

Key solution steps for Mid-term report

Before you read this document, please note that:

(1) Only key steps are provided (for a better understanding of the solution method).

(2) For the standard solution process, please refer to examples in the lecture handout.

Q1:

$$F = 1 \times 10^5 \text{ N}, \sigma_a = \frac{F}{A} = \frac{1 \times 10^5}{0.2 \times 0.03} = 16.67 \text{ MPa (compression)}$$

$$M = F \cdot (x - 100) = 1.5 \times 10^4 \text{ N} \cdot \text{m}, \sigma_m = \frac{M}{I} \cdot y_{\max} = \frac{1.5 \times 10^4}{(0.03 \times 0.2^3)/12} \times \frac{0.2}{2} = 75 \text{ MPa}$$

$$\sigma_{n,\max} = -\sigma_a + \sigma_m = -16.67 + 75 = 58.33 \text{ MPa}$$

$$\sigma_{n,\min} = -\sigma_a - \sigma_m = -16.67 - 75 = -91.67 \text{ MPa}$$

Q2:

$$(a) A_{EF} = \frac{\pi}{4} (0.015^2) = 56.25(10^{-6}) \pi \text{ m}^2$$

$$A_{AB} = \frac{\pi}{4} (0.01^2) = 25(10^{-6}) \pi \text{ m}^2$$

$$\begin{aligned} \delta_F &= \sum \frac{PL}{AE} = \frac{P_{EF} L_{EF}}{A_{EF} E_{st}} + \frac{P_{AB} L_{AB}}{A_{AB} E_{br}} \\ &= \frac{20(10^3)(450)}{56.25(10^{-6})\pi(193)(10^9)} + \frac{5(10^3)(300)}{25(10^{-6})\pi(101)(10^9)} \\ &= 0.453 \text{ mm} \end{aligned}$$

$$(b) \delta_F = \sum \frac{PL}{AE} = \frac{P_{EF} L_{EF}}{A_{EF} E_{st}} + \frac{P_{AB} L_{AB}}{A_{AB} E_{br}}$$

$$0.45 = \frac{4P(450)}{56.25(10^{-6})\pi(193)(10^9)} + \frac{P(300)}{25(10^{-6})\pi(101)(10^9)}$$

$$P = 4967 \text{ N} = 4.97 \text{ kN}$$

Q3:

$$J_{AB} = \frac{\pi}{2} (0.0225^4 - 0.0175^4) = 2.553 \times 10^{-7} \text{ m}^4$$

$$J_{BD} = \frac{\pi}{2} \times 0.0125^4 = 3.835 \times 10^{-8} \text{ m}^4$$

$$\begin{aligned} \phi_D &= \sum \frac{T_i L_i}{J_i G_i} = \frac{T_{AB} L_{AB}}{J_{AB} G_{st}} + \frac{T_{BD} L_{BD}}{J_{BD} G_{st}} = \frac{90 \times 0.4}{2.553 \times 10^{-7} \times 77 \times 10^9} + \frac{-60 \times 0.4}{3.835 \times 10^{-8} \times 77 \times 10^9} \\ &= -6.296 \times 10^{-3} \text{ rad} = -6.296 \times 10^{-3} \times \frac{180}{\pi} = -0.36^\circ \end{aligned}$$

Q4:

$$(a) \uparrow \sum F_y = 0 \Rightarrow R_A - 2P + R_D = 0$$

$$\delta_{AB} = \frac{R_A L}{EA_1}, \quad \delta_{BC} = \frac{PL}{EA} = \frac{(R_A - P)L}{EA_2}, \quad \delta_{CD} = \frac{PL}{EA} = \frac{(R_A - 2P)L}{EA_2}$$

$$\delta_{AB} + \delta_{BC} + \delta_{CD} = 0 \Rightarrow \frac{R_A L}{EA_1} + \frac{(R_A - P)L}{EA_2} + \frac{(R_A - 2P)L}{EA_2} = 0 \Rightarrow R_A = \frac{3PA_1}{A_2 + 2A_1}$$

$$R_D = 2P - R_A = 2P - \frac{3PA_1}{A_2 + 2A_1} = \frac{2PA_2 + PA_1}{A_2 + 2A_1}$$

