



Aalto University  
School of Engineering

**MEC-E8006 Fatigue of Structures**

**Lecture 2: Fatigue design**

# Learning outcomes

**After the lecture, you**

- understand fatigue design principles and philosophies
- can describe and characterize the loading history
- can estimate the fatigue life of un-notched member

# Contents

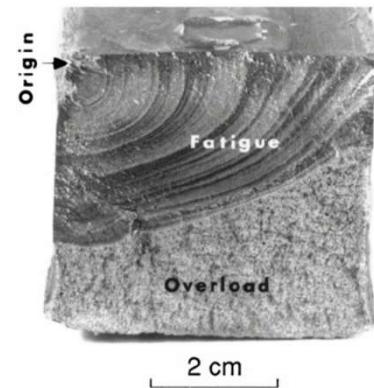
- **Introduction to fatigue design**
- **Fatigue testing and fatigue strength**
- **Variable amplitude loading**
- **Cumulative Damage**
- **Fatigue design philosophies**

# Fatigue design

## **Fatigue:**

*The study of crack, how they form and how they grow due to cyclic loading*

$$\text{total fatigue life} = \frac{\text{cycles to form a crack}}{\text{cycles to grow a crack to failure}}$$



# Fatigue design

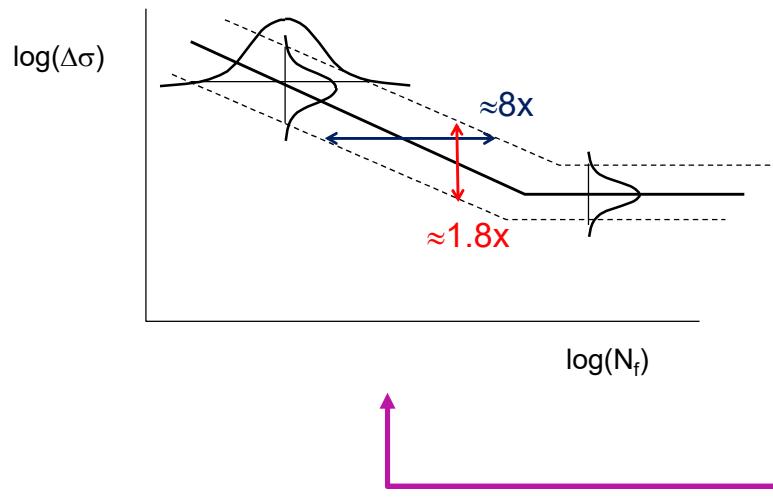
## **Fatigue design:**

*Using our understanding of fatigue and engineering to avoid premature fatigue failure of engineering components*

# Fatigue Design

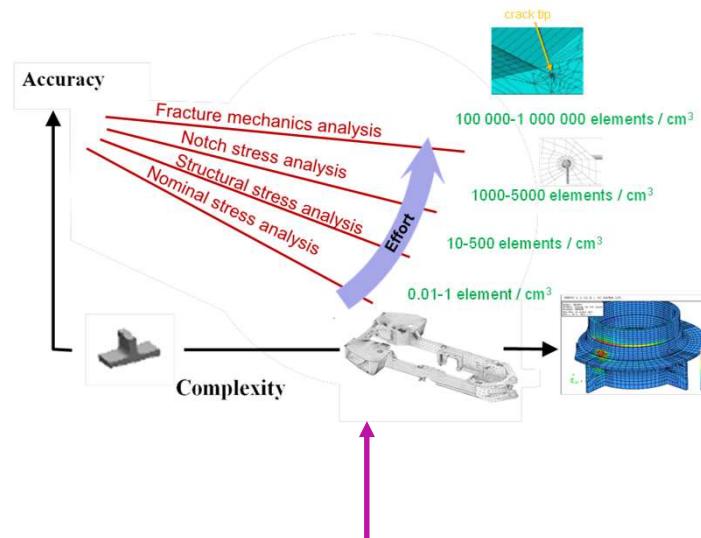
## Testing

to define fatigue resistance



## Analysis

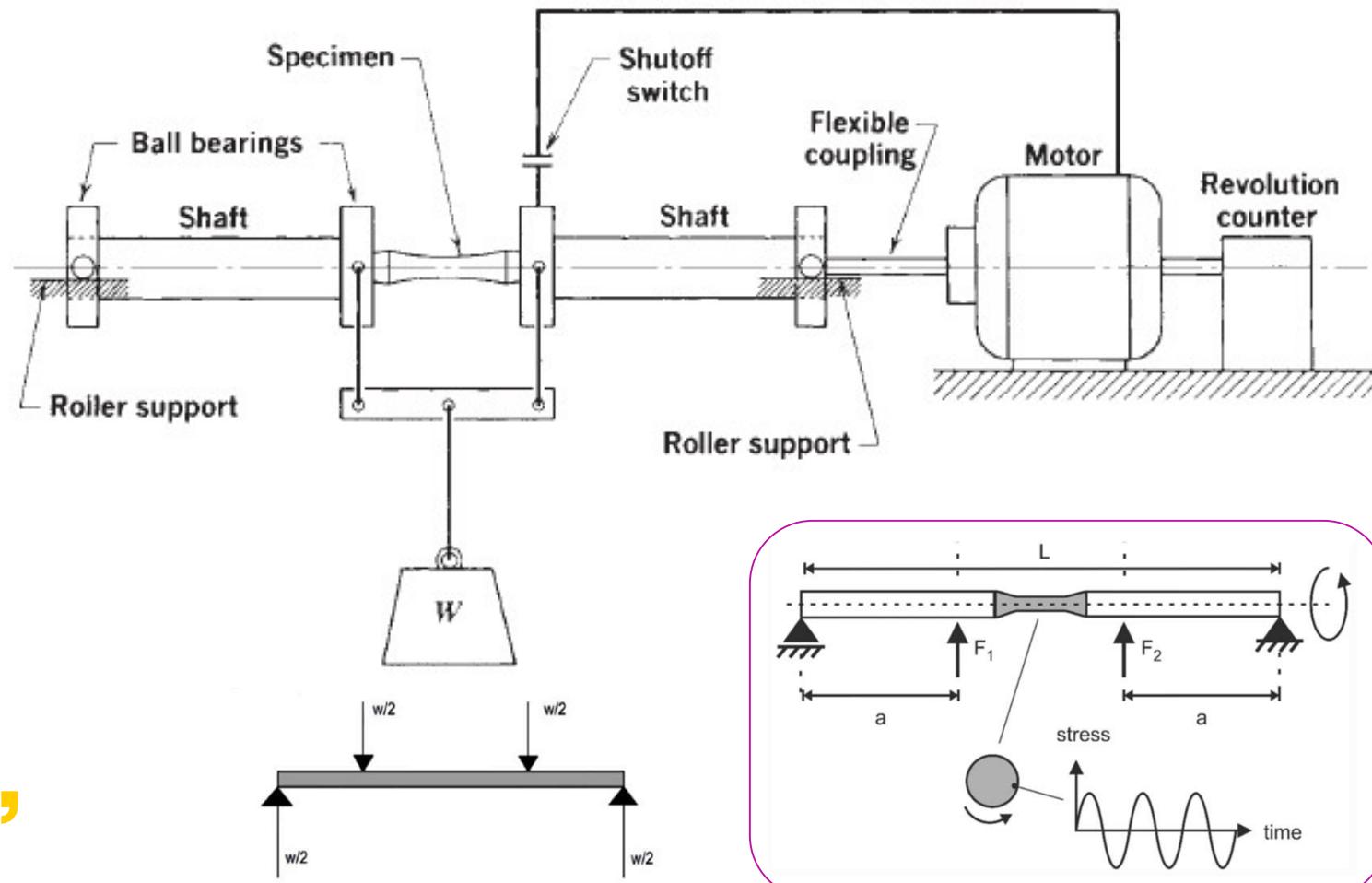
to define fatigue-effective stress/strain



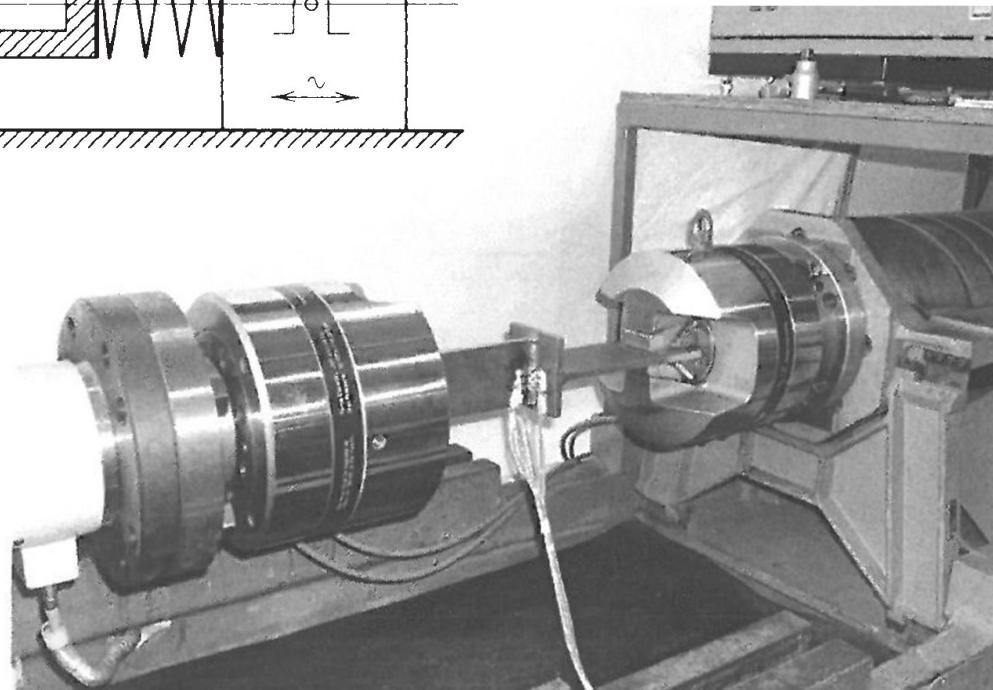
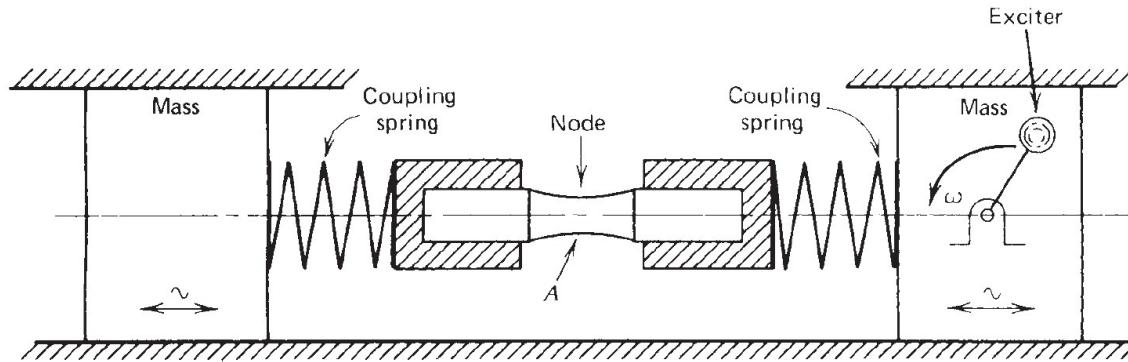
**Theory-based synthesis**  
to estimate fatigue life

