

# Fracture mechanics

## Seminar 5: J-integral, testing, and more



Aalto-yliopisto  
Aalto-universitetet  
Aalto University

Luc St-Pierre

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# Learning outcomes

After this week, you should be able to:

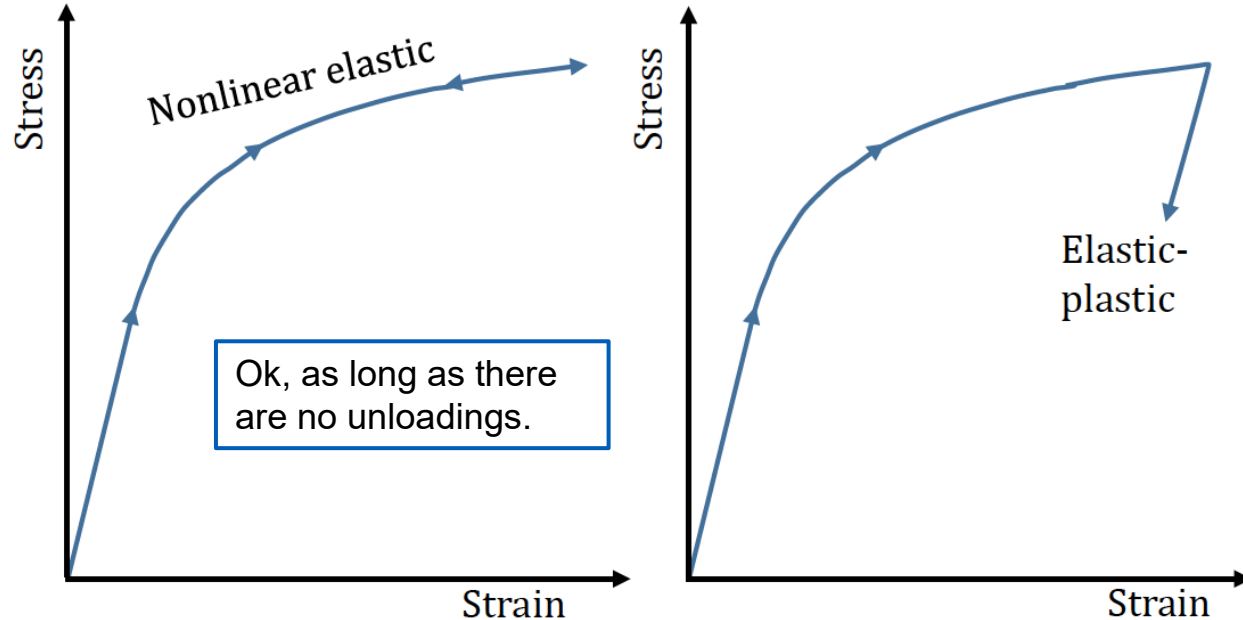
- Understand and use the  $J$ -integral,
- Explain how to measure the fracture toughness,
- Describe the main fracture mechanisms in metals and composites.

# Elastic-Plastic Fracture Mechanics

- Last week, we saw how to estimate the size of the plastic zone at the crack tip.
  - If the plastic zone size is small ( $r_p < a/10$ ), you can use LEFM.
- What can we do if the plastic zone size is large?
  - Use the  $J$ -integral.
  - Fracture will occur when:  $J = J_{Ic}$

# $J$ -integral: material model

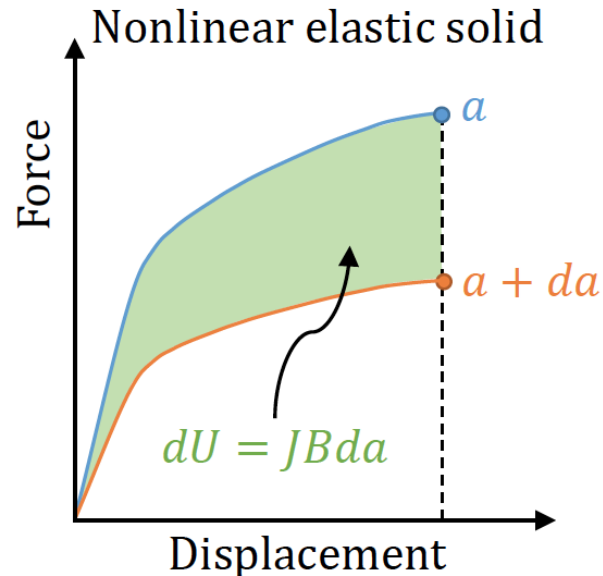
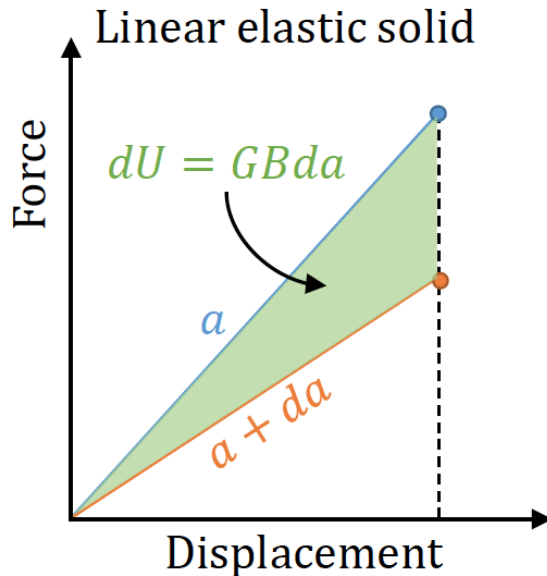
- The  $J$ -integral is developed for a non-linear elastic material.
- This is different from the elastic-plastic behavior of most metals.



