A Transient Stability Simulation Package (TSSP)

User's Manual

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Chapter 1. Structure of TSSP

This user's manual is intended to be a guide in utilizing a simulation tool — the transient stability simulation package (TSSP). The package is implemented on an IBM PC in FORTRAN language. It includes a fast decoupled load flow (FDLF) program, a short circuit calculation program (STCC), the transient stability simulation main body (TSSP) and the plotting utility (WPLOT). A minimum of 410K conventional memory is required for a system of 100 buses and a CGA, EGA or VGA graphics card is needed to run the WPLOT program

The fast decoupled load flow (FDLF) algorithm is very reliable and extremely fast. It explores the loose physical interaction between real power and reactive power flow in a power system by mathematically decoupling the $P \sim \theta$ and $Q \sim V$ calculations. This program requires one data file named *pqlf.inp*.

The short circuit calculation (STCC) program, which requires one data file named *ntwk.inp*, can be used to calculate the equivalent impedances of the drive ports of the three sequence networks under both symmetrical and unsymmetrical fault. To run this program, one has to execute the FDLF program first to compute the pre-fault condition.

The transient simulation (TSSP) program includes a coordinator and many modules each of which simulates a power component or a process. The program utilizes the results from FDLF and STCC as the starting point of computation. Then the differential equations describing the dynamics of the system are integrated step by step with a properly chosen length of time step. At each time step, the computed results of these equations are iteratively interfaced with the solution of the network that is described with algebraic equations. At the time step following a disturbance, it is required to execute the FDLF program as both the voltage and the current in the network are not continuous at this operating point. A data file *mach.inp* is required to pass all machine parameters onto the coordinator and related modules.

The overall structure of the package is shown in Fig. 1. Available modules include: machine modules, automatic voltage regulator (AVR) modules, modules for speed governing and turbine systems (SGTS) and modules for power system stabilizers (PSS). User-defined modules can also be interfaced into the software.

To initialize TSSP, the fast decoupled load flow (FDLF) is run first. Then the short circuit calculation (STCC) program is executed. The results of the two runs are passed onto TSSP coordinator internally. Finally the TSSP is run. The end result of the simulation is stored in the file *simu.out*. A data sorting and plotting program (WPLOT) can then be employed to plot a maximum of five curves on one screen and up to fifteen variables can be sorted out at a time. The sorted data can be further utilized by other applications.

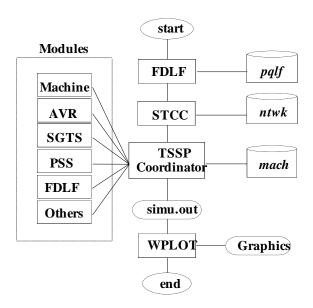


Fig. 1. Overall structure of the TSSP

Chapter 2. Fast Decoupled Load Flow (FDLF) Program

2.1 Bus Numbering

Let us assume that a power system has *n* buses in total, numbered in consecutive numbers starting from *l*, with the ground being always *zero*. There are *m* PQ buses where the injected active and reactive power P and Q are fixed, including those where the P and Q are zero. There is only one *slack* bus where the powers will be calculated after the load flow has been converged to account for power unbalance in the entire system. The rest are PV buses where the active power and the magnitude of the voltage are controlled quantities.

2.2 Preparation of Data File pqlf.inp

A data file named *pqlf.inp* must be prepared for performing the load flow study. This can be done by using the sample data file provided with the FDLF program named *pqlfsam.inp* and by modifying this data file according to the system to be studied.

The sample data file contains simple guidelines for how to input system parameters for the program to conduct the computation. To use this file, simply copy it onto another data file named *pqlf.inp*

Three blocks of data are defined in the data file *pqlf.inp* as described below. Proceeding each block, there are comments and definitions specifying what data are to be entered and how. Any length of comments can be added into the files as long as a (!) precedes each comment line.

2.2.1 System size, convergence criteria and controlling switches

no. of buses = the total number of buses in the system, excluding the grounded bus that is always numbered as zero

max. no. of iterations = computation stop criteria

max. P, Q mismatch = convergence criteria $(0.001 \sim 0.00001 \text{pu})$

ntwk switch = ignored if not conducting stability studies

0, if only FDLF to be executed

1, if STCC and/or TSSP to be executed

per unit switch = 0, if the generation and load are in per unit

based on 100 MVA;

1, if nominal unit MVA is used

2.2.2 Network data

A branch in a power system will fall into one of the following three categories. For each branch one record of data will be required to be input in the data file in the following free format in per unit based on 100MVA. Note that the following parameter notations apply to all branches:

r(+), x(+) = positive sequence resistance and reactance r(-), x(-) = negative sequence resistance and reactance

A). Transmission line shown in Fig. 1 as its equivalent circuit

 $i, j, r(+), r(-), x(+), x(-), b_{i0}$

where

i, j = bus numbers of the two ends of the branch

b_{io} = total line charging susceptance

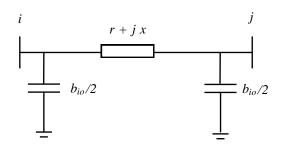


Fig. 1 Equivalent circuit for transmission line.

B). Two winding transformer shown in Fig. 2 as its equivalent circuit

i, -j, r(+), r(-), x(+), x(-), ratio where

- = this negative sign indicating that the ratio is on side j, ratio on side i is not allowed

i, j = bus numbers of the two windings of the transformer

ratio = the actual transformer ratio in per unit on j side

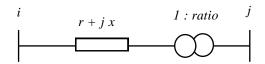


Fig. 2 Equivalent circuit for a two winding transformer.

C). Three winding transformer or auto transformer shown in Fig. 3 as its equivalent circuit

```
i,
     0,
              r_1(+),
                            r_1(-),
                                         x_1(+),
                                                      x_1(-),
                                                                  0.0
                                         x_2(+),
x_2(+),
                            r_2(-),
                                                      x_2(-),
    - j,
              r_2(+),
                                                                 ratio
                                         x_3(+),
                            r_3(-),
0,
    - k,
              r_3(+),
                                                      x_3(-),
                                                                 ratio
```

where

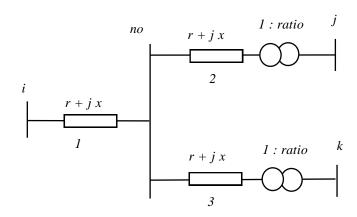
ratio

this negative sign indicating that the ratio is on side j or ratio on side i is not allowed

i, j, k = bus numbers of the three windings of the transformer

o = neutral point of the transformer

1, 2, 3 = indicating the three windings



= the actual transformer ratio in per unit on j side

Fig. 3 Equivalent circuit for a three windings or auto transformer.

