

# ELEMENTARY GEOPHYSICAL FLUID MECHANICS

MATHEMATICS, KINEMATICS, DYNAMICS, SHALLOW WATER FLOW,  
VORTICITY, BALANCED FLOW, SCALAR MECHANICS, VERTICAL COORDINATES

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GRIFFIES, STEPHEN M., 1962-

ELEMENTARY GEOPHYSICAL FLUID MECHANICS

THIS BOOK WAS TYPESET USING L<sup>A</sup>T<sub>E</sub>X.

# Contents

PREFACE . . . . .	iii
A GUIDE TO THIS BOOK . . . . .	ix
PRINCETON UNIVERSITY AOS 571 . . . . .	xv
LIST OF SYMBOLS . . . . .	xxiii
Part I. Mathematical methods and concepts . . . . .	1
1 Cartesian tensor algebra . . . . .	5
2 Cartesian tensor calculus . . . . .	21
3 Partial differential equations . . . . .	45
4 Green's function methods . . . . .	67
5 Curves and surfaces . . . . .	111
6 General tensors in brief . . . . .	121
7 General tensor analysis . . . . .	131
8 Orthogonal coordinates . . . . .	153
Part II. Geophysical particle mechanics . . . . .	167
9 Particle mechanics . . . . .	169
10 Symmetry and conservation . . . . .	205
Part III. Kinematics of fluid flow . . . . .	227
11 Continuum approximation . . . . .	229
12 Fundamentals of fluid kinematics . . . . .	239
13 Material fluid objects . . . . .	269
14 Mass conservation . . . . .	289
15 Tracer conservation . . . . .	313
16 Non-divergent flows . . . . .	335
Part IV. Dynamics of geophysical fluid flows . . . . .	353
17 Momentum dynamics . . . . .	357
18 Stress in fluids . . . . .	373
19 Pressure form stress . . . . .	409
20 Equilibrium thermodynamics . . . . .	433
21 Energetics of fluid flow . . . . .	481
22 Hydrostatic and tangent plane approximations . . . . .	517
23 Oceanic Boussinesq fluid . . . . .	537
24 Buoyancy . . . . .	581
25 Rotating flows . . . . .	607
26 Tangent plane flow balances . . . . .	637
27 Ekman mechanics . . . . .	653
28 Space and time dependent gravity . . . . .	677
29 Surface gravity waves and Stokes drift . . . . .	689
Part V. Shallow water mechanics . . . . .	705
30 Shallow water models . . . . .	707
31 Shallow water dynamics . . . . .	729
Part VI. Vorticity and potential vorticity . . . . .	777
32 Vorticity and circulation . . . . .	779
33 Non-divergent barotropic flow . . . . .	799
34 Shallow water vorticity and potential vorticity . . . . .	825
35 Vorticity mechanics . . . . .	867
36 Potential vorticity mechanics . . . . .	911
37 Potential vorticity budgets . . . . .	929

Part VII. Nearly geostrophic balanced flows . . . . .	947
38 Shallow water planetary and quasi-geostrophy . . . . .	949
39 Continuously stratified planetary geostrophy . . . . .	971
40 Continuously stratified quasi-geostrophy . . . . .	997
Part VIII. Generalized vertical coordinates . . . . .	1019
41 Mathematical basics . . . . .	1023
42 Kinematic equations . . . . .	1043
43 Dynamical equations . . . . .	1067
44 Isopycnal primitive equations . . . . .	1077
45 Shallow water thickness weighted averaging . . . . .	1091
Part IX. Scalar mechanics . . . . .	1109
46 Tracer advection and diffusion . . . . .	1111
47 Eddy and mean tracer kinematics . . . . .	1161
48 Mathematics of parameterized tracer transport . . . . .	1189
49 Ocean density and sea level . . . . .	1219
50 Water mass transformation analysis . . . . .	1241
Bibliography . . . . .	1281

## Contents

CONTENTS

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# Preface

Geophysical fluid mechanics (GFM) is the study of fluid flow on a rotating and gravitating planet using concepts from continuum mechanics. In this book, our primary inspiration comes from terrestrial fluids in the atmosphere and ocean, though the principles and methods are applicable to extra-terrestrial atmospheres and oceans. Geophysical flows are in near solid-body motion with the rotating planet, thus prompting a description from the rotating (non-inertial) planetary reference frame. Body forces from both rotation (Coriolis) and gravitation (buoyancy) are fundamental features of geophysical fluid flows, as are contact forces from stresses (pressure and friction). We encounter a variety of conceptual models within these pages. Some are formulated within the context of a *perfect fluid* comprising a single material constituent and where fundamental processes are limited to the reversible and mechanical. Others are posed within *real fluids* comprised of multiple matter constituents exposed to irreversible processes such as friction, mixing and heating.

We develop geophysical fluid mechanics from a mathematical physics perspective at a level accessible to the graduate student in atmosphere and ocean sciences, physics, engineering, applied mathematics, and allied fields. Mathematical derivations are offered in detail to expose the physics and to develop skills required for the practitioner. Hence, brevity is generally sacrificed to support an exposition of both concepts and methods. Subjects are approached by establishing general principles and afterwards considering specializations, case studies, and approximations that exemplify the fundamentals. Though guided by natural phenomena, the treatment is centered on the mechanics of geophysical fluid mechanics so that we explore many topics to a degree beyond that needed if primarily focused on phenomenological or back-of-the-envelope descriptions. For this reason, we find occasions to examine physics through multiple lenses that render a variety of perspectives and insights.

The presentation is based on the premise that skills as a physicist are best taught by nurturing physical reasoning, and with physical reasoning supported by mathematical precision coupled to the elucidation of concepts and principles. Hence, the presentation style is both deductive and descriptive. The deductive approach supports understanding through elementary physical notions that are expressed mathematically and then used as a foundation for conceptual theories. The descriptive serves to build skills in physical reasoning and the ability to articulate physical ideas using words as a complement to maths. Furthermore, we cultivate the conceptual and technical by embracing the synergistic relation between physics and maths, whereby physics informs the maths and maths reveals the physics. On a practical level, we support these aims by following the rules of [Mermin \(1989\)](#).

- Rule 1: All displayed equations are given numbers for easy cross-referencing.
- Rule 2: When referring to an equation, identify it by a phrase as well as a number.

- Rule 3: Equations are part of the prose and thus subject to punctuation.

## From lecture notes to book

This book grew from lecture notes developed for a first semester graduate course in geophysical fluid mechanics at Princeton University. The course develops fluid mechanics as framed within the arena of geophysical fluid flows and it drew from texts such as [Gill \(1982\)](#), [Pedlosky \(1987\)](#), [Apel \(1987\)](#), [Salmon \(1998\)](#), [McWilliams \(2006\)](#), [Marshall and Plumb \(2008\)](#), [Cushman-Roisin and Beckers \(2011\)](#), [Olbers et al. \(2012\)](#), [Klinger and Haine \(2019\)](#), and [Vallis \(2017, 2019\)](#). Additional insights were gleaned from the fluid mechanics texts by [Aris \(1962\)](#), [Batchelor \(1967\)](#), [Meyer \(1971\)](#), [Landau and Lifshitz \(1987\)](#), [Segel \(1987\)](#), [Acheson \(1990\)](#), and [Kundu et al. \(2016\)](#).

The study of rotating and stratified fluids has evolved much over its history. During recent decades the study has seen particular evolution through deepening physical foundations, refining mathematical formulations, increasing the intellectual and predictive value of numerical simulations, extending applications across terrestrial and planetary systems, and expanding observational and laboratory measurements and techniques. What has emerged is a recognition that a fruitful study of rotating and stratified fluid flows makes use of ideas that go beyond the traditional notions of *geophysical fluid dynamics* (GFD). A contemporary practitioner develops insights by weaving together concepts and tools from mathematics, kinematics, dynamics, thermodynamics, scalar mechanics, numerical simulations, laboratory experiments, and field measurements. Acknowledging this broadening of the practice motivates the term “mechanics” in this book’s title, rather than the more focused “dynamics”. It is a seemingly trivial change in verbiage and yet it represents a nontrivial broadening of the perspective.

## Two pillars of geophysical fluid mechanics

We conceive of two pillars to theoretical geophysical fluid mechanics. The *elements or elementary pillar*, which is the focus of this book, comprises the physical and mathematical formulation of conceptual models used to garner insight into rotating and stratified fluid motion. This pillar is concerned with deductively exposing how physical concepts are mathematically expressed in a mechanical description of geophysical flows. The complement study of geophysical fluid phenomena and corresponding solutions to equations, such as waves, instabilities, turbulence and general circulation, forms the *emergent phenomena pillar*. We introduce emergent phenomena where it serves as motivation for and illustration of elementary concepts. Even so, emergent phenomena are not our primary focus. Rather, this book focuses on the elementary physics forming the core of the equations and less on physics emerging from solutions to the equations.

The elements pillar and the emergent phenomena pillar are synergistic, thus offering lessons and guidance to one another. Our choice to focus on elementary geophysical fluid mechanics rather than on emergent phenomena is partly a product of the course from which this book grew, which is a course that lays the foundations for the subject by deductively formulating the equations and exploring their physical content. Furthermore, the elements pillar is less widely emphasized by existing texts in geophysical fluid mechanics. This book attempts to partly remedy that situation while, hopefully, remaining accessible and relevant to students whose interests are more concerned with phenomena.

## Causality and association

Throughout this book we develop equations describing the evolution of fluid properties, with such equations derived from foundational physical principles such as Newton's laws of motion, thermodynamic principles, mass conservation, and vorticity mechanics. As part of this development we often seek information about what *causes* a particular fluid motion. The question of causality is posed when studying Newton's equation of motion, which says that acceleration (motion) arises from a force (the cause of the motion). Even though seemingly a clear decomposition of cause and effect, this fundamental statement of classical mechanics offers little more than the definition of a force. We make physical progress only after specifying the nature of the force; e.g., gravitational, electromagnetic, etc.<sup>1</sup>

In geophysical fluid mechanics, we refer to equations that determine time changes as *prognostic equations*, whereby knowledge of forces enable one to predict the flow evolution. The question arises how to determine the forces, particularly when the forces are commonly dependent on the flow. Such is the complexity and beauty inherent in nonlinear field theories, such as fluid mechanics, where cause and effect are intrinsically coupled. We can sometimes make progress by turning the problem around, whereby kinematic knowledge of the motion offers inferential knowledge of the dynamical forces. This situation is exemplified by pressure forces acting within a non-divergent flow whereby pressure acts, instantaneously and globally, to satisfy the constraint that the velocity remains non-divergent.

Besides seeking causal relations pointing toward the future, many basic questions of fluid mechanics arise either instantaneously, as in the constraints maintaining non-divergent flows, or when the flow is steady, in which case the flow at each point in space has no time dependence. In steady flows, the net acceleration, and hence the net force, vanish at each point within the fluid, although the fluid itself can still be moving. For steady flows we are unable to make statements about causality since the steady equations are *diagnostic* rather than prognostic. Diagnostic relations thus provide statements about *associations* or *balances* between physical processes. The *geostrophic balance* is the canonical diagnostic relation appearing in geophysical fluid mechanics, where the Coriolis force is associated with (i.e., balances) the horizontal pressure force. Further associative statements are particularly common when studying steady vorticity balances, such as the *Sverdrup balance* familiar to oceanographers. So although a predictive theory requires prognostic equations that manifest causal relations, an understanding of how fluid motion appears, and in particular how it is constrained, can be fruitfully studied through diagnostic relations.

## Geophysical Fluid Mechanics and Climate Science 2.0

Fluid mechanics has a history of applications that span science and engineering, from blood flow to the stability of stars and the evolution of galaxies. A key 21st century application of geophysical fluid mechanics concerns the questions of climate science associated with the uncontrolled greenhouse gas experiment pursued by industrialized civilization's carbon centered energy use. Leading order questions about climate warming have been sufficiently addressed to recognize that the planet has reached a crisis point threatening the viability of the biosphere. Even so, mechanistic answers to a number of questions remain at the cutting edge of climate science research. What will happen to the atmospheric jet stream and storm tracks in a world without summer Arctic sea ice? Will tropical storms be more powerful in a warmer world? What are the patterns for coastal sea level rise and their connections to large-scale ocean circulation? What are the key processes acting to bring relatively warm ocean waters to the base of high latitude ice shelves? How sta-

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<sup>1</sup>For more on this perspective of Newton's laws, see Chapter 1 of *Symon* (1971).

ble are the ocean and atmosphere's large-scale overturning circulations and their associated heat transport? Are there feasible and sustainable geo-engineering options that equitably reduce the negative impacts of climate warming without introducing new problems? These questions, and countless others, constitute the scientific challenges of *Climate Science 2.0*.

Numerical circulation models, a core tool for Climate Science 2.0, have reached a level of maturity that they vividly reveal details of the complex and multi-scaled nature of planetary fluid flow. Geophysical fluid mechanics is essential for the development of robust numerical methods and subgrid scale parameterizations for such models, along with mechanistic analyses and interpretations of simulated data. In turn, geophysical fluid mechanics furthers predictive capability for weather and climate forecast systems and enhances confidence in projections for future climate. Moving from the numerical world to the natural world, we find that the many elements of geophysical fluid mechanics are key to the design of observational field campaigns and novel laboratory experiments, as well as for the analysis of their measurements. Such field campaigns and laboratory experiments probe process-oriented questions through the use of technologies that facilitate increasingly ambitious investigations of fluid flows.

We thus contend that the principles and methods of geophysical fluid mechanics provide the means to conceptually digest and rationalize the underlying physics probed by both natural and simulated experiments, and to communicate the findings to the broader scientific community. In turn, geophysical fluid mechanics, as part of the scientific investigation of the earth's climate, serves an essential role in humanity's quest for sustainability, equity, and justice.

## Gratitudes

This book benefited greatly from students taking part in Princeton University's AOS 571, a course that I taught for many years. Further inspiration was offered by students, postdocs, and fellow research scientists encountered as part of my research career. I wish to particularly highlight a variety of dynamics journal/study clubs where a great deal of head scratching led to many of the topics sprinkled through these pages.

I remain humbled and grateful for being part of the unique research environment cultivated at NOAA's Geophysical Fluid Dynamics Laboratory as well as Princeton University's Atmospheric and Oceanic Sciences program. As part of my research and mentoring in this environment, I have encountered thinkers whose style, questions, and insights have taken root in my work. This environment has also afforded me the opportunity to travel the world to interact with various teachers and colleagues whose wisdom and love of science and life are infectious and inspiring. Throughout these interactions, I have entered into trusting and non-judgmental spaces where deep learning and understanding spontaneously arise. Partaking in these spaces, where heart and mind meld, has been among the most satisfying experiences of my life. Safe spaces for honest, diverse, and inclusive learning are precious, and I am grateful to those who nurture such spaces.

A book of this nature is not a simple endeavor. It starts modestly, grows over time, and eventually becomes a passion if not an obsession. I was particularly drawn to writing during the COVID-19 pandemic that kept me sequestered at home far more than during non-pandemic times. Writing this book has been an exercise in rational thought fed by spiritual food from meditation, yoga, family, and community. In particular, each step of this project was supported by my wife, Adi, and our son, Francisco. I am deeply grateful for their patience and trust as I satisfied the goal of writing this book through countless nights, weekends, and holidays in our home attic space. I treasure being part of this family and I dedicate this work to you two amazing human beings.

## Disclaimer

Facets of this book originate from research papers published while I was a US Government federal employee. Reference to these papers is provided at the appropriate place in the text. However, no sentence in this book was taken verbatim from published papers. Rather, the material has been extensively reworked and refined to enhance pedagogical value for the reader, thus going well beyond that appropriate for research papers or reports. Additionally, this book's writing occupied personal time and was not part of any official assigned government duty, and I made use of personal equipment for typesetting and producing figures.

## About the cover

I took the cover photo of an iceberg, ocean, clouds, and sea bird (can you find the bird?) in the Orkney Passage region of the Southern Ocean during a research cruise from March-May 2017 aboard the British ship James Clark Ross. Although I largely pursue theoretical research, my experiences with field research have greatly enhanced my scientific viewpoint and profoundly deepened a connection to the natural forces and phenomena present on this amazing planet.

## Caveats and limitations

Although reaching some level of maturity, this book remains a work in progress not yet ready for publication. Here are just a few of the items required before it is ready for its next stage.

- A number of further topics will fill these pages.
- More effort is needed to unify notation, complete and organize the index, develop further exercises, enhance figures, improve discussions, and correct errors.
- Many sections and chapters have yet to be scrutinized by readers. I hope to garner help from those interested in providing candid feedback to improve presentation and correct mistakes. Feedback is solicited particularly where the reader identifies poor or confused writing, incorrect concepts, or math errors. Nothing is too trivial for comment.





# A guide to this book and its study

No book is an island, with this book generously making use of other books, review articles, research papers, and online tutorials. Many readers find value in studying a subject from a variety of perspectives, thus justifying the proliferation of books with overlapping subject matter. In an attempt to support this form of study, we commonly provide pointers to written and/or video presentations. Many more resources are available through a quick internet search.

There is no pretense that any reader will penetrate all topics in this book, nor read this book cover-to-cover. This recognition is particularly keen in a world where research and educational agendas often spread rather than focus our attention. Hence, an attempt has been made to facilitate picking up the book at a variety of starting points. For this purpose, each chapter and/or part is written in a reasonably self-contained manner even at the cost of modest redundancy. When redundancy becomes onerous, cross-referencing identifies allied material treated elsewhere in the book. Here we summarize the book's organization and offer some pointers on how to pursue its study.

## Organization

This book is organized into parts according to their particular focus, with each chapter starting with a brief guide to the material and pointing to dependencies to other chapters. Some chapters focus on topics required for a basic understanding of the subject and offer exercises to test that understanding. Other chapters offer monograph style topics that further the foundations and exemplify applications largely taken from a selection of the author's research interests. Although this book is sizable, there are many topics omitted. These omissions reflect on the author's limited energy as well as the desire to keep the book from growing even larger.

### MATHEMATICAL METHODS AND CONCEPTS

Part I provides a suite of mathematics chapters of use in studying geophysical fluid mechanics. Some chapters concern topics readily found in applied mathematics or mathematical physics texts, whereas others provide a grounding in mathematics rarely seen outside of geophysical fluid mechanics, in particular the maths of generalized vertical coordinates. The casual reader can skim these chapters without sacrificing too much from later chapters, assuming a working knowledge of vector differential and integral calculus. Where more difficult math topics arise in later chapters, the reader is encouraged to return here to develop skills and to firm understanding. We propose that a variety of avenues for physical insights should be embraced by the practitioner, with mathematical acuity offering great rewards to the physicist.

## GEOPHYSICAL PARTICLE MECHANICS

Part II provides a summary of Newtonian particle mechanics with particular emphasis on particles moving around a rotating sphere. This study exposes the physics of motion when viewed from the non-inertial reference frame of a terrestrial observer. By doing so, we encounter such topics as the Coriolis and centrifugal accelerations as well as spherical coordinates, all within the relatively simple context of point particle mechanics.

## KINEMATICS OF FLUID FLOW

Mechanics is comprised of kinematics (the study of intrinsic properties of motion) and dynamics (the study of forces causing motion). In Part III we initiate a study of fluid mechanics by focusing on the kinematics of fluid flow and matter transport within that flow. Our treatment exposes both the Eulerian and Lagrangian viewpoints and emphasizes the variety of kinematic notions and tools key to describing fluid motion. We also encounter facets of material transport as described by the tracer equation, thus laying the foundation for *tracer mechanics*. It is in these chapters that we nurture the brain-muscle to think about fluid motion. Fluid flow, and the transport of matter within that flow, have many features fundamentally distinct from point particle and rigid body motion. We thus cultivate distinct tools and concepts that can take much practice to intellectually digest.

Quite often a course in fluid mechanics skims over fluid kinematics and tracer mechanics, preferring instead to focus mostly on dynamics. Indeed, some kinematic topics can seem a bit esoteric, particularly the study of Lagrangian kinematics. However, an incomplete understanding of fluid kinematics and tracer mechanics can lead to many difficulties with fluid dynamics. The reader is thus encouraged to study the chapters here in detail, and to revisit the material as the need arises during later chapters.

## DYNAMICS OF GEOPHYSICAL FLUID FLOW

Part IV presents the core chapters of geophysical fluid dynamics as studied in this book. Within these chapters we study how Newton's laws of mechanics and the principles of thermodynamics are used to describe fluid motion on a rotating and gravitating sphere. We approach the subject by focusing on how forces that act on fluid elements and fluid regions lead to accelerations and thus to motion. These forces both act throughout the volume of a fluid element (*body forces* from gravity, Coriolis, and centrifugal) as well as on the boundary of a fluid element (*contact forces* from pressure and friction).

## SHALLOW WATER MECHANICS

In Part V we study the mechanics of a shallow water fluid, with a shallow water fluid comprised of hydrostatically balanced homogeneous fluid layers. The layers are also typically assumed to be immiscible, so that interactions between layers occur only via mechanical forces from pressure acting at the layer interfaces. The shallow water fluid allows us to focus on rotation and stratification without the complexities of vertically continuous stratification and thermodynamics. Many physical insights garnered by studying shallow water fluids extend to more realistic fluids, thus making the shallow water model very popular among theorists.

## VORTICITY AND POTENTIAL VORTICITY

Part VI dives into the subject of vorticity and potential vorticity. This subject is rich and elegant, though it requires perhaps the most work for the student to penetrate given the heavy reliance

on vector and integral calculus. Vorticity plays a role in the motion of all geophysical fluids since motion on a rotating planet provides a nonzero *planetary vorticity* even to fluids at rest on the planet. This feature of geophysical fluids contrasts to many other areas of fluid mechanics, where irrotational flows are commonly encountered. Potential vorticity is a strategically chosen component of the vorticity vector that marries mechanics (vorticity) to thermodynamics (stratification). Material conservation properties of potential vorticity are striking and render important constraints on fluid motion. Indeed, perhaps the most practical reason to study vorticity concerns the various constraints imposed on the flow moving on a rotating and gravitating sphere. These constraints provide conceptual insights and predictive power.

#### NEARLY GEOSTROPHIC BALANCED FLOWS

Part VII introduces the topic of balanced models, with our attention limited to the shallow water and continuously stratified versions of quasi-geostrophy and planetary geostrophy. Balanced models generally remove the divergent motions associated with gravity waves, thus allowing a focus on the large-scale vortical motions. Balanced models have a rich history among theoretical geophysical fluid studies, providing insights into both laminar flows through planetary geostrophy, and turbulent flows through quasi-geostrophy.

#### ELEMENTS OF GENERALIZED VERTICAL COORDINATES

Part VIII brings together the various elements of a generalized vertical coordinate description of geophysical fluid mechanics. The chapters offer details of the maths, kinematics, dynamics, and applications. This material is central to many current research activities, including subgrid scale parameterizations and the design of numerical atmosphere and ocean models.

#### MECHANICS OF OCEAN SCALARS

Part IX dives into the mechanics of scalar fields as realized in the ocean, with our focus on active tracers (temperature and salinity), passive tracers, and buoyancy. Much of this study forms the basis of *tracer mechanics*, which has proven very important for the ocean given that it is generally very difficult to measure dynamical fields such as velocity and vorticity, whereas tracer distributions are much more readily measured.

## Written and spoken communication

Reading lecture notes, research articles, and books exposes one to sound and clear writing, as well as to unsound and obscure writing. Attending lectures and seminars in person or online also exposes one to a range of speakers. Some speakers offer the benefits of a sleeping aide without the cost and side-effects of a pharmaceutical. Others rush through more material than even they can digest, whereas others pedagogically engage in a lecture even without any prior knowledge of the material. To succeed in research and teaching requires one to master elements of both written and spoken communication.

#### CLEAR THINKING LEADS TO CLEAR COMMUNICATION

Clear communication is the sign of clear thinking. Some people communicate better in writing, where one has the opportunity to carefully organize thoughts and refine the writing style. Others are better at speaking, where spontaneous and interactive reflections and experience can

bolster the clarity of a presentation. Both modes of communication are important in science and engineering.

As inspiration, for both clear and obscure, pick up one of your textbooks or class lecture notes and analyze the presentation for clarity. Where are you confused? Where is the material crystal clear? Then pick up a journal article and perform the same analysis. What do you like? What do you dislike? Then go to YouTube and find a science or engineering lecture, old or new. What makes the speaker engaging and clear, or boring and obscure?

### EMPATHY IS KEY

Empathy is a basic facet of effective communication and teaching. Place your mind inside that of an interested and smart reader or listener. Identify with their quest to understand what you wish to communicate. What assumptions are you making? Are the assumptions justified based on the audience? How compelling is your scientific story?

### CLARITY HELPS, BUT SOME MATERIAL IS JUST TOUGH

Although poor communication hinders our ability to digest new ideas and concepts, it is also important to appreciate that some material is tough no matter how well it is communicated. We should aim to make a subject matter as simple as possible, but not simpler (paraphrasing Einstein). Furthermore, it sometimes takes one or two generations of teaching before some scientific material can be sufficiently digested to allow for the core conceptual nuggets to be revealed. As an example, try reading Newton or Maxwell's original works as compared to a modern presentation of Classical Mechanics or Electromagnetism. So we do strive for clear communication, but we cannot presume that clarity is sufficient to remove the struggles we all experience when learning.

## Pointers on physics problem solving

Most people are not born with *a priori* physics problem solving skills. Rather, it takes extensive practice to develop the necessary brain muscle. Here are some general pointers to keep in mind when diving into a physics problem, whether it is for a class or the basis of a broader research question.

### CHECK FOR DIMENSIONAL CONSISTENCY

The symbols we use in mathematical physics correspond to geometrical objects (e.g., points, vectors, tensors) describing a physical concept (e.g., position in space, velocity, temperature, angular momentum, stress). Hence, the symbols generally carry physical dimensions. The physical dimensions we are concerned with in this book are length (L), time (T), mass (M), and temperature. Physical dimensions of the equations must be self-consistent. For example, if one writes an equation

$$A = B, \quad (1)$$

where  $A$  and  $B$  have different physical dimensions, then the equation makes no sense physically. Something is wrong. Although not always sufficient to uncover errors, dimensional analysis is an incredibly powerful means to debug the maths.

**CHECK FOR TENSORIAL CONSISTENCY**

In the same way that mathematical equations in physics need to maintain dimensional consistency, they must also respect tensor rules. For example, the equation

$$A = B, \quad (2)$$

makes mathematical sense if  $A$  and  $B$  are both scalars. Likewise,

$$\mathbf{A} = \mathbf{B} \quad (3)$$

makes sense if  $\mathbf{A}$  and  $\mathbf{B}$  are both vectors. However, if both  $\mathbf{A}$  and  $\mathbf{B}$  are vectors, then the equation

$$\mathbf{A} = \nabla \cdot \mathbf{B} \quad (4)$$

does not make sense because the left hand side is a vector and the right hand side is a scalar. A more subtle example is when  $\mathbf{A}$  is a vector yet  $\mathbf{B}$  is an axial vector. In this case  $\mathbf{A}$  remains invariant under a change from right hand to left hand coordinates whereas  $\mathbf{B}$  flips sign. Maintaining basic tensorial rules can be considered the next level of sophistication beyond dimensional analysis.

**USE WORDS AND PICTURES**

It is important to explain the problem and solution using words and pictures. Hence, it is good practice to liberally sprinkle sentences in between the key equations, with the purpose to explain what the maths means using clear English. Here are some practical payoffs for this style of presentation.

- The process of explaining the maths using words and pictures requires one to dive deeper into the logic of the problem. Doing so often reveals weak points, incomplete or unmentioned assumptions, and errors. This process is a very important learning stage in preparing to stand in front of an audience to present results and to answer questions. It is a key facet of research and teaching.
- Physics teachers are often more forgiving of math errors if you convince the teacher that you have a sensible physical understanding of the problem. Plain English and pictures are very useful means for this purpose.

**THERE IS OFTEN MORE THAN ONE PATH TO A SOLUTION**

In physics, there is often more than one path to a solution. Pursuing distinct paths offers added physical and mathematical insight, exposes assumptions, and allows one to double-check a solution. Some of the most profound findings in physics came from pursuing distinct formulations. One example concerns the distinct formulation of mechanics offered by Newton (1642-1746), and then later by Lagrange (1736-1813) and then Hamilton (1805-1865). Had Lagrange or Hamilton rested on the merits of Newton's formulation, we may well have had a very different intellectual evolution of 19th and 20th century physics.



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# Princeton University AOS 571

Welcome to AOS 571. This course focuses on geophysical fluid mechanics, which is concerned with motion of rotating and stratified fluids such as those in the earth's atmosphere (mostly a gas) and the ocean (mostly a liquid). We develop certain of the conceptual and mathematical foundations of the subject by studying elemental features of planetary fluid motion, and by providing a mathematical physics basis for understanding these patterns.

## DETAILS OF YOUR TEACHER AND THE COURSE

Dr. Stephen M. Griffies  
[SMG@princeton.edu](mailto:SMG@princeton.edu)  
<https://stephengriffies.github.io/>  
Class Monday and Wednesday 2pm-3:30pm  
In-person classes held at 154 Guyot Hall  
Zoom for Q & A during 10am-11am each Friday  
Worked homeworks uploaded by students to Canvas  
Class materials and communication via Canvas  
Recorded class lectures from 2020 are available via Canvas

## Class structure and expectations

Our goal for this course is learn how to formulate and to solve problems in geophysical fluid mechanics, and to develop an understanding of the basic physical theory. To help reach this goal, I have prepared extensive notes (now a book in progress) and we will work through selected pieces in class. You will also read far more than covered in class.

Garnering an understanding of geophysical fluid mechanics can require great effort and practice. To help that process, you are expected to read the assigned material, work through the derivations, and hand-in homework exercises. You will have many opportunities to develop the necessary brain muscle assuming you maintain the discipline to keep up with the material. Please ask questions, preferably in class, when you are unsure of anything. Also, please strive to solve all of the assigned exercises, either alone or collaboratively with other students.

## CULTIVATING A SAFE SPACE FOR HEALTHY LEARNING

A fundamental feature of any class concerns the atmosphere developed for learning. My aim as class teacher is to foster an inclusive, friendly, generous, patient, and non-judgmental space for learning by students and the teacher. Key principles that support this space include equity, diversity and inclusion, each of which are intrinsically valuable and an essential feature of ethical

research and education. We also acknowledge and honor past generations whose efforts, some of which were garnered through force and oppression, have led to the rewarding research environment that we now work. It is our sincere hope that practicing the above principles supports present and future generations in a way that helps to heal past injustices. Cultivating this safe and grateful space supports deep learning while genuinely appreciating contributions from individuals without regard to race, ethnicity, culture, religion, sexual orientation, gender identity and expression, physical ability, age, socioeconomic status or nationality. As a participant in this space, we each celebrate diversity and nurture an inclusive and friendly community that is optimized for shared learning and mutual understanding.

For many, this class will require a tremendous amount of effort. It will require much focus and energy to master the material even for those with a firm background. Regardless your background, talents, or interests, I am here to help in anyway you need. So please reach out if you are struggling. I also encourage you to develop working relations with your classmates. Homework exercises can be done with groups, and working with others offers great opportunities for learning.

Even if you prefer to work alone, I ask that you develop some form of a relation with one or more of your classmates. Part of this recommendation is based on the need to informally monitor the health of each other, particularly given that the early years of graduate school can be very stressful. Even so, it can be a time for building deep friendships and community as we share in the process of learning how to thrive as budding researchers and teachers.

#### ONLINE LECTURE NOTES FOR THE CLASS

The class lectures closely follow selected material from [Griffies \(2021\)](#) available online. These notes started in 2014 as annotations to the textbooks from [Vallis \(2017\)](#) and [Vallis \(2019\)](#), with both books highly recommended supplements to the course. In recent years, the class notes have grown into an autonomous document from which the course material directly derives.

You are asked to read through the class notes and to view the assigned videos **prior to the class**. During class we will discuss salient points from the assigned notes. To allow sufficient time for interactive discussion and questions, not all of the assigned reading material will be directly covered in class. Hence, you will be expected to read and to understand more material than is covered on the chalkboard. Correspondingly, you are welcome to bring any questions related to the notes to the class, even if the material was not covered in class.

#### CLASS GRADE = HOMEWORK (75%) + FINAL EXAM (25%)

There are two areas where grades are earned: homework exercises and take-home final exam. Additionally, I ask that everyone aim to attend all classes and participate by asking questions.

Worked homework exercises are due at the start of class (uploaded to Canvas) one week after the exercises are assigned (unless otherwise noted). Students can make use of any resources for solving homework exercise, including other people. Clarification of questions can also be obtained via email to me. If you find a solution from a source other than your own head, then be sure that you fully understand both the essence and the detail of the solution. Although you are encouraged to discuss the problems with other students, you are cheating yourself if you merely parrot another person's answer without fully grokking it yourself.

There is no pretense that the exercises offered in class are clearly formulated. Indeed, a certain degree of ambiguity reflects the *status quo* in research, where formulating a novel and insightful question is generally the most difficult part of the research process. Additionally, the solutions may not be 100% correct or ideal from a pedagogical perspective. Rather, they represent a work in progress. If mistakes or ambiguities are found, then please share your questions and concerns.

There is a take-home final exam during exam period. You are asked to do the work as a solo student, with no help or consultation from another human. However, you can make use of books, notes, online resources, etc. The questions are generally taken from published papers with relevant references provided to the student.

#### PLEASE DISCONNECT ELECTRONICS FROM INTERNET DURING CLASS

The class time is comprised of lectures based on the class notes along with discussion. The pace will be gauged on questions during the lectures and my sense for how well the class is grokking the material. You are encouraged to follow lectures by having a copy of the class notes on-hand, either electronically or printed.

To support your learning and teaching experience, and those of your classmates, please ensure that you turn all electronic devices into "airplane mode" so that you are not tempted to divert attention to non-class issues. To get the most from the lectures and class time requires focused attention and participation.

## Assignments and final exam

Here we consider some context for the class assignments and final exam.

#### AIM FOR A BALANCE BETWEEN BEING THOROUGH AND BRIEF

There is often a conflict between showing full mastery of a problem and keeping the solution write-up brief. In general, there is no need to re-derive equations already presented in the class lecture notes. Proper referencing of the equation is all that you need; i.e., tell me something like "starting from equation (X.YY) from the class notes." Additionally, when presenting a derivation, you may choose to show just the key steps rather than all intermediate steps. Determining what is a "key" step is largely up to you, but it should be something you learn to do in time. Nonetheless, as per the previous pointer, you are encouraged to show more than one approach to a solution.

#### QUESTIONS FOR POINTS OF CLARIFICATION

Questions for points of clarification will be entertained if you feel the problem is ill-posed or if you are totally lost. Email is the most efficient means to communicate to me. Responses will generally be sent through Canvas so that all students can see the response, thus keeping everyone with the same information. Correspondingly, questions within 24 hours of the deadline are generally not entertained so to ensure that all students have time to see the response.

#### MISTAKES OFFER SIGNIFICANT OPPORTUNITIES FOR LEARNING

Everyone makes mistakes, some more than others. The toughest part is the self-imposed shame or embarrassment. Please try to keep a positive mind about your mistakes. As you will discover, mistakes offer significant opportunities for learning. I am a poster-child for this process!

So do not be overly anxious if you find many marks on your homeworks and exams. Rather, aim to use mistakes as learning opportunities. That is how life in academics (life in general!) works. Furthermore, be completely honest with yourself to candidly identify weaknesses. I will do my best to work personally with you if something remains uncertain or you feel there is a weakness in your skills that needs some extra help. Please seek help should you wish it. And finally, please do question my marks should you feel they are unfair or incorrect. I am prone to mistakes in my grading.

### SOME SPECIFIC POINTS ABOUT GRADING YOUR WORK

Assignments are generally marked using the following rules, with grading less forgiving as the class progresses through the semester. The following mistakes are marked down by an increasing amount moving through the list.

#### POINTS ABOUT GRADING YOUR WORK

1. **SIGN ERRORS:** Sign errors are a nuisance. We all must spend time to uncover them. One means of detecting errors is to try explaining the maths to yourself or someone else. Does the result make sense? If not, then perhaps there is a sign error. I am generally not too upset with sign errors if they have minimal physical relevance. But when they indicate a physical misconception then I will mark it more harshly.
2. **MATH ERRORS:** Math errors, such as those associated with basic calculus mistakes, are generally marked.
3. **DIMENSIONAL AND TENSORIAL ERRORS:** I am relatively unforgiving of dimensional mistakes and tensorial inconsistencies.
4. **PHYSICALLY MISSING THE POINT:** Evidence of physically missing the point will generally invoke the most negative marks depending on the depth of the misconception. The best way to convince me you grasp the basic physics is to use words and pictures. If the maths is missing or totally wrong, but you present some sensible words and pictures, then that will help earn some credit.

Here are some further considerations for your homework assignments.

- **PRESENTATION OF THE SOLUTION:** Please write clearly and legibly. I strongly encourage you to learn and use L<sup>A</sup>T<sub>E</sub>X as this mark-up language will be an indispensable tool for you throughout your career writing documents with or without mathematics. It is particularly useful if your handwriting is poor. If the equations and words are sloppy, you will find teachers less forgiving of errors. You must convince the teacher that you understand the solution and present the maths in a legible manner. Good communication skills are key to being a good scientist or engineer.
- **DEADLINES:** Please do your best to be on time with handing in homeworks and exams, with disasters, personal tragedy, and significant accidents the only excuses for late assignments. Fairness to those meeting the deadlines is the fundamental reason to insist on this rule.
  - You may hand-in homework late but only with prior arrangement. Otherwise, the homework set will receive zero credit.

### Course material and strategies for thriving

The course material consists of class notes plus a selection of online videos. Ideally, the notes are to be read and the videos viewed **prior to each class**. Salient points related to the material will be presented during class on the chalkboard, along with further discussion and questions. We will *not* cover all the material in class that is expected to be learned as part of the reading assignments and problem sets.

## STRATEGIES FOR THRIVING IN THIS COURSE

- ESSENTIALS FROM PROF. BAZETT TO VIEW AT START OF THE SEMESTER
  - View [this 12-minute lecture](#) on study tips.
  - View [this 12-minute lecture](#) on how to learn effectively.
  - View [this 19-minute lecture](#) on how to write L<sup>A</sup>T<sub>E</sub>X documents using Overleaf.
- PRIOR TO EACH CLASS
  - Review material from previous lecture (5 to 10 minutes).
  - View assigned videos (5 to 45 minutes).
  - Read assigned class notes (30 minutes to two hours).
- AFTER EACH CLASS
  - Reread lecture notes and review assigned videos.
  - Identify questions for class discussion or during Q & A session.
  - As needed, view recorded class lecture from 2020 to fill in gaps.
  - Work assigned exercises alone and then gather with classmates to discuss.
- QUESTIONS: Address questions by reaching out during class, after class, during office hours, during group gatherings, or via Ed Discussion. There are no silly questions, so please ask any and all!

## Course outline

1. Course introduction and mathematics refresher
  - [9-minute video from Prof. N. Hall](#) introducing some basic images from terrestrial fluid flows.
  - [16-minute video from 3Blue1Brown](#) on the divergence and curl operations with examples taken from fluid mechanics.
  - Course introduction
  - Chapter 1: cartesian tensors
  - Chapter 2: vector calculus
  - Chapter 11: the continuum hypothesis used for describing fluids as a continuous media
2. Geophysical particle mechanics
  - [Watch the first 5-minutes from this UCLA Spin Lab video](#) on Coriolis effect.
  - Chapter 9: kinematics of a particle moving around a rotating sphere, including position, velocity, acceleration, Cartesian and spherical coordinates, rotating reference frame, Coriolis acceleration, planetary centrifugal acceleration
  - Chapter 9: dynamics of a particle moving around a rotating sphere using Newton's equation of motion, rotating reference frames, gravitational geopotential
3. Symmetries, conservation laws, and constrained motion

- Chapter 10: mechanical energy, potential momentum, inertial oscillations, axial angular momentum

#### 4. Fluid kinematics

- [4-minute video on Eulerian and Lagrangian descriptions](#) from Prof. Hogg
- [27-minute video on Eulerian and Lagrangian descriptions](#) from Prof. Lumley.
- Chapter 12: Fluid kinematics, Eulerian and Lagrangian descriptions, Galilean invariance, material time derivative, flow lines

#### 5. Mass conservation

- [5-minute video on mass conservation](#) from Prof. Hogg.
- Chapter 14: continuity equation, mass budget for fluid elements and finite regions, kinematic boundary conditions

#### 6. Tracer conservation

- Chapter 15: barycentric velocity, tracer equation, budgets for infinitesimal fluid elements, budgets for finite fluid regions, Leibniz-Reynolds transport theorem, boundary conditions

#### 7. Kinematics of incompressible flow

- [4-minute video on streamlines](#) from Prof. Hogg.
- Chapter 16: scalar streamfunction, vector streamfunction, area and volume conservation, meridional-depth overturning circulation

#### 8. Momentum dynamics

- [6-minute video on momentum](#) from Prof. Hogg.
- Chapter 17: momentum dynamics, accelerations, contact forces, body forces, special forms of the momentum equation, axial angular momentum

#### 9. Stress in fluids

- [2.5-minute video on stress and strain](#) from Prof. Hogg.
- [8-minute video on stress](#) from Prof. Hogg.
- Chapter 18: stresses and the stress tensor, linear momentum budget, relating stress to strain, form stress, boundary conditions
- Chapter 19: pressure form stress

#### 10. Energy dynamics and filtered equations

- Chapter 21: thermodynamics of a moving fluid, mechanical energy, internal energy, total energy
- [8-minute video on hydrostatic pressure](#) from Prof. Hogg.
- Chapter 22: primitive equations, hydrostatic approximation, tangent plane approximation, basics of time evolving a fluid state

#### 11. Boussinesq ocean equations

- Chapter 23: oceanic Boussinesq approximation

## 12. Buoyancy

- [49-minute video from Prof. Lewin](#) for an overview of buoyancy as well as other features of fluid mechanics.
- Chapter 24: Archimedes' principle, buoyancy, stratification, gravitational stability, mass density for perfect and realistic fluids

## 13. Geostrophic mechanics and balanced inviscid horizontal flows

- [30-minute video from Prof. Fultz](#) for an overview of rotating fluids.
- [4-minute video from the UCLA SpinLab](#) for examples of Taylor columns.
- Chapter 25: Rossby number, geostrophy, planetary geostrophy, Taylor-Proudman, thermal wind, isopycnal form stress
- Chapter 26: natural coordinates; centripetal, centrifugal, and Coriolis accelerations; exact geostrophic flow; inertial motion of fluid particles; cyclostrophic balance; gradient wind balance

## 14. Ekman layer mechanics

- Start around the 23-minute mark [of this video from Prof. Fultz](#) for his discussion of Ekman layers.
- Chapter 27: natural coordinates, spiral motion across isobars, non-dimensionalization and the Ekman number, net mass transport

## 15. Formulation of shallow water models

- [30-minute video](#) on shallow water model from Prof. Hall.
- Chapter 30: thickness equation, momentum equation, reduced gravity model, stacked shallow water layers, shallow water layer in a rotating tank

## 16. Shallow water dynamics

- Chapter 31: geostrophy, form stress, mechanical energy including available potential energy, angular momentum in a tank

## 17. Vorticity, circulation, and potential vorticity

- [23-minute video on vorticity](#) from Prof. Shapiro
- Chapter 32: vorticity and circulation
- Chapter 34: shallow water vorticity and potential vorticity

## 18. Vorticity mechanics

- [21-minute video on vorticity](#) from Prof. Shapiro.
- [5-minute video on vortex rings and Helmholtz's theorems](#) from the Physics Girl.
- Chapter 35: vortex lines and tubes, Kelvin's circulation theorem, mechanics of baroclinicity,  $\beta$ -effect

## 19. Balanced models I (single layer)

- Chapter 33: barotropic vorticity equation
  - Chapter 38: Buckingham's  $\Pi$  theorem, asymptotic expansion in terms of small Rossby number, shallow water planetary geostrophy and quasi-geostrophy
20. Balanced models II (continuous stratification)
- Chapter 39: asymptotic derivation of continuously stratified planetary geostrophy and properties of these equations.
  - Chapter 40: asymptotic derivation of continuously stratified quas-geostrophy and properties of these equations.

We generally have 24 classes per semester. So that above 20 lectures will be supplemented with four further lectures depending on the class needs and wants. The following topics have been covered in the past and will be presented if there is time.

1. Kinematics of material objects

- Chapter 13: Eulerian and Lagrangian description of material lines, surfaces, and volumes within a perfect fluid.

2. Advection and diffusion

- Chapter 46: advection maths and physics; diffusion maths and physics

3. Potential vorticity mechanics

- Chapter 36: PV material invariance for perfect fluid; PV evolution with friction and heating; impermeability theorem; isopycnal layer integrated PV

4. Shallow water gravity waves and geostrophic adjustment

- [14-minute video on gravity waves](#) from Prof. N. Hall.
- Section 31.8: gravity waves in single shallow water layer
- Section 34.7: geostrophic adjustment



# List of Symbols

Many symbols encountered in this book are defined local to their usage and are not found far outside of that location. Many other symbols appear in a variety of places and are included in the following list that offers a quick reminder of their meaning. Symbols are here categorized according to whether they are English (Latin-based), Greek, or mathematical operators.

## NON-DIMENSIONAL NUMBERS

SYMBOL	MEANING
Bu	Burger number: $Bu = (\text{deformation radius}/\text{horizontal length scale of flow})^2 = (L_d/L)^2$
Ek	Ekman number: $Ek = \text{friction acceleration from vertical shears divided by coriolis acceleration}$
Fr	Froude number: $Fr = \text{fluid particle speed divided by wave speed}$
Ge	Geostrophic number: $Ge = \text{Coriolis acceleration divided by pressure gradient acceleration}$
Kn	Knudsen number: $Kn = \text{molecular mean free path divided by macroscopic length scale}$
Re	Reynolds number: $Re = \text{inertial acceleration divided by frictional acceleration} = U L/\nu$
Ri	Richardson number: $Ri = \text{squared buoyancy frequency divided by squared vertical shear}$
Ro	Rossby number: $Ro = \text{inertial acceleration divided by Coriolis acceleration} = U/(f L)$

## LATIN SYMBOLS: PART I

SYMBOL	MEANING
$\mathbb{A}$	skew diffusion tensor: $\mathbb{A}_{mn} = -\mathbb{A}_{nm}$
$A_v$	Avogadro's number: $A_v = 6.0222 \times 10^{23} \text{ mole}^{-1}$
$b$	Archimidean buoyancy with $b > 0$ for relatively light fluid: $b = -g(\rho - \rho_0)/\rho_0$
$c_s$	sound speed: $c_s^{-2} = [\partial\rho/\partial p]_{\Theta,S}$
$c_p$	heat capacity at constant pressure: $c_p = [\partial\mathcal{H}/\partial T]_{p,C}$
$C$	tracer concentration = mass of tracer per mass of fluid = tracer mass fraction
$C_D$	dimensionless bottom drag coefficient: $C_D > 0$
$\mathcal{C}$	circulation of velocity around the boundary of a surface $\mathcal{C} \equiv \oint_{\partial S} \mathbf{v} \cdot d\mathbf{r}$
$\mathcal{E}$	total energy per mass of a fluid element = sum of internal plus mechanical energies
$\bar{e}_a$	basis vectors for a chosen coordinate system, with index $a = 1, 2, 3$ for 3-dimensional space.
$f$	Coriolis parameter, also the planetary vorticity: $f = 2\Omega \sin \phi$
$f_0$	Coriolis parameter at a particular latitude: $f_0 = 2\Omega \sin \phi_0$
$F$	frictional acceleration
$F_i^m$	deformation tensor; also transformation matrix between material and position coordinates
$G = G^{\text{grav}}$	Newton's gravitational constant: $G = 6.674 \times 10^{-11} \text{ N m}^2 \text{ kg}^{-2} = 6.674 \times 10^{-11} \text{ m}^3 \text{ kg}^{-1} \text{ s}^{-2}$
$G(\mathbf{x} \mathbf{x}_0)$	Green's function with $\mathbf{x}$ the observation point (or field point) and $\mathbf{x}_0$ the source point
$\mathcal{G}(\mathbf{x} \mathbf{x}_0)$	Free space Green's function; i.e., the Green's function without boundaries
$\mathcal{G}$	Gibbs potential per mass of a fluid element
$g$	effective gravitational acceleration from central gravity + planetary centrifugal: $g \approx 9.8 \text{ m s}^{-2}$
$g^r$	reduced gravity defined between two fluid layers; e.g., $g_{3/2}^r = g(\rho_2 - \rho_1)/\rho_1 \ll g$
$h$	layer thickness for a shallow water fluid
$h$	layer thickness for a continuously stratified fluid: $h = \bar{h} \delta\sigma$
$\hbar$	specific thickness for a generalized vertical coordinate: $\hbar = \partial z / \partial \sigma = 1 / (\partial \sigma / \partial z)$
$\mathcal{H}(x)$	Heaviside step function: $\mathcal{H}(x) = 0$ for $x < 0$ whereas $\mathcal{H}(x) = 1$ for $x > 0$
$H$	vertical depth scale of the flow under consideration
$H$	sometimes used as depth of the ocean bottom: $z = -H(x, y) = \eta_b(x, y)$
$\mathcal{H}$	enthalpy per mass of a fluid element
$\mathcal{I}$	internal energy per mass of a fluid element
$i$	$i = \sqrt{-1}$ used for imaginary numbers
$J$	tracer flux; for material tracers the dimensions are mass per time per area
$K$	kinetic energy for a point particle of mass $m$ : $K = m \mathbf{V} \cdot \mathbf{V} / 2$
$\mathcal{K}$	kinetic energy per mass of a fluid element: $\mathcal{K} = \mathbf{v} \cdot \mathbf{v} / 2$
$\mathbb{K}$	diffusivity tensor; a positive semi-definite symmetric second order tensor
$k$	integer index to label a layer in a shallow water model with $k = 1, N$ layers ( $k = 1$ is top layer)
$k_B$	Boltzmann constant: $k_B = 1.3806 \times 10^{-23} \text{ m}^2 \text{ kg s}^{-2} \text{ K}^{-1}$
$L$	horizontal length scale of the flow under consideration
$L_d$	deformation radius: (a) shallow water $L_d = \sqrt{g H/f}$ ; (b) continuous internal $L_d = H N/f$
$m$	mechanical energy per mass of a fluid element
$M_{\text{air}}$	grams per mole of air: $M_{\text{air}} = 28.8 \times 10^{-3} \text{ kg mole}^{-1}$
$N$	buoyancy frequency
$p$	pressure at a point in the fluid
$p_a$	pressure applied to the ocean surface from the atmosphere or cryosphere
$p_b$	pressure at the bottom of a fluid column
$p_{\text{slp}}$	sea level pressure with an area average, $\langle p_{\text{slp}} \rangle = 101.325 \times 10^3 \text{ N m}^{-2}$
$p_{k-1/2}$	hydrostatic pressure at the layer interface with vertical position $z = \eta_{k-1/2}$
$P_k$	pressure integrated over a shallow water layer: $P_k \equiv \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} p_k(z) dz = h_k (g \rho_k h_k / 2 + p_{k-1/2})$
$\mathcal{P}_k$	potential energy for a shallow water fluid: $\mathcal{P}_k = g \rho_k \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} z dz = (g \rho_k / 2) (\eta_{k-1/2}^2 - \eta_{k+1/2}^2)$

## LATIN SYMBOLS: PART II

SYMBOL	MEANING
$Q$	potential vorticity for continuously stratified (Ertel PV) or shallow water (Rossby PV)
$q$	quasi-geostrophic potential vorticity either for a continuous fluid or shallow water fluid
$Q_m$	mass flux (mass per horizontal area per time) across ocean surface: $Q_m > 0$ enters ocean
$\mathcal{Q}_m$	mass flux (mass per area per time) across ocean surface: $\mathcal{Q}_m d\mathcal{S} = Q_m dA$
$Q_C$	turbulent tracer flux (tracer per horiz area per time) across ocean surface: $Q_C > 0$ enters ocean
$\mathcal{Q}_C$	turbulent tracer flux (tracer per area per time) across ocean surface: $\mathcal{Q}_C d\mathcal{S} = Q_C dA$
$r$	radial distance of a point relative to an origin, typically taken as center of a spherical earth
$\mathbb{R}$	rotation tensor: $2 \mathbb{R}_{mn} = \partial_n v_m - \partial_m v_n = -2 \mathbb{R}_{nm}$
$\mathbb{R}^1$	real number line
$\mathbb{R}^2$	two-dimensional Euclidean space of real numbers
$\mathbb{R}^3$	three-dimensional Euclidean space of real numbers
$R$	radius of a sphere
$R_e$	radius of sphere whose volume approximates that of the earth: $R_e = 6.371 \times 10^6$ m
$R_g$	universal gas constant: $R_g = 8.314 \text{ J mole}^{-1} \text{ K}^{-1} = 8.314 \text{ kg m}^2 \text{ s}^{-2} \text{ mole}^{-1} \text{ K}^{-1}$
$R^{\text{air}}$	specific gas constant for air: $R^{\text{air}} = R_g/M_{\text{air}} = 2.938 \times 10^2 \text{ m}^2 \text{ s}^{-2} \text{ K}^{-1}$
$\mathfrak{S}$	entropy per mass of a fluid element
$\mathbb{S}$	rate of strain tensor: $2 \mathbb{S}_{mn} = \partial_n v_m + \partial_m v_n$
$\mathbb{S}^{\text{dev}}$	deviatoric rate of strain tensor: $\mathbb{S}_{mn}^{\text{dev}} = \mathbb{S}_{mn} - \delta_{mn} \mathbb{S}_{qq}/3$
$S$	salt concentration = mass of salt in a fluid element per mass of seawater
$S$	Absolute Salinity, generically referred to as salinity: $S = 1000 \mathfrak{S}$
$s$	expression for a generic surface: $s = s(x, y, z, t)$ .
$s$	arc-length along a curve $\mathbf{x}(s)$ with infinitesimal increment $ds = \sqrt{d\mathbf{x} \cdot d\mathbf{x}}$
$\hat{s}$	unit tangent vector to a curve, also written as $\hat{s} = \hat{\mathbf{t}}$ (see below)
$\text{sgn}$	sign function related to Heaviside step function via $\text{sgn}(x) = 2 \mathcal{H}(x) - 1$
$T$	absolute thermodynamic <i>in situ</i> temperature (Kelvin if in a thermodynamic equation)
$\mathbb{T}$	stress tensor
$\mathbb{T}^{\text{kinetic}}$	kinetic stress tensor: $\mathbb{T}^{\text{kinetic}} = -\rho \mathbf{v} \otimes \mathbf{v}$
$\mathbb{T}^{\text{sw kinetic}}$	kinetic stress tensor for shallow water fluid: $\mathbb{T}^{\text{sw kinetic}} = -\rho \mathbf{u} \otimes \mathbf{u}$
$t$	time (universal Newtonian time)
$\hat{t}$	unit tangent vector to a curve: $\hat{t} = d\mathbf{x}/ds$ , where $s$ is the arc-length so that $ds = \sqrt{d\mathbf{x} \cdot d\mathbf{x}}$
$\mathbf{u}$	horizontal velocity of a fluid element: $\mathbf{u} = \hat{\mathbf{x}} u + \hat{\mathbf{y}} v$
$U$	horizontal velocity scale of the flow under consideration
$\mathbf{U}$	depth integrated horizontal velocity: $\mathbf{U} = \int_{\eta_b}^{\eta} \mathbf{u} dz$
$\mathbf{v}$	velocity of a fluid element: $\mathbf{v} = D\mathbf{x}/Dt = \hat{\mathbf{x}} u + \hat{\mathbf{y}} v + \hat{\mathbf{z}} w$
$W$	vertical velocity scale of the flow under consideration
$w$	vertical component to the velocity: $w = Dz/Dt$
$w^{\text{dia}}$	dia-surface flux = volume per area per time across a $\sigma$ -surface: $w^{\text{dia}} = (1/ \nabla \sigma ) \dot{\sigma}$
$w^{(\dot{\sigma})}$	dia-surface velocity = volume per <i>horizontal area</i> per time across a $\sigma$ surface: $w^{(\dot{\sigma})} = (\partial z/\partial \sigma) \dot{\sigma}$
$(x, y, z)$	triplet of Cartesian coordinates
$\mathbf{x}$	spatial position with Cartesian representation: $\mathbf{x} = \hat{\mathbf{x}} x + \hat{\mathbf{y}} y + \hat{\mathbf{z}} z$
$(\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}})$	triplet of Cartesian unit vectors oriented in a righthand sense
$z_\sigma$	specific thickness for a generalized vertical coordinate: $z_\sigma = \partial z/\partial \sigma = h$

## GREEK SYMBOLS

SYMBOL	MEANING
$\alpha$	thermal expansion: $\alpha = -\rho^{-1} \partial \rho / \partial \theta$ or $\alpha = -\rho^{-1} \partial \rho / \partial \Theta$ or $\alpha = -\rho^{-1} \partial \rho / \partial T$
$\alpha_T$	thermal expansion in terms of <i>in situ</i> temp: $\alpha = -\rho^{-1} \partial \rho / \partial T$
$\alpha^{(\Theta)}$	thermal expansion in terms of Conservative Temperature: $\alpha^{(\Theta)} = -\rho^{-1} \partial \rho / \partial \Theta$
$\alpha_{\text{aspect}}$	aspect ratio; ratio of vertical to horizontal scales of the flow: $\alpha_{\text{aspect}} = H/L$
$\beta, \beta^{(S)}$	saline contraction coefficient: $\beta = \rho^{-1} \partial \rho / \partial S$
$\beta$	meridional derivative of planetary vorticity: $\beta = \partial_y f$
$\hat{\gamma}$	dianeutral unit vector pointing perpendicular to the neutral tangent plane
$\delta^{ab}$	components to the Kronecker tensor in Cartesian coordinates
$\delta^a_b$	components to the Kronecker tensor in general coordinates
$\epsilon$	kinetic energy dissipation from viscosity (energy per time per mass)
$\epsilon_{ab}$	components to the permutation symbol in two space dimensions
$\epsilon_{abc}$	components to the permutation symbol in three space dimensions
$\eta = \eta_0$	vertical position of the free upper surface of a fluid domain: $z = \eta(x, y, t)$
$\eta_{k-1/2}$	depth of the interface at the top of the shallow water layer k
$\eta_{k+1/2}$	depth of the interface at the bottom of the shallow water layer k
$\eta_b = -H$	vertical position of static solid-earth boundary: $z = \eta_b(x, y) = -H(x, y)$
$(\lambda, \phi)$	(longitude, latitude) on the sphere: $0 \leq \lambda \leq 2\pi$ and $-\pi/2 \leq \phi \leq \phi/2$
$\kappa$	molecular kinematic diffusivity
$\kappa_T$	molecular diffusivity for <i>in situ</i> temperature in water: $\kappa_T = 1.4 \times 10^{-7} \text{ m}^2 \text{ s}^{-1}$
$\kappa_S$	molecular diffusivity for salt in water: $\kappa_S = 1.5 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$
$\kappa_{\text{eddy}}$	kinematic eddy diffusivity: $\kappa_{\text{eddy}} \gg \kappa$
$\mu_n$	chemical potential for constituent $n$ within a fluid (energy per mass)
$\tilde{\mu}_n$	chemical potential for constituent $n$ within a fluid (energy per mole number)
$\mu$	relative chemical potential for a binary fluid
$\mu$	chemical potential for seawater: $\mu = \mu_{\text{salt}} - \mu_{\text{water}}$
$\mu_{\text{vsc}}$	dynamic viscosity = $\rho \nu$
$\nu_s$	specific volume: $\nu_s = \rho^{-1}$
$\nu$	molecular kinematic viscosity
$\nu_{\text{air}}$	molecular kinematic viscosity of air: $\nu_{\text{air}} \approx 1.3 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}$
$\nu_{\text{water}}$	molecular kinematic viscosity of fresh water: $\nu_{\text{water}} \approx 10^{-6} \text{ m}^2 \text{ s}^{-1}$
$\nu_{\text{eddy}}$	eddy viscosity: $\nu_{\text{eddy}} \gg \nu$
$\omega$	relative vorticity axial vector: $\omega = \nabla \times \mathbf{v}$
$\omega$	radial frequency for a wave so that the wave period is $2\pi/\omega$
$\Omega$	earth's angular velocity oriented through north pole: $\Omega = 7.2921 \times 10^{-5} \text{ s}^{-1}$
$\Phi$	geopotential from central gravity plus planetary centrifugal
$\psi$	streamfunction for two-dimensional non-divergent flow: $\mathbf{u} = \hat{\mathbf{z}} \times \nabla \psi$
$\Psi$	vector streamfunction for three-dimensional non-divergent flow: $\mathbf{v} = \nabla \times \Psi$
$\rho$	<i>in situ</i> density (mass per volume) of a fluid element
$\varrho$	potential density referenced to a specified pressure level
$\rho_0$	constant reference density used for the oceanic Boussinesq fluid
$\sigma$	generalized vertical coordinate surface with $\sigma(x, y, z, t) = \text{constant}$
$\tau$	stress vector
$\theta$	potential temperature
$\Theta$	Conservative Temperature
$\zeta$	vertical component to the relative vorticity; e.g., $\zeta = \partial_x v - \partial_y u$
$\zeta_a$	vertical component to the absolute vorticity; .e.g., $\zeta_a = f + \partial_x v - \partial_y u$

## MATHEMATICAL OPERATIONS AND SYMBOLS

SYMBOL	MEANING
$[\equiv]$	read “has dimensions” and used when referring to the physical dimensions
$\times$	vector cross product of vector calculus
$\nabla$	gradient operator
$\nabla_z$	horizontal gradient operator: $\nabla_z = \hat{\mathbf{x}}(\partial/\partial x) + \hat{\mathbf{y}}(\partial/\partial y) = \hat{\mathbf{x}}\partial_x + \hat{\mathbf{y}}\partial_y$
$\nabla \cdot$	divergence operator that acts on a vector to produce a scalar
$\nabla \times$	curl operator
$\nabla_\sigma$	horizontal gradient on constant $\sigma$ -surface: $\nabla_\sigma = \hat{\mathbf{x}}(\partial/\partial x)_\sigma + \hat{\mathbf{y}}(\partial/\partial y)_\sigma$
$\partial_\sigma$	vertical derivative with general vertical coordinate: $\partial_\sigma = \partial/\partial\sigma = (\partial z/\partial\sigma)\partial/\partial z$
$\partial/\partial t$	Eulerian time derivative acting at a fixed spatial position, $\mathbf{x}$
$[\partial/\partial t]_\sigma$	time derivative computed on constant $\sigma$ -surface
$D/Dt$	material, Lagrangian, or substantial time derivative following a fluid particle
$\delta$	inexact differential operator
$\delta$	differential increment often written when following the fluid flow
$\delta(x)$	one-dimensional Dirac delta distribution with dimensions inverse length
$\delta^{(2)}(\mathbf{x})$	two-dimensional Dirac delta distribution with dimensions inverse area
$\delta(\mathbf{x})$	three-dimensional Dirac delta distribution with dimensions inverse volume
$\delta(t)$	temporal Dirac delta distribution with dimensions inverse time
$\Delta$	finite difference increment in space: $\Delta_x, \Delta_y, \Delta_z, \Delta_\sigma$
$dA$	infinitesimal horizontal area element: $dA = dx dy$
$d\mathcal{S}$	infinitesimal area element on a surface
$dV$	infinitesimal volume element
$dV$	infinitesimal volume for a region moving with the fluid (Lagrangian region)
$\int_{\mathcal{R}} dV$	volume integral over an arbitrary region, $\mathcal{R}$
$\int_{\mathcal{R}(\mathbf{v})} dV$	volume integral over a region following the fluid flow (Lagrangian integral)
$\int_{\mathcal{S}} d\mathcal{S}$	surface integral over a surface $\mathcal{S}$
$\oint_{\partial\mathcal{R}} d\mathcal{S}$	surface integral over a closed surface $\partial\mathcal{R}$ that bounds the volume $\mathcal{R}$
$\oint d\ell$	closed line integral over a periodic domain
$\oint_{\partial\mathcal{S}} d\ell$	counter-clockwise closed line integral over the boundary of a surface, $\partial\mathcal{S}$
$\sim$	read “similar to” or “scales as”
$\approx$	approximately equal to
$\dot{\Psi}$	time derivative following a particle trajectory; for fluids, $\dot{\Psi} = D\Psi/Dt$ .



## **Part I**

### **Mathematical methods and concepts**

Fluid mechanics is a field theory based on Newton's laws of mechanics and quasi-equilibrium thermodynamics as applied to a continuous fluid media. Geophysical fluid mechanics is concerned with gravitationally stratified fluids with multiple matter constituents moving on a rotating sphere. The speed for all motion is small relative to the speed of light so that relativistic effects are negligible, thus enabling the use of universal Newtonian time for all observers. Our goal for this part of the book is to review mathematical topics for use in our study of geophysical fluid mechanics. Depending on the reader's background and interests, this material can be readily skipped on first reading and/or accessed later to fill gaps.

#### PHYSICS PROVIDES RELATIONS BETWEEN GEOMETRIC OBJECTS

Mathematical objects of use for the study of fluid mechanics include scalar fields (e.g., temperature, mass density, specific entropy), vector fields (e.g., velocity, vorticity), and second order tensor fields (e.g., diffusion tensor, stress tensor, moment of inertia tensor). These and other fields have an existence independent of the arbitrary coordinate choices used for their description. Thinking abstractly, these physical fields are geometric objects such as points, vectors, surfaces, volumes, etc. In the study of geophysical fluid mechanics, we use physical principles to develop differential equations relating geometric objects. Mathematical tools are used to compute numbers as required to compare with experiments and field measurements, and to formulate discrete equations for numerical simulations.

Our perspective can be summarized by “physics as geometry”, which forms a foundation to theoretical physics such as that detailed in [Thorne and Blandford \(2017\)](#). It has both conceptual and practical use for our study. It furthermore provides the framework for this part of the book, in which we develop mathematical tools that are later used to formulate a variety of theoretical geophysical fluid models. Our overall aim is to develop mathematical tools to help unpack the physics encapsulated by equations. This aim extends to those cases where analytical solutions are unavailable, which is the norm for nonlinear field theories such as fluid mechanics or even in many cases when the equations are linearized. Such qualitative and conceptual tools are of great value for the analysis of numerical simulations and field measurements.

#### TENSOR ANALYSIS AND GEOPHYSICAL FLUID MECHANICS

There are many occasions where a geophysical fluid system is more physically transparent when using a particular coordinate description or reference frame. However, there is no *a priori* choice that fits all systems. Thus, being adept at transforming from one description to another eases the study. Tensor analysis is the proven means for systematically performing such transformations thus motivating its use throughout fluid mechanics. In its more abstract realization via differential forms, tensor analysis provides the means to mathematically express physical ideas without any display of coordinate artefacts, thus exposing the underlying physical and mathematical essence.

The following offers an incomplete list of geophysical fluid systems where various coordinate descriptions or reference frames are encountered, and thus where tensor analysis can be put to use. Granted, each system listed here can be studied without the formalism of tensor analysis. However, by doing so one often encounters clumsy manipulations that can obfuscate the underlying physical concepts. Indeed, imagine the tedium required to write continuous field equations in multiple dimensions prior to vector analysis! That situation is akin to the tedium and awkward nature required to work across multiple coordinate systems and reference frames absent the formalism of tensor analysis. Hence, an adept use of vector analysis, its generalization to tensor analysis, and its further abstraction to differential forms, reveals how maths can inform the physics and how physics can be transparently embodied by the maths.

- RELATING EULERIAN AND LAGRANGIAN KINEMATICS: There is a duality in fluid kinematics between Eulerian and Lagrangian descriptions of fluid motion. To develop an understanding of this duality we make use of tensor analysis to facilitate the transformation between the two kinematic descriptions.
- SPHERICAL PLANET: Geophysical fluids move on an approximately spherical planet, making spherical coordinates the preferred choice for studying planetary flows. We make use of tensor methods to transform between planetary Cartesian coordinates (origin at the center of the planet) and spherical coordinates.
- CYLINDRICAL ROTATING TANK: Rotating laboratory fluids move in a circular tank, with cylindrical polar coordinates of use to respect symmetry of the domain. We make use of tensor methods to transform between Cartesian and cylindrical polar coordinates when considering rotating tank systems.
- ROTATING REFERENCE FRAME: Geophysical fluids move around a rotating earth and the fluid maintains a close to solid-body motion. Terrestrial observers also move in near solid-body motion. We are thus motivated to study geophysical fluids from a rotating reference frame. We use rudimentary tensor methods to transform between a fixed inertial frame and the non-inertial rotating reference frame, with this transformation revealing non-inertial accelerations (Coriolis and centrifugal) that impact on the observed fluid flow.
- STRATIFIED FLUIDS AND GENERALIZED VERTICAL COORDINATES: Geophysical fluids move in a gravitational field that acts to stratify the fluid according to its local buoyancy. For many purposes it can be useful to describe the vertical position of a fluid element according to its buoyancy rather than its height. This “isopycnal” vertical coordinate choice leads to a non-orthogonal coordinate description of the fluid motion. There are other vertical coordinates that can be of use for other situations, such as the terrain following coordinates commonly used for atmospheric simulations and coastal ocean models. Transforming between Cartesian coordinates and such *generalized vertical coordinates* requires the mathematical precision of general tensors.
- WATER MASS ANALYSIS: We may use properties such as temperature, salinity, carbon concentration to define coordinates for a point within a water mass configuration space. This space has arbitrary dimensionality and has no natural metric structure, thus making the use of *differential forms* of use to expose the underlying mathematical structure of this space.

## SUMMARY OF THE MATH CHAPTERS

Some of the chapters in this part of the book are essential for nearly all subsequent chapters (e.g., Chapters 1 and 2), with the bulk of this book accessible to those with a solid undergraduate training in multi-variate calculus and the rudiments of analytic geometry. Other chapters target those interested in penetrating various special topics presented in this book. Readers are encouraged to take a close look at each chapter if only to know where to find topics that might be of use later in the book or later in one’s career.

- CARTESIAN TENSOR ALGEBRA: Chapter 1 is a synopsis of Cartesian tensor analysis. This topic provides a systematization of ideas from Cartesian geometry and linear algebra. Material in this chapter is essential for nearly every topic in this book.
- CARTESIAN TENSOR CALCULUS: Chapter 2 extends the algebraic ideas from Chapter 1 to differential and integral calculus. This chapter provides a resume of multivariate or vector

calculus of use for fluid mechanics. Material in this chapter is essential for nearly every topic in this book.

- PARTIAL DIFFERENTIAL EQUATIONS: Chapter 3 provides a summary of linear partial differential equations (PDEs) commonly encountered in mathematical physics. Even though the equations of fluid mechanics are nonlinear PDEs, their linear counterparts offer much insight into fluid behavior.
- GREEN'S FUNCTIONS: Chapter 4 provides a survey of Green's function methods used to solve linear partial differential equations of mathematical physics. Although this book is less concerned with specific solutions to these equations, we study the Green's function method since it facilitates rather general insights into both the mathematical and physical content of fluid equations. Furthermore, Green's function methods are commonly used across various areas of the geophysical sciences, thus making it quite useful to be familiar with the method.
- GEOMETRY OF CURVES AND SURFACES: Chapter 5 introduces rudimentary differential geometry used to characterize curves (such as fluid particle trajectories) and surfaces (such as isopycnals) embedded in a background Euclidean space. Here we encounter such notions as normal and tangent directions and curvature.
- GENERAL TENSOR INTRODUCTION: Chapter 6 provides an introduction to general tensor analysis and its applications to geophysical fluids. The discussion is accessible to anyone who has read Chapter 1, and is recommended for all readers of this book, even for those who do not wish to study the details of general tensors in Chapter 7.
- GENERAL TENSOR ANALYSIS: Chapter 7 extends the Cartesian tensor algebra and calculus to allow for the use of arbitrary, or general, coordinates. This chapter is essential to understand the mathematics underlying non-Cartesian coordinates, such as spherical coordinates and generalized vertical coordinates.
- ORTHOGONAL COORDINATES: Chapter 8 offers a reference for the three locally orthogonal coordinate systems (Cartesian, spherical, cylindrical) used in this book and how various mathematical objects appear when written in these coordinates.

# Chapter 1

## Cartesian tensor algebra

In this chapter we introduce the formalism of Cartesian tensor analysis with a focus on the basic algebraic relations. The use of Cartesian tensors restricts attention to Cartesian coordinates on a flat Euclidean space, with all Cartesian coordinates related by orthogonal transformations representing rotations.

### CHAPTER GUIDE

We follow standard treatments of Cartesian tensors such as that in Chapter 2 of [Aris \(1962\)](#), Chapter 1 of [Segel \(1987\)](#), and Chapter 2 of [Lovelock and Rund \(1989\)](#) (where they use the term *affine tensors* rather than *Cartesian tensors*). The discussion should be accessible to those having studied undergraduate calculus and linear algebra. For geophysical fluid mechanics, mastery of Cartesian tensors is nearly sufficient for mastery of general tensors. This chapter is basic to all of the maths in this book.

1.1	Introduction to tensors and tensor fields . . . . .	6
1.2	Points and vectors . . . . .	6
1.3	Distance and the scalar product . . . . .	8
1.3.1	Distance between points . . . . .	8
1.3.2	Magnitude of a vector and the scalar product . . . . .	8
1.4	Vector product . . . . .	9
1.4.1	Basis vector orientation and the Levi-Civita tensor . . . . .	9
1.4.2	Axial (or pseudo) vector . . . . .	10
1.4.3	Orthogonality relations between cross products . . . . .	10
1.4.4	Vector product of arbitrary vectors . . . . .	11
1.4.5	Geometric interpretation of the vector product . . . . .	11
1.4.6	Generalization to arbitrary vectors . . . . .	13
1.5	Measuring volume . . . . .	13
1.5.1	Volume defined by three vectors . . . . .	13
1.5.2	Cartesian volume element for integration . . . . .	14
1.5.3	$n$ -space volumes and the Levi-Civita tensor . . . . .	14
1.6	Example vector identities using the Levi-Civita tensor . . . . .	15
1.6.1	Double vector product . . . . .	15
1.6.2	Scalar product of two vector products . . . . .	15
1.7	Transforming the coordinate representations . . . . .	16
1.7.1	Inverse transformation . . . . .	16
1.7.2	Orthogonal transformation . . . . .	16
1.7.3	Geometric interpretation of orthogonal transformations . . . . .	17

1.7.4	Transforming the coordinate representation of a vector . . . . .	18
1.7.5	Invariance of the scalar product . . . . .	18
1.7.6	Transforming the coordinate representation of a second order tensor	18
1.7.7	Importance of distinguishing between tensors and matrices . . . . .	19
1.8	Homogeneity and isotropy . . . . .	19
1.8.1	Homogeneous tensor . . . . .	19
1.8.2	Isotropic and anisotropic tensors . . . . .	19
1.9	Exercises . . . . .	20

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## 1.1 Introduction to tensors and tensor fields

Fluid mechanics involves fields of scalars, vectors, and higher order tensors. We generically refer to all of these geometric objects as *tensors*, with a scalar a zero order tensor and a vector a first order tensor. A scalar field provides a single number at each point in space-time. Example scalar fields include temperature, mass density, entropy, salinity, humidity, and mechanical energy. On a flat manifold, such as the Euclidean space considered in this chapter, a vector connects two points on the manifold and is specified by a direction and a magnitude. Correspondingly, a vector field provides a vector at each point in space. Example vector fields include the fluid velocity and forces acting on fluid elements. A second order tensor can be represented by a matrix, with a tensor field providing a matrix at each point in space. The stress tensor and the diffusion tensor are examples encountered in this book.

Geophysical fluids are embedded in the Newtonian universal time and flat Euclidean space. This space and time structure induces the familiar Euclidean norm when measuring the spatial distance between points, whether the points are on a plane, a sphere, or an arbitrary surface within the fluid such as a surface of constant specific entropy. We can thus make use of Cartesian coordinates as the starting point for a mathematical formulation of geophysical fluid mechanics. Transformations to alternative coordinates are made when they lend insight to the symmetry of the flow and/or the geometry of the space on which the flow occurs. It is for this reason that we devote this chapter to developing the formalism of Cartesian tensor analysis. Furthermore, it is for this reason that Cartesian tensors gives us nearly all of the formalism necessary to study general tensors in geophysical fluid mechanics.

## 1.2 Points and vectors

Consider a point,  $\mathcal{P}$ , in three dimensional Euclidean space  $\mathbb{R}^3$ . We can represent its spatial position by providing its Cartesian coordinates relative to an arbitrary origin. As such, the position is a vector whose tail is at the origin and head at the point as shown in Figure 1.1. We write this coordinate representation as

$$\mathcal{P} \mapsto \vec{P} = \hat{\mathbf{x}} P_1 + \hat{\mathbf{y}} P_2 + \hat{\mathbf{z}} P_3. \quad (1.1)$$

Vectors are denoted by an arrow. The right hand side of equation (1.1) provides the representation of the position vector in terms of a triplet of Cartesian coordinates,  $(P_1, P_2, P_3)$ , that measure distance along their corresponding Cartesian unit vectors,  $(\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}})$ . The Cartesian unit vectors form a basis for three dimensional Euclidean space.<sup>1</sup> Hence, the position vector for any point in space can be represented in terms of these three basis vectors.

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<sup>1</sup>The unit vectors are sometimes denoted  $(\hat{i}, \hat{j}, \hat{k})$  in the literature. We generally avoid that notation in this book.

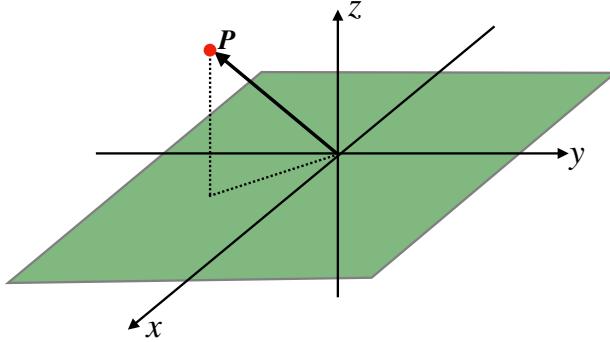


FIGURE 1.1: An arbitrary point in space,  $\mathcal{P}$ , has an objective existence independent of our subjective choice of coordinate system used to describe its position. We here represent its position with respect to the origin of a right-handed Cartesian coordinate system. The Cartesian representation of the position vector is  $\mathcal{P} \mapsto \vec{P} = \mathbf{P} = \hat{\mathbf{x}} P_1 + \hat{\mathbf{y}} P_2 + \hat{\mathbf{z}} P_3$ , with the Cartesian basis vectors the normalized triplet of unit vectors  $(\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}})$  and the triplet of Cartesian coordinates given by  $(P_1, P_2, P_3)$ . There are an infinite number of possible Cartesian coordinate systems that are rotated and/or translated with respect to the one shown here.

At times we find it useful to make use of alternative notations in which the position vector is written

$$\vec{P} = \mathbf{P} \quad (1.2a)$$

$$= \hat{\mathbf{x}} P_1 + \hat{\mathbf{y}} P_2 + \hat{\mathbf{z}} P_3 \quad (1.2b)$$

$$= \sum_{a=1}^3 \vec{e}_a P_a \quad (1.2c)$$

$$= \vec{e}_a P_a. \quad (1.2d)$$

The first equality introduced the boldface notation, which we commonly use for the representation of vectors in Cartesian coordinates. Indeed, although less convenient when moving to the general tensors of Chapter 6, we still maintain the boldface in this book given its common usage in the literature and since much of this book makes use of Cartesian tensors. Equation (1.2d) introduced the Einstein summation convention in which repeated indices are summed over their range, thus allowing us to drop the summation symbol. Equation (1.2c) introduced a generic notation for the basis vectors

$$\vec{e}_1 = \hat{\mathbf{x}} \quad \vec{e}_2 = \hat{\mathbf{y}} \quad \vec{e}_3 = \hat{\mathbf{z}}. \quad (1.3)$$

The Cartesian basis vectors each have unit magnitude (normalized), meaning that their scalar products yield<sup>2</sup>

$$\hat{\mathbf{x}} \cdot \hat{\mathbf{x}} = \hat{\mathbf{y}} \cdot \hat{\mathbf{y}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{z}} = 1. \quad (1.4)$$

Use of a hat or carot symbol over a vector signifies that the vector is normalized to unity. For Cartesian coordinates we generally work with the normalized basis vectors (1.3). Furthermore, a normalized vector can change only through rotation since by definition it remains of unit norm (see Section 2.1.4). For the general tensors of Chapters 6, 8 and 41, we sometimes find it more convenient to work with unnormalized basis vectors. Hence, the basis vectors,  $\vec{e}_a$ , retain the arrow symbol rather than the carot since they are not always normalized.

We emphasize that the tensor labels denote components of a specific coordinate representation,  $P_a$ , as well as members from the set of basis vectors,  $\vec{e}_a$ . These labels are not to be confused with

<sup>2</sup>The Cartesian scalar (or dot or inner) product is discussed more formally in Section 1.3.

partial derivative operations.<sup>3</sup> Finally, we sometimes write the vector components and basis vectors in the form of a list or triplet

$$P_a = (P_1, P_2, P_3) \quad \text{and} \quad \vec{e}_a = (\vec{e}_1, \vec{e}_2, \vec{e}_3) = (\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}}). \quad (1.5)$$

## 1.3 Distance and the scalar product

In defining a vector to have unit magnitude, we are assuming we know how to measure the magnitude of a vector. We here make this notion precise.

### 1.3.1 Distance between points

Consider two points in Euclidean space,  $\mathcal{P}$  and  $\mathcal{P} + d\mathcal{P}$ , separated by a small distance and specified by their respective position vectors

$$\mathcal{P} \mapsto \vec{P} = \vec{e}_a P_a \quad (1.6a)$$

$$\mathcal{P} + d\mathcal{P} \mapsto \vec{P} + d\vec{x} = \vec{e}_a (P_a + dx_a). \quad (1.6b)$$

Euclidean space is afforded a metric whereby the squared distance between two points is measured via Pythagoras' Theorem

$$[\text{distance}(\mathcal{P}, \mathcal{P} + d\mathcal{P})]^2 = (\vec{P} + d\vec{x} - \vec{P}) \cdot (\vec{P} + d\vec{x} - \vec{P}) \quad (1.7a)$$

$$= (\mathbf{P} + d\mathbf{x} - \mathbf{P}) \cdot (\mathbf{P} + d\mathbf{x} - \mathbf{P}) \quad (1.7b)$$

$$= dx_a dx_b (\vec{e}_a \cdot \vec{e}_b) \quad (1.7c)$$

$$= dx_a dx_b \delta_{ab} \quad (1.7d)$$

$$= dx_a dx_a \quad (1.7e)$$

$$= (dx_1)^2 + (dx_2)^2 + (dx_3)^2. \quad (1.7f)$$

To reach this result we introduced the components to the Kronecker delta tensor, which can be represented by the  $3 \times 3$  identity matrix

$$\vec{e}_a \cdot \vec{e}_b = \delta_{ab} = \begin{bmatrix} \delta_{11} & \delta_{12} & \delta_{13} \\ \delta_{21} & \delta_{22} & \delta_{23} \\ \delta_{31} & \delta_{32} & \delta_{33} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}. \quad (1.8)$$

The Kronecker tensor provides the Cartesian coordinate representation of the *metric* for Euclidean space. The metric provides the means to measure the distance between points on a manifold, and how to measure the length of a vector. It thus allows us to *normalize* a vector to have unit magnitude, motivating the often used term *norm* rather than metric. In Section 7.1 we introduce alternative representations for the metric based on the use of non-Cartesian coordinates and non-Euclidean manifolds.

### 1.3.2 Magnitude of a vector and the scalar product

By defining the distance between two points, we in turn have a prescription for defining the squared magnitude of a vector

$$|\mathbf{P}|^2 = \mathbf{P} \cdot \mathbf{P} = P_a P_b (\vec{e}_a \cdot \vec{e}_b) = P_a P_a = (P_1)^2 + (P_2)^2 + (P_3)^2. \quad (1.9)$$

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<sup>3</sup>In this book we eschew the notation where partial derivatives are denoted by a subscript.

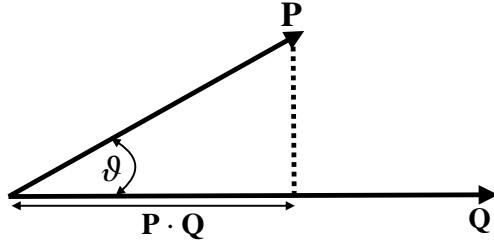


FIGURE 1.2: Illustrating the geometry associated with forming the scalar product between two vectors,  $\mathbf{P} \cdot \mathbf{Q} = |\mathbf{P}| |\mathbf{Q}| \cos \vartheta$ . Since the scalar or inner product requires a metric, we see that angles also require a metric.

Correspondingly, we have the *scalar product* between two arbitrary vectors

$$\mathbf{P} \cdot \mathbf{Q} = P_a Q_b (\vec{e}_a \cdot \vec{e}_b) = P_a Q_a, \quad (1.10)$$

which also goes by the name *dot product* or *inner product*. Given our expression for the scalar product and the magnitude of vectors, we can introduce a geometrical interpretation by defining the angle between the vectors according to

$$\cos \vartheta \equiv \frac{\mathbf{P} \cdot \mathbf{Q}}{|\mathbf{P}| |\mathbf{Q}|} = \frac{P_a Q_a}{\sqrt{P_b P_b} \sqrt{Q_c Q_c}}. \quad (1.11)$$

We illustrate this equation in Figure 1.2. It is useful to convince oneself that this definition is consistent with  $-1 \leq \cos \vartheta \leq 1$ . Furthermore, note that this definition of an angle between two vectors makes use of the metric tensor, so that angles on a manifold, just as distance, require a metric.

## 1.4 Vector product

The scalar product provides a means to measure the magnitude of a vector and the distance between two points. We here introduce the vector (or cross) product, which provides a means to measure area associated with two vectors and to specify the orientation of that area.

### 1.4.1 Basis vector orientation and the Levi-Civita tensor

Consider a flat plane defined by any two of the Cartesian basis vectors,  $\vec{e}_a$  and  $\vec{e}_b$ . We seek a means to specify what side of the plane is up and what side is down. Doing so allows us to orient objects within space.<sup>4</sup> Notably, there is no objective means for this specification, since “up” and “down” are subject to our chosen orientation. Therefore, we must choose a convention. For that purpose, we follow the *right hand rule*, in which the out-stretched thumb, index, and middle fingers of the right hand orient the three Cartesian basis vectors.

We algebraically specify the right hand rule for the basis vectors through the relation

$$\vec{e}_a \times \vec{e}_b = \epsilon_{abc} \vec{e}_c. \quad (1.12)$$

The left hand side introduces the vector (or cross) product of two basis vectors. The right hand side algebraically defines the vector product as the *contraction* of the Levi-Civita tensor with another basis vector. Here, the term contraction can be considered a generalization of the

<sup>4</sup>There are surfaces, such as the Möbius strip, that are not orientable. We only consider orientable surfaces in this book.

inner product. The Cartesian components of the Levi-Civita tensor are given by the totally anti-symmetric permutation symbol or  $\epsilon$ -tensor

$$\epsilon_{123} = 1 \quad (1.13a)$$

$$\epsilon_{abc} = \begin{cases} 1, & \text{even permutation of } abc \text{ (123, 312, 231)} \\ -1, & \text{odd permutation of } abc \text{ (321, 132, 213)} \\ 0, & \text{all other } abc. \end{cases} \quad (1.13b)$$

Exchanging indices (an odd permutation) flips the sign of the permutation symbol

$$\epsilon_{abc} = -\epsilon_{bac} = -\epsilon_{acb}, \quad (1.14)$$

whereas cycling indices (an even permutation) preserves the sign

$$\epsilon_{abc} = \epsilon_{cab} = \epsilon_{bca}. \quad (1.15)$$

Correspondingly, we have

$$\vec{e}_a \times \vec{e}_b = \epsilon_{abc} \vec{e}_c = -\vec{e}_b \times \vec{e}_a. \quad (1.16)$$

## 1.4.2 Axial (or pseudo) vector

The vector cross product defines a vector whose properties are dependent on the orientation of the space. That is, the vector cross product changes its sign upon changing from a right handed to left handed orientation of the coordinate system. Such vectors are known as *axial vectors* or *pseudo vectors*. Example axial vectors that we encounter in this book include the angular velocity for the planet as well as the vorticity of a fluid.

## 1.4.3 Orthogonality relations between cross products

As defined, the permutation symbol ensures that  $\vec{e}_a \times \vec{e}_b$  is orthogonal to both  $\vec{e}_a$  and  $\vec{e}_b$

$$\vec{e}_a \cdot (\vec{e}_a \times \vec{e}_b) = \vec{e}_a \cdot \epsilon_{abc} \vec{e}_c \quad \text{definition} \quad (1.17a)$$

$$= \epsilon_{abc} \vec{e}_a \cdot \vec{e}_c \quad \text{rearrangement} \quad (1.17b)$$

$$= \epsilon_{cba} \vec{e}_c \cdot \vec{e}_a \quad \text{relabel } a \text{ to } c \text{ and } c \text{ to } a \quad (1.17c)$$

$$= -\epsilon_{abc} \vec{e}_c \cdot \vec{e}_a \quad \text{cba is an odd permutation of abc} \quad (1.17d)$$

$$\Rightarrow \vec{e}_a \cdot (\vec{e}_a \times \vec{e}_b) = 0. \quad (1.17e)$$

To fully digest step (1.17c) it can be useful to reintroduce the summation symbol so that

$$\epsilon_{abc} \vec{e}_a \cdot \vec{e}_c = \sum_{a=1}^3 \sum_{c=1}^3 \epsilon_{abc} \vec{e}_a \cdot \vec{e}_c \quad \text{summation symbols reintroduced} \quad (1.18a)$$

$$= \sum_{c=1}^3 \sum_{a=1}^3 \epsilon_{cba} \vec{e}_c \cdot \vec{e}_a \quad \text{swap } a \text{ and } c \quad (1.18b)$$

$$= \epsilon_{cba} \vec{e}_c \cdot \vec{e}_a \quad \text{reintroduce summation convention} \quad (1.18c)$$

Additionally, to digest step (1.17d) we step through the permutations

$$\epsilon_{cba} = -\epsilon_{bca} \quad \text{swap } c \text{ with } b \text{ to pick up a minus sign} \quad (1.19a)$$

$$= \epsilon_{bac} \quad \text{swap } c \text{ with } a \text{ to pick up a minus sign} \quad (1.19b)$$

$$= -\epsilon_{abc} \quad \text{swap } b \text{ with } a \text{ to pick up a minus sign.} \quad (1.19c)$$

The same procedure shows that  $\vec{e}_b \cdot (\vec{e}_a \times \vec{e}_b) = 0$ . Hence, the vector product is orthogonal to the plane specified by any two of the basis vectors. That is, the vector product points orthogonal to that plane and in a direction determined by the right hand rule. We note that this proof reveals a general property. Namely, the contraction of a symmetric tensor (e.g., the scalar product  $\vec{e}_c \cdot \vec{e}_a$ ) with an anti-symmetric tensor results in zero. We further illustrate this property in Exercise 1.2.

#### 1.4.4 Vector product of arbitrary vectors

The expression (1.12) for the vector product of two basis vectors renders the vector product of arbitrary vectors.

$$\mathbf{P} \times \mathbf{Q} = P_a \vec{e}_a \times Q_b \vec{e}_b \quad (1.20a)$$

$$= P_a Q_b \vec{e}_a \times \vec{e}_b \quad (1.20b)$$

$$= P_a Q_b \epsilon_{abc} \vec{e}_c \quad (1.20c)$$

$$= (P_2 Q_3 - P_3 Q_2) \vec{e}_1 + (P_3 Q_1 - P_1 Q_3) \vec{e}_2 + (P_1 Q_2 - P_2 Q_1) \vec{e}_3. \quad (1.20d)$$

We can write the vector product as a determinant

$$\mathbf{P} \times \mathbf{Q} = \det \begin{bmatrix} \vec{e}_1 & \vec{e}_2 & \vec{e}_3 \\ p_1 & p_2 & p_3 \\ q_1 & q_2 & q_3 \end{bmatrix}. \quad (1.21)$$

As with the basis vectors, the vector product is orthogonal to both of the individual vectors

$$\mathbf{P} \cdot (\mathbf{P} \times \mathbf{Q}) = (P_d \vec{e}_d) \cdot (P_a Q_b \epsilon_{abc} \vec{e}_c) \quad (1.22a)$$

$$= P_c P_a Q_b \epsilon_{abc} \quad (1.22b)$$

$$= 0, \quad (1.22c)$$

where the final equality follows since the product  $P_c P_a$  is symmetric on the labels  $ac$ , whereas  $\epsilon_{abc}$  is anti-symmetric.

#### 1.4.5 Geometric interpretation of the vector product

The expression (1.20d) leads to the identity

$$|\mathbf{P} \times \mathbf{Q}|^2 = |\mathbf{P}|^2 |\mathbf{Q}|^2 - (\mathbf{P} \cdot \mathbf{Q})^2 \quad (1.23a)$$

$$= |\mathbf{P}|^2 |\mathbf{Q}|^2 (1 - \cos^2 \vartheta), \quad (1.23b)$$

$$= |\mathbf{P}|^2 |\mathbf{Q}|^2 \sin^2 \vartheta, \quad (1.23c)$$

where we used the scalar product expression (1.11) to introduce the angle subtended by the two vectors. Trigonometry indicates that the area of the parallelogram defined by  $\mathbf{P}$  and  $\mathbf{Q}$  is given by  $|\mathbf{P}| |\mathbf{Q}| \sin \vartheta$ . Hence, the vector product has a magnitude given by this area

$$\text{area}(\mathbf{P}, \mathbf{Q}) = |\mathbf{P}| |\mathbf{Q}| \sin \vartheta = |\mathbf{P} \times \mathbf{Q}|. \quad (1.24)$$

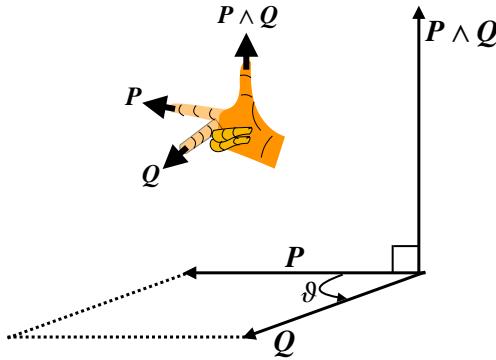


FIGURE 1.3: The magnitude of the vector product between two vectors is given by the product of their magnitudes and the sine of the angle between them,  $|P \times Q| = |P||Q|\sin\vartheta$ . This magnitude equals to the area of the parallelogram subtended by the two vectors. The vector product is directed perpendicular to the plane determined by the two vectors and oriented according to the right hand rule. We depict the right hand rule with the insert, whereby the index finger orients the first vector, the middle finger the second vector, and the thumb orients their vector product.

Since  $P \times Q$  is orthogonal to the plane defined by  $P$  and  $Q$ , we can write the vector product in the purely geometric manner

$$P \times Q = \hat{n} \text{area}(P, Q) = \hat{n} |P| |Q| \sin \vartheta, \quad (1.25)$$

where  $\hat{n}$  is a unit vector pointing normal to the area and in a direction given by the right hand rule. This formula is illustrated in Figure 1.3.

To further emphasize the geometric interpretation, let  $P$  equal to the vertical direction,  $P = \hat{z}$ . The vector cross product then defines a vector,

$$Q^{\hat{z}\perp} = \hat{z} \times Q \quad (1.26a)$$

$$= \hat{z} \times [Q - (\hat{z} \cdot Q) \hat{z}] \quad (1.26b)$$

$$(\hat{z} \times \hat{x})(\hat{x} \cdot Q) + (\hat{z} \times \hat{y})(\hat{y} \cdot Q) \quad (1.26c)$$

$$= \hat{y}(\hat{x} \cdot Q) - \hat{x}(\hat{y} \cdot Q). \quad (1.26d)$$

By construction,  $Q^{\hat{z}\perp}$  is in the horizontal plane and it is perpendicular to the horizontal projection of  $Q$

$$Q^{\hat{z}\perp} \cdot \hat{z} = 0 \quad \text{and} \quad Q^{\hat{z}\perp} \cdot Q = 0 \implies Q^{\hat{z}\perp} \cdot [Q - (\hat{z} \cdot Q) \hat{z}] = 0. \quad (1.27)$$

Hence, the vector  $Q^{\hat{z}\perp}$  is geometrically computed by rotating the horizontal component of  $Q$  by  $\pi/2$  radians counter-clockwise about the  $\hat{z}$  axis. That interpretation holds for all coordinate directions so that

$$\hat{x} \times Q = \hat{z}(\hat{y} \cdot Q) - \hat{y}(\hat{z} \cdot Q) = \text{project } Q \text{ to y-z plane} + \text{rotate CCW by } \pi/2 \text{ around } \hat{x}. \quad (1.28a)$$

$$\hat{y} \times Q = \hat{x}(\hat{z} \cdot Q) - \hat{z}(\hat{x} \cdot Q) = \text{project } Q \text{ to z-x plane} + \text{rotate CCW by } \pi/2 \text{ around } \hat{y}. \quad (1.28b)$$

$$\hat{z} \times Q = \hat{y}(\hat{x} \cdot Q) - \hat{x}(\hat{y} \cdot Q) = \text{project } Q \text{ to x-y plane} + \text{rotate CCW by } \pi/2 \text{ around } \hat{z}. \quad (1.28c)$$

### 1.4.6 Generalization to arbitrary vectors

Thus far the discussion has considered vectors to represent the position of a point in space. As such, the vectors have the physical dimensions of length and area ( $\mathbf{P}, \mathbf{Q}$ ) has dimensions of area. However, the vector analysis is general, so that the above notions extend to vectors of arbitrary physical dimensions, such as velocity. In these more general cases the physical dimensions must be adjusted accordingly.

## 1.5 Measuring volume

The vector product offers a means to measure area defined by two vectors. We now extend that result to measure the volume determined by three non-parallel vectors. This result has particular relevance to the volume element used for integration over space.

### 1.5.1 Volume defined by three vectors

Consider the scalar product of an arbitrary vector with the vector product,  $(\mathbf{P} \times \mathbf{Q}) \cdot \mathbf{R}$ . This scalar product projects that portion of the vector  $\mathbf{R}$  onto the direction parallel to the normal to the plane defined by  $\mathbf{P} \times \mathbf{Q}$ . Given that  $|(\mathbf{P} \times \mathbf{Q})|$  is the area of the parallelogram defined by  $\mathbf{P}$  and  $\mathbf{Q}$ , we conclude that  $(\mathbf{P} \times \mathbf{Q}) \cdot \mathbf{R}$  is the volume of the parallelepiped defined by the three vectors. However, note that this volume is not positive definite since the sign depends on the relative orientation of  $\mathbf{P} \times \mathbf{Q}$  and  $\mathbf{R}$ . So more precisely, we need to apply an absolute value around the triple product to get the volume.

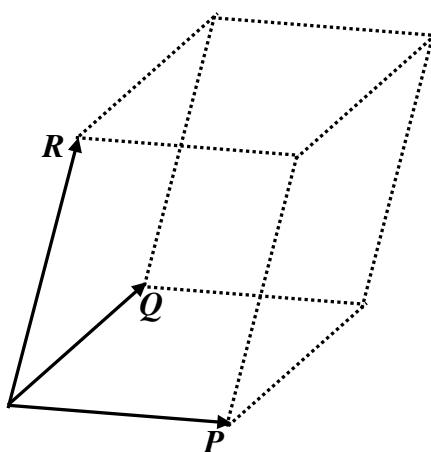


FIGURE 1.4: Three linearly independent position vectors determine a volume given by  $|(\mathbf{P} \times \mathbf{Q}) \cdot \mathbf{R}| = |(\mathbf{R} \times \mathbf{P}) \cdot \mathbf{Q}| = |(\mathbf{Q} \times \mathbf{R}) \cdot \mathbf{P}|$

We can prove cyclic symmetry of  $(\mathbf{P} \times \mathbf{Q}) \cdot \mathbf{R}$  through the following manipulations

$$(\mathbf{P} \times \mathbf{Q}) \cdot \mathbf{R} = (P_a \vec{e}_a \times Q_b \vec{e}_b) \cdot R_d \vec{e}_d \quad (1.29a)$$

$$= P_a Q_b (\vec{e}_a \times \vec{e}_b) \cdot R_d \vec{e}_d \quad (1.29b)$$

$$= P_a Q_b (\epsilon_{abc} \vec{e}_c) \cdot \vec{e}_d R_d \quad (1.29c)$$

$$= P_a Q_b \epsilon_{abc} (\vec{e}_c \cdot \vec{e}_d) R_d \quad (1.29d)$$

$$= P_a Q_b \epsilon_{abc} \delta_{cd} R_d \quad (1.29e)$$

$$= P_a Q_b \epsilon_{abc} R_c \quad (1.29f)$$

$$= R_c P_a Q_b \epsilon_{abc} \quad (1.29g)$$

$$= R_a P_b Q_c \epsilon_{bca} \quad (1.29h)$$

$$= R_a P_b Q_c \epsilon_{abc} \quad (1.29i)$$

$$= (\mathbf{R} \times \mathbf{P}) \cdot \mathbf{Q}. \quad (1.29j)$$

This identity yields the geometric result illustrated in Figure 1.4

$$\text{volume}(\mathbf{P}, \mathbf{Q}, \mathbf{R}) = |(\mathbf{P} \times \mathbf{Q}) \cdot \mathbf{R}| = |(\mathbf{R} \times \mathbf{P}) \cdot \mathbf{Q}| = |(\mathbf{Q} \times \mathbf{R}) \cdot \mathbf{P}|. \quad (1.30)$$

### 1.5.2 Cartesian volume element for integration

We need the volume of an infinitesimal region when performing an integration over space. When making use of Cartesian coordinates we need the volume of a rectangular prism defined by infinitesimal distances along each of the axes. We thus set

$$\mathbf{P} = \hat{\mathbf{x}} dx \quad \text{and} \quad \mathbf{Q} = \hat{\mathbf{y}} dy \quad \text{and} \quad \mathbf{R} = \hat{\mathbf{z}} dz, \quad (1.31)$$

in which case the volume element is

$$dV = (\mathbf{P} \times \mathbf{Q}) \cdot \mathbf{R} = dx dy dz (\hat{\mathbf{x}} \times \hat{\mathbf{y}}) \cdot \hat{\mathbf{z}} = dx dy dz. \quad (1.32)$$

This expression for the volume element could have been written down without the formalism of a vector triple product. However, in Chapter 6 we find the general relation  $(\mathbf{P} \times \mathbf{Q}) \cdot \mathbf{R}$  provides a useful starting point for deriving the volume element with arbitrary coordinates.

### 1.5.3 $n$ -space volumes and the Levi-Civita tensor

We combine the geometric specification of the vector product as a means to measure area, (1.25), with the algebraic specification (1.20d) by writing

$$\text{2-volume} = \epsilon(\mathbf{P}, \mathbf{Q}) = \epsilon_{ab} P_a Q_b = \det \begin{bmatrix} P_1 & Q_1 \\ P_2 & Q_2 \end{bmatrix}. \quad (1.33)$$

In this equation,  $\epsilon_{ab}$  is the totally anti-symmetric  $2 \times 2$  tensor. It has Cartesian components that can be organized as a matrix according to

$$\begin{bmatrix} \epsilon_{11} & \epsilon_{12} \\ \epsilon_{21} & \epsilon_{22} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}. \quad (1.34)$$

In words, the first equality in equation (1.33) states that the  $\epsilon$ -tensor in two dimensions takes two vectors as its argument and produces a 2-volume (i.e., an area). The three dimensional

generalization yields

$$3\text{-volume} = \epsilon(\mathbf{P}, \mathbf{Q}, \mathbf{R}) = \epsilon_{abc} P_a Q_b R_c = \det \begin{bmatrix} P_1 & Q_1 & R_1 \\ P_2 & Q_2 & R_2 \\ P_3 & Q_3 & R_3 \end{bmatrix}. \quad (1.35)$$

Suppressing the first vector argument in the 3-volume produces a vectorial surface area defined by the other two vectors

$$\text{surface area} = \epsilon( \mathbf{\cdot}, \mathbf{Q}, \mathbf{R}). \quad (1.36)$$

By construction, the vectorial surface area is orthogonal to both  $\mathbf{Q}$  and  $\mathbf{R}$ .

## 1.6 Example vector identities using the Levi-Civita tensor

The Levi-Civita tensor is a versatile tool for deriving vector identities. We illustrated some of these features in the previous discussion and here illustrate two more. These examples, and others in this chapter, generally expose many of the *index gymnastics* involved with tensor manipulations. A bit of practice and confidence readily allows one to suppress many of these steps.

### 1.6.1 Double vector product

Consider the double vector product

$$\mathbf{P} \times (\mathbf{Q} \times \mathbf{R}) = P_a Q_b R_c \vec{e}_a \times (\vec{e}_b \times \vec{e}_c) \quad (1.37a)$$

$$= P_a Q_b R_c \vec{e}_a \times (\epsilon_{bcd} \vec{e}_d) \quad (1.37b)$$

$$= P_a Q_b R_c \epsilon_{bcd} \epsilon_{ade} \vec{e}_e \quad (1.37c)$$

$$= -P_a Q_b R_c \epsilon_{bcd} \epsilon_{aed} \vec{e}_e. \quad (1.37d)$$

Explicit substitution verifies that the product  $\epsilon_{bcd} \epsilon_{aed}$  equals to

$$\epsilon_{bcd} \epsilon_{aed} = \delta_{ba} \delta_{ce} - \delta_{be} \delta_{ca}. \quad (1.38)$$

This identity then leads to

$$\epsilon_{bcd} \epsilon_{aed} \vec{e}_e = \delta_{ba} \vec{e}_c - \delta_{ca} \vec{e}_b \quad (1.39)$$

so that

$$\mathbf{P} \times (\mathbf{Q} \times \mathbf{R}) = -P_a Q_b R_c (\delta_{ba} \vec{e}_c - \delta_{ca} \vec{e}_b) \quad (1.40a)$$

$$= -(\mathbf{P} \cdot \mathbf{Q}) \mathbf{R} + (\mathbf{P} \cdot \mathbf{R}) \mathbf{Q}. \quad (1.40b)$$

### 1.6.2 Scalar product of two vector products

We make further use of the Levi-Civita identity (1.38) to write

$$(\mathbf{P} \times \mathbf{Q}) \cdot (\mathbf{R} \times \mathbf{S}) = (\epsilon_{abc} p_a q_b) (\epsilon_{dec} R_d s_e) \quad (1.41a)$$

$$= p_a q_b R_d s_e \epsilon_{abc} \epsilon_{dec} \quad (1.41b)$$

$$= p_a q_b R_d s_e (\delta_{ad} \delta_{be} - \delta_{ae} \delta_{bd}) \quad (1.41c)$$

$$= (\mathbf{P} \cdot \mathbf{R}) (\mathbf{Q} \cdot \mathbf{S}) - (\mathbf{P} \cdot \mathbf{S}) (\mathbf{Q} \cdot \mathbf{R}). \quad (1.41d)$$

## 1.7 Transforming the coordinate representations

The Cartesian basis vectors are mutually orthogonal and fixed in space. However, the orientation of the basis vectors is arbitrary. We thus consider an alternative specification to the basis vectors by performing a linear transformation

$$\vec{e}_{\bar{a}} = \mathcal{R}_{\bar{a}b} \vec{e}_b. \quad (1.42)$$

This expression introduced components to the transformation matrix moving between the unbarred and the barred Cartesian coordinates

$$\mathcal{R}_{\bar{a}b} = \begin{bmatrix} \mathcal{R}_{\bar{1}1} & \mathcal{R}_{\bar{1}2} & \mathcal{R}_{\bar{1}3} \\ \mathcal{R}_{\bar{2}1} & \mathcal{R}_{\bar{2}2} & \mathcal{R}_{\bar{2}3} \\ \mathcal{R}_{\bar{3}1} & \mathcal{R}_{\bar{3}2} & \mathcal{R}_{\bar{3}3} \end{bmatrix}. \quad (1.43)$$

In Cartesian tensor analysis studied in this chapter, the transformation matrix is assumed to be independent of space.<sup>5</sup> Although the transformation matrix carries two indices, it is not a tensor. Instead, it is a matrix operator used to transform from one set of basis vectors to another. We now deduce some constraints on this transformation matrix.

### 1.7.1 Inverse transformation

Assuming the transformation is invertible leads to the inverse transformation

$$\vec{e}_a = (\mathcal{R}^{-1})_{a\bar{b}} \vec{e}_{\bar{b}}. \quad (1.44)$$

As a self-consistency check we combine this relation with equation (1.42) thus rendering

$$\vec{e}_a = (\mathcal{R}^{-1})_{a\bar{b}} \vec{e}_{\bar{b}} = (\mathcal{R})_{a\bar{b}}^{-1} (\mathcal{R}_{\bar{b}c} \vec{e}_c). \quad (1.45)$$

This relation holds since

$$(\mathcal{R}^{-1})_{a\bar{b}} \mathcal{R}_{\bar{b}c} = \delta_{ac}, \quad (1.46)$$

or as a matrix identity

$$\mathcal{R}^{-1} \mathcal{R} = I. \quad (1.47)$$

### 1.7.2 Orthogonal transformation

We now assume that the two sets of Cartesian basis vectors are orthonormal. That assumption leads to the following constraint on the transformation matrix

$$\delta_{\bar{a}\bar{b}} = \vec{e}_{\bar{a}} \cdot \vec{e}_{\bar{b}} \quad (1.48a)$$

$$= \mathcal{R}_{\bar{a}a} \vec{e}_a \cdot \mathcal{R}_{\bar{b}b} \vec{e}_b \quad (1.48b)$$

$$= \mathcal{R}_{\bar{a}a} \mathcal{R}_{\bar{b}b} \vec{e}_a \cdot \vec{e}_b \quad (1.48c)$$

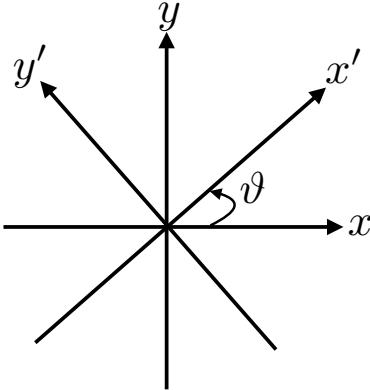
$$= \mathcal{R}_{\bar{a}a} \mathcal{R}_{\bar{b}b} \delta_{ab} \quad (1.48d)$$

$$= \mathcal{R}_{\bar{a}a} \mathcal{R}_{\bar{b}a} \quad (1.48e)$$

$$= \mathcal{R}_{\bar{a}a} (\mathcal{R}^T)_{a\bar{b}}, \quad (1.48f)$$

---

<sup>5</sup>The transformation matrix is a function of space and time for the general tensors considered in Chapter 7.

FIGURE 1.5: Counter-clockwise rotation of horizontal Cartesian axes through an angle  $\vartheta$ .

where  $\mathcal{R}^T$  is the matrix transpose with components

$$(\mathcal{R}^T)_{\bar{a}\bar{b}} = \mathcal{R}_{\bar{b}a}. \quad (1.49)$$

Written as a matrix equation we see that

$$\mathcal{R} \mathcal{R}^T = I. \quad (1.50)$$

This relation defines an *orthogonal transformation*, whereby the inverse matrix equals to the matrix transpose

$$\mathcal{R}^{-1} = \mathcal{R}^T. \quad (1.51)$$

### 1.7.3 Geometric interpretation of orthogonal transformations

Orthogonal transformations convert one set of Cartesian coordinates to another. Geometrically, an orthogonal transformation corresponds to a rotation, with Figure 1.5 illustrating this axis rotation in two dimensions. For this two dimensional example, the rotation matrix can be written in terms of the cosine of the angles between the unit vectors; i.e., the *direction cosines*

$$\mathcal{R}_{\bar{a}a} = \begin{bmatrix} \cos \vartheta & \sin \vartheta \\ -\sin \vartheta & \cos \vartheta \end{bmatrix} = \begin{bmatrix} \cos \vartheta & \cos(\pi/2 - \vartheta) \\ \cos(\pi/2 + \vartheta) & \cos \vartheta \end{bmatrix} = \begin{bmatrix} \vec{e}_1 \cdot \vec{e}_1 & \vec{e}_1 \cdot \vec{e}_2 \\ \vec{e}_2 \cdot \vec{e}_1 & \vec{e}_2 \cdot \vec{e}_2 \end{bmatrix}. \quad (1.52)$$

The final form of the rotation matrix reveals that it is built from the projection of the rotated basis vectors onto the original basis vectors. This result holds for rotations in three dimensions as well, thus leading to

$$\mathcal{R}_{\bar{a}a} = \begin{bmatrix} \vec{e}_1 \cdot \vec{e}_1 & \vec{e}_1 \cdot \vec{e}_2 & \vec{e}_1 \cdot \vec{e}_3 \\ \vec{e}_2 \cdot \vec{e}_1 & \vec{e}_2 \cdot \vec{e}_2 & \vec{e}_2 \cdot \vec{e}_3 \\ \vec{e}_3 \cdot \vec{e}_1 & \vec{e}_3 \cdot \vec{e}_2 & \vec{e}_3 \cdot \vec{e}_3 \end{bmatrix}. \quad (1.53)$$

With the basis vectors all normalized, elements of the rotation matrix have magnitude less than or equal to unity and are given by the cosine of the angle between the respective basis vectors. As such, one sometimes refers to this rotation matrix as being comprised of *direction cosines*.

### 1.7.4 Transforming the coordinate representation of a vector

We introduced the transformation (1.44) according to how it acts on the basis vectors. Now consider how it acts on the coordinate representation of an arbitrary vector by moving brackets

$$\mathbf{P} = P_a \vec{e}_a \quad (1.54a)$$

$$= P_a (\mathcal{R}^T)_{a\bar{a}} \vec{e}_{\bar{a}} \quad (1.54b)$$

$$\equiv P_{\bar{a}} \vec{e}_{\bar{a}}, \quad (1.54c)$$

where we defined the transformation of the vector components

$$P_{\bar{a}} = P_a (\mathcal{R}^T)_{a\bar{a}} = \mathcal{R}_{\bar{a}a} P_a. \quad (1.55)$$

### 1.7.5 Invariance of the scalar product

The above properties of an orthogonal transformation ensure that the scalar product

$$\mathbf{P} \cdot \mathbf{Q} = P_a Q_a \quad (1.56)$$

is the same regardless the choice of Cartesian coordinates

$$\mathbf{P} \cdot \mathbf{Q} = P_a Q_a \quad (1.57a)$$

$$= P_a \vec{e}_a \cdot Q_b \vec{e}_b \quad (1.57b)$$

$$= P_a (\mathcal{R}^T)_{a\bar{a}} Q_b (\mathcal{R}^T)_{\bar{b}\bar{b}} (\vec{e}_{\bar{a}} \cdot \vec{e}_{\bar{b}}) \quad (1.57c)$$

$$= P_a (\mathcal{R}^T)_{a\bar{a}} Q_b (\mathcal{R}^T)_{\bar{b}\bar{b}} \delta_{\bar{a}\bar{b}} \quad (1.57d)$$

$$= P_a (\mathcal{R}^T)_{a\bar{a}} Q_b (\mathcal{R}^T)_{b\bar{a}} \quad (1.57e)$$

$$= P_{\bar{a}} Q_{\bar{a}}. \quad (1.57f)$$

### 1.7.6 Transforming the coordinate representation of a second order tensor

The stress tensor in Chapter 17; the moment of inertia tensor in Section 32.7.4; and the diffusion tensor in Chapter 46 are examples of second order tensors. Second order tensors have a coordinate representation given by

$$\mathcal{T} = T_{ab} \vec{e}_a \otimes \vec{e}_b, \quad (1.58)$$

with  $T_{ab}$  the Cartesian coordinates that can be organized as a matrix. Notably, there is not a scalar product between the basis vectors in equation (1.58). Instead, the  $\otimes$  symbol represents the *outer product* of the two basis vectors. For our purposes the outer product simply provides a formal means for two vectors to be positioned next to one another. For many purposes we drop the  $\otimes$  symbol for brevity.

We determine how the Cartesian coordinate components  $T_{ab}$  transform by following the now familiar procedure for transforming the basis vectors. The key new facet is that now we have two basis vectors to carry around

$$\mathcal{T} = T_{ab} \vec{e}_a \vec{e}_b \quad (1.59a)$$

$$= T_{ab} (\mathcal{R}^T)_{a\bar{a}} \vec{e}_{\bar{a}} (\mathcal{R}^T)_{\bar{b}\bar{b}} \vec{e}_{\bar{b}} \quad (1.59b)$$

$$= T_{ab} (\mathcal{R}^T)_{a\bar{a}} (\mathcal{R}^T)_{\bar{b}\bar{b}} \vec{e}_{\bar{a}} \vec{e}_{\bar{b}} \quad (1.59c)$$

$$\equiv T_{\bar{a}\bar{b}} \vec{e}_{\bar{a}} \vec{e}_{\bar{b}}. \quad (1.59d)$$

The final equality introduced the transformed tensor components

$$T_{\bar{a}\bar{b}} = T_{ab} (\mathcal{R}^T)_{a\bar{a}} (\mathcal{R}^T)_{b\bar{b}} = T_{ab} \mathcal{R}_{\bar{a}a} \mathcal{R}_{\bar{b}b}. \quad (1.60)$$

The transformation of the components to higher order tensors follows analogously.

### 1.7.7 Importance of distinguishing between tensors and matrices

A matrix is an ordered array of objects. Hence, matrices are useful for organizing the coordinate components to a tensor. For example, the coordinate components to a first-order tensor (a vector) can be organized into a row or column matrix. Likewise, the coordinate components to a second-order tensor can be organized into a matrix. Consequently, the algebra of Cartesian tensors shares much with that of matrices familiar from linear algebra. However, tensors are not equivalent to matrices. The key distinction concerns how the components to tensors transform under changes to coordinates.

Namely, tensor components transform in a precise manner when modifying coordinates. In contrast, elements of an arbitrary matrix may or may not transform, with details depending on what the matrix elements represent. One means to help maintain focus on the distinction is to recall that a tensor is a geometric object (Section 1.1) that can be represented using arbitrary coordinates. Since the tensor has an existence independent of coordinates, its coordinate components are constrained to transform in a precise manner under changes to the coordinates. In particular, the Cartesian tensors of this chapter transform only via rotations.

## 1.8 Homogeneity and isotropy

We have many occasions to consider basic symmetry properties of tensor fields, with homogeneity and isotropy two rather basic symmetry properties.

### 1.8.1 Homogeneous tensor

A tensor field is *homogeneous* if it possesses the same value at each point in space. For example, a uniform temperature field is homogeneous, as is a uniform velocity field. As defined, a homogeneous tensor field has no spatial dependence and thus it does not provide any means to distinguish points in space. Likewise, a time independent tensor is said to be homogeneous in time.

### 1.8.2 Isotropic and anisotropic tensors

A tensor field is *isotropic* if its representation remains independent of coordinate basis. A scalar tensor is, by definition, isotropic since it has no information about spatial directions. A nonzero vector field cannot be isotropic since it points in a particular direction and so its representation is dependent on the orientation of the basis vectors.

A second order isotropic tensor,  $I$ , satisfies

$$I_{\bar{a}\bar{b}} = I_{ab} \mathcal{R}_{\bar{a}a} \mathcal{R}_{\bar{b}b} \equiv I_{ab} \quad (1.61)$$

where we used the identity (1.60) for the component transformation. For nonzero tensors, this equation is satisfied by

$$I_{ab} = \lambda \delta_{ab}, \quad (1.62)$$

with  $\lambda$  an arbitrary scalar and  $\delta_{ab}$  the Kronecker tensor (1.8), which is the identity tensor. Hence, the most general second order isotropic tensor is proportional to the identity tensor. We often

find it useful to decompose an arbitrary second order tensor into its anisotropic and isotropic components according to

$$T_{ab} = T_{ab} - \underbrace{\frac{T_{pp}}{\delta_{pp}} \delta_{ab}}_{\text{anisotropic}} + \underbrace{\frac{T_{pp}}{\delta_{pp}} \delta_{ab}}_{\text{isotropic}}, \quad (1.63)$$

where

$$T_{pp} = \sum_{p=1}^N T_{pp} = \text{trace of } T_{ab} \quad \text{and} \quad \delta_{pp} = \sum_{p=1}^N \delta_{pp} = N \quad (1.64)$$

with  $N$  the number of space dimensions.



## 1.9 Exercises

### EXERCISE 1.1: PRODUCT OF SYMMETRIC MATRICES

Let  $A = A^T$  and  $B = B^T$  be two symmetric matrices. Under what condition is their product also symmetric:  $A B = (A B)^T$ ?

### EXERCISE 1.2: PRODUCT OF SYMMETRIC AND ANTI-SYMMETRIC TENSORS

Let  $A = -A^T$  be an anti-symmetric matrix, and  $S = S^T$  be a symmetric matrix. Show that the trace of their product vanishes:  $\text{Tr}(A S) = 0$ . Alternatively, in terms of tensors, show that the full contraction of an anti-symmetric tensor with a symmetric tensor vanishes:  $A_{mn} S_{mn} = 0$ .

### EXERCISE 1.3: PROJECTION OPERATOR

Consider an arbitrary direction in space specified by the unit vector  $\hat{n}$  with components  $\hat{n}_a$ . Define the projection operator

$$P_{ab} = \delta_{ab} - \hat{n}_a \hat{n}_b, \quad (1.65)$$

and show that

$$P_{ab} T_{bc} \hat{n}_a = 0. \quad (1.66)$$

Hence,  $S_{ac} = P_{ab} T_{bc}$  is the projection of  $T$  onto the plane perpendicular to the direction  $\hat{n}$ .



# Chapter 2

## Cartesian tensor calculus

This chapter presents differential and integral calculus for our study of fluid mechanics. We build from the Cartesian tensor algebra of Chapter 1 to develop elements of Cartesian tensor calculus, which is the basis for vector calculus. The material is extensively used throughout this book.

### CHAPTER GUIDE

For further study consult any book on calculus with analytic geometry. Particularly effective treatments, with applications to physics, are given in the following resources.

- FEYNMAN LECTURES: Chapters 2 and 3 in Volume II of the [Feynman Lectures](#) offers insightful discussions of vector differential calculus. Although written for students of electrodynamics, many of the examples are drawn from fluid mechanics.
- DIV, GRAD, CURL AND ALL THAT ([Schey, 2004](#)): This text pedagogically presents the methods and theorems of vector calculus in a manner that greatly assists the development of intuition.
- Chapter 2 in [Segel \(1987\)](#) provides a lucid review of vector calculus using Cartesian tensors.
- THEORY AND PROBLEMS OF VECTOR ANALYSIS ([Spiegel, 1974](#)): This “Schaum’s Outline Series” book has nearly 500 worked exercises. Hence, it is a particularly useful resource for those wishing a refresher on problem solving in vector calculus. Some of the exercises here in Section 2.10 are drawn from this book.
- [This video from 3Blue1Brown](#) provides some compelling graphics to help develop intuition for the divergence and curl operators encountered in fluid mechanics.

2.1	The gradient of a scalar field . . . . .	22
2.1.1	Direction of steepest ascent . . . . .	23
2.1.2	Tangent to an isosurface . . . . .	23
2.1.3	Normal to an isosurface . . . . .	24
2.1.4	Unit vectors change only by rotation . . . . .	24
2.1.5	Showing that $\delta\hat{\mathbf{n}} \cdot \hat{\mathbf{n}} = 0$ . . . . .	25
2.2	The divergence of a vector field . . . . .	25
2.2.1	Divergence of a scalar field times a vector field . . . . .	26

2.2.2	Laplacian of a scalar field . . . . .	26
2.3	The curl of a vector field . . . . .	<b>26</b>
2.3.1	Computing the curl . . . . .	26
2.3.2	Curl-free vector fields . . . . .	27
2.3.3	Curl-free and divergence-free fields . . . . .	28
2.3.4	Identities involving the curl . . . . .	29
2.4	Path integral of a scalar function . . . . .	<b>31</b>
2.5	Path integral of a vector function . . . . .	<b>32</b>
2.5.1	Circulation . . . . .	32
2.5.2	Circulation example . . . . .	32
2.5.3	Fundamental theorem of calculus . . . . .	33
2.6	Stokes' theorem . . . . .	<b>33</b>
2.6.1	Statement of Stokes' theorem . . . . .	33
2.6.2	Stokes' theorem for a rectangular region . . . . .	34
2.7	Gauss's divergence theorem . . . . .	<b>34</b>
2.7.1	An example rectangular volume . . . . .	35
2.7.2	Divergence theorem for scalar fields . . . . .	35
2.7.3	Surface integral of the outward normal . . . . .	36
2.7.4	First and second form of Green's identities . . . . .	36
2.7.5	Integral of a curl over a closed surface . . . . .	36
2.7.6	The domain integral of a non-divergent field . . . . .	37
2.8	Exact and inexact differentials . . . . .	<b>38</b>
2.8.1	Exact differentials . . . . .	38
2.8.2	Inexact differentials . . . . .	38
2.8.3	Integrating factors . . . . .	39
2.8.4	An example using the velocity field . . . . .	39
2.8.5	Heuristic physics of exact and inexact differential operations . . . . .	39
2.9	Helmholtz decomposition . . . . .	<b>40</b>
2.10	Exercises . . . . .	<b>40</b>

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## 2.1 The gradient of a scalar field

Consider a scalar field  $\psi(\mathbf{x})$  defined on Euclidean space with position

$$\mathbf{x} = \sum_{a=1}^3 x_a \vec{e}_a = x_a \vec{e}_a, \quad (2.1)$$

where the second equation made use of the Einstein summation convention used throughout this book. For example, the scalar field,  $\psi$ , can be the temperature, the mass density, or the specific entropy. We may estimate its value at an adjacent spacial point  $\mathbf{x} + d\mathbf{x}$  through a Taylor series

$$\psi(\mathbf{x} + d\mathbf{x}) = \psi(\mathbf{x}) + \frac{\partial \psi}{\partial x_1} dx_1 + \frac{\partial \psi}{\partial x_2} dx_2 + \frac{\partial \psi}{\partial x_3} dx_3 + \mathcal{O}(d\mathbf{x} \cdot d\mathbf{x}) \quad (2.2a)$$

$$\approx [1 + dx_a \partial_a] \psi(\mathbf{x}), \quad (2.2b)$$

where we dropped higher order terms to reach the final approximate expression, and introduced the shorthand notation for the partial derivative operator

$$\partial_a = \frac{\partial}{\partial x_a}. \quad (2.3)$$

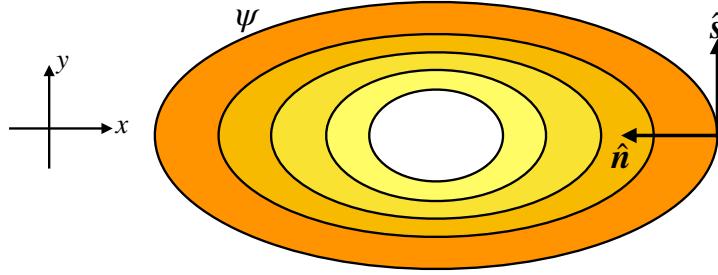


FIGURE 2.1: Contours of a scalar field  $\psi(x, y)$ , with values increasing toward the center. At any point in space,  $\nabla\psi$  points in the direction of steepest increase (ascent) and orients the normal vector  $\hat{n} = |\nabla\psi|^{-1} \nabla\psi$ . The unit tangent vector,  $\hat{s}$ , points in a direction tangent to a  $\psi$  isosurface so that it follows the surface of constant  $\psi$  and it is orthogonal to the direction of steepest ascent:  $\hat{n} \cdot \hat{s} = 0$ .

We can introduce the gradient operator according to

$$\nabla = \vec{e}_a \partial_a = \hat{x} \partial_x + \hat{y} \partial_y + \hat{z} \partial_z \quad (2.4)$$

in which case

$$\psi(\mathbf{x} + d\mathbf{x}) \approx (1 + d\mathbf{x} \cdot \nabla) \psi(\mathbf{x}). \quad (2.5)$$

Note that in some treatments,  $\nabla$  is referred to as *Hamilton's operator*.

### 2.1.1 Direction of steepest ascent

Using the approximate relation (2.5), and the geometric expression (1.11) for the scalar product, renders

$$\psi(\mathbf{x} + d\mathbf{x}) - \psi(\mathbf{x}) \approx |d\mathbf{x}| |\nabla\psi| \cos \vartheta, \quad (2.6)$$

where  $\vartheta$  is the angle between the differential increment  $d\mathbf{x}$  and the gradient  $\nabla\psi$ . Orienting the increment  $d\mathbf{x}$  so that  $\vartheta = 0$  ensures that  $\psi(\mathbf{x} + d\mathbf{x}) - \psi(\mathbf{x})$  is maximal. Consequently,  $\nabla\psi$  points in the direction of *steepest ascent* across constant  $\psi$  isosurfaces (Figure 2.1). The opposite direction is that of *steepest descent*, where  $\vartheta = \pi$ .

### 2.1.2 Tangent to an isosurface

Consider a family of isosurfaces defined by points satisfying

$$\psi(\mathbf{x}) = \text{constant} \quad (2.7)$$

Figure 2.1 shows a two dimensional example where the isosurfaces are lines where  $\psi$  is a constant. As another example, consider  $\psi(\mathbf{x}) = \psi(r)$ , where  $r^2 = \mathbf{x} \cdot \mathbf{x}$  is the squared radius of a sphere. Isosurfaces for this spherically symmetric function are spherical shells of radius  $r$ .

In general, moving along an isosurface keeps the scalar field unchanged. Let  $\hat{s}$  be a unit vector that points in the direction tangent to the isosurface at any point  $\mathbf{x}$ . By construction

$$\psi(\mathbf{x} + \hat{s} ds) - \psi(\mathbf{x}) = 0, \quad (2.8)$$

where  $ds$  is an infinitesimal increment. In words, this identity says that if we move an infinitesimal distance in the direction tangent to the isosurface, then the function  $\psi$  does not change its value. Now expanding this identity in a Taylor series leads to the vanishing of the tangential partial

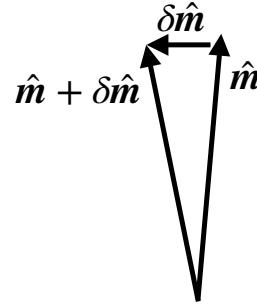


FIGURE 2.2: The infinitesimal change to a unit vector is itself perpendicular to the unit vector:  $\delta\hat{m} \cdot \hat{m} = 0$ . The reason is that the unit vector is constrained to remain unit length, so that the only way that it can change is to change its direction.

derivative

$$\hat{s} \cdot \nabla \psi = \frac{\partial \psi}{\partial s} = 0. \quad (2.9)$$

That is, isosurfaces of a function  $\psi$  are defined by directions along which the partial derivative of the function vanishes. For the spherically symmetric function,  $\psi(\mathbf{x}) = \psi(r)$ , the tangent vector points in either of the two angular directions along the spherical surface.

### 2.1.3 Normal to an isosurface

We may normalize the direction of maximal ascent, in which case we define the normal direction

$$\hat{n} = |\nabla \psi|^{-1} \nabla \psi. \quad (2.10)$$

By construction, the gradient computed in the  $\hat{n}$  direction yields the maximum change for the function so that the *normal derivative* is given by

$$\hat{n} \cdot \nabla \psi = \frac{\partial \psi}{\partial n} = |\nabla \psi|. \quad (2.11)$$

For the spherically symmetric example,

$$\hat{n} = \frac{\mathbf{x}}{|\mathbf{x}|} = \hat{r}, \quad (2.12)$$

where  $\hat{r}$  is the unit vector pointing radially outward from the origin. In this case the normal derivative is equal to the radial derivative

$$\hat{n} \cdot \nabla \psi = \frac{\partial \psi}{\partial r} \quad \text{spherically symmetric } \psi. \quad (2.13)$$

### 2.1.4 Unit vectors change only by rotation

Consider an arbitrary unit vector,  $\hat{m}$ . The defining feature of a unit vector is that it has unit magnitude

$$\hat{m} \cdot \hat{m} = 1. \quad (2.14)$$

Unit vectors can only be modified through changes in their direction since their magnitude is fixed at unity. Hence, they are only modified by rotations. An important consequence of this constraint is that the infinitesimal change to a unit vector is perpendicular to unit vector itself (see Figure 2.2). We see this property through considering an arbitrary infinitesimal change, symbolized by

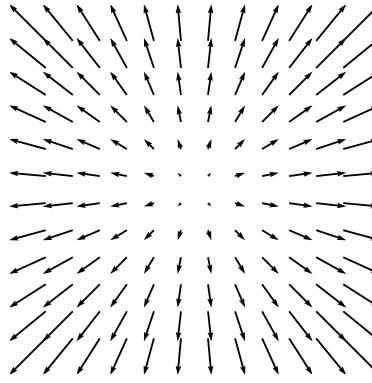


FIGURE 2.3: A vector field with a non-zero horizontal divergence. With  $\mathbf{F} = x\hat{\mathbf{x}} + y\hat{\mathbf{y}}$  the field diverges at each point with a spatially constant divergence  $\nabla \cdot \mathbf{F} = 2$ . Note that this vector field has zero curl,  $\nabla \times \mathbf{F} = 0$ .

$\delta$ , in which

$$0 = \delta(1) = \delta(\hat{\mathbf{m}} \cdot \hat{\mathbf{m}}) = 2\hat{\mathbf{m}} \cdot \delta\hat{\mathbf{m}}. \quad (2.15)$$

In Section 9.4, we formally show that the constraint

$$\delta\hat{\mathbf{m}} \cdot \hat{\mathbf{m}} = 0 \quad (2.16)$$

means that unit vector changes can only arise from rotations. Even so, the above assertion should make intuitive sense.

### 2.1.5 Showing that $\delta\hat{\mathbf{n}} \cdot \hat{\mathbf{n}} = 0$

As an illustration of the constraint (2.16), let us verify that it holds for the special case of a unit normal vector (2.10) defined according to surfaces of constant scalar field

$$\hat{\mathbf{n}} = |\nabla\psi|^{-1} \nabla\psi. \quad (2.17)$$

The proof follows first by writing

$$\delta\hat{\mathbf{n}} = |\nabla\psi|^{-1} [\delta(\nabla\psi) - \hat{\mathbf{n}} \delta|\nabla\psi|], \quad (2.18)$$

so that

$$|\nabla\psi| \hat{\mathbf{n}} \cdot \delta\hat{\mathbf{n}} = \hat{\mathbf{n}} \cdot \delta(\nabla\psi) - \delta|\nabla\psi| = \frac{\nabla\psi \cdot \delta(\nabla\psi)}{|\nabla\psi|} - \delta|\nabla\psi| = 0. \quad (2.19)$$

The last equality made use of the identity

$$\delta(|\nabla\psi|) = \delta(\sqrt{\nabla\psi \cdot \nabla\psi}) = \frac{1}{2\sqrt{\nabla\psi \cdot \nabla\psi}} \delta(\nabla\psi \cdot \nabla\psi) = \frac{\nabla\psi \cdot \delta(\nabla\psi)}{|\nabla\psi|}. \quad (2.20)$$

## 2.2 The divergence of a vector field

The divergence of a vector field,  $\mathbf{F}$ , is the scalar product of the divergence operator with the vector

$$\operatorname{div}(\mathbf{F}) = \nabla \cdot \mathbf{F} = \partial_a F_a \begin{cases} > 0 \Rightarrow \text{diverging vector field,} \\ < 0 \Rightarrow \text{converging vector field} \\ = 0 \Rightarrow \text{divergence-free vector field.} \end{cases} \quad (2.21)$$

If the vector field in the surrounding neighborhood of a point is directed away from that point, then the vector field is diverging as if there is a source at the point (Figure 2.3). In this case the divergence of the vector field is positive. The converse occurs for a vector field converging to a point as if there is a sink. If the vector field under consideration is the velocity field of a fluid, then these considerations are directly related to the conservation of matter (see Chapter 14).

The above example of a point source or sink provide a good introduction to divergence. More generally, a vector field possess a positive divergence at any point where there is more “stuff” leaving than entering. For example, if the vector field is the velocity for a fluid, then there is a net divergence if more fluid leaves a point than enters, and the converse holds if the fluid is converging. We further discuss these ideas when studying Gauss’s divergence theorem in Section 2.7.

