

Electromagnetism

Day 11

Tutorial on magnetic circuits

ILOs – Day 11 (Tutorial 1)

- Solve numerical problems related to magnetic circuits

#1) An iron ring has cross section area of 100 mm² and mean diameter of 10 cm. Calculate the MMF required to produce a flux of 200 μWb. Assume relative permeability of iron as 800.

Length of flux path = mean length of the ring $l = \pi d = \pi \times 10 \times 10^{-2} = 0.314 \text{ m}$

Area of cross section of the ring, $A = 100 \times 10^{-6} \text{ m}^2$

Relative permeability of iron, $\mu_r = 800$

$$\therefore \text{Reluctance} = \frac{l}{\mu_0 \mu_r A} = \frac{0.314}{4\pi \times 10^{-7} \times 800 \times 100 \times 10^{-6}} = 3.123 \times 10^6$$

$$\phi = \frac{MMF}{\text{Reluctance}} \Rightarrow MMF = \phi \times \text{Reluctance}$$
$$= 200 \times 10^{-6} \times 3.123 \times 10^6 = 624.6 \text{ AT}$$

#2) An iron ring of mean length 30 cm has an air gap of 2 mm and a coil with 200 turns on it. If relative permeability of iron is 300 when a current of 1 A flows through the coil; find the flux density.

Length of flux path = mean length of the ring $l = 30 \text{ cm} = 0.3 \text{ m}$

Relative permeability $\mu_r = 300$

Length of air gap $l_g = 2 \text{ mm} = 0.002 \text{ m}$

Number of turns in coil $N = 200$

Current through coil $I = 1 \text{ A}$

$$\therefore MMF = NI = 200 \text{ AT}$$

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Length of flux path = mean length of the ring $l = 30 \text{ cm} = 0.3 \text{ m}$

Relative permeability $\mu_r = 300$

Length of air gap $l_1 = 2 \text{ mm} = 0.002 \text{ m}$

Let, cross sectional area of the ring is $A \text{ m}^2$.

$$\therefore \text{Resultant flux } \phi = \frac{MMF}{\text{Reluctance}} = \frac{NI}{S} = \frac{NI}{\frac{l_1}{\mu_0 \mu_{r1} A_1} + \frac{l_2}{\mu_0 \mu_{r2} A_2}}$$

Putting $l_1 = 0.002 \text{ m}$, $l_2 = 0.298 \text{ m}$, $\mu_{r1} = 1$, $\mu_{r2} = 300$, and $A_1 = A_2 = A$.

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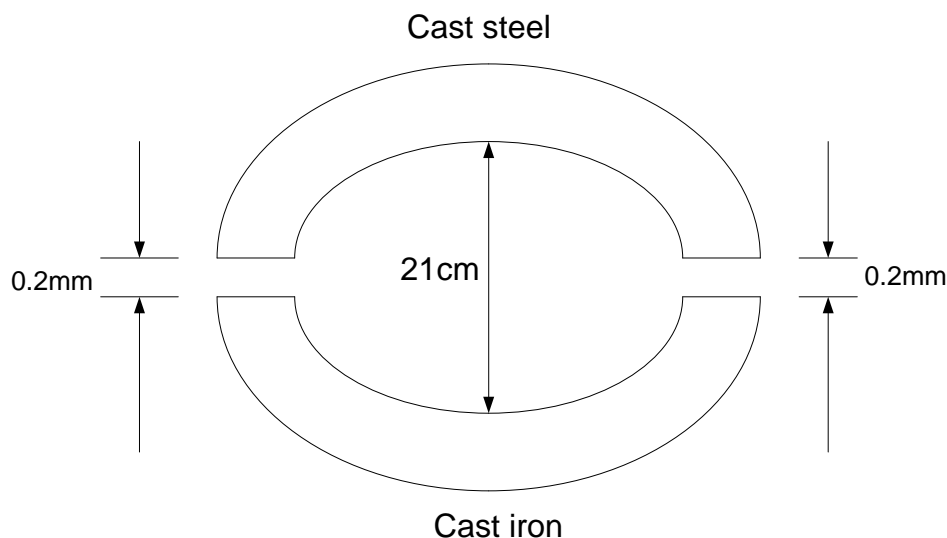
$$\phi = \frac{MMF}{\text{Reluctance}} = \frac{NI}{S} = \frac{NI}{\frac{l_1}{\mu_0 \mu_{r1} A_1} + \frac{l_2}{\mu_0 \mu_{r2} A_2}}$$

