Wear-Resistant TiN - Si₃N₄ Nanocomposites Consolidated By Electric Discharge Sintering

V.G. Kolesnichenko^{1,*} V.T. Varchenko¹, O.B. Zgalat-Lozynskyy¹, M. Herrmann², A.V. Ragulya¹

¹ Frantsevich Institute for problems of Materials Science NASU, Kiev, Ukraine ² IKTS, Winterbergstrasse 28, D-01277 Dresden, Germany

(Received 6 June 2012; published online 19 August 2012)

Dense nanocomposites on the basis of silicon nitride with the size of structural elements less than 150 nm have been consolidated by Electric Discharge Sintering. The improvement of materials properties is expected: wearproofness, fracture toughness ($\sim 5-6$ MPa· $\rm M^{1/2}$), hardness (~ 22 GPa), bend stress (800-1100 MPa), stability to the aggressive environments (acids at a room and high temperatures) as compared to traditional materials which now use as frictional unit.

Keywords: Electric discharge sintering, Nanocomposite, Nanorod, Hardness, Linear wear.

PACS number: 62.20.Qp

1. INTRODUCTION

Electric Discharge Sintering (EDS) is a very fast method to consolidate different materials via direct heating of press instrument together with green pellet by pulse electric current[1, 2]. Presence of pressure makes this method similar to the hot pressing one. The typical scheme of EDS consists of two stages: preliminary and the main. At the preliminary stage relatively low pressure is used to treat the powder. On this stage interparticle contacts play the main role as local overheating takes place here. On the second stage the sample is subjected to a higher pressure; on this stage the

sample is heated by Joule heat. The EDS features help to decrease the process time and temperature as well as to consolidate nanomaterials.

2. EXPERIMENTAL

In our investigation we use silicon nitride and titanium nitride nanopowders (PCT Ltd., Latvia), nanorods of silicon nitride (Nanoamor inc., USA) and their mixtures. Initial powder properties of the nanopowder compositions used in this research are summarized in Table 1.

Table 1 - Properties of the initial nanopowders

Name and an	C	A	Chemical analysis, wt. %	
Nanopowder	Specific surface, m ² /g	Average, nm	[0]	[N]
TiN	25,7	~ 70	1,81	$19,2 \pm 0,3$
Si ₃ N ₄ nanopowder	70	30 - 50	2,1	$38,4 \pm 0,3$
Si ₃ N ₄ nanorod	103	d = 30-70 $1 = 300 - 800$	< 1	-

Mixtures of TiN (nanoparticle) - Si₃N₄ (nanoparticles) - Si₃N₄ (nanorods) were prepared by mixing in the planetary mill (Pulverizette-6, Fritch, Germany), 600 rpm, 4 h. EDS experiments have been carried out using SPS

apparatus FCT-HP D 25 manufactured by FCT Systems GmbH ($T_{max} = 2400$ °C, $P_{max} = 250$ kN, $I_{max} = 8000$ A, $U_{max} = 10$ V, mediums: vacuum $-5 \cdot 10^{-2}$ mbar, nitrogen).

 ${\bf Table~2}-{\bf Nanocomposites~consolidated~by~EDS}$

Nº	Nanocomposite	P, MPa	Heating rate, °C/min.	T, °C	Soak time, min.	ρ, g/cm ³	Open porosity, %
1	$\begin{array}{c} 38,1 \text{ wt. } \% \text{ Si}_3N_4 - 57,1 \text{ wt.} \% \\ \text{TiN} \\ \text{- } 4,8 \text{ wt. } \% \text{ Si}_3N_4 \text{ rods} \end{array}$	50	200	1700	1	3,400	0,0
2	$\begin{array}{c} 16,6 \text{ wt. } \% \text{ Si}_3\text{N}_4 - 66,6 \\ \text{wt. } \% \text{ TiN} - 16,8 \text{ wt. } \% \text{ Si}_3\text{N}_4 \\ \text{rods} \end{array}$	50	200	1600	1	3,140	0,0
3	87,5 в wt. % Si ₃ N ₄ – 12,5 wt. % TiN	50	200	1700	1	2,462	21,7

Regimes of EDS consolidation and characteristics of the sintered nanocomposites are presented in table 2.

