

CIV-E4080 - Material Modelling in Civil Engineering D.

Homework answers

HW exercise 1.1.

$$1. \frac{1}{3}\sigma_0(1 + \alpha).$$

$$2. \sigma_e = \sigma_0\sqrt{\alpha^2 - \alpha + 1}.$$

$$3. \theta = \frac{1}{3} \arccos \frac{2\alpha^3 - 3\alpha^2 - 3\alpha + 2}{2(\alpha^2 - \alpha + 1)^{2/3}}.$$

$$4. \alpha \in [-1, 0] : \tau_{max} = \frac{1}{2}\sigma_0(1 - \alpha); \quad \alpha \in (0, 1] : \tau_{max} = \frac{1}{2}\sigma_0.$$

$$5. \alpha \in [-1, 0) : \mathbf{n} = \begin{bmatrix} \pm 1/\sqrt{2} \\ \pm 1/\sqrt{2} \\ 0 \end{bmatrix}; \quad \alpha \in (0, 1] : \mathbf{n} = \begin{bmatrix} \pm 1/\sqrt{2} \\ 0 \\ \pm 1/\sqrt{2} \end{bmatrix};$$

$\alpha = 0$: both previous cases are applied simultaneously.

For $\alpha = -1$, hydrostatic pressure is equal to zero $p = 0$, and there is no change of volume in the material.

HW exercise 1.2.

$$1. \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ 2\varepsilon_{12} \end{bmatrix} = \begin{bmatrix} \frac{1}{E_1} & -\frac{\nu_{21}}{E_2} & 0 \\ -\frac{\nu_{12}}{E_1} & \frac{1}{E_2} & 0 \\ 0 & 0 & \frac{1}{G_{12}} \end{bmatrix} \begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{12} \end{bmatrix}$$

$$2. \begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{12} \end{bmatrix} = \begin{bmatrix} \frac{E_1}{1-\nu_{12}\nu_{21}} & \frac{\nu_{21}E_1}{1-\nu_{12}\nu_{21}} & 0 \\ \frac{\nu_{12}E_2}{1-\nu_{12}\nu_{21}} & \frac{E_2}{1-\nu_{12}\nu_{21}} & 0 \\ 0 & 0 & G_{12} \end{bmatrix} \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ 2\varepsilon_{12} \end{bmatrix}$$

3. The reciprocal relations can be directly derived from the symmetry property of the compliance matrix.

HW exercise 1.3.

$p = 0.48 \text{ MPa}, M_t = 44.4 \text{ N}\cdot\text{m}.$

HW exercise 1.4.

$\delta_1 = 1.18 \text{ mm}, \delta_2 = -3.1875 \text{ mm}, \delta_3 = 4.5 \mu\text{m}.$

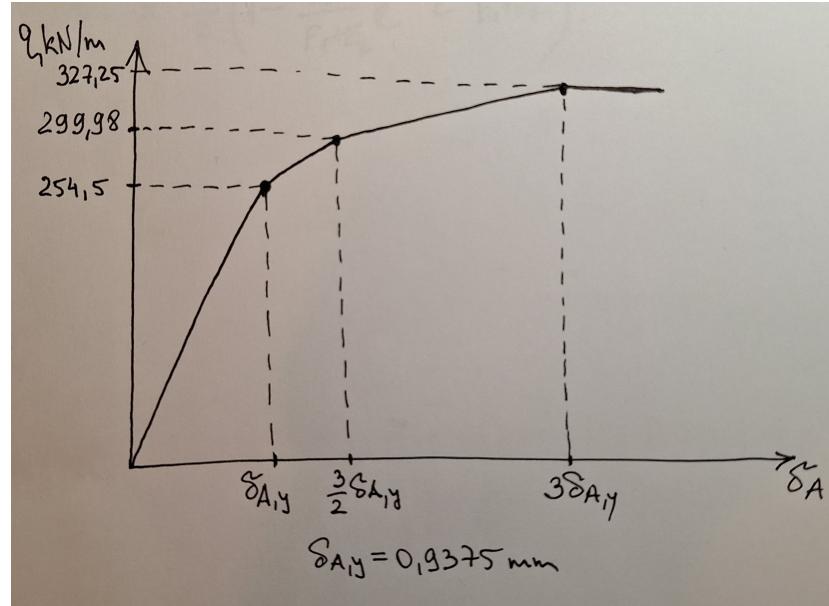
HW exercise 2.1.

a) $q_y = 254.5 \text{ kN/m}$, $\delta_{A,y} = 0.9375 \text{ mm}$.

