



**POLITECNICO**  
**MILANO 1863**

## Extended project work

A Gazebo car simulator, analysis and comparison  
with a single-track model

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## **Abstract**

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# Chapter 1

## Notes on Installation and Launch

### 1.1 Installation

#### 1.1.1 Downloading material

The project is based on the material of original MIT racecar. That's it, we have generated a new ROS environment copying MIT repository packages. In particular the following packages have been downloaded:

- ackermann\_msgs
- racecar
- racecar\_gazebo

They can be found at the link: <https://github.com/mit-racecar>

#### 1.1.2 Additional packages to be installed

To be able to compile the project it is necessary to download two internal ROS packages which will be used by the racecar ones. Launch the following commands:

```
sudo apt install ros-noetic-ros-control  
sudo apt install ros-noetic-ros-controllers
```

Otherwise an error will be thrown when `catkin_make` command is called.

### 1.1.3 Additional modifications

In some cases, to avoid conflicts, it's required to change Python environment to version 3 in each file of the original packages. In particular, if Python environment is set to 3, modifications are needed for `joy_teleop.py` file:

- Row 277: replace `'` with `'as'`
- Row 282: replace `iteritems` with `items`

## 1.2 Launch

### 1.2.1 Original Project

In order to launch original project, once it's compiled following ROS guide, following steps should be followed:

- `(run) roscore`
- `(run) keyboard_teleop.py`
- `(run) racecar_gazebo racecar.tunnel`

If there are no errors the user should be able to see the racecar in a Gazebo environment. WASD keys on keyboard produce car moves.



## Chapter 2

# General Project Structure

## 2.1 Catkin Workspace Directories

### 2.1.1 Original MIT Racecar Packages

ackermann_cmd_mux (racecar folder)	...
ackermann_msgs	Contains definitions of <b>AckermannDrive</b> and <b>AckermannDriveStamped</b> messages, used by the racecar to compute movements.
racecar (racecar folder)	Directory which contains
racecar_control (racecar_gazebo folder)	Contains launch files to load controllers used to manage the motors of the racecar. Also load nodes which dispatch messages to controllers.
racecar_description (racecar_gazebo folder)	Contains a description of the racecar, in terms of models, meshes ecc... It will be used by Gazebo to represent it.
racecar_gazebo (racecar_gazebo folder)	Mainly contains launch scripts used to load all necessary nodes, worlds and other components to open a Gazebo instance with a controllable car.



### 2.1.2 Added Packages

car_control	Contains node which performs the linearization of the nonlinear bicycle <b>dynamic</b> model. It' receives desired velocities from trajectory tracker and sends Ackermann commands to the racecar.
car_kinematic_control	Contains node which performs the exact linearization of the nonlinear bicycle <b>kinematic</b> model. It' receives desired velocities from trajectory tracker and sends Ackermann commands to the racecar.
trajectory_tracker	Generates (or receives in input) a desired trajectory and actual car positions, than compute desired velocities to be sent to controllers.
CarCommandsFr	Interface used to replace inner wheel friction phisical model of ROS with a custom one.