# Fatigue testing

## Rotating 4-point bending



# Fatigue testing



Axial fatigue testing  
machine based on a  
resonant vibration

# Fatigue testing

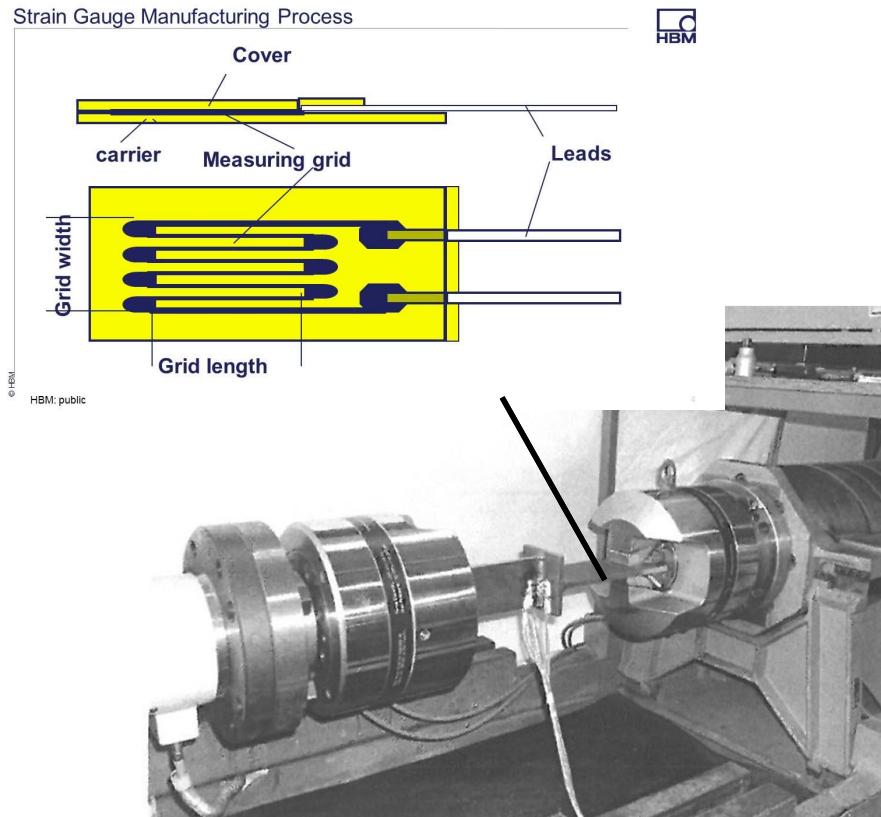
The "universal" testing machine



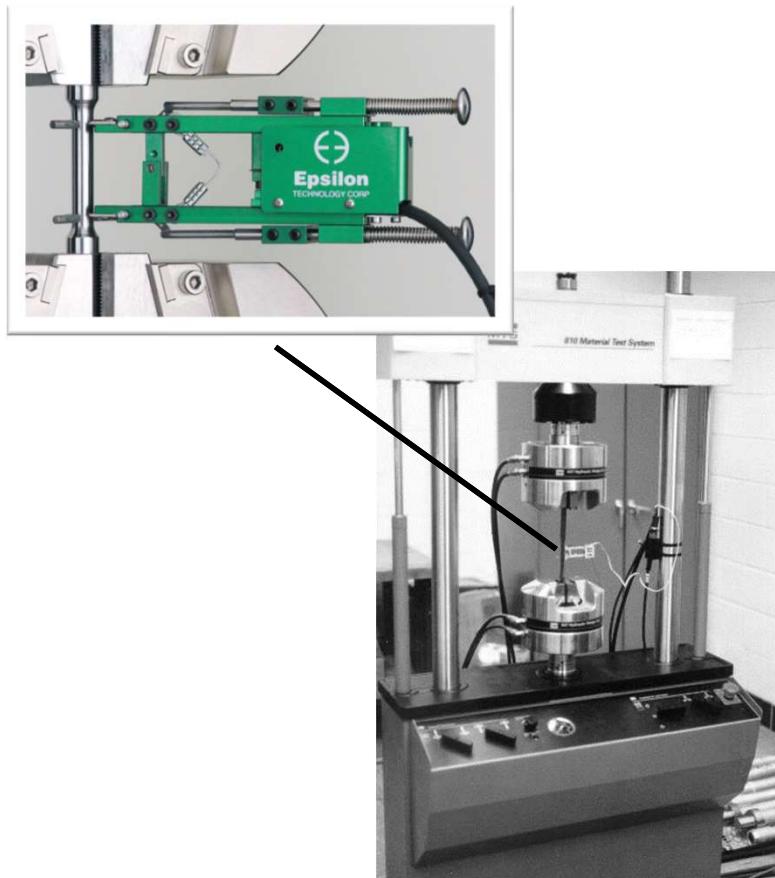
*Closed-loop servo-hydraulic testing machines*

# Fatigue testing

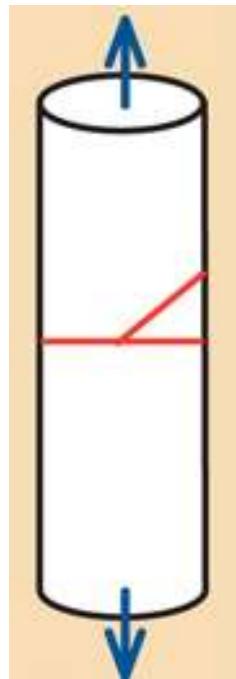
## Strain Gauge (gage)



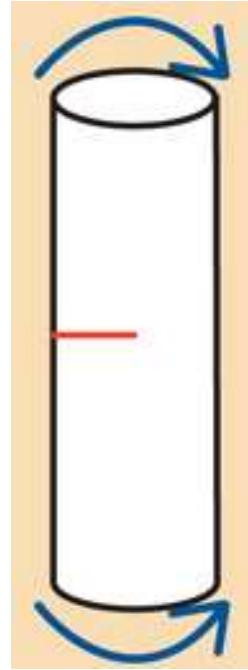
## Extensometer



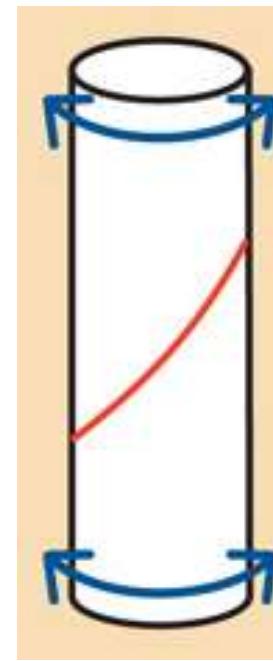
# Fatigue testing



Tension



Bending



Torsion

# Fatigue testing

$$\sigma = \frac{M\rho}{I}$$

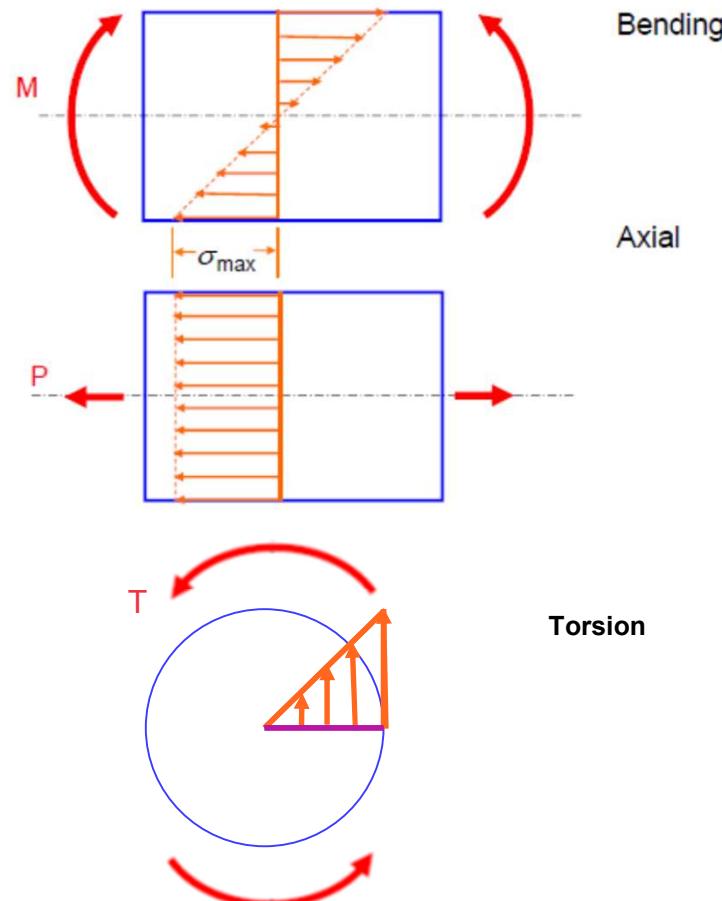
Distance from neutral axis  
Moment of inertia  
Applied load

$$\sigma = \frac{P}{A}$$

Cross-section area

$$\tau = \frac{T\rho}{J}$$

Torque  
Polar moment of inertia

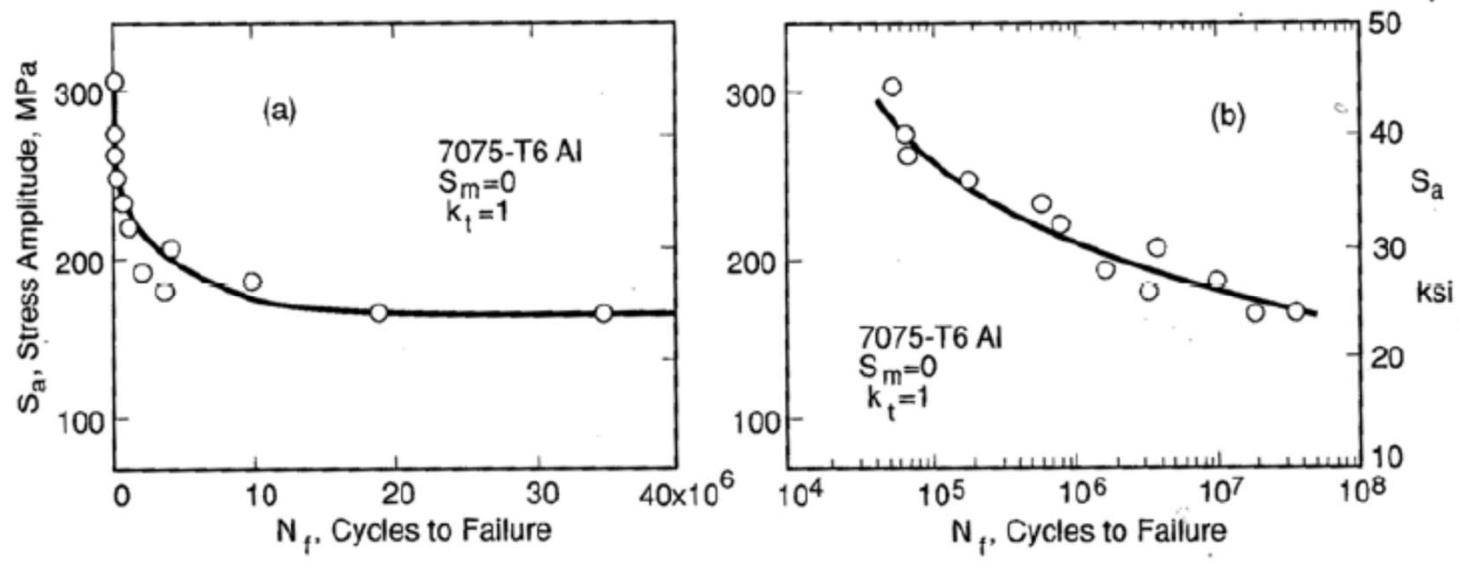


# Fatigue testing

**TABLE 4.1 ASTM Standard Practices Related to Fatigue Testing of Metals [4]**

E466	Conducting Force Controlled Constant Amplitude Axial Fatigue Tests of Metallic Materials
E467	Verification of Constant Amplitude Dynamic Forces in an Axial Fatigue Testing System
E468	Presentation of Constant Amplitude Fatigue Test Results for Metallic Materials
E606	Strain-Controlled Fatigue Testing
E647	Measurement of Fatigue Crack Growth Rates
E739	Statistical Analysis of Linear or Linearized Stress–Life ( $S-N$ ) and Strain–Life ( $\epsilon-N$ ) Fatigue Data
E1012	Verification of Specimen Alignment Under Tensile Loading (under the jurisdiction of Committee E-28 on Mechanical Test Methods)
E1049	Cycle Counting in Fatigue Analysis
E1823	Standard Terminology Relating to Fatigue and Fracture Testing

