



Aalto University
School of Engineering

COE-C2004 - Materials Science and Engineering

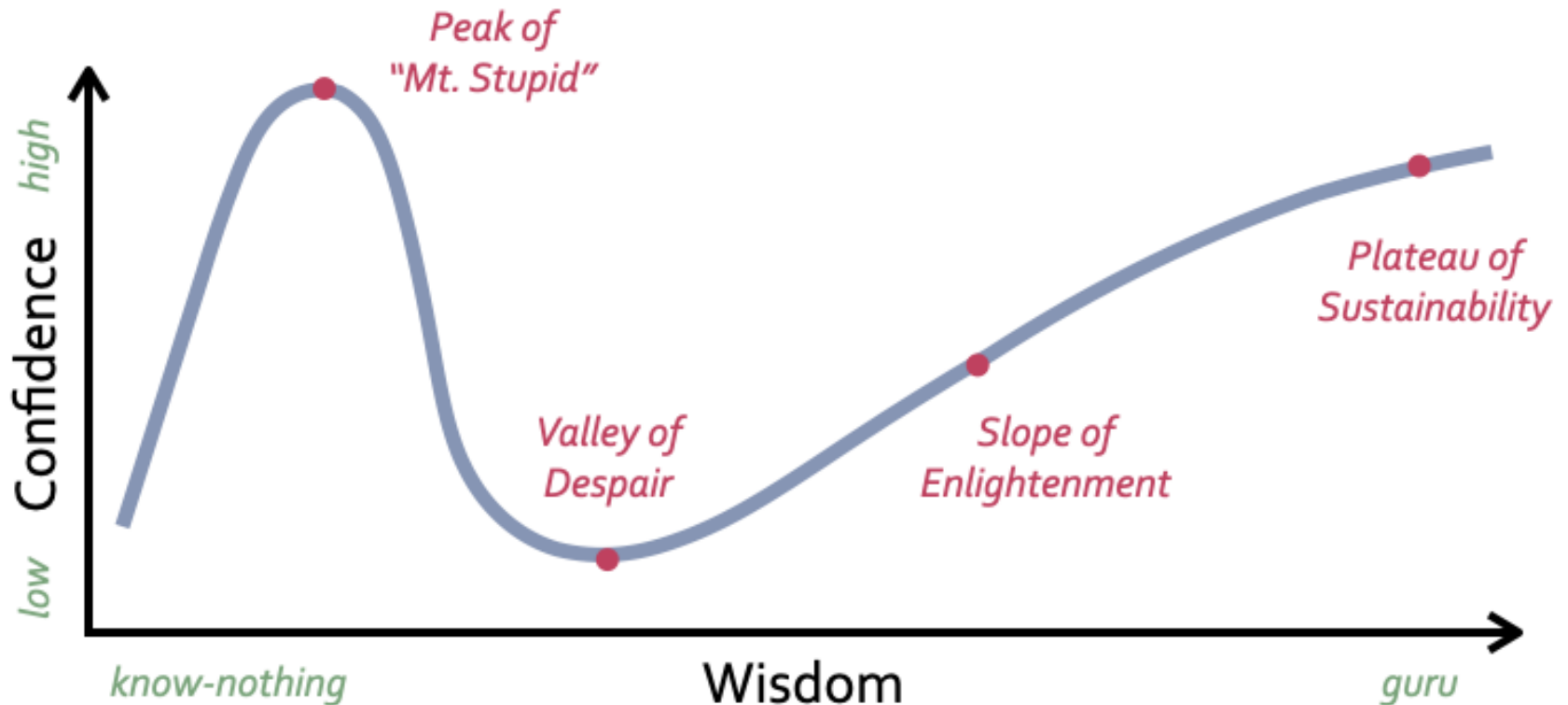
Prof. Junhe Lian

Wenqi Liu (Teaching Assistant)

Updates:

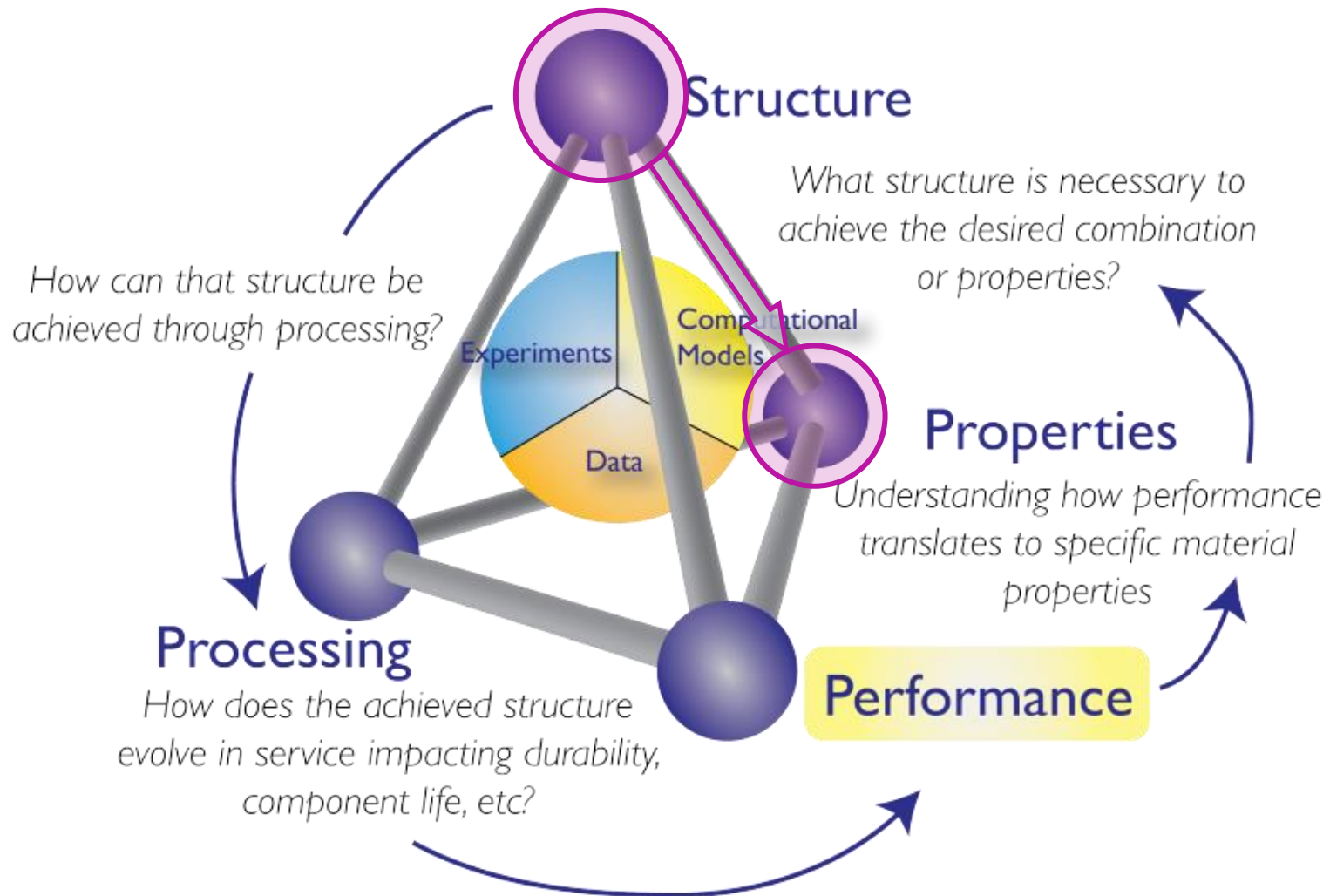
- Slides (pre) were uploaded to MyCourses
- Get familiar with MyCourses
- Active participation is very much appreciated
- Get some paper and pen. Let's derive.

Where are you?



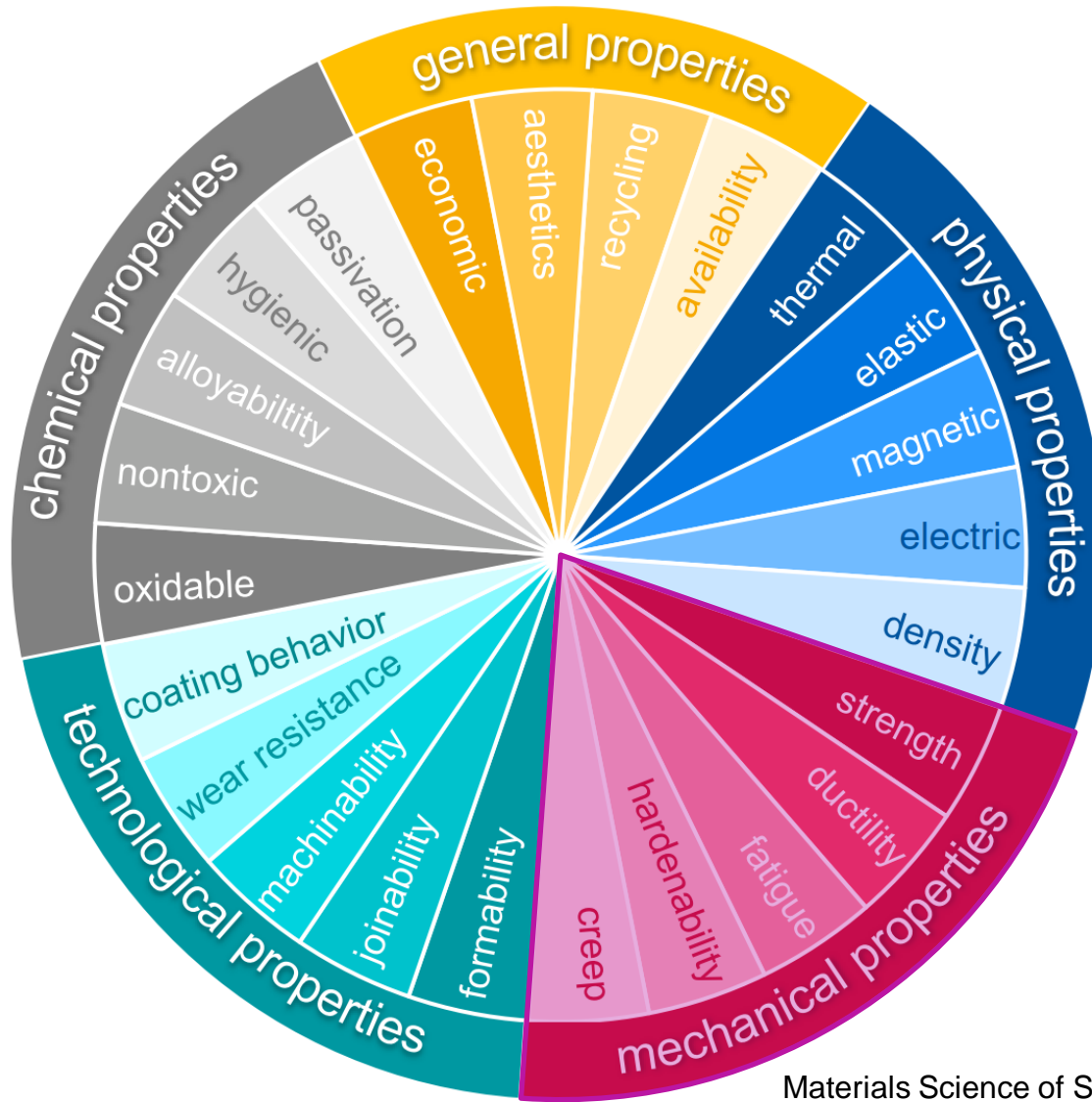
<https://dorsaamir.medium.com/modest-advice-for-new-graduate-students-b0be6b8dbc22>

Previously



<https://gems.matse.illinois.edu/educators/>

Previously



Materials Science of Steel, Wolfgang Bleck

Chapter 3: Mechanical Properties of Metals

ISSUES TO ADDRESS...

- ❑ When a metal is exposed to mechanical forces, what parameters are used to express **force magnitude** and **degree of deformation**?
- ❑ What is the distinction between **elastic** and **plastic** deformations?
- ❑ How are the following mechanical characteristics of metals measured? (a) **Stiffness** (b) **Strength** (c) **Ductility** (d) **Hardness**
- ❑ What is **true stress – true strain** curve?
- ❑ How to determine **necking**?
- ❑ What **structure** decides the elastic properties?

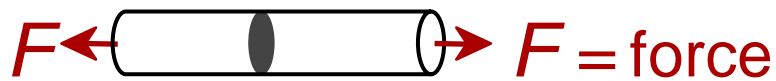
Stress and Strain



Common States of Stress

- Uniaxial tension

Cable



A = cross-sectional
area of cable



Ski lift (photo courtesy
P.M. Anderson)

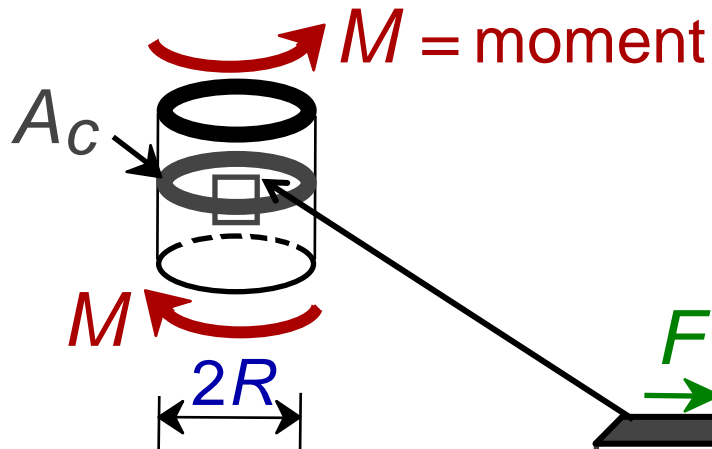
Tensile stress = σ

$$\sigma = \frac{F}{A}$$

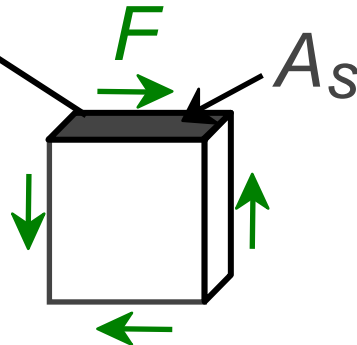
Common States of Stress (cont.)

- Torsion (a form of shear)

Drive shaft



A_c = cross-sectional area of drive shaft

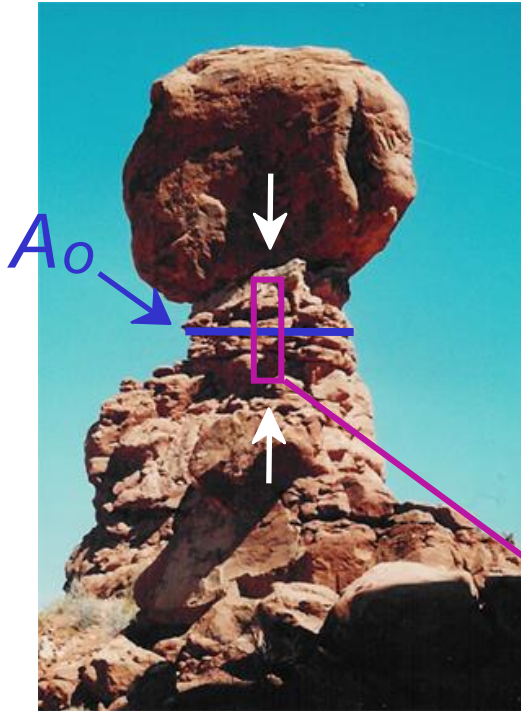


Ski lift (photo courtesy P.M. Anderson)

$$\tau = \frac{F}{A_s} = \frac{M}{A_c R}$$

Common States of Stress (cont.)