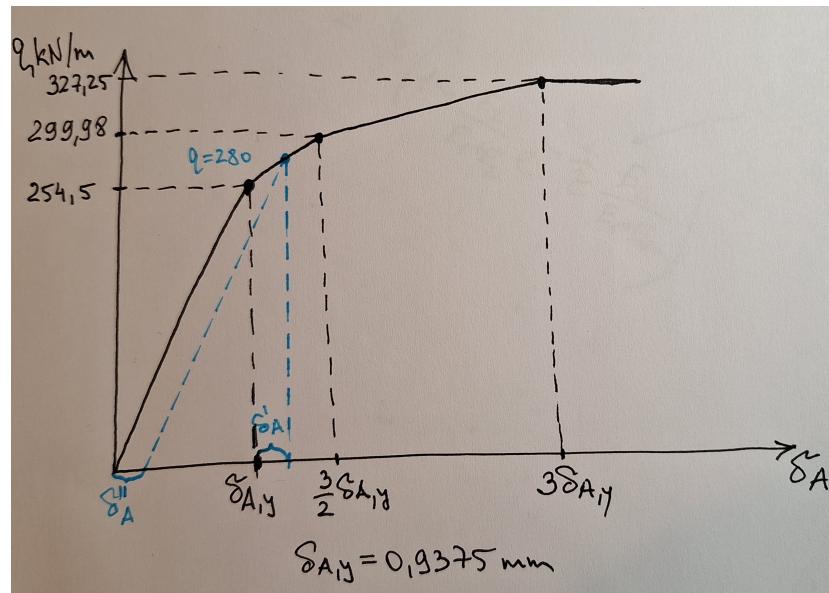
b) $q_p = 327.25 \text{ kN/m}$, $\delta_{A,p} = 2.8125 \text{ mm}$.

c) The wording of this problem allows for ambiguity. First, the permanent deformation at point A can be understood as plastic deformation of bar A under the load of $q = 280 \text{ kN/m}$, it's equal to $\delta'_A = 0.2627 \text{ mm}$. Second, one can interpret it as a displacement of point A after the load is removed, when the system takes a new state of equilibrium (bar A has a new length of 750 mm + plastic deformation δ'_A and elastic forces in B and C tend to return bars B and C to the initial length), then the answer is $\delta''_A = 0.1689 \text{ mm}$. Both answers are considered correct.

d)



e) Both results discussed in c) can be obtained graphically as depicted below:



HW exercise 2.2.

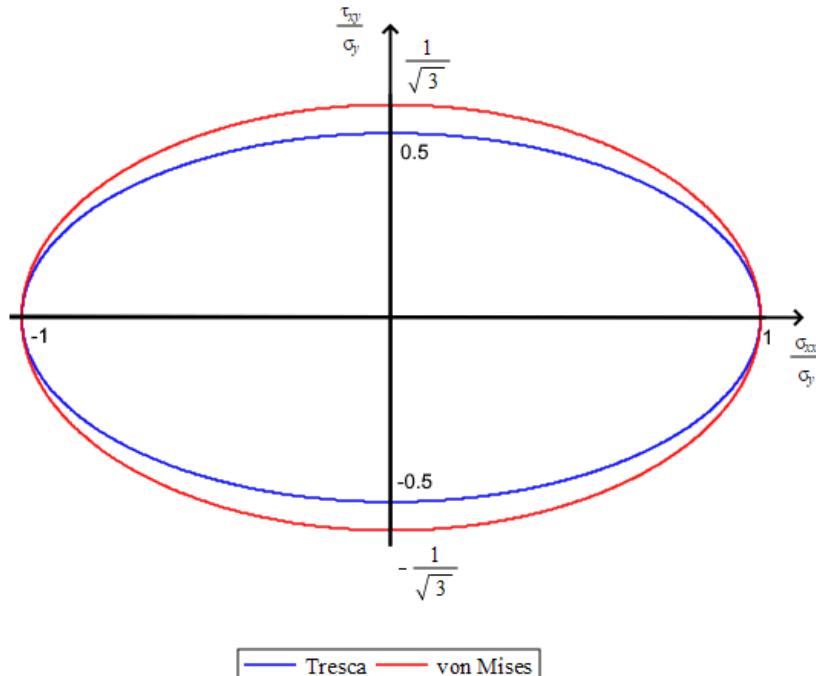
The final answer is given in the exercise description.