# J-integral: definition

The  $J$ -integral is defined just like the energy release rate  $G$ :

$$J = -\frac{d\Pi}{dA} \quad \text{where} \quad \Pi = U - W$$



If the material is linear elastic then  $J = G$ .

# J-integral and the stress field

Assuming that the stress-strain curve of the material follows the Ramberg-Osgood equation:

$$\varepsilon = \frac{\sigma}{E} + K \left( \frac{\sigma}{E} \right)^n$$

Hutchinson, Rice and Rosengren showed that stresses at the crack tip scale as:

$$\sigma_{ij} \propto \left( \frac{J}{r} \right)^{\frac{1}{n+1}}$$

# $J$ as a contour integral

$$J = \int_{\Gamma} \left( w dy - t_i \frac{\partial u_i}{\partial x} ds \right)$$

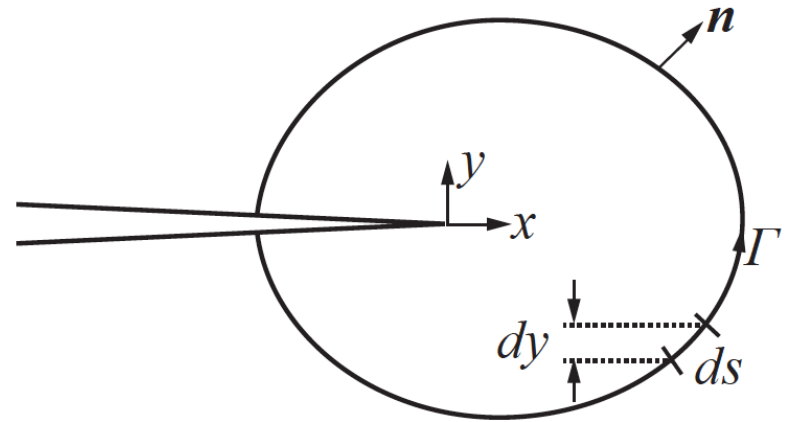
Where,

Strain energy:  $w = \int_0^{\varepsilon_{ij}} \sigma_{ij} d\varepsilon_{ij}$

Traction vector:  $t_i = \sigma_{ij} n_j$

Vector normal to contour:  $n_j$

Displacement vector:  $u_i$



The  $J$ -integral is contour independent.

The  $J$ -integral can be calculated easily in a finite element analysis.

# Example problem

$$J = \int_{\Gamma} \left( w dy - t_i \frac{\partial u_i}{\partial x} ds \right)$$

Where,

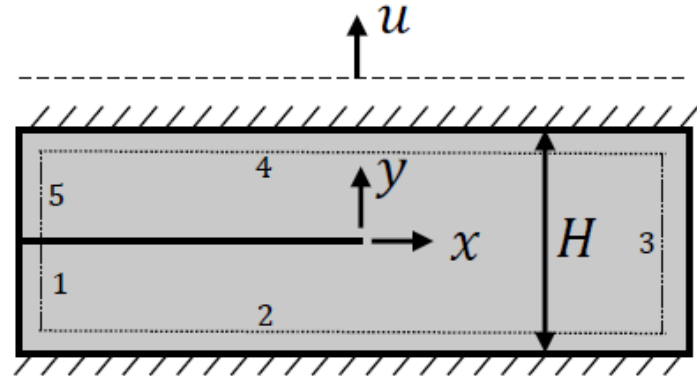
Strain energy:  $w = \int_0^{\varepsilon_{ij}} \sigma_{ij} d\varepsilon_{ij}$

Traction vector:  $t_i = \sigma_{ij} n_j$

Vector normal to contour:  $n_j$

Displacement vector:  $u_i$

Determine the  $J$ -integral for the infinitely wide strip below. Assume that the material is linear elastic, isotropic, and under plane stress.



