

INDIAN INSTITUTE OF TECHNOLOGY, DELHI
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COD892
MTP-1 : Wrinkle Homogenization



DISCUSSION GUIDED BY
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Topic 1

Aug 1 - Aug 31 : Equations for Energy based iterative simulation of Rope

Approach

$x : R \rightarrow R$ where x (curve equation) is parameterised over arc-length s .

Let the arc-length s changes over 0 to l along the curve. And the discrete points under consideration be $x_0 = x(s_0 = 0)$, $x_1 = x(s_1)$, ... $x_n = x(s_n = l)$. Hence, $s_i = i * l/n$.

Unit tangent vector \hat{T} :

Curvature k calculations

$$k(s) = \left| \frac{d(\frac{dx}{ds})}{ds} \right| = \left| \frac{d^2 \mathbf{x}}{ds^2} \right|$$

Structural spring energy calculations : We have spring force $F_i = k_s(|x_i - x_{i-1}| - l)\hat{\mathbf{T}}$. Where l is curve length between points x_i and x_{i-1} . Thus, stress $\sigma(s)$ and Energy per unity length $e(s)$ can be written as

$$\sigma(s) = \left| \lim_{l \rightarrow 0} \frac{k_s(|x_i - x_{i-1}| - l)\hat{\mathbf{T}}}{l} \right| = \left| k_s \left(\left| \frac{dx}{ds} \right| - 1 \right) \hat{\mathbf{T}} \right| = k_s \left(\left| \frac{dx}{ds} \right| - 1 \right)$$
$$\frac{dU}{ds} = e(s) = \frac{\sigma^2}{2k} = \frac{k_s}{2} \left(\left| \frac{dx}{ds} \right| - 1 \right)^2$$

Bending energy calculations : (Couldn't find proof but got the gist)

$$\frac{dU}{ds} = e(s) = \frac{k_b}{2} \left| \frac{d^2 x}{ds^2} \right|^2$$

Total energy calculation U and here $\delta = l/n$

$$U = \sum_{i=1}^n U_i = \sum_{i=1}^n \left(\frac{k_s}{2} \left(\left| \frac{\vec{x}_i - \vec{x}_{i-1}}{\delta} \right| - 1 \right)^2 + \frac{k_b}{2} \left| \frac{\vec{x}_{i+1} + \vec{x}_{i-1} - 2\vec{x}_i}{\delta^2} \right|^2 \right) \delta$$

Force calculations (F_i here is internal force):

$$\vec{F}_i = -\frac{\delta U}{\delta x_i}$$

Here we need to find terms in U with variable x_i in them

$$\vec{F}_{i,struct} = -k_s \left((|\vec{x}_i - \vec{x}_{i-1}| - \delta) \frac{\vec{x}_i - \vec{x}_{i-1}}{|\vec{x}_i - \vec{x}_{i-1}|} + (|\vec{x}_i - \vec{x}_{i+1}| - \delta) \frac{\vec{x}_i - \vec{x}_{i+1}}{|\vec{x}_i - \vec{x}_{i+1}|} \right)$$
$$\vec{F}_{i,bend} = \frac{-k_b}{\delta^3} \left(2 * (2\vec{x}_i - \vec{x}_{i+1} - \vec{x}_{i-1}) + (\vec{x}_i + \vec{x}_{i-2} - 2\vec{x}_{i-1}) + (\vec{x}_i + \vec{x}_{i+2} - 2\vec{x}_{i+1}) \right)$$

$\vec{F}_{i,str}$ and $\vec{F}_{i,bend}$ consists of 2 and 3 terms respectively. But, depending on the edges cases some of the terms in $\vec{F}_{i,str}$ and $\vec{F}_{i,bend}$ will be ignored.

