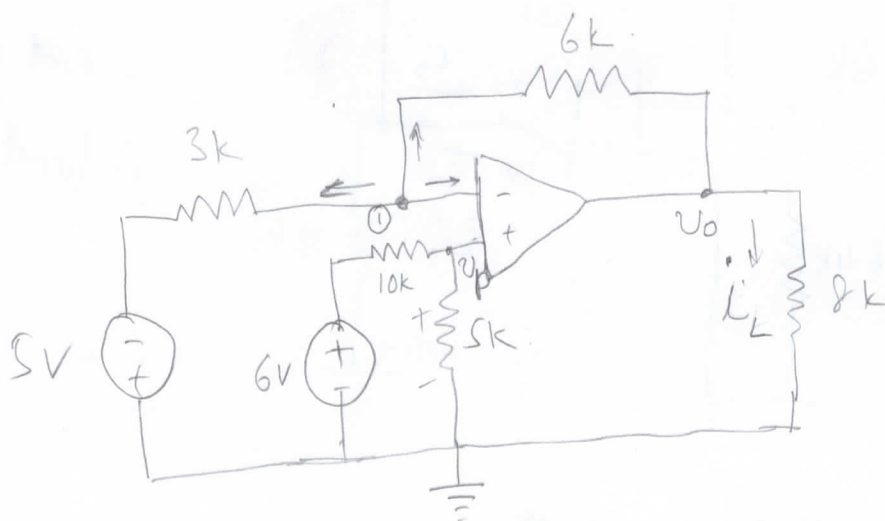


Op Amps

Pr 5.6

Find i_L .



We first need to find v_o , the output voltage.

Since the op amp is ideal:

$$v_p = v_n; i_p = i_n = 0$$

Also, $v_n = v_p = \left(\frac{5k}{5k + 10k} \right) 6 = 2 \text{ volts}$ (not zero!)

Writing KCL at node 1:

$$\frac{v_n + 5}{3k} + \frac{v_n - v_o}{6k} + i_n = 0$$

$$\text{or } \frac{v_n - v_o}{6k} + \frac{v_n + 5}{3k} = 0, \text{ since } i_n = 0$$

$$\text{i.e. } \frac{2 - v_o}{6} + \frac{7}{3} = 0$$

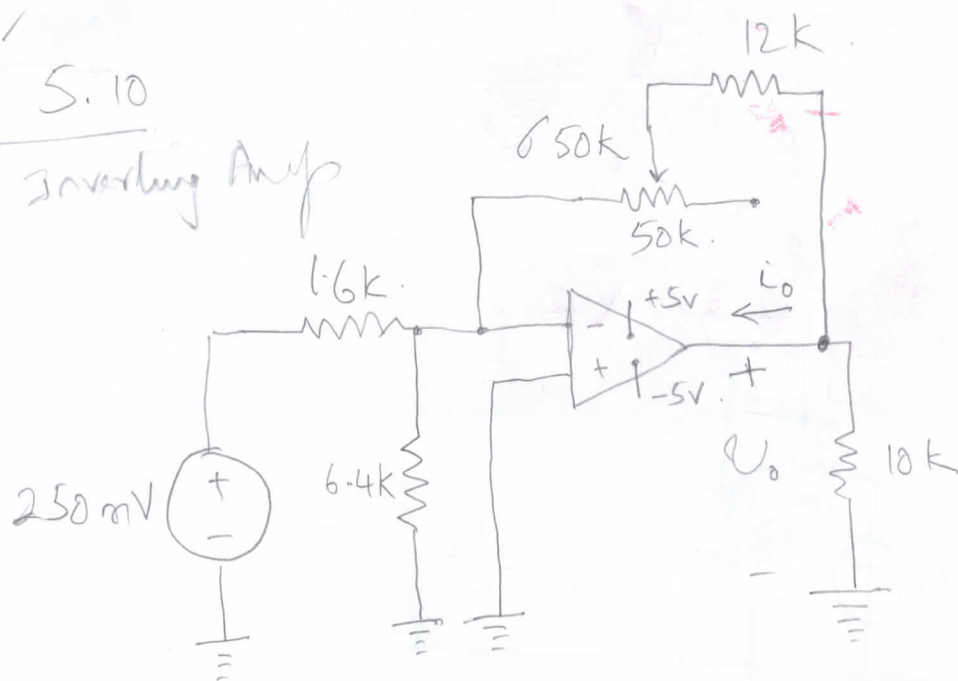
$$2 - v_o + 14 = 0$$

$$v_o = 16V$$

$$\text{Hence, } i_L = \frac{v_o}{R} = \frac{16}{8k} = 2 \text{ mAmps}$$

Pr 5.10
Inverting Amp

Page 2



- a) find σ so no saturation
b) find i_o at $\sigma = 0.272$

Let us solve part b) first

b) Find V_o & i_o when $\sigma = 0.272$.

