

Foundations on Continuum Mechanics - Week 6 - Constitutive Equations - Fluids

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Fluids

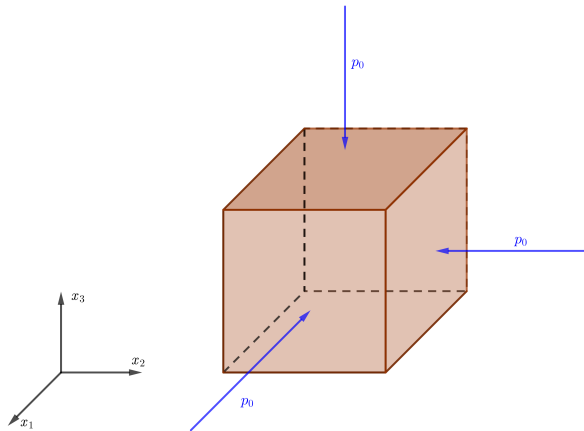
What is fluid?

Fluids can be classified in:

- ▶ Ideal (inviscid) fluids:
 - ▶ Called also perfect fluid
 - ▶ Water is an example of inviscid fluid
 - ▶ Resists only compressive stresses (pressure)
 - ▶ No resistance in fluid moves
- ▶ Real (viscous) fluids:
 - ▶ Has viscous (friction) behavior
 - ▶ Honey is an example of viscous fluid
 - ▶ Resistance in fluid moves

Pascal's Law

For a fluid at rest, the pressure acts on all directions.



Consequences of Pascal's Law

Consequences:

- ▶ No shear stresses at rest
- ▶ Only normal stresses due to pressure

The stress is isotropic at rest and of the form:

$$\underline{\underline{\sigma}} = -p_0 \underline{\underline{1}}$$
$$\sigma_{ij} = -p_0 \delta_{ij} \quad i, j \in \{1, 2, 3\}$$

p_0 denotes the hydrostatic pressure.

Pressure Concepts

Consequences:

- ▶ Hydrostatic pressure p_0 : normal compressive stress on a fluid.
- ▶ Mean pressure \bar{p} :

$$\bar{p} = -\sigma_m = -\frac{1}{3} \text{Tr}(\underline{\underline{\sigma}})$$

$\text{Tr}(\underline{\underline{\sigma}})$ is an invariant and therefore σ_m and \bar{p} are also.

- ▶ Thermodynamic pressure p : used in constitutive equations. It is related to density and temperature through the kinetic equation of state:

$$F(\rho, p, \theta) = 0$$

For a fluid at rest: $p_0 = \bar{p} = p$

Pressure Concepts

Consequences:

- ▶ Barotropic fluid is the fluid in which the pressure depends only on the density, [1]:

$$F(\rho, p) = 0 \Rightarrow p = f(\rho)$$

- ▶ Incompressible fluid, when the density is constant (special case of barometric):

$$F(\rho, p, \theta) \equiv F(\rho) = \rho - k = 0 \Rightarrow p = f(\rho) \Rightarrow \rho = k = \text{const.}$$

Constitutive Equations

Governing Equations: Thermo-mechanical problem

$\dot{\rho} + \rho \vec{\nabla} \cdot \vec{v} = 0$	Conservation of Mass Continuity Equation	1 eqn.	PDE
$\vec{\nabla} \cdot \underline{\underline{\sigma}} + \rho \vec{b} = \rho \dot{\vec{v}}$	Linear Momentum Balance Cauchy's Equation of motion	3 eqns.	PDE
$\underline{\underline{\sigma}} = \underline{\underline{\sigma}}^T$	Angular Momentum Balance Symmetry of Cauchy stress tensor	3 eqns.	ALG
$\rho \dot{u} = \underline{\underline{\sigma}} : \underline{\underline{d}} + \rho r - \vec{\nabla} \cdot \vec{q}$	Energy Balance First Law of Thermodynamics	1 eqn.	PDE
$-\rho(\dot{u} - \theta \dot{s}) + \underline{\underline{\sigma}} : \underline{\underline{d}} \geq 0$	Second Law of Thermodynamics		
$-\frac{1}{\rho \theta^2} \vec{q} \cdot \vec{\nabla} \theta \geq 0$	Clausius-Plank Inequality Heat Flow Inequality	2 restrictions	PDE

8 PDE and 2 restrictions

19 unknown scalars: $\rho, \vec{v}, u, \underline{\underline{\sigma}}, \vec{q}, \theta, s$