$$\vec{F}_i = \vec{F}_{i,str} + \vec{F}_{i,bend}$$

acceleration

$$\vec{a}_i = \frac{\vec{F}_i + \vec{F}_{ext}}{m_i}$$

velocity : \vec{v}_i^k is velocity of i th point in k th iteration

$$\vec{v}_i^k = \vec{a}_i^k t + \vec{v}_i^{k-1}$$

position : \vec{x}_i^k is position of i th point in k th iteration

$$\vec{x}_i^k = \vec{v}_i^k t + \vec{x}_i^{k-1}$$

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Topic 2

Sept 5 - Present : Position, Amplitude and Phase variation mechanism for simulation

Approach

Equation of rope looks like

$$x(s, t) = sx_n(t) + (1 - s)x_0(t) + (sa_n(t) + (1 - s)a_0(t))\sin(s\phi_n(t) + (1 - s)\phi_0(t)) * \hat{n}$$

Potential Energy evaluation will look like,

$$\frac{dU}{ds} = \frac{k_s}{2} \left(\left| \frac{dx}{ds} \right| - 1 \right)^2 + \frac{k_b}{2} \left| \frac{d^2x}{ds^2} \right|^2$$

Assuming, derivative of $x_0, x_n, a_0, a_n, \phi_0, \phi_n, \hat{n}$ w.r.t s is 0,

$$\begin{aligned} \frac{dx}{ds} &= -x_0(t) + x_1(t) + \\ &\hat{n}(-\phi_0(t) + \phi_n(t))(sa_n(t) + (1 - s)a_0(t))\cos(s\phi_n(t) + (1 - s)\phi_0(t)) + \\ &\hat{n}(a_n(t) - a_0(t))\sin(s\phi_n(t) + (1 - s)\phi_0(t)) \end{aligned} \quad (1)$$

(2)

$$\begin{aligned} \left| \frac{dx}{ds} \right|^2 &= |x_0|^2 - 2x_0.x_n + |x_n|^2 + \\ &(\phi_n - \phi_0)^2 * (sa_n + (1 - s)a_0)^2 \cos^2(s\phi_n + (1 - s)\phi_0) + \\ &(a_n - a_0)^2 \sin^2(s\phi_n + (1 - s)\phi_0) \end{aligned} \quad (3)$$

$$\left| \frac{d^2x}{ds^2} \right|^2 = (2(a_n - a_0) * (\phi_n - \phi_0) * \cos(s\phi_n + (1 - s)\phi_0) - (\phi_n - \phi_0)^2 * (sa_n + (1 - s)a_0) * \sin(s\phi_n + (1 - s)\phi_0))^2$$

$$U = \int_0^1 \frac{k_s}{2} \left(\left| \frac{dx}{ds} \right| - 1 \right)^2 ds + \int_0^1 \frac{k_b}{2} \left| \frac{d^2x}{ds^2} \right|^2 ds$$

Evaluating integral $\int \left| \frac{dx}{ds} \right|^2 ds$, from this point $lerp(a) = lerp(a_0, a_n, s)$ and $\Delta a = a_n - a_0$

$$\begin{aligned} \int \left| \frac{dx}{ds} \right|^2 ds &= (|x_0|^2 - 2x_0.x_n + |x_n|^2)s + \\ &\Delta^2 \phi \left\{ lerp^2(a) \left(\frac{s}{2} + \frac{\sin(lerp(2\phi))}{4\Delta\phi} \right) + s^2 \Delta a \left(\frac{s\Delta a}{3} + \frac{a_0}{2} \right) + \right. \\ &\cos(lerp(2\phi)) \left(\frac{a_0 \Delta a}{4\Delta^2 \phi} + \frac{\Delta^2 a}{4\Delta^2 \phi} \right) - \sin(lerp(2\phi)) \frac{\Delta^2 a}{8\Delta^3 \phi} \left. \right\} + \\ &\Delta^2 a \left(\frac{s}{2} - \frac{\sin(lerp(2\phi))}{4\Delta\phi} \right) \end{aligned} \quad (4)$$