### 2.2.1 Divergence of a scalar field times a vector field

We have many opportunities to make use of properties of the divergence operator following from application of the chain rule. For example, use of the chain rule indicates that the divergence of a scalar field times a vector field is given by

$$\nabla \cdot (\phi \mathbf{F}) = \partial_a(\phi F_a) \quad (2.22a)$$

$$= \partial_a(\phi) F_a + \phi \partial_a F_a \quad (2.22b)$$

$$= \mathbf{F} \cdot \nabla \phi + \phi \nabla \cdot \mathbf{F}. \quad (2.22c)$$

### 2.2.2 Laplacian of a scalar field

The Laplacian of a scalar field is the divergence of the gradient

$$\nabla^2 \psi = \nabla \cdot \nabla \psi. \quad (2.23)$$

Scalar fields that have a vanishing Laplacian are said to be *harmonic*

$$\nabla^2 \psi = 0 \quad \text{harmonic function.} \quad (2.24)$$

Familiar examples of harmonic functions are the sines and cosines used for Fourier analysis in Euclidean space, and the spherical harmonics used for Fourier analysis on the sphere. The name *harmonic* originates from the relation of harmonic functions to characteristic vibrational modes of a taut string such as those found on musical instruments (when played with skill). Furthermore, harmonic functions play a central role in complex analysis.

## 2.3 The curl of a vector field

The curl characterizes how a vector field spins around each point in space. In fluid mechanics we make great use of the vorticity field, which is the curl of the velocity (Chapter 35).

### 2.3.1 Computing the curl

We measure the curl of a vector by computing the cross product of the divergence operator and the vector field. Hence, just like the cross product from Section 1.4, the curl is specified by both

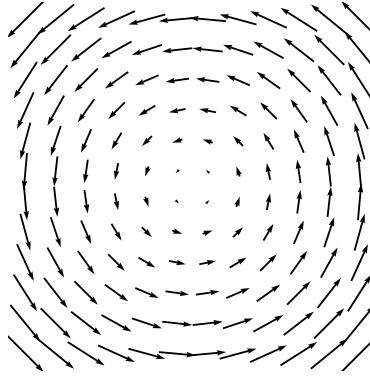


FIGURE 2.4: A horizontal vector field with a constant curl and zero divergence:  $\mathbf{F} = -y \hat{\mathbf{x}} + x \hat{\mathbf{y}}$ ,  $\Rightarrow \nabla \times \mathbf{F} = 2 \hat{\mathbf{z}}$  and  $\nabla \cdot \mathbf{F} = 0$ .

a magnitude and a direction

$$\text{curl}(\mathbf{F}) = \nabla \times \mathbf{F} \quad (2.25a)$$

$$= \vec{e}_a \partial_a \times \vec{e}_b F_b \quad \text{coordinate representation and basis} \quad (2.25b)$$

$$= \vec{e}_a \times \partial_a (\vec{e}_b F_b) \quad \text{move derivative operator onto } \mathbf{F} = \vec{e}_b F_b \quad (2.25c)$$

$$= (\vec{e}_a \times \vec{e}_b) \partial_a F_b + F_b (\vec{e}_a \times \partial_a \vec{e}_b) \quad \text{perform product rule} \quad (2.25d)$$

$$= \epsilon_{abc} \vec{e}_c \partial_a F_b \quad \partial_a \vec{e}_b = 0 \text{ for Cartesian coordinates.} \quad (2.25e)$$

To reach this result we set  $\partial_a \vec{e}_b = 0$  since the Cartesian basis vectors are fixed in space.<sup>1</sup> We also made use of the relation (1.12) for the cross product of basis vectors. Expanding the final expression leads to the familiar expression

$$\text{curl}(\mathbf{F}) = \nabla \times \mathbf{F} = \left( \frac{\partial F_3}{\partial x_2} - \frac{\partial F_2}{\partial x_3} \right) \hat{\mathbf{x}} + \left( \frac{\partial F_1}{\partial x_3} - \frac{\partial F_3}{\partial x_1} \right) \hat{\mathbf{y}} + \left( \frac{\partial F_2}{\partial x_1} - \frac{\partial F_1}{\partial x_2} \right) \hat{\mathbf{z}}, \quad (2.26)$$

which can also be written as a determinant

$$\nabla \times \mathbf{F} = \det \begin{bmatrix} \vec{e}_1 & \vec{e}_2 & \vec{e}_3 \\ \partial_1 & \partial_2 & \partial_3 \\ F_1 & F_2 & F_3 \end{bmatrix}. \quad (2.27)$$

The horizontal vector field  $\mathbf{F} = x \hat{\mathbf{x}} + y \hat{\mathbf{y}}$  shown in Figure 2.3 has zero curl yet non-zero divergence. Figure 2.4 shows another vector field,  $\mathbf{F} = -y \hat{\mathbf{x}} + x \hat{\mathbf{y}}$ , with zero divergence yet nonzero curl  $\nabla \times \mathbf{F} = 2 \hat{\mathbf{z}}$ . As seen in Section 32.5, this vector field corresponds to the velocity due to solid-body motion on a rotating planet, with its curl determining the planetary vorticity.

### 2.3.2 Curl-free vector fields

There are some cases of physically relevant vector fields that have a vanishing curl

$$\nabla \times \mathbf{F} = 0. \quad (2.28)$$

<sup>1</sup>Basis vectors corresponding to non-Cartesian coordinates are spatially dependent (see Chapters 6 and 7), thus making this step invalid for general tensors. We will find a “fix” for this step in Section 7.17 by defining the covariant curl operator.

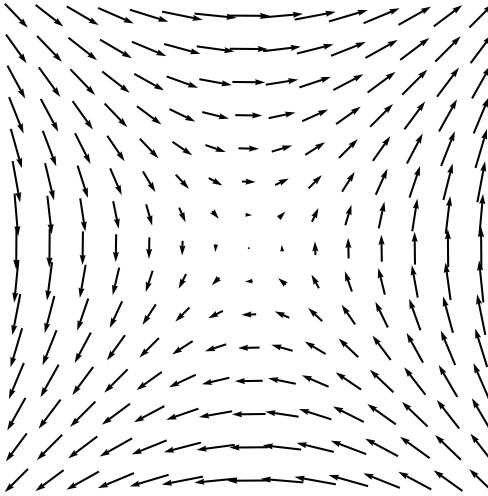


FIGURE 2.5: A horizontal vector field with a zero curl, where  $\mathbf{F} = -\nabla\psi$  with the scalar potential given by  $\psi = \sin(x/10) \sin(y/10)$ .

We sometimes refer to such curl-free vectors as *irrotational*. In fluid mechanics a curl-free velocity field has zero vorticity, which is a property maintained by linear gravity waves in the absence of rotation (Section 31.8.3). We illustrate a curl-free vector field in Figure 2.5.

The curl of a gradient vanishes

$$\nabla \times \nabla\psi = \vec{e}_a \partial_a \times \vec{e}_b \partial_b \psi \quad (2.29a)$$

$$= (\vec{e}_a \times \vec{e}_b) \partial_a \partial_b \psi \quad (2.29b)$$

$$= 0, \quad (2.29c)$$

where the final equality follows since  $\vec{e}_a \times \vec{e}_b$  is anti-symmetric on the labels  $ab$  whereas  $\partial_a \partial_b$  is symmetric. This property allows us to introduce a scalar field  $\psi$  for curl-free vector fields so that

$$\mathbf{F} = -\nabla\psi \quad \text{scalar potential.} \quad (2.30)$$

The scalar  $\psi$  is known as the *scalar potential*. In the specific case of  $\mathbf{F}$  representing the gravitational force, then  $\psi$  is called the gravitational potential (see Section 9.12 and Chapter 28).

### 2.3.3 Curl-free and divergence-free fields

Consider a vector field that has zero curl *and* zero divergence. The curl-free property means that

$$\nabla \times \mathbf{F} = 0 \Rightarrow \mathbf{F} = -\nabla\psi. \quad (2.31)$$

The divergence-free property means that  $\psi$  is a harmonic function (Section 2.2.2)

$$\nabla \cdot \nabla\psi = \nabla^2\psi = 0. \quad (2.32)$$

The velocity field arising from a linear non-rotating gravity wave (Section 31.8.3) in a Boussinesq fluid (Section 23.1) maintains zero vorticity and zero divergence. Furthermore, curl-free and divergence-free velocity fields are commonly encountered in engineering applications such as aerodynamics (e.g., see [Acheson \(1990\)](#) for many elementary examples).

### 2.3.4 Identities involving the curl

We close this section by deriving a suite of identities involving the curl operator. These identities are especially useful when developing dynamical equations for vorticity. Furthermore, by making use of the rules for general tensor analysis developed in Chapters 6 and 7, these formula take on the same form regardless the coordinate choice.

#### *Divergence of the curl vanishes*

The divergence of the curl vanishes, as seen through the following

$$\nabla \cdot (\nabla \times \mathbf{F}) = \partial_a(\epsilon_{abc} \partial_b F_c) \quad (2.33a)$$

$$= \epsilon_{abc} \partial_a \partial_b F_c \quad (2.33b)$$

$$= 0. \quad (2.33c)$$

The final equality holds since  $\partial_a \partial_b$  is symmetric on  $ab$  whereas  $\epsilon_{abc}$  is anti-symmetric.

#### *Divergence of a cross product*

We now derive an expression for the divergence of a cross product

$$\nabla \cdot (\mathbf{F} \times \mathbf{E}) = \mathbf{E} \cdot (\nabla \times \mathbf{F}) - \mathbf{F} \cdot (\nabla \times \mathbf{E}) \quad (2.34)$$

through the following manipulations

$$\nabla \cdot (\mathbf{F} \times \mathbf{E}) = \vec{e}_a \cdot \partial_a (F_b \vec{e}_b \times E_c \vec{e}_c) \quad (2.35a)$$

$$= \vec{e}_a \cdot (\vec{e}_b \times \vec{e}_c) \partial_a (F_b E_c) \quad (2.35b)$$

$$= \epsilon_{abc} \partial_a (F_b E_c) \quad (2.35c)$$

$$= F_b \epsilon_{abc} \partial_a E_c + E_c \epsilon_{abc} \partial_a F_b \quad (2.35d)$$

$$= -\mathbf{F} \cdot (\nabla \times \mathbf{E}) + \mathbf{E} \cdot (\nabla \times \mathbf{F}). \quad (2.35e)$$

#### *Curl of a scalar times a vector*

We can compute the curl of a scalar field  $\psi \mathbf{F}$  through the following steps

$$\nabla \times (\psi \mathbf{F}) = \vec{e}_a \partial_a \times \psi \vec{e}_b F_b \quad (2.36a)$$

$$= (\vec{e}_a \times \vec{e}_b) \partial_a (\psi F_b) \quad (2.36b)$$

$$= \epsilon_{abc} \vec{e}_c (\psi \partial_a F_b + F_b \partial_a \psi) \quad (2.36c)$$

$$= \psi \nabla \times \mathbf{F} + \nabla \psi \times \mathbf{F}. \quad (2.36d)$$

### Curl of a cross product

The curl of a cross product of two vectors is given by

$$\nabla \times (\mathbf{F} \times \mathbf{E}) = \vec{e}_a \partial_a \times (\vec{e}_b F_b \times \vec{e}_c E_c) \quad (2.37a)$$

$$= \vec{e}_a \times (\vec{e}_b \times \vec{e}_c) \partial_a (F_b E_c) \quad (2.37b)$$

$$= \vec{e}_a \times (\epsilon_{bcd} \vec{e}_d) \partial_a (F_b E_c) \quad (2.37c)$$

$$= \epsilon_{ade} \epsilon_{bcd} \vec{e}_e \partial_a (F_b E_c) \quad (2.37d)$$

$$= -\epsilon_{aed} \epsilon_{bcd} \vec{e}_e \partial_a (F_b E_c) \quad (2.37e)$$

$$= -(\delta_{ab} \delta_{ec} - \delta_{ac} \delta_{eb}) \vec{e}_e \partial_a (F_b E_c) \quad (2.37f)$$

$$= (-\delta_{ba} \vec{e}_c + \delta_{ca} \vec{e}_b) \partial_a (F_b E_c) \quad (2.37g)$$

$$= \mathbf{F} (\nabla \cdot \mathbf{E}) + (\mathbf{E} \cdot \nabla) \mathbf{F} - \mathbf{E} (\nabla \cdot \mathbf{F}) - (\mathbf{F} \cdot \nabla) \mathbf{E}. \quad (2.37h)$$

### Curl of a curl

A special case of the identity (2.37h) allows us to write the curl of a curl as

$$\nabla \times (\nabla \times \mathbf{F}) = \vec{e}_a \times (\vec{e}_b \times \vec{e}_c) \partial_a \partial_b F_c \quad (2.38a)$$

$$= (-\delta_{ba} \vec{e}_c + \delta_{ca} \vec{e}_b) \partial_a \partial_b F_c \quad (2.38b)$$

$$= \nabla (\nabla \cdot \mathbf{F}) - \nabla^2 \mathbf{F}. \quad (2.38c)$$

### Relating advection, curl, and kinetic energy

We now apply some of the previous manipulations to derive a relation required to derive the vorticity equation (Section 35.4.1). Here, we aim to show that

$$(\mathbf{v} \cdot \nabla) \mathbf{v} = \boldsymbol{\omega} \times \mathbf{v} + \nabla(\mathbf{v} \cdot \mathbf{v})/2, \quad (2.39)$$

where

$$\boldsymbol{\omega} = \nabla \times \mathbf{v} \quad (2.40)$$

is the vorticity,  $\mathbf{v} \cdot \mathbf{v}/2$  is the kinetic energy per mass, and  $\mathbf{v}$  is the fluid velocity field. We here show all the steps along with their justification

$$\boldsymbol{\omega} \times \mathbf{v} = (\nabla \times \mathbf{v}) \times \mathbf{v} \quad \text{insert } \boldsymbol{\omega} = \nabla \times \mathbf{v} \quad (2.41a)$$

$$= (\vec{e}_a \partial_a \times \vec{e}_b v_b) \times \vec{e}_c v_c \quad \text{Cartesian representation of } \mathbf{v} \text{ and } \nabla \quad (2.41b)$$

$$= (\vec{e}_a \times \vec{e}_b) \times \vec{e}_c (\partial_a v_b) v_c \quad \text{rearrange} \quad (2.41c)$$

$$= \epsilon_{abd} (\vec{e}_d \times \vec{e}_c) (\partial_a v_b) v_c \quad \text{first cross product expanded} \quad (2.41d)$$

$$= \epsilon_{abd} \epsilon_{dce} \vec{e}_e (\partial_a v_b) v_c \quad \text{second cross product expanded} \quad (2.41e)$$

$$= \epsilon_{abd} \epsilon_{ced} \vec{e}_e (\partial_a v_b) v_c \quad \text{arrange indices to prepare for next step} \quad (2.41f)$$

$$= (\delta_{ac} \delta_{be} - \delta_{ae} \delta_{bc}) \vec{e}_e (\partial_a v_b) v_c \quad \text{use identity (1.38)} \quad (2.41g)$$

$$= \vec{e}_a v_c \partial_c v_a - \vec{e}_a v_c \partial_a v_c \quad \text{contract the Kronecker deltas} \quad (2.41h)$$

$$= \vec{e}_a [(\mathbf{v} \cdot \nabla) v_a - \partial_a \mathbf{v}^2/2] \quad \text{re-express as Cartesian tensor} \quad (2.41i)$$

$$= (\mathbf{v} \cdot \nabla) \mathbf{v} - \nabla[\mathbf{v} \cdot \mathbf{v}/2] \quad \text{rearrange.} \quad (2.41j)$$

Note that Section 4.4.4 of [Griffies \(2004\)](#) exhibits these steps making use of general coordinates rather than Cartesian.

## 2.4 Path integral of a scalar function

Consider the integral of a scalar function,  $\psi$ , over an arbitrary one-dimensional path in space,  $C$

$$\mathcal{I} = \int_C \psi(\varphi) d\varphi. \quad (2.42)$$

A path is a one-dimensional curve, so that a point along the path can be specified by a single parameter, denoted here by  $\varphi$  (see Sections 5.1 and 5.2 for more on paths). Now lay down a Cartesian coordinate system with an arbitrary origin. The corresponding Cartesian coordinate representation of a point along the path is written

$$C \mapsto \mathbf{x}(\varphi) = \hat{\mathbf{x}} x(\varphi) + \hat{\mathbf{y}} y(\varphi) + \hat{\mathbf{z}} z(\varphi) \quad (2.43)$$

so that the path integral can be written

$$\mathcal{I} = \int_C \psi(\varphi) d\varphi = \int_C \psi[\mathbf{x}(\varphi)] d\varphi. \quad (2.44)$$

### *Arc length to parameterize the path*

A particularly common special case for path parameterization is where we choose  $\varphi$  to be the arc length along the path. For Euclidean space using Cartesian coordinates, the differential increment of arc length is given by

$$ds = \sqrt{d\mathbf{x} \cdot d\mathbf{x}}. \quad (2.45)$$

Inserting  $\mathbf{x}(s)$  into this expression renders

$$ds = \sqrt{d\mathbf{x} \cdot d\mathbf{x}} = ds \sqrt{\frac{d\mathbf{x}}{ds} \cdot \frac{d\mathbf{x}}{ds}}. \quad (2.46)$$

This expression is self-consistent if

$$\sqrt{\frac{d\mathbf{x}}{ds} \cdot \frac{d\mathbf{x}}{ds}} = 1, \quad (2.47)$$

which is merely a rewrite of the defining expression (2.45). The derivative of the curve according to the arc-length,  $d\mathbf{x}/ds$ , defines a unit tangent vector to the curve

$$\hat{\mathbf{t}} = \frac{d\mathbf{x}}{ds} \implies \hat{\mathbf{t}} \cdot \hat{\mathbf{t}} = 1. \quad (2.48)$$

We offer a more focused discussion of curves and tangents in Section 5.2.1 (see in particular equation (5.6)).

### *Linear path example*

As a specific example, consider a line between two points,  $\mathbf{x}_A$  and  $\mathbf{x}_B$ , as in Figure 2.6. We can parameterize the line using a dimensionless parameter  $\varphi$  according to

$$\mathbf{x}(\varphi) = \mathbf{x}_A + (\mathbf{x}_B - \mathbf{x}_A) \varphi \quad \varphi \in [0, 1]. \quad (2.49)$$

Alternatively, we can parameterize using the arc length

$$\mathbf{x}(s) = \mathbf{x}_A + \hat{\mathbf{t}} s \quad s \in [0, L], \quad (2.50)$$

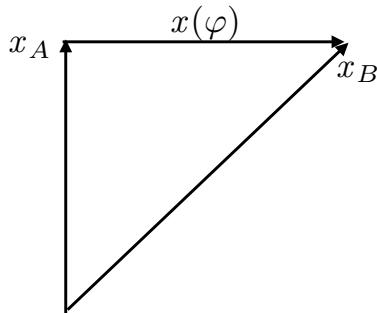


FIGURE 2.6: A linear path,  $\mathbf{x}(\varphi)$  extending from  $\mathbf{x}_A$  to  $\mathbf{x}_B$  can be parameterized by a non-dimensional parameter  $\varphi \in [0, 1]$  via  $\mathbf{x}(\varphi) = \mathbf{x}_A + \varphi(\mathbf{x}_B - \mathbf{x}_A)$ . Alternatively it can be parameterized by the arc-length along the path via  $\mathbf{x}(s) = \mathbf{x}_A + \hat{\mathbf{t}} s$  with  $s \in [0, L]$ ,  $L = |\mathbf{x}_B - \mathbf{x}_A|$ , and  $\hat{\mathbf{t}}$  the unit tangent vector pointing from  $\mathbf{x}_A$  to  $\mathbf{x}_B$ .

where  $L = \int_A^B ds = |\mathbf{x}_B - \mathbf{x}_A|$  is the total arc length of the line, and where  $\hat{\mathbf{t}}$  is the unit tangent vector pointing along the path from  $\mathbf{x}_A$  to  $\mathbf{x}_B$

$$\hat{\mathbf{t}} = \frac{\mathbf{x}'(s)}{|\mathbf{x}'(s)|} = \frac{\mathbf{x}_B - \mathbf{x}_A}{|\mathbf{x}_B - \mathbf{x}_A|}. \quad (2.51)$$

As defined we have  $|\mathbf{x}'(s)| = |\hat{\mathbf{t}}| = 1$ , so that the path integral is given by  $\mathcal{I} = \int_0^L \psi[\mathbf{x}(s)] ds$ .

## 2.5 Path integral of a vector function

Generalizing to a vector field,  $\mathbf{F}(\mathbf{x})$ , we could conceivably integrate each component of the vector along the curve independently using the approach for scalar fields in Section 2.4. In practice, however, that quantity rarely appears in physics. Instead, we more commonly wish to integrate that component of  $\mathbf{F}(\mathbf{x})$  that projects onto a curve

$$\int_C \mathbf{F} \cdot d\mathbf{x} = \int_C \mathbf{F} \cdot \frac{d\mathbf{x}}{ds} ds \quad (2.52)$$

where  $d\mathbf{x}/ds$  is tangent to the curve. The work performed by a force applied along a path provides a common example of this path integral (Section 9.1.5).

### 2.5.1 Circulation

For the case of a closed curve or a circuit (see Section 5.1), we refer to the above path integral as the *circulation* and use the convention of putting an arrowed circle on the integral sign

$$\text{circulation of vector field} = \oint_C \mathbf{F} \cdot d\mathbf{x}. \quad (2.53)$$

The arrow indicates that we conventionally traverse the closed path in a counter-clockwise (right hand) manner.

### 2.5.2 Circulation example

Consider the vector field  $\mathbf{F} = -y \hat{\mathbf{x}} + x \hat{\mathbf{y}}$  shown in Figure 2.4. What is the circulation for this field computed around a circle of radius  $r$  whose center is the origin? To compute this circulation we make use of plane polar coordinates, in which  $x = r \cos \varphi$  and  $y = r \sin \varphi$ , with  $\varphi \in [0, 2\pi]$  the polar angle measured from the positive  $x$ -axis. The position of a point on the circle is thus written

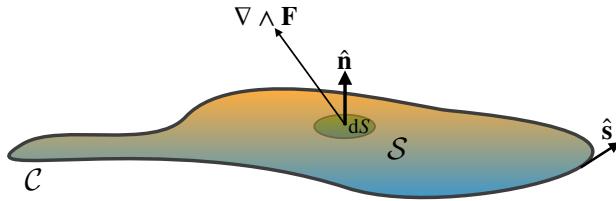


FIGURE 2.7: Illustrating the geometry of Stokes' Theorem. The unit normal  $\hat{\mathbf{n}}$  points outward from the surface,  $\mathcal{S}$ , with  $(\nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}}$  the projection of the curl of a vector field onto the surface normal. The outer boundary of the area,  $\partial\mathcal{S}$ , is traversed counterclockwise following a tangent vector  $\hat{\mathbf{s}}$  when computing the circulation.

$\mathbf{x}(\varphi) = r(\hat{\mathbf{x}} \cos \varphi + \hat{\mathbf{y}} \sin \varphi)$ , and the tangent to the circle is  $d\mathbf{x}(\varphi)/d\varphi = r(-\hat{\mathbf{x}} \sin \varphi + \hat{\mathbf{y}} \cos \varphi)$ . The integrand to the circulation (2.52) thus takes the form

$$\mathbf{F} \cdot \frac{d\mathbf{x}(\varphi)}{d\varphi} = r(y \sin \varphi + x \cos \varphi) = r^2. \quad (2.54)$$

Hence, the circulation around the constant radius circle is given by twice the area of the circle

$$\oint_C \mathbf{F} \cdot d\mathbf{x} = 2\pi r^2. \quad (2.55)$$

This result has application for geophysical fluids when computing the vorticity induced by the rotating planet (see Section 35.7.2).

### 2.5.3 Fundamental theorem of calculus

The special case of  $\mathbf{F} = -\nabla\psi$  for a scalar field  $\psi$  recovers the fundamental theorem of calculus

$$\psi(\mathbf{x}_A) - \psi(\mathbf{x}_B) = \int_{\mathbf{x}_A}^{\mathbf{x}_B} d\psi = \int_{\mathbf{x}_A}^{\mathbf{x}_B} \nabla\psi \cdot d\mathbf{x}. \quad (2.56)$$

It follows that for any closed curve with  $\mathbf{x}_A = \mathbf{x}_B$ , the circulation of  $\nabla\psi$  vanishes

$$\oint_C d\psi = \oint_C \nabla\psi \cdot d\mathbf{x} = 0. \quad (2.57)$$

## 2.6 Stokes' theorem

Stokes' theorem relates a vector field's behavior on the boundary of a surface to its behavior within the area of the surface. It is used extensively in our study of circulation and vorticity in Part VI of this book.

### 2.6.1 Statement of Stokes' theorem

Given an oriented surface  $\mathcal{S}$  with a boundary  $\partial\mathcal{S}$ , Stokes' Theorem says that the circulation around the boundary equals to the area integrated curl projected onto the surface outward normal

$$\oint_{\partial\mathcal{S}} \mathbf{F} \cdot d\mathbf{x} = \int_{\mathcal{S}} (\nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (2.58)$$

In this equation,  $d\mathbf{x}$  is the vector line element along the path,  $\partial\mathcal{S}$  is the closed path defining the boundary to an oriented two-dimensional surface  $\mathcal{S}$ ,  $\hat{\mathbf{n}}$  is the outward normal vector on the

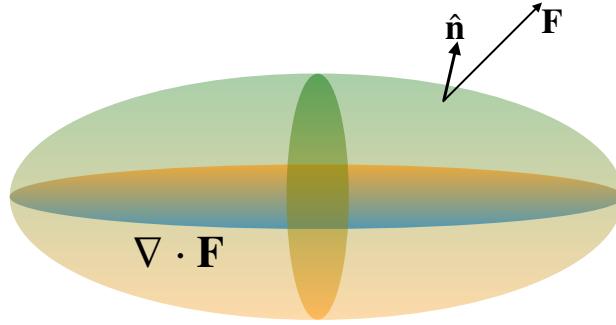


FIGURE 2.8: Illustrating the geometry of Gauss's divergence theorem for an ellipsoidal volume. The outward unit normal  $\hat{\mathbf{n}}$  is projected onto the vector field  $\mathbf{F}$  via the scalar product,  $\mathbf{F} \cdot \hat{\mathbf{n}}$ . Integrating this scalar product over the closed surface  $\mathcal{S}$  yields the same result as computing the volume integral of the divergence,  $\nabla \cdot \mathbf{F}$ , over the region,  $\mathcal{R}$ , bounded by the closed surface.

surface, and  $d\mathcal{S}$  is the infinitesimal surface area element. The orientation of the outward normal is determined by the right hand rule according to the circulation direction.

### 2.6.2 Stokes' theorem for a rectangular region

To build experience with Stokes' theorem, consider the case of a rectangle in the x-y plane with dimensions  $L_x \times L_y$ . In this case  $\hat{\mathbf{n}} = \hat{\mathbf{z}}$ , so that

$$(\nabla \times \mathbf{F}) \cdot \hat{\mathbf{z}} = \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y}, \quad (2.59)$$

in which case the right hand side of Stokes' theorem reduces to

$$\int_{\mathcal{S}} (\nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}} dS = \int_0^{L_x} \int_0^{L_y} \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy. \quad (2.60)$$

Integration around the rectangle then leads to a direct verification of Stokes' Theorem

$$\int_0^{L_x} \int_0^{L_y} \left( \frac{\partial F_2}{\partial x} - \frac{\partial F_1}{\partial y} \right) dx dy = \int_0^{L_y} F_2(x, y) \Big|_{x=0}^{x=L_x} dy - \int_0^{L_x} F_1(x, y) \Big|_{y=0}^{y=L_y} dx \quad (2.61a)$$

$$= \int_0^{L_x} F_1(x, 0) dx + \int_0^{L_y} F_2(L_x, y) dy + \int_{L_x}^0 F_1(x, L_y) dx + \int_{L_y}^0 F_2(0, y) dy \quad (2.61b)$$

$$= \oint_{\partial\mathcal{S}} \mathbf{F} \cdot d\mathbf{x}. \quad (2.61c)$$

We can generalize this result to verify Stokes' Theorem for an arbitrary surface. We do so by breaking the surface into a lattice of tiny rectangles. Integrating around the tiny rectangles and summing their contributions leads to a cancellation of the line integrals over all interior boundaries. The cancellation occurs since an internal edge of a rectangle is integrated once in each direction thus cancelling its contribution. The only nonzero contribution comes from integration over the external boundary.

## 2.7 Gauss's divergence theorem

Gauss's divergence theorem relates the divergence of a vector field integrated over a volume to the area integrated normal projection of the vector field through the closed surface bounding the

volume. For a vector field  $\mathbf{F}$ , the divergence theorem states that

$$\int_{\mathcal{R}} \nabla \cdot \mathbf{F} dV = \oint_{\partial\mathcal{R}} \mathbf{F} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (2.62)$$

where  $\hat{\mathbf{n}}$  is the outward normal to the boundary surface and  $d\mathcal{S}$  is the surface area element. We follow the convention that  $\oint_{\partial\mathcal{R}}$  refers to a surface integral over a closed surface that bounds a volume. This notation is used to contrast with the surface integral  $\int_S$  that generally does not enclose a volume. Figure 2.8 illustrates the geometry of Gauss's divergence theorem. In physics jargon, we say that the divergence of a vector field,  $\nabla \cdot \mathbf{F}$ , integrated over a volume equals to the flux of that vector field,  $\mathbf{F} \cdot \hat{\mathbf{n}}$ , integrated over the area bounding the volume.

### 2.7.1 An example rectangular volume

To build intuition for Gauss's divergence theorem, consider a rectangular volume with dimensions  $L_x \times L_y \times L_z$ . The volume integral on the left hand side of equation (2.62) gives

$$\int_{\mathcal{R}} \left[ \frac{\partial F_1}{\partial x} + \frac{\partial F_2}{\partial y} + \frac{\partial F_3}{\partial z} \right] dx dy dz. \quad (2.63)$$

Focusing on just the leftmost term, integration in  $x$  gives

$$\int_{\mathcal{R}} \frac{\partial F_1}{\partial x} dx dy dz = \int_{y=0}^{y=L_y} \int_{z=0}^{z=L_z} [F_1(L_x, y, z) - F_1(0, y, z)] dy dz \quad (2.64a)$$

$$= \int_{S_1+S_2} \mathbf{F} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (2.64b)$$

where  $S_1$  is the rectangle's face with outward normal  $\hat{\mathbf{n}} = \hat{\mathbf{x}}$  and  $S_2$  is the rectangle's face with normal  $\hat{\mathbf{n}} = -\hat{\mathbf{x}}$ . Repeating this procedure on the other terms in equation (2.63) gives the area integrated flux through the full boundary. To verify the theorem for a general volume  $V$ , we take the approach used to prove Stokes' theorem. First, divide the volume into many rectangular sub-volumes. Then apply the above result to each sub-volume and sum up the result. The fluxes through internal rectangular faces cancel exactly. Therefore, the sum of all the fluxes equals just the flux through the external boundary, yielding the divergence theorem.

### 2.7.2 Divergence theorem for scalar fields

We consider two corollaries of the divergence theorem, the first of which arises from the special case of a vector field  $\mathbf{F} = \phi \mathbf{c}$  with  $\mathbf{c}$  an arbitrary *constant* vector. Substitution into the divergence theorem (2.62) yields

$$\oint_{\partial\mathcal{R}} \phi \mathbf{c} \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\mathcal{R}} \nabla \cdot (\phi \mathbf{c}) dV. \quad (2.65)$$

Pulling the constant vector out of the integrals and rearrangement leads to

$$\mathbf{c} \cdot \left[ \oint_{\partial\mathcal{R}} \phi \hat{\mathbf{n}} d\mathcal{S} - \int_{\mathcal{R}} \nabla \phi dV \right] = 0. \quad (2.66)$$

Since  $\mathbf{c}$  is an arbitrary vector, this equality is true in general only when

$$\oint_{\partial\mathcal{R}} \phi \hat{\mathbf{n}} d\mathcal{S} = \int_{\mathcal{R}} \nabla \phi dV. \quad (2.67)$$

In words, this result says that the integral of a scalar field over the boundary of a closed surface, when weighted by the outward normal to the surface, equals to the volume integral of the gradient of the scalar field integrated over the region bounded by the closed surface. We make use of this result in Section 17.1.3 when formulating the contribution of stresses to the motion of a fluid element, in particular when considering how pressure affects motion.

### 2.7.3 Surface integral of the outward normal

A corollary of equation (2.67) can be found by setting the scalar field,  $\phi$ , to a constant so that  $\nabla\phi = 0$ . We thus find that the area integral of the outward normal vector vanishes when integrated over the surface of a closed volume

$$\oint_{\partial\mathcal{R}} \hat{\mathbf{n}} d\mathcal{S} = 0. \quad (2.68)$$

An example of this result can be seen by integrating over a closed rectangular volume, whereby the area integrals cancel component-wise. Another example is the sphere, where  $\hat{\mathbf{n}} = \hat{\mathbf{r}}$  is the outward radial unit vector. Integration of the unit vector over the spherical surface identically vanishes. For some purposes one take the result (2.68) as the definition of a simply closed volume.

### 2.7.4 First and second form of Green's identities

The second corollary to the divergence theorem arises from considering another special vector field

$$\mathbf{F} = \psi \nabla\phi, \quad (2.69)$$

with  $\psi$  and  $\phi$  scalar fields. Substitution into the divergence theorem (2.62) leads to

$$\oint_{\partial\mathcal{R}} \psi \frac{\partial\phi}{\partial n} d\mathcal{S} = \int_{\mathcal{R}} [\nabla\psi \cdot \nabla\phi + \psi \nabla^2\phi] dV \quad \text{Green's first integral identity.} \quad (2.70)$$

We can make this result more symmetric by swapping  $\psi$  and  $\phi$  and then subtracting, thus yielding

$$\oint_{\partial\mathcal{R}} \left[ \psi \frac{\partial\phi}{\partial n} - \phi \frac{\partial\psi}{\partial n} \right] d\mathcal{S} = \int_{\mathcal{R}} [\psi \nabla^2\phi - \phi \nabla^2\psi] dV \quad \text{Green's second integral identity.} \quad (2.71)$$

Finally, setting  $\phi = 1$  renders

$$\oint_{\partial\mathcal{R}} \frac{\partial\psi}{\partial n} d\mathcal{S} = \int_{\mathcal{R}} \nabla^2\psi dV \iff \oint_{\partial\mathcal{R}} \nabla\psi \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\mathcal{R}} \nabla \cdot \nabla\psi dV. \quad (2.72)$$

These identities are fundamental to the Green's function method for solving linear partial differential equations (see Chapter 4).

### 2.7.5 Integral of a curl over a closed surface

Application of Gauss's divergence theorem leads us to conclude that the following integral vanishes

$$\oint_{\partial\mathcal{R}} (\nabla \times \Psi) \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\mathcal{R}} \nabla \cdot (\nabla \times \Psi) dV = 0, \quad (2.73)$$

where the final equality follows since the divergence of a curl vanishes. Hence, the integral of the normal projection of the curl of a function over an oriented closed surface vanishes. We can understand this result geometrically by splitting the closed volume into two regions and then

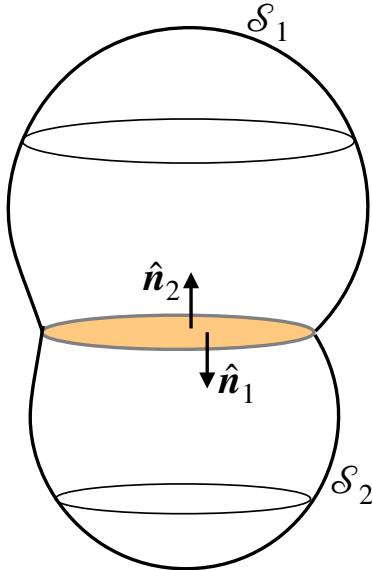


FIGURE 2.9: The integral of the curl of a function vanishes when integrated over an oriented closed surface. This result follows from both Gauss's divergence theorem as well as Stokes' theorem. Here we depict a closed volume that has been split into two surfaces  $\mathcal{S}_1$  and  $\mathcal{S}_2$ . Separately applying Stokes' theorem to the surfaces leads to the calculation of the circulation around the common boundary. Yet the orientation of the outward normal along the closed surface is opposite for the two regions, thus leading to a cancellation of the circulations.

applying Stokes' theorem separately to the two regions (see Figure 2.9)

$$\oint_{\partial\mathcal{R}} (\nabla \times \Psi) \cdot \hat{\mathbf{n}} \, dS = \int_{\mathcal{S}_1} (\nabla \times \Psi) \cdot \hat{\mathbf{n}} \, dS_1 + \int_{\mathcal{S}_2} (\nabla \times \Psi) \cdot \hat{\mathbf{n}} \, dS_2 \quad (2.74a)$$

$$= \oint_{\partial\mathcal{S}_1} \Psi \cdot d\mathbf{x} - \oint_{\partial\mathcal{S}_2} \Psi \cdot d\mathbf{x} \quad (2.74b)$$

$$= 0. \quad (2.74c)$$

The minus sign appearing in front of  $\oint_{\partial\mathcal{S}_2}$  occurs since the orientation of the circulation integral is opposite that for  $\oint_{\partial\mathcal{S}_1}$ . We are thus left with a cancellation of the circulations. When applied to the vorticity of a fluid (Chapter 32), we see that

$$\oint_{\partial\mathcal{R}} \boldsymbol{\omega} \cdot \hat{\mathbf{n}} \, dS = \int_{\mathcal{R}} \nabla \cdot \boldsymbol{\omega} \, dV = 0, \quad (2.75)$$

where  $\boldsymbol{\omega} = \nabla \times \mathbf{v}$  is the vorticity and  $\mathbf{v}$  is the fluid velocity.

## 2.7.6 The domain integral of a non-divergent field

Consider a vector field that has zero divergence everywhere within a domain,  $\mathcal{R}$ . Consequently,  $\int_{\mathcal{R}} \nabla \cdot \mathbf{F} \, dV = \oint_{\partial\mathcal{R}} \mathbf{F} \cdot \hat{\mathbf{n}} \, dS = 0$ . Now what can we say about  $\int_{\mathcal{R}} \mathbf{F} \, dV$ ? One might be tempted to say that it vanishes. But that is generally an incorrect statement as we now show.

Since  $\nabla \cdot \mathbf{F} = 0$  we know that

$$0 = \int_{\mathcal{R}} x_i \nabla \cdot \mathbf{F} \, dV = \int_{\mathcal{R}} [\nabla \cdot (x_i \mathbf{F}) - F_i] \, dV, \quad (2.76)$$

where we used  $\partial_j x_i = \delta_{ij}$ . Use of the divergence theorem leads to

$$\int_{\mathcal{R}} F_i dV = \int_{\mathcal{R}} \nabla \cdot (x_i \mathbf{F}) dV = \oint_{\partial\mathcal{R}} x_i (\hat{\mathbf{n}} \cdot \mathbf{F}) d\mathcal{S}. \quad (2.77)$$

The right hand side does not generally vanish since  $\hat{\mathbf{n}} \cdot \mathbf{F}$  does not generally vanish at each point along  $\partial\mathcal{R}$ . Hence, we find that  $\int_{\mathcal{R}} \mathbf{F} dV = 0$  only for those domains where  $\hat{\mathbf{n}} \cdot \mathbf{F} = 0$  at each point along  $\partial\mathcal{R}$ .

## 2.8 Exact and inexact differentials

Thus far in this chapter all differentials have been exact. However, the thermodynamics discussed in Chapter 20 makes use of both exact and inexact differentials. We here introduce the mathematics of such differentials.

### 2.8.1 Exact differentials

As in Section 2.1, consider an arbitrary function of space,  $\Phi(\mathbf{x})$ . A differential increment for that function, computed between two close points  $\mathbf{x}$  and  $\mathbf{x} + d\mathbf{x}$ , is given by

$$d\Phi(\mathbf{x}) = \Phi(\mathbf{x} + d\mathbf{x}) - \Phi(\mathbf{x}) \quad (2.78a)$$

$$= d\mathbf{x} \cdot \nabla \Phi, \quad (2.78b)$$

where we dropped higher order terms due to the infinitesimal nature of the increments. It follows that we can determine the finite increment between two points through integration

$$\Phi(\mathbf{x}_B) - \Phi(\mathbf{x}_A) = \int_{\mathbf{x}_A}^{\mathbf{x}_B} d\Phi(\mathbf{x}) = \int_{\mathbf{x}_A}^{\mathbf{x}_B} d\mathbf{x} \cdot \nabla \Phi. \quad (2.79)$$

These results are familiar from elementary calculus, with the increment  $d\Phi$  given by equation (2.78b) termed an *exact* differential. Importantly, the finite increment,  $\Phi(\mathbf{x}_B) - \Phi(\mathbf{x}_A)$ , depends only on the endpoint values of  $\Phi$ . It does not depend on the path taken to go from  $\mathbf{x}_A$  to  $\mathbf{x}_B$ . Correspondingly, the integral of an exact differential around a closed loop vanishes

$$\oint d\Phi = 0. \quad (2.80)$$

### 2.8.2 Inexact differentials

Consider now a general differential expression written as

$$\mathbf{A} \cdot d\mathbf{x} = A dx + B dy + C dz, \quad (2.81)$$

where  $\mathbf{A} = A \hat{\mathbf{x}} + B \hat{\mathbf{y}} + C \hat{\mathbf{z}}$  is an arbitrary vector function. If  $\nabla \times \mathbf{A} = 0$ , then  $\mathbf{A}$  can be written as the gradient of a scalar

$$\nabla \times \mathbf{A} = 0 \implies \mathbf{A} = \nabla \Psi, \quad (2.82)$$

in which case we have an exact differential expression

$$\mathbf{A} \cdot d\mathbf{x} = \nabla \Psi \cdot d\mathbf{x} = d\Psi. \quad (2.83)$$

That is, the differential  $\mathbf{A} \cdot d\mathbf{x}$  is exact if

$$\nabla \times \mathbf{A} = 0 \implies \mathbf{A} \cdot d\mathbf{x} \text{ exact differential.} \quad (2.84)$$

In the more general case where  $\nabla \times \mathbf{A} \neq 0$ , then  $\mathbf{A} \cdot d\mathbf{x}$  is termed an *inexact differential*. We make use of the following notation for inexact differentials

$$d\Psi = \mathbf{A} \cdot d\mathbf{x}. \quad (2.85)$$

Notably, the path integral of an inexact differential depends on the path taken between the endpoints. Correspondingly, the integral of an inexact differential around a closed loop does not generally vanish

$$\oint d\Psi \neq 0. \quad (2.86)$$

### 2.8.3 Integrating factors

Consider again the inexact differential  $d\Psi = \mathbf{A} \cdot d\mathbf{x}$ . Let us presume there exists a function  $\tau$  so that the product  $\tau^{-1} d\Psi$  is an exact differential. For  $\tau$  to exist it must be such that

$$\nabla \times (\mathbf{A} \tau^{-1}) = 0. \quad (2.87)$$

Consequently, we can write

$$\mathbf{A} = \tau \nabla \Phi, \quad (2.88)$$

so that

$$d\Psi = \mathbf{A} \cdot d\mathbf{x} = \tau \nabla \Phi \cdot d\mathbf{x} = \tau d\Phi. \quad (2.89)$$

The function  $\tau$  is known as an *integrating factor*. As seen in Section 20.2.3, pressure is the integrating factor for mechanical work, temperature is the integrating factor for heating, and the chemical potential is the integrating factor for chemical work.

### 2.8.4 An example using the velocity field

Consider the product  $\mathbf{v} \cdot d\mathbf{x}$ , where  $\mathbf{v}$  is the velocity field for a fluid and  $d\mathbf{x}$  is a differential increment in space directed along a path. Furthermore, introduce the curl of the velocity, which defines the vorticity (Section 32.1)  $\boldsymbol{\omega} = \nabla \times \mathbf{v}$ . For cases where the vorticity vanishes,  $\boldsymbol{\omega} = 0$ , then  $d\Psi = \mathbf{v} \cdot d\mathbf{x}$  is an exact differential. Consequently, Stokes' theorem means that the circulation of an irrotational velocity field computed around an arbitrary closed loop vanishes (Section 32.3)

$$C \equiv \oint_{\partial S} \mathbf{v} \cdot d\mathbf{x} = \int_S \boldsymbol{\omega} \cdot \hat{\mathbf{n}} dS = 0. \quad (2.90)$$

Another way to see this result is to note that a vanishing curl means that the velocity field can be expressed as the gradient of a scalar,  $\mathbf{v} = \nabla \psi$ , so that  $d\Psi = \nabla \psi \cdot d\mathbf{x}$ , which is manifestly exact.

### 2.8.5 Heuristic physics of exact and inexact differential operations

Consider a hiker climbing a mountain. The mechanical work, which is force applied over a distance, is a function of the path taken. Some paths are smooth and well marked, whereas others are rough and poorly marked. Likewise, the frictional heating (of the hiker's feet, for example) depend on details of the path (and the shoes!). So although the start and finish points are fixed, the work exerted and heat generated in going between these points is a function of the path.

In contrast, the change in gravitational potential energy between the start and finish points is a function only of the relative elevation; it does not depend on the path between the points. So the gravitational potential energy increment between the two points is an exact differential, with the potential energy for each point a function of the elevation at the point. Analogously, the First Law of thermodynamics says that the sum of path-dependent processes (work and heat) used in going from one thermodynamic state to another equals to the difference in the internal energy between the two states. That is, the sum of the inexact differentials for heat and work equal to the exact differential for internal energy.

## 2.9 Helmholtz decomposition

In the development of conservation laws for continuum systems such as a fluid, it is common to express those laws in their flux-form whereby a scalar property (e.g., matter content) has a local time change determined by the convergence of a flux,  $\mathbf{J}$ . Since it is only the divergent portion of the flux that alters the time tendency, the non-divergent “rotational” portion has no impact on the time change; it is a “do nothing” portion of the flux. Therefore, it can be of use to decompose a general flux vector into its divergent and rotational components to focus on just that portion contributing to time changes.

As discussed in [Morse and Feshbach \(1953\)](#), the Helmholtz decomposition theorem states that any vector field,  $\mathbf{J}$ , can be decomposed as

$$\mathbf{J} = -\nabla\Psi + \nabla \times \mathbf{A}. \quad (2.91)$$

That is, we can decompose  $\mathbf{J}$  into a divergent vector plus a solenoidal/rotational vector field so that

$$\nabla \cdot \mathbf{J} = -\nabla^2\Psi \quad \text{and} \quad \nabla \times \mathbf{J} = \nabla \times (\nabla \times \mathbf{A}). \quad (2.92)$$

If we can determine this decomposition in a meaningful and robust manner, then our quest to study just the divergent component is met.

Indeed, the decomposition is unique in an infinite domain assuming suitable decay properties for  $\mathbf{F}$  (faster than  $r^{-2}$  for three-dimensions and faster than  $r^{-1}$  for two-dimensions). Unfortunately, the decomposition is not unique in finite domains since there are no unique choices for the boundary conditions. Furthermore, each of the potentials  $\Psi$  and  $\mathbf{A}$  are unique only up to a *gauge transformation* whereby

$$\Psi' = \Phi + C \quad \text{and} \quad \mathbf{A}' = \mathbf{A} + \nabla\lambda \quad (2.93)$$

lead to the same decomposition, with  $C$  an arbitrary constant and  $\lambda$  an arbitrary function. There are a variety of quasi-methods of use to partially address the ambiguity in a physically sensible manner, with the studies from [Fox-Kemper et al. \(2003\)](#) and [Maddision et al. \(2015\)](#) offering detailed discussions.

## 2.10 Exercises

Throughout these exercises we consider a point whose Cartesian position vector, relative to an arbitrary origin, is written

$$\mathbf{x} = x \hat{\mathbf{x}} + y \hat{\mathbf{y}} + z \hat{\mathbf{z}} \quad (2.94)$$

and whose squared distance from the origin is

$$r^2 = \mathbf{x} \cdot \mathbf{x} = x^2 + y^2 + z^2. \quad (2.95)$$

## EXERCISE 2.1: PRACTICE WITH THE GRADIENT OPERATOR

Prove the following identities:

- (a)  $\nabla(|\mathbf{x}|) = \mathbf{x} |\mathbf{x}|^{-1} \equiv \hat{\mathbf{r}}$
- (b)  $\nabla \ln |\mathbf{x}| = \mathbf{x} |\mathbf{x}|^{-2} = \hat{\mathbf{r}} |\mathbf{x}|^{-1}$
- (c)  $\nabla |\mathbf{x}|^{-1} = -\mathbf{x} |\mathbf{x}|^{-3} = -\hat{\mathbf{r}} |\mathbf{x}|^{-2}$ .

## EXERCISE 2.2: PRACTICE WITH THE LAPLACIAN OPERATOR

Show that the Laplacian of the function

$$\psi = \frac{z x^2}{r^2} \quad (2.96)$$

is given by

$$\nabla^2 \psi = \frac{2 z (r^2 - 5 x^2)}{r^4}. \quad (2.97)$$

Perform the proof using both Cartesian coordinates as well as spherical coordinates (see Figure 8.1), making use of the following expressions for Laplacian operator acting on a scalar field

$$\nabla^2 \psi(x, y, z) = \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + \frac{\partial^2 \psi}{\partial z^2} \quad (2.98a)$$

$$\nabla^2 \psi(\lambda, \phi, r) = \frac{1}{r^2 \cos \phi} \left[ \frac{1}{\cos \phi} \frac{\partial^2 \psi}{\partial \lambda^2} + \frac{\partial}{\partial \phi} \left( \cos \phi \frac{\partial \psi}{\partial \phi} \right) + \cos \phi \frac{\partial}{\partial r} \left( r^2 \frac{\partial \psi}{\partial r} \right) \right]. \quad (2.98b)$$

## EXERCISE 2.3: MORE PRACTICE WITH OPERATORS

Prove the following identities with  $r \neq 0$ :

- (a)  $\nabla^2 r^{-1} = 0$
- (b)  $\nabla \cdot (\mathbf{x}/r^3) = 0$
- (c)  $\nabla \cdot (\mathbf{A} \times \mathbf{x}) = \mathbf{x} \cdot (\nabla \times \mathbf{A})$  for an arbitrary vector field  $A(\mathbf{x})$ .
- (d)  $\nabla \times [\mathbf{x} f(r)] = 0$  for an arbitrary function  $f(r) = f(|\mathbf{x}|)$ .

## EXERCISE 2.4: SOLID-BODY ROTATION

Define a velocity field according to

$$\mathbf{v} = \boldsymbol{\Omega} \times \mathbf{x} \quad (2.99)$$

with  $\boldsymbol{\Omega}$  a spatially constant angular rotation velocity (e.g., rotation of the earth). This velocity field describes solid-body rotation as discussed in Section 32.5. Show that  $2 \boldsymbol{\Omega} = \nabla \times \mathbf{v}$ . See also Exercise 32.1.

## EXERCISE 2.5: DIVERGENCE-FREE AND IRRATIONAL VECTOR

Let  $\Phi$  be a harmonic function so that  $\nabla^2 \Phi = 0$ . Show that  $\mathbf{v} = -\nabla \Phi$  satisfies

- (a)  $\nabla \cdot \mathbf{v} = 0$
- (b)  $\nabla \times \mathbf{v} = 0$ .

In this way we prove that all harmonic scalar fields correspond to a divergence-free and curl-free vector field.

## EXERCISE 2.6: CONSERVATIVE VECTOR FIELD AND SCALAR POTENTIAL

Show that the curl,  $\nabla \times \mathbf{F}$ , of the following vector field vanishes

$$\mathbf{F} = 2xz\hat{\mathbf{x}} + 2yz^2\hat{\mathbf{y}} + (x^2 + 2y^2z - 1)\hat{\mathbf{z}}. \quad (2.100)$$

Hence, deduce that  $\mathbf{F}$  is a *conservative vector field*, meaning that it can be written as the gradient of a scalar potential  $\psi$  according to  $\mathbf{F} = -\nabla\psi$ , where (to within an arbitrary constant)

$$\psi = -[x^2z + (yz)^2 - z]. \quad (2.101)$$

## EXERCISE 2.7: PRODUCT RULE IDENTITIES

Prove the following identities for vectors in  $\mathbb{R}^3$ :

$$(a) \mathbf{F} = \partial_n(F_n \mathbf{x}) - \mathbf{x} \nabla \cdot \mathbf{F}$$

$$(b) 2F_m = [\mathbf{x} \times (\nabla \times \mathbf{F})]_m - \partial_m(\mathbf{x} \cdot \mathbf{F}) + \nabla \cdot (\mathbf{x} F_m).$$

Make use of Cartesian tensors and show all relevant steps, including use of the Levi-Civita tensor from Section 1.4.1 for the cross-product.

As discussed in Section 12.4.1 of [Bühler \(2014a\)](#), these product rule identities have use for the study of impulses imparted by a body force per volume,  $\mathbf{F}$ , to a fluid on an unbounded domain where the force has compact support (i.e., the force vanishes outside a finite domain). In that case the above product rule identities allow us to make use of the corresponding integral identities

$$\int \mathbf{F} dV = - \int \mathbf{x} \nabla \cdot \mathbf{F} dV = \frac{1}{2} \int \mathbf{x} \times (\nabla \times \mathbf{F}) dV. \quad (2.102)$$

## EXERCISE 2.8: BELTRAMI FLOW

Beltrami flow is defined by velocity and vorticity fields satisfying

$$\nabla \cdot \mathbf{v} = 0 \quad (2.103a)$$

$$\boldsymbol{\omega} = \nabla \times \mathbf{v} = \lambda \mathbf{v} \quad (2.103b)$$

where  $\lambda$  is a constant. Show that the following velocity field is a Beltrami flow

$$\mathbf{v} = (A \sin z + C \cos y) \hat{\mathbf{x}} + (B \sin x + A \cos z) \hat{\mathbf{y}} + (C \sin y + B \cos x) \hat{\mathbf{z}}, \quad (2.104)$$

where  $A, B, C$  are constants. Hint: the solution follows directly from computing

$$u = \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \quad v = \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \quad w = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}. \quad (2.105)$$

## EXERCISE 2.9: PRACTICE WITH PATH INTEGRALS

Consider the vector field

$$\mathbf{F} = xy^2 \hat{\mathbf{x}} + 2y\hat{\mathbf{y}} + x\hat{\mathbf{z}}. \quad (2.106)$$

Let  $\mathcal{L}$  be a path parameterized by

$$x = ct \quad y = c/t \quad z = d \quad t \in [1, 2], \quad (2.107)$$

where  $c$  and  $d$  are constants. Show that the following identities hold

$$\int_{\mathcal{L}} \mathbf{F} dt = c^3 \ln 2 \hat{\mathbf{x}} + 2 \hat{\mathbf{y}} + \frac{3c}{2} \hat{\mathbf{z}} \quad (2.108a)$$

$$\int_{\mathcal{L}} \mathbf{F} dy = -\frac{3c^4}{8} \hat{\mathbf{x}} - c \hat{\mathbf{y}} - c^2 \ln 2 \hat{\mathbf{z}} \quad (2.108b)$$

$$\int_{\mathcal{L}} \mathbf{F} \cdot d\mathbf{x} = c^4 \ln 2 - c, \quad (2.108c)$$

where  $d\mathbf{x} = \hat{\mathbf{x}} dx + \hat{\mathbf{y}} dy + \hat{\mathbf{z}} dz$ . Although all three integrals are computed along the same path, they are not necessarily of the same type. In particular, the first two integrals are vector fields, whereas the third integral is a scalar.

#### EXERCISE 2.10: STOKES' THEOREM ON A PLANE

Show that

$$\mathcal{I} = \oint_{\partial\mathcal{S}} [y(4x^2 + y^2) dx + x(2x^2 + 3y^2) dy] = \frac{\pi}{2} b a^3 \quad (2.109)$$

when integrating around the boundary of an ellipse  $\mathcal{S}$  defined by

$$\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1, \quad (2.110)$$

where  $a, b$  are constants. Hint: make use of Stokes' Theorem on a plane, otherwise known as Green's Theorem. Also make use of the substitution  $x = a \cos \phi$  and the identity

$$\int_{\pi}^0 \sin^2(2\phi) d\phi = -\frac{\pi}{2}. \quad (2.111)$$

#### EXERCISE 2.11: PRACTICE WITH GAUSS'S DIVERGENCE THEOREM

We here demonstrate the validity of Gauss's divergence theorem for a particular vector field

$$\mathbf{F} = \frac{\alpha \mathbf{x}}{(r^2 + a^2)^{3/2}}, \quad (2.112)$$

where  $\alpha$  and  $a$  are constants and  $r^2 = \mathbf{x} \cdot \mathbf{x}$  is the squared radial distance to a point. Using fluid mechanics jargon, we think of  $\mathbf{F}$  as a matter flux with physical dimensions of  $M L^{-2} T^{-1}$  (mass length $^{-2}$  time $^{-1}$ ). Now compute the transport of  $\mathbf{F}$  through a spherical surface,  $\mathcal{S}$ , of radius  $|\mathbf{x}| = a\sqrt{3}$

$$\Phi = \oint_{|\mathbf{x}|=a\sqrt{3}} \mathbf{F} \cdot \hat{\mathbf{n}} d\mathcal{S} = \frac{3\pi\alpha\sqrt{3}}{2}. \quad (2.113)$$

With  $\mathbf{F}$  a matter flux then  $\Phi$  has physical dimensions of  $M T^{-1}$ , so that it is the *mass transport* through the spherical surface. Next, show that this transport is equal to the integral of the divergence over the volume of the sphere

$$\Phi = \int_{|\mathbf{x}|=a\sqrt{3}} \nabla \cdot \mathbf{F} dV. \quad (2.114)$$

We thus verify, for this particular vector field, the divergence theorem

$$\int_{\mathcal{R}} \nabla \cdot \mathbf{F} dV = \oint_{\partial\mathcal{R}} \mathbf{F} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (2.115)$$

where  $\hat{\mathbf{n}}$  is the outward normal on the bounding surface  $\mathcal{S}$ .

**EXERCISE 2.12: MORE PRACTICE WITH GAUSS'S DIVERGENCE THEOREM**

Prove the following identities, which are readily shown using Gauss's divergence theorem.

- (a)  $\oint_{\partial\mathcal{R}} \mathbf{x} \cdot \hat{\mathbf{n}} d\mathcal{S} = 3 \int_{\mathcal{R}} dV = 3V$ , where  $\mathcal{R}$  is a closed region bounded by  $\partial\mathcal{R}$  and with volume  $\int_{\mathcal{R}} dV = V$ .
- (b)  $\oint_{\partial\mathcal{R}} (\hat{\mathbf{n}} \times \mathbf{F}) d\mathcal{S} = \int_{\mathcal{R}} \nabla \times \mathbf{F} dV$ , for an arbitrary vector field  $\mathbf{F}$  and with  $\hat{\mathbf{n}}$  the outward normal on the bounding surface  $\partial\mathcal{R}$ . Hint: in a manner similar to the result shown in Section 2.7.2, make use of Gauss's theorem with  $\mathbf{A} = \mathbf{F} \times \mathbf{C}$  where  $\mathbf{C}$  is a constant vector.
- (c) Let  $\partial\mathcal{R}$  be a closed surface bounding a volume  $\mathcal{R}$ , and let  $\mathbf{x}$  denote the position vector of a point measured from an arbitrary origin. Prove the following

$$\oint_{\partial\mathcal{R}} \frac{\hat{\mathbf{n}} \cdot \mathbf{x}}{r^3} d\mathcal{S} = \begin{cases} 0 & \text{if the origin lies outside of } \partial\mathcal{R} \\ 4\pi & \text{if the origin lies inside of } \partial\mathcal{R}. \end{cases} \quad (2.116)$$

**EXERCISE 2.13: HELMHOLTZ DECOMPOSITION FOR CORIOLIS ACCELERATION**

Consider a vector field

$$\mathbf{F} = 2\boldsymbol{\Omega} \times \mathbf{v}, \quad (2.117)$$

where  $\boldsymbol{\Omega}$  is a spatial constant and  $\nabla \cdot \mathbf{v} = 0$ . As seen in Part IV of this book, the vector  $\mathbf{F}$  is minus the Coriolis acceleration in the presence of an incompressible velocity. Since  $\mathbf{v}$  is non-divergent, there exists a vector potential so that

$$\mathbf{v} = \nabla \times \mathbf{B}. \quad (2.118)$$

Show that we can perform a Helmholtz decomposition

$$\mathbf{F} = 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla\Psi + \nabla \times \mathbf{A}, \quad (2.119)$$

where

$$-\nabla^2\Psi = -2\boldsymbol{\Omega} \cdot (\nabla \times \mathbf{v}) \quad (2.120a)$$

$$\nabla \times \mathbf{A} = (\boldsymbol{\Omega} \cdot \nabla) \mathbf{B} + \nabla\lambda, \quad (2.120b)$$

with  $\lambda$  an arbitrary gauge function.



# Chapter 3

## Partial differential equations

Fluid mechanics is a classical field theory whose mathematical description involves partial differential equations (PDEs). Although most of these PDEs are nonlinear, some are linear. Regardless, an understanding of linear PDEs provides useful insights into the physics and maths of geophysical fluids. For this purpose, we here study linear PDEs.

### CHAPTER GUIDE

One can penetrate much of this book without reading this chapter. What this chapter adds, however, is an appreciation for the mathematical structure and physical behavior of the equations describing geophysical fluid mechanics. Indeed, it is remarkable how useful it is, both mathematically and physically, to develop a rudimentary understanding of linear PDEs. Furthermore, those aiming to develop solution methods, either analytical or numerical, should have a working knowledge of this chapter. Additionally, the Green's function method detailed in Chapter 4 assumes a firm understanding of the material in this chapter.

There are many resources devoted to the theory and application of PDEs throughout physics, engineering, and applied mathematics. Chapter 8 of *Hildebrand* (1976) offers a pedagogical starting point whereas *Stakgold* (2000a,b) thoroughly develops the theory and methods available for boundary value problems encountered in physics. *Duchateau and Zachmann* (1986) concisely summarize PDEs and provide nearly 300 worked exercises, with much of the presentation in this chapter following their treatment.

3.1	Loose threads . . . . .	46
3.2	The advection equation . . . . .	46
3.2.1	Constant advection velocity . . . . .	46
3.2.2	Specifying the arbitrary functions resulting from PDEs . . . . .	47
3.2.3	Further study . . . . .	47
3.3	Characteristic curves for first order PDEs . . . . .	48
3.3.1	General formulation . . . . .	48
3.3.2	Examples . . . . .	49
3.4	Classifying second order PDEs . . . . .	50
3.5	Elliptic partial differential equations . . . . .	50
3.5.1	Some general properties of Laplace's equation . . . . .	51
3.5.2	Mean-value property of harmonic functions . . . . .	51
3.5.3	Laplace's boundary value problem . . . . .	52

---

3.5.4	Poisson's equation . . . . .	53
3.5.5	Extended max-min principle for Poisson's equation . . . . .	53
3.5.6	Poisson's boundary value problem . . . . .	54
3.6	Parabolic partial differential equations . . . . .	<b>54</b>
3.6.1	Initial and initial-boundary value problems . . . . .	55
3.6.2	Smoothing property . . . . .	55
3.6.3	Duhamel's superposition integral for the heat equation . . . . .	56
3.6.4	Further study . . . . .	57
3.7	Hyperbolic partial differential equations . . . . .	<b>57</b>
3.7.1	Initial value problem for the infinite-domain wave equation . . . . .	58
3.7.2	Domain of influence for wave signals . . . . .	59
3.7.3	Helmholtz equation . . . . .	60
3.7.4	Duhamel's superposition integral for the wave equation . . . . .	60
3.7.5	Further study . . . . .	62
3.8	Evolution of time averages . . . . .	<b>62</b>
3.8.1	Time averages . . . . .	63
3.8.2	Massaging the double time integrals . . . . .	63
3.8.3	Making use of a double integral identity . . . . .	64

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## 3.1 Loose threads

- Basics of wave kinematics in Section 3.7

## 3.2 The advection equation

Consider a tracer concentration,  $C$ , which for present purposes is a scalar field that is a function of space and time. As derived in Section 46.5, the tracer concentration in the absence of diffusion satisfies the advection equation

$$\frac{\partial C}{\partial t} + \mathbf{v} \cdot \nabla C = 0. \quad (3.1)$$

The highest derivatives in both space and time are first order, indicating that the advection equation is a first order partial differential equation. It is a nonlinear PDE for *active* tracers such as temperature, where active tracers affect the velocity through changes to density and hence to pressure. In contrast, the advection equation is linear for *passive* tracers (e.g., colored dye, dust), which are tracers that do not significantly alter velocity (Section 15.2). We limit the present discussion to passive tracers so that the advection equation is linear.

### 3.2.1 Constant advection velocity

To expose the gist of the advection equation, consider one space dimension and let the advection velocity be constant in space and time,

$$\frac{\partial C}{\partial t} + U \frac{\partial C}{\partial x} = 0 \quad (3.2)$$

where  $U$  is a constant velocity in the  $\hat{x}$  direction. An inspired guess reveals that

$$C(x, t) = \Gamma(x - Ut) \quad (3.3)$$

is a general solution to equation (3.2), where  $\Gamma$  is an arbitrary differentiable function that is determined by the initial conditions of the tracer field. Verification of this result is readily found

by noting

$$\frac{\partial C}{\partial x} = \frac{d\Gamma(x - Ut)}{d(x - Ut)} \frac{\partial(x - Ut)}{\partial x} = \Gamma' \quad (3.4a)$$

$$\frac{\partial C}{\partial t} = \frac{d\Gamma(x - Ut)}{d(x - Ut)} \frac{\partial(x - Ut)}{\partial t} = -\Gamma' U. \quad (3.4b)$$

The functional dependence  $x - Ut$  reveals that as time progresses with  $U > 0$ , an observer that moves in the positive  $\hat{x}$  direction with a speed  $U$  maintains a constant argument to the tracer concentration. This behavior means that the tracer concentration is transported by advection with a speed  $U$  without changing its structure. We illustrate this behavior in Figure 3.1.

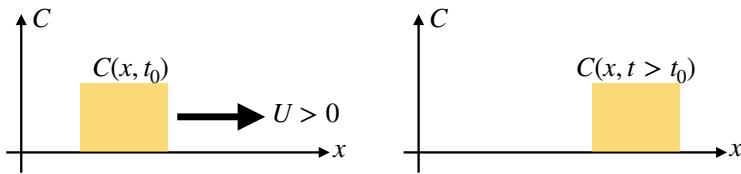


FIGURE 3.1: Illustrating the advection of a scalar field resulting from a constant advection velocity  $\mathbf{v} = U\hat{x}$  with  $U > 0$ . The initially square pulse of tracer concentration is translated, unchanged, by the constant advection velocity.

### 3.2.2 Specifying the arbitrary functions resulting from PDEs

As revealed from the above example, the solution to a PDE is typically given in terms of an arbitrary function with a specified dependence on the independent variables. The function itself is unspecified without additional information from initial and/or boundary conditions. For example, consider an initial tracer concentration in the form of a sine-wave

$$C(x, t = 0) = C_0 \sin x, \quad (3.5)$$

and allow the domain to be infinite in extent (no boundaries). When advected by a constant advection velocity, the solution to the advection equation is a tracer concentration in the form of a sine-wave moving in the positive  $\hat{x}$  direction with speed  $U$

$$C(x, t) = C_0 \sin(x - Ut). \quad (3.6)$$

The arbitrary functional degree of freedom is reminiscent of ordinary differential equations, whose solutions are specified up to unknown constants with values set by initial and/or boundary conditions.

### 3.2.3 Further study

Advection plays a fundamental role in the transport of matter, energy, and momentum within fluids. As seen in our discussion of fluid kinematics in Chapter 12, advection appears in the fluid mechanical equations when viewing the fluid from the fixed laboratory or *Eulerian* reference frame. We thus encounter advection throughout this book, with further development of the mathematics and physics provided in Sections 46.5 and 46.6.

### 3.3 Characteristic curves for first order PDEs

The advection equation is the canonical first order PDE commonly found in fluid mechanics. A more general form for a first order PDE in one space dimension is given by<sup>1</sup>

$$P(x, t, \psi) \frac{\partial \psi}{\partial x} + Q(x, t, \psi) \frac{\partial \psi}{\partial t} = R(x, t, \psi), \quad (3.7)$$

where  $P$ ,  $Q$ , and  $R$  are arbitrary smooth functions. This PDE is linear if  $P$ ,  $Q$ , and  $R$  are independent of  $\psi$ , and quasi-linear if  $P$  and  $Q$  are independent of  $\psi$  and  $R$  is at most a linear function of  $\psi$ . In this section we develop a formalism that determines the functional dependence of solutions to these PDEs. This *method of characteristics* is quite useful for exposing general properties of the solutions, even for those cases where the solution is not analytically available.

#### 3.3.1 General formulation

In the first order PDE given by equation (3.7), assume there is a functional relation

$$\Upsilon(x, t, \psi) = \text{constant} \quad (3.8)$$

that determines  $\psi$  consistent with the PDE (3.7). We refer to  $\Upsilon$  as an *integral surface* that specifies a solution to the PDE. For  $\Upsilon$  to specify an integral surface it must satisfy

$$d\Upsilon = 0, \quad (3.9)$$

so that

$$\frac{d\Upsilon}{dt} = 0 = \frac{\partial \Upsilon}{\partial \psi} \frac{\partial \psi}{\partial t} + \frac{\partial \Upsilon}{\partial t} \quad (3.10a)$$

$$\frac{d\Upsilon}{dx} = 0 = \frac{\partial \Upsilon}{\partial \psi} \frac{\partial \psi}{\partial x} + \frac{\partial \Upsilon}{\partial x}. \quad (3.10b)$$

Assuming  $\partial \Upsilon / \partial \psi \neq 0$  we can write

$$\frac{\partial \psi}{\partial t} = -\frac{\partial \Upsilon / \partial t}{\partial \Upsilon / \partial \psi} \quad \text{and} \quad \frac{\partial \psi}{\partial x} = -\frac{\partial \Upsilon / \partial x}{\partial \Upsilon / \partial \psi} \quad (3.11)$$

so that the first order PDE (3.7) takes on the equivalent form

$$P \frac{\partial \Upsilon}{\partial x} + Q \frac{\partial \Upsilon}{\partial t} + R = 0. \quad (3.12)$$

Through this construct we have brought the functions  $P, Q, R$  into a symmetric form. Consistency of equation (3.12) with

$$d\Upsilon = \frac{\partial \Upsilon}{\partial x} dx + \frac{\partial \Upsilon}{\partial t} dt + \frac{\partial \Upsilon}{\partial \psi} d\psi = 0, \quad (3.13)$$

requires

$$P = \mu dx \quad \text{and} \quad Q = \mu dt \quad \text{and} \quad R = \mu d\psi, \quad (3.14)$$

---

<sup>1</sup>We here summarize the presentation in Section 8.2 of *Hildebrand* (1976).

for some non-dimensional function  $\mu(x, t, \psi)$ . Eliminating the unknown function  $\mu$  renders the ordinary differential equations

$$\frac{dx}{P} = \frac{dt}{Q} = \frac{d\psi}{R}. \quad (3.15)$$

Paths in  $(x, t, \psi)$  space that satisfy these differential equations are known as *characteristic curves*. Note that if any one of the functions  $P$ ,  $Q$ , or  $R$  vanish, then we merely remove that term from these relations.

### 3.3.2 Examples

We now illustrate the method of characteristics by considering some examples. First consider the linear homogeneous advection equation with constant advection speed

$$U \frac{\partial \psi}{\partial x} + \frac{\partial \psi}{\partial t} = 0, \quad (3.16)$$

in which we identify  $P = U$ ,  $Q = 1$ , and  $R = 0$ . The single ordinary differential equation defining the characteristic curve is given by

$$\frac{dx}{U} = \frac{dt}{1}, \quad (3.17)$$

so that characteristics are given by the family of space-time lines

$$x - Ut = \alpha \quad (3.18)$$

with  $\alpha$  an arbitrary constant. These lines determine the paths in space-time along which advective signals are transmitted.

Now add a constant source to the linear advection equation

$$U \frac{\partial \psi}{\partial x} + \frac{\partial \psi}{\partial t} = R. \quad (3.19)$$

The two ODEs defining the characteristic curve are

$$\frac{dx}{U} = \frac{dt}{1} = \frac{d\psi}{R}. \quad (3.20)$$

In addition to the relation  $x - Ut = \alpha_1$  determined from the homogeneous case, we also have  $\psi - Rt = \alpha_2$  for  $\alpha_2$  an arbitrary constant. Hence, the characteristic equations render the general solution of the form

$$\Gamma[x - Ut, \psi - Rt] = 0, \quad (3.21)$$

for  $\Gamma$  an arbitrary function. One example solution is given by

$$\psi = f(x - Ut) + Rt \quad (3.22)$$

for an arbitrary smooth function  $f$ . This solution has the form of a traveling signal,  $f(x - Ut)$ , plus a growing source,  $Rt$ .

For the final example, consider the linear advection equation with non-constant coefficients and non-constant source

$$x \frac{\partial \psi}{\partial x} + t \frac{\partial \psi}{\partial t} = \psi, \quad (3.23)$$

in which the ODEs determining the characteristics are given by

$$\frac{dx}{x} = \frac{dt}{t} = \frac{d\psi}{\psi}. \quad (3.24)$$

We are thus led to the relations

$$\frac{t}{x} = \alpha_1 \quad \frac{\psi}{x} = \alpha_2. \quad (3.25)$$

Hence, the general solution of the PDE (3.23) is given by

$$\Gamma(t/x, \psi/x) = 0 \Rightarrow \psi = x F(t/x) \quad (3.26)$$

for an arbitrary smooth function  $F$ .

## 3.4 Classifying second order PDEs

There are many second order PDEs appearing in fluid mechanics, a general form of which in one space dimension is given by

$$A \frac{\partial^2 \psi}{\partial x^2} + B \frac{\partial^2 \psi}{\partial x \partial t} + C \frac{\partial^2 \psi}{\partial t^2} = \Lambda. \quad (3.27)$$

For linear PDEs,  $A, B, C$  are arbitrary functions of space and time that are independent of  $\psi$ . Furthermore,  $\Lambda$  is a function of space and time and at most a linear function of  $\psi$  and its derivatives. The most general solution to a linear PDE consists of the sum of any *particular solution* and a solution to the homogeneous problem (where  $\Lambda = 0$ ).

The terms involving second derivatives in equation (3.27) are of principle importance for determining the character of the solutions, with importance placed on the sign of the discriminant  $B^2 - 4 A C$ . By analogy with conic sections we classify 2nd order PDEs as follows

$$\text{PDE form} = \begin{cases} \text{hyperbolic} & B^2 - 4 A C > 0 \\ \text{elliptic} & B^2 - 4 A C < 0 \\ \text{parabolic} & B^2 - 4 A C = 0. \end{cases} \quad (3.28)$$

We can further motivate this terminology by considering the case of a homogeneous constant coefficient PDE and an assumed solution of the form

$$\psi(x, t) = f(m x + t). \quad (3.29)$$

Plugging into the 2nd order PDE (3.27) with  $\Lambda = 0$  leads to

$$A m^2 + B m + C = 0. \quad (3.30)$$

The two solutions  $m_1$  and  $m_2$  are both real for the hyperbolic case, conjugate complex for the elliptic case, and a perfect square for the parabolic case.

## 3.5 Elliptic partial differential equations

The elliptic case from Section 3.4 has discriminant  $B^2 - 4 A C < 0$ , in which case there are two imaginary characteristics. The canonical example elliptic equation is Laplace's equation

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = 0, \quad (3.31)$$

where we converted from  $t$  as an independent variable to the space coordinate  $y$ . Formally, this transition is realized by setting  $t = iy$ , where  $i = \sqrt{-1}$ . Laplace's equation is satisfied by time-independent (i.e., *steady state*) solutions to the heat/diffusion equation (Section 3.6). Another common elliptic equation is Poisson's equation, which results from adding a source to Laplace's equation

$$\frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = \Lambda. \quad (3.32)$$

As there is no time present in the Laplace and Poisson equations, their solutions are global. That is, “signals” propagate instantaneously so that their structure is fully determined by specified boundary conditions or boundary *data*. Strictly speaking this behavior is not physical since all signals have a finite propagation speed no greater than the speed of light. However, an infinite speed can be a useful mathematical construct. For example, acoustic signals in fluids propagate much faster than other waves and particle speeds, and they carry a very small energy.<sup>2</sup> For many purposes it is thus suitable to assume acoustic speeds are infinite, and in so doing we *filter* them out of the dynamical equations. In the process, the hyperbolic equation describing acoustic signals is converted into an elliptic equation.

### 3.5.1 Some general properties of Laplace's equation

Solutions to Laplace's equation,  $\nabla^2 \psi = 0$ , are known as *harmonic functions*. Here are some example harmonic functions for two space dimensions:

$$\psi = x^3 - 3xy^2 \quad \psi = \ln(x^2 + y^2) \quad \psi = e^{\gamma x} \cos(\gamma y) \quad \psi = ax + by, \quad (3.33)$$

for arbitrary constants  $a, b, \gamma$ . Furthermore, with

$$\nabla^2(\psi\phi) = \psi\nabla^2\phi + 2\nabla\phi \cdot \nabla\psi + \phi\nabla^2\psi, \quad (3.34)$$

we see that the product of two harmonic functions ( $\nabla^2\psi = \nabla^2\phi = 0$ ) is itself harmonic if and only if their gradients are orthogonal,  $\nabla\psi \cdot \nabla\phi = 0$ . In the remainder of this section we present, without proof, some general properties of harmonic functions and develop self-consistency conditions for the boundary data appearing in the Laplacian boundary value problem defined below by equations (3.37a)-(3.37b).

### 3.5.2 Mean-value property of harmonic functions

Harmonic functions possess a remarkable *mean-value* property. This property says that the value of a harmonic function,  $\psi$ , at a point  $\mathbf{x}_o$  within an open region of  $\mathcal{R}$  equals to the average of  $\psi$  taken over the surface of a sphere within  $\mathcal{R}$  centered at  $\mathbf{x}_o$ . In equations this property states that

$$\psi(\mathbf{x}_o) = \frac{\oint_{\mathcal{S}_R} \psi(\mathbf{x}) d\mathcal{S}}{\oint_{\mathcal{S}_R} d\mathcal{S}}, \quad (3.35)$$

where  $\mathcal{S}_R$  is a sphere with radius  $R$  centered at  $\mathbf{x}_o$  with “area” given by

$$\oint_{\mathcal{S}_R} d\mathcal{S} = \begin{cases} 2\pi R & n = 2 \text{ space dimensions} \\ 4\pi R^2 & n = 3 \text{ space dimensions.} \end{cases} \quad (3.36)$$

---

<sup>2</sup>A scuba diver feeling the beat of a ship underwater, or an audience member at a rock concert may question this statement. However, acoustic energy is in fact tiny relative to planetary waves and gravity waves, and utterly negligible for studies of large scale geophysical fluid motions.

We illustrate this property in Figure 3.2.

The mean-value property of harmonic functions holds anywhere within the domain where  $\nabla^2\psi = 0$ , so long as the sphere is fully contained within that domain. It implies that there can be no extrema of  $\psi$  within the domain, since if there was an extrema then it could not satisfy the mean-value property. Hence, all extrema of harmonic functions must exist on the domain boundary. These properties lend mathematical support for considering harmonic functions to be solutions to continuous physical systems that are in equilibrium or a steady state. As a physical example, consider a temperature field,  $T(\mathbf{x})$ , in a region with zero heat sources and zero fluid flow. As shown in Section 46.3.4, the steady state temperature satisfies  $\nabla^2T = 0$ , and as such it is harmonic and hence has no extrema within the domain.

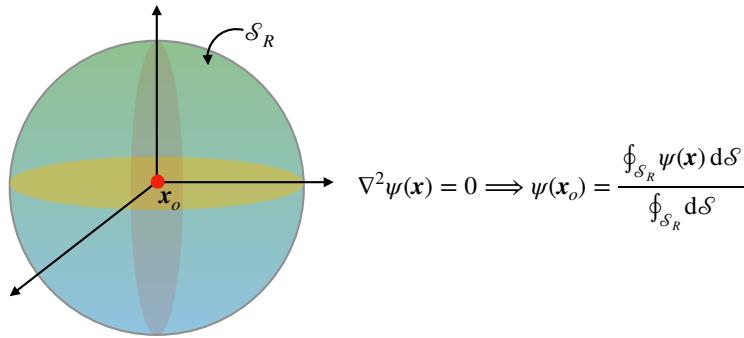


FIGURE 3.2: The value of a harmonic function at a point  $\mathbf{x}_o$  equals to the area average of the function over a sphere centered at  $\mathbf{x}_o$ . We here illustrate this property for 3-dimensions, but it holds for arbitrary space dimensions.

### 3.5.3 Laplace's boundary value problem

Laplace's equation requires boundary conditions to fully specify the unknown harmonic function. We here consider the Laplacian *boundary value problem* in the form

$$\nabla^2\psi = 0 \quad \mathbf{x} \in \mathcal{R} \quad (3.37a)$$

$$\alpha\psi + \beta\hat{\mathbf{n}} \cdot \nabla\psi = \sigma \quad \mathbf{x} \in \partial\mathcal{R}, \quad (3.37b)$$

where  $\mathcal{R}$  is a smooth and simply connected volume,  $\partial\mathcal{R}$  is the boundary surface enclosing  $\mathcal{R}$  and with outward normal  $\hat{\mathbf{n}}$ , and  $\alpha$ ,  $\beta$ , and  $\sigma$  are given boundary data functions.

We can establish constraints on the boundary conditions that lead to a self-consistent Laplacian boundary value problem (3.37a)-(3.37b). We do so through the use of Gauss's divergence theorem (Section 2.7) in which integration over the full domain leads to

$$0 = \int_{\mathcal{R}} \nabla^2\psi dV = \oint_{\partial\mathcal{R}} \hat{\mathbf{n}} \cdot \nabla\psi d\mathcal{S}. \quad (3.38)$$

In physical applications the boundary condition (3.37b) usually appears with either  $\alpha = 0$  or  $\beta = 0$ , and these two cases are associated with distinct self-consistency constraints.

#### *Dirichlet boundary condition*

The case with  $\beta = 0$  is referred to as a *Dirichlet* boundary condition whereby

$$\psi = \sigma \quad \mathbf{x} \in \partial\mathcal{R}, \quad (3.39)$$

where we set  $\alpha = 1$  without loss of generality. In this case all boundary data result in a self-consistent Laplacian boundary value problem so there is no constraint on  $\sigma$ . Thinking again about temperature, this boundary condition specifies the temperature on the domain boundary to equal  $T = \sigma$ , with all boundary functions  $\sigma$  consistent with a harmonic temperature distribution within the domain interior.

#### *Neumann boundary condition*

The case with  $\alpha = 0$  results in a *Neumann* boundary condition. Without loss of generality we set  $\beta = 1$  and reach the following self-consistency condition

$$\oint_{\partial\mathcal{R}} \sigma \, dS = 0. \quad (3.40)$$

That is, a self-consistent boundary condition for Laplace's equation with a Neumann boundary condition must satisfy this surface integral constraint. For the temperature example, this boundary condition says that to realize a steady state harmonic temperature distribution within a region, we can at most apply a zero area averaged boundary heating. If the boundary constraint (3.40) is not satisfied, then the interior temperature field cannot be harmonic so that it will not be in a steady state.

#### 3.5.4 Poisson's equation

The generic boundary value problem for Poisson's equation takes on the form

$$\nabla^2 \psi = \Lambda \quad \mathbf{x} \in \mathcal{R} \quad (3.41a)$$

$$\alpha \psi + \beta \hat{\mathbf{n}} \cdot \nabla \psi = \sigma \quad \mathbf{x} \in \partial\mathcal{R}, \quad (3.41b)$$

where  $\Lambda(\mathbf{x})$  is a specified source function. We here present, without proof, some general properties of solutions to Poisson's equation and develop self-consistency conditions for the boundary data appearing in equation (3.41b).

#### 3.5.5 Extended max-min principle for Poisson's equation

A subharmonic function is one where

$$\nabla^2 \psi = \Lambda \geq 0 \quad \mathbf{x} \in \mathcal{R}. \quad (3.42)$$

Here, the source function makes the curvature of a subharmonic function positive. Correspondingly, every point within  $\mathcal{R}$  satisfies the minimum principle

$$\psi(\mathbf{x}_o) \leq \frac{\oint_{\mathcal{S}_R} \psi(\mathbf{x}) \, dS}{\oint_{\mathcal{S}_R} dS}, \quad (3.43)$$

for spheres,  $\mathcal{S}_R$ , that are fully within  $\mathcal{R}$ . The signs switch for superharmonic functions whereby  $\nabla^2 \psi \leq 0$  for  $\mathbf{x} \in \mathcal{R}$ .

Returning to the temperature example, consider a temperature field in a region with a positive heat source,  $\Lambda > 0$ . The steady state temperature in the presence of zero fluid flow satisfies Poisson's equation  $\nabla^2 T = \Lambda \geq 0$  for regions with the heat source. The minimum principle (3.43) means that the temperature at any point within the heating region is less than the temperature averaged over a sphere centered on the point, so long as the sphere remains within the region of

heating. It is only in the absence of a heat source or sink, where  $\nabla^2 T = 0$ , that we recover the mean-value property of harmonic functions given by equation (3.35).

### 3.5.6 Poisson's boundary value problem

We follow the method in Section 3.5.3 to develop constraints on the boundary conditions applied as part of the Poisson boundary value problem (3.41a)-(3.41b). Use of Gauss's divergence theorem leads to the constraint

$$\oint_{\partial\mathcal{R}} \hat{\mathbf{n}} \cdot \nabla \psi \, d\mathcal{S} = \int_{\mathcal{R}} \Lambda \, dV. \quad (3.44)$$

We separately consider the Dirichlet and Neumann cases.

#### *Dirichlet boundary condition*

The Dirichlet condition with  $\beta = 0$  leads to

$$\psi = \sigma \quad \mathbf{x} \in \partial\mathcal{R}. \quad (3.45)$$

Just as for Laplace's boundary value problem, all boundary data result in a self-consistent Poisson boundary value problem so there is no constraint on  $\sigma$ . Thinking again about temperature, this boundary condition specifies the temperature on the domain boundary to equal  $T = \sigma$ , with all boundary functions  $\sigma$  consistent with the interior heating  $\Lambda$  and a temperature field satisfying  $\nabla^2 T = \Lambda$  within the interior.

#### *Neumann boundary condition*

The *Neumann* boundary condition leads to the following self-consistency condition

$$\oint_{\partial\mathcal{R}} \sigma \, d\mathcal{S} = \int_{\mathcal{R}} \Lambda \, dV. \quad (3.46)$$

That is, a self-consistent boundary condition for Poisson's equation with a Neumann boundary condition must satisfy this surface integral constraint. For the temperature example, this boundary condition says that the area integrated boundary data must be consistent with the volume integrated source function in order for the temperature to satisfy Poisson's equation. Otherwise, the temperature field will evolve in time and thus not be in a steady state.

## 3.6 Parabolic partial differential equations

The parabolic case from Section 3.4,  $B^2 - 4AC = 0$ , contains a single real characteristic. The canonical example is the *heat equation*, which is also known as the *diffusion equation*

$$\frac{\partial \psi}{\partial t} = \kappa \frac{\partial^2 \psi}{\partial x^2}, \quad (3.47)$$

where  $\kappa > 0$  is the kinematic diffusivity with dimensions of squared length per time.

### 3.6.1 Initial and initial-boundary value problems

The *Cauchy Problem* is the name given to the initial value problem for the heat equation over all space, here given by Euclidean space

$$\frac{\partial \psi}{\partial t} = \kappa \nabla^2 \psi \quad \mathbf{x} \in \mathbb{R}^n, t > 0 \quad (3.48a)$$

$$\psi(\mathbf{x}, t = 0) = \sigma(\mathbf{x}) \quad \mathbf{x} \in \mathbb{R}^n \quad (3.48b)$$

$$|\psi(\mathbf{x}, t)| < \infty \quad \mathbf{x} \in \mathbb{R}^n, t > 0. \quad (3.48c)$$

The general initial-boundary value problem over a finite domain  $\mathcal{R}$  takes the form

$$\frac{\partial \psi}{\partial t} = \kappa \nabla^2 \psi \quad \mathbf{x} \in \mathcal{R}, t > 0 \quad (3.49a)$$

$$\psi(\mathbf{x}, t = 0) = \sigma(\mathbf{x}) \quad \mathbf{x} \in \mathcal{R} \quad (3.49b)$$

$$\alpha(\mathbf{x}) \psi(\mathbf{x}, t) + \beta(\mathbf{x}) \hat{\mathbf{n}} \cdot \nabla \psi(\mathbf{x}, t) = g(\mathbf{x}, t) \quad \mathbf{x} \in \partial \mathcal{R}, t > 0, \alpha \beta \geq 0. \quad (3.49c)$$

Following from the discussion of Laplace's and Poisson's boundary value problems, choices for the boundary functions  $\alpha$  and  $\beta$  impact on the character of the boundary conditions. The Neumann condition is most commonly applied to set the flux of a tracer or temperature at the boundaries. The alternative use of the Dirichlet condition is commonly applied for idealized "diagnostic" tracers in geophysical fluid applications.

### 3.6.2 Smoothing property

The extended max-min principle from Section 3.5.5 holds also for the heat equation, which is consistent with solutions to the heat equation generally decaying their initial condition towards zero by reducing the amplitude of all extrema. Hence, no extrema are introduced in the interior of the domain by the heat equation; extrema only arise via boundary and/or initial conditions. Furthermore, the steady state limit of the heat equation is a harmonic function, and so solves Laplace's equation whereby the mean-value property holds (Section 3.5.2). These characteristics of the heat equation are generally shared by all linear parabolic PDEs.

#### *Illustrating the smoothing property in a finite domain*

We illustrate the smoothing property for the specific case of the one-dimensional initial-boundary value problem with homogeneous Dirichlet boundary conditions

$$\frac{\partial \psi}{\partial t} = \kappa \frac{\partial^2 \psi}{\partial x^2} \quad 0 < x < L, t > 0 \quad (3.50a)$$

$$\psi(x, t) = I(x) \quad 0 < x < L, t = 0 \quad (3.50b)$$

$$\psi(0, t) = \psi(L, t) = 0 \quad t > 0. \quad (3.50c)$$

A variety of methods, such as separation of variables, can be used to derive the following Fourier series solution

$$\psi(x, t) = \sum_{n=1}^{\infty} I_n e^{-\kappa t (n\pi/L)^2} \sin(n\pi x/L) \quad \text{with} \quad I_n = \frac{2}{L} \int_0^L I(x) \sin(n\pi x/L) dx. \quad (3.51)$$

As per the smoothing property of diffusion, note how the amplitude of each Fourier mode decays exponentially in time.

*Smoothing property for an initial value problem on the real line*

Now consider the one-dimensional heat equation on the real line, with the only boundary conditions being regularity at infinity

$$\frac{\partial \psi}{\partial t} = \kappa \frac{\partial^2 \psi}{\partial x^2} \quad -\infty < x < \infty, t > 0 \quad (3.52a)$$

$$\psi(x, t) = I(x) \quad -\infty < x < \infty, t = 0. \quad (3.52b)$$

One can show by direct differentiation that the following Gaussian is a solution

$$\psi(x, t) = \frac{1}{\sqrt{4\pi\kappa t}} \int_{-\infty}^{\infty} I(\xi) \exp\left[-\frac{(x-\xi)^2}{4\kappa t}\right] d\xi. \quad (3.53)$$

Again, this function smooths/damps the initial condition function  $I(x)$  as time increases.

### 3.6.3 Duhamel's superposition integral for the heat equation

Consider a scalar field that starts from zero initial conditions and evolves in the presence of a source

$$\frac{\partial \Psi}{\partial t} = \kappa \nabla^2 \Psi + f(\mathbf{x}) \quad \mathbf{x} \in \mathbb{R}^n, t > 0 \quad (3.54a)$$

$$\Psi(\mathbf{x}, t) = 0 \quad \mathbf{x} \in \mathbb{R}^n, t = 0. \quad (3.54b)$$

Now consider the converse, in which another scalar field evolves without a source and yet is initialized according to the source

$$\frac{\partial \psi}{\partial t} = \kappa \nabla^2 \psi \quad \mathbf{x} \in \mathbb{R}^n, t > 0 \quad (3.55a)$$

$$\psi(\mathbf{x}, t) = f(\mathbf{x}) \quad \mathbf{x} \in \mathbb{R}^n, t = 0. \quad (3.55b)$$

The two scalar fields are related by *Duhamel's superposition integral*

$$\Psi(\mathbf{x}, t) = \int_0^t \psi(\mathbf{x}, t-\tau) d\tau. \quad (3.56)$$

We verify the connection by direct differentiation

$$\frac{\partial \Psi(\mathbf{x}, t)}{\partial t} = \psi(\mathbf{x}, 0) + \int_0^t \frac{\partial \psi(\mathbf{x}, t-\tau)}{\partial t} d\tau = f(\mathbf{x}) + \kappa \nabla^2 \Psi(\mathbf{x}, t). \quad (3.57)$$

Duhamel's superposition integral allows us to move the source from the partial differential operator into the initial conditions, and vice-versa. It says that the forced solution  $\Psi(\mathbf{x}, t)$  is built by time integrating the “retarded” values of the unforced solution  $\psi$  from the initial time  $t = 0$  to the current time  $t$ . Note that a more general presentation allows for the source function to be a function of time,  $f(\mathbf{x}, t)$ , in which case we must develop a family of solutions,  $\psi_f(\mathbf{x}, t; \tau)$ , generated by reinitializing  $\psi_f(\mathbf{x}, t = \tau; \tau) = f(\mathbf{x}, \tau)$  and then superposing the members of this family to generate  $\Psi(\mathbf{x}, t)$ .

As an example, consider the initial value problem for the heat equation on a line as given by

equations (3.52a)-(3.52b)

$$\frac{\partial \psi}{\partial t} = \kappa \frac{\partial^2 \psi}{\partial x^2} \quad -\infty < x < \infty, t > 0 \quad (3.58a)$$

$$\psi(x, t) = f(x) \quad -\infty < x < \infty, t = 0, \quad (3.58b)$$

whose solution is given by the Gaussian function in equation (3.53). Duhamel's superposition integral (3.56) says that

$$\Psi(x, t) = \int_0^t \psi(x, t - \tau) d\tau = \int_0^t \frac{1}{\sqrt{4\pi\kappa(t-\tau)}} \int_{-\infty}^{\infty} f(\xi) \exp\left[-\frac{(x-\xi)^2}{4\kappa(t-\tau)}\right] d\tau d\xi \quad (3.59)$$

satisfies the forced (inhomogeneous) initial value problem with zero initial condition

$$\frac{\partial \Psi}{\partial t} = \kappa \frac{\partial^2 \Psi}{\partial x^2} + f(x) \quad -\infty < x < \infty, t > 0 \quad (3.60a)$$

$$\Psi(x, t) = 0 \quad -\infty < x < \infty, t = 0. \quad (3.60b)$$

We make use of this result in our discussion of Green's functions in Chapter 4.

### 3.6.4 Further study

We examine physical and mathematical properties of the heat/diffusion equation in Sections 46.3 and 46.4. Section 9.11 of *Hildebrand (1976)* offers a lucid discussion of Duhamel's superposition integral.

## 3.7 Hyperbolic partial differential equations

The hyperbolic case from Section 3.4 has  $B^2 - 4AC > 0$  and thus contains two real characteristics. The canonical example of a hyperbolic PDE is the linear homogeneous wave equation

$$\frac{\partial^2 \psi}{\partial t^2} - U^2 \frac{\partial^2 \psi}{\partial x^2} = 0. \quad (3.61)$$

Solutions have the form of a moving wave in both directions (the two wave characteristics)

$$\psi(x, t) = \mathcal{F}(x - Ut) + \mathcal{G}(x + Ut), \quad (3.62)$$

where  $\mathcal{F}$  and  $\mathcal{G}$  are differentiable functions whose form is determined by the initial conditions. Note that we can factor the differential operator into the form

$$(\partial_t - U \partial_x)(\partial_t + U \partial_x)\psi = 0. \quad (3.63)$$

Consequently, if either one of the linear first-order PDEs are satisfied

$$(\partial_t - U \partial_x)\psi = 0 \quad (3.64a)$$

$$(\partial_t + U \partial_x)\psi = 0 \quad (3.64b)$$

then  $\psi$  will satisfy the full wave equation. These first-order PDEs are the one-dimensional advection equations considered in Section 3.3 with opposite advection direction, and each of which has a single characteristic. In this manner, we can think of advection by constant velocity as the

square root of the wave equation. Similarly, some disciplines refer to the linear advection equation (3.2), with constant advection speed, as the *one-way wave equation*.

### 3.7.1 Initial value problem for the infinite-domain wave equation

Since there are two time derivatives, specification of a solution requires initial conditions for the field and its first time derivative. To illustrate the structure of a solution to the wave equation, we develop a solution to the *Cauchy problem*, which is the initial value problem for the one-dimensional wave equation on the real line (infinite spatial domain so no boundary conditions)

$$\frac{\partial^2 \psi}{\partial t^2} = c^2 \frac{\partial^2 \psi}{\partial x^2} \quad -\infty < x < \infty, t > 0 \quad \text{wave equation on a line} \quad (3.65a)$$

$$\psi = F(x) \quad -\infty < x < \infty, t = 0 \quad \text{initial condition} \quad (3.65b)$$

$$\frac{\partial \psi}{\partial t} = G(x) \quad -\infty < x < \infty, t = 0 \quad \text{initial tendency,} \quad (3.65c)$$

where the initial condition data,  $F, G$ , are arbitrary functions of space and  $c$  is a constant wave speed. Following from the discussion of characteristics in Section 3.3, we are motivated to transform the wave equation into wave characteristic coordinates

$$\xi = x + ct \quad \text{and} \quad \eta = x - ct \implies \frac{\xi + \eta}{2} = x \quad \text{and} \quad \frac{\xi - \eta}{2c} = t. \quad (3.66)$$

Wave signals propagate in directions defined by constant  $\xi$  and  $\eta$ , so that these coordinates isolate the signal transmission. Furthermore, as we will see, this coordinate transformation facilitates a direct integration of the wave equation.

#### Transformation to characteristic coordinates

To help organize the transformation to characteristic coordinates, we write equation (3.66) as a matrix-vector equation

$$\begin{bmatrix} \xi \\ \eta \end{bmatrix} = \begin{bmatrix} c & 1 \\ -c & 1 \end{bmatrix} \begin{bmatrix} t \\ x \end{bmatrix} \iff \begin{bmatrix} t \\ x \end{bmatrix} = \frac{1}{2} \begin{bmatrix} c^{-1} & -c^{-1} \\ 1 & 1 \end{bmatrix} \begin{bmatrix} \xi \\ \eta \end{bmatrix}. \quad (3.67)$$

Furthermore, define

$$x^n = (x^0, x^1) = (x, t) \quad \text{and} \quad x^{\bar{n}} = (x^{\bar{0}}, x^{\bar{1}}) = (\xi, \eta) \quad (3.68)$$

and use index notation from Chapter 1 so that the transformation (3.67) takes the tidy form

$$x^{\bar{n}} = \Lambda^{\bar{n}}_m x^m \iff x^n = \Lambda^n_{\bar{m}} x^{\bar{m}}, \quad (3.69)$$

where the transformation matrices are given by

$$\Lambda^{\bar{n}}_m = \begin{bmatrix} c & 1 \\ -c & 1 \end{bmatrix} \quad \text{and} \quad \Lambda^n_{\bar{m}} = \frac{1}{2} \begin{bmatrix} c^{-1} & -c^{-1} \\ 1 & 1 \end{bmatrix}. \quad (3.70)$$

Note the use of an upstairs position for the row index on the transformation matrix, which conforms to the use with general tensors from Chapter 6. For present purposes there is no significance to this position placement; it is only used here to anticipate the general tensor machinery. The coordinate transformation (3.69) and the transformation matrices (3.70) then lead to the partial

derivative relationship

$$\partial_{\bar{n}} = \Lambda^{\bar{m}}_{\bar{n}} \partial_m \iff \partial_n = \Lambda^{\bar{m}}_{\bar{n}} x_{\bar{m}}, \quad (3.71)$$

so that

$$\frac{\partial^2}{\partial x^2} = \left[ \frac{\partial}{\partial \xi} + \frac{\partial}{\partial \eta} \right]^2 = \frac{\partial^2}{\partial \xi^2} + 2 \frac{\partial}{\partial \xi} \frac{\partial}{\partial \eta} + \frac{\partial^2}{\partial \eta^2} \quad (3.72a)$$

$$c^{-2} \frac{\partial^2}{\partial t^2} = \left[ \frac{\partial}{\partial \xi} - \frac{\partial}{\partial \eta} \right]^2 = \frac{\partial^2}{\partial \xi^2} - 2 \frac{\partial}{\partial \xi} \frac{\partial}{\partial \eta} + \frac{\partial^2}{\partial \eta^2}. \quad (3.72b)$$

*General solution for the initial value problem*

The operator transformations (3.72a) and (3.72b) bring the initial value problem (3.65a)-(3.65c) into

$$\frac{\partial^2 \psi}{\partial \xi \partial \eta} = 0 \quad -\infty < \eta < \xi < \infty \quad (3.73a)$$

$$\psi(\xi, \eta) = F(\xi) \quad -\infty < \xi < \infty, \xi = \eta \quad (3.73b)$$

$$\frac{\partial \psi}{\partial \xi} - \frac{\partial \psi}{\partial \eta} = c^{-1} G(\xi) \quad -\infty < \xi < \infty, \xi = \eta. \quad (3.73c)$$

Integrating equation (3.73a) in two steps leads to  $\partial_\xi \psi = \theta(\xi)$  so that

$$\psi(\xi, \eta) = \Phi(\eta) + \int^\xi \theta(s) ds \equiv \Phi(\eta) + \Theta(\xi), \quad (3.74)$$

for two functions  $\Phi(\eta)$  and  $\Theta(\xi)$ . The initial conditions (3.73b) and (3.73c) determine relations between  $\Phi(\eta)$  and  $\Theta(\xi)$  and the initial data

$$\Theta(\xi) = \frac{1}{2} \left[ F(\xi) + \frac{1}{c} \int^\xi G(s) ds \right] \quad (3.75a)$$

$$\Phi(\eta) = \frac{1}{2} \left[ F(\eta) - \frac{1}{c} \int^\eta G(s) ds \right], \quad (3.75b)$$

in which case the general solution to the initial value problem (3.65a)-(3.65c) takes the form

$$\psi(x, t) = \frac{1}{2} [F(x + ct) + F(x - ct)] + \frac{1}{2c} \int_{x-ct}^{x+ct} G(s) ds, \quad (3.76)$$

where we reintroduced the variables  $(x, t)$ . This solution is known as the *D'Alembert formula* for the wave equation. Note how the initial profile,  $F(x)$ , is propagated along the two characteristics,  $\xi = x + ct$  and  $\eta = x - ct$ , without any change. In contrast, the initial tendency,  $\partial_t \psi(x, t=0) = G(x)$ , is smoothed through the time integration. This behavior contrasts to the heat equation in Section 3.6, with its single time derivative resulting in a smoothing of the full solution.

### 3.7.2 Domain of influence for wave signals

The wave solution (3.76) at a point in space time,  $(x_o, t_o)$ , depends on data to its past within a causality triangle, or *domain of influence*, as shown in Figure 3.3. The domain of influence is bounded by the two wave characteristics,  $\xi_o = x_o + ct_o$  and  $\eta_o = x_o - ct_o$ . These characteristics are the pathways for propagating information about the initial wave profile,  $\psi(x, t=0) =$

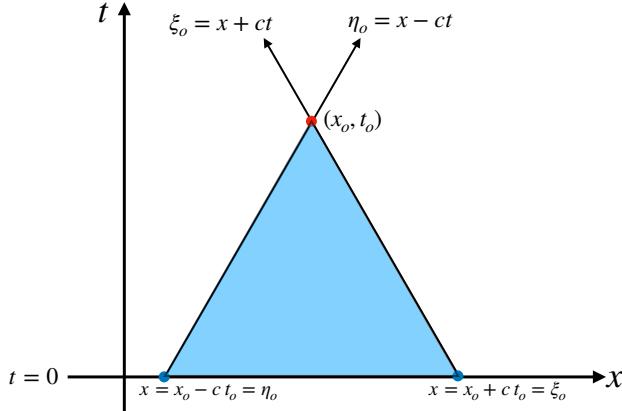


FIGURE 3.3: According to the wave solution (3.76) to the initial value problem on a line, an arbitrary space-time point,  $(x_o, t_o)$ , is causally connected via wave signals to all space-time points within the blue region. This *domain of influence* is bounded by the two wave characteristics,  $\xi_o = x_o + ct_o$  and  $\eta_o = x_o - ct_o$ , with these characteristics the pathway for propagating information about the initial wave profile,  $\psi(x, t = 0) = F(x)$ . Points in between the characteristics are causally connected via the initial time tendency,  $\partial_t \psi(x, t = 0) = G(x)$ , which is integrated over the region  $x_o - ct_o \leq x \leq x_o + ct_o$ . Points outside the domain of influence are causally disconnected from the point  $(x_o, t_o)$ .

$F(x)$ . Points in between the characteristics are causally connected via the initial time tendency,  $\partial_t \psi(x, t = 0) = G(x)$ , which is integrated over the region  $x_o - ct_o \leq x \leq x_o + ct_o$ . Points outside the domain of influence are causally disconnected from the point  $(x_o, t_o)$ .

### 3.7.3 Helmholtz equation

Consider the wave equation with a constant wave speed

$$\frac{\partial^2 \psi}{\partial t^2} - c^2 \nabla^2 \psi = 0. \quad (3.77)$$

Assuming a wave ansatz<sup>3</sup> of the form

$$\psi(\mathbf{x}, t) = e^{i\omega t} \Psi(\mathbf{x}) \quad (3.78)$$

results in the *Helmholtz equation* for the amplitude function

$$(\nabla^2 + k^2) \Psi = 0, \quad (3.79)$$

where  $k = \omega/c$  is the wavenumber. The Helmholtz equation thus plays a central role in wave theory.

### 3.7.4 Duhamel's superposition integral for the wave equation

We here present Duhamel's superposition integral for the wave equation, following from the similar discussion for the heat equation in Section 3.6.3. For this purpose, consider the forced wave

<sup>3</sup>An *Ansatz* is a German word meaning an educated guess for the form of the solution.

equation with time independent forcing

$$\frac{\partial^2 \Psi}{\partial t^2} = c^2 \nabla^2 \Psi + G(\mathbf{x}) \quad \mathbf{x} \in \mathbb{R}^n, t > 0 \quad (3.80a)$$

$$\Psi(\mathbf{x}, t) = 0 \quad \mathbf{x} \in \mathbb{R}^n, t = 0, \quad (3.80b)$$

and the corresponding unforced wave equation with inhomogenous initial time tendency

$$\frac{\partial^2 \psi}{\partial t^2} = c^2 \nabla^2 \psi \quad \mathbf{x} \in \mathbb{R}^n, t > 0 \quad (3.81a)$$

$$\psi(\mathbf{x}, t) = 0 \quad \mathbf{x} \in \mathbb{R}^n, t = 0. \quad (3.81b)$$

$$\frac{\partial \psi(\mathbf{x}, t)}{\partial t} = G(\mathbf{x}) \quad \mathbf{x} \in \mathbb{R}^n, t = 0. \quad (3.81c)$$

The two scalar fields are related by Duhamel's superposition integral

$$\Psi(\mathbf{x}, t) = \int_0^t \psi(\mathbf{x}, t - \tau) d\tau. \quad (3.82)$$

We can verify this formula through direct differentiation

$$\frac{\partial \Psi(\mathbf{x}, t)}{\partial t} = \int_0^t \frac{\partial \psi(\mathbf{x}, t - \tau)}{\partial t} d\tau \quad (3.83a)$$

$$\frac{\partial^2 \Psi(\mathbf{x}, t)}{\partial t^2} = \frac{\partial \psi(\mathbf{x}, 0)}{\partial t} + \int_0^t \frac{\partial^2 \psi(\mathbf{x}, t - \tau)}{\partial t^2} d\tau = G(\mathbf{x}) + c^2 \nabla^2 \Psi(\mathbf{x}, t). \quad (3.83b)$$

As an example, consider the initial value problem for wave equation on a line with time independent forcing

$$\frac{\partial^2 \Psi}{\partial t^2} = c^2 \frac{\partial^2 \Psi}{\partial x^2} + G(x) \quad -\infty < x < \infty, t > 0 \quad (3.84a)$$

$$\Psi(x, t) = 0 \quad -\infty < x < \infty, t = 0 \quad (3.84b)$$

$$\frac{\partial \Psi(x, t)}{\partial t} = 0 \quad -\infty < x < \infty, t = 0. \quad (3.84c)$$

Duhamel's superposition integral says that  $\Psi$  is related to the solution of the unforced wave equation with initial time tendency given by the forcing

$$\frac{\partial^2 \psi}{\partial t^2} = c^2 \frac{\partial^2 \psi}{\partial x^2} \quad -\infty < x < \infty, t > 0 \quad (3.85a)$$

$$\psi(x, t) = 0 \quad -\infty < x < \infty, t = \tau \quad (3.85b)$$

$$\frac{\partial \psi(x, t)}{\partial t} = G(x) \quad -\infty < x < \infty, t = \tau > 0. \quad (3.85c)$$

We know from Section 3.7.1 that the solution  $\psi$  is given by the D'Alembert formula in equation (3.76), only here with the initial condition function set to zero

$$\psi(x, t) = \frac{1}{2c} \int_{x-ct}^{x+ct} G(s) ds. \quad (3.86)$$

Hence, D'Alembert's formula says that the solution to the forced wave equation (3.84a)-(3.84c)

is given by the superposition integral

$$\Psi(x, t) = \frac{1}{2c} \int_0^t \int_{x-c(t-\tau)}^{x+c(t-\tau)} G(s) ds. \quad (3.87)$$

Introducing the *antiderivative* function via

$$\mathcal{G}(s) = \int^s G(s') ds' \iff \frac{\partial \mathcal{G}(s)}{\partial s} = G(s) \quad (3.88)$$

allows us to interpret the solution (3.87) as the superposition of two oppositely traveling waves

$$\Psi(x, t) = \frac{1}{2c} \int_0^t [\mathcal{G}[x + c(t - \tau)] - \mathcal{G}[x - c(t - \tau)]] d\tau. \quad (3.89)$$

### 3.7.5 Further study

[Stakgold \(2000a,b\)](#) provides a thorough discussion of the wave equation and the related Helmholtz equation.

## 3.8 Evolution of time averages

In geophysical fluid mechanics, we generically refer to an equation with a time derivative, such as a parabolic or hyperbolic equation, as a *prognostic equation* or an *evolution equation*. In the analysis of such equations, for example when analyzing simulation output or time series data, it is common to take the time average in order to focus on lower frequency behavior. This section provides a technical discussion concerning this time averaging operation, with the material here following [Bladwell et al. \(2022\)](#).

For this purpose, ignore all space coordinates and write a generic prognostic equation in the form

$$\frac{dA}{dt} = \mathcal{B}. \quad (3.90)$$

For example, the quantity  $A$  might be the velocity or temperature at a point in space, and  $\mathcal{B}$  might be the acceleration due to pressure or the heating due to temperature diffusion. We term  $dA/dt$  the *time tendency* of the quantity  $A$  whereas  $\mathcal{B}$  is the “forcing” that gives rise to the time tendency. In the analysis of fluid flows, we commonly wish to diagnose terms appearing in the evolution equations for the purpose of ascribing physical understanding to the flow regime; e.g., what forces are more active in certain regions. Although sitting a bit outside the scope of a chapter on PDEs, the material in this section exposes some common questions that arise when time averaging terms appearing in the prognostic equations of geophysical fluid mechanics.

Time integration of equation (3.90) leads to

$$A(t) = A(t_0) + \int_{t_0}^t \mathcal{B}(s) ds, \quad (3.91)$$

thus providing an expression for the instantaneous value of  $A$  at an arbitrary time  $t$ , assuming knowledge of the initial value,  $A(t_0)$ , as well as the time integral of  $\mathcal{B}$ . In practice, particularly when working with numerical models, we typically have access to time averages over some time interval (e.g., days, months, years, decades) rather than instantaneous (snapshot) values of  $A$ . Furthermore, instantaneous snapshots can be prone to relatively large fluctuations that expose the diagnostic calculations to numerical precision errors (e.g., small differences between relatively

large fluctuating values). We are thus interested in relating time averages of  $A$  to time averages of  $\mathcal{B}$ .

### 3.8.1 Time averages

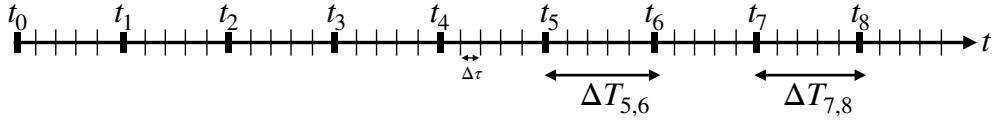


FIGURE 3.4: Example time axis for the discussion of time averaging. The labeled times,  $t_n$ , can represent, for example, days, months or years with the time interval,  $\Delta T_{n,n+1} = t_{n+1} - t_n$ , not necessarily the same (e.g., different number of days in a month or a leap year versus non-leap year). The smaller unlabeled time steps represent the time steps for the model's prognostic equations (e.g., days, hours, seconds, etc.), with fixed time step  $\Delta\tau$ .

Introduce a discrete partitioning of the time axis as in Figure 3.4 and define an unweighted time average over a chosen time interval  $\Delta T_{n,n+1} = t_{n+1} - t_n > 0$

$$\bar{A}_{n,n+1} = \frac{1}{\Delta T_{n,n+1}} \int_{t_n}^{t_{n+1}} A(t) dt \quad (3.92a)$$

$$\bar{\mathcal{B}}_{n,n+1} = \frac{1}{\Delta T_{n,n+1}} \int_{t_n}^{t_{n+1}} \mathcal{B}(t) dt. \quad (3.92b)$$

These integrals are realized in practice as a discrete sum over the model time steps, with only the lower limit inclusive so as to not double-count endpoints; i.e.,  $[t_n, t_{n+1})$ . We allow for non-constant time intervals,  $\Delta T_{n,n+1}$ , as arises in monthly and yearly (with leap-years) time averages.

Substituting expression (3.91) into the time mean (3.92a) renders

$$\bar{A}_{n,n+1} - A(t_0) = \frac{1}{\Delta T_{n,n+1}} \int_{t_n}^{t_{n+1}} \left[ \int_{t_0}^t \mathcal{B}(s) ds \right] dt, \quad (3.93)$$

and a similar expression over a later time interval  $[t_p, t_{p+1})$  with  $p \geq n + 1$  leads to the difference between time averages

$$\bar{A}_{p,p+1} - \bar{A}_{n,n+1} = \frac{1}{\Delta T_{p,p+1}} \int_{t_p}^{t_{p+1}} \left[ \int_{t_0}^t \mathcal{B}(s) ds \right] dt - \frac{1}{\Delta T_{n,n+1}} \int_{t_n}^{t_{n+1}} \left[ \int_{t_0}^t \mathcal{B}(s) ds \right] dt. \quad (3.94)$$

The formalism allows us to take differences between time averages over intervals that are separated, such as might be of interest in taking decadal means between the beginning and end of a century, for example. Importantly, the initial value,  $A(t_0)$ , is absent from the difference in time means so that there are only time integrated quantities appearing in equation (3.94).

### 3.8.2 Massaging the double time integrals

The double time integrals in equation (3.94) can be massaged into a simpler form. We start by making the following decomposition and noting that  $t_n \leq t \leq t_{n+1}$

$$\int_{t_n}^{t_{n+1}} \left[ \int_{t_0}^t \mathcal{B}(s) ds \right] dt = \int_{t_n}^{t_{n+1}} \left[ \int_{t_0}^{t_n} \mathcal{B}(s) ds + \int_{t_n}^t \mathcal{B}(s) ds \right] dt \quad (3.95a)$$

$$= \Delta T_{n,n+1} \int_{t_0}^{t_n} \mathcal{B}(s) ds + \int_{t_n}^{t_{n+1}} \left[ \int_{t_n}^t \mathcal{B}(s) ds \right] dt. \quad (3.95b)$$

We are thus led to the difference

$$\begin{aligned}\overline{A}_{p,p+1} - \overline{A}_{n,n+1} &= \left[ \int_{t_0}^{t_p} \mathcal{B}(s) ds - \int_{t_0}^{t_n} \mathcal{B}(s) ds \right] \\ &+ \frac{1}{\Delta T_{p,p+1}} \int_{t_p}^{t_{p+1}} \left[ \int_{t_p}^t \mathcal{B}(s) ds \right] dt - \frac{1}{\Delta T_{n,n+1}} \int_{t_n}^{t_{n+1}} \left[ \int_{t_n}^t \mathcal{B}(s) ds \right] dt \\ &= \int_{t_n}^{t_p} \mathcal{B}(t) dt + \frac{1}{\Delta T_{p,p+1}} \int_{t_p}^{t_{p+1}} \left[ \int_{t_p}^t \mathcal{B}(s) ds \right] dt - \frac{1}{\Delta T_{n,n+1}} \int_{t_n}^{t_{n+1}} \left[ \int_{t_n}^t \mathcal{B}(s) ds \right] dt.\end{aligned}\quad (3.96)$$

The double integrals in equation (3.96) take place over triangular time domains, such as shown in Figure 3.5.

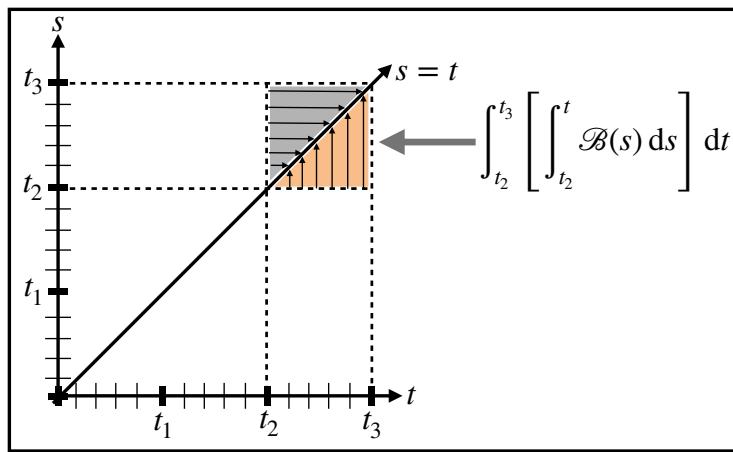


FIGURE 3.5: Gold region depicts the time integration domain used in one of the double integrals from equation (3.96) for the special case of  $n = 2$ . Note that the gray triangular region generally leads to a distinct integral.

### 3.8.3 Making use of a double integral identity

We here derive an identity (originally due to [Cauchy \(1823\)](#)) that reduces the double integral in equation (3.96) to a single integral to expose the underlying geometry of the time windowing. For this purpose we make use of the following identity

$$\int_{t_n}^{t_{n+1}} \left[ \int_{t_n}^t \mathcal{B}(s) ds \right] dt = \int_{t_n}^{t_{n+1}} (t_{n+1} - t) \mathcal{B}(t) dt.\quad (3.97)$$

To prove this identity we make the substitution  $\mathcal{B}(s) = dA/ds$  from equation (3.90) and then show that both sides to equation (3.97) yield the same result. For the left hand side we have

$$\int_{t_n}^{t_{n+1}} \left[ \int_{t_n}^t \mathcal{B}(s) ds \right] dt = \int_{t_n}^{t_{n+1}} \left[ \int_{t_n}^t \frac{dA(s)}{ds} ds \right] dt\quad (3.98a)$$

$$= \int_{t_n}^{t_{n+1}} \left[ \int_{t_n}^t dA(s) \right] dt\quad (3.98b)$$

$$= \int_{t_n}^{t_{n+1}} [A(t) - A(t_n)] dt\quad (3.98c)$$

$$= \int_{t_n}^{t_{n+1}} A(t) dt - (t_{n+1} - t_n) A(t_n),\quad (3.98d)$$

whereas the right hand side is

$$\int_{t_n}^{t_{n+1}} (t_{n+1} - t) \mathcal{B}(t) dt = \int_{t_n}^{t_{n+1}} (t_{n+1} - t) \frac{dA(t)}{dt} dt \quad (3.99a)$$

$$= \int_{t_n}^{t_{n+1}} (t_{n+1} - t) dA(t) \quad (3.99b)$$

$$= \int_{t_n}^{t_{n+1}} d[A(t)(t_{n+1} - t)] + A(t) dt \quad (3.99c)$$

$$= -A(t_n)(t_{n+1} - t_n) + \int_{t_n}^{t_{n+1}} A(t) dt, \quad (3.99d)$$

which is identical to the left hand side given by equation (3.98d). We have thus proven the double integral formula (3.97).

The right hand side of the double integral formula (3.97) can be written

$$\int_{t_n}^{t_{n+1}} (t_{n+1} - t) \mathcal{B}(t) dt = t_{n+1} \Delta T_{n,n+1} \bar{\mathcal{B}}_{n,n+1} - \int_{t_n}^{t_{n+1}} t \mathcal{B}(t) dt, \quad (3.100)$$

which might be useful in some contexts. However, it is awkward for our purposes since it exposes the absolute time,  $t_{n+1}$ , in the first term on the right hand side and the time,  $t$ , within the integral. Since we generally do not hold any initial time as special (i.e., the initial time,  $t_0$ , is arbitrary), it is preferable to retain the time differences throughout the formulation. Hence, when making use of the double integral identity (3.97) we bring equation (3.96) into the form

$$\bar{A}_{p,p+1} - \bar{A}_{n,n+1} = \int_{t_n}^{t_p} \mathcal{B}(t) dt + \int_{t_p}^{t_{p+1}} \frac{(t_{p+1} - t) \mathcal{B}(t)}{t_{p+1} - t_p} dt - \int_{t_n}^{t_{n+1}} \frac{(t_{n+1} - t) \mathcal{B}(t)}{t_{n+1} - t_n} dt \quad (3.101a)$$

$$= \int_{t_n}^{t_{n+1}} \frac{(t - t_n) \mathcal{B}(t)}{t_{n+1} - t_n} dt + \int_{t_{n+1}}^{t_p} \mathcal{B}(t) dt + \int_{t_p}^{t_{p+1}} \frac{(t_{p+1} - t) \mathcal{B}(t)}{t_{p+1} - t_p} dt. \quad (3.101b)$$

The first right hand side term is a weighted integral with a linearly increasing weight from zero to unity, whereas the final right hand side term has a linearly decreasing weight from unity to zero. The middle term has a unity weight throughout and it vanishes if  $p = n+1$ , as when the averaging regions are adjacent. Figure 3.6. illustrates the time windowing used for equation (3.101b).

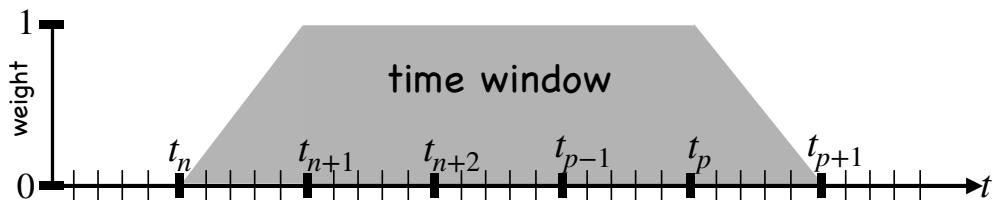


FIGURE 3.6: Illustrating the time window weighting used in computing the right hand side of equation (3.101b). Note that if  $p = n+1$ , then the middle term in equation (3.101b) and there is no plateau region of unit weight, in which case the window region becomes two adjacent triangles.

As a final means to write equation (3.101b), extend the middle term to the end of the time period and then subtract the extra piece and recombine to render

$$\bar{A}_{p,p+1} - \bar{A}_{n,n+1} = \int_{t_{n+1}}^{t_{p+1}} \mathcal{B}(t) dt + \int_{t_n}^{t_{n+1}} \frac{(t - t_n) \mathcal{B}(t)}{t_{n+1} - t_n} dt - \int_{t_p}^{t_{p+1}} \frac{(t - t_p) \mathcal{B}(t)}{t_{p+1} - t_p} dt. \quad (3.102)$$

The first term on the right hand side is an unweighted integral from the end of the first interval to the end of the final interval, whereas the other two terms both have increasing weights over their respective integration intervals. This form allows for some advantages diagnostically since we only need to save unweighted integrals plus linearly increasing weighted integrals; there is no need to save decreasing weighted integrals.



# Chapter 4

## Green's function methods

There are many methods to solve linear partial differential equations (PDEs). Some methods, such as the separation of variables, Fourier transforms, and Laplace transforms, are suited to idealized domains with relatively simple geometries that enable closed form analytic solutions. However, for many physical applications we encounter domains and boundary conditions where analytical methods are unavailable. It is thus often useful to have a general closed-form solution to study properties of the solution either analytically or numerically. The Green's function method provides this solution.

In this chapter we develop the Green's function method for the elliptic and parabolic linear partial differential equations of mathematical physics introduced in Chapter 3. We are most interested in the Green's function method as a conceptual framework and as such we are relatively unconcerned with how to determine the Green's function for any particular problem. Even without an explicit form of the Green's function, an appreciation of Green's function methods deepens both physical and mathematical understanding of the various linear PDEs encountered in this book, such as the Poisson equation in Newtonian gravity (Section 9.12), and quasi-geostrophic theory (Chapter 40), as well as the diffusion equation and the advection-diffusion equation of Chapter 46.

### READER'S GUIDE TO THIS CHAPTER

We encounter a variety of Green's functions that differ according to the differential operator and boundary conditions. Use of the common symbol,  $G$ , minimizes the adornments otherwise needed to distinguish Green's functions. Confusion is avoided by noting that properties of any particular Green's function are specific to the section where the function is discussed. Much in this chapter is based on the treatments found in Chapter 7 of *Morse and Feshbach* (1953) as well as *Stakgold* (2000a,b). Both of these books are classics whose presentations have stood the test of time.

4.1	Conceptual foundations . . . . .	68
4.2	Dirac delta . . . . .	69
4.2.1	A point mass source . . . . .	70
4.2.2	Sifting property . . . . .	70
4.2.3	Cartesian and spherical coordinates . . . . .	71
4.2.4	Example $\delta^{(\epsilon)}(x)$ functions . . . . .	71
4.2.5	Connection to the Heaviside step function . . . . .	73
4.2.6	Sifting property for the Dirac dipole . . . . .	73

4.2.7	Temporal Dirac delta and impulses . . . . .	74
4.2.8	Shifting the space-time position of the source . . . . .	74
4.3	Laplace's free space Green's function . . . . .	<b>75</b>
4.3.1	Gravitational potential from a point mass source . . . . .	75
4.3.2	Free space Green's function for Laplace's equation . . . . .	76
4.3.3	Details of the three-dimensional free space Green's function . . . . .	76
4.4	One-dimensional Poisson's equation . . . . .	<b>77</b>
4.4.1	Integral expression for $\psi$ in terms of $G$ . . . . .	77
4.4.2	Preliminary steps for obtaining the Green's function . . . . .	78
4.4.3	Green's function satisfying Dirichlet boundary conditions . . . . .	79
4.4.4	Green's function satisfying Neumann boundary conditions . . . . .	80
4.4.5	Uniqueness of the solution to the Dirichlet problem . . . . .	81
4.5	Poisson's equation with Dirichlet boundaries . . . . .	<b>81</b>
4.5.1	Constraints on the source and boundary normal derivative . . . . .	81
4.5.2	Uniqueness of the solution . . . . .	82
4.5.3	The Green's function problem . . . . .	82
4.5.4	Reciprocity of the Green's function . . . . .	84
4.5.5	The integral solution . . . . .	85
4.5.6	Properties of the solution . . . . .	86
4.5.7	Boundary Green's function . . . . .	88
4.6	Poisson's equation with Neumann boundaries . . . . .	<b>89</b>
4.6.1	Constraints on the source and boundary data . . . . .	89
4.6.2	Uniqueness of the solution up to a constant . . . . .	89
4.6.3	The Green's function problem . . . . .	90
4.6.4	Properties of the solution . . . . .	90
4.6.5	Verifying the solution . . . . .	91
4.7	The diffusion equation . . . . .	<b>92</b>
4.7.1	Causal free space Green's function . . . . .	93
4.7.2	Causal Green's function . . . . .	93
4.7.3	Adjoint causal Green's function . . . . .	94
4.7.4	Reciprocity of the Green's function and its adjoint . . . . .	95
4.7.5	Composition property of the Green's function . . . . .	97
4.7.6	Integral solution . . . . .	99
4.7.7	Properties of the solution . . . . .	101
4.7.8	Boundary propagator . . . . .	103
4.8	Initial value problems and response functions . . . . .	<b>105</b>
4.8.1	Impulse response function . . . . .	105
4.8.2	Step response function . . . . .	106
4.8.3	Reciprocity relation . . . . .	108
4.8.4	Response function for general forcing . . . . .	109
4.8.5	Connection to the boundary propagator . . . . .	110
4.8.6	Comments and further study . . . . .	110

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## 4.1 Conceptual foundations

Our treatment of the Dirac delta and Green's functions is physically formal, meaning that our priority is to be satisfying from a physical perspective. This physically formal treatment is generally not mathematically rigorous, with a rigorous treatment requiring an array of mathematical apparatus outside our scope.<sup>1</sup> The physically formal treatment found here is generally supported by heuristic arguments taken from Newtonian gravity (see Section 9.12); electrostatics (e.g., [Jackson](#)

<sup>1</sup>The term *physically formal* is often used in the mathematical physics literature as a complement to *mathematically rigorous*.

(1975)); and the diffusion of temperature or matter within a continuous media.<sup>2</sup> The tracer and temperature examples are directly relevant to geophysical fluid mechanics and will be developed in this book. We also make use of the electrostatic and gravity examples since they only require elementary physics and historically they provided motivation for development of Green's function methods in the 19th and 20th centuries.

The basic mathematical problem of classical continuum field theory concerns an arbitrary field,  $\psi(\mathbf{x}, t)$ , that represents a physical property such as material tracer concentration, velocity streamfunction, temperature in a continuous media, Newtonian gravitational potential, or classical electrostatic potential. The space-time structure of the field is the result of a space-time distributed source (e.g., tracer source, potential vorticity distribution, mass distribution, or electric charge distribution) along with differential operators (e.g., time derivative, Laplacian, diffusion operator, wave operator) that connect the field across points in space-time as well as initial and boundary conditions that fix the behavior of  $\psi$  in selected space-time regions.<sup>3</sup>

For our studies, the differential equations describing  $\psi$  are generally nonlinear. However, in some important cases it is possible to linearize the governing equations and learn much about the underlying mathematical and physical properties of the system. Furthermore, the advection-diffusion equation describing a passive tracer (Chapter 46) is linear even when the dynamical flow field is nonlinear. The conceptual foundation of the Green's function method is based on observing that if the field equations are linear, then  $\psi$  can be constructed by accumulating contributions from point-sized portions of the distributed source, including sources on the region boundaries. Let us write  $G(\mathbf{x}, t | \mathbf{x}_0, t_0)$  for the field at an observation space-time point  $(\mathbf{x}, t)$  (the *field point*) caused by a point source at  $(\mathbf{x}_0, t_0)$  (the *source point*). We then observe that  $\psi(\mathbf{x}, t)$  caused by a source that is distributed through space and time is the integral of  $G$  with the source computed over the space-time domain occupied by the source. Similar superpositions are made for the initial and boundary conditions. The function  $G$  is referred to as the *Green's function* in honor of the 19th century mathematician who first developed these functions for studies of electrostatics.

The above arguments rely on the superposition property of linear systems. It does so by finding a particular solution (the Green's function) to a linear initial-boundary value problem with a singular point source (Dirac delta) and homogeneous boundary conditions. The solution to the original problem is found by integrating (convolving) the Green's function with the boundary conditions, initial conditions, and distributed sources. The Green's function is generally simpler to determine than the solution to the original initial-boundary value problem. Furthermore, the Green's function provides a formal inverse to the linear partial differential operator in a manner reminiscent of matrix inversion used to solve a matrix-vector problem. Just as for the matrix-vector problem, once we have the Green's function we can write the solution to any of the associated initial-boundary value problems regardless the details of the distributed source, initial data, or boundary data. Herein lies the power of the Green's function method and why it has found much use across mathematical physics.

## 4.2 Dirac delta

The *Dirac delta* provides an idealization of a point source and it serves a core role in the study of Green's functions. In mathematics, the Dirac delta is known as a *generalized function* (e.g.,

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<sup>2</sup>A heuristic technique or argument employs a practical method not guaranteed to be fully rational or deductive from all perspectives, but is sufficient for establishing a self-consistent formalism. The study of the Dirac delta and Green's functions are examples where physical heuristics established a formalism whose mathematical rigor followed later.

<sup>3</sup>In some cases, sources are present only along spatial boundaries.

chapter 5 of [Stakgold \(2000b\)](#)). We use the terse nomenclature *Dirac delta*, rather than the commonly used “delta function”, to emphasize its special nature as a generalized function.

### 4.2.1 A point mass source

In Newtonian gravity we encounter the Poisson equation for the gravitational potential,  $\Phi$ , arising from an arbitrary mass density,  $\rho$

$$\nabla^2 \Phi = 4\pi G^{\text{grv}} \rho, \quad (4.1)$$

with  $G^{\text{grv}}$  Newton’s gravitational constant (see Section 9.12.1).<sup>4</sup> The gravitational potential for an arbitrary spherically symmetric mass, when sampled at a point outside the mass, equals to the potential of a point mass located at the origin. Making precise the notion of a “point mass” provides a venue to introduce the Dirac delta.

For that purpose, consider a mass,  $M$ , distributed uniformly within a sphere of radius  $\epsilon$  and volume

$$V_\epsilon = \frac{4}{3}\pi\epsilon^3, \quad (4.2)$$

and let the sphere be centered at the origin of a coordinate system. The mass distribution thus has a density

$$\rho(\mathbf{x}) = M \delta^{(\epsilon)}(\mathbf{x}), \quad (4.3)$$

where we introduced the  $\epsilon$ -distribution

$$\delta^{(\epsilon)}(\mathbf{x}) \equiv \begin{cases} V_\epsilon^{-1} & \text{if } |\mathbf{x}| \leq \epsilon \\ 0 & \text{if } |\mathbf{x}| > \epsilon. \end{cases} \quad (4.4)$$

By construction, an integral over a domain fully encompassing the sphere yields the mass

$$\int_{\mathcal{R}} \rho \, dV = M \int_{\mathcal{R}} \delta^{(\epsilon)}(\mathbf{x}) \, dV = M, \quad (4.5)$$

with this result holding even as the radius of the sphere becomes arbitrarily small,  $\epsilon \rightarrow 0$ . We define the Dirac delta as the limiting  $\epsilon$ -distribution

$$\delta(\mathbf{x}) \equiv \lim_{\epsilon \rightarrow 0} \delta^{(\epsilon)}(\mathbf{x}). \quad (4.6)$$

By construction, the Dirac delta arises from taking the limit of a mass source that is zero everywhere in space except at a single point, at which point the Dirac delta is formally infinite. Concerns with how to interpret the infinite value of  $\delta(\mathbf{x})$  at the origin are ameliorated by recognizing that  $\delta(\mathbf{x})$  is evaluated only within an integral, with these integral properties well defined and described in the remainder of this section. Connecting to the other physical analogs, the Dirac delta corresponds to a point charge in electrostatics or to a point source of trace matter within a fluid.

### 4.2.2 Sifting property

Now consider multiplying an  $\epsilon$ -distribution by an arbitrary smooth function,  $\psi(\mathbf{x})$ . Since the  $\epsilon$ -distribution has support only within the  $\epsilon$ -sphere surrounding the origin, an integral of  $\delta^{(\epsilon)}(\mathbf{x}) \psi(\mathbf{x})$

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<sup>4</sup>Elsewhere in this book we write  $G = G^{\text{grv}}$ . We add the “grv” label in this chapter and reserve  $G$  for the Green’s function.

over the sphere, in the limit that  $\epsilon \rightarrow 0$ , leads to the *sifting property*

$$\lim_{\epsilon \rightarrow 0} \int_{\mathcal{R}} \delta^{(\epsilon)}(\mathbf{x}) \psi(\mathbf{x}) dV = \int_{\mathcal{R}} \delta(\mathbf{x}) \psi(\mathbf{x}) dV = \psi(\mathbf{x} = 0). \quad (4.7)$$

Hence, the Dirac delta acts to “sift” out the value of the function at the location of the Dirac delta source, and it is the key defining feature of the Dirac delta for our purposes.