When $\sigma = 0.272$, the feedback resistance

value is $12k + (0.272 * 50k) = 25.6k \Omega$.

$$\text{Hence, } V_o = -\frac{R_f}{R_i} * V_s$$

$$= -\left(\frac{25.6}{1.6k \parallel 6.4k}\right) * \left(\frac{6.4k * 250mV}{1.6k + 6.4k}\right)$$

$$= \frac{-15.6k}{1.28k} * 0.2V$$

$$= -4 \text{ volts}$$

To find i_o :

write KCL at the output node:

$$\frac{V_o}{10k} + \frac{V_o}{25.6k} + i_o = 0 \quad i_o = -\left(\frac{-4}{10k}\right) - \left(\frac{-4}{25.6k}\right)$$

$$= 0.556 \text{ mA}$$

a) Now, let us solve for σ such that the op amp does NOT saturate.

i.e. $-5V \leq V_o \leq +5V$

Since V_s is fixed at $+250mV$, and the output V_o is inverted, we only have to check for saturation at the $-5V$ limit (negative).

At neg saturation;

$$V_o = -5 = -\frac{R_f}{R_s} V_{in} \quad \left(\begin{array}{l} \text{Define} \\ R_\sigma = \sigma * 50k \end{array} \right)$$

$$= -\frac{12k + R_\sigma}{1.6k \parallel 6.4k} * \left(\frac{6.4k}{1.6k + 6.4k} * 250mV \right)$$

$$= -\frac{12k + R_\sigma}{1.28k} * 0.2$$

$$\text{So, } -5 = -1.875 - 0.15625 \times 10^{-3} R_\sigma$$

$$\begin{aligned} \text{Hence, } R_\sigma &= \frac{-3.125}{-0.15625 \times 10^{-3}} \\ &= 20k\Omega \end{aligned}$$

$$\text{i.e. } \sigma * 50k = 20k\Omega$$

$$\text{and so } \sigma = 0.4$$

So the op amp will not-saturate for $0 \leq \sigma \leq 0.40$
 i.e. the feedback resistance $12k \leq R_f \leq 32k$

Pr 5.12 Summing Amp

a) The circuit is an inverting summing amplifier.

$$b). v_o = -\frac{220}{33}v_a - \frac{220}{22}v_b - \frac{220}{80}v_c$$

$$= -\frac{220}{33} \times 1.2 - \frac{220}{22} \times -1.5 - \frac{220}{80} \times 4$$

$$= -8 + 15 - 11$$

$$= -4 \text{ V}$$

c) If v_b is unknown.

$$v_o = -8 - 10v_b - 11$$

$$\text{or } v_o = -19 - 10v_b$$

At saturation, $v_o = \pm V_{cc} = \pm 6$

$$\text{when } v_o = -6, v_b = \frac{-6 + 19}{-10} = -1.3 \text{ V}$$

$$v_o = +6, v_b = \frac{6 + 19}{-10} = -2.5 \text{ V}$$

So, the range for v_b is $\underline{-2.5 \text{ V} \leq v_b \leq -1.3 \text{ V}}$

Given $V_o = -(8V_a + 4V_b + 10V_c + 6V_d)$.

So $\frac{R_f}{R_a} = 8$, and so on from the Summing Amp equation.

Step 1

To pick a convenient R_f and get whole numbers R_a, R_b, R_c, R_d values, find the value of R_f that the other coefficients are all a factor of (or the LCM).

Such a value is 120

So, pick $R_f = 120 \text{ k}$.

Step 2

then $R_a = \frac{R_f}{8} = \frac{120 \text{ k}}{8} = 15 \text{ k}\Omega$.