$$(b) \delta_B = \delta_{AB} = \frac{3PL}{EA_2 + 2EA_1}$$

Q5:

$$\Sigma F_y = 0; F_{AD} + F_{BE} + F_{CF} - 50(10^3) - 80(10^3) = 0$$

$$\Sigma M_D = 0; F_{BE}(2) + F_{CF}(4) - 50(10^3)(1) - 80(10^3)(3) = 0$$

$$\delta_{BE} = \delta_{AD} + \left(\frac{\delta_{CF} - \delta_{AD}}{4} \right) (2)$$

$$\delta_{BE} = \frac{1}{2} (\delta_{AD} + \delta_{CF})$$

$$\frac{F_{BE} L}{AE} = \frac{1}{2} \left(\frac{F_{AD} L}{AE} + \frac{F_{CF} L}{AE} \right)$$

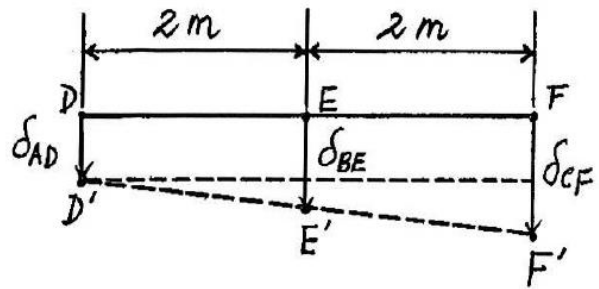
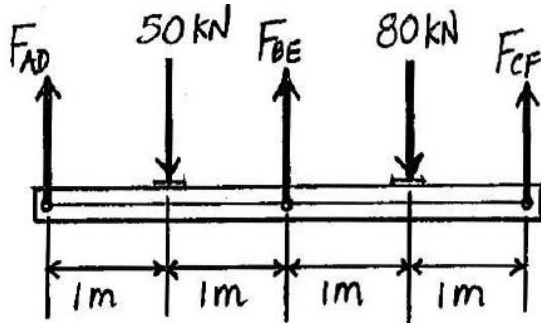
$$F_{AD} + F_{CF} = 2F_{BE}$$

$$F_{BE} = 43.33(10^3) \text{ N}, \quad F_{AD} = 35.83(10^3) \text{ N}, \quad F_{CF} = 50.83(10^3) \text{ N}$$

$$\sigma_{BE} = \frac{F_{BE}}{A} = \frac{43.33(10^3)}{0.45(10^{-3})} = 96.3 \text{ MPa}$$

$$\sigma_{AD} = \frac{F_{AD}}{A} = \frac{35.83(10^3)}{0.45(10^{-3})} = 79.6 \text{ MPa}$$

$$\sigma_{CF} = 113 \text{ MPa}$$



Q6:

$$\Sigma M_x = 0; T_{mg} + T_{st} - T = 0$$

$$(\phi_{st})_A = (\phi_{mg})_A:$$

$$\frac{T_{st}L}{\frac{\pi}{2}(0.02^4)(75)(10^9)} = \frac{T_{mg}L}{\frac{\pi}{2}(0.04^4 - 0.02^4)(18)(10^9)}$$

$$T_{st} = 0.2778 T_{mg}$$

$$T_{mg} = 0.7826 T, \quad T_{st} = 0.2174 T$$

$$(\tau_{allow})_{mg} = \frac{T_{mg}c}{J}; 45(10^6) = \frac{0.7826 T(0.04)}{\frac{\pi}{2}(0.04^4 - 0.02^4)}$$

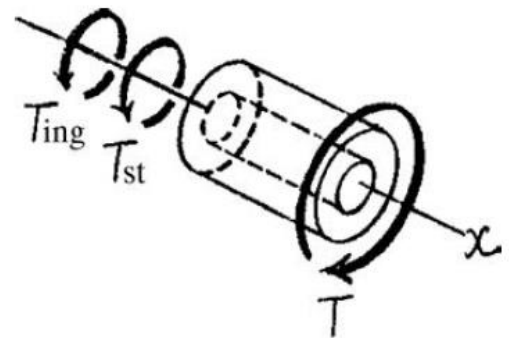
$$T = 5419.25 \text{ N} \cdot \text{m}$$