### 4.2.3 Cartesian and spherical coordinates

The definition (4.6) was constructed in three space dimensions, with the Dirac delta having dimensions of inverse volume. We can consider the same procedure for a single space dimension, with the one-dimensional Dirac delta having dimension of inverse length and thus satisfying the normalization condition

$$\int_{\mathcal{R}} \delta(x) dx = 1, \quad (4.8)$$

where the integration domain,  $\mathcal{R}$ , includes the origin. Correspondingly, we can decompose the three-dimensional Dirac delta according to

$$\delta(\mathbf{x}) = \delta(x) \delta(y) \delta(z), \quad (4.9)$$

so that, with the domain  $\mathcal{R}$  containing the origin, we have

$$\int_{\mathcal{R}} \delta(\mathbf{x}) dV = \int_{\mathcal{R}} \delta(x) \delta(y) \delta(z) dx dy dz = 1. \quad (4.10)$$

Rather than Cartesian coordinates, we sometimes find it useful to make use of the spherical coordinates<sup>5</sup> to render

$$\delta(\mathbf{x}) = \frac{1}{r^2 \cos \phi} \delta(r) \delta(\phi) \delta(\lambda), \quad (4.11)$$

so that

$$\int_{\mathcal{R}} \delta(\mathbf{x}) dx dy dz = \int_{\mathcal{R}} \delta(\mathbf{x}) r^2 \cos \phi dr d\phi d\lambda = \int_{\mathcal{R}} \delta(r) \delta(\phi) \delta(\lambda) dr d\phi d\lambda = 1. \quad (4.12)$$

Notice how the dimensions of a particular Dirac delta equals to the inverse dimensions of its argument, so that both  $\delta(\phi)$  and  $\delta(\lambda)$  are dimensionless whereas  $\delta(r)$  has dimensions of inverse length. Similar treatments hold for other coordinates.

### 4.2.4 Example $\delta^{(\epsilon)}(x)$ functions

The particular construction (4.6) is not unique. That is, there are many other suitable  $\epsilon$ -distributions whose limiting behavior also result in a Dirac delta as defined by the unit nor-

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<sup>5</sup>We discuss spherical coordinates in Section 8.2.

malization and sifting properties. We here list a few that appear in applications

$$\delta^{(\epsilon)}(x) = \epsilon^{-1} \quad \text{for } |x| < \epsilon/2 \text{ and } 0 \text{ for } |x| > \epsilon/2 \quad (4.13a)$$

$$\delta^{(\epsilon)}(x) = \frac{e^{-|x|/\epsilon}}{2\epsilon} \quad (4.13b)$$

$$\delta^{(\epsilon)}(x) = \frac{\epsilon}{\pi(x^2 + \epsilon^2)} \quad (4.13c)$$

$$\delta^{(\epsilon)}(x) = \frac{e^{-x^2/\epsilon^2}}{\epsilon\pi} \quad (4.13d)$$

$$\delta^{(\epsilon)}(x) = \frac{\sin(x/\epsilon)}{x\epsilon} \quad (4.13e)$$

$$\delta^{(\epsilon)}(x) = \frac{\epsilon \sin^2(x/\epsilon)}{\pi x^2}. \quad (4.13f)$$

With  $x$  corresponding to a spatial position, note how each of these one-dimensional functions has dimensions of inverse length. Figure 4.1 depicts the rectangular function (4.13a) as a canonical example.

Consider the multiplication of each of the above functions  $\delta^{(\epsilon)}(x)$ , by a non-dimensional, continuous and bounded function,  $F(x)$ , that is unity at the origin,  $F(0) = 1$ . In this case,  $F(x)\delta^{(\epsilon)}(x)$  still satisfies the normalization and sifting properties required of a Dirac delta

$$\lim_{\epsilon \rightarrow 0} \int_{\mathcal{R}} F(x) \delta^{(\epsilon)}(x) dx = F(0) = 1 \quad \text{and} \quad \lim_{\epsilon \rightarrow 0} \int_{\mathcal{R}} \psi(x) F(x) \delta^{(\epsilon)}(x) dx = \psi(0) F(0) = \psi(0), \quad (4.14)$$

so that

$$\lim_{\epsilon \rightarrow 0} F(x) \delta^{(\epsilon)}(x) = \delta(x). \quad (4.15)$$

Correspondingly, whenever working with a Dirac delta, if it is multiplied by a non-dimensional function  $F(x)$  with  $F(0) = 1$ , then we can disregard this function since it does not modify the Dirac source.

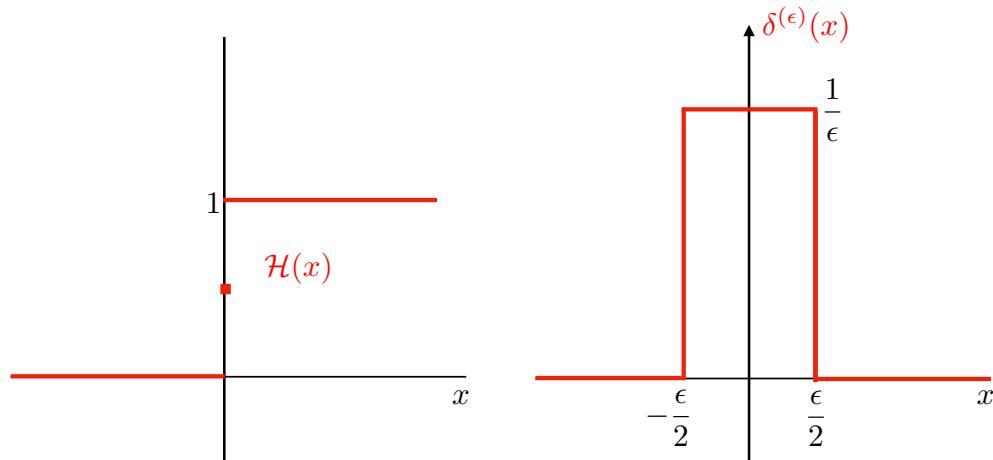


FIGURE 4.1: Left panel: Heaviside step function,  $\mathcal{H}(x)$ , as given by equation (4.16). Right panel: the square pulse function  $\delta^{(\epsilon)}(x)$  given by equation (4.13a), with  $\lim_{\epsilon \rightarrow 0} \delta^{(\epsilon)}(x) = \delta(x) = d\mathcal{H}(x)/dx$ .

### 4.2.5 Connection to the Heaviside step function

The Heaviside step function (Figure 4.1) is given by<sup>6</sup>

$$\mathcal{H}(x) = \begin{cases} 0 & \text{if } x < 0 \\ 1/2 & \text{if } x = 0 \\ 1 & \text{if } x > 0, \end{cases} \quad (4.16)$$

and it is related to the sgn function

$$\operatorname{sgn}(x) = \begin{cases} -1 & \text{if } x < 0 \\ 0 & \text{if } x = 0 \\ 1 & \text{if } x > 0, \end{cases} \quad (4.17)$$

according to

$$\operatorname{sgn}(x) = 2\mathcal{H}(x) - 1. \quad (4.18)$$

Both the Heaviside and sgn functions are piecewise continuous and have infinite derivatives at  $x = 0$ . In particular, the derivative of the Heaviside step function equals to the Dirac delta

$$\frac{d\mathcal{H}(x)}{dx} = \delta(x). \quad (4.19)$$

This identity is most apparent by considering the square pulse approximation to the Dirac delta given by equation (4.13a), which can be written

$$\delta(x) = \lim_{\epsilon \rightarrow 0} \delta^{(\epsilon)}(x) = \lim_{\epsilon \rightarrow 0} \frac{\mathcal{H}(x + \epsilon/2) - \mathcal{H}(x - \epsilon/2)}{\epsilon} = \frac{d\mathcal{H}(x)}{dx}. \quad (4.20)$$

Equivalently, we see that the Heaviside step function is the cumulative distribution of the Dirac delta

$$\int_{-\infty}^x \delta(x') dx' = \int_{-\infty}^x \frac{d\mathcal{H}(x')}{dx'} dx' = \mathcal{H}(x) - \mathcal{H}(-\infty) = \mathcal{H}(x). \quad (4.21)$$

Connecting to the language of probability theory, the Dirac delta corresponds to a probability density function peaked over an infinitesimal region, whereas the Heaviside step function is the corresponding probability distribution function.

### 4.2.6 Sifting property for the Dirac dipole

The derivative of a Dirac delta represents an idealization of a dipole (e.g., see exercise 1.14 of *Stakgold (2000a)*). There are occasions when it is useful to know how a dipole acts on a function inside of an integral. For this purpose we make use of the identity

$$\int_{-\epsilon}^{\epsilon} \frac{d[\psi(x) \delta(x)]}{dx} dx = \psi(\epsilon) \delta(\epsilon) - \psi(-\epsilon) \delta(-\epsilon). \quad (4.22)$$

Each term on the right hand side vanishes when  $\epsilon > 0$  since the Dirac delta never fires. Applying the product rule inside of the integral renders the identity

$$\int_{-\epsilon}^{\epsilon} \frac{d[\psi(x) \delta(x)]}{dx} dx = \int_{-\epsilon}^{\epsilon} \left[ \psi(x) \frac{d\delta(x)}{dx} + \delta(x) \frac{d\psi(x)}{dx} \right] dx = 0, \quad (4.23)$$

<sup>6</sup>In some treatments,  $\mathcal{H}(x)$  is undefined at  $x = 0$ . For our purposes, the properties of the Heaviside step function remain unchanged whether it is defined at  $x = 0$  or not. See footnote on page 20 of *Stakgold (2000a)* for more details.

so that

$$\int_{-\epsilon}^{\epsilon} \psi(x) \frac{d\delta(x)}{dx} dx = - \left[ \frac{d\psi(x)}{dx} \right]_{x=0}. \quad (4.24)$$

For example, let  $\psi(x) = x$ , in which case

$$\int_{-\epsilon}^{\epsilon} x \frac{d\delta(x)}{dx} dx = -1, \quad (4.25)$$

which can be formally written

$$x (d\delta(x)/dx) = -\delta(x). \quad (4.26)$$

### 4.2.7 Temporal Dirac delta and impulses

Poisson's equation for the gravitational potential is an elliptic partial differential equation (see Section 3.5), in which there is no time derivative. We now introduce the temporal Dirac delta to build towards our study of evolution equations, such as the diffusion equation of Section 4.7 and the advection-diffusion equation of Section 46.10. The temporal Dirac delta is a point source that is turned on just at one time instance and it is normalized according to

$$\int_{\mathcal{T}} \delta(t) dt = 1, \quad (4.27)$$

where  $\mathcal{T}$  is a time interval containing the source time,  $t = 0$ . This normalization means that  $\delta(t)$  has dimensions of inverse time. The temporal Dirac delta also possesses the sifting property from Section 4.2.2, in which

$$\int_{\mathcal{T}} \delta(t) \psi(t) dt = \psi(t = 0). \quad (4.28)$$

In the study of transient behavior of dynamical systems, it is often of interest to examine the response of the system to an idealized force,  $\mathcal{F}(t)$ , where the force occurs over a small time increment. The time integral of this force is referred to as the *impulse*

$$I(\tau) = \int_{-\tau}^{\tau} \mathcal{F}(t) dt. \quad (4.29)$$

If the force is further idealized to occur just at a single moment in time, and it is normalized to unity, then we have the *unit impulse*, which is just the integral of the Dirac delta

$$I(\tau) = 1 = \int_{-\tau}^{\tau} \delta(t) dt. \quad (4.30)$$

The corresponding response of the dynamical system is referred to as the *impulse response function*. If the dynamical system is linear, then the impulse response function equals to the Green's function for the initial value problem. We further discuss the response function in Section 4.8.

### 4.2.8 Shifting the space-time position of the source

Thus far we have assumed the point source is located at the origin in space and time. But there is nothing special about that point. Correspondingly, we can arbitrarily place the source at  $(\mathbf{x}_0, t_0)$ , in which case the Dirac delta is written

$$\delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0) = \delta(x - x_0) \delta(y - y_0) \delta(z - z_0) \delta(t - t_0). \quad (4.31)$$

Defining the region,  $\mathcal{R}$ , to now encompass the source point in space,  $\mathbf{x} = \mathbf{x}_0$ , and the time increment  $\mathcal{T}$  to encompasses the source time,  $t = t_0$ , we have the normalization condition

$$\int_{\mathcal{R}} \int_{\mathcal{T}} \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0) dV dt = 1, \quad (4.32)$$

as well as the sifting property

$$\int_{\mathcal{R}} \int_{\mathcal{T}} \psi(\mathbf{x}, t) \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0) dV dt = \psi(\mathbf{x}_0, t_0). \quad (4.33)$$

## 4.3 Laplace's free space Green's function

We introduced the Dirac delta by considering the Newtonian gravitational potential in the presence of a point mass source. This physical example also serves to introduce the notion of a Green's function, in this case a particularly simple Green's function known as a *free space Green's function* for Laplace's equation. The free space Green's function serves an important role in the analytical theory of Green's functions, and it offers us a pedagogical introduction to Green's functions.

### 4.3.1 Gravitational potential from a point mass source

Consider the gravitational potential,  $\Phi$ , in the presence of a point mass source at  $\mathbf{x} = \mathbf{x}_0$  in the absence of boundaries (i.e., in *free space*), and with an assumed decay of the potential when moving away from the source. In the study of Green's functions this potential is referred to as the *fundamental solution* to Laplace's equation. In other contexts it is referred to as the *free space Green's function*, which is the terminology we choose, where “free space” refers to the absence of any spatial boundaries. From the discussion in Section 4.2.1, the free space Green's function for Newtonian gravity satisfies the Poisson equation with a point mass source

$$\nabla_{\mathbf{x}}^2 \Phi(\mathbf{x}|\mathbf{x}_0) = 4\pi G^{\text{grv}} M \delta(\mathbf{x} - \mathbf{x}_0) \quad \text{and} \quad \Phi(\mathbf{x}|\mathbf{x}_0) \rightarrow 0 \text{ as } |\mathbf{x}| \rightarrow \infty, \quad (4.34)$$

where we wrote the point mass density in terms of the Dirac delta

$$\rho(\mathbf{x}|\mathbf{x}_0) = M \delta(\mathbf{x} - \mathbf{x}_0). \quad (4.35)$$

The first argument to the potential,  $\mathbf{x}$ , is the point where the field is sampled and is referred to as the *field point* or sometimes the *observation point*. The second argument,  $\mathbf{x}_0$ , is where the source is located and is thus referred to as the *source point*. Figure 4.2 summarizes the notation. The Laplacian operator acts on the field point and is written as  $\nabla_{\mathbf{x}}^2$  for clarity. The dimensional multiplier,  $4\pi G^{\text{grv}} M$ , acting on the Dirac delta in equation (4.34) is specific to the physical problem, here being for Newtonian gravity. In this case the Green's function has dimensions of  $L^2 T^{-2}$  since it is a gravitational potential. In other cases, the Green's function will have distinct dimensions, whereas the Dirac delta remains with the same dimensions.<sup>7</sup>

The gravitational potential for a point mass source, in the absence of any boundaries, is the free space Green's function for Newtonian gravity. From Section 9.12.2 we can write this free

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<sup>7</sup> As emphasized throughout this book, checking for physical dimensional consistency offers a powerful means to ensure that a mathematical expression makes physical sense. If the equation is not dimensionally consistent, then something is wrong either with the maths or the physics.

space Green's function in the familiar form

$$\Phi(\mathbf{x}|\mathbf{x}_0) = -\frac{M G^{\text{grav}}}{|\mathbf{x} - \mathbf{x}_0|}. \quad (4.36)$$

This function is singular when sampling the field at the source location,  $\mathbf{x} = \mathbf{x}_0$ , and it decreases according to the inverse distance when moving away from the source.

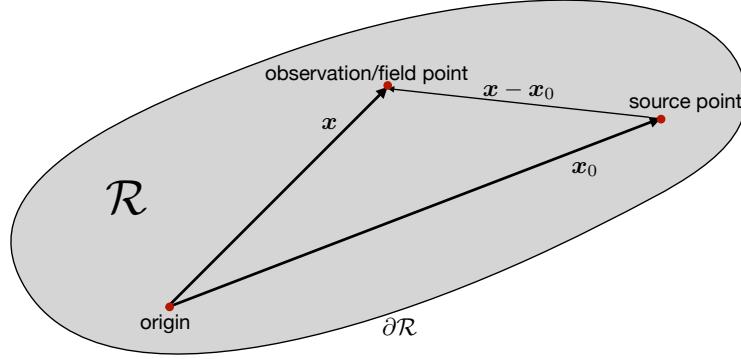


FIGURE 4.2: Depicting the geometry of a typical Green's function problem in space, shown here for a finite domain whereas the free-space Green's function has no boundaries. The field or observation point,  $\mathbf{x}$ , is where the Green's function is sampled, whereas the source point,  $\mathbf{x}_0$ , is where the Dirac delta source is located. The origin is at an arbitrary position within the domain,  $\mathcal{R}$ , whose boundary is written  $\partial\mathcal{R}$ .

### 4.3.2 Free space Green's function for Laplace's equation

Abstracting the previous discussion motivates us to define the free space Green's function,  $\mathcal{G}(\mathbf{x}|\mathbf{x}_0)$ , for the Laplace operator as the solution to the singular Poisson equation

$$-\nabla_{\mathbf{x}}^2 \mathcal{G}(\mathbf{x}|\mathbf{x}_0) = \delta(\mathbf{x} - \mathbf{x}_0) \quad \text{and} \quad \mathcal{G}(\mathbf{x}|\mathbf{x}_0) \rightarrow 0 \text{ as } |\mathbf{x}| \rightarrow \infty. \quad (4.37)$$

It is conventional in many treatments to place a minus sign on the Laplacian operator to correspond to how it appears in the diffusion equation of Section 4.7. In one, two and three space dimensions the free space Green's function is given by

$$\mathcal{G}(\mathbf{x}|\mathbf{x}_0) = -|\mathbf{x} - \mathbf{x}_0|/2 \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \mathbb{R}^1 \quad (4.38a)$$

$$\mathcal{G}(\mathbf{x}|\mathbf{x}_0) = -(2\pi)^{-1} \ln |\mathbf{x} - \mathbf{x}_0| \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \mathbb{R}^2 \quad (4.38b)$$

$$\mathcal{G}(\mathbf{x}|\mathbf{x}_0) = (4\pi |\mathbf{x} - \mathbf{x}_0|)^{-1} \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \mathbb{R}^3. \quad (4.38c)$$

We study the three-dimensional Green's function in Section 4.3.3 and encounter the one-dimensional Green's function in Section 4.4.

### 4.3.3 Details of the three-dimensional free space Green's function

We here verify that the expression (4.38c) is indeed the free space Green's function for  $\mathbb{R}^3$ . This exercise provides some exposure to some of the formal manipulations encountered with Dirac deltas and Green's functions.

To simplify notation place the Dirac delta at  $\mathbf{x}_0 = 0$  so that

$$\mathcal{G}(\mathbf{x}|0) = \frac{1}{4\pi r}, \quad (4.39)$$

where  $|\mathbf{x}| = r$  is the radial distance from the origin. Introduce the continuous and non-singular function

$$G^{(\epsilon)}(\mathbf{x}) = \frac{1}{4\pi} \begin{cases} r^{-1} & \text{for } r > \epsilon \\ \epsilon^{-1} & \text{for } r \leq \epsilon, \end{cases} \quad (4.40)$$

with  $\epsilon > 0$ , in which case  $G^{(\epsilon)}(\mathbf{x})$  has removed the singularity at  $r = 0$ . Now consider the integral

$$\mathcal{I}(\epsilon) = \int_{r \leq \epsilon} \psi(\mathbf{x}) \nabla^2 G^{(\epsilon)}(\mathbf{x}) dV, \quad (4.41)$$

for an arbitrary smooth function  $\psi$  and for a spherical region of radius  $r = \epsilon$  centered on the origin. Since  $\psi$  is a smooth function, taking the limit as  $\epsilon \rightarrow 0$  allows us to remove  $\psi$  from the integral

$$\lim_{\epsilon \rightarrow 0} \mathcal{I}(\epsilon) = \psi(r = 0) \lim_{\epsilon \rightarrow 0} \left[ \int_{r \leq \epsilon} \nabla^2 G^{(\epsilon)}(\mathbf{x}) dV \right]. \quad (4.42)$$

Making use of the divergence theorem brings the volume integral to a surface integral over the  $\epsilon$ -sphere

$$\lim_{\epsilon \rightarrow 0} \mathcal{I}(\epsilon) = \psi(r = 0) \lim_{\epsilon \rightarrow 0} \left[ 4\pi \int_{r=\epsilon} \hat{\mathbf{r}} \cdot \nabla(1/r) r^2 dr \right] = -4\pi \psi(r = 0), \quad (4.43)$$

where we introduced spherical coordinates from Section 8.2. This result establishes the sifting property for  $\nabla^2 |\mathbf{x}|^{-1}$  and hence allows us to write

$$-\nabla^2 \frac{1}{4\pi |\mathbf{x}|} = \delta(\mathbf{x}). \quad (4.44)$$

## 4.4 One-dimensional Poisson's equation

To illustrate the Green's function method for solving differential equations, consider the one-dimensional Poisson equation on a finite domain

$$-\frac{d^2\psi}{dx^2} = \Lambda \quad \text{for } -L \leq x \leq L, \quad (4.45)$$

with boundary conditions unspecified at this point. The corresponding Green's function satisfies

$$-\frac{d^2G(x|x_0)}{dx^2} = \delta(x - x_0) \quad \text{for } -L \leq x, x_0 \leq L, \quad (4.46)$$

with boundary conditions taken as the homogeneous form of the boundary conditions satisfied by  $\psi$ . For the Green's function problem, the source,  $\Lambda(x)$ , appearing in the  $\psi$  equation has been replaced by the Dirac delta,  $\delta(x - x_0)$ . Since the Dirac delta has dimensions of inverse length, equation (4.46) implies that the Green's function has dimensions of length. Keeping track of physical dimensions offers a powerful means to check the integrity of the mathematical manipulations.

### 4.4.1 Integral expression for $\psi$ in terms of $G$

Multiplying the differential equation (4.45) with  $G$  and the Green's function equation (4.46) with  $\psi$ , and then subtracting, yields

$$-G(x|x_0) \frac{d^2\psi(x)}{dx^2} + \psi(x) \frac{d^2G(x|x_0)}{dx^2} = G(x|x_0) \Lambda(x) - \psi(x) \delta(x - x_0). \quad (4.47)$$

Integrating this equation over the domain, and use of the sifting property (4.7), yields

$$\psi(x_0) = \int_{-L}^L G(x|x_0) \Lambda(x) dx + \int_{-L}^L \left[ G(x|x_0) \frac{d^2\psi(x)}{dx^2} - \psi(x) \frac{d^2G(x|x_0)}{dx^2} \right] dx \quad (4.48a)$$

$$= \int_{-L}^L G(x|x_0) \Lambda(x) dx + \int_{-L}^L \frac{d}{dx} \left[ G(x|x_0) \frac{d\psi}{dx} - \psi(x) \frac{dG(x|x_0)}{dx} \right] dx \quad (4.48b)$$

$$= \int_{-L}^L G(x|x_0) \Lambda(x) dx + \left[ G(x|x_0) \frac{d\psi}{dx} \right]_{x=-L}^{x=L} - \left[ \psi(x) \frac{dG(x|x_0)}{dx} \right]_{x=-L}^{x=L}, \quad (4.48c)$$

where the final expression exposed the boundary contributions. Specializing to *Dirichlet boundary conditions*, with  $G(x = \pm L|x_0) = 0$ , renders

$$\psi^{\text{Dirichlet}}(x_0) = \int_{-L}^L G(x|x_0) \Lambda(x) dx - \left[ \psi(x) \frac{dG(x|x_0)}{dx} \right]_{x=L} + \left[ \psi(x) \frac{dG(x|x_0)}{dx} \right]_{x=-L}, \quad (4.49)$$

whereas the solution with *Neumann boundary conditions*, where  $dG(x = \pm L|x_0)/dx = 0$ , is

$$\psi^{\text{Neumann}}(x_0) = \int_{-L}^L G(x|x_0) \Lambda(x) dx + \left[ G(x|x_0) \frac{d\psi(x)}{dx} \right]_{x=L} - \left[ G(x|x_0) \frac{d\psi(x)}{dx} \right]_{x=-L}. \quad (4.50)$$

#### 4.4.2 Preliminary steps for obtaining the Green's function

The solution to the Green's function equation (4.46) is given by the linear functions

$$G(x|x_0) = \begin{cases} Ax + B & \text{for } -L \leq x \leq x_0 \\ Cx + D & \text{for } x_0 \leq x \leq L. \end{cases} \quad (4.51)$$

The constants  $A, B, C, D$  are determined by the following conditions: (i) jump condition for  $dG(x|x_0)/dx$  at  $x = x_0$ , (ii) continuity of  $G(x|x_0)$  at  $x = x_0$ , and (iii) homogeneous boundary conditions at  $x = \pm L$ .

##### *Jump condition for the Green's function derivative at $x = x_0$*

The Green's function differential equation (4.46) shows that the second derivative to the Green's function equals to a Dirac delta. Integrating this equation over an arbitrary region straddling  $x = x_0$  yields the finite jump condition for the first derivative of the Green's function

$$\lim_{\epsilon \rightarrow 0} \left[ \frac{dG(x|x_0)}{dx} \right]_{x=x_0+\epsilon} - \lim_{\epsilon \rightarrow 0} \left[ \frac{dG(x|x_0)}{dx} \right]_{x=x_0-\epsilon} = -1. \quad (4.52)$$

That is, the derivative of the Green's function is not continuous across the point  $x = x_0$ . Instead, it has a finite jump. Making use of this condition in equation (4.51) leads to  $C = A - 1$  so that

$$G(x|x_0) = \begin{cases} Ax + B & \text{for } -L \leq x \leq x_0 \\ (A - 1)x + D & \text{for } x_0 \leq x \leq L. \end{cases} \quad (4.53)$$

##### *Continuity of the Green's function at $x = x_0$*

A finite jump in the derivative at  $x = x_0$  means that the Green's function is continuous at this point

$$\lim_{\epsilon \rightarrow 0} G(x = x_0 + \epsilon|x_0) = \lim_{\epsilon \rightarrow 0} G(x = x_0 - \epsilon|x_0). \quad (4.54)$$

Making use of this condition in equation (4.53) yields

$$G(x|x_0) = \begin{cases} Ax - x_0 + D & \text{for } -L \leq x \leq x_0 \\ (A-1)x + D & \text{for } x_0 \leq x \leq L. \end{cases} \quad (4.55)$$

#### 4.4.3 Green's function satisfying Dirichlet boundary conditions

The two constants  $A$  and  $D$  in equation (4.55) are determined by specifying the boundary conditions. With Dirichlet conditions we set  $G(x = \pm L|x_0) = 0$ , which then leads to

$$G(x|x_0) = \frac{1}{2L} \begin{cases} (L-x_0)(L+x) & \text{for } -L \leq x \leq x_0 \\ (L-x)(L+x_0) & \text{for } x_0 \leq x \leq L, \end{cases} \quad (4.56)$$

which is depicted in Figure 4.3. The structure of this function motivates the name *impulse response function* or *influence function*. We identify the following properties of this Green's function, with these properties also appearing in the higher dimension elliptical problems discussed in Sections 4.5 and 4.6.

##### *Reciprocity condition*

The Green's function (4.56) satisfies the symmetry condition

$$G(x|x_0) = G(x_0|x), \quad (4.57)$$

so that the Green's function is invariant under interchange of the source point,  $x_0$ , and field point,  $x$ . In Section 4.5.4, we show how this *reciprocity condition* generally holds for all Green's functions of the Poisson equation.

##### *Sum of free-space Green's function plus harmonic function*

We can write the Green's function (4.56) as the sum of the free space Green's function (4.38a) plus a harmonic function

$$G(x|x_0) = -|x - x_0|/2 + \frac{L^2 - x x_0}{2L} = \mathcal{G}(x|x_0) + H(x|x_0), \quad (4.58)$$

where

$$-\frac{d^2H(x|x_0)}{dx^2} = 0 \quad \text{and} \quad H(x = \pm L|x_0) = -\mathcal{G}(x = \pm L|x_0). \quad (4.59)$$

As shown in Section 4.5.3, the Green's function for an elliptic PDE generally takes on this form.

##### *Boundary condition satisfied by Green's function derivative*

The Green's function is itself independent of the Dirichlet boundary conditions placed on the function  $\psi$ , as well as the source function  $\Lambda$ . Hence, we can establish general properties of the Green's function by considering special cases for the boundary conditions and source function. For this purpose, set  $\Lambda = 0$  and  $\psi(x = -L) = \psi(x = L)$ , in which case  $\psi$  is itself a constant throughout the domain. The Dirichlet solution (4.49) then leads to the condition placed on the Green's function derivatives at the boundaries

$$\left[ \frac{dG(x|x_0)}{dx} \right]_{x=L} - \left[ \frac{dG(x|x_0)}{dx} \right]_{x=-L} = -1. \quad (4.60)$$

Interpreting  $G$  as a tracer concentration, this result means that the positive tracer input by the Dirac delta source is exactly balanced by a negative tracer departing the region through its boundaries. It is by this balance that the Green's function is able to maintain its homogeneous Dirichlet boundary condition,  $G(x = \pm L|x_0) = 0$ . A similar interpretation holds when  $G$  is the gravitational potential induced by the Dirac source in the region interior. In this case, for the gravitational potential to vanish on the boundaries, the positive gravitational acceleration induced by the Dirac delta source at  $x = x_0$  must be compensated by an opposing gravitational acceleration along the boundaries.

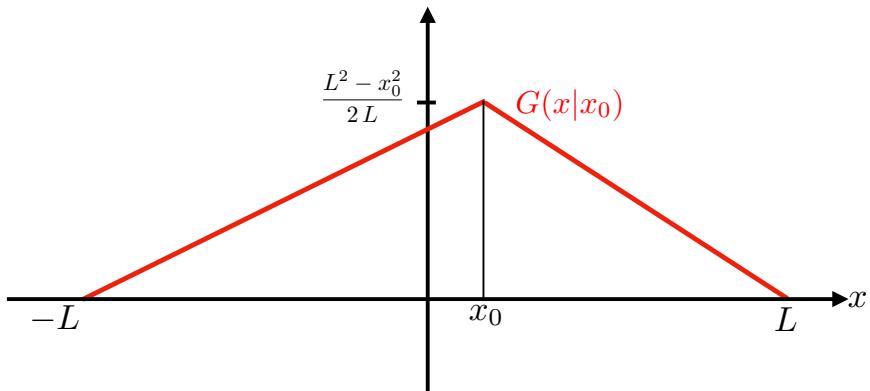


FIGURE 4.3: The Green's function (4.56) for the one-dimensional Poisson equation satisfying Dirichlet boundary conditions at  $x = \pm L$ . The Dirac delta source is located at  $x = x_0$ , which is the point where the Green's function has its maximum displacement of  $(L^2 - x_0^2)/(2L)$ .

#### 4.4.4 Green's function satisfying Neumann boundary conditions

A constant is the only solution to  $-d^2G/dx^2 = 0$  with homogeneous Neumann boundary conditions,  $dG/dx = 0$  at  $x = \pm L$ . However, a constant cannot satisfy the derivative jump condition at  $x = x_0$ , and thus cannot satisfy the differential equation  $-d^2G/dx^2 = \delta(x - x_0)$ . Hence, there is no Green's function satisfying Neumann boundary conditions for a one-dimensional bounded domain. As we will see, in higher space dimensions there are nontrivial Green's functions for the Neumann boundary case. Even so, this result identifies a key condition required for a Green's function to exist. Namely, if the completely homogeneous problem ( $\Lambda = 0$  with homogeneous boundary conditions) only has the trivial solution, then the Green's function exists and is unique. For the case of Dirichlet boundary conditions

$$-\frac{d^2\psi}{dx^2} = 0 \quad \text{and} \quad \psi(x = \pm L) = 0 \implies \psi = 0, \quad (4.61)$$

whereas for Neumann boundary conditions

$$-\frac{d^2\psi}{dx^2} = 0 \quad \text{and} \quad \left[ \frac{d\psi}{dx} \right]_{x=\pm L} = 0 \implies \psi = \text{constant}. \quad (4.62)$$

The existence of a nontrivial (an arbitrary constant) solution to the one-dimensional homogeneous Neumann boundary value problem signals the absence of a Green's function.

#### 4.4.5 Uniqueness of the solution to the Dirichlet problem

Consider again the Dirichlet problem

$$-\frac{d^2\psi}{dx^2} = \Lambda \quad \text{for } -L \leq x \leq L \quad \text{with} \quad \psi(x = \pm L) = \text{prescribed constants.} \quad (4.63)$$

To prove that the solution to this problem is unique, assume there are two distinct solution,  $\psi_a$  and  $\psi_b$ , and define  $\Psi = \psi_a - \psi_b$ . By construction,  $\Psi$  satisfies Laplace's equation with homogeneous Dirichlet boundaries

$$-\frac{d^2\Psi}{dx^2} = 0 \quad \text{for } -L \leq x \leq L, \quad \Psi(x = \pm L) = 0. \quad (4.64)$$

As discussed above, the only solution to this problem is  $\Psi = 0$ , which means that  $\psi_a = \psi_b$ , hence proving that the solution to equation (4.63) is unique. Uniqueness holds regardless the source function, so that the Green's function from Section 4.4.3 is also unique.

## 4.5 Poisson's equation with Dirichlet boundaries

In this section we develop the Green's function method for Poisson's equation in three-dimensions with a *Dirichlet boundary condition*

$$-\nabla^2\psi = \Lambda, \quad \text{for } \mathbf{x} \in \mathcal{R} \quad \text{and} \quad \psi = \sigma, \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.65)$$

We separately consider the Neumann boundary condition in Section 4.6, whereby  $\hat{\mathbf{n}} \cdot \nabla\psi$  is specified on the boundary rather than  $\psi$  itself. Although the Dirichlet and Neumann problems share many features, there are sufficient distinctions to warrant a separate treatment.

In the following, our mathematical goal is to determine an integral expression for  $\psi$  in terms of the distributed source and boundary data. Before doing so, we highlight the two elements determining the solution to any boundary value problem. First there is the partial differential operator (here the Laplacian) and the distributed source,  $\Lambda$ , both of which operate within the region interior,  $\mathbf{x} \in \mathcal{R}$ . Second, there is the boundary data that prescribes the solution (either its value or its boundary normal derivative) for points on the boundary,  $\mathbf{x} \in \partial\mathcal{R}$ . The distributed source can be defined everywhere, including the boundary. However, it only affects the solution for points within the region interior since the boundary conditions determine the boundary structure. Conversely, the boundary conditions are only prescribed along the boundary, and yet they affect the solution throughout the interior. A key feature of the Green's function method is that it clearly delineates these aspects of the solution, and in so doing it provides both a conceptual and computational framework.

#### 4.5.1 Constraints on the source and boundary normal derivative

Assuming there exists a solution to the boundary value problem (4.65), we can derive a constraint on the normal derivative of  $\psi$  along the domain boundary.<sup>8</sup> This constraint is revealed by integrating the Poisson equation (4.65) over the spatial domain, with the left hand side yielding

$$-\int_{\mathcal{R}} \nabla^2\psi \, dV = -\oint_{\partial\mathcal{R}} \nabla\psi \cdot \hat{\mathbf{n}} \, dS, \quad (4.66)$$

---

<sup>8</sup>To be self-contained, we here repeat the discussion of the constraint (4.67) that is also provided in Section 3.5.6.

where we made use of the divergence theorem. Equating this result to the integral of the source,  $\Lambda$ , leads to the constraint

$$\oint_{\partial\mathcal{R}} \nabla\psi \cdot \hat{\mathbf{n}} \, dS = - \int_{\mathcal{R}} \Lambda \, dV. \quad (4.67)$$

We can physically understand this constraint by invoking the steady state tracer diffusion interpretation of the Poisson equation. For a steady state solution to exist in the presence of specified boundary tracer concentration along with interior sources, there must be a balance between the normal gradient of the tracer concentration, as integrated over the boundary, plus the volume integrated source in the interior. This balance is required to maintain the specified Dirichlet boundary values in the presence of the interior source. Absent this balance, there will be depletion or accumulation of  $\psi$  that leads to a transient adjustment, thus breaking the steady state assumption. Notably, the constraint (4.67) can be realized for arbitrary Dirichlet boundary data,  $\sigma$ . An analogous interpretation holds when  $\psi$  is the gravitational potential resulting from the mass source,  $\Lambda$ . For  $\psi$  to be a specified value along the domain boundary requires the volume integrated mass source to balance a gravitational acceleration integrated along the boundary.

### 4.5.2 Uniqueness of the solution

Just like the one-dimensional case in Section 4.4.5, we can readily establish uniqueness of the solution to the Dirichlet problem by considering two functions,  $\psi_a$  and  $\psi_b$ , each satisfying the boundary value problem (4.65). In turn, their difference,  $\Psi = \psi_a - \psi_b$ , satisfies the homogeneous problem

$$-\nabla^2\Psi = 0, \quad \text{for } \mathbf{x} \in \mathcal{R} \quad \text{and} \quad \Psi = 0, \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.68)$$

The solution to this Laplace equation is  $\Psi = 0$ , which then means that  $\psi_a = \psi_b$  so that the solution to equation (4.65) is unique. This result also means that the Green's function considered in Section 4.5.3 is unique.

For the skeptic, let us provide a more formal proof that the solution to equation (4.68) is indeed zero. To do so, assume it is not zero and see what happens. First consider the case where  $\Psi$  is a constant, so that  $\psi_a - \psi_b = \text{constant}$ . But zero is the only constant that can satisfy the Dirichlet boundary condition,  $\Psi = 0$ . Next, assume  $\Psi$  has spatial dependence so that  $\nabla\Psi \neq 0$  and consider the non-negative integral over the domain

$$\mathcal{I} = \int_{\mathcal{R}} \nabla\Psi \cdot \nabla\Psi \, dV. \quad (4.69)$$

Since  $\nabla^2\Psi = 0$  we have  $\nabla \cdot (\Psi \nabla\Psi) = \nabla\Psi \cdot \nabla\Psi$  so that

$$\mathcal{I} = \int_{\mathcal{R}} \nabla \cdot (\Psi \nabla\Psi) \, dV = \oint_{\partial\mathcal{R}} \Psi \nabla\Psi \cdot \hat{\mathbf{n}} \, dS, \quad (4.70)$$

where we used the divergence theorem. But since  $\Psi = 0$  on  $\partial\mathcal{R}$  we find that  $\mathcal{I} = 0$ , in which case  $\nabla\Psi = 0$  everywhere. We are thus led to  $\Psi = 0$  throughout the domain, thus allowing us to conclude that the solution to the boundary value problem (4.65) is indeed unique.

### 4.5.3 The Green's function problem

The Green's function corresponding to the boundary value problem (4.65) is the solution to the Poisson equation with a Dirac delta source (rather than  $\Lambda$ ) and a homogeneous Dirichlet boundary

condition (rather than  $\sigma$ )

$$-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0) = \delta(\mathbf{x} - \mathbf{x}_0) \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \mathcal{R} \quad \text{and} \quad G(\mathbf{x}|\mathbf{x}_0) = 0, \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.71)$$

For this three-dimensional problem, we see that the Green's function has dimensions of inverse length since the Dirac delta has dimensions of inverse volume. By construction, the Green's function,  $G(\mathbf{x}|\mathbf{x}_0)$ , is harmonic everywhere except at the location of the singular Dirac delta source,  $\mathbf{x} = \mathbf{x}_0$ , at which point the Green's function equals to minus the inverse Laplacian of the Dirac delta. Furthermore, the Green's function satisfies a homogenous Dirichlet boundary condition whenever the field point,  $\mathbf{x}$ , is on the boundary and for an arbitrary source position,  $\mathbf{x}_0$ .

#### *Connection to the free space Green's function*

Since  $G(\mathbf{x}|\mathbf{x}_0)$  satisfies a boundary condition, it is distinct from the free space Green's function,  $\mathcal{G}(\mathbf{x}|\mathbf{x}_0)$ , which has no concern for boundaries. Even so, linearity enables us to write the Green's function as the sum of the free space Green's function plus a harmonic function

$$G(\mathbf{x}|\mathbf{x}_0) = \mathcal{G}(\mathbf{x}|\mathbf{x}_0) + H(\mathbf{x}|\mathbf{x}_0), \quad (4.72)$$

where the free space Green's function and harmonic function satisfy

$$-\nabla_{\mathbf{x}}^2 \mathcal{G}(\mathbf{x}|\mathbf{x}_0) = \delta(\mathbf{x} - \mathbf{x}_0) \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \mathbb{R}^3 \quad (4.73a)$$

$$-\nabla_{\mathbf{x}}^2 H(\mathbf{x}|\mathbf{x}_0) = 0 \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \mathcal{R} \quad (4.73b)$$

$$-H(\mathbf{x}|\mathbf{x}_0) = \mathcal{G}(\mathbf{x}|\mathbf{x}_0) \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.73c)$$

Assuming we know the free space Green's function from equation (4.38c), the mathematical problem of finding  $G(\mathbf{x}|\mathbf{x}_0)$  reduces to finding the harmonic function,  $H(\mathbf{x}|\mathbf{x}_0)$ , satisfying the inhomogeneous Dirichlet boundary condition (4.73c).

Although the Green's function,  $G$ , cares about the existence of spatial boundaries, it is independent of the boundary data,  $\sigma$ , and the distributed source,  $\Lambda$ , that appear in the boundary value problem (4.65) for  $\psi$ . In that manner, the Green's function is connected to the original boundary value problem only through the differential operator (here the Laplacian) and the type of boundary condition (here the Dirichlet condition).

#### *Jump condition induced by the Dirac source*

Integrating the Green's function partial differential equation (4.71) over a volume,  $\mathcal{R}_0$ , that encloses the Dirac delta source point at  $\mathbf{x}_0 \in \mathcal{R}_0$  leads to

$$\int_{\mathcal{R}_0} \nabla_{\mathbf{x}} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0) dV = \oint_{\partial\mathcal{R}_0} \hat{\mathbf{n}} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0) dS = -1, \quad (4.74)$$

where we used the divergence theorem for the first equality. This result means that for any domain enclosing the Dirac source point, the normal derivative of the Green's function has a jump condition across the boundary of this region. We encountered this property in Section 4.4.2 for the one-dimensional Green's function, and will see it again when discussing the boundary Green's function in Section 4.5.6.

#### 4.5.4 Reciprocity of the Green's function

The Green's function satisfies reciprocity

$$G(\mathbf{x}|\mathbf{x}_0) = G(\mathbf{x}_0|\mathbf{x}), \quad (4.75)$$

with this property holding for both Dirichlet and Neumann boundary conditions. As introduced in Section 4.4.3 for the one-dimensional Poisson equation, reciprocity says that the Green's function at the field point,  $\mathbf{x}$ , arising from a Dirac delta source at the source point,  $\mathbf{x}_0$  is identical to the Green's function at the field point,  $\mathbf{x}_0$ , arising from a Dirac delta source at point,  $\mathbf{x}$ . By inspection, the free space Green's functions (4.38a)-(4.38c) satisfy reciprocity. Hence, by implication the harmonic function,  $H(\mathbf{x}|\mathbf{x}_0)$ , also satisfies reciprocity. Even so, we find it pedagogically useful to offer a direct derivation of reciprocity by using steps similar to those used for establishing the second form of Green's integral identity (2.71). These steps are utilized for many purposes when working with Green's functions.

##### *Derivation of reciprocity*

Consider the two Green's functions,  $G(\mathbf{x}|\mathbf{a})$  and  $G(\mathbf{x}|\mathbf{b})$ , arising from Dirac delta sources at source points  $\mathbf{a} \in \mathcal{R}$  and  $\mathbf{b} \in \mathcal{R}$

$$-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{a}) = \delta(\mathbf{x} - \mathbf{a}) \quad (4.76a)$$

$$-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{b}) = \delta(\mathbf{x} - \mathbf{b}). \quad (4.76b)$$

Multiplying the first equation by  $G(\mathbf{x}, \mathbf{b})$  and the second by  $G(\mathbf{x}, \mathbf{a})$ , and subtracting leads to

$$-G(\mathbf{x}|\mathbf{b}) \nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{a}) + G(\mathbf{x}|\mathbf{a}) \nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{b}) = G(\mathbf{x}|\mathbf{b}) \delta(\mathbf{x} - \mathbf{a}) - G(\mathbf{x}|\mathbf{a}) \delta(\mathbf{x} - \mathbf{b}). \quad (4.77)$$

Now integrate this equation over the region  $\mathcal{R}$ , with the right hand side rendering

$$\int_{\mathcal{R}} [G(\mathbf{x}|\mathbf{b}) \delta(\mathbf{x} - \mathbf{a}) - G(\mathbf{x}|\mathbf{a}) \delta(\mathbf{x} - \mathbf{b})] dV = G(\mathbf{a}, \mathbf{b}) - G(\mathbf{b}, \mathbf{a}), \quad (4.78)$$

where we made use of the sifting property (4.7). Integrating the left hand side of equation (4.77) leads to

$$\int_{\mathcal{R}} [-G(\mathbf{x}|\mathbf{b}) \nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{a}) + G(\mathbf{x}|\mathbf{a}) \nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{b})] dV \quad (4.79a)$$

$$= \int_{\mathcal{R}} [-\nabla_{\mathbf{x}} \cdot [G(\mathbf{x}|\mathbf{b}) \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{a})] + \nabla_{\mathbf{x}} \cdot [G(\mathbf{x}|\mathbf{a}) \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{b})]] dV \quad (4.79b)$$

$$= \oint_{\partial\mathcal{R}} [-G(\mathbf{x}|\mathbf{b}) \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{a}) + G(\mathbf{x}|\mathbf{a}) \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{b})] \cdot \hat{\mathbf{n}} dS, \quad (4.79c)$$

where we made use of the divergence theorem for the second equality. The final result vanishes when making use of either the homogeneous Dirichlet boundary condition (4.71) or the homogeneous Neumann boundary condition (4.102) considered in Section 4.6. We are thus led to the reciprocity relation (4.75).

##### *Comments on self-adjoint operators*

Reciprocity in the relatively simple form of equation (4.75) is a signature of *self-adjoint* differential operators. Self-adjointness reflects properties of both the differential operator and the boundary

conditions, with the discussion in this section revealing that the Laplacian operator is self-adjoint with either Dirichlet or Neumann boundary conditions. Operators that are not self-adjoint, such as the diffusion operator in Section 4.7, satisfy a slightly more general reciprocity relation (see Section 4.7.4).

The absence of self-adjointness reflects some form of symmetry breaking either through the operator itself or through the boundary and/or initial conditions. The diffusion operator has a single time derivative,  $\partial_t$ , which breaks symmetry between past and future thus leading to the absence of self-adjointness. Furthermore, self-adjointness is a property that depends on the nature of the chosen inner product, with the inner product in the present discussion defined by integration over the domain  $\mathcal{R}$ . See [Stakgold \(2000a,b\)](#) for a thorough discussion accessible to physicists.

### 4.5.5 The integral solution

We have the elements in place to determine  $\psi$  as an integral expression involving  $G(\mathbf{x}|\mathbf{x}_0)$  along with the prescribed source,  $\Lambda$ , and boundary data,  $\sigma$ . To do so we follow steps similar to those used to establish reciprocity. Recall the Poisson boundary value problem for  $\psi$  and the associated Green's function problem, here exposing arguments for clarity

$$-\nabla_{\mathbf{x}}^2 \psi(\mathbf{x}) = \Lambda(\mathbf{x}) \quad (4.80a)$$

$$-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0) = \delta(\mathbf{x} - \mathbf{x}_0). \quad (4.80b)$$

Multiply the  $\psi(\mathbf{x})$  equation by  $G(\mathbf{x}|\mathbf{x}_0)$  and the  $G(\mathbf{x}|\mathbf{x}_0)$  equation by  $\psi(\mathbf{x})$  to find

$$-G(\mathbf{x}|\mathbf{x}_0) \nabla_{\mathbf{x}}^2 \psi(\mathbf{x}) = G(\mathbf{x}|\mathbf{x}_0) \Lambda(\mathbf{x}) \quad (4.81a)$$

$$-\psi(\mathbf{x}) \nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0) = \psi(\mathbf{x}) \delta(\mathbf{x} - \mathbf{x}_0), \quad (4.81b)$$

and then subtract these two equations

$$-G(\mathbf{x}|\mathbf{x}_0) \nabla_{\mathbf{x}}^2 \psi(\mathbf{x}) + \psi(\mathbf{x}) \nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0) = G(\mathbf{x}|\mathbf{x}_0) \Lambda(\mathbf{x}) - \psi(\mathbf{x}) \delta(\mathbf{x} - \mathbf{x}_0). \quad (4.82)$$

Now integrate over observational points,  $\mathbf{x}$ , sampled over the region  $\mathcal{R}$ , in which case the right hand side becomes

$$\int_{\mathcal{R}} [G(\mathbf{x}|\mathbf{x}_0) \Lambda(\mathbf{x}) - \psi(\mathbf{x}) \delta(\mathbf{x} - \mathbf{x}_0)] dV = -\psi(\mathbf{x}_0) + \int_{\mathcal{R}} G(\mathbf{x}|\mathbf{x}_0) \Lambda(\mathbf{x}) dV, \quad (4.83)$$

where we made use of the sifting property (4.7) to expose the function,  $\psi$ , at the location of the Dirac source,  $\mathbf{x}_0$ . Integrating the left hand side of equation (4.82) yields

$$\int_{\mathcal{R}} [-G(\mathbf{x}|\mathbf{x}_0) \nabla_{\mathbf{x}}^2 \psi(\mathbf{x}) + \psi(\mathbf{x}) \nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0)] dV \quad (4.84a)$$

$$= \int_{\mathcal{R}} \nabla_{\mathbf{x}} \cdot [-G(\mathbf{x}|\mathbf{x}_0) \nabla_{\mathbf{x}} \psi(\mathbf{x}) + \psi(\mathbf{x}) \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0)] dV \quad (4.84b)$$

$$= \oint_{\partial\mathcal{R}} [-G(\mathbf{x}|\mathbf{x}_0) \nabla_{\mathbf{x}} \psi(\mathbf{x}) + \psi(\mathbf{x}) \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0)] \cdot \hat{\mathbf{n}}_{\mathbf{x}} d\mathcal{S}. \quad (4.84c)$$

Bringing the two sides to equation (4.82) together leads to

$$\psi(\mathbf{x}_0) = \int_{\mathcal{R}} \Lambda(\mathbf{x}) G(\mathbf{x}|\mathbf{x}_0) dV + \oint_{\partial\mathcal{R}} [G(\mathbf{x}|\mathbf{x}_0) \nabla_{\mathbf{x}} \psi(\mathbf{x}) - \psi(\mathbf{x}) \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0)] \cdot \hat{\mathbf{n}}_{\mathbf{x}} d\mathcal{S}. \quad (4.85)$$

As a final step, it is convenient to relabel  $\mathbf{x}_0 \leftrightarrow \mathbf{x}$  and make use of reciprocity,  $G(\mathbf{x}|\mathbf{x}_0) = G(\mathbf{x}_0|\mathbf{x})$ , so that

$$\psi(\mathbf{x}) = \underbrace{\int_{\mathcal{R}} \Lambda(\mathbf{x}_0) G(\mathbf{x}|\mathbf{x}_0) dV_0}_{\text{volume integral over } \mathcal{R}} + \underbrace{\oint_{\partial\mathcal{R}} [G(\mathbf{x}|\mathbf{x}_0) \nabla_{\mathbf{x}_0} \psi(\mathbf{x}_0) - \psi(\mathbf{x}_0) \nabla_{\mathbf{x}_0} G(\mathbf{x}|\mathbf{x}_0)] \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} d\mathcal{S}_0}_{\text{boundary area integral over } \partial\mathcal{R}}. \quad (4.86)$$

We have thus established  $\psi$  as a volume integral of the Green's function with the source,  $\Lambda$ , plus a boundary integral of the Green's function with the boundary data. This expression holds for either the Dirichlet condition or Neumann condition, whereby the distinction occurs only for the boundary integral. Furthermore, note that the Green's function is independent of the source,  $\Lambda$ , and the boundary data, so that  $G(\mathbf{x}|\mathbf{x}_0)$  can be used to express  $\psi$  for arbitrary source functions and boundary data.

#### 4.5.6 Properties of the solution

Specializing the general solution (4.86) to Dirichlet boundary conditions results in

$$\psi(\mathbf{x}) = \int_{\mathcal{R}} \Lambda(\mathbf{x}_0) G(\mathbf{x}|\mathbf{x}_0) dV_0 - \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0) \nabla_{\mathbf{x}_0} G(\mathbf{x}|\mathbf{x}_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} d\mathcal{S}_0. \quad (4.87)$$

Notice how the boundary integral involves the normal gradient of the Green's function, which is consistent with the one-dimensional case (4.49) derived in Section 4.4.1. We refer to the inward normal gradient of the Green's function as the *boundary Green's function*

$$G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) = -\nabla_{\mathbf{x}_0} G(\mathbf{x}|\mathbf{x}_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} = -\frac{\partial G(\mathbf{x}|\mathbf{x}_0)}{\partial \hat{\mathbf{n}}_{\mathbf{x}_0}}, \quad (4.88)$$

in which case the Dirichlet solution takes the form

$$\psi(\mathbf{x}) = \int_{\mathcal{R}} \Lambda(\mathbf{x}_0) G(\mathbf{x}|\mathbf{x}_0) dV_0 + \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0) G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) d\mathcal{S}_0. \quad (4.89)$$

This form for the solution emphasizes the role of the Green's function as the mediator between the distributed source,  $\Lambda$ , and all surrounding points  $\mathbf{x} \in \mathcal{R}$ , whereas the boundary Green's function mediates between information prescribed along the boundary,  $\mathbf{x} \in \partial\mathcal{R}$ , and interior points. In this subsection we summarize certain properties of the solution (4.87) and (4.89), and infer (through insisting on self-consistency) corresponding properties of the Green's function and boundary Green's function.

##### Linear superposition

The Dirichlet solution (4.87) manifests the linear superposition principle by writing  $\psi = \psi_A + \psi_B$  as given by Table 4.1. By construction,  $\psi_A$  satisfies Poisson's equation with homogeneous Dirichlet boundary conditions, whereas  $\psi_B$  satisfies Laplace's equation with inhomogeneous Dirichlet boundary conditions.

##### Verifying the partial differential equation for $\mathbf{x} \in \mathcal{R}$

We derived the Dirichlet solution (4.87) with manipulations that are reversible; i.e., equal signs were used at every step. Hence, we know that the expression (4.87) indeed satisfies the Dirichlet boundary value problem (4.65). Even so, the exercise of verifying the solution reveals valuable insights into the Green's function.

PDE: $\mathbf{x} \in \mathcal{R}$	BC: $\mathbf{x} \in \partial\mathcal{R}$	SOLUTION $\psi = \psi_A + \psi_B$
$-\nabla^2 \psi_A = \Lambda$	$\psi_A = 0$	$\psi_A(\mathbf{x}) = \int_{\mathcal{R}} G(\mathbf{x} \mathbf{x}_0) \Lambda(\mathbf{x}_0) dV_0$
$-\nabla^2 \psi_B = 0$	$\psi_B = \sigma$	$\psi_B(\mathbf{x}) = \oint_{\partial\mathcal{R}} G^{\text{bd}}(\mathbf{x} \mathbf{x}_0) \sigma(\mathbf{x}_0) dS_0$

TABLE 4.1: Decomposing the Dirichlet solution (4.87) into  $\psi = \psi_A + \psi_B$ , with  $\psi_A$  and  $\psi_B$  satisfying the properties shown in this table. For the boundary contribution we made use of the boundary Green's function,  $G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) = -\nabla_{\mathbf{x}_0} G(\mathbf{x}|\mathbf{x}_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0}$ , as given by equation (4.88).

To verify that the partial differential equation is satisfied for points within the interior of the region,  $\mathbf{x} \in \mathcal{R}$ , operate with  $-\nabla_{\mathbf{x}}^2$  on equation (4.89) to find

$$-\nabla_{\mathbf{x}}^2 \psi(\mathbf{x}) = \int_{\mathcal{R}} \Lambda(\mathbf{x}_0) [-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0)] dV_0 + \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0) [-\nabla_{\mathbf{x}}^2 G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0)] dS_0. \quad (4.90)$$

For the first term on the right hand side, make use of the Green's function identity  $-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0) = \delta(\mathbf{x} - \mathbf{x}_0)$  and then use the sifting property of the Dirac delta,  $\int_{\mathcal{R}} \Lambda(\mathbf{x}_0) \delta(\mathbf{x} - \mathbf{x}_0) dV_0 = \Lambda(\mathbf{x})$ . To show that the boundary contribution vanishes, make use of the following

$$\nabla_{\mathbf{x}}^2 G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) = \nabla_{\mathbf{x}}^2 [-\nabla_{\mathbf{x}_0} G(\mathbf{x}|\mathbf{x}_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0}] \quad (4.91a)$$

$$= \hat{\mathbf{n}}_{\mathbf{x}_0} \cdot \nabla_{\mathbf{x}_0} [-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0)] \quad (4.91b)$$

$$= \hat{\mathbf{n}}_{\mathbf{x}_0} \cdot \nabla_{\mathbf{x}_0} \delta(\mathbf{x} - \mathbf{x}_0), \quad (4.91c)$$

and, without loss of generality, let the normal direction be parallel to the vertical,  $\hat{\mathbf{n}}_{\mathbf{x}_0} = \hat{\mathbf{z}}$ , so that

$$\hat{\mathbf{n}}_{\mathbf{x}_0} \cdot \nabla_{\mathbf{x}_0} \delta(\mathbf{x} - \mathbf{x}_0) = \partial_{z_0} [\delta(x - x_0) \delta(y - y_0) \delta(z - z_0)] = \delta(x - x_0) \delta(y - y_0) \frac{d[\delta(z - z_0)]}{dz_0}. \quad (4.92)$$

With  $\mathbf{x}_0 \in \partial\mathcal{R}$  yet  $\mathbf{x} \notin \partial\mathcal{R}$ , the Dirac delta never fires, thus eliminating the boundary contribution. We have thus verified that  $-\nabla_{\mathbf{x}}^2 \psi = \Lambda$  for points  $\mathbf{x} \in \mathcal{R}$ .

### Verifying the Dirichlet boundary condition for $\mathbf{x} \in \partial\mathcal{R}$

To verify that the boundary conditions are satisfied by the Dirichlet solution (4.87), bring the field point,  $\mathbf{x}$ , onto the boundary

$$\mathbf{x} \rightarrow \mathbf{x}_{\partial\mathcal{R}} \in \partial\mathcal{R}. \quad (4.93)$$

For such boundary points, the volume integral in the solution (4.87) vanishes since the Dirichlet Green's function vanishes on the boundary,  $G(\mathbf{x}_{\partial\mathcal{R}}|\mathbf{x}_0) = 0$ . Self-consistency with the Dirichlet boundary data,  $\psi(\mathbf{x}_{\partial\mathcal{R}}) = \sigma(\mathbf{x}_{\partial\mathcal{R}})$ , leads to

$$\sigma(\mathbf{x}) = \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0) G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) dS_0 = - \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0) \nabla_{\mathbf{x}_0} G(\mathbf{x}_{\partial\mathcal{R}}|\mathbf{x}_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} dS_0 \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.94)$$

This integral equation is consistent so long as the boundary Green's function satisfies the boundary condition

$$G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) = -\nabla_{\mathbf{x}_0} G(\mathbf{x}|\mathbf{x}_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} = \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}, \quad (4.95)$$

where  $\delta^{(2)}(\mathbf{x} - \mathbf{x}_0)$  is the surface Dirac delta with physical dimensions of inverse area. This property of the boundary Green's function is consistent with the jump condition (4.98) found for

the one-dimensional Poisson equation. It furthermore leads to the corresponding integral identity

$$\oint_{\partial\mathcal{R}} G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) d\mathcal{S}_0 = \oint_{\partial\mathcal{R}} \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) d\mathcal{S}_0 = 1 \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}. \quad (4.96)$$

We emphasize<sup>9</sup> that the expressions (4.95) and (4.96) are found by first placing the source point,  $\mathbf{x}_0$ , on the boundary and thereafter moving the field point to the boundary,  $\mathbf{x} \rightarrow \mathbf{x}_{\partial\mathcal{R}} \in \partial\mathcal{R}$ .

### 4.5.7 Boundary Green's function

#### *Boundary value problem for the boundary Green's function*

As part of the development in Section 4.5.6, we revealed that the boundary Green's function satisfies the following boundary value problem

$$-\nabla_{\mathbf{x}}^2 G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) = 0 \quad \text{for } \mathbf{x} \in \mathcal{R} \quad \text{and} \quad G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) = \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}. \quad (4.97)$$

As seen by equation (4.71), the Dirichlet Green's function,  $G(\mathbf{x}|\mathbf{x}_0)$ , feels the Dirac source in the interior of the domain,  $\mathbf{x} \in \mathcal{R}$ , and satisfies homogeneous Dirichlet boundary conditions for  $\mathbf{x} \in \partial\mathcal{R}$ . As a complement, the boundary Green's function,  $G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0)$ , is harmonic everywhere in the domain interior and yet equals to the Dirac source along the boundary. By construction, the boundary Green's function incorporates boundary information into the region as part of the Dirichlet solution (4.89). We make further use of the boundary Green's function when studying the diffusion equation in Section 4.7 and the advection-diffusion equation in Section 46.10, at which point the boundary Green's function is referred to as the *boundary propagator*.

#### *Normalization of the boundary Green's function*

Consider the special case of constant boundary data,  $\sigma = \sigma_{\text{const}}$ , in which case the harmonic function in Table 4.1 is itself a constant,  $\psi_B(\mathbf{x}) = \sigma_{\text{const}}$ . Consequently, the boundary Green's function satisfies

$$-\oint_{\partial\mathcal{R}} \nabla_{\mathbf{x}_0} G(\mathbf{x}|\mathbf{x}_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} d\mathcal{S}_0 = \oint_{\partial\mathcal{R}} G^{\text{bd}}(\mathbf{x}|\mathbf{x}_0) d\mathcal{S}_0 = 1. \quad (4.98)$$

This relation is built by placing Dirac delta sources along the boundary,  $\mathbf{x}_0 \in \partial\mathcal{R}$ , and then area integrating over the boundary area. It holds for any field point,  $\mathbf{x} \in \mathcal{R}$ . Although derived by considering the special case of constant boundary data, equation (4.98) holds in general since the Green's function is independent of the boundary data.

To help understand the identity (4.98), consider the Green's function to be the steady state temperature or tracer concentration resulting from a Dirac delta source placed within the domain interior. The area integrated condition (4.98) acts to maintain the homogeneous Dirichlet boundary condition,  $G(\mathbf{x}_{\partial\mathcal{R}}|\mathbf{x}_0) = 0$ , for every point  $\mathbf{x}_{\partial\mathcal{R}} \in \partial\mathcal{R}$ . It does so by providing a boundary flux, via the normal gradient, whose area integral precisely cancels the unit positive source from the Dirac delta. We encountered this property for the one-dimensional equation studied in Section 4.4.3.

Equation (4.98) represents a normalization of the boundary Green's function at each point within the region interior, and it is consistent with the boundary condition given in equation (4.97). If we place Dirac delta sources along the boundary and integrate over the boundary, then every point within the domain feels a net unit source from these boundary sources, which is

<sup>9</sup>As per page 801 of *Morse and Feshbach* (1953).

reflected by the normalization of the boundary Green's function. We return to this normalization when considering the boundary propagator for the diffusion equation in Section 4.7.8.

## 4.6 Poisson's equation with Neumann boundaries

We now switch from the Dirichlet boundary conditions in Section 4.5 to the Poisson equation with *Neumann boundary conditions*

$$-\nabla^2\psi = \Lambda, \quad \text{for } \mathbf{x} \in \mathcal{R} \quad \text{and} \quad \hat{\mathbf{n}} \cdot \nabla\psi = \Sigma, \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.99)$$

Rather than specifying the value of  $\psi$  along the boundary, the Neumann condition specifies the normal derivative. Although much is shared between the Dirichlet and Neumann problems, there are distinctions that arise in the present section.

### 4.6.1 Constraints on the source and boundary data

As in our discussion of Dirichlet boundary conditions in Section 4.5.1, we can realize a solution to the boundary value problem (4.99) only so long as the constraint (4.67) is satisfied. For Neumann boundary conditions, we specify the normal derivative along the boundary so that the constraint (4.67) is now imposed on the volume source and boundary data<sup>10</sup>

$$\oint_{\partial\mathcal{R}} \Sigma dS = - \int_{\mathcal{R}} \Lambda dV. \quad (4.100)$$

If the source and boundary data do not satisfy this constraint, then this is no solution to the Poisson problem (4.99). If the Poisson problem arises physically from steady state tracer diffusion, then the constraint (4.100) imposes a balance between the diffusive flux integrated around the boundary (left hand side) with the volume integrated tracer source (right hand side). In the absence of this balance, there is no solution to the Poisson problem thus indicating the presence of transients (i.e., time dependent diffusion). If the Poisson problem arises from Newtonian gravity, then the condition (4.100) means that the area integrated gravitational acceleration specified on the boundary must be consistent with the volume integrated mass source distributed within the domain.

### 4.6.2 Uniqueness of the solution up to a constant

As in Section 4.5.2, we consider the uniqueness of the solution to the boundary value problem (4.99). We do so, again, by considering two functions,  $\psi_A$  and  $\psi_B$ , each satisfying the boundary value problem (4.99) and noting that their difference,  $\Psi = \psi_A - \psi_B$ , satisfies the homogeneous problem

$$-\nabla^2\Psi = 0, \quad \text{for } \mathbf{x} \in \mathcal{R} \quad \text{and} \quad \hat{\mathbf{n}} \cdot \nabla\Psi = 0, \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.101)$$

The same arguments we used in Section 4.5.2 lead us to conclude that  $\nabla\Psi = 0$ , but for the Neumann problem this result is consistent with  $\Psi$  being an arbitrary spatial constant. We can understand this arbitrariness since the Neumann boundary condition involves a derivative, with the derivative of a constant vanishing. We thus conclude that the solution to the boundary value problem (4.99) is unique up to an arbitrary constant.

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<sup>10</sup>To be self-contained, we here repeat the discussion of the constraint (4.100) that is also provided in Section 3.5.6.

### 4.6.3 The Green's function problem

The Green's function corresponding to the Poisson boundary value problem (4.99) is the solution to the Poisson equation with a Dirac delta source and a homogeneous Neumann boundary condition

$$-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0) = \delta(\mathbf{x} - \mathbf{x}_0) \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \mathcal{R} \quad \text{and} \quad \hat{\mathbf{n}} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0) = 0, \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.102)$$

Linearity enables us to write the Green's function as the sum of the free space Green's function plus a harmonic function

$$G(\mathbf{x}|\mathbf{x}_0) = \mathcal{G}(\mathbf{x}|\mathbf{x}_0) + H(\mathbf{x}|\mathbf{x}_0), \quad (4.103)$$

where

$$-\nabla_{\mathbf{x}}^2 \mathcal{G}(\mathbf{x}|\mathbf{x}_0) = \delta(\mathbf{x} - \mathbf{x}_0) \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \mathbb{R}^3 \quad (4.104a)$$

$$-\nabla_{\mathbf{x}}^2 H(\mathbf{x}|\mathbf{x}_0) = 0 \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \mathcal{R} \quad (4.104b)$$

$$-\hat{\mathbf{n}} \cdot \nabla_{\mathbf{x}} H(\mathbf{x}|\mathbf{x}_0) = \hat{\mathbf{n}} \cdot \nabla_{\mathbf{x}} \mathcal{G}(\mathbf{x}|\mathbf{x}_0) \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.104c)$$

### 4.6.4 Properties of the solution

Specializing the general solution (4.86) to Neumann boundary conditions results in

$$\psi(\mathbf{x}) = \int_{\mathcal{R}} \Lambda(\mathbf{x}_0) G(\mathbf{x}|\mathbf{x}_0) dV_0 + \oint_{\partial\mathcal{R}} \Sigma(\mathbf{x}_0) G(\mathbf{x}|\mathbf{x}_0) dS_0. \quad (4.105)$$

In this section we summarize certain properties of the solution (4.105) along with properties of the Green's function that are inferred (through insisting on self-consistency) from the solution.

#### *Linear superposition*

This Green's function solution (4.105) manifests the linear superposition principle by writing  $\psi = \psi_A + \psi_B$  as given by Table 4.2. By construction,  $\psi_A$  satisfies Poisson's equation with homogeneous Neumann boundary conditions, whereas  $\psi_B$  satisfies Laplace's equation with inhomogeneous Neumann boundary conditions.

PDE: $\mathbf{x} \in \mathcal{R}$	BC: $\mathbf{x} \in \partial\mathcal{R}$	SOLUTION $\psi = \psi_A + \psi_B$
$-\nabla^2 \psi_A = \Lambda$	$\psi_A = 0$	$\psi_A(\mathbf{x}) = \int_{\mathcal{R}} G(\mathbf{x} \mathbf{x}_0) \Lambda(\mathbf{x}_0) dV_0$
$-\nabla^2 \psi_B = 0$	$\hat{\mathbf{n}} \cdot \nabla \psi_B = \Sigma$	$\psi_B(\mathbf{x}) = \oint_{\partial\mathcal{R}} \Sigma(\mathbf{x}_0) G(\mathbf{x} \mathbf{x}_0) dS_0$

TABLE 4.2: Decomposing the Neumann solution (4.105) into  $\psi = \psi_A + \psi_B$ , with  $\psi_A$  and  $\psi_B$  satisfying the properties shown here. The function  $\psi_A$  is identical to  $\psi_A$  appearing for the Dirichlet problem (see Table 4.1), whereas the function  $\psi_B$  is distinct since it is determined by the respective boundary conditions.

#### *Transforming the boundary data to the interior*

The Neumann solution (4.105) allows for a dual formulation of the boundary data. To motivate this formulation, assume the only nontrivial Neumann boundary data appears along the constant geopotential surface  $z = z_b$ , with all other boundaries maintaining the homogeneous boundary

condition,  $\hat{\mathbf{n}} \cdot \nabla \psi = 0$ . In this special case the Neumann solution (4.105) takes the form

$$\psi(\mathbf{x}) = \int_{\mathcal{R}} \Lambda(\mathbf{x}_0) G(\mathbf{x}|\mathbf{x}_0) dV_0 + \int_{z=z_b} \Sigma(x_0, y_0) G(\mathbf{x}|\mathbf{x}_0) dx_0 dy_0 \quad (4.106a)$$

$$= \int_{\mathcal{R}} [\Lambda(\mathbf{x}_0) + \Sigma(x_0, y_0) \delta(z_0 - z_b)] G(\mathbf{x}|\mathbf{x}_0) dV_0 \quad (4.106b)$$

$$= \int_{\mathcal{R}} \Lambda^*(\mathbf{x}_0) G(\mathbf{x}|\mathbf{x}_0) dV_0. \quad (4.106c)$$

These manipulations have absorbed the non-homogeneous Neumann boundary condition into a modified source,  $\Lambda^*(\mathbf{x})$ . We are thus led to two equivalent formulations for the Poisson boundary value problem with Neumann conditions. The first is given by equation (4.99), whereby  $\psi$  is the solution to the Poisson equation with source  $\Lambda$  and with inhomogeneous Neumann boundary data,  $\Sigma$ . The second formulation considers  $\psi$  to be the solution to Poisson's equation with homogeneous Neumann boundary conditions yet with a modified source function

$$\Lambda^*(\mathbf{x}) = \Lambda(\mathbf{x}) + \Sigma(x, y) \delta(z - z_b) = \Lambda(\mathbf{x}) + \partial_z \psi(\mathbf{x}) \delta(z - z_b). \quad (4.107)$$

As a check, note that the physical dimensionality of  $\Lambda^*(\mathbf{x})$  is indeed correct since the Dirac delta,  $\delta(z - z_b)$ , has dimensions of inverse length. We interpret the term  $\Sigma(x, y) \delta(z - z_b)$  as a flux or *Dirac delta sheet* that sits just inside the boundary (at  $z = z_b - \epsilon$  with  $\epsilon \rightarrow 0$ ), which allows this data to be incorporated into the volume source data rather than be part of the boundary data. The specific form (4.107) can be generalized to the expression

$$\Lambda^*(\mathbf{x}) = \Lambda(\mathbf{x}) + \Sigma(\mathbf{x}) \delta[\hat{\mathbf{n}} \cdot (\mathbf{x} - \mathbf{x}_{\partial\mathcal{R}})] = \Lambda(\mathbf{x}) + \hat{\mathbf{n}} \cdot \nabla \psi(\mathbf{x}) \delta[\hat{\mathbf{n}} \cdot (\mathbf{x} - \mathbf{x}_{\partial\mathcal{R}})], \quad (4.108)$$

where the argument to the Dirac delta picks out the coordinates in the direction of the outward normal. The transformed Neumann problem thus takes the generic form

$$-\nabla^2 \psi = \Lambda^*, \quad \text{for } \mathbf{x} \in \mathcal{R} \quad \text{and} \quad \hat{\mathbf{n}} \cdot \nabla \psi = 0, \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.109)$$

Again, the solution to the boundary value problem (4.109) is identical to the solution of the original problem (4.99).

Notably, the same data,  $\Sigma$ , is needed for both equations (4.109) and (4.99), so there is nothing fundamentally special or efficient about one formulation or the other. Rather, it is a matter of convenience. For example, the formulation using  $\Lambda^*$  has found some favor in the study of quasi-geostrophic potential vorticity ([Bretherton, 1966](#)). We also make use of a similar construct in Section 50.4.3 for studies of boundary buoyancy fluxes in water mass transformation analysis.

### 4.6.5 Verifying the solution

We verify that the solution (4.105) solves the Poisson boundary value problem (4.99). First consider a point in the interior of the region,  $\mathbf{x} \in \mathcal{R}$ , and apply  $-\nabla_{\mathbf{x}}^2$  on equation to find (4.105)

$$-\nabla_{\mathbf{x}}^2 \psi(\mathbf{x}) = \int_{\mathcal{R}} \Lambda(\mathbf{x}_0) [-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0)] dV_0 + \oint_{\partial\mathcal{R}} \Sigma(\mathbf{x}_0) [-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0)] dS_0 = \Lambda(\mathbf{x}). \quad (4.110)$$

To reach this result we used  $-\nabla_{\mathbf{x}}^2 G(\mathbf{x}|\mathbf{x}_0) = \delta(\mathbf{x} - \mathbf{x}_0)$  and noted that the boundary integral vanishes for  $\mathbf{x} \notin \partial\mathcal{R}$ .

To verify the boundary condition, act with the gradient,  $\nabla_{\mathbf{x}}$ , on equation (4.105)

$$\nabla_{\mathbf{x}} \psi(\mathbf{x}) = \int_{\mathcal{R}} \Lambda(\mathbf{x}_0) [\nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0)] dV_0 + \oint_{\partial\mathcal{R}} \Sigma(\mathbf{x}_0) [\nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0)] dS_0. \quad (4.111)$$

Now move the field point onto the boundary,  $\mathbf{x} \rightarrow \mathbf{x}_{\partial\mathcal{R}} \in \partial\mathcal{R}$ , and project the gradient onto the normal direction,  $\hat{\mathbf{n}}_{\mathbf{x}}$ , at the point  $\mathbf{x}_{\partial\mathcal{R}}$ . This projection leads to  $\hat{\mathbf{n}}_{\mathbf{x}} \cdot \nabla_{\mathbf{x}} \psi(\mathbf{x}) = \Sigma(\mathbf{x})$  on the left hand side, and it annihilates the volume term on the right hand side since  $\hat{\mathbf{n}}_{\mathbf{x}} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0) = 0$  for  $\mathbf{x} \in \partial\mathcal{R}$ . We are thus left with

$$\hat{\mathbf{n}} \cdot \nabla_{\mathbf{x}} \psi(\mathbf{x}) = \Sigma(\mathbf{x}) = \oint_{\partial\mathcal{R}} \Sigma(\mathbf{x}_0) [\hat{\mathbf{n}}_{\mathbf{x}} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0)] dS_0 \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.112)$$

Again, both arguments of the Green's function are on the boundary,  $\mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}$ , with the Dirac source point,  $\mathbf{x}_0$ , integrated around the boundary whereas the field point,  $\mathbf{x}$ , is an arbitrary point on the boundary. Equation (4.94) is the analogous integral equation for the solution with Dirichlet boundary conditions. As for the Dirichlet case, we are ensured a solution to the integral equation (4.112) if the Green's function satisfies the property

$$\hat{\mathbf{n}}_{\mathbf{x}} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0) = \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) \quad \text{for } \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}, \quad (4.113)$$

which takes on the integral expression

$$\oint_{\partial\mathcal{R}} \hat{\mathbf{n}}_{\mathbf{x}} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}|\mathbf{x}_0) dS_0 = \oint_{\partial\mathcal{R}} \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) dS_0 \quad \text{for } \mathbf{x} \in \partial\mathcal{R}. \quad (4.114)$$

Table 4.3 compares the boundary properties of the respective Green's functions.

BOUNDARY CONDITION	GREEN'S FUNCTION PROPERTY	EQUATION
Dirichlet	$\partial G / \partial \hat{\mathbf{n}}_0 = \hat{\mathbf{n}}_{\mathbf{x}_0} \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x} \mathbf{x}_0) = -\delta^{(2)}(\mathbf{x} - \mathbf{x}_0)$	(4.95)
Neumann	$\partial G / \partial \hat{\mathbf{n}} = \hat{\mathbf{n}}_{\mathbf{x}} \cdot \nabla_{\mathbf{x}} G(\mathbf{x} \mathbf{x}_0) = \delta^{(2)}(\mathbf{x} - \mathbf{x}_0)$	(4.113)

TABLE 4.3: Comparing the boundary normal derivatives for the Poisson equation Green's function with Dirichlet and Neumann boundary conditions. Each point is on the boundary,  $\mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}$ , and the Dirac delta is two-dimensional so it has dimensions of inverse area. The properties satisfied by these Green's functions are realized by first placing the source point,  $\mathbf{x}_0$ , on the boundary and then moving the field point to the boundary,  $\mathbf{x} \rightarrow \mathbf{x}_{\partial\mathcal{R}} \in \partial\mathcal{R}$ . For the Dirichlet condition, the normal derivative is computed at the source point, whereas the Neumann condition computes the normal derivative at the field point.

## 4.7 The diffusion equation

We continue building our understanding of Green's function methods by now studying the *diffusion equation*, also known as the *heat equation*. We first encountered the diffusion equation in Section 3.6, where it served as the canonical parabolic partial differential equation. It is more thoroughly explored in Chapter 46, with much of the current chapter a foundation for the Green's function treatment of the advection-diffusion equation in Section 46.10. Time dependence appearing in the diffusion equation is the new feature relative to the elliptic Poisson equation encountered thus far in this chapter.

The traditional Green's function formalism for the diffusion equation, and the one pursued in this chapter, assumes that the spatial domain,  $\mathcal{R}$ , is static. Doing so ensures that space and time operations commute, such as differentiation and integration. Although time independent domains

are suitable for many applications, certain geophysical applications of interest in this book make use of time dependent boundaries, with the ocean free surface the key example. We examine time dependent boundaries when studying the advection-diffusion equation in Section 46.10, with that generality best confronted only after further exercising our Green's function brain muscle in the current chapter.

### 4.7.1 Causal free space Green's function

Consider a Dirac delta tracer source at  $(\mathbf{x}_0, t_0)$  and assume a continuous media where there is no advection, such as found in a stagnant fluid or elastic solid. The simplest solution to the diffusion equation is known as the *causal free space Green's function*, which is defined for  $t \in (-\infty, \infty)$  and satisfies

$$(\partial_t - \kappa \nabla_{\mathbf{x}}^2) G(\mathbf{x}, t | \mathbf{x}_0, t_0) = \delta(t - t_0) \delta(\mathbf{x} - \mathbf{x}_0) \quad \mathbf{x} \in \mathbb{R}^n \quad (4.115a)$$

$$G(\mathbf{x}, t | \mathbf{x}_0, t_0) \rightarrow 0 \quad |\mathbf{x} - \mathbf{x}_0| \rightarrow \infty \quad (4.115b)$$

$$G(\mathbf{x}, t | \mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \mathbb{R}^n, \quad t < t_0, \quad (4.115c)$$

where  $\mathbb{R}^n$  is Euclidean space with  $n = 1, 2, 3$  for a line, plane, and volume, respectively, and where  $\kappa > 0$  is a constant diffusivity (dimensions  $L^2 T^{-1}$ ). Equation (4.115b) ensures that the free space Green's function,  $G$ , decays as the field point gets further away from the source point. The *causality condition* (4.115c) means that the Green's function vanishes for times prior to the time,  $t_0$ , at which the Dirac source occurs. Given the dimensions of the Dirac source, we see that the Green's function has dimensions of  $L^{-n}$ .

The causal free-space Green's function is given by

$$G(\mathbf{x}, t | \mathbf{x}_0, t_0) = \frac{H(t - t_0)}{[4 \pi \kappa (t - t_0)]^{n/2}} e^{-|\mathbf{x} - \mathbf{x}_0|^2 / [4 \kappa (t - t_0)]}, \quad (4.116)$$

where the Heaviside step function (equation (4.16)) enforces causality. The amplitude of the Green's function exponentially decays when moving away from the source location, thus satisfying the condition (4.115b). Additionally, as time progresses beyond the source time, the Green's function decays according to the pre-factor  $(t - t_0)^{-n/2}$ . Each of these properties of the causal free space Green's function are reflected in solutions to more general diffusion processes.

### 4.7.2 Causal Green's function

Moving beyond the free space solution, we next introduce the *causal Green's function* for the diffusion equation. This Green's function is defined for  $t \in (-\infty, \infty)$  and satisfies the following equations when assuming Neumann boundary conditions

$$\frac{\partial[G(\mathbf{x}, t | \mathbf{x}_0, t_0)]}{\partial t} - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_0, t_0)] = \delta(t - t_0) \delta(\mathbf{x} - \mathbf{x}_0) \quad \mathbf{x} \in \mathcal{R} \quad (4.117a)$$

$$\hat{\mathbf{n}} \cdot \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \partial \mathcal{R} \quad (4.117b)$$

$$G(\mathbf{x}, t | \mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \mathcal{R}, \quad t < t_0. \quad (4.117c)$$

The Neumann boundary condition is relevant when one knows the boundary flux of heat or tracer concentration. Alternatively, Dirichlet conditions are used when knowing the boundary values for

the field, in which case the corresponding causal Green's function satisfies

$$\frac{\partial[G(\mathbf{x}, t|\mathbf{x}_0, t_0)]}{\partial t} - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t|\mathbf{x}_0, t_0)] = \delta(t - t_0) \delta(\mathbf{x} - \mathbf{x}_0) \quad \mathbf{x} \in \mathcal{R} \quad (4.118a)$$

$$G(\mathbf{x}, t|\mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \partial\mathcal{R} \quad (4.118b)$$

$$G(\mathbf{x}, t|\mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \mathcal{R}, \quad t < t_0. \quad (4.118c)$$

The Dirichlet condition is particularly relevant for passive tracers in the atmosphere and ocean, such as those studied in Section 46.10. In both the Neumann and Dirichlet cases, we generalized the free space solution from Section 4.7.1 by introducing a space-time dependent diffusivity tensor,  $\mathbb{K}(\mathbf{x}, t)$ , which is a symmetric second order tensor with dimensions  $L^2 T^{-1}$  (see Chapter 46 for discussion). The Green's function has dimensions of inverse volume,  $L^{-3}$ , which is implied since the Dirac delta source has dimensions of inverse volume times inverse time,  $L^{-3} T^{-1}$ .

In the presence of boundaries, the spatial position of the Dirac delta source impacts the value of the causal Green's function. In contrast, the causality condition (4.117c) means that the Green's function is dependent only on the time since the introduction of the source,  $t - t_0$ . Hence, there is no added generality afforded by setting the source time,  $t_0$ , to be distinct from  $t_0 = 0$ . Even so, we retain  $t_0$  to maintain symmetry with the spatial location  $\mathbf{x}_0$ . Doing so also helps to distinguish the Dirac source time,  $t_0$ , from the initial time,  $t_{\text{init}}$ , with the intitial time introduced in Section 4.7.6.

### 4.7.3 Adjoint causal Green's function

We make use of the *adjoint causal Green's function* for solving initial-boundary value problems for the diffusion equation. The adjoint causal Green's function is defined for  $t \in (-\infty, \infty)$  and satisfies the following boundary value problem for the Neumann conditions, with these equations representing the adjoint to the Green's function equations (4.117a)-(4.117c)

$$-\frac{\partial[\tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0)]}{\partial t} - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0)] = \delta(t - t_0) \delta(\mathbf{x} - \mathbf{x}_0) \quad \mathbf{x} \in \mathcal{R} \quad (4.119a)$$

$$\hat{\mathbf{n}} \cdot \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \partial\mathcal{R} \quad (4.119b)$$

$$\tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \mathcal{R}, \quad t > t_0. \quad (4.119c)$$

Similarly, the adjoint Green's function satisfying Dirichlet boundary conditions is determined by

$$-\frac{\partial[\tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0)]}{\partial t} - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0)] = \delta(t - t_0) \delta(\mathbf{x} - \mathbf{x}_0) \quad \mathbf{x} \in \mathcal{R} \quad (4.120a)$$

$$\tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \partial\mathcal{R} \quad (4.120b)$$

$$\tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \mathcal{R}, \quad t > t_0. \quad (4.120c)$$

Note the sign change on the time derivative in equations (4.119a) and (4.120a) relative to equations (4.117a) and (4.118a). This change results since the single partial time derivative is not a self-adjoint operator, reflecting the lack of time symmetry of the diffusion equation (i.e., the diffusion equation distinguishes between past and future). Also note the backward causal condition, equations (4.119c) and (4.120c). Pondering the physics of these equations, we propose that the adjoint Green's function provides a solution to the *concentration equation*, which is the diffusion equation run backwards in time.

#### 4.7.4 Reciprocity of the Green's function and its adjoint

When studying Poisson's equation we made use of reciprocity (4.75) satisfied by the Poisson equation Green's function, and we will require a corresponding reciprocity for the diffusion equation Green's function. Deriving reciprocity requires a bit more work for the diffusion equation due to the added time derivative term, which renders the adjoint diffusion operator distinct from the diffusion operator. That is, the diffusion operator is not *self-adjoint* due to sign change on the time derivative, whereas the Laplacian operator is self-adjoint (even with the symmetric diffusion tensor).

Before starting this derivation, note that we did not derive the adjoint in Section 4.7.3, instead we merely wrote it down. However, introduction of the adjoint Green's function is largely motivated by the following derivation of the reciprocity relation, where we see that the Green's function for the diffusion equation satisfies a reciprocity relation with the adjoint Green's function. Hence, as part of the following derivation we indirectly see how to construct the adjoint problem.

##### *Setting up the derivation*

To derive reciprocity, consider the partial differential equation (4.117a) with a Dirac delta source  $\delta(t-t_1)\delta(\mathbf{x}-\mathbf{x}_1)$ , and the adjoint partial differential equation (4.119a) with a distinct Dirac delta source  $\delta(t-t_2)\delta(\mathbf{x}-\mathbf{x}_2)$ . Multiply each of these equations by the complement Green's function and subtract

$$\begin{aligned} & \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2)(\partial_t G(\mathbf{x}, t|\mathbf{x}_1, t_1) - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t|\mathbf{x}_1, t_1)]) \\ & - G(\mathbf{x}, t|\mathbf{x}_1, t_1)(-\partial_t \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2) - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2)]) \\ & = \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2) \delta(t-t_1) \delta(\mathbf{x}-\mathbf{x}_1) - G(\mathbf{x}, t|\mathbf{x}_1, t_1) \delta(t-t_2) \delta(\mathbf{x}-\mathbf{x}_2). \end{aligned} \quad (4.121)$$

The Dirac delta source locations,  $\mathbf{x}_1$  and  $\mathbf{x}_2$ , are arbitrary, so long as they are within the domain  $\mathcal{R}$ . Likewise, the source times,  $t_1$  and  $t_2$ , are arbitrary. In the following, we find it useful to introduce an arbitrarily large time,  $T$ , so that

$$-T < t_1, t_2 < T, \quad (4.122)$$

with  $T$  later dropping out from the results through use of the causality conditions.

##### *Integration and use of the sifting property*

An integral of the right hand side of equation (4.121) over the domain  $\mathcal{R}$  and over time, both for the observational space-time points  $(\mathbf{x}, t)$ , leads to

$$\begin{aligned} & \int_{-T}^T \int_{\mathcal{R}} [\tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2) \delta(t-t_1) \delta(\mathbf{x}-\mathbf{x}_1) - G(\mathbf{x}, t|\mathbf{x}_1, t_1) \delta(t-t_2) \delta(\mathbf{x}-\mathbf{x}_2)] dV dt \\ & = \tilde{G}(\mathbf{x}_1, t_1|\mathbf{x}_2, t_2) - G(\mathbf{x}_2, t_2|\mathbf{x}_1, t_1). \end{aligned} \quad (4.123)$$

As shown in the following, the same integral of the left hand side of equation (4.121) vanishes, which then establishes the reciprocity property between the Green's function and the adjoint Green's function.

*Moving the time derivative from  $G$  to  $\tilde{G}$  and picking up a minus sign*

The left hand side of equation (4.121) requires us to massage just the first term since, as we will show, this term equals to the second so that the left hand side of equation (4.121) vanishes. To prove this assertion, start by examining the time derivative. Since the spatial domain,  $\mathcal{R}$ , is assumed to be static, we can swap the time and space derivatives to find

$$\begin{aligned} & \int_{-T}^T \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) \partial_t G(\mathbf{x}, t | \mathbf{x}_1, t_1) dt \\ &= \int_{-T}^T \left[ \partial_t \left( \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) G(\mathbf{x}, t | \mathbf{x}_1, t_1) \right) - \partial_t \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) G(\mathbf{x}, t | \mathbf{x}_1, t_1) \right] dt. \end{aligned} \quad (4.124)$$

We now set

$$G(\mathbf{x}, t = -T | \mathbf{x}_1, t_1) = 0 \quad \text{and} \quad \tilde{G}(\mathbf{x}, t = +T | \mathbf{x}_2, t_2) = 0, \quad (4.125)$$

which result from the causality conditions (4.117c) and (4.119c). Hence, in moving the time derivative from  $G$  to  $\tilde{G}$  we pick up a minus sign, which means that the time derivative is not self-adjoint

$$\int_{-T}^T \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) \partial_t G(\mathbf{x}, t | \mathbf{x}_1, t_1) dt = - \int_{-T}^T \partial_t \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) G(\mathbf{x}, t | \mathbf{x}_1, t_1) dt. \quad (4.126)$$

*The Laplacian is self-adjoint with a symmetric diffusion tensor*

Consider next the spatial derivative term on the left hand side of equation (4.121)

$$\begin{aligned} & - \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_1, t_1)] dV = \\ & \int_{\mathcal{R}} \left[ -\nabla_{\mathbf{x}} \cdot \left( \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_1, t_1) \right) + \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) \cdot \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_1, t_1) \right] dV. \end{aligned} \quad (4.127)$$

Use of the divergence theorem and either the homogeneous Neumann boundary condition (4.117b) or homogeneous Dirichlet condition (4.118b) allow us to drop the total derivative term. The same manipulation, with either the Neumann condition (4.119b) or Dirichlet condition (4.120b) satisfied by the adjoint Green's function  $\tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2)$ , allows us to seamlessly move the Laplacian operator from  $G(\mathbf{x}, t | \mathbf{x}_1, t_1)$  onto  $\tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2)$ , thus manifesting the self-adjoint nature of the Laplacian operator even in the presence of a symmetric diffusion tensor

$$\begin{aligned} & \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_1, t_1)] dV \\ &= \int_{\mathcal{R}} \nabla_{\mathbf{x}} \cdot \left[ \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) \right] G(\mathbf{x}, t | \mathbf{x}_1, t_1) dV. \end{aligned} \quad (4.128)$$

*Reciprocity of the Green's function and the adjoint Green's function*

The above manipulations show that the space-time integral for the left hand side of equation (4.121) vanishes. Consequently, we are left with the reciprocity relation satisfied by the Green's function and adjoint Green's function for the diffusion equation

$$\tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) = G(\mathbf{x}_0, t_0 | \mathbf{x}, t). \quad (4.129)$$

The right hand side results from placing a Dirac source at  $(\mathbf{x}, t)$  and using the forward diffusion equation to determine the effect at  $(\mathbf{x}_0, t_0)$  with  $t < t_0$ . The left hand side results from placing a Dirac source at  $(\mathbf{x}_0, t_0)$  and using the adjoint diffusion equation to determine the effect at  $(\mathbf{x}, t)$ , again with  $t < t_0$ . The reciprocity relation (4.129) proves the two approaches are identical. We emphasize that reciprocity is the concerted property of the differential operator, the boundary conditions, and causality conditions.

Reciprocity in the form of equation (4.129) means we have no need to bother solving the adjoint Green's function equation for  $\tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0)$  since the adjoint Green's function equals to the Green's function after swapping the space-time points for the field and source. Hence, it is sufficient to determine the Green's function  $G(\mathbf{x}, t|\mathbf{x}_0, t_0)$  and then use reciprocity to determine  $\tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0)$ . The simplicity of the reciprocity relation (4.129) is central to the practical use of the Green's function method for the diffusion equation.

### 4.7.5 Composition property of the Green's function

Following from the reciprocity relation derived in Section 4.7.4, we here derive the *composition property* satisfied by the Green's functions for the diffusion equation. This property connects the Green's function to Markov processes, where the composition property is known as the *Chapman-Kolmogorov relation* (Gardiner, 1985). The derivation closely follows that given in Section 4.7.4 for reciprocity, though it is a bit simpler. Larson (1999) and Holzer (2009) discuss the composition property in the context of the advection-diffusion equation, to which we return to in Section 46.10. Holzer (2009) also provides further connections to probability theory, thus promoting the interpretation of the Green's function as a transition probability.

#### *Setting up the derivation*

Consider again the Green's function partial differential equation (4.117a) with a Dirac delta source at  $(t_1, \mathbf{x}_1)$ ,

$$\partial_t G(\mathbf{x}, t|\mathbf{x}_1, t_1) - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t|\mathbf{x}_1, t_1)] = \delta(t - t_1) \delta(\mathbf{x} - \mathbf{x}_1), \quad (4.130)$$

and the adjoint Green's function partial differential equation (4.119a) with a distinct Dirac delta source at  $(t_2, \mathbf{x}_2)$

$$\partial_t \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2) + \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2)] = -\delta(t - t_2) \delta(\mathbf{x} - \mathbf{x}_2). \quad (4.131)$$

Multiply each of these equations by the complement Green's function and add the two equations.<sup>11</sup> Adding the time derivatives leads to

$$\begin{aligned} \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2) \partial_t G(\mathbf{x}, t|\mathbf{x}_1, t_1) + G(\mathbf{x}, t|\mathbf{x}_1, t_1) \partial_t \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2) \\ = \partial_t [\tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2) G(\mathbf{x}, t|\mathbf{x}_1, t_1)], \end{aligned} \quad (4.132)$$

and adding the space derivatives leads to

$$\begin{aligned} -\tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2) \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t|\mathbf{x}_1, t_1)] + G(\mathbf{x}, t|\mathbf{x}_1, t_1) \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2)] \\ = \nabla_{\mathbf{x}} \cdot [-\tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2) \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t|\mathbf{x}_1, t_1) + G(\mathbf{x}, t|\mathbf{x}_1, t_1) \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t|\mathbf{x}_2, t_2)]. \end{aligned} \quad (4.133)$$

<sup>11</sup>Recall that in Section 4.7.4 we subtracted the two equations to derive the reciprocity relation.

Integrating over the full spatial domain and using the homogeneous Neumann or Dirichlet boundary conditions removes the space derivative terms, thus leaving

$$\begin{aligned} \int_{\mathcal{R}} \partial_t [\tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) G(\mathbf{x}, t | \mathbf{x}_1, t_1)] dV \\ = \tilde{G}(\mathbf{x}_1, t | \mathbf{x}_2, t_2) \delta(t - t_1) - G(\mathbf{x}_2, t | \mathbf{x}_1, t_1) \delta(t - t_2). \end{aligned} \quad (4.134)$$

*Time integration and use of causality*

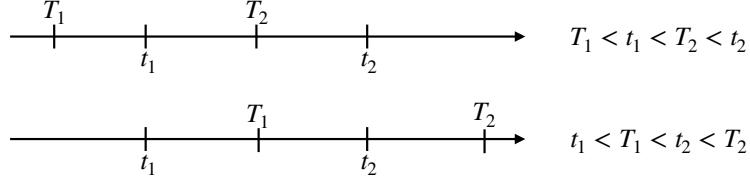


FIGURE 4.4: Two possible placements of the time steps used to derive the Green's function composition property.

Now integrate equation (4.134) over time, assuming the spatial domain is time independent as done for the reciprocity derivation, in which case

$$\begin{aligned} \int_{\mathcal{R}} [\tilde{G}(\mathbf{x}, T_2 | \mathbf{x}_2, t_2) G(\mathbf{x}, T_2 | \mathbf{x}_1, t_1) - \tilde{G}(\mathbf{x}, T_1 | \mathbf{x}_2, t_2) G(\mathbf{x}, T_1 | \mathbf{x}_1, t_1)] dV \\ = \int_{T_1}^{T_2} [\tilde{G}(\mathbf{x}_1, t | \mathbf{x}_2, t_2) \delta(t - t_1) - G(\mathbf{x}_2, t | \mathbf{x}_1, t_1) \delta(t - t_2)] dt, \end{aligned} \quad (4.135)$$

where  $T_1 < T_2$  are time endpoints for the time integration. The causality conditions (4.117c) and (4.119c) lead to the following identities, depending on the placements of  $T_1, T_2$  relative to  $t_1, t_2$  as shown in Figure 4.4

$$\tilde{G}(\mathbf{x}_1, t_1 | \mathbf{x}_2, t_2) = \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, T_2 | \mathbf{x}_2, t_2) G(\mathbf{x}, T_2 | \mathbf{x}_1, t_1) dV \quad \text{if } T_1 < t_1 < T_2 < t_2 \quad (4.136a)$$

$$G(\mathbf{x}_2, t_2 | \mathbf{x}_1, t_1) = \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, T_1 | \mathbf{x}_2, t_2) G(\mathbf{x}, T_1 | \mathbf{x}_1, t_1) dV \quad \text{if } t_1 < T_1 < t_2 < T_2. \quad (4.136b)$$

Use of the reciprocity relation (4.129) then leads to the composition relations

$$G(\mathbf{x}_2, t_2 | \mathbf{x}_1, t_1) = \int_{\mathcal{R}} G(\mathbf{x}_2, t_2 | \mathbf{x}, T_2) G(\mathbf{x}, T_2 | \mathbf{x}_1, t_1) dV \quad \text{if } T_1 < t_1 < T_2 < t_2 \quad (4.137a)$$

$$G(\mathbf{x}_2, t_2 | \mathbf{x}_1, t_1) = \int_{\mathcal{R}} G(\mathbf{x}_2, t_2 | \mathbf{x}, T_1) G(\mathbf{x}, T_1 | \mathbf{x}_1, t_1) dV \quad \text{if } t_1 < T_1 < t_2 < T_2. \quad (4.137b)$$

These equations are identical since both include an arbitrary intermediate time that is bounded by  $t_1 < t_2$ , thus allowing us to write the generic composition relation

$$G(\mathbf{x}_2, t_2 | \mathbf{x}_1, t_1) = \int_{\mathcal{R}} G(\mathbf{x}_2, t_2 | \mathbf{x}, \tau) G(\mathbf{x}, \tau | \mathbf{x}_1, t_1) dV \quad \text{if } t_1 < \tau < t_2 \quad (4.138)$$

*Interpreting the Green's function composition property*

The left hand side of the Green's function composition property (4.138) is the response from a Dirac source diffused from  $(\mathbf{x}_1, t_1)$  and measured at the field space-time point  $(\mathbf{x}_2, t_2)$ . The right

hand side says that this response is identical to the composition of a Green's function feeling the source at  $(\mathbf{x}_1, t_1)$  but now sampled at an intermediate space-time position,  $(\mathbf{x}, \tau)$ , and then further diffused to  $(\mathbf{x}_2, t_2)$ , with integration over all possible intermediate positions  $\mathbf{x}$ . Furthermore, note that the intermediate sampling can occur at an arbitrary intermediate time  $\tau$ , so long as  $t_1 < \tau < t_2$ . The composition property allows us to conceive of a long-time interval Green's function as the composition of an arbitrary number of shorter time interval Green's functions.

### 4.7.6 Integral solution

Having established reciprocity (4.129), we are now ready to derive an integral expression for the field,  $\psi(\mathbf{x}, t)$ , satisfying the diffusion equation initial-boundary value problem with either the Neumann boundary conditions

$$\frac{\partial \psi(\mathbf{x}, t)}{\partial t} - \nabla \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} \psi(\mathbf{x}, t)] = \Lambda(\mathbf{x}, t) \quad \mathbf{x} \in \mathcal{R} \quad (4.139a)$$

$$\hat{\mathbf{n}} \cdot \mathbb{K} \cdot \nabla_{\mathbf{x}} \psi(\mathbf{x}, t) = \Sigma(\mathbf{x}, t) \quad \mathbf{x} \in \partial \mathcal{R} \quad (4.139b)$$

$$\psi(\mathbf{x}, t = t_{\text{init}}) = I(\mathbf{x}) \quad \mathbf{x} \in \mathcal{R}, \quad (4.139c)$$

or Dirichlet boundary conditions

$$\frac{\partial \psi(\mathbf{x}, t)}{\partial t} - \nabla \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} \psi(\mathbf{x}, t)] = \Lambda(\mathbf{x}, t) \quad \mathbf{x} \in \mathcal{R} \quad (4.140a)$$

$$\psi(\mathbf{x}, t) = \sigma(\mathbf{x}, t) \quad \mathbf{x} \in \partial \mathcal{R} \quad (4.140b)$$

$$\psi(\mathbf{x}, t = t_{\text{init}}) = I(\mathbf{x}) \quad \mathbf{x} \in \mathcal{R}. \quad (4.140c)$$

In these equations we introduced the initial time,  $t = t_{\text{init}}$ , which is distinct from the Dirac delta source time,  $t = t_0$ . Correspondingly, the Dirac delta source is fired *after* the initial time,

$$t_{\text{init}} < t_0, \quad (4.141)$$

which follows since we are interested in the evolution of  $\psi$  after specification of the initial data,  $\psi(\mathbf{x}, t = t_{\text{init}}) = I(\mathbf{x})$ . Correspondingly,  $t_{\text{init}}$  defines the lower limit on time integrals in the following. Use of the  $\nabla_{\mathbf{x}}$  notation is not needed for these equations, since there is no source point,  $\mathbf{x}_0$ , in any of the expressions. However, this added detail helps us remain organized during the following manipulations. Finally, note that the diffusion tensor appearing in these equations means that the source function,  $\Lambda(\mathbf{x}, t)$ , in equations (4.139a) and (4.140a), as well as the boundary data,  $\Sigma(\mathbf{x}, t)$ , in equation (4.139b), have different dimensions from their counterparts found in the Poisson boundary value problems (4.65) and (4.99).

The following derivation emulates that for the Poisson equation in Section 4.5.5, yet with distinct features arising from time evolution and the corresponding need to use the adjoint causal Green's function,  $\tilde{G}$ . We expose many details as doing so reveals general notions and tricks arising with Green's function methods for initial-boundary value problems.

#### Setting up the derivation

To start the derivation, multiply the diffusion equation (4.139a) by the adjoint Green's function,  $\tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0)$ , and the adjoint Green's function equation (4.119a) by  $\psi(\mathbf{x}, t)$ . Subtracting and rearranging leads to

$$\partial_t (\tilde{G} \psi) + \nabla \cdot [\psi \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G} - \tilde{G} \mathbb{K} \cdot \nabla \psi] = \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \Lambda(\mathbf{x}, t) - \psi(\mathbf{x}, t) \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0), \quad (4.142)$$

where we temporarily suppressed arguments on the left hand side for brevity. Since the spatial domain is assumed to be static, we can integrate this equation over space and time without concern for the order of integration.

### Time integration

A time integral of the first left hand side term in equation (4.142) leads to

$$\int_{t_{\text{init}}}^T \partial_t [\tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \psi(\mathbf{x}, t)] dt = \tilde{G}(\mathbf{x}, T | \mathbf{x}_0, t_0) \psi(\mathbf{x}, T) - \tilde{G}(\mathbf{x}, t_{\text{init}} | \mathbf{x}_0, t_0) \psi(\mathbf{x}, t_{\text{init}}) \quad (4.143a)$$

$$= -\tilde{G}(\mathbf{x}, t_{\text{init}} | \mathbf{x}_0, t_0) I(\mathbf{x}), \quad (4.143b)$$

where we made use of the backward causal condition (4.119c) satisfied by the adjoint Green's function to set  $\tilde{G}(\mathbf{x}, t = T | \mathbf{x}_0, t_0) = 0$ , and used the initial condition (4.139c) to introduce the initial value data,  $\psi(\mathbf{x}, t_{\text{init}}) = I(\mathbf{x})$ .

### Space integration

A space integral over all observation points, and use of the divergence theorem, brings the divergence term on the left side of equation (4.142) into

$$\begin{aligned} & \int_{\mathcal{R}} \nabla \cdot [\psi \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G} - \tilde{G} \mathbb{K} \cdot \nabla_{\mathbf{x}} \psi] dV \\ &= \oint_{\partial \mathcal{R}} \left[ \psi(\mathbf{x}, t) \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) - \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \mathbb{K} \cdot \nabla_{\mathbf{x}} \psi \right] \cdot \hat{\mathbf{n}} d\mathcal{S}, \end{aligned} \quad (4.144)$$

where we kept both boundary terms pending specification of whether the fields satisfy Dirichlet or Neumann conditions. This boundary integral has the same appearance as found for the Poisson equation in Section 4.5.5, with the added feature here of the diffusion tensor.

### Integrating the right hand side of equation (4.142)

A space and time integral for the right hand side of equation (4.142), along with the sifting properties of the Dirac delta, render

$$\begin{aligned} & \int_{t_{\text{init}}}^T \left[ \int_{\mathcal{R}} [\tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \Lambda(\mathbf{x}, t) - \psi(\mathbf{x}, t) \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0)] dV \right] dt \\ &= -\psi(\mathbf{x}_0, t_0) + \int_{t_{\text{init}}}^T \left[ \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \Lambda(\mathbf{x}, t) dV \right] dt. \end{aligned} \quad (4.145)$$

Notice how this integration over the observation space-time points,  $(\mathbf{x}, t)$ , serves to pick out the field,  $\psi$ , evaluated at the space-time point,  $(\mathbf{x}_0, t_0)$ , where the Dirac delta source is located.

### Rearrangement and use of reciprocity

Bringing the above results together leads to the expression

$$\begin{aligned}\psi(\mathbf{x}_0, t_0) &= \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t_{\text{init}} | \mathbf{x}_0, t_0) I(\mathbf{x}) dV + \int_{t_{\text{init}}}^{t_0} \left[ \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \Lambda(\mathbf{x}, t) dV \right] dt \\ &+ \int_{t_{\text{init}}}^{t_0} \left[ \oint_{\partial\mathcal{R}} \left[ \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \mathbb{K} \cdot \nabla_{\mathbf{x}} \psi(\mathbf{x}, t) - \psi(\mathbf{x}, t) \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \right] \cdot \hat{\mathbf{n}} d\mathcal{S} \right] dt.\end{aligned}\quad (4.146)$$

The time integrals are restricted to the range  $t \in [t_{\text{init}}, t_0]$  through use of the causality condition (4.119c) for the adjoint Green's function. Hence, the arbitrary time,  $T$ , drops out from the solution and there is no dependence on fields at times later than  $t_0$  nor before  $t_{\text{init}}$ .

Use of reciprocity (4.129) allows us to replace the adjoint Green's function with the Green's function to thus bring equation (4.146) to

$$\begin{aligned}\psi(\mathbf{x}_0, t_0) &= \int_{\mathcal{R}} G(\mathbf{x}_0, t_0 | \mathbf{x}, t_{\text{init}}) I(\mathbf{x}) dV + \int_{t_{\text{init}}}^{t_0} \left[ \int_{\mathcal{R}} G(\mathbf{x}_0, t_0 | \mathbf{x}, t) \Lambda(\mathbf{x}, t) dV \right] dt \\ &+ \int_{t_{\text{init}}}^{t_0} \left[ \oint_{\partial\mathcal{R}} [G(\mathbf{x}_0, t_0 | \mathbf{x}, t) \mathbb{K} \cdot \nabla_{\mathbf{x}} \psi(\mathbf{x}, t) - \psi(\mathbf{x}, t) \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}_0, t_0 | \mathbf{x}, t)] \cdot \hat{\mathbf{n}} d\mathcal{S} \right] dt.\end{aligned}\quad (4.147)$$

Finally, it is convenient to relabel  $(\mathbf{x}_0, t_0) \leftrightarrow (\mathbf{x}, t)$  to write

$$\begin{aligned}\psi(\mathbf{x}, t) &= \underbrace{\int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) I(\mathbf{x}_0) dV_0}_{\text{space integral of } G \text{ with } I \text{ on } \mathcal{R}} + \underbrace{\int_{t_{\text{init}}}^t \left[ \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \Lambda(\mathbf{x}_0, t_0) dV_0 \right] dt_0}_{\text{space-time integral of } G \text{ with } \Lambda \text{ over } \mathcal{R}} \\ &+ \underbrace{\int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} [G(\mathbf{x}, t | \mathbf{x}_0, t_0) \mathbb{K} \cdot \nabla_{\mathbf{x}_0} \psi(\mathbf{x}_0, t_0) - \psi(\mathbf{x}_0, t_0) \mathbb{K} \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0)] \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} d\mathcal{S}_0 \right] dt_0}_{\text{space-time integral over } \partial\mathcal{R}}.\end{aligned}\quad (4.148)$$

Specializing to Neumann boundary conditions leads to

$$\begin{aligned}\psi^{\text{Neumann}}(\mathbf{x}, t) &= \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) I(\mathbf{x}_0) dV_0 + \int_{t_{\text{init}}}^t \left[ \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \Lambda(\mathbf{x}_0, t_0) dV_0 \right] dt_0 \\ &+ \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \Sigma(\mathbf{x}_0, t_0) d\mathcal{S}_0 \right] dt_0,\end{aligned}\quad (4.149)$$

whereas the solution with Dirichlet conditions is

$$\begin{aligned}\psi^{\text{Dirichlet}}(\mathbf{x}, t) &= \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) I(\mathbf{x}_0) dV_0 + \int_{t_{\text{init}}}^t \left[ \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \Lambda(\mathbf{x}_0, t_0) dV_0 \right] dt_0 \\ &- \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) \mathbb{K}(\mathbf{x}_0, t_0) \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} d\mathcal{S}_0 \right] dt_0.\end{aligned}\quad (4.150)$$

### 4.7.7 Properties of the solution

Many of the properties of the solution (4.148) are also reflected in the Poisson equation solutions from Sections 4.5.6 and 4.6.4. In particular, the solution manifests the linear superposition principle, with the solution given by the sum of three terms arising from the initial conditions,

distributed volume source, and spatial boundary conditions. We expect to have this connection given that the steady state diffusion equation satisfies a generalized Poisson equation (generalized by the presence of a diffusion tensor). A fundamentally new piece of physics and maths arises from time dependence. In this section we exhibit properties of the Green's function as inferred (through insisting on self-consistency) by the initial and boundary conditions.

### *Uniqueness of the solution*

Uniqueness of a solution to the diffusion boundary value problem follows as in the discussion of the Poisson equation in Sections 4.5.2 and 4.6.2. Namely, consider two solutions to the diffusion equation and take their difference,  $\Psi = \psi_A - \psi_B$ . We readily see that  $\Psi$  satisfies the homogeneous diffusion equation with homogeneous boundary conditions along with a zero initial condition.  $\Psi$  thus remains zero for both the Dirichlet and Neumann cases, thus proving that the solution to both problems is unique.

### *Initial conditions*

By sampling the solution (4.148) as time decreases towards the initial time,  $t \rightarrow t_{\text{init}}$ , and noting the initial condition  $\psi(\mathbf{x}, t_{\text{init}}) = I(\mathbf{x})$ , we are led to<sup>12</sup>

$$\lim_{t \rightarrow t_{\text{init}}} \psi(\mathbf{x}, t) = I(\mathbf{x}) = \lim_{t \rightarrow t_{\text{init}}} \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) I(\mathbf{x}_0) dV_0. \quad (4.151)$$

This temporal sampling of the field time is distinguished from the source time,  $t_0$ , which here is fixed at the initial time,  $t_0 = t_{\text{init}}$ . Self-consistency in equation (4.151) implies that the Green's function for both Neumann and Dirichlet boundary conditions satisfies the initial condition

$$\lim_{t \rightarrow t_{\text{init}}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) = \delta(\mathbf{x} - \mathbf{x}_0) \quad \text{with } \mathbf{x}, \mathbf{x}_0 \in \mathcal{R}. \quad (4.152)$$

That is, the Green's function is initialized by a Dirac delta pulse at the source point,  $\mathbf{x}_0$ , which then leads to

$$\lim_{t \rightarrow t_{\text{init}}} \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) I(\mathbf{x}_0) dV_0 = \int_{\mathcal{R}} \delta(\mathbf{x} - \mathbf{x}_0) I(\mathbf{x}_0) dV_0 = I(\mathbf{x}). \quad (4.153)$$

### *Neumann boundary conditions*

Acting with  $\mathbb{K}(\mathbf{x}, t) \cdot \nabla_{\mathbf{x}}$  on the Neumann solution (4.149); evaluating the expression on the boundary  $\mathbf{x} = \mathbf{x}_{\partial\mathcal{R}} \in \partial\mathcal{R}$ ; and then projecting onto the outward normal  $\hat{\mathbf{n}}_{\mathbf{x}}$ , serves to annihilate the volume integrals as per the homogeneous Neumann conditions satisfied by the Green's function. We are thus left with

$$\hat{\mathbf{n}}_{\mathbf{x}} \cdot \mathbb{K}(\mathbf{x}, t) \cdot \nabla_{\mathbf{x}} \psi(\mathbf{x}, t) = \Sigma(\mathbf{x}, t) = \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \hat{\mathbf{n}}_{\mathbf{x}} \cdot \mathbb{K}(\mathbf{x}, t) \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \Sigma(\mathbf{x}_0, t_0) d\mathcal{S}_0 \right] dt_0. \quad (4.154)$$

Self-consistency implies that the Green's function for the Neumann problem, when evaluated on the spatial boundary, satisfies

$$\hat{\mathbf{n}}_{\mathbf{x}} \cdot \mathbb{K}(\mathbf{x}, t) \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) = \delta(t - t_0) \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) \quad \text{with } \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}, \quad (4.155)$$

which is a generalization of the property (4.113) holding for the Poisson equation Green's function.

<sup>12</sup>Since  $t_{\text{init}}$  is the initial time, the limit  $t \rightarrow t_{\text{init}}$  is taken from above so that  $t = t_{\text{init}} + \epsilon$  with  $\epsilon \rightarrow 0$ .

### Transforming the Neumann boundary data to the interior

In Section 4.6.4, we saw how to transform the Neumann boundary condition into the interior by modifying the source function. The diffusion equation Neumann solution (4.149) allows for the same transformation by writing

$$\psi^{\text{Neumann}}(\mathbf{x}, t) = \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) I(\mathbf{x}_0) dV_0 + \int_{t_{\text{init}}}^t \left[ \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \Lambda^*(\mathbf{x}_0, t_0) dV_0 \right] dt_0, \quad (4.156)$$

where the modified source function follows from that used for the Poisson equation (4.108)

$$\Lambda^*(\mathbf{x}_0, t_0) = \Lambda(\mathbf{x}_0, t_0) + \Sigma(\mathbf{x}_0, t_0) \delta[\hat{\mathbf{n}} \cdot (\mathbf{x}_0 - \mathbf{x}_{\partial\mathcal{R}})]. \quad (4.157)$$

### Dirichlet boundary conditions

Evaluating the Dirichlet solution (4.150) on a spatial boundary,  $\mathbf{x} = \mathbf{x}_{\partial\mathcal{R}} \in \partial\mathcal{R}$ , eliminates both of the volume integrals so that we are left with

$$\psi^{\text{dirichlet}}(\mathbf{x}, t) = \sigma(\mathbf{x}, t) = - \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) \mathbb{K} \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} dS_0 \right] dt_0. \quad (4.158)$$

Self-consistency implies that the Green's function for the Dirichlet problem, when evaluated on the spatial boundary, satisfies

$$\hat{\mathbf{n}}_{\mathbf{x}_0} \cdot \mathbb{K}(\mathbf{x}_0, t_0) \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) = -\delta(t - t_0) \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) \quad \text{with } \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}, \quad (4.159)$$

which is a generalization of the property (4.95) holding for the Poisson equation Green's function.

## 4.7.8 Boundary propagator

In Sections 4.5.6 and 4.5.7 we studied the boundary Green's function for the Poisson equation. Here we extend those ideas to the *boundary propagator* for the diffusion equation, with the boundary propagator mediating the transfer of Dirichlet boundary information into the interior. Boundary propagators for diffusion and advection-diffusion (Section 46.10) have extensive use in geophysical fluids given that many tracers have no interior sources.

### Defining the boundary propagator

To focus on the role of the boundary propagator, consider a tracer in which the initial conditions and interior source both vanish:  $I(\mathbf{x}) = 0$  and  $\Lambda(\mathbf{x}, t) = 0$ . Assuming Dirichlet boundary conditions, the initial-boundary value problem (4.139a)-(4.139c) simplifies to

$$\frac{\partial \psi(\mathbf{x}, t)}{\partial t} - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} \psi(\mathbf{x}, t)] = 0 \quad \mathbf{x} \in \mathcal{R} \quad (4.160a)$$

$$\psi(\mathbf{x}, t) = \sigma(\mathbf{x}, t) \quad \mathbf{x} \in \partial\mathcal{R} \quad (4.160b)$$

$$\psi(\mathbf{x}, t = t_{\text{init}}) = 0 \quad \mathbf{x} \in \mathcal{R}, \quad (4.160c)$$

with the corresponding Dirichlet Green's function solution (4.150) taking the form

$$\psi(\mathbf{x}, t) = - \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) \mathbb{K}(\mathbf{x}_0, t_0) \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} dS_0 \right] dt_0. \quad (4.161)$$

We define the *boundary propagator* as the kernel in this equation

$$G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) \equiv -\mathbb{K}(\mathbf{x}_0, t_0) \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} \quad \text{with } \mathbf{x}_0 \in \partial\mathcal{R}, \quad (4.162)$$

with this definition giving  $G^{\text{bp}}$  the dimensions of  $\text{L}^{-2} \text{T}^{-1}$ . Use of the boundary propagator brings the solution (4.161) into the succinct form

$$\psi(\mathbf{x}, t) = \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) dS_0 \right] dt_0. \quad (4.163)$$

#### *Boundary value problem for the boundary propagator*

If we know the Green's function,  $G(\mathbf{x}, t | \mathbf{x}_0, t_0)$ , then we can compute the boundary propagator through the definition (4.162). Alternatively, we can directly determine the boundary propagator by solving its boundary value problem. Following from the definition (4.162) and the boundary condition (4.159), we know that

$$G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) = \delta(t - t_0) \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) \quad \text{with } \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}. \quad (4.164)$$

Hence, the boundary propagator, when evaluated along the boundary, is a Dirac delta source that fires at time  $t = t_0$  at the location  $\mathbf{x} = \mathbf{x}_0 \in \partial\mathcal{R}$ . To determine the partial differential equation satisfied by the boundary propagator, make use of the solution (4.163) and compute its time derivative

$$\frac{\partial \psi(\mathbf{x}, t)}{\partial t} = \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t) G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t) dS_0 + \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) \frac{\partial G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0)}{\partial t} dS_0 \right] dt_0. \quad (4.165)$$

The first term vanishes since the boundary propagator satisfies causality just like the Green's function when sampled at interior points

$$G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) = 0 \quad \text{if } t \leq t_0 \text{ and } \mathbf{x} \notin \partial\mathcal{R}. \quad (4.166)$$

We are thus left with

$$\begin{aligned} & \frac{\partial \psi(\mathbf{x}, t)}{\partial t} - \nabla_{\mathbf{x}} \cdot (\mathbb{K} \cdot \nabla_{\mathbf{x}} \psi) \\ &= \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) \left[ \frac{\partial G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0)}{\partial t} - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0)] \right] dS_0 \right] dt_0. \end{aligned} \quad (4.167)$$

Since the left hand side vanishes via the partial differential equation (4.160a), and since the boundary data,  $\sigma$ , is arbitrary, we are led to the causal boundary value problem for the boundary propagator

$$\frac{\partial G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0)}{\partial t} - \nabla_{\mathbf{x}} \cdot [\mathbb{K} \cdot \nabla_{\mathbf{x}} G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0)] = 0 \quad \mathbf{x} \in \mathcal{R} \quad (4.168a)$$

$$G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \notin \partial\mathcal{R}, t \leq t_0 \quad (4.168b)$$

$$G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) = \delta(t - t_0) \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) \quad \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}. \quad (4.168c)$$

In words, we see that upon firing the Dirac delta source on the boundary at time  $t = t_0$  and point  $\mathbf{x} = \mathbf{x}_0 \in \partial\mathcal{R}$ , the boundary propagator diffuses the Dirac source into the region interior. We thus

see that whereas the Dirichlet Green's function,  $G(\mathbf{x}, t | \mathbf{x}_0, t_0)$ , is zero along the boundary and yet feels the Dirac delta sources within the interior, the boundary propagator,  $G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0)$ , places the Dirac delta sources just on the boundary and feels no sources within the interior. Just as the causality condition means that the Green's function is a function of  $t - t_0$ , so too is the boundary propagator. Furthermore, a focus on the boundary propagator rather than the Green's function allows us to dispense with the need to compute the normal gradient of the Green's function at the boundary, with that calculation rather awkward in practice.

#### *Normalization of the boundary propagator*

Consider the special case of a uniform constant Dirichlet boundary data,  $\sigma = \sigma_{\text{constant}}$  in the solution (4.163). Diffusion will act on this constant boundary value to spread it throughout the region. After sufficient time the solution will reach a steady state whereby  $\psi = \sigma_{\text{constant}}$  at every point within the domain. This result means that the boundary Green's function satisfies the normalization condition

$$\lim_{t_{\text{init}} \rightarrow -\infty} \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) dS_0 \right] dt_0 = 1, \quad (4.169)$$

where the lower time limit is meant to indicate some arbitrary time sufficiently far in the past so that a steady state has been reached. Again, this normalization condition holds for every point within the domain and for any time. It corresponds to the normalization condition (4.98) satisfied by the boundary Green's function for the Poisson equation.

## 4.8 Initial value problems and response functions

In this section we focus on initial value problems and study the response functions that help to characterize a dynamical system. For this purpose, consider the first order ordinary differential equation

$$[d/dt + \lambda(t)] \psi(t) = F(t) \quad \text{with } \psi(t \leq t_{\text{init}}) = 0, \quad (4.170)$$

where  $\psi$  is some geophysical field, such as the anomalous sea surface temperature,  $\lambda$  is a feedback parameter that is positive for a damped system, and  $F$  is a forcing function such as that introduced by atmospheric variability on the surface ocean. We are only concerned with temporal behavior so that all spatial information is ignored. This equation has found widespread use in the climate dynamics community, largely following the work from [Hasselmann \(1976\)](#).

The material in this section could well have been used near the start of this chapter since it only involves ordinary differential equations. However, placing it at the end helps to tie together some of the material sprinkled throughout this chapter, and to connect to current applications of Green's function technology for studies of climate dynamics.

### 4.8.1 Impulse response function

Consider the system (4.170) with  $\lambda > 0$  a time-independent feedback parameter damping the system back to zero, and with the forcing given by a Dirac delta

$$[d/dt + \lambda] G(t|t_0) = \alpha \delta(t - t_0) \quad \text{with } G(t|t_0) = 0 \text{ for } t < t_0, \quad (4.171)$$

where  $\alpha > 0$  is a constant dimensionless scaling coefficient. We refer to the resulting causal Green's function,  $G(t|t_0)$ , as the *impulse response function* since it represents the response of the

dynamical system to an impulse provided by the Dirac delta.<sup>13</sup>

#### *Initial condition for the impulse response function*

To determine the initial condition for the Green's function, integrate equation (4.171) over an interval containing the source time,  $t_0$ , to render

$$\lim_{\epsilon \rightarrow 0} \left[ G(t_0 + \epsilon|t_0) - G(t_0 - \epsilon|t_0) + \int_{t_0 - \epsilon}^{t_0 + \epsilon} \lambda G(t|t_0) dt \right] = \alpha. \quad (4.172)$$

Causality means that  $G(t_0 - \epsilon|t_0) = 0$  so that

$$\lim_{\epsilon \rightarrow 0} G(t_0 + \epsilon|t_0) + \lim_{\epsilon \rightarrow 0} \int_{t_0}^{t_0 + \epsilon} \lambda G(t|t_0) dt = \alpha. \quad (4.173)$$

We assume that the integral vanishes in the limit of  $\epsilon \rightarrow 0$ , which is a sensible assumption since the only means to have a nonzero integral is if the Green's function had a singularity similar to a Dirac delta. We are thus led to the initial condition for the Green's function

$$G(t = t_0|t_0) = \alpha. \quad (4.174)$$

#### *Solution for the impulse response function*

The causality condition  $G(t < t_0|t_0) = 0$  can be satisfied by introducing the Heaviside step function from Section 4.2.5

$$G(t|t_0) = \mathcal{H}(t - t_0) g(t) \quad \text{with} \quad [d/dt + \lambda] g = 0 \quad \text{and} \quad g(t = t_0) = \alpha, \quad (4.175)$$

and the solution is readily determined to be the damped exponential

$$G(t|t_0) = \mathcal{H}(t - t_0) \alpha e^{-\lambda(t-t_0)}. \quad (4.176)$$

We verify this function satisfies the initial value problem (4.171) by noting that

$$dG(t|t_0)/dt = \alpha \delta(t - t_0) e^{-\lambda(t-t_0)} - \lambda G(t|t_0) = \alpha \delta(t - t_0) - \lambda G(t|t_0) \quad (4.177)$$

as per the discussion leading to equation (4.15). As illustrated in Figure 4.5, the impulse response function (4.176) has a particularly simple interpretation as the damped exponential response of the dynamical system to a Dirac impulse fired at  $t = t_0$ .

#### 4.8.2 Step response function

Rather than hit the system at a particular moment in time with a Dirac delta, we may choose to impose a force that turns on and remains on after some initial time, as per a Heaviside step function. The *step response function*,  $S(t|t_0)$ , measures the response of the dynamical system to this step forcing and it satisfies the differential equation

$$[d/dt + \lambda] S(t|t_0) = \alpha \mathcal{H}(t - t_0) \quad \text{with} \quad S(t|t_0) = 0 \text{ for } t < t_0. \quad (4.178)$$

---

<sup>13</sup>Recall our discussion of impulse in Section 4.2.7.

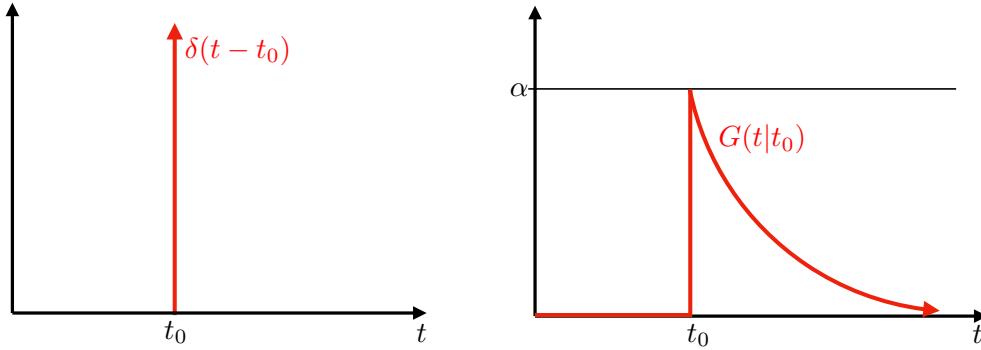


FIGURE 4.5: Left panel: Dirac delta that is fired at time  $t = t_0$ . Right panel: The impulse response function (4.176) resulting from the Dirac delta impulse as realized for the damped linear system (4.171).

Note that in the steady state at  $t \rightarrow \infty$ , the step response function asymptotes to the constant

$$\lim_{t \rightarrow \infty} S(t|t_0) = \alpha/\lambda. \quad (4.179)$$

#### *Connection to the impulse response function*

The time derivative  $d/dt_0$  acting on the step response function equation (4.178) leads to

$$[d/dt + \lambda] dS(t|t_0)/dt_0 = \alpha d\mathcal{H}(t - t_0)/dt_0. \quad (4.180)$$

The derivative of the Heaviside step function equals to the Dirac delta as per equation (4.19), in which

$$d\mathcal{H}(t - t_0)/dt_0 = -d\mathcal{H}(t - t_0)/dt = -\delta(t - t_0). \quad (4.181)$$

Use of this result in equation (4.180), and comparison to the impulse response function equation (4.171), yields the identity

$$\frac{dS(t|t_0)}{dt_0} = -G(t|t_0). \quad (4.182)$$

This identity holds even when the feedback parameter is a function of time,  $\lambda = \lambda(t)$ , since the time derivative operator,  $d/dt_0$ , has no effect on  $\lambda(t)$ .

#### *Initial condition for the step response function*

To determine the initial condition for the step response function, integrate equation (4.178) over an interval bounding  $t_0$  and take the limit as that interval vanishes

$$\lim_{\epsilon \rightarrow 0} \left[ S(t_0 + \epsilon|t_0) - S(t_0 - \epsilon|t_0) + \int_{t_0 - \epsilon}^{t_0 + \epsilon} \lambda S(t|t_0) dt \right] = \int_{t_0 - \epsilon}^{t_0 + \epsilon} \mathcal{H}(t - t_0) dt. \quad (4.183)$$

Causality means that  $S(t_0 - \epsilon|t_0) = 0$ . Furthermore, the integral of the Heaviside is given by

$$\lim_{\epsilon \rightarrow 0} \int_{t_0 - \epsilon}^{t_0 + \epsilon} \mathcal{H}(t - t_0) dt = \lim_{\epsilon \rightarrow 0} \int_{t_0}^{t_0 + \epsilon} \mathcal{H}(t - t_0) dt = \lim_{\epsilon \rightarrow 0} \epsilon = 0, \quad (4.184)$$

so that

$$\lim_{\epsilon \rightarrow 0} S(t_0 + \epsilon|t_0) = \epsilon \lambda \implies S(t = t_0|t_0) = 0. \quad (4.185)$$

That is, the step response function starts at zero and then grows in time in response to the Heaviside step function forcing.

### Solution for the step response function

It is straightforward to show that the causal step response function is given by the saturating exponential

$$S(t|t_0) = \frac{\alpha}{\lambda} \left[ 1 - e^{-\lambda(t-t_0)} \right] \mathcal{H}(t-t_0). \quad (4.186)$$

Figure 4.6 depicts this function along with the Heaviside step forcing. Furthermore, we verify the connection between  $S(t|t_0)$  and  $G(t|t_0)$  by computing

$$\frac{dS(t|t_0)}{dt_0} = -\alpha \mathcal{H}(t-t_0) e^{-\lambda(t-t_0)} - \frac{\alpha}{\lambda} \left[ 1 - e^{-\lambda(t-t_0)} \right] \delta(t-t_0) \quad (4.187a)$$

$$= -G(t|t_0) - \frac{\alpha}{\lambda} \left[ 1 - e^{-\lambda(t-t_0)} \right] \delta(t-t_0). \quad (4.187b)$$

The second term on the right hand side vanishes since

$$\int_{t_0-\epsilon}^{t_0+\epsilon} \left[ 1 - e^{-\lambda(t-t_0)} \right] \delta(t-t_0) dt = 0, \quad (4.188)$$

in which case we have the expected result  $dS(t|t_0)/dt_0 = -G(t|t_0)$ .

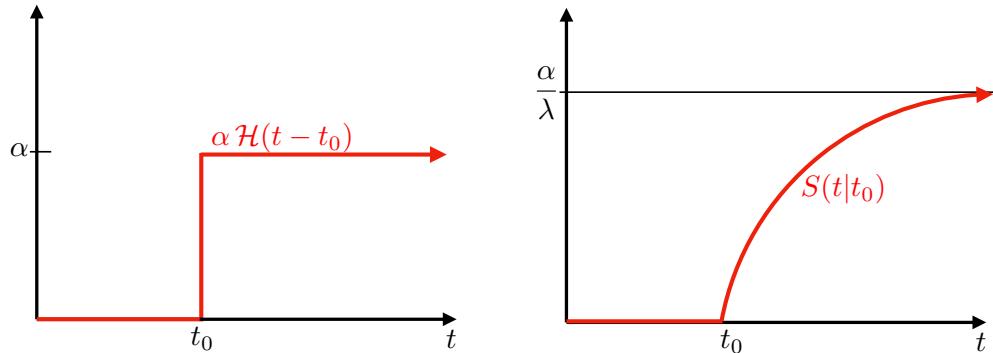


FIGURE 4.6: Left panel: Heaviside step function is fired at time  $t = t_0$  and stays on afterward. Right panel: The step response function (4.186) resulting from the Heaviside step forcing impulse as realized for the damped linear system (4.171).

### 4.8.3 Reciprocity relation

The initial value problem (4.170) is not a self-adjoint system. Hence, we need to develop a reciprocity condition for the impulse response function and its adjoint, following the procedure used for the diffusion equation in Section 4.7.4. Again, the impulse response function satisfies

$$[\frac{d}{dt} + \lambda] G(t|t_1) = \alpha \delta(t-t_1) \quad \text{with } G(t|t_1) = 0 \text{ for } t < t_1 \text{ and } G(t_1|t_1) = \alpha, \quad (4.189)$$

and the adjoint impulse response function satisfies

$$[-\frac{d}{dt} + \lambda] \tilde{G}(t|t_2) = \alpha \delta(t-t_2) \quad \text{with } \tilde{G}(t|t_2) = 0 \text{ for } t > t_2 \text{ and } \tilde{G}(t_2|t_2) = \alpha. \quad (4.190)$$

We here introduced two Dirac delta source times,  $t_1, t_2$ , which both occur after the initial time and before the end time

$$t_{\text{init}} < t_1, t_2 < T. \quad (4.191)$$

As we will see, causality eliminates the final time,  $T$ , from the solution for  $\psi$ . We retain it merely for bookeeping.

Determining the reciprocity relation between  $\tilde{G}$  and  $G$  follows by multiplying equation (4.189) by  $\tilde{G}(t|t_2)$  and multiplying equation (4.190) by  $G(t|t_1)$  and then subtracting

$$\frac{d}{dt} [G(t|t_1) \tilde{G}(t|t_2)] = \alpha [\tilde{G}(t|t_2) \delta(t - t_1) - G(t|t_1) \delta(t - t_2)]. \quad (4.192)$$

Now integrate this equation over the time range  $t_{\text{init}} \leq t \leq T$ . For the right hand side we assume  $\alpha$  to be a constant, which then leads to the difference  $\tilde{G}(t_1|t_2) - G(t_2|t_1)$ . For the left hand side, use of the causality conditions in equations (4.189) and (4.190) render

$$\int_{t_{\text{init}}}^T \frac{d}{dt} [G(t|t_1) \tilde{G}(t|t_2)] dt = 0, \quad (4.193)$$

thus yielding the reciprocity relation

$$\tilde{G}(t|t_0) = G(t_0|t). \quad (4.194)$$

The feedback parameter,  $\lambda$ , dropped out from the derivation, with the reciprocity relation holding even if  $\lambda$  is time dependent. However, we again needed to assume the coefficient  $\alpha$  to be constant.

