

AA 274

Principles of Robotic Autonomy

Course overview, mobile robot kinematics,
introduction to motion control



Stanford
University



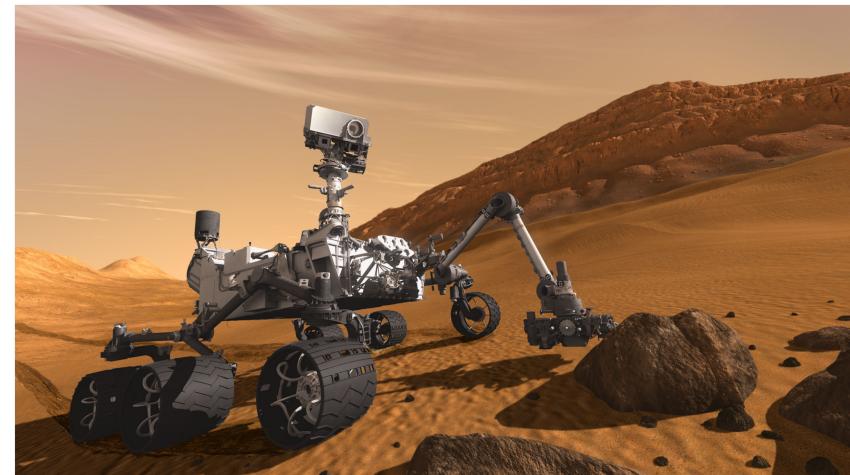
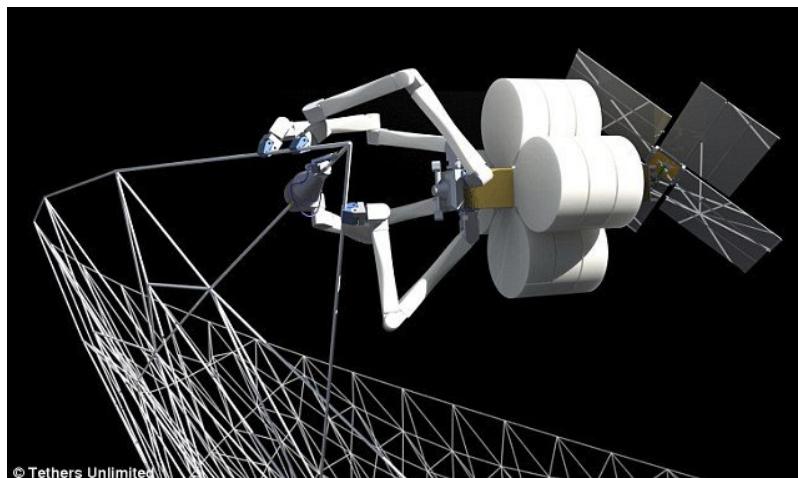
Course goals

- To learn the *theoretical, algorithmic, and implementation* aspects of main techniques for robot autonomy. Specifically, the student will
 1. Gain a fundamental knowledge of the “autonomy stack”
 2. Be able to apply such knowledge in applications / research by using ROS
 3. Devise novel methods and algorithms for robot autonomy

From automation...



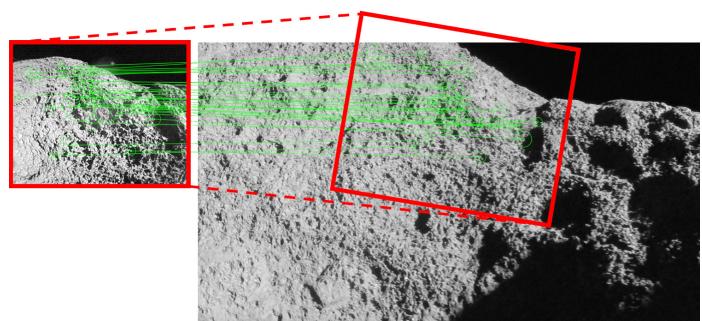
...to autonomy



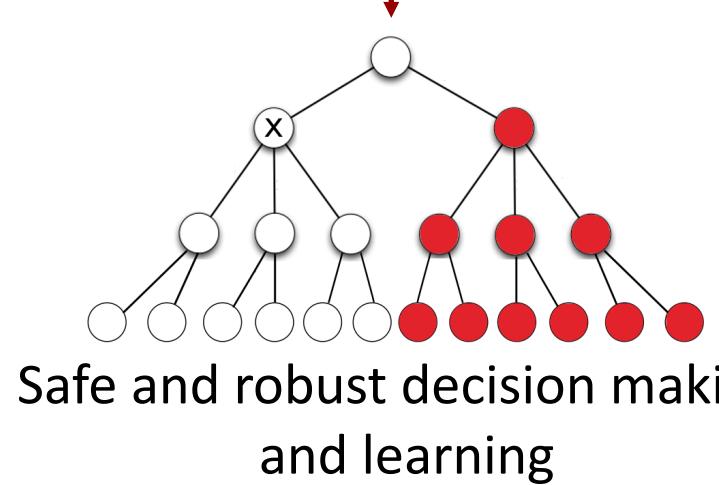
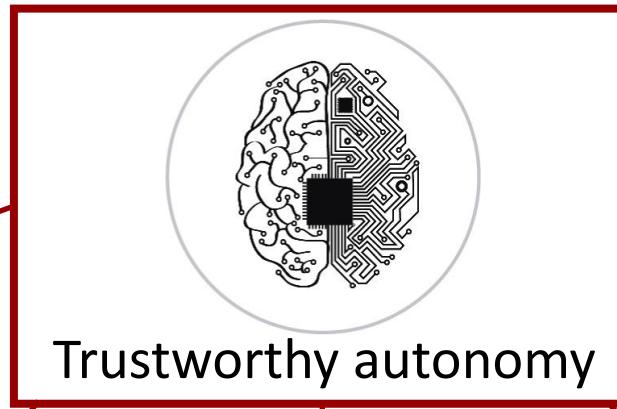
ASL research



