

# Description of Atmospheric Turbulence

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## Description of Atmospheric Turbulence

For this lecture the following material was used:

- Chapter 6 of Lecture notes *Aircraft Responses to Atmospheric Turbulence* by (Mulder, van der Vaart, & van Staveren).

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## Contents of this lecture

Introduction

Meteorological mechanisms of atmospheric turbulence

Different kinds of turbulence

Mathematical description of atmospheric turbulence

- deterministic vs. stochastic models
- stochastic theory
- assumptions
- elementary fields
- correlation functions
- von Karman Spectra
- Dryden Spectra

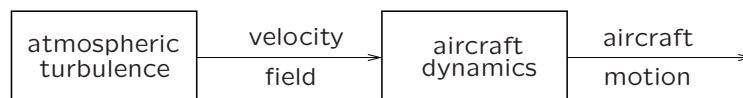
Parameter selection + examples

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## Introduction

Purpose of this course :

**Analysis of aircraft responses (motion) in turbulent air**



Model of aircraft dynamics:

- input: atmospheric turbulence → given as velocity field
- output: aircraft motions

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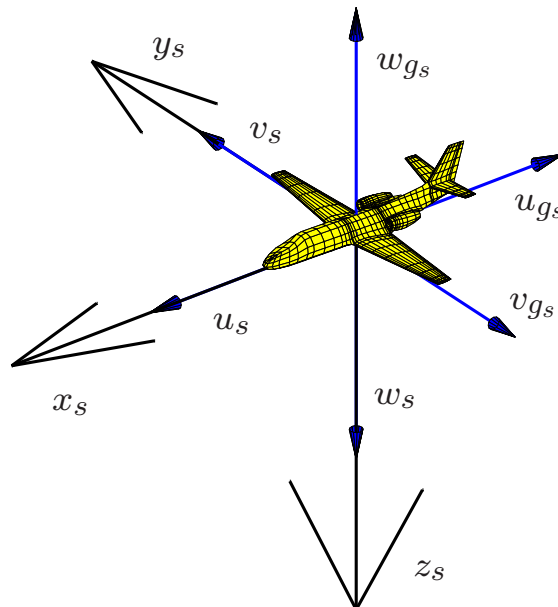
Turbulence **velocity vector** is usually **decomposed** into:  
(*stability reference frame  $F_s$* )

1.  $\bar{u}_g$  : longitudinal gust velocity  
→ *only of importance in ground proximity (+ low-speed)*
2.  $\bar{v}_g$  : side gust velocity  
→ *forces on vertical tail and fuselage, yawing and rolling moments*
3.  $\bar{w}_g$  : vertical gust velocity  
→ *vertical acceleration and pitching moments*

⇒ **fatigue** on structure, **uncomfortable ride** for passengers and pilot

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Stability reference frame  $F_s$  (s: stability, g: gust):  
*!! mind negative directions of gust velocity definitions !!*



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# Meteorological mechanisms: 1. Vertical Stability

Heat convection is one driving force for atmospheric turbulence

**Geometric lapse rate**  $\lambda$  describes the temperature profile of the air (place- & altitude- and weather-dependent).

$$\lambda = \frac{dT}{dh} \Rightarrow T = T_0 + \lambda \Delta h$$

e.g.  $\lambda_{ISA} : -0.0065^\circ/m$

**Process lapse rate**  $\beta$  describes the rate at which the temperature of an air particle decreases during adiabatic ascent (depends on relative air humidity, temperature and pressure).

$$T' = T_0 - \beta \Delta h$$

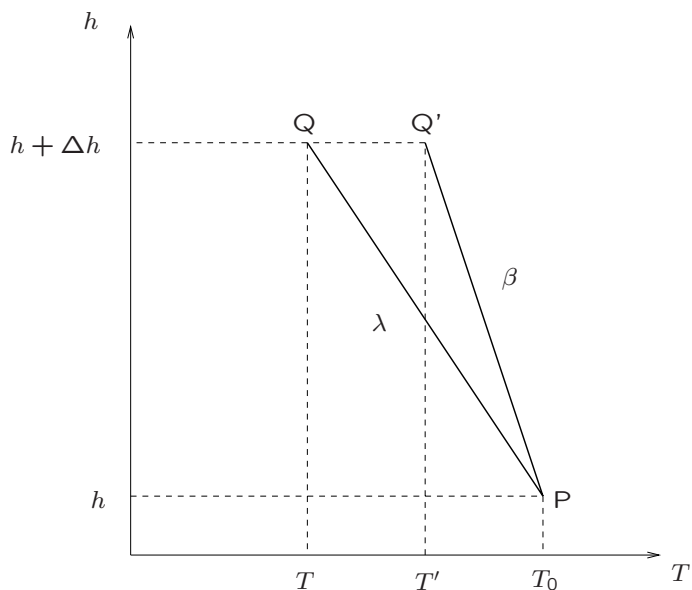
e.g.  $\beta_{dry} = 0.0098^\circ/m$

**Stability:**

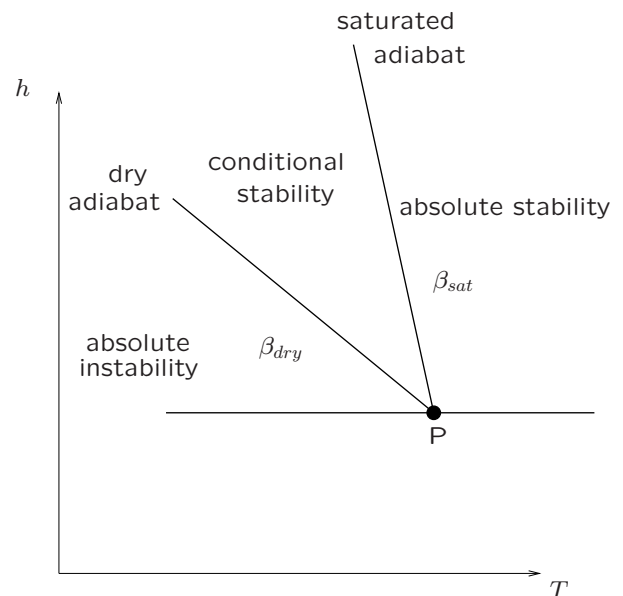
$|\lambda| > \beta$  : unstable situation  
 $|\lambda| < \beta$  : stable situation

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Example vertical instability