#### 4.8.4 Response function for general forcing

We now return to the initial value problem (4.170) and determine the response,  $\psi$ , to a general forcing function,  $F(t)$ , that turns on at some initial time  $t = t_0 > t_{\text{init}}$ . As for our earlier discussions of Green's functions, we express the general response function as an integral over impulse responses. For this purpose, multiply equation (4.170) by  $\tilde{G}(t|t_0)$  and the adjoint equation (4.190) by  $\psi(t)$ , subtract, and then integrate to find

$$\alpha \psi(t_0) = \int_{t_{\text{init}}}^T \tilde{G}(t|t_0) F(t) dt - \int_{t_{\text{init}}}^T \frac{d}{dt} [\tilde{G}(t|t_0) \psi(t)] dt. \quad (4.195)$$

Making use of the causality condition  $\tilde{G}(t|t_0) = 0$  for since  $t > t_0$  leads to

$$\alpha \psi(t_0) = \tilde{G}(t_{\text{init}}|t_0) \psi(t_{\text{init}}) + \int_{t_{\text{init}}}^{t_0} \tilde{G}(t|t_0) F(t) dt, \quad (4.196)$$

where we retained the possibility of  $\psi(t_{\text{init}}) \neq 0$  for a bit of generality. The reciprocity condition (4.194) brings this equation to the form

$$\alpha \psi(t_0) = G(t_0|t_{\text{init}}) \psi(t_{\text{init}}) + \int_{t_{\text{init}}}^{t_0} G(t_0|t) F(t) dt, \quad (4.197)$$

and swapping symbols,  $t \leftrightarrow t_0$ , yields

$$\alpha \psi(t) = G(t|t_{\text{init}}) \psi(t_{\text{init}}) + \int_{t_{\text{init}}}^t G(t|t_0) F(t_0) dt_0. \quad (4.198)$$

As anticipated, the general response is written as an initial response plus the integral of the general forcing with the impulse response function. Causality ensures that  $\psi$  is dependent only on forcing that is active between the initial time,  $t_{\text{init}}$ , and current time,  $t$ . To garner further insights into the general expression (4.198), consider the special case of constant feedback parameter,  $\lambda$ , in which the impulse response function is (4.176) so that

$$\psi(t) = e^{-\lambda(t-t_{\text{init}})} \psi(t_{\text{init}}) + \int_{t_{\text{init}}}^t e^{-\lambda(t-t_0)} F(t_0) dt_0. \quad (4.199)$$

#### 4.8.5 Connection to the boundary propagator

Recall our discussion in Section 4.7.8 of the boundary propagator for the diffusion equation, which solves the causal boundary value problem (4.168a)-(4.168c). Again, the boundary propagator,  $G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0)$ , measures the response of the system at  $(\mathbf{x}, t)$  to a Dirac delta space-time source imposed along the surface boundary. The details of the diffusion process are encoded into the boundary propagator so that the propagator is able to build up the response,  $\psi$ , to a general boundary forcing function,  $\sigma$ , as per equation (4.163). The discussion in the current section thus prompts us to consider the boundary propagator as an impulse response function for spatially distributed sources whose influence is mediated by diffusion.

#### 4.8.6 Comments and further study

Many applications of Green's function methods in geophysical fluid mechanics and climate dynamics do not make use of analytical methods to solve for the Green's function. Instead, they make use of numerical estimates based on time stepping passive tracers in ocean and atmospheric models, with source functions approximating Dirac delta sources. Many applications have focused on boundary propagators, which as shown in this section are equivalent to impulse response functions for boundary sources. We return to this point when discussing the passive tracer equation in Section 46.10.

*Hasselmann et al. (1993)* introduced the impulse response function and step response function to the study of climate model drift. *Marshall et al. (2014)* and *Zanna et al. (2019)* presented further studies using this framework. Some of the mathematical formulation of impulse response and step response functions as presented here follow that offered in Exercise 1.52 of *Stakgold (2000a)*.



# Chapter 5

## Curves and surfaces

We encounter curves and surfaces throughout the study of geophysical fluid mechanics, with fluid particle pathlines through space-time and isopycnal/isentropic surfaces providing two examples. Indeed, curves and surfaces are encountered throughout physics. Hence, there is a well developed mathematical framework to describe the geometric properties of these objects. Our goal in this chapter is to introduce some of the basics of curves and surfaces embedded in Euclidean space.

Although the curves and surfaces of geophysical fluid mechanics are commonly moving as part of the fluid flow, we are concerned in this chapter with describing their instantaneous spatial properties. Hence, time does not appear in this chapter. Furthermore, although curves and surfaces can overturn and intersect themselves, we restrict attention to orientable curves and surfaces whose normal direction has a nonzero projection onto the vertical; i.e., they have no overhangs and no wrapping (Figure 5.1). This constraint is satisfied by the surfaces of constant generalized vertical coordinates (e.g., isopycnal surfaces) considered in Chapter 41 and in many other places in this book. It allows us to make use of coordinates known as the *Monge gauge* in condensed matter physics

### READER'S GUIDE TO THIS CHAPTER

This chapter requires an understanding of the Cartesian calculus of Chapter 2. The differential geometry presented here is of some use throughout this book, and yet the casual reader need not penetrate the material. Conversely, the interested reader can find far more development of the mathematics, along with physical applications, by studying the physics of fluctuating membranes. Section 10.4 of the condensed matter physics textbook from [Chaikin and Lubensky \(1995\)](#) provides a useful starting point.

5.1	Definitions and notation . . . . .	112
5.1.1	Definitions . . . . .	112
5.1.2	Notation . . . . .	112
5.2	Curves in 2D Euclidian space (planar curves) . . . . .	113
5.2.1	Differential increments along the curve . . . . .	114
5.2.2	Length along the curve . . . . .	114
5.2.3	Curvature of a curve . . . . .	115
5.3	Surfaces embedded in 3D Euclidean space . . . . .	117
5.3.1	Area on the surface . . . . .	117
5.3.2	Curvature of a surface . . . . .	118
5.3.3	Curves on the surface $z = \eta(x, y)$ . . . . .	119

## 5.1 Definitions and notation

The basic notions of curves and surfaces embedded in Euclidean space are rather intuitive. Nonetheless, it is important to be precise in our usage. For this purpose we here offer some notation and definitions.

### 5.1.1 Definitions

We assume the notion of a curve and surface embedded in Euclidean space to be self-evident, offering analytical expressions for curves in Section 5.2 and surfaces in Section 5.3. Given such, we here define some related notions used in our study of fluid mechanics.

- **ORIENTABLE:** An *orientable curve* is a curve that allows for normal and tangent directions to specify directions and sides to the curve. Likewise, an *orientable surface* has two sides, allowing one to define positive and negative sides. A Möbius strip is the canonical surface that is not orientable since it only has one side. Likewise, the boundary of a Möbius strip is a non-orientable curve. Although very interesting mathematically, we do not encounter non-orientable objects in this book.
- **PATH or CONTOUR:** A path or contour is a continuous piecewise smooth oriented curve. A *simple path* or *simple contour* does not cross itself. We already encountered contours when considering path integrals in Chapter 2.
- **CIRCUIT:** A circuit is a path that closes, and a *simple circuit* is a circuit that does not cross itself. Finally, a *reducible circuit* is a circuit that can be continuously deformed to a point within the domain without leaving the domain. For example, a circuit within the ocean that encloses an island or continent cannot be deformed to a point since doing so requires the circuit to cross onto land and thus to leave the ocean.

### 5.1.2 Notation

In this chapter we write the Cartesian position of a point on a surface as

$$\mathbf{S} = x \hat{\mathbf{x}} + y \hat{\mathbf{y}} + \eta(x, y) \hat{\mathbf{z}} \quad \text{position on surface,} \quad (5.1)$$

with the vertical position written as

$$z = \eta(x, y) \quad \text{vertical position on surface.} \quad (5.2)$$

If we are instead referring to a point on a planar curve in the  $x$ - $z$ -plane, then we drop the  $y$ -dependence to have

$$\mathbf{S} = x \hat{\mathbf{x}} + \eta(x) \hat{\mathbf{z}} \quad \text{position on planar curve.} \quad (5.3)$$

Time dependence is dropped throughout this chapter since we focus on the spatial geometry of curves and surfaces at a particular time instance.

We assume the outward normal direction on the curve or the surface has a nonzero projection into the vertical as shown in Figure 5.1. Indeed, we are only able to write the vertical position as  $z = \eta(x, y)$  so long as there are no overturns in the surface, in which case the outward normal

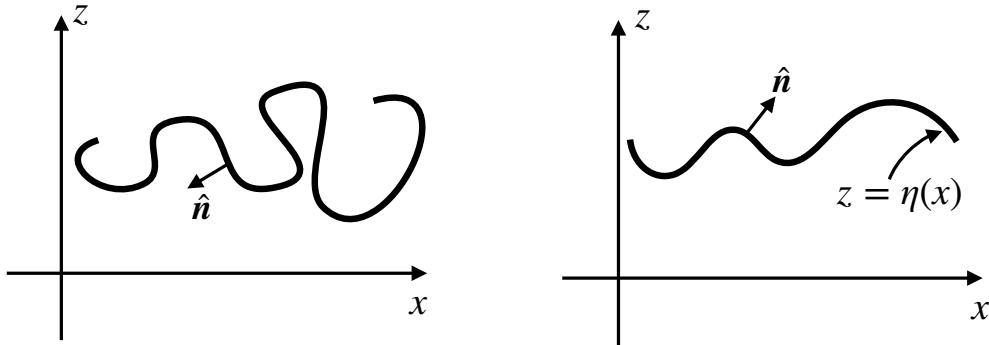


FIGURE 5.1: Two sample curves on the  $x$ - $z$  plane. The left panel shows a curve whose outward normal,  $\hat{n}$ , encounters points where  $\hat{n} \cdot \hat{z} = 0$  and where  $\hat{n} \cdot \hat{z}$  changes sign. This curve, and its generalization to a surface, are not treated in this chapter. The right panel shows a more gently undulating curve where  $\hat{n} \cdot \hat{z} \neq 0$  everywhere, and thus where  $\hat{n} \cdot \hat{z}$  is single signed. For curves such as the right panel, we can express the vertical position as a 1-to-1 function of the horizontal position,  $z = \eta(x)$ . Again, this curve has its natural generalization to a gently undulating surface whereby  $z = \eta(x, y)$  provides a unique mapping between horizontal position and vertical. The assumption regarding no overhanging curves and surfaces is consistent with our study of surfaces defined by a constant generalized vertical coordinate (e.g., isopycnals or isentropes) in Chapter 41.

direction is

$$\hat{n} = \frac{\nabla(z - \eta)}{|\nabla(z - \eta)|} = \frac{\hat{z} - \nabla\eta}{\sqrt{1 + |\nabla\eta|^2}}. \quad (5.4)$$

Figure 5.2 provides an example surface along with the notation.

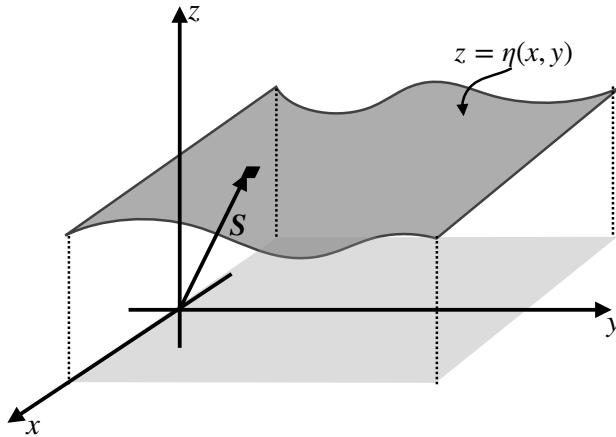


FIGURE 5.2: An example of a surface embedded in Euclidean space. The position of a point on the surface is given by the Cartesian position vector  $S = x\hat{x} + y\hat{y} + \eta(x, y)\hat{z}$ . The relation  $z = \eta(x, y)$  provides a 1-to-1 mapping between the horizontal position and the vertical position of a point on the surface. Correspondingly, the surface is uniquely specified by finding the envelope of points where  $z - \eta(x, y) = 0$ . The lightly shaded region represents the projection of the curved surface onto the flat horizontal  $x$ - $y$  plane below.

## 5.2 Curves in 2D Euclidian space (planar curves)

We here describe the geometry of a curve on the  $x$ - $z$ -plane (a *planar curve*) as depicted in Figure 5.3. These curves are one-dimensional objects living in a two-dimensional Euclidean space. Extensions to curves on non-Euclidean surfaces, such as the sphere or an isopycnal, are straightforward when those surfaces are embedded in a background Euclidean space as in our studies.

### 5.2.1 Differential increments along the curve

As a one-dimensional geometric object, an arbitrary curve can be parameterized by a single coordinate, referred to here as  $\varphi$ . Let  $\mathbf{S}(\varphi)$  specify the position of a point along the curve. Correspondingly, the differential increment between two infinitesimally close points on the curve is given by

$$\mathbf{S}(\varphi + d\varphi) - \mathbf{S}(\varphi) = d\mathbf{S} = \frac{d\mathbf{S}}{d\varphi} d\varphi \equiv \mathbf{t} d\varphi, \quad (5.5)$$

where

$$\mathbf{t} = \frac{d\mathbf{S}}{d\varphi} \quad (5.6)$$

is tangent to the curve. If  $\varphi = s$  is the arc length along the curve, then  $\mathbf{t} = \hat{\mathbf{t}}$  is a unit vector

$$\hat{\mathbf{t}} \cdot \hat{\mathbf{t}} = \frac{d\mathbf{S}}{ds} \cdot \frac{d\mathbf{S}}{ds} = 1. \quad (5.7)$$

In some treatments in this book we also write

$$\hat{s} = \hat{\mathbf{t}} \quad (5.8)$$

to correspond to  $s$  for arc length. Recall we made use of the arc length along a curve in Section 2.4 when describing path integration.

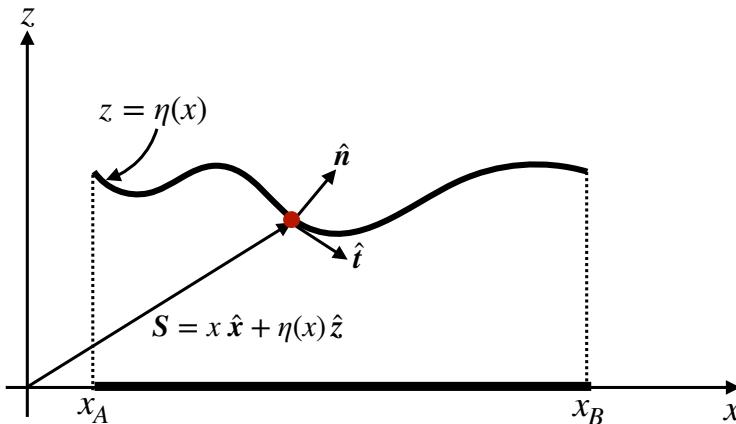


FIGURE 5.3: An orientable path in the  $x$ - $z$  plane defined by a planar curve that does not intersect itself. The Cartesian position of a point on the curve is given by  $\mathbf{S} = x \hat{x} + \eta(x) \hat{z}$ , where  $z = \eta(x)$  is the vertical position of the point. The projection of the curve onto the horizontal  $x$ -axis occupies a range  $x_A \leq x \leq x_B$ . One way to define the curve is by finding the envelope of points where  $z - \eta(x) = 0$ , in which case we can readily find the normal direction pointing upward as  $\hat{n} = \nabla(z - \eta)/|\nabla(z - \eta)| = [\hat{z} - (d\eta/dx) \hat{x}] [1 + (d\eta/dx)^2]^{-1/2}$ , and the normalized tangent direction  $\hat{t} = [\hat{x} + (d\eta/dx) \hat{z}] [1 + (d\eta/dx)^2]^{-1/2}$ .

### 5.2.2 Length along the curve

As in equation (5.3) we can represent the position of a point along the curve using Cartesian coordinates

$$\mathbf{S} = x \hat{x} + \eta(x) \hat{z}. \quad (5.9)$$

Hence, letting  $\varphi = x$  parameterize the curve leads to the representation of the tangent direction

$$\mathbf{t} = \frac{d\mathbf{S}}{dx} = \hat{x} + \frac{d\eta}{dx} \hat{z}, \quad (5.10)$$

which has the magnitude

$$\mathbf{t} \cdot \mathbf{t} = 1 + (\frac{d\eta}{dx})^2, \quad (5.11)$$

so that the normalized tangent vector is

$$\hat{\mathbf{t}} = \frac{\hat{\mathbf{x}} + (\frac{d\eta}{dx}) \hat{\mathbf{z}}}{\sqrt{1 + (\frac{d\eta}{dx})^2}}. \quad (5.12)$$

Likewise, the curve's normal vector is given by

$$\hat{\mathbf{n}} = \frac{\nabla(z - \eta)}{|\nabla(z - \eta)|} = \frac{\hat{\mathbf{z}} - (\frac{d\eta}{dx}) \hat{\mathbf{x}}}{\sqrt{1 + (\frac{d\eta}{dx})^2}}, \quad (5.13)$$

with orthogonality manifest

$$\hat{\mathbf{t}} \cdot \hat{\mathbf{n}} = 0. \quad (5.14)$$

The squared length of an infinitesimal segment along the curve is given by

$$(ds)^2 = d\mathbf{S} \cdot d\mathbf{S} = \left[ \frac{d\mathbf{S}}{dx} \cdot \frac{d\mathbf{S}}{dx} \right] dx dx, \quad (5.15)$$

so that the finite length of the curve is determined by the integral

$$L = \int_0^L ds = \int_{x_A}^{x_B} |d\mathbf{S}/dx| dx = \int_{x_A}^{x_B} \sqrt{1 + (\frac{d\eta}{dx})^2} dx, \quad (5.16)$$

where  $x_A \leq x \leq x_B$  is the range over which  $x$  runs for the projection of the curve onto the  $x$ -axis (see Figure 5.3).

### 5.2.3 Curvature of a curve

Curvature measures the amount that the normal direction changes along the curve. For a planar curve, the curvature at a point equals to the inverse radius of a circle that shares the same tangent plane to the curve at the point (see Figure 5.4). We refer to the radius as the *radius of curvature* and the corresponding circle as the *curvature circle*. To formulate an analytic expression for the radius of curvature at a point on a curve, orient the Cartesian coordinate axes so that the point is at the origin and the tangent plane sits along the  $x$ -axis as in Figure 5.4. Consequently, the outward normal,  $\hat{\mathbf{n}}$ , is parallel to the  $\hat{\mathbf{z}}$  direction.

A Taylor series expansion about the origin tells us that the vertical position of a point along the curve and near to the origin can be written

$$\eta(x) = \eta(0) + x \left[ \frac{d\eta}{dx} \right]_{x=0} + \frac{x^2}{2} \left[ \frac{d^2\eta}{dx^2} \right]_{x=0} + \mathcal{O}(x^3) \quad (5.17a)$$

$$= \frac{x^2}{2} \left[ \frac{d^2\eta}{dx^2} \right]_{x=0} + \mathcal{O}(x^3). \quad (5.17b)$$

This result follows since we placed the origin so that  $\eta(0) = 0$ , and aligned the  $x$ -axis so that it is a tangent plane at the origin, in which case  $d\eta/dx = 0$  at  $x = 0$ . Hence,  $\eta$  has a quadratic behavior near the origin.

Now place a circle with center along the  $z$ -axis so that it is tangent to the curve at the origin, as depicted in Figure 5.4. What is the radius,  $R$ , of the circle that best fits the curve at the origin? To answer this question note that the height of a point on the circle is given by  $h(x) = R(1 - \cos \vartheta)$ ,

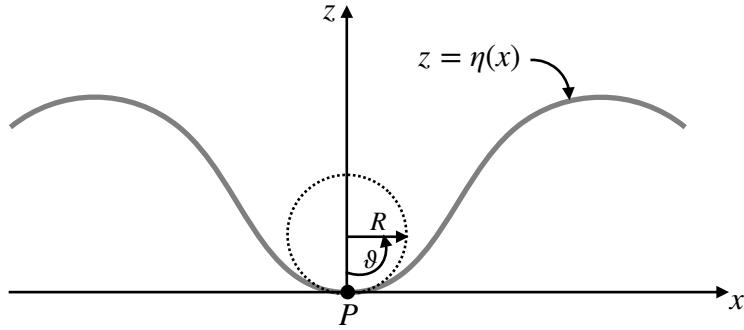


FIGURE 5.4: The radius of curvature at a point on a curve,  $P$ , equals to the radius of the curvature circle that shares the same tangent plane as the curve at the point  $P$ . When constructing the curvature circle we make use of the angle,  $\vartheta$ , to measure the height of a point along the circle,  $h(x) = R(1 - \cos \vartheta) \approx R\vartheta^2/2 \approx x^2/(2R)$ . Setting  $R^{-1} = d^2\eta/dx^2$  provides a second order accurate fit of the curvature circle to the curve at the point  $P$ .

where  $\vartheta = 0$  for a point at the origin and  $\vartheta = \pi$  at the diametrically opposite point. For small  $\vartheta$  this height takes the form

$$h(x) \approx R[1 - 1 + \vartheta^2/2] = x^2/(2R), \quad (5.18)$$

where  $\vartheta = x/R$  near the origin. For the height of a point on the curve (equation (5.17b)) to match the height along the circle, to second order accuracy, requires us to set the circle's radius to

$$\frac{1}{R} = \frac{d^2\eta}{dx^2}. \quad (5.19)$$

Equation (5.19) thus provides an expression for the radius of curvature,  $R$ , whose inverse is the curvature

$$\text{curvature} = \frac{1}{R}. \quad (5.20)$$

This result supports our expectation that the second derivative measures the curvature. As  $R$  gets larger the curvature decreases as the circle approaches a flat plane. In the opposite limit the curvature grows as  $R$  decreases. Note that we could have chosen to orient the circle on the opposite side of the tangent (on the convex side), in which case the radius of curvature is negative. That is,  $R > 0$  when the normal points towards the concave side (side where the curve rises towards  $\hat{n}$ ), whereas  $R < 0$  when the normal points towards the convex side (side where the curve falls away from  $\hat{n}$ ).

In closing this section we note that

$$-\nabla \cdot \hat{n} = \frac{d^2\eta/dx^2}{[1 + (d\eta/dx)^2]^{3/2}}. \quad (5.21)$$

When evaluated at the point of interest along the curve, we set  $d\eta/dx = 0$  so that

$$-\nabla \cdot \hat{n} = \frac{d^2\eta}{dx^2} = \frac{1}{R}. \quad (5.22)$$

This result supports our earlier statement that curvature measures the change in the normal direction along the curve. In fact, the identity

$$-\nabla \cdot \hat{n} = \frac{1}{R} \quad (5.23)$$

holds for an arbitrary point along the curve since it is a coordinate invariant statement.

## 5.3 Surfaces embedded in 3D Euclidean space

We now extend the previous discussion to a two-dimensional surface embedded in three-dimensional Euclidean space such as in Figure 5.2. In general, a 2D surface in 3D space can be parameterized by two variables,  $\varphi^1$  and  $\varphi^2$ , so that infinitesimal increments along the surface satisfy

$$d\mathbf{S} = \frac{\partial \mathbf{S}}{\partial \varphi^1} d\varphi^1 + \frac{\partial \mathbf{S}}{\partial \varphi^2} d\varphi^2 = \mathbf{t}_1 d\varphi^1 + \mathbf{t}_2 d\varphi^2. \quad (5.24)$$

The vectors  $\mathbf{t}_1$  and  $\mathbf{t}_2$  are tangent to the surface at the point  $(\varphi^1, \varphi^2)$ , and yet they are not generally orthogonal to one another.

Making use of the Cartesian expression (5.1)

$$\mathbf{S} = x \hat{\mathbf{x}} + y \hat{\mathbf{y}} + \eta(x, y) \hat{\mathbf{z}} \quad (5.25)$$

brings the two tangent directions into the form

$$\mathbf{t}_1 = \frac{\partial \mathbf{S}}{\partial x} = \hat{\mathbf{x}} + \frac{\partial \eta}{\partial x} \hat{\mathbf{z}} \quad (5.26a)$$

$$\mathbf{t}_2 = \frac{\partial \mathbf{S}}{\partial y} = \hat{\mathbf{y}} + \frac{\partial \eta}{\partial y} \hat{\mathbf{z}}. \quad (5.26b)$$

Likewise, the surface normal vector is given by

$$\hat{\mathbf{n}} = \frac{\nabla(z - \eta)}{|\nabla(z - \eta)|} = \frac{\hat{\mathbf{z}} - \nabla\eta}{|\hat{\mathbf{z}} - \nabla\eta|} = \frac{\hat{\mathbf{z}} - \nabla\eta}{\sqrt{1 + |\nabla\eta|^2}}, \quad (5.27)$$

and it is straightforward to show orthogonality with the two tangent vectors

$$\hat{\mathbf{t}}_1 \cdot \hat{\mathbf{n}} = \hat{\mathbf{t}}_2 \cdot \hat{\mathbf{n}} = 0. \quad (5.28)$$

### 5.3.1 Area on the surface

Recall from Section 1.4.5 that the magnitude of a vector product of two vectors equals to the area of the parallelogram subtended by the vectors. Hence, the area of an infinitesimal surface element with sides  $d\varphi^1$  and  $d\varphi^2$  is given by

$$d\mathcal{S} = \left| \frac{\partial \mathbf{S}}{\partial \varphi^1} \times \frac{\partial \mathbf{S}}{\partial \varphi^2} \right| d\varphi^1 d\varphi^2. \quad (5.29)$$

Making use of Cartesian coordinates brings the area element to

$$d\mathcal{S} = \sqrt{1 + |\nabla\eta|^2} dx dy = \sqrt{1 + |\nabla\eta|^2} dA, \quad (5.30)$$

where

$$dA = dx dy \quad (5.31)$$

is the area of the surface projected onto the horizontal plane. Hence, the area of a finite region is given by the integral

$$\mathcal{S} = \int d\mathcal{S} = \int |\nabla(z - \eta)| dA = \int \sqrt{1 + |\nabla\eta|^2} dx dy, \quad (5.32)$$

where the second and third integrals extend over the region defined by the projection of the surface onto the horizontal (see Figure 5.2).

### 5.3.2 Curvature of a surface

We now seek an expression for the curvature of a point on the surface. Since the surface has two dimensions, we expect the curvature to be measured by two numbers rather than the single curvature for the curve discussed in Section 5.2.3. The method for developing the curvature is analogous to that used for a curve, yet with a bit more mathematics needed to allow for the extra dimension. Figure 5.5 depicts the situation.

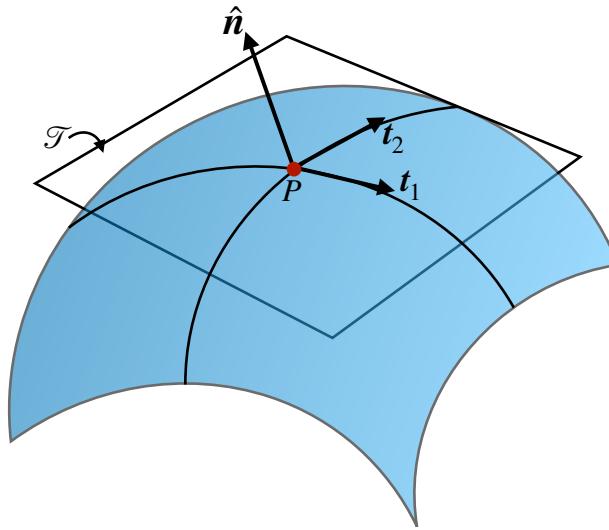


FIGURE 5.5: Depicting the elements needed to construct the curvature of a surface at an arbitrary point,  $P$ . The local normal direction is given by  $\hat{n}$ , along with the two tangent vectors  $t_1$  and  $t_2$ . The tangent vectors span the space of the tangent plane,  $T$ , shown as a flat surface that is tangent at the chosen point on the surface. In this case the surface falls away from the normal direction, as per a convex surface, so that the two radii of curvature are negative. Other surfaces can be concave, whereby both radii of curvature are positive, or hyperbolic (saddle), whereby one is positive and another negative.

Let  $\mathbf{x} = (x_1, x_2) = (x, y)$  be Cartesian coordinates on a tangent plane local to an arbitrary point on the surface, with the origin of the coordinate system taken at the point. Near to the point, we can estimate the vertical distance of a point on the surface from the tangent plane according to the quadratic form

$$\eta \approx \frac{1}{2} x_m \mathbb{C}_{mn} x_n, \quad (5.33)$$

where  $\mathbb{C}$  is the second order tensor of second partial derivatives evaluated at the point

$$\mathbb{C} = \begin{bmatrix} \frac{\partial^2 \eta}{\partial x_1^2} & \frac{\partial^2 \eta}{\partial x_1 \partial x_2} \\ \frac{\partial^2 \eta}{\partial x_1 \partial x_2} & \frac{\partial^2 \eta}{\partial x_2^2} \end{bmatrix}. \quad (5.34)$$

As a symmetric tensor,  $\mathbb{C}$  is diagonalizable and it has two eigenvalues,  $R_1^{-1}$  and  $R_2^{-1}$ , along with its associated eigenvectors,  $\mathbf{e}_1$  and  $\mathbf{e}_2$ . The quadratic form (5.33) can thus be written as

$$\eta \approx \frac{1}{2} R_1^{-1} (\mathbf{x} \cdot \mathbf{e}_1)^2 + \frac{1}{2} R_2^{-1} (\mathbf{x} \cdot \mathbf{e}_2)^2. \quad (5.35)$$

$R_1$  and  $R_2$  are the principle radii of curvature for the surface at the point  $P$ . They correspond, respectively, to the radii of the curvature circles in the  $\hat{\mathbf{n}} \cdot \mathbf{e}_1$  and  $\hat{\mathbf{n}} \cdot \mathbf{e}_2$  planes. If the radius of curvature  $R_m$  is positive, then the surface curves towards  $\hat{\mathbf{n}}$  along the  $\hat{\mathbf{n}} \cdot \mathbf{e}_i$  plane, and conversely if  $R_m$  is negative. The surface takes the shape of a saddle when the two radii of curvature have opposite signs.

There are two scalar invariants of the tensor  $\mathbb{C}$  that commonly arise in applications.

- $\text{Tr}(\mathbb{C}) = R_1^{-1} + R_2^{-1}$ , which is twice the mean curvature for the surface. With the normal vector given by equation (5.4), one can show that

$$-\nabla \cdot \hat{\mathbf{n}} = \frac{\nabla^2 \eta}{[1 + (\nabla \eta)^2]^{3/2}}. \quad (5.36)$$

A bit of algebra leads us to conclude that

$$-\nabla \cdot \hat{\mathbf{n}} = \frac{1}{R_1} + \frac{1}{R_2}, \quad (5.37)$$

for any point along the surface, thus generalizing the result (5.22) found for a curve.

- $\det(\mathbb{C}) = 1/(R_1 R_2)$  is known as the *Gaussian curvature*, which is the product of the two curvatures.

### 5.3.3 Curves on the surface $z = \eta(x, y)$

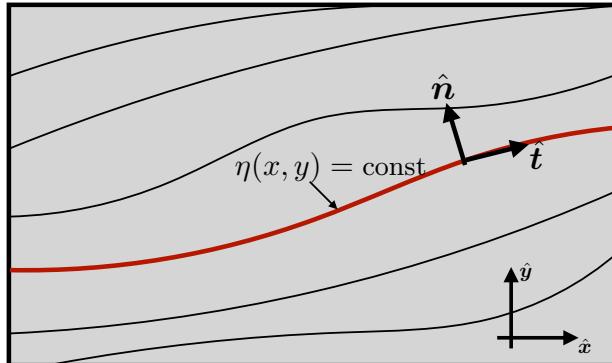


FIGURE 5.6: Geometry depicting a contour along a particular line of constant  $z = \eta(x, y)$ , such as for a constant elevation path along a mountain or valley. The along-contour direction is  $\hat{\mathbf{t}} = d\mathbf{x}/ds$ , with  $s$  the arc length along the contour. The unit direction pointing to the left of the contour direction is  $\hat{\mathbf{n}}$ , with  $\hat{\mathbf{n}} \cdot \hat{\mathbf{t}} = 0$  and  $\hat{\mathbf{t}} \times \hat{\mathbf{n}} = \hat{\mathbf{z}}$ . Both  $\hat{\mathbf{n}}$  and  $\hat{\mathbf{t}}$  are horizontal unit vectors.

We now consider a curve, as in Section 5.2, defined along a two dimensional surface,  $z = \eta(x, y)$ , with the curve defined by lines of constant  $z = \eta(x, y)$ . For example, if  $\eta(x, y)$  is the solid earth topography, then lines of constant  $\eta$  are contours of constant topography. By definition, these contours have no projection into the vertical direction (i.e., they do not go uphill or downhill), and they are determined by

$$d\eta = 0 = \nabla \eta \cdot d\mathbf{x}, \quad (5.38)$$

where  $d\mathbf{x} = \hat{\mathbf{x}} dx + \hat{\mathbf{y}} dy$  is the horizontal space increment along the contour. Following the

introduction of arc length in Section 5.2.1, we write

$$d\eta = 0 = \nabla\eta \cdot d\mathbf{x} = \nabla\eta \cdot \frac{d\mathbf{x}}{ds} ds = \nabla\eta \cdot \hat{\mathbf{t}} ds, \quad (5.39)$$

where  $\hat{\mathbf{t}}$  is a unit vector pointing in the direction of the contour. To build an orthogonal triad of coordinates, we then define an orthogonal unit vector,  $\hat{\mathbf{n}}$ , that points to the left of the contour direction so that

$$\hat{\mathbf{n}} \cdot \hat{\mathbf{t}} = 0 \quad \text{and} \quad \hat{\mathbf{t}} \times \hat{\mathbf{n}} = \hat{\mathbf{z}}, \quad (5.40)$$

as depicted in Figure 5.6.



## 5.4 Exercises

### EXERCISE 5.1: JACOBIAN EVALUATED ALONG A CONTOUR

Consider the vector cross product of two functions,  $\psi(x, y)$  and  $Q(x, y)$

$$\hat{\mathbf{z}} \cdot (\nabla\psi \times \nabla Q) = \partial_x\psi \partial_y Q - \partial_y\psi \partial_x Q \equiv J(\psi, Q), \quad (5.41)$$

where the final equality defined the Jacobian operator. Show that when evaluated along a contour of constant  $Q$ , the Jacobian is given by

$$J(\psi, Q) = -(\hat{\mathbf{n}} \cdot \nabla Q)(\hat{\mathbf{t}} \cdot \nabla\psi) \quad (5.42)$$

where  $\hat{\mathbf{t}}$  is the unit tangent along the contour and  $\hat{\mathbf{n}}$  is a unit vector pointing to the left of the tangent (e.g., see Figure 5.6).

### EXERCISE 5.2: CURVATURE OF A CIRCLE

Make use of equation (5.23), as well as the polar coordinates from Section 8.3, to show that for a circle of radius  $r$  we have

$$-\nabla \cdot \hat{\mathbf{n}} = \frac{1}{r}, \quad (5.43)$$

where  $\hat{\mathbf{n}} = -\hat{\mathbf{r}}$  points to the left when moving around the circle in a counterclockwise direction. Hence, the radius of curvature for the circle equals to the circle's radius.



# Chapter 6

## General tensors in brief

Vector calculus, as formalized by the Cartesian tensor analysis of Chapters 1 and 2, is sufficient for many areas of geophysical fluid mechanics. However, there are a number of applications where general tensors prove of use to ensure that the physics shines through the maths. We thus go beyond Cartesian tensor analysis to here consider general tensors, thus enabling a more versatile, and precise, mathematical framework for the study of geophysical fluid mechanics. Besides enhancing our tools for geophysical fluid mechanics, general tensor analysis is found throughout physics so that understanding the formalism, if only its rudiments, can greatly help to understand the literature.

Geophysical fluid mechanics applications require only a modest level of new formalism in the transition from Cartesian tensors to general tensors. The key reason is that geophysical fluids are assumed to be embedded within Euclidean space,  $\mathbb{R}^3$ , where Euclidean space is the flat space familiar from Newtonian mechanics. Notably,  $\mathbb{R}^3$  has zero intrinsic curvature so we say that it is a *flat space*. So although we are concerned with fluid motion on curved manifolds (e.g., spherical planets); motion on curved and fluctuating manifolds (e.g., isopycnals); and in describing that motion using non-orthogonal coordinates (e.g., generalized vertical coordinates), the fluid remains embedded within a background Euclidean space. Through this embedding, the local geometry inherits features from the Euclidean space such as how to measure distance between points via the Pythagorean theorem. A further simplification for geophysical fluid mechanics arises since we make use of universal Newtonian time. Hence, time is measured the same by all observers and reference frames. That is, the spatial coordinates used by geophysical fluid mechanics can be a function of time, but the time coordinate is always the same. Each of these features of the space and time used for geophysical fluid mechanics means that our mathematical needs are far simpler than the general relativist who studies fluids moving in strong gravity fields and/or over galactic distances.

Throughout our exploration of general tensor analysis it is useful to keep in mind the fundamental goal is to uncover objective statements about how physical systems operate. In particular, we aim to make use of a formalism that

- supports computations to allow for the comparison of theory with measurements;
- provides a systematic technology to transform between coordinate systems, since there are many occasions where such transformations are useful to develop physical insight and support calculations;
- provides equations that are independent of specific coordinate system.

These goals are realized by general tensor analysis so that the technology reflects the underlying objective nature of physical relationships while allowing for a quantitative realization of those relationships in particular situations.

READER'S GUIDE TO THIS CHAPTER

This brief chapter offers an overview sufficient to appreciate why we need general tensors for this book. We do so by offering a conceptual platform for general tensor analysis, with details of the technology presented in Chapter 7. We focus on tensor analysis on spatial manifolds endowed with a metric, thus touching on the rudiments of *Riemannian differential geometry*. Furthermore, we restrict attention to manifolds embedded in Euclidean space, thus providing a natural extension of the Cartesian tensor analysis from Chapters 1 and 2.

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6.1	Coordinate independent physical relations . . . . .	122
6.1.1	Tensor operations . . . . .	123
6.1.2	Comments . . . . .	123
6.2	Points, trajectories, and coordinates . . . . .	124
6.2.1	Time as a parameter and time as a coordinate . . . . .	124
6.2.2	The importance of index placement . . . . .	124
6.3	Example coordinate descriptions . . . . .	125
6.3.1	Eulerian coordinates . . . . .	125
6.3.2	Isopycnal coordinates . . . . .	125
6.3.3	Lagrangian or material coordinates . . . . .	126
6.3.4	Tracer coordinates . . . . .	126
6.4	The velocity vector and basis vectors . . . . .	126
6.4.1	Coordinate representation . . . . .	127
6.4.2	Basis vectors . . . . .	127
6.5	Notational conventions . . . . .	127
6.5.1	Placement of tensor labels . . . . .	127
6.5.2	Covariant, contravariant, and Einstein summation . . . . .	128
6.5.3	The boldface notation . . . . .	128
6.5.4	Space-time approach . . . . .	129

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## 6.1 Coordinate independent physical relations

Physical relations are independent of subjective choices for their mathematical representations. This principle motivates us to seek mathematical expressions between objects whose meaning transcends a particular coordinate representation. At its most profound level, there is no *a priori* notion of the underlying geometry, with an insistence on such generalities leading to general relativity and the notion of *general covariance*. We are not going that far in this book, given that we accept the notion of a background Euclidean space on which the fluid moves, and we make use of a universal Newtonian time measured by all observers. Nonetheless, we insist that the mathematical expression of a physical relation be independent of the choice of coordinates (*coordinate invariance*), which is ensured when expressed as relations between geometric objects such as points, vectors, and tensors.

Although physics does not care about coordinates, physicists often do. Namely, it is convenient, and sometimes necessary, to work with specific coordinates suited to the symmetry of the physical system. After deriving a physical law in one set of coordinates, it is often of interest to establish the form of the law in another set of coordinates. How does the physical law, typically represented as a differential equation, transform into other coordinates? So long as the equations

are written in a proper tensorial form then the equations are form invariant. That is, coordinate invariance means that the equations look the same regardless the choice of coordinates. Consequently, “physics as geometry” has a major practical implication. Namely, we can establish the validity of a physical relation in any convenient set of coordinates, and then extend that relation to all coordinates so long as we respect the basic rules of tensor analysis.

### 6.1.1 Tensor operations

Extending a mathematical equation to all coordinates requires the equations to respect certain tensor rules. In brief, all tensor indices are properly matched and each derivative is covariant as specified in Section 7.10. In chapter 7, we provide the details needed to understand general coordinate invariance. In this chapter we outline the procedure. The elegance and power rendered by coordinate invariance is the key reason that tensor analysis is ubiquitous in theoretical physics.

To ensure an equation respects coordinate invariance requires us to understand certain properties of tensors and operations with tensors that produce components of new tensors. We here summarize the specific properties characterizing coordinate invariance (taken after page 153 of *Schutz, 1985*):

1. Manipulations of tensor components are called *permissible tensor operations* if they produce components of new tensors. The following are permissible operations:
  - (a) Multiplication of a tensor by a scalar produces a new tensor of the same type.
  - (b) Addition of components of two tensors of the same type gives components of a new tensor of the same type. In particular, only tensors of the same type can be equal.
  - (c) Multiplication of components of two tensors of arbitrary type gives components of a new tensor whose type is given by the sum of the types for the individual tensors. This operation is called the *outer product* or *tensor product* and is denoted by the operator  $\otimes$ . For example,  $\mathbf{A} \otimes \mathbf{B}$  is a second order tensor built from the outer product of two vectors,  $\mathbf{A}$  and  $\mathbf{B}$ .
  - (d) A corollary of the multiplication rule is that if two objects yield a tensor, and one of these objects is a tensor then so too is the other. This is the *quotient* rule.
  - (e) Covariant differentiation (Sections 7.10 and 7.11) increases by one the order of a tensor, with the covariant derivative operator denoted by  $\nabla$ .
  - (f) Contraction on a pair of indices of the components of a tensor reduces by one the order of a tensor.
2. If two tensors of the same type have equal components in a given coordinate system, then they have equal components in all coordinate systems. Hence, the tensors are identical.
3. If a mathematical equation consists of tensors combined only by the permissible tensor operations, and if the equation is true in one coordinate system, then it is true in any coordinate system. If the equations involve covariant derivatives, then the equations remain form invariant under changes in coordinates. For the partial differential equations of geophysical fluid mechanics, covariant differentiation is the key to coordinate invariance.

### 6.1.2 Comments

The remainder of this chapter, as well as Chapter 7, provide the needed details for supporting the above notions of coordinate invariance. Even without penetrating these details, the reader should be able to appreciate why coordinate invariance is so central to physics.

## 6.2 Points, trajectories, and coordinates

Consider a point in space,  $\mathcal{P}$ , at a particular time  $\tau$ . As time progresses, the point traces out a curve in space-time. We call that curve a *trajectory*. The trajectory could be of a point particle following the fluid flow, thus defining the Lagrangian reference frame (Section 12.2). Or it could trace the path of something else such as a fish, balloon, boat, or airplane. As the trajectory is a one-dimensional curve, it is specified mathematically by a single parameter (see Section 5.2.1). We choose the time measured by an observer on the trajectory for this parameter, in which case the trajectory is written  $\mathcal{P}(\tau)$ .

A point in the fluid and its trajectory in space-time are geometric objects that exist independently of any coordinate representation. Even so, we find the need to represent points, trajectories, vectors, and other geometric objects using coordinates. For example, coordinates are needed to make quantitative statements about fluid flow in relation to other observers. What is its speed and direction relative to a chosen reference frame? What is the distance from an origin or from another particle? Tensor analysis provides a formalism that enables us to answer such quantitative questions while maintaining a clear view on the underlying physics and geometry.

### 6.2.1 Time as a parameter and time as a coordinate

In special and general relativity, there is a mixing of space and time that warrants the use of four-dimensional space-time tensor analysis. In contrast, for classical mechanics forming the foundation of geophysical fluid mechanics, time remains numerically the same throughout space. We thus make use of the same universal (or Newtonian) time since the fluid velocity and wave speeds are far smaller than the speed of light.

The time parameter,  $\tau$ , specifies a point along a trajectory. The coordinate time,  $t$ , measures time for all positions throughout space. This distinction between the time parameter and time coordinate is pedantic given that  $\tau = t$  (up to a constant offset) in a Newtonian universe. Nonetheless, it is convenient to make the distinction when measuring how fluid properties change since these changes are subject to motion of the observer. For example, changes following a trajectory, found by computing the trajectory time derivative  $\partial/\partial\tau$ , are generally distinct from changes found by computing the time derivative  $\partial/\partial t$ , in which the spatial coordinates are held fixed.

When the trajectory is defined by a fluid particle, we refer to  $\partial/\partial\tau$  as the material or Lagrangian time derivative. This is also the time derivative computed when working with Newtonian particle mechanics as in Part II of this book. In contrast, if the spatial coordinates are fixed in space, then  $\partial/\partial t$  is an Eulerian time derivative. When alternative spatial coordinates are used, some of which can move (see Section 6.2.2), then  $\partial/\partial t$  can be a mixture of Lagrangian and Eulerian or perhaps neither.

### 6.2.2 The importance of index placement

Much of the formalism of general tensor analysis builds from Cartesian representations of vector and matrix analysis, with generalizations that provide objective statements independent of coordinates. One key point of distinction from Cartesian tensors is that the position (up or down) of a tensor label has significance in general tensor analysis. We follow the standard convention by labeling an arbitrary coordinate with indices upstairs in their *contravariant* position,  $\xi^\alpha$ . It is furthermore common to express each of the coordinates in an ordered list according to

$$\xi^\alpha = (\xi^0, \xi^1, \xi^2, \xi^3). \quad (6.1)$$

We emphasize that the index is a label for the coordinate; it is not an exponent or power. We use a convention whereby Greek labels run from  $\alpha = 0, 1, 2, 3$  with  $\alpha = 0$  the time coordinate and  $\alpha = a = 1, 2, 3$  the three coordinates used to locate a point in the Euclidean space of Newtonian mechanics. The following shorthand notations are commonly used in this book

$$\xi^\alpha = (\xi^0, \xi^1, \xi^2, \xi^3) = (\xi^0, \xi^a) = (\xi^0, \boldsymbol{\xi}). \quad (6.2)$$

## 6.3 Example coordinate descriptions

We here offer a few examples of coordinates used for describing geophysical fluid systems. As the time coordinate remains universal in our study, we are here only concerned with the spatial coordinates,  $a = 1, 2, 3$ .

### 6.3.1 Eulerian coordinates

The Cartesian coordinates for a point are written

$$\xi^a = (x, y, z) \quad \text{Cartesian}, \quad (6.3)$$

whereas for spherical coordinates we write (see Figure 8.1)

$$\xi^a = (\lambda, \phi, r) \quad \text{spherical} \quad (6.4)$$

and cylindrical polar coordinates (see Figure 8.2)

$$\xi^a = (r, \vartheta, z) \quad \text{cylindrical}. \quad (6.5)$$

These coordinates identify fixed positions in space. We can use these *Eulerian* coordinates to mark the trajectory  $\mathcal{P}(\tau)$  as it crosses the spatial point  $\xi^a$  at time  $t$ . We provide a more complete discussion of Eulerian coordinates in Section 12.3.

As shown in Section 6.4, Cartesian coordinates are notable for having basis vectors maintaining a fixed direction throughout space. This feature lends much simplicity to Cartesian coordinates and its corresponding Cartesian tensor analysis (Chapters 1 and 2). In contrast, the spherical basis vectors are spatially dependent. Likewise, the radial and angular basis vectors for polar cylindrical coordinates are spatially dependent, whereas the vertical direction is fixed. Additionally, the spherical and cylindrical coordinates do not all have the same physical dimensions. Each of these features of spherical and cylindrical coordinates places them outside the purview of Cartesian tensor analysis.

### 6.3.2 Isopycnal coordinates

In geophysical fluids that are stably stratified in the vertical, it is common to measure the vertical position of a fluid element by specifying its entropy, buoyancy, or potential density depending on the application. We generically write these *isentropic*, *buoyancy*, or *isopycnal* coordinates as

$$\xi^a = (x, y, b) \quad \text{with} \quad b = b(x, y, z, t) \quad \text{isopycnal coordinates}, \quad (6.6)$$

where  $b = b(x, y, z, t)$  is a generic symbol for entropy, buoyancy, or potential density. Entropy, buoyancy, and potential density are materially invariant for perfect fluid flow (flow absent irreversible processes such as mixing or heating). Hence, all fluid particle motion occurs on surfaces

of constant  $b$ . Under such perfect fluid conditions, isopycnal coordinates are of great use for describing fluid mechanics of stably stratified geophysical flows.

The isopycnal coordinates are generally not orthogonal since the direction normal to a buoyancy surface is not generally vertical. Hence, even if the horizontal coordinates are Cartesian, the use of  $b$  to measure the vertical precludes the use of Cartesian tensor analysis. Furthermore, we note the distinct physical dimensions of the three spatial coordinates  $(x, y, b)$ , again necessitating the use of general tensor analysis.

### 6.3.3 Lagrangian or material coordinates

We often conceive of a fluid as a continuum of constant mass fluid elements distinguished by continuum marker coordinates or labels. The initial position for a fluid element offers a common choice for these *material coordinates*. The fluid dynamical equations of motion (i.e., Newton's Law of motion) can be formulated using material coordinates so long as the material coordinate maintains a 1-to-1 relation to points in space. This kinematical framework is termed *Lagrangian* or *material*. The resulting dynamical equations share much in common with Newtonian particle mechanics, though with the added feature of contact forces acting between the fluid elements. We formally describe Lagrangian coordinates in Section 12.3 and encounter Lagrangian descriptions throughout this book.

If we represent material coordinates by the Cartesian positions of fluid elements at an arbitrary initial time, then we can make use of Cartesian tensor analysis. However, it is sometimes useful to make use of alternative markers. One example is the isopycnal coordinate mentioned above, whose value remains invariant under perfect fluid motion. In this manner, we refer to the isopycnal coordinates as "quasi-Lagrangian" since its vertical coordinate follows the vertical position of a perfect fluid parcel whereas its horizontal coordinates are Eulerian.

### 6.3.4 Tracer coordinates

Consider a triplet of linearly independent tracer concentrations  $C^a = C^a(x, y, z, t)$  that spans  $\mathbb{R}^3$ . Hence, at any point in space there is a unique intersection of three constant tracer surfaces, so that we can uniquely determine a point in space by specifying the value for the three tracer concentrations. We can thus use tracer concentrations as the spatial coordinates

$$\xi^a = (C^1, C^2, C^3). \quad (6.7)$$

In some cases there are only two linearly independent tracers, in which case the two may be used in combination with a third spatial coordinate such as depth or pressure. Furthermore, the case of one tracer coordinate formally reduces to the isopycnal coordinate system described above.

## 6.4 The velocity vector and basis vectors

Consider two points in space that sit along a particular trajectory separated by an infinitesimal time increment,  $d\tau$ . The velocity vector for this trajectory is defined by

$$\vec{v}(\tau) = \lim_{\Delta\tau \rightarrow 0} \frac{\mathcal{P}(\tau + \Delta\tau/2) - \mathcal{P}(\tau - \Delta\tau/2)}{\Delta\tau} = \frac{d\mathcal{P}(\tau)}{d\tau}. \quad (6.8)$$

The velocity is a vector pointing in the direction determined by the difference between two points on a trajectory, in the limit as the time separation between the points vanishes. Consequently, the velocity points in a direction tangent to the trajectory. Notably, the above definition for the

velocity makes no use of coordinates. Rather, the velocity vector is determined by the geometry of the trajectory and the specification of the trajectory's time parameter. Hence, velocity is fundamentally an arrow with a length and direction and as such, the velocity is a geometric object with this fact emphasized by exposing the arrow.

The definition of velocity as a vector tangent to the trajectory is a general property of all vectors living on a manifold. Namely, a vector at a point on a manifold lives within the tangent plane to the manifold at that point. This observation signals to us the need to be very careful when comparing vectors on a curved manifold such as the sphere or an isopycnal surface. Before comparing the two vectors they must be brought to the same point so they can be compared.

### 6.4.1 Coordinate representation

We now establish an arbitrary set of spatial coordinates,  $\xi^a$ , to represent points in space. These coordinates are used to measure the spatial position of the trajectory according to

$$\mathcal{P}(\tau) = \mathcal{P}[\xi^a(\tau)], \quad (6.9)$$

where  $\xi^a(\tau)$  is the coordinate position on the trajectory at time  $\tau$ . This coordinate representation for the trajectory induces a coordinate representation for the velocity through use of the chain rule

$$\vec{v}(\tau) = \frac{d\mathcal{P}(\tau)}{d\tau} = \frac{\partial \mathcal{P}}{\partial \xi^a} \frac{d\xi^a}{d\tau} \equiv \vec{e}_a v^a. \quad (6.10)$$

The expansion coefficients

$$v^a = \frac{d\xi^a}{d\tau} \quad (6.11)$$

provide a representation for the velocity vector  $\vec{v}(\tau)$  within the coordinate system  $\xi^a$ .

### 6.4.2 Basis vectors

For each number  $v^a$  there is a corresponding basis vector  $\vec{e}_a$  whose value at the point  $\mathcal{P}$  is given by

$$\vec{e}_a(\mathcal{P}) = \frac{\partial \mathcal{P}}{\partial \xi^a}. \quad (6.12)$$

Abstracting this expression allows us to identify the basis vector as the partial derivative

$$\vec{e}_a = \frac{\partial}{\partial \xi^a}. \quad (6.13)$$

The basis vectors are generally a function of space and time, with Cartesian coordinates a notable exception whereby they are space-time constants.

## 6.5 Notational conventions

We here introduce notational conventions that help to simplify many of the manipulations, sometimes referred to as *index gymnastics*, encountered with general tensors.

### 6.5.1 Placement of tensor labels

As indicated in Section 6.2.2, the placement of tensor labels has specific meaning with general tensor analysis. It is therefore critical to maintain proper usage to ensure *conservation of indices*

across an equals sign. As a first example of this usage, notice how the basis vectors in equation (6.12) inherit a lowered tensor label. This placement follows from the partial derivative operator that carries an upper coordinate label in the denominator of the operator.

### 6.5.2 Covariant, contravariant, and Einstein summation

For general tensors, the Einstein summation convention assumes that labels are summed over their range when a lower *covariant* label matches an upper *contravariant* label. In this way we have an arbitrary vector in space written as

$$\vec{F}(\tau) = \sum_{a=1}^3 \vec{e}_a F^a = \vec{e}_a F^a. \quad (6.14)$$

This rule generalizes that used for Cartesian tensors in Chapter 1. For general tensors, contraction is between a lower and an upper label. We return to such contractions in Section 7.2, where we show that the contraction of a vector and a one-form renders a scalar.

The names *covariant* and *contravariant* originate from their relation to the labels placed on a coordinate basis vectors (Section 6.4.2), and thus how they change under coordinate transformations relative to how basis vectors change (Section 7.1). The covariant tensor label accords with the downstairs label placement for a coordinate basis, whereas the upstairs contravariant label is contrary to the coordinate basis (e.g., see Section 2.26 of *Schutz* (1980)). A useful mnemonic is “co-low” to signal that the covariant label is downstairs (“low”). The names covariant and contravariant are used infrequently in modern tensor analysis, which instead considers tensors as geometric objects and so is not primarily concerned with the coordinate representations of tensors.

### 6.5.3 The boldface notation

In Cartesian tensors we have no need to distinguish  $\vec{F}$  from the boldface  $\mathbf{F}$ . One means to extend this notation to general tensors is to organize the contravariant representation  $F^a$  into an ordered list  $(F^1, F^2, F^3)$  and to use the boldface notation

$$\mathbf{F} = (F^1, F^2, F^3). \quad (6.15)$$

Likewise, we can organize the basis vectors according to

$$\mathbf{\vec{e}} = (\vec{e}_1, \vec{e}_2, \vec{e}_3) \quad (6.16)$$

and the coordinates as

$$\boldsymbol{\xi} = (\xi^1, \xi^2, \xi^3). \quad (6.17)$$

With this notation the velocity vector representation from equation (6.10) takes on the form

$$\vec{v} = \vec{e}_a v^a = \vec{e} \cdot \mathbf{v}. \quad (6.18)$$

Likewise, a trajectory can be represented in terms of a chosen set of coordinates according to

$$\mathcal{P} = \vec{e}_a \xi^a = \vec{e} \cdot \boldsymbol{\xi}. \quad (6.19)$$

Notice that the arrow symbol over the basis vector remains even when using the boldface. This usage is required since the arrow carries information about the vector nature of the object, whereas the boldface is merely a shorthand for an ordered list.

Although the above notation makes good sense, we more generally allow the boldface to be synonymous with the vector arrow notation

$$\mathbf{F} = \vec{F} = \vec{e}_a F^a. \quad (6.20)$$

Though corrupting the convention in equation (6.18), this notation is readily used in the literature and as such will be employed in this book where the meaning is clear and after our tensor brain-muscle has been exercised.

#### 6.5.4 Space-time approach

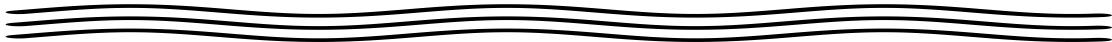
As introduced in Section 6.2.2, we make use of a Greek label when incorporating time to the tensor indices, with  $\alpha = 0$  denoting the time coordinate. Time remains universal in the Newtonian world of geophysical fluid mechanics. However, many coordinates are functions of both space and time. Therefore, when measuring time changes in one coordinate system it will differ from time changes in another. Following equation (6.2) used for coordinates, we make use of the following index notation and ordered list for contravariant components of 4-vectors

$$F^\alpha = (F^0, F^1, F^2, F^3) = (F^0, F^a) = (F^0, \mathbf{F}). \quad (6.21)$$

In Cartesian coordinates, the time component of the velocity 4-vector is unity

$$v^\alpha = (1, v^1, v^2, v^3) = (1, v^a) = (1, \mathbf{v}) \quad \text{4-velocity in Cartesian coordinates.} \quad (6.22)$$

We make use of the 4-vector formalism in Section 7.9 when performing the transformation of partial derivatives. In that discussion we note that the time coordinate is not a function of space and yet the space coordinates are generally a function of time, which makes the 4-vector formalism of use to transform partial derivatives. Otherwise, we retain the space plus time approach (3+1) of classical mechanics.





# Chapter 7

## General tensor analysis

In this chapter we generalize the Cartesian algebra of Chapter 1 and Cartesian calculus of Chapter 2 to general tensors. We focus on space tensors so that time typically remains outside of the tensor formalism. The single exception is that we consider a space-time transformation of the partial time derivative operator (Section 7.9), since the time derivative cares about the motion of space coordinates.

Cartesian tensor analysis provides a systematic formulation of vector analysis. The Euclidean metric provided by the Kronecker symbol (i.e., the identity tensor) underlies Cartesian tensors. Here, we extend the formalism of Cartesian tensors by allowing for an arbitrary spatial metric, and in so doing move into the realm of *Riemannian differential geometry*. A more mathematically deductive approach would be to first study calculus on differential manifolds that are not endowed with a metric.

### READER'S GUIDE TO THIS CHAPTER

This chapter is necessary for understanding the mathematics of generalized vertical coordinates in Chapters 41, 42, and 43. Otherwise, it can be skimmed or returned to later if the need arises. Material here is an updated version of Chapters 20 and 21 from [Griffies \(2004\)](#) along with some streamlining. Other resources include the treatment of tensors for fluid mechanics given by [Aris \(1962\)](#) and the physics treatment by [Thorne and Blandford \(2017\)](#).

7.1	The metric tensor and coordinate transformations . . . . .	132
7.1.1	Cartesian coordinates in Euclidean space . . . . .	132
7.1.2	The metric as a symmetric second order tensor . . . . .	133
7.1.3	Coordinate representation of the metric tensor . . . . .	133
7.1.4	Transforming the coordinate representation of the metric tensor . . . . .	134
7.1.5	Basis vectors . . . . .	135
7.1.6	Finite distance between points . . . . .	135
7.2	One-forms . . . . .	135
7.2.1	Coordinate representation of a one-form . . . . .	135
7.2.2	Basis one-forms and the bi-orthogonality relation . . . . .	136
7.2.3	Metric as a mapping between vectors and one-forms . . . . .	136
7.2.4	Transformation of the coordinate representation . . . . .	137
7.2.5	Arbitrary coordinate representation of inverse metric . . . . .	137
7.2.6	Functions versus scalars . . . . .	137
7.3	Scalar product . . . . .	138
7.4	Worked example: oblique coordinates . . . . .	138

7.4.1	Turning the crank . . . . .	139
7.4.2	Comments . . . . .	140
7.5	The volume element and Jacobian of transformation . . . . .	<b>140</b>
7.5.1	Jacobian of transformation . . . . .	141
7.5.2	Relating the Jacobian to the determinant of the metric . . . . .	141
7.6	The permutation symbol and the determinant . . . . .	<b>142</b>
7.6.1	Connecting the permutation symbol to the determinant . . . . .	142
7.6.2	Further identities satisfied by the determinant . . . . .	142
7.7	The Levi-Civita tensor and the volume element . . . . .	<b>143</b>
7.7.1	General coordinate representation of the Levi-Civita tensor . . . . .	143
7.7.2	The Levi-Civita tensor and the volume element . . . . .	144
7.8	Vector cross product . . . . .	<b>144</b>
7.9	Coordinate transformation of partial derivatives . . . . .	<b>144</b>
7.9.1	The space-time transformation matrix . . . . .	144
7.9.2	Determinant of the transformation matrix . . . . .	145
7.9.3	Multiplying the transformation matrix and its inverse . . . . .	146
7.9.4	Transformation of space and time partial derivatives . . . . .	146
7.10	Covariant derivative of a scalar . . . . .	<b>147</b>
7.11	Covariant derivative of a vector . . . . .	<b>147</b>
7.11.1	Derivative of a vector . . . . .	147
7.11.2	An alternative derivation . . . . .	148
7.11.3	Christoffel symbols as the metric connection . . . . .	148
7.12	Covariant derivative of a one-form . . . . .	<b>148</b>
7.13	Covariant derivative of the metric tensor . . . . .	<b>149</b>
7.14	Christoffel symbols in terms of the metric . . . . .	<b>149</b>
7.15	Covariant divergence of a vector . . . . .	<b>149</b>
7.15.1	Contraction of the Christoffel symbols . . . . .	150
7.15.2	Exponential of the determinant . . . . .	150
7.16	Covariant Laplacian of a scalar . . . . .	<b>150</b>
7.17	Covariant curl of a vector . . . . .	<b>151</b>
7.18	Gauss's divergence theorem . . . . .	<b>151</b>
7.19	Stokes' theorem . . . . .	<b>151</b>

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## 7.1 The metric tensor and coordinate transformations

In the study of fluid mechanics we find the need to measure the distance between two points in space at a particular time instance. Since we assume all points live on a smooth and orientable manifold (e.g., a sphere, an isopycnal), it is sufficient to consider the distance between two infinitesimally close points and use integration to measure finite distances. The measurement of distance requires a metric tensor, which is the subject of this section.

### 7.1.1 Cartesian coordinates in Euclidean space

Consider a Cartesian coordinate representation for the spatial position of two points, with point  $\mathcal{P}$  having space coordinates  $\xi^a = x^a$  and the other point  $\mathcal{Q}$  an infinitesimal distance away at  $x^a + dx^a$ . Furthermore, let

$$d\mathbf{x} = dx^a \vec{e}_a \quad (7.1)$$

be the infinitesimal space vector pointing from  $\mathcal{P}$  to  $\mathcal{Q}$ . Since the space is Euclidean, the squared distance between the two points is based on the Euclidean norm; i.e., the familiar scalar or dot product (Section 1.3)

$$ds^2 = d\mathbf{x} \cdot d\mathbf{x} = \vec{e}_a \cdot \vec{e}_b dx^a dx^b = \delta_{ab} dx^a dx^b. \quad (7.2)$$

In this expression,

$$(ds)^2 \equiv ds^2 \quad (7.3)$$

is the squared infinitesimal arc-length separating the two points. The Kronecker symbol,  $\delta_{ab}$ , is symmetric

$$\delta_{ab} = \delta_{ba}, \quad (7.4)$$

and vanishes when  $a \neq b$  and is unity when  $a = b$

$$\delta_{ab} = \begin{cases} 0 & \text{if } a \neq b \\ 1 & \text{if } a = b. \end{cases} \quad (7.5)$$

The Kronecker symbol is a representation of the identity tensor.

### 7.1.2 The metric as a symmetric second order tensor

As defined by equation (7.2),  $\delta_{ab}$  forms the Cartesian representation of the *metric tensor* for Euclidean space. The metric is a second order tensor, meaning that its coordinate representation carries two tensor labels. Contracting the metric tensor with two vectors leads to a number, namely the squared distance between the two points. Hence, the metric establishes the means to measure the distance between two points that live on a manifold.

We write this distance-measuring property of the metric tensor in a geometric manner through

$$\text{distance}(\vec{P}, \vec{Q}) = \sqrt{\mathcal{G}(\vec{P}, \vec{Q})}. \quad (7.6)$$

Here,  $\mathcal{G}$  is the metric tensor with coordinate representation  $g_{ab}$  and  $\vec{P}, \vec{Q}$  are infinitesimally close vectors with coordinate representations

$$\vec{P} = \xi^a \vec{e}_a \quad \vec{Q} = \vec{P} + d\xi^a \vec{e}_a. \quad (7.7)$$

Equation (7.6) indicates that the metric tensor takes two vectors as argument and produces a scalar. Furthermore, since

$$\text{distance}(\vec{P}, \vec{Q}) = \text{distance}(\vec{Q}, \vec{P}) \geq 0, \quad (7.8)$$

the metric tensor is a symmetric and positive tensor that produces zero only when  $\vec{P} = \vec{Q}$ .

### 7.1.3 Coordinate representation of the metric tensor

Given the geometric expression (7.6) for the metric, we determine its representation in an arbitrary coordinate system by considering the squared distance between the coordinate basis vectors

$$\text{distance}(\vec{e}_a, \vec{e}_b) = \sqrt{\mathcal{G}(\vec{e}_a, \vec{e}_b)}. \quad (7.9)$$

This relation determines the coordinate components of the metric tensor

$$\mathcal{G}(\vec{e}_a, \vec{e}_b) \equiv g_{ab}. \quad (7.10)$$

Furthermore, for a manifold embedded in Euclidean space this relation is written

$$g_{ab} = \vec{e}_a \cdot \vec{e}_b. \quad (7.11)$$

In this manner we see that the basis vectors determine the metric tensor components. Note that if the basis vectors are orthogonal, then the metric tensor components vanish unless  $a = b$ .

### 7.1.4 Transforming the coordinate representation of the metric tensor

We find opportunities to represent the metric tensor in various coordinate systems. Here, we consider the transformation from Cartesian coordinates  $\xi^a = x^a$  to arbitrary coordinates  $\xi^{\bar{a}}$ . Use of the chain rule along with some index gymnastics leads to the equivalent expression for the squared infinitesimal length between two points

$$ds^2 = \delta_{ab} d\xi^a d\xi^b = \delta_{ab} \frac{\partial \xi^a}{\partial \xi^{\bar{a}}} \frac{\partial \xi^b}{\partial \xi^{\bar{b}}} d\xi^{\bar{a}} d\xi^{\bar{b}} \equiv \delta_{ab} \Lambda_{\bar{a}}^a \Lambda_{\bar{b}}^b d\xi^{\bar{a}} d\xi^{\bar{b}} \equiv g_{\bar{a}\bar{b}} d\xi^{\bar{a}} d\xi^{\bar{b}}, \quad (7.12)$$

where

$$g_{\bar{a}\bar{b}} = \delta_{ab} \Lambda_{\bar{a}}^a \Lambda_{\bar{b}}^b \quad (7.13)$$

defines the components to the metric tensor as represented by the new set of coordinates  $\xi^{\bar{a}}$ . We also introduced elements to the *transformation matrix*

$$\Lambda_{\bar{a}}^a = \frac{\partial \xi^a}{\partial \xi^{\bar{a}}}. \quad (7.14)$$

This matrix of partial derivatives has a non-zero entry when a coordinate in one representation changes while moving along the direction of a coordinate in the other representation. As for any partial derivative, the complement coordinates are held fixed when performing the derivative. Although carrying indices, the numbers  $\Lambda_{\bar{a}}^a$  are *not* components of a tensor. Instead, they are components of a matrix used to transform tensor representations from one coordinate system to another. Organized as a matrix, we follow a convention whereby the row is denoted by  $a$  and the column by  $\bar{a}$

$$\Lambda_{\bar{a}}^a = \begin{bmatrix} (\partial \xi^1 / \partial \xi^{\bar{1}})_{\bar{2},\bar{3}} & (\partial \xi^1 / \partial \xi^{\bar{2}})_{\bar{1},\bar{3}} & (\partial \xi^1 / \partial \xi^{\bar{3}})_{\bar{1},\bar{2}} \\ (\partial \xi^2 / \partial \xi^{\bar{1}})_{\bar{2},\bar{3}} & (\partial \xi^2 / \partial \xi^{\bar{2}})_{\bar{1},\bar{3}} & (\partial \xi^2 / \partial \xi^{\bar{3}})_{\bar{1},\bar{2}} \\ (\partial \xi^3 / \partial \xi^{\bar{1}})_{\bar{2},\bar{3}} & (\partial \xi^3 / \partial \xi^{\bar{2}})_{\bar{1},\bar{3}} & (\partial \xi^3 / \partial \xi^{\bar{3}})_{\bar{1},\bar{2}} \end{bmatrix}. \quad (7.15)$$

Note that the lower index is displaced to the right to delineate which index refers to the column. The transformation matrix is nonsingular for one-to-one invertible coordinate transformations, in which case its determinant, called the *Jacobian of the transformation*, is nonvanishing and single signed. Finally, we sometimes find it useful to write the un-barred coordinates as an ordered list in a column,  $\xi = (\xi^1, \xi^2, \xi^3)^T$ , in which case the transformation matrix takes on the abbreviated form

$$\Lambda_{\bar{a}}^a = \begin{bmatrix} (\partial \xi / \partial \xi^{\bar{1}})_{\bar{2},\bar{3}} & (\partial \xi / \partial \xi^{\bar{2}})_{\bar{1},\bar{3}} & (\partial \xi / \partial \xi^{\bar{3}})_{\bar{1},\bar{2}} \end{bmatrix}. \quad (7.16)$$

Use of this transformation matrix leads to the arbitrary coordinate representation of the metric tensor

$$g_{\bar{a}\bar{b}} = \vec{e}_{\bar{a}} \cdot \vec{e}_{\bar{b}} = \begin{bmatrix} \frac{\partial \xi}{\partial \xi^{\bar{1}}} \cdot \frac{\partial \xi}{\partial \xi^{\bar{1}}} & \frac{\partial \xi}{\partial \xi^{\bar{1}}} \cdot \frac{\partial \xi}{\partial \xi^{\bar{2}}} & \frac{\partial \xi}{\partial \xi^{\bar{1}}} \cdot \frac{\partial \xi}{\partial \xi^{\bar{3}}} \\ \frac{\partial \xi}{\partial \xi^{\bar{2}}} \cdot \frac{\partial \xi}{\partial \xi^{\bar{1}}} & \frac{\partial \xi}{\partial \xi^{\bar{2}}} \cdot \frac{\partial \xi}{\partial \xi^{\bar{2}}} & \frac{\partial \xi}{\partial \xi^{\bar{2}}} \cdot \frac{\partial \xi}{\partial \xi^{\bar{3}}} \\ \frac{\partial \xi}{\partial \xi^{\bar{3}}} \cdot \frac{\partial \xi}{\partial \xi^{\bar{1}}} & \frac{\partial \xi}{\partial \xi^{\bar{3}}} \cdot \frac{\partial \xi}{\partial \xi^{\bar{2}}} & \frac{\partial \xi}{\partial \xi^{\bar{3}}} \cdot \frac{\partial \xi}{\partial \xi^{\bar{3}}} \end{bmatrix}. \quad (7.17)$$

### 7.1.5 Basis vectors

We transform the basis vectors from Cartesian into arbitrary coordinates through the transformation

$$\vec{e}_{\bar{a}} = \Lambda_{\bar{a}}^a \vec{e}_a. \quad (7.18)$$

Use of the transformation matrix (7.16) renders the arbitrary coordinate basis vectors

$$\vec{e}_{\bar{1}} = \frac{\partial \xi}{\partial \xi^{\bar{1}}} \quad \text{and} \quad \vec{e}_{\bar{2}} = \frac{\partial \xi}{\partial \xi^{\bar{2}}} \quad \text{and} \quad \vec{e}_{\bar{3}} = \frac{\partial \xi}{\partial \xi^{\bar{3}}}. \quad (7.19)$$

### 7.1.6 Finite distance between points

Once the metric is determined, the distance along a curve between two finitely separated points is given by integration

$$L = \int \sqrt{ds^2} = \int_{\varphi_1}^{\varphi_2} \left| g_{ab} \frac{d\xi^a}{d\varphi} \frac{d\xi^b}{d\varphi} \right|^{1/2} d\varphi, \quad (7.20)$$

where  $\varphi$  is a parameter specifying the curve (e.g., the arc length as in Section 2.4), with  $\varphi_1$  and  $\varphi_2$  specifying the curve's endpoints.

## 7.2 One-forms

The metric tensor  $\mathcal{G}$  is a function of two vectors. When the metric “eats” the two vectors, the result is the scalar distance between the vectors (equation (7.6))

$$\text{distance}(\vec{A}, \vec{B}) = \sqrt{\mathcal{G}(\vec{A}, \vec{B})}. \quad (7.21)$$

What if the metric only eats one vector? The resulting geometric object is known as a one-form

$$\tilde{A} \equiv \mathcal{G}(\vec{A}, ), \quad (7.22)$$

with the tilde used to distinguish a one-form from a vector.

### 7.2.1 Coordinate representation of a one-form

We can determine the coordinate representation of a one-form by eating a basis vector

$$\tilde{A}(\vec{e}_b) = \mathcal{G}(\vec{A}, \vec{e}_b) \quad (7.23a)$$

$$= \mathcal{G}(A^a \vec{e}_a, \vec{e}_b) \quad (7.23b)$$

$$= \mathcal{G}(\vec{e}_a, \vec{e}_b) A^a \quad (7.23c)$$

$$= g_{ab} A^a. \quad (7.23d)$$

To reach this result we pulled the coordinate representation  $A^a$  outside of the metric tensor since the tensor eats vectors rather than numbers. This equation defines the coordinate representation of the one-form  $\tilde{A}$  in terms of its *dual* vector  $\vec{A}$  and the metric tensor

$$A_b = g_{ab} A^a. \quad (7.24)$$

We thus see that the metric tensor provides the means to lower an index on the representation of a vector, thus producing the representation of a one-form. We return to this point in Section

## 7.2.3.

## 7.2.2 Basis one-forms and the bi-orthogonality relation

Just as for vectors, we find use for a basis of one-forms to specify their coordinate representation. The basis of one-forms,  $\tilde{e}^a$ , are defined through the bi-orthogonality relation

$$\mathcal{G}(\tilde{e}^a, \tilde{e}_b) = \tilde{e}^a \cdot \tilde{e}_b = \delta_b^a, \quad (7.25)$$

where

$$\delta_b^a = g^{ac} g_{cb} \quad (7.26)$$

are components to the Kronecker delta tensor, taking the value of unity when  $a = b$  and zero otherwise

$$\delta_b^a = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}. \quad (7.27)$$

It is only for Cartesian coordinates that we have

$$\delta_c^a = g^{ab} \delta_{bc} \quad \text{Cartesian coordinates}, \quad (7.28)$$

which follows since  $g^{ab} = \delta^{ab}$  in Cartesian coordinates.

We can obtain an explicit expression for the basis one-forms in arbitrary coordinates by transforming from Cartesian coordinates through use of the inverse transformation

$$\tilde{e}^{\bar{a}} = \Lambda_a^{\bar{a}} \tilde{e}^a, \quad (7.29)$$

which renders

$$\tilde{e}^{\bar{1}} = \hat{x} \frac{\partial \xi^{\bar{1}}}{\partial x} + \hat{y} \frac{\partial \xi^{\bar{1}}}{\partial y} + \hat{z} \frac{\partial \xi^{\bar{1}}}{\partial z} = \nabla \xi^{\bar{1}} \quad (7.30a)$$

$$\tilde{e}^{\bar{2}} = \hat{x} \frac{\partial \xi^{\bar{2}}}{\partial x} + \hat{y} \frac{\partial \xi^{\bar{2}}}{\partial y} + \hat{z} \frac{\partial \xi^{\bar{2}}}{\partial z} = \nabla \xi^{\bar{2}} \quad (7.30b)$$

$$\tilde{e}^{\bar{3}} = \hat{x} \frac{\partial \xi^{\bar{3}}}{\partial x} + \hat{y} \frac{\partial \xi^{\bar{3}}}{\partial y} + \hat{z} \frac{\partial \xi^{\bar{3}}}{\partial z} = \nabla \xi^{\bar{3}}. \quad (7.30c)$$

In Section 7.9.3 we verify that the basis one-forms satisfy the orthogonality relation (7.25) with the basis vectors

$$\tilde{e}^{\bar{a}} \cdot \tilde{e}_{\bar{b}} = \delta_{\bar{b}}^{\bar{a}}. \quad (7.31)$$

## 7.2.3 Metric as a mapping between vectors and one-forms

We can contract the expression (7.24) with components of the inverse metric tensor,  $g^{ab}$ , to render

$$g^{ab} A_b = g^{ab} g_{bc} A^c = \delta_c^a A^c = A^a. \quad (7.32)$$

This identity, as well as equation (7.24), show that the metric provides a map between coordinate representations of one-forms and vectors.

To every vector  $\vec{A}$  there is a corresponding one-form  $\tilde{A}$ . We say that the one-forms and vectors are *dual*, with the mapping between one-forms and vectors rendered by the metric tensor. Abstractly, we say that a vector at a point on a manifold lives on the tangent space at that point,

whereas a one-form lives on the cotangent space. The metric tensor attaches the tangent space to the co-tangent space. For Cartesian tensor analysis, the duality between one-forms and vectors is the duality between row vectors and column vectors. Furthermore, as for Cartesian tensors, we construct an inner product by contracting one-forms and vectors to produce a scalar. Finally, the duality relation given by equation (7.24) offers us the means to raise and lower tensor indices in a manner akin to the transpose operation in linear algebra that produces a row vector from a column vector.

### 7.2.4 Transformation of the coordinate representation

The transformation matrix (7.14) provides the means to convert any arbitrary coordinate representation of a tensor from one coordinate system to another. For example, consider the coordinate representation of a vector, which is realized by letting the vector eat one of the basis one-forms

$$\vec{F}(\tilde{e}^a) = F^a. \quad (7.33)$$

Now consider another coordinate system with basis one-forms  $\tilde{e}^{\bar{a}}$ , so that the vector has a representation

$$\vec{F}(\tilde{e}^{\bar{a}}) = F^{\bar{a}}. \quad (7.34)$$

Transforming the basis one-form using the transformation matrix leads to

$$F^{\bar{a}} = \vec{F}(\tilde{e}^{\bar{a}}) = \vec{F}(\Lambda_a^{\bar{a}} \tilde{e}^a) = \Lambda_a^{\bar{a}} \vec{F}(\tilde{e}^a) = \Lambda_a^{\bar{a}} F^a. \quad (7.35)$$

Transformation of an arbitrary one-form representation takes place with the inverse transformation matrix

$$F_{\bar{a}} = \tilde{F}(\tilde{e}_{\bar{a}}) = \tilde{F}(\Lambda_{\bar{a}}^a \tilde{e}_a) = \Lambda_{\bar{a}}^a \tilde{F}(\tilde{e}_a) = \Lambda_{\bar{a}}^a F_a. \quad (7.36)$$

### 7.2.5 Arbitrary coordinate representation of inverse metric

The inverse metric tensor has an arbitrary coordinate representation given by

$$g^{\bar{a}\bar{b}} = \tilde{e}^{\bar{a}} \cdot \tilde{e}^{\bar{b}} = \begin{bmatrix} \nabla\xi^{\bar{1}} \cdot \nabla\xi^{\bar{1}} & \nabla\xi^{\bar{1}} \cdot \nabla\xi^{\bar{2}} & \nabla\xi^{\bar{1}} \cdot \nabla\xi^{\bar{3}} \\ \nabla\xi^{\bar{2}} \cdot \nabla\xi^{\bar{1}} & \nabla\xi^{\bar{2}} \cdot \nabla\xi^{\bar{2}} & \nabla\xi^{\bar{2}} \cdot \nabla\xi^{\bar{3}} \\ \nabla\xi^{\bar{3}} \cdot \nabla\xi^{\bar{1}} & \nabla\xi^{\bar{3}} \cdot \nabla\xi^{\bar{2}} & \nabla\xi^{\bar{3}} \cdot \nabla\xi^{\bar{3}} \end{bmatrix}. \quad (7.37)$$

Proof that  $g^{\bar{a}\bar{b}} g_{\bar{b}\bar{c}} = \delta_{\bar{c}}^{\bar{a}}$  requires use of the chain rule relations derived in Section 7.9.3.

### 7.2.6 Functions versus scalars

A scalar field carries no tensor labels and as such it does not transform under coordinate transformations. That is, a scalar is coordinate invariant and it is the simplest type of tensor field. Temperature, kinetic energy, and specific entropy are example scalar fields considered in this book. Now consider the first component of a vector field,  $F^1$ , whose value at a point,  $\mathcal{P}$  and time,  $\tau$ , is written  $F^1(\mathcal{P}, \tau)$ . Now change the coordinates so that the first component to the vector field at the same  $(\mathcal{P}, \tau)$  is written  $F^{\bar{1}}(\mathcal{P}, \tau)$ . Yet under a coordinate transformation we generally have  $F^{\bar{1}}(\mathcal{P}, \tau) \neq F^1(\mathcal{P}, \tau)$ , so that the individual components to a vector field, though functions of space and time, *do not* individually transform as a scalar field. Instead, they transform as components to a vector field. This very basic example illustrates the distinction between functions of space and time, which includes any component of any tensor field, from scalar fields, which are coordinate invariant.

## 7.3 Scalar product

In Section 1.3.2 we defined the scalar product between two Cartesian vectors. The natural generalization is given by

$$\vec{P} \cdot \vec{Q} = P^a Q^b \vec{e}_a \cdot \vec{e}_b = P^a Q^b g_{ab} = P^a Q_a = P_b Q^b, \quad (7.38)$$

where the second equality made use of the metric tensor coordinate representation given by equation (7.11). We can conceive of the scalar product in a somewhat more general manner by recalling that a one-form operates on a vector,  $\tilde{P}(\vec{Q})$ . Conversely, a vector operates on a one-form,  $\vec{Q}(\tilde{P})$ . Exposing components leads to

$$\tilde{P}(\vec{Q}) = \tilde{P}(Q^a \vec{e}_a) = Q^a \tilde{P}(\vec{e}_a) = Q^a P_a, \quad (7.39)$$

which equals to

$$\vec{Q}(\tilde{P}) = \vec{Q}(P_a \tilde{e}^a) = P_a \vec{Q}(\tilde{e}^a) = P_a Q^a. \quad (7.40)$$

The scalar product is invariant to coordinate changes, as seen through

$$\vec{Q}(\tilde{P}) = \vec{Q}(P_a \tilde{e}^a) = P_a Q^a = \vec{Q}(P_{\bar{a}} \tilde{e}^{\bar{a}}) = P_{\bar{a}} Q^{\bar{a}}. \quad (7.41)$$

The invariance is also revealed by working just with the coordinate representations and introducing the transformation matrix elements

$$P_a Q^a = (\Lambda^{\bar{a}}_a P_{\bar{a}}) (\Lambda^a_{\bar{b}} Q^{\bar{b}}) = \Lambda^{\bar{a}}_a \Lambda^a_{\bar{b}} P_{\bar{a}} Q^{\bar{b}} = \delta^{\bar{a}}_{\bar{b}} P_{\bar{a}} Q^{\bar{b}} = P_{\bar{a}} Q^{\bar{a}}. \quad (7.42)$$

## 7.4 Worked example: oblique coordinates

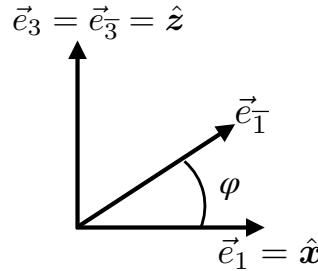


FIGURE 7.1: Oblique basis vectors for the  $x$ - $z$  plane where  $\vec{e}_{\bar{1}} = \vec{e}_1 \cos \varphi + \vec{e}_3 \sin \varphi$  and  $\vec{e}_{\bar{3}} = \vec{e}_3$ , with  $\vec{e}_1 = \hat{x}$  and  $\vec{e}_3 = \hat{z}$ . These coordinate basis vectors are related to those used for generalized vertical coordinates shown in the left panel of Figure 41.2.

We pause here to consider the example of *oblique coordinates* for the  $x$ - $z$  plane as specified by the basis vectors

$$\vec{e}_{\bar{1}} = \vec{e}_1 \cos \varphi + \vec{e}_3 \sin \varphi = \hat{x} \cos \varphi + \hat{z} \sin \varphi. \quad \text{and} \quad \vec{e}_{\bar{3}} = \vec{e}_3 = \hat{z}. \quad (7.43)$$

The oblique coordinate basis vectors,  $\vec{e}_{\bar{a}}$ , are orthogonal when the angle  $\varphi = 0, \pi$ ; otherwise they are non-orthogonal. Also note that if  $\varphi = \pi/2, 3\pi/2$  then  $\vec{e}_{\bar{1}} = \pm \vec{e}_{\bar{3}}$ , in which case the vectors no longer form a basis for the  $x$ - $z$  plane. So in the following we assume  $\varphi \in (-\pi/2, \pi/2)$ . These coordinates are oriented so that they correspond to the generalized vertical coordinate basis vectors depicted in Figure 41.2. Finally, for the purposes of this section we ignore the 2 direction

and just work within the  $x$ - $z$  plane. Tensor indices thus carry values 1 and 3 with 2 ignored.

### 7.4.1 Turning the crank

We here exhibit the results of turning the crank for the oblique coordinates.

#### *Transformation matrix and its inverse*

We can construct the transformation matrix through  $\vec{e}_{\bar{a}} = \Lambda_{\bar{a}}^a \vec{e}_a$ , and use of the coordinate basis definition (7.43)

$$\vec{e}_{\bar{1}} = \Lambda_{\bar{1}}^1 \vec{e}_1 + \Lambda_{\bar{1}}^3 \vec{e}_3 \implies \Lambda_{\bar{1}}^1 = \cos \varphi, \quad \Lambda_{\bar{1}}^3 = \sin \varphi \quad (7.44a)$$

$$\vec{e}_{\bar{3}} = \Lambda_{\bar{3}}^1 \vec{e}_1 + \Lambda_{\bar{3}}^3 \vec{e}_3 \implies \Lambda_{\bar{3}}^1 = 0, \quad \Lambda_{\bar{3}}^3 = 1, \quad (7.44b)$$

so that the transformation matrix is

$$\Lambda_{\bar{a}}^a = \begin{bmatrix} \Lambda_{\bar{1}}^1 & \Lambda_{\bar{1}}^3 \\ \Lambda_{\bar{3}}^1 & \Lambda_{\bar{3}}^3 \end{bmatrix} = \begin{bmatrix} \cos \varphi & 0 \\ \sin \varphi & 1 \end{bmatrix}, \quad (7.45)$$

and a matrix inversion yields the inverse transformation matrix

$$\Lambda_{\bar{a}}^{\bar{a}} = \begin{bmatrix} \Lambda_{\bar{1}}^{\bar{1}} & \Lambda_{\bar{1}}^{\bar{3}} \\ \Lambda_{\bar{3}}^{\bar{1}} & \Lambda_{\bar{3}}^{\bar{3}} \end{bmatrix} = \frac{1}{\cos \varphi} \begin{bmatrix} 1 & 0 \\ -\sin \varphi & \cos \varphi \end{bmatrix}. \quad (7.46)$$

#### *Basis one-forms*

The basis one-forms using oblique coordinates are determined by

$$\tilde{e}^{\bar{a}} = \Lambda_{\bar{a}}^{\bar{a}} \tilde{e}^a = \Lambda_{\bar{1}}^{\bar{a}} \tilde{e}^1 + \Lambda_{\bar{3}}^{\bar{a}} \tilde{e}^3 \quad (7.47)$$

with  $\tilde{e}^1 = \hat{x}$  and  $\tilde{e}^3 = \hat{z}$  for Cartesian coordinates. Making use of the inverse transformation matrix (7.46) leads to

$$\tilde{e}^{\bar{1}} = \Lambda_{\bar{1}}^{\bar{1}} \tilde{e}^1 + \Lambda_{\bar{3}}^{\bar{1}} \tilde{e}^3 = \frac{\hat{x}}{\cos \varphi} \quad (7.48a)$$

$$\tilde{e}^{\bar{3}} = \Lambda_{\bar{1}}^{\bar{3}} \tilde{e}^1 + \Lambda_{\bar{3}}^{\bar{3}} \tilde{e}^3 = -\hat{x} \tan \varphi + \hat{z}. \quad (7.48b)$$

We can readily verify the bi-orthogonality relation (7.25) whereby

$$\vec{e}_{\bar{a}} \cdot \tilde{e}^{\bar{b}} = \delta_{\bar{a}}^{\bar{b}}. \quad (7.49)$$

#### *Representing a vector*

The inverse transformation matrix (7.46) can be used to derive the relation between the Cartesian coordinate representation of an arbitrary vector,  $\vec{P} = P^a \vec{e}_a$ , and the oblique coordinate representation,  $\vec{P} = P^{\bar{a}} \vec{e}_{\bar{a}}$ . Doing so leads to the contravariant components written using oblique coordinates

$$P^{\bar{a}} = \Lambda_{\bar{a}}^{\bar{a}} P^a = \Lambda_{\bar{1}}^{\bar{a}} P^1 + \Lambda_{\bar{3}}^{\bar{a}} P^3 \implies P^{\bar{1}} = \frac{1}{\cos \varphi} P^1 \text{ and } P^{\bar{3}} = -\tan \varphi P^1 + P^3. \quad (7.50)$$

Likewise, the covariant representation can be found by using the transformation matrix (7.45) to render

$$P_{\bar{a}} = \Lambda_{\bar{a}}^a P_a = \Lambda_{\bar{a}}^1 P_1 + \Lambda_{\bar{a}}^3 P_3 \implies P_{\bar{1}} = P_1 \cos \varphi + P_3 \sin \varphi \text{ and } P_{\bar{3}} = P_3, \quad (7.51)$$

where  $P^a = P_a$  for the Cartesian coordinate representation.

### Representing the metric tensor

The covariant representation of the metric tensor is given by

$$g_{\bar{a}\bar{b}} = \delta_{ab} \Lambda_{\bar{a}}^a \Lambda_{\bar{b}}^b = \begin{bmatrix} g_{\bar{1}\bar{1}} & g_{\bar{1}\bar{3}} \\ g_{\bar{3}\bar{1}} & g_{\bar{3}\bar{3}} \end{bmatrix} = \begin{bmatrix} 1 & \sin \varphi \\ \sin \varphi & 1 \end{bmatrix}, \quad (7.52)$$

and its inverse is

$$g^{\bar{a}\bar{b}} = \delta^{ab} \Lambda_{\bar{a}}^a \Lambda_{\bar{b}}^b = \begin{bmatrix} g^{\bar{1}\bar{1}} & g^{\bar{1}\bar{3}} \\ g^{\bar{3}\bar{1}} & g^{\bar{3}\bar{3}} \end{bmatrix} = \frac{1}{(\cos \varphi)^2} \begin{bmatrix} 1 & -\sin \varphi \\ -\sin \varphi & 1 \end{bmatrix}. \quad (7.53)$$

### Scalar product

The scalar product is given by

$$\vec{P} \cdot \vec{P} = g_{\bar{a}\bar{b}} P^{\bar{a}} P^{\bar{b}} \quad (7.54a)$$

$$= P_{\bar{b}} P^{\bar{b}} \quad (7.54b)$$

$$= (P_1 \cos \varphi + P_3 \sin \varphi) \frac{1}{\cos \varphi} P^1 + P_3 (P^3 - \tan \varphi P^1) \quad (7.54c)$$

$$= P_1 P^1 + P_3 P^3 \quad (7.54d)$$

$$= \delta_{ab} P^a P^b. \quad (7.54e)$$

## 7.4.2 Comments

Oblique coordinate offer a pedagogical step towards the more complex case of generalized vertical coordinates studied in Chapter 41. Indeed, much of the tensor algebra needed for generalized vertical coordinates is concisely summarized in the above steps using oblique coordinates.

## 7.5 The volume element and Jacobian of transformation

Recall from Section 1.5.2 that we derived an expression for the volume of an infinitesimal region of Euclidean space,  $\mathbb{R}^3$ , using Cartesian coordinates

$$dV = dx dy dz (\hat{x} \times \hat{y}) \cdot \hat{z} = dx dy dz. \quad (7.55)$$

This volume element is used for integrating over a region of  $\mathbb{R}^3$  when using Cartesian coordinates. Furthermore, its material fluid expression measures the volume of a fluid element. We now generalize this result to arbitrary coordinates.

### 7.5.1 Jacobian of transformation

From multi-variate calculus, the relation between  $d\xi^1 d\xi^2 d\xi^3$  and  $d\xi^{\bar{1}} d\xi^{\bar{2}} d\xi^{\bar{3}}$  for two sets of coordinates is given by

$$d\xi^1 d\xi^2 d\xi^3 = \frac{\partial \boldsymbol{\xi}}{\partial \boldsymbol{\xi}} d\xi^{\bar{1}} d\xi^{\bar{2}} d\xi^{\bar{3}} \quad (7.56a)$$

$$= \frac{\partial(\xi^1, \xi^2, \xi^3)}{\partial(\xi^{\bar{1}}, \xi^{\bar{2}}, \xi^{\bar{3}})} d\xi^{\bar{1}} d\xi^{\bar{2}} d\xi^{\bar{3}} \quad (7.56b)$$

$$= \left[ \frac{\partial \boldsymbol{\xi}}{\partial \xi^{\bar{1}}} \times \frac{\partial \boldsymbol{\xi}}{\partial \xi^{\bar{2}}} \right] \cdot \frac{\partial \boldsymbol{\xi}}{\partial \xi^{\bar{3}}} d\xi^{\bar{1}} d\xi^{\bar{2}} d\xi^{\bar{3}} \quad (7.56c)$$

$$= \det(\Lambda^a_{\bar{a}}) d\xi^{\bar{1}} d\xi^{\bar{2}} d\xi^{\bar{3}}, \quad (7.56d)$$

where  $\det(\Lambda^a_{\bar{a}})$  is the determinant of the transformation matrix, also known as the *Jacobian of transformation*. The transformation is well defined so long as the Jacobian does not vanish. We maintain labels on the transformation matrix inside the determinant symbol to help indicate the sense for the transformation. This notation also helps maintain proper conservation of tensor indices.

### 7.5.2 Relating the Jacobian to the determinant of the metric

Recall the expression (7.12) for the transformation of the metric

$$g_{\bar{a}\bar{b}} = \Lambda^a_{\bar{a}} \Lambda^b_{\bar{b}} g_{ab}. \quad (7.57)$$

We can write this expression as a matrix equation

$$\bar{\mathcal{G}} = \Lambda^T \mathcal{G} \Lambda \quad (7.58)$$

where  $\Lambda^T$  is the transposed matrix. Taking determinants of both sides yields

$$\det(\bar{\mathcal{G}}) = \det(\Lambda^T \mathcal{G} \Lambda) = \det(\Lambda^T) \det(\mathcal{G}) \det(\Lambda) = [\det(\Lambda)]^2 \det(\mathcal{G}). \quad (7.59)$$

To reach this result we used the property of determinants that  $\det(AB) = \det(A)\det(B)$  for any two matrices, and  $\det(\Lambda^T) = \det(\Lambda)$ . Consequently,

$$\det(\Lambda^a_{\bar{a}}) = \frac{\sqrt{\det(g_{\bar{a}\bar{b}})}}{\sqrt{\det(g_{ab})}} = \frac{\sqrt{\det(\bar{\mathcal{G}})}}{\sqrt{\det(\mathcal{G})}}. \quad (7.60)$$

We are thus led to the equivalent expressions for the volume element

$$dV \equiv \sqrt{\det(\mathcal{G})} d\xi^1 d\xi^2 d\xi^3 = \sqrt{\det(\bar{\mathcal{G}})} d\xi^{\bar{1}} d\xi^{\bar{2}} d\xi^{\bar{3}}. \quad (7.61)$$

This relation provides us with our desired general coordinate expression for the volume element. For the special case when the unbarred coordinates are Cartesian,  $g_{ab} = \delta_{ab}$  so that  $\det(\mathcal{G}) = 1$  and

$$\det(\Lambda^a_{\bar{a}}) = \sqrt{\det(g_{\bar{a}\bar{b}})} \quad \text{unbarred coordinates are Cartesian.} \quad (7.62)$$

This is a rather useful expression for our purposes, since we can always use Cartesian as the unbarred coordinates given that geophysical fluids move in a background Euclidean space.

## 7.6 The permutation symbol and the determinant

As discussed in Section 1.4.1, the Cartesian components of the Levi-Civita tensor are given by the permutation symbol,  $\epsilon_{abc}$ . To help determine the general coordinate representation of the Levi-Civita tensor, we here develop some identities satisfied by the determinant of the transformation matrix.

### 7.6.1 Connecting the permutation symbol to the determinant

Consider a two-dimensional space with a transformation matrix  $\Lambda^a_{\bar{a}}$  between two sets of coordinates. The determinant of the transformation is given by

$$\det(\Lambda^a_{\bar{a}}) = \Lambda^1_{\bar{1}} \Lambda^2_{\bar{2}} - \Lambda^1_{\bar{2}} \Lambda^2_{\bar{1}}. \quad (7.63)$$

Introducing the permutation symbol  $\epsilon_{ab}$  allows us to write this expression in a more tidy manner

$$\det(\Lambda^a_{\bar{a}}) = \epsilon_{ab} \Lambda^a_{\bar{1}} \Lambda^b_{\bar{2}} \quad (7.64)$$

with

$$\epsilon_{12} = 1 \quad \text{and} \quad \epsilon_{21} = -1. \quad (7.65)$$

The permutation symbol is defined to have numerically the same values whether the labels are raised or lowered:  $\epsilon^{ab} = \epsilon_{ab}$ .

We can generalize the above to any number of dimensions, each of which adds one more label to the permutation symbol and one more number added to the permutation string. We already encountered the three dimensional version in Section 1.4.1 when discussing the vector cross product, in which case the permutation symbol is

$$\epsilon_{123} = 1 \quad (7.66a)$$

$$\epsilon_{abc} = \begin{cases} 0 & \text{if any two labels are the same,} \\ 1 & \text{if } a, b, c \text{ is an even permutation of 1, 2, 3,} \\ -1 & \text{if } a, b, c \text{ is an odd permutation of 1, 2, 3.} \end{cases} \quad (7.66b)$$

Likewise, the determinant of the transformation matrix takes the form

$$\det(\Lambda^a_{\bar{a}}) = \frac{\partial \xi}{\partial \bar{\xi}} = \frac{\partial(\xi^1, \xi^2, \xi^3)}{\partial(\xi^{\bar{1}}, \xi^{\bar{2}}, \xi^{\bar{3}})} = \epsilon_{abc} \Lambda^a_{\bar{1}} \Lambda^b_{\bar{2}} \Lambda^c_{\bar{3}}. \quad (7.67)$$

### 7.6.2 Further identities satisfied by the determinant

The following identity in two dimensions can be readily verified through enumeration

$$\epsilon_{ab} \Lambda^a_{\bar{a}} \Lambda^b_{\bar{b}} = \epsilon_{\bar{a}\bar{b}} \det(\Lambda^a_{\bar{a}}), \quad (7.68)$$

which follows directly from the definition of the determinant and can be explicitly verified so long as we assume the permutation symbol  $\epsilon_{\bar{a}\bar{b}}$  is numerically identical to  $\epsilon_{ab}$ . Now contract both sides of this relation with  $\epsilon^{\bar{a}\bar{b}}$  to isolate the determinant

$$\frac{1}{2} \epsilon^{\bar{a}\bar{b}} \epsilon_{ab} \Lambda^a_{\bar{a}} \Lambda^b_{\bar{b}} = \det(\Lambda^a_{\bar{a}}), \quad (7.69)$$

where we used

$$\epsilon^{\bar{a}\bar{b}} \epsilon_{ab} = \epsilon^{\bar{1}\bar{2}} \epsilon_{12} + \epsilon^{\bar{2}\bar{1}} \epsilon_{21} = 2. \quad (7.70)$$

The three dimensional version takes the form

$$\epsilon_{abc} \Lambda^a_{\bar{a}} \Lambda^b_{\bar{b}} \Lambda^c_{\bar{c}} = \epsilon_{\bar{a}\bar{b}\bar{c}} \det(\Lambda^a_{\bar{a}}), \quad (7.71)$$

so that

$$\frac{1}{3!} \epsilon^{\bar{a}\bar{b}\bar{c}} \epsilon_{abc} \Lambda^a_{\bar{a}} \Lambda^b_{\bar{b}} \Lambda^c_{\bar{c}} = \det(\Lambda^a_{\bar{a}}). \quad (7.72)$$

## 7.7 The Levi-Civita tensor and the volume element

The metric tensor introduced in Section 7.1 provides a means to measure distance between two points. The Levi-Civita tensor allows us to compute volumes (or areas for two dimensional manifolds). We make particular use of this tensor to compute the volume element used for integration. This section generalizes the Cartesian coordinate discussion provided in Section 1.5.3.

### 7.7.1 General coordinate representation of the Levi-Civita tensor

The relations (7.68) and (7.71) indicate that the permutation symbol *does not* transform as the components to a second order covariant tensor, unless the determinant of the transformation is unity. Unit determinants occur for special transformations, such as rotations (i.e., Cartesian to Cartesian coordinate transformation as in Chapter 1) and the identity transformation. Indeed, we have already noted that the permutation symbol has the same representation regardless the coordinate choice. As we now show, the permutation symbol is the Cartesian coordinate representation of the Levi-Civita tensor.

The above relations for the determinant motivate us to introduce the general coordinate form of the *Levi-Civita tensor*

$$\varepsilon_{abc} = \sqrt{\det(\mathcal{G})} \epsilon_{abc}. \quad (7.73)$$

We highlight the distinct symbols in this definition, with  $\varepsilon$  the Levi-Civita tensor and  $\epsilon$  the permutation symbol. By construction, the components to the Levi-Civita tensor transform as

$$\Lambda^a_{\bar{a}} \Lambda^b_{\bar{b}} \Lambda^c_{\bar{c}} \varepsilon_{abc} = \Lambda^a_{\bar{a}} \Lambda^b_{\bar{b}} \Lambda^c_{\bar{c}} \sqrt{\det(\mathcal{G})} \epsilon_{abc} \quad (7.74a)$$

$$= \sqrt{\det(\mathcal{G})} \epsilon_{\bar{a}\bar{b}\bar{c}} \det(\Lambda^a_{\bar{a}}) \quad (7.74b)$$

$$= \sqrt{\det(\mathcal{G})} \epsilon_{\bar{a}\bar{b}\bar{c}} \quad (7.74c)$$

$$= \varepsilon_{\bar{a}\bar{b}\bar{c}}, \quad (7.74d)$$

where equations (7.60) and (7.68) were used. Therefore,  $\varepsilon_{abc}$  transforms as components to a third order covariant tensor. Likewise,

$$\varepsilon^{abc} = \frac{\epsilon^{abc}}{\sqrt{\det(\mathcal{G})}} \quad (7.75)$$

transforms as the components to a third order contravariant tensor. These transformation rules allow us to identify  $\varepsilon$  as a tensor rather than just a combination of numbers.

### 7.7.2 The Levi-Civita tensor and the volume element

As a third order tensor, the Levi-Civita tensor takes three vectors as its argument. In particular, for three infinitesimal vectors we have

$$\varepsilon(\vec{e}_1 d\xi^1, \vec{e}_2 d\xi^2, \vec{e}_3 d\xi^3) = d\xi^1 d\xi^2 d\xi^3 \varepsilon(\vec{e}_1, \vec{e}_2, \vec{e}_3) \quad (7.76a)$$

$$= d\xi^1 d\xi^2 d\xi^3 \varepsilon_{123} \quad (7.76b)$$

$$= d\xi^1 d\xi^2 d\xi^3 \sqrt{\det(Q)} \epsilon_{123} \quad (7.76c)$$

$$= dV, \quad (7.76d)$$

where we used equation (7.61) for the final step. This result means that geometrically, the Levi-Civita tensor measures the volume defined by three vectors

$$\varepsilon(\vec{A}, \vec{B}, \vec{C}) = \text{volume}(\vec{A}, \vec{B}, \vec{C}). \quad (7.77)$$

This interpretation accords with the Cartesian coordinate discussion of the Levi-Civita tensor in Section 1.5.3.

## 7.8 Vector cross product

The vector cross product of two Cartesian basis vectors yields the third, so that

$$\hat{x} \times \hat{y} = \hat{z} \quad \text{and cyclic permutations.} \quad (7.78)$$

The coordinate invariant generalization of this relation is given by

$$\vec{e}_a \times \vec{e}_b \equiv \varepsilon_{abc} \tilde{e}^c. \quad (7.79)$$

That is, the vector cross product of two vectors leads to a one-form. We are thus led to the general coordinate expression for the vector cross product of two arbitrary vectors

$$\vec{P} \times \vec{Q} = P^a Q^b \vec{e}_a \times \vec{e}_b \quad (7.80a)$$

$$= P^a Q^b \varepsilon_{abc} \tilde{e}^c. \quad (7.80b)$$

## 7.9 Coordinate transformation of partial derivatives

Throughout this book, the background space is Euclidean and time is universal. We are thus concerned with space tensors rather than the space-time tensors of special and general relativity. Nonetheless, our description of points in space generally makes use of curved surfaces that are time dependent. Curved surfaces motivate the use of general tensors. Time dependence motivates a space-time formulation (Section 6.5.4) for the purpose of transforming the partial time derivative operator. In this section we establish some properties of the space-time transformation matrix and then exhibit the transformation of space and time partial time derivatives. We have further use of a space-time formulation in Sections 12.6 and 12.7, also for considering the transformation of partial derivatives.

### 7.9.1 The space-time transformation matrix

As discussed in Section 7.1.4, transformations between coordinate representations are enabled by the transformation matrix built from partial derivatives of the coordinate transformations.

The transformation matrix with a universal Newtonian time plus spatial coordinates (that are functions of space and time) takes on the form

$$\Lambda^{\alpha}_{\bar{\alpha}} = \frac{\partial \xi^{\alpha}}{\partial \xi^{\bar{\alpha}}} = \begin{bmatrix} \frac{\partial \xi^0}{\partial \xi^0} & \frac{\partial \xi^0}{\partial \xi^1} & \frac{\partial \xi^0}{\partial \xi^2} & \frac{\partial \xi^0}{\partial \xi^3} \\ \frac{\partial \xi^1}{\partial \xi^0} & \frac{\partial \xi^1}{\partial \xi^1} & \frac{\partial \xi^1}{\partial \xi^2} & \frac{\partial \xi^1}{\partial \xi^3} \\ \frac{\partial \xi^2}{\partial \xi^0} & \frac{\partial \xi^2}{\partial \xi^1} & \frac{\partial \xi^2}{\partial \xi^2} & \frac{\partial \xi^2}{\partial \xi^3} \\ \frac{\partial \xi^3}{\partial \xi^0} & \frac{\partial \xi^3}{\partial \xi^1} & \frac{\partial \xi^3}{\partial \xi^2} & \frac{\partial \xi^3}{\partial \xi^3} \\ \frac{\partial \xi^0}{\partial \xi^0} & \frac{\partial \xi^0}{\partial \xi^1} & \frac{\partial \xi^0}{\partial \xi^2} & \frac{\partial \xi^0}{\partial \xi^3} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ \frac{\partial \xi^1}{\partial \xi^0} & \frac{\partial \xi^1}{\partial \xi^1} & \frac{\partial \xi^1}{\partial \xi^2} & \frac{\partial \xi^1}{\partial \xi^3} \\ \frac{\partial \xi^2}{\partial \xi^0} & \frac{\partial \xi^2}{\partial \xi^1} & \frac{\partial \xi^2}{\partial \xi^2} & \frac{\partial \xi^2}{\partial \xi^3} \\ \frac{\partial \xi^3}{\partial \xi^0} & \frac{\partial \xi^3}{\partial \xi^1} & \frac{\partial \xi^3}{\partial \xi^2} & \frac{\partial \xi^3}{\partial \xi^3} \\ \frac{\partial \xi^0}{\partial \xi^0} & \frac{\partial \xi^0}{\partial \xi^1} & \frac{\partial \xi^0}{\partial \xi^2} & \frac{\partial \xi^0}{\partial \xi^3} \end{bmatrix}. \quad (7.81)$$

The final equality made use of our assumption that  $\xi^0 = \xi^0$  since the time coordinate remains universal. Hence, when computing  $\partial \xi^0 / \partial \xi^{\bar{\alpha}}$  we keep  $\xi^0$  fixed so that the derivative vanishes as in the specific case of

$$\left[ \frac{\partial \xi^0}{\partial \xi^1} \right]_{\xi^0, \xi^2, \xi^3} = \left[ \frac{\partial \xi^0}{\partial \xi^1} \right]_{\xi^0, \xi^2, \xi^3} = 0. \quad (7.82)$$

Zero elements in the first row of the transformation matrix (7.81) reveals that time is not a function of space

$$\frac{\partial \xi^0}{\partial \xi^{\bar{\alpha}}} = 0. \quad (7.83)$$

In contrast, nonzero elements in the first column indicate that our description of space is a function of time

$$\frac{\partial \xi^a}{\partial \xi^0} \neq 0. \quad (7.84)$$

We see the same overall structure in the inverse space-time transformation matrix

$$\Lambda^{\bar{\alpha}}_{\alpha} = \frac{\partial \xi^{\bar{\alpha}}}{\partial \xi^{\alpha}} = \begin{bmatrix} \frac{\partial \xi^0}{\partial \xi^0} & \frac{\partial \xi^0}{\partial \xi^1} & \frac{\partial \xi^0}{\partial \xi^2} & \frac{\partial \xi^0}{\partial \xi^3} \\ \frac{\partial \xi^1}{\partial \xi^0} & \frac{\partial \xi^1}{\partial \xi^1} & \frac{\partial \xi^1}{\partial \xi^2} & \frac{\partial \xi^1}{\partial \xi^3} \\ \frac{\partial \xi^2}{\partial \xi^0} & \frac{\partial \xi^2}{\partial \xi^1} & \frac{\partial \xi^2}{\partial \xi^2} & \frac{\partial \xi^2}{\partial \xi^3} \\ \frac{\partial \xi^3}{\partial \xi^0} & \frac{\partial \xi^3}{\partial \xi^1} & \frac{\partial \xi^3}{\partial \xi^2} & \frac{\partial \xi^3}{\partial \xi^3} \\ \frac{\partial \xi^0}{\partial \xi^0} & \frac{\partial \xi^0}{\partial \xi^1} & \frac{\partial \xi^0}{\partial \xi^2} & \frac{\partial \xi^0}{\partial \xi^3} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ \frac{\partial \xi^1}{\partial \xi^0} & \frac{\partial \xi^1}{\partial \xi^1} & \frac{\partial \xi^1}{\partial \xi^2} & \frac{\partial \xi^1}{\partial \xi^3} \\ \frac{\partial \xi^2}{\partial \xi^0} & \frac{\partial \xi^2}{\partial \xi^1} & \frac{\partial \xi^2}{\partial \xi^2} & \frac{\partial \xi^2}{\partial \xi^3} \\ \frac{\partial \xi^3}{\partial \xi^0} & \frac{\partial \xi^3}{\partial \xi^1} & \frac{\partial \xi^3}{\partial \xi^2} & \frac{\partial \xi^3}{\partial \xi^3} \\ \frac{\partial \xi^0}{\partial \xi^0} & \frac{\partial \xi^0}{\partial \xi^1} & \frac{\partial \xi^0}{\partial \xi^2} & \frac{\partial \xi^0}{\partial \xi^3} \end{bmatrix}. \quad (7.85)$$

## 7.9.2 Determinant of the transformation matrix

The determinant of the space-time transformation and its inverse remains identical to the determinant of their purely space portions

$$\det(\Lambda^{\alpha}_{\bar{\alpha}}) = \det(\Lambda^a_{\bar{a}}) \quad \text{and} \quad \det(\Lambda^{\bar{\alpha}}_{\alpha}) = \det(\Lambda^{\bar{a}}_a), \quad (7.86)$$

which follows since the first row in both transformations has only a single non-zero value,  $\Lambda^0_{\bar{0}} = 1$  and  $\Lambda^{\bar{0}}_0 = 1$ . Hence, the relations developed in Sections 7.5 and 7.6 for the volume element and Jacobian of transformation remain unchanged when adding the universal time coordinate.

### 7.9.3 Multiplying the transformation matrix and its inverse

We here verify that the transformation matrix (7.81) indeed has its inverse given by (7.85). For this purpose we must prove that

$$\delta_{\beta}^{\alpha} = \Lambda_{\beta}^{\alpha} \Lambda_{\beta}^{\bar{\beta}} \quad \text{and} \quad \delta_{\bar{\beta}}^{\bar{\alpha}} = \Lambda_{\bar{\beta}}^{\bar{\alpha}} \Lambda_{\bar{\beta}}^{\beta}, \quad (7.87)$$

where  $\delta_{\beta}^{\alpha}$  and  $\delta_{\bar{\beta}}^{\bar{\alpha}}$  are components to the identity tensor. The proof relies on writing the space-time coordinate transformation as a composite function

$$\xi^{\bar{\alpha}} = \xi^{\bar{\alpha}}(\xi^{\alpha}) = \xi^{\bar{\alpha}}[\xi^{\alpha}(\xi^{\bar{\beta}})]. \quad (7.88)$$

Taking partial derivatives and using the chain rule renders

$$\delta_{\bar{\beta}}^{\bar{\alpha}} = \frac{\partial \xi^{\bar{\alpha}}}{\partial \xi^{\bar{\beta}}} = \frac{\partial \xi^{\bar{\alpha}}}{\partial \xi^{\alpha}} \frac{\partial \xi^{\alpha}}{\partial \xi^{\bar{\beta}}} = \Lambda_{\alpha}^{\bar{\alpha}} \Lambda_{\beta}^{\alpha} \quad \text{and} \quad \delta_{\beta}^{\alpha} = \frac{\partial \xi^{\alpha}}{\partial \xi^{\beta}} = \frac{\partial \xi^{\alpha}}{\partial \xi^{\bar{\alpha}}} \frac{\partial \xi^{\bar{\alpha}}}{\partial \xi^{\beta}} = \Lambda_{\bar{\alpha}}^{\alpha} \Lambda_{\beta}^{\bar{\alpha}}. \quad (7.89)$$

Furthermore, the space subcomponents decouple from time, which can be seen by considering a few representative cases

$$1 = \delta_0^0 = \Lambda_{\alpha}^0 \Lambda_{\alpha}^{\bar{\alpha}}_0 = \Lambda_{\bar{\alpha}}^0 \Lambda_{\alpha}^{\bar{\alpha}}_0 \quad (7.90a)$$

$$1 = \delta_1^1 = \Lambda_{\alpha}^1 \Lambda_{\alpha}^{\bar{\alpha}}_1 = \Lambda_{\bar{\alpha}}^1 \Lambda_{\alpha}^{\bar{\alpha}}_1 \quad (7.90b)$$

$$0 = \delta_1^0 = \Lambda_{\alpha}^0 \Lambda_{\alpha}^{\bar{\alpha}}_1 = \Lambda_{\bar{\alpha}}^0 \Lambda_{\alpha}^{\bar{\alpha}}_1 \quad (7.90c)$$

$$0 = \delta_2^1 = \Lambda_{\alpha}^1 \Lambda_{\alpha}^{\bar{\alpha}}_2 = \Lambda_{\bar{\alpha}}^1 \Lambda_{\alpha}^{\bar{\alpha}}_2. \quad (7.90d)$$

Consequently, the spatial components satisfy

$$\delta_b^a = \Lambda_{\bar{b}}^a \Lambda_{\bar{b}}^{\bar{b}} \quad \text{and} \quad \delta_{\bar{b}}^{\bar{a}} = \Lambda_{\bar{b}}^{\bar{a}} \Lambda_{\bar{b}}^b, \quad (7.91)$$

which allows for a splitting of the spatial components from the time component.

### 7.9.4 Transformation of space and time partial derivatives

Application of the chain rule leads to the transformation of the partial derivative operator

$$\partial_{\bar{\alpha}} = \frac{\partial}{\partial \xi^{\bar{\alpha}}} = \frac{\partial \xi^{\alpha}}{\partial \xi^{\bar{\alpha}}} \frac{\partial}{\partial \xi^{\alpha}} = \Lambda_{\bar{\alpha}}^{\alpha} \partial_{\alpha}. \quad (7.92)$$

Extracting the time and space components from the transformation matrix (7.81) yields

$$\partial_{\bar{0}} = \Lambda_{\bar{0}}^{\alpha} \partial_{\alpha} = \partial_0 + \Lambda_{\bar{0}}^a \partial_a \quad (7.93a)$$

$$\partial_{\bar{a}} = \Lambda_{\bar{a}}^{\alpha} \partial_{\alpha} = \Lambda_{\bar{a}}^a \partial_a. \quad (7.93b)$$

Notably, the time derivative operator in one coordinate system transforms into both space and time derivative operators in the new coordinate system. We expect this result since time changes in one coordinate system are computed with its spatial coordinates held fixed, but these coordinates are generally moving with respect to the other coordinates. In contrast, the spatial components to the partial derivative operator transform among just the other spatial components; there is no mixing with the time derivative operator. This property of the spatial derivative operator follows from the use of universal Newtonian time. It allows us to focus on space tensors in the following sections.

## 7.10 Covariant derivative of a scalar

We now return to a focus on space tensor analysis by considering the contraction of spatial components to the partial derivative operator with the basis of one-forms. This contraction renders the geometric expression of the gradient operator acting on a scalar

$$\text{grad}(\psi) = \nabla\psi = \tilde{e}^a \partial_a \psi = \tilde{e}^{\bar{a}} \partial_{\bar{a}} \psi. \quad (7.94)$$

From this expression we define the *covariant derivative operator*

$$\nabla = \tilde{e}^a \partial_a \quad (7.95)$$

so that we refer to equation (7.94) as either the gradient acting on a scalar or the covariant derivative acting on a scalar.

## 7.11 Covariant derivative of a vector

The covariant derivative operator can act on a vector, in which case we consider  $\nabla \vec{F}$ . To perform calculations requires us to unpack the manifestly covariant expression  $\nabla \vec{F}$  by introducing a coordinate representation

$$\nabla \vec{F} = (\tilde{e}^b \partial_b) (F^a \vec{e}_a). \quad (7.96)$$

### 7.11.1 Derivative of a vector

The chain rule leads to the expression for the partial derivative operator acting on a vector field

$$\partial_b \vec{F} = \partial_b (\vec{e}_a F^a) \quad \text{coordinate representation of the vector } \vec{F} \quad (7.97a)$$

$$= (\partial_b F^a) \vec{e}_a + F^a \partial_b \vec{e}_a \quad \text{chain rule} \quad (7.97b)$$

$$= (\partial_b F^a) \vec{e}_a + F^a \Gamma_{ba}^c \vec{e}_c \quad \text{define Christoffel symbols} \quad (7.97c)$$

$$= (\partial_b F^a + F^c \Gamma_{bc}^a) \vec{e}_a \quad \text{reorganize} \quad (7.97d)$$

$$= (\nabla_b F^a) \vec{e}_a \quad \text{define covariant derivative acting on vector component.} \quad (7.97e)$$

In the third equality we introduced the *Christoffel symbols*

$$\partial_b \vec{e}_a = \Gamma_{ba}^c \vec{e}_c. \quad (7.98)$$

The Christoffel symbols carry information about the partial derivatives of the basis vectors. They vanish in Cartesian coordinates yet are generally nonzero. In the final equality we introduced components to the covariant derivative acting on the vector components

$$\nabla_b F^a = \partial_b F^a + \Gamma_{bc}^a F^c. \quad (7.99)$$

Contracting  $\partial_b \vec{F}$  with the basis one-form  $\tilde{e}^b$  leads to the coordinate invariant expression for the covariant derivative of a vector field

$$\nabla \vec{F} = (\tilde{e}^b \partial_b) \vec{F} = (\tilde{e}^b \nabla_b F^a) \vec{e}_a. \quad (7.100)$$

### 7.11.2 An alternative derivation

A heuristic explanation of these ideas follows by applying the elementary calculus notions to a vector field  $\vec{F}$  as represented by arbitrary coordinates  $\xi^a$ , in which case

$$\partial_b \vec{F} = \lim_{\Delta \rightarrow 0} \frac{\vec{F}(\vec{P} + \Delta \vec{e}_b) - \vec{F}(\vec{P})}{\Delta}, \quad (7.101)$$

where  $\vec{P} = \vec{e}_a \xi^a$  is the position vector for an arbitrary point and  $\vec{e}_b$  specifies the direction for computing the partial derivative. The basis vectors  $\vec{e}_a$  are spatially independent for Cartesian coordinates, so that the derivative of a vector is computed merely by taking the derivative of each Cartesian component

$$\partial_b \vec{F} = (\partial_b F^a) \vec{e}_a \quad \text{Cartesian coordinates.} \quad (7.102)$$

However, for general coordinates both the vector components and the basis vectors are spatially dependent, in which case

$$\vec{F}(\vec{P} + \Delta \vec{e}_b) - \vec{F}(\vec{P}) = [F^a + \Delta \partial_b F^b] [\vec{e}_a + \Delta \partial_b \vec{e}_a] - F^a \vec{e}_a \quad (7.103a)$$

$$= \Delta \partial_b (F^a \vec{e}_a) + \mathcal{O}(\Delta^2). \quad (7.103b)$$

This is the same result as found in the first step of the chain rule used in equation (7.97a). Following through that derivation then leads to the same coordinate expression for the covariant derivative acting on a vector field.

### 7.11.3 Christoffel symbols as the metric connection

Recall from elementary calculus that the derivative of a function is computed by comparing the function at two points in space, dividing by the distance between those points, and taking the limit as the points get infinitesimally close. This operation is well defined for scalar fields on arbitrary manifolds. However, it is problematic for vectors since the vectors live on distinct tangent spaces and so cannot be directly compared. For example, how do we compare two vectors at distinct points on a sphere? To do so we must provide a method to move one vector to the position of the other before comparing. As seen through the above discussion of covariant derivative of a vector, the Christoffel symbols provide the means to move vectors. Namely, they connect the two vectors by carrying information about how the basis vectors change in space. It is for this reason that some refer to the Christoffel symbols as the *metric connection*.

There is a distinct coordinate dependence of Christoffel symbols. For example, the Christoffel symbols all vanish in Euclidean space when using Cartesian coordinates whereas they are nonzero with other coordinates. As discussed in Section 6.1, a tensor that vanishes in one coordinate system remains zero for all coordinate systems. We thus conclude that the Christoffel symbols are *not* components to a tensor. Rather, they carry information regarding the partial derivatives of the coordinate basis vectors and as such they are fundamentally tied to a chosen coordinate system.

## 7.12 Covariant derivative of a one-form

The product of a one-form and a vector is a scalar. As seen in Section 7.10, the covariant derivative of a scalar field is given by the gradient operator

$$\nabla(\tilde{E} \cdot \vec{F}) = \tilde{e}^b \partial_b (E_a F^a). \quad (7.104)$$

Expanding the partial derivative yields

$$\partial_b(E_a F^a) = F^a \partial_b E_a + E_a \partial_b F^a \quad (7.105a)$$

$$= F^a \partial_b E_a + E_a (\nabla_b F^a - \Gamma_{bc}^a F^c) \quad (7.105b)$$

$$= F^a (\partial_b E_a - \Gamma_{ba}^c E_c) + E_a \nabla_b F^a \quad (7.105c)$$

$$\equiv F^a \nabla_b E_a + E_a \nabla_b F^a. \quad (7.105d)$$

The last equality defines the covariant derivative when acting on the components to a one form

$$\nabla_b E_a = \partial_b E_a - \Gamma_{ba}^c E_c, \quad (7.106)$$

which leads to the coordinate invariant expression for the covariant derivative of a one-form

$$\nabla \tilde{E} = (\tilde{e}^b \partial_b) \tilde{E} = (\tilde{e}^b \nabla_b E_a) \tilde{e}^a. \quad (7.107)$$

## 7.13 Covariant derivative of the metric tensor

When written in Cartesian coordinates, the covariant derivative of components to the metric tensor for Euclidean space vanishes,

$$\nabla g_{ab} = \nabla \delta_{ab} = 0, \quad (7.108)$$

because the Cartesian representation of the metric is the unit tensor  $\delta_{ab}$  so that all Christoffel symbols vanish. Previous results establish the tensorial nature of the covariant derivative. Hence,  $\nabla g_{ab} = 0$  is a valid result for *all* coordinates. This result is often called the *metricity* condition. It represents a self-consistency condition required for the manifolds considered in geophysical fluid mechanics.

## 7.14 Christoffel symbols in terms of the metric

We can develop an expression for the covariant derivative when acting on the components to a second order tensor. When applied to the metric tensor, its vanishing covariant derivative (equation (7.108)) then leads to the identity

$$0 = \nabla_c g_{ab} = \partial_c g_{ab} - \Gamma_{ca}^d g_{db} - \Gamma_{cb}^d g_{ad}. \quad (7.109)$$

We can solve this equation for the Christoffel symbols

$$\Gamma_{ab}^c = \frac{1}{2} g^{cd} (\partial_b g_{da} + \partial_a g_{db} - \partial_d g_{ab}). \quad (7.110)$$

This expression exhibits the symmetry property of the lower two indices on the Christoffel symbols

$$\Gamma_{ab}^c = \Gamma_{ba}^c. \quad (7.111)$$

## 7.15 Covariant divergence of a vector

The covariant divergence of the components to a vector results in a scalar

$$\nabla_a F^a = \partial_a F^a + \Gamma_{ab}^a F^b. \quad (7.112)$$

We now bring this expression into a form more convenient for practical calculations.

### 7.15.1 Contraction of the Christoffel symbols

Expression (7.110) for the Christoffel symbols yields the contraction

$$\Gamma_{ab}^a = \frac{1}{2} g^{ad} (\partial_b g_{da} + \partial_a g_{db} - \partial_d g_{ab}) = \frac{1}{2} g^{ad} \partial_b g_{ad} \quad (7.113)$$

where symmetry of the metric tensor and its inverse was used.

### 7.15.2 Exponential of the determinant

For any symmetric positive definite matrix such as the metric tensor we can write

$$\det(A) = e^{\ln \det(A)} \quad \text{simple identity} \quad (7.114a)$$

$$= e^{\ln(\Pi_i \Lambda_i)} \quad \text{determinant related to product of eigenvalues} \quad (7.114b)$$

$$= e^{\Sigma_i \ln \Lambda_i} \quad \text{simple identity} \quad (7.114c)$$

$$= e^{\text{Tr}(\ln A)} \quad \text{sum of eigenvalues related to trace of matrix.} \quad (7.114d)$$

Each of these identities is trivial to verify using a set of coordinates in which the matrix is diagonal. For any symmetric and positive definite matrix, such a set of coordinates always exists, in which case

$$\partial_c \ln \det(A) = \partial_c [\text{Tr}(\ln A)] = \text{Tr}(\partial_c \ln A) = \text{Tr}(A^{-1} \partial_c A). \quad (7.115)$$

With  $A$  now set equal to the metric tensor  $\mathcal{G}$  with components  $g_{ab}$ , this result yields

$$\partial_c \ln \det(\mathcal{G}) = g^{ab} \partial_c g_{ab} \quad (7.116)$$

which in turn yields for the contracted Christoffel symbol

$$\Gamma_{ac}^a = \partial_c \ln \sqrt{\det(\mathcal{G})}. \quad (7.117)$$

This result brings the covariant divergence of a vector to the form

$$\nabla_a F^a = \partial_a F^a + F^a \partial_a \ln \sqrt{\det(\mathcal{G})} = \frac{1}{\sqrt{\mathcal{G}}} \partial_a [\sqrt{\mathcal{G}} F^a]. \quad (7.118)$$

This is a very convenient result since it only requires partial derivatives in the chosen coordinate system, with all of the coordinate dependent properties summarized by  $\sqrt{\det(\mathcal{G})}$ .

## 7.16 Covariant Laplacian of a scalar

Making use of equation (7.118) with

$$F^a = g^{ab} \partial_b \psi \quad (7.119)$$

leads to the covariant Laplacian of a scalar field

$$\nabla_a (g^{ab} \partial_b \psi) = \frac{1}{\sqrt{\mathcal{G}}} \partial_a [\sqrt{\mathcal{G}} g^{ab} \partial_b \psi]. \quad (7.120)$$

This expression is fundamental to the evolution of scalar fields under the impacts from diffusion (Chapter 46).

## 7.17 Covariant curl of a vector

The Levi-Civita tensor

$$\varepsilon_{abc} = \sqrt{\det(\mathcal{G})} \epsilon_{abc} \quad (7.121)$$

from Section 7.7 is useful for generalizing the curl operation from Cartesian coordinates in Euclidean space to arbitrary coordinates on a curved manifold. Consequently, we define the curl according to the coordinate invariant expression

$$\text{curl}(\vec{F}) = \vec{e}_a \varepsilon^{abc} (\nabla_b F_c) = \vec{e}^a \varepsilon_{abc} (\nabla^b F^c). \quad (7.122)$$

This expression simplifies by making use of equation (7.106) for the covariant derivative  $\nabla_b F_c = \partial_b F_c - \Gamma_{cb}^a F_a$ . Conveniently, the contraction  $\varepsilon^{abc} \Gamma_{cb}^a$  vanishes identically since  $\varepsilon^{abc} = -\varepsilon^{acb}$  whereas  $\Gamma_{cb}^a = \Gamma_{bc}^a$ . Hence, we are left with a general expression for the covariant curl that involves just the partial derivatives

$$\text{curl}(\vec{F}) = \vec{e}_a \varepsilon^{abc} (\partial_b F_c) = \vec{e}_a \varepsilon^{abc} [\partial_b (g_{cd} F^d)]. \quad (7.123)$$

The second equality made use of the identity  $F_c = g_{cd} F^d$ .

## 7.18 Gauss's divergence theorem

The integral theorems from Cartesian vector analysis transform in a straightforward manner to arbitrary coordinates in arbitrary smooth and oriented spaces. An easy way to prove the theorems is to invoke the ideas of general coordinate invariance from Section 6.1, in which the integral theorems are written in a tensorially proper manner with partial derivatives changed to covariant derivatives. The divergence theorem offers a particularly simple example. For this purpose, we make use of the volume element (7.61)

$$dV = \sqrt{\det(\mathcal{G})} d\xi^1 d\xi^2 d\xi^3, \quad (7.124)$$

multiplied by the covariant divergence (7.118). Hence, the volume integral of the divergence is given by

$$\int_{\mathcal{R}} (\nabla_a F^a) dV = \int_{\mathcal{R}} \partial_a [\sqrt{\det(\mathcal{G})} F^a] d\xi^1 d\xi^2 d\xi^3 = \oint_{\partial\mathcal{R}} F^a \hat{n}_a d\mathcal{S}, \quad (7.125)$$

where  $\hat{n}$  is the outward normal one-form for the boundary,  $\partial\mathcal{R}$ ,  $\hat{n}_a$  are its covariant components, and  $d\mathcal{S}$  is the invariant area element on the boundary.

## 7.19 Stokes' theorem

The Cartesian form of Stokes' Theorem from Section 2.6 is generalized in a manner similar to the divergence theorem

$$\oint_{\partial\mathcal{S}} \vec{F} \cdot d\vec{x} = \int_{\mathcal{S}} \text{curl}(\vec{F}) \cdot \hat{n} d\mathcal{S}, \quad (7.126)$$

where  $d\vec{x}$  is the vector line element along the path and  $\partial\mathcal{S}$  is the closed path defining the boundary to a simply connected two-dimensional surface  $\mathcal{S}$ . For the circulation on the left hand side we

have

$$\vec{F} \cdot d\vec{x} = F^a \vec{e}_a \cdot \vec{e}_b dx^b = F_b dx^b = F_{\bar{b}} d\xi^{\bar{b}}. \quad (7.127)$$

For the curl on the right hand side we have

$$\text{curl}(\vec{F}) \cdot \hat{\mathbf{n}} = \varepsilon^{abc} (\partial_b F_c) \vec{e}_a \cdot \hat{\mathbf{n}} = \varepsilon^{abc} (\partial_b F_c) \hat{n}_a = \varepsilon^{\bar{a}\bar{b}\bar{c}} (\partial_{\bar{b}} F_{\bar{c}}) \hat{n}_{\bar{a}}, \quad (7.128)$$

thus leading to the expression of Stokes' theorem in arbitrary coordinates

$$\oint_{\partial\mathcal{S}} F_{\bar{b}} d\xi^{\bar{b}} = \int_{\mathcal{S}} \varepsilon^{\bar{a}\bar{b}\bar{c}} (\partial_{\bar{b}} F_{\bar{c}}) \hat{n}_{\bar{a}} d\mathcal{S}. \quad (7.129)$$



# Chapter 8

## Orthogonal coordinates

### READER'S GUIDE TO THIS CHAPTER

This chapter provides a compendium of mathematical results for Cartesian, spherical, and cylindrical coordinates, thus providing explicit examples of the general tensor analysis machinery from Chapter 7. These coordinates are all time independent and orthogonal. Hence, they are simpler than the non-orthogonal generalized vertical coordinates detailed in Chapter 41.

8.1	Cartesian coordinates . . . . .	153
8.1.1	The basics . . . . .	154
8.1.2	Summary . . . . .	154
8.2	Spherical coordinates . . . . .	155
8.2.1	Cartesian and spherical transformation . . . . .	155
8.2.2	Basis vectors . . . . .	157
8.2.3	Basis one-forms . . . . .	157
8.2.4	Position and velocity . . . . .	157
8.2.5	Metric tensor . . . . .	158
8.2.6	Components of a vector field . . . . .	159
8.2.7	Differential operators . . . . .	159
8.2.8	Summary . . . . .	160
8.3	Cylindrical-polar coordinates . . . . .	160
8.3.1	Cartesian and cylindrical-polar transformation . . . . .	162
8.3.2	Basis vectors . . . . .	162
8.3.3	Basis one-forms . . . . .	162
8.3.4	Position and velocity . . . . .	163
8.3.5	Metric tensor . . . . .	163
8.3.6	Volume element and Levi-Civita tensor . . . . .	163
8.3.7	Vector cross product of basis vectors . . . . .	163
8.3.8	Components of a vector field . . . . .	164
8.3.9	Differential operators . . . . .	164
8.3.10	Summary . . . . .	165
8.4	General orthogonal coordinates . . . . .	165

### 8.1 Cartesian coordinates

Whenever developing a general tensor relation it is useful to check its validity by considering Cartesian coordinates, in which case we can make use of familiar rules from vector calculus. We

here summarize some results from our discussion of Cartesian tensors in Chapters 1 and 2.

