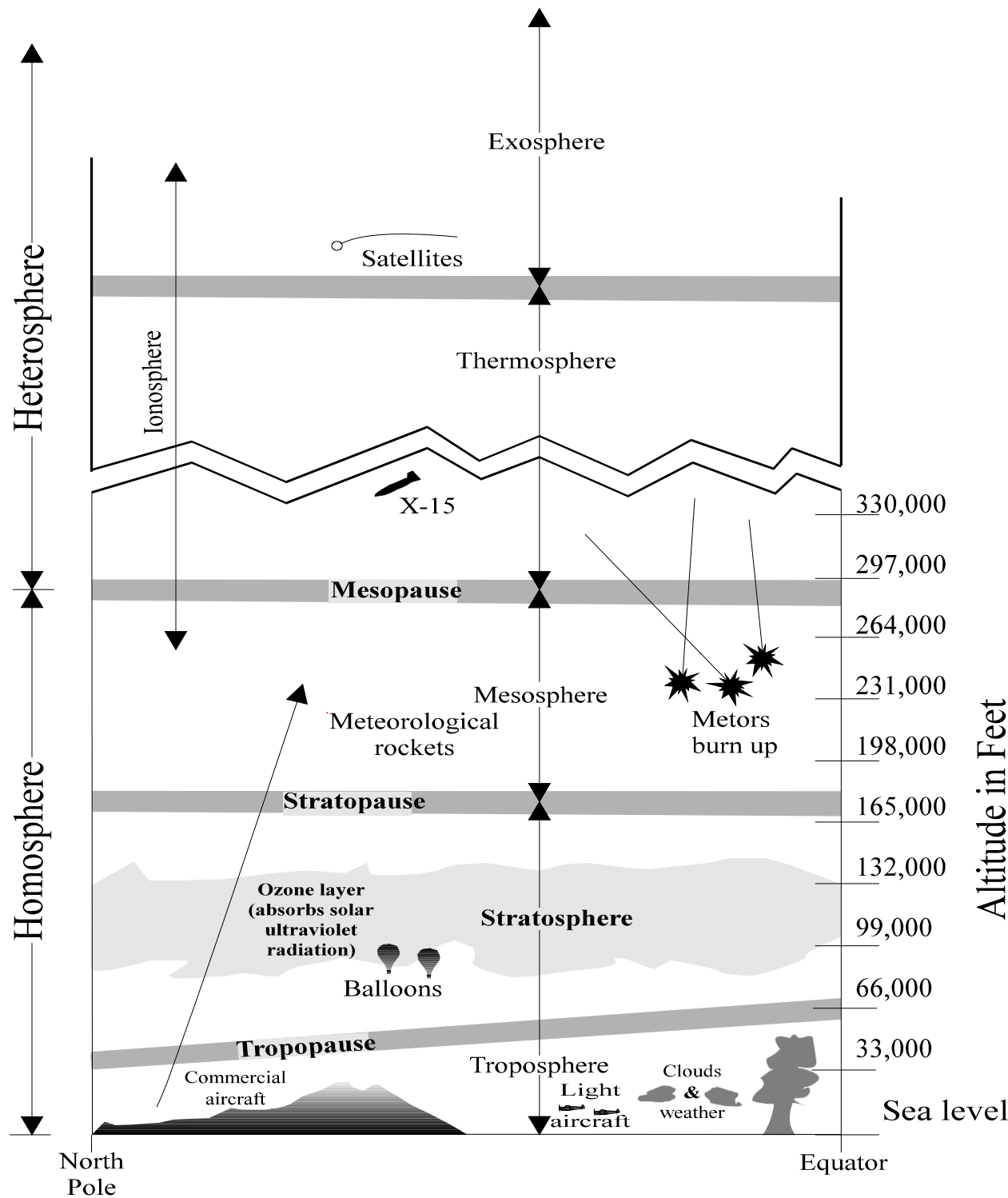
Atmospheric Viscosity (U.S. Standard Atmosphere)

Pressure Altitude <i>ft</i>	Kinematic Viscosity ν (<i>ft²/sec</i>)	Absolute Viscosity μ (<i>lb sec/ft²</i>)
0	1.572 x 10 ⁻⁴	3.737 x 10 ⁻⁷
5,000	1.776	3.638
10,000	2.013	3.538
15,000	2.293	3.435
20,000	2.625	3.330
25,000	3.019	3.224
30,000	3.493	3.115
35,000	4.065	3.004
40,000	5.074	2.981
45,000	6.453	2.982
50,000	8.206	2.983
55,000	10.44	2.985
60,000	13.27	2.986
70,000	21.69	3.005
80,000	35.75	3.043
90,000	58.53	3.080
100,000	95.19	3.118
150,000	1066	3.572
200,000	6880	3.435



Section 3.4 Standard Atmosphere

Divisions of the Atmosphere



Constantly changing atmospheric conditions cannot be duplicated at will to provide the exact environment in which a flight takes place. A standard atmosphere provides a common basis to relate all flight test, wind tunnel results, aircraft design and general performance. Several models of “standard atmosphere” exist with minor differences based on mathematical constants used in the calculations.

