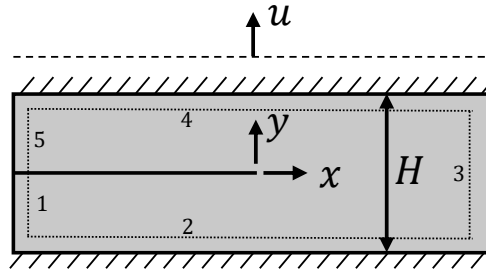


**A? Question**

An infinite strip of height  $H$  with a semi-infinite crack is rigidly clamped along its top and bottom faces, see below. Determine the J-integral for mode I loading, where top edge is moved upward by a prescribed displacement  $u$ . Assume that the material is linear elastic, isotropic, and under plane stress conditions.

**A! Solution**

In this case, the J-integral can be expressed as the sum of five segments labelled on the figure above:

$$J = J_1 + J_2 + J_3 + J_4 + J_5,$$

where each term is given by:

$$J = \int_{\Gamma} \left( w dy - t_i \frac{\partial u_i}{\partial x} ds \right).$$

Over segments 1 and 5, we have no deformations,  $u_x = 0$  and  $u_y$  is a constant. This implies:

$$w = 0 \quad \text{and} \quad \frac{\partial u_i}{\partial x} = 0 \quad \implies \quad J_1 = J_5 = 0.$$

Next, over segments 2 and 4 we have  $dy = 0$ ,  $u_x = 0$  (the top and bottom edges are clamped and cannot contract). Also,  $u_y = 0$  for the bottom edge, whereas  $u_y = u$  along the top edge. This implies:

$$dy = 0 \quad \text{and} \quad \frac{\partial u_i}{\partial x} = 0 \quad \implies \quad J_2 = J_4 = 0$$

Finally, along segment 3, we have  $dy \neq 0$  and  $w \neq 0$ , whereas the displacement  $u_x = 0$  and  $u_y = f(y)$ , which implies  $\frac{\partial u_i}{\partial x} = 0$ . Therefore, we conclude that:

$$J = J_3 = \int_{\Gamma} \left( w dy - t_i \frac{\partial u_i}{\partial x} ds \right) = \int_{-H/2}^{H/2} w dy$$

For a linear elastic material the strain energy density  $w = \frac{1}{2} \sigma_{ij} \epsilon_{ij}$ . The stress and strain components are:

$$\begin{array}{llll} \sigma_{xx} \neq 0 & \sigma_{yy} \neq 0 & \sigma_{xy} = 0 & \sigma_{zz} = 0 \\ \epsilon_{xx} = 0 & \epsilon_{yy} = \frac{u}{H} & \epsilon_{xy} = 0 & \epsilon_{zz} \neq 0 \end{array}$$

The stresses  $\sigma_{xx}$  and  $\sigma_{yy}$  can be obtained using Hooke's law. For a linear elastic isotropic material under plane stress, Hooke's law is:

$$\begin{bmatrix} \sigma_{xx} \\ \sigma_{yy} \\ \sigma_{xy} \end{bmatrix} = \frac{E}{1-\nu^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & \frac{1-\nu}{2} \end{bmatrix} \begin{bmatrix} \epsilon_{xx} \\ \epsilon_{yy} \\ \epsilon_{xy} \end{bmatrix}$$

Substituting in the values above, we find that:

$$\sigma_{yy} = \frac{E}{1-\nu^2} \epsilon_{yy} = \frac{Eu}{H(1-\nu^2)}$$

With this, we can compute the strain energy density  $w$ :

$$w = \frac{1}{2} \sigma_{ij} \epsilon_{ij} = \frac{1}{2} \sigma_{yy} \epsilon_{yy} = \frac{Eu^2}{2(1-\nu^2)H^2}$$

Finally, we can compute the J-integral using the above equation:

$$\begin{aligned} J &= \int_{-H/2}^{H/2} w dy \\ &= \int_{-H/2}^{H/2} \frac{Eu^2}{2(1-\nu^2)H^2} dy \\ &= \frac{Eu^2}{2(1-\nu^2)H^2} [y]_{-H/2}^{H/2} \\ &= \frac{Eu^2}{2(1-\nu^2)H} \end{aligned}$$

Since the material is linear elastic,  $J = G$ . From this, we can find the stress intensity factor  $K_I$  using:

$$K_I = \sqrt{EG} = \sqrt{EJ} = \sqrt{\frac{E^2 u^2}{2(1-\nu^2)H}} = \sqrt{\frac{1}{2(1-\nu^2)H}} Eu$$

This is equal to the formula given in the datasheet.