# Fatigue testing

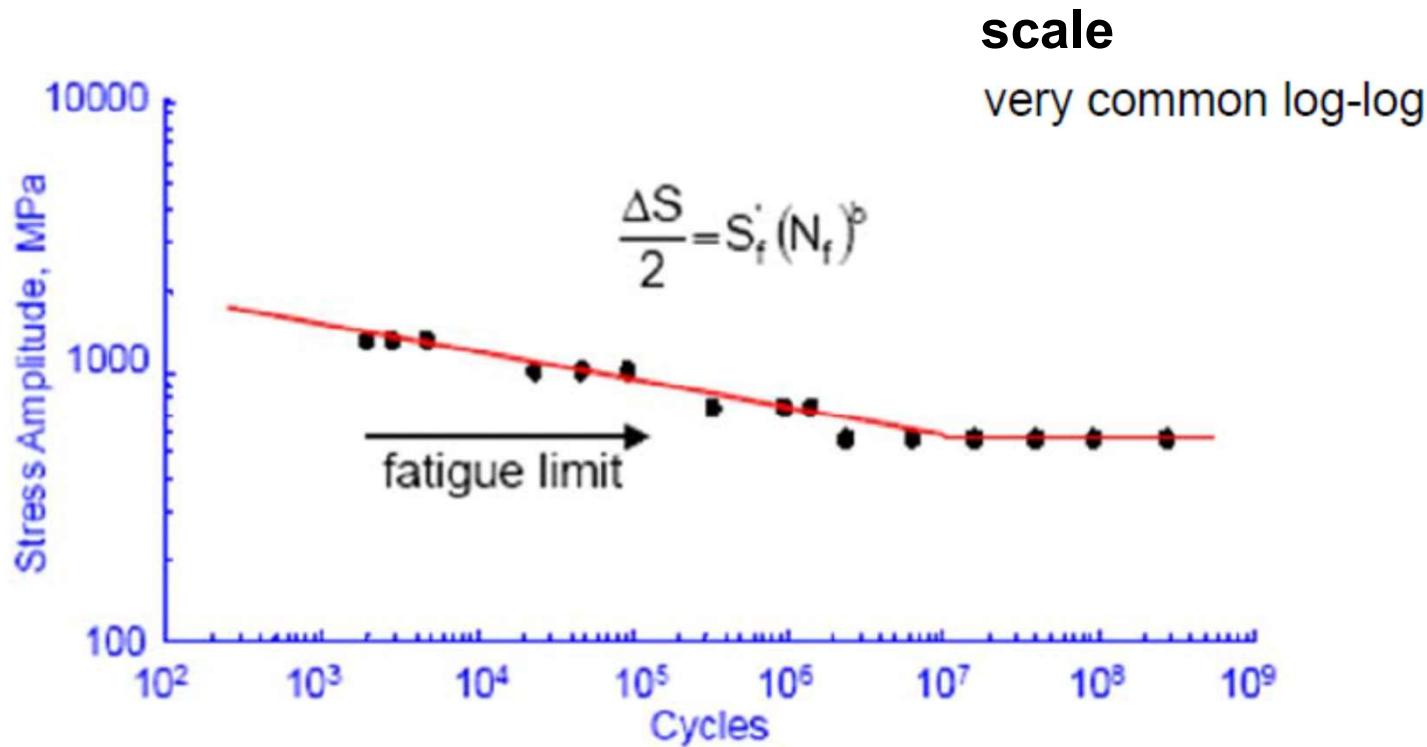


Scale: linear-linear

log-linear

very common log-log

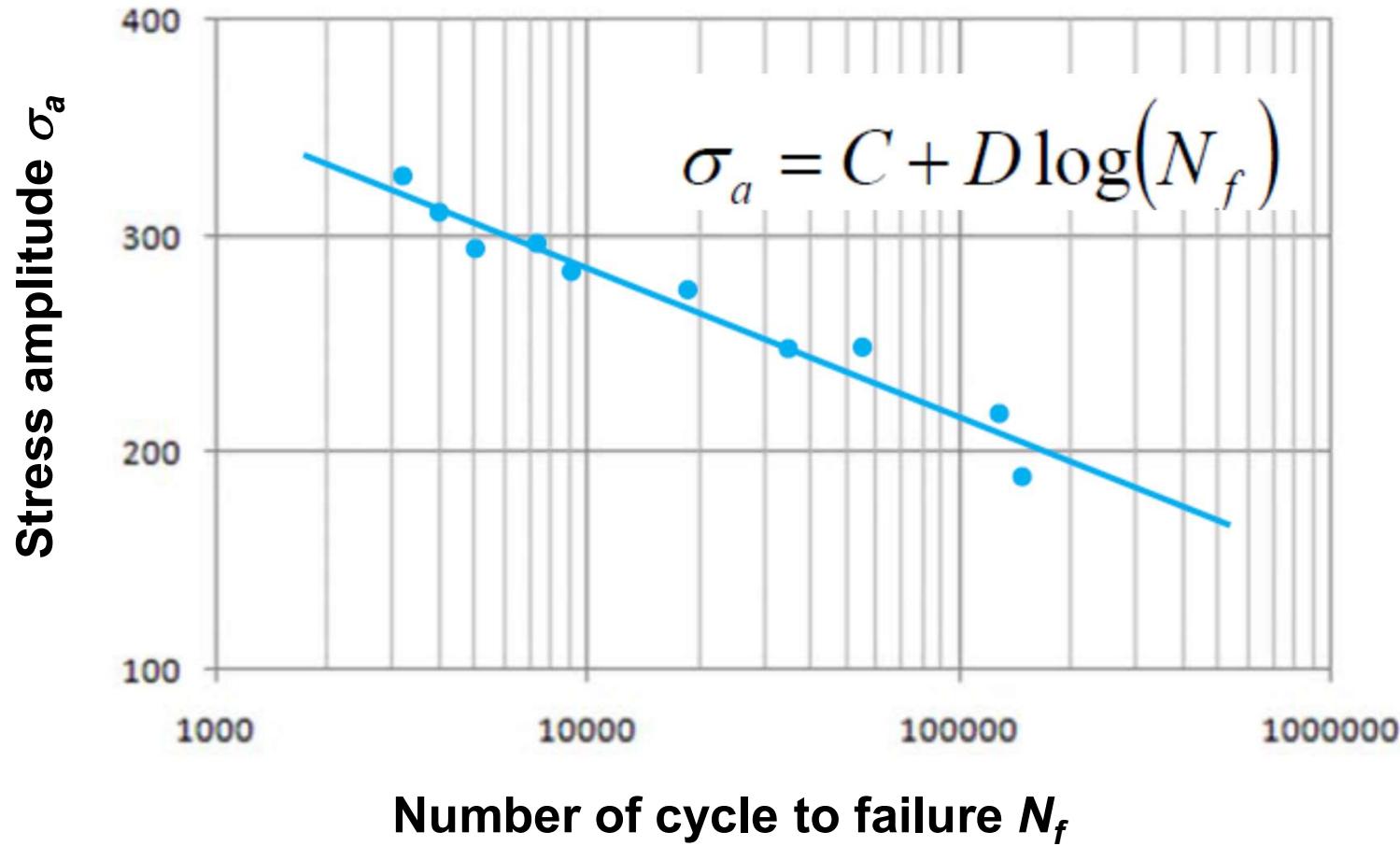
# Fatigue testing



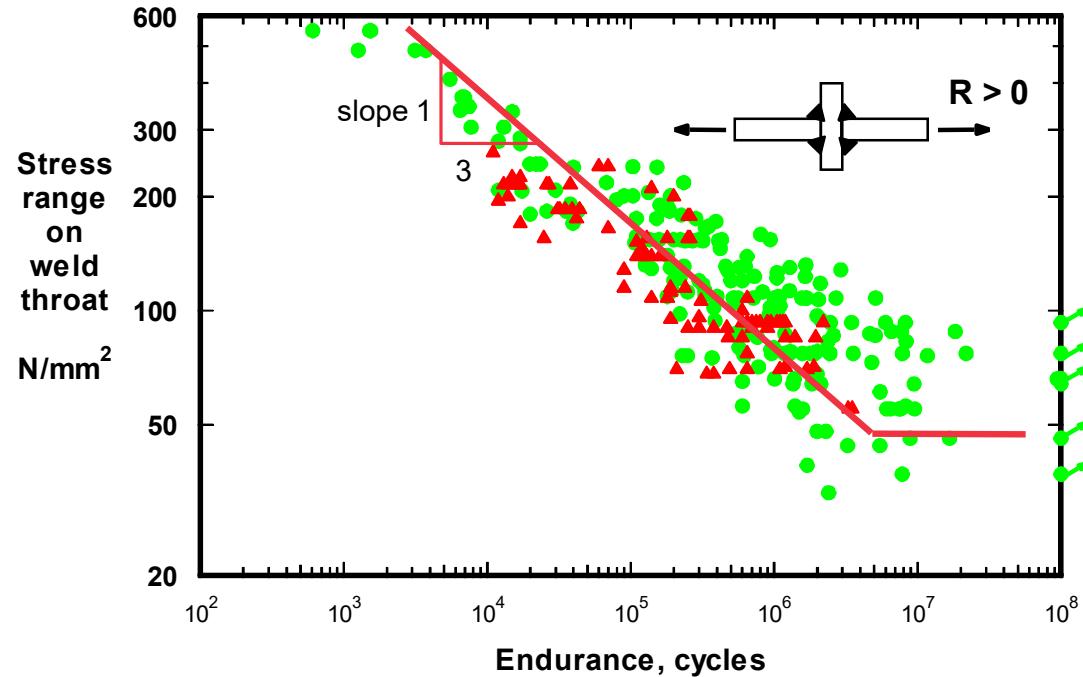
Note: Many textbooks report that the fatigue limit (or endurance limit) represents a stress where the life goes to infinity during constant amplitude loading. A better definition is that it represents a stress where the S-N curve shows a change of slope. Fatigue life becomes long, but recent tests suggest that failure will still occur – eventually.

# Fatigue testing

Log-linear scale



# Fatigue testing



log-linear

$$\sigma_a = C + D \log(N_f)$$

log-log

$$\sigma_a = A \cdot N_f^B$$

# Fatigue testing

## Linear regression

$$y = A + Bx$$

$$B = \frac{n \sum x_i y_i - \sum x_i \sum y_i}{n \sum x_i^2 - (\sum x_i)^2}$$

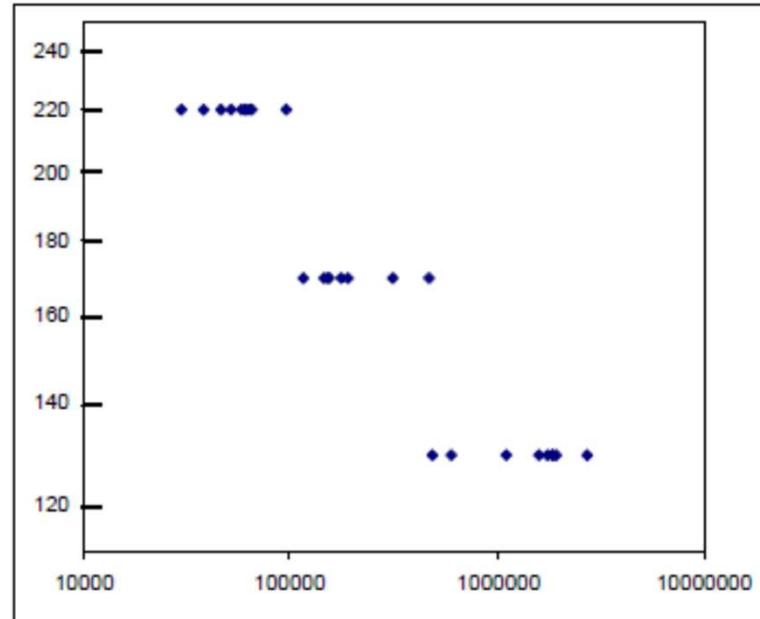
$$A = \frac{\sum y_i}{n} - B \frac{\sum x_i}{n}$$

$n$  = number of data points  
 $x_i, y_i$  values of data  $i$

Note: equations assume that  $y_i$  is the dependent variable (that what we measure)  
equations assume that  $x_i$  is the independent variable (that what we control)

