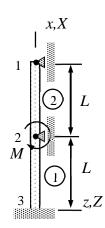
Assignment 4

Beam structure of the figure is loaded by a point moment acting on node 2. Determine the rotations θ_{Y1} and θ_{Y2} by using two beam bending elements. Displacements are confined to the XZ-plane. The cross-section properties of the beam A, I and Young's modulus of the material E are constants.



Solution template

Virtual work expression for the displacement analysis consists of parts coming from internal and external forces. For the beam bending mode in *xz*-plane, the element contribution is

$$\delta W = - \begin{cases} \delta u_{z1} \\ \delta \theta_{y1} \\ \delta u_{z2} \\ \delta \theta_{y2} \end{cases}^{\mathrm{T}} \underbrace{\begin{pmatrix} EI_{yy} \\ h^3 \end{pmatrix}}_{-6h} \begin{bmatrix} 12 & -6h & -12 & -6h \\ -6h & 4h^2 & 6h & 2h^2 \\ -12 & 6h & 12 & 6h \\ -6h & 2h^2 & 6h & 4h^2 \end{bmatrix} \begin{bmatrix} u_{z1} \\ \theta_{y1} \\ u_{z2} \\ \theta_{y2} \end{bmatrix}}_{-\frac{f_z h}{12}} \begin{bmatrix} 6 \\ -h \\ 6 \\ h \end{bmatrix}.$$

The element contribution of the point force/moment follows from the definition or work and is given by

$$\delta W = \begin{cases} \delta u_{X1} \\ \delta u_{Y1} \\ \delta u_{Z1} \end{cases}^{\mathsf{T}} \begin{cases} F_X \\ F_Y \\ F_Z \end{cases} + \begin{cases} \delta \theta_{X1} \\ \delta \theta_{Y1} \\ \delta \theta_{Z1} \end{cases}^{\mathsf{T}} \begin{cases} M_X \\ M_Y \\ M_Z \end{cases}.$$

For beam 1, the element contribution simplifies to

$$\delta W^{1} = -\begin{cases} 0 \\ 0 \\ 0 \\ \delta\theta_{Y2} \end{cases}^{T} \frac{EI}{L^{3}} \begin{bmatrix} 12 & -6L & -12 & -6L \\ -6L & 4L^{2} & 6L & 2L^{2} \\ -12 & 6L & 12 & 6L \\ -6L & 2L^{2} & 6L & 4L^{2} \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ \theta_{Y2} \end{cases} = -\delta\theta_{Y2} 4 \frac{EI}{L} \theta_{Y2}.$$

For beam 2, the element contribution is given by

$$\delta W^2 = - \begin{cases} 0 \\ \delta \theta_{Y2} \\ 0 \\ \delta \theta_{Y1} \end{cases}^{\mathrm{T}} \underbrace{\frac{EI}{L^3}}_{-6L} \begin{bmatrix} 12 & -6L & -12 & -6L \\ -6L & 4L^2 & 6L & 2L^2 \\ -12 & 6L & 12 & 6L \\ -6L & 2L^2 & 6L & 4L^2 \end{cases} \begin{bmatrix} 0 \\ \theta_{Y2} \\ 0 \\ \theta_{Y1} \end{bmatrix} = - \begin{bmatrix} \delta \theta_{Y2} \\ \delta \theta_{Y1} \end{bmatrix}^{\mathrm{T}} \begin{bmatrix} 4 \frac{EI}{L} & 2 \frac{EI}{L} \\ 2 \frac{EI}{L} & 4 \frac{EI}{L} \end{bmatrix} \begin{bmatrix} \theta_{Y2} \\ \theta_{Y1} \end{bmatrix}.$$

Virtual work expression of the point moment (considered as element 3) takes the form

$$\delta W^3 = -M \, \delta \theta_{Y2}$$
.

Virtual work expression of structure is sum of the element contributions. In the standard form

$$\delta W = \delta W^{1} + \delta W^{2} + \delta W^{3} = - \begin{cases} \delta \theta_{Y2} \\ \delta \theta_{Y1} \end{cases}^{T} \begin{pmatrix} 8 \frac{EI}{L} & 2 \frac{EI}{L} \\ 2 \frac{EI}{L} & 4 \frac{EI}{L} \end{cases} \begin{pmatrix} \theta_{Y2} \\ \theta_{Y1} \end{pmatrix} - \begin{pmatrix} -M \\ 0 \end{pmatrix}).$$

Principle of virtual work and the fundamental lemma of variation calculus imply that

$$\begin{bmatrix} 8\frac{EI}{L} & 2\frac{EI}{L} \\ 2\frac{EI}{L} & 4\frac{EI}{L} \end{bmatrix} \begin{Bmatrix} \theta_{Y2} \\ \theta_{Y1} \end{Bmatrix} - \begin{Bmatrix} -M \\ 0 \end{Bmatrix} = 0.$$

Solution to the linear equation system is given by

$$\theta_{Y2} = -\frac{1}{7} \frac{ML}{EI}$$
 and $\theta_{Y1} = \frac{1}{14} \frac{ML}{EI}$.

Use the code of MEC-E1050 to check your solution!