$$l_1 = 0.002 \text{ m}, l_2 = 0.298 \text{ m}, \mu_{r1} = 1, \mu_{r2} = 300, \text{ and } A_1 = A_2 = A$$

$$\phi = \frac{200}{\frac{0.002}{4\pi \times 10^{-7} \times 1 \times A} + \frac{0.298}{4\pi \times 10^{-7} \times 300 \times A}} = 0.085A \text{ Wb}$$

$$\therefore \text{Flux density } B = \frac{\phi}{A} = \frac{0.085A}{A} = 0.085 \text{ Wb/m}^2$$

#3) A ring having a mean diameter of 21cm, and a cross section of 10cm² is made of two semi circular sections of cast-iron and cast-steel respectively with each joint having reluctance equal to air-gap of 0.2mm as shown in figure. Determine the ampere-turns required to produce a flux of 0.8mWb. The relative permeabilities of cast-iron and cast-steel are 166 and 800 respectively. Neglect fringing and leakage effects. .



$$\phi = \frac{MMF}{\text{Reluctance}} = \frac{NI}{S} = \frac{AT}{S}$$

$$\therefore AT = \phi \times S$$

For a series magnetic circuit, the total AT required will be summation of ATs required for steel, iron, and air separately:

$$AT = \phi \times [S_{St} + S_{Fe} + S_{air}] = \phi \times \left[\frac{l_1}{\mu_0 \mu_{r1} A_1} + \frac{l_2}{\mu_0 \mu_{r2} A_2} + \frac{l_3}{\mu_0 \mu_{r3} A_3} \right]$$

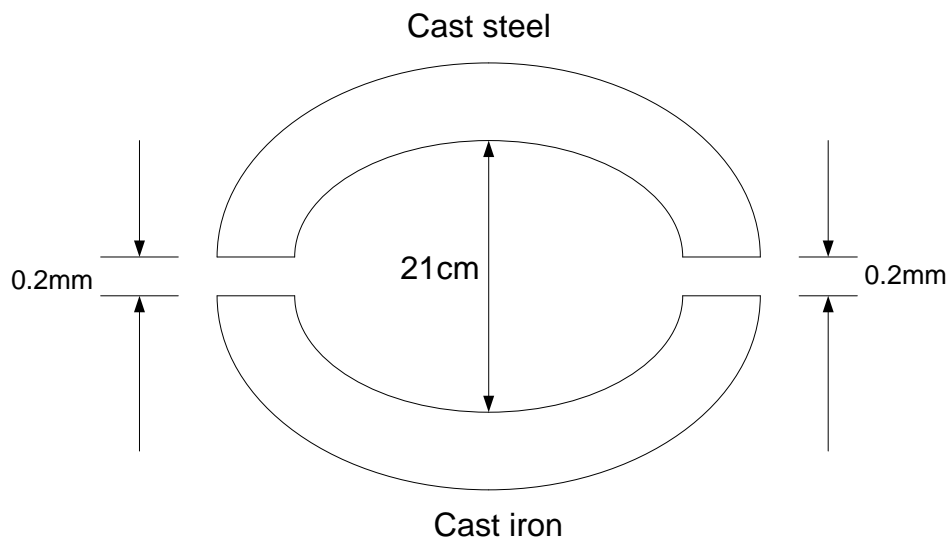
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$$A_1 = A_2 = A_3 = 10 \text{ cm}^2 = 10 \times 10^{-4} \text{ m}^2$$

