
LINEAR SYSTEMS CONTROL
Solutions to Problems

Problem 5.10

This problem concerns a D.C. motor which is to be used as an electronic throttle control for a spark ignition engine. The control object is basically a D.C. motor which has an increased moment of inertia due to the throttle plate (see example 2.3).

- a. The system matrices are (given that position control is desired):

$$\mathbf{A} = \begin{pmatrix} 0 & 1 \\ 0 & -\alpha \end{pmatrix}, \quad \mathbf{B} = \begin{pmatrix} 0 \\ \beta \end{pmatrix}, \quad \mathbf{R}_1 = \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix}, \quad \mathbf{R}_2 = r_2$$

The Riccati equation for this system is

$$0 = \mathbf{P}\mathbf{A} + \mathbf{A}^T\mathbf{P} + \mathbf{R}_1 - \mathbf{P}\mathbf{B}\mathbf{R}_2^{-1}\mathbf{B}^T\mathbf{P}$$

$$\begin{aligned} 0 &= \begin{pmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{pmatrix} \begin{pmatrix} 0 & 1 \\ 0 & -\alpha \end{pmatrix} + \begin{pmatrix} 0 & 0 \\ 1 & -\alpha \end{pmatrix} \begin{pmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{pmatrix} \\ &+ \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix} - \begin{pmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{pmatrix} \begin{pmatrix} 0 \\ \beta \end{pmatrix} \frac{1}{r_2} \begin{pmatrix} 0 & \beta \end{pmatrix} \begin{pmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{pmatrix} \end{aligned}$$

$$0 = 1 - \frac{\beta^2}{r_2} p_{12}^2$$

$$\Rightarrow 0 = p_{11} - \alpha p_{12} - \frac{\beta^2}{r_2} p_{12} p_{22}$$

$$0 = 2(p_{12} - \alpha p_{22}) - \frac{\beta^2}{r_2} p_{22}^2$$

These equations can be solved simultaneously to find that:

$$p_{12} = \frac{\sqrt{r_2}}{\beta}$$

$$p_{22} = \frac{r_2}{\beta^2} \left(-\alpha + \sqrt{\alpha^2 + \frac{2\beta}{\sqrt{r_2}}} \right)$$

$$p_{11} = \frac{\sqrt{r_2}}{\beta} \sqrt{\alpha^2 + \frac{2\beta}{\sqrt{r_2}}}$$

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The LQR gain is then given by

$$\begin{aligned}
 \mathbf{K} &= \mathbf{R}_2^{-1} \mathbf{B}^T \mathbf{P} = -\frac{1}{r_2} \begin{pmatrix} 0 & \beta \end{pmatrix} \begin{pmatrix} p_{11} & p_{12} \\ p_{12} & p_{22} \end{pmatrix} \\
 &= -\frac{\beta}{r_2} \begin{pmatrix} p_{12} & p_{22} \end{pmatrix} \\
 &= -\begin{bmatrix} \frac{1}{\sqrt{r_2}} & \frac{1}{\beta} \left(-\alpha + \sqrt{\alpha^2 + \frac{2\beta}{\sqrt{r_2}}} \right) \end{bmatrix}
 \end{aligned}$$

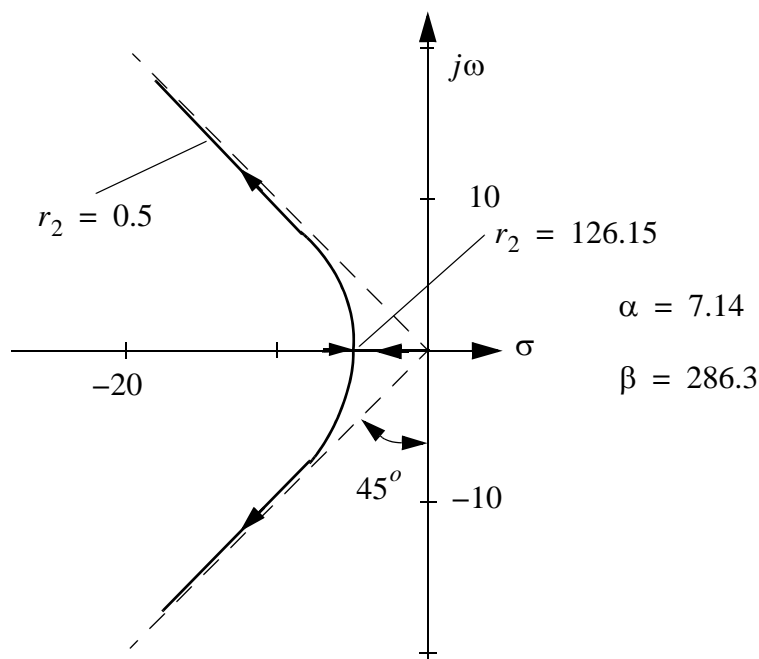
b. The characteristic equation for the system is

$$\det[s\mathbf{I} - (\mathbf{A} - \mathbf{BK})] = s^2 + s \sqrt{\alpha^2 + \frac{2\beta}{\sqrt{r_2}}} + \frac{\beta}{\sqrt{r_2}} = 0$$

which has the solutions:

$$s_0 = -\frac{1}{2} \sqrt{\alpha^2 + \frac{2\beta}{\sqrt{r_2}}} \pm \frac{1}{2} \sqrt{\alpha^2 - \frac{2\beta}{\sqrt{r_2}}}.$$