- Uniaxial compression:



Balanced Rock, Arches National Park
(photo courtesy P.M. Anderson)



Canyon Bridge, Los Alamos, NM
(photo courtesy P.M. Anderson)

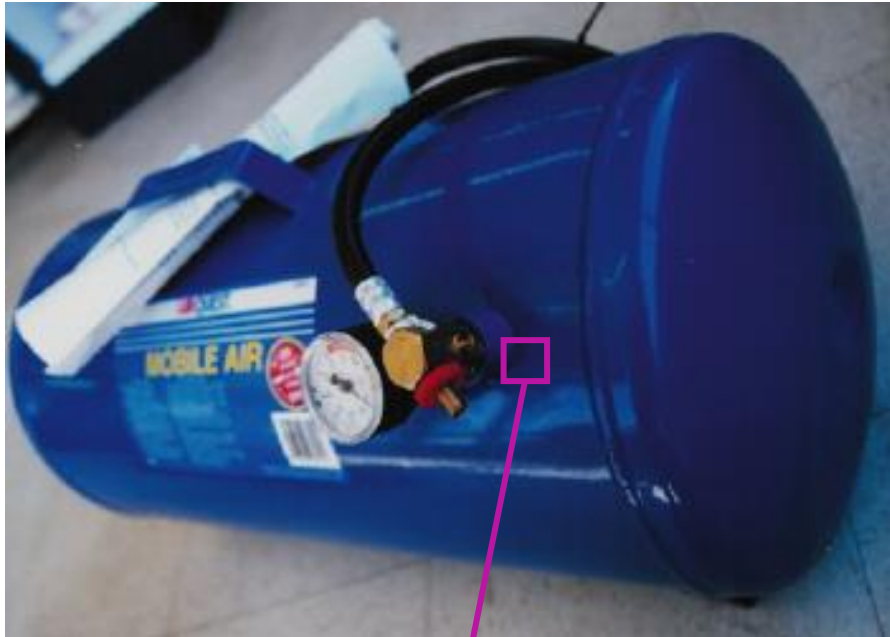
$$\sigma = \frac{F}{A_o}$$



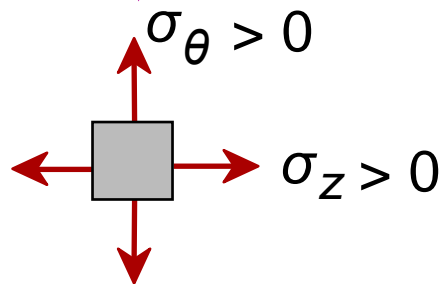
Structure members are under compression ($F < 0$ and $\sigma < 0$).

Common States of Stress (cont.)

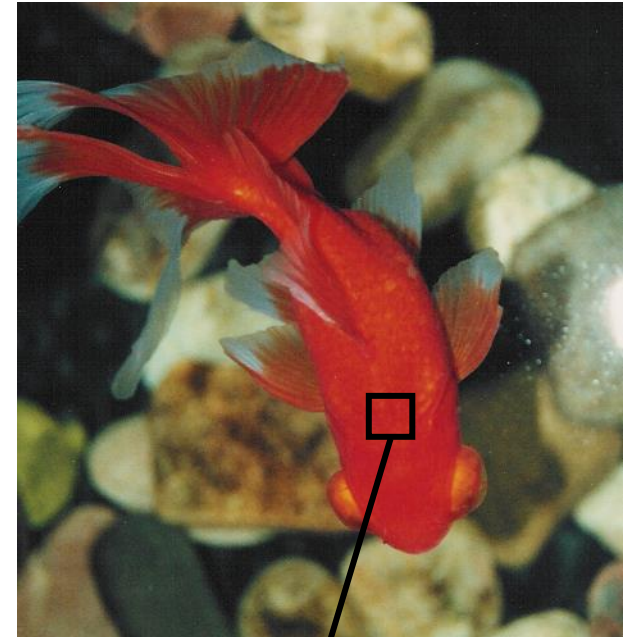
- Biaxial tension



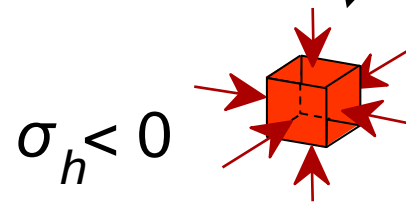
Pressurized tank
(photo courtesy
P.M. Anderson)



- Hydrostatic compression

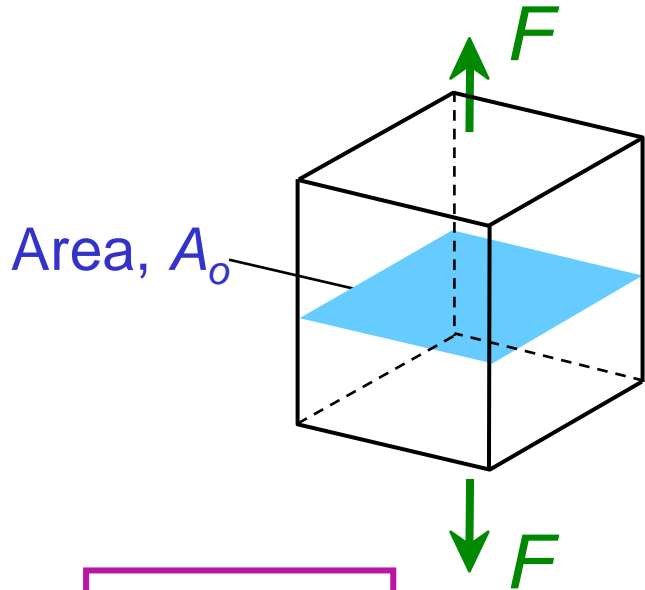


Fish under water
(photo courtesy
P.M. Anderson)



Engineering Stress

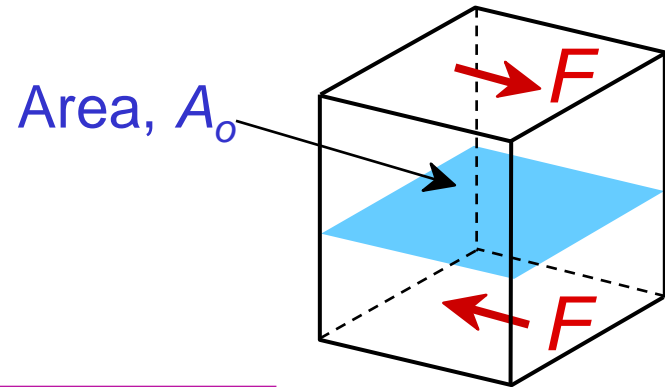
- Tensile stress, σ :



$$\sigma = \frac{F}{A_o}$$

original cross-sectional
area before loading

- Shear stress, τ :



$$\tau = \frac{F}{A_o}$$

Unit for stress:
 $\text{MPa} = 10^6 \text{ Pa} = 10^6 \text{ N/m}^2$

Engineering Strain

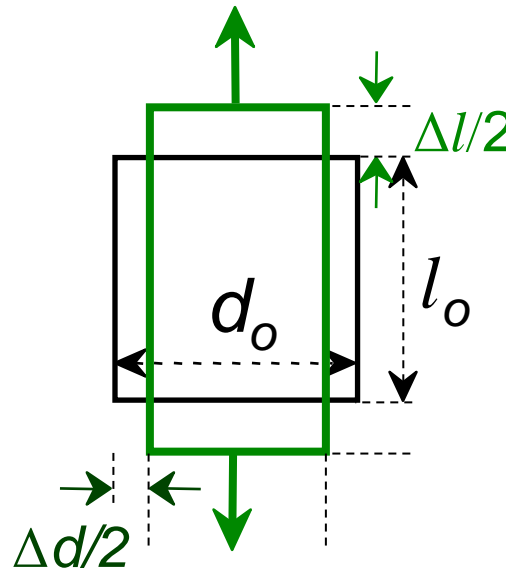
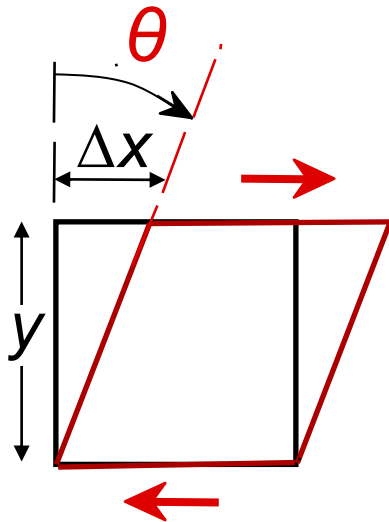
- **Tensile strain** (ε_z):

$$\varepsilon_z = \frac{\Delta l}{l_o}$$

- **Lateral strain** (ε_x):

$$\varepsilon_x = -\frac{\Delta d}{d_o}$$

- **Shear strain** (γ):



$$\gamma = \Delta x/y = \tan \theta$$

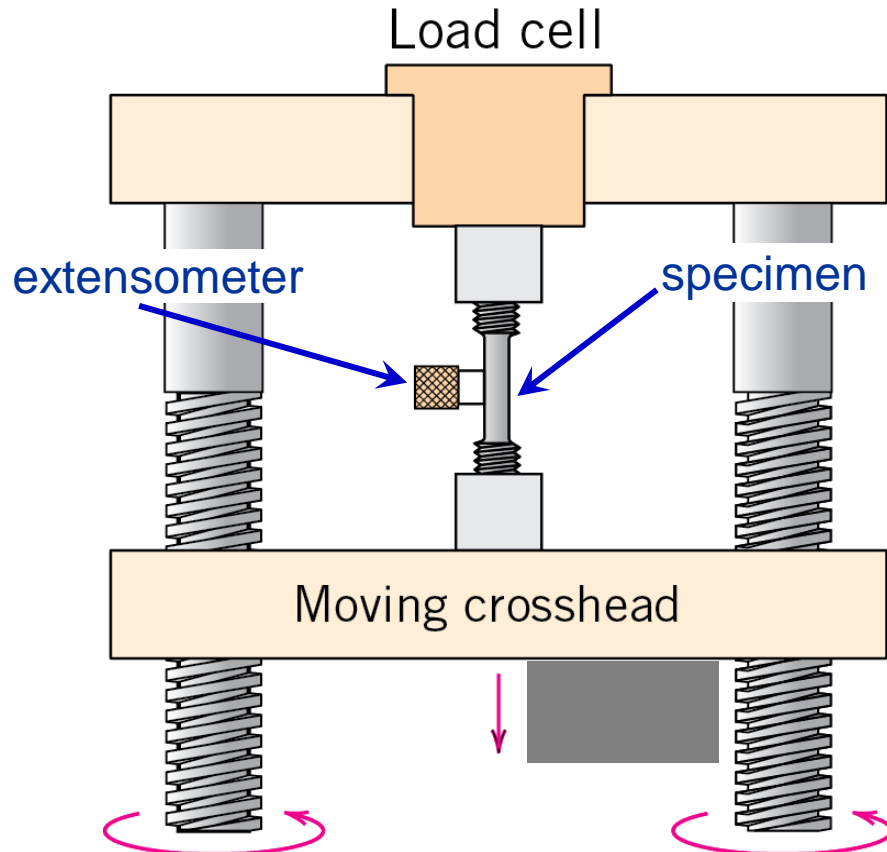
Both tensile and shear strain are dimensionless

Stress – Strain Testing and Curve



Stress-Strain Testing

- Typical tensile test machine



- Typical tensile specimen

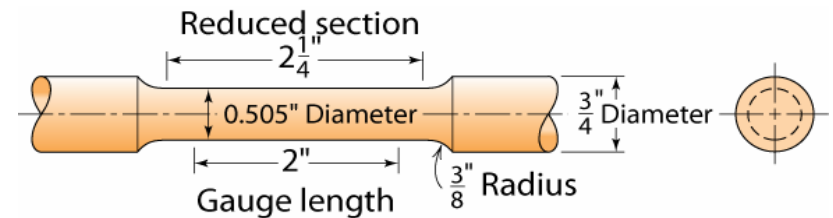
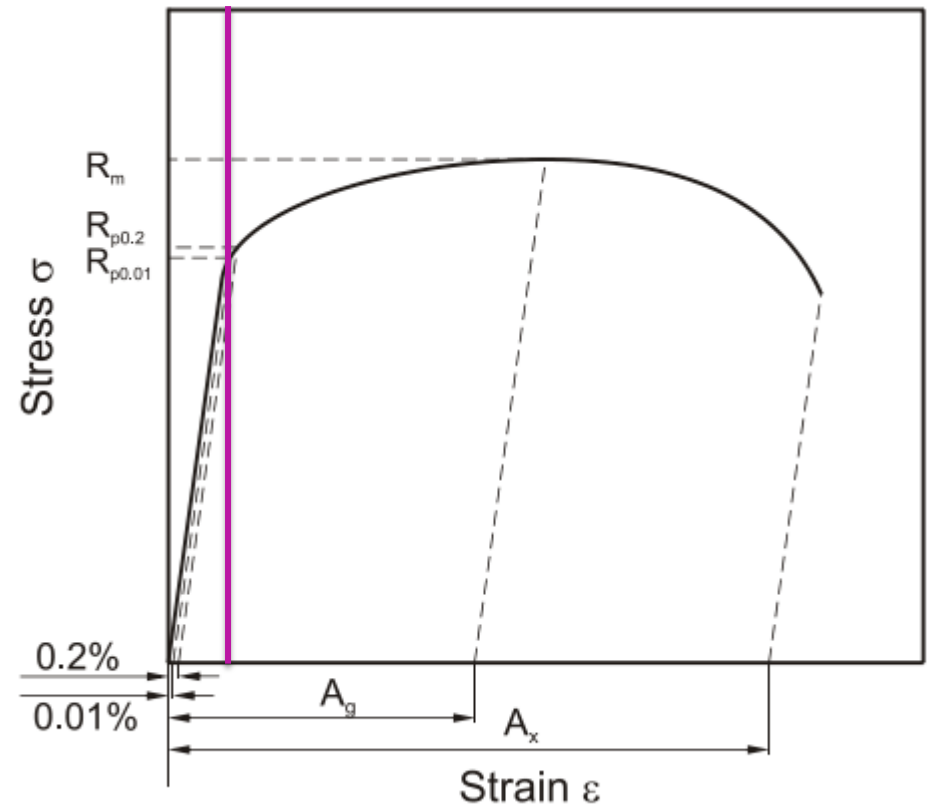
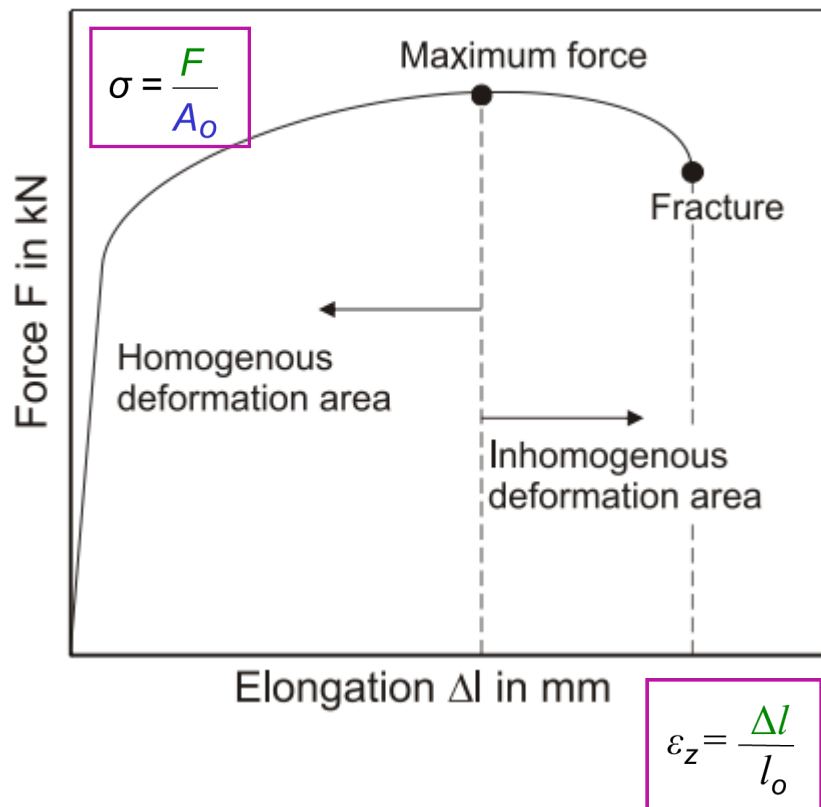


Fig. 6.2, Callister & Rethwisch 10e.