Conditions for vertical stability

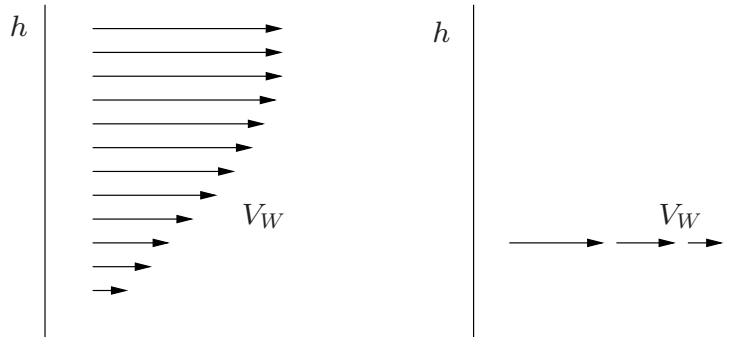


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## Meteorological mechanisms: 2. wind shear

Wind shear causes turbulence due to 'mechanical friction' between layers of air.

Wind shear is primarily induced by local surface roughness.



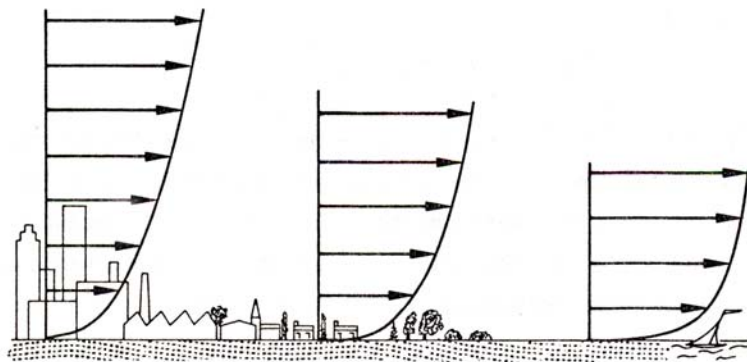
Vertical wind shear

Horizontal wind shear

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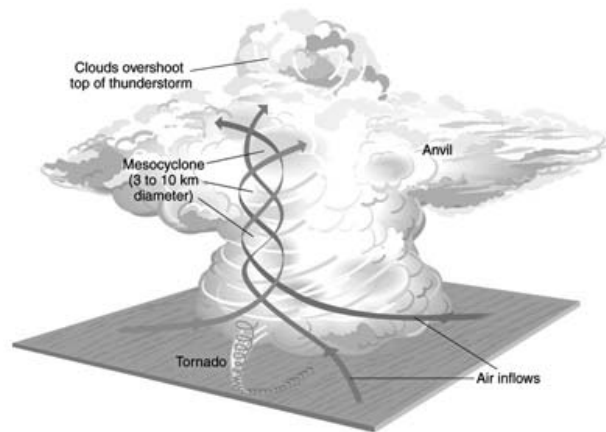
## Different kinds of turbulence

**Turbulence near ground** due to increased wind shear. Wind shear effect is dominant near ground. Vertical stability/heat convection has a larger contribution with increasing altitude.



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**Turbulence in clouds** due to saturated and unstable air in cumulus clouds (sometimes severe turbulence)



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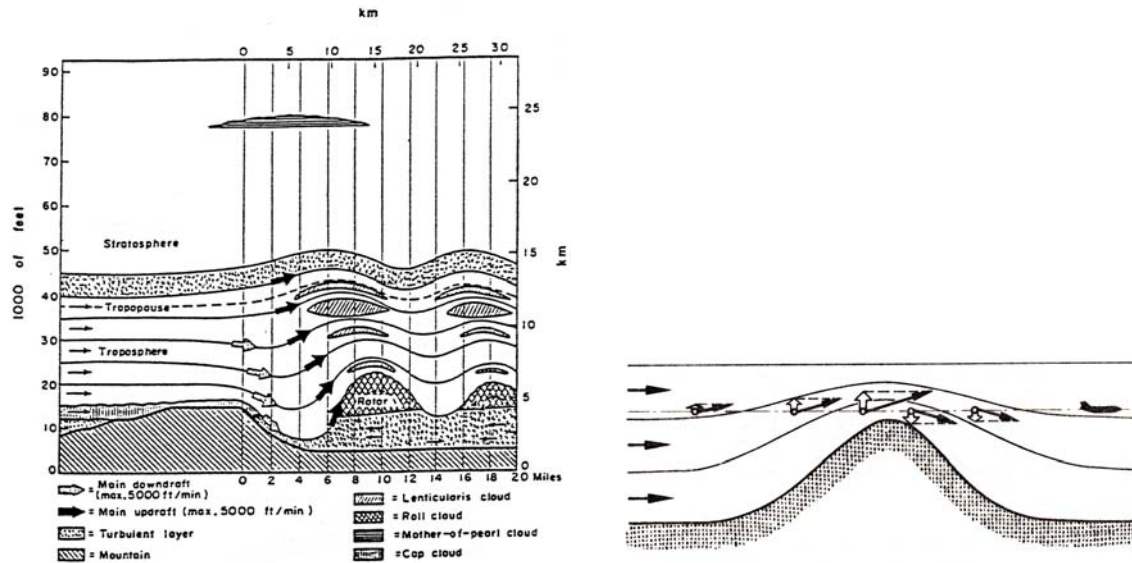
**Clear-air turbulence** can occur at any altitude, and can have any cause: wind shear or convective currents. e.g. in regions of jet streams (light to moderate turbulence)



jet-stream above Canada

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**Mountain wave turbulence** when strong winds cross mountain chain:  
heavy vertical wind shear + severe turbulence in 'rotor' cloud



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### Turbulence intensity

Turbulence is divided into four degrees of intensity.

- **Light** The occupants may be required to use seat belts, but objects in the aircraft remain at rest.
- **Moderate** The occupants require seat belts and are occasionally thrown against the belt. Unsecured objects in the aircraft move about.
- **Severe** The aircraft may be momentarily out of control. Occupants are thrown violently against the belt and back into the seat. Objects not secured in the aircraft are tossed about.
- **Extreme** This is a rarely encountered condition in which the aircraft is violently tossed about and is practically impossible to control. It may cause structural damage.