Geometric altitude, h_G , is defined as the height of an aircraft above sea level (also called **tapeline** altitude)

Absolute altitude, h_a , is defined as the height of an aircraft above the center of the earth: (geometric altitude + radius of the earth).

Geopotential altitude, h , is required because g changes with height. If potential energy is calculated using sea level weight ($W_{SL} = mg_o$) instead of actual weight ($W = mg$), then the altitude must be lower.

$$W h_G = W_{SL} h$$

Pressure altitude, H_p is the altitude, on a standard day, at which the test day pressure would be found

Density altitude is the altitude, on a standard day, at which the test day density would be found

Temperature altitude is the altitude, on a standard day, at which the test day temperature would be found

Assumptions on which the standard atmosphere is built

1. The air is dry (only 0.4% per volume of water vapor)
2. The air is a perfect gas and obeys the equation of state,

$$P = \rho g R T$$

where $R = 53.35 \text{ ft lb/}^\circ\text{R lbm}$
3. The gravitational field decreases with altitude
4. Hydrostatic equilibrium exists ($\Delta p = -\rho g_o \Delta h$)

Standard Day Sea Level Atmospheric Conditions

$$P_o = 2116.22 \text{ lb/ft}^2 = 14.696 \text{ lb/in}^2 = 29.921 \text{ in Hg} \\ = 1013.25 \text{ HPa (mb)} = 101325 \text{ Pa}$$

$$T_o = 288.15 \text{ K} = 518.67 \text{ R} = 59^\circ \text{F} = 15^\circ \text{C}$$

$$\rho_o = 0.0023769 \text{ slugs/ft}^3 = 0.07647 \text{ lbm/in}^3 = 1.255 \text{ kg/m}^3 \text{ (at } 15^\circ \text{C)}$$

$$a_o = 1116.45 \text{ ft/sec} = 661.478 \text{ KTAS} = 761.14 \text{ mph} = 340.294 \text{ m/sec}$$

$$g_o = 32.174 \text{ ft/sec}^2 = 9.80665 \text{ m/sec}^2$$

$$L = \text{standard temperature lapse rate} = 0.0019812 \text{ K/ft}$$

1976 U.S Standard Atmosphere Equations

Troposphere - below 36,089 ft (11,000 m) < 22636 Pa

$$\theta = 1 - (L/T_o) h = 1 - (6.8755856 \times 10^{-6}) h$$

$$\sigma = \theta^{n-1}$$

$$\delta = \theta^n$$

where $n = 5.255876$, $h = \text{geopotential altitude (ft)}$

Stratosphere- between 36,089 ft and 65,616 ft (20,000 m) the standard day temperature is a constant 216.65 K, therefore:

$$\theta = 0.751865$$

$$\sigma = .297076 e^{-0.000048063 [h-36,089]}$$

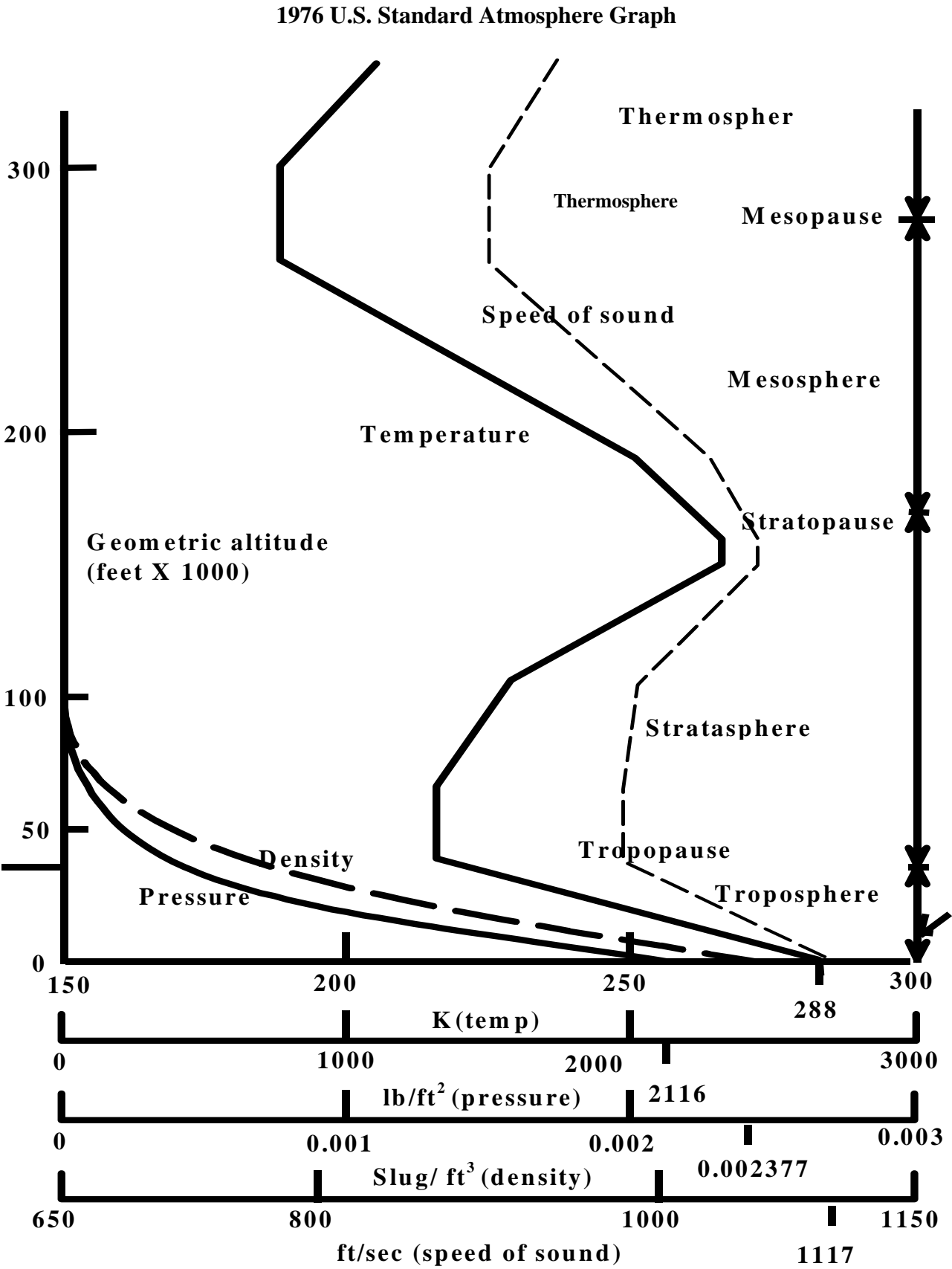
$$\delta = .223361 e^{-0.000048063 [h-36,089]}$$

The above relations characterize the standard atmosphere table in this handbook. They may be re-written