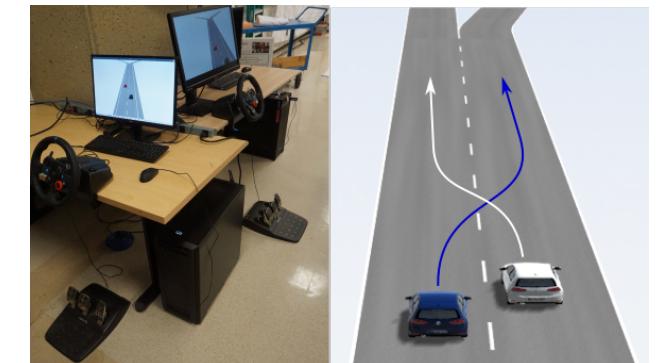
Agile motion planning



Interplay with perception



System-level coordination

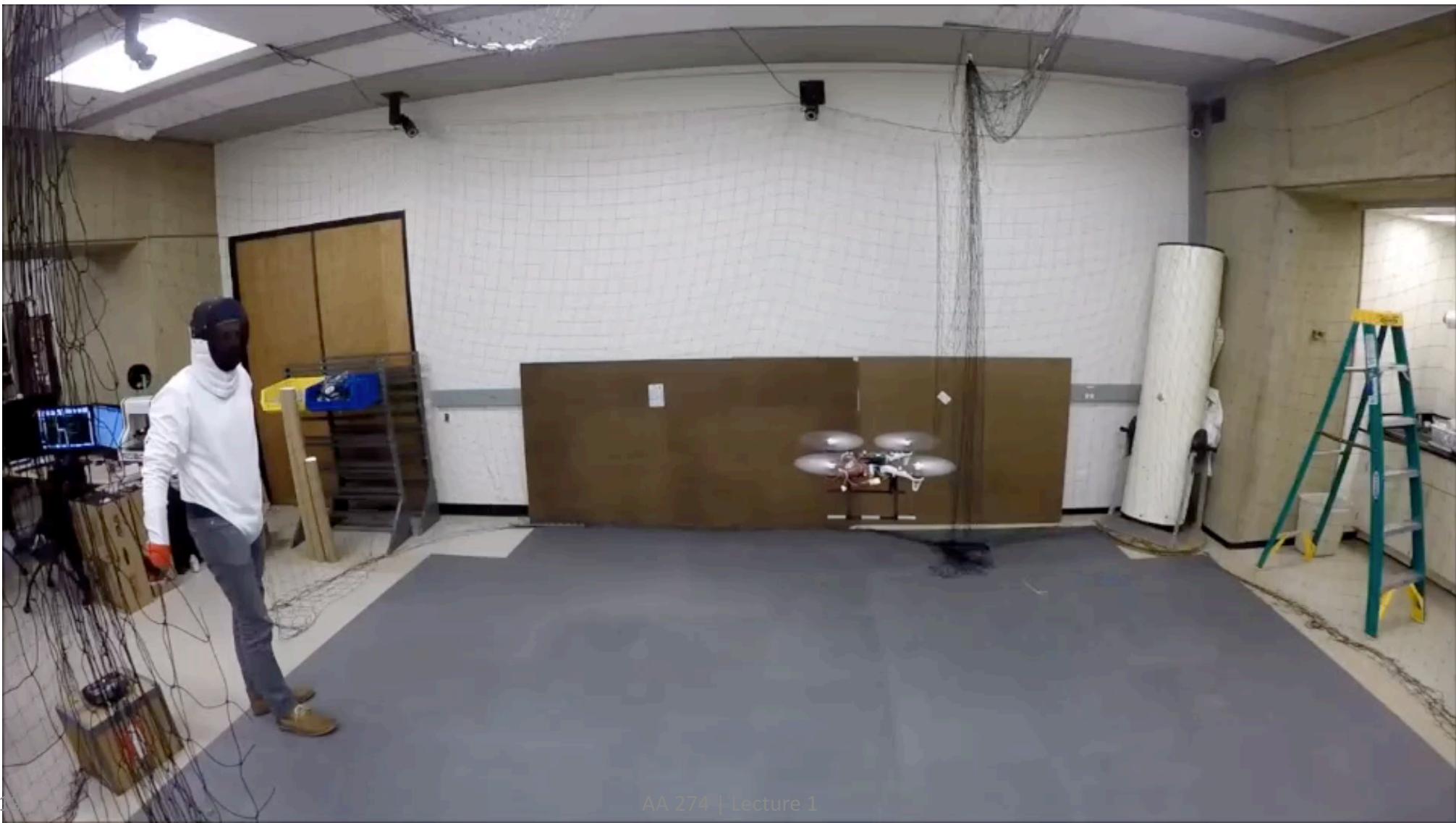