HW exercise 3.1.

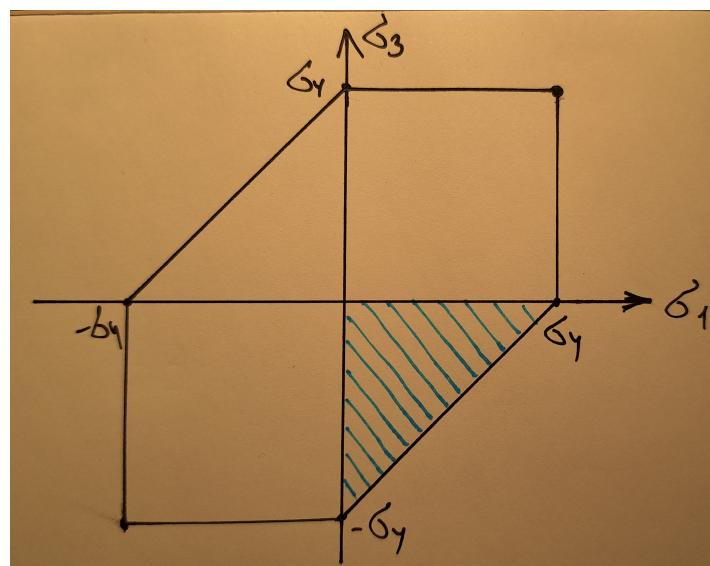
- a) $\alpha = 0.7047$;
- b) $\alpha = 0.2646$.

HW exercise 3.2.

a)



- b) In general, if we do not impose that $\sigma_1 > \sigma_2 > \sigma_3$, the failure envelope according to the Tresca criterion looks like this:



For this problem, and if we assume $\sigma_1 > \sigma_2 > \sigma_3$, the stress state belongs to the dashed area ($\sigma_1 > 0$, $\sigma_2 = 0$, $\sigma_3 < 0$).

HW exercise 3.3.

- a) $\frac{1}{2\pi Rt} \sqrt{N^2 + \frac{3T^2}{R^2}}$;
- b) $\theta = \pi/6$;
- c) $\theta = 0$;
- d) $p_y = \frac{1 + \sqrt{13}}{4} \frac{t\sigma_y}{R}$ ($N > 0$ assumed).

HW exercise 4.1.

- 1. $\varepsilon = \frac{\sigma_0}{E}(1 - e^{-Et/\eta})$;
- 2. (i) $\varepsilon = 0.3874$; (ii) $t = 14.34$ s.

HW exercise 4.2.

- 1. $G(t) = Ee^{-Et/\eta}$;
- 2. $\tau = 693$ days;
- 3. $\sigma_0 \geq 254$ MPa.

HW exercise 4.3.

$$F_1 = \frac{P_0}{2} \left(1 - \frac{E_2}{E_1 + E_2} e^{-\frac{tE_1E_2}{\eta(E_1+E_2)}} \right); \quad F_2 = P_0 \frac{E_2}{E_1 + E_2} e^{-\frac{tE_1E_2}{\eta(E_1+E_2)}}.$$

HW exercise 5.

- 1. $\dot{\varepsilon}^{cr} = A\sigma_e^n \left[\frac{(m+1)\varepsilon^{cr}}{A\sigma_e^n} \right]^{m/(m+1)}$;
- 2. $t = \left[\frac{m+1}{A\sigma_0^n} \left(\frac{u_0}{L} - \frac{\sigma_0}{E} \right) \right]^{1/(m+1)}$;
- 3. $\sigma = \left[\left(\frac{u_0 E}{L_0} \right)^{1-n} + \frac{AE(n-1)}{m+1} t^{m+1} \right]^{1/(1-n)}$;
- 4. $E_{diss} = 4\sigma_m \left(\frac{u_0}{L} - \frac{\sigma_m}{E} \right)$.