Constitutive Equations: Thermo-mechanical problem

The Constitutive Equations:

$\underline{\underline{\sigma}} = \underline{\underline{\sigma}}(\vec{v}, \theta, \zeta)$	Thermo-Mechanical Constitutive Equations	6 eqns.
$s = s(\vec{v}, \theta, \zeta)$	Entropy Constitutive Equation	1 eqn.
$\vec{q} = \vec{q}(\vec{v}, \theta) = -k\vec{\nabla}\theta$	Thermal Constitutive Equation Fourier's Law of Conduction	3 eqns.
$u = u(\rho, \vec{v}, \theta, \zeta)$	Heat State Equation	(1+p) eqns.
$F_i(\rho, \theta, \zeta); \quad i \in \{1, 2, \dots, p\}$	Kinetic State Equation	

Constitutive Equations

The constitutive equations along with governing equations can be used to solve the problem. In fluid mechanics, they can be grouped as:

- ▶ Thermo-mechanical constitutive equations:

$$\underline{\underline{\sigma}} = -p\underline{\underline{1}} + \underline{\underline{f}}(\underline{\underline{d}}, \rho, \theta)$$
$$\sigma_{ij} = -p\delta_{ij} + f_{ij}(\underline{\underline{d}}, \rho, \theta); \quad i, j \in \{1, 2, 3\}$$

- ▶ Caloric equation of state

$$u = g(\rho, \theta)$$

- ▶ Entropy constitutive equation

$$s = s(\underline{\underline{d}}, \rho, \theta)$$

- ▶ Fourier's Law:

$$\vec{q} = -k\vec{\nabla}\theta$$
$$q_i = -k\frac{\partial\theta}{\partial x_i} \quad i, j \in \{1, 2, 3\}$$

- ▶ Kinetic equation of state:

$$F(\rho, p, \theta) = 0$$

Viscous Fluid Models

General form of the thermo-mechanical constitutive equations:

$$\underline{\underline{\boldsymbol{\sigma}}} = -p\underline{\underline{\mathbf{1}}} + \underline{\underline{\mathbf{f}}}(\underline{\underline{\mathbf{d}}}, \rho, \theta)$$
$$\sigma_{ij} = -p\delta_{ij} + f_{ij}(\underline{\underline{\mathbf{d}}}, \rho, \theta); \quad i, j \in \{1, 2, 3\}$$

Fluids are classified as:

- ▶ Perfect fluid (no viscosity), $\underline{\underline{\mathbf{f}}}(\underline{\underline{\mathbf{d}}}, \rho, \theta) = 0 \Rightarrow \underline{\underline{\boldsymbol{\sigma}}} = -p\underline{\underline{\mathbf{1}}}$.
- ▶ Newtonian fluid (viscous), $\underline{\underline{\mathbf{f}}}(\underline{\underline{\mathbf{d}}}, \rho, \theta)$ is a linear function of strain rate.
- ▶ Stokesian fluid (viscous), $\underline{\underline{\mathbf{f}}}(\underline{\underline{\mathbf{d}}}, \rho, \theta)$ is a non-linear function of its arguments, [1].

Note that $\underline{\underline{\mathbf{d}}} = \frac{1}{2} \left(\vec{\mathbf{v}} \otimes \vec{\nabla} + \vec{\nabla} \otimes \vec{\mathbf{v}} \right)$ is the symmetric part of the velocity gradient tensor $\underline{\underline{\mathbf{d}}}$.

Constitutive Equations: Newtonian Fluids

Constitutive equations:

$$\underline{\underline{\sigma}} = -p\underline{\underline{1}} + \underline{\underline{C}} : \underline{\underline{d}}$$
$$\sigma_{ij} = -p\delta_{ij} + C_{ijkl}d_{kl}; \quad i, j \in \{1, 2, 3\}$$

where $\underline{\underline{D}}$ is a 4th order constant VISCOUS constitutive tensor.

For an isotropic material the viscous constitutive tensor becomes:

$$\underline{\underline{C}} = \lambda \underline{\underline{1}} \otimes \underline{\underline{1}} + 2\mu \underline{\underline{I}}$$
$$C_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk})$$

Finally in the constitutive equation:

$$\underline{\underline{\sigma}} = -p\underline{\underline{1}} + \lambda \text{Tr}(\underline{\underline{d}})\underline{\underline{1}} + 2\mu \underline{\underline{d}}$$
$$\sigma_{ij} = -p\delta_{ij} + \lambda d_{ll}\delta_{ij} + \mu d_{ij}; \quad i, j \in \{1, 2, 3\}$$

Note that λ and μ can vary with ρ and θ .