Safe interactions with humans

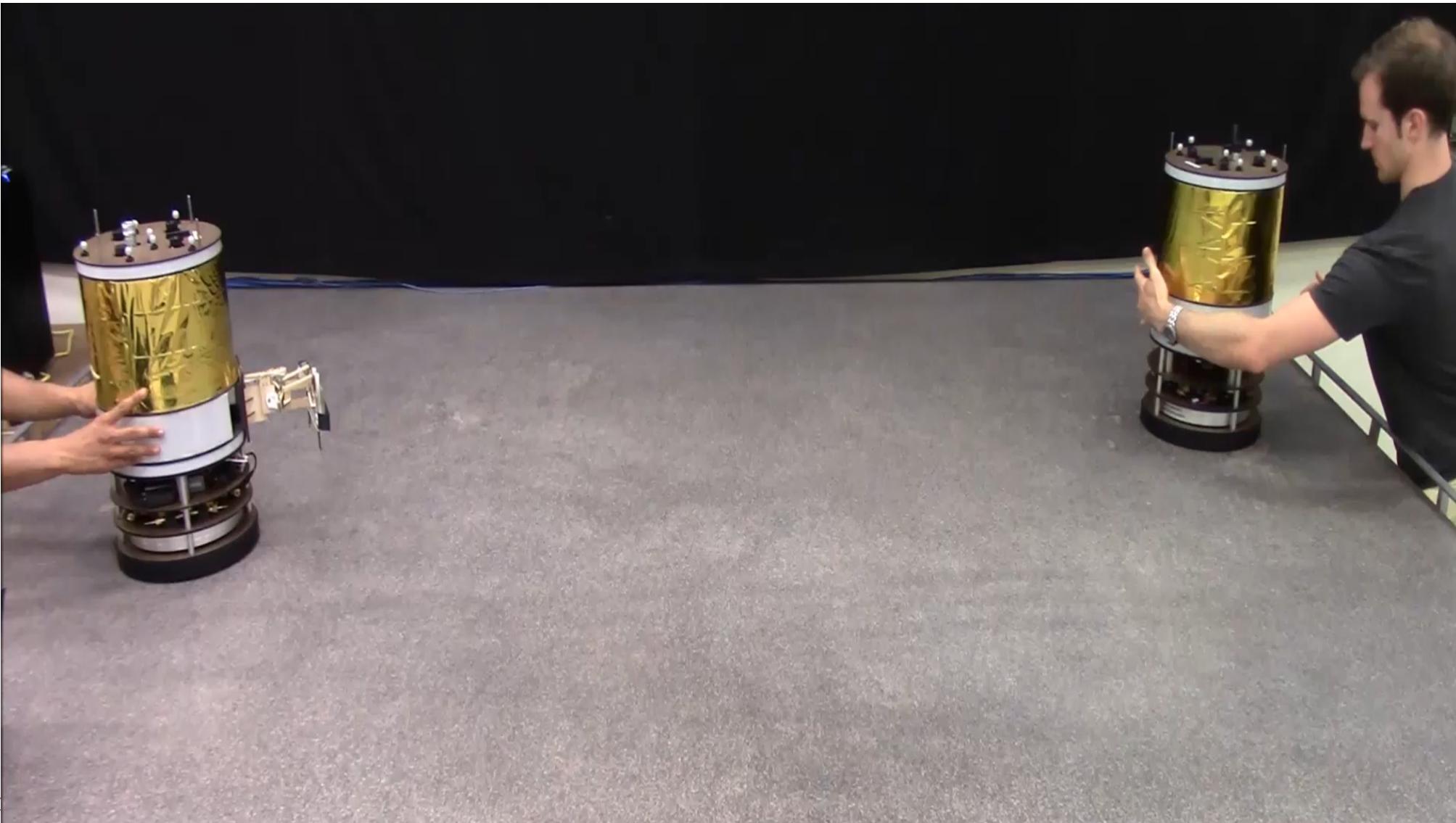
Sample of ASL research



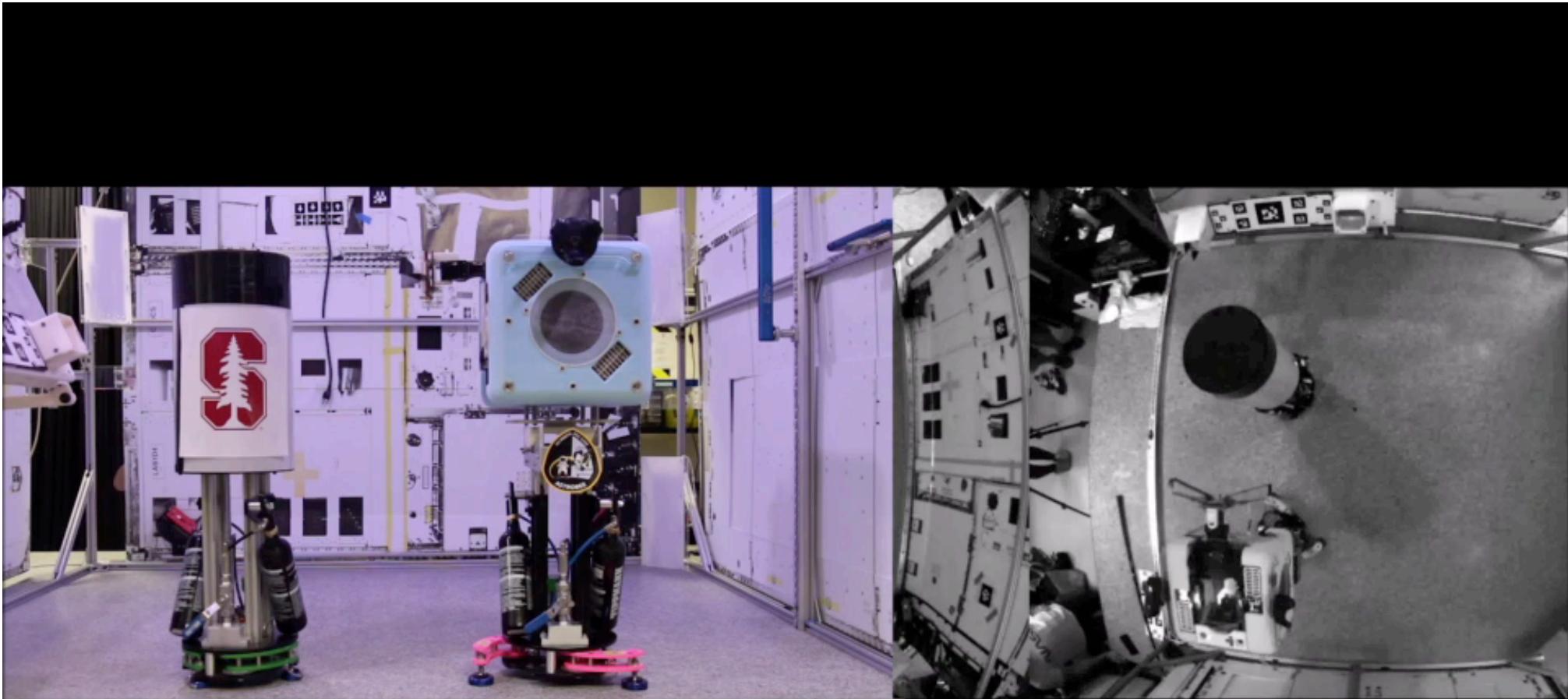
Sample of ASL research



