

Name: Spencer Goulette

- Make sure you write your name on all pages.
- Detailed descriptions of how you solved the problem will get you maximum partial credit if your final answer is wrong.
- You must provide the correct unit along with your answer in the answer areas. An answer without its unit will be considered incorrect.
- You may use any calculator, as long as it is a calculator and not another instrument being used in calculator mode.
- A table of commonly used constants, parameters and equations was provided to you in class and on BlackBoard.
- Unless noted otherwise, assume room temperature conditions, i.e. $T = 300\text{K}$
- All MOSFETs in this exam are enhancement-mode MOSFETs, as studied in class to date.

Question	Grade	Out of
#1	15	15
#2	20	20
#3	20	22
#4	16	16
#5	22	27
Total Grade	93	100

YES OPIE!!!

Name: Spencer Goodell

1. (15 pts.) Each correct answer is worth +1 points. *Indicate if the following statements are True or False:*

T

Active loads are preferred in IC design because large gains can be obtained with small devices.

F

A cascode amplifier has a larger output voltage swing than a single stage common source amplifier when biased with the same supply voltages.

F

If a BJT and a MOSFET are biased with the same current, the MOSFET will most likely have the larger intrinsic gain.

T

A BJT's intrinsic gain is device parameter dependent.

T

A cascode amplifier has larger voltage gain than a single stage common source amplifier because it has larger output resistance.

T

A source follower is a suitable choice to put before a common gate stage to increase the input resistance of the amplifier.

T

A cascode current mirror's advantage over a simple current mirror is that its output current is more stable with respect to voltage variations across its output terminals.

F

A simple current mirror has a smaller voltage compliance range than a cascode current mirror.

F

Active loads don't have any advantages over resistors for discrete amplifier circuits.

T

A common gate amplifier is a current buffer.

F

The body effect makes a MOSFET's threshold voltage magnitude smaller.

T

Biasing amplifiers with current mirrors instead of resistor networks ensures operating point stability.

T

Using a current mirror as a load allows the amplifier designer to decouple the DC bias voltages from the small-signal voltage gain.

F

An amplifier's performance is independent of temperature.

F

A MOSFET is a current controlled current source.

Name: Spencer Gaudette

2. (20 points). Each of the questions below are quick calculation-questions, usually requiring a single equation.

- a) A BJT is biased with a nominal collector current of $I_{C0} = 2 \text{ mA}$ has an output resistance of $r_o = 40 \text{ k}\Omega$ and a collector-emitter voltage drop of $V_{CE} = 8 \text{ V}$. What is the actual collector current, assuming $V_{CE,sat}$ is negligible?

$$I_C = I_{C0} \left(1 + \frac{\Delta V_{CE}}{V_A} \right)$$

$$I_C = 2 \text{ mA} \left(1 + \frac{8 \text{ V}}{80} \right)$$

$$I_C = \underline{2.2 \text{ mA}}$$

$$r_o = \frac{V_A}{I_{C0}} = 40 \text{ k}\Omega \cdot 2 \text{ mA} = 80$$

- b) What is the intrinsic gain A_o of a BJT which has $r_o = 300 \text{ k}\Omega$ at $I_C = 200 \mu\text{A}$?

$$r_o = \frac{V_A}{I_C} = 300 \text{ k}\Omega = \frac{V_A}{200 \mu\text{A}}$$

$$A_o = \underline{2.31 \text{ KV/V}}$$

$$V_A = 60$$

$$A_o = \frac{V_A}{V_T} = \frac{60}{26 \text{ mV}} = 2,307,692.308$$

- c) What is the output resistance of a MOSFET which has $L = 0.5 \mu\text{m}$, $V_A' = 8 \text{ V}/\mu\text{m}$, and is biased with $I_{DS} = 100 \mu\text{A}$?

$$r_o = \frac{V_A' L}{I_{DS}}$$

$$r_o = \frac{8 \text{ V}/\mu\text{m} \cdot 0.5 \mu\text{m}}{100 \mu\text{A}} = 40 \text{ k}\Omega$$

$$r_o = \underline{40 \text{ k}\Omega}$$

- d) A MOSFET cascode current mirror is biased such that the transistors have a small signal transconductance of $g_m = 0.1 \text{ mA/V}$ and an output resistance of $r_o = 200 \text{ k}\Omega$?