$$\begin{aligned}
\int \left| \frac{d^2x}{ds^2} \right|^2 ds &= 4\Delta^2 a \Delta^2 \phi \left(\frac{s}{2} + \frac{\sin(\text{lerp}(2a))}{4\Delta a} \right) + \Delta^4 \phi \left(s a_0^2 + s^2 a_0 \Delta a + \frac{s^3 \Delta a^2}{3} \right) \\
&+ 2\Delta a \Delta^3 \phi \left(\frac{a_0 \cos(\text{lerp}(2\phi))}{2\Delta \phi} + \frac{s \Delta a \cos(\text{lerp}(2\phi))}{2\Delta \phi} - \frac{\Delta a \sin(\text{lerp}(2\phi))}{4\Delta \phi^2} \right) \\
&- \Delta^4 \phi \left\{ \text{lerp}^2(a) \left(\frac{s}{2} + \frac{\sin(\text{lerp}(2\phi))}{4\Delta \phi} \right) + s^2 \Delta a \left(\frac{s \Delta a}{3} + \frac{a_0}{2} \right) + \right. \\
&\left. \cos(\text{lerp}(2\phi)) \left(\frac{a_0 \Delta a}{4\Delta^2 \phi} + \frac{\Delta^2 a}{4\Delta^2 \phi} \right) - \sin(\text{lerp}(2\phi)) \frac{\Delta^2 a}{8\Delta^3 \phi} \right\}
\end{aligned} \tag{5}$$

If $|\frac{dx}{ds}| > 1$ always then $\int_0^1 |\frac{dx}{ds}|^2 ds \leq 1 + \int_0^1 (|\frac{dx}{ds}| - 1)^2 ds$ ■

Topic 3

Oct 1 - Present : Lagrangian mechanics: Potential Energy

Approach

Equation of rope looks like

$$x(s, t) = sx_1(t) + (1 - s)x_0(t) + (sa_1(t) + (1 - s)a_0(t))\sin(s\phi_1(t) + (1 - s)\phi_0(t)) * \hat{n}$$

$\Delta\phi = \phi_1 - \phi_0$ and $\phi_s = \text{lerp}(\phi_0, \phi_1, s)$. Similarly for a:

$$\frac{dx}{ds} = x_1 - x_0 + ((\Delta\phi)(a_s)\cos(\phi_s) + (\Delta a)\sin(\phi_s)) * \hat{n}$$

$$\left| \frac{dx}{ds} \right| = \sqrt{|x_1 - x_0|^2 + ((\Delta\phi)(a_s)\cos(\phi_s) + (\Delta a)\sin(\phi_s))^2}$$

$$\left| \frac{dx}{ds} \right| \approx |x_1 - x_0| + \frac{((\Delta\phi)(a_s)\cos(\phi_s) + (\Delta a)\sin(\phi_s))^2}{2|x_1 - x_0|}$$

$$\left| \frac{dx}{ds} \right|^2 = |x_1 - x_0|^2 + ((\Delta\phi)(a_s)\cos(\phi_s) + (\Delta a)\sin(\phi_s))^2$$

$$\left| \frac{d^2x}{ds^2} \right| = 2(\Delta a)(\Delta\phi)\cos(\phi_s) - (\Delta\phi)^2(a_s)\sin(\phi_s)$$

$$\left| \frac{d^2x}{ds^2} \right|^2 = 4(\Delta a)^2(\Delta\phi)^2(\cos^2(\phi_s)) + (\Delta\phi)^4(a_s)^2\sin^2(\phi_s) - 2 * (\Delta a)(\Delta\phi)^3\sin(2\phi_s)$$

