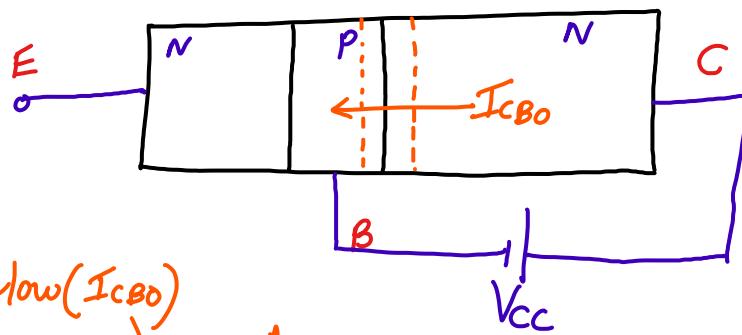


* Leakage currents in BJT:

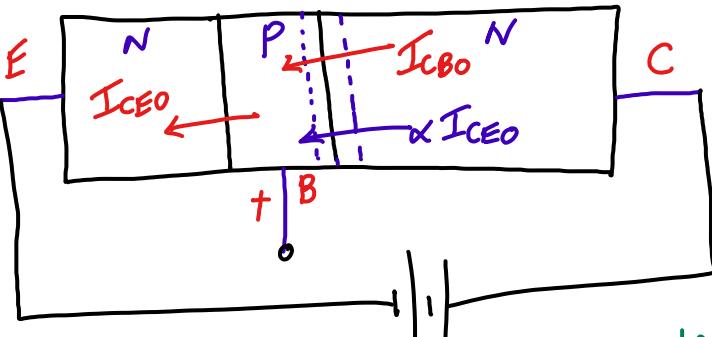
- If we set $I_E = 0$
(emitter open)
- Transistor \rightarrow cut-off mode
- $B-C J^n$ is still R.B

\rightarrow R.B leakage current will flow (I_{CBO})



$\rightarrow I_{CBO}$: Collector leakage current in CB configuration
 $I_{CEO} = 10 \text{nA}$ $\alpha I_{CEO} = 9 \text{nA}$ $\alpha = 0.9$

$$I_C = \alpha I_E$$



$$I_{CEO}^{10 \text{nA}} = \alpha I_{CEO} + I_{CBO}$$

$$I_{CEO} (1-\alpha) = I_{CBO}$$

$$* I_{CEO} = \frac{I_{CBO}}{1-\alpha}$$

$$I_B = 0 \mu\text{A}$$

- $I_{CEO} \rightarrow$ leakage current betw E & C with Base open ($I_B = 0$)

$I_{CBO} \rightarrow$ R.B BC p-n-j^n

cause base potential to rise

F.B B-EJ^n & induces
B-E current ' I_{CEO}'

αI_{CEO} — collector current resulting from emitter current I_{CEO}

$$\rightarrow I_C = \alpha I_E + I_{CBO}$$

$$I_E = I_C + I_B$$

$$I_C = \alpha (I_C + I_B) + I_{CBO}$$

$$I_C (1-\alpha) = \alpha I_B + I_{CBO}$$

$$I_C = \left(\frac{\alpha}{1-\alpha} \right) I_B + \left(\frac{1}{1-\alpha} \right) I_{CBO}$$

$$\text{i.e. } I_C = \beta I_B + (1+\beta) I_{CBO}$$

$$\text{if } I_B = 0, I_C = (1+\beta) I_{CBO}$$

$$I_C = 100 \mu\text{A}$$

$$\beta = \frac{\alpha}{1-\alpha}$$

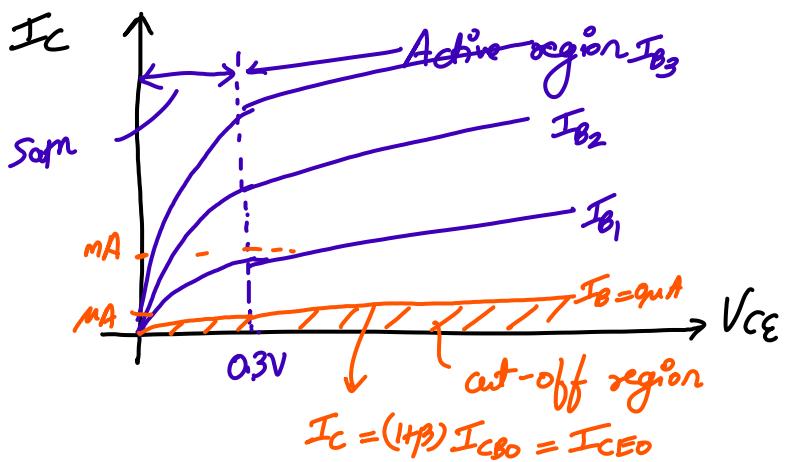
$$1+\beta = 1 + \frac{\alpha}{1-\alpha}$$