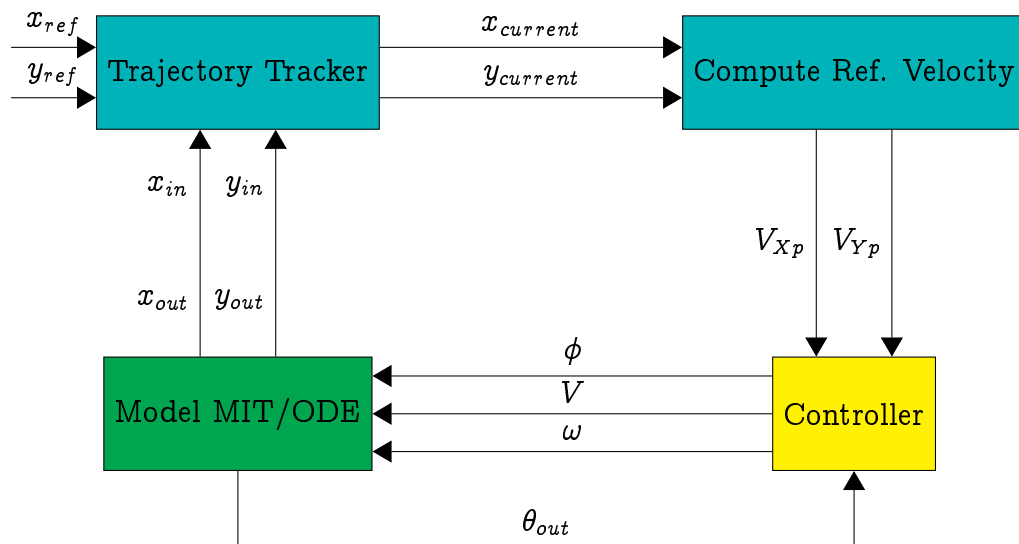
## Chapter 3

# Original System Introduction

# Chapter 4

## (Our) System Description

### 4.1 Scheme of the whole system



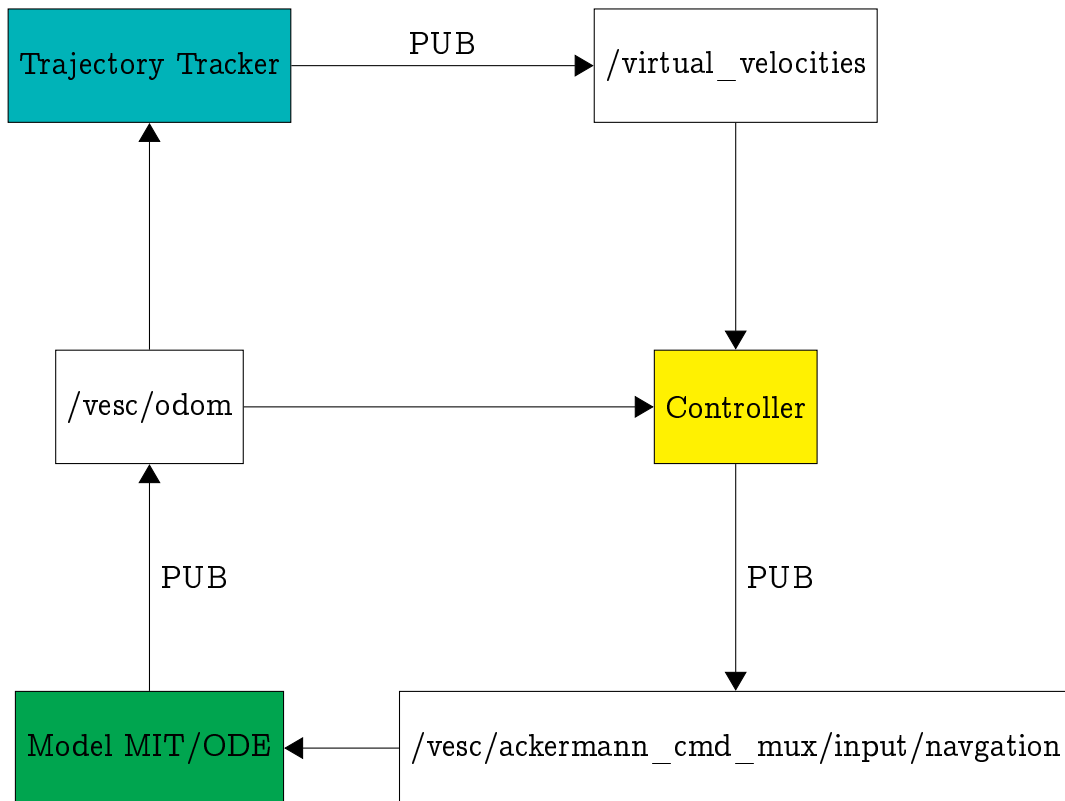
Symbol	Meaning
$x_{ref}, y_{ref}$	Ref. position of the trajectory
$V_{Xp}, V_{Yp}$	Required velocities of the point. They will be imposed by controller
$\phi$	Steer degree of rotation
$V$	Vector velocity
$\omega$	Steer speed of rotation
$\theta_{out}$	Car pose: rotation around center axis
$x_{out}, y_{out}$	Car pose: x, y

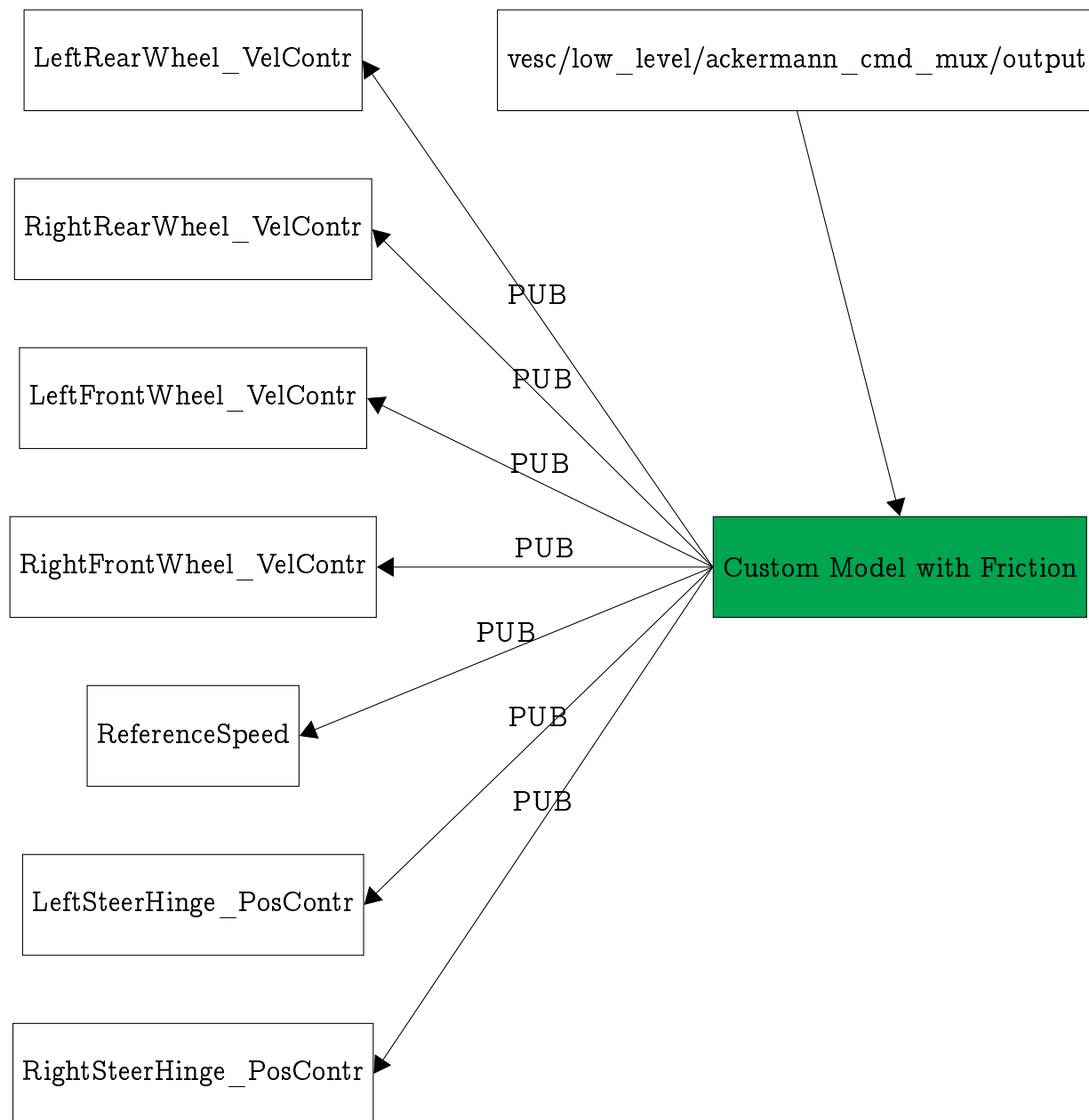
Note that "trajectory tracker" generated trajectories are hard-coded, even if  $x_{ref}$  and  $y_{ref}$  are shown as input parameters. The user can select the trajectory using YAML configuration file (which will be explained in the relative section).