D). Grounded line shown in Fig. 4 as its equivalent circuit:

r(+)r(-), x(+)x(-),1.0 i, 0, or b(+), 0, g(-), b(-), - 1.0 g(+),where = bus number of the grounded branch g(+), b(+)= positive sequence conductance and susceptance of the branch = negative sequence conductance and susceptance of the g(-), b(-) branch 1.0, - 1.0 = indicating impedance and admittance, respectively

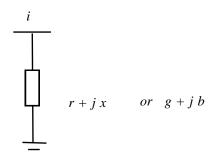


Fig. 4 Equivalent circuit for a grounded line.

If only the fast decoupled load flow (FDLF) program is to be executed, the negative sequence parameters can be entered as any real numbers. Otherwise the actual values should be entered.

To end branch data input, use 0/ as a record of data in a new line.

2.2.3 Bus data

For a bus belonging to one or more categories of the following four, one record of data must be entered. No data are required to be entered for buses which do not belong to the defined categories. The four categories are:

- a) the voltage magnitude of the bus is regulated
- b) one or more generators are present
- c) a load is present
- d) a SVC is present

The data to be entered for each bus are of the following format:

 $i, \quad bus_type, \quad P_{\scriptscriptstyle G}, Q_{\scriptscriptstyle G}, P_{\scriptscriptstyle L}, Q_{\scriptscriptstyle L}, V_0$ where

i = bus number

bus type = 1, if it is a PQ bus

2, if it is a PV bus

3, if it is the slack bus

 P_{G} , Q_{G} = active and reactive generation in p.u. or MVA,

respectively

 P_L, Q_L = active and reactive load in p.u. or MVA, respectively

 V_0 = given voltage in p.u., if the bus_type is 2 or 3

1.0, if bus_type is 1

To end bus data input, use 0/ as a record of data in a new line.

Chapter 3. Short Circuit Calculation (STCC) Program

3.1 Symmetrical and Asymmetrical Faults

Power system faults can be categorized into two classes, symmetrical and asymmetrical. Symmetrical faults can be easily modeled in both short circuit calculations and stability study, because the three phases of the network are still symmetrical after the disturbance. In case of asymmetrical faults, the network has to be decomposed into three symmetrical ones to obtain accurate modeling. They are positive, negative and zero sequence networks, respectively. Accurate modeling can be accomplished for short circuit analysis based on these sequence networks, while for stability studies it could be cumbersome and very difficult to do three phase time domain simulation for even a medium size power system.

Assume that only a single asymmetrical fault happens at a time. I has been understood that the average braking torque produced by the reaction of the two magnetic fields, one produced by the negative sequence current and the other by the rotor winding current, is approximately zero, and that zero sequence currents yield a zero compound torque as the three-phase zero sequence currents are electrically in phase and have 120 degree displacement in space. Hence only the positive sequence quantities are needed to be computed during a transient process. However, the negative and zero sequence networks have to be incorporated into the positive sequence network, at the faulted point through an *additional impedance* Z_{eq} can be calculated that is a certain combination of the negative and zero sequence impedances (Z_- , Z_0), fault impedance Z_f and grounding impedance Z_g .

3.2 Data Preparation

A data file named *ntwk.inp* is required to perform a short circuit analysis. This can be done by using the sample data file provided with the STCC program named *ntwksam.inp* and modify this data file according to the system and fault type under study.

This sample data file contains simple guidelines for inputting fault information and system parameters. To use this file, simply copy it to another data file named *ntwk.inp*.

3.2.1 Fault information

no of buses the total number of buses in the system, excluding the grounded one that is always numbered as zero no of fault 1. only one fault at a time

no of events no of events of the fault

fault at nearby the bus with a minus (-) sign $\pm i$, $\pm j$ i, i denote the bus numbers of the two ends

of the line on which the fault occurs

double/single circuit = 2, indicating the faulted line is

a double circuit

1, indicating the faulted line is a single circuit

0, indicating no fault during this event (prefault)

start time starting time of a event (≥ 0.0) =

end time = ending time of a event (> starting time)

grounding impedance in p.u., Z_{gnd}

it is a complex number

fault impedance in p.u., it is a complex number Zfault

fault type indicator 3-phase-to-ground

> 1-phase-to-ground 2-phases-to-ground phase-to-phase 1-phase-open 2-phases-open

3.2.2 Positive, negative sequence network data

This block of data is similar to that described in FDLF, see 2.4 for details. The only difference is that the sequence impedance for each generator must be entered here. The negative sequence parameters must be entered as the actual data obtained from either nameplates or tests.

3.2.3 Zero sequence network data

The zero sequence network configuration and its parameters are dependent on the connections of the various power components and the location of the fault.

1) Transmission lines

All the transmission lines in the system will be present in the data file, no matter whether they are in service or not during the fault. The raison for this is that in this way different faults at different locations can be modeled without changing the zero sequence parameters of the various power components in the system.

Generally the zero sequence impedance of a transmission line is $2 \sim 5$ times the positive sequence impedance. For each such line, one record of data of the following free format is entered:

```
i, \quad j, \quad r(0), \quad x(0), \quad b(0)
where
```

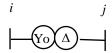
i, j = bus numbers of the two ends of a line
 (0) = indicating zero sequence parameters

2) Transformers

The zero sequence reactance of a transformer is dependent on the structure of the transformer and network configuration connected to it. The following list serves as examples of how the zero sequence reactances of the transformers are recognized and prepared in the data file. The following notations apply whenever appropriate.

```
x_n = grounding reactance of a transformer x_{mo} = zero sequence magnetizing reactance i, j, k = bus numbers of the three windings x_1, x_2, x_3 = leakage reactances of the three windings numbered 1, 2, 3 that are connected to bus i, j, k, respectively no = neutral point of a multiwinding transformer o = grounding indication except otherwise stated l/l = indicating parallel connection of two reactances
```

A) Wye-grounded Delta connected two-winding transformers

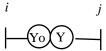


One record of data of free format is entered.

i, 0,
$$\mathbf{r}(0)$$
, $\mathbf{x}(0)$, 1.0
where
$$\mathbf{x}(0) = 3 \mathbf{x}_n + \mathbf{x}_1 + \mathbf{x}_2 /\!/ \mathbf{x}_{mo}$$

$$= 3 \mathbf{x}_n + \mathbf{x}(+), \text{ if } \mathbf{x}_{mo} \text{ is very large or infinitive}$$

B) Wye-grounded Wye connected two-winding transformers



One record of data of free format is entered.

i, 0,
$$r(0)$$
, $x(0)$, 1.0

where

$$x(0) = 3 x_n + x_1 + x_{mo}$$

C) Wye Wye connected two-winding transformers



No date are entered.

