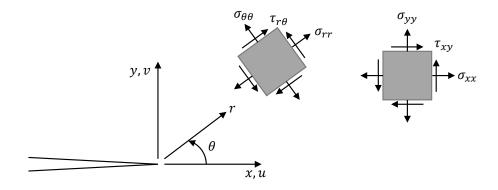
1 Crack tip stress field



1.1 Mode I

$$\sigma_{yy} = \frac{K_I}{\sqrt{2\pi r}} \cos \frac{\theta}{2} \left(1 + \sin \frac{\theta}{2} \sin \frac{3\theta}{2} \right) \qquad \sigma_{rr} = \frac{K_I}{\sqrt{2\pi r}} \left(\frac{5}{4} \cos \frac{\theta}{2} - \frac{1}{4} \cos \frac{3\theta}{2} \right)$$

$$\sigma_{xx} = \frac{K_I}{\sqrt{2\pi r}} \cos \frac{\theta}{2} \left(1 - \sin \frac{\theta}{2} \sin \frac{3\theta}{2} \right) \qquad \sigma_{\theta\theta} = \frac{K_I}{\sqrt{2\pi r}} \left(\frac{3}{4} \cos \frac{\theta}{2} + \frac{1}{4} \cos \frac{3\theta}{2} \right)$$

$$\tau_{xy} = \frac{K_I}{\sqrt{2\pi r}} \cos \frac{\theta}{2} \sin \frac{\theta}{2} \cos \frac{3\theta}{2} \qquad \tau_{r\theta} = \frac{K_I}{\sqrt{2\pi r}} \left(\frac{1}{4} \sin \frac{\theta}{2} + \frac{1}{4} \sin \frac{3\theta}{2} \right)$$

$$u = \begin{cases} \frac{K_I}{G} \sqrt{\frac{r}{2\pi}} \left(\frac{1 - \nu}{1 + \nu} + \sin^2 \frac{\theta}{2} \right) \cos \frac{\theta}{2} & \text{plane stress} \\ \frac{K_I}{G} \sqrt{\frac{r}{2\pi}} \left(1 - 2\nu + \sin^2 \frac{\theta}{2} \right) \cos \frac{\theta}{2} & \text{plane stress} \end{cases}$$

$$v = \begin{cases} \frac{K_I}{G} \sqrt{\frac{r}{2\pi}} \left(\frac{2}{1 + \nu} - \cos^2 \frac{\theta}{2} \right) \sin \frac{\theta}{2} & \text{plane stress} \\ \frac{K_I}{G} \sqrt{\frac{r}{2\pi}} \left(2 - 2\nu - \cos^2 \frac{\theta}{2} \right) \sin \frac{\theta}{2} & \text{plane strain} \end{cases}$$

$$w = 0$$

1.2 Mode II

$$\sigma_{yy} = \frac{K_{II}}{\sqrt{2\pi r}} \cos \frac{\theta}{2} \sin \frac{\theta}{2} \cos \frac{3\theta}{2}$$

$$\sigma_{rr} = \frac{K_{II}}{\sqrt{2\pi r}} \left(-\frac{5}{4} \sin \frac{\theta}{2} + \frac{3}{4} \sin \frac{3\theta}{2} \right)$$

$$\sigma_{xx} = -\frac{K_{II}}{\sqrt{2\pi r}} \sin \frac{\theta}{2} \left(2 + \cos \frac{\theta}{2} \cos \frac{3\theta}{2} \right)$$

$$\sigma_{\theta\theta} = -\frac{K_{II}}{\sqrt{2\pi r}} \left(\frac{3}{4} \sin \frac{\theta}{2} + \frac{3}{4} \sin \frac{3\theta}{2} \right)$$

$$\tau_{xy} = \frac{K_{II}}{\sqrt{2\pi r}} \cos \frac{\theta}{2} \left(1 - \sin \frac{\theta}{2} \sin \frac{3\theta}{2} \right)$$

$$\tau_{r\theta} = \frac{K_{II}}{\sqrt{2\pi r}} \left(\frac{1}{4} \cos \frac{\theta}{2} + \frac{3}{4} \cos \frac{3\theta}{2} \right)$$