### 8.1.1 The basics

We start by expressing the trajectory of a point through space in the following equivalent forms

$$\mathcal{P}(\tau) = \vec{e}_1 x(\tau) + \vec{e}_2 y(\tau) + \vec{e}_3 z(\tau) \quad (8.1a)$$

$$= \hat{\mathbf{x}} x(\tau) + \hat{\mathbf{y}} y(\tau) + \hat{\mathbf{z}} z(\tau) \quad (8.1b)$$

$$= \vec{x}(\tau) \quad (8.1c)$$

$$= \mathbf{x}(\tau), \quad (8.1d)$$

with the basis vectors written

$$\vec{e}_1 = \hat{\mathbf{x}} \quad \text{and} \quad \vec{e}_2 = \hat{\mathbf{y}} \quad \text{and} \quad \vec{e}_3 = \hat{\mathbf{z}}. \quad (8.2)$$

The boldface notation is used for the position vector in the final equality of equation (8.1d), with the boldface commonly used throughout this book. Notably, the orthogonal unit vectors for Cartesian coordinates are normalized so that

$$\vec{e}_1 \cdot \vec{e}_1 = \vec{e}_2 \cdot \vec{e}_2 = \vec{e}_3 \cdot \vec{e}_3 = 1. \quad (8.3)$$

Furthermore, the basis vectors are identical to the basis one-forms

$$\vec{e}_1 = \tilde{e}^1 = \hat{\mathbf{x}} \quad \text{and} \quad \vec{e}_2 = \tilde{e}^2 = \hat{\mathbf{y}} \quad \text{and} \quad \vec{e}_3 = \tilde{e}^3 = \hat{\mathbf{z}}. \quad (8.4)$$

Since the Cartesian basis vectors are independent of both space and time, we compute the coordinate representation of the velocity vector through taking the time derivative as

$$\vec{v}(\tau) = \mathbf{v}(\tau) = \frac{d\mathcal{P}}{d\tau} = \frac{d\mathbf{x}}{d\tau}, \quad (8.5)$$

which takes on the expanded expressions

$$\vec{v}(\tau) = \vec{e}_1 \frac{dx(\tau)}{d\tau} + \vec{e}_2 \frac{dy(\tau)}{d\tau} + \vec{e}_3 \frac{dz(\tau)}{d\tau} \quad (8.6a)$$

$$= \hat{\mathbf{x}} v^1(\tau) + \hat{\mathbf{y}} v^2(\tau) + \hat{\mathbf{z}} v^3(\tau). \quad (8.6b)$$

$$= \hat{\mathbf{x}} u(\tau) + \hat{\mathbf{y}} v(\tau) + \hat{\mathbf{z}} w(\tau). \quad (8.6c)$$

### 8.1.2 Summary

In Cartesian coordinates, mathematical operators and integral theorems take their familiar form from vector calculus. We here list the key ones in forms that are encountered throughout this

book.

$\mathbf{x} = (x^1, x^2, x^3) = (x, y, z)$	Cartesian coordinates	(8.7)
$\mathbf{F} = \hat{\mathbf{x}}F^1 + \hat{\mathbf{y}}F^2 + \hat{\mathbf{z}}F^3 = \hat{\mathbf{x}}F_1 + \hat{\mathbf{y}}F_2 + \hat{\mathbf{z}}F_3$	covariant = contravariant	(8.8)
$\frac{\partial}{\partial x^a} = \partial_a \text{ or } (\partial_x, \partial_y, \partial_z)$	partial derivative operator	(8.9)
$\nabla = \hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y + \hat{\mathbf{z}} \partial_z$	gradient operator	(8.10)
$\nabla_z = \hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y$	horizontal gradient operator	(8.11)
$\nabla \cdot \mathbf{F} = \partial_x F_x + \partial_y F_y + \partial_z F_z$	divergence of a vector	(8.12)
$\nabla_z \cdot \mathbf{F} = \partial_x F_x + \partial_y F_y$	horizontal divergence of a vector	(8.13)
$(\nabla \times \mathbf{F})_a = \epsilon_{abc} \partial_b F_c$	components to curl of a vector	(8.14)
$\nabla \cdot \nabla \psi = \nabla^2 \psi = (\partial_{xx} + \partial_{yy} + \partial_{zz}) \psi$	Laplacian of a scalar	(8.15)
$\int_{\mathcal{R}} \nabla \cdot \mathbf{F} dV = \oint_{\partial \mathcal{R}} \mathbf{F} \cdot \hat{\mathbf{n}} dS$	Gauss's divergence theorem	(8.16)
$\oint_{\partial S} \mathbf{F} \cdot d\mathbf{x} = \int_S (\nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}} dS.$	Stokes' theorem.	(8.17)

## 8.2 Spherical coordinates

We now consider spherical coordinates defined by Figure 8.1 and related to Cartesian coordinates through the transformation

$$x = r \cos \phi \cos \lambda \quad (8.18a)$$

$$y = r \cos \phi \sin \lambda \quad (8.18b)$$

$$z = r \sin \phi. \quad (8.18c)$$

The radial coordinate

$$r = |\mathbf{x}| = \sqrt{\mathbf{x} \cdot \mathbf{x}} = \sqrt{x^2 + y^2 + z^2} \quad (8.19)$$

measures the distance from the center of the sphere to the position of the point. The spherical angle coordinates

$$0 \leq \lambda \leq 2\pi \quad \text{longitude} \quad (8.20)$$

$$-\pi/2 \leq \phi \leq \pi/2 \quad \text{latitude} \quad (8.21)$$

specify the longitude, measuring the radians of the position east of the prime meridian, and latitude, measuring the radians north or south from the equator. To streamline notation in the following, we introduce the unbarred and barred labels for the Cartesian and spherical coordinates, respectively

$$(x, y, z) = (\xi^1, \xi^2, \xi^3) \equiv \xi^a \quad \text{and} \quad (\lambda, \phi, r) = (\bar{\xi}^1, \bar{\xi}^2, \bar{\xi}^3) \equiv \bar{\xi}^a. \quad (8.22)$$

### 8.2.1 Cartesian and spherical transformation

Following the general discussion in Section 7.1.4, we consider the infinitesimal distance along one of the Cartesian coordinate axes,  $d\xi^a$ . The chain rule allows us to relate this distance to those

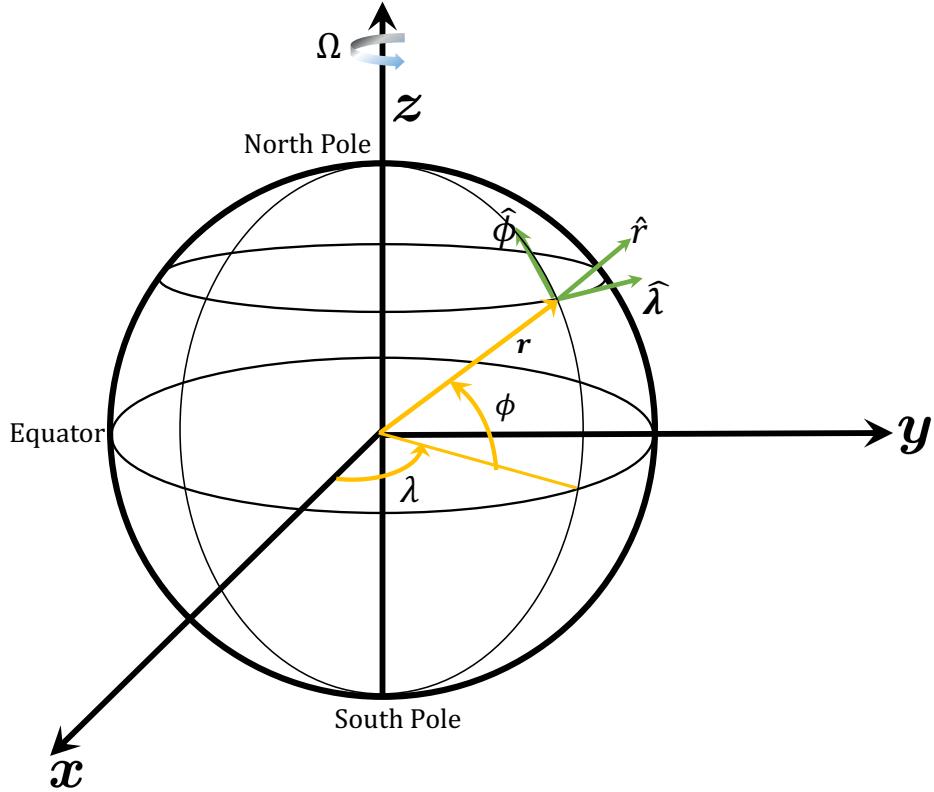


FIGURE 8.1: This schematic illustrates the geometry and notation for motion around a rotating sphere of radius  $R$ . For geophysical applications, the sphere rotates counter-clockwise when looking down from the north polar axis and it has an angular speed  $\Omega$ . The planetary Cartesian triad of orthonormal basis vectors,  $(\hat{x}, \hat{y}, \hat{z})$  points along the orthogonal axes and rotates with the sphere. The planetary spherical triad (also rotating with the sphere) of orthonormal basis vectors,  $(\hat{\lambda}, \hat{\phi}, \hat{r})$ , makes use of the longitudinal unit vector  $\hat{\lambda}$ , which points in the longitudinal direction (positive eastward), the latitudinal unit vector  $\hat{\phi}$ , which points in the latitudinal direction (positive northward) and the radial unit vector  $\hat{r}$ , which point in the radial direction (positive away from the center).

along the axes of the spherical coordinate system

$$d\xi^a = \frac{\partial \xi^a}{\partial \xi^{\bar{a}}} d\xi^{\bar{a}} = \Lambda_{\bar{a}}^a d\xi^{\bar{a}}. \quad (8.23)$$

The partial derivatives  $\partial \xi^a / \partial \xi^{\bar{a}}$  form components to the transformation matrix that transforms between coordinate representations. For the coordinate transformation (8.18a)-(8.18c), the transformation matrix is given by

$$\Lambda_{\bar{a}}^a = \begin{bmatrix} \partial \xi^1 / \partial \xi^{\bar{1}} & \partial \xi^1 / \partial \xi^{\bar{2}} & \partial \xi^1 / \partial \xi^{\bar{3}} \\ \partial \xi^2 / \partial \xi^{\bar{1}} & \partial \xi^2 / \partial \xi^{\bar{2}} & \partial \xi^2 / \partial \xi^{\bar{3}} \\ \partial \xi^3 / \partial \xi^{\bar{1}} & \partial \xi^3 / \partial \xi^{\bar{2}} & \partial \xi^3 / \partial \xi^{\bar{3}} \end{bmatrix} = \begin{bmatrix} -r \cos \phi \sin \lambda & -r \sin \phi \cos \lambda & \cos \phi \cos \lambda \\ r \cos \phi \cos \lambda & -r \sin \phi \sin \lambda & \cos \phi \sin \lambda \\ 0 & r \cos \phi & \sin \phi \end{bmatrix}. \quad (8.24)$$

The determinant of the transformation (Jacobian) is given by

$$\det(\Lambda_{\bar{a}}^a) = r^2 \cos \phi. \quad (8.25)$$

The Jacobian vanishes at the north and south poles ( $\phi = \pm\pi/2$ ), where the transformation is singular. Methods familiar from linear algebra render the inverse transformation matrix

$$\Lambda^{\bar{a}}_a = \frac{1}{r^2 \cos \phi} \begin{bmatrix} -r \sin \lambda & r \cos \lambda & 0 \\ -r \cos \phi \sin \phi \cos \lambda & -r \cos \phi \sin \phi \sin \lambda & r \cos^2 \phi \\ r^2 \cos^2 \phi \cos \lambda & r^2 \cos^2 \phi \sin \lambda & r^2 \cos \phi \sin \phi \end{bmatrix}. \quad (8.26)$$

### 8.2.2 Basis vectors

The spherical coordinate basis vectors,  $\vec{e}_{\bar{a}}$ , are related to the Cartesian coordinate basis vectors,  $\vec{e}_a$ , through the transformation

$$\vec{e}_{\bar{a}} = \Lambda^a_{\bar{a}} \vec{e}_a. \quad (8.27)$$

The transformation matrix (8.24) leads to

$$\vec{e}_\lambda = r \cos \phi (-\hat{x} \sin \lambda + \hat{y} \cos \lambda) \quad (8.28a)$$

$$\vec{e}_\phi = r (-\hat{x} \sin \phi \cos \lambda - \hat{y} \sin \phi \sin \lambda + \hat{z} \cos \phi) \quad (8.28b)$$

$$\vec{e}_r = \hat{x} \cos \phi \cos \lambda + \hat{y} \cos \phi \sin \lambda + \hat{z} \sin \phi. \quad (8.28c)$$

We can introduce the orthonormal unit vectors through

$$\vec{e}_\lambda = r \cos \phi \hat{\lambda} \quad \text{and} \quad \vec{e}_\phi = r \hat{\phi} \quad \text{and} \quad \vec{e}_r = \hat{r}, \quad (8.29)$$

so that

$$\hat{\lambda} = -\hat{x} \sin \lambda + \hat{y} \cos \lambda \quad (8.30a)$$

$$\hat{\phi} = -\hat{x} \cos \lambda \sin \phi - \hat{y} \sin \lambda \sin \phi + \hat{z} \cos \phi \quad (8.30b)$$

$$\hat{r} = \hat{x} \cos \lambda \cos \phi + \hat{y} \sin \lambda \cos \phi + \hat{z} \sin \phi \quad (8.30c)$$

along with the inverse relations

$$\hat{x} = -\hat{\lambda} \sin \lambda - \hat{\phi} \cos \lambda \sin \phi + \hat{r} \cos \lambda \cos \phi \quad (8.31a)$$

$$\hat{y} = \hat{\lambda} \cos \lambda - \hat{\phi} \sin \lambda \sin \phi + \hat{r} \sin \lambda \cos \phi \quad (8.31b)$$

$$\hat{z} = \hat{\phi} \cos \phi + \hat{r} \sin \phi. \quad (8.31c)$$

### 8.2.3 Basis one-forms

Since spherical coordinates are orthogonal, we can readily derive the one-form basis through inverting the vector basis

$$\tilde{e}^\lambda = (r \cos \phi)^{-1} \hat{\lambda} \quad \text{and} \quad \tilde{e}^\phi = r^{-1} \hat{\phi} \quad \text{and} \quad \tilde{e}^r = \hat{r}, \quad (8.32)$$

which satisfy the bi-orthogonality relation with the basis vectors (Section 7.2.2)

$$\tilde{e}^{\bar{b}} \cdot \vec{e}_{\bar{a}} = \delta^{\bar{b}}_{\bar{a}}. \quad (8.33)$$

### 8.2.4 Position and velocity

In spherical coordinates, the position of a point is fully specified by the radial position

$$\mathcal{P}(\tau) = r \vec{e}_r = r \hat{r}. \quad (8.34)$$

The velocity requires all three spherical coordinates since the radial basis vector is a function of the angular positions, which are in turn functions of time. Use of the chain rule renders

$$\vec{v}(\tau) = \vec{v} \quad (8.35a)$$

$$= \frac{d\vec{v}}{d\tau} \quad (8.35b)$$

$$= \vec{e}_r \frac{dr}{d\tau} + r \frac{d\vec{e}_r}{d\tau} \quad (8.35c)$$

$$= \vec{e}_r \frac{dr}{d\tau} + r \frac{\partial \vec{e}_r}{\partial \lambda} \frac{d\lambda}{d\tau} + r \frac{\partial \vec{e}_r}{\partial \phi} \frac{d\phi}{d\tau} \quad (8.35d)$$

$$\equiv \vec{e}_r \frac{dr}{d\tau} + \vec{e}_\lambda \frac{d\lambda}{d\tau} + \vec{e}_\phi \frac{d\phi}{d\tau} \quad (8.35e)$$

$$= \vec{e}_r v^r + \vec{e}_\lambda v^\lambda + \vec{e}_\phi v^\phi. \quad (8.35f)$$

To reach this result we made use of the identities satisfied by the spherical basis vectors

$$\vec{e}_\lambda = r \frac{\partial \vec{e}_r}{\partial \lambda} \quad \text{and} \quad \vec{e}_\phi = r \frac{\partial \vec{e}_r}{\partial \phi}. \quad (8.36)$$

### 8.2.5 Metric tensor

The metric tensor for spherical coordinates takes on the diagonal form

$$g_{\bar{a}\bar{b}} = \vec{e}_{\bar{a}} \cdot \vec{e}_{\bar{b}} = \begin{bmatrix} (r \cos \phi)^2 & 0 & 0 \\ 0 & r^2 & 0 \\ 0 & 0 & 1 \end{bmatrix}, \quad (8.37)$$

as does the spherical representation of the inverse metric tensor

$$g^{\bar{a}\bar{b}} = \vec{e}^{\bar{a}} \cdot \vec{e}^{\bar{b}} = \begin{bmatrix} (r \cos \phi)^{-2} & 0 & 0 \\ 0 & r^{-2} & 0 \\ 0 & 0 & 1 \end{bmatrix}. \quad (8.38)$$

A diagonal metric tensor is a property of orthogonal coordinates.

### Volume element and Levi-Civita tensor

The square root of the determinant of the metric tensor written in spherical coordinates (from equation (8.37)) is given by

$$\sqrt{\det(\mathcal{G})} = r^2 \cos \phi \quad (8.39)$$

so that the volume element is

$$dV = r^2 \cos \phi dr d\lambda d\phi. \quad (8.40)$$

The covariant Levi-Civita tensor has the spherical representation

$$\epsilon_{\bar{a}\bar{b}\bar{c}} = (r^2 \cos \phi) \epsilon_{\bar{a}\bar{b}\bar{c}}, \quad (8.41)$$

where  $\epsilon_{\bar{a}\bar{b}\bar{c}}$  are components to the permutation symbol (i.e., the Cartesian components to the Levi-Civita tensor) from Section 1.4.1.

## Vector cross product of basis vectors

As a check on the formalism for cross products, let us verify the relation (7.79) for the vector cross product of two basis vectors using spherical coordinates

$$\vec{e}_{\bar{a}} \times \vec{e}_{\bar{b}} = \epsilon_{\bar{a}\bar{b}\bar{c}} \tilde{e}^{\bar{c}} \implies \vec{e}_{\bar{a}} \times \vec{e}_{\bar{b}} = (r^2 \cos \phi) \epsilon_{\bar{a}\bar{b}\bar{c}} \tilde{e}^{\bar{c}}. \quad (8.42)$$

Making use of the spherical coordinate basis vectors and one-forms renders

$$\vec{e}_r \times \vec{e}_{\lambda} = (r \cos \phi) (\hat{r} \times \hat{\lambda}) = (r \cos \phi) \hat{\phi} = (r^2 \cos \phi) \tilde{e}^{\phi} = \epsilon_{r\lambda\phi} \tilde{e}^{\phi} \quad (8.43a)$$

$$\vec{e}_{\lambda} \times \vec{e}_{\phi} = (r^2 \cos \phi) (\hat{\lambda} \times \hat{\phi}) = (r^2 \cos \phi) \hat{r} = (r^2 \cos \phi) \tilde{e}^r = \epsilon_{\lambda\phi r} \tilde{e}^r \quad (8.43b)$$

$$\vec{e}_{\phi} \times \vec{e}_r = r (\hat{\phi} \times \hat{r}) = r \hat{\lambda} = (r^2 \cos \phi) \tilde{e}^{\lambda} = \epsilon_{\phi r \lambda} \tilde{e}^{\lambda}. \quad (8.43c)$$

To reach these results we made use of the cross products for the spherical coordinate unit vectors

$$\hat{r} \times \hat{\lambda} = \hat{\phi} \quad \text{and} \quad \hat{\lambda} \times \hat{\phi} = \hat{r} \quad \text{and} \quad \hat{\phi} \times \hat{r} = \hat{\lambda}. \quad (8.44)$$

### 8.2.6 Components of a vector field

A vector field  $\vec{F}$  has Cartesian components,  $F^a$ , related to spherical components,  $F^{\bar{a}}$ , via the transformation matrix,  $F^{\bar{a}} = \Lambda^{\bar{a}}_a F^a$ . This transformation leads to

$$F^{\bar{1}} = (r \cos \phi)^{-1} [-F^x \sin \lambda + F^y \cos \lambda] \quad (8.45a)$$

$$F^{\bar{2}} = r^{-1} [-F^x \sin \phi \cos \lambda - F^y \sin \phi \sin \lambda + F^z \cos \phi] \quad (8.45b)$$

$$F^{\bar{3}} = F^x \cos \phi \cos \lambda + F^y \cos \phi \sin \lambda + F^z \sin \phi. \quad (8.45c)$$

Making use of the spherical unit vector (8.30a)-(8.30c) leads to the more tidy relations

$$(r \cos \phi) F^{\bar{1}} = \hat{\lambda} \cdot \mathbf{F} \quad (8.46a)$$

$$r F^{\bar{2}} = \hat{\phi} \cdot \mathbf{F} \quad (8.46b)$$

$$F^{\bar{3}} = \hat{r} \cdot \mathbf{F}, \quad (8.46c)$$

where  $\mathbf{F}$  is the Cartesian representation.

### 8.2.7 Differential operators

In spherical coordinates the gradient operator  $\nabla = \tilde{e}^a \partial_a$  takes on the form

$$\nabla = \hat{\lambda} (r \cos \phi)^{-1} \partial_{\lambda} + \hat{\phi} r^{-1} \partial_{\phi} + \hat{r} \partial_r \quad (8.47)$$

and the covariant divergence of a vector field is given by

$$\nabla_{\bar{a}} F^{\bar{a}} = (r^2 \cos \phi)^{-1} \partial_{\bar{a}} [r^2 \cos \phi F^{\bar{a}}] \quad (8.48a)$$

$$= (r^2 \cos \phi)^{-1} \left( \partial_{\lambda} [r^2 \cos \phi F^{\bar{1}}] + \partial_{\phi} [r^2 \cos \phi F^{\bar{2}}] + \partial_r [r^2 \cos \phi F^{\bar{3}}] \right) \quad (8.48b)$$

$$= \frac{1}{r \cos \phi} \frac{\partial (\hat{\lambda} \cdot \mathbf{F})}{\partial \lambda} + \frac{1}{r \cos \phi} \frac{\partial (\hat{\phi} \cdot \mathbf{F} \cos \phi)}{\partial \phi} + \frac{1}{r^2} \frac{\partial (\hat{r} \cdot \mathbf{F} r^2)}{\partial r}. \quad (8.48c)$$

The covariant Laplacian of a scalar,  $\nabla^2\psi = \nabla \cdot \nabla\psi$ , is given by

$$\nabla^2\psi = \nabla \cdot [\hat{\lambda}(r \cos \phi)^{-1} \partial_\lambda \psi + \hat{\phi} r^{-1} \partial_\phi \psi + \hat{r} \partial_r \psi] \quad (8.49a)$$

$$= \frac{1}{(r \cos \phi)^2} \frac{\partial^2 \psi}{\partial \lambda^2} + \frac{1}{r^2 \cos \phi} \frac{\partial}{\partial \phi} \left[ \cos \phi \frac{\partial \psi}{\partial \phi} \right] + \frac{1}{r^2} \frac{\partial}{\partial r} \left[ r^2 \frac{\partial \psi}{\partial r} \right]. \quad (8.49b)$$

The covariant curl (Section 7.17) takes the form

$$(\text{curl } \vec{F})^{\bar{1}} = (r^2 \cos \phi)^{-1} [\partial_\phi F^{\bar{3}} - \partial_r (r^2 F^{\bar{2}})] \quad (8.50a)$$

$$(\text{curl } \vec{F})^{\bar{2}} = (r^2 \cos \phi)^{-1} [\partial_r (r^2 \cos^2 \phi F^{\bar{1}}) - \partial_\lambda F^{\bar{3}}] \quad (8.50b)$$

$$(\text{curl } \vec{F})^{\bar{3}} = (r^2 \cos \phi)^{-1} [\partial_\lambda (r^2 F^{\bar{2}}) - \partial_\phi (r^2 \cos^2 \phi F^{\bar{1}})], \quad (8.50c)$$

which can be written in the more conventional form (e.g., equation (2.33) of [Vallis \(2017\)](#))

$$r \cos \phi (\text{curl } \vec{F})^{\bar{1}} = \frac{1}{r} \left[ \frac{\partial(\hat{r} \cdot \mathbf{F})}{\partial \phi} - \frac{\partial(r \hat{\phi} \cdot \mathbf{F})}{\partial r} \right] \quad (8.51a)$$

$$r (\text{curl } \vec{F})^{\bar{2}} = \frac{1}{r} \left[ \frac{\partial(r \hat{\lambda} \cdot \mathbf{F})}{\partial r} - \frac{1}{\cos \phi} \frac{\partial(\hat{r} \cdot \mathbf{F})}{\partial \lambda} \right] \quad (8.51b)$$

$$(\text{curl } \vec{F})^{\bar{3}} = \frac{1}{r \cos \phi} \left[ \frac{\partial(\hat{\phi} \cdot \mathbf{F})}{\partial \lambda} - \frac{\partial(\cos \phi \hat{\lambda} \cdot \mathbf{F})}{\partial \phi} \right]. \quad (8.51c)$$

### 8.2.8 Summary

We here summarize the spherical coordinate version of some common mathematical operators.

$$(\lambda, \phi, r) = (x^{\bar{1}}, x^{\bar{2}}, x^{\bar{3}}) \quad \text{spherical coordinates} \quad (8.52)$$

$$(r \cos \phi) F^{\bar{1}} = \hat{\lambda} \cdot \mathbf{F} \quad r F^{\bar{2}} = \hat{\phi} \cdot \mathbf{F} \quad F^{\bar{3}} = \hat{r} \cdot \mathbf{F} \quad \text{vector components} \quad (8.53)$$

$$\nabla = \hat{\lambda} (r \cos \phi)^{-1} \partial_\lambda + \hat{\phi} r^{-1} \partial_\phi + \hat{r} \partial_r \quad \text{gradient operator} \quad (8.54)$$

$$\nabla_{\bar{a}} F^{\bar{a}} = \frac{1}{r \cos \phi} \frac{\partial(\hat{\lambda} \cdot \mathbf{F})}{\partial \lambda} + \frac{1}{r \cos \phi} \frac{\partial(\hat{\phi} \cdot \mathbf{F} \cos \phi)}{\partial \phi} + \frac{1}{r^2} \frac{\partial(\hat{r} \cdot \mathbf{F} r^2)}{\partial r} \quad \text{divergence of vector} \quad (8.55)$$

$$\nabla^2 \psi = \frac{1}{(r \cos \phi)^2} \frac{\partial^2 \psi}{\partial \lambda^2} + \frac{1}{r^2 \cos \phi} \frac{\partial}{\partial \phi} \left[ \cos \phi \frac{\partial \psi}{\partial \phi} \right] + \frac{1}{r^2} \frac{\partial}{\partial r} \left[ r^2 \frac{\partial \psi}{\partial r} \right] \quad \text{Laplacian of scalar} \quad (8.56)$$

$$(\nabla \times \mathbf{F})_{\bar{a}} = \epsilon_{\bar{a}\bar{b}\bar{c}} \partial_b F^{\bar{c}} \quad \text{see equations (8.51a) -- (8.51c)} \quad \text{curl of vector.} \quad (8.57)$$

## 8.3 Cylindrical-polar coordinates

Many physical systems exhibit circular symmetry in two-dimensions or cylindrical symmetry in three-dimensions. The primary example encountered in this book is the laboratory motion of liquid in a rotating circular tank. In the following, we emulate the discussion presented for the spherical coordinates in Section 8.2, here focusing on cylindrical-polar coordinates as shown in Figure 8.2. Our task here is somewhat simpler than for the spherical coordinates since the vertical/axial position,  $z$ , remains unchanged from its Cartesian value. In a slight corruption of notation, we use the symbol  $r$  for the radial distance from the vertical axis in cylindrical-polar coordinates (Figure 8.2), which is distinct from the radial distance,  $r$ , used to measure the distance from the origin in spherical coordinates (Figure 8.1).

The coordinate transformation between Cartesian coordinates and cylindrical-polar coordi-

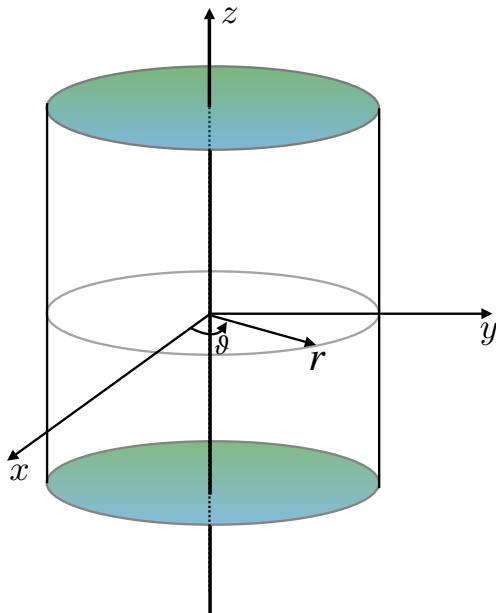


FIGURE 8.2: This schematic illustrates the geometry and notation for cylindrical-polar coordinates. The Cartesian triad of orthonormal basis vectors,  $(\hat{x}, \hat{y}, \hat{z})$  points along the orthogonal axes. The cylindrical-polar triad of orthonormal basis vectors,  $(\hat{r}, \hat{\theta}, \hat{z})$ , makes use of the radial unit vector  $\hat{r}$ , which points outward from the vertical axis, the angular unit vector  $\hat{\theta}$ , which points in the counter-clockwise direction around the circle, and the vertical unit vector  $\hat{z}$ . Note that the radial unit vector used for cylindrical-polar coordinates is distinct from that radial vector used in spherical coordinates shown in Figure 8.1.

nates is given by

$$x = r \cos \vartheta \equiv \xi^1 \cos \xi^2 \quad (8.58a)$$

$$y = r \sin \vartheta \equiv \xi^1 \sin \xi^2 \quad (8.58b)$$

$$z = \xi^3. \quad (8.58c)$$

The radial coordinate for cylindrical-polar coordinates

$$r = \sqrt{x^2 + y^2} \quad (8.59)$$

measures the distance from the vertical  $z$ -axis, and the angular coordinate  $0 \leq \vartheta \leq 2\pi$  measures the angle counter-clockwise from the positive  $x$ -axis. We introduce the unbarred and barred labels for the Cartesian and cylindrical polar coordinates

$$(x, y, z) = (\xi^1, \xi^2, \xi^3) \equiv \xi^a \quad \text{and} \quad (r, \vartheta, z) = (\xi^1, \xi^2, \xi^3) \equiv \xi^{\bar{a}}. \quad (8.60)$$

Although the vertical position  $z$  remains the same in both coordinates, and it is orthogonal to the other coordinates, we find it useful to introduce a distinct symbols,  $\xi^3$  and  $\xi^{\bar{3}}$ , to specify what other coordinates are held fixed when performing derivative operations.

### 8.3.1 Cartesian and cylindrical-polar transformation

The coordinate transformation (8.58a)-(8.58c) leads to the transformation matrix

$$\Lambda_{\bar{a}}^a = \begin{bmatrix} \partial\xi^1/\partial\xi^{\bar{1}} & \partial\xi^1/\partial\xi^{\bar{2}} & \partial\xi^1/\partial\xi^{\bar{3}} \\ \partial\xi^2/\partial\xi^{\bar{1}} & \partial\xi^2/\partial\xi^{\bar{2}} & \partial\xi^2/\partial\xi^{\bar{3}} \\ \partial\xi^3/\partial\xi^{\bar{1}} & \partial\xi^3/\partial\xi^{\bar{2}} & \partial\xi^3/\partial\xi^{\bar{3}} \end{bmatrix} = \begin{bmatrix} \cos\vartheta & -r\sin\vartheta & 0 \\ \sin\vartheta & r\cos\vartheta & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad (8.61)$$

and the inverse transformation is given by

$$\Lambda^{\bar{a}}_a = \frac{1}{r} \begin{bmatrix} r\cos\vartheta & r\sin\vartheta & 0 \\ -\sin\vartheta & \cos\vartheta & 0 \\ 0 & 0 & r \end{bmatrix}. \quad (8.62)$$

The determinant of the transformation (Jacobian) is given by

$$\det(\Lambda_{\bar{a}}^a) = r, \quad (8.63)$$

which vanishes along the vertical axis, which is where the transformation is singular.

### 8.3.2 Basis vectors

The cylindrical-polar coordinate basis vectors,  $\vec{e}_{\bar{a}}$ , are related to the Cartesian coordinate basis vectors,  $\vec{e}_a$ , through the transformation  $\vec{e}_{\bar{a}} = \Lambda_{\bar{a}}^a \vec{e}_a$ . The transformation matrix (8.61) leads to

$$\vec{e}_r = \hat{x}\cos\vartheta + \hat{y}\sin\vartheta \quad (8.64a)$$

$$\vec{e}_\vartheta = r(-\hat{x}\sin\vartheta + \hat{y}\cos\vartheta) \quad (8.64b)$$

$$\vec{e}_{\bar{z}} = \hat{z}. \quad (8.64c)$$

We sometimes make use of the following orthonormal unit vectors  $(\hat{r}, \hat{\vartheta}, \hat{z})$

$$\vec{e}_r = \hat{r} \quad \text{and} \quad \vec{e}_\vartheta = r\hat{\vartheta} \quad \text{and} \quad \vec{e}_{\bar{z}} = \hat{z} \quad (8.65)$$

along with the inverse relations

$$\hat{x} = \hat{r}\cos\vartheta - \hat{\vartheta}\sin\vartheta \quad (8.66a)$$

$$\hat{y} = \hat{r}\sin\vartheta + \hat{\vartheta}\cos\vartheta \quad (8.66b)$$

$$\hat{z} = \hat{z}. \quad (8.66c)$$

### 8.3.3 Basis one-forms

Since cylindrical-polar coordinates are orthogonal, we can readily derive the one-form basis through inverting the vector basis

$$\tilde{e}^r = \hat{r} \quad \text{and} \quad \tilde{e}^\vartheta = r^{-1}\hat{\vartheta} \quad \text{and} \quad \tilde{e}^{\bar{z}} = \hat{z}, \quad (8.67)$$

which satisfy the orthogonality relation (Section 7.2.2)

$$\tilde{e}^{\bar{b}} \cdot \vec{e}_{\bar{a}} = \delta_{\bar{a}}^{\bar{b}}. \quad (8.68)$$

### 8.3.4 Position and velocity

In cylindrical-polar coordinates, the position of a point is specified by the radial position plus the vertical position

$$\mathcal{P}(\tau) = r \vec{e}_r + z \vec{e}_{\bar{z}}. \quad (8.69)$$

The velocity requires all three coordinates since the radial basis vector is a function of the angular positions, which are in turn functions of time. Use of the chain rule renders

$$\vec{v}(\tau) = \frac{d\mathcal{P}}{d\tau} \quad (8.70a)$$

$$= \vec{e}_r \frac{dr}{d\tau} + r \frac{d\vec{e}_r}{d\tau} + \vec{e}_{\bar{z}} \frac{dz}{d\tau} \quad (8.70b)$$

$$= \vec{e}_r \frac{dr}{d\tau} + r \frac{\partial \vec{e}_r}{\partial \vartheta} \frac{d\vartheta}{d\tau} + \vec{e}_{\bar{z}} \frac{dz}{d\tau} \quad (8.70c)$$

$$= \vec{e}_r \frac{dr}{d\tau} + \vec{e}_{\vartheta} \frac{d\vartheta}{d\tau} + \vec{e}_{\bar{z}} \frac{dz}{d\tau} \quad (8.70d)$$

$$= \vec{e}_r v^r + \vec{e}_{\vartheta} v^{\vartheta} + \vec{e}_{\bar{z}} v^{\bar{z}}. \quad (8.70e)$$

To reach this result we made use of the identity

$$\vec{e}_{\vartheta} = r \frac{\partial \vec{e}_r}{\partial \vartheta} = r \hat{\boldsymbol{\vartheta}}. \quad (8.71)$$

### 8.3.5 Metric tensor

Cylindrical-polar coordinates are orthogonal with the metric tensor and its inverse represented by the diagonal matrices

$$g_{\bar{a}\bar{b}} = \vec{e}_{\bar{a}} \cdot \vec{e}_{\bar{b}} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & r^2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad \text{and} \quad g^{\bar{a}\bar{b}} = \vec{e}^{\bar{a}} \cdot \vec{e}^{\bar{b}} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & r^{-2} & 0 \\ 0 & 0 & 1 \end{bmatrix}. \quad (8.72)$$

### 8.3.6 Volume element and Levi-Civita tensor

The square root of the determinant of the metric tensor written in cylindrical-polar coordinates (from equation (8.72)) is given by

$$\sqrt{\det(\bar{\mathcal{G}})} = r \quad (8.73)$$

so that the volume element is

$$dV = r dr d\vartheta dz. \quad (8.74)$$

The covariant Levi-Civita tensor has the cylindrical-polar representation

$$\varepsilon_{\bar{a}\bar{b}\bar{c}} = r \epsilon_{\bar{a}\bar{b}\bar{c}}. \quad (8.75)$$

### 8.3.7 Vector cross product of basis vectors

As a check on the formalism for vector cross products, let us verify the relation (7.79) for the cross product of two basis vectors using cylindrical-polar coordinates

$$\vec{e}_{\bar{a}} \times \vec{e}_{\bar{b}} = \varepsilon_{\bar{a}\bar{b}\bar{c}} \vec{e}^{\bar{c}} \implies \vec{e}_{\bar{a}} \times \vec{e}_{\bar{b}} = r \epsilon_{\bar{a}\bar{b}\bar{c}} \vec{e}^{\bar{c}}. \quad (8.76)$$

Making use of the cylindrical-polar coordinate basis vectors and one-forms renders

$$\vec{e}_r \times \vec{e}_\vartheta = r(\hat{\mathbf{r}} \times \hat{\boldsymbol{\vartheta}}) = r\tilde{e}^z = \varepsilon_{r\vartheta z}\tilde{e}^z \quad (8.77a)$$

$$\vec{e}_\vartheta \times \vec{e}_{\bar{z}} = r(\hat{\boldsymbol{\vartheta}} \times \hat{\mathbf{z}}) = r\hat{\mathbf{r}} = r\tilde{e}^r = \varepsilon_{\vartheta\bar{z}r}\tilde{e}^r \quad (8.77b)$$

$$\vec{e}_{\bar{z}} \times \vec{e}_r = \hat{\mathbf{z}} \times \hat{\mathbf{r}} = \hat{\boldsymbol{\vartheta}} = r\tilde{e}^\vartheta = \varepsilon_{\bar{z}r\vartheta}\tilde{e}^\vartheta. \quad (8.77c)$$

To reach these results we made use of the cross products for the unit vectors

$$\hat{\mathbf{r}} \times \hat{\boldsymbol{\vartheta}} = \hat{\mathbf{z}} \quad \text{and} \quad \hat{\boldsymbol{\vartheta}} \times \hat{\mathbf{z}} = \hat{\mathbf{r}} \quad \text{and} \quad \hat{\mathbf{z}} \times \hat{\mathbf{r}} = \hat{\boldsymbol{\vartheta}}. \quad (8.78)$$

### 8.3.8 Components of a vector field

A vector field  $\vec{F}$  has Cartesian components,  $F^a$ , related to cylindrical-polar components,  $F^{\bar{a}}$ , via the transformation matrix,  $F^{\bar{a}} = \Lambda_a^{\bar{a}} F^a$ . This transformation leads to

$$F^{\bar{1}} = F^x \cos \vartheta + F^y \sin \vartheta \quad (8.79a)$$

$$F^{\bar{2}} = r^{-1} [-F^x \sin \vartheta + F^y \cos \vartheta] \quad (8.79b)$$

$$F^{\bar{3}} = F^z. \quad (8.79c)$$

Introducing the cylindrical-polar unit vectors (8.65) leads to the more tidy expressions

$$F^{\bar{1}} = \hat{\mathbf{r}} \cdot \mathbf{F} \quad (8.80a)$$

$$r F^{\bar{2}} = \hat{\boldsymbol{\vartheta}} \cdot \mathbf{F} \quad (8.80b)$$

$$F^{\bar{3}} = \hat{\mathbf{z}} \cdot \mathbf{F}, \quad (8.80c)$$

where  $\mathbf{F}$  is the Cartesian representation.

### 8.3.9 Differential operators

In cylindrical-polar coordinates, the gradient operator  $\nabla = \tilde{e}^a \partial_a$  takes on the form

$$\nabla = \hat{\mathbf{r}} \frac{\partial}{\partial r} + \frac{\hat{\boldsymbol{\vartheta}}}{r} \frac{\partial}{\partial \vartheta} + \hat{\mathbf{z}} \frac{\partial}{\partial z} \quad (8.81)$$

and the covariant divergence of a vector field is given by

$$\nabla_{\bar{a}} F^{\bar{a}} = r^{-1} \partial_{\bar{a}} (r F^{\bar{a}}) \quad (8.82a)$$

$$= r^{-1} \left( \partial_r [r F^{\bar{1}}] + \partial_\vartheta [r F^{\bar{2}}] + \partial_z [r F^{\bar{3}}] \right) \quad (8.82b)$$

$$= \frac{1}{r} \frac{\partial (r \hat{\mathbf{r}} \cdot \mathbf{F})}{\partial r} + \frac{1}{r} \frac{\partial (\hat{\boldsymbol{\vartheta}} \cdot \mathbf{F})}{\partial \vartheta} + \frac{\partial (\hat{\mathbf{z}} \cdot \mathbf{F})}{\partial z}. \quad (8.82c)$$

The covariant Laplacian of a scalar,  $\nabla^2 \psi = \nabla \cdot \nabla \psi$ , is given by

$$\nabla^2 \psi = \nabla \cdot \left[ \hat{\mathbf{r}} \frac{\partial \psi}{\partial r} + \frac{\hat{\boldsymbol{\vartheta}}}{r} \frac{\partial \psi}{\partial \vartheta} + \hat{\mathbf{z}} \frac{\partial \psi}{\partial z} \right] \quad (8.83a)$$

$$= \frac{1}{r} \frac{\partial}{\partial r} \left[ r \frac{\partial \psi}{\partial r} \right] + \frac{1}{r^2} \frac{\partial^2 \psi}{\partial \vartheta^2} + \frac{\partial^2 \psi}{\partial z^2}. \quad (8.83b)$$

The covariant curl (Section 7.17) takes the form

$$(\text{curl} \vec{F})^{\bar{1}} = r^{-1} [\partial_{\vartheta} F^{\bar{3}} - \partial_{\bar{z}} (r^2 F^{\bar{2}})] \quad (8.84a)$$

$$(\text{curl} \vec{F})^{\bar{2}} = r^{-1} [\partial_{\bar{z}} F^{\bar{1}} - \partial_r F^{\bar{3}}] \quad (8.84b)$$

$$(\text{curl} \vec{F})^{\bar{3}} = r^{-1} [\partial_r (r^2 F^{\bar{2}}) - \partial_{\vartheta} F^{\bar{1}}], \quad (8.84c)$$

which can be written more conventionally as

$$(\text{curl} \vec{F})^{\bar{1}} = \frac{1}{r} \frac{\partial(\hat{z} \cdot \mathbf{F})}{\partial \vartheta} - \frac{\partial(\hat{\vartheta} \cdot \mathbf{F})}{\partial z} \quad (8.85a)$$

$$r (\text{curl} \vec{F})^{\bar{2}} = \frac{\partial(\hat{r} \cdot \mathbf{F})}{\partial z} - \frac{\partial(\hat{z} \cdot \mathbf{F})}{\partial r} \quad (8.85b)$$

$$(\text{curl} \vec{F})^{\bar{3}} = \frac{1}{r} \frac{\partial(r \hat{\vartheta} \cdot \mathbf{F})}{\partial r} - \frac{1}{r} \frac{\partial(\hat{r} \cdot \mathbf{F})}{\partial \vartheta}. \quad (8.85c)$$

### 8.3.10 Summary

We here summarize the cylindrical coordinate version of some common mathematical operators.

$$(r, \vartheta, z) = (x^{\bar{1}}, x^{\bar{2}}, x^{\bar{3}}) \quad \text{cylindrical coordinates} \quad (8.86)$$

$$F^{\bar{1}} = \hat{r} \cdot \mathbf{F} \quad r F^{\bar{2}} = \hat{\vartheta} \cdot \mathbf{F} \quad F^{\bar{3}} = \hat{z} \cdot \mathbf{F} \quad \text{vector components} \quad (8.87)$$

$$\nabla = \hat{r} \frac{\partial}{\partial r} + \frac{\hat{\vartheta}}{r} \frac{\partial}{\partial \vartheta} + \hat{z} \frac{\partial}{\partial z} \quad \text{gradient} \quad (8.88)$$

$$\nabla_{\bar{a}} F^{\bar{a}} = \frac{1}{r} \frac{\partial(r \hat{r} \cdot \mathbf{F})}{\partial r} + \frac{1}{r} \frac{\partial(\hat{\vartheta} \cdot \mathbf{F})}{\partial \vartheta} + \frac{\partial(\hat{z} \cdot \mathbf{F})}{\partial z}. \quad \text{divergence} \quad (8.89)$$

$$\nabla^2 \psi = \frac{1}{r} \frac{\partial}{\partial r} \left[ r \frac{\partial \psi}{\partial r} \right] + \frac{1}{r^2} \frac{\partial^2 \psi}{\partial \vartheta^2} + \frac{\partial^2 \psi}{\partial z^2} \quad \text{Laplacian of scalar} \quad (8.90)$$

$$(\nabla \times \mathbf{F})_{\bar{a}} = \varepsilon_{\bar{a}\bar{b}\bar{c}} \partial_{\bar{b}} F^{\bar{c}} \quad \text{see equations (8.84a) -- (8.84c).} \quad \text{curl of a vector} \quad (8.91)$$

## 8.4 General orthogonal coordinates

We can generalize the spherical and cylindrical coordinates by considering a nonsingular and orthogonal set of coordinates defined such that the metric tensor takes on the diagonal form

$$g_{\bar{a}\bar{b}} = \vec{e}_{\bar{a}} \cdot \vec{e}_{\bar{b}} = \begin{bmatrix} h_{\bar{1}} & 0 & 0 \\ 0 & h_{\bar{2}} & 0 \\ 0 & 0 & h_{\bar{3}} \end{bmatrix}, \quad (8.92)$$

where  $h_{\bar{a}} > 0$  are “stretching” functions. The corresponding volume element is expressed as

$$dV = h_{\bar{1}} h_{\bar{2}} h_{\bar{3}} d\xi^{\bar{1}} d\xi^{\bar{2}} d\xi^{\bar{3}}. \quad (8.93)$$

These *generalized orthogonal curvilinear coordinates* have a corresponding orthogonal set of basis vectors

$$\vec{e}_{\bar{a}} = h_{\bar{a}} \hat{\mathbf{e}}_{(\bar{a})} \quad \text{no implied sum.} \quad (8.94)$$

The objects  $\hat{\mathbf{e}}_{(\bar{a})}$  are the dimensionless unit directions. The corresponding one-form basis is given by

$$\tilde{e}^{\bar{a}} = (h_{\bar{a}})^{-1} \hat{\mathbf{e}}_{(\bar{a})}. \quad (8.95)$$

The index on the unit directions is enclosed in parentheses to advertise that it is not tensorial; i.e., the unit directions do not transform as tensors. Rather, the functions  $h_{\bar{a}}$  carry the tensorial properties of the basis vectors  $\vec{e}_{\bar{a}}$ . Results for the trajectory and velocity are straightforward generalizations of the spherical results in Section 8.2 and cylindrical-polar results from Section 8.3. A detailed presentation of generalized orthogonal coordinates is found in Section 21.11 of [Griffies \(2004\)](#), with these coordinates commonly used for ocean models.



**Part II**

**Geophysical particle mechanics**

The earth's rotation and gravitation are two defining features of atmospheric and oceanic fluid mechanics. Geophysical fluids exhibit motions whose speed is small relative to that of the rotating planet. We thus say that geophysical fluids are in near solid-body motion. Hence, it is very convenient to make use of a rotating (non-inertial) terrestrial reference frame for a physical description.

Rotating and gravitating motion around a sphere introduces many new physical ideas beyond the non-rotating case. We are thus motivated to develop our understanding of geophysical fluids in a stepwise manner to ensure concepts and tools are mastered at each stage. For that purpose, we here study the Newtonian mechanics of a point particle moving around a rotating and gravitating sphere as viewed in the terrestrial (rotating) reference frame. This study of *geophysical particle mechanics* provides a particle mechanics preview of concepts later encountered in geophysical fluid mechanics, such as trajectories, linear momentum, angular momentum, body forces, non-inertial accelerations (Coriolis and centrifugal), symmetries, planetary Cartesian coordinates and planetary spherical coordinates.

# Chapter 9

## Particle mechanics

In this chapter we study the kinematics and dynamics of a point particle of fixed mass and zero electric charge moving around a rotating and gravitating sphere. The motion of the gravitating sphere is prescribed with a fixed kinetic energy and fixed angular momentum around its axis of rotation. Hence, the only interesting mechanics is that of the moving particle. We examine that motion in a spherical geometry as observed from a non-inertial rotating reference frame. This perspective is motivated by our concern with particle motion that is in near solid-body motion with the planet, with such motion relevant to the study of geophysical fluids. Notably, a particle at rest on the rotating sphere has both kinetic energy and angular momentum. Motion relevant to geophysical fluids modifies these solid body values.

The only inertial force acting on the particle arises from the gravitational field of the sphere (ignoring friction and other forces). Two non-inertial accelerations (planetary centrifugal and Coriolis) appear when viewing the motion from the rotating terrestrial reference frame. We make use of both the planetary Cartesian and planetary spherical coordinates to represent the position, velocity, and acceleration vectors, working through both the physics and the maths in support of later descriptions of geophysical fluid motions.

### CHAPTER GUIDE

This chapter makes use of basic features of both Cartesian and general tensor algebra as presented in Chapters 1, 6, 7, and Section 8.2. We offer the salient features of tensor technology in this chapter where needed, thus providing a reasonably self-contained presentation. This chapter is notable for working through some relatively tedious algebra as part of developing the spherical coordinate representation of acceleration. This work is relevant also for geophysical fluids, although we rarely encounter the full spherical coordinate equations in later chapters. Even so, the reader is encouraged to read through the details, at least once, as they are part of all numerical models of atmosphere and ocean circulation.

9.1	A survey of Newtonian particle mechanics . . . . .	170
9.1.1	Mechanics of a point particle . . . . .	171
9.1.2	Galilean invariance of inertial reference frames . . . . .	171
9.1.3	Inertial and non-inertial reference frames . . . . .	172
9.1.4	Angular velocity and angular momentum . . . . .	172
9.1.5	Mechanical work and kinetic energy . . . . .	174
9.1.6	Kinetic energy of rotational motion . . . . .	174
9.1.7	Conservative forces and mechanical energy conservation . . . . .	174

9.1.8	Friction as a non-conservative force . . . . .	175
9.1.9	Comments . . . . .	176
9.2	The rotating earth . . . . .	176
9.3	Reference frames and non-inertial accelerations . . . . .	178
9.4	Rotation of a vector . . . . .	178
9.4.1	Brief derivation . . . . .	179
9.4.2	Detailed derivation for planar motion . . . . .	179
9.4.3	Changes to Cartesian basis vectors under rotation . . . . .	180
9.4.4	Changes to polar coordinate unit vectors under rotation . . . . .	180
9.5	Some tensor algebra . . . . .	181
9.5.1	Why we need general tensors . . . . .	181
9.5.2	The coordinate representation of a vector . . . . .	181
9.5.3	Transformation of a coordinate representation . . . . .	182
9.6	The velocity vector . . . . .	183
9.6.1	Coordinate velocity . . . . .	183
9.6.2	Changes to the basis vectors . . . . .	183
9.7	Inertial acceleration and its decomposition . . . . .	184
9.8	Representing the position vector . . . . .	184
9.9	Representing the velocity vector . . . . .	185
9.9.1	Planetary Cartesian coordinate representation . . . . .	185
9.9.2	Planetary spherical coordinate representation . . . . .	186
9.9.3	Transforming from Cartesian to spherical . . . . .	187
9.9.4	Axial angular momentum . . . . .	187
9.10	Planetary Cartesian representation of acceleration . . . . .	188
9.10.1	Planetary Cartesian representation . . . . .	188
9.10.2	Summary of acceleration representation . . . . .	189
9.10.3	Further study . . . . .	190
9.11	Spherical representation of acceleration . . . . .	190
9.11.1	Transforming from Cartesian to spherical . . . . .	191
9.11.2	Decomposing the acceleration . . . . .	192
9.11.3	Spherical coordinate acceleration . . . . .	192
9.11.4	Metric acceleration . . . . .	192
9.11.5	Centrifugal acceleration . . . . .	193
9.11.6	Coriolis acceleration . . . . .	193
9.11.7	Coriolis acceleration for large-scale motions . . . . .	194
9.12	Newtonian gravity . . . . .	194
9.12.1	Newtonian gravity from Poisson's equation . . . . .	195
9.12.2	Gravitational field for a spherical earth . . . . .	195
9.12.3	Approximate gravitational acceleration . . . . .	196
9.12.4	Effective gravitational force from the geopotential . . . . .	197
9.12.5	Further study . . . . .	197
9.13	Newton's law of motion . . . . .	197
9.13.1	Cartesian coordinate representation . . . . .	198
9.13.2	Spherical coordinate representation . . . . .	198
9.13.3	Geopotential coordinate representation . . . . .	199
9.13.4	Comments . . . . .	201
9.13.5	Further study . . . . .	201
9.14	Exercises . . . . .	201

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## 9.1 A survey of Newtonian particle mechanics

Before diving into the mechanics of a particle moving around a rotating sphere, we here summarize foundational elements of Newtonian particle mechanics. Doing so exposes some basic concepts such as space, time, mass, and force. Notably, within the bounds of classical physics these

concepts remain intuitive in that they are based on common experience rather than deduced from something more fundamental. This perspective is sufficient for this book.

### 9.1.1 Mechanics of a point particle

Let  $\mathbf{X}(t)$  be the position in space of a point particle at a particular time instance,  $t$ . The spatial position is measured relative to an arbitrary origin, with the vector  $\mathbf{X}$  pointing from the origin to the particle. As the particle moves in time it traces out a *trajectory* through space-time. The velocity of the particle at any time instance is measured by the time derivative

$$\mathbf{V} = \frac{d\mathbf{X}}{dt} = \dot{\mathbf{X}}, \quad (9.1)$$

where the second equality introduced a common “dot” notation for time derivatives that will sometimes be used in this book. Geometrically, the velocity at each point in space-time is tangent to the trajectory.

The *linear momentum* of the particle equals to the mass of the particle,  $m$ , times its velocity

$$\mathbf{P} = m \dot{\mathbf{X}}. \quad (9.2)$$

The momentum of the particle changes when it interacts with other objects and/or experiences forces. The vector sum of these forces is written  $\mathbf{F}$ , and Newton’s second law of motion states that there exists *inertial reference frames* where motion of the particle is described by the differential equation

$$\frac{d\mathbf{P}}{dt} = \mathbf{F}. \quad (9.3)$$

If the particle mass is fixed, then this equation becomes a second order differential equation for the particle position or trajectory

$$\mathbf{A} = \frac{d\mathbf{V}}{dt} = \frac{d^2\mathbf{X}}{dt^2} = \mathbf{F}/m. \quad (9.4)$$

We refer to  $\mathbf{A} = \dot{\mathbf{V}}$  as the *acceleration*.

Many conclusions in mechanics are expressed in terms of conservation laws (Chapter 10), which provide relations or conditions whereby mechanical properties of a physical system remain unchanged in time. Newton’s second law provides our first conservation law. Namely, in the absence of a force, the linear momentum of a physical system remains unchanged:  $d\mathbf{P}/dt = 0$ . Depending on the nature of the forces, this conservation law might hold for one, two, or all three of the vector components to the linear momentum.

### 9.1.2 Galilean invariance of inertial reference frames

If the forces acting on the particle are not directly dependent on the particle velocity, then the inertial frame equation of motion (9.4) is unchanged if shifting the velocity by a constant. Such velocity-independent forces (such as Newtonian gravity) are commonly found in reversible (non-dissipative) motion of charge-free particles. This arbitrariness in the velocity reflects a *symmetry* respected by the equation of motion, where symmetry refers to an operation that can be performed on the system without changing any physics. We give the symmetry the name *Galilean invariance*, with Galilean invariance a property of all inertial reference frames in Newtonian mechanics.

These considerations indicate that there is no experiment that can distinguish between two arbitrary inertial reference frames, so long as the experiments are described by Newton’s equation

of motion (9.4) and the force is independent of the velocity. The reason we cannot make a distinction is that the equation of motion is indistinguishable in the two inertial frames. As a corollary, two inertial reference frames can at most be moving relative to one another by a constant velocity. Otherwise, at least one of the reference frames must be accelerating, which in turn would mean that it is not an inertial frame.

This discussion offers an example of the mathematical transformation theory introduced in Part I of this book. Mathematically, the Galilean transformation is written

$$\bar{t} = t \quad \text{and} \quad \bar{\mathbf{X}} = \mathbf{X} + \mathbf{U}t, \quad (9.5)$$

where the barred position vector is measured in the moving reference frame. Time remains unchanged, as per the normal situation with Newtonian universal time. In contrast, the position of the particle in the new frame equals to that in the original reference frame plus a contribution from the constant velocity,  $\mathbf{U}$ . We may sometimes refer to the barred reference frame as a *Galilean boosted* frame. The particle velocity in the moving (boosted) reference frame is given by

$$\bar{\mathbf{V}} = \frac{d\bar{\mathbf{X}}}{dt} = \frac{d\mathbf{X}}{dt} + \frac{d(\mathbf{U}t)}{dt} = \mathbf{V} + \mathbf{U}, \quad (9.6)$$

where we set  $d\mathbf{U}/dt = 0$  since  $\mathbf{U}$  has a fixed magnitude and direction (as per our assumption that it is a constant vector). As expected, the velocity is shifted by the constant reference frame velocity  $\mathbf{U}$ . Furthermore, as advertised, the acceleration in the two reference frames is identical

$$\bar{\mathbf{A}} = \frac{d^2\bar{\mathbf{X}}}{dt^2} = \frac{d\mathbf{V}}{dt} = \mathbf{A}. \quad (9.7)$$

### 9.1.3 Inertial and non-inertial reference frames

As seen above, inertial reference frames (also called *absolute* reference frames) have a special status in Newtonian mechanics since it is in these reference frames that Newton's second law holds as per equations (9.3) or (9.4). In practice, inertial reference frames are an idealization never met exactly. For experiments taking place within many laboratories, the earth or *laboratory reference frame* provide a good approximation to an inertial reference frame. However, when the scale of the physical system under study increases, then it can become untenable to ignore the earth's rotation. In such cases the rotating earth reference frame is no longer a good approximation to an inertial frame, with this situation holding for most geophysical fluid motions.

### 9.1.4 Angular velocity and angular momentum

The *angular momentum* of a particle defined relative to an arbitrary chosen origin is given by the vector cross product

$$\mathbf{L} = \mathbf{X} \times \mathbf{P}. \quad (9.8)$$

Making use of Newton's second law (9.3) leads to the equation of motion for the angular momentum

$$\frac{d\mathbf{L}}{dt} = \mathbf{X} \times \mathbf{F}, \quad (9.9)$$

where we set  $\dot{\mathbf{X}} \times \mathbf{P} = \dot{\mathbf{X}} \times m\dot{\mathbf{X}} = 0$ . The cross product,  $\mathbf{X} \times \mathbf{F}$ , is the *torque* acting on the system relative to the origin. Equation (9.9) leads to our second conservation law: a particle has a constant angular momentum when experiencing zero torques, with this statement dependent on the choice of origin for the angular momentum and the corresponding torques.

We thus see that the utility and relevance of angular momentum stems from its conservation for systems exhibiting rotational symmetry about special points or special directions. For example, motion on a smooth sphere exhibits rotational symmetry with respect to the center of the sphere. Consequently, all components of angular momentum for a particle are constant in the absence of externally applied torques. Likewise, for motion on a smooth rotating sphere, we show in Section 10.7 that the component of angular momentum about the rotation axis is a constant of the motion.

### *Angular velocity and moment of inertia*

Whereas linear momentum has physical dimensions of

$$[\mathbf{P}] \equiv \text{mass} \times \text{length} \times \text{time}^{-1}, \quad (9.10)$$

angular momentum has dimensions of

$$[\mathbf{L}] \equiv \text{mass} \times \text{length}^2 \times \text{time}^{-1}. \quad (9.11)$$

We can pursue the analog by introducing the *angular velocity* of a particle relative to a chosen origin

$$\boldsymbol{\Omega} = \frac{\mathbf{X} \times \mathbf{V}}{|\mathbf{X}|^2}. \quad (9.12)$$

The angular velocity has physical dimensions of inverse time, and it is defined with respect to the chosen coordinate origin. Furthermore, by construction the angular velocity vector is orthogonal to both the velocity and to the position

$$\boldsymbol{\Omega} \cdot \mathbf{X} = \boldsymbol{\Omega} \cdot \mathbf{V} = 0. \quad (9.13)$$

The angular velocity is not defined at the origin since  $|\mathbf{X}| = 0$ .

Inserting the definition of the angular velocity (9.12) into the angular momentum (9.8) renders

$$\mathbf{L} = m (\mathbf{X} \times \mathbf{V}) \quad (9.14a)$$

$$= m |\mathbf{X}|^2 \boldsymbol{\Omega} \quad (9.14b)$$

$$\equiv I \boldsymbol{\Omega}. \quad (9.14c)$$

In the final equality we introduced the moment of inertia for a point particle

$$I = m |\mathbf{X}|^2. \quad (9.15)$$

The moment of inertia measures the inertia appropriate for determining angular momentum relative to a chosen coordinate origin. The moment of inertia scalar,  $I$ , generalizes to the moment of inertia tensor,  $I_{mn}$ , when considering angular momentum for extended matter, such as a rigid body or a material fluid region (Section 32.7.4).

The cross product of the position vector with the angular velocity (9.12) is given by

$$\boldsymbol{\Omega} \times \mathbf{X} = \mathbf{V} - \mathbf{X} \frac{\mathbf{V} \cdot \mathbf{X}}{|\mathbf{X}|^2}. \quad (9.16)$$

For the special case of velocity  $\mathbf{V}$  orthogonal to the position vector,  $\mathbf{X}$ , we have

$$\mathbf{V} = \boldsymbol{\Omega} \times \mathbf{X} \quad \text{when } \mathbf{V} \cdot \mathbf{X} = 0. \quad (9.17)$$

In particular, for circular motion the velocity is orthogonal to the position.

### 9.1.5 Mechanical work and kinetic energy

When a force is applied to a particle as it moves along its trajectory, the force does *mechanical work* on the particle. The work is computed by the line integral along the trajectory

$$W = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \mathbf{F} \cdot d\mathbf{x}, \quad (9.18)$$

where

$$\mathbf{x}_1 = \mathbf{X}(t = t_1) \quad \text{and} \quad \mathbf{x}_2 = \mathbf{X}(t = t_2) \quad (9.19)$$

are the spatial coordinates of the endpoints for the trajectory at times  $t_1$  and  $t_2$ , and  $d\mathbf{x}$  is the differential vector increment along the trajectory. Since the particle is moving along its dynamical trajectory, we can write  $d\mathbf{x} = \mathbf{V} dt$  and make use of Newton's equation of motion (9.4) to reach

$$W = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \mathbf{F} \cdot d\mathbf{x} = \frac{m}{2} \int_{\mathbf{x}_1}^{\mathbf{x}_2} \frac{d(\mathbf{V} \cdot \mathbf{V})}{dt} dt = K(t_2) - K(t_1), \quad (9.20)$$

where we identified the kinetic energy of the particle

$$K = \frac{m}{2} \mathbf{V} \cdot \mathbf{V}. \quad (9.21)$$

We conclude that the work done on the particle over a time interval is equal to its change in kinetic energy. The result (9.20) is called the *work-energy theorem*.

### 9.1.6 Kinetic energy of rotational motion

If the particle is undergoing rotational motion so that  $\mathbf{V} = \boldsymbol{\Omega} \times \mathbf{X}$  (equation (9.17)), then the kinetic energy of the particle takes on the form

$$(2/m) K = V_i V_i \quad (9.22a)$$

$$= \epsilon_{ijk} \Omega_j V_k \epsilon_{ist} \Omega_s V_t \quad (9.22b)$$

$$= \epsilon_{ijk} \epsilon_{ist} \Omega_j X_k \Omega_s X_t \quad (9.22c)$$

$$= (\delta_{js} \delta_{kt} - \delta_{jt} \delta_{ks}) \Omega_j X_k \Omega_s X_t \quad (9.22d)$$

$$= \mathbf{X} \cdot \mathbf{X} \boldsymbol{\Omega} \cdot \boldsymbol{\Omega} \quad (9.22e)$$

where we set  $\boldsymbol{\Omega} \cdot \mathbf{X} = 0$  as per equation (9.13), and made use of the epsilon tensor identity (1.38). The kinetic energy is thus given by

$$K = \frac{1}{2} I \boldsymbol{\Omega} \cdot \boldsymbol{\Omega}, \quad (9.23)$$

where  $I = m \mathbf{X} \cdot \mathbf{X}$  is the moment of inertia for the point particle as defined by equation (9.15).

### 9.1.7 Conservative forces and mechanical energy conservation

If the work done on the particle between two points in space is independent of the path taken between the points, then the force is said to be *conservative*.

### Conservation of mechanical energy

Recalling our discussion of exact differentials in Section 2.8, we know that a conservative force can be written as the gradient of a *force potential*<sup>1</sup>

$$\mathbf{F} = -\nabla V, \quad (9.24)$$

where  $V$  is called the *potential* or the *potential energy*. Inserting the potential into the work equation (9.20) leads to an expression of *mechanical energy* conservation

$$W = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \mathbf{F} \cdot d\mathbf{x} = \Delta K = -\Delta V \implies K(t_2) + V(t_2) = K(t_1) + V(t_1). \quad (9.25)$$

That is, the sum of the kinetic energy plus potential energy remains constant for a particle moving in a conservative force field. The conservation of kinetic plus potential energy within a conservative force field offers our third conservation law: the conservation of mechanical energy. As a result of mechanical energy conservation (9.25), we see that if a particle takes a closed trajectory within a conservative force field, then there is zero work applied to the particle

$$W = \oint_{\mathcal{C}} \mathbf{F} \cdot d\mathbf{x} = 0, \quad (9.26)$$

where  $\mathcal{C}$  is an arbitrary closed trajectory.

### Conservative force from the effective gravity field

The earth's gravitational field as well as the planetary centrifugal acceleration (due to motion on a rotating planet) both give rise to conservative forces. We discuss these ideas in Section 9.12.4, where we see that the combined accelerations from gravity and centrifugal are encapsulated by the gradient of the geopotential,  $\Phi$ . Hence, the effective gravitational force acting on a point particle of mass,  $m$ , is given by

$$\mathbf{F} = -m \nabla \Phi. \quad (9.27)$$

Consequently, the work done on the particle by the effective gravitational field is given by

$$W = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \mathbf{F} \cdot d\mathbf{x} = -m \int_{\mathbf{x}_1}^{\mathbf{x}_2} \nabla \Phi \cdot d\mathbf{x} = -m [\Phi(\mathbf{x}_2) - \Phi(\mathbf{x}_1)]. \quad (9.28)$$

The effective gravitational force field does positive work on the particle if  $\Phi(\mathbf{x}_1) > \Phi(\mathbf{x}_2)$ . That is, work is applied to the particle as it moves from a high geopotential at  $\mathbf{x}_1$  to a lower geopotential at  $\mathbf{x}_2$ , in which case the work-energy theorem (9.20) means that the kinetic energy increases. Conversely, if  $\Phi(\mathbf{x}_1) < \Phi(\mathbf{x}_2)$ , then gravity does negative work on the particle. In this case the potential energy of the particle increases as it moves to a higher geopotential, while, through the work-energy theorem, the kinetic energy of the particle decreases.

#### 9.1.8 Friction as a non-conservative force

Friction is the canonical non-conservative force that typically depends on the velocity field. For example, a common form of friction is given by *Rayleigh drag*

$$\mathbf{F}_{\text{Rayleigh}} = -\gamma m \mathbf{V}, \quad (9.29)$$

---

<sup>1</sup>Do not confuse the potential,  $V$ , in equation (9.24) with the magnitude of the velocity,  $|\mathbf{V}|$ . They are distinct.

where  $\gamma > 0$  is a constant with dimensions of inverse time. Newton's equation of motion with Rayleigh drag (and no other forces) takes the form

$$\frac{d\mathbf{V}}{dt} = -\gamma \mathbf{V}. \quad (9.30)$$

Notably, Rayleigh drag is not Galilean invariant since it is dependent on the velocity. We can understand this lack of invariance by noting that the friction force distinguishes the state of rest ( $\mathbf{V} = 0$ ) in a particular reference frame from motion in a Galilean boosted reference frame.

The solution to the first order ordinary differential equation (9.30) is the exponential decay

$$\mathbf{V}(t) = \mathbf{V}(0) e^{-\gamma t}, \quad (9.31)$$

with  $\mathbf{V}(0)$  the initial condition. We thus see that Rayleigh drag exponentially drives the velocity towards zero. Correspondingly, Rayleigh drag dissipates the kinetic energy according to twice the exponential decay

$$\frac{dK}{dt} = m \mathbf{V} \cdot \frac{d\mathbf{V}}{dt} = -2\gamma K \implies K(t) = K(0) e^{-2\gamma t}, \quad (9.32)$$

where  $K(0) = \mathbf{V}(0) \cdot \mathbf{V}(0)/2$ .

### 9.1.9 Comments

Every classical mechanics textbook has some form of the material presented in this section. The book from [Goldstein \(1980\)](#) is targeted at the entering physics graduate student, whereas [Marion and Thornton \(1988\)](#) is targeted at second year undergraduates.

We now move from generalities to the special case of a particle moving around a rotating and gravitating sphere. Throughout that discussion it can be useful to return to the general considerations presented in this section as a reminder of the fundamental physical notions, which are quite simple in their essence. Such reminders are particularly useful when encountering the somewhat tedious mathematical manipulations with spherical coordinates in a rotating reference frame that are encountered later in this chapter.

## 9.2 The rotating earth

The earth's angular velocity is comprised of two main contributions: the spin of the earth about its axis and the orbit of the earth about the sun (see Figure 9.1). Other astronomical motions can be neglected for geophysical fluid mechanics. Therefore, in the course of a single period of 24 hours, or  $24 \times 3600 = 86400$  seconds, the earth experiences an angular rotation of  $(2\pi + 2\pi/365.24)$  radians. As such, the angular rotation rate is given by

$$\Omega = \frac{2\pi + 2\pi/365.24}{86400\text{s}} = \left[ \frac{\pi}{43082} \right] \text{s}^{-1} = 7.2921 \times 10^{-5} \text{ s}^{-1}. \quad (9.33)$$

The earth's angular velocity, both its direction through the polar axis and its magnitude, is assumed constant in time for purposes of geophysical fluid mechanics

$$\frac{d\Omega}{dt} = 0. \quad (9.34)$$

The angular speed (9.33) seems quite small. However, a terrestrial reference frame on the

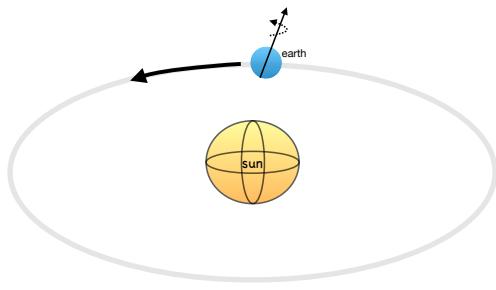


FIGURE 9.1: The angular velocity of the earth arises from the spin about the polar axis plus the orbit of the planet around the sun. This angular velocity determines the strength of the Coriolis acceleration and the planetary centrifugal acceleration.

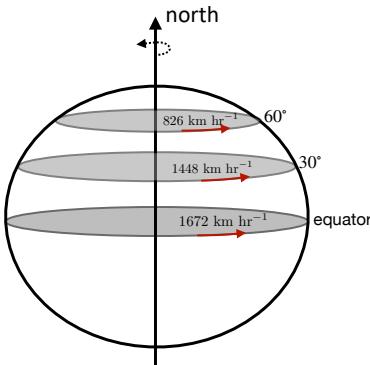


FIGURE 9.2: For an observer at rest on the earth's surface, the solid body speed is  $\Omega R_e \cos \phi = 7.2921 \times 10^{-5} \text{ s}^{-1} \times 6.371 \times 10^6 \text{ m} \cos \phi \approx 465 \text{ m s}^{-1} \cos \phi = 1672 \text{ km hr}^{-1} \cos \phi$ . We here display solid-body speeds for motion at the equator, 30° latitude, and 60° latitude. These speeds are much larger than motion of the ocean and atmosphere relative to the earth, thus motivating a description of geophysical fluid motion from the rotating terrestrial frame moving with the solid-body.

surface of the earth, undergoing *solid body motion*, moves with linear speed

$$U_{\text{solid-body}}(\phi) = \Omega R_e \cos \phi \approx 465 \text{ m s}^{-1} \cos \phi = 1672 \text{ km hr}^{-1} \cos \phi, \quad (9.35)$$

where we set the earth's radius to

$$R_e = 6.371 \times 10^6 \text{ m}. \quad (9.36)$$

This speed is quite large relative to a fixed frame outside the planet (see Figure 9.2)

$$U_{\text{solid-body}}(0) = 1672 \text{ km hr}^{-1} \quad (9.37a)$$

$$U_{\text{solid-body}}(30^\circ) = 1448 \text{ km hr}^{-1} \quad (9.37b)$$

$$U_{\text{solid-body}}(60^\circ) = 826 \text{ km hr}^{-1}. \quad (9.37c)$$

Even so, motion of the atmosphere and ocean are generally quite close to the solid-body motion, so that their speeds relative to the planet are much smaller than the speed of the rotating planet itself. Therefore, it is sensible to describe geophysical fluid motion from the non-inertial rotating terrestrial reference frame.

### 9.3 Reference frames and non-inertial accelerations

Motion of geophysical fluids deviates relatively little from solid-body motion. That is, motion of fluid elements deviates relatively little from motion of the earth itself. For these reasons, the preferred frame for studying geophysical motion is the rotating planetary frame (a non-inertial frame) rather than a frame fixed relative to the stars (an approximate inertial frame). Figure 9.3 illustrates the case for the position vector of a particle relative to the origin of a rotating sphere.

A set of basis vectors is needed in order to use coordinates for representing vectors. The basis vectors hold two key pieces of information, with the first being details of the coordinates. The second concerns the reference frame, whereby non-inertial accelerations arise from time dependence to the basis vectors. When represented in terms of non-inertial reference frame coordinates, the inertial acceleration (a vector) is decomposed into the sum of relative acceleration (relative to the non-inertial frame), centrifugal acceleration, and Coriolis acceleration.

When multiplied by mass, non-inertial accelerations can be interpreted as non-inertial forces. However, these forces are not imparted by an external force. Rather, they arise from accelerated motion of the non-inertial reference frame. In this sense, non-inertial accelerations are often termed “fictitious” or “kinematic”. Nonetheless, a terrestrial observer interprets motion that includes non-inertial accelerations, so that non-inertial accelerations are central to rationalizing observed planetary fluid motions. Indeed, as seen in Section 10.8, the Coriolis acceleration that appears in a non-inertial reference frame has its counterpart in axial angular momentum conservation, with angular momentum conservation a property of all reference frames. Hence, there is nothing imaginary about non-inertial accelerations.

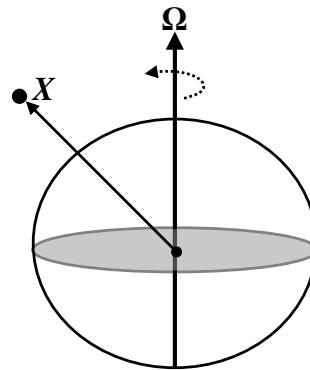


FIGURE 9.3: The position vector,  $\mathbf{X}(t)$ , for a particle moving around a rotating sphere with coordinate origins at the center of the sphere. The rotation axis is through the north pole, with angular velocity vector  $\boldsymbol{\Omega}$ . The sphere rotates in a positive right hand sense through the north polar axis (counter clockwise from above). The rotating frame has a solid-body velocity  $\mathbf{U}_{\text{solid}} = \boldsymbol{\Omega} \times \mathbf{X}$  (equation (9.65)).

### 9.4 Rotation of a vector

How does a vector change under a solid-body rotation such as that shown in Figure 9.4? That is, when a vector is assumed to not translate nor to change its magnitude, how does it change as a result of solid-body rotation? To answer this question, observe that a pure rotation does not change the magnitude of a vector so that

$$|\mathbf{X}(t)| = |\mathbf{X}(t + \delta t)|. \quad (9.38)$$

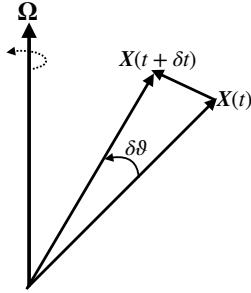


FIGURE 9.4: The change in a vector under a pure rotation leaves its origin fixed and the vector magnitude unchanged,  $|\mathbf{X}(t)| = |\mathbf{X}(t + \delta t)|$ . Only the vector direction changes by the angle  $\delta\vartheta = \Omega \delta t$ . Infinitesimal changes generated by the angular velocity  $\boldsymbol{\Omega}$  lead to the vector differences  $\mathbf{X}(t + \delta t) - \mathbf{X}(t) = \delta t \boldsymbol{\Omega} \times \mathbf{X}(t)$ .

The condition (9.38) can be written as

$$\frac{d(\mathbf{X} \cdot \mathbf{X})}{dt} = 0, \quad (9.39)$$

which leads to the constraint

$$\mathbf{X} \cdot \frac{d\mathbf{X}}{dt} = 0. \quad (9.40)$$

That is, the velocity generated by a pure rotation is itself perpendicular to the position. We encountered this result in Section 2.1.4 when showing that unit vectors (vectors of a fixed unit length) can only change through rotations. What we see here is that any vector of fixed magnitude and fixed origin can change only through a rotation of its direction.

### 9.4.1 Brief derivation

Referring to Figure 9.4, we see that the infinitesimal difference  $\mathbf{X}(t + \delta t) - \mathbf{X}(t)$  equals to the vector cross product of the angular velocity with the position vector

$$\mathbf{X}(t + \delta t) - \mathbf{X}(t) = \delta t \boldsymbol{\Omega} \times \mathbf{X}(t). \quad (9.41)$$

Dividing by  $\delta t$  leads to

$$\frac{d\mathbf{X}}{dt} = \boldsymbol{\Omega} \times \mathbf{X} \quad \text{pure rotation.} \quad (9.42)$$

Note that this evolution equation satisfies the constraint (9.40) since  $\mathbf{X} \cdot (\boldsymbol{\Omega} \times \mathbf{X}) = 0$ , meaning that the magnitude of the vector indeed remains fixed. We sometimes say that  $\boldsymbol{\Omega}$  is the generator of rotations of  $\mathbf{X}$ .

### 9.4.2 Detailed derivation for planar motion

To determine the change in direction generated by a pure rotation, first consider the simplified case of planar rotation. Let  $\boldsymbol{\Omega}$  be entirely in the vertical, and let  $\mathbf{X}$  be confined to the horizontal plane. In a time increment  $\delta t$ , the vector  $\mathbf{X}(t)$  is rotated by an angle

$$\delta\vartheta = |\boldsymbol{\Omega}| \delta t \quad (9.43)$$

relative to  $\mathbf{X}(t + \delta t)$ . In the limit of small  $\delta\vartheta$ , the difference vector,  $\mathbf{X}(t + \delta t) - \mathbf{X}(t)$ , is perpendicular to  $\mathbf{X}(t)$  and is of magnitude equal to the arc length

$$\delta s = |\mathbf{X}(t)| \delta\vartheta = |\mathbf{X}(t)| |\boldsymbol{\Omega}| \delta t. \quad (9.44)$$

We observe that the vector  $\boldsymbol{\Omega} \times \mathbf{X}(t)$  points in the same direction as  $\mathbf{X}(t + \delta t) - \mathbf{X}(t)$  and is of length  $|\mathbf{X}(t)| |\boldsymbol{\Omega}|$ . We conclude that

$$\mathbf{X}(t + \delta t) - \mathbf{X}(t) = \boldsymbol{\Omega} \times \mathbf{X}(t) \delta t. \quad (9.45)$$

Dividing through by  $\delta t$  and taking the limit  $\delta t \rightarrow 0$  gives

$$\frac{d\mathbf{X}}{dt} = \boldsymbol{\Omega} \times \mathbf{X} \quad \text{pure rotation.} \quad (9.46)$$

The proof for the case in which  $\boldsymbol{\Omega}$  has a component along  $\mathbf{X}$  is a straightforward generalization. The trajectory is still confined to a plane, but only the component of  $\boldsymbol{\Omega}$  normal to the trajectory generates rotation.

### 9.4.3 Changes to Cartesian basis vectors under rotation

We make use of the result (9.42) in many places when working with rotating physics. One place of particular note concerns the changes to unit vectors under rotation. Cartesian unit vectors exhibit changes solely due to pure rotations. With  $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$  as per a rotating spherical earth, the change in planetary Cartesian unit vectors under rotation is given by

$$\frac{d\hat{\mathbf{x}}}{dt} = \boldsymbol{\Omega} \times \hat{\mathbf{x}} = \Omega \hat{\mathbf{y}} \quad \text{and} \quad \frac{d\hat{\mathbf{y}}}{dt} = \boldsymbol{\Omega} \times \hat{\mathbf{y}} = -\Omega \hat{\mathbf{x}} \quad \text{and} \quad \frac{d\hat{\mathbf{z}}}{dt} = \boldsymbol{\Omega} \times \hat{\mathbf{z}} = 0. \quad (9.47)$$

### 9.4.4 Changes to polar coordinate unit vectors under rotation

As another example of how unit vectors change under rotation, consider the polar coordinates from Section 8.3 with rotation assumed to be about the vertical axis,  $\hat{\mathbf{z}}$ . In the horizontal plane we have the radial and angular unit vectors

$$\hat{\mathbf{r}} = \hat{\mathbf{x}} \cos \vartheta + \hat{\mathbf{y}} \sin \vartheta \quad (9.48a)$$

$$\hat{\boldsymbol{\vartheta}} = -\hat{\mathbf{x}} \sin \vartheta + \hat{\mathbf{y}} \cos \vartheta. \quad (9.48b)$$

We can directly verify that the time derivative of these unit vectors is given by

$$\frac{d\hat{\mathbf{r}}}{dt} = (\Omega + \dot{\vartheta}) \hat{\boldsymbol{\vartheta}} = (\Omega + \dot{\vartheta}) (\hat{\mathbf{z}} \times \hat{\mathbf{r}}) \quad (9.49a)$$

$$\frac{d\hat{\boldsymbol{\vartheta}}}{dt} = -(\Omega + \dot{\vartheta}) \hat{\mathbf{r}} = (\Omega + \dot{\vartheta}) (\hat{\mathbf{z}} \times \hat{\mathbf{r}}). \quad (9.49b)$$

Notice how these unit vectors change both due to the rotation of the reference frame,  $\Omega$ , plus the change in the angular position relative to the reference frame,  $\dot{\vartheta}$ . We thus see that unit vectors, such as those for spherical coordinates and cylindrical-polar coordinates, change due to the solid-body rotation, just like the Cartesian unit vectors. Additionally, non-Cartesian unit vectors change when their orientation is modified relative to the Cartesian coordinate axes at a rate distinct from the solid-body. This situation occurs when a trajectory moves relative to the solid-body. We further discuss this notion in Section 9.6.2 and detail the spherical coordinate case in Sections 9.9.2 and 9.11.

## 9.5 Some tensor algebra

In Part I of this book, we detailed the use of tensor analysis for geophysical motions. We here summarize some of the salient points that will be of use later in this chapter when dealing with spherical coordinates.

### 9.5.1 Why we need general tensors

Cartesian tensors are sufficient for many purposes of fluid mechanics, such as when using Cartesian coordinates for a tangent plane approximation to study geophysical fluid motion (e.g., Section 22.3). However, we make routine use of spherical coordinates when describing geophysical motion, and cylindrical-polar coordinates for studies of rotating tank experiments (see Section 31.7). Finally, we use generalized vertical coordinates in the description of stratified flows (Chapters 41, 42, and 43). The basis vectors for curvilinear coordinates and generalized vertical coordinates change direction when moving through space. In contrast, Cartesian basis vectors always point in the same direction. This distinction between the basis vectors is the key reason curvilinear coordinates and generalized vertical coordinates require a more general formalism than afforded by Cartesian tensors.

### 9.5.2 The coordinate representation of a vector

The coordinate representation of a vector follows from decomposing the vector into components aligned according to a set of basis vectors. In particular, the coordinate representation of the position vector is given by

$$\vec{X} = \sum_{a=1}^3 \xi^a \vec{e}_a = \xi^a \vec{e}_a, \quad (9.50)$$

where the Einstein summation convention is defined by the final equality. In this equation,

$$\vec{e}_a = (\vec{e}_1, \vec{e}_2, \vec{e}_3) \quad (9.51)$$

is a set of linearly independent basis vectors, and  $\xi^a$  are the corresponding coordinate representations of the position vector  $\vec{X}$ . The basis vectors may be normalized to unit magnitude, as in the case of Cartesian coordinates, or may be unnormalized as for spherical coordinates (see Section 8.2.2). Note that we commonly make use of the boldface notation for a vector rather than the arrowed symbol (Section 6.5)

$$\mathbf{X} = \vec{X} = \xi^a \vec{e}_a. \quad (9.52)$$

The basis vectors in equation (9.50) have a lower index while the coordinate representation of a vector has an upper index. Why? For arbitrary coordinates (e.g., spherical), we make a distinction between a coordinate representation with an index upstairs (contravariant) versus the downstairs (covariant) representation. Moving between the covariant and contravariant representations requires a metric tensor. For much of this book we can keep this mathematical framework at a modest distance, with exposure only in selected places. The key crutch we rely on is that the planet is assumed to be embedded in a background Euclidean space  $\mathbb{R}^3$ . That is, we are not considering the curved space-time of general relativity nor the marriage of space and time afforded by special relativity. These assumptions simplify our use of general tensors.

When working with general coordinates, it is necessary to distinguish between a basis vector  $\vec{e}_a$  and its dual partner known as a *one-form*,  $\tilde{e}^a$ . Duality here is defined using the familiar

(Euclidean) inner product that leads to the bi-orthogonality relation

$$\vec{e}_a \cdot \vec{e}^b = \delta_a^b, \quad (9.53)$$

with  $\delta_a^b$  the Kronecker delta tensor

$$\delta_a^b = \begin{cases} 1 & \text{if } b = a \\ 0 & \text{if } b \neq a. \end{cases} \quad (9.54)$$

In linear algebra, a row vector is dual to its column vector, with that analog appropriate for the present context. Cartesian basis vectors equal to the basis one-forms, in which case there is no distinction between contravariant and covariant. However, the distinction is important for the general coordinates used in geophysical fluids such as encountered in Chapters 8 and 41.

### 9.5.3 Transformation of a coordinate representation

A vector is a geometric object; i.e., a line determined by its length and direction. More general tensors are also geometric objects. The coordinate representation of a tensor is a subjective description of the object. More specifically, the coordinate representation of a vector as given by equation (9.50) does not alter the vector, it only alters the representation of the vector. Hence, we can represent the vector using arbitrary coordinates

$$\vec{X} = \xi^a \vec{e}_a = \xi^{\bar{a}} \vec{e}_{\bar{a}}, \quad (9.55)$$

where  $\xi^{\bar{a}}$  is the representation of the vector in a coordinate system defined by the basis vector  $\vec{e}_{\bar{a}}$ , whereas  $\xi^a$  is the representation in the unbarred coordinate system with basis vectors  $\vec{e}_a$ . In this chapter we choose the unbarred coordinates as planetary Cartesian and the barred coordinates as planetary spherical

$$(\xi^1, \xi^2, \xi^3) = (x, y, z) \quad \text{and} \quad (\xi^{\bar{1}}, \xi^{\bar{2}}, \xi^{\bar{3}}) = (r, \lambda, \phi), \quad (9.56)$$

with the coordinates related by (see Section 8.2 and Figure 8.1)

$$x = r \cos \phi \cos \lambda \quad \text{and} \quad y = r \cos \phi \sin \lambda \quad \text{and} \quad z = r \sin \phi. \quad (9.57)$$

The transformation of coordinate representations for a vector and basis vectors is provided by the transformation matrix and its inverse. For example, the relation between the coordinate representation of the velocity vector and acceleration vector, as well as the coordinate basis vectors, are given by

$$V^{\bar{a}} = \Lambda_{\bar{a}}^{\bar{a}} V^a \quad \text{and} \quad A^{\bar{a}} = \Lambda_{\bar{a}}^{\bar{a}} A^a \quad \text{and} \quad \vec{e}_{\bar{a}} = \Lambda_{\bar{a}}^a \vec{e}_a, \quad (9.58)$$

where the transformation matrix and its inverse are given by (see Section 8.2.1)

$$\Lambda_{\bar{a}}^a = \begin{bmatrix} \partial \xi^1 / \partial \xi^{\bar{1}} & \partial \xi^1 / \partial \xi^{\bar{2}} & \partial \xi^1 / \partial \xi^{\bar{3}} \\ \partial \xi^2 / \partial \xi^{\bar{1}} & \partial \xi^2 / \partial \xi^{\bar{2}} & \partial \xi^2 / \partial \xi^{\bar{3}} \\ \partial \xi^3 / \partial \xi^{\bar{1}} & \partial \xi^3 / \partial \xi^{\bar{2}} & \partial \xi^3 / \partial \xi^{\bar{3}} \end{bmatrix} = \begin{bmatrix} -r \cos \phi \sin \lambda & -r \sin \phi \cos \lambda & \cos \phi \cos \lambda \\ r \cos \phi \cos \lambda & -r \sin \phi \sin \lambda & \cos \phi \sin \lambda \\ 0 & r \cos \phi & \sin \phi \end{bmatrix} \quad (9.59)$$

$$\Lambda_{\bar{a}}^{\bar{a}} = \frac{1}{r^2 \cos \phi} \begin{bmatrix} -r \sin \lambda & r \cos \lambda & 0 \\ -r \cos \phi \sin \phi \cos \lambda & -r \cos \phi \sin \phi \sin \lambda & r \cos^2 \phi \\ r^2 \cos^2 \phi \cos \lambda & r^2 \cos^2 \phi \sin \lambda & r^2 \cos \phi \sin \phi \end{bmatrix}, \quad (9.60)$$

with

$$\Lambda^{\bar{a}}_a \Lambda^a_{\bar{b}} = \delta^{\bar{a}}_{\bar{b}} \quad \text{and} \quad \Lambda^a_{\bar{a}} \Lambda^{\bar{a}}_b = \delta^a_b. \quad (9.61)$$

We thus see that if we have a Cartesian representation to a vector, such as the velocity or acceleration, then we can use the above transformation rules to derive the spherical representation.

## 9.6 The velocity vector

The velocity is the time derivative of the position vector

$$\mathbf{V} = \frac{d\mathbf{X}}{dt}. \quad (9.62)$$

This equation is manifestly geometric in that the velocity at a space-time point is the tangent vector to the trajectory at that point. When expressing this relation using a coordinate representation we note that time dependence lives with both the coordinate representation of the position vector as well as the basis vectors

$$\mathbf{V} = \frac{d\mathbf{X}}{dt} = \frac{d(\xi^a \vec{e}_a)}{dt} = \frac{d\xi^a}{dt} \vec{e}_a + \xi^a \frac{d\vec{e}_a}{dt}. \quad (9.63)$$

### 9.6.1 Coordinate velocity

The first term on the right hand side of equation (9.63) is the velocity as measured within the chosen reference frame using the chosen coordinates

$$\mathbf{V}_{\text{coord}} \equiv \frac{d\xi^a}{dt} \vec{e}_a. \quad (9.64)$$

This is the contribution to velocity as measured in the reference frame that moves with the basis vectors. In the context of geophysical motions, this is the velocity measured in the rotating terrestrial reference frame.

### 9.6.2 Changes to the basis vectors

The second term on the right hand side of equation (9.63) arises from changes to the basis vectors. There are three means for a basis vector to change, and we encounter them when considering coordinate representations later in this chapter.

- **SOLID-BODY ROTATION:** For a solid-body rotation of the reference frame, the solid-body velocity is given by (see Section 9.4)

$$\mathbf{U}_{\text{solid}} = \boldsymbol{\Omega} \times \mathbf{X}. \quad (9.65)$$

- **ROTATION RELATIVE TO SOLID-BODY:** We can also change a vector through rotation by changing its direction at a rate that differs from the solid-body.
- **CHANGE IN MAGNITUDE:** Finally, if the basis vectors are not normalized, then they can change their magnitude during motion (stretching or compression).

## 9.7 Inertial acceleration and its decomposition

The inertial acceleration is given by the time derivative of the inertial velocity, which is the second derivative of the position vector

$$\mathbf{A} = \frac{d\mathbf{V}}{dt} = \frac{d^2\mathbf{X}}{dt^2}. \quad (9.66)$$

This equation is independent of any coordinate representation so that the physical and geometrical content are manifest. When introducing a coordinate representation, the resulting expression becomes subject to details of the chosen coordinates and those details possibly obscure the underlying geometric basis. Hence, it is important to keep the geometric form in mind when offering an interpretation for coordinate dependent terms that arise in a coordinate representation.

Introducing a coordinate representation  $\mathbf{X} = \xi^a \vec{e}_a$  into the acceleration (9.66), and making use of the chain rule, leads to

$$\mathbf{A} = \frac{d}{dt} \frac{d\mathbf{X}}{dt} \quad (9.67a)$$

$$= \frac{d}{dt} \frac{d(\xi^a \vec{e}_a)}{dt} \quad (9.67b)$$

$$= \frac{d}{dt} \left[ \frac{d\xi^a}{dt} \vec{e}_a + \xi^a \frac{d\vec{e}_a}{dt} \right] \quad (9.67c)$$

$$= \frac{d^2\xi^a}{dt^2} \vec{e}_a + 2 \frac{d\xi^a}{dt} \frac{d\vec{e}_a}{dt} + \xi^a \frac{d^2\vec{e}_a}{dt^2}. \quad (9.67d)$$

The first term on the right hand side is the acceleration of the coordinate representation as measured in the rotating reference frame

$$\mathbf{A}_{\text{coord}} \equiv \frac{d^2\xi^a}{dt^2} \vec{e}_a. \quad (9.68)$$

It is the acceleration measured by an observer in the rotating frame using coordinates  $\xi^a$ . The remaining two terms arise from changes to the basis vectors, and they give rise to the Coriolis and centrifugal accelerations associated with the rotating reference frame. In non-Cartesian coordinates, they also give rise to a “metric acceleration” arising from the change in directions of the unit vectors associated with motion of the particle relative to the rotating reference frame (Section 9.6.2).

Some presentations of the kinematic result (9.67d) suggest that the factor of two on the middle term (the Coriolis term) is mysterious. In fact, there is nothing mysterious. Rather, the factor of two merely results from the need to take two time derivatives of the basis vectors as part of a representation of acceleration.

## 9.8 Representing the position vector

We make use of some results from Section 8.2 relating Cartesian and spherical coordinates and as furthermore defined by Figure 8.1. Starting with the position vector, we introduce the *planetary* Cartesian basis vectors,  $(\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}})$ , and corresponding spherical basis vectors,  $(\hat{\lambda}, \hat{\phi}, \hat{\mathbf{r}})$ . We thus

have the suite of equivalent expressions for the position of a particle moving around the sphere

$$\mathbf{X} = x \hat{\mathbf{x}} + y \hat{\mathbf{y}} + z \hat{\mathbf{z}} \quad (9.69a)$$

$$= (r \cos \phi \cos \lambda) \hat{\mathbf{x}} + (r \cos \phi \sin \lambda) \hat{\mathbf{y}} + (r \sin \phi) \hat{\mathbf{z}} \quad (9.69b)$$

$$= r \hat{\mathbf{r}} \quad (9.69c)$$

$$= |\mathbf{X}| \hat{\mathbf{r}}. \quad (9.69d)$$

Note how the expression for the position vector is quite simple when written in spherical coordinates, as it is merely the distance from the origin with a direction that points radially from the origin to the particle.

## 9.9 Representing the velocity vector

As seen in Section 9.6, the inertial velocity vector has a coordinate representation written as

$$\mathbf{V} = \frac{d\mathbf{X}}{dt} = \frac{d(\xi^a \vec{e}_a)}{dt} = \frac{d\xi^a}{dt} \vec{e}_a + \xi^a \frac{d\vec{e}_a}{dt}. \quad (9.70)$$

Contributions arise from both the time changes in the coordinates,  $\xi^a$ , and time changes to the basis vectors,  $\vec{e}_a$ . We now consider the Cartesian and spherical forms for these changes.

### 9.9.1 Planetary Cartesian coordinate representation

The basis vectors for the Cartesian coordinates,  $(\vec{e}_1, \vec{e}_2, \vec{e}_3) = (\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}})$ , are normalized, so they do not change their magnitude. Furthermore, they move only through solid-body motion of the rotating reference frame. We refer to these coordinates as *planetary Cartesian coordinates* since they are oriented according to the rotating planet. In Section 22.3 we introduce the distinct *tangent plane Cartesian coordinates*. Tangent plane Cartesian coordinates are also moving with the rotating planet. Yet they are defined according to a tangent plane at a point on the surface of the sphere. It is important to distinguish these two uses for Cartesian coordinates in geophysical fluid mechanics.

The angular velocity is oriented around the polar axis

$$\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}, \quad (9.71)$$

so that the solid-body velocity only has components in the  $\hat{\mathbf{x}}$  and  $\hat{\mathbf{y}}$  directions

$$\mathbf{U}_{\text{solid}} = \boldsymbol{\Omega} \times \mathbf{X} = \Omega (-\hat{\mathbf{x}} y + \hat{\mathbf{y}} x). \quad (9.72)$$

The inertial velocity thus has the following representation in terms of planetary Cartesian coordinates

$$\mathbf{V} = \frac{d}{dt} [\hat{\mathbf{x}} x + \hat{\mathbf{y}} y + \hat{\mathbf{z}} z] \quad (9.73a)$$

$$= \left[ \hat{\mathbf{x}} \frac{dx}{dt} + \hat{\mathbf{y}} \frac{dy}{dt} + \hat{\mathbf{z}} \frac{dz}{dt} \right] + x \frac{d\hat{\mathbf{x}}}{dt} + y \frac{d\hat{\mathbf{y}}}{dt} + z \frac{d\hat{\mathbf{z}}}{dt} \quad (9.73b)$$

$$= \left[ -y \Omega + \frac{dx}{dt} \right] \hat{\mathbf{x}} + \left[ x \Omega + \frac{dy}{dt} \right] \hat{\mathbf{y}} + \frac{dz}{dt} \hat{\mathbf{z}} \quad (9.73c)$$

$$= \mathbf{V}_{\text{Cartesian}} + \boldsymbol{\Omega} \times \mathbf{X} \quad (9.73d)$$

$$= \mathbf{V}_{\text{Cartesian}} + \mathbf{U}_{\text{solid}}, \quad (9.73e)$$

where we defined the Cartesian velocity vector

$$\mathbf{V}_{\text{Cartesian}} \equiv \frac{dx}{dt} \hat{\mathbf{x}} + \frac{dy}{dt} \hat{\mathbf{y}} + \frac{dz}{dt} \hat{\mathbf{z}}, \quad (9.74)$$

which is the velocity as measured in the rotating reference frame when using planetary Cartesian coordinates. We also made use of equation (9.47) to express the time rate of change for the planetary Cartesian unit vectors, with this change arising solely from the planetary rotation. Note that the results here hold whether  $\Omega$  is constant or varying in time.

### 9.9.2 Planetary spherical coordinate representation

The position vector in the planetary spherical coordinate representation is given by

$$\mathbf{X} = r \hat{\mathbf{r}}. \quad (9.75)$$

The basis vector  $\hat{\mathbf{r}}$  is normalized, so that its evolution arises just from rotations. It can rotate either through solid-body motion of the rotating reference frame, or through changes in the spherical angles,  $\lambda, \phi$  relative to the rotating reference frame. We see these two forms of time changes by taking the time derivative of  $\hat{\mathbf{r}}$  as given by equation (8.30c)

$$\frac{d\hat{\mathbf{r}}}{dt} = \frac{d}{dt} [\hat{\mathbf{x}} \cos \lambda \cos \phi + \hat{\mathbf{y}} \sin \lambda \cos \phi + \hat{\mathbf{z}} \sin \phi]. \quad (9.76)$$

Expanding the right hand side leads to

$$\frac{d}{dt} [\hat{\mathbf{x}} \cos \lambda \cos \phi] = \frac{d\hat{\mathbf{x}}}{dt} \cos \lambda \cos \phi - \hat{\mathbf{x}} \dot{\lambda} \sin \lambda \cos \phi - \hat{\mathbf{x}} \dot{\phi} \cos \lambda \sin \phi \quad (9.77a)$$

$$\frac{d}{dt} [\hat{\mathbf{y}} \sin \lambda \cos \phi] = \frac{d\hat{\mathbf{y}}}{dt} \sin \lambda \cos \phi + \hat{\mathbf{y}} \dot{\lambda} \cos \lambda \cos \phi - \hat{\mathbf{y}} \dot{\phi} \sin \lambda \sin \phi \quad (9.77b)$$

$$\frac{d}{dt} [\hat{\mathbf{z}} \sin \phi] = \hat{\mathbf{z}} \dot{\phi} \cos \phi. \quad (9.77c)$$

Making use of equation (9.47) for the change in planetary Cartesian unit vectors due to rotation, and substituting the expressions (8.30a)-(8.30c) for the spherical unit vectors, leads to<sup>2</sup>

$$\frac{d\hat{\mathbf{r}}}{dt} = \cos \phi \left[ \frac{d\lambda}{dt} + \Omega \right] \hat{\mathbf{\lambda}} + \frac{d\phi}{dt} \hat{\mathbf{\phi}}. \quad (9.78)$$

Consequently, the inertial velocity has the following spherical coordinate representation

$$\mathbf{V} = \frac{d\mathbf{X}}{dt} \quad (9.79a)$$

$$= \frac{d(r \hat{\mathbf{r}})}{dt} \quad (9.79b)$$

$$= \frac{dr}{dt} \hat{\mathbf{r}} + r \frac{d\hat{\mathbf{r}}}{dt} \quad (9.79c)$$

$$= r_{\perp} \left[ \frac{d\lambda}{dt} + \Omega \right] \hat{\mathbf{\lambda}} + r \frac{d\phi}{dt} \hat{\mathbf{\phi}} + \frac{dr}{dt} \hat{\mathbf{r}} \quad (9.79d)$$

$$= (u + r_{\perp} \Omega) \hat{\mathbf{\lambda}} + v \hat{\mathbf{\phi}} + w \hat{\mathbf{r}} \quad (9.79e)$$

$$= \mathbf{V}_{\text{spherical}} + \mathbf{U}_{\text{solid}}. \quad (9.79f)$$

<sup>2</sup>The reader is encouraged to work through the details to derive equation (9.78).

In this equation we introduced the spherical coordinate velocity vector

$$\mathbf{V}_{\text{spherical}} = r_{\perp} \frac{d\lambda}{dt} \hat{\lambda} + r \frac{d\phi}{dt} \hat{\phi} + \frac{dr}{dt} \hat{r} = u \hat{\lambda} + v \hat{\phi} + w \hat{r}, \quad (9.80)$$

where

$$u = r_{\perp} \frac{d\lambda}{dt} \quad \text{and} \quad v = r \frac{d\phi}{dt} \quad \text{and} \quad w = \frac{dr}{dt}, \quad (9.81)$$

are components to the spherical velocity vector, and with

$$r_{\perp} = r \cos \phi \quad (9.82)$$

the distance to the polar axis. The spherical velocity,  $\mathbf{V}_{\text{spherical}}$ , is the velocity measured in the rotating reference frame when using planetary spherical coordinates. We also noted that the solid-body velocity has the spherical coordinate representation

$$\mathbf{U}_{\text{solid}} = \boldsymbol{\Omega} \times \mathbf{X} = r_{\perp} \Omega \hat{\lambda}. \quad (9.83)$$

That is, the solid-body velocity is purely zonal.

### 9.9.3 Transforming from Cartesian to spherical

We can make use of the tensor algebra from Section 9.5 to transform from the Cartesian representation of the velocity vector to the spherical representation. This approach leads to an equivalent result to that pursued thus far in this section, but it is somewhat more telescopic. In particular, we make use of the transformation rule (9.58) along with the transformation matrix (9.59) and its inverse (9.60) to have

$$V^{\bar{1}} = V^r = \Lambda_1^{\bar{1}} V^1 + \Lambda_2^{\bar{1}} V^2 + \Lambda_3^{\bar{1}} V^3 \quad (9.84a)$$

$$V^{\bar{2}} = V^{\lambda} = \Lambda_1^{\bar{2}} V^1 + \Lambda_2^{\bar{2}} V^2 + \Lambda_3^{\bar{2}} V^3 \quad (9.84b)$$

$$V^{\bar{3}} = V^{\phi} = \Lambda_1^{\bar{3}} V^1 + \Lambda_2^{\bar{3}} V^2 + \Lambda_3^{\bar{3}} V^3, \quad (9.84c)$$

where the Cartesian components are

$$V^1 = \dot{x} - \Omega y = \dot{r} \cos \phi \cos \lambda - r \dot{\phi} \sin \phi \cos \lambda - r (\dot{\lambda} + \Omega) \cos \phi \sin \lambda \quad (9.85a)$$

$$V^2 = \dot{y} + \Omega x = \dot{r} \cos \phi \sin \lambda - r \dot{\phi} \sin \phi \sin \lambda + r (\dot{\lambda} + \Omega) \cos \phi \cos \lambda \quad (9.85b)$$

$$V^3 = \dot{z} = \dot{r} \sin \phi + r \dot{\phi} \cos \phi. \quad (9.85c)$$

Making use of the inverse transformation matrix components  $\Lambda_b^{\bar{a}}$  given by equation (9.60), as well as the relation (9.58) between the coordinate basis vectors, leads to

$$\vec{V} = \mathbf{V} = V^{\bar{a}} \vec{e}_{\bar{a}} = r_{\perp} (\dot{\lambda} + \Omega) \hat{\lambda} + r \dot{\phi} \hat{\phi} + \dot{r} \hat{r}, \quad (9.86)$$

which is the same expression (9.79f) determined without the formalism of tensor algebra.

### 9.9.4 Axial angular momentum

As seen in Section 10.7, the zonal component of the inertial velocity equals to the axial angular momentum per unit mass

$$L^z = m \hat{\lambda} \cdot \mathbf{V} = m (u + r_{\perp} \Omega). \quad (9.87)$$

The distance to the rotational axis is given by  $r_\perp$ , and this is the *moment arm* for the axial angular momentum. For cases with rotational symmetry around polar axis, as for motion of a particle around a smooth sphere, the axial angular momentum is a constant of the motion. As discussed in Section 10.7, this conservation law offers a very important constraint on the particle trajectory and it plays a role in the motion of geophysical fluids (Section 17.4).

## 9.10 Planetary Cartesian representation of acceleration

The inertial acceleration vector is given by the second time derivative of the position vector

$$\mathbf{A} = \frac{d\mathbf{V}}{dt} = \frac{d^2\mathbf{X}}{dt^2}. \quad (9.88)$$

We here consider its representation using planetary Cartesian coordinates  $(x, y, z)$  and the Cartesian basis  $(\vec{e}_1, \vec{e}_2, \vec{e}_3) = (\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}})$ .

### 9.10.1 Planetary Cartesian representation

For our study of geophysical fluid motion, we assume the planetary angular velocity,  $\boldsymbol{\Omega}$ , is a constant in time

$$\frac{d\boldsymbol{\Omega}}{dt} = 0. \quad (9.89)$$

Making use of the results from Section 9.4 leads to

$$\frac{d\vec{e}_a}{dt} = \boldsymbol{\Omega} \times \vec{e}_a \quad (9.90)$$

and

$$\frac{d^2\vec{e}_a}{dt^2} = \frac{d}{dt}(\boldsymbol{\Omega} \times \vec{e}_a) = \boldsymbol{\Omega} \times \frac{d\vec{e}_a}{dt} = \boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \vec{e}_a), \quad (9.91)$$

which yields the inertial acceleration

$$\mathbf{A} = \frac{d}{dt} \frac{d\mathbf{X}}{dt} \quad (9.92a)$$

$$= \frac{d^2\xi^a}{dt^2} \vec{e}_a + 2 \frac{d\xi^a}{dt} (\boldsymbol{\Omega} \times \vec{e}_a) + \xi^a \boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \vec{e}_a) \quad (9.92b)$$

$$= \hat{\mathbf{x}} [\ddot{x} - 2\Omega\dot{y} - \Omega^2x] + \hat{\mathbf{y}} [\ddot{y} + 2\Omega\dot{x} - \Omega^2y] + \hat{\mathbf{z}} \ddot{z} \quad (9.92c)$$

$$= \ddot{x}\hat{\mathbf{x}} + \ddot{y}\hat{\mathbf{y}} + \ddot{z}\hat{\mathbf{z}} + 2\Omega(-\dot{y}\hat{\mathbf{x}} + \dot{x}\hat{\mathbf{y}}) - \Omega^2(x\hat{\mathbf{x}} + y\hat{\mathbf{y}}) \quad (9.92d)$$

$$= \mathbf{A}_{\text{Cartesian}} + 2\boldsymbol{\Omega} \times \mathbf{V}_{\text{Cartesian}} + \boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \mathbf{X}) \quad (9.92e)$$

$$= \mathbf{A}_{\text{Cartesian}} - \mathbf{A}_{\text{Coriolis}} - \mathbf{A}_{\text{centrifugal}}. \quad (9.92f)$$

The inertial acceleration is thus decomposed into three terms. The first contribution is the Cartesian expression

$$\mathbf{A}_{\text{Cartesian}} = \frac{d^2x}{dt^2} \hat{\mathbf{x}} + \frac{d^2y}{dt^2} \hat{\mathbf{y}} + \frac{d^2z}{dt^2} \hat{\mathbf{z}} = \ddot{x}\hat{\mathbf{x}} + \ddot{y}\hat{\mathbf{y}} + \ddot{z}\hat{\mathbf{z}}, \quad (9.93)$$

which is the coordinate acceleration measured in the rotating frame using planetary Cartesian coordinates. The second contribution on the right hand side of equation (9.92f) is minus the Coriolis acceleration

$$\mathbf{A}_{\text{Coriolis}} = -2\boldsymbol{\Omega} \times \mathbf{V}_{\text{Cartesian}}. \quad (9.94)$$

The Coriolis acceleration plays a fundamental role in geophysical fluid mechanics and will be central to our development in this book. One key feature of the Coriolis acceleration is that it vanishes when there is no motion relative to the rotating reference frame. The third contribution is the *centripetal acceleration*, which is also minus the *centrifugal acceleration*

$$\mathbf{A}_{\text{centripetal}} = -\mathbf{A}_{\text{centrifugal}} = \boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \mathbf{X}) = -\Omega^2 \mathbf{X}. \quad (9.95)$$

The centrifugal acceleration points outward from (perpendicular to) the polar axis of rotation whereas the centripetal acceleration points inward; they are action/reaction pairs. They can be written as the gradient of a potential

$$\mathbf{A}_{\text{centrifugal}} = -\nabla \Phi_{\text{centrifugal}} \quad (9.96)$$

with

$$-\Phi_{\text{centrifugal}} \equiv \frac{(\boldsymbol{\Omega} \times \mathbf{x}) \cdot (\boldsymbol{\Omega} \times \mathbf{x})}{2} = \frac{\Omega^2 r_{\perp}^2}{2} = \frac{(\Omega r \cos \phi)^2}{2} = \frac{\Omega^2 (x^2 + y^2)}{2}. \quad (9.97)$$

The centripetal acceleration (pointing towards the rotational axis) is that part of the inertial acceleration that keeps the rotating particle from flying away from the rotational axis. On a massive rotating sphere, the centripetal acceleration is provided by that component of the gravitational force (Section 9.12) directed towards the rotation axis. The centripetal acceleration's opposing partner, the centrifugal acceleration, is a non-inertial acceleration that accounts for the slight equatorial bulge of the planet. It is what pulls one outward from the center of a rotating merry-go-round.

### 9.10.2 Summary of acceleration representation

For the purpose of formulating the equation of motion in the rotating terrestrial frame, we write the rotating frame acceleration as

$$\mathbf{A}_{\text{Cartesian}} = \mathbf{A} + \mathbf{A}_{\text{Coriolis}} + \mathbf{A}_{\text{centrifugal}} \quad (9.98a)$$

$$= \mathbf{A} - 2\boldsymbol{\Omega} \times \mathbf{V}_{\text{Cartesian}} - \nabla \Phi_{\text{centrifugal}} \quad (9.98b)$$

and summarize the following accelerations (force per unit mass).

- **INERTIAL:** Newton's law of motion is formulated within an inertial reference frame. It is the inertial acceleration,  $\mathbf{A}$ , that is directly affected by forces such as gravitation.
- **CORIOLIS:** The Coriolis acceleration

$$\mathbf{A}_{\text{Coriolis}} = -2\boldsymbol{\Omega} \times \mathbf{V}_{\text{Cartesian}} = -2\Omega \hat{\mathbf{z}} \times \mathbf{V}_{\text{Cartesian}} = -2\Omega \left[ -\frac{dy}{dt} \hat{\mathbf{x}} + \frac{dx}{dt} \hat{\mathbf{y}} \right], \quad (9.99)$$

arises from our choice to describe motion within the rotating reference frame. The Coriolis acceleration gives rise to a rich suite of fundamentally new phenomena relative to non-rotating motion. It has components only in the horizontal planetary Cartesian plane spanned by the unit vectors  $(\hat{\mathbf{x}}, \hat{\mathbf{y}})$ . That is, the Coriolis acceleration occurs in a plane parallel to the equatorial plane. This geometric results is to be expected since the Coriolis acceleration arises from rotation about the polar  $\hat{\mathbf{z}}$  axis.

- **CENTRIFUGAL:** The centrifugal acceleration

$$\mathbf{A}_{\text{centrifugal}} = -\nabla \Phi_{\text{centrifugal}} = \Omega^2 \mathbf{r}_{\perp} = \Omega^2 (x \hat{\mathbf{x}} + y \hat{\mathbf{y}}) \quad (9.100)$$

is another term arising from the rotating reference frame. As for the Coriolis acceleration, the centrifugal acceleration has components only in the horizontal planetary Cartesian plane spanned by the unit vectors  $(\hat{\mathbf{x}}, \hat{\mathbf{y}})$ ; i.e., the centrifugal acceleration occurs in a plane parallel to the equatorial plane, which is again expected since the centrifugal acceleration arises from rotation about the polar axis. The centrifugal acceleration is directed outward from (perpendicular to) the polar axis of rotation. We see this orientation in Figure 9.6 to be discussed later. Furthermore, the centrifugal acceleration is nonzero even when the particle is fixed relative to the rotating planet, whereas the Coriolis acceleration is zero when the particle has zero motion relative to the planet.

The centrifugal acceleration can be written as the gradient of a scalar potential,  $\mathbf{A}_{\text{centrifugal}} = -\nabla\Phi_{\text{centrifugal}}$  where  $\Phi_{\text{centrifugal}} = -\Omega^2(x^2 + y^2)/2$  (equation (9.97)). Hence, the centrifugal acceleration can be combined with the gravitational acceleration in the equation of motion (see Section 9.12). The resulting “effective gravity” leads to a conservative force field that is modified relative to the central gravitational field of the non-rotating spherical planet. We detail these points in Section 9.12.4.

### 9.10.3 Further study

Section 3.5 of [Apel \(1987\)](#) offers an insightful presentation of the Coriolis acceleration. Visualizations from rotating tank experiments are useful to garner an intuitive understanding of the Coriolis acceleration. The first few minutes of [this video from Prof. Dave Fultz of the University of Chicago](#) is particularly insightful. We will further build up our understanding of the Coriolis acceleration as the book develops.

## 9.11 Spherical representation of acceleration

The spherical representation of the inertial velocity is given by equation (9.79f)

$$\mathbf{V} = \frac{d\mathbf{X}}{dt} = (u + r_{\perp}\Omega)\hat{\lambda} + v\hat{\phi} + w\hat{r} = \mathbf{V}_{\text{sphere}} + r_{\perp}\Omega\hat{\lambda}, \quad (9.101)$$

where we introduced the spherical velocity from equation (9.81)

$$\mathbf{V}_{\text{sphere}} \equiv u\hat{\lambda} + v\hat{\phi} + w\hat{r}. \quad (9.102)$$

We will also make use of the notation for the zonal component of the inertial velocity,

$$u_I = u + r_{\perp}\Omega. \quad (9.103)$$

Just as for computing the inertial velocity vector, the inertial acceleration must take into account changes in both the spherical coordinates and spherical basis vectors

$$\mathbf{A} = \frac{d}{dt} \left( u_I \hat{\lambda} + v\hat{\phi} + w\hat{r} \right) \quad (9.104a)$$

$$= \frac{du_I}{dt}\hat{\lambda} + \frac{dv}{dt}\hat{\phi} + \frac{dw}{dt}\hat{r} + u_I \frac{d\hat{\lambda}}{dt} + v \frac{d\hat{\phi}}{dt} + w \frac{d\hat{r}}{dt}. \quad (9.104b)$$

The spherical unit vectors change due to both the solid-body rotation of the rotating reference frame, plus motion of the particle relative to the rotating frame. Making use of the expressions

given in Section (8.2.2), a bit of algebra yields the time derivatives

$$\frac{d\hat{\lambda}}{dt} = \left[ \Omega + \frac{d\lambda}{dt} \right] (\hat{\phi} \sin \phi - \hat{r} \cos \phi) \quad (9.105)$$

$$\frac{d\hat{\phi}}{dt} = -\hat{\lambda} \left[ \Omega + \frac{d\lambda}{dt} \right] \sin \phi - \hat{r} \dot{\phi} \quad (9.106)$$

$$\frac{d\hat{r}}{dt} = \hat{\lambda} \left[ \frac{d\lambda}{dt} + \Omega \right] \cos \phi + \frac{d\phi}{dt} \hat{\phi}. \quad (9.107)$$

We are thus led to the inertial acceleration components

$$\mathbf{A} \cdot \hat{\lambda} = \frac{du_I}{dt} + \left[ \frac{d\lambda}{dt} + \Omega \right] (w \cos \phi - v \sin \phi) \quad (9.108a)$$

$$\mathbf{A} \cdot \hat{\phi} = \frac{dv}{dt} + \left[ \frac{d\lambda}{dt} + \Omega \right] u_I \sin \phi + w \frac{d\phi}{dt} \quad (9.108b)$$

$$\mathbf{A} \cdot \hat{r} = \frac{dw}{dt} - \left[ \frac{d\lambda}{dt} + \Omega \right] u_I \cos \phi - v \frac{d\phi}{dt}. \quad (9.108c)$$

Use of the identities

$$u = r_{\perp} \frac{d\lambda}{dt} \quad \text{and} \quad u_I = u + r_{\perp} \Omega \quad \text{and} \quad \frac{du_I}{dt} = \frac{du}{dt} + \Omega (w \cos \phi - v \sin \phi) \quad (9.109)$$

and some reorganization leads to the spherical coordinate representation of the inertial acceleration

$$\begin{aligned} \mathbf{A} = & \hat{\lambda} \left[ \frac{du}{dt} + \frac{u(w - v \tan \phi)}{r} + 2\Omega(w \cos \phi - v \sin \phi) \right] \\ & + \hat{\phi} \left[ \frac{dv}{dt} + \frac{v w + u^2 \tan \phi}{r} + 2\Omega u \sin \phi + r_{\perp} \Omega^2 \sin \phi \right] \\ & + \hat{r} \left[ \frac{dw}{dt} - \frac{u^2 + v^2}{r} - 2\Omega u \cos \phi - r_{\perp} \Omega^2 \cos \phi \right]. \end{aligned} \quad (9.110)$$

When encountering this expression for the first time it can be rather intimidating. The reader is encouraged to remember the underlying kinematic origin of the various terms, in which case the expression can be seen as both familiar and aesthetically pleasing.

### 9.11.1 Transforming from Cartesian to spherical

As in Section 9.9.3, we can make use of the tensor algebra from Section 9.5 to transform from the Cartesian representation of the acceleration vector to the spherical representation. Following the same steps as for the velocity leads to

$$A^{\bar{a}} = \Lambda_{\bar{a}}^a A^a \quad (9.111)$$

where the Cartesian components to the inertial acceleration are

$$A^1 = \ddot{x} - 2\Omega \dot{y} - \Omega^2 x \quad (9.112a)$$

$$A^2 = \ddot{y} + 2\Omega \dot{x} - \Omega^2 y \quad (9.112b)$$

$$A^3 = \ddot{z}. \quad (9.112c)$$

Making use of the coordinate transformation (9.57) allows us to express these Cartesian components of the acceleration in terms of spherical coordinates. Then we make use of the inverse transformation matrix components  $\Lambda^{\bar{a}}_b$  given by equation (9.60), as well as the relation (9.58) between the coordinate basis vectors, which leads to

$$\vec{A} = \mathbf{A} = A^a \vec{e}_a = A^{\bar{a}} \vec{e}_{\bar{a}} \quad (9.113)$$

with the spherical coordinate representation given by equation (9.110) as derived without the formalism of tensor algebra. Both approaches require algebraic manipulations, so that it is useful to have two approaches to double-check results.

### 9.11.2 Decomposing the acceleration

We decompose the inertial acceleration (9.110) into the following terms

$$\mathbf{A} = \mathbf{A}_{\text{sphere}} + \mathbf{A}_{\text{metric}} - \mathbf{A}_{\text{Coriolis}} - \mathbf{A}_{\text{centrifugal}}, \quad (9.114)$$

with signs chosen so that in the rotating frame the acceleration is written

$$\underbrace{\mathbf{A}_{\text{sphere}} + \mathbf{A}_{\text{metric}}}_{\text{net spherical acceleration}} = \mathbf{A} + \mathbf{A}_{\text{Coriolis}} + \mathbf{A}_{\text{centrifugal}}. \quad (9.115)$$

We identify the net spherical acceleration as the sum of the coordinate acceleration and metric acceleration. In the absence of rotation, this sum provides an expression for the inertial acceleration as represented by spherical coordinates. The Coriolis and centrifugal terms arise from rotation.

### 9.11.3 Spherical coordinate acceleration

The spherical coordinate acceleration is given by the time change in the spherical velocity components

$$\mathbf{A}_{\text{sphere}} = \frac{du}{dt} \hat{\lambda} + \frac{dv}{dt} \hat{\phi} + \frac{dw}{dt} \hat{r}. \quad (9.116)$$

This term has no contribution from changes to the spherical unit vectors.

### 9.11.4 Metric acceleration

We define the metric acceleration as that contribution to the acceleration arising from the time dependence of the spherical unit vectors that appears when taking the time derivative of the velocity vector. For spherical coordinates we have

$$\mathbf{A}_{\text{metric}} = \hat{\lambda} \left[ \frac{u(w - v \tan \phi)}{r} \right] + \hat{\phi} \left[ \frac{v w + u^2 \tan \phi}{r} \right] - \hat{r} \left[ \frac{u^2 + v^2}{r} \right] \quad (9.117a)$$

$$= \hat{\lambda} \left[ \frac{u(w \cos \phi - v \sin \phi)}{r \cos \phi} \right] + \hat{\phi} \left[ \frac{v w \cos \phi + u^2 \sin \phi}{r \cos \phi} \right] - \hat{r} \left[ \frac{u^2 + v^2}{r} \right] \quad (9.117b)$$

$$= \frac{1}{r} [u \tan \phi (\hat{r} \times \mathbf{V}_{\text{sphere}}) + w \mathbf{U}_{\text{sphere}} - \hat{r} \mathbf{U}_{\text{sphere}} \cdot \mathbf{U}_{\text{sphere}}], \quad (9.117c)$$

where we wrote the horizontal (angular) and vertical (radial) components of the spherical velocity according to

$$\mathbf{V}_{\text{sphere}} = \mathbf{U}_{\text{sphere}} + \hat{r} w = \hat{\lambda} u + \hat{\phi} v + \hat{r} w. \quad (9.118)$$

Note that

$$\mathbf{V}_{\text{sphere}} \cdot \mathbf{A}_{\text{metric}} = 0, \quad (9.119)$$

so that the metric acceleration is orthogonal to the spherical velocity, in which case with (see equation (9.79f))  $\mathbf{V} = \mathbf{V}_{\text{sphere}} + r_{\perp} \Omega \hat{\lambda}$  we have

$$\mathbf{V} \cdot \mathbf{A}_{\text{metric}} = \Omega u (-v \sin \phi + w \cos \phi). \quad (9.120)$$

Furthermore, the metric acceleration vanishes when the curvature of the sphere vanishes (i.e.,  $r \rightarrow \infty$ ), as per a flat plane.

### 9.11.5 Centrifugal acceleration

The spherical coordinate representation of the centrifugal acceleration is given by

$$\mathbf{A}_{\text{centrifugal}} = -\nabla \Phi_{\text{centrifugal}} = \Omega^2 (x \hat{x} + y \hat{y}) = r_{\perp} \Omega^2 (-\hat{\phi} \sin \phi + \hat{r} \cos \phi). \quad (9.121)$$

The centrifugal acceleration points outward from the axis of rotation (see Figure 9.6 to be discussed later), so that it has no component in the longitudinal direction. Furthermore, note that

$$\mathbf{V} \cdot \mathbf{A}_{\text{centrifugal}} = \mathbf{V}_{\text{sphere}} \cdot \mathbf{A}_{\text{centrifugal}} = r_{\perp} \Omega^2 (-v \sin \phi + w \cos \phi). \quad (9.122)$$

### 9.11.6 Coriolis acceleration

The spherical coordinate representation of the Coriolis acceleration makes use of the spherical representation of the earth's angular velocity

$$\boldsymbol{\Omega} = \Omega \hat{z} = \Omega (\hat{\phi} \cos \phi + \hat{r} \sin \phi) \quad (9.123)$$

to reach the form

$$\mathbf{A}_{\text{Coriolis}} = -2 \boldsymbol{\Omega} \times \mathbf{V}_{\text{sphere}} \quad (9.124a)$$

$$= -2 \Omega (\hat{\phi} \cos \phi + \hat{r} \sin \phi) \times \mathbf{V}_{\text{sphere}} \quad (9.124b)$$

$$= -2 \Omega (\hat{\phi} \cos \phi + \hat{r} \sin \phi) \times (u \hat{\lambda} + v \hat{\phi} + w \hat{r}) \quad (9.124c)$$

$$= -2 \Omega [\hat{\lambda} (w \cos \phi - v \sin \phi) + \hat{\phi} u \sin \phi - \hat{r} u \cos \phi]. \quad (9.124d)$$

As for the metric acceleration, we note that the Coriolis acceleration is orthogonal to the spherical velocity

$$\mathbf{V}_{\text{sphere}} \cdot \mathbf{A}_{\text{Coriolis}} = 0, \quad (9.125)$$

so that

$$\mathbf{V} \cdot \mathbf{A}_{\text{Coriolis}} = 2 r_{\perp} \Omega^2 (v \sin \phi - w \cos \phi). \quad (9.126)$$

We find it convenient to introduce a shorthand notation

$$\mathbf{f} = (2 \Omega \sin \phi) \hat{r} \quad \text{and} \quad \mathbf{f}^* = (2 \Omega \cos \phi) \hat{\phi}, \quad (9.127)$$

so that the Coriolis acceleration takes the form

$$\mathbf{A}_{\text{Coriolis}} = -(\mathbf{f} + \mathbf{f}^*) \times \mathbf{V}_{\text{sphere}}. \quad (9.128)$$

There are two contributions to the Coriolis acceleration: one from the radial and one from the meridional component of the earth's rotation vector.

### 9.11.7 Coriolis acceleration for large-scale motions

Let us again write the Coriolis acceleration in equation (9.124d), only now underlining two terms

$$\mathbf{A}_{\text{Coriolis}} = -2\Omega \left[ \hat{\lambda} (\underline{w} \cos \phi - v \sin \phi) + \hat{\phi} u \sin \phi - \hat{r} \underline{u} \cos \phi \right]. \quad (9.129)$$

For many applications in geophysical fluid dynamics, the term  $\hat{r}(2\Omega u \cos \phi)$  is much smaller than the competing gravitational acceleration that also contributes to the radial acceleration, thus prompting  $\hat{r}(2\Omega u \cos \phi)$  to be dropped from the  $\hat{r}$  equation of motion.<sup>3</sup> Furthermore, the vertical velocity term is generally much smaller than the horizontal velocity term appearing in the  $\hat{\lambda}$  component. Dropping these two terms results in the form for the Coriolis acceleration used for large-scale dynamics, such as when considering the hydrostatic primitive equations for geophysical fluids (Section 22.1)

$$\mathbf{A}_{\text{Coriolis}}^{\text{large-scale}} \equiv -2\Omega \sin \phi (-\hat{\lambda} v + \hat{\phi} u) \equiv -f \hat{r} \times \mathbf{V}_{\text{sphere}}. \quad (9.130)$$

For the last equality we introduced the Coriolis parameter

$$f \equiv 2\Omega \sin \phi. \quad (9.131)$$

As illustrated in Figure 9.5, we see that it is the radial (i.e., the local vertical) component of the earth's angular rotation that plays the most important role in large-scale geophysical fluid mechanics

$$\boldsymbol{\Omega} \cdot \hat{r} = \Omega \hat{z} \cdot \hat{r} = [\Omega (\hat{\phi} \cos \phi + \hat{r} \sin \phi)] \cdot \hat{r} = \Omega \sin \phi \hat{r} = (f/2) \hat{r}. \quad (9.132)$$

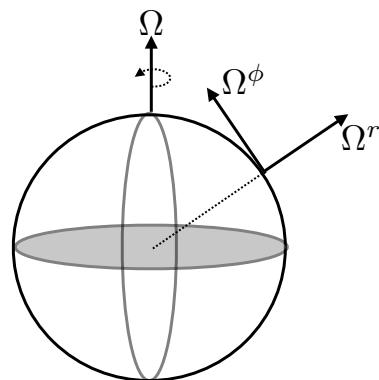


FIGURE 9.5: This figure illustrates the two components of the earth's rotational velocity,  $\boldsymbol{\Omega} = \Omega \hat{z} = \Omega (\hat{\phi} \cos \phi + \hat{r} \sin \phi)$ . The radial component (also known as the local vertical component),  $\boldsymbol{\Omega} \approx \Omega \sin \phi \hat{r}$ , is the most important component for large scale geophysical fluid dynamics.

## 9.12 Newtonian gravity

Thus far we have focused on kinematics of a particle moving around a rotating sphere. We now acknowledge that the particle is moving in the gravitational field of the planet. The gravitational

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<sup>3</sup>The term  $\hat{r}(2\Omega u \cos \phi)$  is called the Eötvös correction in the study of marine gravity.

force acting on the particle is the only inertial force felt by the point particle. Since the point particle contains no internal structure and it has no surface area, the total energy for the particle equals to the mechanical energy (Chapter 10). We here discuss the gravitational potential energy and the associated gravitational force, all within the context of Newtonian mechanics.

### 9.12.1 Newtonian gravity from Poisson's equation

The Newtonian gravitational potential,  $\Phi$ , in the presence of a mass distribution with density,  $\rho$ , satisfies Poisson's equation (see Section 3.5)

$$\nabla^2 \Phi = 4\pi G \rho, \quad (9.133)$$

where

$$G = 6.674 \times 10^{-11} \text{ N m}^2 \text{ kg}^{-2} = 6.674 \times 10^{-11} \text{ m}^3 \text{ kg}^{-1} \text{ s}^{-2} \quad (9.134)$$

is Newton's gravitational constant. Gravity is a conservative force, so that the gradient of the gravitational potential gives the gravitational acceleration

$$\mathbf{g} = -\nabla \Phi. \quad (9.135)$$

The gravitational potential has dimensions of  $\text{L}^2 \text{T}^{-2}$  so that its gradient indeed has the dimensions of acceleration,  $\text{L T}^{-2}$ . Note that the gravitational potential responds instantaneously to any changes in the mass distribution. It took a few centuries, and the genius of Einstein, to provide a local connection between mass and gravity as rendered by space-time curvature and gravitational waves.

A volume integral of Poisson's equation (9.133) over a region in space leads to

$$\int_{\mathcal{R}} \nabla^2 \Phi \, dV = 4\pi G \int_{\mathcal{R}} \rho \, dV. \quad (9.136)$$

The integral on the right hand side is the mass contained in the region,

$$M = \int_{\mathcal{R}} \rho \, dV, \quad (9.137)$$

whereas the divergence theorem (Section 2.7) allows us to write the left hand side as a surface integral

$$\int_{\partial\mathcal{R}} \nabla \Phi \cdot \hat{\mathbf{n}} \, dS = 4\pi G M. \quad (9.138)$$

We now consider the special case of a spherical mass distribution as viewed from a point outside of the mass.

### 9.12.2 Gravitational field for a spherical earth

In this book we assume the mass density of the planet to be spherically symmetric, in which case the gravitational potential is a function only of the radial distance from the center of the mass distribution,  $\Phi = \Phi(r)$ . Letting the integration region  $\mathcal{R}$  be a sphere of radius  $r > R_e$ , where  $R_e$  is the radius of the planet, and making use of spherical coordinates from Section 8.2.8, brings equation (9.138) to

$$4\pi r^2 \frac{\partial \Phi}{\partial r} = 4\pi G M. \quad (9.139)$$

Integration leads to the gravitational potential for an arbitrary point outside the spherically symmetric mass distribution

$$\Phi_e = -\frac{GM}{r}, \quad (9.140)$$

where we set the integration constant to zero. We see that when sampling the gravity field at a radius equal to or larger than the spherical planet radius, the gravitational potential is identical to that of a point mass at the origin. The gradient of the gravitational potential (9.140) yields the gravitational acceleration

$$\mathbf{g}_e = -\nabla\Phi_e = -\frac{GM}{r^2}\hat{\mathbf{r}} \quad (9.141)$$

along with the gravitational force acting on a point particle of mass  $m$

$$\mathbf{F}_{\text{gravity}} = m\mathbf{g}_e = -m\nabla\Phi_e. \quad (9.142)$$

Furthermore, the gravitational potential energy of the particle (dimensions  $M L^2 T^{-2}$ ) is given by

$$P = m\Phi_e. \quad (9.143)$$

### 9.12.3 Approximate gravitational acceleration

For most applications of atmospheric and oceanic fluid dynamics, it is sufficient to assume the gravitational acceleration is constant and equal to its value at the earth's surface. This assumption holds so long as the radial position of the particle is a distance from the earth surface that is small relative to the earth radius. We generally make this assumption throughout this book.<sup>4</sup> In this case we can assume the earth's gravitational acceleration,  $g_e$ , is a constant so that

$$\mathbf{g}_e = -g_e\hat{\mathbf{r}}, \quad (9.144)$$

where

$$g_e = \frac{GM_e}{R_e^2} \approx 9.8 \text{ m s}^{-2}. \quad (9.145)$$

To reach this value, we assumed a sphere of mass equal to the earth mass

$$M_e = 5.977 \times 10^{24} \text{ kg}, \quad (9.146)$$

and radius

$$R_e = 6.371 \times 10^6 \text{ m} \quad (9.147)$$

determined so that the sphere has the same volume as the earth.

The corresponding gravitational potential for the particle is given by

$$\Phi_e = g_e r, \quad (9.148)$$

with the gravitational acceleration

$$\mathbf{g}_e = -\nabla\Phi_e = -g_e\hat{\mathbf{r}}, \quad (9.149)$$

---

<sup>4</sup>The assumption of constant gravitational field is not appropriate when considering details of oceanic or atmospheric tidal motions or when aiming for precise measures of sea level. We consider more general gravitational fields in Chapter 28.

and the gravitational potential energy

$$m \Phi_e = m g_e r. \quad (9.150)$$

We emphasize that the expression for the gravitational potential, (9.148), and potential energy, (9.150), are accurate only so long as the radial position of the particle is a distance from the earth surface that is small relative to the earth radius. Furthermore, note that the approximate gravitational potential (9.148) is positive whereas the unapproximated potential (9.140) is negative. However, the absolute zero of the potential has no physical significance. Instead, what is relevant is the change between two points in space, with both potentials increasing when moving away from the earth center.

#### 9.12.4 Effective gravitational force from the geopotential

We can combine the potential for the planetary centrifugal acceleration as given by equation (9.97) with the gravitational potential (9.140), thus resulting in the *geopotential*

$$\Phi = r [g_e - U_{\text{solid}}^2 / (2r)]. \quad (9.151)$$

Again, this form for the geopotential is relevant for motion that is close enough to the earth surface that we can assume the earth's gravitational acceleration,  $g_e$ , is constant as discussed in Section 9.12.3. In Exercise 9.6 we examine the geopotential when this assumption is not made.