D) Wye-Wye-grounded two-winding transformers



Three records of data of free format are entered.

i, j,
$$r(0)$$
, $x_{ii}(0)$, 0.0

i, 0,
$$r(0)$$
, $x_{io}(0)$, 1.0

j, 0,
$$r(0)$$
, $x_{i0}(0)$, 1.0

where

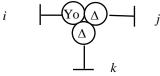
$$x_{ij}(0) = (x_1 * x_2 + x_2 * x_{mo} + x_{mo} * x_1) / x_{mo}$$

 $x_{io}(0) = (x_1 * x_2 + x_2 * x_{mo} + x_{mo} * x_1) / x_2$

$$x_{io}(0) = (x_1 * x_2 + x_2 * x_{mo} + x_{mo} * x_1) / x_2$$

$$x_{jo}(0) = (x_1 * x_2 + x_2 * x_{mo} + x_{mo} * x_1) / x_1$$

E) Wye-grounded Delt Delta connected three-winding transformers



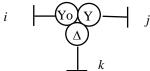
One record of data of free format is entered.

i, 0,
$$r(0)$$
, $x(0)$, 1.0

where

$$x(0) = x_1 + x_2 // x_3$$

F) Wye-grounded Wye Delta connected three-winding transformers



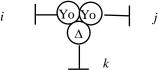
One record of data of free format is entered.

i, 0, r(0), x(0), 1.0

where

$$\mathbf{x}(0) = \mathbf{x}_1 + \mathbf{x}_2$$

G) Wye-Wye-grounded Delta connected three-winding transformers



Three records of data of free format are entered.

i, no,
$$r_1(0)$$
, $x_1(0)$, 1.0

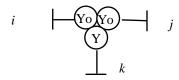
no, j,
$$r_2(0)$$
, $x_2(0)$, 1.0

no, 0,
$$r_3(0)$$
, $x_3(0)$, 1.0

where

$$x_{30} = x_3(0) // x_{mo}$$

H) Wye- Wye-grounded Wye connected three-winding transformers



Three records of data of free format are entered.

i, no,
$$r_1(0)$$
, $x_1(0)$, 1.0

no, j,
$$r_2(0)$$
, $x_2(0)$, 1.0

3) Synchronous machines

The passage of a zero sequence current from the network to the ground through a generator will be dependent on the structure of the generator and its connection to the network. If no passage exists, no zero sequence impedance for the generator is required to be entered. Otherwise the actual zero sequence impedance and the grounding impedance if any should be entered for that generator.

To end data input for zero sequence branches, use 0/ as a record of data in a new line.

4) Bus classification

All the buses in the zero sequence network under a fault can be classified into two groups. One is that of which the buses are **in** the zero sequence network, while the other is that of which they are **not in** the zero sequence network.

There are two ways to input this information which will be used to form the zero sequence network admittance. If the bus numbers which are **not** in the zero sequence network are chosen to be input, a '-1' is entered as the first record in this block of data. If the bus numbers which are in the zero sequence network are chosen to be input, a '+1' is entered as the first record. These two sets of buses are complementary to each other. Usually the smaller set is chosen. A slash (/) is added only to the end of the bus number list to end it. The list can have as many lines as needed. A coma(,) is also necessary between bus numbers.

Chapter 4. Transient Stability Simulation Program (TSSP)

4.1 Sample data file: machsam.inp

A sample data file named *machsam.inp* is provided with the program. Simple guidelines are also included in the file. To use this file, simply copy it to a file named *mach.inp*.

4.2 Modify your data file: mach.inp

There are five blocks of data in this data file, corresponding to the following categories: computing control variables, synchronous machines, excitation systems, speed governing and turbine systems, and power system stabilizers, respectively.

4.2.1 Computing control variables

time step length = this is the step length used through out the

TSSP in integrating differential equations

 $(0.05 \sim 0.0005 \text{ sec})$

printing interval = this is the sample frequency to output

simulated state variables (0.01 ~.50 sec)

no of generators = this number is entered here again

4.2.2 Synchronous machines

Five synchronous machine models, including the one for infinite-busbar modeling, have been incorporated in TSSP. Their input data formats are given below, respectively.

A) Two-axis model with subtransient

This is a subtransient machine model designated as model #4. It has a field winding (f), one damper winding (D) on d-axis and one damper winding (Q) on q-axis.

Generator #,4

$$M_{base}$$
, H , r_{a} , x_{ℓ}
 x_{d} , $x_{d}^{'}$, $x_{d}^{''}$, $x_{q}^{''}$, $x_{q}^{''}$
 $\tau_{do}^{'}$, $\tau_{do}^{''}$, $\tau_{qo}^{''}$
 D , A_{G} , B_{G} , or D , S_{10} , S_{12} , -1

B) Two-axis model with transient only

This is a transient model for round-rotor machines. It has a field winding (f) on d-axis, one damper winding (Q) on q-axis. It is similar to model #4, but its subtransient is ignored. It is designated as model #3.

Generator#,3
$$M_{base}, H, r_a, x_{\ell}$$

$$x_d, x_d^{'}, x_q, x_q^{'}$$

$$\tau_{do}^{'}, \tau_{qo}^{'}$$

$$D, A_G, B_G \text{ or } D, S_{10}, S_{12}, -1$$

C) One-axis model with transient

This is also a transient model. It has only one rotor winding, i.e., the field winding (f). It is designated as model #2.

Generator#,2
$$M_{base}, H, r_a, x_{\ell}$$

$$x_d, x_d^{'}, x_q$$

$$\tau_{do}^{'}$$

$$D, A_G, B_G \text{ or } D, S_{1,0}, S_{1,2}, -1$$

D) Classic model

This is a representation of the synchronous machine where its transient effects have been totally ignored. It is designated as model #1.

Generator#,1 M_{base}, H, r_a, x_ℓ x_d, x_d $D, A_G, B_G \text{ or } D, S_{1.0}, S_{1.2}, -1$

E) Infinite bus

The infinite bus is treated as a machine with large inertia constant and only the input of an assumed machine capacity(MVA), usually 100.0, is required.

Generator#,0

 M_{base}

4.2.3 Excitation systems

Fur groups of excitation systems can be simulated in the TSSP. They are DC, AC, ST and modified types.

1) Type DC systems

They are exciters with rotating direct current commentator. They are designated as model #11 ~ model #14.