# Fatigue testing

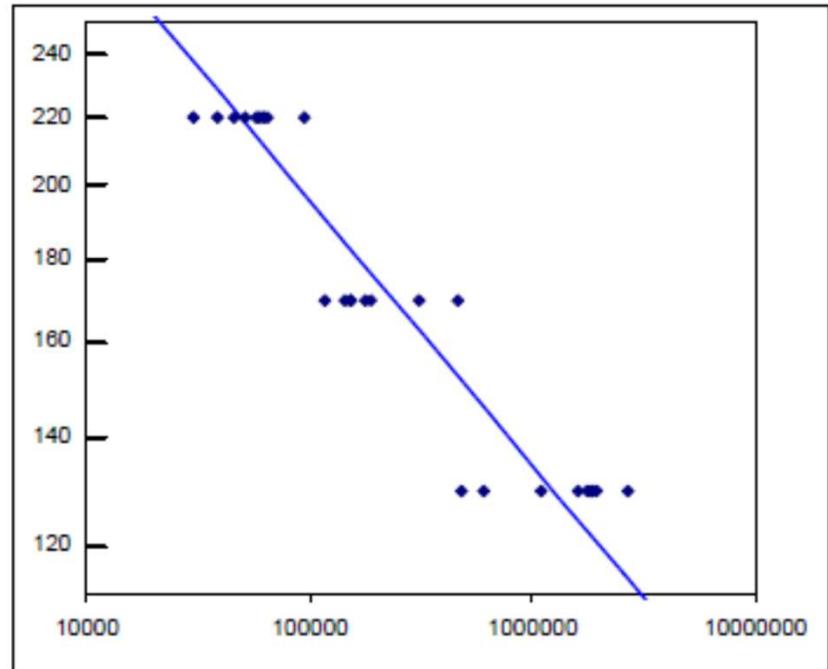
Stress (MPa)	Nf
130	485000
130	1750000
130	1600000
130	601300
130	1840000
130	1860000
130	1100000
130	1930000
130	2700000
170	190567
170	465000
170	153140
170	311250
170	144430
170	152060
170	176960
170	116430
220	46240
220	30000
220	62500
220	95000
220	65300
220	60200
220	38500
220	58200
220	52020



$$y = A + Bx$$
$$\sigma_a = C + D \log(N_f) \quad \sigma_a = A \cdot N_f^B$$

**log-linear**                            **log-log**

# Fatigue testing

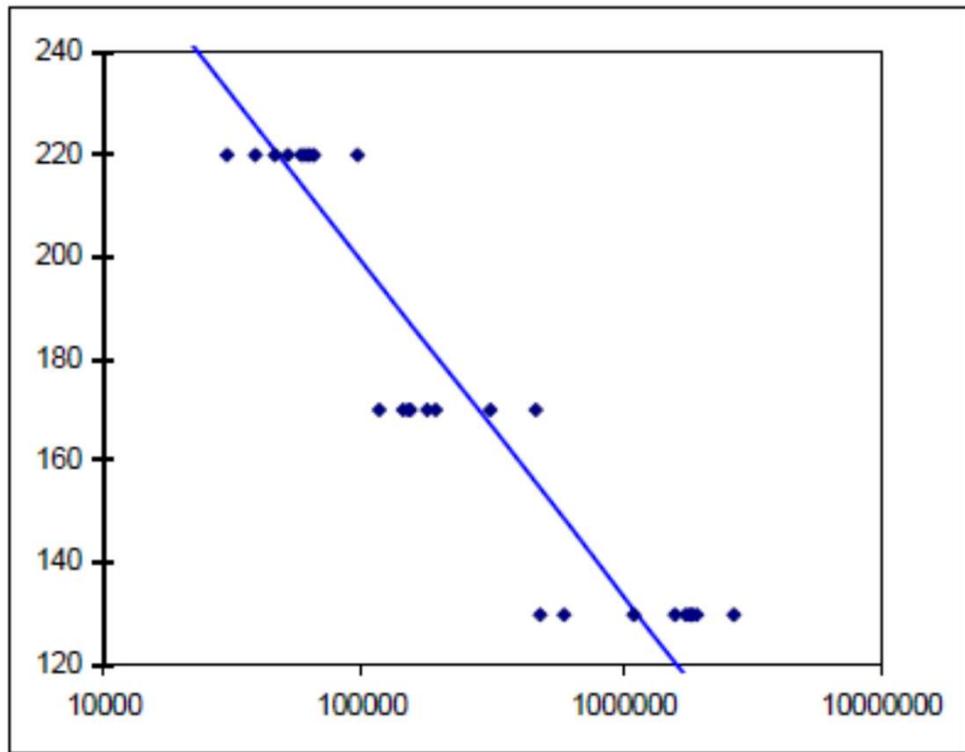


$$\sigma_a = A \cdot N_f^B$$

A = 1274 MPa

B = -0.163

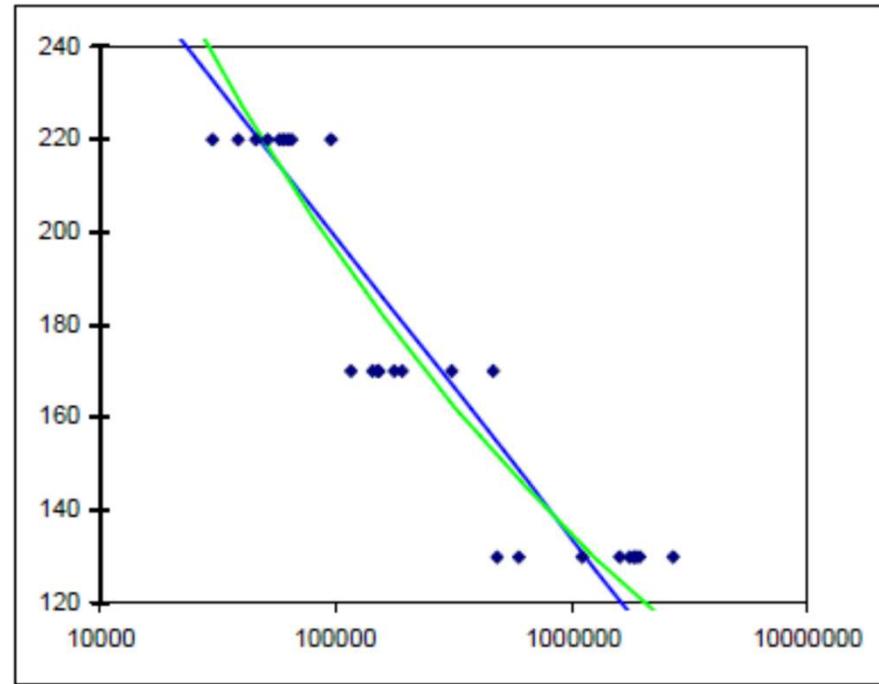
# Fatigue testing



$$\sigma_a = C + D \log(N_f)$$

$$C = 523 \text{ MPa}$$

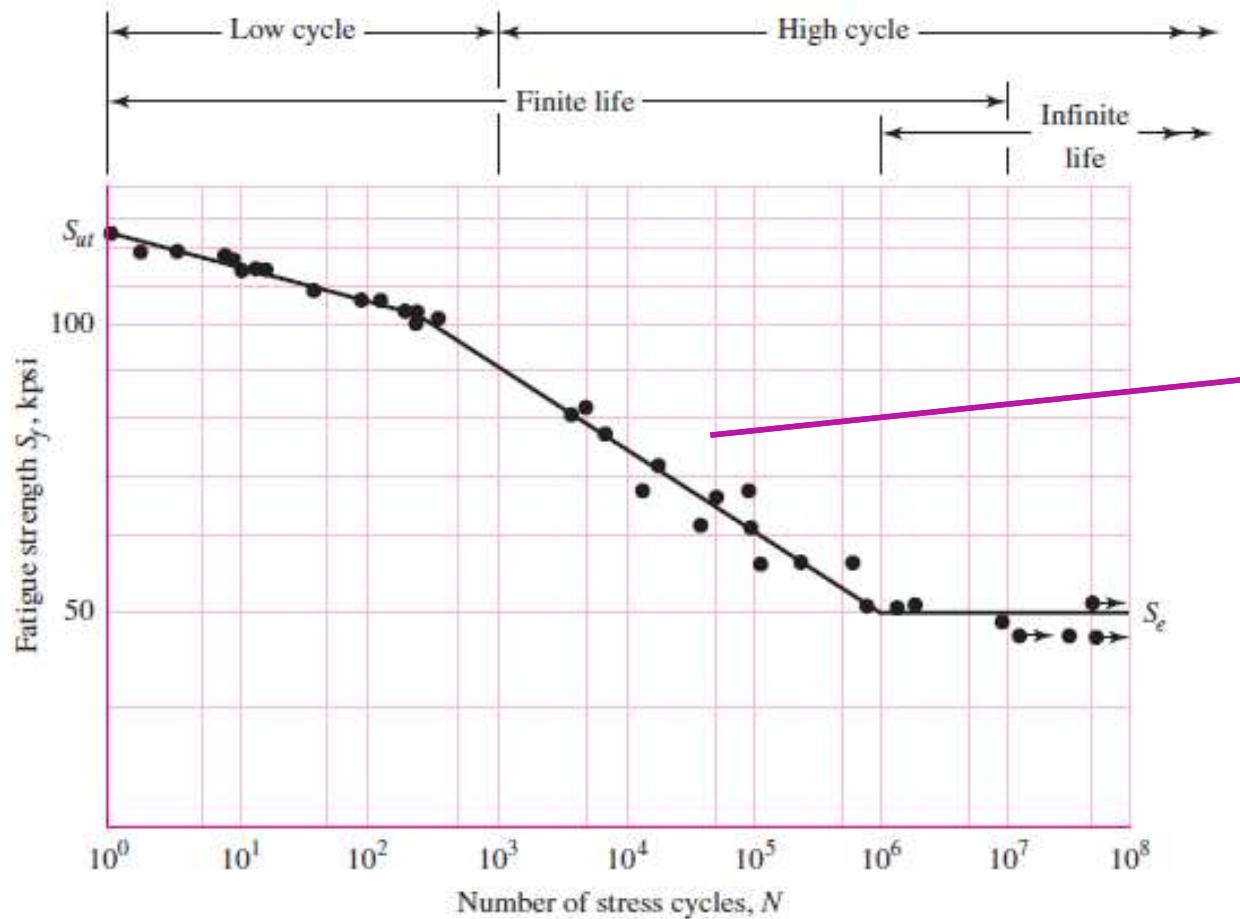
# Fatigue testing



$$\sigma_a = C + D \log(N_f) \quad \text{--- blue line}$$

$$\sigma_a = A \cdot N_f^B \quad \text{--- green line}$$

# Fatigue strength



$$S_f = a N^b$$

$$a = \frac{(f S_{ut})^2}{S_e}$$

$$b = -\frac{1}{3} \log \left( \frac{f S_{ut}}{S_e} \right)$$

# Example

Given a 1050HR steel, estimate

- the endurance strength corresponding to  $10^4$  cycles
- the expected life of the specimen under the stress of 379 MPa

Solution:

$$S_{ut} = 620 \text{ MPa}, S_e = 310 \text{ MPa}$$

$$a = \frac{[0.86(620)]^2}{310} = 917.10 \text{ MPa}$$

$$b = -\frac{1}{3} \log \frac{[0.86(620)]}{310} = -0.0785$$

$$S_f = 917.10 N^{-0.0785}$$

For  $10^4$  cycles

$$S_f = 917.10 (10^4)^{-0.0785} = 445.05 \text{ MPa}$$

Under stress of 379 MPa

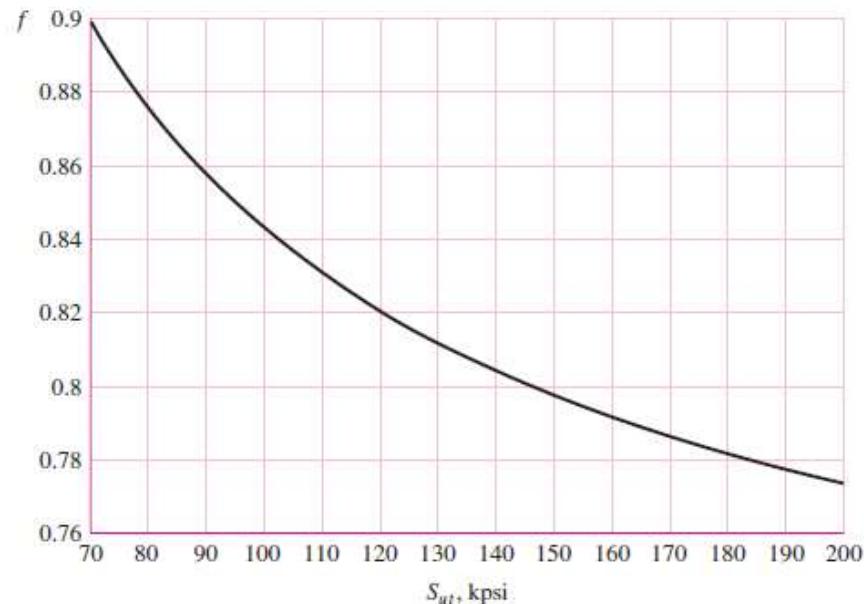
$$N = \left(\frac{379}{917.10}\right)^{\frac{1}{-0.0785}} = 7.75 * 10^4 \text{ cycles}$$