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## Statistical description: deterministic vs. stochastic models

### Navier-Stokes equations:

- Fundamental physical laws governing air motion.
- *Deterministic* set of coupled partial differential equations
- Very complex and hard to solve (only numerical)

### Field of application:

- Different types of flow: around bicycle, airplane, etc.
- Turbulence in aircraft boundary layer (small scale)
- Atmospheric turbulence (large to very large scale)
- Etc.

→ Differences in **scale**.

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The Navier-Stokes equations are **deterministic**, but:

**the predictability of turbulent flow is limited to very short time intervals, no matter how well the initial conditions are known.**

⇒ atmospheric turbulence is 'random' (*for current application*)

⇒ **stochastic methods** are required.

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**Stochastic variables** enter classical **dynamic equations of motions** through:

$$\begin{aligned} u &= u' + \bar{u} = u' + \bar{u}_g, \\ v &= v' + \bar{v} = v' + \bar{v}_g, \\ w &= w' + \bar{w} = w' + \bar{w}_g, \\ &\text{etc.} \end{aligned} \tag{1}$$

where  $u'$  : mean value  
 $\bar{u}$  : stochastic variation  
 $u_g$  : gust component

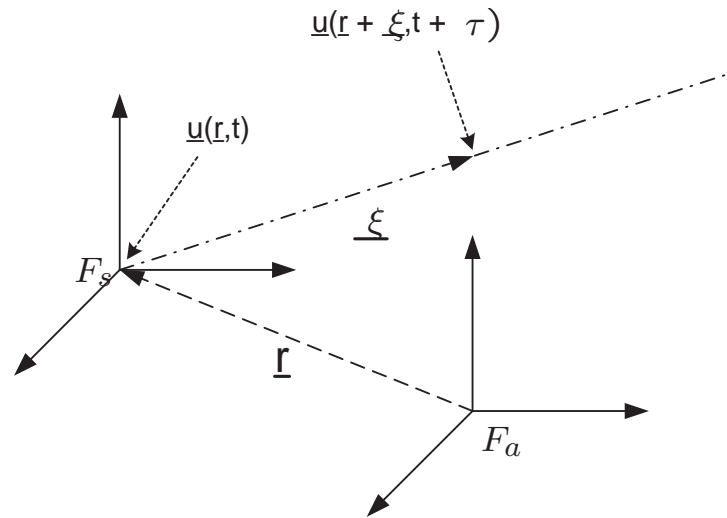
The **mean components** of the gust velocity field :  
 - important for navigation and guidance  
 - does not affect aerodynamics.

Now, interested in statistics of the random gust velocity vector  $\underline{\bar{u}}_g$ .

Choose an arbitrary 'atmosphere fixed frame of reference  $F_a'$ ,  
 relative to which mean motion is zero  $\Rightarrow$  mean gust velocity eliminated

**Definitions**

$t$	absolute time	[s]
$\tau$	time separation	[s]
$\lambda$	wave length	[m]
$\omega$	circular frequency	[rad/s]
$\Omega = \frac{2\pi}{\lambda}$	spatial frequency	[rad/m]
$\underline{\bar{u}} = (\bar{u}_1, \bar{u}_2, \bar{u}_3)^T$	stochastic (gust) wind field	[m/s]
$\underline{r} = (x_1, x_2, x_3)^T$	position vector	[m]
$\underline{\xi} = (\xi_1, \xi_2, \xi_3)^T$	separation distance vector	[m]
$\underline{\Omega} = (\Omega_1, \Omega_2, \Omega_3)^T$	spatial frequency vector	[rad/m]



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### Time domain:

*Stochastic processes* can be characterized by (ref. previous lectures) *correlation functions*:

$$C_{\underline{u}\underline{u}}(\underline{r}, t, \underline{r} + \underline{\xi}, t + \tau) = E\{\underline{u}(\underline{r}, t) \cdot \underline{u}(\underline{r} + \underline{\xi}, t + \tau)\} \quad (2)$$

### Frequency domain:

When these correlation functions are transformed to the frequency domain, *spectral densities* are obtained, with the multi-dimensional Fourier-transform.

$$S_{\underline{u}\underline{u}}(\underline{r}, t, \underline{\Omega}, \omega) = \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} C_{\underline{u}\underline{u}}(\underline{r}, t, \underline{r} + \underline{\xi}, t + \tau) e^{-j(\underline{\Omega} \cdot \underline{\xi} + \omega \tau)} d\xi_1 d\xi_2 d\xi_3 d\tau \quad (3)$$

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Very generally, **atmospheric turbulence** can be described as :

$$\underline{\bar{u}}(\underline{r}, t) = (\bar{u}_1, \bar{u}_2, \bar{u}_3)^T,$$

which is a **velocity field**, being a

*3-dimensional stochastic field, depending on four variables  
(three space dimensions and one time dimension).*

This problem is **too complex** to handle generally

→ **assumptions** have to be made.

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### Statistical description: assumptions

Atmospheric turbulence is ...

1. **a random process** with Gaussian distribution. Not theoretically correct, but true for many practical situations. With this assumption, covariance matrix describes stochastic process completely !
  
2. **stationary + frozen.** Taylor's hypothesis. Speed of air particles through air relatively small compared to speed aircraft.  
Time (t) and time separation ( $\tau$ ) vanishes in covariance matrix:

$$\begin{array}{ll} C_{\bar{u}\bar{u}}(\underline{r}, t; \underline{r} + \underline{\xi}, t + \tau) & \rightarrow C_{\bar{u}\bar{u}}(\underline{r}; \underline{r} + \underline{\xi}) \\ S_{\bar{u}\bar{u}}(\underline{r}, t; \underline{\Omega}, \omega) & \rightarrow S_{\bar{u}\bar{u}}(\underline{r}; \underline{\Omega}) \end{array}$$

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Atmospheric turbulence is ...

3. **homogeneous** along the flight path. For nearly horizontal flight this is a reasonable approximation.