Fig. 6.3, Callister & Rethwisch 10e. (Taken from H.W. Hayden, W.G. Moffatt, and J. Wulff, *The Structure and Properties of Materials*, Vol. III, *Mechanical Behavior*, p. 2, John Wiley and Sons, New York, 1965.)

Stress-Strain Curve



Materials Science of Steel, Wolfgang Bleck

Linear Elastic Properties

- **Elastic deformation** is **nonpermanent** and **reversible**!
 - generally valid at small deformations
 - linear stress strain curve

- **Modulus of Elasticity, E :**
(also known as Young's modulus)

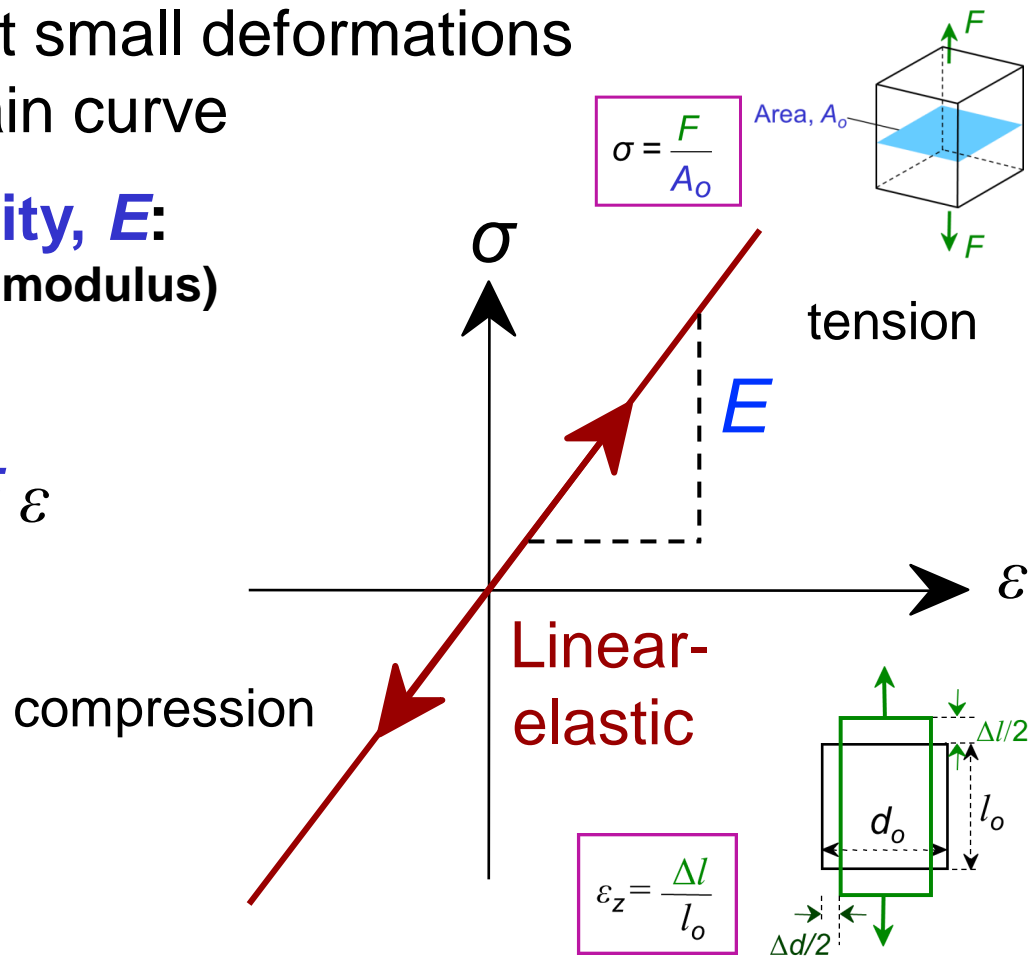
- **Hooke's Law:**

$$\sigma_z = E \varepsilon_z \text{ or } \sigma = E \varepsilon$$

Units:

E : [GPa]

1 GPa = 10^9 Pa



Poisson's ratio

- Poisson's ratio, ν :

$$\nu = - \frac{\varepsilon_x}{\varepsilon_z}$$

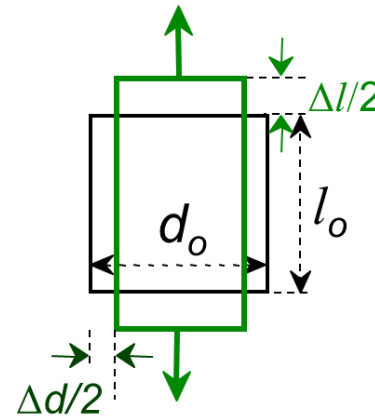
metals: $\nu \sim 0.33$

ceramics: $\nu \sim 0.25$

polymers: $\nu \sim 0.40$

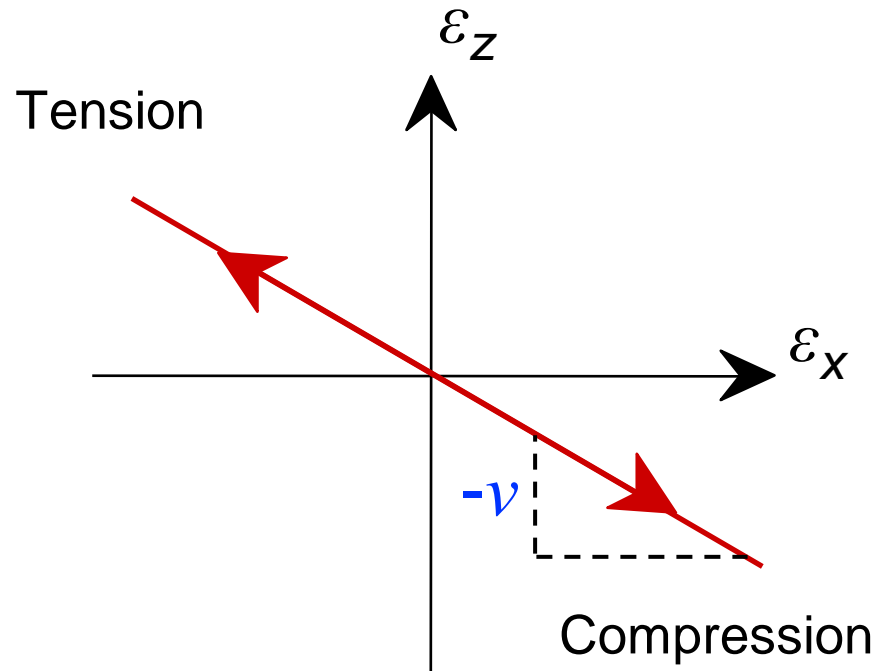
Units:

ν : dimensionless



$$\varepsilon_z = \frac{\Delta l}{l_0}$$

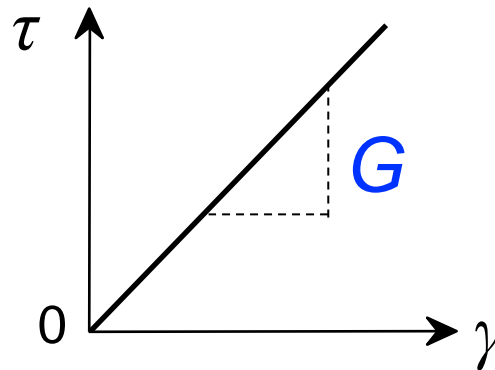
$$\varepsilon_x = -\frac{\Delta d}{d_0}$$



Other Elastic Properties

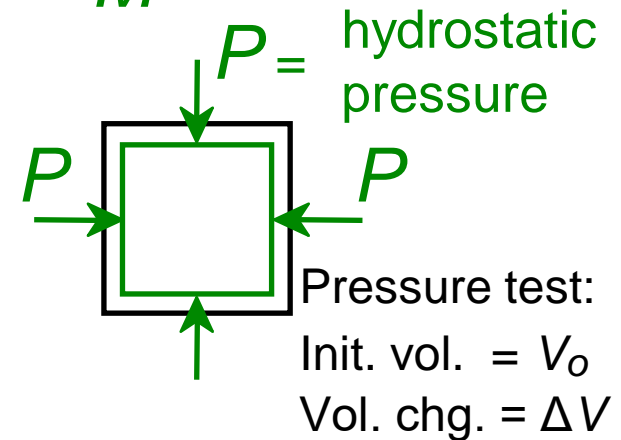
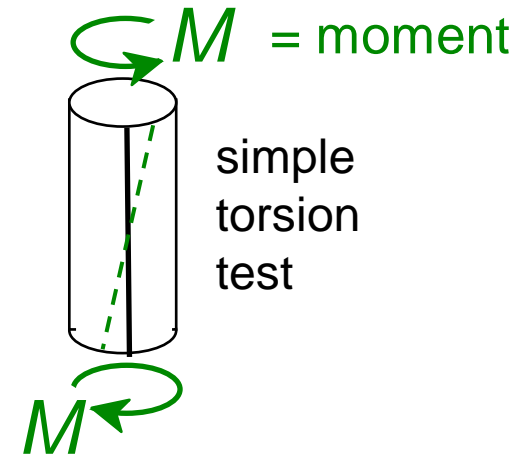
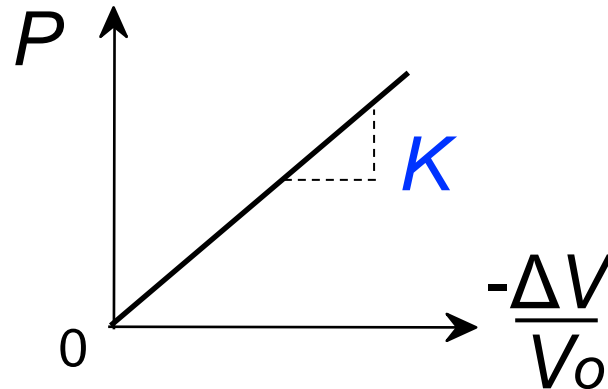
- Elastic Shear modulus, G :

$$\tau = G \gamma$$



- Elastic Bulk modulus, K :

$$P = -K \frac{\Delta V}{V_0}$$



- Elastic constant relationships for **isotropic** materials:

$$G = \frac{E}{2(1 + \nu)}$$

$$K = \frac{E}{3(1 - 2\nu)}$$

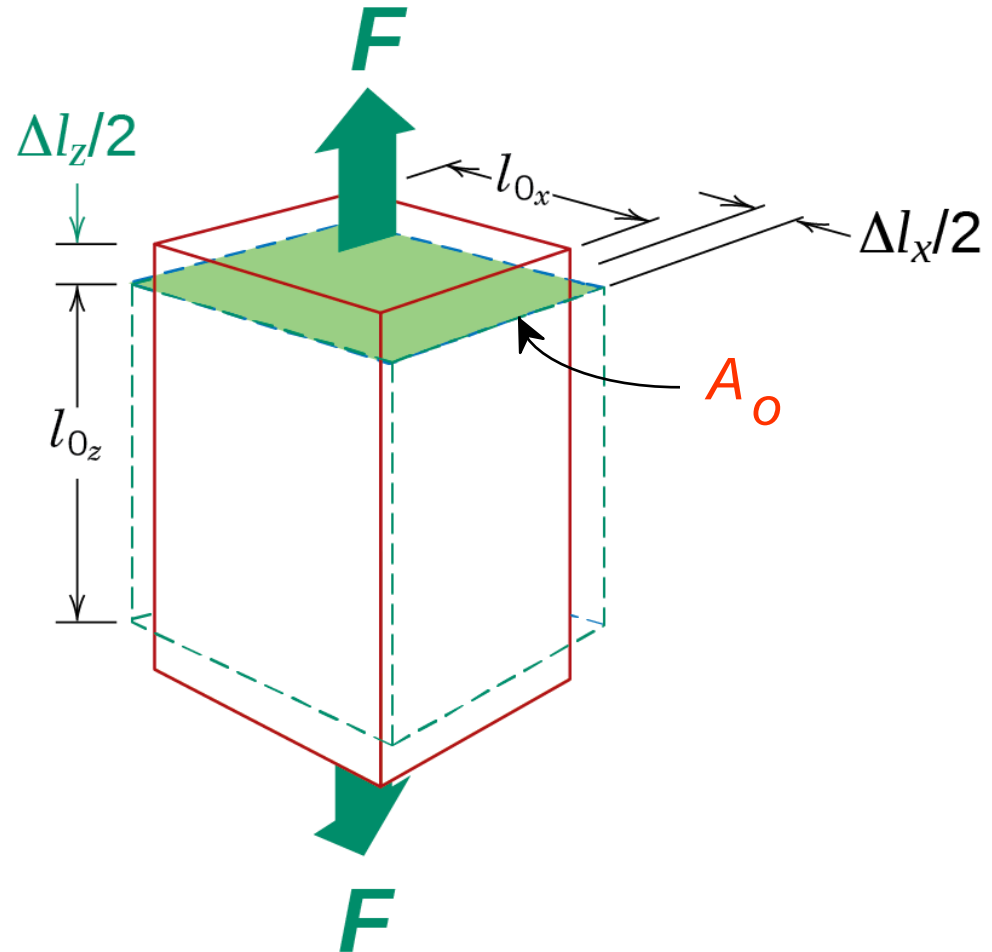
Linear Elastic Relationships

- **Uniaxial tension**

Known: F and A_0 ; E and $\nu \Rightarrow$ derive axial and lateral deformation

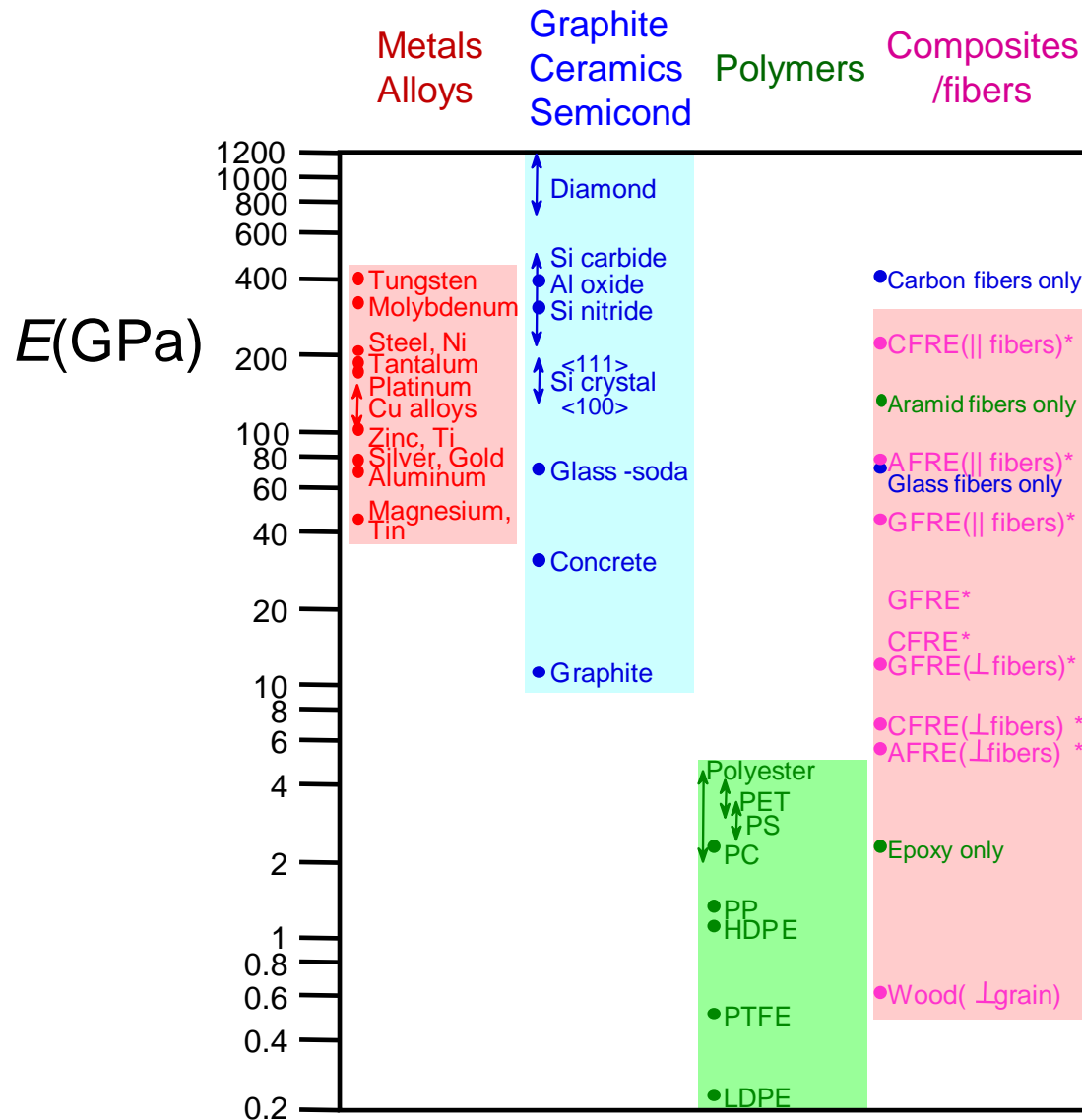
$$\Delta l_z = \frac{F l_{0z}}{EA_0}$$

$$\Delta l_x = -\nu \frac{F l_{0x}}{EA_0}$$



- Deflection is dependent on material, geometric, and loading parameters.
- Materials with large elastic moduli deform less

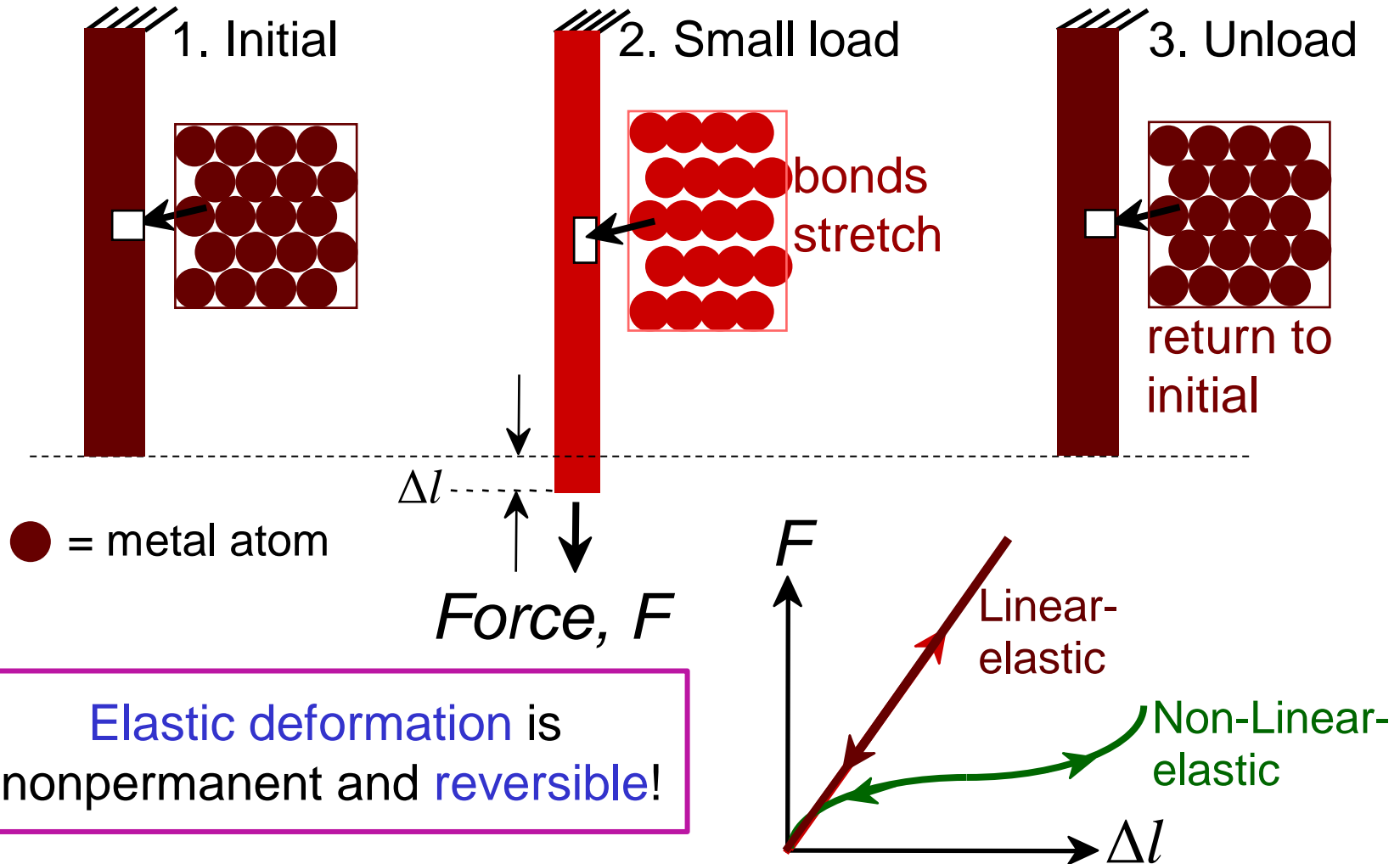
Elastic Modulus – Material Types



Based on data in Table B.2, *Callister & Rethwisch 10e*.
Composite data based on reinforced epoxy with 60 vol% of aligned carbon (CFRE), aramid (AFRE), or glass (GFRE) fibers.

Elastic Deformation

Atomic configurations—before, during, after load (force) application



Influence of Bonding Forces

- Elastic modulus depends on interatomic bonding forces
- Modulus proportional to slope of interatomic force-separation curve $\left(\frac{dF}{dr}\right)_{r_0}$

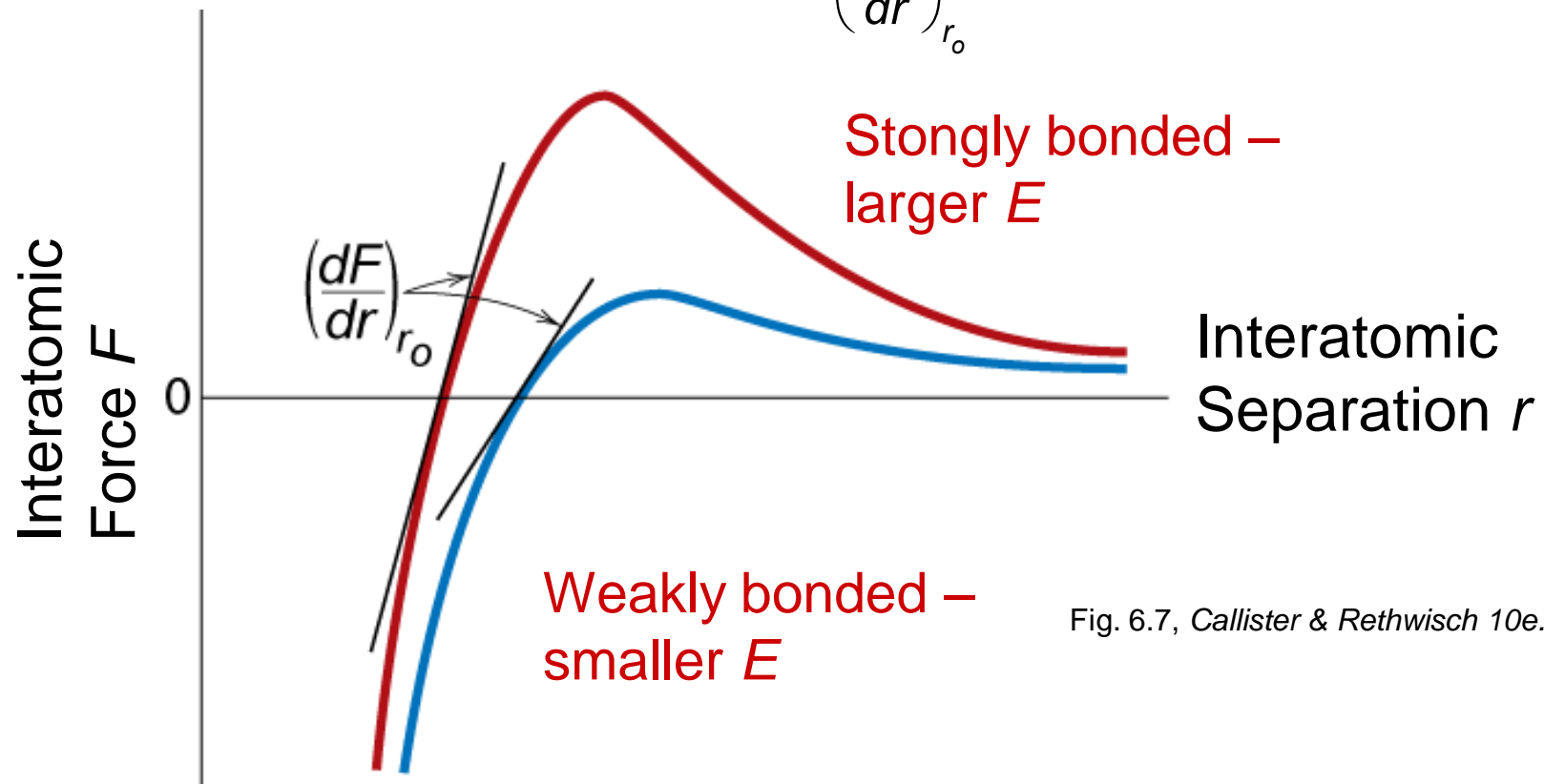
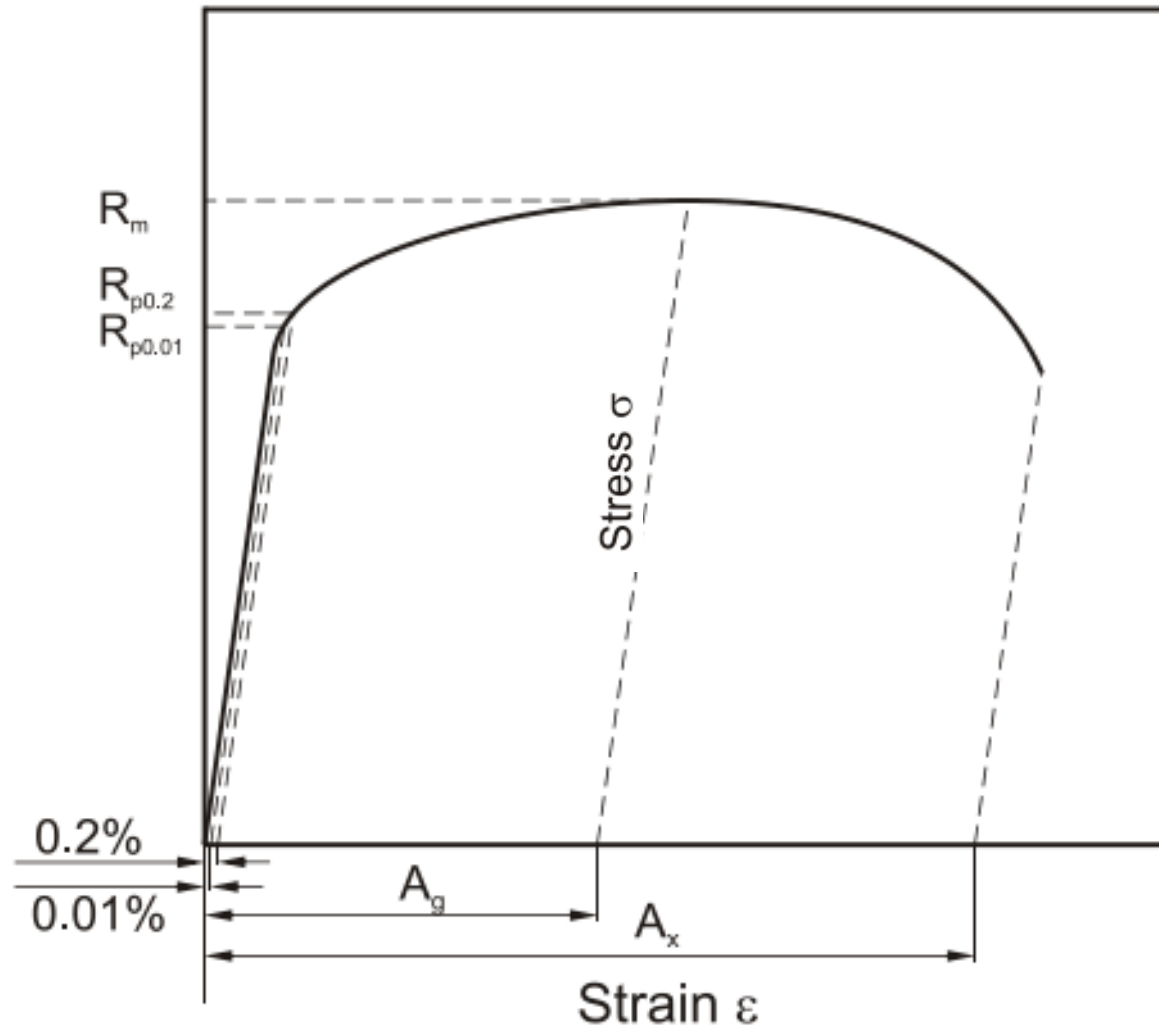