$$= \frac{1-\alpha+\alpha}{1-\alpha}$$

$$1+\beta = \frac{1}{1-\alpha}$$

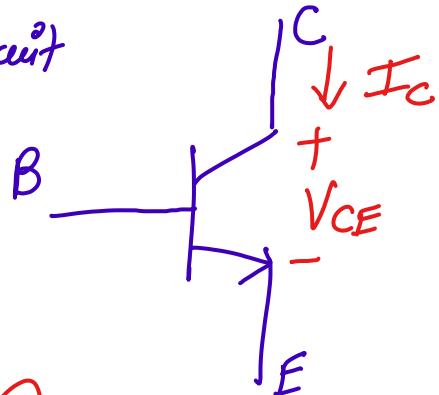
$$I_{CEO} = \frac{I_{CBO}}{1-\alpha} = 1+\beta (I_{CBO})$$

$$I_c = \beta I_B + I_{CEO}$$



* Transistor Biasing (BJT):

→ establishing & maintaining proper collector to emitter voltage ' V_{CE} ' and collector current in the circuit
 "Transistor biasing"



I_c and V_{CE} can change due to

- ① Variation in temperature
- ② -||- gain
- ③ -||- leakage current
- ④ -||- supply voltage

I_c & V_{CE} should not change

Need of Biasing:

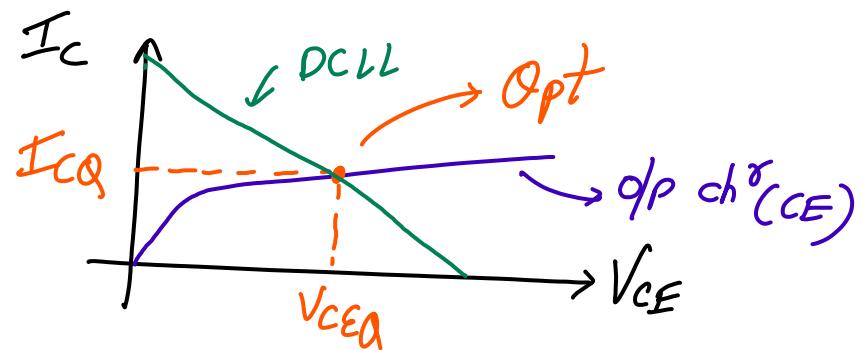
- ① I_c
- ② V_{BE}
- ③ V_{CE}
- ④ Eliminates additional dc supply

→ Value of I_c & V_{CE} is expressed in terms of Operation Point (Q pt)

$$Q_{opt} \equiv (V_{CEQ}, I_{CQ})$$

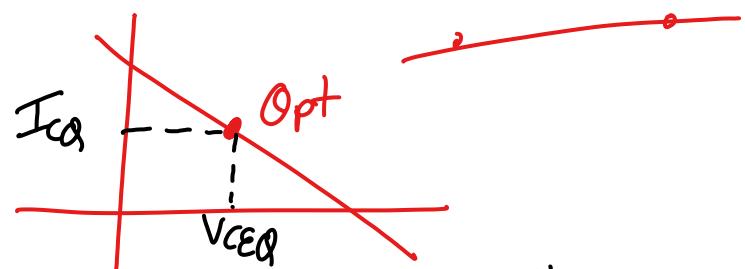
→ For faithful amplification: Q_{opt} must be selected properly

"DC Load Line"
(DC LL)



* Need of Stabilization:

The rate of change of collector current w.r.t collector leakage current "I_{co}" at constant β & V_{BE} is called "Stability factor" (S)



$$S_{I_{CO}} = \frac{\partial I_c}{\partial I_{CO}} \quad | \quad \beta, V_{BE} \text{ constant}$$

3 methods to bias the BJT "Three Biasing ckt's"

- ① Fixed bias
- ② Collector to base bias
- ③ Voltage divider bias

$$I_c = \beta I_B + I_{CO} (1+\beta) \quad \text{--- (1)}$$

Differentiate eq (1) w.r.t I_c ,

$$\frac{\partial I_c}{\partial I_c} = \beta \frac{\partial I_B}{\partial I_c} + (1+\beta) \frac{\partial I_{CO}}{\partial I_c}$$

$$S = \frac{\partial I_c}{\partial I_{CO}}$$

$$1 - \beta \frac{\partial I_B}{\partial I_c} = (1+\beta) \frac{1}{S}$$

$$S_{I_{CO}} = \frac{(1+\beta)}{1 - \beta \left(\frac{\partial I_0}{\partial I_C} \right)}$$

or S'
Stability factor

30, 40, 72, 78, 67, 16,
6, 58

→ Attendance AEC lec 5 (28/7/23)