Sample of ASL research

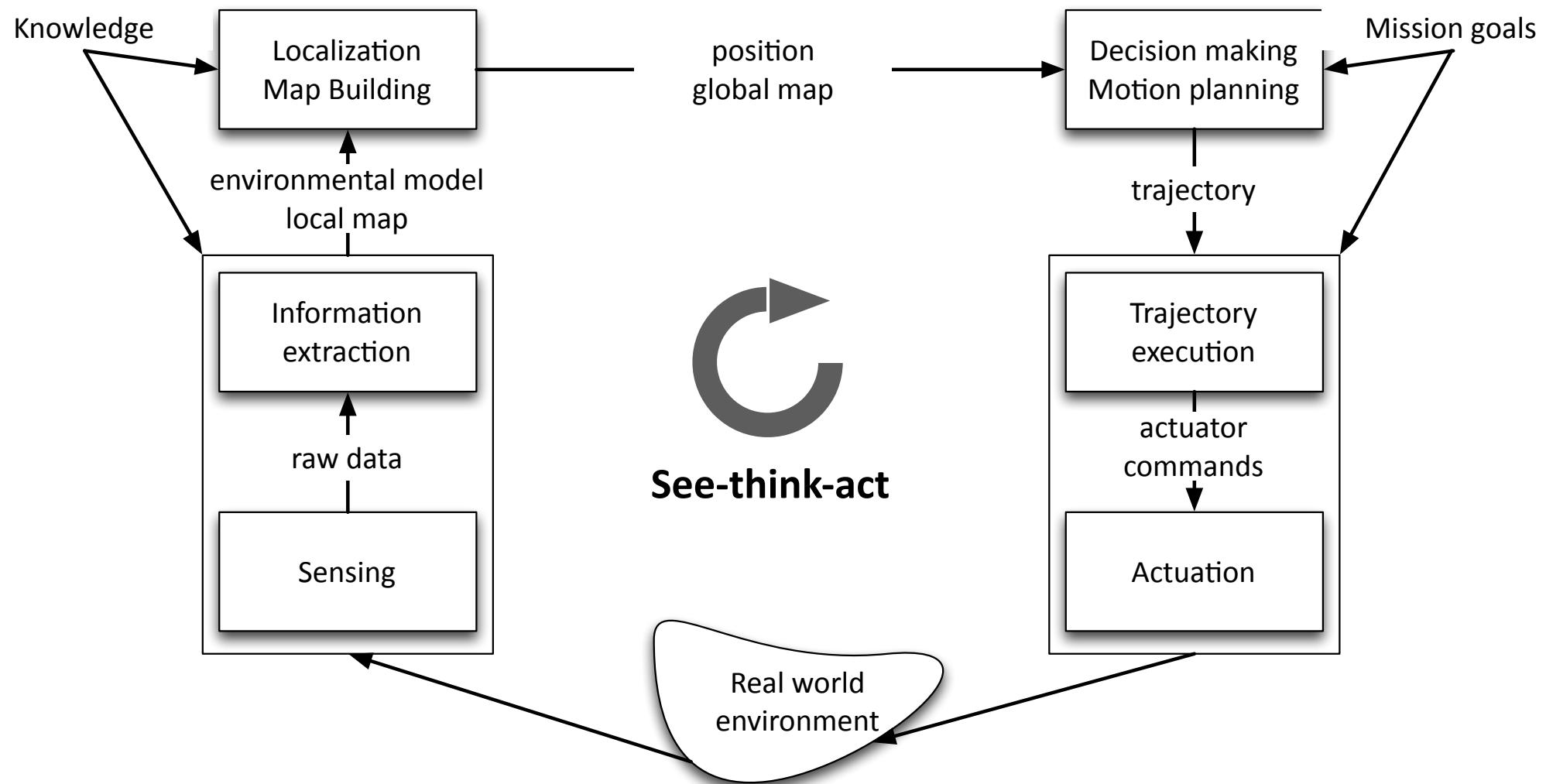


Sample of ASL research



Gripper equipped with gecko-inspired dry adhesive
(2X)