## 4.2 Topics

### 4.2.1 Scheme of topic publications/subscriptions

#### ROS Friction Model



**Custom Friction Model**

## 4.2.2 Topics meaning

### Common Topics

/virtual_velocities	Used by "trajectory tracker" to publish desired velocity components. These are read by controller in order to perform linearization and compute instructions for the model.
/vesc/ackermann_cmd_mux /input/navigation	Contains AckermannDriveStamped messages sent by controller. These messages contains information for the racecar, about velocity and steering.
/vesc/odom	The model uses this topic to publish odometry information of the racecar (position and orientation). These data are used both by tracker and controller. The first one compute differences between actual car position and desired position imposed by trajectory. The last one reads z-axis orientation useful to perform linearization.

There is another topic in which "trajectory tracker" publish, the */reference\_trajectory*. This is used to read trajectory information to perform debug and register data for analysis.



**Specific Topics**

/vesc/low_level/ ackermann_cmd_mux/output	xyz
/racecar/ left_rear_wheel _velocity_controller/command	xyz
/racecar/ right_rear_wheel _velocity_controller/command	xyz
/racecar/ left_front_wheel _velocity_controller/command	xyz
/racecar/ right_front_wheel _velocity_controller/command	xyz
/reference_speed	xyz
/racecar/ left_steering_hinge _position_controller/command	xyz
/racecar/ right_steering_hinge _position_controller/command	xyz



# Chapter 5

## Detailed Package Description

### 5.1 Package (original) ackermann\_msgs

### 5.2 Package (original) racecar

### 5.3 Package (original) racecar\_gazebo

### 5.4 Package car\_control

#### 5.4.1 Intro

Even if this package is not used, it's correct to do a description of the objective it should have reached.

The aim was to implement a dynamic controller, which perform exact linearization of the nonlinear bicycle dynamic model. To do this it needs more parameter respect to the kinematic one.

In addition, we put a scheme (5.1) of the principal parameters and variables used for linearization.

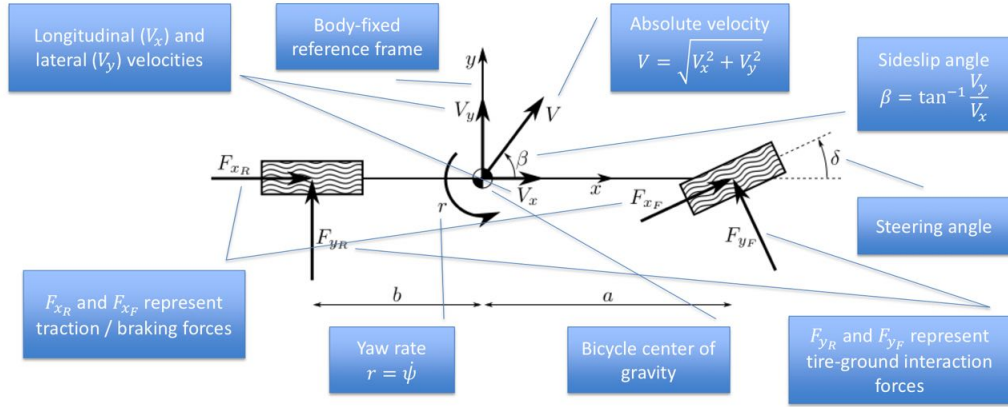


Figure 5.1: dynamic model with main parameters and variables

### 5.4.2 Configuration

Input values	
$Vp_x$	Point velocity x
$Vp_y$	Point velocity y
$\psi$	Yaw <sup>1</sup>
$\dot{\psi}$	Yaw rate <sup>2</sup>

Model parameters	
$C_f, C_r$	Viscous friction coefficients
a, b	Distance between wheels center and Center of Gravity
$M$	Vehicle mass
$\epsilon$	Distance between Center of Gravity and a point $P$ , along the velocity vector. Linearization is done around point $P$ . This parameter should be chosen empirically

<sup>1</sup>In the System Scheme, this is represented by  $\theta_{out}$

<sup>2</sup>In the System Scheme, this is **not** represented (as we have used, for tests, only the kinematic model)

Intermediate computed values	
$\beta$	Sideslip angle: $\tan^{-1} \left( \frac{Vp_y}{Vp_x} \right)$

Output values	
$V$	Point absolute velocity
$\delta$	Steering angle
$\omega$	Steering speed

### 5.4.3 Launch

There is a lunch file which should be used to execute the node. This contains also information about debugging level and loads configuration file.