Position ( $\underline{r}$ ) vanishes from covariance matrix:

$$\begin{array}{ccc} C_{\bar{u}\bar{u}}(\underline{r}; \underline{r} + \underline{\xi}) & \rightarrow & C_{\bar{u}\bar{u}}(\underline{\xi}) \\ S_{\bar{u}\bar{u}}(\underline{r}; \underline{\Omega}) & \rightarrow & S_{\bar{u}\bar{u}}(\underline{\Omega}) \end{array}$$

4. **an isotropic process.** All statistical properties are independent of the orientation of the axis. This is true for high-altitude, away from the earth's boundary layer.

$$\sigma_{u_1}^2 = \sigma_{u_2}^2 = \sigma_{u_3}^2 = \sigma^2$$

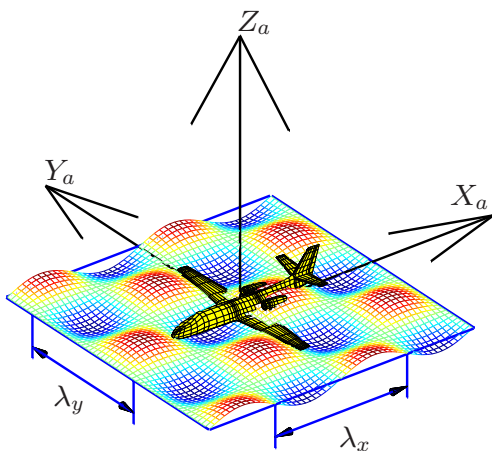
⇒ the simplest model:

**Gaussian, frozen, homogeneous and isotropic turbulence.**

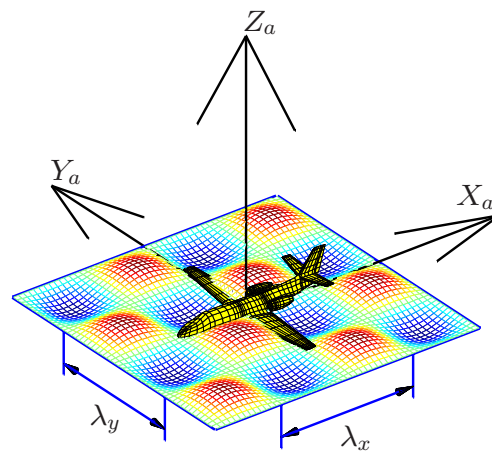
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### Statistical description: elementary field

An elementary turbulence field (1 spatial frequency  $\Omega$ ):



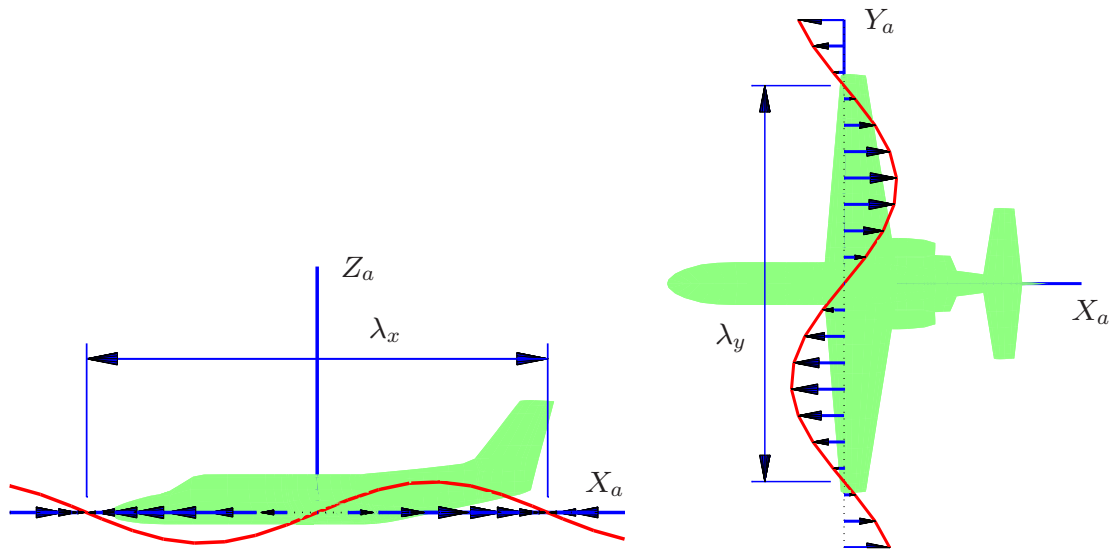
Symmetric field



Asymmetric field

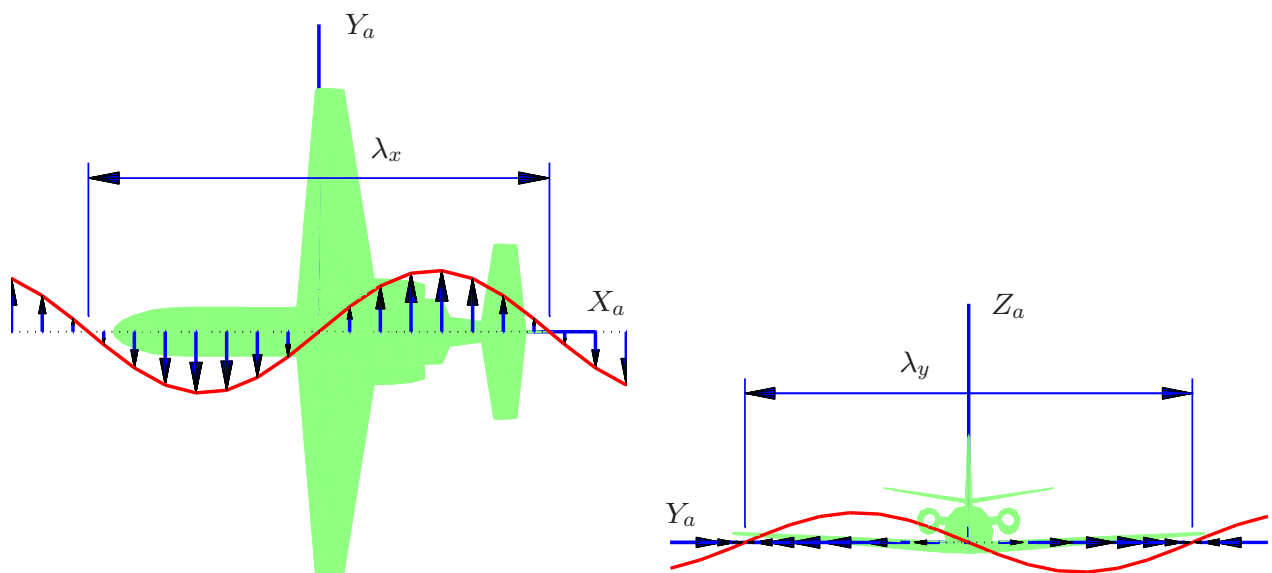
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Longitudinal turbulence  $u_g$ :