Dissipative and Recoverable Parts of Stress Tensor

The mechanical energy balance:

$$\underbrace{P_e(t)}_{\text{mechanical power}} = \int \int \int_V \rho \vec{b} \cdot \vec{v} dV + \int \int_{\partial V} \vec{t} \cdot \vec{v} dS = \underbrace{\frac{d}{dt} \int \int \int_V \frac{1}{2} \rho v^2 dV}_{\text{kinetic energy}} + \underbrace{\int \int \int_V \underline{\underline{\sigma}} : \underline{\underline{d}} dV}_{\text{stress power}}$$

Then:

$$P_e(t) = \frac{d}{dt} K(t) + P_\sigma$$

Note that a rigid body will have zero stress power.

The stress power is mechanical in the system, which is not spent in changing the kinetic energy, [1].

Dissipative and Recoverable Stress

Knowing that:

$$\int \int \int_V \underline{\underline{\sigma}} : \underline{\underline{d}} \, dV; \quad \underline{\underline{d}} = \frac{1}{3} \text{Tr}(\underline{\underline{d}}) \underline{\underline{1}} + \underline{\underline{d}}_{dev}; \quad \underline{\underline{\sigma}} = -\bar{p} \underline{\underline{1}} + \underline{\underline{\sigma}}_{dev}; \quad \bar{p} = -\frac{1}{3} \text{Tr}(\underline{\underline{\sigma}})$$

Then:

$$\begin{aligned} \underline{\underline{\sigma}} : \underline{\underline{d}} &= \left(-\bar{p} \underline{\underline{1}} + \underline{\underline{\sigma}}_{dev} \right) : \left(\frac{1}{3} \text{Tr}(\underline{\underline{d}}) \underline{\underline{1}} + \underline{\underline{d}}_{dev} \right) = \\ &= -\frac{1}{3} \bar{p} \text{Tr}(\underline{\underline{d}}) \underbrace{\underline{\underline{1}} : \underline{\underline{1}}}_{=3} + \underline{\underline{\sigma}}_{dev} : \underline{\underline{d}}_{dev} - \bar{p} \underbrace{\underline{\underline{1}} : \underline{\underline{d}}_{dev}}_{=\text{Tr}(\underline{\underline{d}}_{dev})=0} + \frac{1}{3} \text{Tr}(\underline{\underline{d}}) \underbrace{\underline{\underline{\sigma}}_{dev} : \underline{\underline{1}}}_{\text{Tr}(\underline{\underline{\sigma}}_{dev})=0} = -\bar{p} \text{Tr}(\underline{\underline{d}}) + \underline{\underline{\sigma}}_{dev} : \underline{\underline{d}}_{dev} \end{aligned}$$

Noting that $\underline{\underline{\sigma}}_{dev} = 2\mu \underline{\underline{d}}_{dev}$ and $\bar{p} = p - \kappa \text{Tr}(\underline{\underline{d}})$, we have:

$$\underline{\underline{\sigma}} : \underline{\underline{d}} = \underbrace{-p \text{Tr}(\underline{\underline{d}})}_{\text{Recoverable Power } W_R} + \underbrace{\kappa \text{Tr}^2(\underline{\underline{d}}) + 2\mu \underline{\underline{d}}_{dev} : \underline{\underline{d}}_{dev}}_{\text{Dissipative Power } 2W_D}$$

where $\kappa = \lambda + \frac{2}{3}\mu$ is the bulk viscosity.

Dissipative and Recoverable Parts of Stress Tensor

In the Cauchy stress tensor the dissipative and recoverable parts can be split as follows:

$$\underline{\underline{\sigma}} = \underbrace{-p\underline{\underline{1}}}_{\text{Recoverable Part } \underline{\underline{\sigma}}_R} + \underbrace{\lambda \text{Tr}(\underline{\underline{d}})\underline{\underline{1}} + 2\mu\underline{\underline{d}}}_{\text{Dissipative Part } \underline{\underline{\sigma}}_D}$$

More specifically, the recoverable and the dissipative part can be written:

$$W_R = -p \text{Tr}(\underline{\underline{d}}) = -p\underline{\underline{1}} : \underline{\underline{d}} = \underline{\underline{\sigma}}_R : \underline{\underline{d}}$$
$$2W_D = \kappa \text{Tr}^2(\underline{\underline{d}}) + 2\mu\underline{\underline{d}}_{dev} : \underline{\underline{d}}_{dev} = \underline{\underline{\sigma}}_D : \underline{\underline{d}}$$

Note that for incompressible fluid: $W_R = -p \text{Tr}(\underline{\underline{d}}) = 0$.