#### 5.4.4 Node car\_control

$$\beta = \tan^{-1} \left( \frac{Vp_y}{Vp_x} \right)$$

$$\delta = \frac{MV}{C_f} \omega + \frac{C_f + C_r}{C_f} \beta - \frac{bC_r - aC_f}{C_f} \frac{\dot{\psi}}{V}$$

$$\begin{bmatrix} V \\ \omega \end{bmatrix} = \begin{bmatrix} \cos(\beta + \psi) & \sin(\beta + \omega) \\ -\frac{\sin(\beta + \psi)}{\epsilon} & \frac{\cos(\beta + \psi)}{\epsilon} \end{bmatrix} \begin{bmatrix} Vp_x \\ Vp_y \end{bmatrix}$$

## 5.5 Package car\_kinematic\_control

### 5.5.1 Intro

Before starting the explanation, we add a brief high level description of Quaternions, which are used in messages to represent orientations. Even a distinction between pose and position is done.

**Quaternion:** a different way to describe the orientation of a frame only. It's an alternative to Yaw, Pitch and Roll. A quaternion has four parameters: x, y, z, w. Pay attention, they are NOT a position vector.

**Position:** position of the robot in a 3D space.

**Pose:** position (3 DOF) + orientation (3 DOF).

In conclusion the pose has 6 D.O.F. which are:  $x$ ,  $y$ ,  $z$ , roll, pitch, yaw. Euler angles can be converted to quaternions, which are better. Transformation functions of ROS can do this conversion and the reverse one.

In addition, we put a scheme (5.2) of the principal parameters and variables used for linearization.

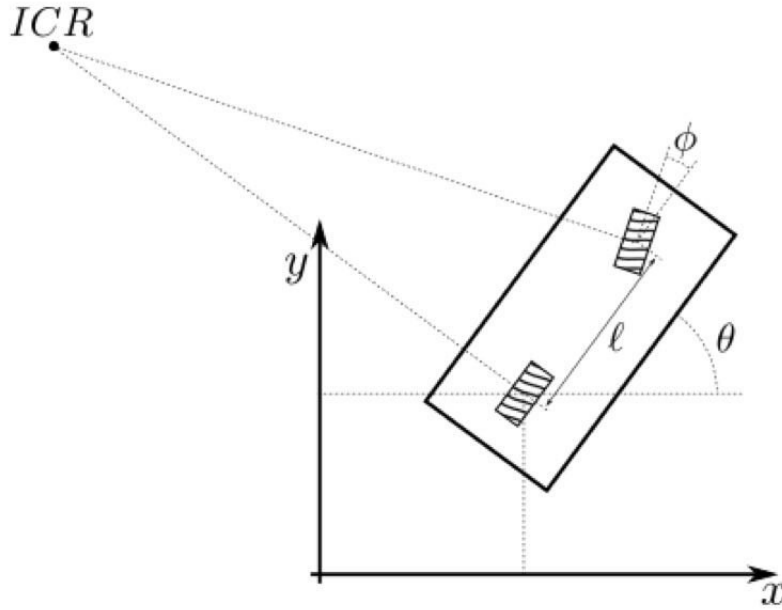


Figure 5.2: bicycle vehicle with main parameters and variables

### 5.5.2 Configuration

In the package there is a configuration file, containing: the parameter  $L$ , which represents distance between rear and front wheels; the parameter  $\epsilon$ , the distance between Center of Gravity and a point  $P$ , along the velocity vector. Linearization is done around point  $P$ . This parameter should be chosen empirically.

Both are used in the linearization.

### 5.5.3 Launch

There is a lunch file which should be used to execute the node. This contains also information about debugging level and loads configuration file.

### 5.5.4 Node car\_kin\_controller

**Node requirements:** distance between rear and front wheels as parameter.

The node has two callbacks:

- One used to retrieve desired velocities of the point. These velocities are computed by trajectory tracker and published in `/virtual_velocities` topic, subscribed by the controller node.
- One used to retrieve the orientation of the car around z axis. This is done reading from `/vesc/odom`. The information retrieved are in the form of a quaternion and are converted into roll, pitch and yaw. Yaw is taken. In addition, even the speed around z axis is read (`twist.angular.z`).

The node perform an exact linearization of the nonlinear bicycle cinematic model. The change of coordinates is applied as follows:

$$V = V_{Xp}\cos(\theta) + V_{Yp}\sin(\theta)$$

$$\phi = \arctan\left(\frac{l V_{Yp}\cos(\theta) - V_{Xp}\sin(\theta)}{\epsilon V_{Xp}\cos(\theta) + V_{Yp}\sin(\theta)}\right)$$

Where

- $l$  is the distance between rear and front wheels
- $\epsilon$  is the distance between Center of Gravity and a point  $P$
- $V_{Xp}$  and  $V_{Yp}$  are the desired point velocities
- $\theta$  is the car orientation around z-axis
- $\phi$  is the steering angle

- $V$  is the driving velocity of the front wheel

In addition, the program compute the steering speed as  $\omega = \frac{V}{l} \tan(\phi)$ . This value is not used in the construction of the message because it's ignored by the model.

Once the linearization is performed an AckermannDriveStamped message is built, containing  $V$  and  $\phi$ . This message is published on `/vesc/ackermann_cmd_mux/input/navigation` topic, which is read by the model to make the car move. Linearization and command sending operations are repeated in a loop, which is the core of the node.

## 5.6 Package trajectory\_tracker

### 5.6.1 Package description

The *trajectory\_tracker* package is responsible for two main tasks:

- generating the setpoints of the desired trajectory;
- applying the control law to make the robot track such trajectory.