A) Field controlled DC commutator exciters with continuously acting voltage regulators

Exciter #, 11 K_A, K_E, K_F T_C, T_B, T_A, T_E, T_F $V_{RMIN, V_{RMAX}}$ $A_E, B_E \ Or \ E_I, S_I, E_2, S_2, -1$

B) Field controlled DC commutator exciters with continuously acting voltage regulators, having supplies obtained from the generator or auxiliaries bus voltage

Exciter #, 12

$$K_A$$
, K_E , K_F
 T_C , T_B , T_A , T_E , T_F
 V_{RMIN} , V_{RMAX}
 A_E , B_E 0 r E_I , S_I , E_2 , S_2 , -1

C) Field controlled DC commutator exciters with non-continuously acting voltage regulators

Exciter #, 13
$$K_{E}, K_{V}$$

$$T_{RH}, T_{E}$$

$$V_{RMIN}, V_{RMAX}$$

$$A_{E}, B_{E} \text{ Or } E_{I}, S_{I}, E_{2}, S_{2}, -1$$

D) Modified DC type 2 excitation system with its block diagram shown in Fig. 5

Exciter #, 14
$$K_A, K_E, K_F$$

$$T_C, T_B, T_A, T_E, T_F$$

$$V_{RMIN, V_{RMAX}}$$

$$A_E, B_E \ Or \ E_I, S_I, E_2, S_2, -1$$

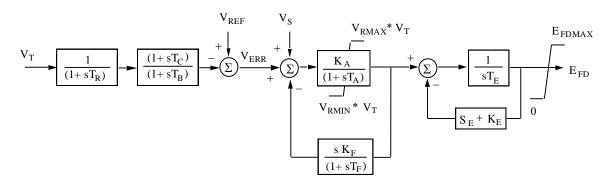


Fig. 5 Modified IEEE DC type 2 exciter.

2) Type AC systems

They are alternator supplied rectifier excitation systems designated as model # 21 \sim model #24.

A) Field controlled alternator rectifier excitation systems

Exciter #, 21
$$K_A, K_C, K_D, K_E, K_F$$

$$T_C, T_B, T_A, T_E, T_F$$

$$V_{RMIN}, V_{RMAX}$$

$$A, B$$

B) High initial response field controlled alternator rectifier excitation systems

Exciter #, 22
$$K_A, K_C, K_D, K_E, K_F, K_H, K_L$$

$$T_C, T_B, T_A, T_E, T_F$$

$$V_{AMIN}, V_{AMAX}, V_{RMIN}, V_{RMAX}$$

$$A, B, V_{LR}$$

C) Field controlled alternator rectifier excitation systems

Exciter #, 23
$$K_A, K_C, K_D, K_E, K_F, K_N, K_R, K_{LV}$$

$$T_C, T_B, T_A, T_E, T_F$$

$$V_{AMIN}, V_{AMAX}$$

$$A, B, V_{LR}$$

D) Alternator supplied controlled rectifier excitation systems

Exciter #, 24
$$K_A, K_C$$

$$T_C, T_B, T_A$$

$$V_{AMIN}, V_{AMAX}, V_{RMIN}, V_{RMAX}$$

3) Type ST systems

They are static excitation systems and designated as model #31 ~ model #33.

A) Type ST1 potential source controlled rectifier excitation system supplied through a transformer from either the bus terminal or the auxiliary bus of the unit and regulated by a controlled rectifier

Exciter #, 31

$$K_A, K_C, K_F$$

$$T_C, T_B, T_A, T_E$$

$$V_{AMIN}, V_{AMAX}, V_{RMIN}, V_{RMAX}$$

B) Type ST2 compound source controlled rectifier excitation system supplied by a phaser combination of terminal voltage VT and terminal current IT

Exciter #, 32

$$K_A, K_C, K_E, K_F, K_I, K_P$$

$$T_A, T_E, T_F$$

$$V_{RMIN}, V_{RMAX}, E_{FDMAX}$$

C) Type ST3 compound source controlled rectifier excitation system similar to model # 32, with internal quantities of the unit being used to form the source of the excitation power

Exciter #, 33

$$K_A, K_C, K_G, K_I, k_{PR}, K_{PI}g$$

$$T_C, T_R, T_I$$

$$V_{IMIN}, V_{IMAX}, V_{RMIN}, V_{RMAX}, E_{FDMAX}, V_{GMAX}$$

4) Modified type excitation systems

They are SCRX type exciters and designated as model #41 ~ model #42.

A) Solid state exciter SCRX is supplied either from the ac bus voltage (busfed = 1) or from a fixed independent source (busfed = 0). If the exciter can accept negative current, then set the Neglogic = 1, otherwise 0. The block diagram of the exciter is shown in Fig. 6.

Exciter #, 41 K_E , Neg log ic, Busfed T_I , T_B , T_A , T_E E_{MIN} , E_{RMAX}

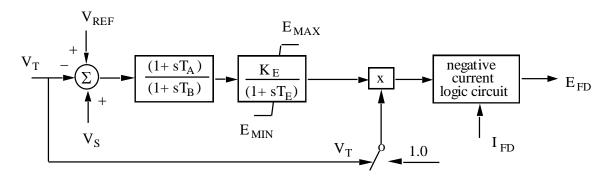


Fig. 6 SCRX excitation system fed either by bus or by solid.

B) SCRXIL model with maximum field current limit (Ifdmax)

Exciter #, 42 K_E , Neg log ic, Busfed T_I , T_B , T_A , T_E E_{MIN} , E_{RMAX} , I_{FDMAX}

4.2.4 Speed Governing and Turbine Systems

Two categories of speed governing and turbine systems: speed governing and steam turbine system, and speed governing and hydro turbine systems.

1) Speed governing and steam turbine systems

They are designated as model #211~#216.

A) Non-reheat steam system

Governor#,211
$$T_{CH}$$
 $\dot{G}_{MIN}, \dot{G}_{MAX}, G_{MIN}, G_{MAX}$
 T_3, T_2, T_1

B) Tandem - Compound, Single - Reheat steam systems

Governor#,212
$$T_{CH},T_{RH},T_{CO}$$

$$F_{HP},F_{IP},F_{LP},K$$

$$\dot{G}_{MIN},\dot{G}_{MAX},G_{MIN},G_{MAX}$$

$$T_{3},T_{2},T_{1}$$

C) Tandem - Compound, Double - Reheat steam systems

Governor#,213
$$T_{CH},T_{RHI},T_{RH2},T_{CO}$$

$$F_{VHP},F_{HP},F_{IP},F_{LP},K$$

$$\dot{G}_{MIN},\dot{G}_{MAX},G_{MIN},G_{MAX}$$

$$T_{3},T_{2},T_{I}$$

D) Cross - Compound , Single - Reheat steam systems

Governor#,214
$$T_{CH},T_{RH},T_{CO}$$

$$F_{HP},F_{IP},F_{LP/2},F_{LP/2},K$$

$$\dot{G}_{MIN},\dot{G}_{MAX},G_{MIN},G_{MAX}$$

$$T_{3},T_{2},T_{1}$$

E) Cross - Compound, Single - Reheat steam systems

Governor#,215
$$T_{CH},T_{RH},T_{CO}$$

$$F_{HP},F_{IP},F_{LP},K$$

$$\dot{G}_{MIN},\dot{G}_{MAX},G_{MIN},G_{MAX}$$

$$T_{3},T_{2},T_{1}$$

F) Cross - Compound, Double - Reheat steam systems

Governor#,216
$$T_{CH},T_{RHI},T_{RH2},T_{CO} \\ F_{VHP},F_{HP},F_{IP/2},F_{IP/2},F_{LP/2},F_{LP/2},K \\ \dot{G}_{MIN},\dot{G}_{MAX},G_{MIN},G_{MAX} \\ T_3,T_2,T_I$$

2) Speed governing and hydro turbine systems

They are designated as model #221~#222.