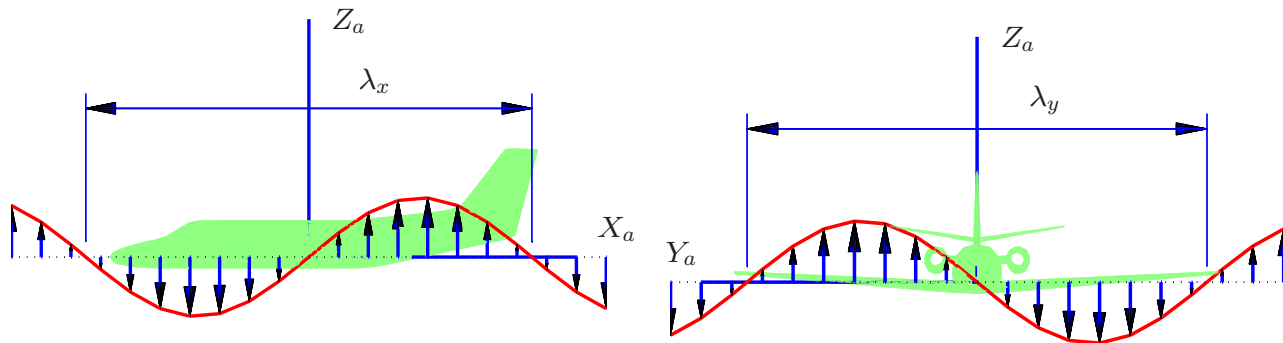
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Lateral turbulence  $v_g$ :



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Vertical turbulence  $w_g$ :

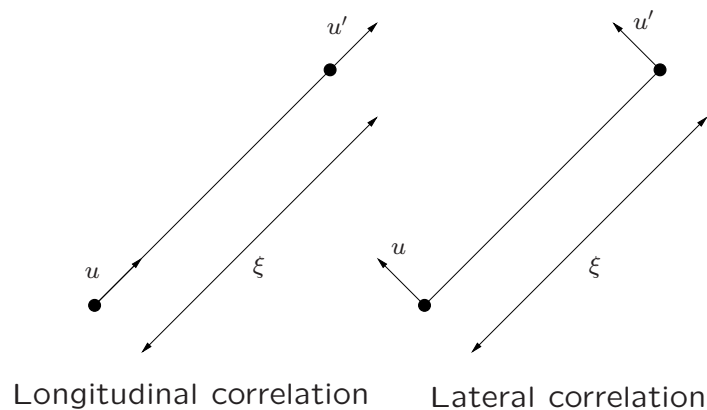


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## Statistical description: correlation functions

Given the assumptions, two fundamental spatial correlation functions can be found, valid for the whole turbulence field:

$f(\xi)$  **longitudinal** parallel to a connecting line between two points  
 $g(\xi)$  **lateral** normal to a connecting line between two points



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Based on these two correlation function, the covariance matrix of atmospheric turbulence can be written as:

$$C_{ij}(\underline{\xi}) = \sigma^2 \left( \frac{f(|\underline{\xi}|) - g(|\underline{\xi}|)}{|\underline{\xi}|^2} \xi_i \xi_j + g(|\underline{\xi}|) \delta_{ij} \right), \quad (4)$$

where  $\delta_{ij}$  is the Kronecker delta (1 if  $i=j$ , 0 if  $i \neq j$ ).

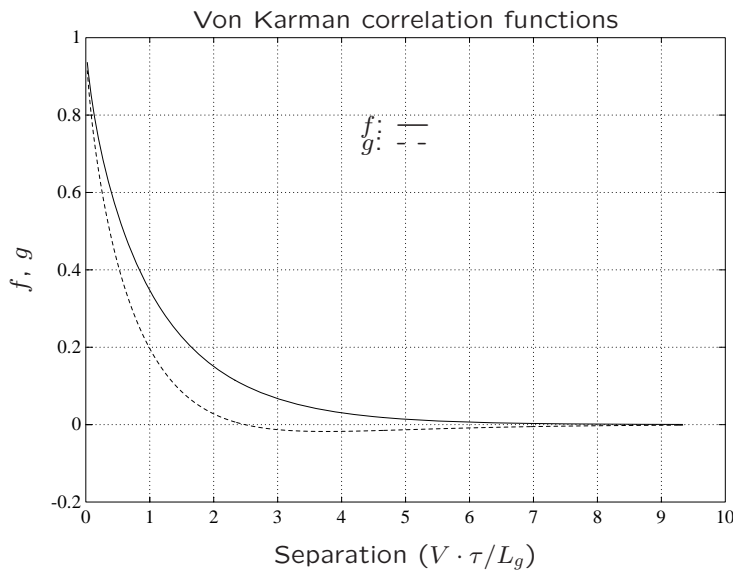
Now, restrict to atmospheric turbulence that varies **along the aircraft's flight path**, so which is encountered in the aircraft's c.g.

⇒ select separation distance vector  $\underline{\xi}$  along flight path  
(in stability reference frame)

$$\underline{\xi} = (\xi_1, \xi_2, \xi_3)^T = (V \cdot \tau, 0, 0)^T \quad (5)$$

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The accompanying correlation functions are found **theoretically** (Von Karman) and have shown to be well-correlated with **wind tunnel experiments**.



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**Turbulence** can be found at **different scales**:

- boundary layer of wing
- wake of an aircraft
- atmosphere

These differences can be quantified by the 'integral scale of turbulence'  $L_g$ :

**Longitudinal scale:**

$$L_g = \int_0^{\infty} f(\xi) d\xi$$

**Lateral scale :**

$$L'_g = \int_0^{\infty} g(\xi) d\xi$$

with  $\xi = \sqrt{\xi_1^2 + \xi_2^2 + \xi_3^2}$

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**Interpretation:**

$L_g$  is a measure of the **spacial extent** of **significant correlation**. It can be interpreted as "*the width of a unit-height rectangle that contains the same area as the correlation function*".

Typical value at high-altitudes:

$$L_g = 300m$$

**Relation:**

Because of the **continuity condition** for incompressible fluids, a direct relation between  $f(\xi)$  and  $g(\xi)$  can be found.

This is also reflected in the relation between  $L_g$  and  $L'_g$ .