The X-ray diffraction method (XRD) was used for the qualitative phase analysis (XRD -7 with Cu K α

radiation, Seifert-FPM, Freiberg, Germany). The particle size distribution of investigated nanopowders was estimated by a light scattering particle size analyzer (Zetasizer 1000 HS, Malvern Instruments, United

^{*} vgk001@ipms.kiev.ua

Kingdom) and by a transmission electron microscope (JEOL JEM-2100F, Japan). Vickers hardness and fracture toughness of sintered composite ceramics were measured at 50 g and 2 kg load conditions by MMT-3 (Buehler, USA) hardness testers. Microstructure of the polished surface of sintered composites was examined by a Field Emission Scanning Electron Microscopy NVision 40 (Carl Zeiss SMT AG, Germany) and HD 2700 (Hitachi, Japan). Density of the SPS consolidated nanocomposites has been measured by Archimedes method in deionised water at room temperature.

3. RESULTS

The typical microstructure of EDS consolidated TiN - Si_3N_4 nanocomposites is presented on fig. 1. As one can observe, grains of TiN (average size $100-150\,\text{nm})$ and Si_3N_4 (average size $\sim70\,\text{nm})$ are distributed homogeneously in the nanocomposite structure.

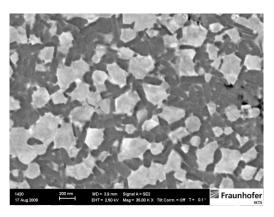


Fig. 1 – Microstructure of EDS consolidated $\mathrm{Ti}N-\mathrm{Si}_3N_4$ nanocomposite

Consolidated nanocomposites were tested on wear resistance at unlubricated friction in the pair with steel 15. All composites with Si₃N₄ nanorod additives showed good wear resistance and relatively low friction coefficient (Fig. 2-3).

It should be mentioned that the wear of friction pair is mainly determined by the wear of counterbody: the gravimetric wear of samples makes ~ 0.3 -0.5 mg/km and depends on loading, and a gravimetric wear of counterbody is in a range of 1-5 mg/km and increases with loading increase. The most preferable composite to use in the condition of high loads and wear in pair with steel 15 is composition $16.6~\rm wt.~\%~Si_3N_4-66.6~\rm wt.~\%~TiN-16.8~\rm wt.~\%~Si_3N_4$ rods. For the composite the coefficient of friction and linear wear are the lowest.

REFERENCES

V.G. Kolesnichenko, Powder Metallurgy and Metal Ceramics 35, 157 (2010).

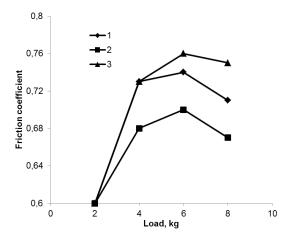


Fig. 2 – Friction coefficient as a function of load at V = 0.5 m/s

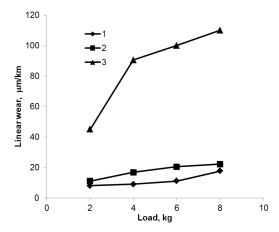


Fig. 3 – Linear wear as a function of load at $V=0.5\ m/s$

4. CONCLUSIONS

Dense nanoceramics on the basis of silicon nitride with the size of structural elements less than 150 nm are consolidated by EDS. The improvement of materials properties is expected: wearproof in the pair with steel 15, hardness, bend stress as compared to traditional materials which are now used as frictional units.

5. ACKNOWLEDGEMENTS

The authors wish to thank B. Weise and J. Raethel for his kind help regarding the experiments, and K. Sempf for relevant technical support.

2. O. Zgalat-Lozynskyy, M. Herrmann, A. Ragulya, *J. Europ. Ceram. Soc.* **31**, 809 (2011).