Potential Energy evaluation is,

$$\frac{dU}{ds} = \frac{k_s}{2} \left(\left| \frac{dx}{ds} \right| - 1 \right)^2 + \frac{k_b}{2} \left| \frac{d^2x}{ds^2} \right|^2$$

$$U = \int_0^1 \frac{k_s}{2} \left(\left| \frac{dx}{ds} \right| - 1 \right)^2 ds + \int_0^1 \frac{k_b}{2} \left| \frac{d^2x}{ds^2} \right|^2 ds$$

$$U = \int_0^1 \frac{k_s}{2} \left(\left| \frac{dx}{ds} \right|^2 - 2 * \left| \frac{dx}{ds} \right| + 1 \right) ds + \int_0^1 \frac{k_b}{2} \left| \frac{d^2x}{ds^2} \right|^2 ds$$

$$U = \int_0^1 \frac{k_s}{2} (|x_1 - x_0|^2 + ((\Delta\phi)(a_s)\cos(\phi_s) + (\Delta a)\sin(\phi_s))^2 - 2 * (|x_1 - x_0| + \frac{((\Delta\phi)(a_s)\cos(\phi_s) + (\Delta a)\sin(\phi_s))^2}{2|x_1 - x_0|}) + 1) ds + \int_0^1 \frac{k_b}{2} 4(\Delta a)^2(\Delta\phi)^2(\cos^2(\phi_s)) + (\Delta\phi)^4(a_s)^2\sin^2(\phi_s) - 2 * (\Delta a)(\Delta\phi)^3\sin(2\phi_s) ds$$

$$U = \int_0^1 \frac{k_s}{2} \left((|x_1 - x_0| - 1)^2 + ((\Delta\phi)(a_s)\cos(\phi_s) + (\Delta a)\sin(\phi_s))^2 - \frac{((\Delta\phi)(a_s)\cos(\phi_s) + (\Delta a)\sin(\phi_s))^2}{|x_1 - x_0|} \right) ds + \int_0^1 \frac{k_b}{2} (4(\Delta a)^2(\Delta\phi)^2(\cos^2(\phi_s)) + (\Delta\phi)^4(a_s)^2\sin^2(\phi_s) - 2(\Delta a)(\Delta\phi)^3\sin(2\phi_s)) ds$$

$$U = \int_0^1 \frac{k_s}{2} \left((|x_1 - x_0| - 1)^2 + ((\Delta\phi)(a_s)\cos(\phi_s) + (\Delta a)\sin(\phi_s))^2 \left(1 - \frac{1}{|x_1 - x_0|} \right) \right) ds + \int_0^1 \frac{k_b}{2} (4(\Delta a)^2(\Delta\phi)^2(\cos^2(\phi_s)) - (\Delta\phi)^4(a_s)^2\sin^2(\phi_s) - 2(\Delta a)(\Delta\phi)^3\sin(2\phi_s)) ds$$

$$U = \int_0^1 \frac{k_s}{2} \left((|x_1 - x_0| - 1)^2 + ((\Delta\phi)^2(a_s)^2 \cos^2(\phi_s) + (\Delta a)^2 \sin^2(\phi_s) + (\Delta a)(\Delta\phi)a_s \sin(2\phi_s)) \left(1 - \frac{1}{|x_1 - x_0|}\right) \right) ds + \int_0^1 \frac{k_b}{2} (4(\Delta a)^2(\Delta\phi)^2(\cos^2(\phi_s)) + (\Delta\phi)^4(a_s)^2 \sin^2(\phi_s) - 2(\Delta a)(\Delta\phi)^3 \sin(2\phi_s)) ds$$

$$U = \int_0^1 \frac{k_s}{2} ((|x_1 - x_0| - 1)^2 + (\frac{(\Delta\phi)^2(a_s)^2}{2} + \frac{(\Delta a)^2}{2}) (1 - \frac{1}{|x_1 - x_0|})) ds + \int_0^1 \frac{k_b}{2} (2(\Delta a)^2(\Delta\phi)^2 + \frac{(\Delta\phi)^4(a_s)^2}{2}) ds$$

$$U = \frac{k_s}{2} ((|x_1 - x_0| - 1)^2 + (\frac{(\Delta\phi)^2(a_0^2 + a_0 a_1 + a_1^2)}{6} + \frac{(\Delta a)^2}{2}) (1 - \frac{1}{|x_1 - x_0|})) + \frac{k_b}{2} ((2(\Delta a)^2(\Delta\phi)^2 + \frac{(\Delta\phi)^4(a_0^2 + a_0 a_1 + a_1^2)}{6}))$$