Due to second principle of thermodynamics:

- ▶ the dissipative part $2W_D \geq 0$,
- ▶ the bulk viscosity $\kappa = \lambda + \frac{2}{3}\mu \geq 0$
- ▶ the shear viscosity $\mu \geq 0$.

Fluid Mechanics

Governing Equations

$\dot{\rho} + \rho \vec{\nabla} \cdot \vec{v} = 0$	Conservation of Mass Continuity Equation	1 eqn.	PDE
$\vec{\nabla} \cdot \underline{\underline{\sigma}} + \rho \vec{b} = \rho \dot{\vec{v}}$	Linear Momentum Balance Cauchy's Equation of motion	3 eqns.	PDE
$\underline{\underline{\sigma}} = \underline{\underline{\sigma}}^T$	Angular Momentum Balance Symmetry of Cauchy stress tensor	3 eqns.	ALG
$\rho \dot{u} = \underline{\underline{\sigma}} : \underline{\underline{d}} + \rho r - \vec{\nabla} \cdot \vec{q}$	Energy Balance First Law of Thermodynamics	1 eqn.	PDE
$-\rho(\dot{u} - \theta \dot{s}) + \underline{\underline{\sigma}} : \underline{\underline{d}} \geq 0$	Second Law of Thermodynamics		
$-\frac{1}{\rho \theta^2} \vec{q} \cdot \vec{\nabla} \theta \geq 0$	Clausius-Plank Inequality Heat Flow Inequality	2 restrictions	PDE

8 Eqns and 2 restrictions

Constitutive Equations: Newtonian Fluids

The 12 missing equations:

$\underline{\underline{\sigma}} = -p\underline{\underline{1}} + \lambda Tr(\underline{\underline{d}})\underline{\underline{1}} + 2\mu\underline{\underline{d}}$	Thermo-Mechanical Constitutive Equations	6 eqns.
$s = s(\vec{v}, \theta, \zeta)$	Entropy Constitutive Equation	1 eqn.
$\vec{q} = \vec{q}(\vec{v}, \theta) = -k\vec{\nabla}\theta$	Thermal Constitutive Equation Fourier's Law of Conduction	3 eqns.
$u = u(\rho, \theta, \zeta)$ $F(\rho, p, \theta) = 0$	Caloric State Equation Kinetic State Equation	2 eqns.

In total: 20 Eqns. with 20 unknowns:

$$\rho \rightarrow 1, \vec{v} \rightarrow 3, \underline{\underline{\sigma}} \rightarrow 9, u \rightarrow 1, \vec{q} \rightarrow 3, \theta \rightarrow 1, s \rightarrow 1, p \rightarrow 1$$

Constitutive Equations: Barotropic Fluids

A barotropic fluid is defined by the kinetic state equation, not depend on temperature θ :

$$F(\rho, p) = 0 \Rightarrow \rho = \rho(p)$$

The uncoupled problem becomes:

$\dot{\rho} + \rho \vec{\nabla} \cdot \vec{v} = 0$	Conservation of Mass Continuity Equation	1 eqn.
$\vec{\nabla} \cdot \underline{\underline{\sigma}} + \rho \vec{b} = \rho \dot{\vec{v}}$	Linear Momentum Balance Cauchy's Equation of motion	3 eqns.
$\underline{\underline{\sigma}} = -p \underline{\underline{1}} + \lambda Tr(\underline{\underline{d}}) \underline{\underline{1}} + 2\mu \underline{\underline{d}}$	Thermo-Mechanical Constitutive Equations	6 eqns.
$\rho = \rho(p)$	Kinetic State Equation	1 eqn.
11 scalar unknowns: $\rho(1), \vec{v}(3), \underline{\underline{\sigma}}(6), p(1)$		