The contribution from the planetary centrifugal term in the geopotential (9.151) can be estimated by making use of terrestrial values, in which  $R = R_e = 6.371 \times 10^6$  m (equation (9.147)), and  $\Omega_e = 7.292 \times 10^{-5}$  s<sup>-1</sup> (Section 9.2). The planetary centrifugal term is its largest at the equator,  $\phi = 0$ , where

$$\frac{U_{\text{solid}}^2}{2R_e} \approx 0.017 \text{ m s}^{-2}, \quad (9.152)$$

so that the ratio of the gravitational to centrifugal accelerations is (at most)

$$\frac{g_e}{U_{\text{solid}}^2 / (2R_e)} = \frac{M_e G / R_e^2}{\Omega_e^2 R_e / 2} \approx 576. \quad (9.153)$$

The geopotential is thus dominated by the earth's gravitational potential. Even so, the centrifugal acceleration leads to a slight equatorial bulge on the earth. To account for this slight non-sphericity, geophysical fluid models generally interpret the radial direction  $\hat{\mathbf{r}}$  as pointing parallel to  $\nabla\Phi$  rather than parallel to  $\nabla\Phi_e$ . We have more to say on this topic in Section 9.13.3.

#### 9.12.5 Further study

Newton's gravitational law is standard material from freshman physics. Some commonly used physical properties of the earth are summarized in Appendix Two of [Gill \(1982\)](#).

### 9.13 Newton's law of motion

As seen in Section 9.1, Newton's law of motion says that in an inertial reference frame, temporal changes to the linear momentum arise only from externally applied forces. With gravity the only inertial force acting on the constant mass particle, Newton's equation of motion says that

$$m \mathbf{A} = -m \nabla\Phi_e. \quad (9.154)$$

This is a relatively simple equation of motion. However, it becomes more complex, yet useful for practical purposes, when moving to the rotating reference frame of terrestrial observers and furthermore when represented using spherical coordinates.

### 9.13.1 Cartesian coordinate representation

The inertial acceleration using planetary Cartesian coordinates is given by equation (9.98b)

$$\mathbf{A} = \mathbf{A}_{\text{Cartesian}} - \mathbf{A}_{\text{Coriolis}} - \mathbf{A}_{\text{centrifugal}} \quad (9.155a)$$

$$= \mathbf{A}_{\text{Cartesian}} + 2\boldsymbol{\Omega} \times \mathbf{V}_{\text{Cartesian}} + \nabla\Phi_{\text{centrifugal}}, \quad (9.155b)$$

so that the rotating frame Cartesian equation of motion is given by

$$\mathbf{A}_{\text{Cartesian}} = -\nabla\Phi_e - 2\boldsymbol{\Omega} \times \mathbf{V}_{\text{Cartesian}} - \nabla\Phi_{\text{centrifugal}} \quad (9.156a)$$

$$= -2\boldsymbol{\Omega} \times \mathbf{V}_{\text{Cartesian}} - \nabla\Phi, \quad (9.156b)$$

where the geopotential is the sum of the gravitational and centrifugal potentials (equation (9.151))

$$\Phi = \Phi_e + \Phi_{\text{centrifugal}}. \quad (9.157)$$

We can write the equation of motion in component form by exposing indices (Cartesian tensors) and using a dot for time derivative

$$\ddot{X}_a + 2\epsilon_{abc}\boldsymbol{\Omega}_b\dot{X}_c = -\partial_a\Phi. \quad (9.158)$$

We can write this equation in the standard vector form within the rotating reference frame

$$\frac{d^2\mathbf{X}}{dt^2} + 2\boldsymbol{\Omega} \times \dot{\mathbf{X}} = -\nabla\Phi. \quad (9.159)$$

Note that the basis vectors need not be time differentiated again since their change has already been taken care of when exposing the Coriolis and centrifugal accelerations. This equation of motion is the standard form that will recur for a fluid, with the addition of contact forces from pressure and friction (Chapter 17).

Since the rotation of the reference frame is assumed to be constant in time, the equation of motion (9.159) can be written

$$\frac{d\mathbf{M}}{dt} = \frac{d}{dt}(\mathbf{V}_{\text{Cartesian}} + 2\boldsymbol{\Omega} \times \mathbf{X}) = -\nabla\Phi, \quad (9.160)$$

where we introduced the *potential momentum* per mass

$$\mathbf{M} = \mathbf{V}_{\text{Cartesian}} + 2\boldsymbol{\Omega} \times \mathbf{X}. \quad (9.161)$$

We further discuss potential momentum in Section 10.4.

### 9.13.2 Spherical coordinate representation

We now make use of the acceleration written in planetary spherical coordinates as given in Section 9.11

$$\mathbf{A}_{\text{sphere}} + \mathbf{A}_{\text{metric}} = \mathbf{A}_{\text{Coriolis}} + \mathbf{A} + \mathbf{A}_{\text{centrifugal}} = -2\boldsymbol{\Omega} \times \mathbf{V}_{\text{sphere}} - \nabla\Phi. \quad (9.162)$$

The effective gravitational force is not a central force due to the contribution from the centrifugal acceleration. We see this fact more explicitly by using the equations in Section 9.11 to write the spherical equations of motion

$$\dot{u} + \frac{u(w - v \tan \phi)}{r} + 2\Omega(w \cos \phi - v \sin \phi) = 0 \quad (9.163)$$

$$\dot{v} + \frac{v w + u^2 \tan \phi}{r} + 2\Omega u \sin \phi = -r_{\perp} \Omega^2 \sin \phi \quad (9.164)$$

$$\dot{w} - \frac{u^2 + v^2}{r} - 2\Omega u \cos \phi = r_{\perp} \Omega^2 \cos \phi - g_e. \quad (9.165)$$

The  $\Omega^2$  term in both the meridional equation, (9.164), and the radial equation, (9.165), are the two components of the planetary centrifugal acceleration,  $\mathbf{A}_{\text{centrifugal}} = r_{\perp} \Omega^2 (-\hat{\phi} \sin \phi + \hat{r} \cos \phi)$ . The centrifugal acceleration is directed outward from the planetary axis of rotation, and it is balanced by an inward directed planetary centripetal acceleration provided by that portion of the gravitational acceleration directed oppositely to the centrifugal. Notably, a particle initially at rest on a smooth spherical planet will accelerate meridionally toward the equator due to the meridional component of the centrifugal acceleration (from equation (9.164) we find  $\dot{v} = -r_{\perp} \Omega^2 \sin \phi$ ).

Imagine setting the centripetal acceleration to zero, in which case the particle would still feel the central force from gravity but its trajectory would differ. As seen in Section 9.12.4, the earth's gravitational acceleration is much larger than the planetary centrifugal acceleration, so that in the absence of the planetary centrifugal acceleration the particle would still be bound to the planet. But in more extreme conditions where the rotational rate is much higher (e.g., a rotating neutron star), removing the centripetal acceleration causes a huge modification to the particle trajectory. Indeed, with enough rotation, the particle can overcome gravitational effects from the planet to leave its orbit.

### 9.13.3 Geopotential coordinate representation

As we saw in Section 9.12.2, the radius of a sphere that best fits the volume of the earth is given by  $R_e = 6.371 \times 10^6$  m. The non-central nature of the effective gravitational force (arising from central gravity plus planetary centrifugal) leads to an oblate spheroidal shape for planets such as the earth. The result is a distinction between the earth's equatorial and polar radii (Appendix Two of [Gill \(1982\)](#))

$$R_{\text{equator}} = 6.378 \times 10^6 \text{ m} \quad \text{and} \quad R_{\text{pole}} = 6.357 \times 10^6 \text{ m}, \quad (9.166)$$

with a corresponding ratio

$$1 - \frac{R_{\text{pole}}}{R_{\text{equator}}} \approx 3 \times 10^{-3}. \quad (9.167)$$

An oblate spheroid shape does a better job fitting the actual earth shape than a sphere, thus motivating the use of oblate spheroid coordinates for describing planetary scale mechanics. In this case, the radial coordinate is constant on the oblate spheroid shaped geopotential, and the effective gravitational acceleration is precisely aligned with the geopotential direction.

Even though oblate spheroidal coordinates are better than spherical for describing geopotentials, it is possible, to a high degree of accuracy, to describe the earth's geometry as spherical. Doing so simplifies the mathematics since oblate spheroidal coordinates are less convenient and less familiar than standard spherical coordinates. We are thus led to assume that the radial coordinate measures distances perpendicular to the geopotential, yet to use geometric/metric functions based on spherical coordinates. The error in this approach is small for the earth, and

well worth the price since we no longer have a component to the effective gravitational force that is within the surface.

We illustrate the change in coordinates in Figure 9.6, with the figure caption also explaining how the force balances are reorganized. Absorbing the centrifugal term into an effective gravitational potential then leads to the effective gravitational acceleration vector

$$-\nabla\Phi = -g \hat{r}, \quad (9.168)$$

with  $g$  the effective gravitational acceleration. Using this convention, the particle equations of motion take the following form

$$\dot{u} + \frac{u(w - v \tan \phi)}{r} + 2\Omega(w \cos \phi - v \sin \phi) = 0 \quad (9.169)$$

$$\dot{v} + \frac{v w + u^2 \tan \phi}{r} + 2\Omega u \sin \phi = 0 \quad (9.170)$$

$$\dot{w} - \frac{u^2 + v^2}{r} - 2\Omega u \cos \phi = -g. \quad (9.171)$$

Notably, in geopotential vertical coordinates the effective gravitational acceleration only impacts the radial equation of motion.

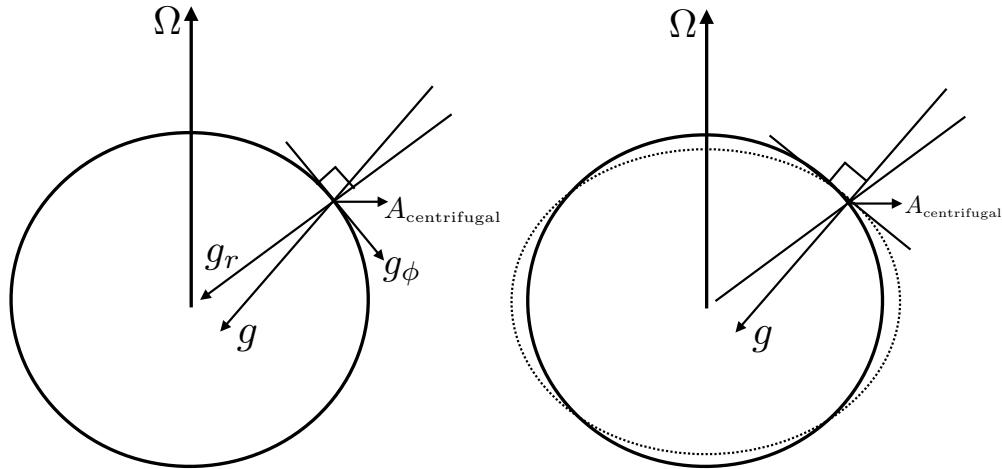


FIGURE 9.6: This figure illustrates the spherical (left panel) versus geopotential (right panel) coordinate systems used to study geophysical fluids. The left panel shows the non-central nature of the effective gravitational acceleration  $\mathbf{g}$  on a rotating spherical planet, with the effective gravity given by the sum of the gravitational acceleration,  $\mathbf{g}_r = -g_e \hat{\mathbf{r}}$ , plus centrifugal acceleration (equation (9.121)),  $\mathbf{A}_{\text{centrifugal}} = r_\perp \Omega^2 (-\hat{\phi} \sin \phi + \hat{\mathbf{r}} \cos \phi)$ . The gravitational acceleration points radially to the center of the sphere whereas the centrifugal acceleration points outward away from the polar axis of rotation. A particle initially at rest on a smooth spherical planet will accelerate meridionally toward the equator due to the meridional component of the centrifugal acceleration (from equation (9.164) we have  $\dot{v} = -r_\perp \Omega^2 \sin \phi$ ). The right panel shows a *geopotential vertical coordinate*,  $r = R + z$ , that measures the distance perpendicular to the oblate spheroid shaped geopotential surface (dotted surface). The geopotential vertical coordinate precisely aligns the effective gravitational force with the vertical coordinate, so that there is no component of the effective gravity along the surface directions ( $g_\phi = 0$ ). Equivalently, the central gravitational acceleration now has a meridional component on the oblate spheroid that exactly balances the meridional component to the centrifugal acceleration, leaving an effective gravity that is only vertical. Hence, a frictionless oblate spheroidal planet allows for a particle at rest on the planet's surface to remain at rest (see equation (9.170)). Note that this figure is not drawn to scale, with the oblate nature highly exaggerated compared to the real earth system (see equation (9.167)), and the centrifugal acceleration much smaller than the gravitational (see equation (9.153)).

### 9.13.4 Comments

Figure 9.6, including its caption, offers a view on the transition from spherical coordinates to geopotential coordinates. The use of geopotential coordinates is rather accurate and extremely convenient for most purposes of geophysical fluid mechanics, with a notable exception being the study of tides and sea level, in which detailed models of the earth's mass distribution and gravity field are used (e.g., see [Gregory et al. \(2019\)](#) for a review). Although precise, the transition to geopotential coordinates is somewhat subtle in principle since we are reorganizing how the centrifugal acceleration appears. It is through this reorganization that we can largely ignore the centrifugal acceleration in our further studies of geophysical fluid mechanics.<sup>5</sup>

### 9.13.5 Further study

Section 4.12 of [Gill \(1982\)](#) and section 2.2.1 of [Vallis \(2017\)](#) present the terrestrial scaling needed to justify spherical coordinates with a radial effective gravitational potential. [Morse and Feshbach \(1953\)](#) and [Veronis \(1973\)](#) present details of spheroidal coordinates.

## 9.14 Exercises

### EXERCISE 9.1: INERTIAL ACCELERATION WITH $d\Omega/dt \neq 0$

Geophysical applications warrant taking the planetary rotation to be a constant vector,  $d\Omega/dt = 0$ , and that assumption is made throughout this book. However, for some applications, such as for rotating machines, we cannot make that assumption. What extra term appears in the inertial acceleration vector (9.92e) when  $d\Omega/dt \neq 0$ ?

### EXERCISE 9.2: WORKING THROUGH THE SPHERICAL ACCELERATION

Convince yourself that the spherical form of the acceleration given by equation (9.110) is indeed correct.

### EXERCISE 9.3: VELOCITY AND ACCELERATION IN CYLINDRICAL-POLAR COORDINATES

In Section 8.3 we worked through the transformation from Cartesian coordinates to cylindrical-polar coordinates for describing motion in a rotating reference frame. We also made use of polar coordinates in Section 9.4.4 to illustrate how polar unit vectors change under rotations. Here we develop an expression for the position, velocity, and acceleration vectors in a reference frame rotating with a constant rate about the vertical axis ( $\Omega = \Omega \hat{z}$ ) using rotating cylindrical-polar coordinates. The cylindrical-polar coordinates are useful when describing physical systems such as rotating fluid columns (e.g., fluids in a rotating circular tank as in Section 31.7) or when studying cyclostrophically balanced flow (Section 26.5).

- (A) Determine the representation of the inertial velocity vector,  $\mathbf{V} = d\mathbf{X}/dt$ , in terms of cylindrical-polar coordinates. Hint: do not forget to include the solid body motion of the rotating reference frame, which was discussed in Section 9.4.4.
- (B) Determine the representation of the inertial acceleration vector,  $\mathbf{A} = d\mathbf{V}/dt$ , in terms of cylindrical-polar coordinates.
- (C) Writing the inertial acceleration in the form

$$\mathbf{A} = \mathbf{A}_{\text{cylindrical-polar}} + \mathbf{A}_{\text{metric}} - \mathbf{A}_{\text{centrifugal}} - \mathbf{A}_{\text{Coriolis}}, \quad (9.172)$$

---

<sup>5</sup>An exception is in our study of rotating laboratory tank experiments in which it is more convenient to expose the centrifugal acceleration (Section 22.4).

give the mathematical expressions for these terms:

- $\mathbf{A}_{\text{cylindrical-polar}} =$  acceleration in the rotating reference frame using cylindrical-polar coordinates;
- $\mathbf{A}_{\text{metric}} =$  acceleration due to motion of the cylindrical-polar unit vectors relative to the rotating reference frame;
- $\mathbf{A}_{\text{centrifugal}} =$  centrifugal acceleration;
- $\mathbf{A}_{\text{Coriolis}} =$  Coriolis acceleration.

#### EXERCISE 9.4: VELOCITY PROJECTED ONTO ACCELERATION

The kinetic energy per mass of a particle is given by

$$\mathcal{K} = \mathbf{V} \cdot \mathbf{V}/2, \quad (9.173)$$

where  $\mathbf{V}$  is the inertial velocity of a particle. In an inertial reference frame it is trivial to show that

$$\frac{d\mathcal{K}}{dt} = \mathbf{V} \cdot \mathbf{A} \quad (9.174)$$

through use of the chain rule, where  $\mathbf{A} = d\mathbf{V}/dt$  is the inertial acceleration. Verify that this identity also holds in the rotating reference frame. For simplicity make use of planetary Cartesian coordinates.

#### EXERCISE 9.5: GEOMETRY OF CONSTANT GEOPOTENTIAL SURFACES

Here we examine some properties of the geopotential given by equation (9.151), where the squared solid-body speed is  $\mathbf{U}_{\text{solid}}^2 = (\Omega r \cos \phi)^2$ . We only consider geopotentials that are close to the radius of the planet, so that we can assume the gravitational acceleration,  $g_e$ , is constant and takes on its value at  $R_e$  as in Sections 9.12.2 and 9.12.4.

- Sketch surfaces of constant geopotential according to the expression (9.151). Draw both meridional (north-south) lines and zonal (east-west) lines.
- By equating the geopotential going around the pole to that going around the equator, show that the polar radius is less than the equatorial radius when  $\Omega > 0$ .
- Taking the terrestrial values of  $g_e$ ,  $R_{\text{equator}}$ , and  $\Omega$ , what is the polar radius  $R_{\text{pole}}$ ? Compare to the measured value of the polar radius given by equation (9.166).

#### EXERCISE 9.6: GENERAL FORM OF THE GEOPOTENTIAL

In Exercise 9.5, as in Sections 9.12.3 and 9.12.4, we only considered geopotentials that are close to the radius of the planet. Show that geopotentials have larger radius at the equator than at the poles even when not making this assumption. Hint: maintain the general form of the gravitational potential as given by equation (9.140), then add to the potential for the centrifugal acceleration (9.97). Evaluate the geopotential at the pole and then show that this same geopotential has a larger radial position anywhere equatorward of the pole.

#### EXERCISE 9.7: SCALING TO JUSTIFY USE OF GEOPOTENTIAL COORDINATES

Summarize the argument that justifies the use of geopotential coordinates while retaining the spherical geometry. Make use of your favorite textbook discussion such that given in Chapter 2 of [Vallis \(2017\)](#).

#### EXERCISE 9.8: ACCELERATIONS ACTING ON A RESTING PARTICLE

In this exercise we consider the accelerations acting on a particle at rest on a smooth/frictionless rotating spherical planet and a rotating oblate spheroidal planet. We also consider similar questions in Section 10.10.

- (A) Motion of a particle on a rotating spherical planet is described using the spherical coordinates from Section 9.13.2 with the corresponding equations of motion (9.163)-(9.165). Suppose that we drop a particle on a rotating sphere and that we describe its motion using the spherical coordinates. Discuss the initial acceleration of the particle that is released from rest.
- (B) Motion of a particle on a rotating oblate spheroid planet is described using the geopotential coordinates from Section 9.13.3 with the corresponding equations of motion (9.169)-(9.171). Suppose that we drop a particle on a rotating oblate spheroid and that we describe its motion using the geopotential coordinates. Discuss the initial acceleration of the particle that is released from rest.

**EXERCISE 9.9: GRAVITATIONAL POTENTIAL INSIDE A SPHERE**

In Section 9.12.1 we found the gravitational,  $\Phi$ , for a point outside of the spherical earth. Here we find the gravitational potential inside of the earth. That is, solve the Poisson equation

$$\nabla^2 \Phi = 4\pi G \rho, \quad (9.175)$$

for a radial position  $r < R_e$ . Hint: follow the approach in Section 9.12.1 and then match the potential at  $r = R_e$ . Note: the solution can be found in most first year undergraduate physics texts.





# Chapter 10

## Symmetry and conservation

A symmetry is a discrete or continuous operation that leaves a physical system unchanged. For example, let  $\mathbf{X}$  be a trajectory satisfying Newton's equation of motion and  $\mathcal{A}$  be an operation, then if  $\mathcal{A}[\mathbf{X}]$  also satisfies Newton's equation of motion then  $\mathcal{A}$  is a symmetry of the physical system. There is a connection between symmetries and conservation laws and these connections are explored in this chapter. These ideas are fundamental to how we garner a qualitative understanding of motion in which, for many purposes, it is more useful to know the dynamically conserved properties shared by all trajectories rather than details of any particular trajectory. Furthermore, conservation laws provide predictive capabilities and guidance for designing analytical and numerical solution methods.

### CHAPTER GUIDE

This chapter relies on the particle mechanics material studied in Chapter 9, and here we explore many facets of rotational physics that are central to geophysical fluid motions. We make use of ideas from this chapter throughout the book.

10.1	Loose threads . . . . .	206
10.2	Trajectories and dynamical constraints . . . . .	206
10.2.1	Connecting symmetries to conservation laws . . . . .	207
10.2.2	Further study . . . . .	207
10.3	Time reversal symmetry . . . . .	207
10.4	Potential momentum . . . . .	208
10.4.1	Basics . . . . .	208
10.4.2	Comment about terminology . . . . .	209
10.5	Inertial oscillations . . . . .	209
10.5.1	Oscillator equation for inertial oscillations . . . . .	210
10.5.2	Particle trajectory and velocity . . . . .	210
10.5.3	Period of inertial oscillations . . . . .	211
10.5.4	Comments and further study . . . . .	211
10.6	Dynamical constraints from spatial symmetries . . . . .	212
10.6.1	Linear momentum conservation . . . . .	212
10.6.2	Potential momentum conservation . . . . .	212
10.6.3	Angular momentum conservation . . . . .	213
10.7	Axial angular momentum conservation . . . . .	213
10.7.1	Angular momentum . . . . .	214
10.7.2	Conservation of axial angular momentum . . . . .	214

10.8	Constraints from axial angular momentum conservation . . . . .	215
10.8.1	Deriving the constraints . . . . .	215
10.8.2	Axial angular momentum conservation yields zonal Coriolis acceleration . . . . .	216
10.8.3	Zonal acceleration induced by meridional motion . . . . .	217
10.8.4	Zonal acceleration induced by radial motion . . . . .	217
10.8.5	Zonal acceleration derived from axial angular momentum conservation	218
10.8.6	Coriolis acceleration from meridional motion . . . . .	218
10.8.7	When lateral motions dominate vertical motions . . . . .	219
10.8.8	Comments . . . . .	220
10.9	Mechanical energy conservation . . . . .	220
10.9.1	Some properties of kinetic energy . . . . .	220
10.9.2	Planetary Cartesian mechanical energy . . . . .	222
10.9.3	Planetary spherical mechanical energy . . . . .	222
10.9.4	Geopotential mechanical energy . . . . .	224
10.10	Sample trajectories using spherical coordinates . . . . .	224
10.10.1	Free fall to the center . . . . .	224
10.10.2	Free fall to the equatorial plane . . . . .	225
10.11	Exercises . . . . .	225

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## 10.1 Loose threads

- None ATT.

## 10.2 Trajectories and dynamical constraints

From Newton's law of motion, the trajectory of a particle is specified so long as we know the forces acting on the particle and the particle's initial position and initial velocity. The trajectory encapsulates all dynamical information about the moving particle. However, it is often difficult to unpack that information to understand the nature of the motion. Knowledge of the trajectory is not always the best route to dynamical insight nor to predictive capabilities.

For dynamical insight it is generally more useful to develop an understanding of constraints respected by the motion, with dynamical constraints manifesting as conservation laws. For example, does the motion conserve mechanical energy? What about angular momentum? If dynamical constraints are present, then all trajectories, regardless their complexity, satisfy the constraints. Knowledge of the constraints can reveal information often hidden when just having knowledge of the trajectory. Constraints also provide predictive statements of value when studying the stability of motion and for developing numerical methods for simulations.

An example is useful to illustrate the differences noted above. Consider the following two situations.

- We have the analytic expression for the trajectory of a particle moving around a rotating sphere. So we know this trajectory for all time.
- Instead imagine we know that all particles, no matter what their trajectory, conserve both the axial angular momentum around the rotational axis and the mechanical energy.

Knowledge of the trajectory for a single particle does not readily reveal that this particle is constrained in its motion to conserve angular momentum and mechanical energy. In contrast, knowing that all particles, no matter what trajectory, conserve angular momentum and mechanical energy gives us the ability to understand basic properties of the motion and to furthermore predict

the response under perturbations. We offer specifics to this predictive capability later in this chapter and provide more examples throughout this book. Dynamical constraints imposed by conservation laws are especially relevant for fluids since it is rare to determine the analytical expression for fluid motion, making the knowledge of constraints incredibly valuable.

### 10.2.1 Connecting symmetries to conservation laws

The discovery of conservation laws often comes from inspired manipulations of the equations of motion. However, there is a more robust and fundamental means to deduce conservation laws through their connection to symmetries, with a symmetry manifesting as an operation that leaves the physical system unchanged. For example, does the physical system remain unchanged when shifting the origin of time? If so, then mechanical energy is a constant of the motion. Likewise, if there is rotational symmetry around an axis, then the associated angular momentum is a constant of the motion.

The connection between symmetries (kinematics) and conservation laws (dynamics) was made by [Noether \(1918\)](#) (see [Noether and Tavel \(2018\)](#) for an English translation). Noether's Theorem is fundamental to nearly all areas of theoretical physics. It is sufficient for our study to make use of this theorem as a conceptual framework for understanding conservation laws and their connections to symmetries. Quite simply, if there is a symmetry then there is a corresponding conservation law, and vice versa.

It is very useful to identify conserved quantities as a means to understand and to constrain the motion. This perspective holds even when the symmetries giving rise to conserved quantities are broken in realistic cases. For example, as seen in Section 9.1.8, friction breaks time translation symmetry and so leads to the dissipation of mechanical energy. Nonetheless, understanding the frictionless motion, and the associated energy conservation law, offers insights for the frictional case. Indeed, for many purposes, knowledge of the trajectory is less important than knowledge of conserved, or partially conserved, dynamical quantities. In this chapter, we offer two examples to support this point: the case of mechanical energy conservation and axial angular momentum conservation. These conservation laws also hold in a modified form when moving to the continuum fluid (e.g., Chapter 17). Additional conservation properties also arise that are unique to the continuum, with conservation of potential vorticity the most notable one for geophysical fluids (Chapter 36).

### 10.2.2 Further study

Conservation laws and symmetries in classical mechanics are lucidly discussed in Chapters 1 and 2 of [Landau and Lifshitz \(1976\)](#). Pedagogical presentations on these topics can be found in this [online lecture from the Space Time series](#) and this [online lecture from Physics with Elliot](#). This [essay about Emmy Noether](#) provides insights into this mathematician whose work, conducted under some very unfortunate circumstances, forever connected symmetry and conservation laws, with this connection providing the basis for nearly all modern theories of physics.

## 10.3 Time reversal symmetry

A deterministic process is time-reversible if the time-reversed process satisfies the same dynamic equations as the forward-time process. That is, the dynamical equations are symmetric under a change in the sign of time so that the time-reversed evolution of one state is equivalent to the forward-time evolution of a corresponding state. We here discuss time reversal symmetry in the context of the point particle with trajectory,  $\mathbf{X}(t)$ , and velocity,  $\mathbf{V}(t) = d\mathbf{X}(t)/dt$ .

If  $\mathbf{X}(t)$  is a solution to the equations of motion, then what is needed for

$$\mathbf{X}^*(t^*) = \mathbf{X}(-t) \quad \text{and} \quad \mathbf{V}^*(t^*) = d\mathbf{X}^*(t^*)/dt^* = -d\mathbf{X}(-t)/dt \quad (10.1)$$

to define the same trajectory traversed backwards in time, where  $t^* = -t$ ? We answer this question by recalling from Section 9.13.1 that with planetary rotation a constant in time then the Cartesian coordinate equation of motion is given by

$$\frac{d}{dt} \left[ \dot{\mathbf{X}}(t) + 2\boldsymbol{\Omega} \times \mathbf{X}(t) \right] = -\nabla\Phi(t). \quad (10.2)$$

We are interested in the constraints that ensure the following equation to also satisfied

$$\frac{d}{dt^*} \left[ \frac{d\mathbf{X}^*(t^*)}{dt^*} + 2\boldsymbol{\Omega}^* \times \mathbf{X}^*(t^*) \right] = -\nabla\Phi(t^*). \quad (10.3)$$

The effective gravitational acceleration remains time reversible if

$$\Phi^*(t^*) = \Phi(t), \quad (10.4)$$

which is trivially satisfied for  $\Phi = g z$ . The Coriolis acceleration is velocity dependent so that it generally breaks time reversal symmetry. However, we can recover time symmetry by assuming that the rotation direction switches when time reverses so that

$$\boldsymbol{\Omega}^* = -\boldsymbol{\Omega}. \quad (10.5)$$

With this transformation, a trajectory,  $\mathbf{X}(t)$ , that solves the forward equation (10.2) yields a trajectory  $\mathbf{X}(-t)$  that solves the same equation but with time reversed. We return to this question of time reversal symmetry for the Euler equations of perfect fluid mechanics in Exercise 17.2.

## 10.4 Potential momentum

In Section 9.13.1 we introduced the *potential momentum*. In this section we study its conservation properties given that it is a constant of the motion for a particle moving on a time independent geopotential in a direction where the geopotential does not change. That is, the conservation of potential momentum arises from a symmetry of the geopotential.

### 10.4.1 Basics

We again start with the Cartesian coordinate equation of motion

$$\frac{d}{dt} \left[ \dot{\mathbf{X}} + 2\boldsymbol{\Omega} \times \mathbf{X} \right] = -\nabla\Phi. \quad (10.6)$$

As written it suggests we introduce the *potential momentum* per mass

$$\mathbf{M} \equiv \dot{\mathbf{X}} + 2\boldsymbol{\Omega} \times \mathbf{X} = \hat{\mathbf{x}}(u - 2\Omega y) + \hat{\mathbf{y}}(v + 2\Omega x) + \hat{\mathbf{z}}w, \quad (10.7)$$

in which case

$$\dot{\mathbf{M}} = -\nabla\Phi. \quad (10.8)$$

Now let  $\hat{\mathbf{s}}$  be a unit vector tangent to the geopotential surface so that  $\hat{\mathbf{s}} \cdot \nabla\Phi = 0$ . Assuming the geopotential surface is time independent so that  $\hat{\mathbf{s}}$  is also time independent, then the equation

of motion (10.8) leads to

$$\frac{d(\hat{s} \cdot \mathbf{M})}{dt} = 0. \quad (10.9)$$

That is, the projection of the potential momentum onto a static geopotential surface is a constant of motion. This dynamical constraint arises since we cannot distinguish one point on the geopotential from another; i.e., there is a symmetry associated with motion along the static geopotential. Noether's Theorem (Section 10.2.1) then says that this geometric symmetry leads to a constant of the motion, here given by that component of potential momentum within the geopotential surface. We illustrate this situation in Figure 10.1 with a horizontal geopotential surface.

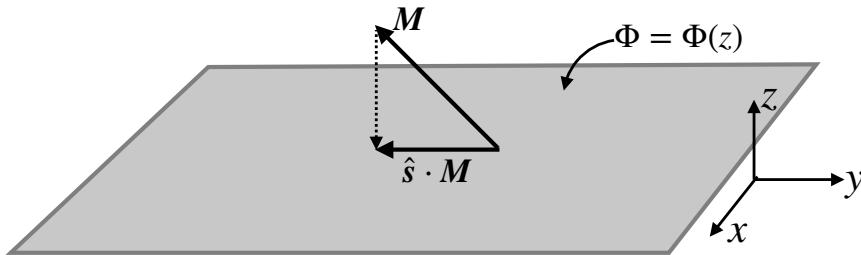


FIGURE 10.1: The projection of the potential momentum onto the geopotential surface is a constant of the motion,  $d(\hat{s} \cdot \mathbf{M})/dt = 0$ . Here the geopotential surface is the  $x$ - $y$ -plane so that  $\hat{x} \cdot \mathbf{M} = u - 2\Omega y$  and  $\hat{y} \cdot \mathbf{M} = v + 2\Omega x$  are the two conserved components of potential momentum.

Consider a particle with potential momentum  $\mathbf{M}$  and move it from an arbitrary point to a reference position with  $\mathbf{X} = 0$ . Upon reaching the reference position, the horizontal velocity of the particle must equal to  $\mathbf{M}$  in order to maintain the same potential momentum. This example motivates the name “potential momentum”, since  $\mathbf{M}$  measures the potential for relative motion contained in the particle as it moves along a geopotential.

#### 10.4.2 Comment about terminology

As noted on page 51 of [Markowski and Richardson \(2010\)](#), one might see potential momentum referred to as *pseudo angular momentum*, with some dropping the “pseudo” portion to the name. In either case, it is important to note that potential momentum is distinct from angular momentum. In particular, there is no moment-arm as part of the potential momentum.

Furthermore, most authors use the term “absolute” momentum rather than potential momentum, perhaps in reference to the momentum measured in the absolute or inertial reference frame. However, that connection is incorrect since the inertial velocity is (Section 9.9.1)

$$\mathbf{V} = \mathbf{V}_{\text{Cartesian}} + \mathbf{U}_{\text{solid-body}} = \mathbf{V}_{\text{Cartesian}} + \boldsymbol{\Omega} \times \mathbf{X}. \quad (10.10)$$

The factor of two multiplying the rotation rate in the potential momentum arises from the Coriolis acceleration. In contrast, solid-body rotation velocity contributes to the inertial velocity and it has a factor of unity multiplying the rotation rate.

## 10.5 Inertial oscillations

In Section 22.3 we introduce the tangent plane approximation for motion on a rotating sphere. In this approximation, motion occurs on a rotating geopotential surface with the surface approximated as horizontal. Furthermore, we use local tangent plane Cartesian coordinates (which are distinct from the planetary Cartesian coordinates used in Chapter 9 and illustrated in Figure 8.1).

The  $f$ -plane approximation furthermore sets the Coriolis parameter to a constant,

$$f = 2\Omega \sin \phi_0, \quad (10.11)$$

where  $\phi_0$  is a chosen latitude. Consequently, a particle moving on the  $f$ -plane maintains a constant horizontal potential momentum

$$\frac{dM_x}{dt} = \frac{d(u - f y)}{dt} = 0 \quad (10.12a)$$

$$\frac{dM_y}{dt} = \frac{d(v + f x)}{dt} = 0, \quad (10.12b)$$

where we introduced the horizontal velocity components  $(u, v) = (\dot{x}, \dot{y})$ . These two conservation laws greatly constrain the motion of the particle moving on a constant geopotential surface.

### 10.5.1 Oscillator equation for inertial oscillations

Taking the time derivative of the zonal equation (10.12a) and using the meridional equation (10.12b) leads to

$$\ddot{u} - f \dot{v} = \ddot{u} + f^2 u = 0. \quad (10.13)$$

Similar manipulations for the meridional velocity equation render the free oscillator equation for each component of the horizontal velocity

$$\frac{d^2u}{dt^2} + f^2 u = 0 \quad \text{and} \quad \frac{d^2v}{dt^2} + f^2 v = 0. \quad (10.14)$$

Motions that satisfy this equation are termed *inertial oscillations*.

### 10.5.2 Particle trajectory and velocity

Time integrating the equation of motion (10.14) renders the particle trajectory and its velocity

$$\mathbf{X}(t) = (U/f) [\hat{\mathbf{x}} \sin(ft) + \hat{\mathbf{y}} \cos(ft)] \quad (10.15a)$$

$$\mathbf{U}(t) = U [\hat{\mathbf{x}} \cos(ft) - \hat{\mathbf{y}} \sin(ft)], \quad (10.15b)$$

where  $U > 0$  is the particle speed, which is a constant, and we assumed the initial conditions

$$\mathbf{X}(0) = (U/f) \hat{\mathbf{y}} \quad \text{and} \quad \mathbf{U}(0) = U \hat{\mathbf{x}}. \quad (10.16)$$

From the particle trajectory equation (10.15a), we see that motion of a particle exhibiting inertial oscillations is circular with radius

$$R = U/|f|. \quad (10.17)$$

As depicted in Figure 10.2, northern hemisphere ( $f > 0$ ) inertial oscillations occur in the clockwise direction whereas southern hemisphere motion is counter-clockwise. Consequently, particle motion undergoing inertial oscillations occurs in an anti-cyclonic sense (opposite to the sense of the rotating reference frame). As we discuss in more detail in Section 26.4, inertial oscillations arise from a balance between the Coriolis acceleration of the rotating frame and the centrifugal acceleration arising from the particle's circular motion.<sup>1</sup> The only way to realize this balance is for the particle to move anti-cyclonically, with the Coriolis acceleration pointing towards the

<sup>1</sup>This centrifugal acceleration is distinct from the planetary centrifugal acceleration absorbed into the geopotential (Section 9.12.4). The planetary centrifugal acceleration plays no role in inertial oscillations.

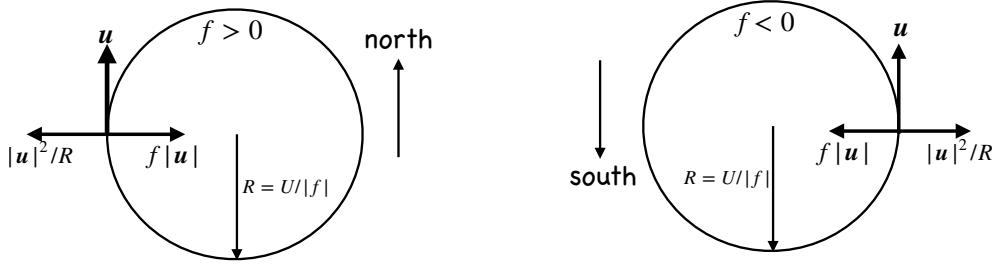


FIGURE 10.2: Inertial oscillation of a particle on a plane occurs when the centrifugal acceleration balances the Coriolis acceleration. Left panel:  $f > 0$  for the northern hemisphere, revealing that inertial motion is an anti-cyclonic (clockwise) circular motion with radius  $|R| = U/|f|$ . The Coriolis acceleration is to the right, pointing into the center of the inertial circle, whereas the centrifugal acceleration points away from the center. Right panel: Counterclockwise inertial motion in the southern hemisphere with the same balance between Coriolis and centrifugal accelerations.

inside of the inertial circle and the centrifugal acceleration pointing outside. Finally, note that the potential momentum for inertial oscillations vanishes since

$$\mathbf{M}(t) = \mathbf{U}(t) + f \hat{\mathbf{z}} \times \mathbf{X}(t) = 0. \quad (10.18)$$

Adding an arbitrary constant to the initial position makes the potential momentum equal to a nonzero constant.

### 10.5.3 Period of inertial oscillations

Inertial oscillations possess a constant speed and move around the inertial circle with a period

$$T_{\text{inertial}} = \frac{2\pi}{f} = \frac{11.97}{|\sin \phi_0|} \text{ hour}, \quad (10.19)$$

where we set  $\Omega = 7.292 \times 10^{-5} \text{ s}^{-1}$  (equation (9.33)). This period is the time it takes to go around the circle. It is smallest at the poles, where the latitude  $\phi_0 = \pm\pi/2$  and  $T_{\text{smallest}} \approx 12 \text{ hour}$ . At the equator,  $\phi_0 = 0$ , so that the radius of the inertial circle is infinite and inertial oscillations are unavailable. Furthermore,  $T_{\text{inertial}}$  is the time for a Foucault pendulum to turn through  $\pi$  radians, so that  $T_{\text{inertial}}$  is sometimes referred to as one-half a pendulum day.

### 10.5.4 Comments and further study

Inertial oscillations of fluid elements are described by the above constant potential momentum equation of motion. Such oscillations are commonly measured by ocean current meters, especially in higher latitude regions where diurnal (day-night) variations in wind forcing have a strong projection onto the inertial period. This resonant forcing puts energy into inertial or near-inertial motions. It is quite amazing that such oscillations are indeed found in the ocean, given that we have ignored pressure and friction, which are two forces that impact on fluid elements (as opposed to point particles). The main reason we can observe this motion in the ocean is that upper ocean currents are often generated by winds even in the absence of horizontal pressure gradients, so that there are occasions when the motion is not affected much by pressure gradients.

We study inertial waves in Section 25.6 as part of our study of rapidly rotating fluid motion. We also encounter inertial motions in Section 26.4 as part of our characterization of horizontal fluid motion according to the balance between forces. As noted above, we arrive at inertial motion by balancing the Coriolis acceleration with the centrifugal acceleration due to the curved motion

of a fluid particle. The name “inertial” does not here refer to motion in an inertial reference frame (Section 9.3). Instead, it refers to the balance between accelerations arising only when the particle is in motion (i.e., has inertia), with these accelerations being the Coriolis and centrifugal.

A rotating tank fluid experiment offers a useful controlled setting to observe inertial waves in a fluid, such as shown near the 18 minute mark in [this video from Prof. Fultz](#).

## 10.6 Dynamical constraints from spatial symmetries

We here position the conservation of potential momentum among two other dynamical conservation laws by summarizing the spatial symmetries that lead to the conservation laws via Noether’s Theorem. We follow this discussion in Section 10.9, which studies mechanical energy conservation arising from time symmetry.

### 10.6.1 Linear momentum conservation

As seen in Section 9.1.1, linear momentum remains constant for a particle moving without any forces acting on it; i.e., a *free particle*. This type of motion is not common for geophysical particles or fluids since they feel gravity and so are not free. Even so, we consider this limiting case as a point of comparison for the other conservation laws.

The conservation of linear momentum is simply viewed within the particle’s inertial reference frame, where a vanishing inertial acceleration leads to a constant inertial velocity

$$\mathbf{A} = d\mathbf{V}/dt = 0. \quad (10.20)$$

In a Euclidean space, a vanishing acceleration means the particle is moving in a straight line with constant velocity. When viewed from a rotating frame using Cartesian coordinates, a vanishing inertial acceleration means that the Cartesian acceleration balances Coriolis and centrifugal accelerations

$$\ddot{\mathbf{X}} = -2\boldsymbol{\Omega} \times \dot{\mathbf{X}} - \nabla\Phi_{\text{centrifugal}}. \quad (10.21)$$

This equation is clearly not a very useful means to describe unaccelerated free particle motion. We can provide a bit more compactness to this equation by introducing the potential momentum (10.7) so that

$$d\mathbf{M}/dt = -\nabla\Phi_{\text{centrifugal}}. \quad (10.22)$$

While the inertial acceleration vanishes ( $\mathbf{A} = d\mathbf{V}/dt = 0$ ), time changes to the potential momentum are balanced by the gradient of the centrifugal potential.

### 10.6.2 Potential momentum conservation

Conservation of potential momentum arises from symmetry of particle motion on a constant geopotential surface. The conservation law is most readily viewed within the rotating frame, whereby (equation (10.9))

$$\frac{d(\hat{\mathbf{s}} \cdot \mathbf{M})}{dt} = 0. \quad (10.23)$$

A geopotential is a two-dimensional surface so that this conservation law corresponds to two dynamical constraints such as shown in Figure 10.1.

### 10.6.3 Angular momentum conservation

As detailed in Section 10.7, the angular momentum computed with respect to the axis of rotation is a constant of the motion (Figure 10.3). This conservation law arises from rotational symmetry of the system about the rotational axis. Axial ( $z$ -axis) angular momentum conservation takes the form

$$dL^z/dt = 0, \quad (10.24)$$

where the axial angular momentum is

$$L^z = m r_{\perp}^2 (\dot{\lambda} + \Omega) \quad \text{with} \quad r_{\perp} = \sqrt{x^2 + y^2} = r \cos \phi. \quad (10.25)$$

The distance from the rotation axis,  $r_{\perp}$ , is the *moment arm* for the axial angular momentum. The longitude,  $\lambda$ , measures the angle in the counter-clockwise direction from the positive  $x$ -axis, and  $\dot{\lambda}$  is the time change of the longitude.

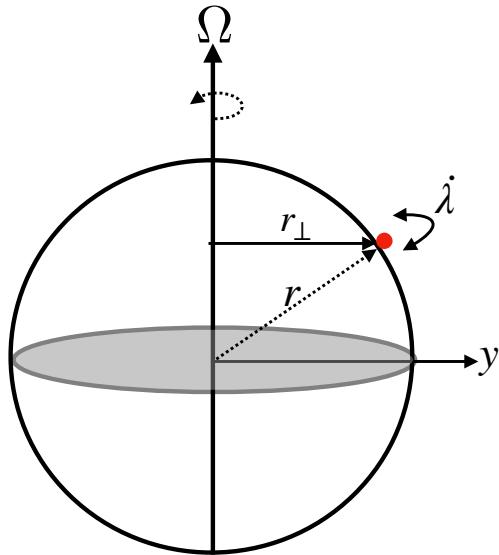


FIGURE 10.3: Axial angular momentum,  $L^z = m r_{\perp}^2 (\dot{\lambda} + \Omega)$ , is the moment of the zonal momentum around the sphere, with  $r_{\perp} = r \cos \phi = \sqrt{x^2 + y^2}$  the moment arm length; i.e., the distance of the particle to the axis of rotation, whereas  $r^2 = \sqrt{x^2 + y^2 + z^2}$  is the radial distance to the center of the sphere.  $L^z$  is a constant of the motion for the particle moving in the absence of friction.

## 10.7 Axial angular momentum conservation

Does the particle know anything about the longitudinal angle,  $\lambda$ ? Since we assume that the sphere is smooth (i.e., no mountains), and since the sphere is rotating around the polar axis, there is an arbitrariness in how we choose the zero for the longitudinal angle. That is, the physical system remains unchanged if we shift the longitudinal angle by a constant. Noether's Theorem then says that this rotational symmetry leads to a corresponding angular momentum conservation. Hence, the particle's angular momentum around the rotational axis remains fixed by the initial conditions. We here prove that axial angular momentum is constant by manipulating the equations of motion. Many of the same manipulations also occur when considering angular conservation for a continuous fluid (see Section 17.4).

### 10.7.1 Angular momentum

The angular momentum of the particle, computed with respect to the origin of the sphere, is given by

$$\mathbf{L} = m \mathbf{X} \times \mathbf{V}. \quad (10.26)$$

This is the moment of the linear momentum computed relative to the origin. We write the angular momentum computed along the polar axis as

$$L^z = \mathbf{L} \cdot \hat{\mathbf{z}} \quad (10.27a)$$

$$= m (\mathbf{X} \times \mathbf{V}) \cdot \hat{\mathbf{z}} \quad (10.27b)$$

$$= m (\hat{\mathbf{z}} \times \mathbf{X}) \cdot \mathbf{V} \quad (10.27c)$$

$$= m r \cos \phi (\hat{\lambda} \cdot \mathbf{V}) \quad (10.27d)$$

$$= m r_{\perp} (\hat{\lambda} \cdot \mathbf{V}). \quad (10.27e)$$

Hence, the angular momentum about the polar axis equals to the component of the linear momentum in the longitudinal direction, multiplied by the distance to the polar rotational axis (the moment-arm)

$$r_{\perp} = r \cos \phi. \quad (10.28)$$

In deriving equation (10.27e), we made use of the identity

$$\hat{\mathbf{z}} \times \mathbf{X} = r_{\perp} \hat{\lambda}, \quad (10.29)$$

which will prove useful below for proving that axial angular momentum is a constant of the motion.

We now write the axial angular momentum in equation (10.27e) in terms of the rotating frame quantities. To do so, introduce the inertial velocity written using spherical coordinates according to equation (9.79f), which yields

$$L^z = m r_{\perp} (\hat{\lambda} \cdot \mathbf{V}) = m r_{\perp}^2 (\dot{\lambda} + \Omega) = m r_{\perp} (u + r_{\perp} \Omega). \quad (10.30)$$

When measured from the rotating terrestrial frame, the axial angular momentum consists of two terms: one from the zonal velocity of the particle relative to the planet and another from the solid-body motion of the planet.

### 10.7.2 Conservation of axial angular momentum

The time derivative of the axial angular momentum is given by

$$\frac{dL^z}{dt} = m \frac{d}{dt} [(\mathbf{X} \times \mathbf{V}) \cdot \hat{\mathbf{z}}] \quad (10.31a)$$

$$= m \frac{d}{dt} [(\hat{\mathbf{z}} \times \mathbf{X}) \cdot \mathbf{V}] \quad (10.31b)$$

$$= m (\hat{\mathbf{z}} \times \mathbf{V}) \cdot \mathbf{V} + m (\hat{\mathbf{z}} \times \mathbf{X}) \cdot \mathbf{A} \quad (10.31c)$$

$$= m (\hat{\mathbf{z}} \times \mathbf{X}) \cdot \mathbf{A} \quad (10.31d)$$

$$= m r_{\perp} \hat{\lambda} \cdot \mathbf{A}. \quad (10.31e)$$

To reach this result we noted that the polar axis direction,  $\hat{\mathbf{z}}$ , is time independent, and we used the identity (10.29) for the final step. The inertial acceleration arises just from the central-force

gravitational field (equation (9.154))

$$\mathbf{A} = -\nabla\Phi_e = -g_e \hat{\mathbf{r}}. \quad (10.32)$$

Since  $\hat{\lambda} \cdot \hat{\mathbf{r}} = 0$ , we have axial angular momentum conservation

$$\frac{dL^z}{dt} = 0. \quad (10.33)$$

## 10.8 Constraints from axial angular momentum conservation

Axial angular momentum conservation constrains the particle motion and in turn it offers a means for interpreting and predicting motion on the sphere. It is also a natural means for describing the motion when viewed from a non-rotating inertial reference frame. We here explore how these constraints manifest through thought experiments illustrated in Figure 10.4. In doing so, we show that the acceleration induced by axial angular momentum conserving motion corresponds to the Coriolis acceleration that is part of a rotating non-inertial reference frame description. That is, angular momentum constrained motion described in an inertial reference frame corresponds to the Coriolis acceleration appearing in a rotating non-inertial frame description.

Throughout the following we write the axial angular momentum as

$$L^z = m l^z = m r_{\perp}^2 (\dot{\lambda} + \Omega) = m r_{\perp} (u + r_{\perp} \Omega), \quad (10.34)$$

where

$$l^z = L^z/m \quad \text{and} \quad u = r_{\perp} \dot{\lambda} \quad (10.35)$$

are the axial angular momentum per mass and zonal velocity component. Since the mass of the particle is constant, conservation of  $L^z = m l^z$  implies conservation of  $l^z$ . Note that for most geophysical applications,  $l^z > 0$  since solid-body motion dominates over the relative zonal velocity:

$$r_{\perp} \Omega > |u| \quad \text{for most terrestrial motions,} \quad (10.36)$$

with  $r_{\perp} \Omega = 465 \text{ m s}^{-1}$  at the equator (see Figure 9.2). In Exercise 10.1 we consider the interesting, but geophysically uncommon, case where  $l^z \leq 0$ .

### 10.8.1 Deriving the constraints

Conservation of axial angular momentum says that it is not possible to change  $u$  or  $\dot{\lambda}$  without also changing  $r_{\perp}$  in such a manner to ensure that  $l^z$  remains fixed. To determine the relation between these changes we set  $\delta l^z = 0$ , where  $\delta$  refers to any small change. When writing  $l^z = r_{\perp}^2 (\dot{\lambda} + \Omega)$  we have

$$\delta l^z = 2 r_{\perp} \delta r_{\perp} (\dot{\lambda} + \Omega) + r_{\perp}^2 \delta \dot{\lambda} = 2 l^z \frac{\delta r_{\perp}}{r_{\perp}} + r_{\perp}^2 \delta \dot{\lambda}, \quad (10.37)$$

where we set  $\delta \Omega = 0$  since the earth's rotation rate is assumed to be fixed. Furthermore, we find it useful to write the changes in terms of  $l^z$  since it is a constant of the motion. Likewise, when writing  $l^z = r_{\perp} (u + r_{\perp} \Omega)$  we have

$$\delta l^z = \delta r_{\perp} (u + r_{\perp} \Omega) + r_{\perp} (\delta u + \Omega \delta r_{\perp}) = \Omega r_{\perp} \delta r_{\perp} \left[ 1 + \frac{l^z}{\Omega r_{\perp}^2} \right] + r_{\perp} \delta u. \quad (10.38)$$

Setting  $\delta l^z = 0$  then leads to the constraints

$$\delta \dot{\lambda} = -\frac{2l^z}{r_\perp^2} \frac{\delta r_\perp}{r_\perp} \iff \delta u = -\Omega \delta r_\perp \left[ 1 + \frac{l^z}{\Omega r_\perp^2} \right]. \quad (10.39)$$

As noted above,  $l^z > 0$  is generally the case for geophysical fluid motion. Consequently, axial angular momentum conserving motion that brings the particle closer to the rotation axis ( $\delta r_\perp < 0$ ) leads to an eastward velocity change ( $\delta \dot{\lambda} > 0$  and  $\delta u > 0$ ). The opposite occurs for motion with  $\delta r_\perp > 0$ . These results hold in both the northern and southern hemispheres.

Since  $r_\perp = r \cos \phi$ , the distance to the rotational axis can change either by changing the radial position or the meridional position

$$\delta r_\perp = (\cos \phi) \delta r - (r \sin \phi) \delta \phi. \quad (10.40)$$

Assuming these changes occur over a small time increment  $\delta t$  allows us to write

$$\delta r_\perp / \delta t = w \cos \phi - v \sin \phi, \quad (10.41)$$

where

$$v = r \delta \phi / \delta t = r \dot{\phi} \quad \text{and} \quad w = \delta r / \delta t = \dot{r} \quad (10.42)$$

introduced the meridional and vertical components to the particle velocity according to equation (9.81). For geophysical fluid motion, changes in vertical distance  $\delta r$  are far smaller than the distance to the earth's center,  $\delta r \ll r$ . In this case, when  $\phi \neq 0$ , then  $\delta r_\perp$  is affected much more by meridional motion at constant radial position (second term on right hand side of equation (10.41)) than by vertical motion at constant latitude (first term). We return to this observation in Section 10.8.7 when discussing nearly the shallow fluid approximation used to develop the primitive equations for the atmosphere and ocean in Section 22.1.2.

## 10.8.2 Axial angular momentum conservation yields zonal Coriolis acceleration

Consider the zonal acceleration felt by a particle at rest (in the rotating frame) whose angular momentum per mass equals  $l^z = r_\perp^2 \Omega$ . In this case the zonal acceleration in equation (10.39) is

$$\delta \dot{\lambda} = -2\Omega \frac{\delta r_\perp}{r_\perp} \iff \dot{u} = -2\Omega (\delta r_\perp / \delta t) = -2\Omega (w \cos \phi - v \sin \phi), \quad (10.43)$$

where we used equation (10.41) for  $\delta r_\perp / \delta t$ . The expression for  $\dot{u}$  is precisely the same as the Coriolis acceleration appearing in the zonal momentum equation (9.169)

$$\dot{u} + \frac{u(w - v \tan \phi)}{r} = \underbrace{-2\Omega (w \cos \phi - v \sin \phi)}_{\text{Coriolis acceleration}}. \quad (10.44)$$

Hence, the Coriolis acceleration appearing in the zonal momentum equation is identical to the zonal acceleration induced by constraining the motion to conserve axial angular momentum. That is, by unpacking the constraint of axial angular momentum conservation to reveal the zonal momentum equation, the Coriolis acceleration is revealed as part of that package. We pursue this connection in Section 10.8.5 by deriving the zonal momentum equation from the axial angular momentum equation.

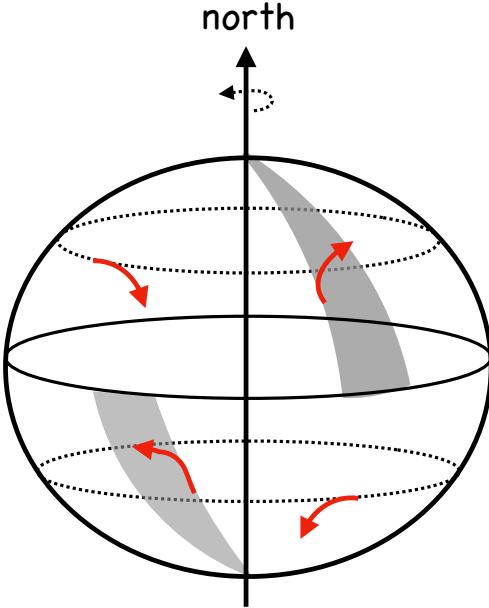


FIGURE 10.4: In the northern hemisphere, the Coriolis acceleration viewed from the rotating reference frame deflects a particle to its right whereas it deflects a particle to the left in the southern hemisphere. This deflection is also a result of axial angular momentum conservation, which is the natural way to describe the motion from a non-rotating inertial reference frame. We can summarize the ideas developed in Section 10.8 as follows. For a meridionally displaced trajectory, the spinning earth causes the trajectory to pick up motion relative to the earth surface, zonally to the right in the northern hemisphere and zonally to the left in the southern hemisphere. Equivalently, consider a projectile (say a cannon ball) shot poleward. As the projectile started from the ground closer to the equator, it has a zonal velocity component that is larger than the more poleward ground underneath it as it flies away from the equator. Hence, as it moves poleward it also picks up an eastward velocity component, which is to the right of the poleward motion in the northern hemisphere and to the left in the southern. For a zonally displaced trajectory to conserve angular momentum, the particle must pick up meridional motion; poleward if the zonal displacement is westward and equatorward if the displacement is eastward.

### 10.8.3 Zonal acceleration induced by meridional motion

Consider a particle moving meridionally ( $\delta\phi \neq 0$ ) while maintaining a constant radial position ( $\delta r = 0$ ). The axial angular momentum constraint (10.43) induces a zonal acceleration

$$\dot{u} = 2\Omega v \sin \phi, \quad (10.45)$$

which, as seen by equation (10.44), is the Coriolis acceleration appearing in the zonal momentum equation arising from the meridional motion. For poleward motion in either hemisphere,  $v \sin \phi > 0$ . Hence, axial angular momentum conserving motion towards either pole induces an eastward acceleration, whereas a westward acceleration is induced for equatorward motion. For the northern hemisphere, the induced acceleration deflects the particle to the right when looking downstream whereas in the southern hemisphere the induced acceleration deflects the particle to the left. These deflections are illustrated in Figure 10.4.

### 10.8.4 Zonal acceleration induced by radial motion

Now consider a particle moving radially while holding the latitude fixed ( $\delta r \neq 0$  and  $\delta\phi = 0$ ). The axial angular momentum constraint (10.43) induces a zonal acceleration

$$\dot{u} = -2\Omega w \cos \phi, \quad (10.46)$$

which, as seen by equation (10.44), is the Coriolis acceleration appearing in the zonal momentum equation arising from the vertical motion. Hence, for vertically downward motion ( $w < 0$ ), axial angular momentum conservation induces a positive zonal acceleration,  $\dot{u} > 0$ , which we expect from axial angular momentum conservation since the particle is moving closer to the rotation axis.

### 10.8.5 Zonal acceleration derived from axial angular momentum conservation

The above discussion can be formalized by analyzing how the conservation of axial angular momentum leads to an expression for the zonal acceleration. For this purpose, compute the time derivative of the first form of the axial angular momentum in equation (10.34), in which case

$$\frac{1}{m} \frac{dL^z}{dt} = \frac{d[(r \cos \phi)^2 (\dot{\lambda} + \Omega)]}{dt} \quad (10.47a)$$

$$= 2(\dot{r} \cos \phi - r \dot{\phi} \sin \phi)(\dot{\lambda} r \cos \phi + r \Omega \cos \phi) + (r \cos \phi)^2 \ddot{\lambda} \quad (10.47b)$$

$$= 2(w \cos \phi - v \sin \phi)(u + r \Omega \cos \phi) + (r \cos \phi)^2 \ddot{\lambda}, \quad (10.47c)$$

where we introduced the  $(u, v, w)$  velocity components according to equation (9.81). With the zonal velocity  $u = \dot{\lambda} r_{\perp} = \dot{\lambda} r \cos \phi$ , we have

$$r \cos \phi \ddot{\lambda} = \dot{u} + \frac{u}{r \cos \phi} (v \sin \phi - w \cos \phi), \quad (10.48)$$

so that equation (10.47c) takes the form

$$\frac{1}{m} \frac{dL^z}{dt} = 2(w \cos \phi - v \sin \phi)(u + r \Omega \cos \phi) + (r \cos \phi)^2 \ddot{\lambda} \quad (10.49a)$$

$$= (w \cos \phi - v \sin \phi)(u + 2r \Omega \cos \phi) + \dot{u} r \cos \phi. \quad (10.49b)$$

Setting  $dL^z/dt = 0$  and rearranging then leads to a prognostic equation for the zonal velocity

$$\frac{du}{dt} = \left[ \frac{u}{r \cos \phi} + 2\Omega \right] (v \sin \phi - w \cos \phi). \quad (10.50)$$

The first term in the bracket arises from curvature of the sphere (the “metric acceleration”) whereas the second term is the Coriolis acceleration.

The same result can be obtained by performing the time derivative on the second form of the axial angular momentum in equation (10.34), in which case

$$\frac{1}{m} \frac{dL^z}{dt} = \frac{d[u r \cos \phi + \Omega(r \cos \phi)^2]}{dt} \quad (10.51a)$$

$$= \dot{u} r \cos \phi + u \dot{r} \cos \phi - u r \dot{\phi} \sin \phi + 2\Omega r \cos \phi (\dot{r} \cos \phi - r \dot{\phi} \sin \phi). \quad (10.51b)$$

Again, setting  $dL^z/dt = 0$  and rearranging leads to the zonal acceleration (10.50).

### 10.8.6 Coriolis acceleration from meridional motion

What happens when zonal motion is perturbed in the meridional direction? Following the angular momentum constraint (10.43), a poleward perturbation,  $\delta\phi > 0$ , to a northern hemisphere particle will have  $\dot{u} > 0$ , with this zonal acceleration corresponding to a rightward deflection relative to the  $\delta\phi > 0$  perturbation. Likewise, for  $\delta\phi < 0$  a northern hemisphere particle will have  $\dot{u} < 0$ , which corresponds to a rightward deflection relative to the  $\delta\phi < 0$  perturbation.

We see the correspondence to the Coriolis acceleration when viewed in the rotating reference frame by examining the meridional momentum equation (9.170)

$$\dot{v} + \frac{v w + u^2 \tan \phi}{r} = -\underline{2 \Omega u \sin \phi}, \quad (10.52)$$

with the Coriolis acceleration underlined on the right hand side. In the northern hemisphere ( $\sin \phi > 0$ ), the Coriolis acceleration gives rise to a rightward (equatorward) acceleration,  $-2 \Omega u \sin \phi < 0$ , when the particle is moving eastward,  $u > 0$  (super-rotating), thus inducing a negative meridional acceleration,  $\dot{v} < 0$ . Conversely, if the particle is moving to the west so that  $u < 0$ , then the Coriolis acceleration is again to the right, only this time it deflects the particle in the poleward direction with  $\dot{v} > 0$ . The analogous considerations hold in the southern hemisphere where the particle is deflected to the left by the Coriolis acceleration. These motions are reflected in Figure 10.4.

### 10.8.7 When lateral motions dominate vertical motions

We here consider two approximations relevant to large scale geophysical fluid motions.

1. The particle kinetic energy is dominated by lateral motions on the sphere (i.e., motion at constant radial position).
2. Vertical (radial) excursions are much smaller than the earth radius.

When applied to a fluid, the first assumption leads to the hydrostatic approximation (Section 22.2), and the second assumption leads to the shallow fluid approximation (Section 22.1.2). Self-consistency of the equations of motion means that these two assumptions must be applied together.

Dropping the vertical velocity component to the kinetic energy leads to

$$K \approx \frac{m}{2} [(u + r_{\perp} \Omega)^2 + v^2]. \quad (10.53)$$

The second assumption means that the axial angular momentum takes the approximate form

$$L^z \approx m R_{\perp} (u + \Omega R_{\perp}) = m R_{\perp}^2 (\dot{\lambda} + \Omega), \quad (10.54)$$

where

$$r = R + z \approx R \quad \text{and} \quad R_{\perp} = R \cos \phi. \quad (10.55)$$

The approximate angular momentum (10.54) ignores contributions from vertical motion in changing the moment-arm. Indeed, as noted in Section 10.8.1, vertical movements within the atmosphere and ocean (relatively thin fluid layers over the earth's surface) lead to a relatively small modification to the moment-arm, so the assumption that  $r_{\perp} \approx R \cos \phi$  is reasonable. With  $r \approx R$ , the zonal acceleration (10.50) is modified to the form

$$\frac{du}{dt} = v \left[ \frac{u \tan \phi}{R} + f \right] \quad \text{where} \quad f = 2 \Omega \sin \phi. \quad (10.56)$$

That is, we dropped the vertical velocity component,  $w$ , from the general form of the acceleration (10.50). Correspondingly, the meridional momentum equation takes the form

$$\frac{dv}{dt} = -u \left[ \frac{u \tan \phi}{R} + f \right]. \quad (10.57)$$

These approximate forms for the zonal and meridional accelerations appear in the primitive equations of geophysical fluid dynamics presented in Section 22.1.

### 10.8.8 Comments

To orient oneself according to the Coriolis acceleration, one needs to remember one fact: in the northern hemisphere motion on the sphere at constant radius ( $\delta r = 0$ ) leads to a rightward deflection whereas in the southern hemisphere the particle experiences a leftward deflection. Figure 10.4 depicts some sample deflections.

A concise summary of many features of rotating physics is provided by [this video from SciencePrimer](#).

## 10.9 Mechanical energy conservation

Does the particle know anything about the origin of time? Since the angular velocity of the planet and the gravitational acceleration are both assumed constant in time, then changing the time will leave the physical system unaltered. That is, the physical system remains unchanged if we shift all clocks by a constant amount. Through Noether's Theorem, this symmetry in time leads to mechanical energy conservation. That is, the particle's mechanical energy is fixed by the initial conditions. We here prove that mechanical energy is constant in time by manipulating the equations of motion. Many of the manipulations also occur when considering the mechanical energy conservation laws for a continuum fluid discussed in Chapter 17.

### 10.9.1 Some properties of kinetic energy

In this subsection we establish some basic properties of kinetic energy for a particle. As we saw in Section 9.1.5, changes in the kinetic energy of a particle equal to the *mechanical work* done on the particle as it moves along its trajectory

$$K(t_2) - K(t_1) = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \mathbf{F} \cdot d\mathbf{x} = \int_{t_1}^{t_2} \mathbf{F} \cdot \mathbf{V} dt, \quad (10.58)$$

where  $\mathbf{V} dt = d\mathbf{x}$  defines the vector increment along the trajectory, and  $\mathbf{x}_{1,2}$  are the endpoints of the trajectory. The integrand,  $\mathbf{F} \cdot \mathbf{V}$ , is known as the *power*. Hence, equation (10.58) says that the time integral of the power equals to the difference in kinetic energy between the final and initial times.

The kinetic energy is *not* Galilean invariant since movement to another inertial reference frame leads to the kinetic energy change

$$\bar{\mathbf{V}} = \mathbf{V} + \mathbf{U} \implies \bar{K} = K + \frac{m}{2} (2 \mathbf{V} \cdot \mathbf{U} + \mathbf{U} \cdot \mathbf{U}), \quad (10.59)$$

where  $\mathbf{U}$  is a constant boost velocity so that  $d\mathbf{U}/dt = 0$ . We do not expect kinetic energy to be Galilean invariant since it measures energy of motion relative to the chosen reference frame. Even so, the time change of the kinetic energy in a different inertial frame is given by the power in the new frame

$$\frac{d\bar{K}}{dt} = \frac{dK}{dt} + m \mathbf{A} \cdot \mathbf{U} = \mathbf{F} \cdot \mathbf{V} + \mathbf{F} \cdot \mathbf{U} = \mathbf{F} \cdot \bar{\mathbf{V}}. \quad (10.60)$$

Hence, we can directly connect kinetic energy changes to forces within an arbitrary inertial reference frame.

*Cartesian expression for kinetic energy*

Consider the expression for kinetic energy when introducing the velocity of the rotating reference frame. Writing the inertial velocity in the planetary Cartesian form

$$\mathbf{V} = \mathbf{V}_{\text{Cartesian}} + \mathbf{U}_{\text{solid}}, \quad (10.61)$$

leads to

$$K = \frac{m}{2} [\mathbf{V}_{\text{Cartesian}} \cdot \mathbf{V}_{\text{Cartesian}} + 2 \mathbf{V}_{\text{Cartesian}} \cdot \mathbf{U}_{\text{solid}} + \mathbf{U}_{\text{solid}} \cdot \mathbf{U}_{\text{solid}}] \quad (10.62)$$

The first term arises from motion of the particle relative to the rotating sphere; the second arises from coupling between relative velocity and solid-body velocity; and the third arises from solid-body motion of the sphere.

*Spherical expression for kinetic energy: Part I*

To expose spherical symmetry of the physical system, we express the kinetic energy in terms of the planetary spherical coordinates defined in Figure 8.1. Doing so for the solid body velocity leads to equation (9.83)

$$\mathbf{U}_{\text{solid}} = \Omega r \cos \phi (-\sin \lambda \hat{\mathbf{x}} + \cos \lambda \hat{\mathbf{y}}). \quad (10.63)$$

Likewise, the velocity components measured in the rotating frame are given by

$$\dot{X} = \frac{d(r \cos \phi \cos \lambda)}{dt} = \dot{r} \cos \phi \cos \lambda - r \dot{\phi} \sin \phi \cos \lambda - r \dot{\lambda} \cos \phi \sin \lambda \quad (10.64a)$$

$$\dot{Y} = \frac{d(r \cos \phi \sin \lambda)}{dt} = \dot{r} \cos \phi \sin \lambda - r \dot{\phi} \sin \phi \sin \lambda + r \dot{\lambda} \cos \phi \cos \lambda \quad (10.64b)$$

$$\dot{Z} = \frac{d(r \sin \phi)}{dt} = \dot{r} \sin \phi + r \dot{\phi} \cos \phi. \quad (10.64c)$$

Bringing terms together then leads to the kinetic energy in terms of spherical coordinates

$$K = \frac{m}{2} [(r^2 + r^2 \dot{\phi}^2 + \dot{\lambda}^2 r^2 \cos^2 \phi) + (2 \Omega r^2 \dot{\lambda} \cos^2 \phi) + (\Omega r \cos \phi)^2]. \quad (10.65)$$

*Spherical expression for kinetic energy: Part II*

An alternative means for deriving the kinetic energy in equation (10.65) makes use of the spherical coordinate form of the inertial velocity given by equation (9.79f), in which case

$$\mathbf{V} = (u + r_{\perp} \Omega) \hat{\lambda} + v \hat{\phi} + w \hat{r}, \quad (10.66)$$

so that

$$K = \frac{m}{2} [(u + r_{\perp} \Omega)^2 + v^2 + w^2], \quad (10.67)$$

where  $r_{\perp} = r \cos \phi$ . Additionally, as discussed in Section 10.7, the axial angular momentum is given by

$$L^z = m r_{\perp} (u + r_{\perp} \Omega) \equiv m l^z, \quad (10.68)$$

and this property is a constant of the motion when there is azimuthal (zonal) symmetry. It is thus convenient to write the kinetic energy as

$$K = \frac{m}{2} [(l^z/r_{\perp})^2 + v^2 + w^2]. \quad (10.69)$$

*Geopotential expression for mechanical energy*

As seen in Section 10.9.4, the conserved form of the mechanical energy using geopotential coordinates takes on the form

$$M_{\text{geop}} = \frac{m}{2} [u^2 + v^2 + w^2 + 2g r], \quad (10.70)$$

where each of these symbols takes on their geopotential interpretation.

### 10.9.2 Planetary Cartesian mechanical energy

The time derivative of the kinetic energy is given by

$$\frac{dK}{dt} = m \mathbf{V} \cdot \frac{d\mathbf{V}}{dt} = m \mathbf{V} \cdot \mathbf{A} = -m \mathbf{V} \cdot \nabla \Phi_e. \quad (10.71)$$

For the final equality we introduced the gravitational potential given that the particle only feels an external force from gravity as per equation (9.154). The gravitational potential is given by (see equation (9.148))

$$\Phi_e = g_e r, \quad (10.72)$$

so that

$$\frac{dK}{dt} = -m \mathbf{V} \cdot \nabla \Phi_e = -m g_e \dot{r}. \quad (10.73)$$

This result means that kinetic energy is reduced when moving the particle away from the earth center ( $\dot{r} > 0$ ). Moving away from the earth requires work to overcome the gravitational attraction. This work to overcome the gravitational attraction is taken away from the kinetic energy of the particle. Furthermore, the work is added to the gravitational potential energy, whose evolution is given by (see equation (9.150))

$$\frac{dP_e}{dt} = m g_e \dot{r}, \quad (10.74)$$

where we assumed a constant gravitational acceleration  $g_e$ . Consequently, as the particle moves away from the earth center, its reduction in kinetic energy is exactly compensated by an increase in potential energy. Hence, the mechanical energy for the particle remains constant throughout the motion

$$\frac{d(K + P_e)}{dt} = 0, \quad (10.75)$$

where the mechanical energy is the sum of the inertial kinetic energy plus the gravitational potential energy

$$M = K + P_e \quad (10.76a)$$

$$= \frac{m}{2} \mathbf{V} \cdot \mathbf{V} + m \Phi_e \quad (10.76b)$$

$$= \frac{m}{2} [(u + r_\perp \Omega)^2 + v^2 + w^2] + m g_e r \quad (10.76c)$$

$$= \frac{m}{2} [(l^z/r_\perp)^2 + v^2 + w^2] + m g_e r. \quad (10.76d)$$

### 10.9.3 Planetary spherical mechanical energy

It is physically revealing to expose the exchange of mechanical energy between kinetic and gravitational potential energies. Furthermore, knowledge of the total mechanical energy at any time affords knowledge for all time since the mechanical energy remains constant. Following from the discussion in Section 10.8, where we examined the constraints on particle motion due to

conservation of axial angular momentum, we here ask similar questions about mechanical energy conservation. We make use of the spherical form of the equations of motion, equations (9.163)-(9.165), which expose the planetary centrifugal and Coriolis accelerations, and pursue the calculation for geopotential coordinates in Section 10.9.4.

We find it convenient to write the momentum equations (9.163)-(9.165) in terms of the distance to the polar axis,  $r_\perp = r \cos \phi$ , and its time derivative,  $\dot{r}_\perp = w \cos \phi - v \sin \phi$

$$\frac{d}{dt} [r_\perp u + \Omega r_\perp^2] = 0 \quad (10.77a)$$

$$\dot{v} = -\frac{v w}{r} - \frac{u \tan \phi}{r} (u + 2 \Omega r_\perp) - r_\perp \Omega^2 \sin \phi \quad (10.77b)$$

$$\dot{w} = \frac{u^2 + v^2}{r} + 2 \Omega u \cos \phi + r_\perp \Omega^2 \cos \phi - g_e. \quad (10.77c)$$

Equation (10.77a) expresses the conservation of axial angular momentum,  $\dot{l}^z = 0$ , where the axial angular momentum per mass is  $l^z = r_\perp (u + r_\perp \Omega)$  (Section 10.7). For the mechanical energy, we have

$$\dot{M} = 0 \quad \text{with} \quad M = \frac{m}{2} [(l^z/r_\perp)^2 + v^2 + w^2] + m g_e r, \quad (10.78)$$

where  $l^z/r_\perp = u + r_\perp \Omega$  is the zonal component to the inertial velocity (equation (9.79f)). We now show that  $\dot{M} = 0$  arises from the momentum equations. Performing the time derivative, and setting  $dl^z/dt = 0$ , leads to

$$\frac{1}{m} \dot{M} = \frac{1}{2} \frac{d}{dt} [(l^z/r_\perp)^2 + v^2 + w^2 + 2 g_e r] = -\frac{(l^z)^2 \dot{r}_\perp}{(r_\perp)^3} + v \dot{v} + w (\dot{w} + g_e). \quad (10.79)$$

Use of the meridional momentum equation (10.77b) renders

$$v \dot{v} = -v \left[ \frac{v w}{r} + \frac{u \tan \phi}{r} (u + 2 \Omega r_\perp) + r_\perp \Omega^2 \sin \phi \right] \quad (10.80a)$$

$$= -\frac{v^2 w}{r} - \frac{v \tan \phi}{r} (u + r_\perp \Omega)^2. \quad (10.80b)$$

Likewise, the vertical momentum equation (10.77c) renders

$$w (\dot{w} + g_e) = \frac{v^2 w}{r} + \frac{w}{r} [u^2 + 2 \Omega u r_\perp + (r_\perp \Omega)^2] \quad (10.81a)$$

$$= \frac{v^2 w}{r} + \frac{w}{r} (u + r_\perp \Omega)^2, \quad (10.81b)$$

so that

$$v \dot{v} + w (\dot{w} + g_e) = r^{-1} (-v \tan \phi + w) (u + r_\perp \Omega)^2 = \frac{(l^z)^2 \dot{r}_\perp}{(r_\perp)^3}. \quad (10.82)$$

Combining this result with equation (10.79) leads to the expected  $\dot{M} = 0$ , so that angular momentum conservation combined with the meridional and vertical momentum equations is equivalent to mechanical energy conservation.

### 10.9.4 Geopotential mechanical energy

Now consider the mechanical energy conservation when using geopotential coordinates with the equations of motion (9.169)-(9.171)

$$\dot{u} + \frac{u(w - v \tan \phi)}{r} + 2\Omega(w \cos \phi - v \sin \phi) = 0 \quad (10.83a)$$

$$\dot{v} + \frac{v w + u^2 \tan \phi}{r} + 2\Omega u \sin \phi = 0 \quad (10.83b)$$

$$\dot{w} - \frac{u^2 + v^2}{r} - 2\Omega u \cos \phi = -g. \quad (10.83c)$$

Multiplying each equation by its respective velocity component and summing yields

$$\frac{1}{m} \dot{M}_{\text{geop}} = \frac{1}{2} \frac{d}{dt} [u^2 + v^2 + w^2 + 2gr] = 0. \quad (10.84)$$

The conserved mechanical energy for the particle written in geopotential coordinates

$$M_{\text{geop}} = m(u^2 + v^2 + w^2)/2 + mg r \quad (10.85)$$

is compared to that written using spherical coordinates in equation (10.78). We note that since the coordinates are different (spherical versus geopotential), the velocity components  $(u, v, w)$  are slightly different in the two coordinate systems, as is the radial position.

## 10.10 Sample trajectories using spherical coordinates

We here examine two relatively simple trajectories using spherical coordinates. We do so to illustrate how the dynamical properties discussed in this chapter, particularly angular momentum conservation, help to determine trajectories. The discussion complements that considered in Exercise 9.8.

### 10.10.1 Free fall to the center

A particle freely falling to the center of the sphere has a trajectory given by

$$u = -r_\perp \Omega \quad \text{and} \quad v = 0 \quad \text{and} \quad \dot{w} = -g_e \implies w = -g_e t + w_0. \quad (10.86)$$

A zonal velocity of  $u = -r_\perp \Omega$  (to the west) means that the particle has zero zonal inertial velocity; i.e., the particle has a fixed longitude in absolute space. It also means there is zero axial angular momentum,  $l^z = 0$ . To verify that axial angular momentum remains zero, note that

$$\dot{l}^z = 0 \implies \dot{u} r_\perp = -\dot{r}_\perp (u + 2\Omega r_\perp), \quad (10.87)$$

which is satisfied since  $u = -r_\perp \Omega$  means that  $\dot{u} = -\dot{r}_\perp \Omega$ . Furthermore, note that the zonal acceleration is given by

$$\dot{u} = -\Omega \dot{r}_\perp = -\Omega(w \cos \phi - v \sin \phi) = -\Omega w \cos \phi = (\Omega g_e \cos \phi) t > 0, \quad (10.88)$$

where we assumed the particle is released with  $w_0 = 0$ . As the particle falls, and thus reduces its distance from the polar axis, it zonally accelerates with  $\dot{u} > 0$  to maintain zero angular momentum. This acceleration slows the particle's relative speed, which is expected since  $u = -r_\perp \Omega$  means

the relative zonal velocity goes to zero as the particle approaches the axis of rotation.

### 10.10.2 Free fall to the equatorial plane

Now consider a trajectory with a constant zonal velocity, in which case  $\dot{u} = 0$  so that the angular momentum equation (10.77a) leads to

$$\dot{r}_\perp (u + 2\Omega r_\perp) = 0. \quad (10.89)$$

There are two ways to satisfy this constraint, one being to set  $u = -2\Omega r_\perp$ . We here choose to instead examine the case with a fixed moment-arm,

$$\dot{r}_\perp = 0 \implies w \cos \phi = v \sin \phi. \quad (10.90)$$

This relation couples vertical and meridional motion in a manner that keeps the distance to the rotational axis fixed. For example, if the particle is falling towards the earth center so that  $w \cos \phi < 0$ , then there is an equatorward meridional velocity to keep the distance from the rotational axis fixed. In this manner, the particle is freely falling not towards the earth center but instead towards the equatorial plane, all while maintaining a fixed zonal velocity with  $\dot{u} = 0$ .

Use of the relation (10.90) between  $v$  and  $w$  leads to the meridional acceleration

$$r_\perp \dot{v} = -v w \cos \phi - u \sin \phi (u + 2\Omega r_\perp) - (r_\perp \Omega)^2 \sin \phi = -\sin \phi [v^2 + (l^z/r_\perp)^2], \quad (10.91)$$

which is negative in the northern hemisphere and positive in the southern; i.e., it is always directed to lower latitudes. Similarly, the vertical momentum equation leads to

$$r (\dot{w} + g_e) = v^2 + (l^z/r_\perp)^2 > 0, \quad (10.92)$$

which is always positive, meaning the vertical acceleration is always dominated by the earth's gravitational acceleration. Finally, the meridional and vertical accelerations are related by

$$\dot{v} \cos \phi + (\dot{w} + g_e) \sin \phi = 0. \quad (10.93)$$

When the particle reaches the equator at  $\phi = 0$ , both the meridional acceleration and the vertical velocity vanish. In contrast, at the poles where  $\phi = \pm\pi/2$ , the vertical acceleration is  $\dot{w} = -g_e$  whereas the meridional velocity vanishes.



## 10.11 Exercises

### EXERCISE 10.1: NEGATIVE AXIAL ANGULAR MOMENTUM

Recall in Section 10.8 we assume the axial angular momentum is positive, which is geophysically the common situation since axial angular momentum from the solid-body motion is so large relative to motion of geophysical fluids. But let us consider the uncommon case where the particle moves zonally westward at a speed greater than the planetary rotation speed so that

$$\dot{\lambda} + \Omega < 0 \iff u + \Omega r_\perp < 0, \quad (10.94)$$

which means the axial angular momentum per mass of the particle is negative

$$l^z = r_{\perp} (u + r_{\perp} \Omega) = -|l^z| < 0. \quad (10.95)$$

- (A) Discuss what happens to  $\delta\dot{\lambda}$  for the particle as it is deflected poleward with constant radius while conserving axial angular momentum. Hint: consider the first form of equation (10.39).
- (B) Discuss what happens to  $\delta u$  for the particle as it is deflected poleward with constant radius while conserving axial angular momentum. Discuss the cases where
- (i)  $|l^z| = 0$
  - (ii)  $|l^z| < \Omega r_{\perp}^2$ .
  - (iii)  $|l^z| > \Omega r_{\perp}^2$

Hint: consider the second form of equation (10.39).

- (C) Is fluid particle motion with  $u + \Omega r_{\perp} < 0$  relevant for the terrestrial atmosphere and ocean? Why? To help answer this question, what is  $\Omega r_{\perp}$  for  $\phi = \pi/4$  and  $r = R_e$ ? Note, we already provided the result for the equator just after equation (10.36). Compare these speeds to that of a category 5 tropical cyclone (Google it).



**Part III**

**Kinematics of fluid flow**

In this part of the book we move from the discrete particle mechanics studied in Part II to now focus on continuous fluid media. We motivate the study of continuous media in Chapter 11 by noting the huge space and time scale separation between molecular motions and the motion of macroscopic fluid elements. Thereafter we develop kinematics for classical non-relativistic fluid flow. Quite conveniently, key kinematic properties of non-rotating flows also hold for the fluid flow on steady rotating planets such as considered in this book. The reason is that steady solid-body rotation does not directly impart any strain to the flow, where strain refers to the relative motion between fluid elements (Chapter 12). Rotation does impart a planetary component to the vorticity of geophysical fluids, with implications for our study of vorticity in Part VI. However, for the purpose of this part of the book we can ignore planetary rotation.

### EULERIAN AND LAGRANGIAN REFERENCE FRAMES

The *Eulerian and Lagrangian reference frames* provide dual kinematic descriptions of fluid flows. The Eulerian frame describes fluid motion relative to a frame fixed in the laboratory whereas the Lagrangian frame follows a moving fluid particle. The Eulerian frame is inertial (when the laboratory is not accelerating), whereas the Lagrangian is non-inertial since fluid particles generally accelerate. Having two descriptions of the same motion provides a synergy that is missing with either alone, thus exemplifying a maxim:

If you can study, describe, solve, or understand a physics problem more than one way,  
then do so!

We require skills to move between the Eulerian and Lagrangian descriptions, with tools from mathematical transformation theory of Part I of great use for this purpose. Elements of Eulerian and Lagrangian kinematics are the focus of Chapter 12, and Chapter 13 further develops the kinematics of material lines, areas, and volumes.

### MASS AND MATTER CONSERVATION ARE PART OF FLUID KINEMATICS

The conservation of mass plays a central role in physics. For fluids, mass conservation constrains the flow regardless what forces act on the fluid. Hence, we include mass conservation as a part of fluid kinematics rather than fluid dynamics. Mass conservation, and its expression as volume conservation for incompressible flows, are the topics of Chapters 14 and 16. Chapter 15 develops the allied study of matter conservation and matter flow, with this study forming the foundations for *tracer mechanics* that form much of Part IX in this book.

### FLUID KINEMATICS + FLUID DYNAMICS = FLUID MECHANICS

Kinematics is concerned with the intrinsic properties of motion, including properties of the space and time in which motion occurs. It is the complement to dynamics, which is concerned with the causes of motion that arise through the action of forces. In one sense, kinematics deduces the acceleration whereas dynamics deduces the forces, with Newton's second law linking the two via the equation of motion:  $\mathbf{F} = m \mathbf{a}$ . In fluid mechanics, kinematics studies the flow of a fluid and its matter constituents, whereas dynamics studies the forces causing the motion. Furthermore, as discussed in Chapter 10, symmetries of a mechanical system lead, through Noether's Theorem, to dynamical conservation laws. That is, symmetries, which embody kinematic properties, lead to dynamical invariants maintained by the motion, with these invariants constraining the motion. The intellectual avenues pursued in developing a mechanical description of fluid motion are many and varied, with fluid kinematics and fluid dynamics intimately woven into the fabric of that description.

# Chapter 11

## Continuum approximation

Viewed macroscopically, a fluid deforms continuously when applying a force so that a fluid has no preferred shape. Correspondingly, a fluid responds to a shearing stress by moving. Ordinary gases and liquids are canonical examples of fluids, with gases filling any container with its molecules widely separated whereas molecules in liquids are much closer together so that liquids are far less compressible than gases.

For geophysical fluid mechanics, we are concerned with the atmosphere (mostly a gas) and the ocean (mostly a liquid). We are furthermore interested in macroscopic properties of fluid motion, with no interest in describing molecular degrees of freedom. Nor do we consider rarefied gas dynamics, which is a subject appropriate for the upper bounds of the atmosphere. For these reasons we pursue a phenomenological approach that makes use of conservation laws describing the motion of a continuous fluid media. This treatment is based on the *continuum approximation*, which assumes that mathematical limits for fluid volumes tending to zero are reached on length and time scales very large compared to molecular scales.<sup>1</sup> The temporal version of the continuum approximation corresponds to *quasi-static processes*, which forms the basis for quasi-equilibrium thermodynamics. Quasi-static processes refer to macroscopic motion that evolves with time scales far larger than time scales of molecular motions, so that when treated thermodynamically a fluid element evolves smoothly from one local thermodynamic equilibrium state to another.<sup>2</sup>

The huge space and time scale separation that supports the continuum approximation allows us to make use of calculus for describing the mechanics of fluid motion. That is, the continuum approximation makes fluid mechanics a continuous field theory. Correspondingly, the conservation laws describing fluid motion are partial differential equations.

### READER'S GUIDE TO THIS CHAPTER

This chapter presents salient points supporting our use of a space and time continuous description of fluid mechanics. Section 11.2 summarizes the key results and Section 11.3 provides a bit more detail by quoting from kinetic theory. Our overall goal here is to unpack the dictum *macroscopically small yet microscopically large*, which summarizes the regime considered by the continuum approximation and the quasi-static approximation. For this purpose, we borrow from the kinetic theory of gases as treated in statistical physics books such as [Reif \(1965\)](#) and [Huang \(1987\)](#). Chapter 1 of [Salmon \(1998\)](#) also provides a compelling discussion with application to geophysical fluid mechanics. No prior exposure to these treatments is necessary

<sup>1</sup>The continuum approximation used for continuum mechanics is not to be confused with the *continuum hypothesis* in mathematical set theory.

<sup>2</sup>We study equilibrium thermodynamics in Chapter 20.

nor do we dive into the details.

11.1	Loose ends . . . . .	230
11.2	A variety of length scales . . . . .	230
11.2.1	Molecular and macroscopic length scales . . . . .	230
11.2.2	Continuous fields rather than discrete molecules . . . . .	231
11.2.3	Reynolds number and the continuum length scale . . . . .	232
11.2.4	Resolution of measurements and simulations . . . . .	233
11.2.5	Comments . . . . .	234
11.3	Results from kinetic theory . . . . .	234
11.3.1	A mole and Avogadro's number . . . . .	234
11.3.2	Ideal gas law . . . . .	234
11.3.3	Molecular mean free path . . . . .	235
11.3.4	Root mean square molecular speed . . . . .	236
11.3.5	Basis for the quasi-static approximation . . . . .	236
11.3.6	Macroscopically small and microscopically large . . . . .	237
11.3.7	Whence a rigorous treatment? . . . . .	237
11.3.8	Further study . . . . .	238

## 11.1 Loose ends

- Add a figure for Section 11.2.4.
- Can one be more precise about the scale in Figure 11.2 where measurements become fuzzy?

## 11.2 A variety of length scales

Matter is comprised of molecules. However, fluid mechanics is not concerned with the motion of individual molecular degrees of freedom. Rather, fluid mechanics is concerned with phenomenological conservation laws satisfied by a continuous fluid material. This approach represents an idealization that is supported by centuries of successful descriptions of macroscopic fluid motion.

We here outline the essential features of the continuum approximation. This approximation supports our macroscopic description of a fluid in terms of continuous fields rather than discrete molecules. More details are offered in Section 11.3, although a full discussion is outside the subject of fluid mechanics, instead resting deep within the field of statistical physics and kinetic theory.

### 11.2.1 Molecular and macroscopic length scales

A fluid mechanical description focuses on fluid regions that are macroscopically small (e.g.,  $L_{\text{macro}} \sim 10^{-3}$  m) yet microscopically large (e.g.,  $L_{\text{macro}} \gg L_{\text{mfp}} \sim 10^{-7}$  m, where  $L_{\text{mfp}}$  is the molecular mean free path). A region of air with volume  $L_{\text{macro}}^3$  contains roughly  $10^{16}$  air molecules at standard temperature ( $T_{\text{stand}} = 0^\circ\text{C} = 273.15$  K) and standard atmospheric pressure ( $p_{\text{stand}} = 101.325 \times 10^3$  Pa), whereas that same volume contains roughly  $10^{19}$  water molecules. These numbers (justified in Section 11.3) illustrate the notions of macroscopically small yet microscopically large. It is only when reaching length scales on the order of the molecular mean free path that we need to be concerned with the discrete nature of matter. Figure 11.1 offers a schematic to illustrate these quite distinct length scales.

The huge number of molecules within a macroscopically tiny region justifies our assumption that physical properties are homogeneous over regions of size  $L_{\text{macro}}$ . In essence, this *continuum*

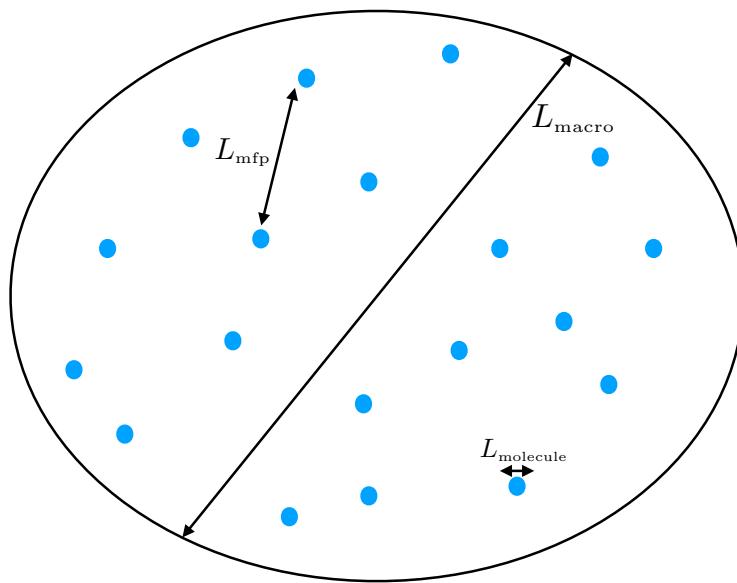


FIGURE 11.1: Schematic to illustrate the three length scales considered when making the continuum approximation. The blue circles represent molecules with diameter  $L_{\text{molecule}}$ . On average, molecules are separated by the mean free path,  $L_{\text{mfp}} \approx 1000 L_{\text{molecule}}$ . The smallest macroscopic length scale of interest for fluid mechanics is  $L_{\text{macro}} \sim 10^{-3}$  m, which is roughly  $L_{\text{macro}} = 10^4 L_{\text{mfp}}$  for an ideal gas at standard conditions. A region of air with volume  $L_{\text{macro}}^3$  contains roughly  $10^{16}$  air molecules, whereas that same volume contains roughly  $10^{19}$  water molecules. For either case, the Law of Large Numbers greatly helps in taking the continuum limit. Note that this schematic is not drawn to scale!

*approximation* works with small but finite sized fluid elements whose mean dynamical properties (e.g., velocity, vorticity) and thermodynamical properties (e.g., mass density, matter concentration, temperature, specific entropy) are defined locally at any point within the continuous fluid media.

### 11.2.2 Continuous fields rather than discrete molecules

When measured on length scales of the mean free path, material properties exhibit very large fluctuations on time scales of order  $L_{\text{mfp}}/v_{\text{rms}}$ , where  $v_{\text{rms}}$  is the root-mean-square speed of a fluid molecule (see Section 11.3.4). However, on macroscopic scales encompassing many molecular degrees of freedom, fluid matter appears continuous in both space and time.

Let us be a bit more precise by considering the measurement of mass density for a prescribed region of fluid,  $\delta V$ . To compute the mass density we simply take the ratio of the mass of fluid in the region,  $\delta m$ , to the region volume. When the region volume is sizable and thus containing many molecules, we can maintain a relatively fixed mass since molecular fluctuations have a relatively tiny effect on  $\delta m$ . Hence, we can maintain a precise measurement of the mass density,  $\delta m/\delta V$ . However, when the volume of the region reaches down to the order of  $\delta V \sim L_{\text{mfp}}^3$ , then molecular fluctuations lead to a relatively large fluctuation in the region mass. We thus lose the notion of a smooth and continuous mass density when the volume approaches that set by the molecular mean free path. This situation is depicted in Figure 11.2.

The ratio of the mean free path to the macroscopic length scale is known as the Knudsen number

$$\text{Kn} = \frac{L_{\text{mfp}}}{L_{\text{macro}}}. \quad (11.1)$$

For our purposes, we are concerned only with fluid conditions where the mean free path is micro-

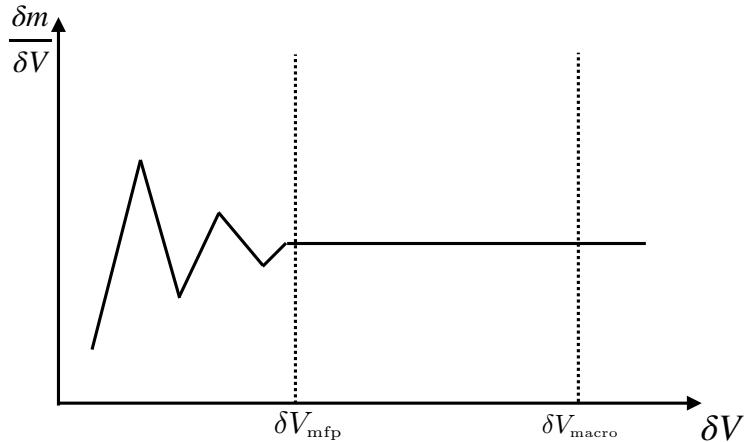


FIGURE 11.2: The measurement of mass density of a fluid becomes erratic for volumes smaller than that determined by the molecular mean free path,  $\delta V_{\text{mfp}} \sim L_{\text{mfp}}^3$ . For fluid mechanics we are concerned with macroscopic length scales much larger than the mean free path,  $L_{\text{macro}} \gg L_{\text{mfp}}$ , in which case the density is a smooth function of space and time. This figure is adapted from Figure 1.2.1 of [Batchelor \(1967\)](#).

scopic so that the Knudsen number is tiny

$$\text{Kn} \ll 1. \quad (11.2)$$

For tiny Knudsen numbers, we are led to make use of the continuum approximation. The continuum approximation allows us to employ fluid properties that take values at each point within a space and time continuum,  $(\mathbf{x}, t)$ . For example, we make use of the mass density,  $\rho(\mathbf{x}, t)$ , fluid velocity,  $\mathbf{v}(\mathbf{x}, t)$ , pressure  $p(\mathbf{x}, t)$ , temperature  $T(\mathbf{x}, t)$ , tracer concentration,  $C(\mathbf{x}, t)$ , and other thermodynamic fields.

We contrast the above to the study of a rarefied gas, such as in the outer reaches of the earth's atmosphere. With a relatively small number density of molecules, rarefied gases have macroscopic mean free paths so that there are relatively few molecular collisions in a given time increment. Correspondingly, a rarefied gas is far from thermodynamic equilibrium and the continuum approximation is not well suited to its description.

### 11.2.3 Reynolds number and the continuum length scale

The continuum field equations of fluid mechanics are formally established for fluid motions with length scales on the order of  $L_{\text{macro}}$  and larger. We stated earlier that  $L_{\text{macro}}$  is on the order of a millimetre, with that length loosely based on noting that there are a huge number of molecules in a volume with this size. Furthermore, most macroscopic measurements in a fluid cannot distinguish features much smaller than a millimetre. We here describe another means to determine this length scale.

Namely, we set  $L_{\text{macro}}$  to the length scale at which the Reynolds number is order unity

$$\text{Re}_{\text{macro}} = \frac{U L_{\text{macro}}}{\nu} \sim 1. \quad (11.3)$$

In this equation,  $\nu > 0$  is the kinematic viscosity (dimensions squared length per time), and  $U$  is the scale for a macroscopic fluid velocity fluctuation. The Reynolds number measures the ratio of inertial accelerations (accelerations felt by fluid elements) to frictional accelerations from viscous forces (forces due to the rubbing of fluid elements against one another). We provide more details concerning the Reynolds number when studying fluid stresses in Chapter 18. For present purposes,

we note that when the Reynolds number on the order of unity, viscous forces play a leading role in the acceleration of the fluid. In particular, it is at this scale that viscous accelerations act to dissipate kinetic energy, with this dissipation an important process in fluid turbulence. We are thus motivated to let the length scale where viscosity is important determine  $L_{\text{macro}}$ .

The kinematic viscosity is the ratio of the *dynamic viscosity* and the mass density. For air, the kinematic viscosity is (page 75 of [Gill \(1982\)](#))

$$\nu_{\text{air}} = \frac{1.7 \times 10^{-5} \text{ kg m}^{-1} \text{ s}^{-1}}{1.3 \text{ kg m}^{-3}} = 1.3 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}, \quad (11.4)$$

and a typical fluid velocity fluctuation has a scale  $10^{-1} \text{ m s}^{-1}$ , so that

$$L_{\text{macro}} \approx 10^{-4} \text{ m} = 0.1 \text{ mm}. \quad (11.5)$$

Water has a kinematic viscosity (page 75 of [Gill \(1982\)](#))

$$\nu_{\text{water}} = \frac{10^{-3} \text{ kg m}^{-1} \text{ s}^{-1}}{1000 \text{ kg m}^{-3}} \approx 10^{-6} \text{ m}^2 \text{ s}^{-1}, \quad (11.6)$$

and a fluid velocity fluctuation about 10 times smaller than air. Hence, the macroscopic length scale for water is on the order of that for air, both of which are roughly  $10^{-4} \text{ m}$ . The Reynolds number based macroscale length is not too far from the millimetre scale proposed earlier. We are thus further compelled to consider the macroscopic length scale to be on the order  $10^{-4} - 10^{-3} \text{ m}$ .

#### 11.2.4 Resolution of measurements and simulations

When we measure fluid motions in the laboratory or field, we generally do not measure the motions at scales on the order of  $L_{\text{macro}}$ . That is, our measurement devices generally have a spatial resolution much coarser than  $L_{\text{macro}}$ , so that  $L_{\text{measure}} \gg L_{\text{macro}}$ . Likewise, numerical simulations are generally made with discrete grids with length scales  $L_{\text{numerical}} \gg L_{\text{macro}}$ . The equations describing motions at the measurement/simulation length scales involve effects from coupled and nonlinear fluctuations occurring at the smaller (unmeasured) scales. These fluctuations, generally associated with turbulent or chaotic motions, have statistical correlations that can play a role, sometimes a dominant role, in the evolution of flow features at the measured/simulated scales. The parameterization of these correlations in terms of measured/simulated motions constitutes the *turbulence closure* problem. We do not study turbulence closure in this book though we do identify its implications at certain points.

It is important to acknowledge the limited ability of macroscopic measurements to accurately characterize fine scale motions. For this purpose define a gradient length scale

$$L_{\text{gradient}} = \frac{|\mathbf{v}|}{|\nabla \mathbf{v}|}, \quad (11.7)$$

where  $\mathbf{v}$  is the velocity of a fluid element and  $|\nabla \mathbf{v}|$  is the magnitude of velocity gradients. Decomposing fluctuations into Fourier modes allows us to see that an accurate measurement of velocity fluctuations with length scales  $L_{\text{gradient}}$  requires a measurement length scale that satisfies

$$2\pi L_{\text{measure}} \leq L_{\text{gradient}}. \quad (11.8)$$

This constraint means that to measure velocity fluctuations on a scale  $L_{\text{gradient}}$  requires a finer measurement sampling with  $L_{\text{measure}} = L_{\text{gradient}}/(2\pi)$ .

### 11.2.5 Comments

The above discussion of length scales transfers seamlessly over to time scales through dividing the length scale by the velocity scale. Correspondingly, fluctuations with time scales shorter than  $2\pi T_{\text{measure}}$  cannot be accurately measured.

## 11.3 Results from kinetic theory

If the reader is content to accept the continuum approximation on face value, then the material in this section can be readily skipped. For others, this section outlines results from the kinetic theory of ideal gases in support of the continuum approximation. Deductive treatments that transition from molecular mechanics to macroscopic fluid mechanics is a topic of the kinetic theory of gases and liquids, which is well outside our scope. In Section 11.3.8, we provide literature pointers for those wishing more rigor.

### 11.3.1 A mole and Avogadro's number

There are a tremendous number of molecules in the tiniest drop of water or puff of air. Just how many? To answer this question, we introduce the notion of a mole of matter. A mole is defined as the mass of a material substance that contains Avogadro's number of that substance, where

$$A_v = 6.022 \times 10^{23} \text{ mole}^{-1}. \quad (11.9)$$

Avogadro's number,  $A_v$ , is the proportionality constant converting from one molar mass of a substance to the mass of a substance. Avogadro's number is conventionally specified so that one mole of the carbon isotope  $^{12}\text{C}$  contains exactly 12 grams. Hence, 12 grams of  $^{12}\text{C}$  contains  $6.022 \times 10^{23}$  atoms of  $^{12}\text{C}$ . Avogadro's number provides a connection between scales active in the microscopic world of molecules to the macroscopic world of everyday experience.

Dry air (air with no water vapor) is comprised of oxygen molecules  $O_2$ , at roughly 22% by molecular mass, and nitrogen molecules  $N_2$ , at roughly 78% molecular mass.<sup>3</sup> The molar mass of dry air is thus

$$M_{\text{air}} = 0.22 * 32 \text{ g mole}^{-1} + 0.78 * 28 \text{ g mole}^{-1} \approx 28.8 \text{ g mole}^{-1}. \quad (11.10)$$

Pure (fresh) water is comprised of two hydrogen atoms and one oxygen atom. The molar mass of pure water is thus given by

$$M_{\text{water}} = 2 * 1 \text{ g mole}^{-1} + 16 \text{ g mole}^{-1} = 18 \text{ g mole}^{-1}. \quad (11.11)$$

### 11.3.2 Ideal gas law

The ideal gas law is given by

$$pV = nR_gT, \quad (11.12)$$

where  $p$  is the pressure,  $V$  is the volume,  $n$  is the number of moles,  $R_g$  is the universal gas constant,<sup>4</sup> and  $T$  is the absolute or thermodynamic temperature (temperature relative to absolute

<sup>3</sup>We here ignore the presence of other trace gases, such as  $CO_2$  and  $H_2O$ , although these gases are critical for understanding atmospheric radiation and hence the earth's energy budget.

<sup>4</sup>We write  $R_g$  rather than the more conventional  $R$  to distinguish from  $R$  commonly used in this book for the radius of a spherical earth.

zero). Measuring the temperature in Kelvin leads to the universal gas constant

$$R_g = 8.314 \text{ J mole}^{-1} \text{ K}^{-1} = 8.314 \text{ kg m}^2 \text{ s}^{-2} \text{ mole}^{-1} \text{ K}^{-1}, \quad (11.13)$$

where the second equality replaced the energy unit, Joule, by its MKS equivalent,

$$\text{J} = \text{kg m}^2 \text{ s}^{-2}. \quad (11.14)$$

Use of the ideal gas law (11.12) says that one mole of ideal gas at standard temperature ( $T_{\text{stand}} = 0^\circ\text{C} = 273.15 \text{ K}$ ) and standard atmospheric pressure ( $p_{\text{stand}} = 101.325 \times 10^3 \text{ Pa}$ ) occupies the following volume

$$V = \frac{n R_g T_{\text{stand}}}{p_{\text{stand}}} \quad (11.15a)$$

$$= \frac{(1 \text{ mole})(8.314 \text{ kg m}^2 \text{ s}^{-2} \text{ mole}^{-1} \text{ K}^{-1})(273.15 \text{ K})}{101.325 \times 10^3 \text{ kg m}^{-1} \text{ s}^{-2}} \quad (11.15b)$$

$$\approx 2.25 \times 10^{-2} \text{ m}^3, \quad (11.15c)$$

where we introduced the MKS units for pressure (force per unit area)

$$\text{Pa} = \text{N m}^{-2} = \text{kg m}^{-1} \text{ s}^{-2}. \quad (11.16)$$

Hence, the number density (number of molecules) for a mole of ideal gas is given by

$$n_{\text{gas}} = \frac{\text{number per mole}}{\text{volume per mole}} \quad (11.17a)$$

$$= \frac{A_v}{V} \quad (11.17b)$$

$$= \frac{6.022 \times 10^{23}}{2.25 \times 10^{-2} \text{ m}^3} \quad (11.17c)$$

$$= 2.68 \times 10^{25} \text{ m}^{-3}. \quad (11.17d)$$

Specializing to air, we compute the mass density of air at standard temperature and pressure as

$$\rho_{\text{air}} = \frac{M_{\text{air}}}{V} = \frac{28.8 \times 10^{-3} \text{ kg}}{2.25 \times 10^{-2} \text{ m}^3} = 1.28 \text{ kg m}^{-3}, \quad (11.18)$$

where we set  $M_{\text{air}} = 28.8 \times 10^{-3} \text{ kg}$  according to equation (11.10). This ideal gas density is close to the  $1.225 \text{ kg m}^{-3}$  density measured for air at standard conditions, thus giving us confidence for using the ideal gas law for dry air. Differences arise from trace constituents in air as well as inter-molecular forces (an ideal gas has no inter-molecular forces).

### 11.3.3 Molecular mean free path

We are in search of length scales relevant for molecular motion. One length scale is that of the molecule itself. Another is set by the distance between molecular collisions. The molecular mean free path is the mean distance that a molecule travels before colliding with another molecule. Arguments from kinetic theory of gases, applied to an ideal gas, lead to the expression

$$L_{\text{mfp}} = \frac{1}{\pi \sqrt{2} n_{\text{gas}} d^2} \quad (11.19)$$

where  $d$  is the diameter of the molecule. The mean diameter of air molecules is roughly

$$d_{\text{molecule air}} \approx 2 \times 10^{-10} \text{ m.} \quad (11.20)$$

Hence, the mean free path for air molecules at standard temperature and pressure is

$$L_{\text{mfp}} = \frac{1}{\pi \sqrt{2} n_{\text{gas}} d_{\text{molecule air}}^2} \quad (11.21a)$$

$$= \frac{1}{\pi \sqrt{2} (2.68 \times 10^{25} \text{ m}^{-3}) (2 \times 10^{-10} \text{ m})^2} \quad (11.21b)$$

$$= 2 \times 10^{-7} \text{ m.} \quad (11.21c)$$

The mean free path for an air molecule is roughly 1000 times larger than the molecular diameter (e.g., Figure 11.1).

### 11.3.4 Root mean square molecular speed

What is the mean speed for molecules moving through a gas? Again, kinetic theory for ideal gases offers an explicit expression, here written in terms of the pressure and density of the gas

$$v_{\text{rms}} = \sqrt{\frac{3p}{\rho}} = \sqrt{\frac{3R_g T}{M}}. \quad (11.22)$$

Note the direct relation between pressure, temperature, and speed. That is, molecules move faster at higher temperature, and thus impart larger pressure on their surrounding. At standard pressure and temperature, the root-mean-square speed for an air molecule is given by

$$v_{\text{rms}} = \sqrt{\frac{3p_{\text{stand}}}{\rho_{\text{air}}}} \quad (11.23a)$$

$$= \sqrt{\frac{3(101.325 \times 10^3 \text{ kg m}^{-1} \text{ s}^{-2})}{1.28 \text{ kg m}^{-3}}} \quad (11.23b)$$

$$= 487 \text{ m s}^{-1}. \quad (11.23c)$$

To get a sense for the relative scale of this speed, note that the speed of sound in air at standard temperature and pressure is  $331 \text{ m s}^{-1}$ . So these molecules are moving faster than sound! These speeds are correspondingly much higher than the speeds typical for fluid elements in the atmosphere and ocean.

### 11.3.5 Basis for the quasi-static approximation

Assuming one collision occurs within a mean free path, and the molecules are moving at the root-mean-square speed, we can estimate the time between collision according to

$$t_{\text{collision}} = \frac{L_{\text{mfp}}}{v_{\text{rms}}} \quad (11.24)$$

The corresponding time for air is given by

$$t_{\text{air}} = \frac{2 \times 10^{-7} \text{ m}}{487 \text{ m s}^{-1}} = 4.1 \times 10^{-10} \text{ s.} \quad (11.25)$$

Inverting this number, we see that there are roughly  $t_{\text{air}}^{-1} = 2.5 \times 10^9 \text{ s}^{-1}$  collisions per second.

The huge number of collisions per second means that for all macroscopic processes, including geophysical fluid flow, the dynamical time scales for the macroscopic motion are much larger than the time scales for molecular equilibration. We are thus led to define a *quasi-static macroscopic process* as one that occurs through a series of thermodynamic equilibrium states. Consequently, we can use equilibrium thermodynamic relations while allowing for time evolution of the macroscopic system. We have more to say on this topic in Chapters 20 and 21 when studying thermodynamics, with particular emphasis on the implications of the quasi-static approximation presented in Section 20.1.3.

### 11.3.6 Macroscopically small and microscopically large

For environmental measurements of the atmosphere and ocean, or for conventional measurements in laboratories, we can detect differences in fluid properties (e.g., mass density, velocity, tracer concentration, thermodynamic state properties) for length scales on the order of

$$L_{\text{macro}} = 10^{-3} \text{ m.} \quad (11.26)$$

For macroscopic purposes, fluid properties are homogeneous over regions with length scales on the order of  $L_{\text{macro}}$ . Although macroscopically rather tiny, a fluid region of volume  $L_{\text{macro}}^3$  is huge microscopically. We can see so by computing the number of molecules in this region.

At standard conditions, a volume of air of size  $L_{\text{macro}}^3$  contains

$$N_{\text{air molecules}} = V n_{\text{gas}} = (10^{-3} \text{ m})^3 (2.68 \times 10^{25} \text{ m}^{-3}) \approx 3 \times 10^{16} \text{ air molecules.} \quad (11.27)$$

To compute the number of water molecules in this same volume, we first use the water mass density of  $\rho \approx 10^3 \text{ kg m}^{-3}$  to determine the water mass in this region

$$M_{\text{water}} = \rho_{\text{water}} V = (1000 \text{ kg m}^{-3}) (10^{-9} \text{ m}^3) = 10^{-6} \text{ kg.} \quad (11.28)$$

Water has a molar mass of  $0.018 \text{ kg mole}^{-1}$ , so a volume of  $(10^{-3} \text{ m})^3$  contains<sup>5</sup>

$$N_{\text{water molecules}} = \left( \frac{10^{-6} \text{ kg}}{0.018 \text{ kg mole}^{-1}} \right) \times 6.022 \times 10^{23} \text{ molecules mole}^{-1} = 3 \times 10^{19} \text{ water molecules.} \quad (11.29)$$

Water thus has roughly  $10^3$  more molecules in this volume than air at standard pressure, which reflects the roughly  $10^3$  times larger mass density for water. Regardless, both water and air contain a huge number of molecules in this macroscopically tiny region.

### 11.3.7 Whence a rigorous treatment?

A rigorous derivation of continuum field theory, starting from molecular dynamics, is nontrivial even for an ideal gas, and largely non-existent for liquids. Indeed, some say a Nobel Prize awaits the person providing a fully deductive theory. For our purpose, we remain satisfied to postulate that a continuum description is valid for fluid mechanics of the atmosphere and ocean. A means for evaluating this postulate is to perform experimental measures and compare to the continuum theory. Centuries of experiments with fluid motions in the environment and laboratory lend credence to the continuum description. We consider these tests to be sufficient motivation to pursue the continuum approach for fluid mechanics and geophysical fluid dynamics.

<sup>5</sup>The calculation on page 9 of [Griffies \(2004\)](#) has a factor of  $10^6$  error.

### 11.3.8 Further study

Pedagogical treatments of the ideal gas law and kinetic theory can be found in most books on introductory physics or chemistry. [Vallis \(2017\)](#) provides extensions of the ideal gas law for an atmosphere with moisture.

For discussions of the continuum approximation reflecting that given here, see the discussion on page 1 of [Olbers et al. \(2012\)](#), or the more thorough treatments given in Section 1.2 of [Batchelor \(1967\)](#) and Section 1.4 of [Kundu et al. \(2016\)](#). Chapter 1 of [Salmon \(1998\)](#) offers an even more thorough treatment, touching on elements from kinetic theory and details for how to coarse grain average over molecular degrees of freedom (see his pages 3 and 4 and Sections 9, 10, and 11). A rigorous account of kinetic theory is offered in many treatments of statistical mechanics. That given by [Reif \(1965\)](#) and [Huang \(1987\)](#) are accessible to those with a physics undergraduate training. When reading the statistical mechanics literature, look for discussions of the “hydrodynamical limit,” which concerns the transition from discrete particle mechanics to continuum mechanics.



# Chapter 12

## Fundamentals of fluid kinematics

Fluid motion is very complex and experience has shown that it is very useful to have more than one means to describe the motion. For this purpose we study fluid motion when viewed in both the Eulerian and Lagrangian reference frames, where the Eulerian frame is fixed in the laboratory and the Lagrangian frame moves with a fluid particle. These dual descriptions form the foundation for fluid kinematics. Although the Eulerian frame is more familiar to many, and often the only kinematics needed for many purposes, a Lagrangian description offers useful insights into the theoretical foundations of the subject. It does so by providing the natural reference frame to formulate dynamical laws given that it follows seamlessly from the formulation of point particle mechanics discussed in Part II of this book. Lagrangian methods are also becoming ubiquitous in numerical modeling and have been important for certain field and laboratory methods. We thus give attention to the needs of both Eulerian and Lagrangian kinematics in this chapter and elsewhere in this book.

### READER'S GUIDE TO THIS CHAPTER

To keep the discussion focused, we assume that spatial positions and fluid particle trajectories are represented using Cartesian coordinates. Even so, we require elements of the tensor transformation theory from Part I to systematically move between the Eulerian and Lagrangian descriptions. We review the salient formalism in this chapter to keep the discussion reasonably self-contained. This is a relatively long chapter that introduces many concepts and tools used in nearly every subsequent chapter of this book.

The key references for this chapter include the text by [Salmon \(1998\)](#), who provides an elegant and accessible treatment of Eulerian and Lagrangian fluid mechanics. Chapter 4 of [Aris \(1962\)](#) offers a lucid treatment of fluid kinematics in the context of tensor analysis. Much of the treatment here follows Chapters 1 and 2 of the ocean fluid mechanics book of [Olbers et al. \(2012\)](#).

12.1	Strong and weak formulations . . . . .	240
12.2	Conceptually partitioning the continuum . . . . .	241
12.2.1	Fluid particle . . . . .	241
12.2.2	Material fluid parcel in perfect fluids . . . . .	242
12.2.3	Finite sized material objects in perfect fluids . . . . .	243
12.2.4	Fluid elements in real fluids . . . . .	243
12.2.5	Test fluid element in real fluids . . . . .	243
12.2.6	Finite sized fluid region in real fluids . . . . .	243

12.2.7	Comments . . . . .	244
12.3	Lagrangian and Eulerian reference frames . . . . .	244
12.4	Material and position coordinates . . . . .	245
12.4.1	Trajectories of fluid particles . . . . .	245
12.4.2	Material coordinates . . . . .	246
12.4.3	Transforming between material and position coordinates . . . . .	246
12.4.4	Transformation matrix and its Jacobian . . . . .	247
12.4.5	A discrete algorithm to compute the transformation matrix . . . . .	248
12.4.6	Jacobian as the ratio of volumes . . . . .	249
12.4.7	Further study . . . . .	250
12.5	Lagrangian and Eulerian time derivatives . . . . .	250
12.5.1	Infinitesimal space-time increment of a function . . . . .	250
12.5.2	Total time derivative of a function . . . . .	251
12.5.3	Eulerian: evolution measured in the laboratory frame . . . . .	251
12.5.4	Lagrangian: evolution measured in the material frame . . . . .	251
12.5.5	Lagrangian time derivative formulated from the material frame . . . . .	252
12.5.6	Sample material time derivative operations . . . . .	253
12.5.7	Worked example: velocity and acceleration from a trajectory . . . . .	255
12.5.8	Summarizing some terminology . . . . .	255
12.6	Galilean invariance . . . . .	256
12.6.1	Galilean transformation . . . . .	256
12.6.2	Transformation matrix . . . . .	256
12.6.3	Transforming the differential operators . . . . .	257
12.6.4	Comments . . . . .	258
12.7	Invariance of the material time derivative . . . . .	258
12.7.1	Invariance based on definition of the material time derivative . . . . .	258
12.7.2	Invariance for a rotating reference frame . . . . .	259
12.7.3	Invariance using space-time tensors . . . . .	261
12.7.4	Comments . . . . .	261
12.8	Fluid flow lines . . . . .	261
12.8.1	Material pathlines from fluid particle trajectories . . . . .	262
12.8.2	Fluid streamlines and streamtubes . . . . .	262
12.8.3	Distinguishing streamlines and pathlines . . . . .	263
12.8.4	Fluid streaklines . . . . .	264
12.8.5	An analytic example of flow lines . . . . .	265
12.8.6	Further study . . . . .	267
12.9	Exercises . . . . .	267

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## 12.1 Strong and weak formulations

The continuum approximation (Chapter 11) allows us to consider fluid flow from a field theoretic perspective, whereby physical properties are described by fields that take on values at each point of a space and time continuum. Consequently, we make use of a differential equation formulation of the governing fluid equations as well as an integral formulation. The differential equation formulation is sometimes referred to as the *strong* formulation. This name is motivated by the need to make “strong” assumptions about the smoothness of the continuum fields. Without such smoothness assumptions the differential equations lack predictive skill. Even so, some fluid phenomena (e.g., shocks) do not satisfy the necessary smoothness assumptions, thus making the strong formulation unsuitable for their description. Non-smooth flows are where the integral formulation is essential, with the integral formulation known as the *weak* formulation since it requires fewer assumptions about smoothness.

In this book, we are not concerned with shocks or other discontinuities within the fluid con-

tinuum, though we do study discontinuities at boundaries. Consequently, we can make use of both the strong and weak formulations. Smooth fluid flows are afforded a connection between the weak and strong formulations through the Leibniz-Reynolds transport theorem derived in Section 15.3.4. As we will see, each formulation is suited for particular needs. For example, the strong formulation provides a more concise view of the fluid equations and allows for familiar manipulations/transformations based on the rules of differential calculus studied in Part I. In contrast, the weak formulation is needed to develop budgets over finite fluid regions. Correspondingly, the weak formulation provides a starting point for the derivation of finite volume budgets that serve as the basis for certain numerical methods (e.g., [Griffies et al. \(2020\)](#)).

## 12.2 Conceptually partitioning the continuum

As part of a continuum description of fluid motion, we make use of conceptual physical systems to frame the mechanics and describe the motion. These physical systems are bounded by imagined partitions that help to organize questions about forces and transport within the continuum, and the partitions can be either open or closed to matter and energy exchange depending on the character of the fluid. There is no pretense that these partitions can be experimentally determined, nor are the fluid systems to be considered discrete molecules or solid objects. Rather, partitions are drawn within the continuum fluid by the theorist for purposes of formulation and conceptualization. We are afforded the ability to draw these partitions through our use of the continuum approach to fluid mechanics.<sup>1</sup>

### 12.2.1 Fluid particle

A *fluid particle* is a zero dimensional mathematical point that follows the fluid flow as specified by the velocity field (left panel in Figure 12.1). Since it has zero spatial extent, a fluid particle has no impact on the flow. Notably, a fluid particle is not a molecule since even a molecule has nonzero spatial extent and impacts the flow.

The space-time position of a fluid particle is uniquely specified by its material coordinate and time (we discuss material coordinates in Section 12.4.1). The trajectory or pathline of a fluid particle is an *integral curve* of the velocity field, where each point along a trajectory has a tangent that is parallel to the velocity vector (Section 12.8). The accumulation of a continuum of fluid particle trajectories define the pathlines that prescribe the Lagrangian reference frame (Section 12.3).

Fluid particles are directly analogous to *test mass particles* in Newtonian gravitation that are used to map gravitational field lines, and *test electric charges* in electromagnetism used for mapping the electromagnetic field. However, fluid particles have zero mass and are fully defined kinematically through specifying the velocity field. Fluid particles can be used to study perfect fluids, which necessarily have a single matter constituent, as well as real fluids with multiple matter constituents. For the perfect fluid, fluid particles trace out integral curves of the velocity field, whereas for a real fluid the fluid particles provide integral curves for the *barycentric velocity* studied in Section 15.1.

Some books define fluid particles as finite sized fluid regions, much like the fluid parcel described in Section 12.2.2 or the fluid element in Section 12.2.4. Some treatments also suggest that a fluid particle is akin to a fluid molecule. We instead find it conceptually simpler and less troubling to define a fluid particle as a mathematical point with zero spatial extent and zero mass,

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<sup>1</sup>This conceptual formulation of fluid mechanics, namely as a continuous collection of infinitesimally small fluid elements, originates from the work of Leonard Euler (1707-1783). Indeed, as detailed by [Truesdell \(1953\)](#), both the Eulerian and Lagrangian formulation of fluid kinematics originates with Euler!

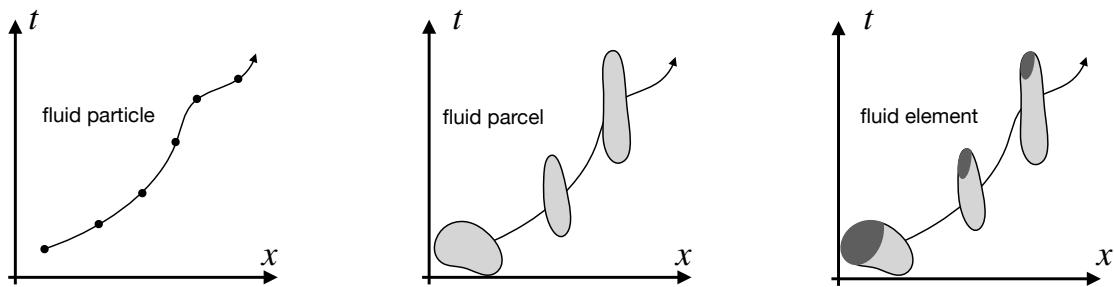


FIGURE 12.1: Schematic of the motion in space-time for the conceptual systems used in our considerations of fluid kinematics. Left panel: a fluid particle has zero spatial extent and has zero impact on the flow. Its motion in space-time defines a path/trajetory as determined by integral curves of the velocity field,  $\mathbf{v}(\mathbf{x}, t)$ . The trajectories of fluid particles define the Lagrangian reference frame. Middle panel: a material fluid parcel is comprised of a fixed material content (and thus a fixed mass) and fixed thermodynamic properties. Fluid parcels are infinitesimal deformable regions of a perfect fluid whose motion within a straining velocity field changes the parcel's shape. The center of mass for the fluid parcel follows a path that is approximated by that of a fluid particle at the center of mass. Right panel: a fluid element is comprised of a fixed mass but with matter and thermodynamic properties exchanged across its boundary, here depicted by the loss of dark gray matter and increase of light gray matter through exchanges with the surrounding fluid. The fluid element moves with the barycentric velocity (see Section 15.1), which is the center of mass velocity for the material constituents contained in the fluid element. Just like the fluid parcel, a fluid element changes its shape in the presence of fluid strains. Over time, a fluid parcel and a fluid element change their shape so much that their practical use requires a reinitialization of the their boundaries to maintain coherency as identifiable regions in the fluid.

thus serving solely as a probe for the flow and as a means to specify the Lagrangian reference frame.

### 12.2.2 Material fluid parcel in perfect fluids

For many purposes we find it useful to study fluid mechanics in the absence of irreversible processes such as friction, heat exchange, and diffusive mixing. In this case the fluid is referred to as an *ideal fluid* or equivalently a *perfect fluid*. More precisely, perfect fluid mechanics is concerned with motion of a homogeneous fluid (e.g., pure water) with zero viscosity (no friction), and in the absence of any heat exchange (adiabatic).<sup>2</sup> In describing perfect fluids we follow Euler by making use of *material fluid parcels*, which are infinitesimal deformable fluid regions (middle panel in Figure 12.1). A material fluid parcel maintains a fixed matter content so that it has fixed mass. Furthermore, it does not experience irreversible exchanges of momentum arising from friction since the perfect fluid has zero viscosity. Hence, its only interaction with the surrounding fluid environment is through reversible mechanical exchanges from pressure. The material fluid parcel is thus a closed thermodynamic system that is open to reversible mechanical interactions.

A material parcel is not a point. Rather, it has an infinitesimal volume that deforms with the flow. Conceptually we can imagine the material fluid parcel as a tiny region of fluid surrounded by a perfectly slippery bag that is also perfectly insulating. This bag is closed to matter exchange but it deforms in response to the pressure of the surrounding fluid. Additionally, the bag expands or contracts according to the density of the fluid within the bag. This conceptual picture is qualified by noting that we never have occasion to precisely specify the boundary of a material fluid parcel. Rather, we make use of the conceptual framework provided by fluid parcels as a means to formulate the differential equations of perfect fluid mechanics.

<sup>2</sup>We study frictional stresses arising from viscosity in Chapter 18, with viscosity the means for the irreversible transfer of momentum within a non-perfect fluid. We study enthalpy in the Chapter 20, with a perfect fluid maintaining constant enthalpy since it is entirely adiabatic.

### 12.2.3 Finite sized material objects in perfect fluids

Any extended region in a perfect fluid, either infinitesimal or finite, open or closed, remains exactly coherent (fixed matter content) as the region moves through the fluid. The reason for such coherency is that a perfect fluid supports no mixing or other irreversible processes that would act to diffuse the matter content. A closed material region in a perfect fluid is a finite volume generalization of a material fluid parcel. Conversely, a material fluid parcel is the infinitesimal limit of a closed material fluid region. Likewise, we can define finite sized material regions of any shape, each of which retains a fixed mass and fixed matter content as it moves through a perfect fluid. We study the kinematics of perfect fluid material lines, surfaces, and volumes in Chapter 13.

### 12.2.4 Fluid elements in real fluids

A fluid element is an infinitesimal and deformable fluid region of fixed mass yet non-fixed matter and non-fixed thermodynamic properties (right panel in Figure 12.1). For a homogeneous fluid comprised of a single matter constituent and no irreversible processes, then a fluid element reduces to a material fluid parcel. However, there is a distinction for real fluids such as the ocean and atmosphere, both of which have multiple constituents and support irreversible processes.

The exchange of matter across the boundary of a fluid element arises from the irreversible mixing of matter constituents within the fluid (Sections 15.1 and 46.3). As detailed in Section 15.1, diffusive matter exchange leaves the mass of the fluid element unchanged since the fluid element velocity is determined by its center of mass (*barycentric velocity*). Just as for a material fluid parcel, we have no need to experimentally specify the boundary of a fluid element. Instead, fluid elements are conceptual systems used to formulate the differential equations of a real fluid. Much of the kinematics in the current chapter holds for both material fluid parcels and fluid elements. However, in Chapter 14 and elsewhere, we make the distinction when studying the kinematics of multi-constituent fluids.

Many authors do not distinguish between material fluid parcels and fluid elements, choosing instead to retain a single overloaded term for both a perfect fluid and real fluid. In studying fluid kinematics, we have found this approach can lead to confusion, thus motivating the distinction between parcel (perfect fluid) and element (real fluid).<sup>3</sup> The distinction offers an added signal for when the fluid under study is perfect or real.

### 12.2.5 Test fluid element in real fluids

A *test fluid element* is a fluid element that has no effect on the surrounding fluid environment and it is used as a conceptual probe of the fluid much like the fluid particle in Section 12.2.1. Unlike the fluid particle, the test fluid element has nonzero spatial extent and it can exchange matter and energy with its surrounding environment. The test fluid element is of particular use when studying buoyancy in Chapter 24.

### 12.2.6 Finite sized fluid region in real fluids

A region within a real fluid is the most general subsystem we consider, with the region having boundaries that are open to the exchange of matter, mechanical forces, and thermodynamic properties with the surrounding environment. Here, we are often concerned with details of the region boundary and study the transport of properties across that boundary.

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<sup>3</sup>We were inspired to introduce the term “fluid element” from page 3 of *Olbers et al. (2012)*.

### 12.2.7 Comments

Throughout the study of fluid kinematics, it is important to maintain an appreciation of the continuum approximation. In particular, the continuum approximation affords information about the continuous velocity field at each point of space and each instance of time. The velocity field allows us to determine fluid particle trajectories, as well as the motion of fluid parcels in perfect fluids and fluid elements in real fluids. As part of a diagnostic framework for laboratory or field experiments, it can be useful to seed the fluid flow with a large number of tiny objects that approximate fluid particles and thus whose motion approximate fluid particle trajectories. Similarly, in numerical experiments we may seed the flow with numerical fluid particles and compute their trajectories ([van Sebille et al., 2018](#)). If we initially seed these particles in a tiny region, then deformation of the region provides the means to study deformation of fluid parcels and fluid elements as they move through the fluid. Likewise, seeding particles over larger regions allows one to study how finite sized regions are deformed.

## 12.3 Lagrangian and Eulerian reference frames

There are two reference frames commonly used as the basis for describing motion of a fluid continuum. These reference frames retain a 1-to-1 relation that allows for the transformation of descriptions between the frames.

- **LAGRANGIAN OR MATERIAL REFERENCE FRAME:** This reference frame is defined by that of fluid particles (Section 12.2.1). A mechanical description in this reference frame aims to determine the trajectory for each fluid element. The material approach is commonly termed *Lagrangian*. We note that since fluid particles generally experience accelerations (i.e., they change their speed and/or direction), the Lagrangian frame is a non-inertial reference frame.
- **EULERIAN OR LABORATORY REFERENCE FRAME:** The second reference frame is based on observing the fluid from a fixed spatial position,  $\mathbf{x}$ , within a “laboratory”. This *Eulerian* approach measures fluid properties as the fluid streams by a fixed observer. It is not concerned with determining fluid particle trajectories. Instead, the focus of Eulerian kinematics is on fluid properties determined as a function of position  $\mathbf{x}$  and time  $t$ .

The Eulerian and Lagrangian approaches complement one another. For example, the Lagrangian approach lends itself to fruitful physical insights since we can borrow freely from the point particle mechanics of Part II. In contrast, the Eulerian approach is often more straightforward when developing numerical methods for simulations and it is typically simpler when making laboratory or field measurements. In general, we make use of both Eulerian and Lagrangian kinematics. A goal of this chapter is to provide the foundation for these two perspectives and to develop tools for transforming from one to the other.

In classical fluid mechanics, the laboratory frame is fixed in space and thus it represents an inertial reference frame, which contrasts to the non-inertial Lagrangian frame. However, for geophysical fluid mechanics we generally consider an Eulerian reference frame fixed with respect to the rotating planet (a rotating laboratory frame), and as such the laboratory frame is not inertial. However, the discussion in this chapter is not concerned with such non-inertial features that give rise to planetary centrifugal and Coriolis accelerations. Instead, since the constant rotation of the planet does not impart any new strain to the fluid, classical fluid kinematics is sufficient for geophysical fluid kinematics.

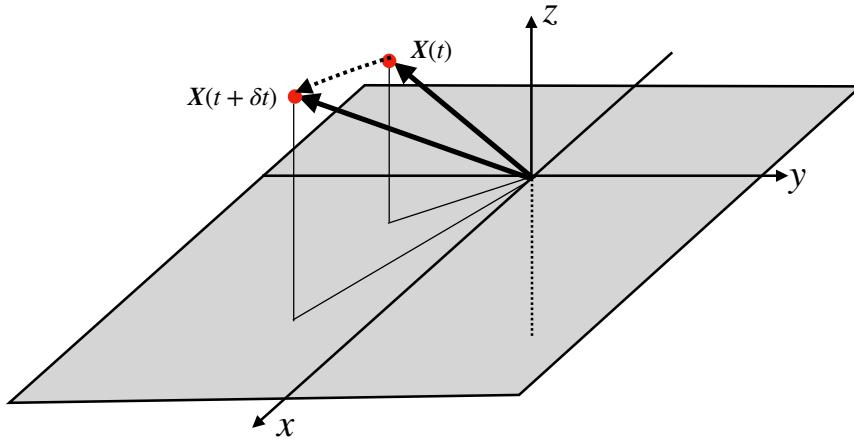


FIGURE 12.2: Sample trajectory of a fluid particle with endpoints  $\mathbf{X}(t)$  and  $\mathbf{X}(t + \delta t)$ . The trajectory passes through the point  $\mathbf{x} = \mathbf{X}(t)$  at time  $t$  and  $\mathbf{x} + \delta\mathbf{x} = \mathbf{X}(t + \delta t)$  at time  $t + \delta t$ . Eulerian kinematics describes the fluid flow from the perspective of an observer fixed with respect to the laboratory frame. Lagrangian kinematics describes the fluid flow from the perspective of an observer moving in the frame of fluid particles.

## 12.4 Material and position coordinates

A material description is suggested by the Lagrangian reference frame, whereby fluid particles are labeled with a material coordinate,  $\mathbf{a}$ , and sometimes referred to as the  $\mathbf{a}$ -space description. This description complements the Eulerian or  $\mathbf{x}$ -space description, whereby each point in space is labeled by its position. The trajectory of a fluid particle provides the mathematical transformation between the material coordinates and position coordinates. We explore this transformation in this section.