to solve for pressure altitude (H_p) for any ambient pressure. Below the tropopause (ambient pressure greater than 472.683 psf or 22632 Pa)

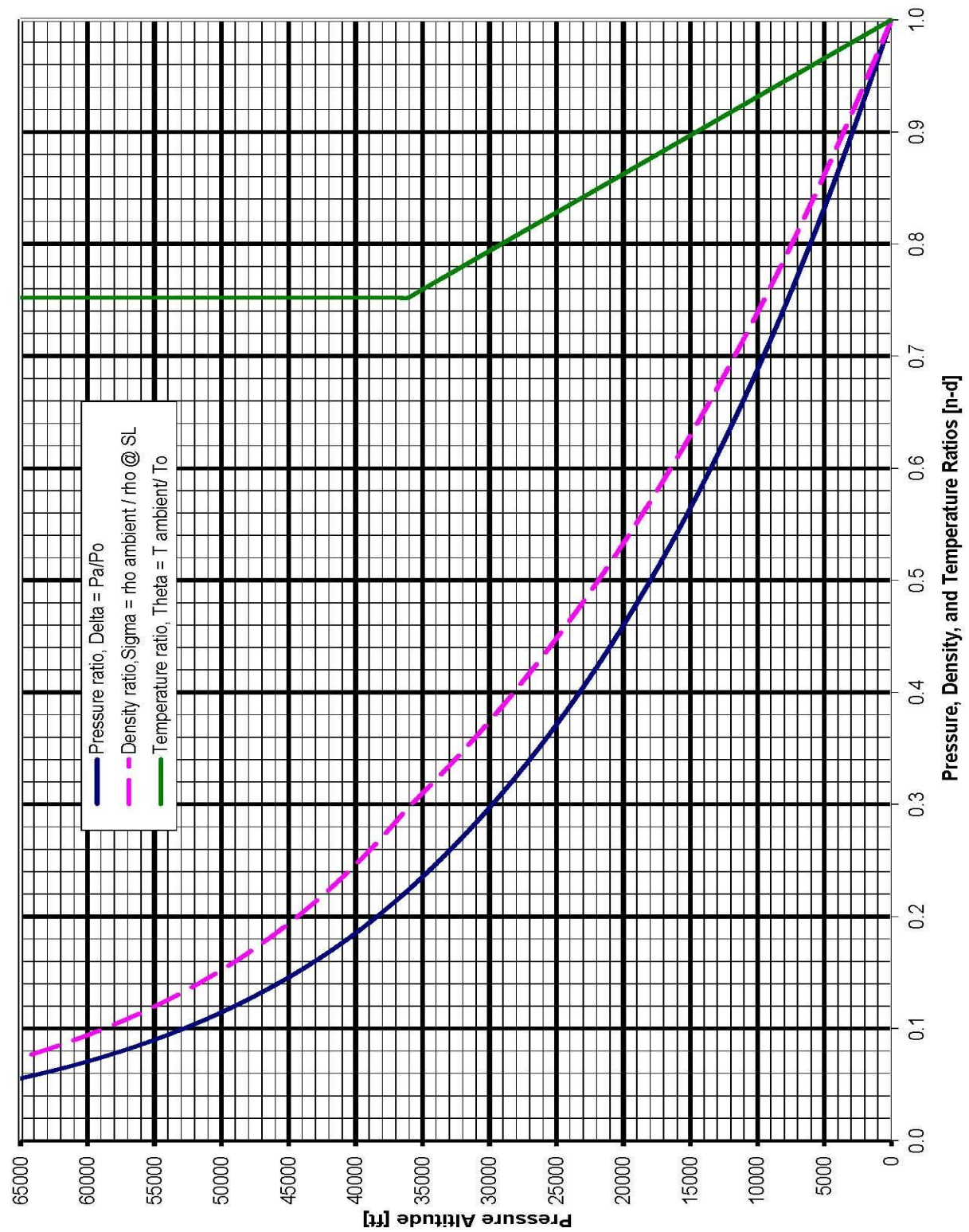
$$H_p [\text{ft}] = [1 - (P_a/P_o)^{0.1902632}] / [6.8755856 \times 10^{-6}]$$