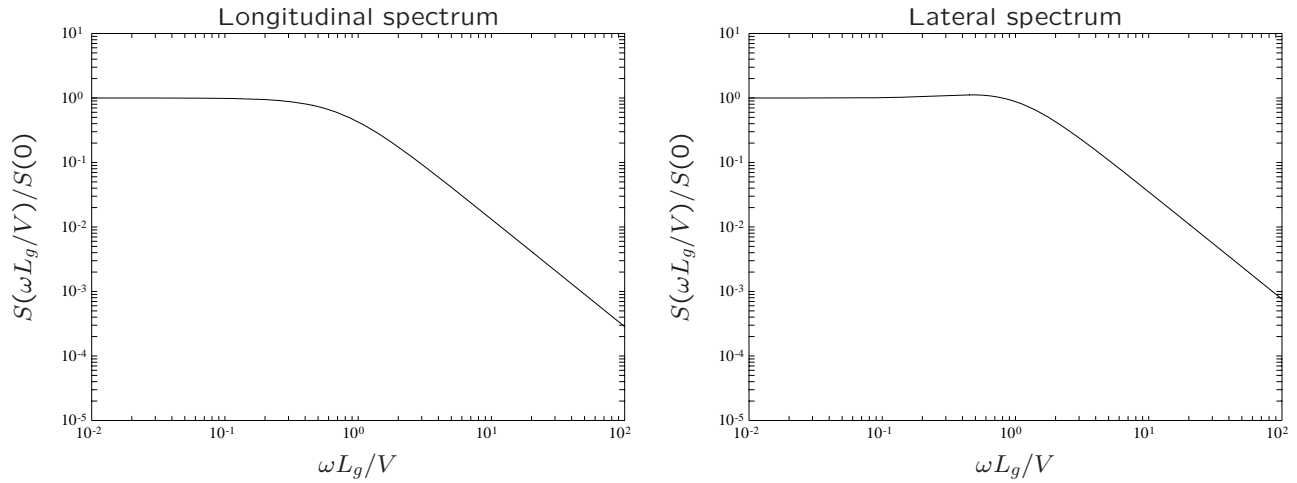
$$L_g = 2L'_g$$

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## Statistical description: von Kármán spectra

The von Kármán functions  $f(\xi)$  and  $g(\xi)$  yield spectra that seem to **best fit the available theoretical and experimental data** on atmospheric turbulence.



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With transformation from spatial  $(\xi, \Omega)$  to time domain  $(\tau, \omega)$ :

$$\xi = V \cdot \tau \quad \text{and} \quad \Omega = \frac{\omega}{V} \quad (\rightarrow \text{from Taylor's hypothesis}),$$

the **analytic functions of von Kármán spectra** for the turbulence velocities  $(\bar{u}_g, \bar{v}_g, \bar{w}_g)^T$  in  $F_s$  are:

$$S_{\bar{u}_g \bar{u}_g}(\omega) = 2\sigma^2 \frac{L_g}{V} \frac{1}{[1 + (1.339 L_g \frac{\omega}{V})^2]^{\frac{5}{6}}} \quad (6)$$

$$S_{\bar{v}_g \bar{v}_g}(\omega) = \sigma^2 \frac{L_g}{V} \frac{1 + \frac{8}{3}(1.339 L_g \frac{\omega}{V})^2}{[1 + (1.339 L_g \frac{\omega}{V})^2]^{\frac{11}{6}}} \quad (7)$$

$$S_{\bar{w}_g \bar{w}_g}(\omega) = \sigma^2 \frac{L_g}{V} \frac{1 + \frac{8}{3}(1.339 L_g \frac{\omega}{V})^2}{[1 + (1.339 L_g \frac{\omega}{V})^2]^{\frac{11}{6}}} \quad (8)$$

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However, these functions are **not rational functions** and are **difficult to use** in computations (non-linear).

**Rational transfer functions** can be transformed to **linear differential equations**.

$$H(s) = \frac{Y(s)}{X(s)} = \frac{k \cdot s + l}{a \cdot s^2 + b \cdot s + c} \quad (9)$$

$$\Rightarrow a \cdot y'' + b \cdot y' + c \cdot y = k \cdot x' + l \cdot x \quad (10)$$

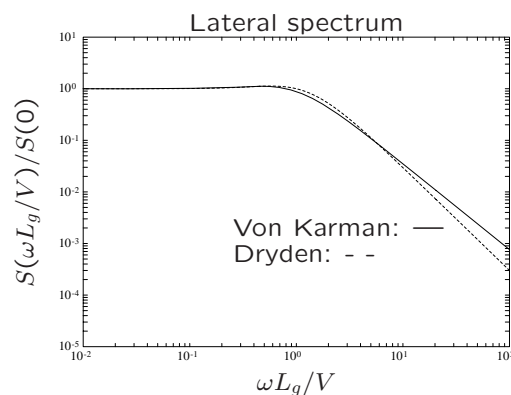
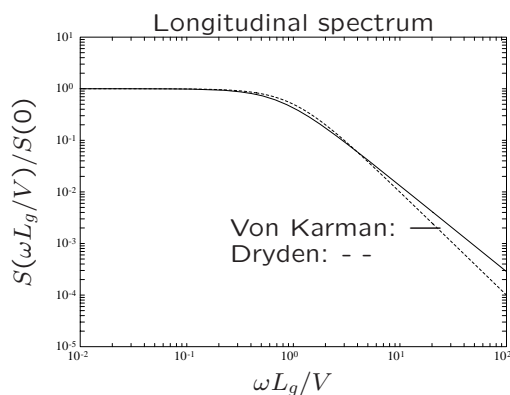
⇒ Solution: **Dryden spectra**.

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### Statistical description: Dryden spectra

Difference between **von Kármán** spectra and **Dryden** spectra:

- low-frequent: same asymptote
- high-frequent: slight difference (Dryden: 2<sup>nd</sup> order)
- yield **much the same results** for aircraft responses



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## Dryden spectral densities (frequency domain):

$$S_{\bar{u}_g \bar{u}_g}(\omega) = 2\sigma^2 \frac{L_g}{V} \frac{1}{1 + (L_g \frac{\omega}{V})^2} \quad (11)$$

$$S_{\bar{v}_g \bar{v}_g}(\omega) = \sigma^2 \frac{L_g}{V} \frac{1 + 3(L_g \frac{\omega}{V})^2}{[1 + (L_g \frac{\omega}{V})^2]^2} \quad (12)$$

$$S_{\bar{w}_g \bar{w}_g}(\omega) = \sigma^2 \frac{L_g}{V} \frac{1 + 3(L_g \frac{\omega}{V})^2}{[1 + (L_g \frac{\omega}{V})^2]^2} \quad (13)$$

Again,

- since stationary turbulence field (Taylor's hypothesis):  $\omega = \Omega \cdot V$
- since isotropic turbulence field: spectra for  $\bar{v}$  and  $\bar{w}$  are identical.