### 12.4.1 Trajectories of fluid particles

In describing the motion of a classical point particle (Chapter 9), we specify its spatial position according to a time dependent position vector,  $\mathbf{X}$ , that is a function of time,  $t$ . At a given time,  $t$ , the position vector is located at a space point denoted by the Cartesian position,  $\mathbf{x}$ , in which case we write

$$\mathbf{x} = \mathbf{X}(t) \quad \text{point particle.} \quad (12.1)$$

A sample trajectory is shown in Figure 12.2. We emphasize the notation convention used here, which may seem pedantic but in later discussions proves essential. Namely, the time dependent position of a particle is denoted with the capital,  $\mathbf{X}(t)$ , whose instantaneous space position is denoted by the lowercase,  $\mathbf{x}$ . This convention aims to distinguish time dependent functions, such as  $\mathbf{X}(t)$ , from the value of these functions evaluated at a point in time,  $\mathbf{x}$ .

When there are  $N$  discrete particles, we distinguish the various particle trajectories by introducing a discrete label. The position of particle  $n$  at time  $t$  is thus written

$$\mathbf{x} = \mathbf{X}(n, t). \quad (12.2)$$

When the matter is a continuum, such as for a rigid body, an elastic solid, or a fluid, then the discrete label becomes a continuous vector,  $\mathbf{a}$ , which is referred to as the *material* coordinate. At time  $t$ , the position of a fluid element labelled by the material coordinate,  $\mathbf{a}$ , is written

$$\mathbf{x} = \mathbf{X}(\mathbf{a}, t) \quad \text{continuum of matter.} \quad (12.3)$$

The continuous vector,  $\mathbf{a}$ , labels a point of matter within the continuum fluid.

### 12.4.2 Material coordinates

In classical fluid mechanics, we ignore special relativistic effects of fluid particles. Consequently, both the material reference frame and the laboratory reference frame measure the same universal Newtonian time,  $t$ . In contrast, the spatial coordinates are distinct for the Eulerian and Lagrangian references frames. Again, the spatial coordinates for the Eulerian frame are given by the position relative to a fixed laboratory frame, whereas the three components of a material Lagrangian coordinate remains unchanged as the fluid particle moves. Additionally, the three coordinates for both the Eulerian and Lagrangian description must be linearly independent to allow for a unique specification of the fluid particle.

One common choice for material coordinate is to define it as the spatial position of a fluid particle at an arbitrary time

$$\mathbf{a} = \mathbf{X}(t = t_0). \quad (12.4)$$

As a slightly more refined example, consider a perfect fluid (single material component with no irreversible processes). For this fluid, the specific entropy of each fluid parcel remains fixed at its initial value. When the fluid is placed in a gravitational field, layers of constant specific entropy are generally found to be monotonically stacked, or *stratified*, in the vertical direction (Chapter 24). As a result, we can uniquely specify a fluid parcel by giving its horizontal coordinate position,  $(x, y)$ , as well as the specific entropy. The material coordinates for a parcel can thus be written as

$$\mathbf{a} = (X, Y, \theta)_{t=t_0}, \quad (12.5)$$

where we write  $\theta$  as a measure of the specific entropy (or potential temperature as discussed in Section 20.11). As indicated by this example, the physical dimensions of material coordinates can generally differ. It is this generality that necessitates the use of general tensor methods when developing the mechanical equations using arbitrary Lagrangian coordinates. The mathematics and physics of these *generalized vertical coordinates* are detailed in Chapters 41, 42, and 43. For the current chapter we assume the Lagrangian coordinates are Cartesian, as given by the initial Cartesian positions as in equation (12.4).

### 12.4.3 Transforming between material and position coordinates

Motion of a fluid continuum is described by a *point transformation*. A point transformation is a mathematical way of saying that the fluid motion causes a fluid particle labeled by  $\mathbf{a}$  to continuously move from an initial position,  $\mathbf{x}_0 = \mathbf{X}(\mathbf{a}, t_0)$ , to another position,  $\mathbf{x} = \mathbf{X}(\mathbf{a}, t)$ , at time  $t > t_0$ . The point transformation is defined by the vector relation

$$\mathbf{x} = \mathbf{X}(\mathbf{a}, t), \quad (12.6)$$

which is written in component form as<sup>4</sup>

$$x^m = X^m(a^i, t). \quad (12.7)$$

The relation (12.6) defines a single-valued and invertible transformation from material coordinates  $(\mathbf{a}, t)$  to position coordinates  $(\mathbf{x}, t)$ . That is, for each material coordinate  $\mathbf{a}$  and time  $t$ , there is a unique spatial point  $\mathbf{x}$ , with this point specified by the trajectory  $\mathbf{X}(\mathbf{a}, t)$ . Conversely, for each space-time point  $(\mathbf{x}, t)$  there exists a unique material coordinate found by inverting equation

<sup>4</sup>We choose tensor labels  $m, n, p$  for spatial coordinates and trajectories, and  $i, j, k$  for material coordinates.

(12.6)<sup>5</sup>

$$\mathbf{a} = \mathbf{A}(\mathbf{x}, t). \quad (12.8)$$

In this equation,  $\mathbf{A}$  is the inverse function that specifies the material coordinate  $\mathbf{a}$  given  $(\mathbf{x}, t)$ . The single-valued property means that a fluid particle trajectory does not split, nor do two trajectories occupy the same point at the same time. This assumption is fundamental to the continuum approximation and the associated use of fluid particles to map out pathlines of the fluid flow. We acknowledge that fluid particle trajectories generally become increasingly complex in turbulent flow, thus making the Lagrangian description less convenient. However, so long as trajectories do not split or merge, the trajectories are well defined, as is the corresponding Lagrangian formulation.

#### 12.4.4 Transformation matrix and its Jacobian

In our analysis of fluid motions, we make routine use of the position coordinates ( $\mathbf{x}$  – space) of an Eulerian description and material coordinates ( $\mathbf{a}$  – space) of a Lagrangian description. We here introduce the transformation matrix allowing us to transform from one description to the other. Recall that in Section 8.2.1 we encountered the transformation matrix between Cartesian and spherical coordinates. We will later consider a transformation matrix for moving between different references frames in Sections 12.6 and 12.7. Here, we develop the transformation matrix between  $\mathbf{x}$ -space and  $\mathbf{a}$ -space.

The fluid particle trajectories,  $\mathbf{X}(\mathbf{a}, t)$ , are fundamental to this transformation. Namely, the trajectories as given by equation (12.6) provide a transformation between position coordinates,  $(\mathbf{x}, t)$ , and material coordinates,  $(\mathbf{a}, t)$ . The transformation is invertible so long as the Jacobian (determinant) of the transformation matrix remains nonzero.

The transformation matrix is given by the matrix of partial derivatives, and we organize this matrix according to the following convention<sup>6</sup>

$$F_i^m = \frac{\partial X^m}{\partial a^i} \equiv \begin{bmatrix} \partial X^1 / \partial a^1 & \partial X^1 / \partial a^2 & \partial X^1 / \partial a^3 \\ \partial X^2 / \partial a^1 & \partial X^2 / \partial a^2 & \partial X^2 / \partial a^3 \\ \partial X^3 / \partial a^1 & \partial X^3 / \partial a^2 & \partial X^3 / \partial a^3 \end{bmatrix}. \quad (12.9)$$

The upper label,  $m$ , denotes the row and the lower label,  $i$ , is the column. The transformation matrix  $F_i^m$  is also known as the *deformation tensor*, as it provides a means to measure how trajectories are deformed by the flow. That is, each element of the tensor measures how much the  $m$ 'th component of the trajectory is modified when altering the  $i$ 'th component of the material coordinate. We can more easily understand these partial derivatives when the material coordinate is the initial position,  $\mathbf{a} = \mathbf{X}(\mathbf{z}, t = 0)$ , in which case the partial derivatives measure how trajectories are modified when altering the initial position. If there the fluid has no deformation, then the trajectory remains unaffected if changing the material coordinate (i.e., the initial position), in which case the deformation tensor is the identity tensor

$$F_i^m = \delta_i^m \quad \text{if there is no flow deformation.} \quad (12.10)$$

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<sup>5</sup>The use of  $\mathbf{A}$  for the inverse function in equation (12.8) should not be confused with the acceleration, also written as  $\mathbf{A}$  elsewhere in this book. We will not have much use for equation (12.8), thus minimizing the opportunity for confusion.

<sup>6</sup>The use of covariant and contravariant notation in equation (12.9), with the upstairs and downstairs tensor labels, is strictly not needed since we assume in this chapter that both the  $\mathbf{x}$ -space and  $\mathbf{a}$ -space coordinates are Cartesian. However, the notation is quite helpful in keeping track of the ordering of partial derivatives and the corresponding coordinate transformations.

Generally each component of the deformation tensor is nonzero so that trajectories are deformed by the flow and as such they are dependent on the initial position.<sup>7</sup>

The Jacobian of the transformation matrix is the determinant, which can be written in either of the following manners

$$\det(F_i^m) = \frac{\partial \mathbf{X}}{\partial \mathbf{a}} = \det \begin{bmatrix} \partial X^1 / \partial a^1 & \partial X^1 / \partial a^2 & \partial X^1 / \partial a^3 \\ \partial X^2 / \partial a^1 & \partial X^2 / \partial a^2 & \partial X^2 / \partial a^3 \\ \partial X^3 / \partial a^1 & \partial X^3 / \partial a^2 & \partial X^3 / \partial a^3 \end{bmatrix}. \quad (12.11)$$

We make use of the notation  $\partial \mathbf{X} / \partial \mathbf{a}$  for the Jacobian as it offers a useful means to distinguish between the determinant of the transformation (12.9), and the determinant of the inverse transformation, written as  $\partial \mathbf{a} / \partial \mathbf{X}$ .

#### 12.4.5 A discrete algorithm to compute the transformation matrix

To help further our understanding of the transformation matrix (12.9), we here sketch an algorithm for its discrete approximation. For this purpose, we illustrate an algorithm for two-dimensional flow and write the trajectory using Cartesian coordinates

$$\mathbf{X}(t) = X^1(t) \hat{\mathbf{x}} + X^2(t) \hat{\mathbf{y}}, \quad (12.12)$$

and use a Cartesian representation for the material coordinate

$$\mathbf{a} = a^1 \hat{\mathbf{x}} + a^2 \hat{\mathbf{y}}. \quad (12.13)$$

Now lay down a two-dimensional lattice with discrete indices  $(e, f)$  for each of the nodal points (grid points) on the lattice, and with corresponding spatial coordinates

$$\mathbf{x}(e, f) = x(e, f) \hat{\mathbf{x}} + y(e, f) \hat{\mathbf{y}}. \quad (12.14)$$

Initialize fluid particles at each of the lattice grid points,

$$\mathbf{X}(e, f; t = 0) = \mathbf{x}(e, f) = \mathbf{a}(e, f), \quad (12.15)$$

with the discrete material coordinates defined by the initial positions. Then time step the trajectories using the velocity field to compute the particle pathlines  $\mathbf{X}[\mathbf{a}(e, f); t]$  as illustrated in Figure 12.3. At any particular time, the position of a fluid particle is found by interpolating from the lattice grid points. Setting the material coordinates equal to the initial position then leads to the finite difference approximation to the transformation matrix

$$F_i^m = \begin{bmatrix} F_1^1 & F_2^1 \\ F_1^2 & F_2^2 \end{bmatrix} \approx \begin{bmatrix} \frac{X^1(e+1, f; t) - X^1(e-1, f; t)}{X^1(e+1, f; 0) - X^1(e-1, f; 0)} & \frac{X^1(e, f+1; t) - X^1(e, f-1; t)}{X^2(e, f+1; 0) - X^2(e, f-1; 0)} \\ \frac{X^2(e+1, f; t) - X^2(e-1, f; t)}{X^2(e+1, f; 0) - X^2(e-1, f; 0)} & \frac{X^2(e, f+1; t) - X^2(e, f-1; t)}{X^2(e, f+1; 0) - X^2(e, f-1; 0)} \end{bmatrix}. \quad (12.16)$$

If the grid is regular in both directions, then the initial positions have a separation,  $\Delta$ , given by the grid spacing so that

$$F_i^m \approx \frac{1}{2\Delta} \begin{bmatrix} X^1(e+1, f; t) - X^1(e-1, f; t) & X^1(e, f+1; t) - X^1(e, f-1; t) \\ X^2(e+1, f; t) - X^2(e-1, f; t) & X^2(e, f+1; t) - X^2(e, f-1; t) \end{bmatrix}. \quad (12.17)$$

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<sup>7</sup>We have much more to say about the deformation tensor in Section 13.3.

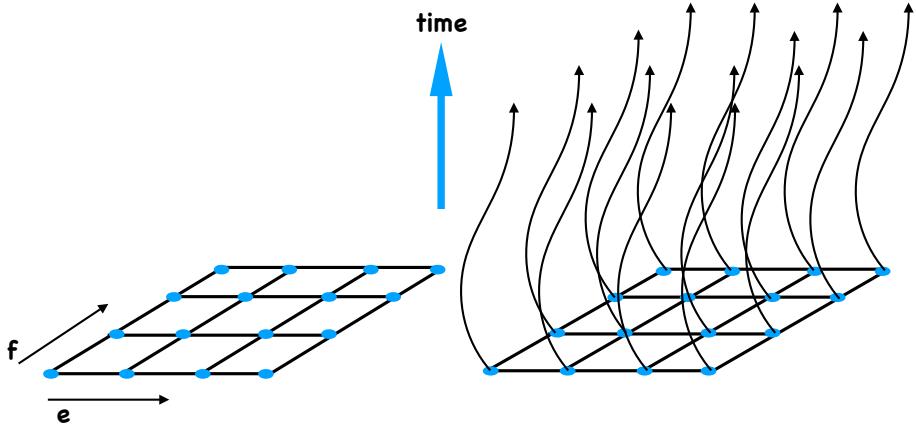


FIGURE 12.3: Illustrating the computational algorithm of Section 12.4.5 used to approximate the transformation matrix (also known as the deformation tensor)  $F_i^m$ . The left panel shows the two-dimensional grid with nodal points defining the initial positions for fluid particles. Each position on the grid is labeled by a unique integer  $(e, f)$ . The initial position of each particle is taken as the material coordinate, with the discrete label  $(e, f)$  maintained by the particles as they evolve. The right panel shows the pathlines for the fluid particles after time  $t > 0$ . When working on a discrete grid, the position of the fluid particles is not generally at a nodal point. Hence, the position must be found by interpolating between the node points.

This expression illustrates how the transformation matrix provides a measure of trajectory spreading as fluid particles move away from their initial positions. As a check on the formulation, consider the case without any deformation. In this case  $X^1(e, f; t) = X^1(e; t)$  and  $X^2(e, f; t) = X^2(f; t)$  so that the deformation tensor is diagonal, and furthermore,  $X^1(e+1; t) - X^1(e-1; t) = 2\Delta$  and  $X^2(f+1; t) - X^2(f-1; t) = 2\Delta$ , so that the deformation tensor is the identity.

#### 12.4.6 Jacobian as the ratio of volumes

We here establish the Jacobian as the ratio of the coordinate volume of fluid parcels as written using position space coordinates and material space coordinates. This property holds at each point within the continuum fluid so that it also holds on fluid parcels.

##### *Volume of an infinitesimal region of space within the fluid continuum*

Consider the volume of an infinitesimal region of space. For simplicity, write this volume in terms of Cartesian coordinates

$$dV(\mathbf{x}) = dx dy dz. \quad (12.18)$$

The  $\mathbf{x}$  argument is introduced on the left hand side to distinguish this volume, which has dimensions  $L^3$ , from the volume written in material coordinates

$$dV(\mathbf{a}) = da db dc, \quad (12.19)$$

where  $\mathbf{a} = (a^1, a^2, a^3) = (a, b, c)$  are coordinates in material space. Note that  $dV(\mathbf{a})$  does not generally have dimension  $L^3$ , since the dimension for each component of the material coordinates is not necessarily length (e.g., see the example in equation (12.5)).

The two volumes are related by the Jacobian of transformation between the two coordinate systems

$$dV(\mathbf{x}) = \frac{\partial \mathbf{X}}{\partial \mathbf{a}} dV(\mathbf{a}). \quad (12.20)$$

This relation indicates that the Jacobian measures the ratio of the volume written in terms of

position coordinates to the volume written in terms of material coordinates

$$\frac{\partial \mathbf{X}}{\partial \mathbf{a}} = \frac{dV(\mathbf{x})}{dV(\mathbf{a})}. \quad (12.21)$$

Hence, the Jacobian is a function of space according to the ratio of the volume of a fluid element in  $\mathbf{x}$ -space to the volume in  $\mathbf{a}$ -space. This is a key result of great value for transforming between Eulerian and Lagrangian coordinates.

#### *Volume of an infinitesimal fluid element*

The above results have been formulated for an arbitrary region of the fluid continuum. Hence, the expressions also hold when evaluated on an arbitrary material fluid parcel or fluid element. We use the notation  $\delta V$  for the parcel/element volume, in terms of which the above relations take the form

$$\delta V(\mathbf{x}) = \frac{\partial \mathbf{X}}{\partial \mathbf{a}} \delta V(\mathbf{a}) \Rightarrow \frac{\partial \mathbf{X}}{\partial \mathbf{a}} = \frac{\delta V(\mathbf{x})}{\delta V(\mathbf{a})}. \quad (12.22)$$

Hence, when evaluated on a moving material parcel, the Jacobian measures the ratio of the parcel volume written in terms of position coordinates to the parcel volume written in terms of material coordinates. In the particular case where the material coordinates are the initial fluid particle positions, then the Jacobian measures the ratio of the instantaneous volume of a fluid element to its initial volume

$$\frac{\partial \mathbf{X}}{\partial \mathbf{X}(0)} = \frac{\delta V(\mathbf{x})}{\delta V(0)}. \quad (12.23)$$

#### 12.4.7 Further study

[This video](#) from the *National Committee for Fluid Mechanics Films* offers insightful visualizations to help understand Eulerian and Lagrangian fluid descriptions.

## 12.5 Lagrangian and Eulerian time derivatives

As noted in Section 12.4.2, we assume non-relativistic motion so that the material reference frame and the laboratory reference frame both measure the same universal time,  $t$ . However, when computing time derivatives, the laboratory frame does so by fixing the space coordinate,  $\mathbf{x}$ , whereas the material frame computes time derivatives by fixing the material coordinate,  $\mathbf{a}$ . These two time derivatives generally measure distinct changes in the fluid since one is computed in the laboratory frame and the other from the material frame. Relating their changes constitutes a key result of fluid kinematics.

### 12.5.1 Infinitesimal space-time increment of a function

Consider a fluid property as represented by a space-time dependent field,  $\Pi$ . For example,  $\Pi$  could be the temperature, mass density, or velocity component. When measured at a fixed point in space this fluid property is written mathematically as

$$\Pi = \Pi(\mathbf{x}, t). \quad (12.24)$$

The difference between  $\Pi(\mathbf{x}, t)$  and  $\Pi(\mathbf{x} + d\mathbf{x}, t + dt)$  delivers the differential increment, computed to leading order via a Taylor series expansion

$$d\Pi = \Pi(\mathbf{x} + d\mathbf{x}, t + dt) - \Pi(\mathbf{x}, t) \quad (12.25a)$$

$$= dt \partial_t \Pi + d\mathbf{x} \cdot \nabla \Pi. \quad (12.25b)$$

In this equation,  $dt$  is the infinitesimal time increment, and  $d\mathbf{x}$  is the vector of infinitesimal space increments. For example, making use of Cartesian coordinates leads to the increment

$$d\mathbf{x} = \hat{\mathbf{x}} dx + \hat{\mathbf{y}} dy + \hat{\mathbf{z}} dz. \quad (12.26)$$

We ignore higher order terms in equation (12.25b) since the space and time increments are infinitesimal.

### 12.5.2 Total time derivative of a function

In fluid mechanics, it is common to sample properties of the fluid from moving reference frames. In this case, the sampling position is a function of time. Consequently, the total time derivative of  $\Pi$  is determined by dividing both sides of equation (12.25b) by the infinitesimal time increment

$$\frac{d\Pi}{dt} = \frac{\partial \Pi}{\partial t} + \frac{d\mathbf{x}}{dt} \cdot \nabla \Pi. \quad (12.27)$$

The first term measures the time derivative of  $\Pi$  at the space point  $\mathbf{x}$ . The second term accounts for changes in  $\Pi$  arising from movement of the reference frame relative to a point  $\mathbf{x}$  according to the velocity,  $d\mathbf{x}/dt$ . Expression (12.27) holds in general since the velocity of the moving frame is arbitrary. We next specialize to the two common cases in fluid mechanics.

### 12.5.3 Eulerian: evolution measured in the laboratory frame

The Eulerian time derivative considers the evolution of a fluid property when sampled at a fixed space point

$$\text{Eulerian time derivative} = \frac{\partial \Pi(\mathbf{x}, t)}{\partial t}. \quad (12.28)$$

This result follows from specializing the total time derivative in equation (12.27) to the case of fixed spatial points, so that  $d\mathbf{x}/dt = 0$ . In the geophysical fluids literature, the Eulerian time derivative is often termed the *time tendency* and flows with a nonzero time tendency are said to be *developing flows* or *evolving flows*. When the Eulerian time derivative vanishes everywhere the flow is said to be in a *steady state* or in a *steady flow* condition, with all points in the laboratory (inertial) frame measuring a zero time change for fluid properties. Steady fluid flows are the analog of static configurations in classical particle mechanics.

### 12.5.4 Lagrangian: evolution measured in the material frame

The Lagrangian or material time derivative measures the evolution of a fluid property sampled along the trajectory of a moving fluid particle. The Lagrangian time derivative for a field is thus written

$$\text{Lagrangian time derivative} = \frac{D\Pi}{Dt} = \frac{\partial \Pi}{\partial t} + \mathbf{v} \cdot \nabla \Pi. \quad (12.29)$$

The second equality follows by setting  $d\mathbf{x}/dt = \mathbf{v}$  in equation (12.27) since we are sampling points along the fluid particle trajectory  $\mathbf{x} = \mathbf{X}(\mathbf{a}, t)$ . The operator  $\partial/\partial t$  is the Eulerian time derivative

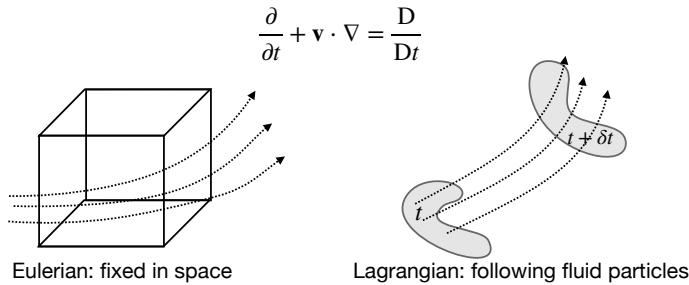


FIGURE 12.4: Illustrating the distinctions between the Eulerian (laboratory) and Lagrangian (material) reference frames for describing fluid motion. For the Eulerian description we consider a fixed control volume in the laboratory frame and measure properties as the fluid moves through the volume. For the Lagrangian description we tag fluid particles and measure fluid properties as sampled along the particle trajectories. The Eulerian representation of the material time derivative has two terms, one due to time changes local to the fixed laboratory point, and one due to the advection of properties that are swept by the local position.

from equation (12.28), whereas  $\mathbf{v} \cdot \nabla$  is referred to as the *advection* operator. Use of the capital D for the material time operator

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \quad (12.30)$$

signals that the time derivative is computed along a fluid particle trajectory. This notation distinguishes the material time derivative from the more generic total time derivative of equation (12.27). In some texts the material time derivative is referred to as the *convective time derivative*, since the term “convection” is often used rather than our preferred term “advection”.<sup>8</sup> It is also sometimes referred to as the *substantial time derivative* since it refers to the time changes following a material substance.

Equation (12.30) provides an Eulerian expression (right hand side) to the material time derivative D/Dt. There are two Eulerian contributions: the local (fixed space point) time tendency  $\partial/\partial t$  and advection,  $\mathbf{v} \cdot \nabla$ . Advection arises in the Eulerian reference frame due to the fluid passing by the fixed laboratory observer, whereas it is absent from the material reference frame since the material frame moves with the fluid particles. Figure 12.4 illustrates the differences between the Eulerian and Lagrangian perspectives.

A *steady flow* is one with zero Eulerian time derivatives so that a steady flow does not imply a vanishing Lagrangian time derivative. Rather, a steady flow is a statement that the flow is static when viewed from the Eulerian (laboratory) reference frame. Hence, a steady flow generally has changing properties when sampled along a fluid particle trajectory. That is, there can be a nonzero Lagrangian evolution (via advection) even when the Eulerian time tendency vanishes.

### 12.5.5 Lagrangian time derivative formulated from the material frame

Rather than start from the total time derivative (12.27), it is instructive to work in the moving material frame *a priori*. For this purpose, we measure the function,  $\Pi$ , on a fluid particle, in which case it is useful to introduce the shorthand notation

$$\Pi[\mathbf{X}(\mathbf{a}, t), t] \equiv \Pi^L(\mathbf{a}, t) \quad \Longleftarrow \text{sampling } \Pi \text{ on a trajectory } \mathbf{x} = \mathbf{X}(\mathbf{a}, t) \text{ at time } t. \quad (12.31)$$

<sup>8</sup>In the geophysical fluids literature, “convection” generally refers to gravitationally unstable vertical motion initiated by buoyancy forces.

In words,  $\Pi^L(\mathbf{a}, t)$  is the function,  $\Pi$ , evaluated on a fluid particle trajectory  $\mathbf{x} = \mathbf{X}(\mathbf{a}, t)$ . That is,  $\Pi^L$  is the Lagrangian version of the function. For example, the Lagrangian velocity is given by

$$\mathbf{v}^L(\mathbf{a}, t) \equiv \mathbf{v}[\mathbf{X}(\mathbf{a}, t), t] = \left[ \frac{\partial \mathbf{X}(\mathbf{a}, t)}{\partial t} \right]_{\mathbf{a}}. \quad (12.32)$$

The  $\mathbf{a}$  subscript emphasizes that the partial time derivative is computed while holding the material coordinate,  $\mathbf{a}$ , fixed.

The time derivative along a fluid particle trajectory is the material derivative, and we introduce a finite difference along the trajectory to estimate the derivative

$$\left[ \frac{\partial \Pi[\mathbf{X}(\mathbf{a}, t), t]}{\partial t} \right]_{\mathbf{a}} = \lim_{\Delta t \rightarrow 0} \left[ \frac{\Pi[\mathbf{X}(\mathbf{a}, t + \Delta t/2), t + \Delta t/2] - \Pi[\mathbf{X}(\mathbf{a}, t - \Delta t/2), t - \Delta t/2]}{\Delta t} \right]. \quad (12.33)$$

Expanding the numerator in a Taylor series, and keeping just the leading terms, yields

$$\left[ \frac{\partial \Pi[\mathbf{X}(\mathbf{a}, t), t]}{\partial t} \right]_{\mathbf{a}} = \lim_{\Delta t \rightarrow 0} \left[ \frac{\Pi[\mathbf{X}(\mathbf{a}, t + \Delta t/2), t + \Delta t/2] - \Pi[\mathbf{X}(\mathbf{a}, t - \Delta t/2), t - \Delta t/2]}{\Delta t} \right] \quad (12.34a)$$

$$= \left[ \left( \frac{\partial}{\partial t} \right)_{\mathbf{X}} + \left( \frac{\partial \mathbf{X}(\mathbf{a}, t)}{\partial t} \right)_{\mathbf{a}} \cdot \nabla \right] \Pi[\mathbf{X}(\mathbf{a}, t), t] \quad (12.34b)$$

$$= \left[ \left( \frac{\partial}{\partial t} \right)_{\mathbf{X}} + \mathbf{v}[\mathbf{X}(\mathbf{a}, t), t] \cdot \nabla \right] \Pi[\mathbf{X}(\mathbf{a}, t), t]. \quad (12.34c)$$

We included a subscript on the derivative operators on the right hand side to be explicit about what variables are held fixed during differentiation. This extra notation can generally be dropped, since a partial derivative operation is based on holding all variables fixed except for the variable being differentiated. Evaluating the trajectory at the spatial point,  $\mathbf{X}(\mathbf{a}, t) = \mathbf{x}$ , allows us to dispense with the trajectory notation to recover the more succinct expression (12.29). Even so, it is useful to keep in mind the underlying trajectory basis for the material time derivative.

## 12.5.6 Sample material time derivative operations

The material time derivative operator is perhaps the most important operator in fluid mechanics, and its relation to the Eulerian time derivative plus advection is a key result of fluid kinematics. Therefore, it is critical to develop experience with this operator and its generalizations. The examples here offer a starting point.

### *Linear wave characteristics*

Consider the phase function,  $\Gamma(\mathbf{x}, t) = \mathbf{k} \cdot \mathbf{x} - \omega t$ , where  $\omega$  is a constant angular frequency and  $\mathbf{k}$  is a constant wavevector. In the study of linear waves, surfaces of constant  $\Gamma$  are surfaces on which the wave phase remains constant. In the theory of partial differential equations, the direction normal to these phase surfaces define characteristic lines for linear hyperbolic equations, such as the advection equation (Section 3.2) and wave equation (Section 3.7). Now consider the material

time derivative of the phase function

$$\frac{D\Gamma(\mathbf{x}, t)}{Dt} = \frac{D(\mathbf{k} \cdot \mathbf{x} - \omega t)}{Dt} \quad (12.35a)$$

$$= \left[ \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \right] (\mathbf{k} \cdot \mathbf{x} - \omega t) \quad (12.35b)$$

$$= \mathbf{v} \cdot \nabla (\mathbf{k} \cdot \mathbf{x}) - \frac{\partial(\omega t)}{\partial t} \quad (12.35c)$$

$$= \mathbf{v} \cdot \mathbf{k} - \omega. \quad (12.35d)$$

The first term says that the velocity of a point following a fluid particle is none other than the fluid velocity. This result, which follows by definition, serves as a useful means to verify internal consistency of the formalism. The second term arises from the constant angular frequency.

### Material invariant

Consider a scalar function that remains constant on a material trajectory so that its material time derivative vanishes

$$\frac{D\Pi}{Dt} = 0. \quad (12.36)$$

Material constancy is generally referred to as *material invariance* in this book. We may also say that the property  $\Pi$  is materially conserved. At a fixed point in space, a materially invariant property has its Eulerian time derivative arising only via advection

$$\frac{\partial\Pi}{\partial t} = -\mathbf{v} \cdot \nabla\Pi. \quad (12.37)$$

Recall the case of a wave characteristic whereby  $\partial\Pi/\partial t = \omega$ . Wave characteristics are material if the fluid particle velocity satisfies  $\mathbf{k} \cdot \mathbf{v} = \omega$ . In one space dimension and for linear non-rotating gravity waves (Section 31.8.3), the wave phase speed is given by  $\omega/k$  so that the wave characteristics are material if the fluid particle speed matches the wave speed,  $|v| = \omega/k$ . The ratio of the particle speed to the wave speed is known as the Froude number. The Froude number is typically much less than unity, through highly nonlinear behavior (e.g., hydraulic jumps as discussed in [Pratt and Whitehead \(2008\)](#)) occurs when the Froude number reaches unity or larger (see Exercise 30.2).

We garner geometric insight into relation (12.37) by introducing the unit normal vector to the surface of constant  $\Pi$

$$\hat{\mathbf{n}} = \frac{\nabla\Pi}{|\nabla\Pi|}. \quad (12.38)$$

Material invariance of  $\Pi$  thus means that the normalized Eulerian time tendency equals to the negative of the projection of the velocity into the direction normal to constant  $\Pi$  surfaces

$$\frac{\partial\Pi/\partial t}{|\nabla\Pi|} = -\mathbf{v} \cdot \hat{\mathbf{n}}. \quad (12.39)$$

That is, the fluid particle velocity,  $\mathbf{v}$ , is matched precisely to the velocity of the moving surface of constant  $\Pi$ . As detailed in Section 14.4.2, this result means there are no fluid parcels that cross surfaces of constant  $\Pi$ . That is, constant  $\Pi$  surfaces are material.

### Time derivative measured in a general moving frame

Now consider a reference frame moving at an arbitrary velocity,  $\mathbf{v}^{(s)}$ . Examples include the quasi-Lagrangian reference frames of a float in the ocean or balloon in the atmosphere. Due to their finite size and associated drag effects, these objects only approximate material particle motion, so that  $\mathbf{v}^{(s)} \neq \mathbf{v}$ . Returning to the general expression (12.27) for the total time derivative, we have the time derivative operator as measured in this non-material moving reference frame

$$\frac{D^{(s)}}{Dt} = \frac{\partial}{\partial t} + \mathbf{v}^{(s)} \cdot \nabla. \quad (12.40)$$

A function that remains constant within this general moving frame thus satisfies

$$\frac{D^{(s)}\Pi}{Dt} = 0 \implies \frac{\partial\Pi}{\partial t} = -\mathbf{v}^{(s)} \cdot \nabla\Pi. \quad (12.41)$$

Introducing the normal direction  $\hat{\mathbf{n}} = |\nabla\Pi|^{-1} \nabla\Pi$  leads to

$$\frac{\partial\Pi/\partial t}{|\nabla\Pi|} = -\mathbf{v}^{(s)} \cdot \hat{\mathbf{n}}, \quad (12.42)$$

which is an analog to the material constancy condition (12.39).

### 12.5.7 Worked example: velocity and acceleration from a trajectory

Following example 3.2 from [Kundu et al. \(2016\)](#), we here consider a one-dimensional fluid motion whereby the trajectory of a fluid particle is given by

$$\mathbf{X}(t) = \hat{\mathbf{x}} X(t) = \hat{\mathbf{x}} [K(t - t_0) + x_0^3]^{1/3}, \quad (12.43)$$

where  $K$  is a constant with dimensions volume per time and  $x_0$  is the particle position at time  $t_0$ . The particle velocity and particle acceleration are determined through time differentiation

$$\frac{d\mathbf{X}}{dt} = \hat{\mathbf{x}} \frac{K}{3X^2} \quad \text{and} \quad \frac{d^2\mathbf{X}}{dt^2} = -\hat{\mathbf{x}} \frac{2K^2}{9X^5}. \quad (12.44)$$

The Eulerian velocity field is then determined by

$$\mathbf{v}(\mathbf{x}, t) \equiv \left[ \frac{d\mathbf{X}}{dt} \right]_{\mathbf{x}=\mathbf{X}(t)} = \hat{\mathbf{x}} \frac{K}{3x^2}, \quad (12.45)$$

which reveals that the flow is steady since there is no time dependence to the Eulerian velocity field. The Eulerian acceleration is given by the material time derivative of the Eulerian velocity, which is equal to the second time derivative of the trajectory evaluated at the field point

$$\frac{Du}{Dt} = \frac{\partial u}{\partial t} + \mathbf{v} \cdot \nabla u = 0 + u \partial_x u = -[K/(3x^2)] [(2K)/(3x^3)] = -\frac{2K^2}{9x^5} = \left[ \frac{d^2X(t)}{dt^2} \right]_{\mathbf{x}=\mathbf{X}(t)}. \quad (12.46)$$

### 12.5.8 Summarizing some terminology

We here summarize certain terminology used in this book in reference to the variety of equations in geophysical fluid mechanics. Some of this terminology was introduced in this chapter, whereas others will be encountered in subsequent development.

- PROGNOSTIC: This is an equation that determines the time tendency (Eulerian evolution) of a quantity such as the temperature or velocity.
- DIAGNOSTIC: This is an equation that determines the value of a field at a particular instance in time. An example is the non-divergence condition satisfied by flow in an incompressible fluid as well in Boussinesq fluids (see Chapters 16 and 23). There are no time derivatives appearing in diagnostic equations.
- STEADY STATE: All Eulerian time derivatives vanish, so that all fluid properties are time independent when measured in the laboratory frame.
- MATERIAL INVARIANCE: The Lagrangian time derivative vanishes for a property that is a material invariant.

## 12.6 Galilean invariance

Galilean invariance means that the laws of motion are the same in all inertial reference frames. Furthermore, two inertial reference frames can only be moving with a constant velocity relative to one another. We discussed Galilean invariance for a point particle in Section 9.1.2. Here we consider its expression for a fluid. As for the particle, Galilean invariance means that the material acceleration of a fluid particle remains the same when viewed in an arbitrary inertial reference frame. Some care is required when translating this invariance into a mathematical statement when decomposing the material acceleration into its Eulerian components. Our considerations here provide a useful warmup to the more general discussion in Section 12.7, where we transform space and time derivative operators between an inertial frame and a rotating frame.

The notions of Galilean invariance hold in free space. In the presence of boundaries we do not generally expect the physical system to respect Galilean invariance since boundaries generally distinguish between reference frames. Our discussion here ignores boundaries, which is generally a useful starting point when considering the equations of motion and their kinematic properties.

### 12.6.1 Galilean transformation

A Galilean transformation is given by the linear space-time transformation

$$\bar{t} = t \quad \text{and} \quad \bar{\mathbf{x}} = \mathbf{x} + \mathbf{U}t \quad \text{and} \quad \bar{\mathbf{v}} = \mathbf{v} + \mathbf{U}. \quad (12.47)$$

By convention, we say that the barred coordinates are those measured in the moving (boosted) reference frame and the unbarred are measured in the rest frame. However, since both reference frames are inertial, there is no experiment on a Galilean invariant physical system that can determine which frame is at rest or which is moving. Instead, what is relevant is that the two inertial frames are moving relative to one another. Furthermore, note that time remains unchanged (universal Newtonian time), whereas the position of a point in the new frame equals to that in the original reference frame plus a contribution from the constant velocity  $\mathbf{U}$ . The inverse transformation is trivially given by

$$t = \bar{t} \quad \text{and} \quad \mathbf{x} = \bar{\mathbf{x}} - \mathbf{U}\bar{t} \quad \text{and} \quad \mathbf{v} = \bar{\mathbf{v}} - \mathbf{U}. \quad (12.48)$$

### 12.6.2 Transformation matrix

We take this opportunity to make use of the transformation matrix formalism to derive relations between the partial differential operators. Details of this formalism were presented in Section

7.9. However, the reader skipping that section should still be able to understand the gist of the following. For simplicity we work in the 1+1 dimensional case with time along with one space dimension.

Writing the space and time coordinates as  $(t, x) = (x^0, x^1)$  and  $(\bar{t}, \bar{x}) = (x^{\bar{0}}, x^{\bar{1}})$  renders the transformation of partial derivatives (following the chain rule)

$$\frac{\partial}{\partial x^{\alpha}} = \frac{\partial x^{\alpha}}{\partial x^{\bar{\alpha}}} \frac{\partial}{\partial x^{\bar{\alpha}}}, \quad (12.49)$$

where  $\alpha = 0, 1$  is a tensor index that has  $\alpha = 0$  for the time coordinate. The transformation matrix for the Galilean transformation is thus given by the  $2 \times 2$  matrix

$$\frac{\partial x^{\bar{\alpha}}}{\partial x^{\alpha}} = \begin{bmatrix} \partial x^{\bar{0}}/\partial x^0 & \partial x^{\bar{0}}/\partial x^1 \\ \partial x^{\bar{1}}/\partial x^0 & \partial x^{\bar{1}}/\partial x^1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ U & 1 \end{bmatrix}, \quad (12.50)$$

and the inverse is

$$\frac{\partial x^{\alpha}}{\partial x^{\bar{\alpha}}} = \begin{bmatrix} 1 & 0 \\ -U & 1 \end{bmatrix}. \quad (12.51)$$

The Jacobian determinant of the transformation matrix is unity, so that the Galilean transformation always has an inverse.

### 12.6.3 Transforming the differential operators

Given the transformation matrix, we can compute the Eulerian time derivative as measured in the moving frame as

$$\frac{\partial}{\partial x^{\bar{0}}} = \frac{\partial x^0}{\partial x^{\bar{0}}} \frac{\partial}{\partial x^0} + \frac{\partial x^1}{\partial x^{\bar{0}}} \frac{\partial}{\partial x^1} = \frac{\partial}{\partial x^0} - U \frac{\partial}{\partial x^1} = \frac{\partial}{\partial t} - U \frac{\partial}{\partial x}. \quad (12.52)$$

In words, this identity says that the time derivative computed between two inertial reference frames differs due to an advective term (with the constant Galilean boost velocity) arising from the relative motion of the two inertial observers. The space derivatives are related by

$$\frac{\partial}{\partial x^{\bar{1}}} = \frac{\partial x^0}{\partial x^{\bar{1}}} \frac{\partial}{\partial x^0} + \frac{\partial x^1}{\partial x^{\bar{1}}} \frac{\partial}{\partial x^1} = \frac{\partial}{\partial x^1}, \quad (12.53)$$

so that the space derivative operator remains form invariant under a Galilean transformation. This result holds also for the other two space dimensions. We thus prove that the material time derivative operator is form invariant under a Galilean transformation

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \quad (12.54a)$$

$$= \frac{\partial}{\partial \bar{t}} + \mathbf{U} \cdot \bar{\nabla} + (\bar{\mathbf{v}} - \mathbf{U}) \cdot \bar{\nabla} \quad (12.54b)$$

$$= \frac{\partial}{\partial \bar{t}} + \bar{\mathbf{v}} \cdot \bar{\nabla} \quad (12.54c)$$

$$= \frac{D}{D\bar{t}}, \quad (12.54d)$$

where we used the shorthand

$$\bar{\mathbf{v}} \cdot \bar{\nabla} = \bar{u} \frac{\partial}{\partial x^{\bar{1}}} + \bar{v} \frac{\partial}{\partial x^{\bar{2}}} + \bar{w} \frac{\partial}{\partial x^{\bar{3}}}. \quad (12.55)$$

So although the individual pieces to the material time operator are modified by a Galilean transformation, the material time derivative operator is form invariant. Hence, if a function has a material time derivative  $D\mathbf{U}/dt$  in one inertial reference frame, it has the same material time operator in any other inertial reference frame. That is, all properties sampled from a boosted fluid particle reference frame have the same material time evolution.

### 12.6.4 Comments

There are many features of geophysical fluid flows that break Galilean invariance. For example, a solid boundary breaks Galilean invariance since it establishes a special reference frame and thus breaks symmetry of the space. Additionally, a rotating planet distinguishes between longitude and latitude even if the planet is perfectly smooth. Nonetheless, as a starting point in our study of the equations of fluid mechanics, it is useful to establish their properties under a Galilean transformation. In general, if space is Galilean invariant and yet the equations of motion are not, then we question the physical relevance of the equations. Exercise 33.7 provides an example of this reasoning.

There are further symmetries of the equations of fluid mechanics, especially when there is no dissipation (inviscid). Section 2.2 of [Frisch \(1995\)](#) and Section 1.4 of [Badin and Crisciani \(2018\)](#) provide a discussion of these symmetries.

## 12.7 Invariance of the material time derivative

In our discussion of Galilean invariance in Section 12.6, we showed that the material time derivative operator remains form invariant under changes to the inertial reference frame. Consequently, the acceleration of a fluid particle is identical when measured in any inertial reference frame. We here consider the more general case of non-inertial reference frames that differ by both rotations and translations. We already know that the form for fluid particle accelerations differs between an inertial frame and a non-inertial frame. Nonetheless, we show here that the material time derivative operator remains form invariant. This is a result of great practical relevance, as it means that the scalar equations of fluid mechanics (e.g., mass continuity and tracer equations) remain form-invariant when changing reference frames.

### 12.7.1 Invariance based on definition of the material time derivative

We first determine invariance by focusing on the conceptual definition of the material time derivative. Namely, the material time derivative measures time changes of a fluid property in the reference frame of a moving fluid particle. The Lagrangian reference frame follows fluid particles, so it is the natural reference frame for measuring material time changes. In contrast, the Eulerian reference frame is fixed in a laboratory. The material time derivative computed from the laboratory reference frame is composed of an Eulerian time tendency plus an advection operator

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla. \quad (12.56)$$

Importantly, this expression holds regardless the choice of laboratory reference frames, either inertial or non-inertial. Our choice of laboratory frames only impacts on the form of the Eulerian time derivative and on the advection operator. The sum of the two terms returns the same material time derivative operator, no matter what laboratory frame is chosen.

Again for emphasis, the reason for the form invariance is that the material time derivative operator is, by definition, computed in the fluid particle reference frame. The particle reference

frame is unconcerned with the subjective choice made by the observer in the laboratory reference frame. In the following, we exhibit how the mathematics respects this invariance. Namely, we show how the Eulerian expression for the material time derivative remains form invariant when changing reference frames.

### 12.7.2 Invariance for a rotating reference frame

Consider two reference frames. The first is at rest and so serves as an inertial frame, whereas the second is rotating with rotational axis aligned with the vertical direction as in Figure 8.1. Introduce Cartesian coordinates for the inertial frame, with corresponding basis vectors  $(\hat{\bar{x}}, \hat{\bar{y}}, \hat{\bar{z}})$ . Let these inertial frame unit vectors be related to rotating frame unit vectors according to

$$\hat{\bar{x}} = \hat{x} \cos \vartheta - \hat{y} \sin \vartheta \quad (12.57a)$$

$$\hat{\bar{y}} = \hat{x} \sin \vartheta + \hat{y} \cos \vartheta \quad (12.57b)$$

$$\hat{\bar{z}} = \hat{z}, \quad (12.57c)$$

and let time be the same in the two reference frames. The angle  $\vartheta$  measures the counter-clockwise angle between the inertial frame direction  $\hat{\bar{x}}$  and the moving frame direction  $\hat{x}$ , with this angle a linear function of time

$$\vartheta = \Omega t. \quad (12.58)$$

The above relations between the two sets of basis vectors translates into the same relations between the corresponding coordinate representations for an arbitrary vector. Including time, we have the relation between inertial coordinates (the barred frame) and rotating coordinates (unbarred frame)

$$\bar{t} = t \quad (12.59a)$$

$$\bar{x} = x \cos \vartheta - y \sin \vartheta \quad (12.59b)$$

$$\bar{y} = x \sin \vartheta + y \cos \vartheta \quad (12.59c)$$

$$\bar{z} = z. \quad (12.59d)$$

The inverse transformation can be easily found

$$t = \bar{t} \quad (12.60a)$$

$$x = \bar{x} \cos \vartheta + \bar{y} \sin \vartheta \quad (12.60b)$$

$$y = -\bar{x} \sin \vartheta + \bar{y} \cos \vartheta \quad (12.60c)$$

$$z = \bar{z}. \quad (12.60d)$$

We are now prepared to make use of the transformation formalism generally considered in Section 7.9, and specifically applied for the Galilean transformation in Section 12.6. As in these other cases, we include time as part of the formalism by introducing the Greek label  $\alpha = 0, 1, 2, 3$  so that the transformation matrix between the inertial frame and rotating frame is given by

$$\frac{\partial x^{\bar{\alpha}}}{\partial x^{\alpha}} = \begin{bmatrix} \partial x^{\bar{0}}/\partial x^0 & \partial x^{\bar{0}}/\partial x^1 & \partial x^{\bar{0}}/\partial x^2 & \partial x^{\bar{0}}/\partial x^3 \\ \partial x^{\bar{1}}/\partial x^0 & \partial x^{\bar{1}}/\partial x^1 & \partial x^{\bar{1}}/\partial x^2 & \partial x^{\bar{1}}/\partial x^3 \\ \partial x^{\bar{2}}/\partial x^0 & \partial x^{\bar{2}}/\partial x^1 & \partial x^{\bar{2}}/\partial x^2 & \partial x^{\bar{2}}/\partial x^3 \\ \partial x^{\bar{3}}/\partial x^0 & \partial x^{\bar{3}}/\partial x^1 & \partial x^{\bar{3}}/\partial x^2 & \partial x^{\bar{3}}/\partial x^3 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\Omega \bar{y} & \cos \vartheta & -\sin \vartheta & 0 \\ \Omega \bar{x} & \sin \vartheta & \cos \vartheta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}. \quad (12.61)$$

Similarly, the inverse transformation is given by

$$\frac{\partial x^\alpha}{\partial \bar{x}^{\bar{\alpha}}} = \begin{bmatrix} \partial x^0/\partial \bar{x}^0 & \partial x^0/\partial \bar{x}^1 & \partial x^0/\partial \bar{x}^2 & \partial x^0/\partial \bar{x}^3 \\ \partial x^1/\partial \bar{x}^0 & \partial x^1/\partial \bar{x}^1 & \partial x^1/\partial \bar{x}^2 & \partial x^1/\partial \bar{x}^3 \\ \partial x^2/\partial \bar{x}^0 & \partial x^2/\partial \bar{x}^1 & \partial x^2/\partial \bar{x}^2 & \partial x^2/\partial \bar{x}^3 \\ \partial x^3/\partial \bar{x}^0 & \partial x^3/\partial \bar{x}^1 & \partial x^3/\partial \bar{x}^2 & \partial x^3/\partial \bar{x}^3 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ \Omega y & \cos \vartheta & \sin \vartheta & 0 \\ -\Omega x & -\sin \vartheta & \cos \vartheta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}. \quad (12.62)$$

The derivative operators transform according to

$$\frac{\partial}{\partial x^\alpha} = \frac{\partial x^{\bar{\alpha}}}{\partial x^\alpha} \frac{\partial}{\partial \bar{x}^{\bar{\alpha}}}, \quad (12.63)$$

in which case

$$\frac{\partial}{\partial t} = \frac{\partial}{\partial \bar{t}} + (\boldsymbol{\Omega} \times \bar{\boldsymbol{x}}) \cdot \bar{\nabla} \quad (12.64a)$$

$$\frac{\partial}{\partial x} = \cos \vartheta \frac{\partial}{\partial \bar{x}} + \sin \vartheta \frac{\partial}{\partial \bar{y}} \quad (12.64b)$$

$$\frac{\partial}{\partial y} = -\sin \vartheta \frac{\partial}{\partial \bar{x}} + \cos \vartheta \frac{\partial}{\partial \bar{y}} \quad (12.64c)$$

$$\frac{\partial}{\partial z} = \frac{\partial}{\partial \bar{z}}. \quad (12.64d)$$

The velocity vector components transform according to

$$v^\alpha = \frac{\partial x^\alpha}{\partial \bar{x}^{\bar{\alpha}}} v^{\bar{\alpha}}, \quad (12.65)$$

so that

$$v^0 = v^{\bar{0}} \quad (12.66a)$$

$$u = \Omega y + \bar{u} \cos \vartheta + \bar{v} \sin \vartheta \quad (12.66b)$$

$$v = -\Omega x - \bar{u} \sin \vartheta + \bar{v} \cos \vartheta \quad (12.66c)$$

$$w = \bar{w}, \quad (12.66d)$$

where

$$v^0 = v^{\bar{0}} = 1. \quad (12.67)$$

Bringing these result together leads to the transformation of the horizontal advection operator

$$u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} = (\bar{\boldsymbol{u}} - \boldsymbol{\Omega} \times \bar{\boldsymbol{x}}) \cdot \bar{\nabla}. \quad (12.68)$$

Combining this result with the transformed Eulerian time derivative leads to the material time

derivative

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \quad (12.69a)$$

$$= \frac{\partial}{\partial t} + u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} + w \frac{\partial}{\partial z} \quad (12.69b)$$

$$= \frac{\partial}{\partial \bar{t}} + (\boldsymbol{\Omega} \times \bar{\mathbf{x}}) \cdot \bar{\nabla} + (\bar{\mathbf{u}} - \boldsymbol{\Omega} \times \bar{\mathbf{x}}) \cdot \bar{\nabla} + \bar{w} \frac{\partial}{\partial \bar{z}} \quad (12.69c)$$

$$= \frac{\partial}{\partial \bar{t}} + \bar{\mathbf{v}} \cdot \bar{\nabla}. \quad (12.69d)$$

As advertised, the operator is form invariant under time dependent transformations to a non-inertial reference frame.

### 12.7.3 Invariance using space-time tensors

We can generalize the previous result by writing the material time derivative operator using space-time tensor notation, in which case

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \quad (12.70a)$$

$$= \frac{\partial}{\partial x^0} + v^m \frac{\partial}{\partial x^m} \quad (12.70b)$$

$$= v^\alpha \frac{\partial}{\partial x^\alpha}, \quad (12.70c)$$

where we introduced the velocity 4-vector

$$(v^0, v^1, v^2, v^3) = (1, v^1, v^2, v^3). \quad (12.71)$$

All space-time indices are contracted in equation (12.70c), which means the material time derivative is a space-time scalar. Consequently, we can change coordinates or change reference frames without changing the material time operator.

### 12.7.4 Comments

As argued at the start of this section, the invariance of the material time derivative to changes in the laboratory reference frame is rather obvious: why would a time derivative computed in a material frame be concerned with the nature of the laboratory frame? Even so, it is satisfying to see the tools of coordinate transformations put to use verifying this result. It is this sort of exercise that nurtures trust in tensor analysis, at which point it becomes a reliable tool for exploration where the answer is not *a priori* known.

## 12.8 Fluid flow lines

There are three types of flow lines commonly used to visualize fluid motion: *pathlines*, *streamlines*, and *streaklines*. These flow lines are identical for time independent (steady) flow, where steady flow means that all fields are constant in time when observed in the Eulerian reference frame. However, these flow lines differ for unsteady flow. They each offer complementary information about the flow field, and have uses in both theoretical and experimental contexts. We have use for pathlines and streamlines in this book, yet also introduce streaklines for completeness.

### 12.8.1 Material pathlines from fluid particle trajectories

As introduced in Section 12.4.1, a fluid particle traces out a *trajectory* as it moves through space and time (Figure 12.2). We use the term material *pathline* for a fluid particle trajectory, with a collection of pathlines providing a means to visualize fluid particle motion throughout the flow. In this book we are only concerned with *smooth velocity fields*, which allow for an unambiguous specification of the particle trajectory at each point of the fluid.

Mathematically, a fluid particle trajectory is a curve,  $\mathbf{X}(\mathbf{a}, t)$ , in space that is traced by fixing the material coordinate,  $\mathbf{a}$ , and letting time advance. Trajectories are computed by time integrating the ordinary differential equation

$$\frac{\partial \mathbf{X}(\mathbf{a}, t)}{\partial t} = \mathbf{v}[\mathbf{X}(\mathbf{a}, t), t] \quad (12.72a)$$

$$\mathbf{X}(\mathbf{a}, t = 0) = \mathbf{a}, \quad (12.72b)$$

where

$$\mathbf{v}[\mathbf{X}(\mathbf{a}, t), t] = \mathbf{v}^L(\mathbf{a}, t) \quad (12.73)$$

is Lagrangian velocity of the fluid particle (see equation (12.32)), and we have assumed the material coordinates are determined by the initial position. Again, the partial time derivative is computed with the material coordinate held fixed, so that the material coordinate distinguishes between particle trajectories. In a mathematical context we refer to a particle trajectory as the *integral curve* for the velocity vector.

In the laboratory, we can insert tiny particles into the fluid to offer a means for visualizing the flow, with a time exposed photograph providing an estimate of fluid particle pathlines. Experimental particles provide an accurate estimate of fluid particle pathlines if the particles do not disperse through diffusion (see Chapter 46). As another example, consider cars moving at night with a time exposed photograph revealing car pathlines formed by car head and tail lights. Like cars, the material pathlines in a fluid can intersect, cross, and become quite complex, particularly when the flow is turbulent.

### 12.8.2 Fluid streamlines and streamtubes

*Streamlines* are curves whose tangent is parallel to the instantaneous fluid velocity field. Streamlines can intersect only at a stagnation point; i.e., a point where the fluid is not moving. Let

$$d\mathbf{x} = \hat{\mathbf{x}} dx + \hat{\mathbf{y}} dy + \hat{\mathbf{z}} dz \quad (12.74)$$

be an infinitesimal increment along a streamline written using Cartesian coordinates. The family of streamlines at a given time,  $t$ , satisfy the tangent constraint

$$\mathbf{v} \times d\mathbf{x} = 0, \quad (12.75)$$

which is equivalent to

$$\frac{dx}{u(\mathbf{x}, t)} = \frac{dy}{v(\mathbf{x}, t)} = \frac{dz}{w(\mathbf{x}, t)}. \quad (12.76)$$

Alternatively, we can introduce a pseudo-time parameter,  $s$ , that determines a position along a streamline. Streamlines are the curves  $\mathbf{x} = \mathbf{X}(s; \mathbf{a}, t)$  computed with  $(\mathbf{a}, t)$  held fixed, but with

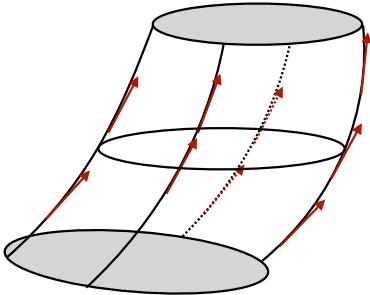


FIGURE 12.5: This image shows an example streamtube. The side boundaries of a streamtube consist of streamlines. At each point of a streamline, the local tangent vector equals to the velocity field (see equation (12.75)). Streamlines are identical to pathlines only for steady flow; they differ for unsteady flows. Hence, for unsteady flows, particle trajectories generally cross through the streamtube boundary.

the pseudo-time varied

$$\frac{\partial \mathbf{X}(s; \mathbf{a}, t)}{\partial s} = \mathbf{v}[\mathbf{X}(s; \mathbf{a}, t), t] \quad (12.77a)$$

$$\mathbf{X}(s = 0; \mathbf{a}, t) = \mathbf{a}. \quad (12.77b)$$

Again, both the material coordinate  $\mathbf{a}$  and time  $t$  are held fixed when determining streamlines, so that  $(\mathbf{a}, t)$  act as parameters to distinguish streamlines. Streamlines thus do not know about the time evolution of unsteady flow. Instead, streamlines only sample a snapshot of the velocity field; they are freshly computed at each time instance.

A *streamtube* is a bundle of streamlines crossing through an arbitrary closed curve (see Figure 12.5). Hence, at each time instance, streamtube sides are parallel to the velocity vector. Furthermore, when the flow is steady then streamlines are identical to material particle pathlines. Hence, a streamtube is a material tube for steady flow, in which case no fluid particles cross the streamtube boundary.

### 12.8.3 Distinguishing streamlines and pathlines

The tangent to a streamline gives the velocity at a single point in time, whereas the tangent to a material pathline (i.e., a trajectory) gives the velocity at subsequent times. These tangents are identical when the flow is steady. However, if the flow is time dependent (unsteady), then streamlines differ from material pathlines. Furthermore, for unsteady flow, the pseudo-time parameter,  $s$ , determining the streamlines in equation (12.77a) is not equal to the time,  $t$ , used to compute fluid particle trajectories in equation (12.72a). Consequently, the condition  $\mathbf{v} \cdot \hat{\mathbf{n}} = 0$  satisfied at each instance by a streamline does not ensure that fluid particles do not cross streamlines. The reason is that a material pathline moves with the fluid in such a way that

$$(\mathbf{v} - \mathbf{v}^{\text{line}}) \cdot \hat{\mathbf{n}} = 0 \implies \mathbf{v} \cdot \hat{\mathbf{n}} = \mathbf{v}^{\text{line}} \cdot \hat{\mathbf{n}} \quad \text{material lines,} \quad (12.78)$$

where  $\mathbf{v}^{\text{line}}$  is the velocity of a point on the material pathline. The material pathline thus moves so that no fluid particles cross it. Only when the flow is steady, so that  $\mathbf{v}^{\text{line}} \cdot \hat{\mathbf{n}} = 0$ , will material pathlines and streamlines be equal. That is, the streamline constraint  $\mathbf{v} \cdot \hat{\mathbf{n}} = 0$  is not a material constraint when  $\mathbf{v}^{\text{line}} \cdot \hat{\mathbf{n}} \neq 0$ . The key point is that streamlines do not probe the time behavior of the flow, so they do not know whether the velocity is steady or unsteady.

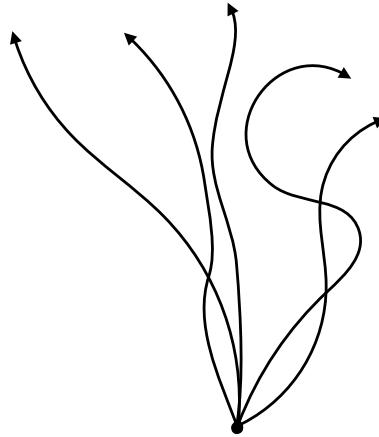


FIGURE 12.6: A suite of trajectories emanating from a single point. Common realizations include the paths of fluid particles that leave from a chimney, or the smoke from a point source. A streakline is defined as the accumulation of positions at time  $t$  of particles that passed through the common point at some earlier time  $s < t$ .

#### 12.8.4 Fluid streaklines

A *streakline* is a curve obtained by connecting the positions for all fluid particles that emanate from a fixed point in space (see Figure 12.6). Streaklines are simple to define conceptually and to realize experimentally. However, they are a bit convoluted to specify mathematically. We thus present two formulations.

At any time  $t$ , the streakline passing through a fixed point  $\mathbf{y}$  is a curve going from  $\mathbf{y}$  to  $\mathbf{X}(\mathbf{y}, t)$ , the position reached by the particle initialized at  $t = 0$  at the point  $\mathbf{y}$ . A particle is on the streakline if it passed the fixed point  $\mathbf{y}$  at some time between 0 and  $t$ . If this time was  $s$ , then the material coordinate of the particle would be given by  $\mathbf{a}(\mathbf{y}, s)$  (see equation (12.8) relating the material coordinate to its corresponding laboratory position). Furthermore, at time  $t$ , this particle is at  $\mathbf{x}$ , so that the equation of the streakline at time  $t$  is

$$\mathbf{x} = \mathbf{X}[\mathbf{a}(\mathbf{y}, s), t] \quad 0 \leq s \leq t. \quad (12.79)$$

We can connect the streakline specification to that given for a pathline and streamline through the following. A streakline at some time instance  $\tilde{t}$  is a curve defined by fixing  $\tilde{t}$  and varying  $s$  over  $s \leq \tilde{t}$  in the function  $\mathbf{X}(s; \mathbf{a}, \tilde{t})$ . We determine the curves  $\mathbf{x} = \mathbf{X}(s; \mathbf{a}, \tilde{t})$  by solving the following set of initial value problems for trajectories with initial conditions imposed at  $t = s$  rather than  $t = 0$

$$\frac{\partial \mathbf{X}(s; \mathbf{a}, t)}{\partial t} = \mathbf{v}[\mathbf{X}(s; \mathbf{a}, t), t] \quad (12.80a)$$

$$\mathbf{X}(t = s; \mathbf{a}, t) = \mathbf{a}. \quad (12.80b)$$

Note that  $\mathbf{a}$  remains fixed, as we start all trajectories determining a streakline from the same initial point (e.g., the chimney does not move). A streakline can thus be generated by emitting a dye from a point over a time interval equal to the range of  $s$ , with the dye following fluid particle trajectories.

### 12.8.5 An analytic example of flow lines

Consider the following two-dimensional example as taken from Section 4.13 of *Aris* (1962). Let the Eulerian velocity field be given by

$$u = \frac{x}{\tau + t} \quad (12.81a)$$

$$v = \frac{y}{\tau} \quad (12.81b)$$

$$w = 0, \quad (12.81c)$$

where  $\tau > 0$  is a constant with the dimensions of time.

#### Pathlines

Pathlines are determined by solving the trajectory equations

$$\frac{dX(t)}{dt} = \frac{X(t)}{\tau + t} \quad (12.82a)$$

$$\frac{dY(t)}{dt} = \frac{Y(t)}{\tau} \quad (12.82b)$$

$$\frac{dZ(t)}{dt} = 0, \quad (12.82c)$$

which are found to be

$$X(t) = X_0 (1 + t/\tau) \quad (12.83a)$$

$$Y(t) = Y_0 e^{t/\tau} \quad (12.83b)$$

$$Z(t) = Z_0, \quad (12.83c)$$

where  $\mathbf{X}(t=0) = \mathbf{X}_0$ . Sample trajectories are shown in Figure 12.7 over time  $t \in [0, 2]$ . We can eliminate time to yield a curve in the horizontal  $(x, y)$  plane

$$y = Y_0 e^{(x-X_0)/X_0}. \quad (12.84)$$

#### Streamlines

Streamlines are determined by solving the differential equations

$$\frac{dX(s; t)}{ds} = \frac{X(s; t)}{\tau + t} \quad (12.85a)$$

$$\frac{dY(s; t)}{ds} = \frac{Y(s; t)}{\tau} \quad (12.85b)$$

$$\frac{dZ(s; t)}{ds} = 0, \quad (12.85c)$$

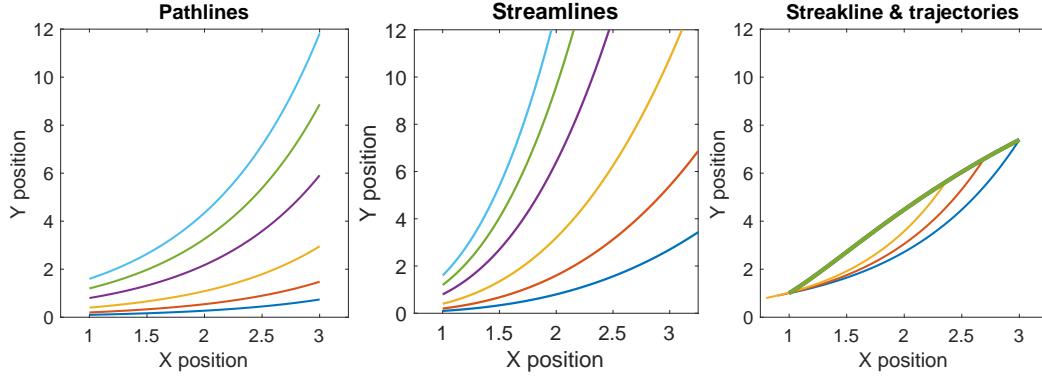


FIGURE 12.7: Left panel: sample pathlines  $X(t) = X_0(1 + t/\tau)$  and  $Y(t) = Y_0 e^{t/\tau}$  (see equations (12.83a) and (12.83b)) during times  $t \in [0, 2]$ . The trajectories drawn here all start at  $X_0 = 1$  and set the parameter  $\tau = 1$ . Note that those pathlines with  $X_0 = 0$  remain on the y-axis, and those with  $Y_0 = 0$  remain on the x-axis. Middle panel: Sample streamlines  $X(s; t) = X_0 e^{s/(\tau+t)}$  and  $Y(s; t) = Y_0 e^{s/\tau}$  (see equations (12.86a) and (12.86b)). We set  $t = 2$  and let the pseudo-time run from  $s \in [0, 4]$ . All streamlines shown here start at  $X_0 = 1$ . Note that those that start with  $X_0 = 0$  remain on the y-axis, and those that start with  $Y_0 = 0$  remain on the x-axis. Right panel: sample analytic streakline (dark bold line) at  $t = 2$  according to equations (12.89a) and (12.89b). This streakline is determined by the position of particles at  $t = 2$  that pass through  $(X, Y) = (1, 1)$  during times  $t \in (-\infty, 2)$ . We show three sample trajectories that fall onto the streakline. The longest trajectory starts at  $(X, Y) = (1, 1)$  at  $t = 0$ , whereas the two shorter trajectories pass through  $(X, Y) = (1, 1)$  at some time  $0 < t < 2$ . Notice the distinction between all three flow lines, which is to be expected since the flow field is unsteady.

where time,  $t$ , is a fixed parameter whereas the pseudo-time,  $s$ , is varied. Integration renders the streamlines

$$X(s; t) = X_0 e^{s/(\tau+t)} \quad (12.86a)$$

$$Y(s; t) = Y_0 e^{s/\tau} \quad (12.86b)$$

$$Z(s; t) = Z_0. \quad (12.86c)$$

Sample streamlines are shown in Figure 12.7. Note that we can eliminate the pseudo-time  $s$  to render a curve in the horizontal  $(x, y)$  plane

$$y = Y_0 \left[ \frac{x}{X_0} \right]^{(\tau+t)/\tau} \quad (12.87a)$$

$$z = Z_0. \quad (12.87b)$$

### Streaklines

For streaklines, invert the trajectory expressions (12.83a)-(12.83b) to find the material coordinates  $\mathbf{a}(y, s)$  in the form

$$a_1 = \frac{y_1}{1 + s/\tau} \quad (12.88a)$$

$$a_2 = y_2 e^{-s/\tau} \quad (12.88b)$$

$$a_3 = y_3. \quad (12.88c)$$

We next evaluate the trajectory expressions (12.83a)-(12.83b) with  $\mathbf{a}$  as the initial positions to find the streaklines

$$X(s; \mathbf{a}, t) = \frac{y_1(1 + t/\tau)}{1 + s/\tau} \quad (12.89a)$$

$$Y(s; \mathbf{a}, t) = y_2 e^{(t-s)/\tau} \quad (12.89b)$$

$$Z(s; \mathbf{a}, t) = y_3. \quad (12.89c)$$

Figure 12.7 illustrates the streakline for a particular point  $(X, Y) = (1, 1)$ .

### 12.8.6 Further study

A discussion of flow lines can be found in most books on fluid mechanics. The presentation here borrows from Sections 4.11-4.13 of *Aris* (1962), Section 3.3 of *Kundu et al.* (2016), and online lecture notes on fluid kinematics from Professor McIntyre of Cambridge University.

## 12.9 Exercises

### EXERCISE 12.1: FLUID VELOCITY AND ACCELERATION DERIVED FROM A TRAJECTORY

Following the example in Section 12.5.7, consider the one-dimensional fluid particle trajectory

$$\mathbf{X}(t) = \hat{\mathbf{x}} X(t) = \hat{\mathbf{x}} [k(t - t_0)^2 + x_0^3]^{1/3}, \quad (12.90)$$

where  $k$  is a constant with dimensions  $L^3 T^{-2}$  and  $x_0$  is the particle position at time  $t_0$ .

- (a) Determine the velocity of the fluid particle.
- (b) Determine the acceleration of the fluid particle.
- (c) Determine the Eulerian velocity field.
- (d) Determine the Eulerian acceleration field and show that it equals to the particle acceleration when evaluated at the field point,  $\mathbf{x} = \mathbf{X}(t)$ .

### EXERCISE 12.2: MATERIAL EVOLUTION OF THE PARTIAL DERIVATIVE OF A FUNCTION

In this exercise we establish some properties of the material time derivative operator when acting on spatial derivatives of a scalar field.

- (a) If a scalar field  $\Pi$  is materially constant, prove that the material evolution of its spatial derivative is given by

$$\frac{D(\partial_m \Pi)}{Dt} = -\partial_m \mathbf{v} \cdot \nabla \Pi. \quad (12.91)$$

For example, if  $D\Pi/Dt = 0$ , then the zonal partial derivative  $\partial_x \Pi$  has a material time derivative given by

$$\frac{D(\partial \Pi / \partial x)}{Dt} = -\frac{\partial \mathbf{v}}{\partial x} \cdot \nabla \Pi. \quad (12.92)$$

- (b) What is the material time derivative of  $\nabla \Pi$  for the case that  $\Pi$  is not materially constant?

Hint: Some might find it more suitable to first solve the general case in part (a) and then specialize to  $D\Pi/Dt = 0$  in part (b). Also, use Cartesian tensors for convenience.





# Chapter 13

## Material fluid objects

Draw an imaginary line, area, or volume within a perfect fluid. Since the fluid is perfect, all fluid particles that start on the geometric object remain on the object, even as the shape of the geometric object is deformed by the moving fluid. We say that the geometric object is a perfectly *coherent structure*. We study the kinematics of such objects in this chapter by using both Lagrangian and Eulerian descriptions, with the two offering complementary insights. Some extra attention is given to the kinematics of two-dimensional flow due to the relative mathematical ease and the associated intuition that proves useful for more general three dimensional flows.

The kinematic ideas developed in this chapter for a perfect fluid have use in the study of mixing and transport within real geophysical fluids. That is, for a real fluid we also find it useful to study geometric objects that follow the flow. However, in a real fluid such objects are not perfectly coherent since matter generally crosses all surfaces through diffusive mixing. The question then becomes whether there are special surfaces where such mixing is suppressed, with this question forming a key part of the study of coherent structures in real fluids (e.g., [Haller \(2015\)](#)).

### READER'S GUIDE FOR THIS CHAPTER

This chapter builds from the kinematics of Chapter 12 and makes some use of Section 3.1 of [Batchelor \(1967\)](#). A more thorough development is given by [Ottino \(1989\)](#). These ideas and methods are of interest to a variety of kinematic aspects of fluid motion, with particular application to the kinematics of mixing, stirring, and coherency in eddying geophysical fluids. The discussion is restricted to Cartesian tensors to reduce the math overhead. Consequently, all tensor labels are downstairs with no distinction between covariant and contravariant. Extensions to arbitrary coordinates follow the methods of Chapter 7.

13.1	Loose threads . . . . .	270
13.2	Increments in material and position space . . . . .	270
13.2.1	Eulerian/position space differential . . . . .	270
13.2.2	Lagrangian/material space differential . . . . .	271
13.2.3	Duality between Eulerian and Lagrangian perspectives . . . . .	271
13.3	Evolution of material curves . . . . .	272
13.3.1	Deformation gradient tensor . . . . .	272
13.3.2	Cauchy-Green strain tensor . . . . .	273
13.3.3	Kinematic evolution equation . . . . .	273
13.3.4	Cauchy's solution . . . . .	273
13.3.5	Velocity gradient tensor . . . . .	275

13.3.6	Stretching and tilting of a material lines . . . . .	276
13.3.7	Rate of strain tensor . . . . .	276
13.3.8	Rotation tensor . . . . .	277
13.3.9	Cauchy-Stokes decomposition . . . . .	278
13.4	Evolution of material surfaces . . . . .	278
13.4.1	Surfaces in three-dimensional flow . . . . .	279
13.4.2	Evolution of the area . . . . .	280
13.4.3	Evolution of the normal vector . . . . .	281
13.4.4	Material area in two-dimensional flow . . . . .	281
13.5	Volume and the Jacobian of transformation . . . . .	282
13.5.1	Material parcel volume . . . . .	283
13.5.2	Evolution of the Jacobian of transformation . . . . .	283
13.6	Kinematics of two-dimensional flow . . . . .	284
13.6.1	Diverging flow . . . . .	284
13.6.2	Rotational flow with nonzero vorticity . . . . .	285
13.6.3	Flow with nonzero deformation . . . . .	285
13.6.4	Further study . . . . .	286
13.7	Exercises . . . . .	286

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## 13.1 Loose threads

- Convert Figure 13.2 into Keynote and gray shade the color.

## 13.2 Increments in material and position space

In this section we summarize some of the maths associated with the differential increment of a function. In particular, we expose how the increment appears in both position/Eulerian space ( $\mathbf{x}$ -space or  $\mathbf{x}$ -coordinates) and in material/Lagrangian space ( $\mathbf{a}$ -space or  $\mathbf{a}$ -coordinates).

### 13.2.1 Eulerian/position space differential

In Section 12.5.1, we considered the space-time increment of a function. Here we consider just the space increment, as defined by the differential increment of a function evaluated at the same time but at two infinitesimally close points in space

$$d\Pi(\mathbf{x}, t) = \Pi(\mathbf{x} + d\mathbf{x}, t) - \Pi(\mathbf{x}, t) \quad (13.1a)$$

$$= (d\mathbf{x} \cdot \nabla)\Pi. \quad (13.1b)$$

The dimensionless operator

$$d\mathbf{x} \cdot \nabla = dx_m \frac{\partial}{\partial x_m} \quad (13.2)$$

is a scalar since it remains form invariant when switching to another set of Cartesian position coordinates.<sup>1</sup>

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<sup>1</sup>This form invariance also holds when using curvilinear coordinates if we make use of the general tensor analysis formalism of Chapter 7.

### 13.2.2 Lagrangian/material space differential

Consider the same function  $\Pi$  evaluated on a material fluid particle trajectory, and write this “Lagrangian” function as

$$\Pi^L(\mathbf{a}, t) = \Pi[\mathbf{X}(\mathbf{a}, t), t]. \quad (13.3)$$

We sometimes use the notation  $\Pi^L(\mathbf{a}, t)$  as a shorthand, which is defined by this equality.<sup>2</sup>

Consider an infinitesimal increment of  $\Pi^L(\mathbf{a}, t)$  within material coordinate space. This increment represents the difference of  $\Pi$  when evaluated on two separate fluid particles labelled by  $\mathbf{a}$  and  $\mathbf{a} + \delta\mathbf{a}$ . Note that we use the  $\delta$  symbol to signal material increments. Just like when working in  $\mathbf{x}$ -space, we can take a Taylor series and truncate to leading order, in which case

$$\delta\Pi^L(\mathbf{a}, t) = \Pi[\mathbf{X}(\mathbf{a} + \delta\mathbf{a}, t), t] - \Pi[\mathbf{X}(\mathbf{a}, t), t] \quad (13.4a)$$

$$= \Pi^L(\mathbf{a} + \delta\mathbf{a}, t) - \Pi^L(\mathbf{a}, t) \quad (13.4b)$$

$$= (\delta\mathbf{a} \cdot \nabla_{\mathbf{a}})\Pi^L(\mathbf{a}, t). \quad (13.4c)$$

The dimensionless operator

$$\delta\mathbf{a} \cdot \nabla_{\mathbf{a}} = \delta a_j \frac{\partial}{\partial a_j} \quad (13.5)$$

is a scalar since it remains form invariant when switching to another set of Cartesian material coordinates.<sup>3</sup> We use the notation  $\nabla_{\mathbf{a}}$  to emphasize that the gradient operator is in material space rather than position space.

### 13.2.3 Duality between Eulerian and Lagrangian perspectives

By construction, the value of a function at a postion  $\mathbf{x}$  (Eulerian perspective) equals to the function evaluated on a moving fluid particle (Lagrangian perspective) when the particle trajectory passes through  $\mathbf{x}$ . Mathematically, this identity takes the form

$$\Pi^L(\mathbf{a}, t) = \Pi[\mathbf{X}(\mathbf{a}, t), t] = \Pi(\mathbf{x}, t) \quad \text{if } \mathbf{X}(\mathbf{a}, t) = \mathbf{x}. \quad (13.6)$$

Likewise, if the infinitesimal increment in space,  $\delta\mathbf{x}$ , equals to the vector increment of the two fluid particles,

$$\delta\mathbf{X}(\mathbf{a}, t) = \mathbf{X}(\mathbf{a} + \delta\mathbf{a}, t) - \mathbf{X}(\mathbf{a}, t), \quad (13.7)$$

then the functional increments are identical

$$\delta\Pi^L(\mathbf{a}, t) = \delta\Pi(\mathbf{x}, t) \quad \text{if } \delta\mathbf{X}(\mathbf{a}, t) = \delta\mathbf{x}, \quad (13.8)$$

where

$$\delta\Pi(\mathbf{x}, t) = \Pi(\mathbf{x} + \delta\mathbf{x}, t) - \Pi(\mathbf{x}, t). \quad (13.9)$$

These identities allow us to develop relations using either a Lagrangian or an Eulerian perspective, and then to interpret them in the complementary perspective. It is very useful in studying fluid mechanics to become versed in the routine use of this Eulerian/Lagrangian duality.

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<sup>2</sup>We introduced this notation in Section 12.5.5.

<sup>3</sup>As for the position space ( $\mathbf{x}$ -space), this invariance also holds when using curvilinear material coordinates if we make use of the general tensor analysis formalism of Chapter 7.

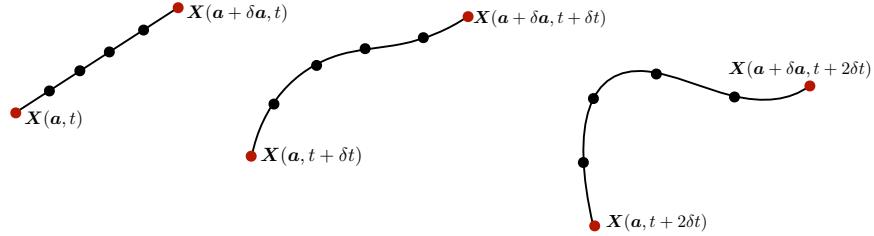


FIGURE 13.1: Three time instances of a material curve with endpoints determined by the trajectories of two fluid particles,  $\mathbf{X}(\mathbf{a}, t)$  and  $\mathbf{X}(\mathbf{a} + \delta\mathbf{a}, t)$ . All points between the endpoints are part of the material curve, and the curve moves through the fluid by following the trajectories of the fluid particles. Kinematics of the curve are determined by properties of the velocity gradient tensor discussed in Section 13.3.5.

## 13.3 Evolution of material curves

Material curves are one-dimensional geometric objects that follow fluid particles in a perfect fluid. We initialize a material curve by drawing a line in the fluid and then following the fluid particles contained on the initial line. The material curve is stretched and folded by the fluid flow (see Figure 13.1). But since the fluid is perfect, the same fluid particles remain on the curve so that it retains exact coherency. We here develop the rudimentary kinematics of material curves.

### 13.3.1 Deformation gradient tensor

Assume the material curve is initially infinitesimal with endpoints given by fluid particles with trajectories  $\mathbf{X}(\mathbf{a}, t)$  and  $\mathbf{X}(\mathbf{a} + \delta\mathbf{a}, t)$  (see Figure 13.1). At time  $t$ , the vector displacement between these two particles is written

$$\delta\mathbf{X}(\mathbf{a}, t) = \mathbf{X}(\mathbf{a} + \delta\mathbf{a}, t) - \mathbf{X}(\mathbf{a}, t). \quad (13.10)$$

Expanding this expression to leading order yields an expression of *Cauchy's solution* (further explored in Section 13.3.4)

$$\delta\mathbf{X}(\mathbf{a}, t) = \mathbf{X}(\mathbf{a} + \delta\mathbf{a}, t) - \mathbf{X}(\mathbf{a}, t) \approx (\delta\mathbf{a} \cdot \nabla_{\mathbf{a}}) \mathbf{X}(\mathbf{a}, t), \quad (13.11)$$

where again  $\nabla_{\mathbf{a}}$  is the gradient operator acting on the material coordinates. Writing this equation in component form leads to

$$\delta X_m = \delta a_j \frac{\partial X_m}{\partial a_j}. \quad (13.12)$$

As in Chapter 12, we assign the labels  $m, n, p$  for position/Eulerian coordinates,  $\mathbf{x}$ , and the labels  $i, j, k$  for material/Lagrangian coordinates,  $\mathbf{a}$ .

The components

$$F_{mj} \equiv \frac{\partial X_m}{\partial a_j} \quad (13.13)$$

appearing in equation (13.12) form elements of the transformation matrix linking position space ( $\mathbf{x}$ -space) to material space ( $\mathbf{a}$ -space). We already encountered this tensor in Section 12.4.3 (see equation (12.9)). In the continuum mechanics literature, the tensor (13.13) is known as the *displacement gradient tensor* or the *deformation gradient tensor*.

### 13.3.2 Cauchy-Green strain tensor

The deformation gradient tensor plays a role in measuring the length of material curves. We see this role by considering the squared length of an infinitesimal portion of a material curve

$$\delta \mathbf{X} \cdot \delta \mathbf{X} = \frac{\partial \mathbf{X}}{\partial a_i} \cdot \frac{\partial \mathbf{X}}{\partial a_j} \delta a_i \delta a_j \equiv C_{ij} \delta a_i \delta a_j. \quad (13.14)$$

Algebraically, this expression is a quadratic form, and the symmetric tensor

$$C_{ij} \equiv \frac{\partial \mathbf{X}}{\partial a_i} \cdot \frac{\partial \mathbf{X}}{\partial a_j} = F_{mi} F_{mj} \quad (13.15)$$

is the metric tensor that provides the means to measure distance along an infinitesimal material curve. This metric tensor is called the *Cauchy-Green strain* tensor.

### 13.3.3 Kinematic evolution equation

Now consider the material time derivative of the material increment

$$\frac{\partial[\delta \mathbf{X}(\mathbf{a}, t)]}{\partial t} = \frac{\partial \mathbf{X}(\mathbf{a} + \delta \mathbf{a}, t)}{\partial t} - \frac{\partial \mathbf{X}(\mathbf{a}, t)}{\partial t} \quad (13.16a)$$

$$= \mathbf{v}^L(\mathbf{a} + \delta \mathbf{a}, t) - \mathbf{v}^L(\mathbf{a}, t) \quad (13.16b)$$

$$\equiv \delta \mathbf{v}^L(\mathbf{a}, t). \quad (13.16c)$$

In these equations, we introduced the Lagrangian velocity

$$\mathbf{v}^L(\mathbf{a}, t) = \mathbf{v}[\mathbf{X}(\mathbf{a}, t), t] \quad (13.17)$$

as per equation (12.32) and the discussion in Section 13.2.2. As for the manipulations in Section 13.3.1, we can massage the expression (13.16c) by performing a Taylor series expansion and truncating to leading order

$$\frac{\partial[\delta \mathbf{X}(\mathbf{a}, t)]}{\partial t} = \delta \mathbf{v}^L(\mathbf{a}, t) = (\delta \mathbf{a} \cdot \nabla_{\mathbf{a}}) \mathbf{v}^L(\mathbf{a}, t). \quad (13.18)$$

Alternatively, we can choose to evaluate this expression using an Eulerian perspective (see Section 13.2.3), in which case

$$\frac{D(\delta \mathbf{x})}{Dt} = \delta \mathbf{v}(\mathbf{x}, t) = (\delta \mathbf{x} \cdot \nabla_{\mathbf{x}}) \mathbf{v}(\mathbf{x}, t). \quad (13.19)$$

### 13.3.4 Cauchy's solution

We can determine a general solution to the kinematic evolution equation (13.19) following the method used by Cauchy<sup>4</sup> to solve the perfect fluid barotropic vorticity equation discussed in Section 35.6. Indeed, we already encountered the Cauchy solution in Section 13.3.1. We rederive it here, following a more laborious route, to expose some of the formalism that can be of use when working with Lagrangian coordinates, and to offer some further insight into the meaning of the solution.

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<sup>4</sup>See [Frisch and Villone \(2014\)](#) for an insightful discussion of the enduring impact of Cauchy's solution.

*Derivation*

The derivation that follows involves strategic uses of the transformation between  $\mathbf{a}$ -coordinates and  $\mathbf{x}$ -coordinates, which we start by writing

$$\frac{D(\delta x_n)}{Dt} = (\delta \mathbf{x} \cdot \nabla_{\mathbf{x}}) v_n \quad \text{kinematic evolution} \quad (13.20a)$$

$$= \delta x_m \frac{\partial}{\partial x_m} \left[ \frac{Dx_n}{Dt} \right] \quad v_n = Dx_n/Dt \quad (13.20b)$$

$$= \delta x_m \frac{\partial a_j}{\partial x_m} \frac{\partial}{\partial a_j} \left[ \frac{Dx_n}{Dt} \right] \quad \text{chain rule (13.20c)}$$

$$= \delta x_m \frac{\partial a_j}{\partial x_m} \frac{D}{Dt} \frac{\partial x_n}{\partial a_j} \quad \text{commute } \partial/\partial a_j \text{ and } D/Dt \quad (13.20d)$$

$$= \delta x_m \frac{D}{Dt} \left[ \frac{\partial a_j}{\partial x_m} \frac{\partial x_n}{\partial a_j} \right] - \delta x_m \frac{D}{Dt} \left[ \frac{\partial a_j}{\partial x_m} \right] \frac{\partial x_n}{\partial a_j} \quad \text{move } D/Dt \quad (13.20e)$$

$$= -\delta x_m \frac{D}{Dt} \left[ \frac{\partial a_j}{\partial x_m} \right] \frac{\partial x_n}{\partial a_j}. \quad \frac{\partial a_j}{\partial x_m} \frac{\partial x_n}{\partial a_j} = \delta_{mn} = \text{constant.} \quad (13.20f)$$

The commutation in equation (13.20d) follows since the material coordinates are fixed on a fluid particle so that

$$\frac{\partial}{\partial a_j} \frac{D}{Dt} = \frac{D}{Dt} \frac{\partial}{\partial a_j}. \quad (13.21)$$

Contracting the identity (13.20f) with  $\partial a_k / \partial x_n$  yields

$$\frac{\partial a_k}{\partial x_n} \frac{D(\delta x_n)}{Dt} = -\delta x_m \frac{D}{Dt} \left[ \frac{\partial a_j}{\partial x_m} \right] \frac{\partial x_n}{\partial a_j} \frac{\partial a_k}{\partial x_n} \quad \text{contraction (inner product)} \quad (13.22a)$$

$$= -\delta x_m \frac{D}{Dt} \left[ \frac{\partial a_k}{\partial x_m} \right] \quad \frac{\partial x_n}{\partial a_j} \frac{\partial a_k}{\partial x_n} = \delta_{jk} \quad (13.22b)$$

$$= -\delta x_n \frac{D}{Dt} \left[ \frac{\partial a_k}{\partial x_n} \right] \quad \text{change indices from } m \text{ to } n. \quad (13.22c)$$

We can thus identify the material invariant

$$\frac{D}{Dt} \left[ \delta x_n \frac{\partial a_k}{\partial x_n} \right] = 0 \implies \delta \mathbf{x} \cdot \nabla_{\mathbf{x}} a_k = \text{material invariant.} \quad (13.23)$$

This result follows rather trivially by recognizing the coordinate transformation

$$\delta \mathbf{x} \cdot \nabla_{\mathbf{x}} a_k = \delta x_n \frac{\partial a_k}{\partial x_n} = \delta a_k, \quad (13.24)$$

and noting that  $\delta a_k$  is a material invariant, in which case  $\delta \mathbf{x} \cdot \nabla_{\mathbf{x}} a_k$  must also be materially invariant.

If we choose the material coordinates as the initial positions of fluid particles,

$$\mathbf{a} = \mathbf{x}(t = 0), \quad (13.25)$$

then the Jacobian at the initial time is given by the unit tensor

$$\frac{\partial a_k}{\partial x_m} = \delta_{km}, \quad (13.26)$$

so that the material invariance in equation (13.23) leads to

$$\delta\mathbf{x}(t) \cdot \nabla_{\mathbf{x}} a_k = \delta x_k(t=0) \iff \delta x_m \frac{\partial a_k}{\partial x_m} = \delta x_k(t=0). \quad (13.27)$$

Inverting this equation by contracting with  $\partial x_n / \partial a_k$  and using  $(\partial x_n / \partial a_k)(\partial a_k / \partial x_m) = \delta_{mn}$  leads to *Cauchy's solution*

$$\delta x_n(t) = \delta x_k(t=0) \frac{\partial x_n}{\partial a_k}. \quad (13.28)$$

#### *Discussion and extension to vorticity*

The Cauchy solution (13.28) says that the increment along a line segment defined by fluid particles,  $\delta\mathbf{x}(t)$ , expands or contracts according to the time and space dependent Jacobian,  $\partial x_n / \partial a_k$ . This result follows from our assumption that the increment is defined by fixed  $\mathbf{a}$ -space coordinates (fixed fluid particles), which then constrains the increment's  $\mathbf{x}$ -space evolution. It is also an expression that we wrote down, rather trivially, in equation (13.11) when performing a truncated Taylor series expansion of the spatial increment between two material fluid particles. The ability to derive certain kinematic results using either simple (indeed trivial) methods versus more long-winded methods is somewhat exemplary of fluid kinematics. Both approaches offer distinct insights as well as confidence in the validity of the result.<sup>5</sup>

As seen in Section 35.4, the relative vorticity,  $\boldsymbol{\omega} = \nabla \times \mathbf{v}$ , for a homogeneous inviscid, barotropic fluid satisfies the same kinematic equation (13.19) as for a material line increment

$$\frac{D\boldsymbol{\omega}}{Dt} = (\boldsymbol{\omega} \cdot \nabla_{\mathbf{x}}) \mathbf{v}(\mathbf{x}, t). \quad (13.29)$$

We can thus invoke the Cauchy solution to write the vorticity

$$\omega_n(t) = \omega_k(t=0) \frac{\partial x_n}{\partial a_k}, \quad (13.30)$$

which is one form of Kelvin's circulation theorem detailed in Section 35.3.

#### 13.3.5 Velocity gradient tensor

Writing the Eulerian result (13.19) in component form leads to

$$\frac{D(\delta x_m)}{Dt} = \frac{D(x_m + \delta x_m - x_m)}{Dt} = v_m(\mathbf{x} + \delta\mathbf{x}) - v_m(\mathbf{x}) = \delta x_n \frac{\partial v_m}{\partial x_n}. \quad (13.31)$$

The derivatives  $\partial v_m / \partial x_n$  form components to the second-order *velocity gradient* tensor whose dimensions are inverse time (i.e., a rate). The velocity gradient tensor determines how an infinitesimal material line is deformed as it moves through the flow field.

As with any matrix, a second-order tensor can be decomposed into its symmetric and anti-

---

<sup>5</sup>If there is more than one way to solve a problem, then do so!

symmetric components

$$\frac{\partial v_m}{\partial x_n} = \frac{1}{2} \left[ \frac{\partial v_m}{\partial x_n} + \frac{\partial v_n}{\partial x_m} \right] + \frac{1}{2} \left[ \frac{\partial v_m}{\partial x_n} - \frac{\partial v_n}{\partial x_m} \right] \equiv \mathbb{S}_{mn} + \mathbb{R}_{mn}, \quad (13.32)$$

where<sup>6</sup>

$$\mathbb{S}_{mn} = \frac{1}{2} \left[ \frac{\partial v_m}{\partial x_n} + \frac{\partial v_n}{\partial x_m} \right] = \mathbb{S}_{nm} \quad \text{rate of strain tensor} \quad (13.33a)$$

$$\mathbb{R}_{mn} = \frac{1}{2} \left[ \frac{\partial v_m}{\partial x_n} - \frac{\partial v_n}{\partial x_m} \right] = -\mathbb{R}_{nm} \quad \text{rotation tensor.} \quad (13.33b)$$

As seen in the following, these tensors affect the motion of a line element in very distinct manners.

### 13.3.6 Stretching and tilting of a material lines

Consider a material line that is initially aligned with the vertical axis

$$\delta \mathbf{x}_{t=0} = \hat{z} \delta Z_0. \quad (13.34)$$

Consequently, the initial evolution of this material line takes on the form

$$\underbrace{\frac{D(\delta x)}{Dt}}_{\text{tilting}} = \delta Z_0 \underbrace{\left[ \frac{\partial u}{\partial z} \right]}_{\text{tilting}} \quad \text{and} \quad \underbrace{\frac{D(\delta y)}{Dt}}_{\text{tilting}} = \delta Z_0 \underbrace{\left[ \frac{\partial v}{\partial z} \right]}_{\text{tilting}} \quad \text{and} \quad \underbrace{\frac{D(\delta z)}{Dt}}_{\text{stretching}} = \delta Z_0 \underbrace{\left[ \frac{\partial w}{\partial z} \right]}_{\text{stretching}}. \quad (13.35)$$

In the presence of a vertical derivative in the horizontal velocity field (vertical shear), the first and second terms create a non-zero projection of the material line onto the horizontal plane. That is, these terms *tilt* the material line. Additionally, in the presence of a vertical derivative in the vertical velocity, the material line is expanded or compressed along its initial axis. This term is called *stretching*. We return to the tilting and stretching mechanisms when discussing the dynamics of vorticity in Chapter 35. There, we see that vortex lines in a perfect fluid flow are material lines. Consequently, vortex lines are also affected by tilting and stretching just like a material line.

### 13.3.7 Rate of strain tensor

Recall the expression (13.14) for the squared length of a line element

$$\delta \mathbf{X} \cdot \delta \mathbf{X} = \frac{\partial \mathbf{X}}{\partial a_i} \cdot \frac{\partial \mathbf{X}}{\partial a_j} \delta a_i \delta a_j. \quad (13.36)$$

Its material time derivative is given by

$$\left[ \frac{\partial (\delta \mathbf{X} \cdot \delta \mathbf{X})}{\partial t} \right]_{\mathbf{a}} = 2 \frac{\partial \mathbf{v}^L}{\partial a_i} \cdot \frac{\partial \mathbf{X}}{\partial a_j} \delta a_i \delta a_j. \quad (13.37)$$

---

<sup>6</sup>The rate of strain tensor,  $\mathbb{S}_{mn}$ , is sometimes called the *deformation* tensor in the literature. We do not use this nomenclature to avoid confusion with the *deformation gradient* tensor defined by equation (13.13).

We can express this result using Eulerian  $\mathbf{x}$ -coordinates by making use of the duality described in Section 13.2.3, which leads to

$$\frac{\partial \mathbf{v}^L}{\partial a_i} \delta a_i = \frac{\partial \mathbf{v}}{\partial x_n} \delta x_n \quad (13.38a)$$

$$\frac{\partial \mathbf{X}}{\partial a_j} \delta a_j = \delta \mathbf{x}, \quad (13.38b)$$

so that

$$\frac{D(\delta \mathbf{x} \cdot \delta \mathbf{x})}{Dt} = 2 \frac{\partial v_m}{\partial x_n} \delta x_n \delta x_m. \quad (13.39)$$

Since the product  $\delta x_n \delta x_m$  is symmetric on the labels  $m, n$ , it projects out the symmetric portion of the velocity gradient tensor, thus yielding

$$\frac{1}{2} \frac{D(\delta \mathbf{x} \cdot \delta \mathbf{x})}{Dt} = \mathbb{S}_{mn} \delta x_n \delta x_m. \quad (13.40)$$

Consequently, the rate of strain tensor,  $\mathbb{S}_{mn}$ , determines the rate at which a material curve changes its length.

To help understand the result (13.40), consider two fluid particles initialized very close together. Equation (13.40) says that the distance between the two particles is modified so long as there are nonzero strains in the fluid flow, with strains measured by the rate of strain tensor. In the special case of a zero of strain tensor, then the curve retains a constant length.

As a symmetric matrix, the rate of strain tensor can be diagonalized, with the diagonal elements equal to the eigenvalues (e.g., see section 2.2 of Segel (1987)). Each eigenvalue measures the rate that material lines oriented according to the principle axes (eigenvectors) expand/contract under the impacts of straining motion in the fluid. According to equation (13.40), the expansion/contraction is exponential when aligned along the principle axes, with the exponential rate determined by the eigenvalues of  $\mathbb{S}$ . Furthermore, as shown in Section 13.5, the sum of these eigenvectors (trace of the rate of strain tensor) measures the rate that a material volume changes through the divergence of the velocity

$$\mathbb{S}_{mm} = \nabla \cdot \mathbf{v}. \quad (13.41)$$

### 13.3.8 Rotation tensor

The rotation tensor is given by

$$\mathbb{R}_{mn} = (1/2) (\partial_n v_m - \partial_m v_n) = (1/2) (v_{m,n} - v_{n,m}), \quad (13.42)$$

with the second equality introducing the commonly used comma notation for the partial derivative; a notation that is helpful to keep the signs properly sorted with the definition. Notably, the rotation tensor is anti-symmetric:

$$\mathbb{R}_{mn} = -\mathbb{R}_{nm}. \quad (13.43)$$

Its components are related to the vorticity vector  $\boldsymbol{\omega} = \nabla \times \mathbf{v}$  according to

$$\mathbb{R}_{mn} = -\epsilon_{mnp} \omega_p / 2 \iff \mathbb{R} = \frac{1}{2} \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix} \iff \omega_p = -\epsilon_{pmn} \mathbb{R}_{mn}, \quad (13.44)$$

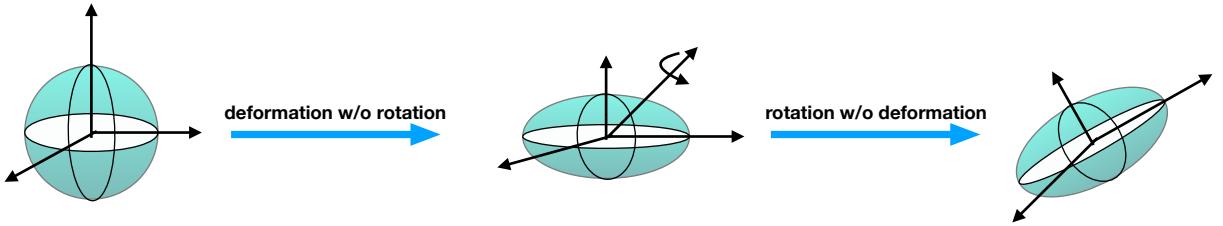


FIGURE 13.2: Schematic illustrating the Cauchy-Stokes decomposition of how fluid flow can modify a material region according to equation (13.48). First the sphere can be deformed without rotation, with this process encompassed by the rate of strate tensor,  $\mathbb{S}_{mn}$ . Next it can be rigidly rotated without changing its shape, as encompassed by the rotation tensor,  $\mathbb{R}_{mn}$ . The axes shown represent the principle axes so that deformation corresponds to expansion or contraction along the principle axes directions.

where the final expression made use of the identity (1.38) in the form

$$\epsilon_{mns} \epsilon_{mnp} = 2 \delta_{sp}. \quad (13.45)$$

We see that the squared rotation tensor equals to half the squared vorticity

$$\mathbb{R}^2 = \mathbb{R}_{mn} \mathbb{R}_{mn} = |\boldsymbol{\omega}|^2/2. \quad (13.46)$$

The contribution of the rotation matrix to evolution of the material curve is given by

$$\left[ \frac{D(\delta x_m)}{Dt} \right]_{\text{rot}} = \mathbb{R}_{mn} \delta x_n = -(\epsilon_{mnp} \omega_p/2) \delta x_n \implies \left[ \frac{D(\delta \mathbf{x})}{Dt} \right]_{\text{rot}} = \frac{1}{2} (\boldsymbol{\omega} \times \delta \mathbf{x}). \quad (13.47)$$

This relation is in the form of a pure rotation of the vector  $\delta \mathbf{x}$  generated by the vector  $\boldsymbol{\omega}/2$  (recall the discussion of rotations in Section 9.4). We thus conclude that the anti-symmetric rotation tensor,  $\mathbb{R}$ , provides a rigid body rotation to a material curve (or any infinitesimal fluid region) about the axis defined by the vorticity vector. It rotates the objects without altering the size (length, area, volume). Notably, when acting on vorticity the rotation tensor has no affect since  $\boldsymbol{\omega} \times \boldsymbol{\omega} = 0$ . We return to this point when discussing vortex filaments in Section 35.6.

### 13.3.9 Cauchy-Stokes decomposition

The above discussion of how fluid motion impacts on a material curve falls under the more general insights from the *Cauchy-Stokes decomposition theorem*. This theorem says that the arbitrary motion of a body can be decomposed into a uniform translation, dilation along three perpendicular axes, plus a rigid body rotation. Mathematically, this decomposition can be written by expanding equation (13.31) to read

$$v_m(\mathbf{x}, t) = v_m(\mathbf{x}_0, t) + \mathbb{S}_{mn} \delta x_n + \mathbb{R}_{mn} \delta x_n \iff \mathbf{v}(\mathbf{x}, t) = \mathbf{v}(\mathbf{x}_0, t) + \mathbb{S} \cdot \delta \mathbf{x} + \mathbb{R} \cdot \delta \mathbf{x}. \quad (13.48)$$

Figure 13.2 illustrates the deformation and rotation portion of this decomposition. A more thorough discussion of these fundamental kinematic notions can be found in Chapter 4 of [Aris \(1962\)](#), Section 3.1 of [Segel \(1987\)](#), and with a brief summary in Section 1.1 of [Olbers et al. \(2012\)](#).

## 13.4 Evolution of material surfaces

We extend the discussion of material curves in Section 13.3 to a material surface such as that shown in Figure 13.3, with consideration given to both three-dimensional and two-dimensional

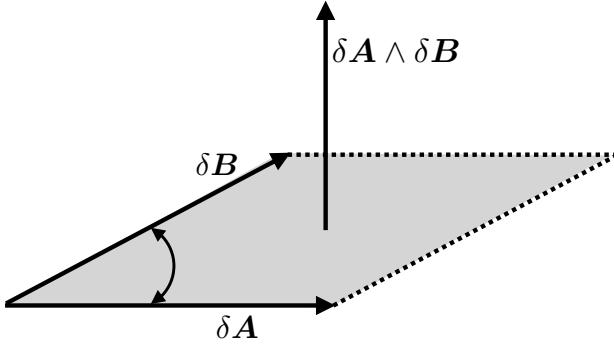


FIGURE 13.3: A material surface as defined by the cross product of two material line elements,  $\delta S = \delta A \times \delta B$ . In the special case of  $\delta A = \hat{x} \delta x$  and  $\delta B = \hat{y} \delta y$ , then  $\delta S = \delta x \delta y \hat{z}$ .

flows.

### 13.4.1 Surfaces in three-dimensional flow

Following from the geometric interpretation of the vector product in Section 1.4.5, we here define a material surface by (see Figure 13.3)

$$\delta S = \delta A \times \delta B \Rightarrow \delta S_m = \epsilon_{mnp} \delta A_n \delta B_p \quad (13.49)$$

where  $\delta A$  and  $\delta B$  are non-parallel infinitesimal material lines. The surface projected onto the direction  $\hat{n}$  is given by

$$\hat{n} \cdot \delta S = \hat{n} \cdot (\delta A \times \delta B). \quad (13.50)$$

The evolution of the material surface is given by

$$\frac{D(\delta S)}{Dt} = \frac{D(\delta A)}{Dt} \times \delta B + \delta A \times \frac{D(\delta B)}{Dt} \quad (13.51a)$$

$$= [(\delta A \cdot \nabla) v] \times \delta B + \delta A \times [(\delta B \cdot \nabla) v], \quad (13.51b)$$

where the second equality made use of the material line evolution equation (13.19). To proceed we expose indices and make use of some tensor identities

$$\frac{D(\delta S_m)}{Dt} = \epsilon_{mnp} [(\delta A_q \partial_q) v_n] \delta B_p + \epsilon_{mnp} \delta A_n [(\delta B_q \partial_q) v_p] \quad (13.52a)$$

$$= \epsilon_{mnp} [\delta A_q \delta B_p \partial_q v_n + \delta A_n \delta B_q \partial_q v_p] \quad (13.52b)$$

$$= \epsilon_{mnp} \partial_q v_n [\delta A_q \delta B_p - \delta A_p \delta B_q] \quad (13.52c)$$

$$= \epsilon_{mnp} \partial_q v_n \epsilon_{rqp} \delta S_r \quad (13.52d)$$

$$= (\delta_{mr} \delta_{nq} - \delta_{mq} \delta_{nr}) \partial_q v_n \delta S_r \quad (13.52e)$$

$$= (\nabla \cdot v) \delta S_m - (\partial_m v) \cdot \delta S. \quad (13.52f)$$

To reach this result we made use of the following identities available for the permutation symbol from Chapter 1

$$\delta A_q \delta B_p - \delta A_p \delta B_q = \epsilon_{rqp} \delta S_r \quad (13.53a)$$

$$\epsilon_{mnp} \epsilon_{rqp} = \delta_{mr} \delta_{nq} - \delta_{mq} \delta_{nr} \quad (13.53b)$$

where  $\delta_{mn}$  is the Kronecker (or identity) tensor.

### 13.4.2 Evolution of the area

Now orient the material surface area according to its outward normal vector

$$\delta S = \hat{n} \delta \mathcal{S} \implies \delta S_m = \hat{n}_m \delta \mathcal{S}. \quad (13.54)$$

Doing so brings equation (13.52f) to the form

$$\frac{1}{\delta \mathcal{S}} \frac{D(\hat{n}_m \delta \mathcal{S})}{Dt} = (\nabla \cdot \mathbf{v}) \hat{n}_m - (\partial_m \mathbf{v}) \cdot \hat{n}. \quad (13.55)$$

We can thus develop evolution equations for the surface area,  $\delta \mathcal{S}$ , and the normal vector,  $\hat{n}$ .

For the surface area evolution we take the inner product with  $\hat{n}_m$  to yield

$$\frac{1}{\delta \mathcal{S}} \frac{D\delta \mathcal{S}}{Dt} = \nabla \cdot \mathbf{v} - [(\hat{n} \cdot \nabla) \mathbf{v}] \cdot \hat{n} \quad (13.56)$$

where we set  $\hat{n} \cdot \hat{n} = 1$  and followed the discussion in Section 2.1.5 to find that

$$\hat{n} \cdot \hat{n} = 1 \implies \hat{n} \cdot \frac{D\hat{n}}{Dt} = 0, \quad (13.57)$$

so that the normal vector is always perpendicular to its material time derivative. Rearrangement of equation (13.56) then leads to the kinematic evolution equation for the area

$$\frac{1}{\delta S} \frac{D\delta S}{Dt} = [\partial_m - \hat{n}_m (\hat{n} \cdot \nabla)] v_m. \quad (13.58)$$

We next provide some interpretation of this result.

#### Surface derivative operator

The derivative operator on the right hand side of equation (13.58),

$$\partial_m^{\text{surf}} \equiv \partial_m - \hat{n}_m (\hat{n} \cdot \nabla), \quad (13.59)$$

is a *surface derivative operator* since it subtracts from the gradient operator the projection onto the local normal, thus leaving a gradient operator just in the tangent plane of the surface. The area evolution equation (13.58) can thus be written in the tidy form

$$\frac{1}{\delta S} \frac{D\delta S}{Dt} = \nabla^{\text{surf}} \cdot \mathbf{v}, \quad (13.60)$$

so that the relative area of the material surface changes according to the surface divergence of the velocity field.

#### Special case of a horizontal surface

To help understand the kinematic equation (13.60), consider the special case of a horizontal surface with a vertical normal vector,  $\hat{n} = \hat{z}$ , so that

$$\frac{1}{\delta S} \frac{D\delta S}{Dt} = \nabla \cdot \mathbf{v} - \hat{z} \cdot \partial_z \mathbf{v} = \nabla_z \cdot \mathbf{u}. \quad (13.61)$$

In this case we see that the area of a horizontal surface increases when the horizontal velocity diverges, and the area decreases when the velocity converges. We expect this behavior since the

surface is material and thus is moving with the flow. We encounter this result again in Section 13.4.4 for two-dimensional flow, in which the area is always horizontal.

As another special case, consider a three dimensional flow that is non-divergent,  $\nabla \cdot \mathbf{v} = 0$  (see Chapter 16). In this case the area changes are only due to the projection of the normal gradient onto the normal direction. So again considering a horizontal area with  $\hat{\mathbf{n}} = \hat{\mathbf{z}}$ , the area evolution in a non-divergent flow is given by

$$\frac{1}{\delta S} \frac{D\delta S}{Dt} = -\hat{\mathbf{z}} \cdot (\hat{\mathbf{z}} \cdot \nabla) \mathbf{v} = -\partial_z w, \quad (13.62)$$

which follows from equation (13.61) with  $\nabla_x u + \partial_y v + \partial_z w = \nabla_z \mathbf{u} + \partial_z w = 0$ .

### 13.4.3 Evolution of the normal vector

We make use of the area evolution equation (13.60) within equation (13.55) to derive an evolution equation for the normal vector

$$\frac{D\hat{\mathbf{n}}_m}{Dt} = -\hat{\mathbf{n}}_m \frac{1}{\delta S} \frac{D\delta S}{Dt} + (\partial_p v_p) \hat{\mathbf{n}}_m - (\partial_m v_p) \hat{\mathbf{n}}_p \quad (13.63a)$$

$$= -\hat{\mathbf{n}}_m [\partial_p v_p - \hat{\mathbf{n}}_p (\hat{\mathbf{n}}_q \partial_q) v_p] + (\partial_p v_p) \hat{\mathbf{n}}_m - (\partial_m v_p) \hat{\mathbf{n}}_p \quad (13.63b)$$

$$= -\hat{\mathbf{n}}_p [\partial_m - \hat{\mathbf{n}}_m \hat{\mathbf{n}}_q \partial_q] v_p \quad (13.63c)$$

$$= -\hat{\mathbf{n}}_p \partial_m^{\text{surf}} v_p \quad (13.63d)$$

$$= -\hat{\mathbf{n}} \cdot \partial_m^{\text{surf}} \mathbf{v}. \quad (13.63e)$$

We can readily verify that this expression satisfies the kinematic constraint (13.57) in which  $\hat{\mathbf{n}} \cdot D\hat{\mathbf{n}}/Dt = 0$ .

To help understand the evolution equation (13.63e) consider again a horizontal area with its normal vector initially in the vertical direction. The evolution of this normal vector is thus given by

$$\frac{D\hat{\mathbf{n}}_m}{Dt} = -(\partial_m - \hat{\mathbf{z}}_m \partial_z) w, \quad (13.64)$$

with each component evolving according to

$$\frac{D\hat{n}_1}{Dt} = -\partial_x w \quad (13.65a)$$

$$\frac{D\hat{n}_2}{Dt} = -\partial_y w \quad (13.65b)$$

$$\frac{D\hat{n}_3}{Dt} = 0. \quad (13.65c)$$

Hence, an initially vertical normal vector tilts into the horizontal direction according to minus the horizontal shear in the vertical velocity. We understand this result by noting that such a shear creates undulations in the initially horizontal surface that render a horizontal component to the normal vector (Figure 13.4).

### 13.4.4 Material area in two-dimensional flow

Now consider a material area for two-dimensional fluid flow with velocity,  $\mathbf{v} = (u, v, 0)$ , and  $\delta \mathbf{A} = \hat{\mathbf{x}} \delta x$ ,  $\delta \mathbf{B} = \hat{\mathbf{y}} \delta y$ , with zero dependence on  $z$ . In this case, the area of an infinitesimal material region is

$$\delta S = (\delta \mathbf{A} \times \delta \mathbf{B}) \cdot \hat{\mathbf{z}} = \delta x \delta y, \quad (13.66)$$

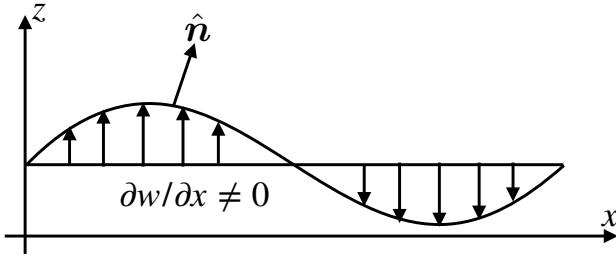


FIGURE 13.4: Horizontal shear in the vertical velocity,  $\nabla_z w$ , creates undulations in an initially horizontal material surface that leads to a horizontal component in the normal vector. We here show the case where  $\partial w / \partial x \neq 0$ , thus leading to a zonal component to the normal vector according to  $D\hat{n}_x/Dt = -\partial_x w$ .

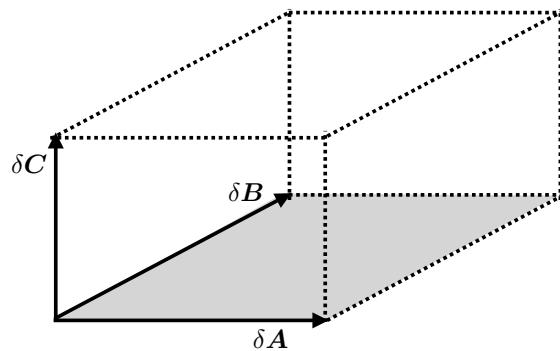


FIGURE 13.5: A parallelepiped defined by three material lines with volume (to within a sign) given by  $\delta V = (\delta\mathbf{A} \times \delta\mathbf{B}) \cdot \delta\mathbf{C}$ . See also the discussion surrounding Figure 1.4.

and its evolution is given by

$$\frac{D(\delta\mathcal{S})}{Dt} = (\delta\mathbf{B} \times \hat{\mathbf{z}}) \cdot (\delta\mathbf{A} \cdot \nabla) \mathbf{u} + (\hat{\mathbf{z}} \times \delta\mathbf{A}) \cdot (\delta\mathbf{B} \cdot \nabla) \mathbf{u} \quad (13.67a)$$

$$= \delta x \delta y \nabla \cdot \mathbf{u}, \quad (13.67b)$$

so that

$$\frac{1}{\delta\mathcal{S}} \frac{D(\delta\mathcal{S})}{Dt} = \nabla \cdot \mathbf{u}. \quad (13.68)$$

Hence, the area of the material region evolves according to the divergence of the horizontal velocity. Correspondingly, the area remains constant in a horizontally non-divergent flow. This result follows from specializing the three-dimensional result (13.52f) to the case of two-dimensional flow by assuming no dependence on the vertical direction.

## 13.5 Volume and the Jacobian of transformation

The mass of a material parcel is constant. However, the volume is not generally constant since the fluid density is not generally uniform. We here derive the expression for how volume evolves for a material parcel. We also derive the material evolution equation for the Jacobian of transformation between position space and material space. We will see that the relative change for both the parcel volume and the Jacobian are determined by the divergence of the velocity field.

### 13.5.1 Material parcel volume

Consider a material region with a volume  $\delta V$  spanned by the infinitesimal material lines  $\delta \mathbf{A}$ ,  $\delta \mathbf{B}$ , and  $\delta \mathbf{C}$  (see Figure 13.5). To within a sign the volume is given by

$$\delta V = (\delta \mathbf{A} \times \delta \mathbf{B}) \cdot \delta \mathbf{C}. \quad (13.69)$$

Making use of the material line evolution equation (13.19) renders

$$\frac{D(\delta V)}{Dt} = (\delta \mathbf{B} \times \delta \mathbf{C}) \cdot (\delta \mathbf{A} \cdot \nabla) \mathbf{v} + (\delta \mathbf{C} \times \delta \mathbf{A}) \cdot (\delta \mathbf{B} \cdot \nabla) \mathbf{v} + (\delta \mathbf{A} \times \delta \mathbf{B}) \cdot (\delta \mathbf{C} \cdot \nabla) \mathbf{v}. \quad (13.70)$$

Now specialize to the case where the parcel is a parallelepiped oriented according to the coordinate axes

$$\delta \mathbf{A} = \hat{\mathbf{x}} \delta x \quad \text{and} \quad \delta \mathbf{B} = \hat{\mathbf{y}} \delta y \quad \text{and} \quad \delta \mathbf{C} = \hat{\mathbf{z}} \delta z, \quad (13.71)$$

so that

$$\delta V = \delta x \delta y \delta z. \quad (13.72)$$

Plugging into equation (13.70) leads to

$$\frac{1}{\delta V} \frac{D(\delta V)}{Dt} = \nabla \cdot \mathbf{v}. \quad (13.73)$$

This result is a three-dimensional generalization of the material area equation derived in Section 13.4.4.

We offer an alternative derivation of equation (13.73) in Section 14.2, where no assumptions are made concerning the shape of the material region. That derivation leads us to conclude that the relative volume of a material parcel increases when the parcel moves through a region where the velocity diverges ( $\nabla \cdot \mathbf{v} > 0$ ). We think of a diverging velocity field as “spreading out” the material parcel boundary, thus increasing its volume. In contrast, the volume of a material parcel decreases where the fluid velocity converges ( $\nabla \cdot \mathbf{v} < 0$ )

$$\nabla \cdot \mathbf{v} > 0 \Rightarrow \text{material volume increases in diverging flow} \Rightarrow \text{parcel expands} \quad (13.74a)$$

$$\nabla \cdot \mathbf{v} < 0 \Rightarrow \text{material volume decreases in converging flow} \Rightarrow \text{parcel contracts.} \quad (13.74b)$$

### 13.5.2 Evolution of the Jacobian of transformation

Recall the discussion in Section 12.4.6, where we showed that the Jacobian of transformation between material space ( $\mathbf{a}$ -space) and position space ( $\mathbf{x}$ -space) is related to the ratio of the volume elements written in the two coordinate systems. In particular, equation (12.22) is given by

$$\delta V(\mathbf{x}) = \frac{\partial \mathbf{X}}{\partial \mathbf{a}} \delta V(\mathbf{a}) \Rightarrow \frac{\partial \mathbf{X}}{\partial \mathbf{a}} = \frac{\delta V(\mathbf{x})}{\delta V(\mathbf{a})}. \quad (13.75)$$

The material coordinate volume  $\delta V(\mathbf{a})$  is time independent when following the flow. Consequently, the material evolution of the Jacobian is given by

$$\frac{D}{Dt} \frac{\partial \mathbf{X}}{\partial \mathbf{a}} = \frac{1}{\delta V(\mathbf{a})} \frac{D(\delta V(\mathbf{x}))}{Dt} \quad (13.76a)$$

$$= \frac{\delta V(\mathbf{x})}{\delta V(\mathbf{a})} \nabla \cdot \mathbf{v} \quad (13.76b)$$

$$= \frac{\partial \mathbf{X}}{\partial \mathbf{a}} \nabla \cdot \mathbf{v}. \quad (13.76c)$$

The second equality made use of the equation (13.73), which expresses the material time change for the volume of a material fluid parcel, as measured in position space, in terms of the velocity divergence. We thus see that the relative change of the Jacobian is determined by the divergence of the velocity

$$\left[ \frac{\partial \mathbf{X}}{\partial \mathbf{a}} \right]^{-1} \frac{D}{Dt} \left[ \frac{\partial \mathbf{X}}{\partial \mathbf{a}} \right] = \nabla \cdot \mathbf{v}. \quad (13.77)$$

This equation is identical to the parcel volume equation (13.73), which is expected given the relation between the Jacobian and the parcel volume. In Exercise 13.5, we derive this result using the explicit expression for the Jacobian in terms of the permutation symbol  $\epsilon$ .

## 13.6 Kinematics of two-dimensional flow

In this section we consider the rudiments of two-dimensional flow as a venue to illustrate certain topics presented earlier in this chapter such as dilation, rotation, and strains. In so doing we expose kinematic properties commonly used to characterize two-dimensional flow, with generalizations to three-dimensions available with a bit more mathematics.

Our starting point is Figure 13.6, which shows a square region of fluid exposed to a variety of flow regimes. We can kinematically describe these changes by making use of the velocity gradient tensor introduced in Section 13.3.5, here written for the two-dimensional flow with horizontal velocity components,  $(u, v)$

$$\frac{\partial v_m}{\partial x_n} = \begin{bmatrix} \partial u / \partial x & \partial u / \partial y \\ \partial v / \partial x & \partial v / \partial y \end{bmatrix} \quad (13.78a)$$

$$= \begin{bmatrix} \partial u / \partial x & (1/2)(\partial u / \partial y + \partial v / \partial x) \\ (1/2)(\partial u / \partial y + \partial v / \partial x) & \partial v / \partial y \end{bmatrix} + \frac{\zeta}{2} \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \quad (13.78b)$$

$$= \mathbb{S}_{mn} + \mathbb{R}_{mn}, \quad (13.78c)$$

where

$$\zeta = \hat{\mathbf{z}} \cdot \nabla \times \mathbf{v} = \partial v / \partial x - \partial u / \partial y \quad (13.79)$$

is the vertical component to the vorticity.

### 13.6.1 Diverging flow

Recall from Section 13.4.4 that a material surface in two-dimensional flow changes its area according to the divergence. The upper left panel of Figure 13.6 thus illustrates equation (13.68)

$$\frac{1}{\delta \mathcal{S}} \frac{D(\delta \mathcal{S})}{Dt} = \nabla \cdot \mathbf{u} = \mathbb{S}_{mm}, \quad (13.80)$$

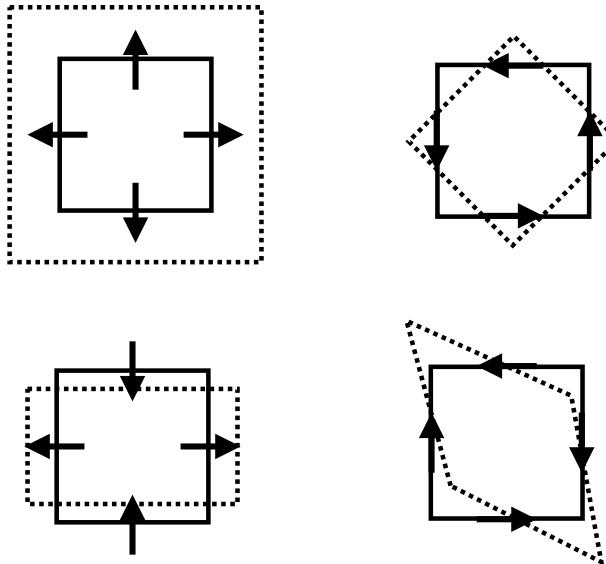


FIGURE 13.6: Illustrating the varieties of shape changes for a square material fluid region. Upper left: purely divergent flow, whereby  $\nabla \cdot \mathbf{u} > 0$  yet with zero vorticity, thus leading to a uniform increase in the area. Upper right: rotational flow with nonzero vorticity,  $\zeta = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u})$ , yet zero divergence, thus leading to a pure rotation of the square patch. Lower left: result of a pure tension/compression straining flow with zero divergence and zero vorticity, leading to compression in one direction and dilation in the orthogonal direction. This flow is realized by the velocity field  $\mathbf{u} = \hat{\mathbf{z}} \times \nabla \psi$ , which is generated by the streamfunction  $\psi = -\gamma xy$ . Lower right: pure shearing strain flow with zero divergence and zero vorticity, as as realized by the flow  $\mathbf{u} = \hat{\mathbf{z}} \times \nabla \psi$  generated by the streamfunction  $\psi = -(\gamma/2)(x^2 - y^2)$ . This figure is adapted from Figure 2.4 of [Hoskins and James \(2014\)](#).

where  $\delta\mathcal{S}$  is the area and  $\mathbb{S}_{mm}$  is the trace of the rate of strain tensor. That is, a diverging flow as depicted by this figure, with  $\nabla \cdot \mathbf{u} > 0$ , leads to an expansion of the area. The opposite occurs for a converging flow, where the area compresses.

### 13.6.2 Rotational flow with nonzero vorticity

The upper right panel of Figure 13.6 illustrates the effects from a flow with a non-zero vorticity  $\zeta = \partial v / \partial x - \partial u / \partial y$ , or a nonzero circulation. We provide extensive discussion of vorticity and circulation in Part VI of this book. For now we remain satisfied by noting that vorticity measures the spin at a point within a fluid. The nonzero spin imparts a rotation to an area element, in this case bringing about a counter-clockwise rotation. All components of the strain tensor vanish for a purely rotational flow, so that there is no deformation of the square as it rotates.

### 13.6.3 Flow with nonzero deformation

The lower left panel of Figure 13.6 shows the square within a deformational flow whereby it contracts along the  $y$ -axis and dilates along the  $x$ -axis. This flow is non-divergent,  $\nabla \cdot \mathbf{u} = 0$ , and has zero vorticity,  $\zeta = 0$ , so that the area remains constant and the orientation is fixed. However, it has shear that acts to deform the area. This particular non-divergent deformational flow is determined by

$$\mathbf{u} = \hat{\mathbf{z}} \times \nabla \psi, \quad (13.81)$$

with the streamfunction,  $\psi = -\gamma xy$  where  $\gamma$  is a constant inverse time scale and hence the strength of the strain. The resulting velocity components are  $u = -\partial \psi / \partial y = \gamma x$  and  $v = \partial \psi / \partial x = -\gamma y$ .

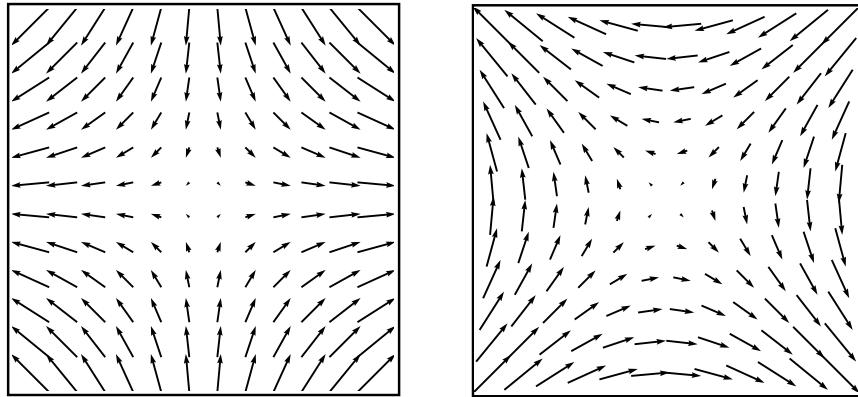


FIGURE 13.7: Two-dimensional non-divergent and irrotational flow with nonzero deformation/strain. Left panel: pure tension strain as determined by the streamfunction,  $\psi = -\gamma xy$ , so that the velocity components are  $u = -\partial\psi/\partial y = \gamma x$  and  $v = \partial\psi/\partial x = -\gamma y$ . The vertical axis orients the direction along which flow contracts (compression) whereas the horizontal axis is the dilation axis (tension). Right panel: pure shearing flow as determined by the streamfunction  $\psi = -(\gamma/2)(x^2 - y^2)$  so that the velocity components are  $u = -\gamma y$  and  $v = -\gamma x$ . We set  $\gamma = 1$  for both examples.

There are two combinations of the rate of strain tensor elements that are useful in describing deformational flows:

$$\text{tension strain} = S_T = \mathbb{S}_{11} - \mathbb{S}_{22} = \partial u / \partial x - \partial v / \partial y \quad (13.82a)$$

$$\text{shearing strain} = S_S = 2 \mathbb{S}_{12} = \partial u / \partial y + \partial v / \partial x. \quad (13.82b)$$

The tension strain and shearing strain are also known as tension and shearing *deformation rates*. Note that negative tension is known as *compression*. For the deformation flow with streamfunction  $\psi = -\gamma xy$ , we have

$$S_T = 2\gamma \quad \text{and} \quad S_S = 0, \quad (13.83)$$

so that this velocity leads to a purely tension straining flow. In contrast, the following non-divergent irrotational flow is a purely shearing strain flow

$$\psi = -(\gamma/2)(x^2 - y^2) \quad u = -\gamma y \quad v = -\gamma x \quad S_T = 0 \quad S_S = -2\gamma, \quad (13.84)$$

as depicted by the right panel of Figure 13.7. This pure shearing flow leads to the deformation of the fluid square shown in the lower right panel of Figure 13.6.

#### 13.6.4 Further study

Elements of this section can be found in Section 2.3 of [Hoskins and James \(2014\)](#). More detailed examinations of two-dimensional flow kinematics are offered by [Weiss \(1991\)](#) and [Lilly \(2018\)](#).

## 13.7 Exercises

### EXERCISE 13.1: MATERIAL EVOLUTION OF THE ACCELERATION DIVERGENCE

This exercise is based on problem 10(a) from Section 3.1 of [Segel \(1987\)](#). Here, we derive the relation

$$\nabla \cdot \frac{D\mathbf{v}}{Dt} = \frac{D(\nabla \cdot \mathbf{v})}{Dt} + \mathcal{S}^2 - \mathcal{A}^2, \quad (13.85)$$

where  $\mathcal{S}^2 = \mathcal{S}_{mn}\mathcal{S}_{mn}$  and  $\mathcal{A}^2 = \mathcal{A}_{mn}\mathcal{A}_{mn}$  are the squared rate of strain and squared rotation tensors (Sections 13.3.7 and 13.3.8). Make use of Cartesian tensors for your solution.

**EXERCISE 13.2: VELOCITY FIELD WITH ZERO STRAIN** (*Aris (1962)* EXERCISE 4.41.1)

If the rate of strain tensor vanishes, show that the velocity field can be written

$$\mathbf{v} = \mathbf{U} + \boldsymbol{\Omega} \times \mathbf{x}, \quad (13.86)$$

where  $\boldsymbol{\Omega}$  is a constant angular rotation rate and  $\mathbf{U}$  is a constant velocity. That is, a fluid velocity equal to a constant rotation plus translation renders zero strain. Hint: if  $\mathcal{S}_{mn} = 0$ , what does that imply about the velocity field? You may also wish to make use of the general decomposition (13.48).

**EXERCISE 13.3: RATE OF STRAIN AND ROTATION TENSORS** (*Aris (1962)* EXERCISE 4.43.3)

Consider a two-dimensional flow with horizontal velocity

$$\mathbf{u} = (f/r)(\hat{\mathbf{x}}y - \hat{\mathbf{y}}x), \quad (13.87)$$

where  $f = f(r)$  is an arbitrary function of the radial distance  $r = \sqrt{x^2 + y^2}$ . Note:  $f$  is here *not* the Coriolis parameter found elsewhere in this book, but it is instead just an arbitrary function of the radial distance.

- (a) Show that the velocity field is non-divergent.
- (b) Determine the streamlines.
- (c) Determine the elements to the rate of strain tensor,  $\mathbb{S}$ , given by equation (13.78c). Write the expression using polar coordinates  $x = r \cos \varphi$  and  $y = r \sin \varphi$  (see Section 8.3) and the structure function  $F(r) = [f' - f/r]/2$ , where  $f' = df/dr$ .
- (d) Determine elements to the rotation tensor,  $\mathbb{R}$ , given by equation (13.78c), also written in polar coordinates.

**EXERCISE 13.4: RATE OF STRAIN AND ROTATION FOR PARALLEL SHEAR FLOW**

Consider a two-dimensional parallel shear flow with horizontal velocity

$$\mathbf{u} = a x \hat{\mathbf{y}}, \quad (13.88)$$

where  $a$  is a constant with dimension inverse time.

- (a) Compute the rate of strain tensor,  $\mathbb{S}$  (equation (13.78c)) for this velocity field.
- (b) Compute the rotation tensor,  $\mathbb{R}$  (equation (13.78c)) for this velocity field.
- (c) Decompose the velocity field according to equation (13.48), and show that each of the velocity components is non-divergent. That is, write

$$\mathbf{u} = \mathbf{u}^0 + \mathbf{u}^{(S)} + \mathbf{u}^{(A)} \quad \text{with} \quad \nabla \cdot \mathbf{u}^{(S)} = \nabla \cdot \mathbf{u}^{(A)} = 0, \quad (13.89)$$

with  $u_m^0$  the velocity at the point where  $\delta x_m = x_m - x_m^0 = 0$ . The velocity  $\mathbf{u}^{(S)}$  has a constant strain but no vorticity whereas  $\mathbf{u}^{(A)}$  has a constant vorticity but no strain. Hint: both  $\mathbf{u}^{(S)}$  and  $\mathbf{u}^{(A)}$  have nonzero  $\hat{\mathbf{x}}$  and  $\hat{\mathbf{y}}$  components.

- (d) Determine the streamfunctions for  $\mathbf{u}^{(S)}$  and  $\mathbf{u}^{(A)}$ .

- (e) Sketch the velocity vectors  $\mathbf{u}^{(S)}$  and  $\mathbf{u}^{(A)}$ .

EXERCISE 13.5: EVOLUTION OF THE JACOBIAN USING  $\epsilon$ -TENSOR GYMNASTICS

There is another way to derive the identity (13.77) for the evolution of the Jacobian. This other method is somewhat more tedious. However, it exercises some useful methods of index gymnastics involving the  $\epsilon$ -tensor. It also has a natural generalization to curved spaces. This exercise is only for aficionados of tensor analysis.

An explicit expression for the Jacobian of transformation is given by

$$\frac{\partial \mathbf{X}}{\partial \mathbf{a}} = \frac{1}{3!} \epsilon_{mnp} \epsilon_{ijk} \frac{\partial X_m}{\partial a_i} \frac{\partial X_n}{\partial a_j} \frac{\partial X_p}{\partial a_k}. \quad (13.90)$$

Take the material derivative of this expression and show that we get the same expression as equation (13.77). Hint: make use of the identity

$$\frac{D}{Dt} \frac{\partial X_m}{\partial a_i} = \frac{\partial V_m}{\partial a_i}, \quad (13.91)$$

which holds since the material time derivative is taken with the material coordinates,  $\mathbf{a}$ , held fixed.



# Chapter 14

## Mass conservation

We assume that mass is neither created nor destroyed within the fluid domain. Since this assumption holds independently of the forces acting on the fluid, mass conservation is a topic within fluid kinematics. In this chapter, we derive the mathematical expressions for mass conservation in a homogeneous fluid and the associated kinematic constraints placed on fluid motion. These constraints are examined both in the interior of the fluid as well as at fluid boundaries.

### READER'S GUIDE TO THIS CHAPTER

In this chapter we are concerned with homogeneous fluids, with generalizations to multiple-component fluids given in Chapter 15. Spatial positions and trajectories are represented using Cartesian coordinates to simplify the maths, with generalizations following the tensor analysis methods of Chapter 7. We build on our understanding of the Eulerian and Lagrangian kinematic descriptions developed in Chapters 12 and 13.