A) Accurate speed governing and turbine system for hydro generators

Governor#,221
$$T_{W},T_{P},T_{G},T_{R}$$
 σ,δ

$$\dot{G}_{MIN},\dot{G}_{MAX},G_{MIN},G_{MAX}$$

$$T_{3},T_{2},T_{I}$$

B) Approximate speed governing and turbine system for hydro generators

Governor#,222
$$T_W, T_1, T_2, T_3$$
 K
 P_{MIN}, P_{MAX}

4.2.5 Power system stabilizers

Three power system stabilizer models are incorporated in TSSP. Different signals can be employed as input. These input signals are identified by the following input type indicators:

- 1 = deviation of rotor speed in per unit
- 2 = net accelerating power in per unit
- 3 = electrical power in per unit
- 4 = deviation of terminal voltage in per unit
- 5 = deviation of terminal frequency
- A) Power system stabilizer with Fig. 7 as its block diagram, identified as IEEEST PSS in TSSP

Input type indicator

 A_{1}

$$T_1, T_2, T_3, T_4, T_5, T_6$$

$$K_S$$
, V_{MIN} , V_{MAX}

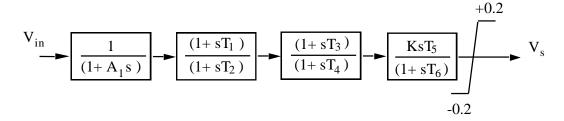


Fig. 7 Model IEEEST power system stabilizer

B) Power system stabilizer with Fig. 8 as its block diagram, identified as IEEESN PSS in TSSP

Stabilizer #,312

Input type indicator

 A_{I}

 $T_1, T_2, T_3, T_4, T_5, T_6$

 K_S, V_{MIN}, V_{MAX}

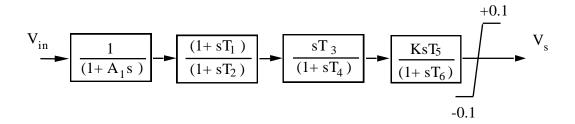


Fig. 8 Model IEEESN power system stabilizer.

C) Power system stabilizer with Fig. 9 as its block diagram, identified as IEEE standard PSS in TSSP

Stabilizer #,313 Input type indicator $A_1, A_2, A_3, A_4, A_5, A_6$ $T_1, T_2, T_3, T_4, T_5, T_6$ K_S, V_{MIN}, V_{MAX}

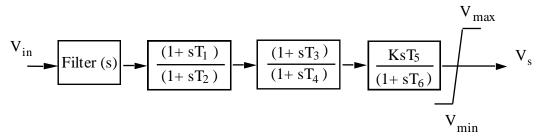


Fig. 9 IEEE standard PSS model.

where the transfer function of the filter in the diagram can be expressed by:

$$\frac{(\,I + A_5\,s + A_6\,s^2\,)}{(\,I + A_1\,s + A_2\,s^2\,)(\,I + A_3\,s + A_4\,s^2\,)}$$

Chapter 5. Numerical Examples

5.1 The Sample System

The WSCC simplified three machine system [12] is used to illustrate how to prepare the data files needed to perform load flow and stability studies. The system has three generators, three loads and nine buses. A single line diagram of the system is given in Fig. 10. Complete system data and generator parameters can be found in [12]. A three phase to ground fault on line 5-7 near bus 7 for a period of 5 cycles (0.083s) is applied to the system. The fault is cleared by opening the line. This scenario can be used to study the effects of various power components.

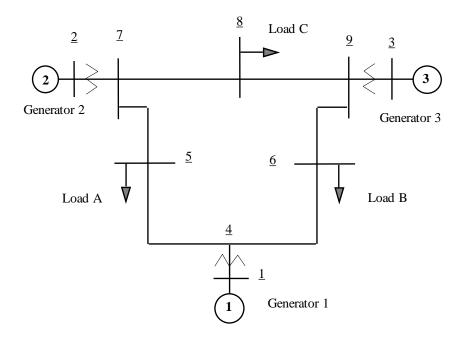


Fig. 10 Single line diagram of the WSCC system

5.2 Data file pqlf.inp and load flow results

! Example: 3-machine 9-bus sy! Data file for P-Q Decoupled L	
! ⇒no of max. max. P, Q	ntwk pu (0)
! buses iterations mismatch	switch MVA (1)

```
30 , 0.0001 , 0 ,
     9,
                                           1 /
l ------
! ⇒Positive(+), negative(-) sequence network data:
  This block of data can be copied to or from the ntwk.inp file.
  Attention should be paid to that the grounded
  reactances of the generators used in ntwk.inp data file
  are excluded here.
                   r(-), x(+),
                                  x(-), ratio/b/1.0/-1.0
            r(+)
1 -----
                          0.0576, 0.0576,
   1,
      -4,
            0.000,
                   0.000,
                                          1.000/
      -7,
                   0.000,
                          0.0625, 0.0625,
                                          1.000/
   2,
            0.000,
   3,
      -9,
            0.000,
                   0.000,
                          0.0586, 0.0586,
                                          1.000/
                          0.0850, 0.0850,
   4,
       5,
            0.010,
                   0.010,
                                         0.176/
                          0.0920, 0.0920,
   4.
            0.017,
                   0.017,
                                         0.158/
       6,
   5,
       7,
                          0.1610, 0.1610,
            0.032,
                   0.032,
                                         0.306/
   6,
       9.
            0.039,
                   0.039,
                          0.1700, 0.1700,
                                         0.358/
            0.0085, 0.0085, 0.0720, 0.0720,
   7,
       8,
                                          0.149/
   8,
       9,
            0.0119, 0.0119, 0.1008, 0.1008,
                                          0.209/
   0 /
! ⇒Bus data input includes the following:
1 ------
! bus | bus | generation | load | voltage |
! no | type | PG
                   QG | PL
                              QL
                                 |V(pu)|
                                   1.04/
 1.
            0.0.
                 0.0,
                       0.0,
                             0.0,
 2.
            163.0, 6.7,
                             0.0,
                                   1.00/
      1,
                       0.0,
 3.
            85.0, -10.9, 0.0,
                             0.0.
                                   1.00/
      1.
 5,
      1,
            0.0,
                 0.0,
                       125.0, 50.0,
                                   1.00/
      1.
            0.0.
                  0.0.
                       90.0, 30.0,
                                   1.00/
 6,
                  0.0,
                       100.0, 35.0,
                                   1.00/
 8,
            0.0.
 0/
______
        end of data file
```

The load flow FDLF program was executed, the following table lists generations (MVA), loads (MVA) and bus voltages (magnitude in p.u. and angle in degrees):

P-Q Decoupled LF converged at 9th iteration!