$$l_3 = 2 \times 0.2 \text{ mm} = 2 \times 0.0002 \text{ m}$$

$$l_1 = l_2 \approx \pi \times 21 \times 10^{-2} / 2 = 0.33 \text{ m}$$



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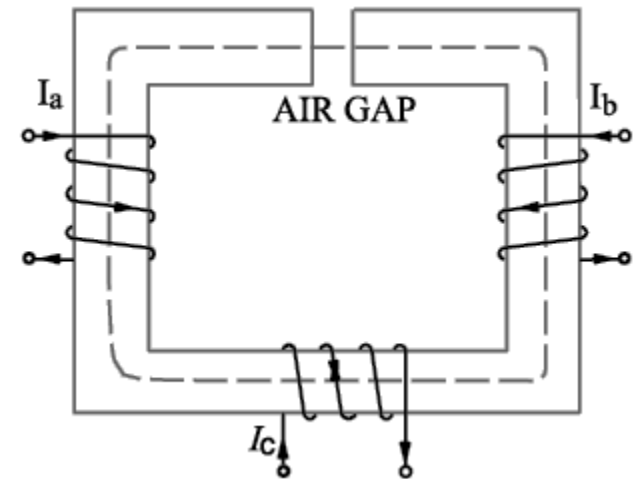
$$l_1 = l_2 \approx \pi \times 21 \times 10^{-2} / 2 = 0.33 \text{ m}$$

$$\therefore AT = 0.8 \times 10^{-3} \times \left[\frac{0.33}{4\pi \times 10^{-7} \times 800 \times 10 \times 10^{-4}} + \frac{0.33}{4\pi \times 10^{-7} \times 166 \times 10 \times 10^{-4}} + \frac{2 \times 0.0002}{4\pi \times 10^{-7} \times 1 \times 10 \times 10^{-4}} \right]$$

$$AT = 0.8 \times 10^{-3} \times [328125 + 1581325 + 318310] = 1782.2$$

#4) A rectangular iron core has a mean length of magnetic path of 100 cm, cross-section of (2 cm × 2 cm), relative permeability of 1400 and an air-gap of 5 mm cut in the core. The three coils carried by the core have number of turns $N_a = 335$, $N_b = 600$ and $N_c = 600$; and the respective currents are 1.6 A, 4 A and 3 A. The directions of the currents are as shown. Find the flux in the air-gap.

By applying the Right-Hand Thumb rule, it is found that fluxes produced by the current I_a and I_b are directed in the clockwise direction through the iron core whereas that produced by current I_c is directed in the anticlockwise direction through the core.



$$\therefore \text{Total MMF} = N_a I_a + N_b I_b - N_c I_c = 335 \times 1.6 + 600 \times 4 - 600 \times 3 = 1136 \text{ AT}$$

$$\text{Reluctance of the air-gap} = \frac{l_G}{\mu_0 A} = \frac{5 \times 10^{-3}}{4\pi \times 10^{-7} \times 4 \times 10^{-4}} = 9.95 \times 10^6 \text{ AT/Wb}$$

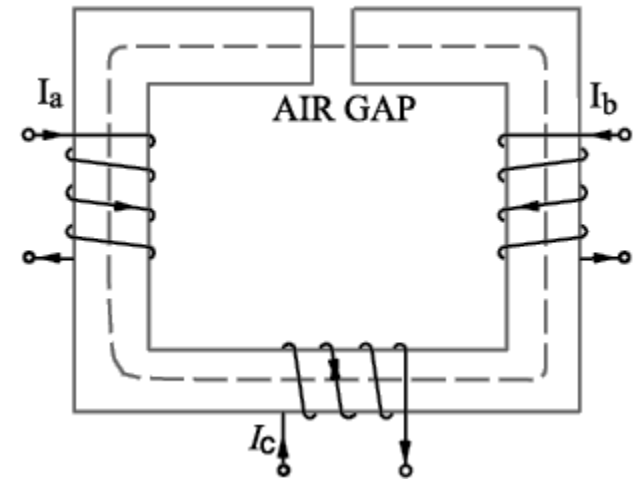
$$\text{Reluctance of iron path} = \frac{l_i}{\mu_0 A} = \frac{100 \times 10^{-2} - 5 \times 10^{-3}}{4\pi \times 10^{-7} \times 1400 \times 4 \times 10^{-4}} = 1.414 \times 10^6 \text{ AT/Wb}$$