$$R_{out} = r_o + r_o + g_m r_o^2 \approx g_m r_o^2 \quad R_{out} = \underline{4.4 \text{ M}\Omega}$$

$$\text{actual: } 4.4 \text{ M}\Omega$$

$$\text{approx: } 4 \text{ M}\Omega$$

- e) A MOSFET has an intrinsic gain of $A_o = 50 \text{ V/V}$ when biased with $I_{DS} = 400 \mu\text{A}$. What is its intrinsic gain when it is biased with $I_{DS} = 100 \mu\text{A}$?

$$A_o \propto \frac{1}{\sqrt{I_{DS}}}$$

$$A_o = \underline{100 \text{ V/V}}$$

$$\frac{1}{\sqrt{\frac{1}{4} I_{DS}}} = \frac{1}{\frac{1}{2} \sqrt{I_{DS}}} = 2 \cdot \frac{1}{\sqrt{I_{DS}}}$$

Name: Spencer Gaudette

3. (22 points) The small-signal equivalent circuit of a two-stage amplifier is shown in the figure below. The transistors have been replaced with their hybrid- π equivalent circuits. The component values are given below.

$g_{m1} = 5 \text{ mA/V}$

$r_{o1} = 20 \text{ k}\Omega$

$g_{m2} = 40 \text{ mA/V}$

$r_{o2} = 40 \text{ k}\Omega$

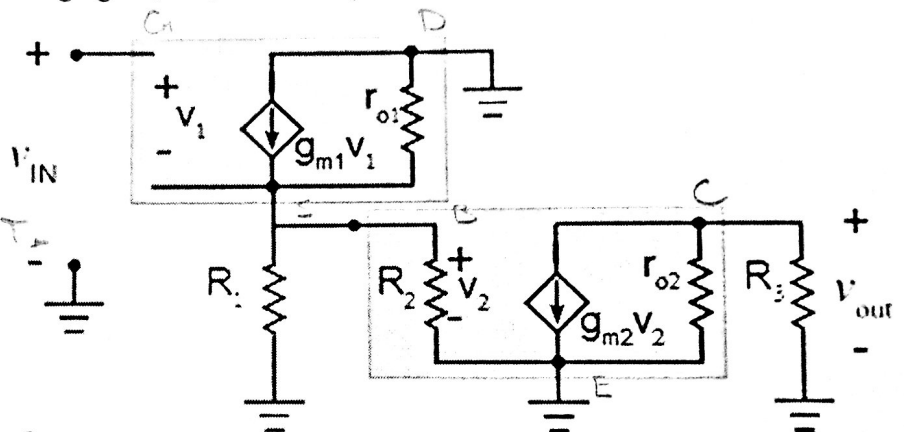
$R_1 = 20 \text{ k}\Omega$

$R_2 = 5 \text{ k}\Omega$

$R_3 = 40 \text{ k}\Omega$

- (a) Identify if the transistors are MOSFET or BJT. Explain how you determined transistor type.
- (b) Identify each of the two stages: CS / CE, CG / CB, or SF / EF.
- (c) Calculate the overall voltage gain, G_v , of the amplifier.

a. 1st transistor doesn't have an r_{π} , but has an open as the input so it is a MOSFET. The 2nd transistor does have an r_{π} , so it is a BJT.



b. Drain is connected to common, so Source Follower. Emitter is connected to common, so Common Emitter.

c. $G_v = A_{v1} \cdot A_{v2}$

$$A_{v1} = \frac{R_1 \parallel R_2 \parallel g_{m1}}{g_{m1} \parallel R_1 \parallel R_2 + 1/g_{m1}} = \frac{20\text{k} \parallel 5\text{k}}{20\text{k} \parallel 5\text{k} + 1/5\text{mA/V}} = 0.9524 \text{ V/V}$$

$$A_{v2} = -g_{m2}(r_{o2} \parallel R_3)$$

$$A_{v2} = -40\text{mA/V}(40\text{k} \parallel 40\text{k})$$

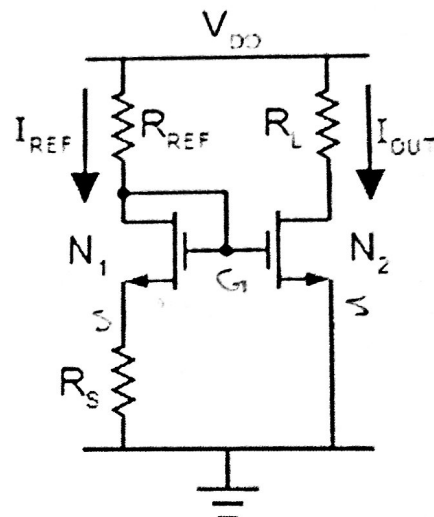
$$A_{v2} = -800$$

$G_v = -762 \text{ V/V}$

(a) Transistor 1	<u>MOSFET</u>
Transistor 2	<u>BJT</u>
(b) Stage 1	<u>SF</u>
Stage 2	<u>CE</u>
(c) G_v	<u>-762 V/V</u>