I	TYF	PE PG	QG	PL	QL	V	ANGL
			-		-		
1	3	71.64069	27.03000	.00000	.00000	1.04000	0.00000

2	1	163.00000	6.70000	.00000	.00000	1.02508	9.27864
3	1	85.00000	-10.90000	.00000	.00000	1.02497	4.66492
4	1	.00000	.00000	.00000	.00000	1.02580	-2.21676
5	1	.00000	.00000	125.00000	50.00000	.99565	-3.98875
6	1	.00000	.00000	90.00000	30.00000	1.01266	-3.68737
7	1	.00000	.00000	.00000	.00000	1.02582	3.71904
8	1	.00000	.00000	100.00000	35.00000	1.01591	.72731
9	1	.00000	.00000	.00000	.00000	1.03234	1.96678

5.3 Data file ntwk.inp

```
Data file for short circuit calculations
     -----
! \Rightarrow No \text{ of buses }, no of faults and no of events:
   nbus, nfault, nevent/
1_____
! ⇒Fault information input: ( time in seconds )
  The sequence events of a disturbance are distributed on TIME-axis
   as follows:
  0.0 ----- .3 ----- .4 ----- 10.0
  | pre-fault | fault period | post-fault | autoreclose |
! | | | db/s| start | end |
! | i | j | cir. | time | time | Zgnd | Zfault
 -7, 5, 0, 0.0,
                   0.0, (0,0),
                                 (0,0) /
  -7, 5, 1, 0.0,
                   0.1, (0,0),
                                 (0,0) /
                  20.1, (0,0),
  -7, 5, 1, 0.1,
                                 (0,0) /
  -7, 5, 1, 20.0, 20.0, (0,0),
                                 (0,0) /
! ⇒Fault type indicator input:
  Choosing by deleting [!!!] at beginning of a line.
  If no fault, no [!!!!] should be deleted.
3-phase-to-ground
! !!! 1-phase-to-ground
! !!! 2-phases-to-ground
! !!! phase-to-phase
! !!! 1-phase-open
! !!! 2-phases-open
! ⇒Positive(+), negative(-) sequence network data:
```

i,	j,	r(+),	r(-),	x(+), x	(-), ratio/b	0/1.0/-1.0
1,	-4,	0.000,	0.000,	0.0576,	0.0576,	1.0 /
2,	-7,	0.000,	0.000,	0.0625,	0.0625,	1.0 /
3,	-9,	0.000,	0.000,	0.0586,	0.0586,	1.0 /
4,	5,	0.010,	0.010,	0.0850,	0.0850,	0.176/
4,	6,	0.017,	0.017,	0.0920,	0.0920,	0.158/
5,	7,	0.032,	0.032,	0.1610,	0.1610,	0.306/
6,	9,	0.039,	0.039,	0.1700,	0.1700,	0.358/
7,	8,	0.0085,	0.0085,	0.0720,	0.0720,	0.149/
8,	9,	0.0119,	0.0119,	0.1008,	0.1008,	0.209/
1,	0,	0.0,	0.0,	0.0608,	0.0608,	1.0/
2,	0,	0.0,	0.0,	0.1198,	0.1198,	1.0/
3,	0,	0.0,	0.0,	0.1813,	0.1813,	1.0/
0 /						

 $! \Rightarrow Zero(0)$ sequence network data:

! 1) The non-grounded lines are:

Yo/Yo connected three-winding transformer branches; Yo/Yo connected single-winding transformer branches; Transmission lines.

- ! 2) The grounded zero sequence reactancs are:
 ! generator grounding during a fault. Usually they
 ! do not contribute to zero sequence currents
 ! if the generator-transformers are in
 ! Delta/Delta connection.
- ! 3) Other kinds of grounded reactances are:
 ! Yo/Delta two-winding transformers;
 ! tertiary windings of Yo/Yo/Delta
 ! connected three winding transformers.

!	i,	j,	r(0),	x(0),	b/1.0/-1.0	
٠	1,	4,	0.000,	0.0576,	1.0 /	
	2,	7,	0.000,	0.0625,	1.0 /	
	3,	9,	0.000,	0.0586,	1.0 /	
	4,	5,	0.010,	0.0850,	0.176/	
	4,	6,	0.017,	0.0920,	0.158/	
	5,	7,	0.032,	0.1610,	0.306/	
	6,	9,	0.039,	0.1700,	0.358/	
	7,	8,	0.0085,	0.0720,	0.149/	

```
8.
          9, 0.0119,
                        0.1008,
                                      0.209/
     1.
          0, 0.0,
                        0.0608.
                                      1.0/
     2,
          0, 0.0,
                        0.1198,
                                      1.0/
     3,
          0, 0.0,
                        0.1813,
                                      1.0/
     0 /
!\RightarrowInput the bus numbers which are either in(1) or not in(-1)
   the zero sequence network under the fault in concern.
   The in_zero sequence network bus set is chosen here,
   hence a '1/' is input as the first record of data in this
   data block. Transmission lines will be automatically
   connected to these buses, including line charges. If the fault
   location changes, it may be necessary to modify this list.
   This bus list is required for both 'during fault' period and
   'fault cleared' period.
 -1 /
                                             / during fault
 0 /
-1/
                                             / fault cleared
 0 /
1_____
           End of data file
```