[Rahul: Looks OK. Can you collect the two $(\Delta\phi)^2 \dots /6$ terms together? Actually I'm a bit surprised that the second term is there. If $\|x_1 - x_0\| < 1$ (the rope is compressed) then I would expect the terms involving $(\Delta\phi)2a^2$ to always have a negative sign (decrease the energy by buckling).]

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Topic 3

Oct 1 - Present : Lagrangian mechanics: Kinetic Energy

Approach

Equation of rope looks like

$$x(s, t) = sx_1(t) + (1 - s)x_0(t) + (sa_1(t) + (1 - s)a_0(t))\sin(s\phi_1(t) + (1 - s)\phi_0(t)) * \hat{n}$$

$\Delta\phi = \phi_1 - \phi_0$ and $\phi_s = \text{lerp}(\phi_0, \phi_1, s)$. Similarly for a, x :

$$\frac{dx}{dt} = \dot{X} = \dot{x}_s + ((\Delta\dot{\phi}_s)(a_s)\cos(\phi_s) + (\dot{a}_s)\sin(\phi_s)) * \hat{n}$$

$$|\dot{X}|^2 = |\dot{x}_s|^2 + ((\Delta\dot{\phi}_s)(a_s)\cos(\phi_s) + (\dot{a}_s)\sin(\phi_s))^2$$

Kinetic Energy evaluation is,

$$T = \int_0^1 \rho |\dot{X}|^2 ds$$

$$T = \int_0^1 \rho (|\dot{x}_s|^2 + ((\Delta\dot{\phi}_s)(a_s)\cos(\phi_s) + (\dot{a}_s)\sin(\phi_s))^2) ds$$

$$T = \int_0^1 \rho (|\dot{x}_s|^2 + (\Delta\dot{\phi}_s)^2(a_s)^2\cos^2(\phi_s) + (\dot{a}_s)^2\sin^2(\phi_s) + (\Delta\dot{\phi}_s)(a_s)(\dot{a}_s)\sin(2\phi_s)) ds$$

$$T = \int_0^1 \rho (|\dot{x}_s|^2 + \frac{(\Delta\dot{\phi}_s)^2(a_s)^2}{2} + \frac{(\dot{a}_s)^2}{2} + (\Delta\dot{\phi}_s)(a_s)(\dot{a}_s)\sin(2\phi_s)) ds$$

$$T = \rho \left(\frac{|\dot{x}_0|^2 + \dot{x}_0 \cdot \dot{x}_1 + |\dot{x}_1|^2}{3} + \frac{a_0^2(6\dot{\phi}_0^2 + 3\dot{\phi}_0\dot{\phi}_1 + \dot{\phi}_1^2) + a_0a_1(3\dot{\phi}_0^2 + 4\dot{\phi}_0\dot{\phi}_1 + 3\dot{\phi}_1^2) + a_1^2(\dot{\phi}_0^2 + 3\dot{\phi}_0\dot{\phi}_1 + 6\dot{\phi}_1^2)}{60} + \frac{\dot{a}_0^2 + \dot{a}_0\dot{a}_1 + \dot{a}_1^2}{6} \right)$$

[Rahul: Looks OK. Probably we can make some approximations here, after all even in the absence of the buckling model we usually approximate $(\|\dot{x}_0\|^2 + \dot{x}_0 \cdot \dot{x}_1 + \|\dot{x}_1\|^2)/3$ by $(\|\dot{x}_0\|^2 + \|\dot{x}_1\|^2)/2$.]

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