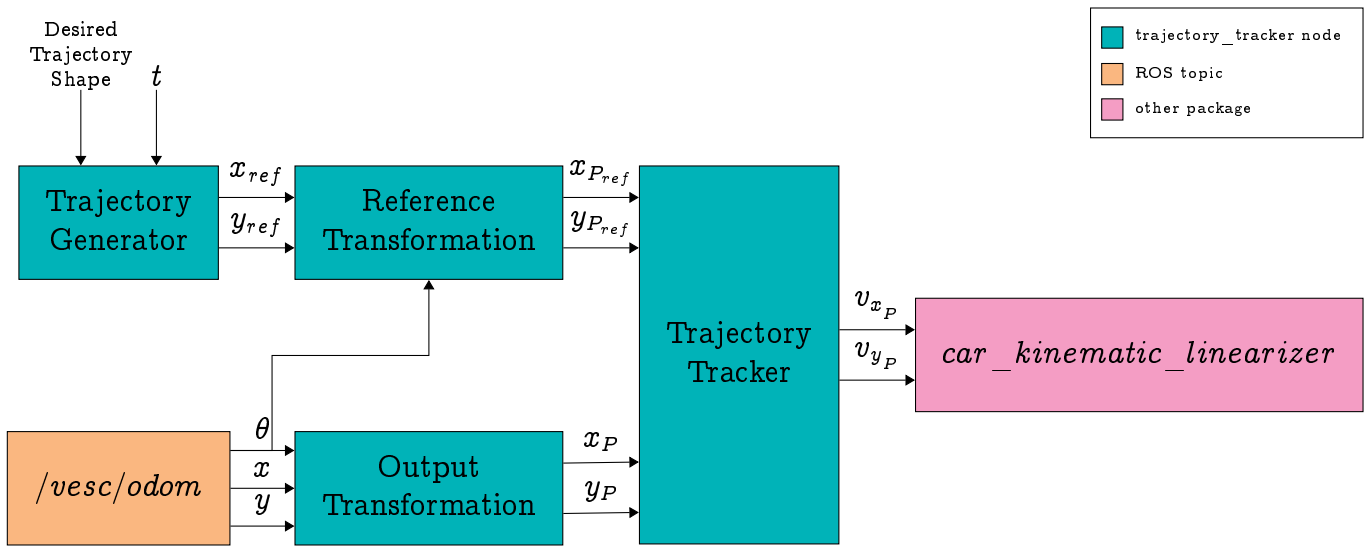


Figure 5.3: trajectory\_tracker package schematic

The main components of the package are:

- **Trajectory Generator** which is in charge of computing the appropriate setpoint given the desired trajectory shape and the time  $t$  elapsed since the starting of the motion.

The implemented trajectory shapes are:

- Line, a simple linear path described by equations:

$$x_{ref} = at \quad (x_{ref}^{\cdot} = a)$$

$$y_{ref} = bt \quad (y_{ref}^{\cdot} = b)$$

Where  $a$  and  $b$  determine the direction (the line is parallel to the direction vector  $\vec{d} = (a, b)$ ) and the speed of the trajectory;

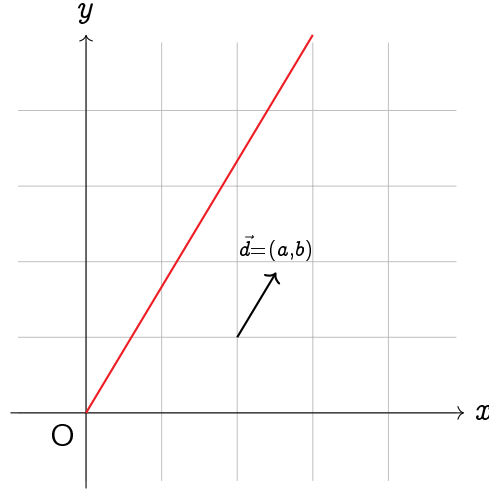


Figure 5.4: Linear trajectory (where  $\vec{d} = (3, 5)$ )

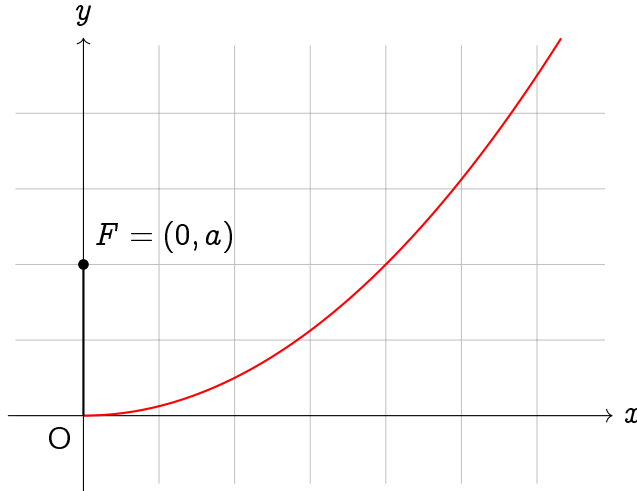
► Parabola, a parabolic path described by equations:

$$x_{ref} = 2at \quad (x_{ref} = 2a)$$

$$y_{ref} = at^2 \quad (y_{ref} = 2at)$$

Where  $a$  is the focal length of the parabola;



Figure 5.5: Parabolic trajectory (where  $a = 2$ )

- Circle, a circular path described by equations:

$$x_{ref} = r \cos(\omega t - \frac{\pi}{2}) \quad (\dot{x}_{ref} = -\omega r \sin(\omega t - \frac{\pi}{2}))$$

$$y_{ref} = r \sin(\omega t - \frac{\pi}{2}) + r \quad (\dot{y}_{ref} = \omega r \cos(\omega t - \frac{\pi}{2}))$$

Where  $r$  is the radius of the circumference and  $\omega$  is the angular velocity.

Since the robot starts at (0,0), a phase shift of  $\frac{\pi}{2}$  and an offset of  $r$  on the y axis are needed so to have a continuous trajectory (to have it starting at (0,0) when  $t = 0$ ).