The plot below shows the root curve as a function of the weight parameter r_2 .



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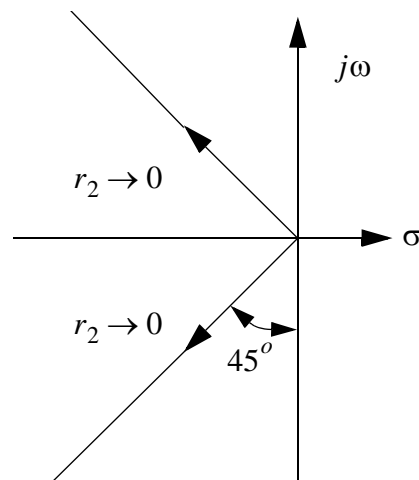
The asymptotes for the root curve are shown dashed on the figure: they correspond to the order of the system which is 2. Using the parameter values, $\alpha = 7.14$, $\beta = 286.3$, and the input weighting, $r_2 = 0.5$, the specified system response time (time constant) of 50 msec can be achieved with the feedback matrix:

$$\mathbf{K} = [1.414 \quad 0.0775].$$

The time constant is reasonable for a real automotive throttle control.

The branch point is at $s_{bp} = -5.049$. Notice that as $r_2 \rightarrow 0$ more and more power is used to control the system as it becomes faster and faster.

- c. If the motor damping, α , is zero then the root curve look like the figure below



- d. The value of r_2 which gives a response time (time constant) of 50 msec is 0.5. The system response to a given set of initial conditions can be calculated by finding the systems transition matrix.

$$\bar{\mathbf{x}}(t) = \bar{\Phi}(t, 0) \bar{\mathbf{x}}(0) \quad \text{since} \quad u(t) = 0$$

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$$\mathbf{A}_K = \mathbf{A} - \mathbf{B}\mathbf{K} = \begin{pmatrix} 0 & 1 \\ -404.8 & -29.33 \end{pmatrix}$$

$$\Rightarrow [s\mathbf{I} - \mathbf{A}_K]^{-1} = \begin{pmatrix} \frac{s + 29.33}{\Delta} & \frac{1}{\Delta} \\ \frac{-404.8}{\Delta} & \frac{s}{\Delta} \end{pmatrix},$$

$$\Delta = s^2 + 29.33s + 404.8$$

The roots of the characteristic equation are $s_0 = -14.67 \pm j13.77$.

Note now that:

$$L^{-1}\left\{\frac{1}{(s+a)^2 + b^2}\right\} = \frac{e^{-at} \sin bt}{b}$$

$$L^{-1}\left\{\frac{s+a}{(s+a)^2 + b^2}\right\} = e^{-at} \cos bt$$

$$s^2 + 2sa + a^2 + b^2 = s^2 + 29.33s + 404.8$$

$$\begin{cases} \Rightarrow 2a = 29.33 \Rightarrow a = 14.665 \\ \Rightarrow a^2 + b^2 = 404.8 \Rightarrow b = 13.775 \end{cases}$$

$$\Phi(t, 0) = L^{-1}[s\mathbf{I} - \mathbf{A}_K]^{-1} = \begin{pmatrix} \Phi_{11}(t, 0) & \Phi_{12}(t, 0) \\ \Phi_{21}(t, 0) & \Phi_{22}(t, 0) \end{pmatrix}$$

$$x(0) = \begin{pmatrix} 0.3 \\ 0 \end{pmatrix} \Rightarrow x(t) = \Phi(t, 0)x(0) = 0.3 \begin{bmatrix} \Phi_{11}(t, 0) \\ \Phi_{21}(t, 0) \end{bmatrix}$$

Thus

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$$\begin{aligned}x(t) &= 0.3L^{-1} \left[\frac{s + 29.33}{(s + 14.665)^2 + 13.775^2} \right. \\&\quad \left. \frac{-404.8}{(s + 14.665)^2 + 13.775^2} \right] \\&= \begin{bmatrix} 0.3e^{-14.665t} \cos(189.74t) \\ -0.64e^{-14.665t} \sin(189.74t) \end{bmatrix}\end{aligned}$$

□