$$S_f = a N^b$$

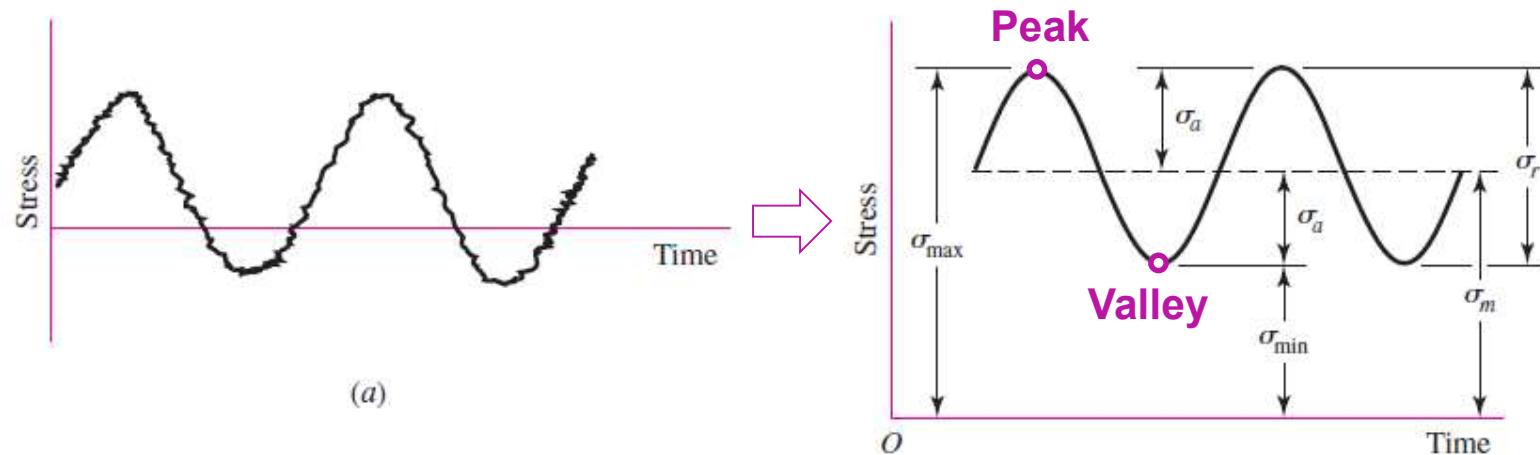
$$a = \frac{(f S_{ut})^2}{S_e}$$

$$b = -\frac{1}{3} \log \left( \frac{f S_{ut}}{S_e} \right)$$

$$S_e = 0.5 S_{ut}$$



# Different loading history



$$\sigma_m = \frac{\sigma_{max} + \sigma_{min}}{2}$$

$$\sigma_a = \left| \frac{\sigma_{max} - \sigma_{min}}{2} \right|$$

$\sigma_{min}$  = minimum stress

$\sigma_{max}$  = maximum stress

$\sigma_m$  = mean stress

$\sigma_a$  = amplitude stress

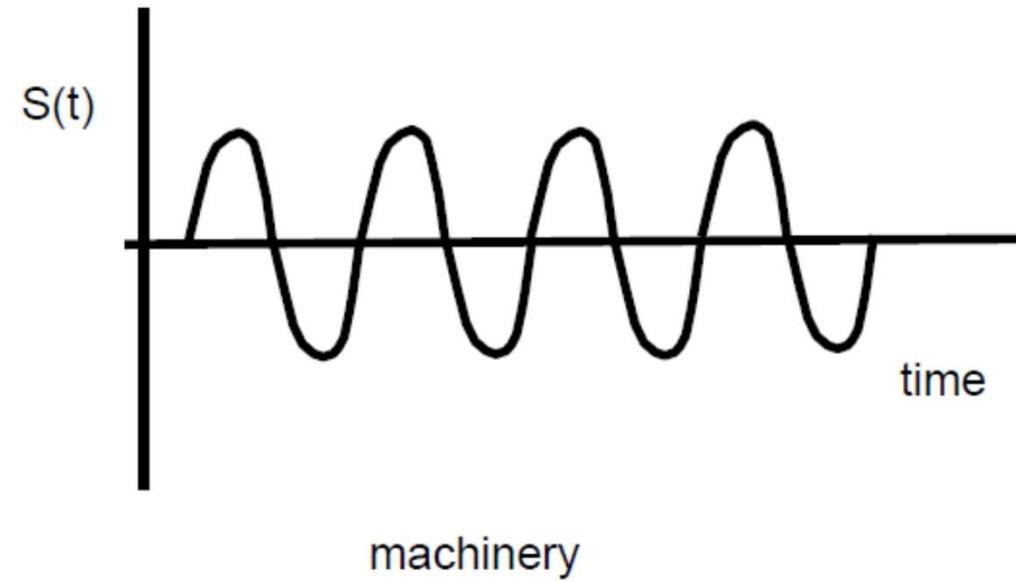
**Stress ratio**

$$R = \frac{\sigma_{min}}{\sigma_{max}}$$

# Variable amplitude loading



Constant amplitude, constant mean stress

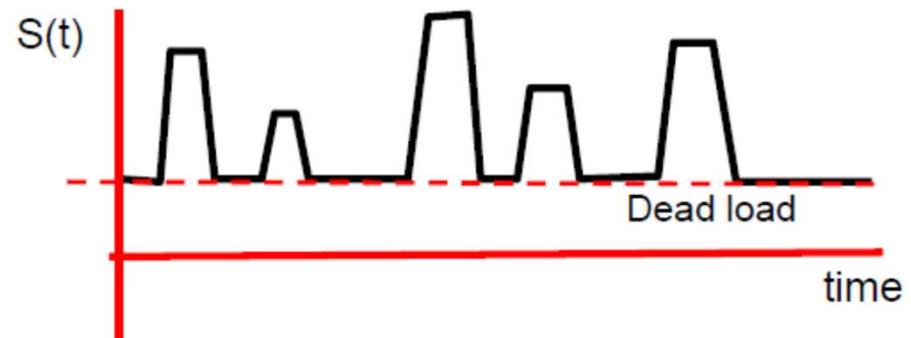


machinery

# Variable amplitude loading



Constant minimum, changing amplitude

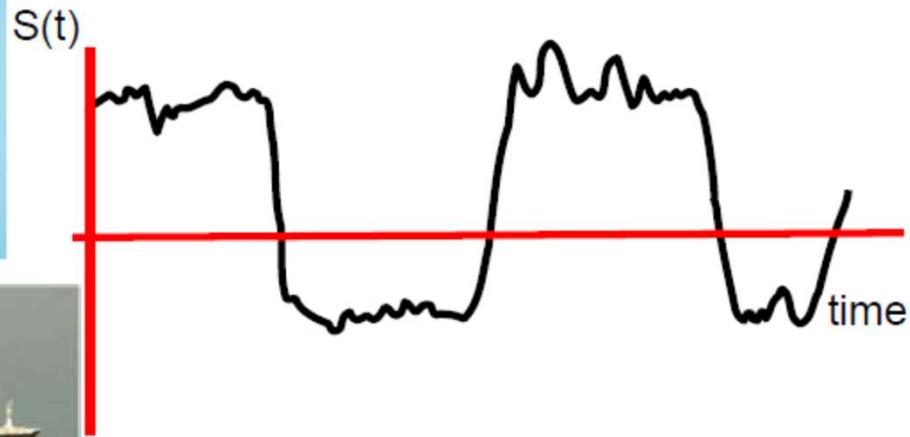


Pressure vessels, cranes,  
short span bridges, ...

# Variable amplitude loading



Mean changes at intervals,  
Constantly changing amplitude

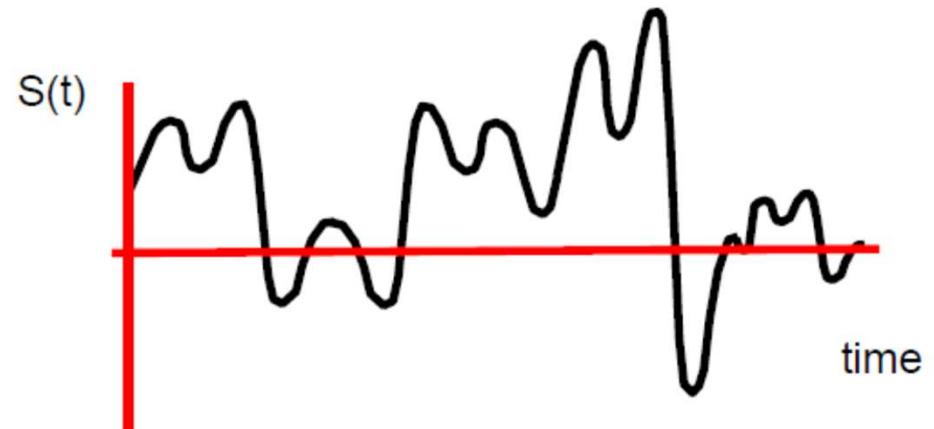


aircraft / tankers

# Variable amplitude loading

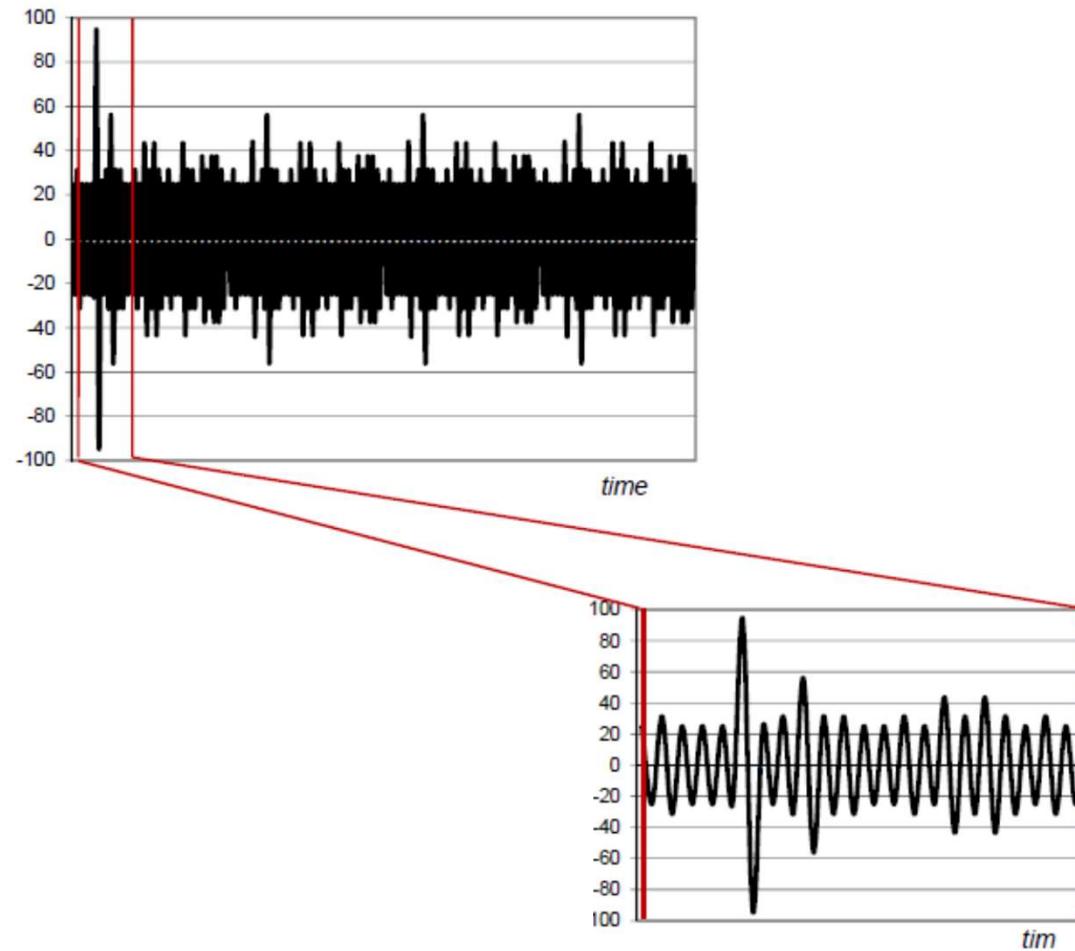


Constantly changing mean, constantly changing amplitude

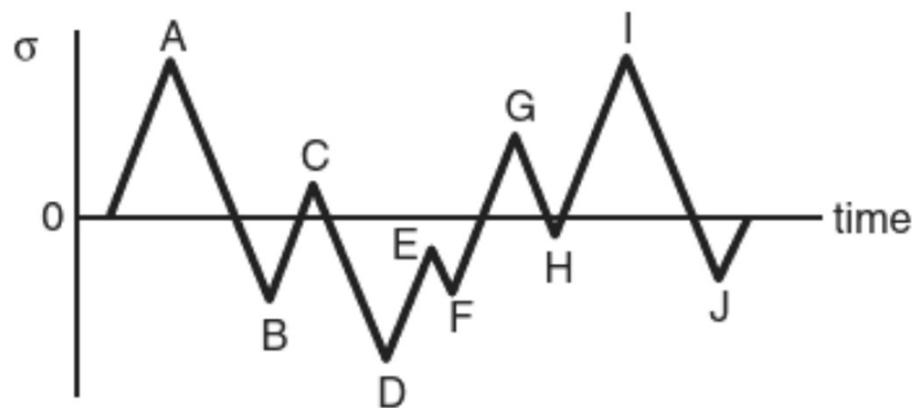


Vehicles, wave loading, wind loading, ...