#4) A rectangular iron core has a mean length of magnetic path of 100 cm, cross-section of (2 cm × 2 cm), relative permeability of 1400 and an air-gap of 5 mm cut in the core. The three coils carried by the core have number of turns $N_a = 335$, $N_b = 600$ and $N_c = 600$; and the respective currents are 1.6 A, 4 A and 3 A. The directions of the currents are as shown. Find the flux in the air-gap.

$$\therefore \text{Total MMF} = 1136 \text{ AT}$$

$$\text{Reluctance of the air-gap} = 9.95 \times 10^6 \text{ AT/Wb}$$

$$\text{Reluctance of iron path} = 1.414 \times 10^6 \text{ AT/Wb}$$



$$\therefore \text{Total reluctance, } S = 9.95 \times 10^6 + 1.414 \times 10^6 = 11.36 \times 10^6 \text{ AT/Wb}$$

In the series circuit, flux in the air-gap is the same as in the iron core

$$\therefore \text{Air-gap flux, } \phi = \frac{\text{MMF}}{\text{Reluctance}} = \frac{1136}{11.36 \times 10^6} = 100 \times 10^{-6} \text{ Wb} = 100 \mu\text{Wb}$$

#5) A magnetic circuit made of mild steel is arranged as shown in Fig. The central limb is wound with 500 turns and has a cross-sectional area of 800 mm^2 . Each of the outer limbs has a cross-sectional area of 500 mm^2 . The air-gap has a length of 1 mm . Calculate the current required to set up a flux of 1.3 mWb in the central limb assuming no magnetic leakage and fringing. Mild steel required 3800 AT/m to produce flux density of 1.625 T and 850 AT/m to produce flux density of 1.3 T .

Central limb

Flux in the central limb, $\phi_c = 1.3 \times 10^{-3} \text{ Wb}$

Area of central limb, $A_c = 800 \times 10^{-6} \text{ m}^2$

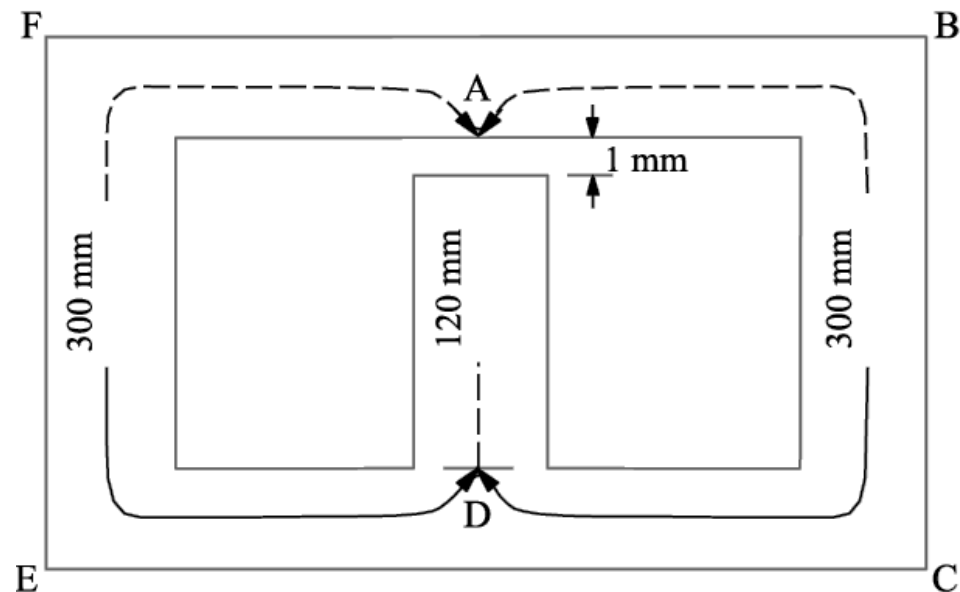
\therefore Flux density in central limb:

$$B_c = \frac{\phi_c}{A_c} = \frac{1.3 \times 10^{-3}}{800 \times 10^{-6}} = 1.625 \text{ T}$$

Corresponding value of H for this flux density is given as 3800 AT/m .

Since the length of the central limb is ($l_c = 120 - 1 = 119$) mm, MMF required is:

$$AT_c = H_c \times l_c = 3800 \times (119 \times 10^{-3}) = 452.2 \text{ AT}$$



#5) A magnetic circuit made of mild steel is arranged as shown in Fig. The central limb is wound with 500 turns and has a cross-sectional area of 800 mm^2 . Each of the outer limbs has a cross-sectional area of 500 mm^2 . The air-gap has a length of 1 mm . Calculate the current required to set up a flux of 1.3 mWb in the central limb assuming no magnetic leakage and fringing. Mild steel required 3800 AT/m to produce flux density of 1.625 T and 850 AT/m to produce flux density of 1.3 T .

Air gap

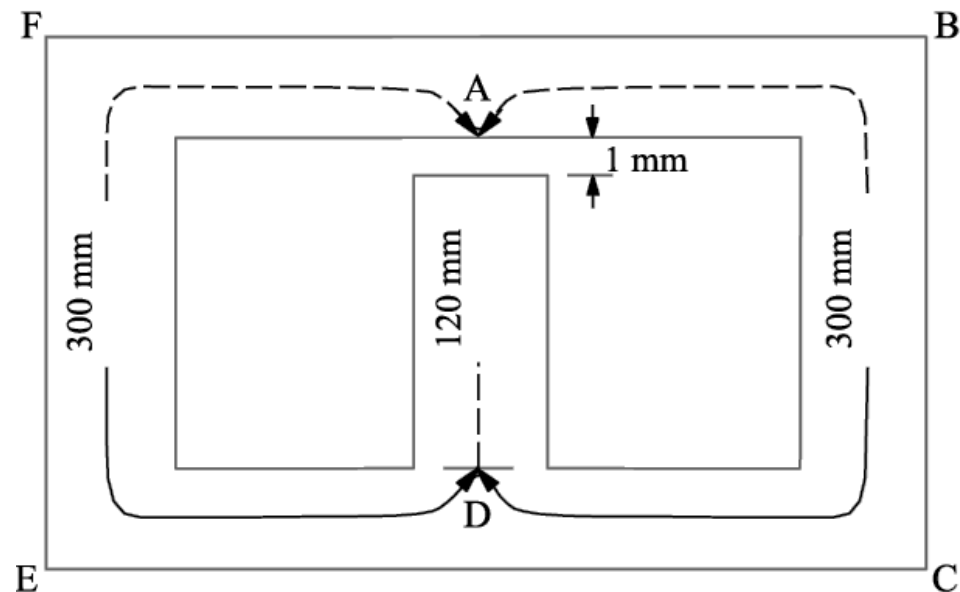
Since air gap is in the central limb, flux density in the air-gap is the same as that in the central limb, $B_{air} = 1.625 \text{ T}$

Corresponding value of H for this flux density is given by:

$$H_{air} = \frac{B_{air}}{\mu_0} = \frac{1.625}{4\pi \times 10^{-7}} = 0.1293 \times 10^7 \text{ AT/m}$$