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**GOAL** to model atmospheric turbulence,  
characterized by given Dryden spectra

**HOW?** white noise through a **forming filter**.



With  $\bar{n}$  being white noise:

$$S_{\bar{n}\bar{n}} = 1, \quad (14)$$

$$S_{\bar{y}\bar{y}}(\omega) = |H(\omega)|^2 S_{\bar{n}\bar{n}} \quad (15)$$

$$\Rightarrow |H(\omega)|^2 = S_{\bar{y}\bar{y}}(\omega) \quad (16)$$

where  $S_{\bar{y}\bar{y}}(\omega)$  is known = Dryden spectra

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The variance of the gust velocities is given by  $\sigma^2$ . Perform check:

$$\begin{aligned}
 \sigma_{\bar{u}_g}^2 &= \frac{1}{2\pi} \int_{-\infty}^{+\infty} S_{\bar{u}_g \bar{u}_g}(\omega) d\omega \\
 &= \frac{1}{2\pi} 2\sigma^2 \frac{L_g}{V} \int_{-\infty}^{+\infty} \frac{1}{1 + (L_g \frac{\omega}{V})^2} d\omega \\
 &= \frac{\sigma^2 L_g}{\pi V} [\arctan(L_g \frac{\omega}{V})]_{-\infty}^{+\infty} \\
 &= \frac{\sigma^2}{\pi} [\frac{\pi}{2} + \frac{\pi}{2}] \\
 &= \sigma^2 \\
 &= C_{\bar{u}_g \bar{u}_g}(\tau = 0)
 \end{aligned}$$

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## Transformation: Frequency domain $\rightarrow$ Time domain

Spectral densities  $\xrightarrow{1}$  transfer functions  $\xrightarrow{2}$  differential equations  $\xrightarrow{3}$  state-space

### 1. Spectral densities $\rightarrow$ transfer functions:

$$S_{\bar{u}_g \bar{u}_g}(\omega) = 2\sigma^2 \frac{L_g}{V} \frac{1}{1 + (L_g \frac{\omega}{V})^2} = |H_{\bar{u}_g w_1}(\omega)|^2 \quad (17)$$

$$S_{\bar{v}_g \bar{v}_g}(\omega) = \sigma^2 \frac{L_g}{V} \frac{1 + 3(L_g \frac{\omega}{V})^2}{[1 + (L_g \frac{\omega}{V})^2]^2} = |H_{\bar{v}_g w_2}(\omega)|^2 \quad (18)$$

$$S_{\bar{w}_g \bar{w}_g}(\omega) = \sigma^2 \frac{L_g}{V} \frac{1 + 3(L_g \frac{\omega}{V})^2}{[1 + (L_g \frac{\omega}{V})^2]^2} = |H_{\bar{w}_g w_3}(\omega)|^2 \quad (19)$$

with  $w_1, w_2$  &  $w_3$  being white noise.

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So,

$$H_{\bar{u}_g w_1}(\omega) = \frac{\bar{u}_g(\omega)}{w_1(\omega)} = \sigma \sqrt{\frac{2L_g}{V}} \frac{1}{1 \pm \frac{L_g}{V} j\omega} \quad (20)$$

$$H_{\bar{v}_g w_2}(\omega) = \frac{\bar{v}_g(\omega)}{w_2(\omega)} = \sigma \sqrt{\frac{L_g}{V}} \frac{1 \pm \sqrt{3} \frac{L_g}{V} j\omega}{(1 \pm \frac{L_g}{V} j\omega)^2} \quad (21)$$

$$H_{\bar{w}_g w_3}(\omega) = \frac{\bar{w}_g(\omega)}{w_3(\omega)} = \sigma \sqrt{\frac{L_g}{V}} \frac{1 \pm \sqrt{3} \frac{L_g}{V} j\omega}{(1 \pm \frac{L_g}{V} j\omega)^2} \quad (22)$$

Two solutions are possible (+ and -). Minus signs would lead to unstable filters and are rejected (physical reasons).

2. Transfer functions  $\rightarrow$  differential equations: ( $j\omega = s = \frac{d}{dt}$ )

$$\frac{L_g}{V} \dot{u}_g(t) + u_g(t) = \sigma \sqrt{\frac{2L_g}{V}} w_1(t) \quad (23)$$

$$\frac{L_g^2}{V^2} \ddot{w}_g(t) + 2 \frac{L_g}{V} \dot{w}_g(t) + w_g(t) = \sigma \sqrt{\frac{L_g}{V}} w_3(t) + \sigma \frac{L_g}{V} \sqrt{\frac{3L_g}{V}} \dot{w}_3(t) \quad (24)$$

Second order equation of  $w_g$  (and  $v_g$ )  $\rightarrow$  2 first order equations:

Extra parameter :

$$w_g^*(t) = \dot{w}_g(t) - \sigma \sqrt{\frac{3V}{L_g}} w_3(t) \quad (25)$$

### 3. Dryden in state-space: white noise $\rightarrow$ turbulence velocity field:

$$\dot{u}_g(t) = -\frac{V}{L_g}u_g(t) + \sigma\sqrt{\frac{2V}{L_g}}w_1(t) \quad (26)$$