Hydrostatics

Hydrostatic stress state

- Uniform velocity:

$$\vec{v}(\vec{x}, t) \equiv \vec{v}(\vec{x}) \Rightarrow \vec{\nabla} \vec{v} = \vec{\nabla} \otimes \vec{v} = \vec{v} \otimes \vec{\nabla} = \underline{\underline{\underline{0}}}$$

$$\underline{\underline{\underline{d}}} = \frac{1}{2} \left(\vec{v} \otimes \vec{\nabla} + \vec{\nabla} \otimes \vec{v} \right) = \underline{\underline{\underline{0}}}$$

Therefore, the hydrostatic stress state can be defined as:

$$\underline{\underline{\underline{\sigma}}} = -p \underline{\underline{\underline{1}}} + \lambda \underbrace{Tr(\underline{\underline{\underline{d}}})}_{=0} \underline{\underline{\underline{1}}} + 2\mu \underbrace{\underline{\underline{\underline{d}}}}_{=\underline{\underline{\underline{0}}}} \Rightarrow \underline{\underline{\underline{\sigma}}} = -p \underline{\underline{\underline{1}}} \Rightarrow \bar{p} = p$$

- Uniform and stationary velocity $\vec{v}(\vec{x}, t) = \text{constant}$:

$$\vec{a} = \frac{d\vec{v}}{dt} = \frac{\partial \vec{v}}{\partial t} + \vec{v} \cdot \vec{\nabla} \vec{v} = \vec{0}$$

There the hydrostatic case can be derived as:

$$\underline{\underline{\underline{\sigma}}} = -p_0 \underline{\underline{\underline{1}}} \Rightarrow Tr(\underline{\underline{\underline{\sigma}}}) = -3p_0 \Rightarrow \bar{p} = p = p_0$$

- Fluid at rest $\vec{v}(\vec{x}, t) = \text{constant} = \vec{0}$. Hydrostatic (from Greek and means water at rest).

Hydrostatic Problem

Hydrostatic problem $\vec{v}(\vec{x}, t) = \text{constant}$ is defined as:

$\dot{\rho} + \rho \vec{\nabla} \cdot \vec{v} = 0 \Rightarrow \rho(\vec{X}, t) = \rho_0(\vec{X})$	Conservation of Mass Continuity Equation	1 eqn.
$\vec{\nabla} \cdot \underline{\underline{\sigma}} + \rho \vec{b} = \rho \dot{\vec{v}} \Rightarrow \vec{\nabla} \cdot \underline{\underline{\sigma}} + \rho \vec{b} = \vec{0}$	Linear Momentum Balance Cauchy's Equation of motion	3 eqns.
$\underline{\underline{\sigma}} = -p \underline{\underline{1}} + \lambda \text{Tr}(\underline{\underline{d}}) \underline{\underline{1}} + 2\mu \underline{\underline{d}} \Rightarrow \underline{\underline{\sigma}} = -p \underline{\underline{1}}$	Thermo-Mechanical Constitutive Equations	6 eqns.

Introducing the constitutive equation in the Cauchy equation, we get the fundamental equation of hydrostatics:

$$\underline{\underline{\sigma}} = -p \underline{\underline{1}} \Rightarrow \vec{\nabla} \cdot (-p \underline{\underline{1}}) = -\vec{\nabla} p_0 \rightarrow \begin{cases} -\vec{\nabla} p_0 + \rho_0 \vec{b} = \vec{0} \\ \frac{\partial p_0}{\partial x_i} + \rho_0 b_i = 0; \quad i \in \{1, 2, 3\} \end{cases}$$

We know the ρ_0 we find the pressure p from above equation, then we define the stress $\underline{\underline{\sigma}}$

Barotropic Perfect Fluids

Barotropic Perfect Fluids

A perfect fluid is a Newtonian fluid without viscosity ($\mu = \lambda = 0$):

$$\underline{\underline{\sigma}} = -p\underline{\underline{1}} + \lambda \text{Tr}(\underline{\underline{d}})\underline{\underline{1}} + 2\mu\underline{\underline{d}} \Rightarrow \underline{\underline{\sigma}} = -p\underline{\underline{1}} \Rightarrow \underline{\underline{\sigma}} = -p\underline{\underline{1}}$$

at hydrostatic stress state. Therefore:

$$\begin{aligned}\vec{\nabla} \cdot \underline{\underline{\sigma}} &= -\vec{\nabla} p \\ \underline{\underline{\sigma}} : \underline{\underline{d}} &= -p\underline{\underline{1}} : \underline{\underline{d}} = -p \text{Tr}(\underline{\underline{d}})\end{aligned}$$

In a barotropic fluid temperature does not affect the kinetic state equation:

$$F(\rho, p) = 0 \Rightarrow \rho = \rho(p)$$

Note that most liquids can be assumed as barotropic (but not perfect). Some gases under certain circumstances.