In the troposphere (ambient pressure between 114.347 and 472.683 psf or between 5475 and 22632.1 Pascal)

$$H_p [\text{ft}] = 36089 + [\ln(P_a/P_o) + 1.498966] / 0.000048063$$



1976 U.S. Standard Atmosphere



1976 U.S. Standard Atmosphere - Below Tropopause [<11 Km]

Hp [ft]		P _o = 14.696					P _o = 2116.22807					P _o = 101325					P _o = 29.92126					ρ _o = .0023769					ρ _o = 1.225														
		Ambient Air Pressure (P _a)										Amb. Air Density (ρ _a)										θ (=T _a /T _o)										Ambient Air Temperature (T _a)									
		[ft]	δ (=P _a /P _o)	[psi]	[psf]	[Pa]	[in Hg]	[in Hg]	σ (= ρ _a /ρ _o)	[slg/ft ³]	[kg/m ³]	[deg C]	[R]	[deg F]	[deg F]																										
-1000	1.036670	15.23490	2193.8300	105040.58	31.01847	31.01847	1.029591	0.0024472	1.261249	1.00688	290.131	16.98	522.24	62.57																											
0	1.000000	14.69600	2116.2281	101325.00	29.92126	29.92126	1.000000	0.0023769	1.225000	1.00000	288.150	15.00	518.67	59.00																											
1000	0.964388	14.17264	2040.8640	97716.57	28.85569	28.85569	0.971064	0.0023081	1.189554	0.99312	286.169	13.02	515.10	55.43																											
2000	0.929809	13.66447	1967.6881	94212.91	27.82106	27.82106	0.942773	0.0022409	1.154897	0.98625	284.188	11.04	511.54	51.87																											
3000	0.896241	13.17116	1896.6514	90811.67	26.81668	26.81668	0.915117	0.0021751	1.121019	0.97937	282.206	9.06	507.97	48.30																											
4000	0.863662	12.69238	1827.7057	87510.55	25.84185	25.84185	0.888086	0.0021109	1.087906	0.97250	280.225	7.08	504.41	44.74																											
5000	0.832048	12.22778	1760.8036	84307.27	24.89593	24.89593	0.861671	0.0020481	1.055546	0.96562	278.244	5.09	500.84	41.17																											
6000	0.801378	11.77705	1695.8984	81199.62	23.97824	23.97824	0.835860	0.0019868	1.023929	0.95875	276.263	3.11	497.27	37.60																											
7000	0.771630	11.33987	1632.9442	78185.37	23.08813	23.08813	0.810645	0.0019268	0.993040	0.95187	274.282	1.13	493.71	34.04																											
8000	0.742782	10.91592	1571.8959	75262.38	22.22497	22.22497	0.786016	0.0018683	0.962870	0.94500	272.300	-0.85	490.14	30.47																											
9000	0.714814	10.50490	1512.7089	72428.50	21.38813	21.38813	0.761964	0.0018111	0.933406	0.93812	270.319	-2.83	486.57	26.90																											
10000	0.687705	10.10651	1455.3396	69681.66	20.57699	20.57699	0.738479	0.0017553	0.904637	0.93124	268.338	-4.81	483.01	23.34																											
11000	0.661434	9.72043	1399.7449	67019.78	19.79093	19.79093	0.715552	0.0017008	0.876551	0.92437	266.357	-6.79	479.44	19.77																											
12000	0.635982	9.34639	1345.8825	64440.85	19.02938	19.02938	0.693173	0.0016476	0.849137	0.91749	264.376	-8.77	475.88	16.21																											
13000	0.611329	8.98409	1293.7108	61942.87	18.29172	18.29172	0.671334	0.0015957	0.822384	0.91062	262.394	-10.76	472.31	12.64																											
14000	0.587455	8.63324	1243.1889	59523.88	17.57740	17.57740	0.650025	0.0015450	0.796281	0.90374	260.413	-12.74	468.74	9.07																											
15000	0.564342	8.29357	1194.2766	57181.96	16.88583	16.88583	0.629238	0.0014956	0.770816	0.89687	258.432	-14.72	465.18	5.51																											
16000	0.541971	7.96481	1146.9344	54915.22	16.21646	16.21646	0.608963	0.0014474	0.745979	0.88999	256.451	-16.70	461.61	1.94																											
17000	0.520324	7.64668	1101.1234	52721.79	15.56874	15.56874	0.589191	0.0014004	0.721759	0.88312	254.470	-18.68	458.05	-1.62																											
18000	0.499382	7.33891	1056.8054	50599.84	14.94213	14.94213	0.569915	0.0013546	0.698145	0.87624	252.488	-20.66	454.48	-5.19																											
19000	0.479127	7.04126	1013.9430	48547.59	14.33610	14.33610	0.551124	0.0013100	0.675127	0.86936	250.507	-22.64	450.91	-8.76																											
20000	0.459544	6.75345	972.4992	46563.26	13.75013	13.75013	0.532812	0.0012664	0.652694	0.86249	248.526	-24.62	447.35	-12.32																											
21000	0.440613	6.47525	932.4379	44645.13	13.18370	13.18370	0.514968	0.0012240	0.630836	0.85561	246.545	-26.61	443.78	-15.89																											
22000	0.422319	6.20640	893.7235	42791.48	12.63632	12.63632	0.497585	0.0011827	0.609542	0.84874	244.564	-28.59	440.21	-19.46																											
23000	0.404645	5.94666	856.3211	41000.65	12.10749	12.10749	0.480655	0.0011425	0.588802	0.84186	242.582	-30.57	436.65	-23.02																											
24000	0.387575	5.69580	820.1964	39271.00	11.59672	11.59672	0.464169	0.0011033	0.568607	0.83499	240.601	-32.55	433.08	-26.59																											
25000	0.371092	5.45357	785.3157	37600.92	11.10355	11.10355	0.448119	0.0010651	0.548946	0.82811	238.620	-34.53	429.52	-30.15																											
26000	0.355182	5.21975	751.6460	35988.81	10.62749	10.62749	0.432497	0.0010280	0.529809	0.82123	236.639	-36.51	425.95	-33.72																											
27000	0.339829	4.99412	719.1548	34433.13	10.16810	10.16810	0.417296	0.0009919	0.511187	0.81436	234.658	-38.49	422.38	-37.29																											
28000	0.325017	4.77645	687.8104	32932.36	9.72492	9.72492	0.402506	0.0009567	0.493070	0.80748	232.676	-40.47	418.82	-40.85																											
29000	0.310733	4.56653	657.5815	31485.00	9.29752	9.29752	0.388121	0.0009225	0.475448	0.80061	230.695	-42.45	415.25	-44.42																											
30000	0.296961	4.36414	628.4375	30089.59	8.88545	8.88545	0.374133	0.0008893	0.458312	0.79373	228.714	-44.44	411.69	-47.98																											

Standard Conditions									
$P_o = 14.696$	$P_o = 2116.2280$	$P_o = 101325$	$P_o = 29.92126$						
Ambient Air Pressure (P_a)									
Hp [ft]	$\delta (=P_a/P_o)$	[psi]	[psf]	[Pa]	[in Hg]	$\sigma (=p_a/p_o)$	[slg/ft ³]	[kg/m ³]	$\rho_o = 1.225$
Ambient Air Density (ρ_a)									
$\rho_o = .0023769$									
$\rho_o = 1.225$									
Ambient Air Temperature (T_a)									
$T_o = 288.15$									
$T_o = 518.67$									
$T_o = 59$									