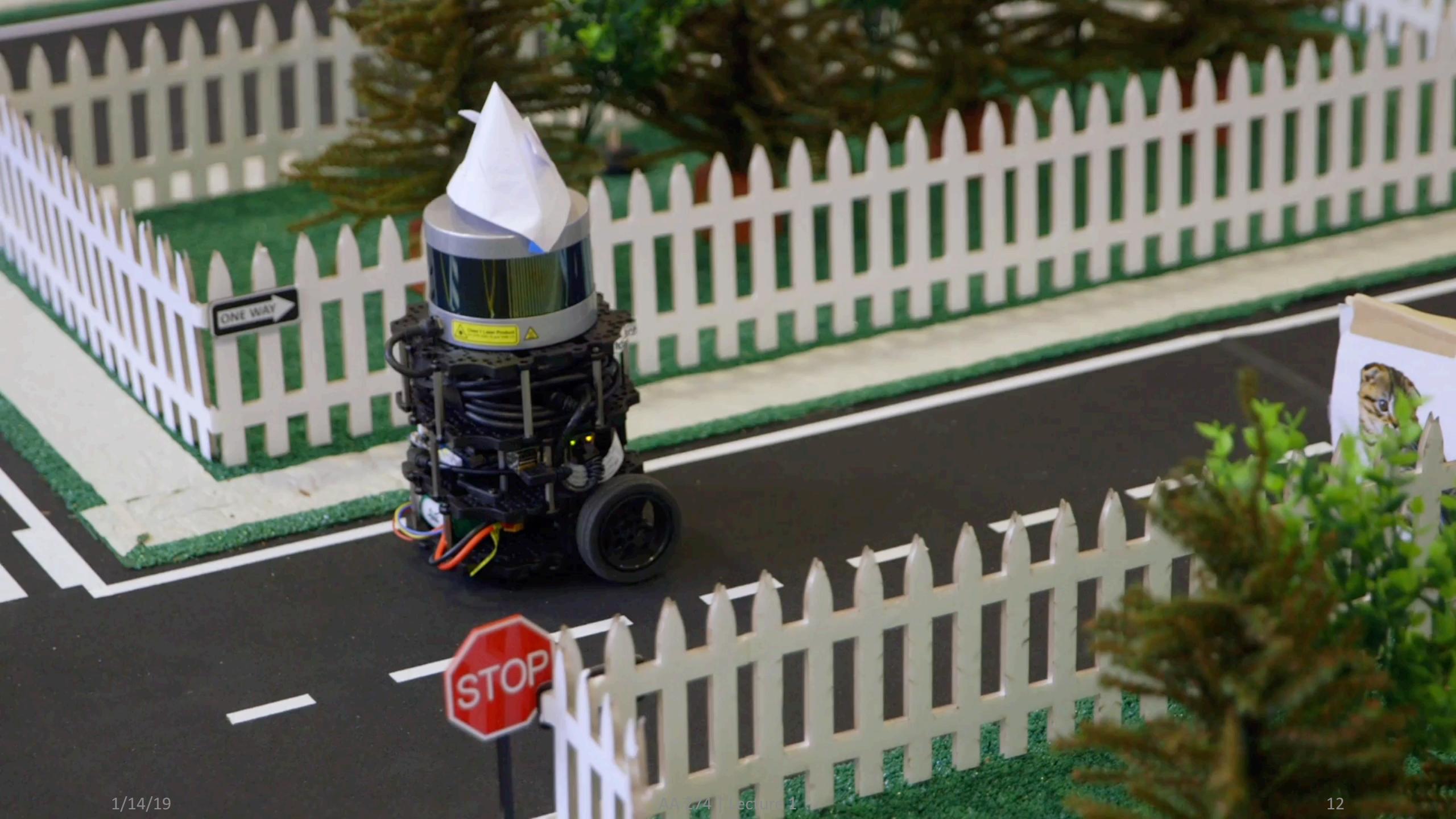
The see-think-act cycle



Course structure

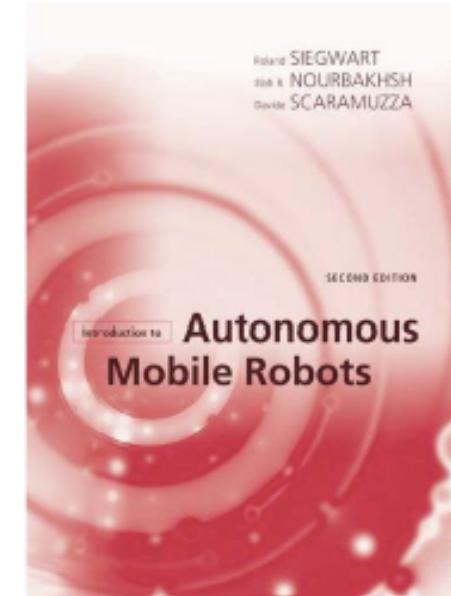
- Four modules, roughly of equal length
 1. motion control
 2. perception, from classic to deep learning approaches
 3. localization and SLAM
 4. planning, decision making, and system architecting
- Extensive use of the Robot Operating System (ROS)
 - Requirement: familiarity with programming
(e.g., CS 106A or equivalent)
- Course grade calculation
 - 72% homework (four problem sets)
 - 23% final project
 - 5% scribe quality
 - Extra 5%: participation on Piazza





Recommended textbook

- R. Siegwart, I. R. Nourbakhsh, D. Scaramuzza.
Introduction to Autonomous Mobile Robots.
MIT Press, 2nd Edition, 2011.



- Additional reading material:
 - S. Thrun, W. Burgard, D. Fox. Probabilistic Robotics. MIT Press, 2005.
 - P. Goebel. ROS By Example. 2013.

Schedule

Date	Topic	Assignment	Readings
01/07	Course overview, mobile robot kinematics, introduction to motion control		SNS:3.1-3.5;
01/09	The Robot Operating System (ROS)	HW1 out	Lecture notes
01/11	<i>Recitation:</i> Python (optional)		
01/14	Open-loop and closed-loop motion control		SNS:3.6
01/16	Robotic sensors and introduction to computer vision		SNS:4.1-4.2
01/18	<i>Recitation:</i> dynamical systems (optional)		
01/21	Martin Luther King, Jr., Day (no classes)		
01/23	Camera models and camera calibration	HW2 out, HW1 due	SNS:4.2
01/25	<i>Recitation:</i> advanced Python (optional)		
01/28	Stereo vision and image processing		SNS:4.3-4.5
01/30	Feature detection & description, information extraction, and “classic” visual recognition		SNS:4.7
02/05	Machine learning for robot autonomy		Lecture notes
02/06	Deep learning for visual recognition		Lecture notes
02/11	Localization I	HW3 out, HW2 due	SNS:5.1-5.4
02/13	Localization II		SNS:5.5-5.6
02/18	Presidents’ Day (no classes)		
02/20	Localization III		SNS:5.6-5.7
02/25	SLAM I		SNS:5.8
02/27	SLAM II		SNS:5.8
03/04	Motion planning I: combinatorial motion planning	HW4 out, HW3 due	SNS:6.1-6.5
03/06	Motion planning II: sampling-based motion planning		Lecture notes
03/11	Decision making and reinforcement learning		Lecture notes
03/13	State machines and “architecting” the autonomy stack	HW4 due	Lecture notes
TBD	Final project, TBD		