$$u = \begin{cases} \frac{K_{II}}{G} \sqrt{\frac{r}{2\pi}} \left(\frac{2}{1+\nu} + \cos^2 \frac{\theta}{2} \right) \sin \frac{\theta}{2} & \text{plane stress} \\ \frac{K_{II}}{G} \sqrt{\frac{r}{2\pi}} \left(2 - 2\nu + \cos^2 \frac{\theta}{2} \right) \sin \frac{\theta}{2} & \text{plane strain} \end{cases}$$

$$v = \begin{cases} \frac{K_{II}}{G} \sqrt{\frac{r}{2\pi}} \left(\frac{\nu - 1}{1+\nu} + \sin^2 \frac{\theta}{2} \right) \cos \frac{\theta}{2} & \text{plane stress} \\ \frac{K_{II}}{G} \sqrt{\frac{r}{2\pi}} \left(2\nu - 1 + \sin^2 \frac{\theta}{2} \right) \cos \frac{\theta}{2} & \text{plane strain} \end{cases}$$

$$w = 0$$

1.3 Mode III

$$\tau_{xz} = -\frac{K_{III}}{\sqrt{2\pi r}} \sin \frac{\theta}{2}$$

$$\tau_{yz} = \frac{K_{III}}{\sqrt{2\pi r}} \cos \frac{\theta}{2}$$

$$w = \frac{K_{III}}{G} \sqrt{\frac{2r}{\pi}} \sin \frac{\theta}{2}$$

$$u = v = 0$$

$$u = v = 0$$

2 Energy release rate

$$G = \frac{P^2}{2B} \frac{dC}{da}$$

$$G = \begin{cases} \frac{1}{E} K_I^2 & \text{plane stress} \\ \frac{1 - \nu^2}{E} K_I^2 & \text{plane strain} \end{cases}$$

3 Crack tip plastic zone sizes

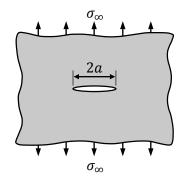
diameter,
$$d_p = \begin{cases} \frac{1}{\pi} \left(\frac{K_I}{\sigma_y} \right)^2 & \text{plane stress} \\ \frac{1}{3\pi} \left(\frac{K_I}{\sigma_y} \right)^2 & \text{plane strain} \end{cases}$$

4 Crack opening displacement

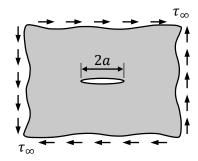
$$\delta = \begin{cases} \frac{K_I^2}{E\sigma_y} & \text{plane stress} \\ \frac{1}{2} \frac{K_I^2}{E\sigma_y} & \text{plane strain} \end{cases}$$

5 Stress intensity factors

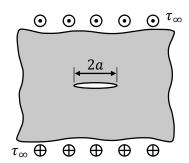
5.1 Infinitely large plates



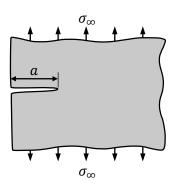
$$K_I = \sigma_{\infty} \sqrt{\pi a}$$



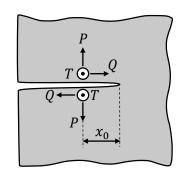
$$K_{II} = \tau_{\infty} \sqrt{\pi a}$$

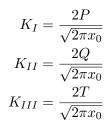


$$K_{III} = \tau_{\infty} \sqrt{\pi a}$$

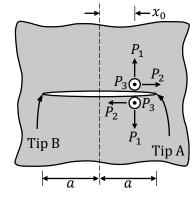


$$K_I = 1.12\sigma_{\infty}\sqrt{\pi a}$$



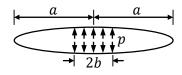


P, Q, and T are forces per unit depth (N/m).