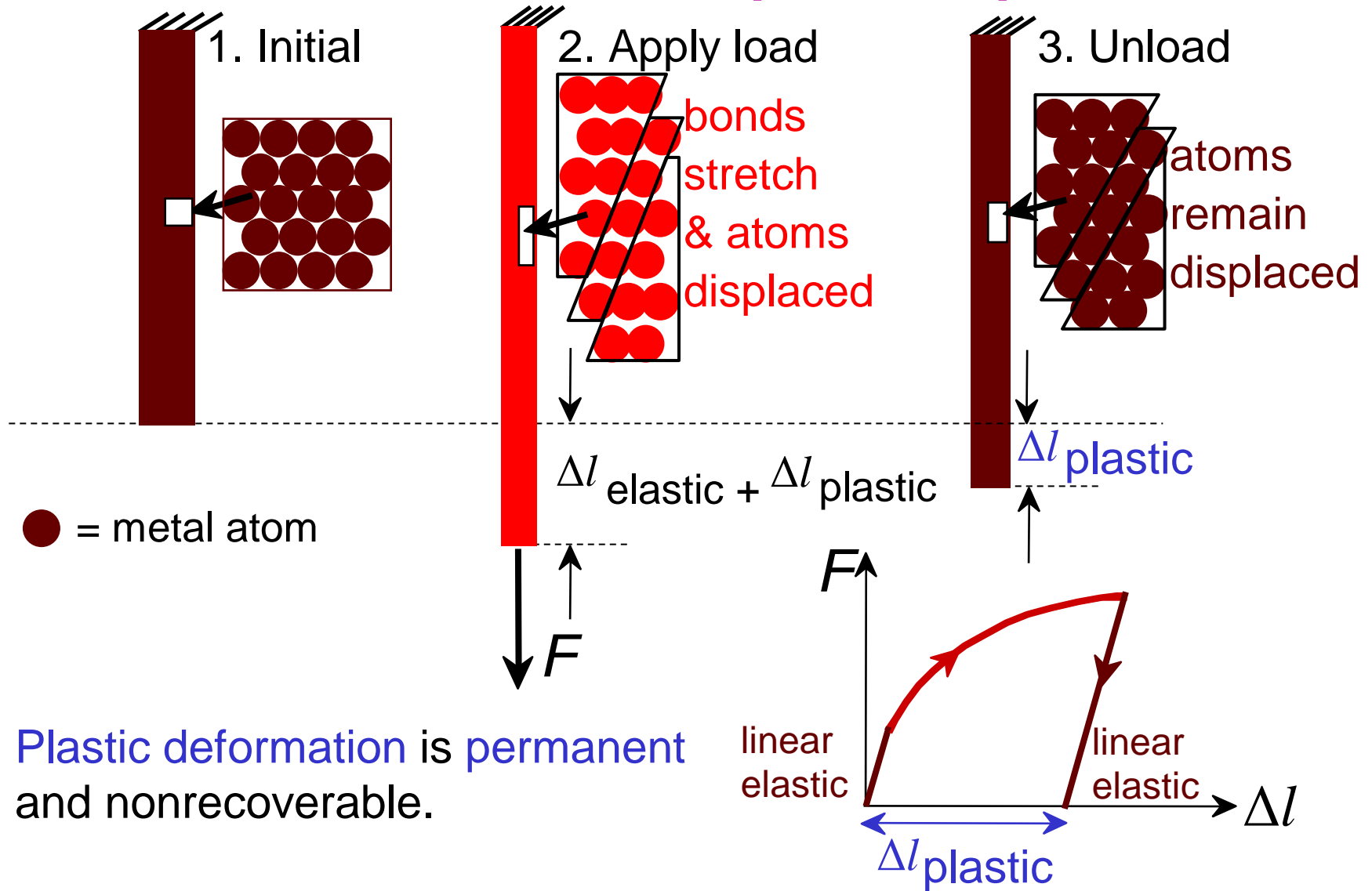
Fig. 6.7, Callister & Rethwisch 10e.

Stress-Strain Curve



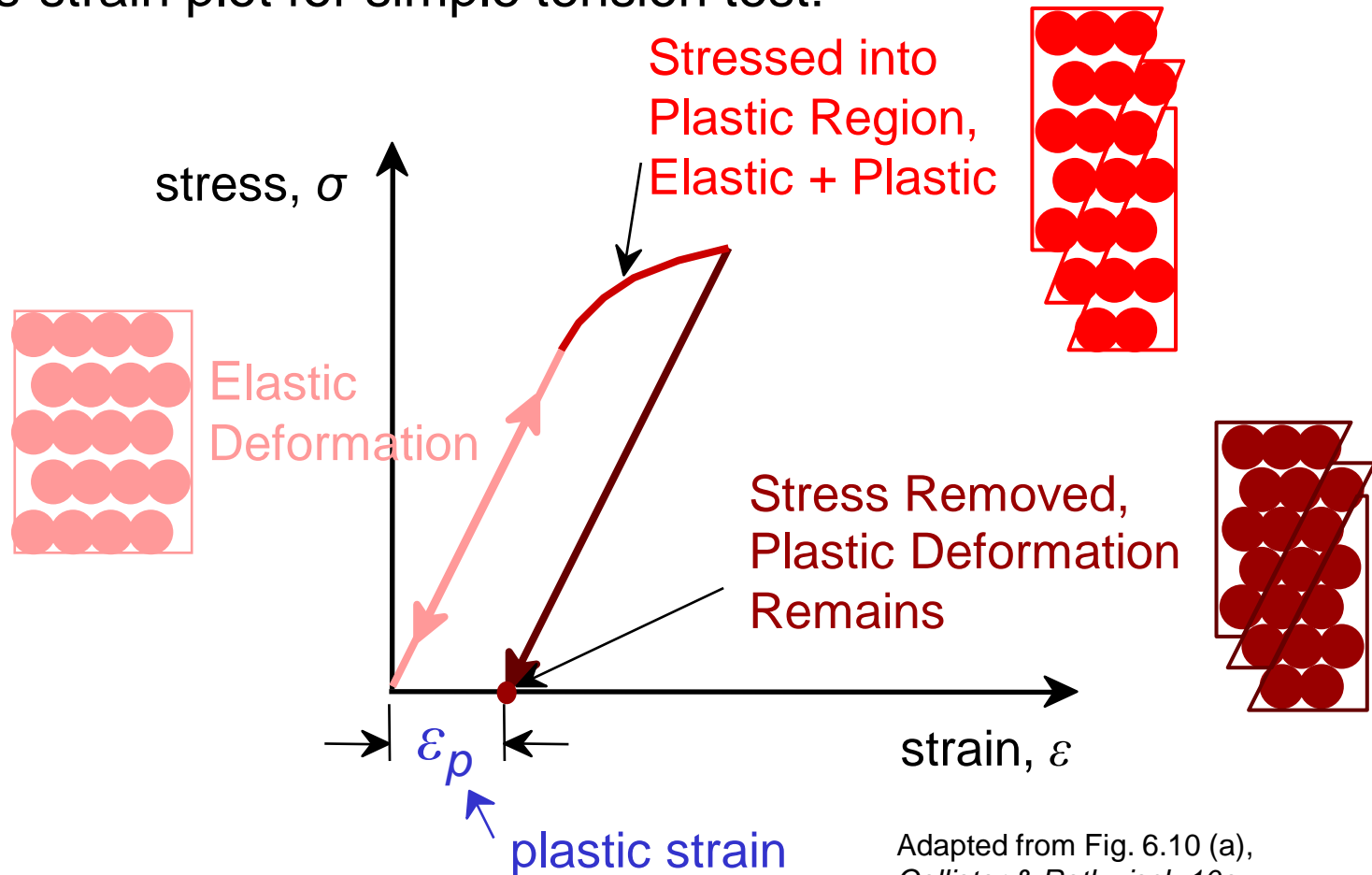
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Plastic Deformation (Metals)



Plastic Deformation

- Plastic Deformation is permanent and nonrecoverable
- Stress-strain plot for simple tension test:



Adapted from Fig. 6.10 (a),
Callister & Rethwisch 10e.

Elastic Strain Recovery

yield strength for 2nd

deformation = σ_{yi} →

initial yield strength = σ_{yo} →

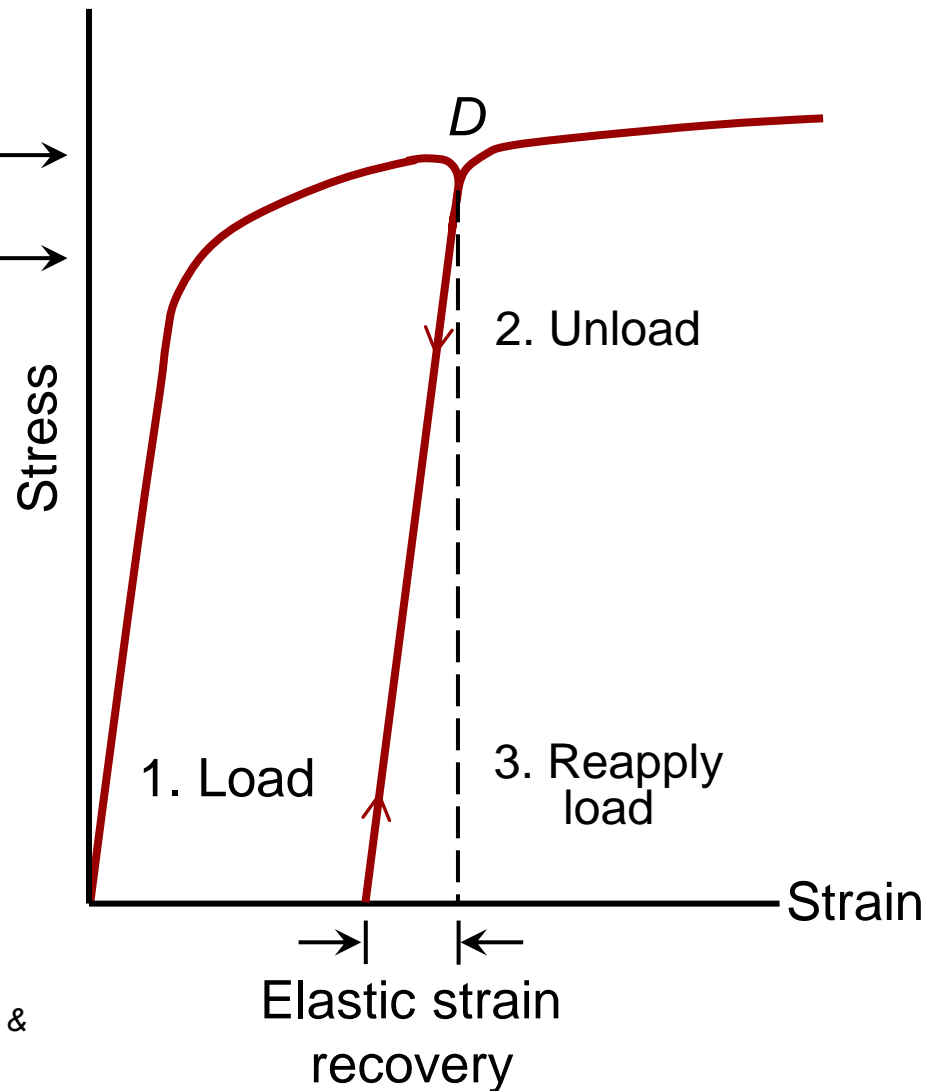


Fig. 6.17, Callister & Rethwisch 10e.

Yield Strength

- Transition from elastic to plastic deformation is gradual
- Yield strength = stress at which *noticeable* plastic deformation has occurred

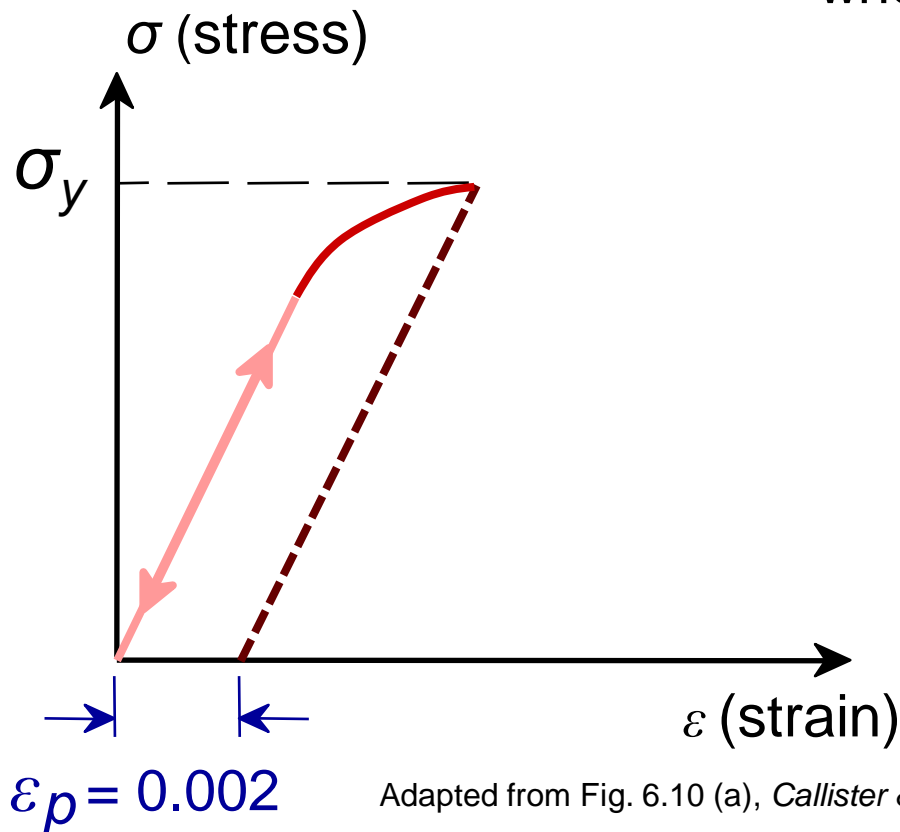
↑
when $\varepsilon_p = 0.002$

$\sigma_y =$ yield strength

Note: for 5 cm sample

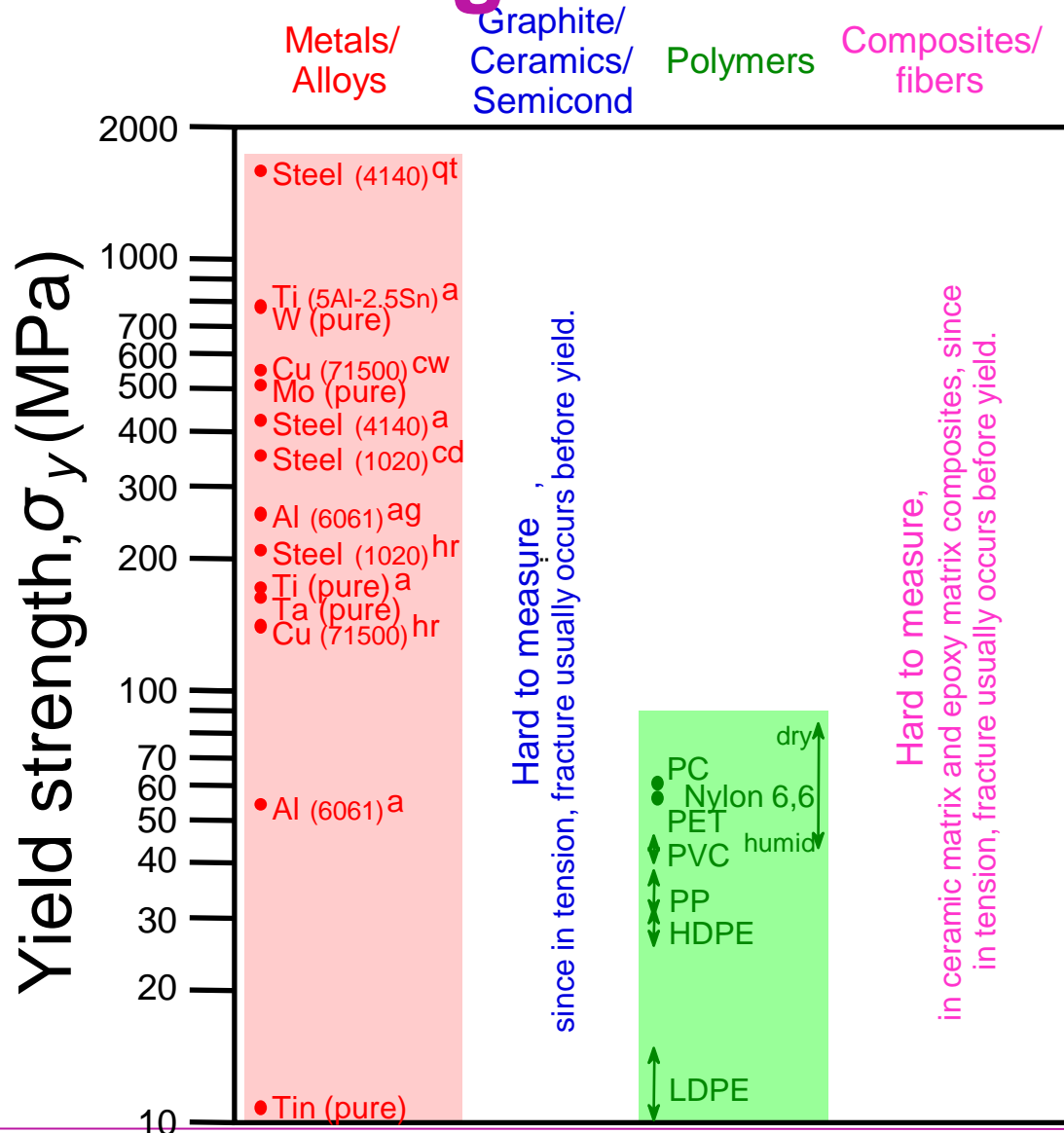
$$\varepsilon = 0.002 = \Delta z / z$$

$$\Delta z = 0.01 \text{ cm}$$



Adapted from Fig. 6.10 (a), Callister & Rethwisch 10e.