$$R_b = \frac{R_f}{4} = \frac{120 \text{ k}}{4} = 30 \text{ k}\Omega$$

$$R_c = \frac{R_f}{10} = \frac{120 \text{ k}}{10} = 12 \text{ k}\Omega$$

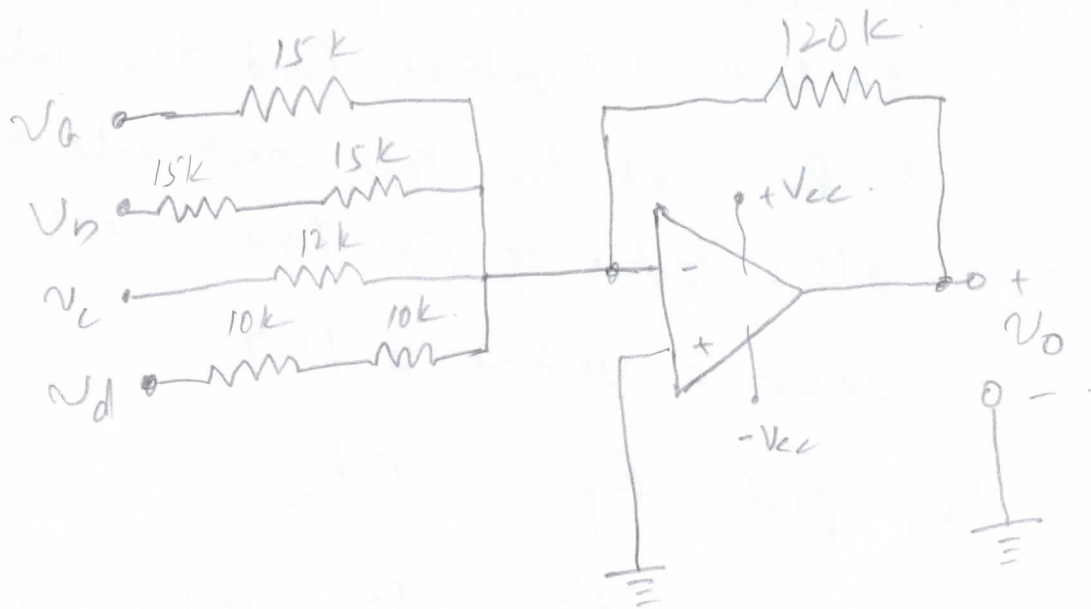
$$R_d = \frac{R_f}{6} = \frac{120 \text{ k}}{6} = 20 \text{ k}\Omega$$

Step 3

Next, compare these values to the standard resistor values.
Only $R_b (30 \text{ k})$ & $R_d (20 \text{ k})$ are not standard

step 4. $R_b = 30k = 15k + 15k$ (Two 15k in series)
 $R_d = 20k = 10k + 10k$.

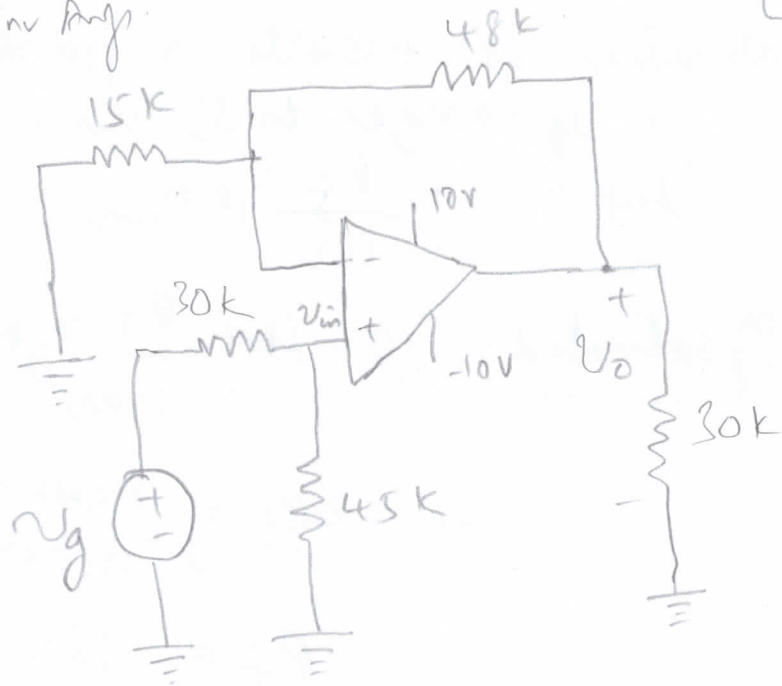
Final circuit:



Pr 5.20

Non-Inv Amp.

Page 7



a). Standard Non-Inv amplifier equation is:

$$V_o = \left(1 + \frac{R_f}{R_s}\right) V_{in}$$

where V_{in} is signal voltage at the +ve terminal.

In the circuit, $R_f = 48k$, $R_s = 15k$, $V_g = 3V$.

$$\begin{aligned} V_{out} &= \left(1 + \frac{48k}{15k}\right) * \underbrace{\frac{45k \times 3V}{45k + 30k}}_{V_{in}} \\ &= (1 + 3.2) * 1.8V \\ &= 7.56 \text{ volts} \end{aligned}$$

b). $(\text{Gain})_{is} \frac{V_{out}}{V_g} = \frac{7.56}{3} = 2.52$ $V_g = \frac{V_{out}}{2.52}$

V_{out} is bound by $-10 \leq V_o \leq +10$

So V_g is $\underline{-3.97 \leq V_g \leq +3.97}$

c). Saturation at +10V is possible.