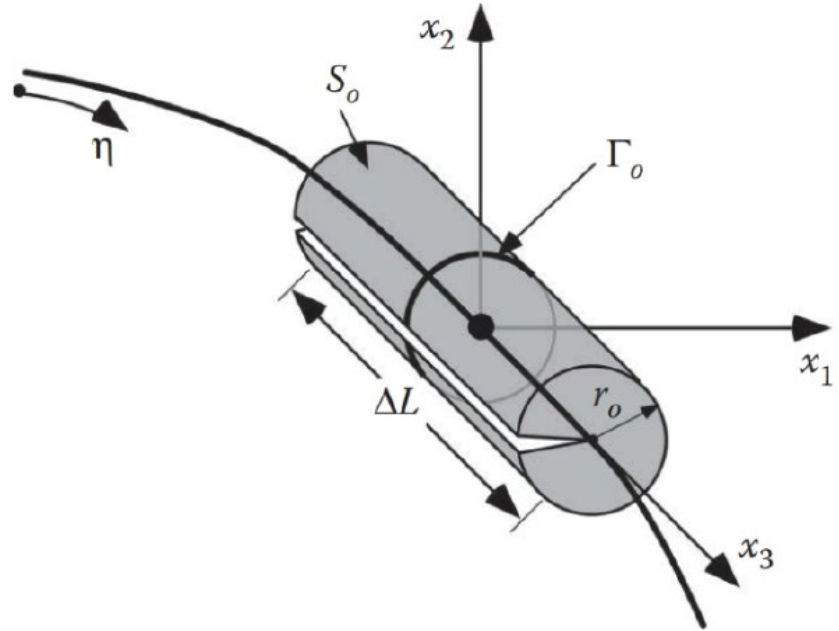


# Computational implementation

# Contour integral

Most Finite Element packages can compute the  $J$ -integral.

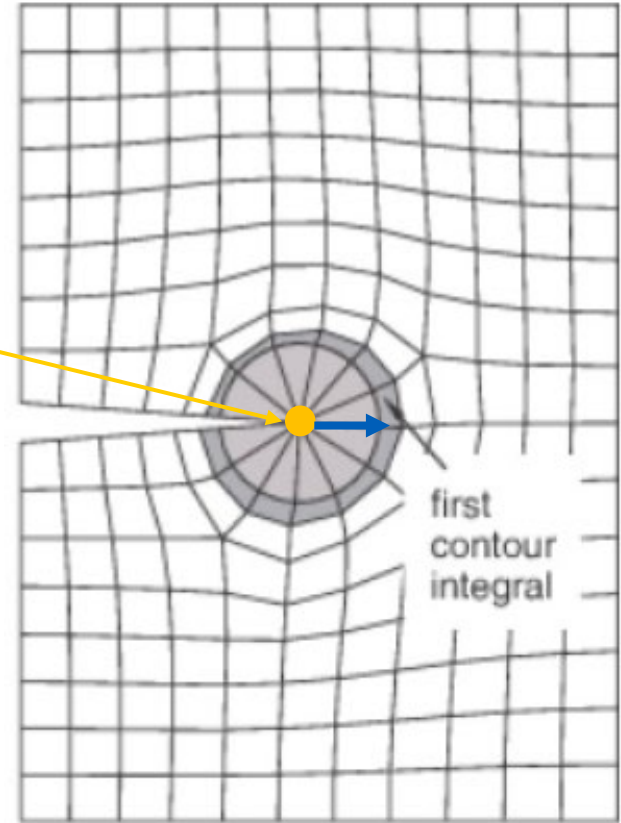
- Its definition has been extended to 3D cracks.
- The software may be able to convert  $J$  to  $K_I, K_{II}, K_{III}$ .



# Contour integral

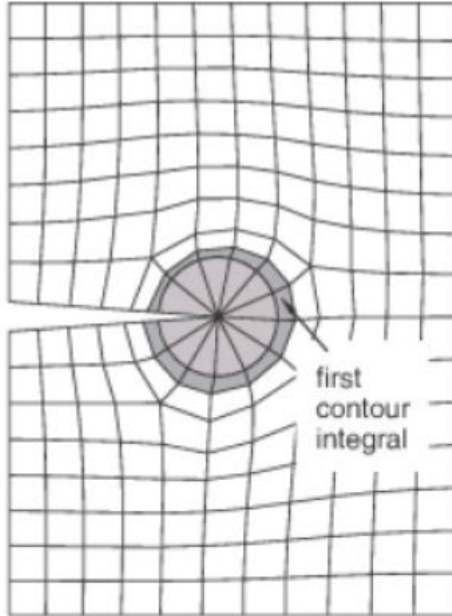
To compute the contour integral, you need to provide:

1. A crack tip (2D) or crack front (3D),
2. The direction of crack propagation (shown here in **blue**),
3. The number of contours.