5.4 Data file mach.inp

```
Example: 3-machine 9-bus system
         Data file for stability study
  ______
! \Rightarrow \text{No of machines, time step, print interval}
! ------
       13 , 0.002 , 0.02 /
_____
! ⇒Machine no, model no and corresponding parameters
  (for detail, please refer to the user's manual)
! Data input examples:
! 1, 4/
                           / generator no, Model #:
                        / Mbase, H, R, Xl
! 13.2, 2.24, 0.0, 0.326
! 1.05, 0.3818, 0.344, 0.741, 0.344 / Xd,Xdo',Xdo'',Xq,Xqo''
! 2.62, 0.0500, 0.060
                           / Tdo', Tdo", Tqo"
```

```
! 0.00, 0.2470, 0.5612, -1
                                    / damp,s(1.0),s(1.2),-1
! 11, 2/
                                    / Gen #, Model #:
! 3.0, 2.7 , 0.0 , 0.0
                                    / Mbase, H, R, Xl
! 0.876, 0.272, 0.5
                                    / Xd , Xdo', Xq
! 2.27
                                    / Tdo'
! 0.00, 0.179, 0.43, -1/damp,s(1.0),s(1.2),-1
! 13,0
                                    / infinite bus
! 100
                                    / capacity of system
 1, 3 /
 245.7, 23.64,
                 0.0,
                          0.0336
 0.146, 0.0608, 0.0969, 0.0969
                                    /
 8.96, 0.001
                                    /
 0.0,
        0.0,
                 0.0
 2, 3 /
 192.0, 6.4,
                 0.0,
                          0.0521
 0.8958,0.1198, 0.8645, 0.1969
 6.0,
        0.535
 0.0,
        0.0,
                 0.0
 3, 3 /
 128.0, 3.01,
                 0.0,
                          0.0742
 1.3125,0.1813, 1.2578, 0.25
 5.89, 0.6
 0.0,
        0.0,
                 0.0
! -----
!⇒ Exciter model no and its parameters
   (for detail, please refer to the user's manual)
   Data input examples:
! 1 , 41/
                                    / Gen #, AVR model #
! 56.0, 1, 1
                                    / Ke, neg. logic, busfed
! 0.0, 1.0, 1.0, 0.035
                                    /T1, Ta, Tb, Te
! -3.94, 3.94
                                    / Emin , Emax
! 10,14/
                                    / EXDC2B model
  369.0, 1.000, 0.022
                                    / Ka, Ke, Kf
  1.000, 0.226, 0.000, 2.000, 1.0
                                    / Tc, Tb, Ta, Te, Tf1
  -3.97, 4.960
                                    / Vrmin, Vrmax
  1.830, 0.108, 2.3570, 0.506, -1
                                    /E1, S1, E2, S2, -1
   13, 888 /
                                    / no AVR
 1, 11 /
 25.0,
        -0.044, 0.0805
 0.0,
        0.0,
               0.20, 0.50, 0.35
```

```
-1.0,
        1.0
0.0016, 1.465
 2, 11 /
400.0, -0.17, 0.0400
0.0.
        0.0.
               0.05, 0.95, 1.00
-3.5,
        3.5
0.0039, 1.555
3,41/
 56.0, 1,
               1
0.0,
        1.0,
               1.0,
                     0.035
 -3.94, 3.94
!⇒ Turbine governor model no and its parameters
   (for detail, please refer to the user's manual)
  Data input example:
  1, 222/
                                   / Gen #, governor model #
  0.620, 0.320, 3.290, 33.150
                                   / Tw, T1, T2, T3
  20.0
                                   / K
  0.00, 1.05
                                   / Gmin, Gmax
                                   / Gen #, governor model #
  8,221/
  1.05, 0.05, 0.24, 4.2
                                   / Tw, Tp, Tg, Tr
  0.03, 0.55
                                   / perm-R, temp-r
                                   /Ġ<sub>min</sub>,Ġ<sub>max</sub>, Gmin,Gmax
  -0.16, 0.16, 0.00, 1.0
! 13,888/
                                   / no governor here
 1, 212 /
0.1,
        5.0, 0.35
0.3,
        0.4, 0.3,
                    20.0
-2.0,
        2.0, 0.0,
                    1.05
0.2,
        0.0, 0.0
 1, 221 /
 1.05,
        0.05, 0.24, 4.2
0.03,
        0.55
-0.16,
        0.16, 0.0, 1.1
 1, 222 /
0.62,
        0.320,3.290, 33.15
20.0
0.000, 1.05
|
! ⇒Power system stabilizer and its parameters
  (for detail, please refer to the user's manual)
  Data input example:
! 1,311/
                                   / Gen #, PSS model #
! 3/
                                   / input 3: elec. power
```

```
! 0.014
                                    /Ta1
! 0.000, 0.025, 4.4, 4.4, 5.0, 5.0 / T1,T2,T3, T4, T5,T6
! -0.05, -0.100, 0.100
                                    / Ks ,Vsmin , Vsmax
 1, 312 /
 1/
 .0000
                         .0310, 8.0, 8.0 /
         .0310, .2230,
 .2230,
4.0000, -.1000, .1000
 2, 312 /
 1 /
 .0000
         .0342, .2465,
                         .0342, 8.0, 8.0 /
 .2465,
4.0000, -.1000, .1000
 3, 312 /
 1 /
 .0000
        .0310, .2230, .0310, 8.0, 8.0 /
 .2230,
4.0000, -.1000, .1000
       End of data file
```

5.5 Application of plotting utility programs

The results obtained from the simulation package (TSSP) is stored in the file *simu.out*. In order to facilitate the analysis of the results, plotting utility programs in TSSP can be used to plot and/or sort the variables of interest.

5.5.1 The WPLOT program

For analyzing the variables of a specific generator, the WPLOT program can be employed to plot a maximum of five variables at a time. To start the program, type WPLOT at the DOS prompt and press the <<ENTER>> key. The following display will be brought up on the screen.

To plot the variables of interest, the following information is entered first:

The total number of machines in the system (there are 3 machines), **3** The specific machines of interest (say machine #2), **2** The number of interested variables of that machine (say 1), **1**

Then, the variable strings are entered exactly the same as given in the variable list. A maximum of five variables can be entered and plotted at a time. An example is given below.

Enter the 1st variable string (rotor angle), ang

The <<ENTER>> key must be pressed to enter each item of the above stated information. The rotor angle (absolute value in degrees) and terminal voltage (in per unit) of generator #2 in the sample system can be displayed as follows by entering the variable identifying information. Figure 11 shows the absolute rotor angle of generator #2. Similarly, the terminal voltage of generator #2 is shown in Fig. 12.

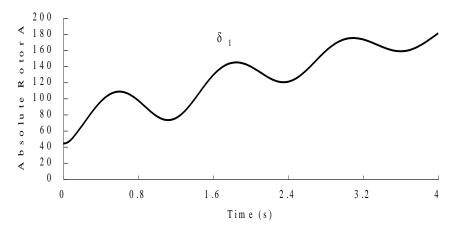


Fig. 11 Absolute rotor angle plotting of generator #2

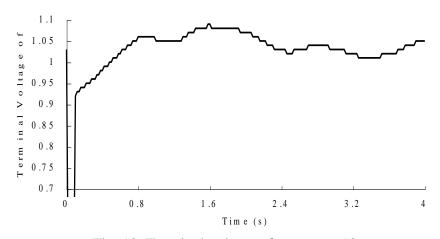


Fig. 12 Terminal voltage of generator #2

5.5.2 The SORT Program

It may be interesting or necessary to compare the same variable, for example, the machine shaft speed, of several generators in analyzing the results. The SORT program can be used to plot and/or sort out a maximum of twelve variables of different generators at a time. Generator rotor angles in respect to any generator in the system can be plotted.

To start the program, type SORT at the DOS prompt and press the <<ENTER>> key. The following display will be brought up on the screen.

Input filename of results from TSSP : simu.out
Input filename for storing sorted data : angspd23
Input reference machine no. : 1

To plot the variables of interest, the following information is entered first:

```
The total number of machines in the system (there are 3 machines), 3. The number of interested machines (say 2), 2. The specific machines of interest (say machines #2 and #3), 2, 3.
```

The number of interested variables of each machine (say 1), 2

Then, the variable strings are entered exactly the same as given in the variable list. A maximum of five variables can be entered and plotted at a time. An example is given below.