Team

Instructor



Marco
Pavone

Collaborators:

- Andrew Bylard
- Patrick Goebel
- Boris Ivanovic
- Benoit Landry
- Joseph Steven Lorenzetti

Labs:



CAs



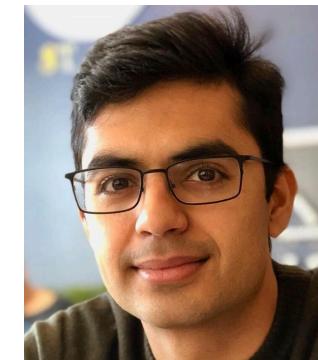
Christopher
Covert



Amine
Elhafsi



Karen
Leung



Apoorva
Sharma

Logistics

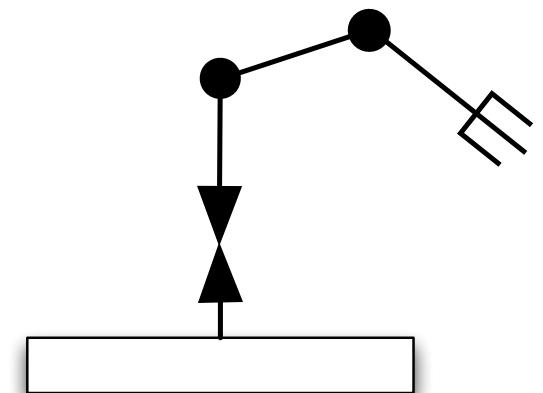
- Location / time: 420-041, Mondays and Wednesdays, 1:30 -- 2:50pm
- Office hours:
 - Prof. Pavone: Mondays, 3:00 -- 5:00pm, after class, and by appointment
 - CAs (homework support): Tuesdays and Fridays, 2:00 -- 4:00pm, location TBD
 - CAs (ROS support): Mondays, Wednesdays, and Thursdays, 5:00 -- 7:00pm, location TBD
- Course website:
 - <http://asl.stanford.edu/aa274/>
 - <https://piazza.com/stanford/winter2019/aa274>
 - <https://www.gradescope.com/courses/35120>
- To contact the AA274 staff, use the email: aa274-win1819-staff@lists.stanford.edu

Mobile robot kinematics

- Aim
 - Understand motion constraints
 - Learn about basic motion models for wheeled vehicles
 - Gain insights for motion control
- Readings
 - SNS: 3.1-3.3
 - B. Siciliano, L. Sciavicco, L. Villani, G. Oriolo. *Robotics: Modelling, Planning, and Control*. Springer, 2008 (chapter 11).

Holonomic constraints

- Let $\xi = [\xi_1, \dots, \xi_n]^T$ denote the configuration of a robot (e.g., $\xi = [x, y, \theta]^T$ for a wheeled mobile robot)
- *Holonomic* constraints
 - $h_i(\xi) = 0$, for $i = 1, \dots, k < n$
 - Reduce space of accessible configurations to an $n - k$ dimensional subset
 - If all constraints are holonomic, the mechanical system is called holonomic
 - Generally the result of mechanical interconnections



Kinematic constraints

- Kinematic constraints

$$a_i(\xi, \dot{\xi}) = 0, \quad i = 1, \dots, k < n$$

- constrain the instantaneous admissible motion of the mechanical system
- generally expressed in Pfaffian form, i.e., linear in the generalized velocities

$$a_i^T(\xi) \dot{\xi} = 0, \quad i = 1, \dots, k < n$$

- Clearly, k holonomic constraints imply the existence of an equal number of kinematic constraints

$$\frac{d h_i(\xi)}{dt} = \frac{\partial h_i(\xi)}{\partial \xi} \dot{\xi} = 0, \quad i = 1, \dots, k < n$$

- However, the converse is not true in general...

Nonholonomic constraints

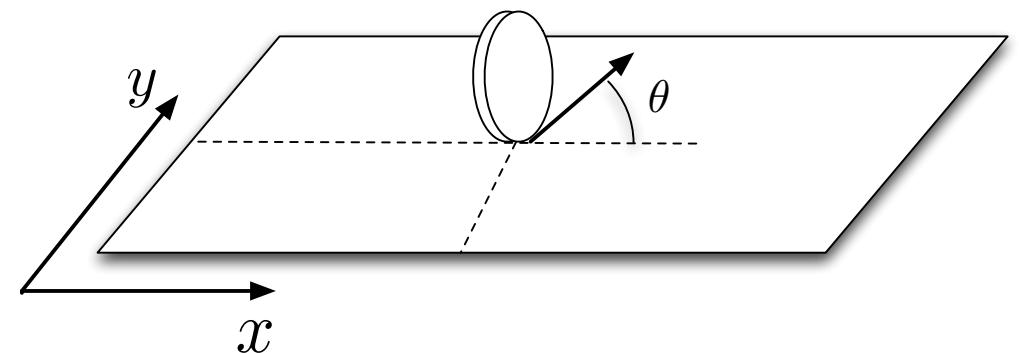
- If a kinematic constraint is not integrable in the form $h_i(\xi) = 0$, then it is said *nonholonomic* -> nonholonomic mechanical system
- Nonholonomic constraints reduce mobility in a completely different way. Consider a single Pfaffian constraint

$$a^T(\xi) \dot{\xi} = 0$$

- Holonomic
 - Can be integrated to $h(\xi) = 0$
 - Loss of accessibility, motion constrained to a level surface of dimension $n - 1$
- Nonholonomic
 - *Velocities* constrained to belong to a subspace of dimension $n - 1$, the null space of $a^T(\xi) = 0$
 - No loss of accessibility