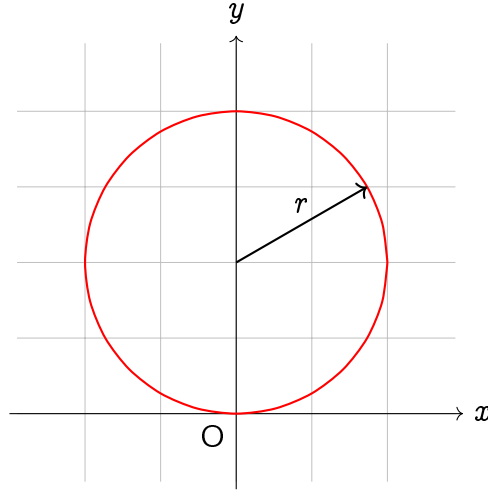


Figure 5.6: Circular trajectory (where  $r = 2$ )

► Figure Eight, an eight shaped path described by equations:

$$x_{ref} = a \sin(\omega t) \quad (\dot{x}_{ref} = \omega a \cos(\omega t))$$

$$y_{ref} = a \sin(\omega t) \cos(\omega t) \quad (\dot{y}_{ref} = \omega a [\cos(\omega t)^2 - \sin(\omega t)^2])$$

Where  $a$  is the trajectory amplitude (the eight shape goes from  $-a$  to  $a$  [m]) and  $\omega$  is the angular velocity;

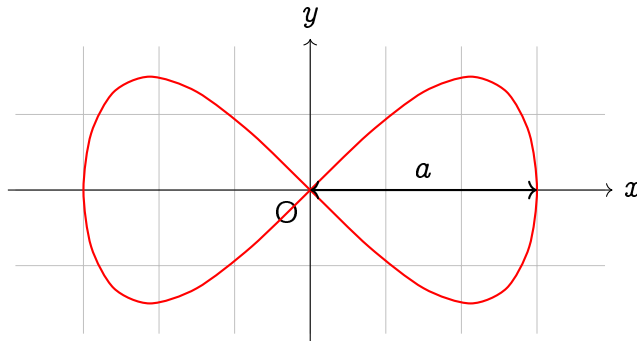


Figure 5.7: Figure eight trajectory (where  $a = 3$ )

- **Curtate Cycloid**, the path traced out by a fixed point at a radius  $d < r$ , where  $r$  is the radius of a rolling circle. It is described by equations:

$$x_{ref} = rt - d \sin(t) \quad (\dot{x}_{ref} = r - d \cos(t))$$

$$y_{ref} = d - d \cos(t) \quad (\dot{y}_{ref} = d \sin(t))$$

Where  $r$  is the radius of the rolling circle, and  $d$  is the distance of the point drawing the cycloid from the center such circle ( $d < r$  to have a curtate cycloid).

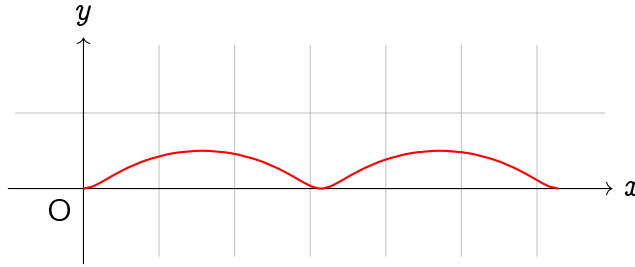


Figure 5.8: Cycloidal trajectory (where  $r = 0.5$  and  $d = 0.25$ )

- **Reference Transformation** which is in charge of performing a coordinate transformation from robot frame (attached to its center of gravity) to the P frame, where P is the point around which we are performing the feedback linearization of the bicycle model.

Since the trajectory will be tracked by point P, and not by the COG of the robot, we have to apply a reference transformation to every trajectory setpoint in order to achieve the desired behaviour.

The required transformation is:

$$x_{P_{ref}} = x_{ref} + \overrightarrow{PL} \cdot \cos(\theta)$$

$$y_{P_{ref}} = y_{ref} + \overrightarrow{PL} \cdot \sin(\theta)$$

Where  $x_{P_{ref}}$  and  $y_{P_{ref}}$  are the setpoints for point P,  $x_{ref}$  and  $y_{ref}$  are the setpoints generated by the *Trajectory Generator*,  $\overrightarrow{PL}$  is the distance between point P and the COG of the robot, and  $\theta$  is the robot velocity direction (yaw of the robot).

- **Output Transformation**, for the same reasons we introduced the *Reference Transformation* we need an analogous transformation for the robot odometry data obtained through the "`|vesc|odom`" topic: from the coordinates of the COG we need to retrieve the coordinates of point P which are the control variables of the *Trajectory Tracker*. The required transformation is:

$$x_P = x + \overrightarrow{PL} \cdot \cos(\theta)$$

$$y_P = y + \overrightarrow{PL} \cdot \sin(\theta)$$

Where  $x_P$  and  $y_P$  are the coordinates of point P,  $x$  and  $y$  are the coordinates of the robot COG,  $\overrightarrow{PL}$  is the distance between point P and the COG of the robot, and  $\theta$  is the robot velocity direction (yaw of the robot).