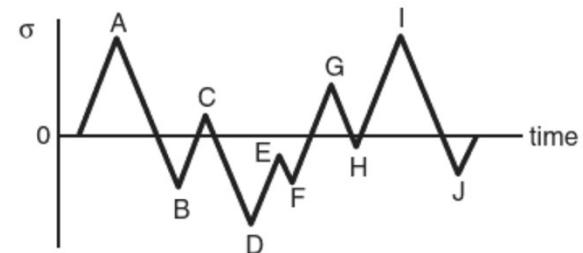
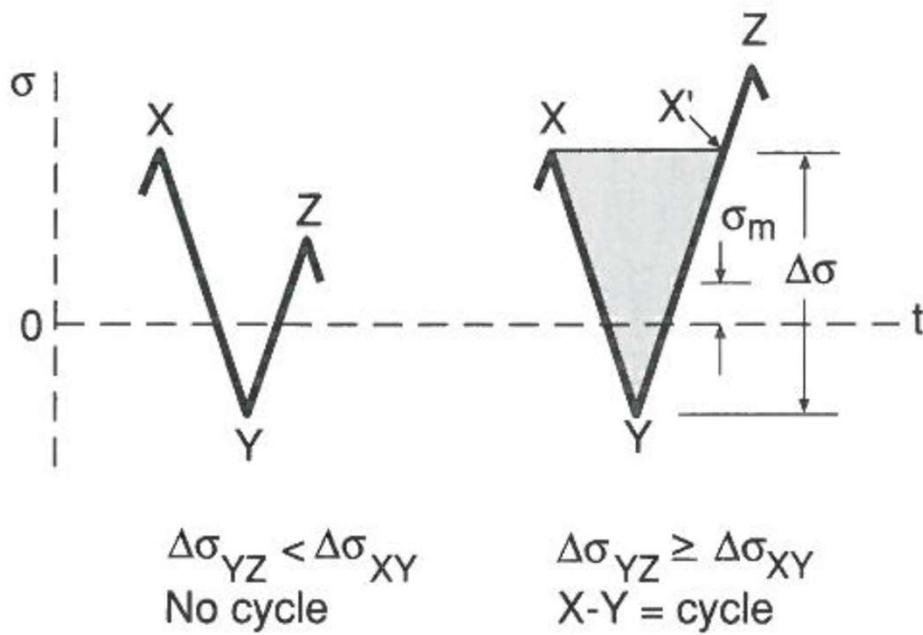
# Variable amplitude loading



# Rainflow cycle counting



# Rainflow cycle counting



For cycle X-Y

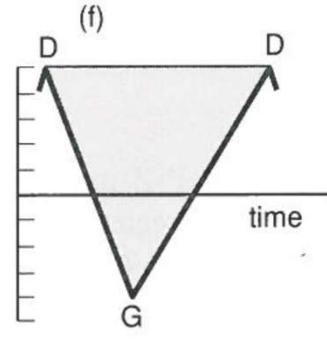
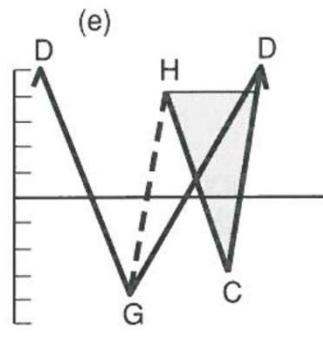
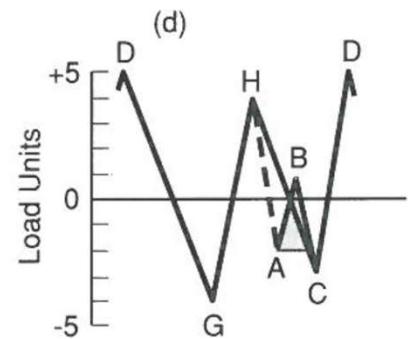
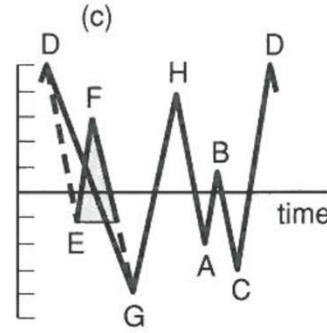
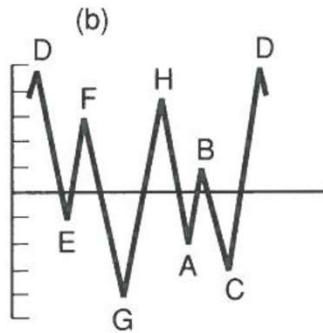
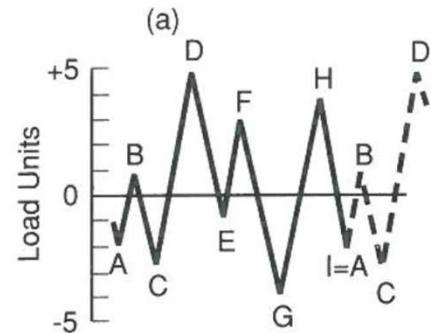
Peak:  $\sigma_X$

Valley:  $\sigma_Y$

Range:  $\Delta\sigma = \sigma_X - \sigma_Y$

Mean:  $\sigma_m = (\sigma_X + \sigma_Y)/2$

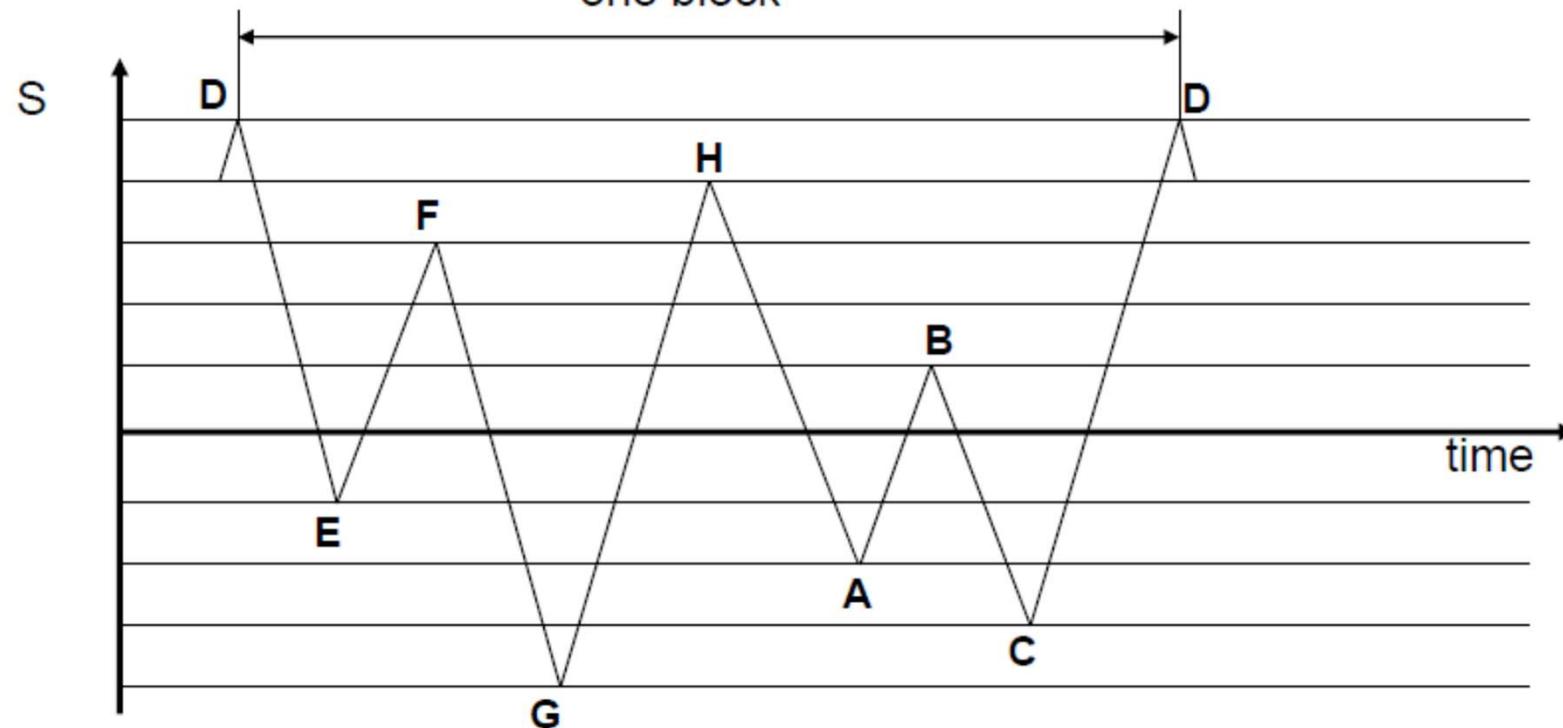
# Rainflow cycle counting



Cycle	Range	Mean
E-F	4.0	1.0
A-B	3.0	-0.5
H-C	7.0	0.5
D-G	9.0	0.5

# Rainflow cycle counting

- Re-sequence load block with max peak first
  - block is shifted to begin ASTM rainflow cycle counting demonstration one block