Name: Spencer Colette

4. (16 points) The current mirror in the figure below is designed with MOSFETs that have $k_n = 10 \text{ mA/V}^2$ and $V_t = 0 \text{ V}$. The circuit is to have $I_{\text{load}} = 20 \text{ mA}$ and $I_{\text{ref}} = 200 \mu\text{A}$. $V_{\text{DD}} = +10\text{V}$. Calculate the values of R_S and R_{REF} needed to meet these design specifications.



$$k_n = 10 \text{ mA/V}^2$$

MOSFET M_1 and M_2 are the same

$$I_{\text{out}} = \frac{1}{2} k_n V_{\text{ov},1}^2$$

$$20 \text{ mA} = \frac{1}{2} \cdot 10 \text{ mA/V}^2 \cdot V_{\text{ov},1}^2$$

$$V_{\text{ov},1} = \sqrt{\frac{2 \cdot 20 \text{ mA}}{10 \text{ mA/V}^2}} = 2$$

$$V_{\text{ov},1} = V_{\text{gs},1} - V_t$$

$$V_{\text{ov},1} = V_{\text{gs},1} = 2$$

$$V_G = 2 \text{ V}$$

$$I_{\text{ref}} = \frac{1}{2} k_n V_{\text{ov}}^2$$

$$200 \mu\text{A} = \frac{1}{2} \cdot 10 \text{ mA/V}^2 \cdot V_{\text{ov}}^2$$

$$V_{\text{ov}} = \sqrt{\frac{2 \cdot 200 \mu\text{A}}{10 \text{ mA/V}^2}}$$

$$V_{\text{ov}} = 0.2 \text{ V}$$

$$V_{\text{ov}} = V_{\text{gs}} - V_t$$

$$V_{\text{gs}} = 0.2 \text{ V}$$

$$V_{\text{gs}} = V_G - V_S$$

$$V_S = V_G - V_{\text{gs}} = 2 - 0.2$$

$$V_S = 1.8 \text{ V}$$

$$R_S = \frac{1.8}{200 \mu\text{A}} = 9 \text{ k}\Omega$$

$$R_{\text{ref}} = \frac{V_{\text{DD}} - V_G}{I_{\text{ref}}} = \frac{10 - 2}{200 \mu\text{A}} = 40 \text{ k}\Omega$$