- **Trajectory Tracker** which is a controller in charge of performing trajectory tracking on point P. Since we have two independent process variables  $x_P$  and  $y_P$ , we have two independent PID (Proportional-Integral-Derivative) controllers to achieve the trajectory tracking task. The *Trajectory Generator* generates both position and velocity set-points, thus we can use the latter as feed forward terms to increase the stability of the trajectory tracking controllers. The position errors are computed as:

$$x_{P_{err}} = x_{P_{ref}} - x_P$$

$$y_{P_{err}} = y_{P_{ref}} - y_P$$

The control actions are:

$$v_{P_x} = \dot{x}_{P_{ref}} + K_p \cdot x_{P_{err}} + K_i \cdot x_{int} + K_d \cdot x_{der}$$

$$v_{P_y} = \dot{y}_{P_{ref}} + K_p \cdot y_{P_{err}} + K_i \cdot y_{int} + K_d \cdot y_{der}$$

Where  $\dot{x}_{P_{ref}}$  and  $\dot{y}_{P_{ref}}$  are the feed forward terms,  $x_{int}$  and  $y_{int}$  are the integrals of the variables, approximated using Riemann sums:

$$x_{int_t} = x_{int_{t-1}} + x_{P_{err}} \cdot \Delta t$$

$$y_{int_t} = y_{int_{t-1}} + y_{P_{err}} \cdot \Delta t$$

Lastly,  $x_{der}$  and  $y_{der}$  are the derivatives of the errors, computed using finite differences:

$$x_{der} = \frac{x_{P_{err_t}} - x_{P_{err_{t-1}}}}{\Delta t}$$

$$y_{der} = \frac{y_{P_{err_t}} - y_{P_{err_{t-1}}}}{\Delta t}$$

The PID controllers are identical for both process variables, here we present the schematic of the PID controlling  $x_P$ :

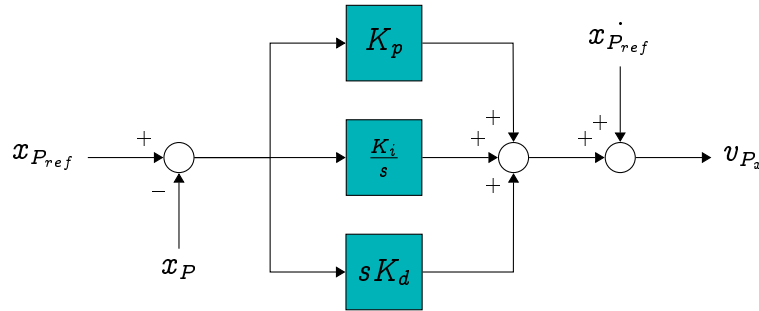


Figure 5.9: PID schematic for controlling  $x_P$

### 5.6.2 Configuration

The node can be configured through the parameters present in the *trajectory\_tracker.yaml* configuration file, in particular we have:

Parameter Name	Values Domain	Description
trajectory_type	0, 1, 2, 3, 4	Desired trajectory shape. Values: 0 linear trajectory; 1 parabolic trajectory; 2 circular trajectory; 3 eight-shape trajectory; 4 cycloidal trajectory.

a_coeff	$\mathbb{R}$	The line describing the linear trajectory is parallel to the direction vector: $\vec{d} = (a\_coeff, b\_coeff)$  (only used when <i>trajectory_type</i> =0)
b_coeff	$\mathbb{R}$	
focal_length	$\mathbb{R}$	Focal length 'a' [m] of the parabolic trajectory described by equation $y = ax^2$ .  (only used when <i>trajectory_type</i> =1)
R	$\mathbb{R}^+$	Radius of the circular trajectory [m].  (only used when <i>trajectory_type</i> =2)
W	$\mathbb{R}^+$	Angular velocity of the circular trajectory [rad/s].  (only used when <i>trajectory_type</i> =2)
a	$\mathbb{R}^+$	Amplitude of the eight shape trajectory [m].  (only used when <i>trajectory_type</i> =3)
w	$\mathbb{R}^+$	Angular velocity of the eight shape trajectory [rad/s].  (only used when <i>trajectory_type</i> =3)
cycloid_radius	$\mathbb{R}^+$	Radius of the wheel [m].  (only used when <i>trajectory_type</i> =4)
cycloid_distance	$\mathbb{R}^+$	Distance from the center of the wheel to the point drawing the cycloid ( $d < r$ ) [m].  (only used when <i>trajectory_type</i> =4)
Kp	$\mathbb{R}^+$	Proportional gain for both PID controllers

Ki	$\mathbb{R}^+$	Integral gain for both PID controllers
Kd	$\mathbb{R}^+$	Derivative gain for both PID controllers
FFWD	0, 1	Feedforward flag for both PID controllers. Values: 0 disable feedforward component; 1 enable feedforward component;
PL_distance	$\mathbb{R}^+$	Distance from the odometric centre of the robot to the selected point P used for the linearization

### 5.6.3 Dynamic reconfigure

The package uses *dynamic reconfigure* to update some parameters at runtime without having to restart the node. In particular, it can be used to change the PIDs configuration:  $K_p$ ,  $K_i$ ,  $K_d$  and FFWD values.

Furthermore, the user can also toggle a boolean flag called "active" to start the trajectory generation (and tracking) process at will.

### 5.6.4 Choiche of PID controller and parameters

Performing an empiric PID tuning, we achieved good performances with a P controller with feed forward enabled; thus setting:

$$K_p = 5 \quad K_i = 0$$

$$K_d = 0 \quad FFWD = true$$

## 5.7 Package CarCommndsFr

### 5.7.1 Intro

### 5.7.2 Configuration

Surface Parameters	
surface_type	Select surface type among 1:DRY, 2:WET, 3:SNOW, 4:ICE, 5:CUSTOM (parameters calculated with racecar values)

### 5.7.3 Launch

### 5.7.4 Node car\_commands\_fr

#### Compute surface type

Values are assigned to coefficients depending on the chosen ground type.