If V_g changes to 5, $V_{in} = \frac{45 \times 5}{45 + 30}$ or 3 volts

$$V_{out} = \left(1 + \frac{R_f}{15k}\right) \times V_{in}$$

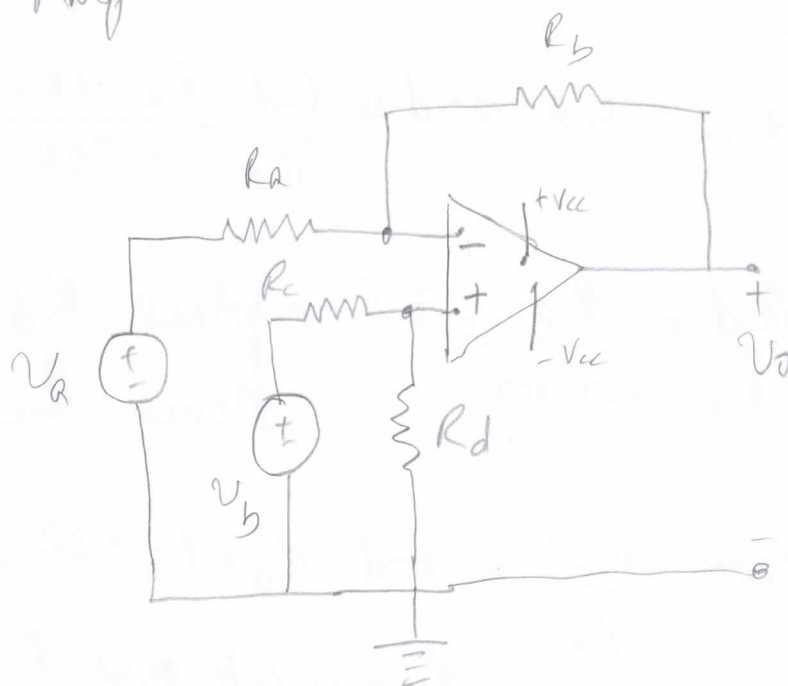
If saturated; $10 = \left(1 + \frac{R_f}{15000}\right) \times 3$

$$\text{So } 3R_f = 150,000 - 45,000$$

$$= 105,000$$

$$R_f = \underline{35k \text{ ohms.}}$$

So an $R_f \geq 35k$ will cause saturation



$$V_o = 3V_b - 4V_a \rightarrow (1)$$

the difference-amplifier eq is:

$$V_o = \frac{R_d(R_a + R_b)}{R_a(R_c + R_d)} V_b - \frac{R_b V_b}{R_a}$$

Also, given that:

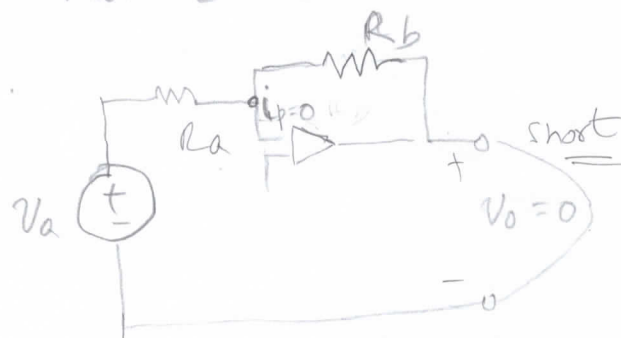
R_{in} for source V_b is $470k$

i.e. $R_c + R_d = 470k$; (Since $i_p = i_n = 0$ for an ideal opamp)

R_{in} for source V_a is $22k$ when V_o is 0

i.e. $R_a + R_b = 22k$

(See figure)



Comparing (1) to the Difference Amp eq;

[10]

$$\frac{R_b}{R_a} = 4, \quad R_b = 4R_a, \text{ and so } \frac{R_d}{R_a} \frac{(R_a + 4R_a)}{470k} = 3.$$

$$\Rightarrow \frac{R_d}{R_a} * \frac{5R_a}{470,000} = 3; \text{ implies } R_d = 282k\Omega \\ \text{Hence } R_c = 188k\Omega //$$

Also: from $\frac{R_b}{R_a} = 4$ and $R_a + R_b = 22$, we get

$$R_a = 4.4k\Omega \text{ and } R_b = 17.6k\Omega$$

from Appendix N:

$$R_d = 282k, \text{ Use } 270k.$$

$$R_c = 188k, \text{ Use } 180k.$$

$$R_b = 17.6k, \text{ Use } 12k + 5.6k$$

$$R_a = 4.4k, \text{ Use } 2.2k + 2.2k.$$