Yield Strength – Material Types



Room temperature
values

Based on data in Table B.4,
Callister & Rethwisch 10e.

a = annealed

hr = hot rolled

ag = aged

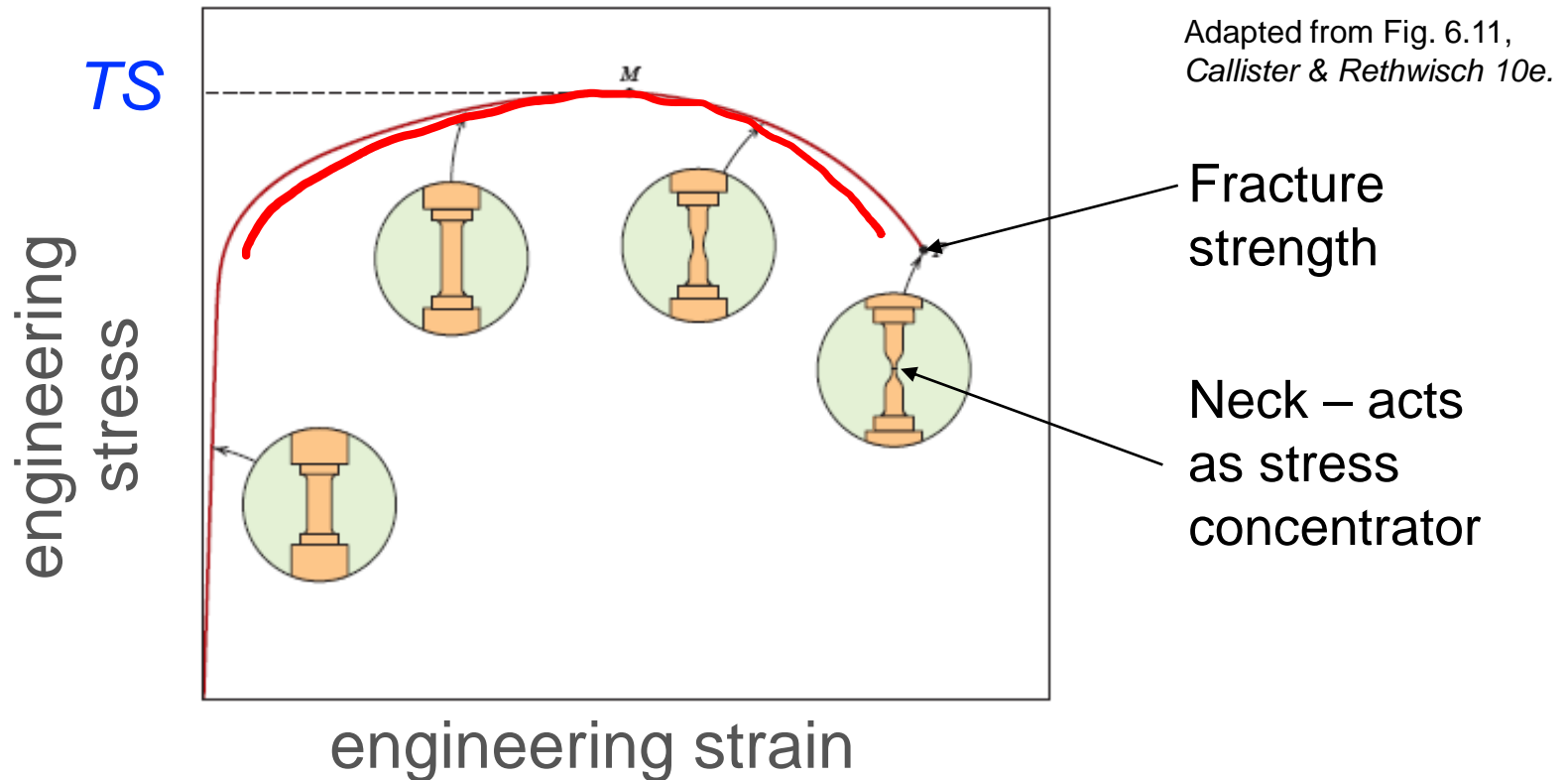
cd = cold drawn

cw = cold worked

qt = quenched & tempered

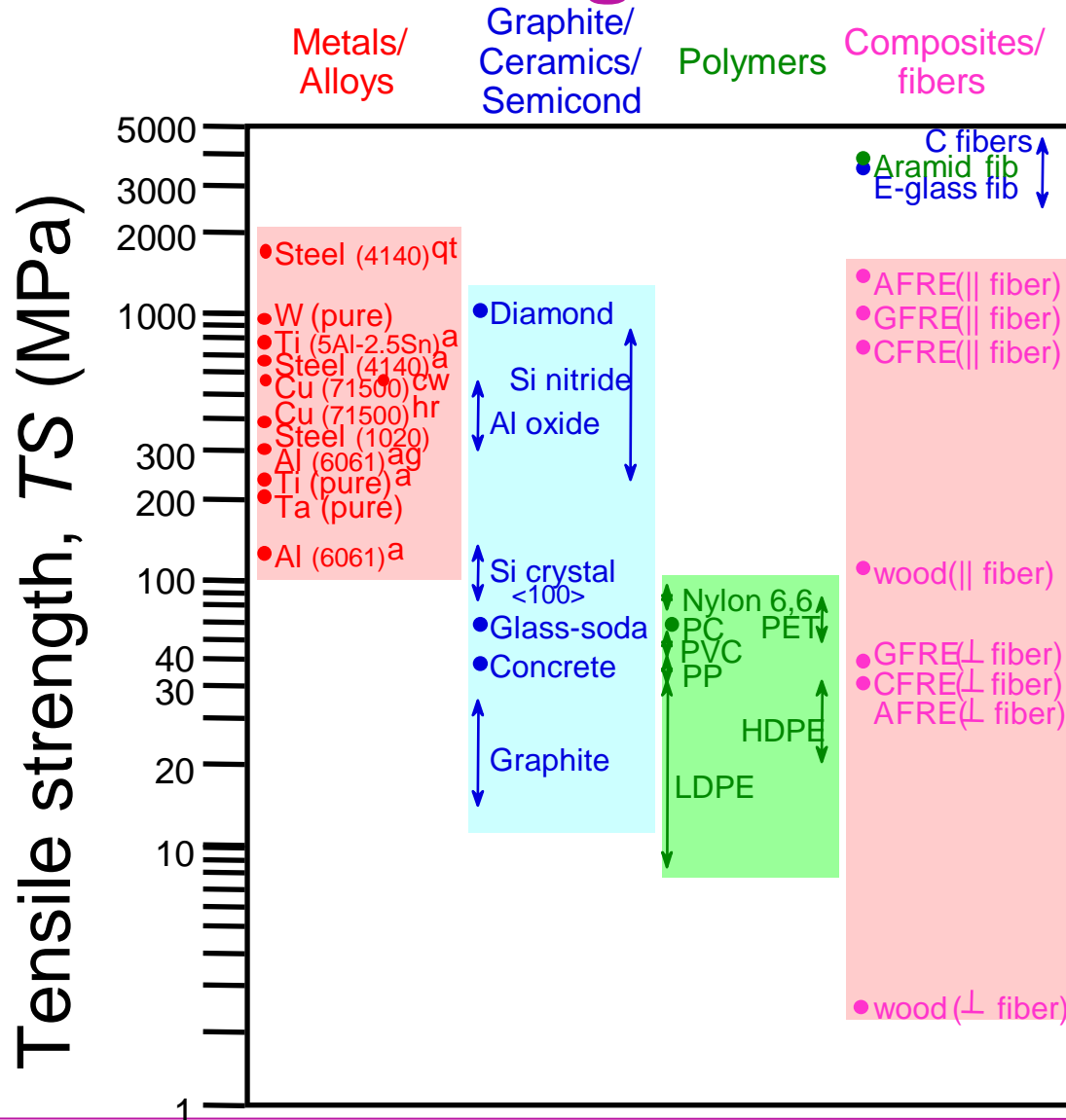
Tensile Strength

- Tensile strength (TS) = maximum stress on engineering stress-strain curve.



- **Metals:** Maximum on stress-strain curve appears at the onset of noticeable **necking**

Tensile Strength – Material Types



Room temperature values

Based on data in Table B4, *Callister & Rethwisch 10e*.

a = annealed

hr = hot rolled

ag = aged

cd = cold drawn

cw = cold worked

qt = quenched & tempered

AFRE, GFRE, & CFRE = aramid, glass, & carbon fiber-reinforced epoxy composites, with 60 vol% fibers.

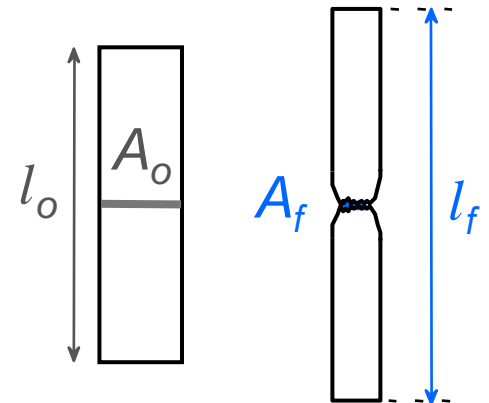
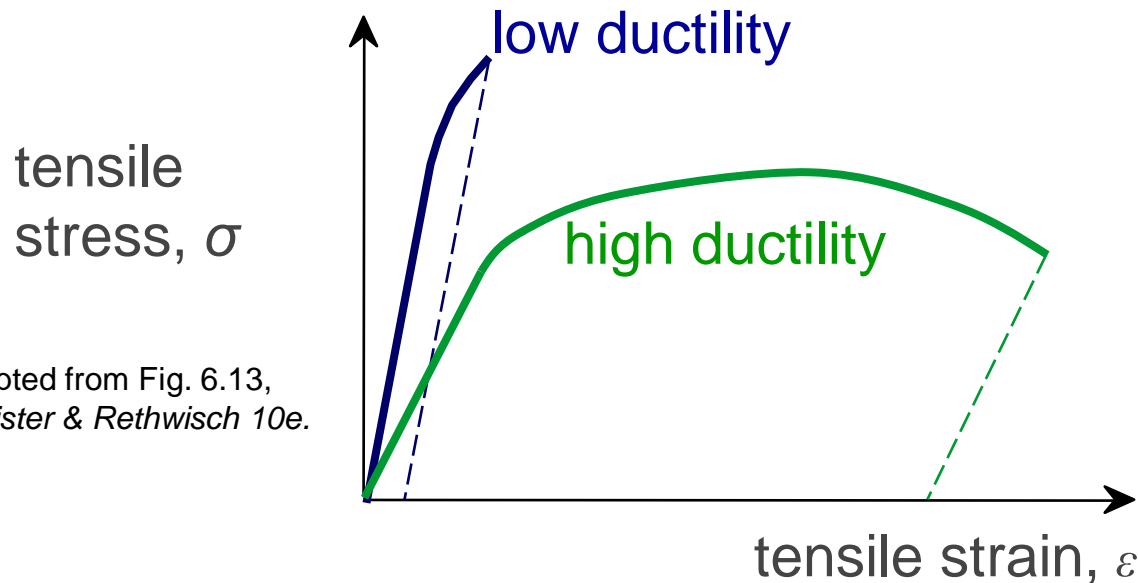
Ductility

- Ductility = amount of plastic deformation at failure:
- Specification of ductility
 - Percent elongation:

$$\%EL = \frac{l_f - l_0}{l_0} \times 100$$

- Percent reduction in area:

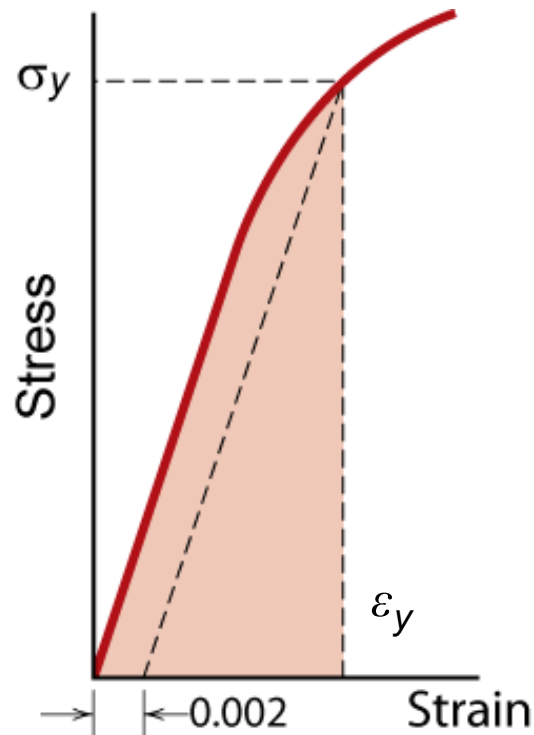
$$\%RA = \frac{A_0 - A_f}{A_0} \times 100$$



Adapted from Fig. 6.13,
Callister & Rethwisch 10e.