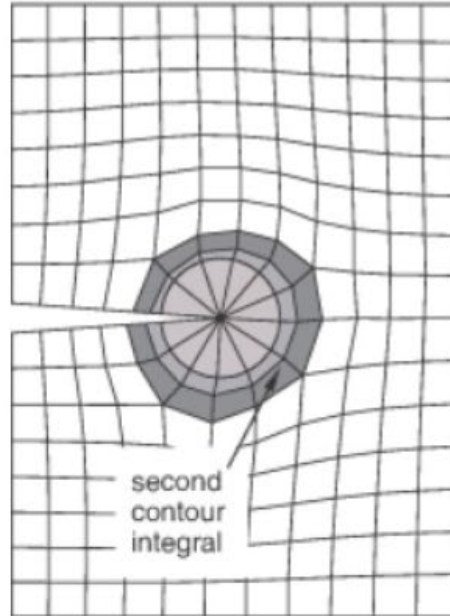


# Number of contours

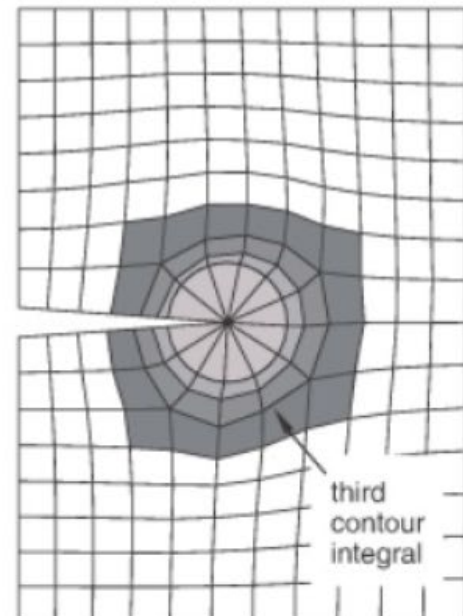
1 contour



2 contours



3 contours



# Contour integral

- The  $J$ -integral should converge to a certain value after a few contours.
  - How many contours? This is highly dependent on the mesh size and on the problem.
- **Warning:** results may diverge if you request more contours than there are elements!

# Fracture testing

# Fracture testing

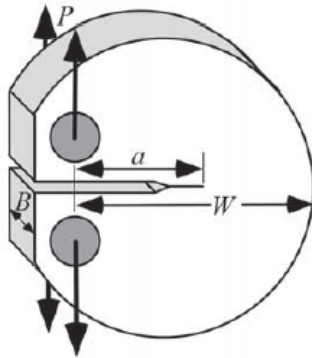
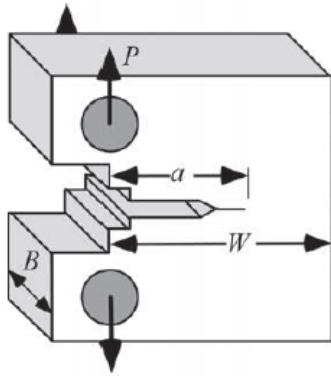
Measuring the fracture toughness is complex. Consult the relevant standard, e.g. ASTM E1820.

There are two testing methods:

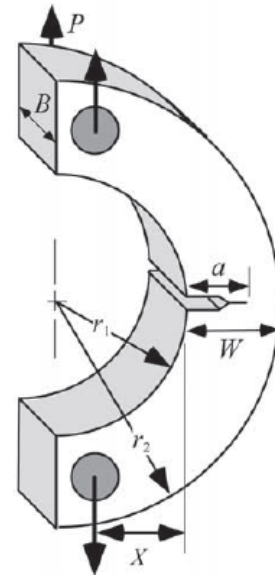
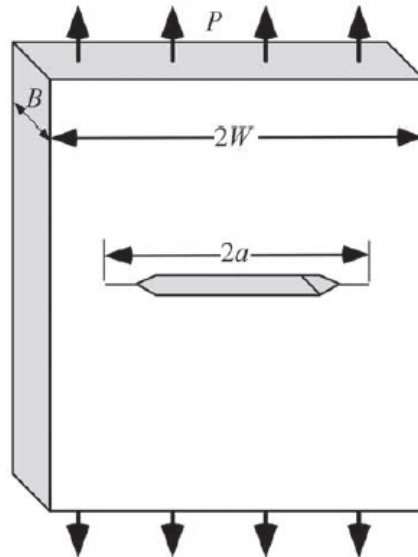
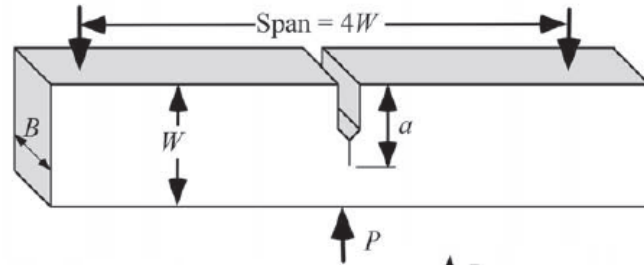
1. To measure the fracture toughness  $K_{Ic}$
2. Measure the R-curve using the  $J$ -integral.