Since the length of air gap is ($l_{air} = 1$) mm, MMF required for air gap is:

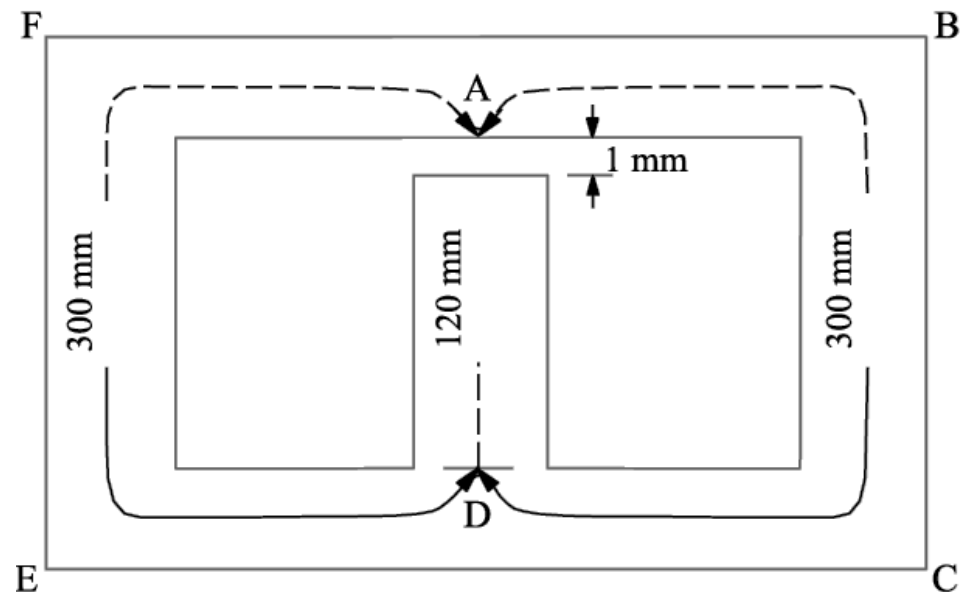
$$AT_{air} = H_{air} \times l_{air} = 0.1293 \times 10^7 \times 1 \times 10^{-3} = 1293 \text{ AT}$$



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Outer limb

The flux of the central limb divides equally at point A in figure along the two parallel path $ABCD$ and $AFED$. We may consider either path, say $ABCD$ and calculate the MMF required for it. The same MMF will also send the flux through the other parallel path $AFED$.



Flux through $ABCD$, $\phi_o = \phi_c/2 = 1.3 \times 10^{-3}/2 = 0.65 \times 10^{-3} \text{ Wb}$

Area of outer limb, $A_o = 500 \times 10^{-6} \text{ m}^2$

\therefore Flux density in outer limb: $B_o = \frac{\phi_o}{A_o} = \frac{0.65 \times 10^{-3}}{500 \times 10^{-6}} = 1.3 \text{ T}$