Resilience

- ❑ **Resilience**—ability of a material to absorb energy during elastic deformation
- ❑ Energy recovered when load released
- ❑ Resilience specified by **modulus of resilience, U_r**



U_r = Area under stress-strain curve
to yielding = $\int_0^{\epsilon_y} \sigma d\epsilon$

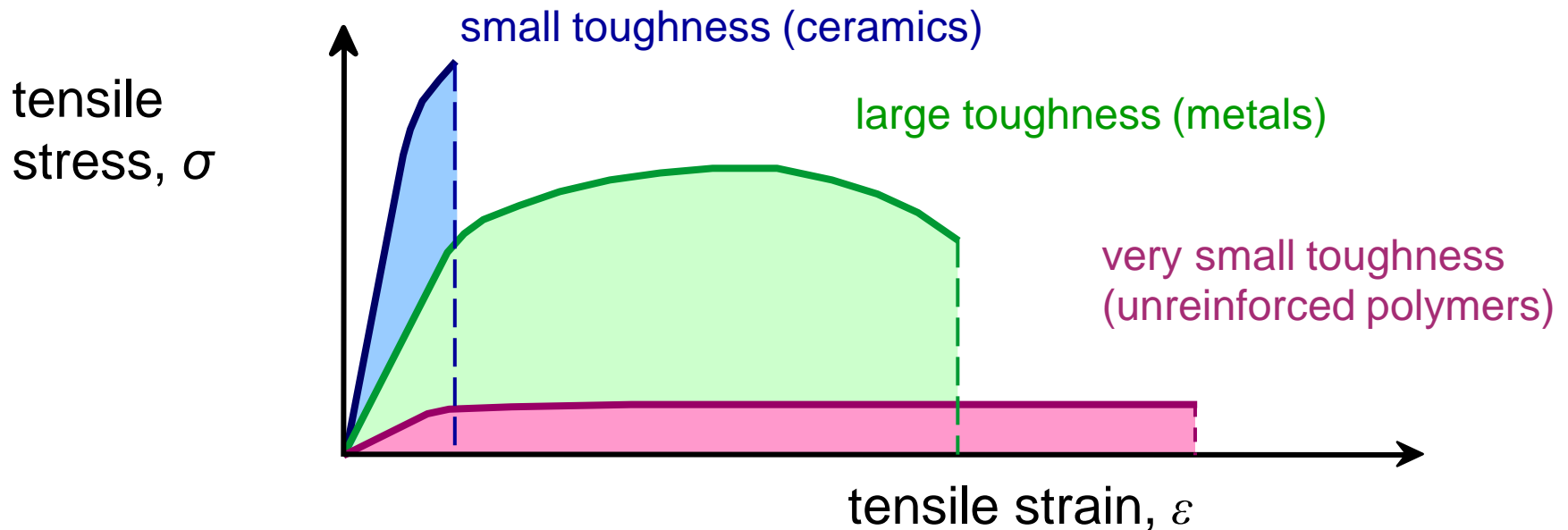
If assume a linear stress-strain
curve this simplifies to

$$U_r \approx \frac{1}{2} \sigma_y \epsilon_y$$

Fig. 6.15, Callister & Rethwisch 10e.

Toughness

- Toughness of a material is expressed in several contexts
- For this chapter, toughness = amount of energy absorbed before fracture
- Approximate by area under the stress-strain curve—units of energy per unit volume



Brittle fracture:

Ductile fracture:

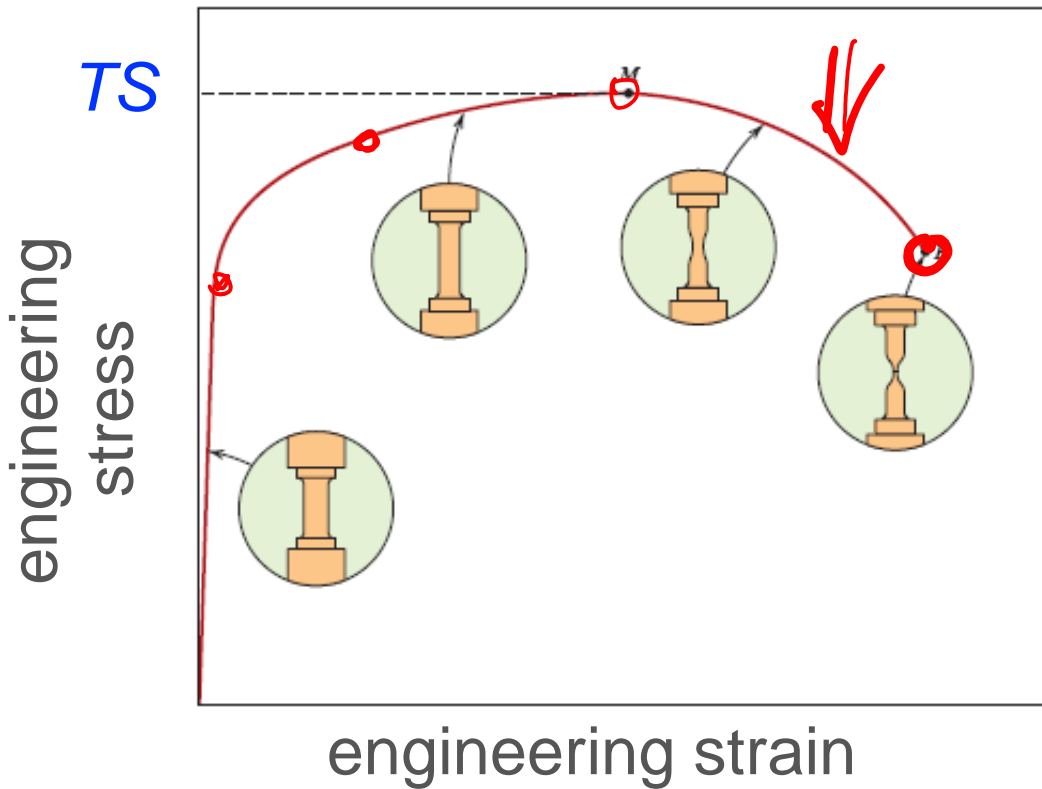
small toughness

large toughness

Are Engineering Stress & Strain Correct?

- ❑ True stress $\sigma_T = F / A$
- ❑ True strain $d\varepsilon_T = dl / L$

where A = instantaneous cross-sectional area
 L = instantaneous length



$$\sigma = \frac{F}{A_o}$$

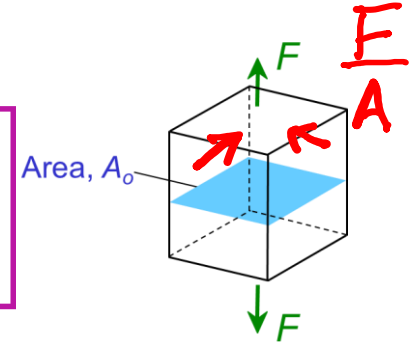


Diagram illustrating the change in length of a material under stress. A rectangular block of initial length l_0 and width d_0 is shown. A green arrow indicates a change in length Δl , and a red arrow indicates a change in width Δd . The resulting length is $l_0 + \Delta l$ and the resulting width is $d_0 + \Delta d$. The diagram is annotated with red handwritten notes: $dl @ dt$ at the top, 4 above the block, and l below the block. The equation $\epsilon_z = \frac{\Delta l}{l_0}$ is written inside the block.

True Stress & True Strain



True Stress & Strain

- True stress $\sigma_T = F / A$ where A = instantaneous cross-sectional area
- True strain $d\varepsilon_T = dl / L$ L = instantaneous length

Volume consistency

$$L \cdot A = L_0 \cdot A_0 = V_c$$

$$A = \frac{L_0 \cdot A_0}{L}$$

$$\sigma_T = \frac{F}{A} = \frac{F \cdot L}{L_0 \cdot A_0} = \sigma \cdot \frac{L}{L_0} = \sigma \cdot \frac{L_0 + \Delta L}{L_0}$$

$$\sigma_T = \sigma (1 + \varepsilon)$$

True Stress & Strain

- True stress $\sigma_T = F / A$ where A = instantaneous cross-sectional area
- True strain $\underline{d\varepsilon_T} = \underline{dl} / L$ L = instantaneous length

$$\varepsilon_T = \int \frac{dl}{L} = \int_{L_0}^L \frac{1}{L} dl$$

$$= \ln L - \ln L_0$$

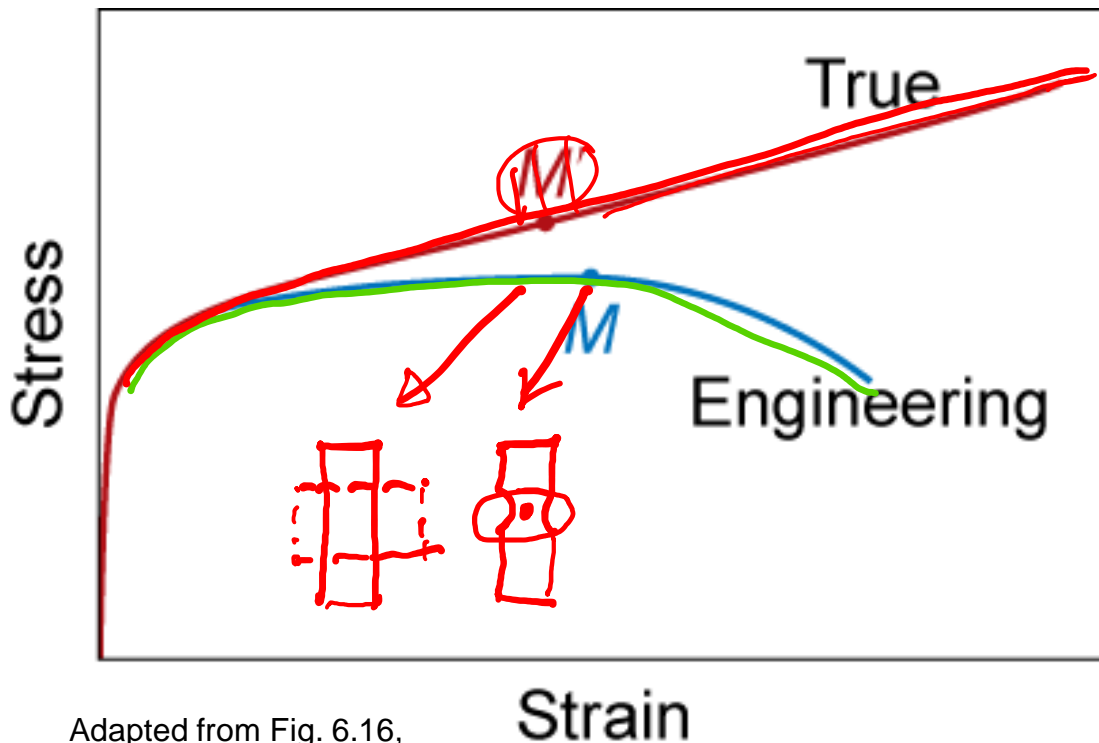
$$= \ln \frac{L}{L_0} = \ln \frac{L_0 + \Delta L}{L_0}$$

$$\varepsilon_T = \ln(1 + \varepsilon)$$

$$y = \int \frac{1}{x} dx \\ = \ln x$$

True Stress & Strain

- True stress $\sigma_T = F / A$ where A = instantaneous cross-sectional area
- True strain $d\varepsilon_T = dl / L$ L = instantaneous length



$$S_T = S(1 + e)$$
$$e_T = \ln(1 + e)$$

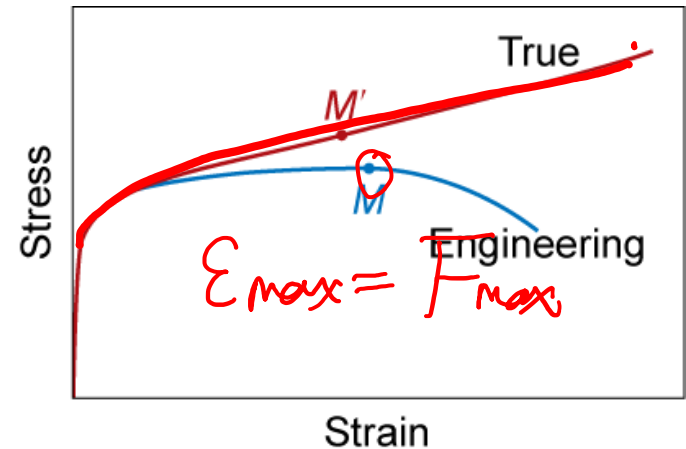
Conversion Equations:
valid only to the onset
of necking

Adapted from Fig. 6.16,
Callister & Rethwisch 10e.

Why is there necking?

□ True stress $\sigma_T = F / A$

□ True strain $d\varepsilon_T = dl / L$



$$\bullet F = \sigma_T \cdot (\hat{A}) \quad F_{\max} \Rightarrow dF = 0$$

$$dF = d\sigma_T \cdot A + \sigma_T \cdot dA = 0$$

$$\frac{d\sigma_T \cdot A}{\sigma_T} + \frac{\sigma_T \cdot dA}{A} = 0$$

$$\frac{d\sigma_T}{\sigma_T} = -\frac{dA}{A} \quad (1)$$

$$\boxed{\frac{d\sigma_T}{\sigma_T} = \frac{dL}{L} = d\varepsilon_T}$$

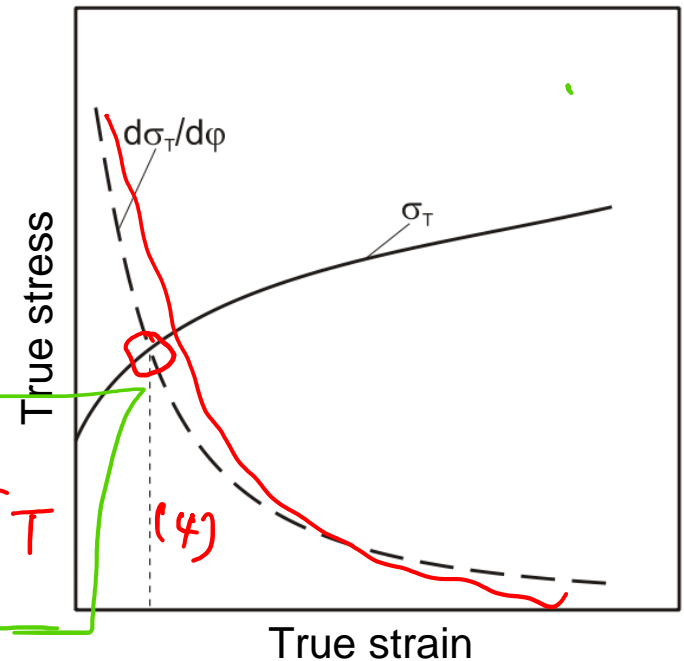
$$\bullet V_c = L_0 \cdot A_0 = L \cdot A \Rightarrow dV = 0 \Rightarrow \frac{dL}{L} = -\frac{dA}{A} \quad (2)$$

$$dV = dL \cdot A + L \cdot dA$$

Considère criterion

- True stress $\sigma_T = F / A$
- True strain $d\varepsilon_T = dl / L$

$$\frac{d\sigma_T}{\sigma_T} = d\varepsilon_T \Rightarrow \left[\begin{array}{l} d\sigma_T > \\ d\varepsilon_T < \end{array} \right] = \sigma_T$$