R_{REF}	<u>40 kΩ</u>
R_S	<u>9 kΩ</u>

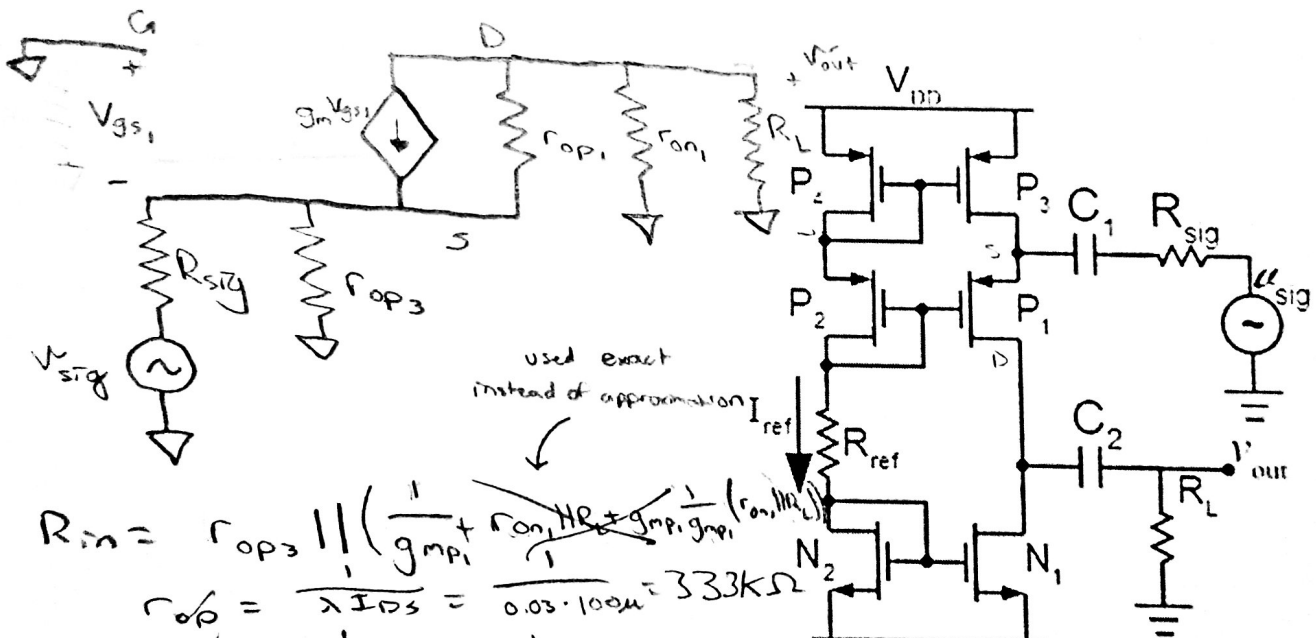
Name: Spencer Goulette

5. (27 points) The common gate amplifier in figure 5 below is from lab project Task 2. The MOSFETs are the ALD1106 NMOS and ALD1107 PMOS FETs, whose relevant parameters are given below. The signal source resistance is $R_{sig} = 1\text{ k}\Omega$ and the load resistance is $R_L = 100\text{ k}\Omega$. The bias current is $I_{ref} = 100\text{ }\mu\text{A}$. The coupling capacitances C_S and C_D are very large. The supply voltages are $\pm 5\text{ V}$.

ALD 1107: $\mu_p C_{ox} W/L = 200\text{ }\mu\text{A}/V^2$, $V_{tp} = -0.75\text{ V}$, $\lambda = 0.03$

ALD 1106: $\mu_n C_{ox} W/L = 500\text{ }\mu\text{A}/V^2$, $V_{tn} = 0.75\text{ V}$, $\lambda = 0.03$

- (a) Draw the small signal equivalent model of the amplifier.
 (b) What are the input resistance and output resistance of the amplifier, including the effects of R_{sig} and R_L ?
 (c) What is the overall voltage gain, G_v , of the amplifier?



b.

$$R_{in} = r_{op3} \parallel \left(\frac{1}{g_{mp1}} + r_{on1} \parallel R_{ref} + \frac{1}{g_{mp1} \cdot g_{mp1}} (r_{on1} \parallel R_L) \right)$$

$$r_{op} = \frac{1}{\lambda I_{DS}} = \frac{1}{0.03 \cdot 100\text{ }\mu\text{A}} = 333\text{ k}\Omega$$

$$r_{on} = \frac{1}{\lambda I_{DS}} = \frac{1}{0.03 \cdot 100\text{ }\mu\text{A}} = 333\text{ k}\Omega$$

$$g_{mp1} = \sqrt{2 k_p I_{DS}} = \sqrt{2 \cdot 200\text{ }\mu\text{A}/V^2 \cdot 100\text{ }\mu\text{A}} = 200\text{ }\mu\text{A}/V$$

$$R_{in} = 333\text{ k}\Omega \parallel \left(\frac{1}{200\text{ }\mu\text{A}/V} + 333\text{ k}\Omega + 333\text{ k}\Omega \parallel 100\text{ k}\Omega \right)$$

$$R_{in} = 108\text{ k}\Omega$$

$$R_{out} = r_{on1} \parallel \left(r_{op1} + (r_{op3} \parallel R_{sig}) + g_{mp1} r_{op1} (r_{op3} \parallel R_{sig}) \right)$$

$$R_{out} = 333\text{ k}\Omega \parallel \left(333\text{ k}\Omega + (333\text{ k}\Omega \parallel 1\text{ k}\Omega) + 200\text{ }\mu\text{A}/V \cdot 333\text{ k}\Omega (333\text{ k}\Omega \parallel 1\text{ k}\Omega) \right)$$

$$R_{out} = 182\text{ k}\Omega$$

c.

$$G_v = \frac{R_{in}}{R_{in} + R_{sig}} \cdot \frac{R_L}{R_{out} + R_L} \cdot g_{mp1} R_{out}$$

$$G_v = \frac{108\text{ k}\Omega}{108\text{ k}\Omega + 1\text{ k}\Omega} \cdot \frac{100\text{ k}\Omega}{182\text{ k}\Omega + 100\text{ k}\Omega} \cdot 200\text{ }\mu\text{A}/V \cdot 182\text{ k}\Omega$$

$$G_v = 12.8\text{ V/V}$$

(b) R_{in}	<u>108 kΩ</u>
R_{out}	<u>182 kΩ</u>
(c) G_v	<u>12.8 V/V</u>

8/8