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Outer limb

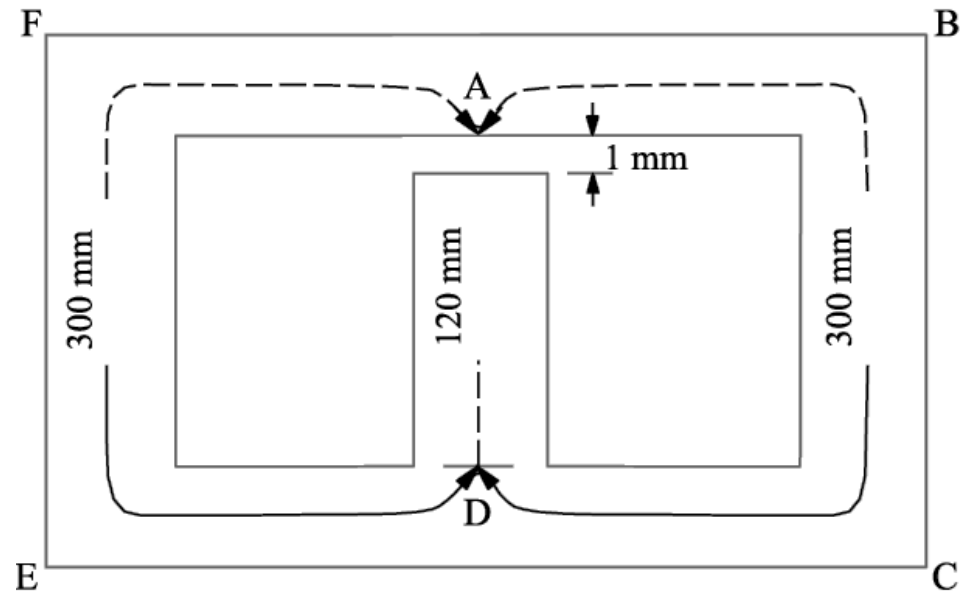
$$B_o = \frac{\phi_o}{A_o} = \frac{0.65 \times 10^{-3}}{500 \times 10^{-6}} = 1.3 \text{ T}$$

The corresponding value of H for this value of B_o is given as 850 AT/m

Since the length of the outer limb ABCD is ($l_o = 300$) mm, MMF required is:

$$AT_o = H_o \times l_o = 850 \times (300 \times 10^{-3}) = 255 \text{ AT}$$

Since the two outer limbs are in parallel, this MMF will also send the same flux in the parallel path $AFED$ also.



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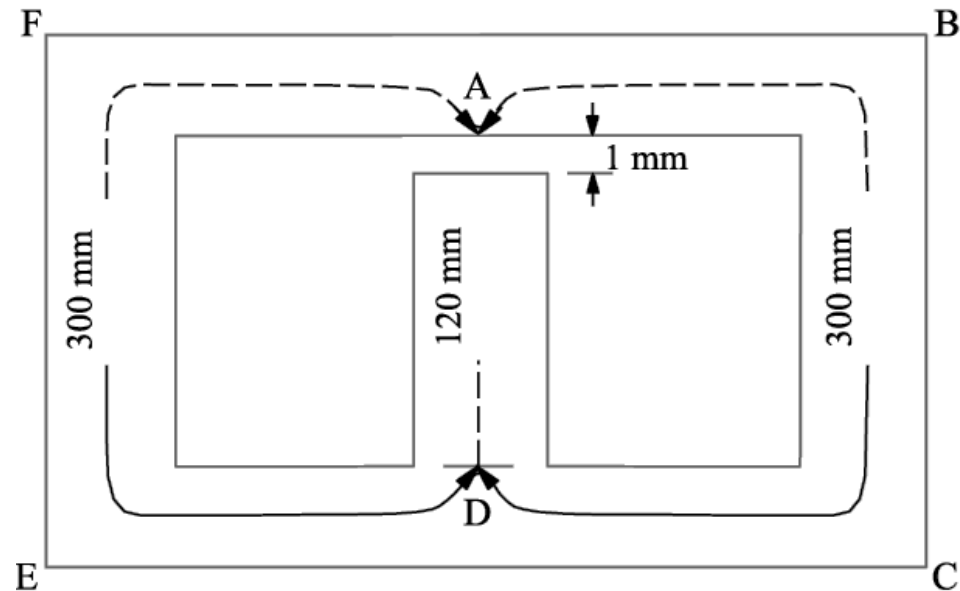
Total MMF

Central limb : $AT_c = 452.2 \text{ AT}$

Air gap : $AT_{air} = 1293 \text{ AT}$

Outer limb : $AT_o = 255 \text{ AT}$

$$= 452.2 + 1293 + 255 = 2000.2 \text{ AT}$$



Since the number of turns is 500, current required in coil: $I = 2000.2/500 \approx 4\text{A}$