$$\varepsilon_T = \ln(1 + \varepsilon)$$

$$d\varepsilon_T = \frac{1}{1 + \varepsilon} \cdot d\varepsilon \quad (3)$$

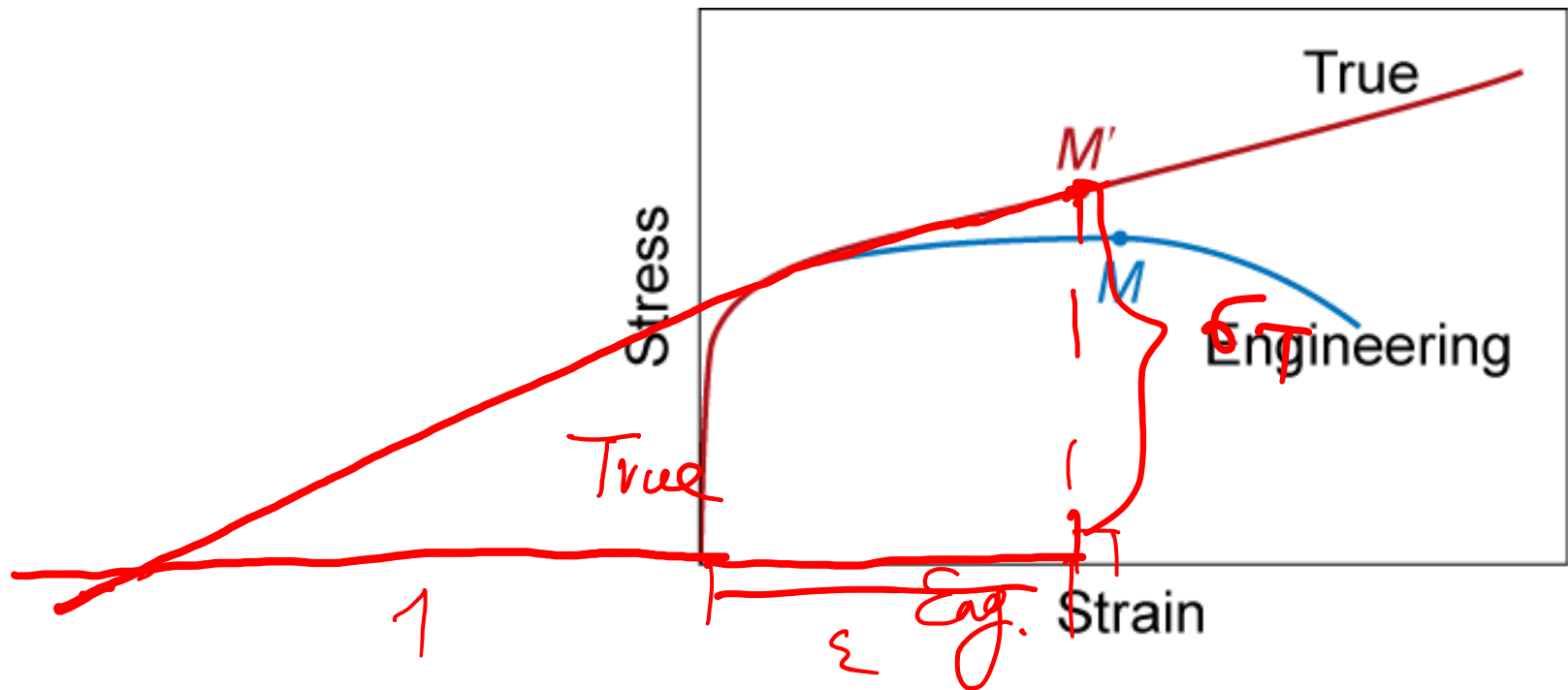
$$\frac{d\sigma_T}{\frac{d\varepsilon}{1 + \varepsilon}} = \sigma_T \Rightarrow \frac{d\sigma_T}{d\varepsilon} = \frac{\sigma_T}{1 + \varepsilon}$$

Considère criterion II

$$\frac{d\sigma_T}{d\varepsilon} = \frac{\sigma_T}{1+\varepsilon}$$

$$\sigma_T = \sigma(1+\varepsilon)$$

$$\varepsilon_T = \ln(1+\varepsilon)$$

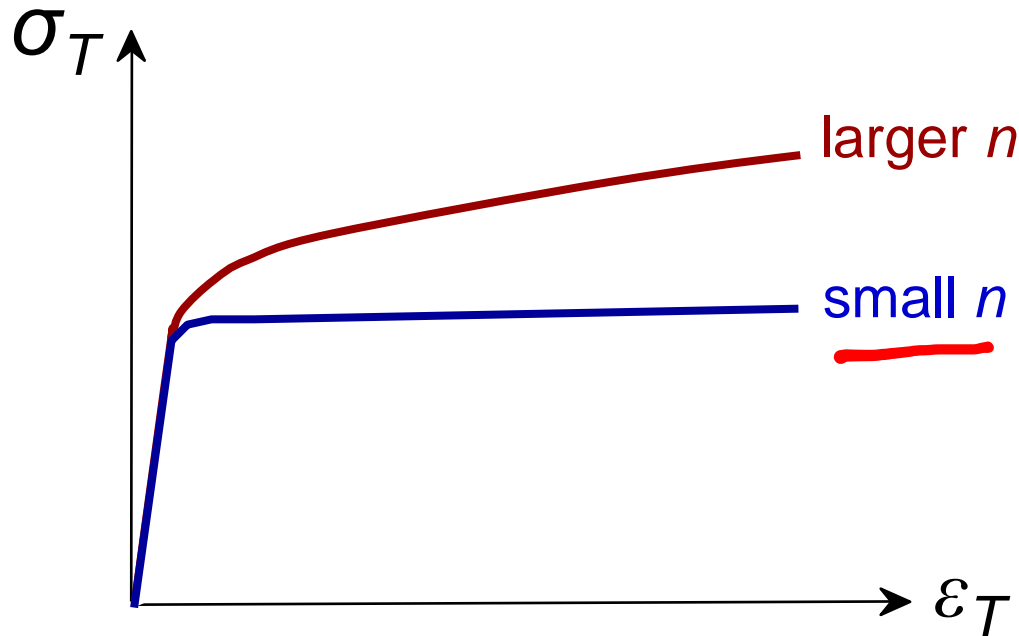


True Stress-True Strain Relationship

- Most alloys, between point of yielding and onset of necking

$$\sigma_T = K(\varepsilon_T)^n$$

- n and K values depend on alloy and treatment
- n = strain-hardening exponent
- $n < 1.0$
- σ_T vs. ε_T -- influence of n .



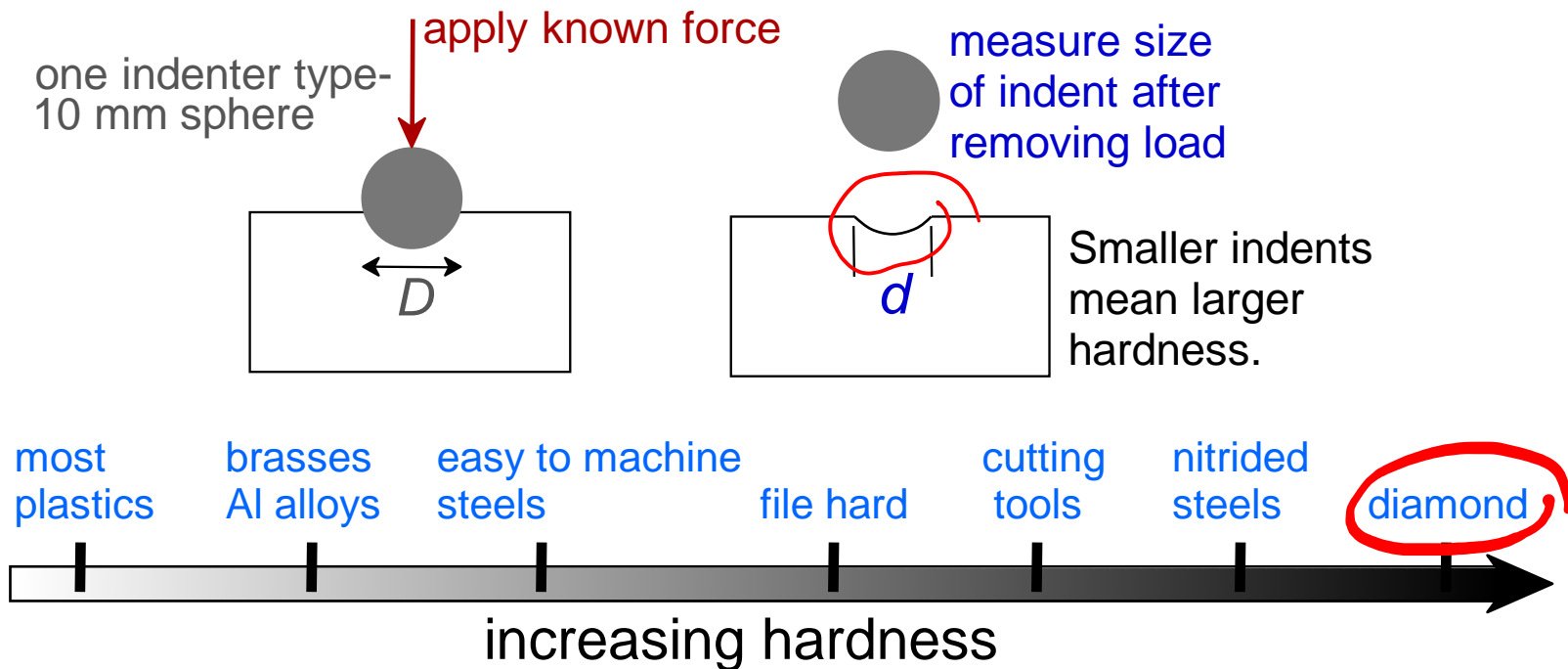
$$\frac{d\sigma_T}{d\varepsilon_T}$$

Hardness



Hardness

- Measure of resistance to surface plastic deformation—indentation or scratch.
- Large hardness means:
 - high resistance to deformation from compressive loads.
 - better wear properties.

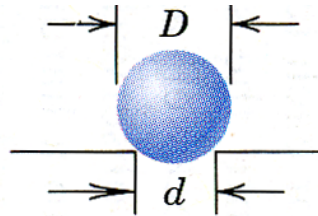


Measurement of Hardness

Brinell Hardness

- ❑ Single scale
- ❑ Brinell hardness designation: (hardness reading) HB

10-mm sphere
of steel or
tungsten carbide



$$\text{HB} = \frac{2P}{\pi D [D - \sqrt{D^2 - d^2}]}$$

- $P = \text{load (kg)}$
- $500 \text{ kg} \leq P \leq 3000 \text{ kg}$ (500 kg increments)
- Relationships—Brinell hardness & tensile strength
 - $TS \text{ (psia)} = 500 \times \text{HB}$
 - $TS \text{ (MPa)} = 3.45 \times \text{HB}$

Variability of Material Properties

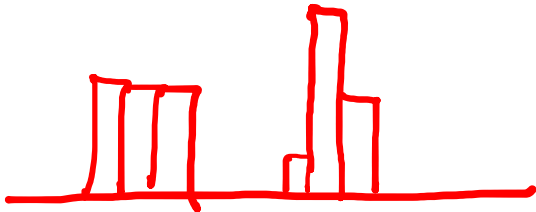
- ❑ Measured material properties—always scatter in values for same material
- ❑ Statistical treatments
- ❑ Typical value—take average value, \bar{X} for some parameter x :

n = number of measurements

x_i = specific measured value

$$\bar{X} = \frac{\sum_{i=1}^n x_i}{n}$$

- ❑ Degree of scatter—use standard deviation, s

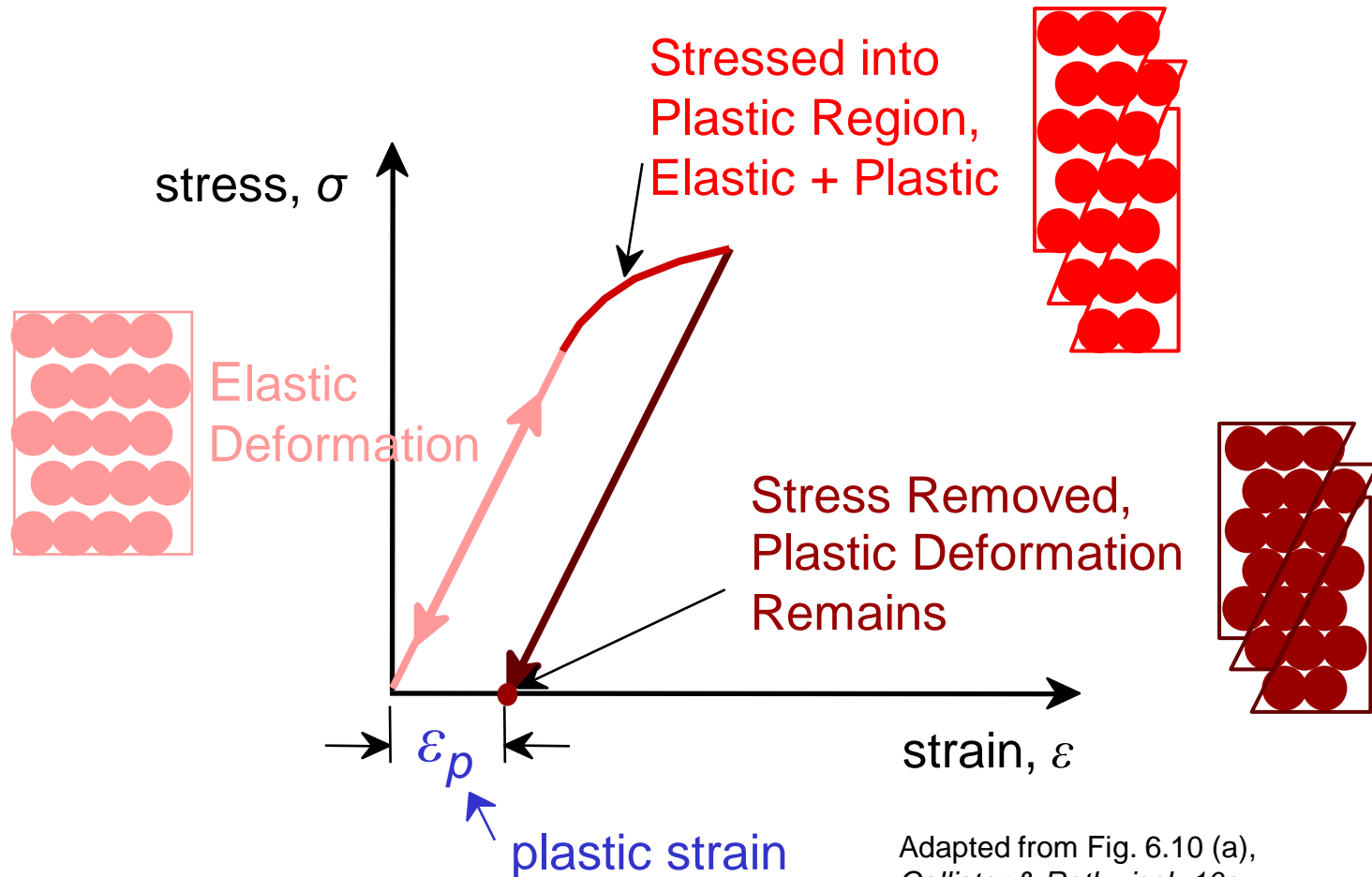


$$s = \left[\frac{\sum_{i=1}^n (x_i - \bar{X})^2}{n - 1} \right]^{\frac{1}{2}}$$

Summary so far

- ❑ Applied mechanical force => normalized to **stress**; and Degree of deformation => normalized to **strain**
- ❑ Deformation is classified into **elastic** deformation and **plastic** deformation:
 - ❑ **non-permanent**; low levels of stress
 - ❑ **permanent**; higher levels of stress
 - ❑ stress-strain behavior is **linear**
 - ❑ stress-strain behavior is **nonlinear**
- ❑ **Stiffness** is a material's resistance to elastic deformation
 - ❑ elastic (or Young's) modulus
- ❑ **Strength** is a material's resistance to plastic deformation
 - ❑ yield and tensile strengths
- ❑ **Ductility** is amount of plastic deformation at failure
 - ❑ percentage of elongation, reduction in area
- ❑ **Hardness** is a resistance to localized surface deformation & compressive stresses
 - ❑ Brinell harnesses

What happened during plastic deformation?



Adapted from Fig. 6.10 (a),
Callister & Rethwisch 10e.

Questions?