Barotropic Perfect Fluids: Field Equations

Hydrostatic problem $\vec{v}(\vec{x}, t) = \text{constant}$ is defined as:

$\dot{\rho} + \rho \vec{\nabla} \cdot \vec{v} = 0$	Conservation of Mass Continuity Equation	1 eqn.
$\vec{\nabla} \cdot \underline{\underline{\sigma}} + \rho \vec{b} = \rho \dot{\vec{v}} \Rightarrow -\vec{\nabla} p + \rho \vec{b} = \rho \dot{\vec{v}}$	Linear Momentum Balance Euler's Equation	3 eqns.
$F(\rho, p) = 0 \Rightarrow \rho = \rho(p)$	Kinetic State Equation	1 eqn.

There are 5 scalar quantities unknowns: ρ, \vec{v}, p

Bernoilli's Trinomial

Consider a barotropic fluid under potential body forces:

$$\phi(\vec{x}, t) = gz \Rightarrow -\vec{\nabla}\phi(\vec{x}, t) = -\left[\frac{\partial\phi}{\partial x} \quad \frac{\partial\phi}{\partial y} \quad \frac{\partial\phi}{\partial z}\right]^T = \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix}$$

The following lemmas hold:

- ▶ Lemma 1. For barotropic fluids there exist a function $P(\vec{x}, t) = \hat{P}(p(\vec{x}, t))$ such that.

$$\vec{\nabla}p = \rho\vec{\nabla}P$$

- ▶ Lemma 2. The convective term of the acceleration can be expressed as:

$$\vec{v} \cdot \vec{\nabla}\vec{v} = 2\vec{\omega} \times \vec{v} + \vec{\nabla}\left(\frac{1}{2}v^2\right)$$

where $2\vec{\omega} = \vec{\nabla} \times \vec{v}$ is the vorticity vector.

Bernoulli's Trinomial

Using the Euler's equation:

$$-\vec{\nabla} p + \rho \vec{b} = \rho \vec{v} \rightarrow -\frac{1}{\rho} \vec{\nabla} p + \vec{b} = \frac{d\vec{v}}{dt}$$

$$\frac{1}{\rho} \vec{\nabla} p = \vec{\nabla} P; \vec{b} = \vec{\nabla} \phi$$

$$\vec{v} \vec{\nabla} \cdot \vec{v}$$

Combining the equations:

$$-\vec{\nabla} P - \vec{\nabla} \phi = \frac{\partial \vec{v}}{\partial t} + 2\vec{\omega} \times \vec{v} + \vec{\nabla} \left(\frac{1}{2} v^2 \right)$$

Finally we can derive the equation of motion for a barotropic perfect fluid:

$$-\vec{\nabla} \underbrace{\left[P + \phi + \frac{1}{2} v^2 \right]}_{\text{Bernoulli's Trinomial}} = \frac{\partial \vec{v}}{\partial t} + 2\vec{\omega} \times \vec{v}$$

Newtonian Viscous Fluids

Governing Equations

The general fluid mechanics problem:

$\dot{\rho} + \rho \vec{\nabla} \cdot \vec{v} = 0$	Conservation of Mass Continuity Equation	1 eqn.
$\vec{\nabla} \cdot \underline{\underline{\sigma}} + \rho \vec{b} = \rho \dot{\vec{v}}$	Linear Momentum Balance Cauchy's Equation of motion	3 eqns.
$\rho \dot{u} = \underline{\underline{\sigma}} : \underline{\underline{d}} + \rho r - \vec{\nabla} \cdot \vec{q}$	Energy Balance First law of Thermodynamics	1 eqns.
$\underline{\underline{\sigma}} = -p \underline{\underline{1}} + \lambda Tr(\underline{\underline{d}}) \underline{\underline{1}} + 2\mu \underline{\underline{d}}$	Mechanical Constitutive Equations	6 eqns.
$s = s(\underline{\underline{d}}, \theta, \rho)$	Entropy Constitutive equation	1 eqn.
$\vec{q} = -K \vec{\nabla} \theta$	Thermal constitutive equation. Fourier Law of conduction	3 eqns.
$u = u(\rho, \theta) \quad F(\rho, \theta, p) = 0$	Caloric and Kinetic State	2 eqns.