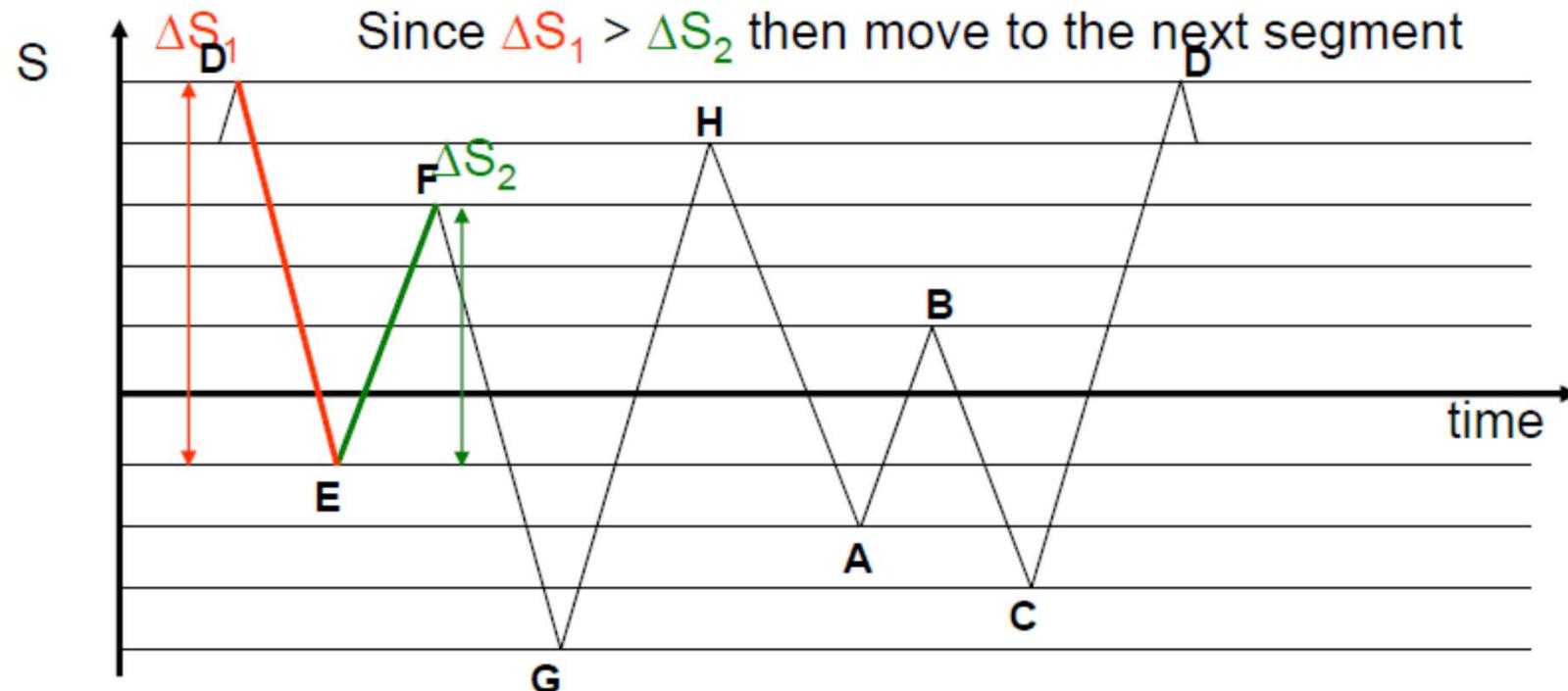


# Rainflow cycle counting

define first range

define second range

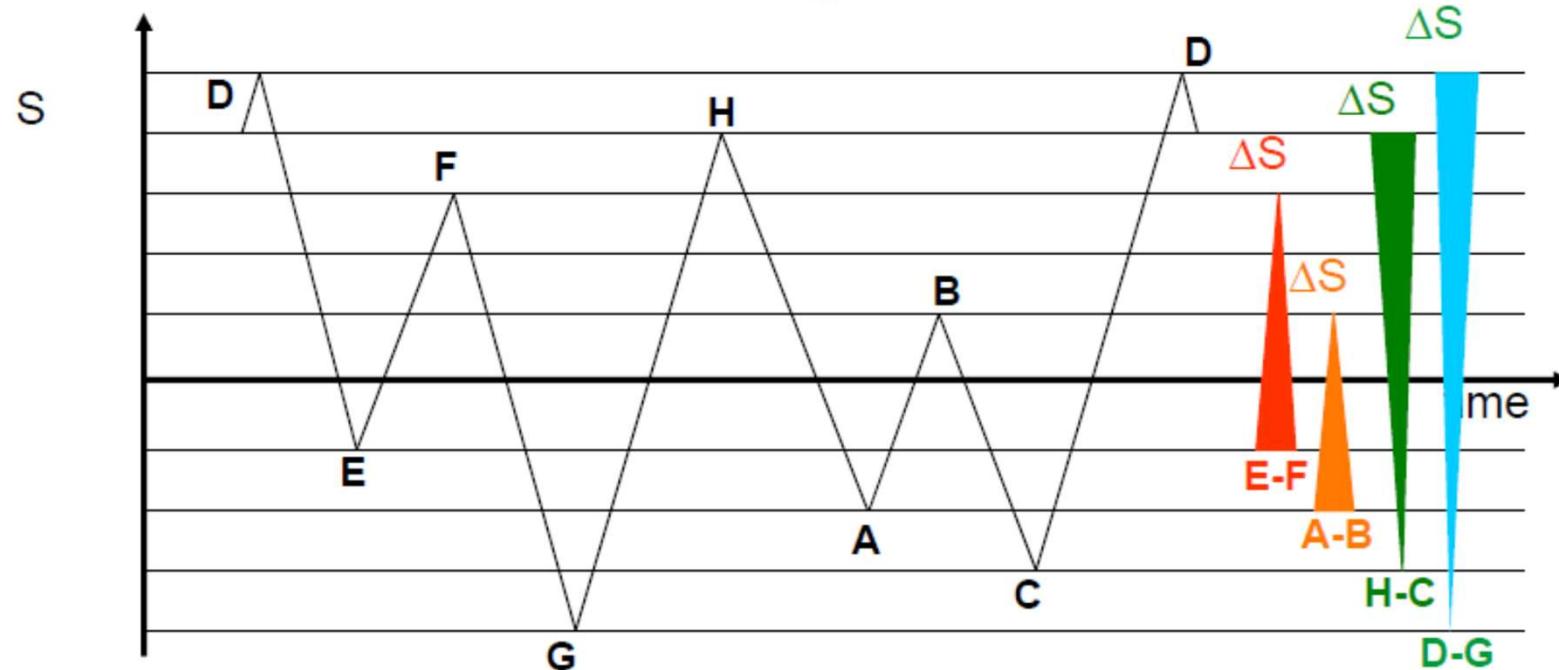
Compare the two:  
IF  $\Delta S_1 \leq \Delta S_2$  THEN  
COUNT A CYCLE



# Rainflow cycle counting

**NOTE!**  
*8 reversals and 4 cycles*

4 ranges counted from  
block, as shown below



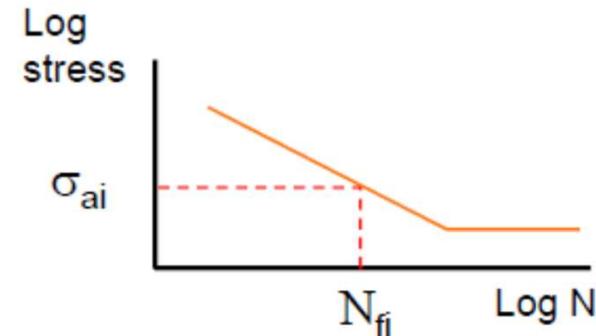
# Cumulative damage

Palmgren-Miner

The damage caused by a cycle when it is part of a variable amplitude loading history is the same as the damage caused by that cycle during constant amplitude loading.

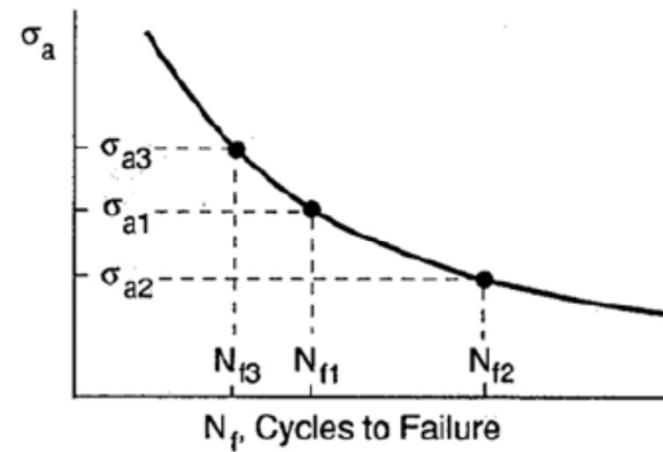
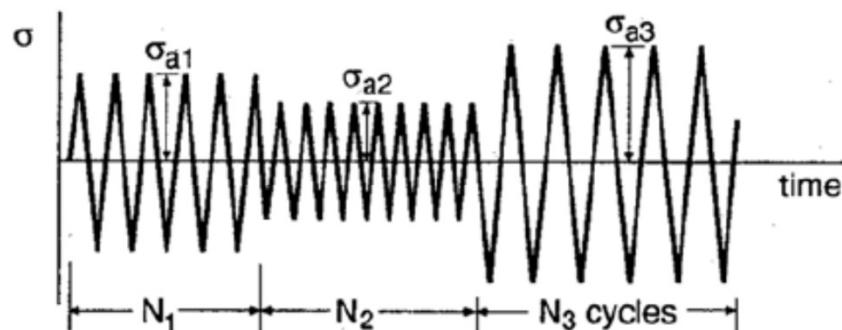
Suppose cycle  $\sigma_{ai}$  results in a fatigue life  $N_{fi}$  cycles.

Damage from one cycle is  $D_i = 1/N_{fi}$



At failure  $D = 1$

# Cumulative damage



$$\frac{N_1}{N_{f1}} + \frac{N_2}{N_{f2}} + \frac{N_3}{N_{f3}} + \dots = 1$$

# Cumulative damage

Palmgren-Miner

The damage caused by a cycle when it is part of a variable amplitude loading history is the same as the damage caused during constant amplitude loading

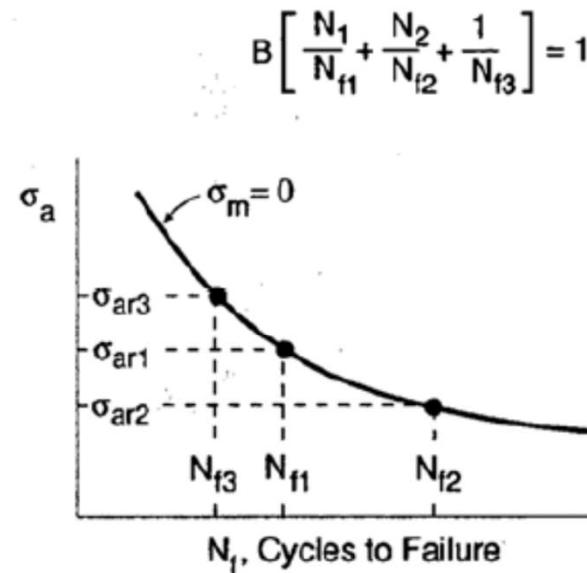
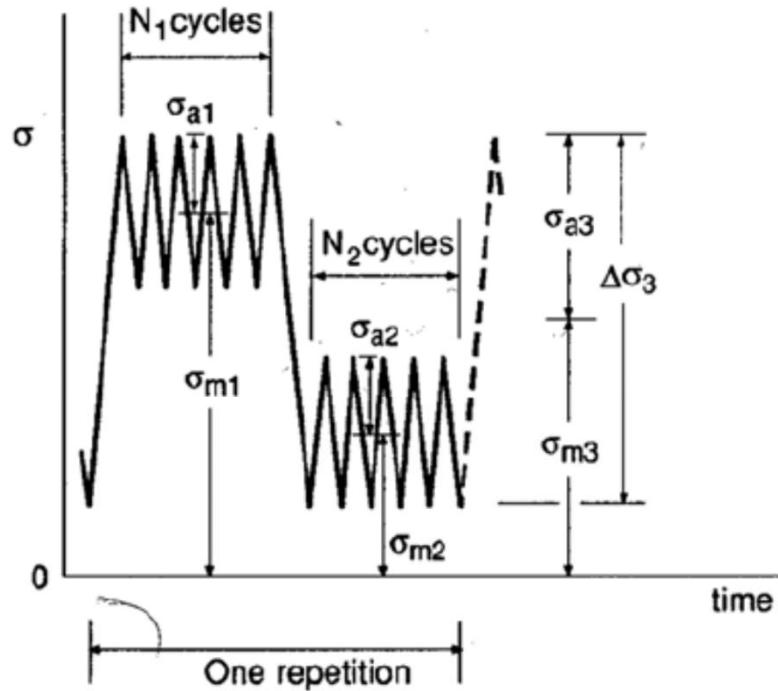
$$D = \frac{N_1}{N_{f_1}} + \frac{N_2}{N_{f_2}} + \frac{N_3}{N_{f_3}} + \dots = \sum \frac{N_i}{N_{f_i}} = 1$$

# Cumulative damage

Often a load history is a series of repeating blocks.  
Then we calculate the damage done for one block,  $1/B_f$

$$D = B_f \left[ \sum \frac{N_i}{N_{fi}} \right]_{\text{onerepetition}} = 1$$

# Cumulative damage



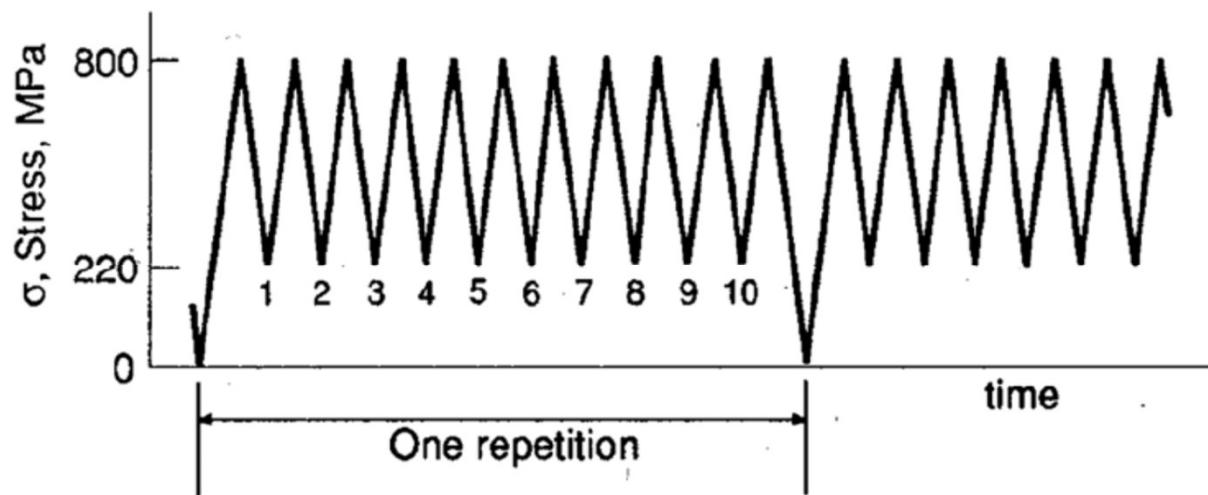
Goodman mean stress correction

$$\sigma_a = \left(1 - \frac{\sigma_m}{\sigma_u}\right) \cdot A \cdot N_f^b$$

$\sigma_m$  Mean stress  
 $\sigma_u$  Tensile strength

# Example

An unnotched member made of the AISI 4340 steel



# solution

## Rainflow counting

$j$	$N_j$	$\sigma_{\min}$	$\sigma_{\max}$	$\sigma_a$	$\sigma_m$
1	1	0	800	400	400
2	10	220	800	290	510