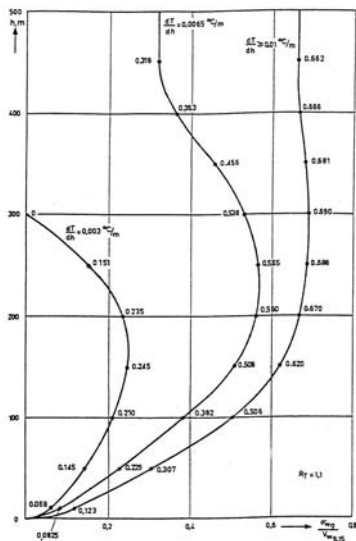
$$\begin{bmatrix} \dot{v}_g(t) \\ \dot{v}_g^*(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{V^2}{L_g^2} & -2\frac{V}{L_g} \end{bmatrix} \begin{bmatrix} v_g(t) \\ v_g^*(t) \end{bmatrix} + \begin{bmatrix} \sigma\sqrt{\frac{3V}{L_g}} \\ (1-2\sqrt{3})\sigma\sqrt{(\frac{V}{L_g})^3} \end{bmatrix} w_2(t) \quad (27)$$

$$\begin{bmatrix} \dot{w}_g(t) \\ \dot{w}_g^*(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{V^2}{L_g^2} & -2\frac{V}{L_g} \end{bmatrix} \begin{bmatrix} w_g(t) \\ w_g^*(t) \end{bmatrix} + \begin{bmatrix} \sigma\sqrt{\frac{3V}{L_g}} \\ (1-2\sqrt{3})\sigma\sqrt{(\frac{V}{L_g})^3} \end{bmatrix} w_3(t) \quad (28)$$

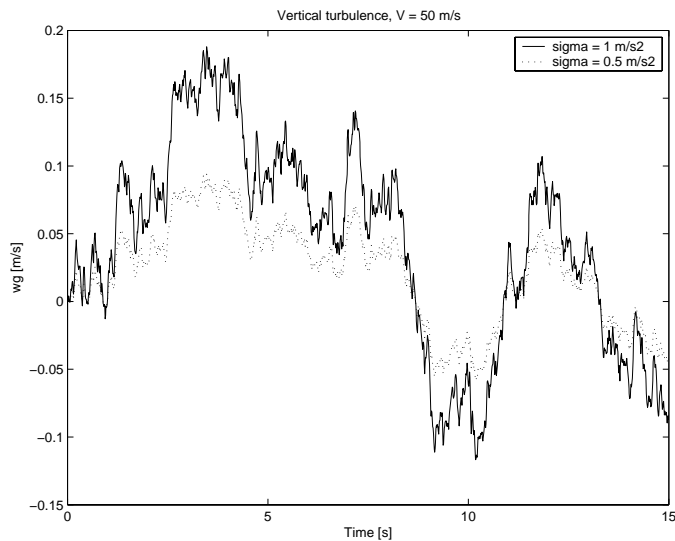
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### Parameter selection $\sigma$ and $L_g$

The quantitative values of  $\sigma$  and  $L_g$  are based on experimental data.



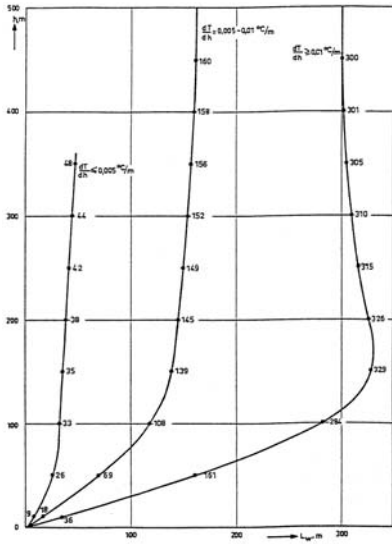
$$\sigma_{w_g} = f(h, \lambda, V_{w9.15})$$



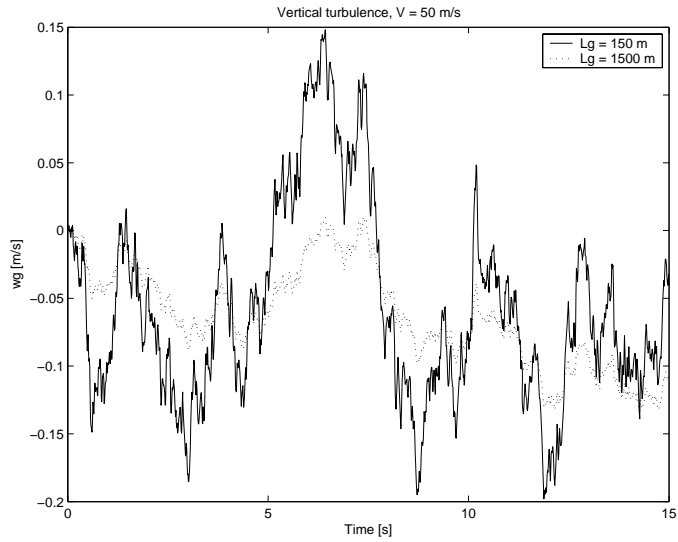
$$\sigma_{w_g} = 1 \text{ m/s}^2 \text{ vs } 0.5 \text{ m/s}^2$$

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Parameter selection  $\sigma$  and  $L_g$



scale  $L_g(h) = f(h, \lambda)$

 $L_g = 150m$  vs  $1500m$ 

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## Turbulence at low altitude

At low altitudes, turbulence can **NO LONGER** be considered:

- **Homogeneous** (position independent) due to varying terrain roughness
- **Isotropic** (orientation independent) since  $w_g$  appears to behave differently from  $u_g$  and  $v_g$  at low altitudes.

However,

- terrain variations around most airports are relatively small
- approach and landing manoeuvres are nearly horizontal flights

⇒ Turbulence can be considered quasi-homogeneous

⇒ Dryden model is still good approximation of encountered turbulence during approach and landing of aircraft

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## Turbulence at low altitude

Remember, for isotropic turbulence  $\sigma_{\bar{u}_g}$ ,  $\sigma_{\bar{v}_g}$  and  $\sigma_{\bar{w}_g}$  are equal.

For turbulence at low altitudes, the followings relations have been found from measured data:

$$\begin{aligned}\frac{\sigma_{\bar{u}_g}}{\sigma_{\bar{w}_g}} &= \frac{\sigma_{\bar{v}_g}}{\sigma_{\bar{w}_g}} = 2.5 & 0 \text{ m} \leq h < 15 \text{ m} \\ \frac{\sigma_{\bar{u}_g}}{\sigma_{\bar{w}_g}} &= \frac{\sigma_{\bar{v}_g}}{\sigma_{\bar{w}_g}} = 1.25 - 0.001 h & 15 \text{ m} \leq h < 250 \text{ m} \\ \frac{\sigma_{\bar{u}_g}}{\sigma_{\bar{w}_g}} &= \frac{\sigma_{\bar{v}_g}}{\sigma_{\bar{w}_g}} = 1 & h > 250 \text{ m}\end{aligned} \quad (29)$$

⇒ A complete turbulence model (Dryden) applicable at high altitude and during approach and landing.