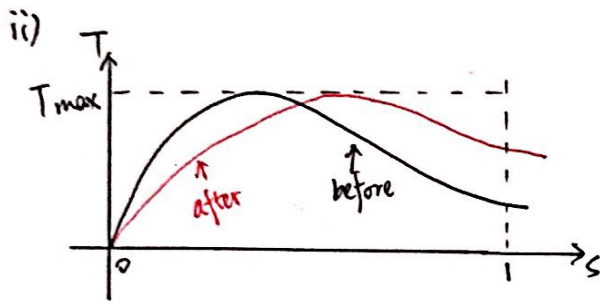


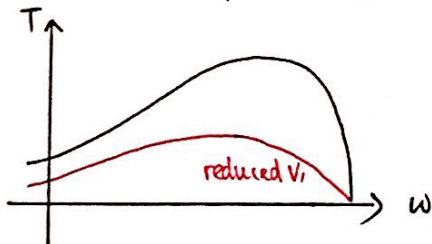
Q1. a) i) increase r_2 

iii) yes, the efficiency will be reduced (rotor loss is increased, slip is also increased)

① try to reduce r_1 , so that there will be less loss at stator.

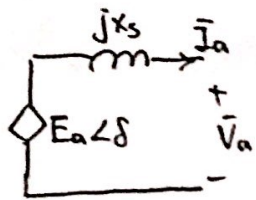
② if a higher starting torque is required, a potentiometer could be used to increase rotor resistance at starting, and set potentiometer to zero at normal operation.

b) When the input voltage is reduced, the torque curve will be affected. ($T \propto V_1^2$)
Like shown in the plot on the left.



At low speeds, when the input voltage is not large enough, the torque provided by the motor may not overcome the friction and windage loss, and thus stop. It will then lead to short circuit and have very high current, which may damage the motor.

Q2 a) 3 phase. 4 pole. 60 Hz. $|\bar{I}_a| = 20 \text{ A}$. PF = 0.9 Lagging.



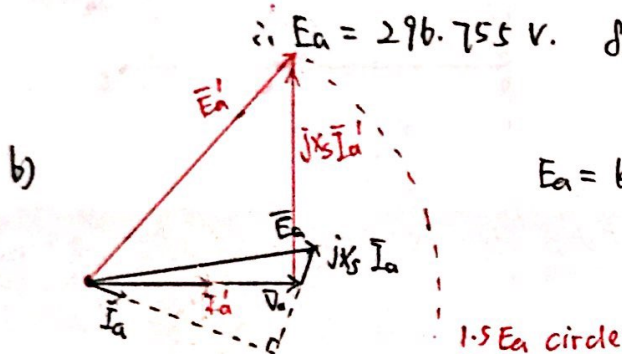
generator convention., \bar{V}_a as reference: $V_a = \frac{480}{\sqrt{3}} \angle 0^\circ \text{ V}$.

PF = 0.9 lagging: $\bar{I}_a = 20 \angle -\cos^{-1}(0.9) = 20 \angle -25.842^\circ \text{ A}$

$$\bar{E}_a = \bar{V}_a + jX_s \bar{I}_a$$

$$= 277.13 \angle 0^\circ + j(2)(20 \angle -25.842^\circ) = 296.755 \angle 6.968^\circ \text{ V}.$$

$$\therefore E_a = 296.755 \text{ V. } \delta = 6.968^\circ$$



$$E_a = k_f \omega I_f, \quad I_f' = \frac{3}{2} I_f = \frac{15}{2} \text{ A} \Rightarrow E_a' = 1.5 E_a$$

c) $\bar{E}_a' = \bar{V}_a + jX_s \bar{I}_a'$, $E_a' = 1.5 E_a = 445.14 \text{ V}$.

$$445.14 \angle \delta' = 277.13 \angle 0^\circ + j(2)(I_a' \angle 0^\circ)$$

$$\hookrightarrow \cos(\delta') = \frac{277.13}{445.14}$$

$$445.14 \sin(\delta') = 2 I_a'$$

$$\delta' = 51.496^\circ$$

$$I_a' = 174.176 \text{ A}.$$

Q3 a) key point.

1) goal: study the stability of the system.

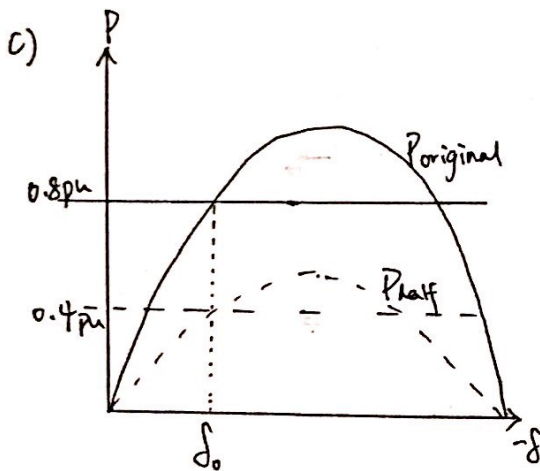
2) method: derive from Newton's second law,

neglect damping torque; assume rotor speed is close to ω_s during transient3) result: get a relation between δ and $\angle P$ to understand the system stability under different changes

$$\left(\frac{d\delta}{dt}\right)^2 \propto \int (P_m - P_e) d\delta$$

4) interpretation: only when the two areas (one for $(P_m - P_e)$; one for $(P_e - P_m)$) are equal, the system can maintain stable.

5) application: e.g. sudden load limit, critical clearing angle.

b) Because the internal voltage is low ($E_a = K \omega I_f$, low field current),
 $P_{max} = \frac{3 E_a V_a}{X_s}$ is low, and the motor operates at a higher torque angle for a given power (P_m) compared to the overexcited case. Hence, the motor can quickly approach unstable operating. (close $\delta = 90^\circ$)
Design change: reduce X_s , E.g. increase airgap.

$$\left. \begin{aligned} 0.8 &= P_{max} \sin \delta_0 \\ 0.4 &= \frac{1}{2} P_{max} \sin \delta_1 \end{aligned} \right\} \Rightarrow \delta_0 = \delta_1$$

no change in torque angle

no area exists

the motor is in stable motor mode.