# solution

S-N curve for  $\sigma_m = 0$  (A and B from table)

$$\sigma_a = AN_f^{\frac{B}{f}} = 1643 \cdot N_f^{-0.0977}$$

S-N curve for  $\sigma_m \neq 0$

$$\sigma_{ar} = \frac{\sigma_a}{\left(1 - \frac{\sigma_m}{1172}\right)} = 1643 \cdot N_f^{-0.0977}$$

Goodman mean stress correction

$j$	$N_j$	$\sigma_{\min}$	$\sigma_{\max}$	$\sigma_a$	$\sigma_m$	$\sigma_{ar}$	$N_{fj}$
1	1	0	800	400	400	607	26,600
2	10	220	800	290	510	513	148,000

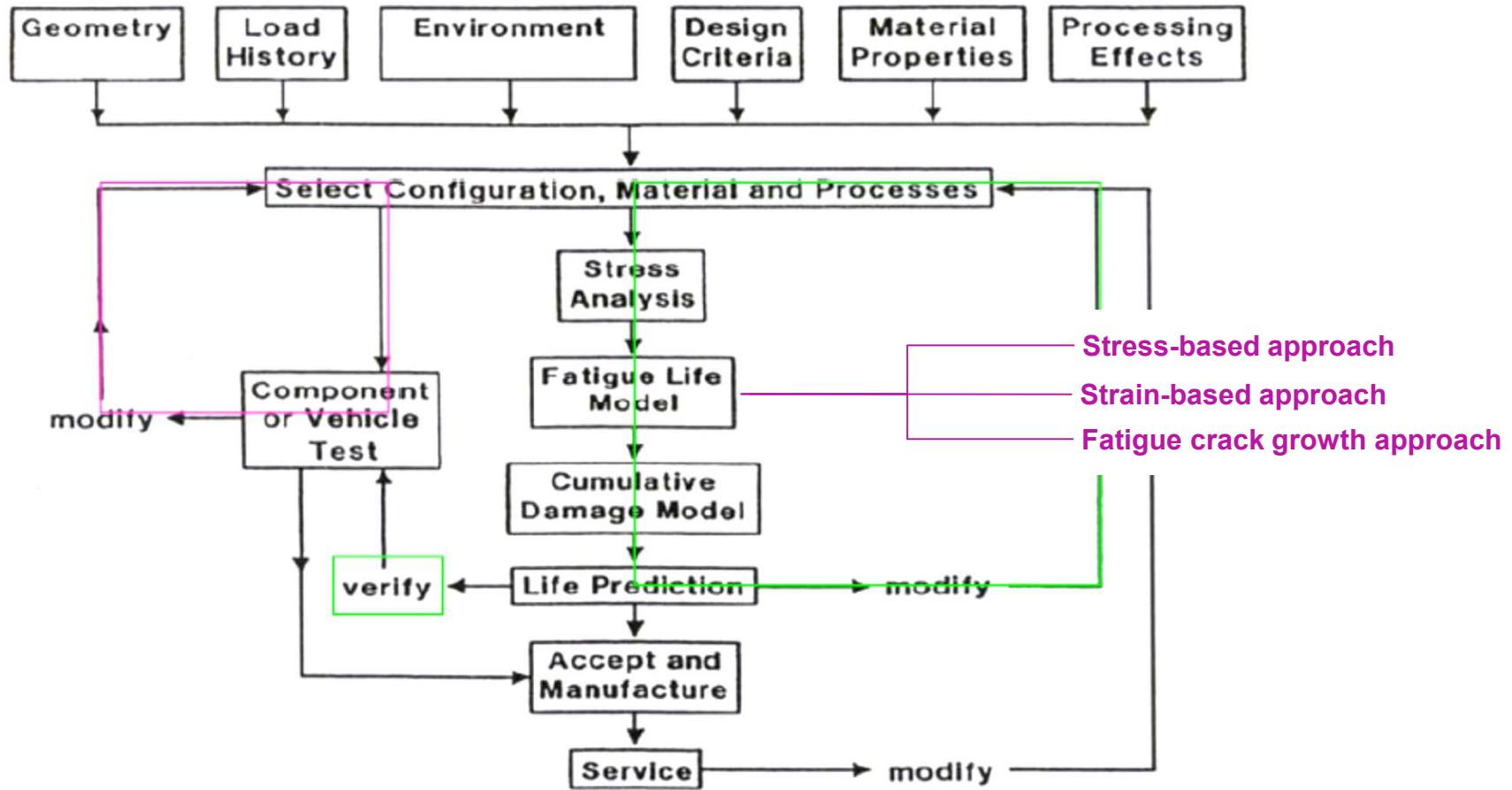
# solution

$j$	$N_j$	$\sigma_{\min}$	$\sigma_{\max}$	$\sigma_a$	$\sigma_m$	$\sigma_{ar}$	$N_{fj}$
1	1	0	800	400	400	607	26,600
2	10	220	800	290	510	513	148,000

$$B_f = 1/\left[ \sum \frac{N_i}{N_{fi}} \right]_{\text{one repetition}} = 1/\left[ \frac{1}{26,600} + \frac{10}{148,000} \right]$$

$$B_f = 1/\left[ 3,76 \times 10^{-5} + 6,76 \times 10^{-5} \right] = \underline{\underline{9510 \text{ repetitions}}}$$

# Fatigue design flow chart



# Analysis and testing

- Analysis and testing are both key aspects of fatigue design.
- A more complete and correct analysis involving iteration and optimization can provide prototypes that are closer to the final product and thus require less testing.
- Insufficient or incorrect analysis may result in too much dependence upon testing and re-testing creating both time and cost inefficiencies.

# Approaches to Fatigue Design

## Stress-based approach

### Nominal stress-life method

- Major development 1850-1930.
- Uses nominal stresses and relates these to local fatigue strengths for notched and unnotched members
- Continues to dominate fatigue assessment in most industries

### Structural stress-life method

- First proposed in 1960s and developed in 1980-2000.
- Uses a well defined “structural stress” in place of the nominal stresses and relates these to local fatigue strengths
- Widely used in offshore and shipbuilding. Used for complex welded structures where nominal stress is difficult to define

### Effective notch stress-life method

- Major development 1990-2011
- Important method for welded structures

# Approaches to Fatigue Design

## Strain-based approach

### Local strain-life ( $\varepsilon$ -N) method

- Major development 1960-1980
- Local strain at a notch is related to smooth specimen strain-controlled fatigue behavior.
- Analytical models can be used to determine local strains from global or nominal stresses or strains.

# Approaches to Fatigue Design

## Fatigue crack growth approach

### Fatigue crack growth ( $da/dN-\Delta K$ ) method

- First formulated in the 1960s.
- Requires the use of **fracture mechanics** to obtain the number of cycles to grow a crack from a given length to another length and/or to fracture.
- This model can be considered a total fatigue life model when used in conjunction with existing initial crack size following manufacture.
- Computationally demanding but very accurate. Used in aircraft and nuclear industry and increasingly by others.

# Approaches to Fatigue Design

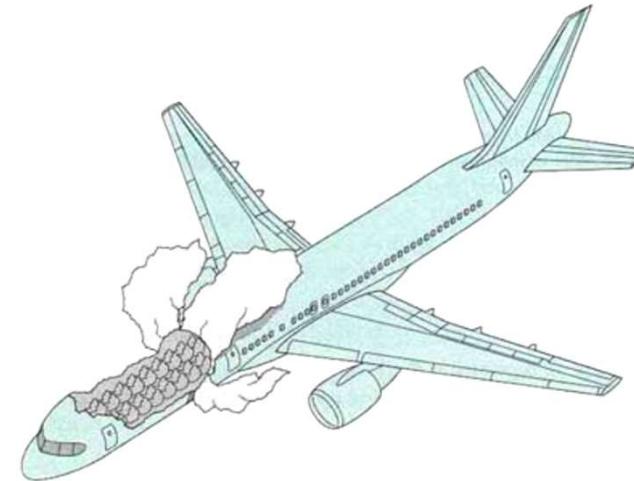
## Other approaches

### Multi-stage methods.

- For example combine  $\epsilon\text{-N}$  for crack initiation and  $da/dN\text{-}\Delta K$  for crack growth.
- The two lives are added together to obtain the total fatigue life.
- OR
- microstructural fracture mechanics to model cracks in one or a few grains plus  $da/dN\text{-}\Delta K$
- scientifically important but rarely applied in engineering

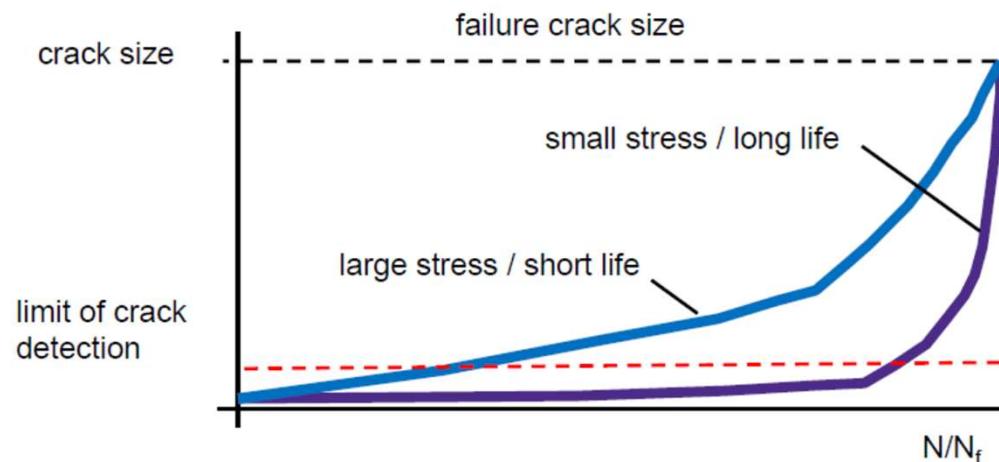
# Fatigue design philosophies

- Infinite-Life Design
- Safe-life Design
- Fail safe



# Fatigue design philosophies

- Infinite-Life Design
- Safe-life Design
- Fail safe
- Damage tolerant

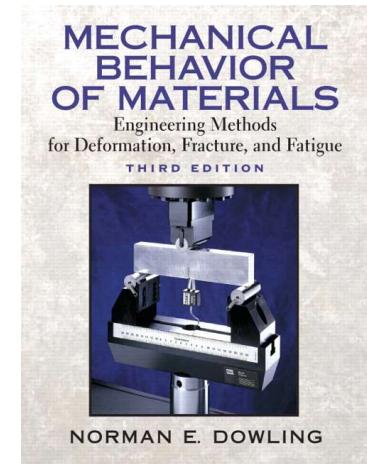


# Readings – Course material

## Course book

Mechanical Behavior of Materials Engineering Methods for Deformation, Fracture, and Fatigue, Norman E. Dowling

- Chapter 9.1-9.4
- Chapter 9.9



## Optional reading materials given on MyCourses webpages

- Metal fatigue in engineering, S.I. Stephens, A. Fatemi, R.R. Stephens, H.O. Fuchs, Chapter 2 – Fatigue design methods
- MEC-E8006\_L2-Loading history analysis\_SelfStudy.pdf
- MEC-E8006\_LA Rainflow\_counting\_Step-by-step.pdf
- ASM International. 2008, Elements of Metallurgy and Engineering Alloys, Chapter 14 – Fatigue