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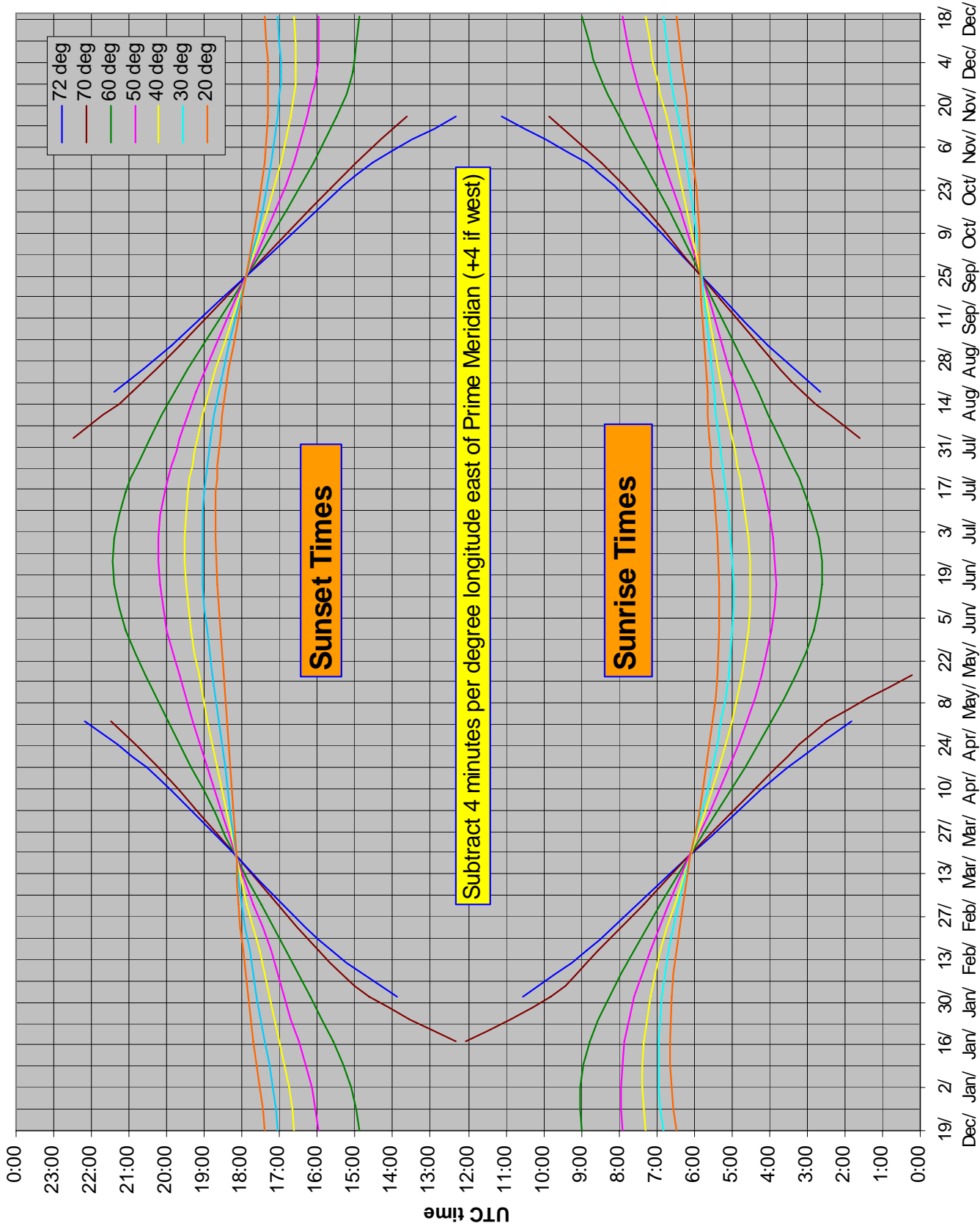
1976 U.S. Standard Atmosphere - Troposphere [11-20 Km]