$$(\tau_{allow})_{st} = \frac{T_{st}c}{J}; 75(10^6) = \frac{0.2174 T(0.02)}{\frac{\pi}{2}(0.02^4)}$$

$$T = 4335.40 \text{ N} \cdot \text{m} = 4.34 \text{ kN} \cdot \text{m} \text{ (control!)}$$

$$T_{st} = 942.48 \text{ N} \cdot \text{m}$$

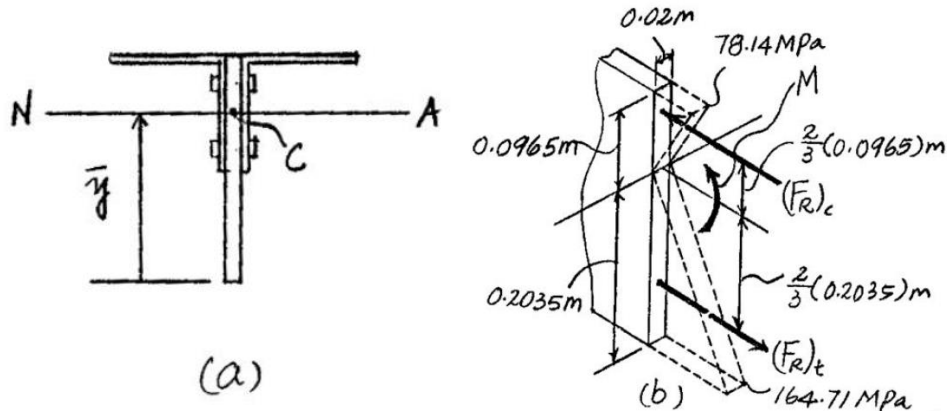
$$\phi_A = \frac{T_{st}L}{J_{st}G_{st}} = \frac{942.48(0.9)}{\frac{\pi}{2}(0.02^4)(75)(10^9)} = 0.045 \text{ rad} = 2.58^\circ$$



Q7:

Section Properties: The neutral axis passes through centroid C of the cross section as shown in Fig. *a*. The location of C is

$$\bar{y} = \frac{\sum \tilde{y}A}{\sum A} = \frac{0.15(0.3)(0.02) + 2[0.225(0.15)(0.01)] + 2[0.295(0.01)(0.14)]}{0.3(0.02) + 2(0.15)(0.01) + 2(0.01)(0.14)} = 0.2035\text{m}$$



Thus, the moment of inertia of the cross section about the neutral axis is

$$\begin{aligned} I &= \bar{I} + Ad^2 \\ &= \frac{1}{12}(0.02)(0.3^3) + 0.02(0.3)(0.2035 - 0.15)^2 \\ &\quad + 2\left[\frac{1}{12}(0.01)(0.15^3) + 0.01(0.15)(0.225 - 0.2035)^2\right] \\ &\quad + 2\left[\frac{1}{12}(0.14)(0.01^3) + 0.14(0.01)(0.295 - 0.2035)^2\right] \\ &= 92.6509(10^{-6})\text{m}^4 \end{aligned}$$

Bending Stress: The distance from the neutral axis to the top and bottom of plate A is $y_t = 0.3 - 0.2035 = 0.0965\text{m}$ and $y_b = 0.2035\text{m}$.

$$\begin{aligned} \sigma_t &= \frac{My_t}{I} = \frac{75(10^3)(0.0965)}{92.6509(10^{-6})} = 78.14\text{MPa(C)} \\ \sigma_b &= \frac{My_b}{I} = \frac{75(10^3)(0.2035)}{92.6509(10^{-6})} = 164.71\text{MPa(T)} \end{aligned}$$

The bending stress distribution across the cross section of plate A is shown in Fig. *b*. The resultant forces of the tensile and compressive triangular stress blocks are