Enter the 1st variable string (rotor angle), **ang** Enter the 2nd variable string (rotor angle), **spd**

The <<ENTER>> key must be pressed to enter each item of the above stated information. The relative rotor angles (referred to generator #1, in degrees) of generators #2 and #3 in the sample system can be displayed as shown in Fig. 13, after entering the variable identifying information accordingly.

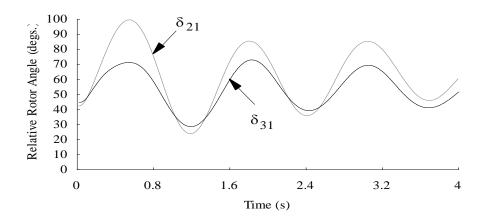


Fig. 13 Relative rotor angle swings of generators #2 and #3

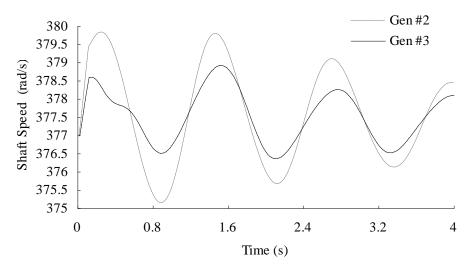


Fig. 14 Machine shaft speed of generators #2 and #3.

Appendix Interface with User-defined Module

If the module of a power component or a controller is not available in the TSSP, it is required to derive its transfer function. A block diagram can be built with integrators according to the transfer function. Then the block diagram can be programmed into a module. The name of the module is the name of the component, (for instance, SGTS), plus the identifying number corresponding to it as given in Table A.1. A dumb variable is required to identify the machine on which the component is installed. Other parameters for the module are passed through the input data file *mach.inp*. These parameters are stored in three different arrays. They are AVR(#, 20), TUR(#, 20), PSS(#, 20), where # is the identifying number of the machine on which the component or controller to modeled is to be installed. A maximum of tweenty parameters can be stored for each device. Parameters are compactly placed in its corresponding array according the definition of the data input format which is also defined by the user.

For example, a module for the simplified hydro speed governing and turbine system is to be programmed. The block diagram of the transfer function is given again in Fig. A.1.

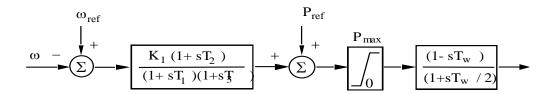
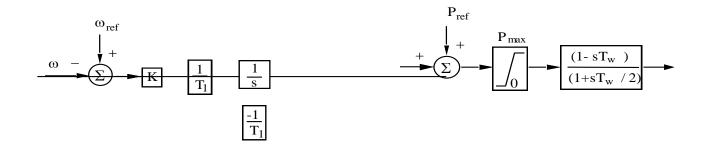


Fig. A.1 Simplified representation of hydrogovernor turbine system.



$$\frac{K_1 (1+sT_2)}{(1+sT)(1+sT_3)}$$

Table A.1: Module identifying numbers in the TSSP.

AVR	SGTS	PSS
11 - DC 1	211 - NR	311 - IEEEST
12 - DC 2	212 - TCSR	312 - IEEESN
13 - DC 3	213 - TCDR	313 - IEEE standard
14 - EXDC2B	214 - CCSR-A	
	215 - CCSR-B	Input Identifier:
21 - AC 1	216 - CCDR	1 - Deviation of speed
22 - AC 2		2 - Deviation of
23 - AC 3	221 - Hydro A	frequency
24 - AC 4	222 - Hydro B	3 - Electrical power
31 - ST 1		4 - Accelerating power
32 - ST 2		5 - Deviation of
33 - ST 3		voltage
41 - SCRX		
42 - SCRXIL		
51 - 55 User -	231 - 235 User -	321 - 325 User -
Defined	Defined	Defined

```
C ~ hydro turbine and governor systems ~ C ~ IEEE model ~ C ~ (simplified speed - governor model) ~ C ~ C ~ (simplified speed - governor model) ~ (simplified speed - govern
```

```
SUBROUTINE SGTS231(I)
C
    INCLUDE 'CMM.DM'
C
    double precision OME
    DOUBLE PRECISION \,X0,\,X1\, , \,X2\, , \,X3\, , \,X4\, , \,X5\, , \,X6,\,X7,\,X8\,
C define integrator output
    OME = OUT(I,1)
    X2 = OUT(I,9)
    X4 = OUT(I,10)
    X6 = OUT(I,11)
C calculate intermediate variables
    X1 = TUR(I,6) * (WREF(I) - OME)
    X3 = X2 + X1 * TUR(I,4) / TUR(I,3)
    IF (TUR(I,5).LT.0.0001) X4 = X3
    X5 = GREF(I) - X4
    IF (X5.GT.TUR(I,8)) X5 = TUR(I,8)
    IF (X5.LT.TUR(I,7)) X5 = TUR(I,7)
    X8 = 1.5 * X5 - X6
    X7 = X5 - X8
    PM(I) = X7 * TUR(I,1) / 100.0
C
C define integer inputs
    PLUG(I,9) = (X1 - X3) / TUR(I,3)
    PLUG(I,10) = (X3 - X4) / TUR(I,5)
    PLUG(I,11) = X8 / TUR(I,2)
    PVAR(I,12) = X5
    RETURN
C
C initialize the system variables
    ENTRY initializeSGTS231(I)
C define default time constants
    IF (TUR(I,3).EQ.0.0) TUR(I,3) = 1.0E+6
    IF (TUR(I,4).EQ.0.0) TUR(I,4) = 1.0E+6
    IF (TUR(I,5).LT.0.0001) TUR(I,5) = 1.0E-6
    X0
           = PM(I) * 100.0 / TUR(I,1)
    GREF(I) = X0
```

```
OUT(I,9) = 0.0

OUT(I,10) = 0.0

OUT(I,11) = 1.5 * X0

WREF(I) = OUT(I,1)

C

IF ( X0.GT.TUR(I,8) ) WRITE( *, 10) I

IF ( X0.LT.TUR(I,7) ) WRITE( *, 10) I

10 FORMAT( ' Gate limits exceeded at governor', i4/ )

RETURN

END
```

Reference

- [1] IEEE Committee Report, "Excitation System Models for Power System Stability Studies," *IEEE Transactions on Power Apparatus and System*, Vol. PAS-100, pp. 494-507, February 1981.
- [2] IEEE Committee Report, "Dynamic Models for Steam and Hydro Turbines in Power System Studies," *IEEE Trans. on Power Apparatus and System*, Vol. PAS-92, pp. 1904-1915, November 1973.
- [3] P. M. Anderson, A. A. Fouad, *Power System Control and Stability*, The Iowa State University Press, Ames, Iowa, U.S.A., 1977.