Ambient Air Pressure (Pa)					Amb. Air Density (ρ _a)			Ambient Air Temperature (T _a)					
H _p [ft]	δ (=P _a /P ₀)	[psi]	[psf]	[Pa]	[in Hg]	σ (= p _a /p ₀)	[slg/ft ³]	[kg/m ³]	θ (=T _a /T ₀)	[K]	[deg C]	[R]	[deg F]
36089	0.223361	3.28251	472.683	22632.1	6.68324	0.297076	0.0007061	0.363918	0.751865	216.650	-56.50	389.97	-69.70
37000	0.213795	3.14192	452.438	21662.7	6.39700	0.284352	0.0006759	0.348332	0.751865	216.650	-56.50	389.97	-69.70
38000	0.203762	2.99449	431.207	20646.2	6.09681	0.271009	0.0006442	0.331986	0.751865	216.650	-56.50	389.97	-69.70
39000	0.194200	2.85397	410.972	19677.3	5.81071	0.258291	0.0006139	0.316407	0.751865	216.650	-56.50	389.97	-69.70
40000	0.185087	2.72004	391.686	18753.9	5.53804	0.246171	0.0005851	0.301559	0.751865	216.650	-56.50	389.97	-69.70
41000	0.176402	2.59240	373.306	17873.9	5.27816	0.234619	0.0005577	0.287408	0.751865	216.650	-56.50	389.97	-69.70
42000	0.168124	2.47075	355.788	17035.1	5.03048	0.223609	0.0005315	0.273921	0.751865	216.650	-56.50	389.97	-69.70
43000	0.160234	2.35480	339.092	16235.7	4.79441	0.213116	0.0005066	0.261067	0.751865	216.650	-56.50	389.97	-69.70
44000	0.152715	2.24430	323.180	15473.9	4.56943	0.203115	0.0004828	0.248816	0.751865	216.650	-56.50	389.97	-69.70
45000	0.145549	2.13899	308.014	14747.7	4.35500	0.193584	0.0004601	0.237140	0.751865	216.650	-56.50	389.97	-69.70
46000	0.138719	2.03861	293.560	14055.7	4.15064	0.184500	0.0004385	0.226012	0.751865	216.650	-56.50	389.97	-69.70
47000	0.132209	1.94295	279.785	13396.1	3.95587	0.175842	0.0004180	0.215406	0.751865	216.650	-56.50	389.97	-69.70
48000	0.126005	1.85177	266.656	12767.5	3.77023	0.167590	0.0003983	0.205298	0.751865	216.650	-56.50	389.97	-69.70
49000	0.120092	1.76487	254.142	12168.3	3.59331	0.159726	0.0003797	0.195664	0.751865	216.650	-56.50	389.97	-69.70
50000	0.114457	1.68206	242.216	11597.3	3.42469	0.152230	0.0003618	0.186482	0.751865	216.650	-56.50	389.97	-69.70
51000	0.109086	1.60312	230.850	11053.1	3.26398	0.145087	0.0003449	0.177731	0.751865	216.650	-56.50	389.97	-69.70
52000	0.103967	1.52789	220.017	10534.4	3.11081	0.138278	0.0003287	0.169391	0.751865	216.650	-56.50	389.97	-69.70
53000	0.099088	1.45620	209.693	10040.1	2.96484	0.131790	0.0003133	0.161442	0.751865	216.650	-56.50	389.97	-69.70
54000	0.094438	1.38786	199.853	9568.9	2.82571	0.125605	0.0002986	0.153866	0.751865	216.650	-56.50	389.97	-69.70
55000	0.090006	1.32273	190.474	9119.9	2.69311	0.119711	0.0002845	0.146646	0.751865	216.650	-56.50	389.97	-69.70
56000	0.085783	1.26066	181.536	8691.9	2.56673	0.114093	0.0002712	0.139764	0.751865	216.650	-56.50	389.97	-69.70
57000	0.081757	1.20151	173.017	8284.1	2.44628	0.108739	0.0002585	0.133206	0.751865	216.650	-56.50	389.97	-69.70
58000	0.077921	1.14512	164.898	7895.3	2.33149	0.103637	0.0002463	0.126955	0.751865	216.650	-56.50	389.97	-69.70
59000	0.074264	1.09139	157.160	7524.8	2.22208	0.098773	0.0002348	0.120997	0.751865	216.650	-56.50	389.97	-69.70
60000	0.070779	1.04017	149.785	7171.7	2.11781	0.094138	0.0002238	0.115319	0.751865	216.650	-56.50	389.97	-69.70
61000	0.067458	0.99136	142.756	6835.2	2.01842	0.089721	0.0002133	0.109908	0.751865	216.650	-56.50	389.97	-69.70
62000	0.064292	0.94484	136.057	6514.4	1.92371	0.085510	0.0002032	0.104750	0.751865	216.650	-56.50	389.97	-69.70
63000	0.061275	0.90050	129.673	6208.7	1.83344	0.081498	0.0001937	0.099835	0.751865	216.650	-56.50	389.97	-69.70
64000	0.058400	0.85825	123.588	5917.4	1.74740	0.077673	0.0001846	0.095150	0.751865	216.650	-56.50	389.97	-69.70
65000	0.055659	0.81797	117.788	5639.7	1.66540	0.074028	0.0001760	0.090685	0.751865	216.650	-56.50	389.97	-69.70
65617	0.054034	0.79408	114.347	5475.0	1.61675	0.071866	0.0001708	0.088036	0.751865	216.650	-56.50	389.97	-69.70