# Specimen geometries

Compact Tension (CT)

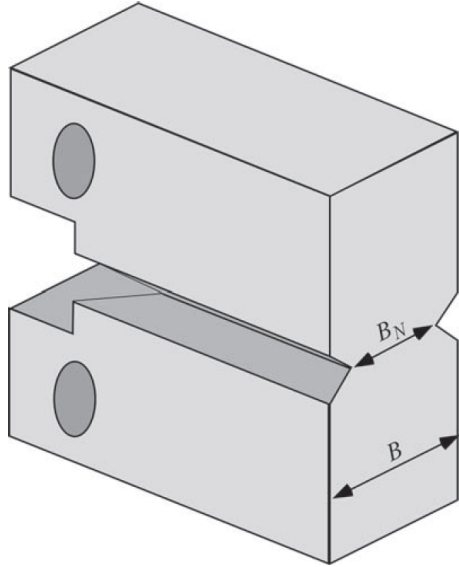


Single-Edge-Notched Bend (SENB)

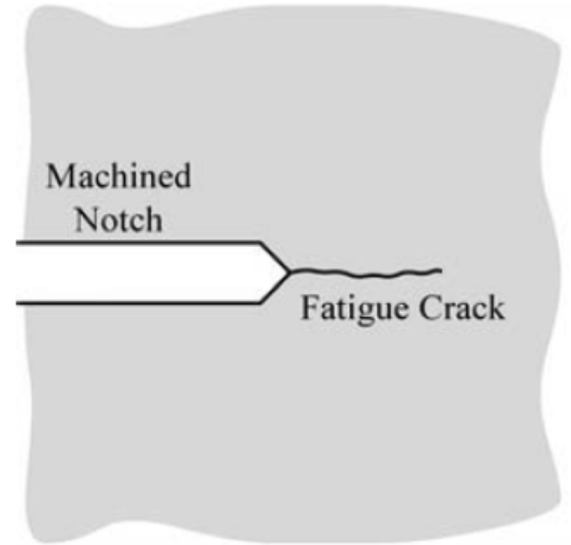




# Side grooves and precrack

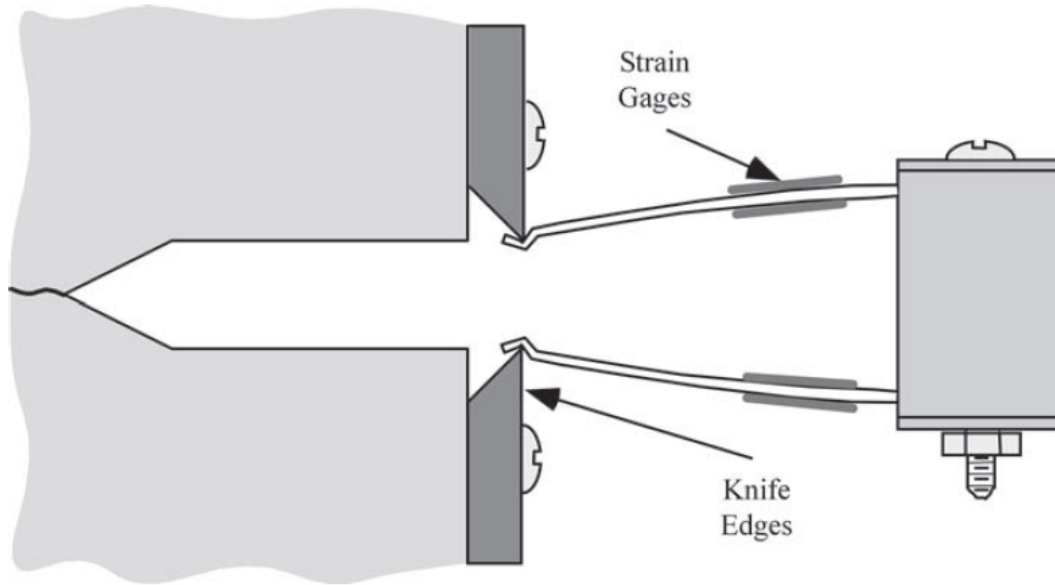


Side grooves help to propagate a straight crack.