17 scalar unknowns: $\rho(1), \vec{v}(3), \underline{\underline{\sigma}}(6), u(1), \vec{q}(3), \theta(1), s(1), p(1)$

Navier-Stokes equations

Consider the lemmas:

► Lemma 1:

$$\vec{\nabla} \cdot \underline{\underline{d}} = \frac{1}{2} \Delta \vec{v} + \frac{1}{2} \vec{\nabla} (\vec{\nabla} \cdot \vec{v})$$

where $\underline{\underline{d}}$ is the deformation rate tensor.

► Lemma 2:

$$\vec{\nabla} \cdot (a \underline{\underline{1}}) = \vec{\nabla} a$$

where $a(\vec{x}, t)$ is a scalar function

Introducing the constitutive equation of stress in the term of Cauchy's equation ($Tr(\underline{\underline{d}}) = \vec{\nabla} \cdot \vec{v}$):

$$\vec{\nabla} \cdot \underline{\underline{\sigma}} = \vec{\nabla} \cdot (-p \underline{\underline{1}} + \lambda Tr(\underline{\underline{d}}) \underline{\underline{1}} + 2\mu \underline{\underline{d}}) = -\vec{\nabla} p + \lambda \underbrace{\vec{\nabla} (Tr(\underline{\underline{d}}))}_{\vec{\nabla} (\vec{\nabla} \cdot \vec{v})} + \mu \Delta \vec{v} + \mu \vec{\nabla} (\vec{\nabla} \cdot \vec{v})$$

Navier-Stokes equations

The linear momentum balance equation can be arranged as follows:

$$\vec{\nabla} \cdot \underline{\underline{\sigma}} + \rho \vec{b} = \rho \dot{\vec{v}} \Rightarrow -\vec{\nabla} p + (\lambda + \mu) \vec{\nabla} (\vec{\nabla} \cdot \vec{v}) + \mu \Delta \vec{v} + \rho \vec{b} = \rho \frac{d\vec{v}}{dt}$$

Finally the NAVIER-STOKES equations can be written as:

$$\begin{aligned} & -\vec{\nabla} p + (\lambda + \mu) \vec{\nabla} (\vec{\nabla} \cdot \vec{v}) + \mu \Delta \vec{v} + \rho \vec{b} = \rho \frac{d\vec{v}}{dt} \\ & -\frac{\partial p}{\partial x_i} + (\lambda + \mu) \frac{\partial^2 v_j}{\partial x_i \partial x_j} + \mu \frac{\partial^2 v_i}{\partial x_i \partial x_j} + \rho b_i = \rho \frac{dv_i}{dt}, \quad 1, j \in \{1, 2, 3\} \end{aligned}$$

The Navier-Stokes equations are the equation of motion (balance of linear momentum) written in terms of velocities.

There are 4 unknowns: $\vec{v}(3)$, $p(1)$ and 3 equations.

For incompressible fluids the $(\vec{\nabla} \cdot \vec{v}) = 0$ and $\underline{\underline{\sigma}} = -p\underline{\underline{1}} + 2\mu\underline{\underline{d}}$

Energy Equations

The energy balance equation can be given as, [1]:

$$\rho \frac{du}{dt} = -p \vec{\nabla} \cdot \vec{v} + \rho r + \vec{\nabla} \cdot (K \vec{\nabla} \theta) + \underbrace{\kappa \text{Tr}^2(\underline{\underline{d}}) + 2\mu \underline{\underline{d}}_{dev} : \underline{\underline{d}}_{dev}}_{\text{Dissipative Power } 2W_D}$$

$$\rho \frac{du}{dt} = -p \frac{\partial v_i}{\partial x_i} + \rho r + \frac{\partial}{\partial x_i} \left(K \frac{\partial \theta}{\partial x_i} \right) + \kappa \left(\frac{\partial v_i}{\partial x_i} \right)^2 + 2\mu d_{ij}^{dev} d_{ij}^{dev}; \quad i, j \in \{1, 2, 3\}$$

The energy equation is just the energy balance in terms of velocity and pressure.

References I



X. Oliver and C. Agelet de Saracibar.

Continuum Mechanics for Engineers. Theory and Problems.
2017.