Example of nonholonomic system

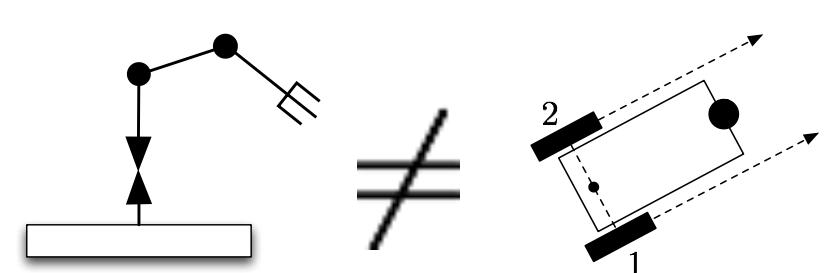
- System: disk that rolls without slipping
- $\xi = [x, y, \theta]^T$



- No side slip constraint

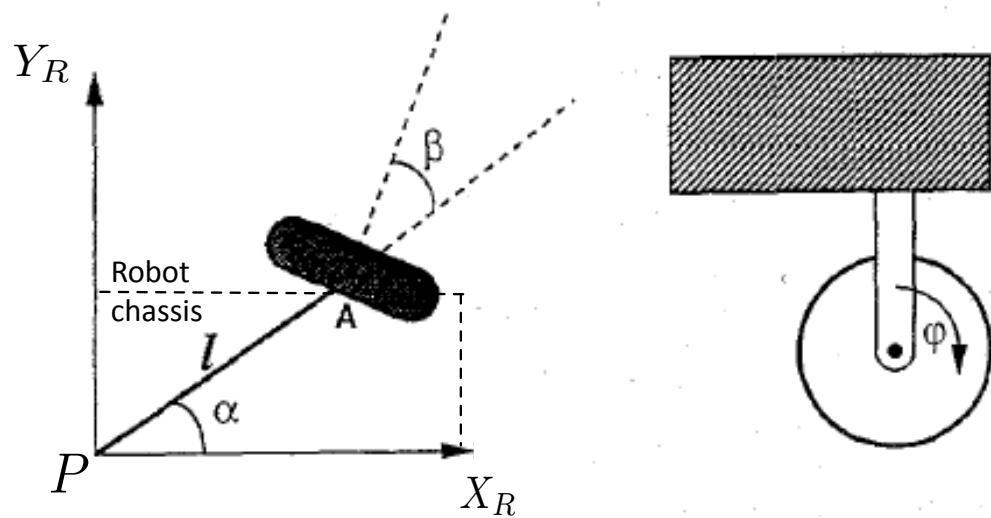
$$[\dot{x}, \dot{y}] \cdot \begin{bmatrix} \sin \theta \\ -\cos \theta \end{bmatrix} = \dot{x} \sin \theta - \dot{y} \cos \theta = [\sin \theta, -\cos \theta, 0] \dot{\xi} = 0$$

- Facts:
 - No loss of accessibility
 - Wheeled vehicles are generally nonholonomic

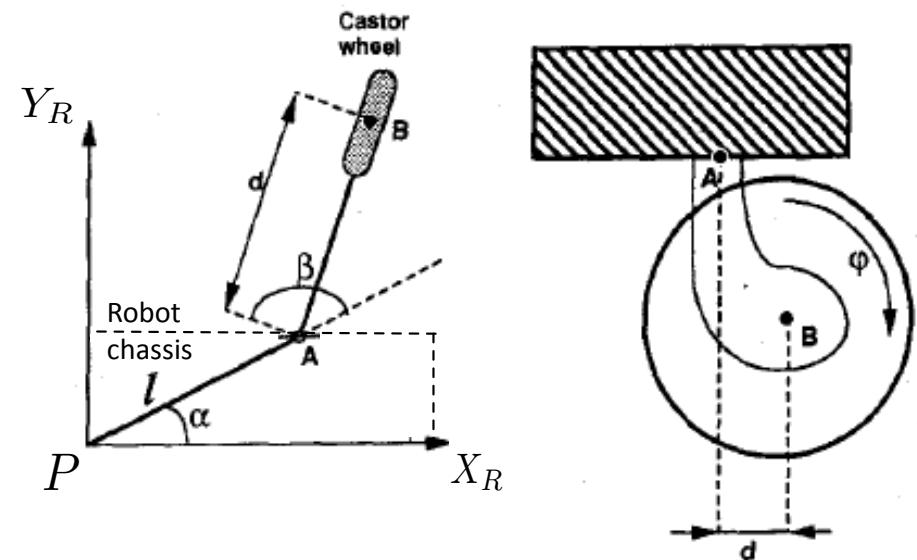


Types of wheels

- Standard wheels (four types)



Standard wheel -- fixed or steerable



Standard, off-centered wheel (caster)
-- passive or active

- Special wheels: achieve omnidirectional motion (e.g., Swedish or spherical wheels)

Kinematic models

- Assume the motion of a system is subject to k Pfaffian constraints

$$\begin{bmatrix} a_1^T(\xi) \\ \vdots \\ a_k^T(\xi) \end{bmatrix} \dot{\xi} := A^T(\xi) \dot{\xi} = 0$$

- Then, the admissible velocities at each configuration ξ belong to the $(n - k)$ -dimensional null space of matrix $A^T(\xi)$
- Denoting by $\{g_1(\xi), \dots, g_{n-k}(\xi)\}$ a basis of the null space of $A^T(\xi)$, admissible trajectories can be characterized as solutions to

$$\dot{\xi} = \sum_{j=1}^{n-k} g_j(\xi) u_j = G(\xi) u$$

Input vector

Example: unicycle

- Consider pure rolling constraint for the wheel:

$$\dot{x} \sin \theta - \dot{y} \cos \theta = [\sin \theta, -\cos \theta, 0] \dot{\xi} = a^T(\xi) \dot{\xi} = 0$$