	$B_x$	$B_y$	$C_x$	$C_y$	$D$	$E$
Dry	10	10	1.9	1.9	1	0.97
Wet	12	12	2.3	2.3	0.82	1
Snow	5	5	2	2	0.3	1
Ice	4	4	2	2	0.1	1
Custom	0.21	0.017	1.65	1.3	-548	0.2

#### Compute desired speed

$S$  = slip

$V$  = |speed|

$R_w$  = wheel radius

$M$  = mass

Longitudinal Slip

$$\omega = \frac{V}{R_w}$$



Sempre 0?

$$S_{long} = \frac{V - R_w \omega}{V}$$

Lateral Slip

$$S_{lat} = \arctan\left(\frac{V_y}{V_x}\right)$$

Acceleration

Pacejka Magic Formula

$$y(x) = D \sin\{C \arctan[Bx - E(Bx - \arctan(Bx))]\}$$

$$a_{long} = \frac{y(S_{long})}{M}$$

$$a_{lat} = \frac{y(S_{lat})}{M}$$

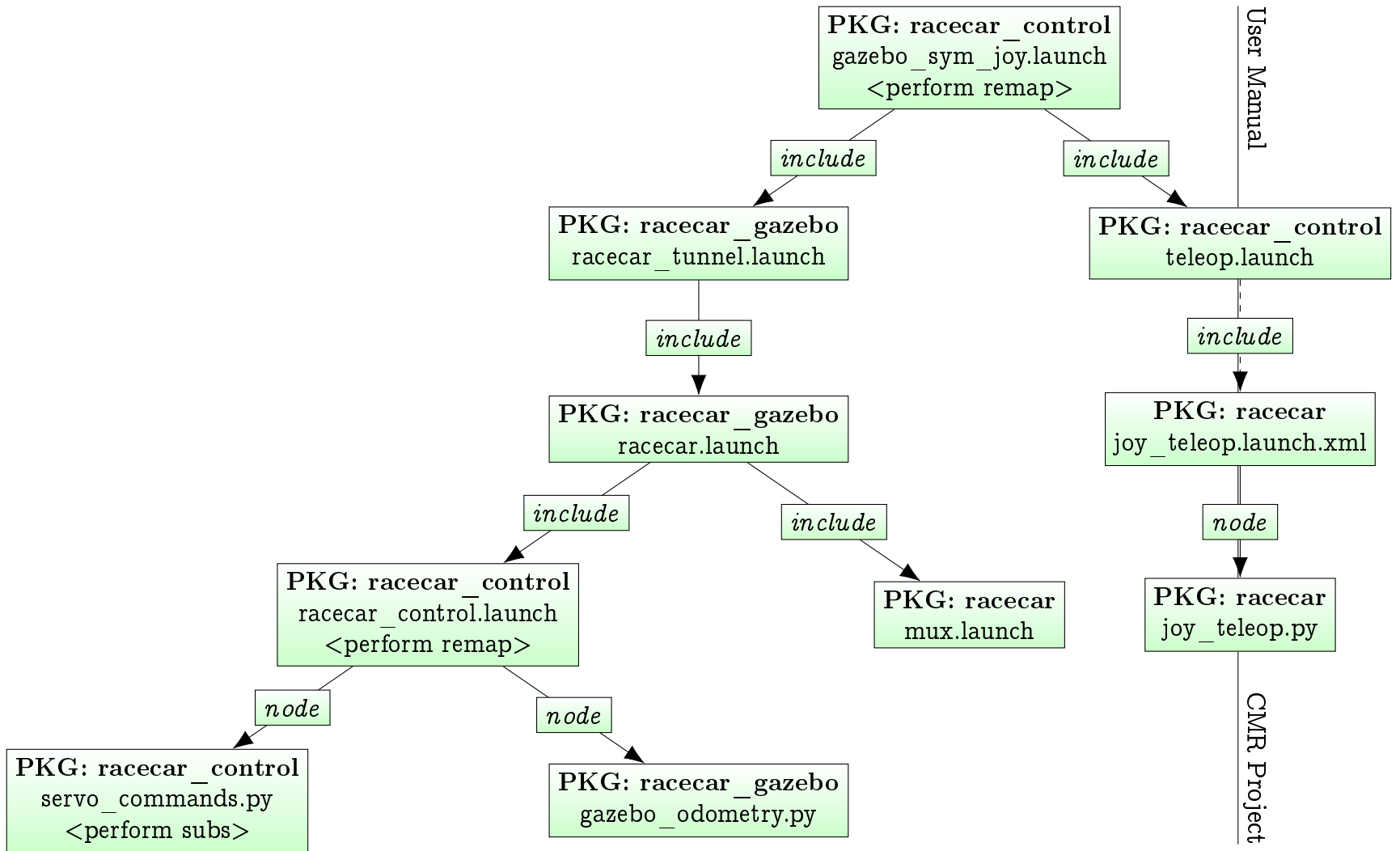
$$a = \sqrt[2]{a_{long}^2 + a_{lat}^2}$$

$$V_{desired} = \frac{\left(V + a \left(\frac{1}{100}\right)\right)}{0.1}$$

# Appendix A

launch package inclusion





```
PKG: racecar_control  
  keyboard_teleop.py  
  <perform publish>
```

Package	File	Remap
racecar	joy_teleop.launch.xml	(none)
racecar	joy_teleop.py	(none)
racecar	mux.launch	(none)
racecar_control	gazebo_sim_joy.launch	REMAP /ackermann_cmd_mux/input/teleop TO /racecar/ackermann_cmd_mux/input/teleop
racecar_control	teleop.launch	(none)
racecar_control	racecar_control.launch	REMAP /racecar/ack/output TO /vesc/low_level/ack/output
racecar_control	servo_commands.py	SUBSCRIBE /racecar/ackermann_cmd_mux/output
racecar_control	keybpard_teleop.py	PUBLISH /vesc/achermann_cmd_mux/input/teleop
racecar_gazebo	racecar_tunnel.launch	(none)
racecar_gazebo	racecar.launch	(none)
racecar_gazebo	gazebo_odometry.py	(none)