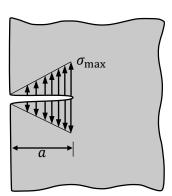


At tip A: At tip B:
$$K_{I} = \frac{P_{1}}{\sqrt{\pi a}} \sqrt{\frac{a + x_{0}}{a - x_{0}}} \qquad K_{I} = \frac{P_{1}}{\sqrt{\pi a}} \sqrt{\frac{a - x_{0}}{a + x_{0}}}$$
$$K_{II} = \frac{P_{2}}{\sqrt{\pi a}} \sqrt{\frac{a + x_{0}}{a - x_{0}}} \qquad K_{II} = \frac{P_{2}}{\sqrt{\pi a}} \sqrt{\frac{a - x_{0}}{a + x_{0}}}$$
$$K_{III} = \frac{P_{3}}{\sqrt{\pi a}} \sqrt{\frac{a + x_{0}}{a - x_{0}}} \qquad K_{III} = \frac{P_{3}}{\sqrt{\pi a}} \sqrt{\frac{a - x_{0}}{a + x_{0}}}$$

where P_i are forces per unit depth (N/m).

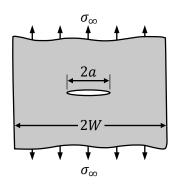


$$K_I = \frac{2pb}{\sqrt{\pi a}} \frac{a}{b} \arcsin \frac{b}{a}$$

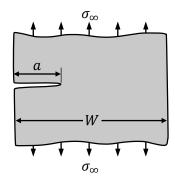


$$K_I = 0.683\sigma_{max}\sqrt{\pi a}$$

5.2 Finite width plates

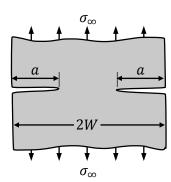


$$K_I = \sigma_{\infty} \sqrt{\pi a} \left(\frac{1 - 0.5a/W + 0.326(a/W)^2}{\sqrt{1 - a/W}} \right)$$

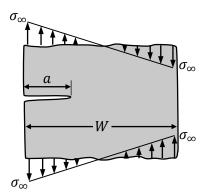


For
$$a/W < 0.7$$
:

$$K_I = \sigma_{\infty} \sqrt{\pi a} \left(1.12 - 0.23 \frac{a}{W} + 10.6 \frac{a^2}{W^2} - 21.7 \frac{a^3}{W^3} + 30.4 \frac{a^4}{W^4} \right)$$



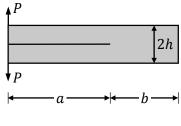
$$K_I = \sigma_{\infty} \sqrt{\pi a} \left(\frac{1.12 - 0.61a/W + 0.13(a/W)^3}{\sqrt{1 - a/W}} \right)$$



For
$$a/W < 0.7$$
:

$$K_I = \sigma_{\infty} \sqrt{\pi a} \left(1.12 - 1.39 \frac{a}{W} + 7.3 \frac{a^2}{W^2} - 13 \frac{a^3}{W^3} + 14 \frac{a^4}{W^4} \right)$$

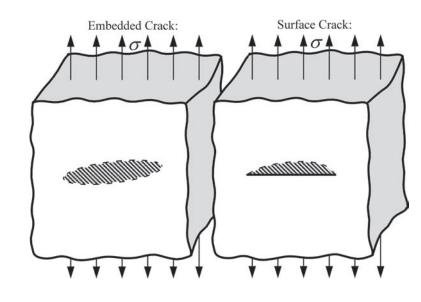
5.3 Other configurations

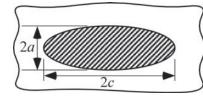


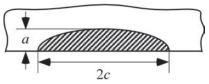
$$K_I = \frac{2\sqrt{3}}{h\sqrt{h}} \frac{Pa}{B}$$
 for $h \ll a$ and $h \ll b$

$$K_I = \sqrt{\frac{1}{2\alpha H}} Eu$$
 for $H \ll a$ and $H \ll b$

$$\alpha = \begin{cases} 1 - \nu^2 & \text{plane stress} \\ 1 - 3\nu^2 - 2\nu^3 & \text{plane strain} \end{cases}$$







where

$$K_I = \sigma \sqrt{\frac{\pi a}{Q}}$$

$$K_I = \lambda_s \sigma \sqrt{\frac{\pi a}{Q}}$$

$$Q = 1 + 1.464 \left(\frac{a}{c}\right)^{1.65}$$
 and $\lambda_s = 1.13 - 0.09 \left(\frac{a}{c}\right)$