- Consider the matrix

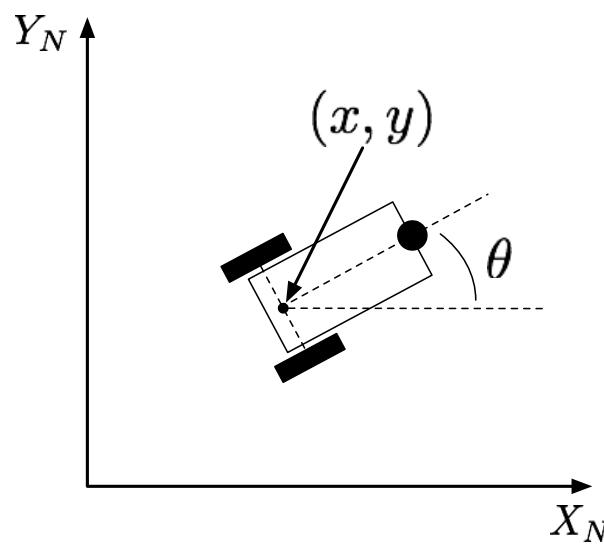
$$G(\xi) = [g_1(\xi), g_2(\xi)] = \begin{bmatrix} \cos \theta & 0 \\ \sin \theta & 0 \\ 0 & 1 \end{bmatrix}$$

where $[g_1(\xi), g_2(\xi)]$ is a basis of the null space of $a^T(\xi)$

- All admissible velocities are therefore obtained as linear combination of $g_1(\xi)$ and $g_2(\xi)$

Kinematic models (examples)

$$\begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{pmatrix} = \begin{pmatrix} \cos \theta \\ \sin \theta \\ 0 \end{pmatrix} v + \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \omega$$

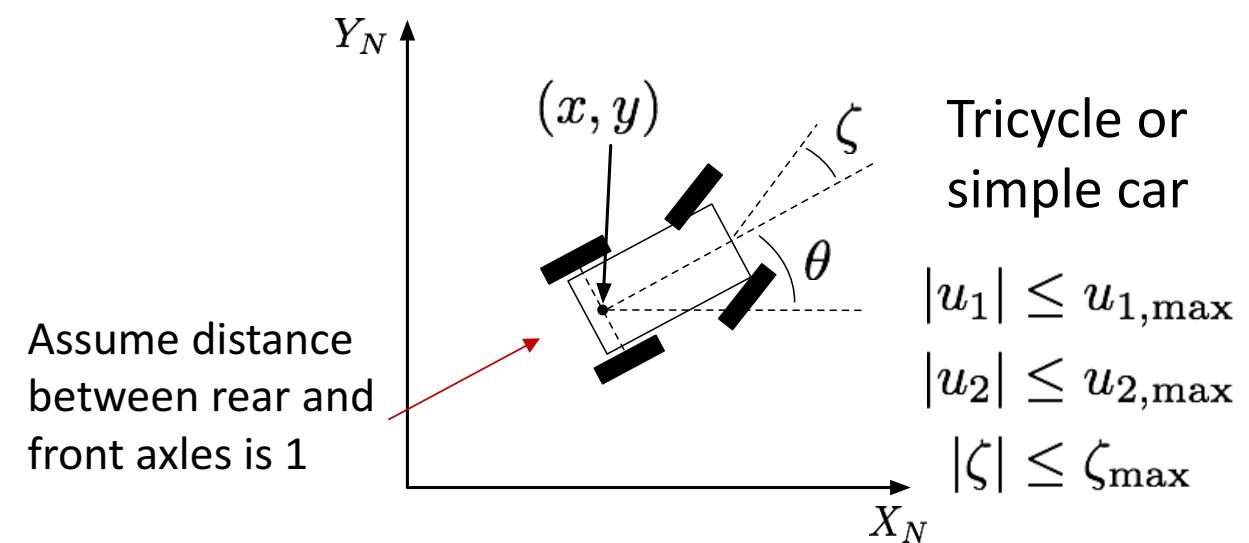


Unicycle or
differential drive

$$|v| \leq v_{\max}$$

$$|\omega| \leq \omega_{\max}$$

$$\begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \\ \dot{\zeta} \end{pmatrix} = \begin{pmatrix} \cos \zeta \cos \theta \\ \cos \zeta \sin \theta \\ \sin \zeta \\ 0 \end{pmatrix} u_1 + \begin{pmatrix} 0 \\ 0 \\ 0 \\ 1 \end{pmatrix} u_2$$



Assume distance
between rear and
front axles is 1

Tricycle or
simple car

$$|u_1| \leq u_{1,\max}$$

$$|u_2| \leq u_{2,\max}$$

$$|\zeta| \leq \zeta_{\max}$$

Warning: a kinematic state space model should be interpreted only as a subsystem of a more general dynamical model

Simplified car models

- Assuming we do not care about the direction of the front wheels, set

$$v = u_1 \cos \zeta, \quad \omega = u_1 \sin \zeta$$

$$\begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \\ \dot{\zeta} \end{pmatrix} = \begin{pmatrix} \cos \zeta & \cos \theta \\ \cos \zeta & \sin \theta \\ \sin \zeta & 0 \\ 0 & 1 \end{pmatrix} u_1 + \begin{pmatrix} 0 \\ 0 \\ 0 \\ 1 \end{pmatrix} u_2 \quad \rightarrow \quad \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \end{pmatrix} = \begin{pmatrix} \cos \theta \\ \sin \theta \\ 0 \end{pmatrix} v + \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \omega$$

$|v| \leq u_{1,\max} \cos \zeta_{\max}, \quad |\omega| \leq |v| \tan \zeta_{\max}$ → Car-like robot

$|v| = u_{1,\max} \cos \zeta_{\max}, \quad |\omega| \leq |v| \tan \zeta_{\max}$ → Reeds&Shepp's car

$v = u_{1,\max} \cos \zeta_{\max}, \quad |\omega| \leq |v| \tan \zeta_{\max}$ → Dubins' car

- Reference: J.-P. Laumond. Robot Motion Planning and Control. 1998.

Next time