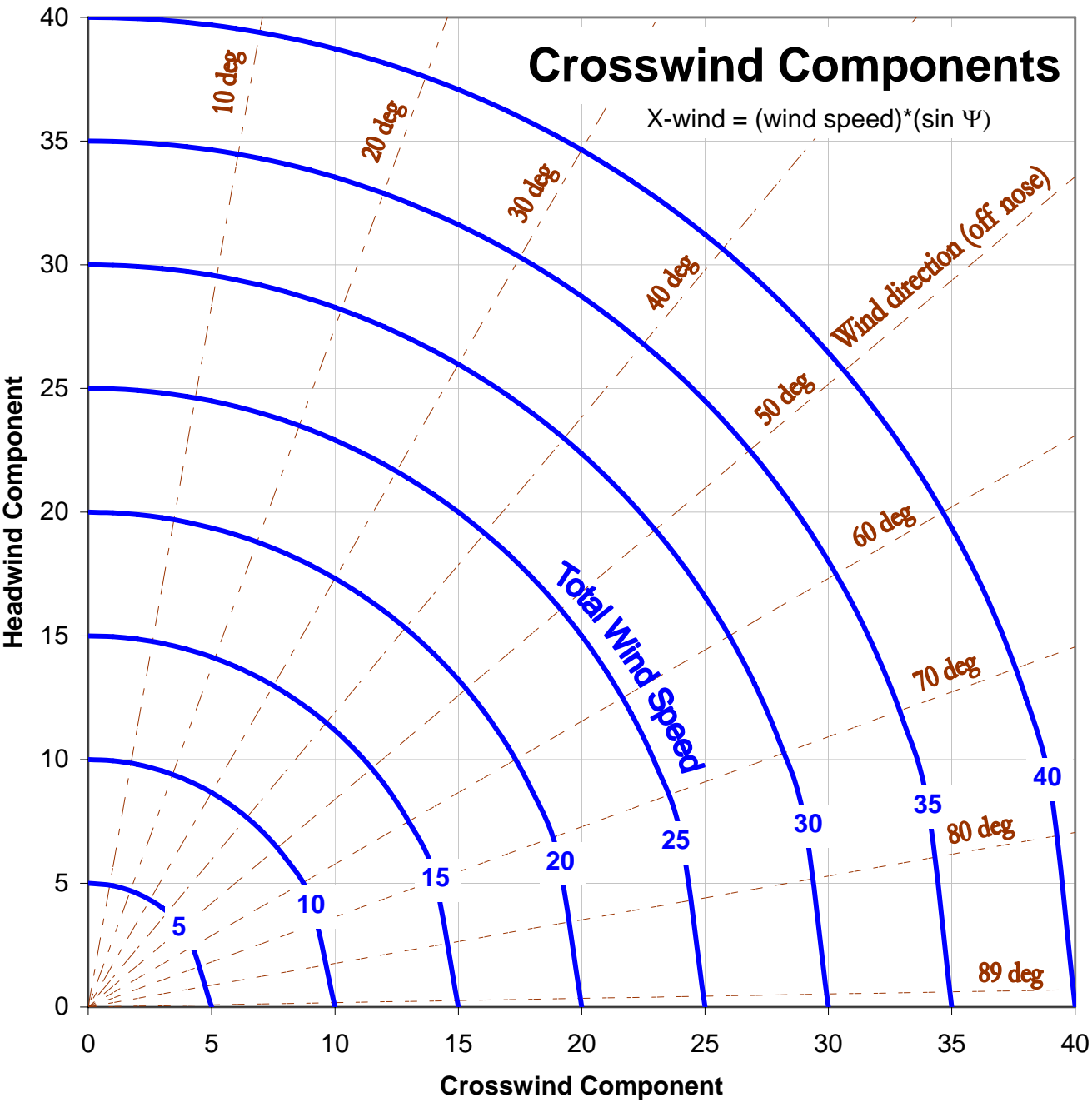
Section 3.5 Sea States(ref 3.3) Sea State
International Swell Scale

Code	Sea	Wave Height, Crest to Trough (ft)
0	Calm	0
1	Smooth	Less than 1
2	Slight	1-3
3	Moderate	3-5
4	Rough	5-8
5	Very rough	8-12
6	High	12-20
7	Very high	20-40
8	Mountainous	40+
9	Confused, Used as additional description 1-8	
Code	Swell	In Open Sea
0	None	low
1	Short or average	
2	Long	
3	Short	Moderate height
4	Average	
5	Long	
6	Short	heavy
7	Average	
8	Long	
9	Confused, Used as additional description 1-8	

Section 3.6 Sunrise Sunset Times



Section 3.7 Crosswind Components



Section 3.9 References

- 3.1 Anon., “Aeronautical Vestpocket Handbook” ,Part No. P&W 079500, United Technologies Pratt & Whitney, Canada, 1990.
- 3.2 Lawless, Alan. R. et al, “Aerodynamics for Flight Testers”, National Test Pilot School, P.O. Box 658, Mojave CA, 93501, 1999.
- 3.3 Denno, Richard R., et al “AIAA Aerospace Design Engineers Guide” ISBN 0-930403-21-5, AIAA, 1987.
- 3.4 Global Positioning System Overview, Peter H. Dana, Department of Geography, University of Texas at Austin, 1994. (www.colorado.edu/geography/gcraft/notes/gps/gps_f.html)
- 3.5 Charles D Ghilani, Penn State College of Engineering, 2008 (<http://surveying.wb.psu.edu/sur351/georef/Ellip4.htm>)
- 3.6 Standard Atmosphere Calculator Website Link <http://www.digitaldutch.com/atmoscalc/>.

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