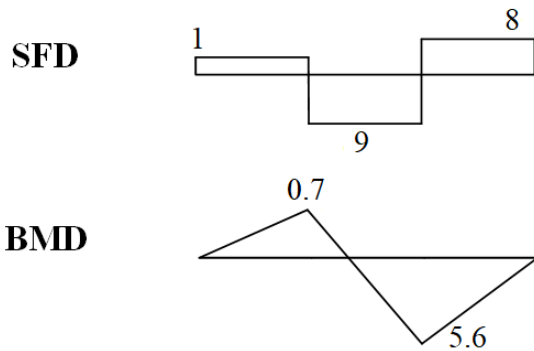
$$\begin{aligned} (F_R)_t &= \frac{1}{2}(164.71)(10^6)(0.2035)(0.02) = 335144.46\text{N} \\ (F_R)_c &= \frac{1}{2}(78.14)(10^6)(0.0965)(0.02) = 75421.50\text{N} \end{aligned}$$

Thus, the amount of internal moment resisted by plate A is

$$M = 335144.46 \left[\frac{2}{3} (0.2035) \right] + 75421.50 \left[\frac{2}{3} (0.0965) \right]$$

$$= 50315.65 \text{ N} \cdot \text{m} = 50.3 \text{ kN} \cdot \text{m}$$

Q8:

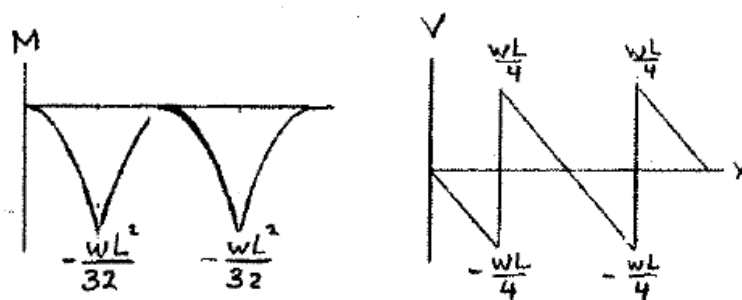


$$\tau_{max} = \frac{3V}{2A} = 1.5 \times \frac{9 \times 10^3}{0.02 \times 0.08} = 8.44 \text{ MPa}$$

$$\sigma_{max} = \frac{My}{I} = \frac{5.6 \times 10^3 \times 0.04}{\frac{0.02 \times 0.08^3}{12}} = 262.5 \text{ MPa}$$

Q9:

(a)



$$R_A = R_B = \frac{wL}{2}$$

$$|V|_{max} = \frac{wL}{4}, \tau_{max} = \frac{3}{2} \frac{|V|_{max}}{A} = \frac{3wL}{8bh}$$

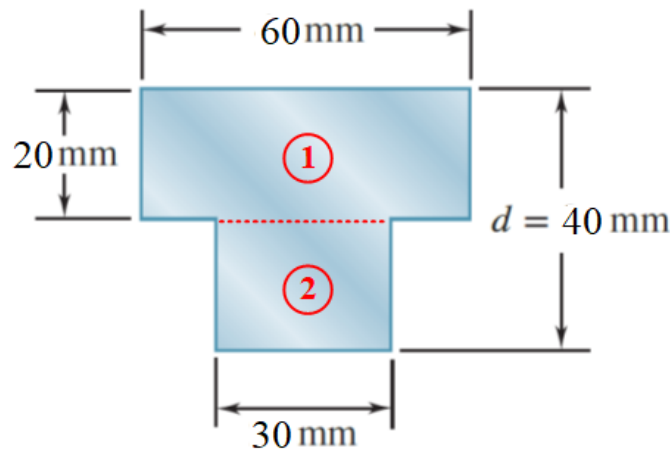
$$|M|_{max} = \frac{wL^2}{32}, S = \frac{bh^2}{6}, \sigma_{max} = \frac{|M|_{max}}{S} = \frac{3wL^2}{16bh^2}$$

$$\frac{\tau_{\max}}{\sigma_{\max}} = \left(\frac{3}{2} \frac{|V|_{\max}}{A} \right) \bigg/ \left(\frac{3wL^2}{16bh^2} \right) = \frac{2h}{L}$$

$$(b) \quad h = \frac{L}{2} \frac{\tau_{\max}}{\sigma_{\max}} = \frac{4}{2} \times \frac{1.28}{9.8} = 0.261 \text{ m}$$

$$b = \frac{3wL}{8\tau_{\max}} = \frac{3}{8} \times \frac{10 \times 10^3 \times 4}{0.261 \times 1.28 \times 10^6} = 0.0449 \text{ m}$$

Q10:



	Area, mm ²	y, mm	yA, mm ³
1	1200	30	36000
2	600	10	6000
Σ	1800		42000

$$\bar{y}_c = \frac{42000}{1800} = 23.3 \text{ mm}$$

$$y_{top} = 40 - \bar{y}_c = 40 - 23.3 = 16.7 \text{ mm}$$

$$y_{bot} = -\bar{y}_c = -23.3 \text{ mm}$$

$$I_1 = \frac{b_1 h_1^3}{12} + A_1 d^2 = \frac{60 \times 20^3}{12} + 1200 \times 6.7^2 = 93868 \text{ mm}^4$$

$$I_2 = \frac{b_2 h_2^3}{12} + A_2 d^2 = \frac{30 \times 20^3}{12} + 600 \times 13.3^2 = 126134 \text{ mm}^4$$

$$I = I_1 + I_2 = 220002 \text{ mm}^4$$

$$M_{top} = \left| \frac{\sigma I}{y} \right| = \frac{24 \times 10^6 \times 22 \times 10^{-8}}{0.0167} = 316.17 \text{ kNm}$$

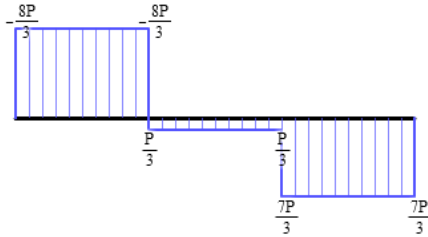
$$M_{bot} = \left| \frac{\sigma I}{y} \right| = \frac{30 \times 10^6 \times 22 \times 10^{-8}}{0.0233} = 283.26 \text{ kNm}$$

$$M = \min(M_{top}, M_{bot}) = 283.26 \text{ kNm}$$

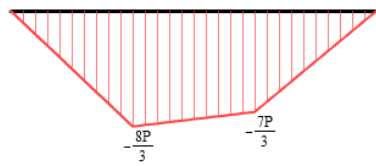
Q11:

$$\uparrow \sum F_y = 0 \Rightarrow R_A - 5P + R_B = 0$$

$$\leftarrow \sum M_A = 0 \Rightarrow 3P \cdot 1 + 2P \cdot 2 - R_B \cdot 3 = 0 \Rightarrow R_B = \frac{7P}{3}, R_A = 5P - R_B = \frac{8P}{3}$$



SFD:



BMD:

$$\bar{y} = \frac{y_1 A_1 + y_2 A_2}{A_1 + A_2} = \frac{(150 + 12.5) \times 25 \times 150 + 75 \times 150 \times 25}{25 \times 150 + 150 \times 25} = 118.75 \text{ mm}$$

$$\begin{aligned} I &= I_1 + A_1 (y_{c1} - \bar{y})^2 + I_2 + A_2 (y_{c2} - \bar{y})^2 \\ &= \frac{150 \times 25^3}{12} + (150 \times 25) \times (162.5 - 118.75)^2 + \frac{25 \times 150^3}{12} + (150 \times 25) \times (75 - 118.75)^2 \\ &= 2.158 \times 10^7 \text{ mm}^4 \end{aligned}$$

$$\begin{aligned} \sigma_{max} &= \frac{M_{max}}{I} \cdot y_{max} \leq 25 \text{ MPa} \Rightarrow M_{max} = \frac{8P}{3} \leq \frac{25 \cdot I}{y_{max}} = \frac{25 \times 10^6 \times 2.158 \times 10^{-5}}{0.11875} = 4.543 \text{ kN} \cdot \text{m} \\ &\Rightarrow P \leq 1.704 \text{ kN} \end{aligned}$$

$$\begin{aligned} \tau_{max} &= \frac{V_{max} Q}{I t} \leq 2.5 \text{ MPa} \Rightarrow V_{max} = \frac{8P}{3} \leq \frac{2.5 \cdot I t}{Q} = \frac{2.5 \times 10^6 \times 2.158 \times 10^{-5} \times 0.025}{0.11875 \times 0.025 \times 0.11875 \times 0.5} = 7.652 \text{ kN} \\ &\Rightarrow P \leq 2.869 \text{ kN} \end{aligned}$$

$$P = \min\{1.704, 2.869\} = 1.704 \text{ kN}$$