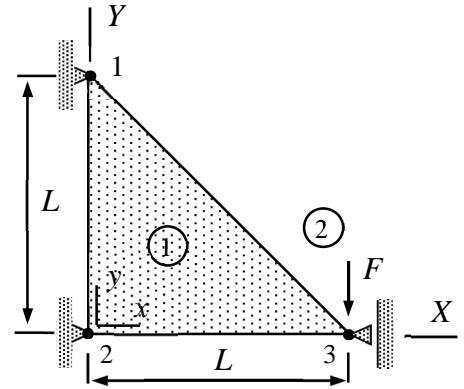


Assignment 5

A thin triangular slab is loaded by a point force at node 3. Nodes 1 and 2 are fixed and node 3 moves only in the vertical direction. Derive the equilibrium equation of the structure according to the large displacement theory in terms of the dimensionless displacement component $a = u_{Y3} / L$. Approximation is linear and material parameters C and ν are constants. Assume plane-stress conditions. When $F = 0$, side length and thickness of the slab are L and t , respectively. Also find the solution to a small displacement problem by simplifying the equilibrium equations with the assumption $|a| \ll 1$.



Solution

Virtual work density of internal forces, when modified for large displacement analysis with the same constitutive equation as in the linear case of plane stress, is given by

$$\delta w_{\Omega^0}^{\text{int}} = - \left\{ \begin{matrix} \delta E_{xx} \\ \delta E_{yy} \\ 2\delta E_{xy} \end{matrix} \right\}^T \frac{tC}{1-\nu^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & (1-\nu)/2 \end{bmatrix} \left\{ \begin{matrix} E_{xx} \\ E_{yy} \\ 2E_{xy} \end{matrix} \right\}, \left\{ \begin{matrix} E_{xx} \\ E_{yy} \\ 2E_{xy} \end{matrix} \right\} = \left\{ \begin{matrix} \frac{\partial u}{\partial x} + \frac{1}{2} \left(\frac{\partial u}{\partial x} \right)^2 + \frac{1}{2} \left(\frac{\partial v}{\partial x} \right)^2 \\ \frac{\partial v}{\partial y} + \frac{1}{2} \left(\frac{\partial u}{\partial y} \right)^2 + \frac{1}{2} \left(\frac{\partial v}{\partial y} \right)^2 \\ \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} + \frac{\partial u}{\partial x} \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \frac{\partial v}{\partial y} \end{matrix} \right\}.$$

Let us start with the approximations and the corresponding components of the Green-Lagrange strain. Linear shape functions can be deduced from the figure. Only the shape function $N_3 = x/L$ of node 3 is needed. Displacement components and their non-zero derivatives are

$$u = 0 \text{ and } v = \frac{x}{L} u_{Y3} \Rightarrow \frac{\partial u}{\partial x} = \frac{\partial u}{\partial y} = 0 \text{ and } \frac{\partial v}{\partial x} = \frac{u_{Y3}}{L} = a, \quad \frac{\partial v}{\partial y} = 0.$$

Green-Lagrange strain measures and their variations

$$\left\{ \begin{matrix} E_{xx} \\ E_{yy} \\ 2E_{xy} \end{matrix} \right\} = \left\{ \begin{matrix} a^2/2 \\ 0 \\ a \end{matrix} \right\} \Rightarrow \left\{ \begin{matrix} \delta E_{xx} \\ \delta E_{yy} \\ 2\delta E_{xy} \end{matrix} \right\} = \left\{ \begin{matrix} a\delta a \\ 0 \\ \delta a \end{matrix} \right\}.$$

When the strain component expressions are substituted there, virtual work density simplifies to

$$\delta w_{\Omega^0}^{\text{int}} = -\frac{tC}{1-\nu^2} \begin{Bmatrix} a\delta a \\ 0 \\ \delta a \end{Bmatrix}^T \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & (1-\nu)/2 \end{bmatrix} \begin{Bmatrix} a^2/2 \\ 0 \\ a \end{Bmatrix} \Rightarrow$$

$$\delta w_{\Omega^0}^{\text{int}} = -\frac{tC}{1-\nu^2} \delta a \left(\frac{1}{2} a^3 + \frac{1-\nu}{2} a \right)$$

Integration over the (initial) domain gives the virtual work expression. As the integrand is constant

$$\delta W^1 = \frac{L^2}{2} \delta w_{\Omega^0}^{\text{int}} = -\frac{L^2}{2} \frac{tC}{1-\nu^2} \delta a \left(\frac{1}{2} a^3 + \frac{1-\nu}{2} a \right).$$

Virtual work expression of the external point force components

$$\delta W^2 = -F \delta u_{Y3} = -FL \delta a.$$

Virtual work expression of the structure is obtained as sum over the element contributions. In terms of the dimensionless displacement

$$\delta W = -\frac{L^2}{2} \frac{tC}{1-\nu^2} \delta a \left(\frac{1}{2} a^3 + \frac{1-\nu}{2} a \right) - FL \delta a$$

or, when written in the standard form,

$$\delta W = -\delta a \left[\frac{L^2}{2} \frac{tC}{1-\nu^2} \left(\frac{1}{2} a^3 + \frac{1-\nu}{2} a \right) + FL \right].$$

Principle of virtual work and the basic lemma of variation calculus imply the equilibrium equation

$$(a^2 + 1 - \nu)a + 4(1 - \nu^2) \frac{F}{tLC} = 0. \quad \leftarrow$$

Assuming that $|a| \ll 1$ the equilibrium equation simplifies to

$$(1 - \nu)a + 4(1 - \nu^2) \frac{F}{tLC} = 0 \quad \Rightarrow \quad a = -4 \frac{F}{tCL} (1 + \nu). \quad \leftarrow$$