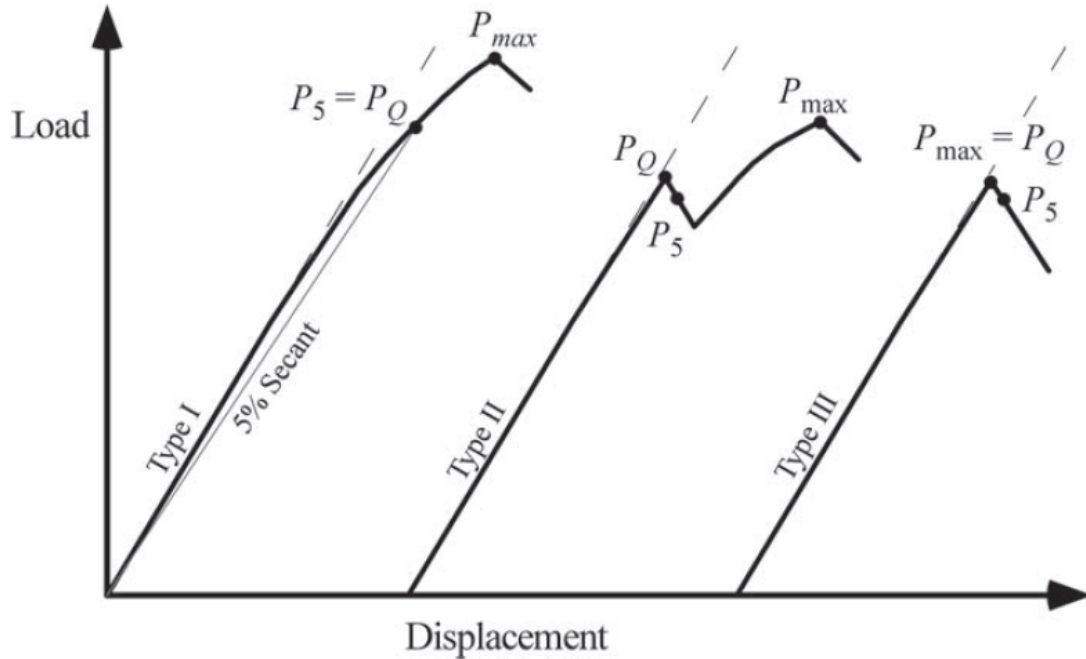
For metals, fatigue is the only way to produce a sharp crack.

# Instrumentation



- Displacement is measured at the crack mouth by a clip-gauge.
- Force is measured by the testing machine.

# Method 1: $K_{Ic}$



Calculate the stress intensity factor with:

$$K_Q = \frac{P_Q}{B\sqrt{W}} f\left(\frac{a}{W}\right)$$

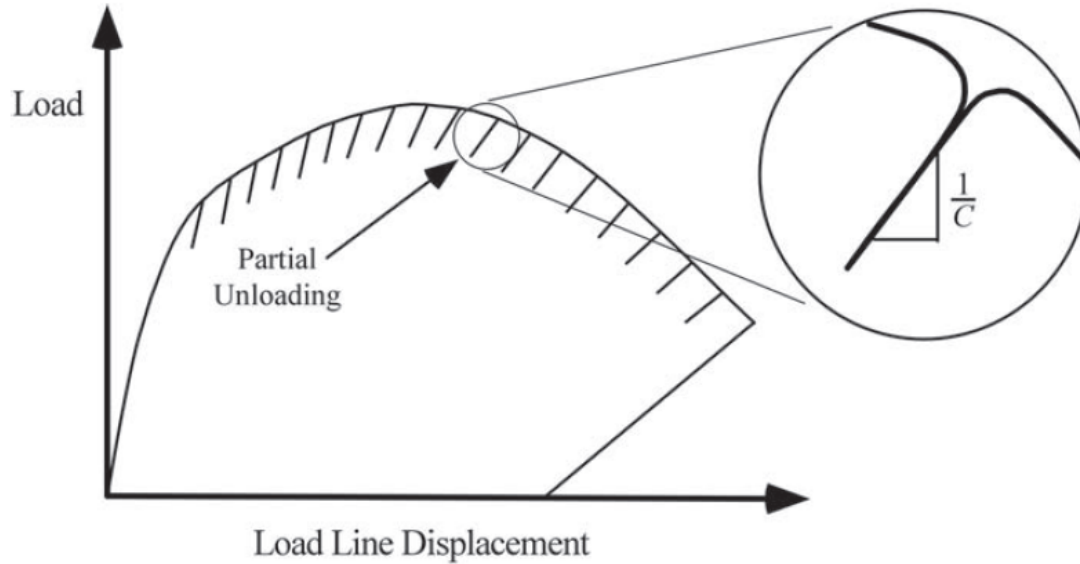
A valid test should respect these conditions:

$$0.45 \leq \frac{a}{W} \leq 0.55$$

$$P_{max} \leq 1.10P_Q$$

$$a, (W - a), B \geq 2.5 \left( \frac{K_{Ic}}{\sigma_Y} \right)^2$$

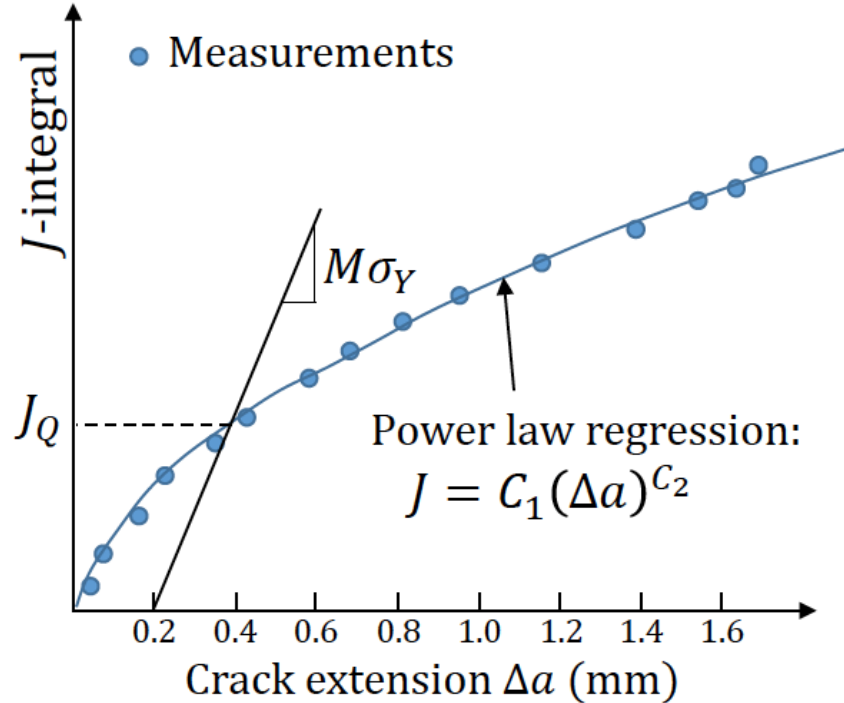
# Method 2: R-curve



Use the compliance  $C$  to calculate the crack length  $a$  during the test.

Calculate  $J$  as a function of  $a$  (for each partial unloading).

# Method 2: R-curve



The value  $J_Q = J_{Ic}$  if:

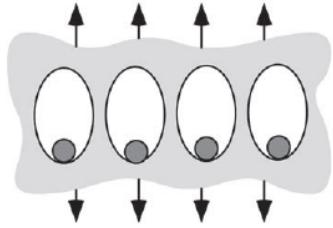
$$B, b_0 \geq \frac{25J_Q}{\sigma_Y}$$

If this is satisfied, you can get:

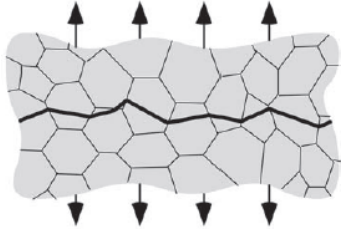
$$K_{Ic} = \sqrt{\frac{EJ_{Ic}}{1 - \nu^2}}$$

# Fracture mechanics

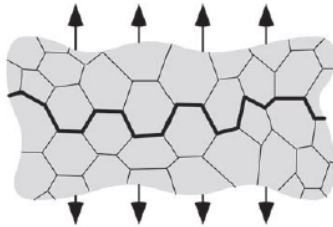
# Fracture mechanisms in metals



1. Ductile fracture,

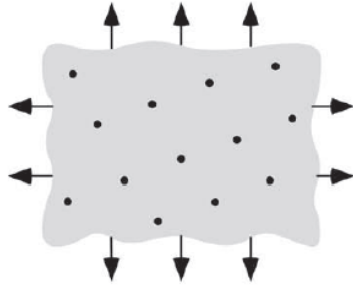


2. Cleavage,

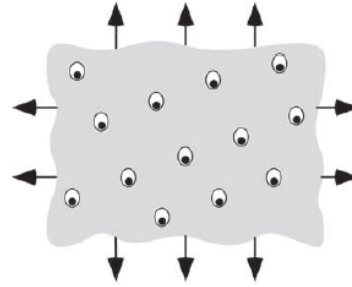


3. Intergranular fracture

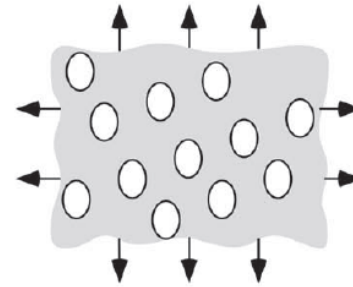
# Ductile fracture



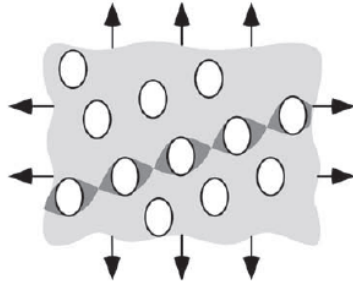
1. Inclusions in a ductile matrix



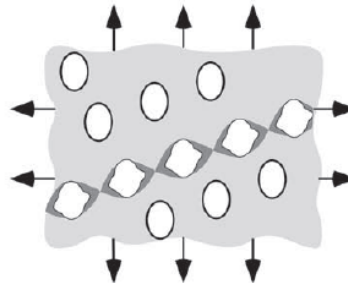
2. Void nucleation



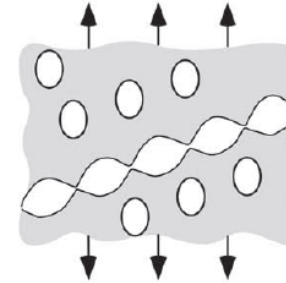
3. Void growth



4. Strain localisation between voids



5. Necking between voids

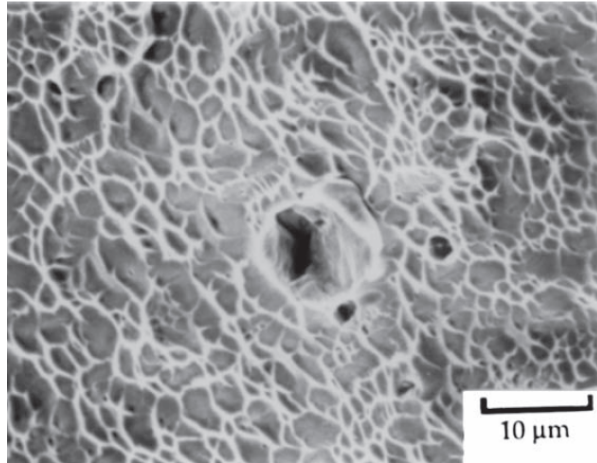


6. Void coalescence and fracture



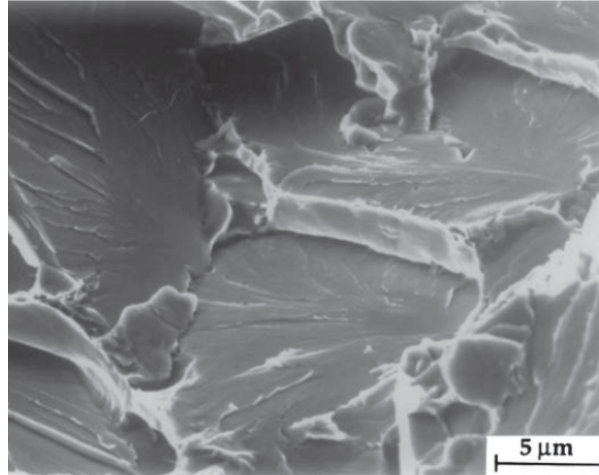
# Fractography

**Ductile fracture**



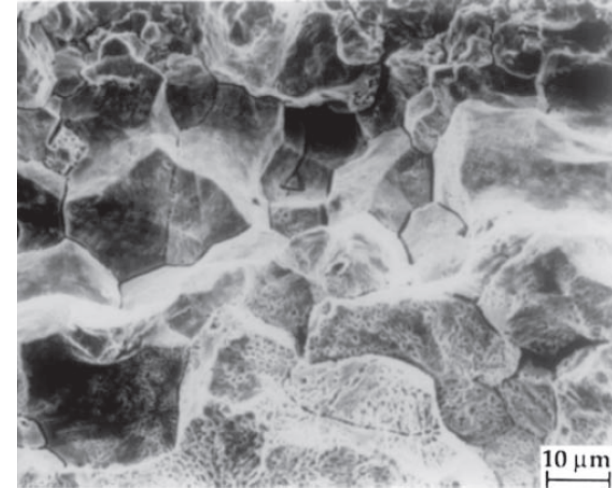
Most metals at room temperature

**Cleavage**



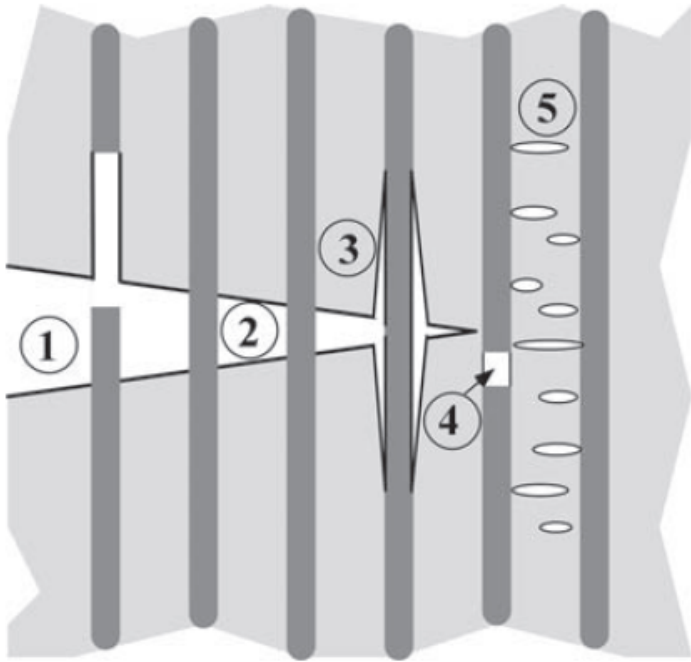
Metals at low temperatures

**Intergranular fracture**



Metals in harsh environments

# Fracture mechanisms in composites



1. Fibre pull-out,
2. Fibre bridging,
3. Fibre/matrix debonding,
4. Fibre failure,
5. Matrix cracking.

# In summary

We covered:

- How to use the  $J$ -integral, and how it is implemented in FEM.
- The procedure to measure fracture toughness,
- What are the main fracture mechanisms.