14.1	Eulerian fluid regions . . . . .	<b>290</b>
14.1.1	Finite volume expression . . . . .	290
14.1.2	Arbitrary Eulerian region . . . . .	291
14.2	Material fluid parcels . . . . .	<b>292</b>
14.2.1	Lagrangian expression for mass conservation . . . . .	292
14.2.2	Alternative derivation based on the Jacobian . . . . .	293
14.2.3	Summary of material kinematic equations . . . . .	293
14.3	Material fluid regions . . . . .	<b>293</b>
14.3.1	Evolution of volume . . . . .	294
14.3.2	Mass conservation . . . . .	294
14.3.3	Mass conservation using Lagrangian methods . . . . .	295
14.3.4	Reynolds transport theorem . . . . .	296
14.3.5	Comments on notation for the time derivative . . . . .	297
14.4	Kinematic boundary conditions . . . . .	<b>298</b>
14.4.1	Static material surface . . . . .	298
14.4.2	Moving material surface . . . . .	299
14.4.3	Dynamic and permeable surface . . . . .	302
14.5	Volume and mass budgets for an ocean column . . . . .	<b>306</b>
14.5.1	Kinematic free surface equation . . . . .	306
14.5.2	Budget for mass per horizontal area . . . . .	307
14.6	Exercises . . . . .	<b>308</b>

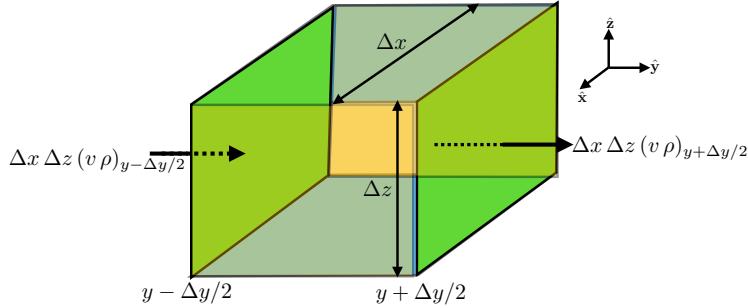


FIGURE 14.1: A finite sized cube (also known as a cell) of fixed dimensions and position (an Eulerian region) used to formulate the Eulerian form of mass conservation. We highlight two cell faces with area  $\Delta x \Delta z$  and with meridional mass transport crossing the faces given by  $\Delta x \Delta z (v \rho)_{y-\Delta y/2}$  and  $\Delta x \Delta z (v \rho)_{y+\Delta y/2}$ . To establish signs we assume the meridional velocity is positive,  $v > 0$ , so that mass enters the face at  $y - \Delta y/2$  and leaves the face at  $y + \Delta y/2$ . Differences between these two transports leads to an accumulation of mass within the cell. Note that the resulting mass budget holds regardless the direction of the flow velocity.

## 14.1 Eulerian fluid regions

We here develop expressions for the mass budget within an Eulerian region, both infinitesimal and finite. Recall that Eulerian regions are fixed in space and thus have constant volumes.

### 14.1.1 Finite volume expression

Consider a finite sized cube region that is fixed in space; i.e., an Eulerian region such as shown in Figure 14.1. The mass contained within the cube is given by

$$\Delta M = \rho \Delta V = \rho \Delta x \Delta y \Delta z, \quad (14.1)$$

where the cube volume,

$$\Delta V = \Delta x \Delta y \Delta z, \quad (14.2)$$

is constant in time. As we will be taking the limit as the size of the cube gets smaller, it is sufficient to approximate the density as that at the cube center,  $\rho = \rho(x, y, z, t)$ . In the absence of mass sources within the fluid, the mass within the cube changes only through the transport of mass across the six cube faces.

Focusing on the mass transported in the meridional direction as illustrated in Figure 14.1, the accumulation of mass within the cube through this transport is determined by the difference in mass transport crossing the two adjacent cell faces

$$\text{mass change from meridional transport} = (\Delta x \Delta z) [(v \rho)_{y-\Delta y/2} - (v \rho)_{y+\Delta y/2}]. \quad (14.3)$$

Expanding the difference into a Taylor series leads to

$$\text{mass change from meridional transport} \approx -(\Delta x \Delta y \Delta z) \frac{\partial(v \rho)}{\partial y}. \quad (14.4)$$

The same analysis for the zonal and vertical directions leads to the mass budget for the cube

$$\frac{\partial(\rho \Delta V)}{\partial t} = -\Delta V \left[ \frac{\partial(u \rho)}{\partial x} + \frac{\partial(v \rho)}{\partial y} + \frac{\partial(w \rho)}{\partial z} \right]. \quad (14.5)$$

Hence, the cube mass changes according to the convergence of mass across the cube boundaries.

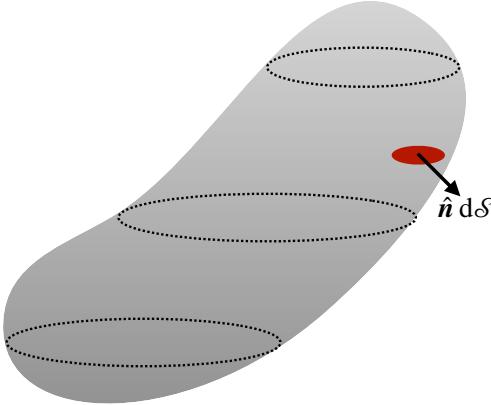


FIGURE 14.2: An arbitrarily shaped simply closed region,  $\mathcal{R}$ , within the fluid. If the region is fixed in space, then it represents a general Eulerian region for considering mass budgets. A surface area element,  $d\mathcal{S}$ , is oriented according to the outward normal,  $\hat{\mathbf{n}}$ .

Cancelling the constant volume  $\Delta V$  (again, the volume is assumed fixed as per an Eulerian region) renders the *flux-form* Eulerian mass continuity equation

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0. \quad (14.6)$$

The mass continuity equation (14.6) is in the form of a *flux-form conservation law*, in which the local time tendency of a field is determined by the convergence of a flux

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot (\rho \mathbf{v}). \quad (14.7)$$

The *mass flux*,  $\rho \mathbf{v}$ , with dimensions  $M L^{-2} T^{-1}$ , measures the mass per time of matter crossing a unit area oriented with an outward normal in each of the three Cartesian directions. If more mass flux comes into a point than leaves, then the density increases (mass converges), and vice versa for a mass flux that diverges from a point. It is notable that the mass flux also serves as a measure of the *momentum flux*, which we discuss in Chapter 17.

### 14.1.2 Arbitrary Eulerian region

The discussion for the infinitesimal cube can be generalized by making use of the divergence theorem. For that purpose, consider an arbitrary static and simply closed region within the fluid such as in Figure 14.2. Integrating the continuity equation (14.6) over that region leads to

$$\int_{\mathcal{R}} \frac{\partial \rho}{\partial t} dV = - \int_{\mathcal{R}} \nabla \cdot (\rho \mathbf{v}) dV. \quad (14.8)$$

Since the region is static we can move the partial time derivative outside on the left hand side. Furthermore, the divergence theorem can be applied to the right hand side to convert the volume integral to a surface integral over the boundaries of the static domain. The resulting mass budget is given by

$$\frac{d}{dt} \int_{\mathcal{R}} \rho dV = - \oint_{\partial \mathcal{R}} \rho \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (14.9)$$

where  $\hat{\mathbf{n}}$  is the outward normal vector along the closed boundary of the region, and  $d\mathcal{S}$  is the surface area element along that boundary. This equation says that the mass within a fixed region

of the fluid changes in time (left hand side) according to the accumulation of mass crossing the region boundary (right hand side). The minus sign means that the mass decreases in the region if there is a flux of mass leaving the domain in the direction of the outward normal.

## 14.2 Material fluid parcels

We here derive the differential expressions for mass conservation of a constant mass fluid parcel within a Lagrangian reference frame. The differential expressions for volume and density arise as a corollary. This discussion complements the Eulerian discussion from Section 14.1. To motivate the derivations we expand the Eulerian flux-form mass continuity equation (14.6) to have

$$\frac{1}{\rho} \frac{D\rho}{Dt} = -\nabla \cdot \mathbf{v}, \quad (14.10)$$

where  $D/Dt = \partial_t + \mathbf{v} \cdot \nabla$  is the material time derivative operator. We now derive this form of the mass continuity using Lagrangian methods.

### 14.2.1 Lagrangian expression for mass conservation

The mass of an infinitesimal fluid parcel is written

$$\delta M = \rho \delta V, \quad (14.11)$$

where  $\delta V$  is the volume and

$$\rho = \frac{\delta M}{\delta V} \quad (14.12)$$

is the mass density of the parcel. By definition, the fluid parcel has a constant mass so that its material time derivative vanishes

$$\frac{D(\delta M)}{Dt} = 0. \quad (14.13)$$

Equation (14.13) is the most basic form of mass conservation for a material parcel. However, one often has need to express this result in terms of parcel density and parcel volume

$$\frac{D(\delta M)}{Dt} = \frac{D(\rho \delta V)}{Dt} \quad (14.14a)$$

$$= \delta M \left[ \frac{1}{\rho} \frac{D\rho}{Dt} + \frac{1}{\delta V} \frac{D(\delta V)}{Dt} \right]. \quad (14.14b)$$

Comparing to the mass continuity equation (14.10) leads to<sup>1</sup>

$$\frac{1}{\delta M} \frac{D(\delta M)}{Dt} = \frac{1}{\rho} \frac{D\rho}{Dt} + \nabla \cdot \mathbf{v}. \quad (14.15)$$

Setting  $D(\delta M)/Dt = 0$  renders the continuity equation (14.10) derived from the Eulerian expression

$$\frac{1}{\rho} \frac{D\rho}{Dt} = -\nabla \cdot \mathbf{v}. \quad (14.16)$$

The parcel volume contracts in regions where the velocity converges (we prove that property in Sections 13.5.1 and 14.3.1). The continuity equation (14.16) then says that regions of volume

---

<sup>1</sup>In Section 13.5.1 we derived the material evolution of volume, and will again see this result in equation (14.26).

contraction are where the parcel density increases whereas the opposite occurs for regions where the velocity diverges.

### 14.2.2 Alternative derivation based on the Jacobian

An alternative approach to deriving the mass conservation equation makes use of the material time evolution of the Jacobian. We detail this approach for integrals in Section 14.3.3, and discussed it for fluid parcels in Section 13.5.2. Making use of those results, in particular equation (13.77), allows us to write the material evolution for the fluid parcel mass in the form

$$\frac{D}{Dt} [\rho \delta V(\mathbf{x})] = \frac{D}{Dt} \left[ \rho \frac{\partial \mathbf{X}}{\partial \mathbf{a}} \delta V(\mathbf{a}) \right] \quad (14.17a)$$

$$= \left[ \frac{D\rho}{Dt} + \rho \nabla \cdot \mathbf{v} \right] \left[ \frac{\partial \mathbf{X}}{\partial \mathbf{a}} \right] \delta V(\mathbf{a}) \quad (14.17b)$$

$$= \left[ \frac{D\rho}{Dt} + \rho \nabla \cdot \mathbf{v} \right] \delta V(\mathbf{x}). \quad (14.17c)$$

We recover the mass conservation equation (14.16) when noting that the mass of a material parcel is constant so that  $D\rho/Dt = -\rho \nabla \cdot \mathbf{v}$ .

### 14.2.3 Summary of material kinematic equations

Let us now summarize the variety of differential evolution equations for mass, volume, and density as viewed from a material reference frame

$$\frac{D(\delta M)}{Dt} = 0 \quad \text{parcel mass is constant} \quad (14.18)$$

$$\frac{1}{\delta V} \frac{D(\delta V)}{Dt} = \nabla \cdot \mathbf{v} \quad \text{parcel volume increases in divergent flow} \quad (14.19)$$

$$\frac{1}{\rho} \frac{D\rho}{Dt} = -\nabla \cdot \mathbf{v} \quad \text{parcel density increases in convergent flow.} \quad (14.20)$$

To help remember the signs on the right hand side, recall that as the fluid diverges from a point ( $\nabla \cdot \mathbf{v} > 0$ ), it expands the boundaries of the material parcel and so increases the parcel volume as per equation (14.19). Since the parcel has a fixed mass, the diverging velocity field causes the material parcel density to decrease ( $-\nabla \cdot \mathbf{v} < 0$ ) as per equation (14.20).

## 14.3 Material fluid regions

We now extend the kinematics of material fluid parcels in Section 14.2 to finite sized material fluid regions. Just as for material fluid parcels, the finite sized material fluid region retains the same matter content, and thus maintains a constant mass. We contrast the discussion here with that for the Eulerian regions (fixed in space) considered in Section 14.1. One key operational distinction between the Eulerian and material domains is that partial time derivative operators commute with integration over a fixed Eulerian domain, whereas material time derivative operators commute with integration over a material domain as per Reynolds transport theorem derived in Section 14.3.4.

### 14.3.1 Evolution of volume

Consider a finite material region,  $\mathcal{R}(\mathbf{v})$ , whose volume is given by the integral

$$V = \int_{\mathcal{R}(\mathbf{v})} dV, \quad (14.21)$$

with  $dV$  the volume element. The region changes its shape according to the motion of the fluid particles fixed to the boundary of the material region. We designate this volume as

$$\mathcal{R}(\mathbf{v}) = \text{region following flow}, \quad (14.22)$$

with the  $\mathbf{v}$  argument emphasizing that the volume moves with the flow. The material region expands when the flow moves outward and contracts when the flow moves inward. These statements take on the following mathematical expression

$$\frac{d}{dt} \int_{\mathcal{R}(\mathbf{v})} dV = \oint_{\partial\mathcal{R}(\mathbf{v})} \mathbf{v} \cdot \hat{\mathbf{n}} dS, \quad (14.23)$$

where  $\hat{\mathbf{n}}$  is the outward normal on the region's closed boundary,  $dS$  is the area element on the boundary, and

$$\mathbf{v} \cdot \hat{\mathbf{n}} dS = \text{volume transport (volume per time) at the boundary } \partial\mathcal{R}. \quad (14.24)$$

Use of the divergence theorem then leads to the equivalent expression

$$\frac{d}{dt} \int_{\mathcal{R}(\mathbf{v})} dV = \int_{\mathcal{R}(\mathbf{v})} \nabla \cdot \mathbf{v} dV. \quad (14.25)$$

We now take the limit as the material region becomes a material parcel, in which case we recover the differential expression

$$\frac{1}{\delta V} \frac{D(\delta V)}{Dt} = \nabla \cdot \mathbf{v}, \quad (14.26)$$

where we make use of  $D/Dt$  since the infinitesimal volume is moving with the fluid. This equation is also derived in Section 13.5.1 using different methods.

### 14.3.2 Mass conservation

The mass of fluid contained in a finite material region is given by

$$M = \int_{\mathcal{R}(\mathbf{v})} \rho dV. \quad (14.27)$$

As a material fluid region, it maintains a constant mass as it moves through the fluid

$$\frac{d}{dt} \int_{\mathcal{R}(\mathbf{v})} \rho dV = 0. \quad (14.28)$$

Just as for the volume in Section 14.3.1, taking the limit as the material region becomes infinitesimally small, the region mass conservation statement (14.28) becomes the parcel mass conservation statement (14.13)

$$\frac{D(\delta M)}{Dt} = \frac{D(\rho \delta V)}{Dt} = 0. \quad (14.29)$$

### 14.3.3 Mass conservation using Lagrangian methods

Rather than take the limit as the finite material region  $\mathcal{R}(\mathbf{v})$  becomes infinitesimal, we develop some formalism that specifies how to move the time derivative across an integral of the mass within a finite sized material region as in equation (14.28). As part of this discussion we introduce two coordinate representations of the mass within a material region. The first is the Cartesian  $\mathbf{x}$ -space representation

$$\int_{\mathcal{R}(\mathbf{v})} \rho dV = \int_{x_1(t)}^{x_2(t)} \int_{y_1(t)}^{y_2(t)} \int_{z_1(t)}^{z_2(t)} \rho dx dy dz \equiv \int_{\mathcal{R}[\mathbf{v}(\mathbf{x}, t)]} \rho dV(\mathbf{x}). \quad (14.30)$$

The first equality expresses the integral with bounds that are functions of time, with the time dependence needed since the material region is moving with the fluid. The second equality uses a notation that emphasizes the region bounds and volume element are moving with the fluid velocity,  $\mathbf{v}$ , as specified using the  $\mathbf{x}$ -space representation,  $\mathbf{v}(\mathbf{x}, t)$ .

An alternative representation of mass in a material fluid region makes use of  $\mathbf{a}$ -space material coordinates. For this representation we perform a coordinate transformation from the  $\mathbf{x}$ -space representation to the  $\mathbf{a}$ -space representation, with this coordinate transformation requiring the Jacobian of transformation. To capture the gist of this transformation let us consider the one-dimensional case in which

$$\int_{x_1(t)}^{x_2(t)} \rho dx = \int_{a[x_1(t)]}^{a[x_2(t)]} \rho \frac{\partial X}{\partial a} da = \int_{a_1}^{a_2} \rho \frac{\partial X}{\partial a} da. \quad (14.31)$$

The first equality introduced the Jacobian,  $\partial X / \partial a$ , for the one-dimensional coordinate transformation from  $x$ -space to  $a$ -space, with corresponding changes to the limits of integration. We are allowed to make this coordinate transformation since there is a 1-to-1 relation between the  $a$ -space and  $x$ -space representation of a material fluid parcel. The second equality wrote the integral bounds in terms of the material coordinate. Since we are considering a material region that follows fluid particles, the integral bounds have fixed material coordinate values,  $a[x_1(t)] = a_1$  and  $a[x_2(t)] = a_2$ . Generalizing to three dimensions then renders

$$\int_{\mathcal{R}[\mathbf{v}(\mathbf{x}, t)]} \rho dV(\mathbf{x}) = \int_{\mathcal{R}[\mathbf{v}(\mathbf{a})]} \rho \frac{\partial \mathbf{X}}{\partial \mathbf{a}} dV(\mathbf{a}). \quad (14.32)$$

Again, we distinguish the  $\mathbf{x}$  and  $\mathbf{a}$  arguments for the material region, with the  $\mathbf{x}$  representation also requiring a time argument whereas the material  $\mathbf{a}$  representation has no time dependence since it is attached to the moving fluid particles.

We now make use of the equality (14.32) to take the time derivative of the mass contained in the material region. Since the time derivative follows the material region, we can make use of the

material space coordinate representation as part of the manipulations

$$\frac{d}{dt} \left[ \int_{\mathcal{R}[\mathbf{v}(\mathbf{x},t)]} \rho dV(\mathbf{x}) \right] = \frac{d}{dt} \left[ \int_{\mathcal{R}[\mathbf{v}(\mathbf{a})]} \rho \frac{\partial \mathbf{X}}{\partial \mathbf{a}} dV(\mathbf{a}) \right] \quad (14.33a)$$

$$= \int_{\mathcal{R}[\mathbf{v}(\mathbf{a})]} \frac{D}{Dt} \left[ \rho \frac{\partial \mathbf{X}}{\partial \mathbf{a}} \right] dV(\mathbf{a}) \quad (14.33b)$$

$$= \int_{\mathcal{R}[\mathbf{v}(\mathbf{x},t)]} \left[ \frac{D\rho}{Dt} + \rho \nabla \cdot \mathbf{v} \right] dV(\mathbf{x}) \quad (14.33c)$$

$$= \int_{\mathcal{R}[\mathbf{v}(\mathbf{x},t)]} \left[ \frac{1}{\rho} \frac{D\rho}{Dt} + \nabla \cdot \mathbf{v} \right] \rho dV(\mathbf{x}), \quad (14.33d)$$

where we used equation (13.77) for the equality (14.33c). When expressing the integral bounds using  $\mathbf{a}$ -space coordinates, the integral bounds have no time dependence since they are fixed on fluid particles. We can thus move the time derivative inside of the integral sign to reach the second equality. Upon entering the integral the time derivative is written as a material time derivative,  $D/Dt$ , since it is a time derivative computed by following the fluid particles that define the material region. The third equality made use of equation (14.17c) and converted back to  $\mathbf{x}$ -space. As the material region  $\mathcal{R}$  has a materially constant mass, we recover the mass continuity equation (14.16) by setting the integrand in equation (14.33d) to zero.

#### 14.3.4 Reynolds transport theorem

On first encounter, the method from Section 14.3.3 that involves moving between Eulerian ( $\mathbf{x}$ -space) and Lagrangian ( $\mathbf{a}$ -space) representations is clumsy at best and a black box at worse. However, with some practice it becomes an elegant means to study the time evolution of fluid properties integrated over a material region. The method is formalized by the *Reynolds transport theorem* discussed in this section.

Manipulations leading to the mass conservation statement (14.33d) can be generalized by considering the material time derivative of a mass-weighted field  $\psi$  (e.g., a tracer concentration as in Section 15.1)

$$\frac{D(\psi \rho \delta V)}{Dt} = \frac{D\psi}{Dt} \rho \delta V + \psi \frac{D(\rho \delta V)}{Dt} \quad (14.34a)$$

$$= \rho \delta V \left[ \frac{D\psi}{Dt} + \frac{\psi}{\rho} \frac{D\rho}{Dt} + \psi \nabla \cdot \mathbf{v} \right] \quad (14.34b)$$

$$= \delta V \left[ \frac{\partial(\rho \psi)}{\partial t} + \nabla \cdot (\rho \psi \mathbf{v}) \right]. \quad (14.34c)$$

The first equality used the product rule, which holds for material time derivatives. Mass conservation means that the material derivative  $D(\rho \delta V)/Dt = 0$ . However, we choose to write mass conservation in the form of equation (14.17c), which allows us to introduce the flux-form Eulerian expression after replacing the material time derivative with its Eulerian form from equation

(12.29). Another, perhaps more direct means, to derive this result is to write

$$\rho \frac{D\psi}{Dt} = \rho \left[ \frac{\partial \psi}{\partial t} + \mathbf{v} \cdot \nabla \psi \right] \quad (14.35a)$$

$$= \rho \left[ \frac{\partial \psi}{\partial t} + \mathbf{v} \cdot \nabla \psi \right] + \psi \left[ \frac{\partial \rho}{\partial t} + \nabla \cdot (\mathbf{v} \rho) \right] \quad (14.35b)$$

$$= \frac{\partial(\rho \psi)}{\partial t} + \nabla \cdot (\rho \mathbf{v} \psi). \quad (14.35c)$$

Following the discussion in Section 14.3.3, we can extend the material parcel result (14.34c) to a finite size material region. Again, each point in the material region is following a fluid particle. The result is known as the *Reynolds transport theorem*

$$\frac{d}{dt} \int_{\mathcal{R}(\mathbf{v})} \psi \rho dV = \int_{\mathcal{R}(\mathbf{v})} \frac{D\psi}{Dt} \rho dV \quad (14.36a)$$

$$= \int_{\mathcal{R}(\mathbf{v})} \left[ \frac{\partial(\rho \psi)}{\partial t} + \nabla \cdot (\rho \psi \mathbf{v}) \right] dV \quad (14.36b)$$

$$= \int_{\mathcal{R}(\mathbf{v})} \frac{\partial(\rho \psi)}{\partial t} dV + \oint_{\partial \mathcal{R}(\mathbf{v})} \rho \psi \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (14.36c)$$

where the final equality follows from the divergence theorem. Additionally, we returned to the notation  $\mathcal{R}(\mathbf{v})$  for material region as introduced in Section 14.3.1. This notation is sufficient to designate that the region is following fluid particles along with the fluid velocity,  $\mathbf{v}$ . Note that for the surface integral term,  $\mathbf{v} \cdot \hat{\mathbf{n}}$  generally does not vanish. Rather, it is given by  $\mathbf{v} \cdot \hat{\mathbf{n}} = \mathbf{v}^{(s)} \cdot \hat{\mathbf{n}}$ , where  $\mathbf{v}^{(s)}$  is the velocity of a point on the boundary of the material region. We detail this result in Section 14.4.2 when discussing the kinematics of a moving material surface.

### 14.3.5 Comments on notation for the time derivative

In this book we write  $d/dt$  for the time derivative operator acting on an integral. Furthermore, when the domain is specialized to follow fluid particles, we identify the special nature of such domains by introducing the fluid velocity argument to the domain name,  $\mathcal{R}(\mathbf{v})$ . This notation designates that all points in the domain,  $\mathcal{R}$ , move with the fluid velocity,  $\mathbf{v}$ , since all points have fluid particles attached. However, many authors choose an alternative notation by using the material time derivative,  $D/Dt$ , when acting on an integral over a material region. We thus have the following equality across the two notational conventions

$$\frac{D}{Dt} \int_{\mathcal{R}} \psi \rho dV = \frac{d}{dt} \int_{\mathcal{R}(\mathbf{v})} \psi \rho dV. \quad (14.37)$$

The use of one convention versus the other is a matter of taste. We follow Section 2.1 of [Batchelor \(1967\)](#) by restricting the  $D/Dt$  operator to act only on space-time fields, such as  $\psi(\mathbf{x}, t)$ . Hence, the  $D/Dt$  operator is not used when acting on integrals over spatial regions. Following this convention leads us to write  $\mathcal{R}(\mathbf{v})$  for a region that moves with the fluid flow and to retain  $d/dt$  when acting on the integral over that region.

Admittedly, the  $\mathcal{R}(\mathbf{v})$  notation is rarely used in the literature, with authors generally dropping the  $\mathbf{v}$  and thus letting words designate whether a region follows the flow or otherwise. As we have occasion in this book to consider a variety of fluid regions, we find it essential to introduce the somewhat more pedantic notation,  $\mathcal{R}(\mathbf{v})$ , to denote that a region moving with  $\mathbf{v}$  is being considered. This usage hopefully helps the reader freely swim along with the mathematical flow

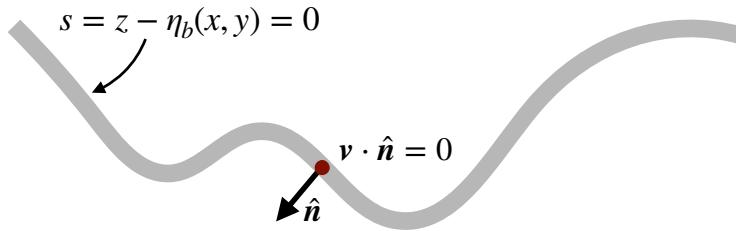


FIGURE 14.3: Illustrating the no-normal flow boundary condition maintained for a solid boundary, on which  $\mathbf{v} \cdot \hat{\mathbf{n}} = 0$  (equation (14.38)). When the solid boundary denotes the ground or ocean bottom, then the position of the interface is written  $s(x, y, z) = z - \eta_b(x, y) = 0$  (equation (14.39)). Correspondingly, the outward normal is given by  $\hat{\mathbf{n}} = -\nabla s/|\nabla s| = -(\hat{z} - \nabla \eta_b)/\sqrt{1 + |\nabla \eta_b|^2}$  (equation (14.40)).

rather than struggling to swim in a turbulent sea driven by confused notation.

## 14.4 Kinematic boundary conditions

When a fluid encounters a boundary, either at the edge of the fluid region or an imaginary boundary within the fluid itself, the fluid must accommodate the boundary. Conversely, the boundary must accommodate the fluid flow. Some boundaries are impermeable, so that they do not allow matter to cross. For material boundaries, any fluid originally in contact with the boundary stays in contact; at most this fluid can move tangential to the boundary without leaving it. Other boundaries are permeable, thus allowing matter to cross. Our goal in this section is to develop the various kinematic boundary conditions appropriate for the variety of cases encountered in fluid mechanics. These boundary conditions, and the considerations arising in their derivation, recur throughout fluid mechanics.

### 14.4.1 Static material surface

When a fluid encounters a static material surface, such as the solid-earth, the normal component of the fluid velocity must vanish since there is no fluid crossing the boundary (see Figure 14.3)

$$\mathbf{v} \cdot \hat{\mathbf{n}} = 0 \quad \text{no-normal flow condition on static material boundary.} \quad (14.38)$$

This relation constrains the flow so that any horizontal motion that is directed up or down a slope must have an associated vertical motion. Furthermore, recall our discussion of streamlines in Section 12.8.2, where  $\mathbf{v} \cdot \hat{\mathbf{n}} = 0$  along a streamline. We thus see that the static material boundary is a flow streamline. That is, fluid that is in contact with the boundary will remain in contact. As the boundary is static, this result holds even in the case of a time dependent flow. Note that specification of the tangential velocity along a material boundary requires dynamical information unavailable from the purely kinematic analysis considered here.

For many cases in practice, the material surface is monotonic in the vertical, meaning there are no overturns. In this case, it is useful to introduce some differential geometry (at the level of introductory calculus) to unpack the boundary condition (14.38). Doing so helps to develop a geometric formalism especially useful for the more complicated moving boundary conditions in Sections 14.4.2 and 14.4.3. For this purpose, introduce a coordinate expression for the boundary according to

$$s(x, y, z) = z - \eta_b(x, y) = 0 \quad \text{static material boundary,} \quad (14.39)$$

with  $z = \eta_b(x, y)$  the vertical position of the boundary. The outward normal vector at the

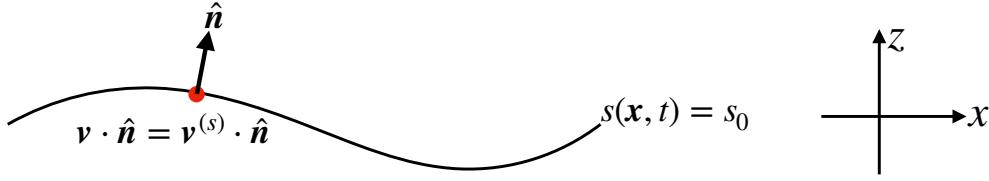


FIGURE 14.4: Illustrating the boundary condition for a moving material surface, on which  $\hat{\mathbf{n}} \cdot (\mathbf{v} - \mathbf{v}^{(s)}) = 0$  (equation (14.42)). For many cases, we can specify the surface by the value of a function that is a constant on the surface:  $s(x, y, z, t) = s_0$  for some constant  $s_0$  (equation (14.43)), in which case the normal direction is given by  $\hat{\mathbf{n}} = |\nabla s|^{-1} \nabla s$  (equation (14.44)). For example,  $s$  could represent a surface of constant buoyancy (Chapter 24) in a buoyancy stratified fluid.

boundary is thus given by

$$\hat{\mathbf{n}} = -\frac{\nabla s}{|\nabla s|} = -\frac{\nabla(z - \eta_b)}{|\nabla(z - \eta_b)|} = -\frac{\hat{\mathbf{z}} - \nabla \eta_b}{\sqrt{1 + |\nabla \eta_b|^2}}. \quad (14.40)$$

Consequently, the no-flux boundary condition (14.38) takes the form

$$\nabla(z - \eta_b) \cdot \mathbf{v} = w - \mathbf{u} \cdot \nabla \eta_b = 0 \quad \text{at } z = \eta_b(x, y), \quad (14.41)$$

where the velocity is decomposed into its horizontal and vertical components,  $\mathbf{v} = (\mathbf{u}, w)$ . Hence, to maintain the no-flux boundary condition requires the vertical velocity component to precisely balance the projection of the horizontal velocity onto the slope of the material surface. If the material surface is flat, so that  $\nabla \eta_b = 0$ , then the kinematic boundary condition reduces to  $w = 0$ . Alternatively, if the flow is purely horizontal and thus moves along a constant  $\eta_b$  isoline, then  $\mathbf{u} \cdot \eta_b = 0$  so that  $w = 0$ .

#### 14.4.2 Moving material surface

Now consider the kinematic constraints imposed by a material surface moving with the fluid flow. Such material surfaces follow the flow as defined by the fluid particle velocity. Consequently, they do not allow net mass to cross the surface.<sup>2</sup>

##### *General expression of the kinematic boundary condition*

To ensure no matter crosses the material surface, the velocity of the surface must match that of fluid particles. More precisely, the normal component of the velocity for a point on the surface must match the normal component of the fluid at the surface. We are thus led to the kinematic boundary condition for a moving material surface

$$(\mathbf{v} - \mathbf{v}^{(s)}) \cdot \hat{\mathbf{n}} = 0 \quad \text{moving material boundary condition.} \quad (14.42)$$

We illustrate this boundary condition in Figure 14.4, where  $\mathbf{v}^{(s)}$  is the velocity of a point fixed on the moving material surface and  $\mathbf{v}$  is the velocity of the fluid particles.

The boundary condition (14.42) does not mean  $\mathbf{v}$  and  $\mathbf{v}^{(s)}$  are identical. It only says that their normal components are the same when evaluated on the material surface. As a Corollary, we see that  $\mathbf{v} \cdot \hat{\mathbf{n}}$  is not generally zero so that a moving material boundary does *not* coincide with a flow streamline (see discussion in Sections 12.8.2 and 12.8.3).

<sup>2</sup>As we discuss in Chapter 15, with multiple components a surface that allows for zero net mass to cross it can still allow for the exchange of tracer mass in the presence of matter diffusion.

*Specialized expression of the boundary condition*

Now specialize the kinematic condition (14.42) to the case of a material surface specified by a function that takes on a constant value on the surface

$$s(\mathbf{x}, t) = s_0. \quad (14.43)$$

Correspondingly, the surface normal vector is given by

$$\hat{\mathbf{n}} = |\nabla s|^{-1} \nabla s. \quad (14.44)$$

From Section 12.5.6, we know that a point fixed on an arbitrary surface has a velocity that satisfies (see equation (12.42))

$$\frac{\partial s}{\partial t} + \mathbf{v}^{(s)} \cdot \nabla s = 0 \quad \text{on an iso-surface } s(\mathbf{x}, t) = s_0. \quad (14.45)$$

Use of the identity

$$\frac{\partial s}{\partial t} = \frac{D s}{D t} - \mathbf{v} \cdot \nabla s \quad (14.46)$$

renders

$$\frac{D s}{D t} - \mathbf{v} \cdot \nabla s + \mathbf{v}^{(s)} \cdot \nabla s = \frac{D s}{D t} + (\mathbf{v}^{(s)} - \mathbf{v}) \cdot \nabla s = 0. \quad (14.47a)$$

Since  $(\mathbf{v}^{(s)} - \mathbf{v}) \cdot \nabla s = 0$  from the boundary condition (14.42), we are left with the material constancy condition

$$\frac{D s}{D t} = \frac{\partial s}{\partial t} + \mathbf{v} \cdot \nabla s = 0 \quad \text{on material surface } s(\mathbf{x}, t) = s_0. \quad (14.48)$$

Consequently, no matter crosses a surface of constant  $s$  as long as  $s$  is materially constant. This is an important kinematic property that reappears in many forms throughout fluid mechanics.

*Boundary condition for a material interface*

Consider the interface between two immiscible fluids. Assume this surface interface has an outward normal that has a nonzero vertical component, so that there are no breaking waves, for example. In this case we can express its vertical position of a point on the interface as

$$s(x, y, z, t) = z - \eta(x, y, t) = s_0. \quad (14.49)$$

The function  $\eta(x, y, t)$  is the vertical deviation of the interface relative to the horizontal. The kinematic boundary condition (14.48) thus takes the form

$$\frac{D s}{D t} = \frac{D(z - \eta)}{D t} = 0. \quad (14.50)$$

Hence, the vertical velocity component at the interface equals to the material time derivative of the interface displacement

$$\frac{D z}{D t} = \frac{D \eta}{D t} \implies w = \frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla \eta \quad \text{material b.c. at interface } z = \eta(x, y, t). \quad (14.51)$$

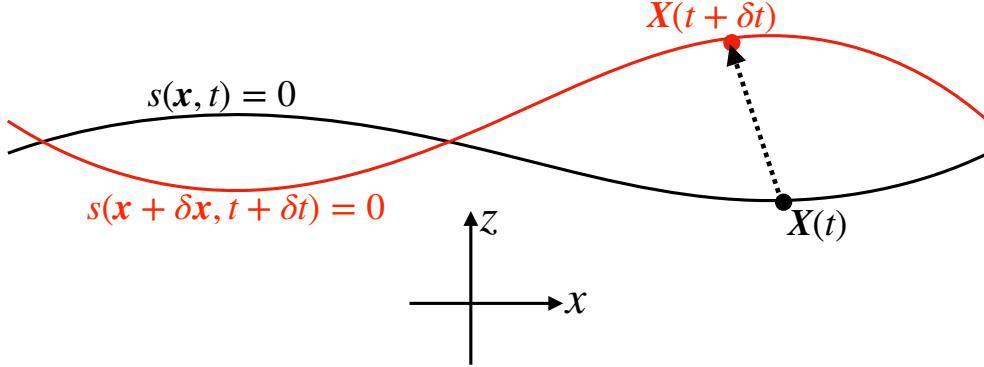


FIGURE 14.5: A surface that separates two fluid regions as realized at two time instants, along with the position of a sample point on the surface located at  $\mathbf{X}(t)$  and  $\mathbf{X}(t + \delta t)$ . The equation  $s(\mathbf{x}, t) = z - \eta(x, y, t) = 0$  specifies the vertical position for points on the surface as a function of horizontal position and time. At both time instances the vertical position is determined by  $s(\mathbf{x}, t) = s(\mathbf{x} + \delta\mathbf{x}, t + \delta t) = 0$ .

This boundary condition can be equivalently written in the form

$$\mathbf{v} \cdot \hat{\mathbf{n}} = \frac{\partial \eta / \partial t}{\sqrt{1 + |\nabla \eta|^2}}, \quad (14.52)$$

where

$$\hat{\mathbf{n}} = \frac{\nabla(z - \eta)}{|\nabla(z - \eta)|} = \frac{-\nabla \eta + \hat{\mathbf{z}}}{\sqrt{1 + |\nabla \eta|^2}} \quad (14.53)$$

is the outward normal at the material surface. These are expressions for the boundary condition placed on the ocean free surface when there is no water penetrating the surface (i.e., no rain or evaporation). In general, they provide kinematic expressions for the motion of an interface between two immiscible fluid layers.

#### *A geometric derivation of the material boundary condition*

The material invariance condition  $Ds/Dt = 0$  is a key kinematic result. We thus offer yet another derivation to help solidify its meaning. As before, define the surface according to

$$s(\mathbf{x}, t) = z - \eta(x, y, t) = s_0, \quad (14.54)$$

which specifies the vertical position of a point on the surface at time  $t$ . Now consider the position of the surface after a small time interval,  $t + \delta t$  (see Figure 14.5). The vertical position of the surface at the new time is determined by the same condition

$$s(\mathbf{x} + \delta\mathbf{x}, t + \delta t) = s_0, \quad (14.55)$$

where  $\mathbf{X}(t + \delta t) = \mathbf{x} + \delta\mathbf{x}$  is the displaced position of a point on the surface that started at  $\mathbf{X}(t) = \mathbf{x}$ . Expanding equation (14.55) in a Taylor series to leading order yields

$$s(\mathbf{x}, t) + \delta\mathbf{x} \cdot \nabla s + \delta t \partial_t s = s_0. \quad (14.56)$$

Since  $s(\mathbf{x}, t) = s_0$  from equation (14.54) we thus have

$$\frac{\partial s}{\partial t} + \frac{\delta\mathbf{x}}{\delta t} \cdot \nabla s = \frac{\partial s}{\partial t} + \frac{\delta\mathbf{x}}{\delta t} \cdot \hat{\mathbf{n}} |\nabla s| = 0, \quad (14.57)$$

where  $\hat{\mathbf{n}} = |\nabla s|^{-1} \nabla s$  is the surface normal direction. This result means that when positioned at a fixed point in space, it is the normal component of the displacement that corresponds to a temporal modification of  $s(\mathbf{x}, t)$

$$\frac{\partial s}{\partial t} = -\frac{\delta \mathbf{x}}{\delta t} \cdot \hat{\mathbf{n}} |\nabla s|. \quad (14.58)$$

In contrast, any tangential displacement along an  $s$ -isosurface leaves  $s(\mathbf{x}, t)$  unchanged. Hence, when following motion of points on the surface, we are only concerned with motion along the direction set by the normal component of the velocity of that point,  $\hat{\mathbf{n}} (\mathbf{v}^{(s)} \cdot \hat{\mathbf{n}})$ . It is this velocity component that corresponds to movement of the surface normal to itself, thus leading to nonzero motion through space.

The above considerations mean that we are just concerned with the normal component of the velocity of a point on the surface, and so can write for the displacement

$$\delta \mathbf{x} = \delta t \hat{\mathbf{n}} (\mathbf{v}^{(s)} \cdot \hat{\mathbf{n}}). \quad (14.59)$$

Making use of this result in equation (14.57) leads to the differential equation satisfied by a point fixed on the moving surface

$$\frac{\partial s}{\partial t} + \mathbf{v}^{(s)} \cdot \nabla s = 0, \quad (14.60)$$

where we used the identity

$$\frac{\delta \mathbf{x}}{\delta t} \cdot \nabla s = \hat{\mathbf{n}} (\mathbf{v}^{(s)} \cdot \hat{\mathbf{n}}) \cdot \nabla s = \mathbf{v}^{(s)} \cdot \nabla s. \quad (14.61)$$

Assuming the surface is material means that

$$\mathbf{v}^{(s)} \cdot \hat{\mathbf{n}} = \mathbf{v} \cdot \hat{\mathbf{n}}, \quad (14.62)$$

so that motion of the surface normal to itself is identical to that of the fluid in the same direction. The identity in equation (14.60) renders the material invariance condition  $Ds/Dt = 0$ .

### 14.4.3 Dynamic and permeable surface

We now consider the kinematic boundary condition for a moving permeable surface that separates two fluid media (e.g., ocean and atmosphere) or two regions within a single media (e.g., surface of constant buoyancy within the ocean or within the atmosphere). As before, the kinematic boundary condition is a statement about the mass transport through the boundary. Whereas the previous conditions enforced a zero net mass transport through the boundary, here we allow for a generally non-zero net transport (mass per time). We write this transport condition as

$$\rho (\mathbf{v} - \mathbf{v}^{(s)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = -\mathcal{Q}_m d\mathcal{S} \quad \text{moving non-material boundary condition.} \quad (14.63)$$

In this equation,  $d\mathcal{S}$  is an infinitesimal area element on the surface, and  $\mathcal{Q}_m$  is the mass per time per surface area (mass flux) crossing the boundary. The minus sign is a convention that will be motivated in the following. We now massage this kinematic boundary condition into alternative forms of use for a variety of purposes.

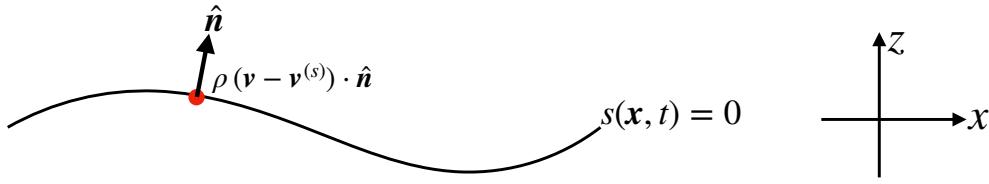


FIGURE 14.6: Illustrating the boundary condition for a moving permeable surface, such as the interface between two miscible fluid layers. On this surface, the boundary condition states that  $\rho(\mathbf{v} - \mathbf{v}^{(s)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = -Q_m d\mathcal{S}$  (equation (14.63)). In the special case of an ocean free surface with no overturns, this boundary condition reduces to the surface kinematic boundary condition (14.79).

#### *Coordinate representation of the permeable surface*

The expression (14.45) for  $\mathbf{v}^{(s)} \cdot \hat{\mathbf{n}}$  holds for a point on an arbitrary surface so that

$$\mathbf{v}^{(s)} \cdot \hat{\mathbf{n}} = -\frac{\partial s / \partial t}{|\nabla s|}. \quad (14.64)$$

Furthermore, the projection of the fluid velocity onto the normal direction can be written

$$\frac{Ds}{Dt} = \frac{\partial s}{\partial t} + \mathbf{v} \cdot \nabla s \implies \mathbf{v} \cdot \hat{\mathbf{n}} = \frac{1}{|\nabla s|} \left[ \frac{Ds}{Dt} - \frac{\partial s}{\partial t} \right]. \quad (14.65)$$

Bringing these results together leads to

$$\rho(\mathbf{v} - \mathbf{v}^{(s)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = \frac{\rho d\mathcal{S}}{|\nabla s|} \frac{Ds}{Dt} \implies Q_m = -\frac{\rho}{|\nabla s|} \frac{Ds}{Dt}. \quad (14.66)$$

This equation says that the mass transport crossing the surface is proportional to the material time derivative of the surface coordinate. The material time derivative vanishes when there is no mass transport across the surface (see discussion in Section 14.4.2).

#### *In terms of the horizontal projection of the surface area*

Assume that the surface is not vertical, so that its normal direction has a nonzero component in the vertical (e.g., waves that do not overturn). This assumption means that

$$\frac{\partial s}{\partial z} \neq 0, \quad (14.67)$$

so that we can further massage the boundary condition (14.66) by writing the area factor in the form

$$\frac{d\mathcal{S}}{|\nabla s|} = \frac{d\mathcal{S}}{\sqrt{(\partial s/\partial x)^2 + (\partial s/\partial y)^2 + (\partial s/\partial z)^2}} \quad (14.68a)$$

$$= \frac{d\mathcal{S}}{|\partial s/\partial z| \sqrt{[(\partial s/\partial x)/(\partial s/\partial z)]^2 + [(\partial s/\partial y)/(\partial s/\partial z)]^2 + 1}} \quad (14.68b)$$

$$= \frac{d\mathcal{S}}{|\partial s/\partial z| \sqrt{1 + \tan^2 \vartheta}} \quad (14.68c)$$

$$= \left| \frac{\partial z}{\partial s} \right| |\cos \vartheta| d\mathcal{S} \quad (14.68d)$$

$$= \left| \frac{\partial z}{\partial s} \right| dA. \quad (14.68e)$$

The equality (14.68c) introduced the angle,  $\vartheta$ , between the boundary surface and the horizontal plane. The squared slope of this surface given by

$$\tan^2 \vartheta = \frac{\nabla_z s \cdot \nabla_z s}{(\partial s/\partial z)^2} = \nabla_s z \cdot \nabla_s z \quad (14.69)$$

with

$$\nabla_z = \hat{x} \left[ \frac{\partial}{\partial x} \right]_{y,z} + \hat{y} \left[ \frac{\partial}{\partial y} \right]_{x,z} \quad (14.70)$$

the horizontal gradient operator on constant  $z$  surfaces, and

$$\nabla_s = \hat{x} \left[ \frac{\partial}{\partial x} \right]_{y,s} + \hat{y} \left[ \frac{\partial}{\partial y} \right]_{x,s} \quad (14.71)$$

the horizontal gradient operator on constant  $s$  surfaces, and  $z(x, y, s, t)$  the vertical position of the constant  $s$  surface.<sup>3</sup> The equality (14.68d) made use of a trigonometric identity, and the equality (14.68e) introduced the horizontal projection of the area,

$$dA = |\cos \vartheta| d\mathcal{S}. \quad (14.72)$$

These results bring the kinematic boundary condition (14.66) into the form

$$\rho (\mathbf{v} - \mathbf{v}^{(s)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = -Q_m d\mathcal{S} \quad (14.73a)$$

$$= \rho \frac{Ds}{Dt} \left| \frac{\partial z}{\partial s} \right| dA \quad (14.73b)$$

$$\equiv -Q_m dA. \quad (14.73c)$$

As defined, the flux  $Q_m$  is the net mass per time per horizontal area crossing the boundary surface

$$Q_m = -\rho (\mathbf{v} - \mathbf{v}^{(s)}) \cdot \hat{\mathbf{n}} \frac{d\mathcal{S}}{dA} = -\rho \frac{Ds}{Dt} \left| \frac{\partial z}{\partial s} \right|. \quad (14.74)$$

We motivate the minus sign through the ocean free surface case in the following.

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<sup>3</sup>We study in detail such operators in Chapter 41 when developing the mathematics of generalized vertical coordinates.

*Kinematic boundary condition at the ocean free surface*

Consider the ocean free surface located at

$$s(x, y, z, t) = z - \eta(x, y, t) = 0 \quad \text{ocean free surface.} \quad (14.75)$$

For this boundary,  $\partial s / \partial z = 1$  so that the area elements are related by

$$d\mathcal{S} = |\nabla(z - \eta)| dA = \sqrt{1 + |\nabla\eta|^2} dA. \quad (14.76)$$

The normal projection for the velocity of a point fixed on the free surface is given by

$$\mathbf{v}^{(\eta)} \cdot \hat{\mathbf{n}} = -\frac{\partial s / \partial t}{|\nabla s|} = \frac{\partial \eta / \partial t}{|\nabla(z - \eta)|} = \frac{\partial \eta / \partial t}{\sqrt{1 + |\nabla\eta|^2}} \implies \mathbf{v}^{(\eta)} \cdot \hat{\mathbf{n}} d\mathcal{S} = \partial_t \eta dA, \quad (14.77)$$

so that the mass flux crossing the free surface is

$$-\mathcal{Q}_m = \rho (\mathbf{v} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}}. \quad (14.78)$$

The boundary condition (14.74) thus takes the form

$$\rho (\mathbf{v} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} \frac{d\mathcal{S}}{dA} = \rho \left[ \frac{D(z - \eta)}{Dt} \right] = -Q_m \implies w + \rho^{-1} Q_m = \frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla \eta. \quad (14.79)$$

We now motivate the sign convention chosen for equation (14.73c) by considering the special case of a flat free surface and a resting fluid with  $\mathbf{v} = 0$ . Adding mass to the ocean raises the free surface, so that  $\partial \eta / \partial t > 0$ . Hence, the chosen sign convention means that  $Q_m > 0$  corresponds to mass added to the ocean.

*Kinematic boundary condition on a buoyancy surface*

Now consider the boundary surface to be a surface of constant potential density in the ocean (or analogously a surface of constant specific entropy in the atmosphere). These buoyancy isosurfaces are also known as isopycnals, and we use the symbol<sup>4</sup>

$$s = \sigma(x, y, z, t) \quad (14.80)$$

for a particular isopycnal,  $\sigma$ . The mass transport crossing the isopycnal is written

$$Q_m = \rho \frac{D\sigma}{Dt} \left| \frac{\partial z}{\partial \sigma} \right| \equiv \rho w^{(\dot{\sigma})}, \quad (14.81)$$

where we introduced the *diapycnal transport velocity*

$$w^{(\dot{\sigma})} \equiv \frac{D\sigma}{Dt} \left| \frac{\partial z}{\partial \sigma} \right|. \quad (14.82)$$

A key aspect of physical oceanography concerns the development of theories for processes that cause a non-zero diapycnal transport. Examples include breaking waves, which act to mix matter across density surfaces; i.e., to *entrain* water from one density class to another.

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<sup>4</sup>In this book, we use  $\sigma$  as an arbitrary generalized vertical coordinate, here chosen to be an isopycnal.

## 14.5 Volume and mass budgets for an ocean column

We close this chapter by deriving the budget for the volume per horizontal area in a column of ocean fluid such as that shown in Figure 14.7, as well as the budget for the mass per horizontal area in this column. The derivations require much of the formalism discussed earlier, thus serving as a useful close to the chapter. Note that since the upper boundary of the domain is the free surface, and since the free surface is a function of time, the region is not strictly Eulerian even though the sides are fixed in space. Furthermore, the free surface is permeable, as are the sides, so that the region is not material.

### 14.5.1 Kinematic free surface equation

We here derive an equation for the free surface evolution, with this equation providing a budget for the volume per horizontal area in the column. In outline form, the derivation proceeds by vertically integrating the mass continuity equation (14.16) over the depth of an ocean column, from  $z = \eta_b(x, y)$  at the bottom to  $z = \eta(x, y, t)$  at the free surface. Use of the bottom and surface kinematic boundary conditions renders a kinematic expression for the free surface time tendency.

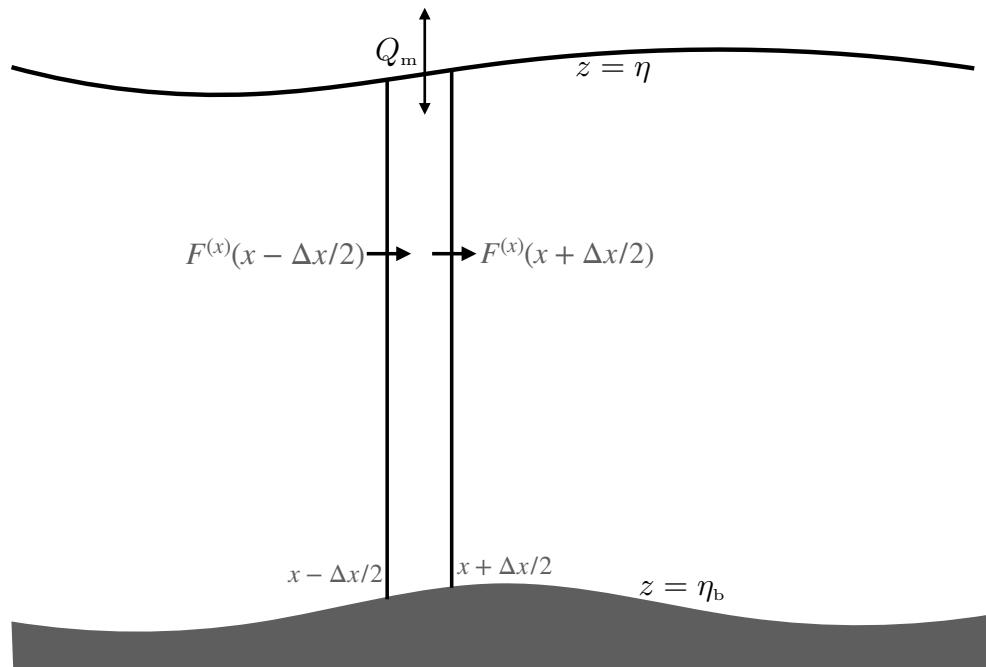


FIGURE 14.7: A longitudinal-vertical slice of ocean fluid from the surface at  $z = \eta(x, y, t)$  to bottom at  $z = \eta_b(x, y)$ . The horizontal boundaries of the column at  $x - \Delta x/2$  and  $x + \Delta x/2$  are static and are penetrated by zonal mass transport,  $F^{(x)}$ . The zonal mass transport is computed by integrating the zonal mass flux,  $\rho u$  over the area of the column sides. A similar transport acts in the meridional direction as well. The free surface is time dependent thus making the horizontal cross-sectional area for the fluid column time independent. The ocean bottom at the solid-earth boundary,  $z = \eta_b(x, y)$ , is static with no mass crossing this interface. The ocean surface at  $z = \eta(x, y, t)$  is time dependent with mass flux  $Q_m$  crossing this interface.

Vertically integrating the continuity equation (14.16) for a compressible fluid renders

$$-\int_{\eta_b}^{\eta} \frac{1}{\rho} \frac{D\rho}{Dt} dz = \int_{\eta_b}^{\eta} \nabla \cdot \mathbf{v} dz \quad (14.83a)$$

$$= w(\eta) - w(\eta_b) + \int_{\eta_b}^{\eta} \nabla_z \cdot \mathbf{u} dz \quad (14.83b)$$

$$= w(\eta) - w(\eta_b) + \nabla_z \cdot \left[ \int_{\eta_b}^{\eta} \mathbf{u} dz \right] - \mathbf{u}(\eta) \cdot \nabla_z \eta + \mathbf{u}(\eta_b) \cdot \nabla_z \eta_b \quad (14.83c)$$

$$= [w(\eta) - \mathbf{u}(\eta) \cdot \nabla_z \eta] - [w(\eta_b) - \mathbf{u}(\eta_b) \cdot \nabla_z \eta_b] + \nabla_z \cdot \left[ \int_{\eta_b}^{\eta} \mathbf{u} dz \right], \quad (14.83d)$$

where we made use of Leibniz's rule to move the horizontal divergence outside of the integral. Also note that  $\nabla \cdot \mathbf{u} = \nabla_z \cdot \mathbf{u}$  since  $\mathbf{u}$  is the horizontal velocity, and likewise for  $\nabla_z \eta_b$  and  $\nabla \eta$  since  $\eta_b$  and  $\eta$  are both functions of horizontal space and time.

Use of the surface kinematic boundary condition (14.79) and no-normal flow bottom boundary condition yield

$$\frac{\partial \eta}{\partial t} = \frac{Q_m}{\rho(\eta)} - \nabla \cdot \mathbf{U} - \int_{\eta_b}^{\eta} \frac{1}{\rho} \frac{D\rho}{Dt} dz \quad (14.84)$$

where

$$\mathbf{U} = \int_{\eta_b}^{\eta} \mathbf{u} dz \quad (14.85)$$

is the depth integrated horizontal transport. Hence, as deduced from the mass continuity equation, the ocean free surface time tendency is affected by the passage of mass across the surface boundary (as normalized by the surface density), the convergence of depth integrated flow, and the depth integral of the material changes in density. *Griffies and Greatbatch* (2012) provide a more complete analysis of the sea surface height budget (14.84) by unpacking the physical processes leading to the material evolution of density.

### 14.5.2 Budget for mass per horizontal area

The mass per horizontal area in the fluid column is given by  $\int_{\eta_b}^{\eta} \rho dz$ . Use of Leibniz's rule, the bottom kinematic boundary condition, (14.41), surface kinematic boundary condition (14.79), and the mass continuity equation (14.6), leads to

$$\frac{d}{dt} \left[ \int_{\eta_b}^{\eta} \rho dz \right] = \rho(\eta) \frac{\partial \eta}{\partial t} + \int_{\eta_b}^{\eta} \frac{\partial \rho}{\partial t} dz \quad (14.86a)$$

$$= \rho(\eta) \frac{\partial \eta}{\partial t} - \int_{\eta_b}^{\eta} \nabla \cdot (\rho \mathbf{v}) dz \quad (14.86b)$$

$$= \rho(\eta) \left[ \frac{\partial \eta}{\partial t} - w(\eta) \right] + \rho(\eta_b) w(\eta_b) - \int_{\eta_b}^{\eta} \nabla_z \cdot (\rho \mathbf{u}) dz \quad (14.86c)$$

$$= \rho(\eta) \left[ \frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla \eta - w(\eta) \right] + \rho(\eta_b) [w(\eta_b) - \mathbf{u}(\eta_b) \cdot \nabla_z \eta_b] - \nabla_z \cdot \mathbf{U}^\rho \quad (14.86d)$$

$$= Q_m - \nabla_z \cdot \mathbf{U}^\rho, \quad (14.86e)$$

where

$$\mathbf{U}^\rho = \int_{\eta_b}^{\eta} \rho \mathbf{u} dz. \quad (14.87)$$

Hence, the mass per horizontal area within a column evolves according to

$$\frac{d}{dt} \left[ \int_{\eta_b}^{\eta} \rho dz \right] = Q_m - \nabla \cdot \mathbf{U}^\rho, \quad (14.88)$$

with terms on the right hand side representing the convergence of mass onto the column either through the sides or surface. We consider an alternative derivation of this budget in Exercise 14.3.

## 14.6 Exercises

### EXERCISE 14.1: VELOCITY THAT DOES NOT PENETRATE A SURFACE

Consider a static surface defined by

$$s(x, y) = x y = \text{constant}. \quad (14.89)$$

Provide an example velocity,  $\mathbf{v} = u \hat{x} + v \hat{y} + w \hat{z}$ , that has nonzero horizontal components and that satisfies  $\mathbf{v} \cdot \hat{\mathbf{n}} = 0$ , where  $\mathbf{n}$  is the unit normal to the surface. Hint: see Section 33.4.5.

### EXERCISE 14.2: CENTER OF MASS MOTION

Consider a material fluid region,  $\mathcal{R}(\mathbf{v})$ , with constant mass written as

$$M = \int_{\mathcal{R}(\mathbf{v})} \rho dV. \quad (14.90)$$

- (a) Show mathematically that the centre of mass for the region moves with the region's total linear momentum

$$\frac{d}{dt} \left[ \frac{1}{M} \int_{\mathcal{R}(\mathbf{v})} \mathbf{x} \rho dV \right] = \frac{1}{M} \int_{\mathcal{R}(\mathbf{v})} \frac{D\mathbf{x}}{Dt} \rho dV = \frac{1}{M} \int_{\mathcal{R}(\mathbf{v})} \mathbf{v} \rho dV. \quad (14.91)$$

Precisely describe the reasoning behind each step. Note: a brief solution is sufficient, so long as the reasoning is sound.

- (b) Show mathematically (or precisely describe why) that the time change in the linear momentum for the region is given by

$$\frac{d}{dt} \left[ \int_{\mathcal{R}(\mathbf{v})} \rho \mathbf{v} dV \right] = \int_{\mathcal{R}(\mathbf{v})} \frac{D\mathbf{v}}{Dt} \rho dV. \quad (14.92)$$

Precisely describe the reasoning behind each step. Note: a brief solution is sufficient, so long as the reasoning is sound.

### EXERCISE 14.3: MASS BUDGET FOR A FLUID COLUMN

We here provide an alternative derivation of equation (14.88), the budget for the mass per horizontal area over a column of fluid.

The mass within an arbitrary fluid region is given by

$$M = \int \rho dV. \quad (14.93)$$

Consider the fluid mass within the column shown in Figure 14.7. In this column, the vertical side-walls are fixed in time, the bottom surface,  $z = \eta_b(x, y)$ , is at the solid-earth boundary, and

the top,  $z = \eta(x, y, t)$ , is the fluctuating ocean free surface. Convince yourself that the mass for this column can be written

$$M = \iint \left[ \int_{\eta_b(x,y)}^{\eta(x,y,t)} \rho dz \right] dx dy, \quad (14.94)$$

where the horizontal  $(x, y)$  integrals extend over the horizontal extent of the column. Mass conservation for this column means that the change in mass arises just through boundary fluxes, so that

$$\frac{dM}{dt} = - \int \rho \Delta \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (14.95)$$

where  $\hat{\mathbf{n}}$  is the outward normal to the surface of the fluid region,  $d\mathcal{S}$  is the area of an infinitesimal element on the surface, and the minus sign means that fluid leaving the region contributes to a reduction in mass within the region. The term

$$\Delta \mathbf{v} = \mathbf{v} - \mathbf{v}^{(s)} \quad (14.96)$$

is the velocity of the fluid relative to the velocity of the boundary; e.g., see the kinematic boundary condition discussion in Section 14.4.3. We also derive a general form of this relation in equation (15.46), though this exercise can be solved without knowing the details of that derivation.

- (a) Mass transported in the zonal direction ( $\hat{\mathbf{x}}$ ) that crosses the column's vertical boundary at  $x$  is given by

$$F^{(x)}(x, y, t) = \int_{y-\Delta y/2}^{y+\Delta y/2} \left[ \int_{\eta_b(x,y')}^{\eta(x,y',t)} u(x, y', z', t) \rho(x, y', z', t) dz' \right] dy' \quad (14.97a)$$

$$\equiv \int_{y-\Delta y/2}^{y+\Delta y/2} U^\rho(x, y', t) dy', \quad (14.97b)$$

and similarly for mass transport in the meridional direction

$$F^{(y)}(x, y, t) = \int_{x-\Delta x/2}^{x+\Delta x/2} \left[ \int_{\eta_b(x',y)}^{\eta(x',y,t)} v(x', y, z', t) \rho(x', y, z', t) dz' \right] dx' \quad (14.98a)$$

$$\equiv \int_{x-\Delta x/2}^{x+\Delta x/2} V^\rho(x', y, t) dx', \quad (14.98b)$$

where

$$\mathbf{U}^\rho(x, y, t) = \int_{\eta_b(x,y)}^{\eta(x,y,t)} \mathbf{u}(x, y, z', t) \rho(x, y, z', t) dz' = \hat{\mathbf{x}} U^\rho + \hat{\mathbf{y}} V^\rho. \quad (14.99)$$

What are the physical dimensions [in terms of length (L), mass (M), and time (T)] for the mass transports,  $F^{(x)}$  and  $F^{(y)}$ ?

- (b) Using these expressions for the mass crossing the vertical side boundaries of a fluid column, take the limit as the horizontal cross-sectional area of the column becomes infinitesimally small to show that the evolution equation for the mass per unit area of the column is given by

$$\frac{d}{dt} \left[ \int_{\eta_b}^{\eta} \rho dz \right] = -\nabla \cdot \mathbf{U}^\rho + Q_m, \quad (14.100)$$

where  $Q_m$  is the mass transport entering the ocean through the surface, per horizontal area,

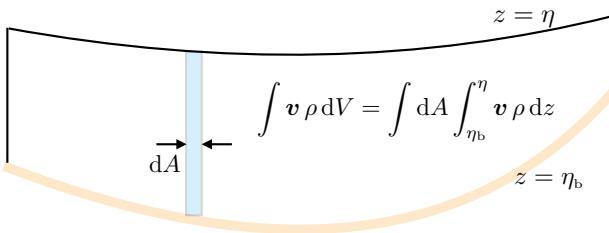


FIGURE 14.8: Cross-section of the integration region for Exercise 14.4, with the region extending from the ocean bottom at  $z = \eta_b(x, y)$  and the free surface at  $z = \eta(x, y, t)$ . The sides are assumed to be vertical and rigid. An infinitesimal column is shown with cross-sectional area  $dA$ , extending from the bottom to the surface. The cross-sectional area for the column is time independent, so that a time derivative passes across the area integral to act only on the upper limit  $z = \eta$  and the integrand in equation (14.104).

as defined by equation (14.73c), so that

$$\int Q_m dA = - \int \rho \Delta \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S} \quad \text{at } z = \eta. \quad (14.101)$$

The derivation of equation (14.100) is part of this exercise, using methods distinct from those used in Section 14.5.2.

- (c) In words, the mass budget in equation (14.100) says that mass changes in a column of fluid if there is a convergence of mass into the column across its vertical boundaries (first term on right hand side), and a mass flux entering the column across the ocean surface (second term on right hand side). What are the physical dimensions of all terms in equation (14.100)?

#### EXERCISE 14.4: CHANGE IN LINEAR MOMENTUM OF A FLUID REGION

Consider a closed ocean basin with zero boundary fluxes of matter; i.e., zero precipitation/evaporation and zero mass fluxes through the solid-earth bottom. Consequently, this region is bounded by material surfaces and so it maintains constant matter content with fixed mass

$$M = \int_{\mathcal{R}} \rho dV. \quad (14.102)$$

Show that the time change in the linear momentum for this ocean basin is given by

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho \mathbf{v} dV \right] = \int_{\mathcal{R}} \frac{D\mathbf{v}}{Dt} \rho dV. \quad (14.103)$$

This result is identical to that derived in Exercise 14.2. Rather than just repeating the solution method used there, make use of Leibniz's rule, the kinematic boundary condition detailed in Section 14.4.2, and mass conservation.

Hint: Refer to Figure 14.8 for a schematic of the integration where we have expanded the volume integral into the form

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho \mathbf{v} dV \right] = \frac{d}{dt} \left[ \int \left( \int_{\eta_b}^{\eta} \rho \mathbf{v} dz \right) dA \right], \quad (14.104)$$

where the horizontal integral extends over the rigid and fixed horizontal area of the basin,  $dA = dx dy$  is the time independent horizontal area element,  $z = \eta_b(x, y)$  is the solid-earth bottom and  $z = \eta(x, y, t)$  is the ocean free surface. Time dependence appears in the upper boundary at  $z = \eta$  and within the integrand. Perform the time derivative operation and make use of mass continuity and the kinematic boundary condition. Also make use of the trigonometry presented in Section

14.4.3 (in particular equation (14.72)). Unlike the formulation in Exercise 14.2, there is no use of a material time derivative in this approach. Rather, it is a straightforward use of integration over a domain with fixed horizontal/bottom boundaries and a time dependent free surface boundary.





# Chapter 15

## Tracer conservation

Throughout this book, we assume that fluid mass is neither created nor destroyed anywhere within the fluid domain. We qualify this statement by noting that constituent matter may be created or destroyed via chemical reactions that convert matter from one form to the other. Such processes are typically represented as sources or sinks for matter components. Yet even in the presence of chemical reactions, we assume that mass is conserved. Hence, the net mass within a given fluid domain changes only via transport crossing the domain boundary. We here extend the discussion from Chapter 14, which focused on homogeneous fluids, to the case of a non-homogeneous fluid comprised of multiple matter constituents. In so doing we develop budgets for material tracers.

### READER'S GUIDE TO THIS CHAPTER

The formulation pursued in this chapter is inspired by similar treatments in the chemical physics literature (e.g., Chapter 11 of [Aris \(1962\)](#) and Chapter II of [DeGroot and Mazur \(1984\)](#)), where they develop the theory for transport processes in multi-component fluids (along with chemical reactions, which we do not cover in this book). For this chapter, we assume an understanding of the Eulerian and Lagrangian kinematic descriptions detailed in Chapter 12 and the mass conservation analysis in Chapter 14. Much of the material from this chapter is used for the study of scalar fields such as potential enthalpy and material tracers. Furthermore, the Leibniz-Reynolds transport theorem of Section 15.3.4 is a kinematic expression that is central to all finite volume budgets in fluid mechanics.

15.1	The tracer equation . . . . .	314
15.1.1	Mass conservation for each constituent . . . . .	314
15.1.2	Total mass conservation . . . . .	315
15.1.3	The tracer equation . . . . .	316
15.1.4	Compatibility between total mass and tracer mass . . . . .	318
15.1.5	Summary of some conceptual points . . . . .	318
15.1.6	Further study . . . . .	319
15.2	Passive tracers . . . . .	320
15.3	Budgets for arbitrary fluid regions . . . . .	320
15.3.1	Extensive and intensive fluid properties . . . . .	320
15.3.2	General form of the finite domain integral . . . . .	321
15.3.3	Eulerian (static) domain . . . . .	322
15.3.4	Deriving the Leibniz-Reynolds transport theorem . . . . .	322
15.3.5	Interpreting the Leibniz-Reynolds transport theorem . . . . .	325
15.3.6	Revisiting Reynolds transport theorem . . . . .	326

15.3.7	Summary of the time derivatives acting on integrals . . . . .	328
15.4	Brute force illustration of Leibniz-Reynolds . . . . .	<b>328</b>
15.4.1	Leibniz's rule plus kinematic boundary conditions . . . . .	329
15.4.2	Summarizing the result . . . . .	330
15.5	Boundary conditions . . . . .	<b>330</b>
15.5.1	Interior layer boundary conditions . . . . .	331
15.5.2	Solid-earth boundary conditions . . . . .	331
15.5.3	Upper ocean surface boundary conditions . . . . .	332
15.6	Evolution of region mean tracer concentration . . . . .	<b>333</b>
15.6.1	Formulation . . . . .	333
15.6.2	Application to a numerical ocean model grid cell . . . . .	334
15.7	Exercises . . . . .	<b>334</b>

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## 15.1 The tracer equation

As defined in Section 12.2, a fluid element is an infinitesimal region of constant mass within the fluid continuum. Although possessing a constant mass, it generally has a non-constant material composition. That is, a fluid element is a non-material fluid parcel. Fluid element boundaries are open to the exchange of matter (i.e., tracers) with adjacent fluid elements. They are also open to the exchange of thermodynamic properties such as temperature and specific entropy. The kinematics of fluid elements share certain features with material fluid parcels. For example, we can uniquely specify the position of a fluid element by providing a material coordinate and time. Correspondingly, we can generalize Reynolds transport theorem for integration over a constant mass fluid region (Section 15.3.4). We make use of fluid elements to develop the mass budgets for non-homogeneous fluids such as the ocean and atmosphere. The constituent mass budgets are commonly referred to as *tracer equations*.

### 15.1.1 Mass conservation for each constituent

In this subsection we formulate the mass conservation equation for each constituent within the fluid. The mass equation is formulated by taking an integral or weak formulation approach with a fixed (Eulerian) region.

#### *Density and velocity for each matter constituent*

Consider a fluid with  $n = 1, N$  matter constituents. For example, seawater has  $N = 2$  when concerned just with its freshwater and salt content, whereas  $N > 2$  when also concerned with other material constituents such as  $CO_2$  and other biogeochemical species. Now focus on a fixed (Eulerian) region of the fluid with volume  $V$  and total mass  $M$ . Inside of the region, count the number of molecules of each constituent and determine their corresponding velocities. This information can be used to construct the molecular center of mass velocity for each constituent,  $\mathbf{v}^{(n)}$ , as well as the mass density,

$$\rho^{(n)} = V^{-1} M^{(n)}. \quad (15.1)$$

In the continuum limit, the volume and mass in the region get tiny ( $V \rightarrow dV$  and  $M \rightarrow dM$ ), yet the mass density remains smooth and finite (see Figure 11.2). Correspondingly, the constituent velocity and mass density are continuous fields whose values are available at each point within the continuum fluid.

### Integral formulation of the constituent mass budget

Consider an arbitrary region,  $\mathcal{R}$ , assumed to be fixed in space (an Eulerian region). The mass of component  $n$  within  $\mathcal{R}$  is given by the integral

$$M^{(n)} = \int_{\mathcal{R}} \rho^{(n)} dV, \quad (15.2)$$

and it changes in time according to the finite volume budget equation (there is no implied summation on the right hand side)

$$\frac{d}{dt} \int_{\mathcal{R}} \rho^{(n)} dV = - \int_{\partial\mathcal{R}} \rho^{(n)} \mathbf{v}^{(n)} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (15.3)$$

This equation is a constituent form of the finite volume mass budget given for a homogeneous fluid by equation (14.9). Since the region,  $\mathcal{R}$ , is assumed to be fixed in space, we can move the time derivative across the integral to reveal

$$\int_{\mathcal{R}} \left[ \frac{\partial \rho^{(n)}}{\partial t} + \nabla \cdot (\rho^{(n)} \mathbf{v}^{(n)}) \right] dV = 0, \quad (15.4)$$

where we also used the divergence theorem to convert the surface integral to a volume integral. Arbitrariness of the region means that this integral expression must be satisfied at each point of the continuum, thus leading to the Eulerian form of the constituent mass continuity equation

$$\frac{\partial \rho^{(n)}}{\partial t} + \nabla \cdot (\rho^{(n)} \mathbf{v}^{(n)}) = 0. \quad (15.5)$$

This equation can also be written using a material time derivative

$$\frac{D^{(n)} \rho^{(n)}}{Dt} = -\rho^{(n)} \nabla \cdot \mathbf{v}^{(n)} \quad \text{for each of the } n = 1, N \text{ constituents,} \quad (15.6)$$

where the constituent material time derivative is given by

$$\frac{D^{(n)}}{Dt} = \frac{\partial}{\partial t} + \mathbf{v}^{(n)} \cdot \nabla. \quad (15.7)$$

We thus have  $N$  statements of mass conservation corresponding to each constituent material fluid parcel moving according to the velocity  $\mathbf{v}^{(n)}$ .

#### 15.1.2 Total mass conservation

Summing the Eulerian mass continuity equation (15.5) over all constituents leads to the continuity equation for the total mass

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0, \quad (15.8)$$

where the total mass density and *barycentric velocity* are given by

$$\rho = \sum_{n=1}^N \rho^{(n)} \quad \text{and} \quad \mathbf{v} = \rho^{-1} \sum_{n=1}^N \rho^{(n)} \mathbf{v}^{(n)}. \quad (15.9)$$

Introducing the material time derivative following the barycentric velocity,  $D/Dt = \partial/\partial t + \mathbf{v} \cdot \nabla$ , leads to the equivalent material form for the mass conservation equation

$$\frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{v}. \quad (15.10)$$

The *barycenter* of a distribution of matter is the center of inertia for that matter. We choose the term *barycentric velocity* to distinguish  $\mathbf{v}$  from the molecular *center of mass velocity*,  $\mathbf{v}^{(n)}$ , of each constituent. The barycentric velocity plays a key role in the conservation laws for multi-component fluids.

### 15.1.3 The tracer equation

Rather than keep track of each constituent velocity,  $\mathbf{v}^{(n)}$ , and the corresponding material parcels, it is generally more convenient to focus on the fluid element that moves with the barycentric velocity. For this purpose, we consider again the constituent mass continuity equation (15.5)

$$\left[ \frac{\partial}{\partial t} + \mathbf{v}^{(n)} \cdot \nabla \right] \rho^{(n)} = -\rho^{(n)} \nabla \cdot \mathbf{v}^{(n)} \quad (15.11)$$

and insert the barycentric velocity to both sides by adding  $0 = \mathbf{v} - \mathbf{v}$

$$\left[ \frac{\partial}{\partial t} + (\mathbf{v} - \mathbf{v} + \mathbf{v}^{(n)}) \cdot \nabla \right] \rho^{(n)} = -\rho^{(n)} \nabla \cdot [\mathbf{v} - \mathbf{v} + \mathbf{v}^{(n)}]. \quad (15.12)$$

Rearrangement leads to

$$\left[ \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \right] \rho^{(n)} = -\rho^{(n)} \nabla \cdot \mathbf{v} - \nabla \cdot [\rho^{(n)} (\mathbf{v}^{(n)} - \mathbf{v})], \quad (15.13)$$

which can be written

$$\frac{D\rho^{(n)}}{Dt} = -\rho^{(n)} \nabla \cdot \mathbf{v} - \nabla \cdot \mathbf{J}^{(n)}, \quad (15.14)$$

where we defined the constituent mass flux

$$\mathbf{J}^{(n)} = \rho^{(n)} (\mathbf{v}^{(n)} - \mathbf{v}), \quad (15.15)$$

which arises from the difference between the constituent velocity and the barycentric velocity. The dimensions of  $\mathbf{J}^{(n)}$  are mass of constituent  $n$  per time per area.

The material mass conservation equation (15.14) takes on the Eulerian form

$$\frac{\partial \rho^{(n)}}{\partial t} + \nabla \cdot (\mathbf{v} \rho^{(n)}) = -\nabla \cdot \mathbf{J}^{(n)}. \quad (15.16)$$

Introducing the tracer concentration  $C^{(n)}$  according to

$$C^{(n)} = \frac{\rho^{(n)}}{\rho} = \frac{\delta M^{(n)}}{\delta M} = \frac{\text{mass of constituent } n \text{ in fluid element}}{\text{mass of fluid element}}, \quad (15.17)$$

leads to the tracer flux

$$\mathbf{J}^{(n)} = \rho C^{(n)} (\mathbf{v}^{(n)} - \mathbf{v}), \quad (15.18)$$

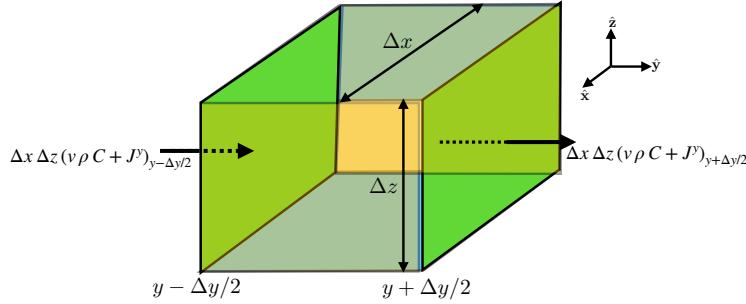


FIGURE 15.1: A finite sized cube as in Figure 14.1, here used to illustrate the budget of tracer mass over an Eulerian region. In addition to the advective flux of tracer moving with the barycentric velocity,  $\mathbf{v}$ , there is a diffusive flux,  $\mathbf{J}$ , that contributes to the transfer of tracer across the cell face.

the Eulerian flux-form tracer budget

$$\frac{\partial(\rho C^{(n)})}{\partial t} + \nabla \cdot [\mathbf{v} \rho C^{(n)} + \mathbf{J}^{(n)}] = 0. \quad (15.19)$$

In Figure 15.1 we illustrate the contributions to the tracer evolution according to this Eulerian flux-form equation (15.19).

#### Eulerian and Lagrangian forms of the tracer equation

The Eulerian flux-form equation (15.19) has a corresponding material time derivative form derived by expanding the derivatives to find

$$\begin{aligned} C^{(n)} \frac{\partial \rho}{\partial t} + \rho \frac{\partial C^{(n)}}{\partial t} + \rho \mathbf{v} \cdot \nabla C^{(n)} + C^{(n)} \nabla \cdot (\rho \mathbf{v}) \\ = C^{(n)} \left[ \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) \right] + \rho \left[ \frac{\partial C^{(n)}}{\partial t} + \mathbf{v} \cdot \nabla \right] C^{(n)}. \end{aligned} \quad (15.20)$$

The first term on the right hand side vanishes through mass continuity in the form of equation (15.8). The second term on the right hand side is the material time derivative of the tracer concentration. We are thus led to the equivalent forms for the tracer equation<sup>1</sup>

$$\frac{\partial(\rho C^{(n)})}{\partial t} + \nabla \cdot [\mathbf{v} \rho C^{(n)}] = \rho \frac{DC^{(n)}}{Dt} = -\nabla \cdot \mathbf{J}^{(n)}. \quad (15.21)$$

#### Advection plus diffusive tracer fluxes

The above definitions allow us to decompose an advective tracer flux defined according to the tracer velocity into an advective flux based on the barycentric velocity plus a *diffusive flux*

$$\rho C^{(n)} \mathbf{v}^{(n)} = \rho C^{(n)} (\mathbf{v}^{(n)} - \mathbf{v} + \mathbf{v}) = \mathbf{J}^{(n)} + \rho C^{(n)} \mathbf{v}. \quad (15.22)$$

The diffusive flux vanishes when the tracer velocity equals to the barycentric velocity. Correspondingly, the diffusive flux also vanishes for a single-component fluid, since in that case there is only one matter component and so the constituent velocity equals to the barycentric velocity.

<sup>1</sup>The same result was also derived in equation (14.35c) when discussing Reynolds transport theorem for a homogenous fluid.

We refer to this flux as “diffusive” since it is common in practice to parameterize this term as a downgradient diffusive flux. We study such parameterizations in Chapter 48.

#### 15.1.4 Compatibility between total mass and tracer mass

By construction, the Eulerian flux-form of the tracer equation (15.19) is compatible with the flux-form continuity equation

$$\frac{\partial(\rho C^{(n)})}{\partial t} + \nabla \cdot [\rho \mathbf{v} C^{(n)} + \mathbf{J}^{(n)}] = 0 \iff \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0. \quad (15.23)$$

Compatibility is manifest by summing the tracer equation over all constituents and using the identities

$$\sum_{n=1}^N C^{(n)} = 1 \quad \text{and} \quad \sum_{n=1}^N \mathbf{J}^{(n)} = 0. \quad (15.24)$$

Furthermore, through use of the barycentric velocity (15.9), we are ensured that the continuity equation for the total density of a fluid element is only transported by the barycentric velocity. There is no contribution from  $\mathbf{J}^{(n)}$  since  $\sum_{n=1}^N \mathbf{J}^{(n)} = 0$ .

#### 15.1.5 Summary of some conceptual points

What is a fluid element? How does it maintain constant mass but not constant matter? These questions can lead to some puzzles when encountering the notion of a fluid element. Here we aim to explain some of the conceptual points to resolve the puzzles, building from our initial specification of fluid elements and parcels in Section 12.2.

##### *Revisiting a fluid element*

The mass continuity equation (15.10) motivates us to define a fluid element as an infinitesimal fluid parcel that moves with barycentric velocity,  $\mathbf{v}$ , and maintains a constant total mass

$$\delta M = \sum_{n=1}^N \delta M^{(n)}. \quad (15.25)$$

The fluid element does not maintain a constant mass for each constituent, since the fluid element moves at the barycentric velocity,  $\mathbf{v}$ , which generally differs from the constituent velocities  $\mathbf{v}^{(n)}$ . Consequently, a fluid element boundary is permeable to matter transport that leaves its mass constant but allows for exchanges of matter constituents with adjacent fluid elements. Hence, if some matter leaves the fluid element, then an equal amount must enter the element in order to maintain a constant mass.

The exchange of matter across a fluid element’s boundary can arise from the direct motion of matter crossing the boundary, or from the motion of the fluid element boundary relative to the matter. This point is central to resolving some conundrums associated with the notion of matter exchange constrained to retain constant mass. We have more to say on this point in the following.

##### *Conceptual summary of the formulation*

The formulation pursued in this section is based on considering the non-homogeneous fluid to be a continuum with distinct matter constituents (e.g., salt and freshwater for the ocean or water vapor and dry air for the atmosphere). Furthermore, the mass concentration for each constituent

is represented by a scalar field whose value at any point in space-time gives the mass of tracer per mass of fluid. We then formulate mass conservation equations (i.e., continuity equations) for each matter constituent following methods used for the homogeneous fluid in Chapter 14. By choosing to use the *barycentric* (center of mass) velocity for describing fluid flow, the mass continuity equation for the total mass in a fluid element takes on the same form as for a homogeneous fluid. The resulting constituent mass budgets (i.e., tracer equations) have “diffusive” fluxes since the velocity of each matter constituent is generally distinct from the barycentric velocity.

To expose a bit of the details, we saw in this section that the tracer equation expresses the balance of mass for each trace constituent in the fluid. Furthermore, a nonzero tracer flux,  $\mathbf{J}^{(n)} = \rho C^{(n)} (\mathbf{v}^{(n)} - \mathbf{v})$ , arises when the barycentric velocity,  $\mathbf{v}$ , differs from the constituent velocity,  $\mathbf{v}^{(n)}$ . In that case, matter and thermodynamic properties are exchanged between fluid elements, with the exchange made without altering the mass of a fluid element. In the presence of random motion within a turbulent fluid, or in the presence of random interactions with molecular degrees of freedom, tracer exchange is akin to a random walk. Such exchange is commonly parameterized by a diffusion process (see Section 46.3). Correspondingly, the mass of tracers in a fluid element is altered in the presence of differences in tracer concentration between fluid elements (i.e., tracer concentration gradients). However, the total mass of the element remains fixed.

#### *How to maintain constant mass*

As defined, a fluid element provides a generalization to multi-component fluids of the notion of a constant mass material fluid parcel that we used in describing a homogeneous fluid (see Section 12.2). Later in this chapter we will encounter a finite volume extension of the fluid element, which we refer to as a *Lagrangian region*. A Lagrangian region has boundaries that follow the barycentric velocity,  $\mathbf{v}$ , so that the region maintains constant mass as per our discussion of Reynolds transport theorem in Section 15.3.6.

To maintain constant mass, any matter that leaves the fluid element by crossing its boundary is compensated by an equal mass that enters the boundary. Kinematically, there are two means for matter to cross a boundary. First, the matter itself can move across the boundary, with the limiting case being a stationary boundary with matter moving across. Second, the boundary can move relative to the matter, with the limiting case being stationary matter with the boundary moving. In either case, by choosing to follow the barycentric velocity, a fluid element’s boundary (or a corresponding Lagrangian region’s boundary) adjusts so that mass remains constant.

The strategic choice to formulate the kinematics of multi-component fluids using the barycentric velocity is directly analogous to the choice in classical mechanics to describe motion relative to the center of mass for a system of many moving objects such as planets or point particles. In particular, by describing the motion of a multi-component fluid using the barycentric velocity, we simplify the kinematics by linking to the kinematics of homogeneous fluids while also supporting a generalization in the form of constituent tracer equations. As seen in Part IV of this book, a dynamical description of fluid motion is also facilitated by working with constant mass fluid elements/regions.

#### 15.1.6 Further study

An extension of the ideas presented in this section allows for chemical reactions to transfer mass from one constituent to others, while retaining fixed net mass. This extension is relevant for discussion of atmospheric chemistry and ocean biogeochemistry. Fundamental discussions of these extensions, using nomenclature similar to that used here, are provided in Chapter 11 of *Aris* (1962) and Chapter II of *DeGroot and Mazur* (1984).

## 15.2 Passive tracers

As defined in equation (15.17), the concentration of a material tracer is the mass of the trace constituent per mass of a fluid element. Such material tracers modify the barycentric velocity (15.9) since they carry mass and thus affect the mass density. We here introduce the related construct known as a *passive tracer*. A passive tracer satisfies the advection-diffusion equation, but it has zero impact on the velocity and is thus dynamically passive. Mathematically, we conceive of a passive tracer as a material tracer in the limit where the tracer mass and mass of the fluid element together go to zero. The passive tracer is thus analogous to the massless fluid particle of Section 12.2 whose trajectories define the Lagrangian reference frame. We make use of passive tracers to probe the advective and diffusive features of the flow without modifying the flow. For example, a passive tracer can be used to define tracer pathways and time scales for transport between fluid regions.

In Chapter 13 and Section 14.4.2, we discussed the notion of a material fluid object, which is an object comprised of fluid particles that follow the velocity,  $\mathbf{v}$ . In a homogeneous fluid, such material objects are impenetrable to matter, by construction. For a multi-component fluid, trace matter will generally cross the material object through diffusion since  $\mathbf{v}^{(n)} \neq \mathbf{v}$ . Hence, there is no perfectly impenetrable fluid object in a fluid with any form of diffusion, including molecular diffusion. However, we can conceive of a passive tracer that follows the barycentric velocity and either diffuses or not. Again, these enhanced features are afforded the passive tracer given that it is a massless idealization used to probe the fluid flow properties. Hence, it is not subject to the same physical constraints as a material tracer.

## 15.3 Budgets for arbitrary fluid regions

Thus far in this chapter we have considered the evolution of mass within a variety of fluid regions, including infinitesimal and finite domains either moving with the fluid or fixed in space. We have also considered similar domains in Chapter 14 where the fluid domains were typically material regions. In this section we synthesize these presentations by considering mass budgets over an arbitrary finite sized domain within multi-component fluids. The resulting mass equations form the basis for matter budget analyses used in geophysical fluid mechanics.

### 15.3.1 Extensive and intensive fluid properties

Physical properties can be characterized as *extensive* or *intensive*. An extensive property changes when the size of the sample changes. Examples are particle number, mass, length, volume, kinetic energy, entropy, enthalpy, and linear momentum. An intensive property is not affected when removing some of the sample. Examples are number density (number of particles per volume), mass density (mass of substance per volume), tracer concentration (mass of tracer per mass of fluid), temperature, velocity (linear momentum per mass), kinetic energy per mass, entropy per mass, and enthalpy per mass.

To further this discussion, consider a bucket of seawater that has homogeneous temperature and salinity. Removing a cup of water from this bucket does not alter the temperature and salinity (both are intensive properties), but it does alter the enthalpy, salt mass, and freshwater mass (each are extensive properties). We thus make the distinction between intensive and extensive properties for the purpose of developing budget equations, with budget equations formulated for extensive properties.<sup>2</sup>

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<sup>2</sup>We have more to say about intensive and extensive properties when considering thermodynamics in Chapter 20.

We are concerned in this section with how scalar extensive properties change as a function of time. Determining the evolution of such properties constitutes a budget analysis for the scalar property. What are the processes responsible for these changes? Where are the changes coming from? Those are basic questions asked when performing a budget analysis. In addition to physical and biogeochemical processes active within the fluid, details of the region over which one performs a budget have an important impact on the budget. Is the region open to matter and energy transport, or is it closed? Is the region static (Eulerian) or do boundaries move? If the boundaries move, do they move with fluid elements (Lagrangian) or are they moving in some other manner (arbitrary)?

In the following, let  $\Pi$  represent an intensive scalar fluid property of a fluid element so that  $\Pi \rho \delta V$  is the corresponding extensive property

$$\Pi = \text{intensive fluid property such as tracer concentration} \quad (15.26a)$$

$$\Pi \rho \delta V = \text{extensive fluid property such as tracer mass.} \quad (15.26b)$$

For example, if  $\Pi$  is the tracer concentration in a fluid element (i.e., mass of tracer per mass of fluid), then the corresponding extensive property,  $\Pi \rho \delta V$ , is the mass of tracer in the fluid element. Anticipating our discussion in Section 21.8, let  $\Pi$  be the Conservative Temperature,  $\Theta$ , of a fluid element, then the corresponding extensive property,  $\Theta c_p \rho \delta V$ , is the potential enthalpy with  $c_p$  the specific heat capacity.

We furthermore assume that  $\Pi$  satisfies the scalar conservation equation, written here in both its material form and Eulerian flux-form

$$\rho \frac{D\Pi}{Dt} = -\nabla \cdot \mathbf{J} \quad \Longleftrightarrow \quad \frac{\partial(\rho \Pi)}{\partial t} + \nabla \cdot (\rho \Pi \mathbf{v} + \mathbf{J}) = 0, \quad (15.27)$$

where  $\mathbf{J}$  is a flux such as that associated with the tracer equation derived in Section 15.1.3. Depending on the context, the budget equation (15.27) is sometimes referred to as a *conservation law* for  $\Pi$ . Notably, satisfaction of a conservation law does not mean that  $\Pi$  is constant either at a point in space nor following a fluid particle. Instead, there are two cases of “constancy” that naturally arise. First, with  $-\nabla \cdot \mathbf{J} = 0$ , the scalar field is constant following a material fluid particle

$$-\nabla \cdot \mathbf{J} = 0 \implies \frac{D\Pi}{Dt} = 0. \quad (15.28)$$

In this case we say that  $\Pi$  is a *material invariant* or a *material constant*. Second, if the Eulerian time derivative vanishes,  $\partial_t \Pi = 0$ , then  $\Pi$  remains constant at a fixed spatial point in the fluid and we say that  $\Pi$  is in a *steady state*. Furthermore, recall that the Eulerian reference frame is stationary with respect to a laboratory frame, with the laboratory frame inertial when connected by a Galilean transformation to the universal Newtonian reference frame (Section 12.3). Hence, if the flow in one laboratory frame is steady, then flow in all laboratory frames is steady so long as the laboratory frames are connected by a Galilean transformation (see Section 12.6).

### 15.3.2 General form of the finite domain integral

We are concerned here with the evolution of extensive fluid properties integrated over an arbitrary region. Let us make use of the following notation for such integrals

$$\mathcal{I}[\mathcal{R}(t), t] = \int_{\mathcal{R}(t)} \Pi \rho dV \equiv \int_{\mathcal{R}(t)} \varphi dV, \quad (15.29)$$

where we introduced the shorthand

$$\varphi = \rho \Pi. \quad (15.30)$$

The integrand in equation (15.29) is a function of space and time,  $\varphi = \varphi(\mathbf{x}, t)$ , and the integration region is generally a function of time,  $\mathcal{R}(t)$ . In previous sections,  $\mathcal{R}$  was a material region of fixed matter content (Section 14.3) or a constant mass fluid region open to the exchange of matter with the surroundings (Section 15.1). In both of these cases the region was denoted by  $\mathcal{R}(\mathbf{v})$  since it moved with the fluid flow. Here we make no *a priori* assumption about how the region moves.

The total time derivative of  $\mathcal{I}$  can be written as

$$\frac{d\mathcal{I}}{dt} = \left[ \frac{\partial \mathcal{I}}{\partial t} \right]_{\mathcal{R}} + \frac{d\mathcal{R}}{dt} \left[ \frac{\partial \mathcal{I}}{\partial \mathcal{R}} \right]_t. \quad (15.31)$$

The first term on the right hand side is the time derivative of the integral when holding the region fixed in space as per an Eulerian time derivative. The second term accounts for changes due to evolution of the region as weighted by dependence of the integral on the region itself. How the integral changes in time depends on both the evolution of the fluid property relative to the chosen region and evolution of the fluid region itself. Equation (15.31) is directly analogous to the total time derivative of a field in a moving fluid as given by equation (12.27).

### 15.3.3 Eulerian (static) domain

We first consider an Eulerian domain, which is fixed in space and thus static so that

$$\frac{d\mathcal{I}}{dt} = \left[ \frac{\partial \mathcal{I}}{\partial t} \right]_{\mathcal{R}} = \frac{\partial}{\partial t} \left[ \int_{\mathcal{R}} \Pi \rho dV \right] = \int_{\mathcal{R}} \left[ \frac{\partial (\rho \Pi)}{\partial t} \right] dV. \quad (15.32)$$

Movement of the time derivative across the integral sign is available since the domain boundaries are static; i.e., the second term on the right hand side of equation (15.31) vanishes. Furthermore, since the domain is static, the volume element,  $dV$ , provides a static partition of the total domain volume so that  $dV$  does not appear inside the time derivative. This case corresponds to the Eulerian budgets depicted in Figures 14.1, 14.2, and 15.1.

### 15.3.4 Deriving the Leibniz-Reynolds transport theorem

We now allow the domain boundaries to be time dependent so that both terms in the total time derivative (15.31) contribute. The resulting *Leibniz-Reynolds transport theorem* is a general expression of conservation over an arbitrary region. We derive this theorem here using two methods, one naive and another a bit more rigorous. Interpretation and application of this theorem are then presented in Section 15.3.5.

#### A rectangular region

Consider a one-dimensional domain with time dependent endpoints. Integrals of this type commonly arise when integrating over the depth of the atmosphere or ocean, in which case the boundary terms are replaced by kinematic boundary conditions (see Section 14.4). The chain rule for differentiating integrals is known as *Leibniz's rule*. It results in the time derivative acting on

the upper integral limit, the lower limit, and the integrand

$$\frac{d}{dt} \left[ \int_{x_1(t)}^{x_2(t)} \varphi(x, t) dx \right] = \int_{x_1(t)}^{x_2(t)} \frac{\partial \varphi}{\partial t} dx + \frac{d}{dt} \left[ \int_{x_1(t)}^{x_2(t)} \right] \varphi(x, t) dx \quad (15.33a)$$

$$= \int_{x_1(t)}^{x_2(t)} \frac{\partial \varphi}{\partial t} dx + \frac{dx_2(t)}{dt} \varphi(x_2, t) - \frac{dx_1(t)}{dt} \varphi(x_1, t) \quad (15.33b)$$

$$= \int_{x_1(t)}^{x_2(t)} \left[ \frac{\partial \varphi}{\partial t} + \frac{\partial}{\partial x} \left( \varphi \frac{dx}{dt} \right) \right] dx. \quad (15.33c)$$

As a matter of convenience we brought the boundary terms back inside the integral for the final equality. Importantly, the term  $dx/dt$  is the velocity of the endpoints and so is only defined at the boundary.

We can generalize the one-dimensional result (15.33c) to three dimensions by assuming the three dimensional domain is expressible by Cartesian coordinates whose extents are mutually independent. That is, we assume the domain,  $\mathcal{R}(t)$ , is rectangular. In this case we can immediately generalize equation (15.33c) to

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \varphi dV \right] = \int_{\mathcal{R}} \left[ \frac{\partial \varphi}{\partial t} + \nabla \cdot (\varphi \mathbf{v}^{(b)}) \right] dV = \int_{\mathcal{R}} \frac{\partial \varphi}{\partial t} dV + \oint_{\partial \mathcal{R}} \varphi \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (15.34)$$

where the second equality made use of the divergence theorem to transfer the volume integral into a boundary integral. We also introduced the shorthand for the velocity of a point on the region boundary

$$\mathbf{v}^{(b)} = \frac{d\mathbf{x}}{dt}. \quad (15.35)$$

As for the one-dimensional case, we note that even though  $\mathbf{v}^{(b)}$  appears inside the divergence operator in the middle of equation (15.34), it is defined only on the region boundary,  $\partial \mathcal{R}$ . The identity (15.34) is the *Leibniz-Reynolds transport theorem*.

### An arbitrary simply connected region

We now outline the derivation for an arbitrary simply connected domain,  $\mathcal{R}(t)$ . Besides generalizing the domain geometry, this derivation offers further insight into the transport theorem. For this purpose, again let the region boundary,  $\partial \mathcal{R}$ , have an outward normal,  $\hat{\mathbf{n}}$ , and let points on the boundary move with the velocity,  $\mathbf{v}^{(b)}$ . In Figure 15.2 we depict the region geometry as it evolves over a time step of size,  $\Delta t$ . In particular, this figure illustrates the identity<sup>3</sup>

$$\mathcal{R}(t + \Delta t/2) = \mathcal{R}(t - \Delta t/2) + [\mathcal{R}(t + \Delta t/2) - \mathcal{R}(t - \Delta t/2)], \quad (15.36)$$

with the corresponding equation for the region volume given by

$$\int_{\mathcal{R}(t+\Delta t/2)} dV = \int_{\mathcal{R}(t-\Delta t/2)} dV + \int_{\mathcal{R}(t+\Delta t/2)-\mathcal{R}(t-\Delta t/2)} dV. \quad (15.37)$$

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<sup>3</sup>For those familiar with numerical methods, note that we make use of centered finite time differences in this discussion. Doing so offers a second order accurate expression of the finite difference approximations to the time derivative, whereas forward or backward differences are only first order accurate. Central differences also provides an intuitive centering of the time differences around the central time,  $t$ .

From Figure 15.2 we see that the volume of the time incremented region,  $\mathcal{R}(t+\Delta t/2) - \mathcal{R}(t-\Delta t/2)$ , in the limit  $\Delta t \rightarrow 0$ , is given by

$$\lim_{\Delta t \rightarrow 0} \frac{1}{\Delta t} \int_{\mathcal{R}(t+\Delta t/2) - \mathcal{R}(t-\Delta t/2)} dV = \lim_{\Delta t \rightarrow 0} \frac{1}{\Delta t} \left[ \int_{\mathcal{R}(t+\Delta t/2)} dV - \int_{\mathcal{R}(t-\Delta t/2)} dV \right] \quad (15.38a)$$

$$= \frac{d}{dt} \left[ \int_{\mathcal{R}(t)} dV \right] \quad (15.38b)$$

$$= \oint_{\partial\mathcal{R}(t)} \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (15.38c)$$

This result follows since  $\mathbf{v}^{(b)} \cdot \hat{\mathbf{n}}$  measures the rate that the boundary is moving normal to itself, so that its area integral over  $\partial\mathcal{R}(t)$  measures the rate that the volume of  $\mathcal{R}(t)$  changes.

The same ideas used to derive the volume budget equation (15.38c) are now applied when  $\varphi(\mathbf{x}, t)$  is included within the integral, in which case we consider

$$\frac{d}{dt} \left[ \int_{\mathcal{R}(t)} \varphi(t) dV \right] = \lim_{\Delta t \rightarrow 0} \frac{1}{\Delta t} \left[ \int_{\mathcal{R}(t+\Delta t/2)} \varphi(t + \Delta t/2) dV - \int_{\mathcal{R}(t-\Delta t/2)} \varphi(t - \Delta t/2) dV \right], \quad (15.39)$$

where we suppress the  $\mathbf{x}$  dependence for brevity. Expanding the first integral on the right hand side around the central time leads to the expression, which is accurate to  $\mathcal{O}(\Delta t)^2$ ,

$$\begin{aligned} & \int_{\mathcal{R}(t+\Delta t/2)} \varphi(t + \Delta t/2) dV \\ &= \int_{\mathcal{R}(t)} \left[ \varphi(t) + \frac{\Delta t}{2} \frac{\partial \varphi(t)}{\partial t} \right] dV + \int_{\mathcal{R}(t+\Delta t/2) - \mathcal{R}(t)} \left[ \varphi(t) + \frac{\Delta t}{2} \frac{\partial \varphi(t)}{\partial t} \right] dV. \end{aligned} \quad (15.40)$$

A similar expansion for the second integral in equation (15.39) leads to the finite difference

$$\begin{aligned} & \int_{\mathcal{R}(t+\Delta t/2)} \varphi(t + \Delta t/2) dV - \int_{\mathcal{R}(t-\Delta t/2)} \varphi(t - \Delta t/2) dV \\ &= \Delta t \int_{\mathcal{R}(t)} \frac{\partial \varphi(t)}{\partial t} dV + \int_{\mathcal{R}(t+\Delta t/2) - \mathcal{R}(t-\Delta t/2)} \varphi(t) dV, \end{aligned} \quad (15.41)$$

which is again accurate to  $\mathcal{O}(\Delta t)^2$ . Following our derivation of equation (15.38c) leads us to

$$\int_{\mathcal{R}(t+\Delta t/2) - \mathcal{R}(t-\Delta t/2)} \varphi(t) dV = \Delta t \oint_{\partial\mathcal{R}(t)} \varphi \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (15.42)$$

where all terms on the right hand side are evaluated at the central time,  $t$ . Bringing the pieces together, and taking the limit as  $\Delta t \rightarrow 0$ , leads to the Leibniz-Reynolds transport theorem

$$\frac{d}{dt} \left[ \int_{\mathcal{R}(t)} \varphi(t) dV \right] = \int_{\mathcal{R}(t)} \frac{\partial \varphi}{\partial t} dV + \oint_{\partial\mathcal{R}(t)} \varphi \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (15.43)$$

which agrees with the earlier result given by equation (15.34).

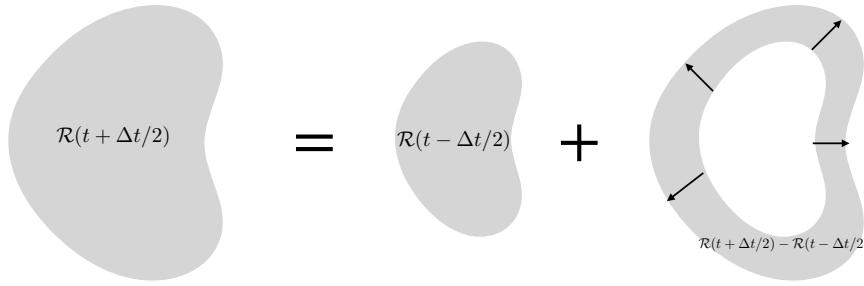


FIGURE 15.2: Illustrating the geometry of the Leibniz-Reynolds transport theorem. The region at time  $t + \Delta t/2$ , is written as  $\mathcal{R}(t + \Delta t/2)$ , which results from changing  $\mathcal{R}(t - \Delta t/2)$  by the increment  $\mathcal{R}(t + \Delta t/2) - \mathcal{R}(t - \Delta t/2)$ . We here depict the case with an expanding boundary that renders a larger volume at  $t + \Delta t/2$ . At each point along the boundary the velocity of the boundary,  $\mathbf{v}^{(b)}$ , has an outward normal projection,  $\mathbf{v}^{(b)} \cdot \hat{\mathbf{n}}$ , with this projection measuring the rate that the boundary moves at that point. Area integrating  $\mathbf{v}^{(b)} \cdot \hat{\mathbf{n}}$  over the boundary yields the rate that the region volume changes.

### 15.3.5 Interpreting the Leibniz-Reynolds transport theorem

The Leibniz-Reynolds transport theorem (15.34) is a central kinematic result in fluid mechanics since it forms the starting point for all finite volume budgets. Although we made use of Cartesian coordinates for both derivations, the result is a coordinate invariant measure of how an extensive fluid property evolves within a region. Hence, by the rules of tensor analysis from Chapter 7, the result holds for arbitrary coordinates. Furthermore, we can extend it to multiply connected domains for which one sums over the distinct sub-domains to render the complete budget. These results confirm our notions regarding extensive properties, such as fluid mass, tracer mass, and enthalpy, and how they are budgeted throughout the fluid. It also holds for vector extensive properties, as we will see when studying the linear momentum equation in Chapter 17.

#### *Comments on the boundary velocity*

The appearance of the boundary velocity,  $\mathbf{v}^{(b)}$ , warrants some comment. As defined by equation (15.35), it measures the velocity of a point on the domain boundary. However, the resulting budget only requires information about the normal component to that velocity,  $\mathbf{v}^{(b)} \cdot \hat{\mathbf{n}}$ . For example, the domain boundary could be exhibiting arbitrary motion in the direction tangent to the bounding surface. However, such tangential motion is of no concern for a budget developed over the domain. The reason is that we are only concerned with transport across the boundary when developing the budget. Indeed, information concerning the tangential component is not available without making dynamical assumptions that go beyond the kinematics considered here.

#### *Transport theorem for region volume*

As part of the general derivation, we derived the expression (15.38c) for the volume changes of the region, which is recovered by setting  $\varphi = 1$  in the transport theorem (15.34)

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} dV \right] = \oint_{\partial\mathcal{R}} \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} dS. \quad (15.44)$$

This result says that the volume for an arbitrary region changes in time so long as there is motion of the region boundary normal to itself. We can compare this expression to that for a material region given by equation (14.25). The expressions are the same since  $\mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} = \mathbf{v} \cdot \hat{\mathbf{n}}$  for a material region. The volume budget (15.44) holds for both compressible and incompressible fluids, with specialization to the incompressible case in Section 16.6.2.

### Transport theorem for a scalar field

We here derive a corollary to the transport theorem (15.34) that proves useful for budget analyses over moving regions, with generalization to the vector linear momentum provided in Section 18.6. For this purpose, make use of the Eulerian flux-form of the scalar conservation equation (15.27) so that the transport theorem is written

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho \Pi dV \right] = - \oint_{\partial \mathcal{R}} \left[ \rho \Pi (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J} \right] \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (15.45)$$

Setting  $\Pi = 1$  gives an expression for the change in mass for the region

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho dV \right] = - \oint_{\partial \mathcal{R}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (15.46)$$

The transport theorem (15.45) has a straightforward interpretation. Namely, the left hand side is the time tendency for the total  $\Pi$ -stuff within the moving region. The right hand side is the surface area integral of the flux of  $\Pi$ -stuff through the boundary of the region. The first right hand side term arises from the difference between the barycentric fluid velocity and the velocity of the boundary, and the second term arises from the diffusive flux. Both fluxes are projected onto the outward normal at the boundary and then integrated over the surface area. Hence, the budget is not affected by fluxes tangential to the boundary. Finally, for the mass budget (15.46), the diffusive flux vanishes since the mass of a fluid element moves according to the barycentric velocity of Section (15.1.2).

In Figure 15.3 we illustrate the transport theorem (15.45) for the special case of a discrete numerical model grid cell. This cell has fixed positions for the vertical sides whereas the top and bottom interfaces are time dependent. This application of the transport theorem provides the framework for finite volume methods in numerical models (e.g., Griffies et al. (2020)). We offer further discussion of the kinematics of such *general vertical coordinate* models in Chapter 42 and their dynamics in Chapter 43.

#### 15.3.6 Revisiting Reynolds transport theorem

We here consider a region that is moving with the fluid flow, in which case we provide a more general derivation of the *Reynolds transport theorem* than originally given for material regions in Section 14.3.4. The following results are special cases of the general expression (15.45).

##### Reynolds Transport Theorem

Let us apply the result (15.34) to a region that follows the fluid flow as defined by the barycentric velocity,  $\mathbf{v}$ . For this moving region, the time derivative of the region boundaries in equation (15.34) is given by the fluid velocity thus leading to

$$\frac{d}{dt} \left[ \int_{\mathcal{R}(\mathbf{v})} \varphi dV \right] = \int_{\mathcal{R}(\mathbf{v})} \left[ \frac{\partial \varphi}{\partial t} + \nabla \cdot (\mathbf{v} \varphi) \right] dV = \int_{\mathcal{R}(\mathbf{v})} \left[ \frac{D\varphi}{Dt} + \varphi \nabla \cdot \mathbf{v} \right] dV. \quad (15.47)$$

This result is the Reynolds transport theorem. The derivation given here is more general than that in Section 14.3.4 where we assumed the region to be material (i.e., no matter crosses the region boundary). For the present derivation we only assumed that the region boundaries move with the barycentric velocity,  $\mathbf{v}$ . We did not assume the region boundaries are material. We can thus make use of Reynolds transport theorem (15.47) for constant mass regions of a multi-component fluid

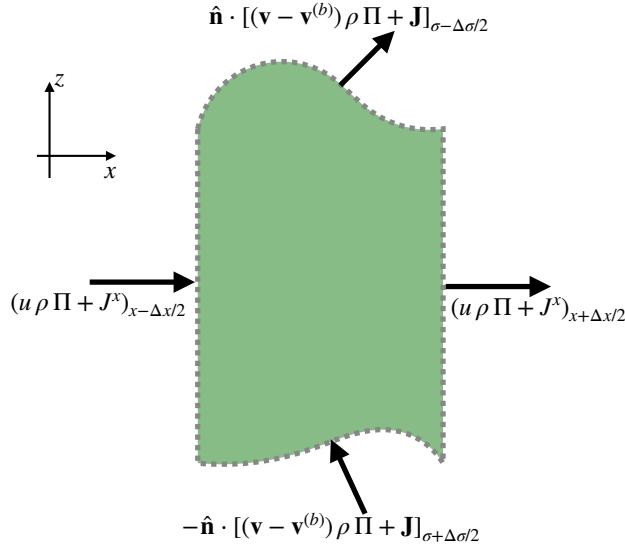


FIGURE 15.3: This figure depicts the contributions to the Leibniz-Reynolds transport theorem (15.45). The theorem is applied to a domain corresponding to a numerical model grid cell with the top and bottom interfaces defined by generalized vertical coordinates of Chapters 41, 42, and 43. In particular, the vertical cell faces are assumed to have fixed positions, so that  $(\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = \mathbf{v} \cdot \hat{\mathbf{n}}$  for these cell faces. Hence, the fluxes crossing these faces are due to advection by the barycentric velocity plus the diffusive flux. However, the top and bottom faces of the cell are allowed to move according to the generalized vertical coordinate surfaces. Hence, transport through these faces must take into account the nonzero velocity of the boundaries. Note that numerical models generally assume the top and bottom interfaces have a nonzero projection in the vertical direction so that they never overturn (e.g., [Griffies et al. \(2020\)](#)).

so long as the region moves with the the barycentric velocity. Furthermore, the region boundary is generally permeable via the diffusion of tracers.

#### *Alternative form of Reynolds Transport Theorem*

We can put the Reynolds Transport Theorem (15.47) into another useful form by reintroducing  $\varphi = \rho \Pi$  and making use of mass continuity

$$\frac{1}{\rho} \frac{D\rho}{Dt} = -\nabla \cdot \mathbf{v}. \quad (15.48)$$

Doing so yields the rather tidy result

$$\frac{d}{dt} \left[ \int_{\mathcal{R}(\mathbf{v})} \Pi \rho dV \right] = \int_{\mathcal{R}(\mathbf{v})} \left[ \frac{D\varphi}{Dt} + \varphi \nabla \cdot \mathbf{v} \right] dV \quad (15.49a)$$

$$= \int_{\mathcal{R}(\mathbf{v})} \left[ \frac{D(\rho \Pi)}{Dt} + \rho \Pi \nabla \cdot \mathbf{v} \right] dV \quad (15.49b)$$

$$= \int_{\mathcal{R}(\mathbf{v})} \left[ \Pi \left( \frac{D\rho}{Dt} + \rho \nabla \cdot \mathbf{v} \right) + \rho \frac{D\Pi}{Dt} \right] dV \quad (15.49c)$$

$$= \int_{\mathcal{R}(\mathbf{v})} \frac{D\Pi}{Dt} \rho dV. \quad (15.49d)$$

Heuristically, this result follows since  $\rho dV$  is a constant when following the flow, so that passage of the time derivative across the integral only picks up the material derivative of  $\Pi$ .

We can take the result (15.49d) one more step by inserting the material form of the scalar

conservation equation (15.27) so that

$$\frac{d}{dt} \left[ \int_{\mathcal{R}(\mathbf{v})} \Pi \rho dV \right] = - \oint_{\partial \mathcal{R}(\mathbf{v})} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (15.50)$$

which is a special case of the general transport theorem (15.45) found by setting  $(\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = 0$  along the region boundary. This result says that the change in  $\Pi$ -stuff within a region moving with the barycentric velocity arises only from the area integrated diffusive flux crossing normal to the boundary. It is a finite volume generalization of the mass conservation statement for a fluid element as discussed in Section 15.1.3. We can set  $\Pi = 1$  to render a statement of mass conservation for a Lagrangian region

$$\frac{d}{dt} \left[ \int_{\mathcal{R}(\mathbf{v})} \rho dV \right] = 0, \quad (15.51)$$

where the diffusive flux,  $\mathbf{J}$ , vanishes for the mass.

### 15.3.7 Summary of the time derivatives acting on integrals

We here summarize the variety of time derivatives acting on integrals of scalar fields

$$\frac{d}{dt} \int_{\mathcal{R}} \rho \Pi dV = \begin{cases} \int_{\mathcal{R}} \frac{\partial(\rho \Pi)}{\partial t} dV = - \oint_{\partial \mathcal{R}} (\rho \mathbf{v} \Pi + \mathbf{J}) \cdot \hat{\mathbf{n}} d\mathcal{S} & \text{Eulerian } \mathcal{R} \\ \int_{\mathcal{R}(\mathbf{v})} \rho \frac{D\Pi}{Dt} dV = - \oint_{\partial \mathcal{R}(\mathbf{v})} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} & \text{Lagrangian } \mathcal{R}(\mathbf{v}) \\ - \oint_{\partial \mathcal{R}} [\rho \Pi (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J}] \cdot \hat{\mathbf{n}} d\mathcal{S} & \text{arbitrary } \mathcal{R}, \end{cases} \quad (15.52)$$

with the scalar fields assumed to satisfy the source-free differential equation

$$\rho \frac{D\Pi}{Dt} = -\nabla \cdot \mathbf{J} \iff \frac{\partial(\rho \Pi)}{\partial t} + \nabla \cdot (\rho \mathbf{v} \Pi + \mathbf{J}) = 0. \quad (15.53)$$

As discussed in Section 12.1, the partial differential equation (15.53) is referred to as the *strong formulation* of the scalar budget, whereas the integral expressions in equation (15.52) provide a variety of *weak formulations*.

## 15.4 Brute force illustration of Leibniz-Reynolds

The Leibniz-Reynolds transport theorem

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = - \int_{\partial \mathcal{R}} [\rho C (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J}] \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (15.54)$$

is an incredibly useful and elegant expression of the tracer budget over an arbitrary domain. Correspondingly, we make great use of it throughout this book. To further our understanding, we here consider the tracer budget for an ocean domain such as in Figure 15.4. Rather than make direct use of Leibniz-Reynolds, we use a brute force approach by expanding the volume integral according to

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = \frac{d}{dt} \left[ \int_{A(t)} dA \int_{\eta_b}^{\eta} \rho C dz \right]. \quad (15.55)$$

In this equation,  $\int_{A(t)} dA$  is an integral over the horizontal area of the domain, with the lateral boundaries of the domain generally a function of time. This exercise requires the use of various

kinematic boundary conditions and provides further practice with the Leibniz rule.

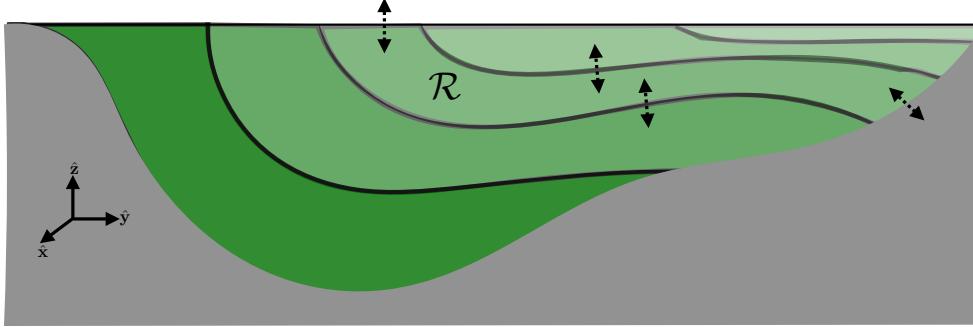


FIGURE 15.4: A depiction of fluid layers in which we formulate the budget for the total mass of tracer (or total potential enthalpy). The tracer mass within the layer, such as that one denoted by  $\mathcal{R}$ , is modified by dia-surface transport across interior layer interfaces, as well as transport across the surface and bottom boundaries. Note that an arbitrary layer might never intersect the bottom or surface boundaries. However, the layers depicted here each intersect boundaries, with such layers requiring extra care in formulating their tracer budgets.

### 15.4.1 Leibniz's rule plus kinematic boundary conditions

Performing the time derivative in equation (15.55) and using Leibniz's rule yields

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = \frac{dA}{dt} \left[ \int_{\eta_b}^{\eta} \rho C dz \right]_{\text{bounds}} + \int_{A(t)} [\partial_t \eta (\rho C)_{z=\eta}] dA + \int_{A(t)} dA \int_{\eta_b}^{\eta} \frac{\partial(\rho C)}{\partial t} dz. \quad (15.56)$$

The first term on the right hand side is evaluated along the lateral boundaries of the domain. If the boundaries are fixed in time, as in a rectangular box of seawater or a periodic channel, then  $dA/dt = 0$ . The more general case has a lateral boundary that is time dependent such as along a beach where fluid moves up and down the sloping shoreline. However, in that case the thickness of fluid vanishes at the lateral boundary,  $\eta - \eta_b = 0$ , thus again revealing that the first term on the right hand side drops from the budget to render

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = \int_{A(t)} [\partial_t \eta (\rho C)_{z=\eta}] dA + \int_{A(t)} dA \int_{\eta_b}^{\eta} \frac{\partial(\rho C)}{\partial t} dz. \quad (15.57)$$

For the second term on the right hand side of equation (15.57) we make use of the tracer equation (15.67) and Leibniz's rule to write

$$\int_{\eta_b}^{\eta} \frac{\partial(\rho C)}{\partial t} dz = - \int_{\eta_b}^{\eta} \nabla_z \cdot (\rho C \mathbf{u} + \mathbf{J}_h) dz - \int_{\eta_b}^{\eta} \frac{\partial(\rho C w + J^z)}{\partial z} dz \quad (15.58a)$$

$$\begin{aligned} &= - \nabla_z \cdot \int_{\eta_b}^{\eta} (\rho C \mathbf{u} + \mathbf{J}_h) dz + \nabla(\eta - z) \cdot (\rho C \mathbf{v} + \mathbf{J})_{z=\eta} \\ &\quad + \nabla(z - \eta_b) \cdot (\rho C \mathbf{v} + \mathbf{J})_{z=\eta_b} \end{aligned} \quad (15.58b)$$

where we wrote  $\mathbf{J} = \mathbf{J}_h + \hat{z} J^z$ . The surface terms ( $z = \eta$ ) combine with the  $\partial_t \eta$  term appearing in equation (15.57) to yield

$$\rho C \left[ \frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla \eta - w \right] = C Q_m, \quad (15.59)$$

where we used the surface kinematic boundary condition (14.79) to introduce the surface boundary mass flux  $Q_m$ . The bottom kinematic boundary condition eliminates the advective contribution

at the bottom,  $z = \eta_b$ , via the no normal flow condition (14.41)

$$\nabla(z - \eta_b) \cdot \mathbf{v} = w - \mathbf{u} \cdot \nabla \eta_b = 0 \quad \text{at } z = \eta_b(x, y). \quad (15.60)$$

Finally, when integrated over the horizontal extent of the domain, the horizontal convergence term from equation (15.58b) vanishes. The reason it vanishes is because either the thickness of fluid vanishes at the horizontal boundaries (as along a beach); there is a no flux boundary condition if the boundary is a vertical wall; or the domain is periodic.

### 15.4.2 Summarizing the result

Bringing the results together yields the budget equation

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = \int_{z=\eta} (C Q_m + \nabla(\eta - z) \cdot \mathbf{J}) dA + \int_{z=\eta_b} \nabla(z - \eta_b) \cdot \mathbf{J} dA. \quad (15.61)$$

We now use the identity (14.68e) between horizontal area element,  $dA = dx dy$ , and area element on the surface

$$\hat{\mathbf{n}} d\mathcal{S} = -\nabla(\eta - z) dA \quad \text{at } z = \eta \quad (15.62a)$$

$$\hat{\mathbf{n}} d\mathcal{S} = -\nabla(z - \eta_b) dA \quad \text{at } z = \eta_b, \quad (15.62b)$$

to write

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = - \int_{z=\eta} (-C Q_m + \hat{\mathbf{n}} \cdot \mathbf{J}) d\mathcal{S} - \int_{z=\eta_b} \hat{\mathbf{n}} \cdot \mathbf{J} d\mathcal{S}, \quad (15.63)$$

where

$$Q_m dA = Q_m d\mathcal{S} = -\rho (\mathbf{v} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (15.64)$$

according to equation (14.73c). The budget for fluid mass is realized by setting  $C$  to a constant and thus dropping the non-advection flux

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho dV \right] = \int_{z=\eta} Q_m d\mathcal{S} = - \int_{z=\eta} \rho (\mathbf{v} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (15.65)$$

The manipulations in this section have succeeded in bringing the tracer and mass budgets into the form of the Leibniz-Reynolds transport theorem (15.54). The process of doing so required far more tedium as compared to the elegance of merely starting from equation (15.54). Even so, our efforts provide a useful means to ground the formalism by unpacking the many steps summarized by Leibniz-Reynolds.

## 15.5 Boundary conditions

We here extend our understanding of boundary conditions relevant at the variety of boundaries encountered by a fluid. We continue to focus on a fluid layer such as shown in Figure 15.4, paying particular interest to fluid layers that intersect surface (as for the ocean) and/or bottom boundaries (as for the ocean or atmosphere). We commonly think of this layer as defined by isosurfaces of generalized vertical coordinates whose layers are monotonically stacked in the vertical according to the discussion from Sections 41.9.1 and 42.3. However, the treatment given here allows for the layers to be non-monotonic in the vertical (e.g., overturns are allowed), so that these results can be used for the water mass transformation analysis discussed in Chapter 50. For example,

the layers can be defined by surfaces of constant Conservative Temperature or salinity within the ocean, with these fields generally exhibiting regions of non-monotonic vertical stratification.

The Leibniz-Reynolds transport theorem (15.45) provides the starting point

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = - \int_{\partial \mathcal{R}} [\rho C (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J}] \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (15.66)$$

where  $C$  is the concentration of a tracer that satisfies the advection-diffusion equation

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho C \mathbf{v} + \mathbf{J}) = 0. \quad (15.67)$$

The left hand side of equation (15.66) is the time tendency for the mass of tracer within the region, such as the region  $\mathcal{R}$  shown in Figure 15.4. This tendency is affected by transport across the layer boundaries, with three boundaries considered here. We ignore interior sources, though note that the formalism can be readily extended in their presence.

### 15.5.1 Interior layer boundary conditions

The boundary transport across interior layer interfaces,

$$\text{interior boundary transport} = [\rho C (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J}] \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (15.68)$$

measures the tracer mass transport due to advective fluxes across the moving layer boundaries (first term) and subgrid scale fluxes (second term). The advective flux is sometimes known as the *dia-surface transport*, with the kinematics of this transport discussed in Section 42.4.

### 15.5.2 Solid-earth boundary conditions

At the bottom boundary, the no-normal flow condition means that

$$\mathbf{v} \cdot \hat{\mathbf{n}} = 0. \quad (15.69)$$

Consider the velocity of a point attached to the layer interface,  $\mathbf{v}^{(b)}$ , and focus on where the interface intersects the bottom boundary. At this point,  $\mathbf{v}^{(b)}$  tracks the position of the interface as it intersects the bottom boundary. By construction, the movement of this intersection point is tangential to the bottom boundary so that it too is orthogonal to the boundary outward normal direction

$$\mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} = 0. \quad (15.70)$$

Hence, the only contribution to the tracer budget at the bottom boundary comes through the non-advective flux  $\mathbf{J}$

$$\text{bottom boundary transport} = -\mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (15.71)$$

This equation says that if there is any transport through the bottom boundary (left hand side), then it induces a non-advective transport within the ocean whose normal component at the boundary equals to the bottom transport (right hand side).

Geothermal heating is the canonical solid-earth transport in the ocean. Assuming a known geothermal heat flux,  $\mathcal{Q}_{\text{geo-heat}}$ , it leads to a non-advective ocean boundary flux

$$\mathcal{Q}_{\text{geo-heat}} = -c_p \mathbf{J}(\Theta) \cdot \hat{\mathbf{n}}, \quad (15.72)$$

where  $c_p$  is the ocean heat capacity and  $\Theta$  is the Conservative Temperature (see Chapter 49).

Furthermore, if we assume the non-advection flux is parameterized as the downgradient diffusive flux (49.54), then the geothermal boundary condition (15.72) takes the form

$$\mathcal{Q}_{\text{geo-heat}} = c_p \rho (\mathbb{K} \cdot \nabla \Theta) \cdot \hat{\mathbf{n}}, \quad (15.73)$$

where  $\mathbb{K}$  is the diffusion tensor (Chapter 48).

For those cases where the geothermal heating vanishes, or more generally for tracers that have zero bottom boundary flux, then the tracer must satisfy the following no-normal flux (Neumann) boundary condition

$$\text{no flux bottom boundary} = (\mathbb{K} \cdot \nabla \Theta) \cdot \hat{\mathbf{n}} = 0. \quad (15.74)$$

In the case where diffusion next to the boundary is isotropic, as per molecular diffusion, then we reach the simpler result

$$\text{no flux bottom boundary} = \nabla C \cdot \hat{\mathbf{n}} = 0. \quad (15.75)$$

Namely, in this case, tracer isosurfaces are oriented normal to the boundary as depicted in Figure 15.5. Notably, this kinematic boundary condition holds at each point in time. For the dynamical tracers like temperature and salinity, this boundary condition affects flow near the boundary by modifying the density field and thus the pressure.

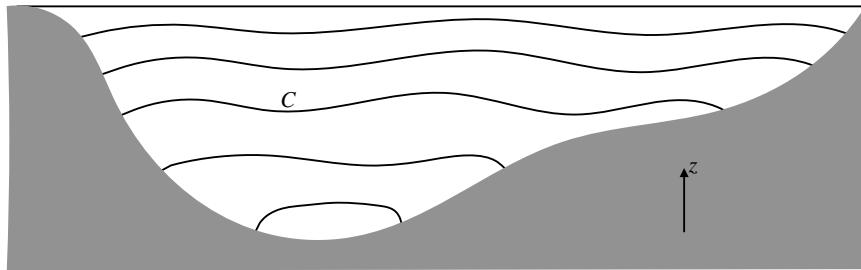


FIGURE 15.5: In the absence of a boundary tracer flux, and in the presence of isotropic downgradient diffusion, the isosurfaces of tracer,  $C$ , intersect solid boundaries normal to the boundary as per equation (15.75):  $\nabla C \cdot \hat{\mathbf{n}} = 0$ , where  $\hat{\mathbf{n}}$  is the outward normal direction. This constraint holds at each time instance.

### 15.5.3 Upper ocean surface boundary conditions

Let us write the upper ocean surface boundary tracer transport as

$$\mathcal{Q}_C d\mathcal{S} = \text{net tracer mass per time crossing ocean surface}. \quad (15.76)$$

The surface boundary transport is generally comprised of two terms: a non-advection term just like at the solid-earth in Section 15.5.2, plus an advective term afforded since the ocean surface is permeable. If we assume that the tracer transported via the advected matter is either a dissolved tracer, such as salinity, or a thermodynamic tracer, such as Conservative Temperature, then we can write the net tracer flux as

$$\mathcal{Q}_C = C_m \mathcal{Q}_m + \mathcal{Q}_C^{\text{non-adv}}, \quad (15.77)$$

where  $\mathcal{Q}_C^{\text{non-adv}}$  is the non-advection tracer flux,  $C_m$  is the tracer concentration within the mass transported across the surface, and  $\mathcal{Q}_m$  the mass per time per surface area of matter that crosses the boundary, as defined according to the kinematic boundary condition (14.63)

$$\mathcal{Q}_m = -\rho \hat{\mathbf{n}} \cdot (\mathbf{v} - \mathbf{v}^{(\eta)}) \quad \text{surface ocean boundary}. \quad (15.78)$$

As for the solid-earth boundary condition, specification of  $\mathcal{Q}_C$  requires information concerning

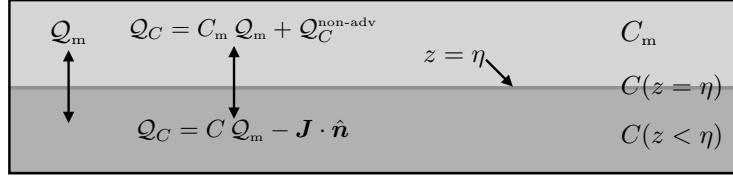


FIGURE 15.6: A schematic of an infinitesimal region of the ocean surface boundary at  $z = \eta(x, y, t)$ , with  $z < \eta$  the ocean.  $\mathcal{Q}_m d\mathcal{S}$  is the mass transport (mass per time) that crosses the interface and carries a tracer concentration  $C_m$ .  $\mathcal{Q}_C d\mathcal{S}$  is the tracer mass transport that crosses the ocean surface. Continuity across the  $z = \eta$  boundary means that the tracer mass transport at  $z = \eta - \epsilon$  (ocean side) equals to that at  $z = \eta + \epsilon$  (atmospheric side), with  $\epsilon > 0$  a tiny number. The tracer concentration at the interface,  $C(z = \eta)$ , is not determined by kinematics. Many analyses and numerical model applications approximate  $C(z = \eta)$  as the bulk tracer concentration within the upper few meters of the ocean. However, as model vertical resolution is refined, this assumption must be reconsidered.

the flux of tracer mass into or out of the ocean, and this flux equals to the net flux on the ocean side of the surface

$$\mathcal{Q}_C = C_m \mathcal{Q}_m + \mathcal{Q}_C^{\text{non-adv}} \equiv -[\rho C (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J}] \cdot \hat{\mathbf{n}} = C \mathcal{Q}_m - \mathbf{J} \cdot \hat{\mathbf{n}}, \quad (15.79)$$

We thus see that the surface transport of tracer mass induces the following non-advective flux within the ocean at  $z = \eta$

$$-\mathbf{J} \cdot \hat{\mathbf{n}} = \mathcal{Q}_C - C \mathcal{Q}_m = \mathcal{Q}_C^{\text{non-adv}} + (C_m - C) \mathcal{Q}_m. \quad (15.80)$$

Figure 15.6 offers a schematic to summarize these results. We make use of these results when discussing the surface ocean boundary conditions in Sections 49.5 and 50.8.3.

## 15.6 Evolution of region mean tracer concentration

We close this chapter by deriving the evolution equations for the domain averaged tracer concentration defined by

$$\langle C \rangle = M^{-1} \int_{\mathcal{R}} \rho C dV \quad \text{with} \quad M = \int_{\mathcal{R}} \rho dV. \quad (15.81)$$

We will then apply the resulting budgets to a numerical model grid cell.

### 15.6.1 Formulation

Use of the product rule leads to

$$\frac{d[\langle C \rangle M]}{dt} = M \frac{d\langle C \rangle}{dt} + \langle C \rangle \frac{dM}{dt} = M \frac{d\langle C \rangle}{dt} - \langle C \rangle \oint_{\partial\mathcal{R}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (15.82)$$

where the second equality made use of the mass budget (15.46). Inserting the transport theorem (15.45) for the left hand side yields

$$M \frac{d\langle C \rangle}{dt} = - \oint_{\partial\mathcal{R}} [\rho [C - \langle C \rangle] (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J}] \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (15.83)$$

The first term on the right hand side vanishes if the averaged concentration equals to the boundary concentration. That is, the region averaged tracer concentration is unchanged if the boundary fluxes of mass have a tracer concentration that matches the region average.

### 15.6.2 Application to a numerical ocean model grid cell

If the region is an ocean model grid cell that is adjacent to the ocean surface (see Figure 15.3 or 15.6), then use of the surface boundary condition (15.79) leads to

$$M \frac{d\langle C \rangle}{dt} = \int_{z=\eta} [C - \langle C \rangle] Q_m dA - \int_{\partial R_{int}} [\rho [C - \langle C \rangle] (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J}] \cdot \hat{\mathbf{n}} d\mathcal{S} - \oint_{\partial R} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (15.84)$$

where  $\partial R_{int}$  is the interior boundary to the grid cell.

As noted above, the first term on the right hand side of equation (15.84) vanishes if  $C(z = \eta) = \langle C \rangle$ . This situation is commonly assumed for temperature in the surface grid cell of an ocean model. That is, the temperature of evaporation, precipitation, and river runoff is commonly taken as the temperature in the surface model grid cell. In contrast,  $C(z = \eta) = 0$  is commonly the case for material tracers such as salt, whose concentration is zero within boundary water fluxes.

## 15.7 Exercises

### EXERCISE 15.1: EQUATION FOR TRACER MASS PER FLUID VOLUME

In some treatments it can be suitable to define a volumetric tracer concentration as the mass of tracer per volume of fluid

$$\phi = \frac{\text{mass of constituent } n \text{ in fluid element}}{\text{volume of fluid element}} = C \rho, \quad (15.85)$$

where  $C$  is the mass concentration defined by equation (15.17) and satisfying the tracer equation (15.21). Derive the corresponding equation satisfied by  $\phi$ .



# Chapter 16

## Non-divergent flows

In this chapter, we study the kinematics of a non-divergent velocity field.<sup>1</sup> In many areas of fluid mechanics, fluids with a non-divergent velocity,  $\nabla \cdot \mathbf{v} = 0$ , are referred to as *incompressible* since the density is assumed to be constant everywhere; i.e., “incompressible”.<sup>2</sup> However, as seen when studying the oceanic Boussinesq fluid in Chapter 23, a non-divergent flow can still admit compressibility effects and the associated density variations. This discussion emphasizes the distinction between a fluid property and a flow property. Namely, the Boussinesq fluid allows for an expression of compressibility (a property of the fluid), whereas the flow admitted by a Boussinesq fluid is non-divergent (a property of the flow). In this chapter we focus on the non-divergent nature of the flow, with the non-divergent velocity written as the curl of a streamfunction. The streamfunction plays a central role in the kinematics of non-divergent flows.

### READER’S GUIDE TO THIS CHAPTER

We presume an understanding of the kinematics of mass conservation from Chapter 14 as well as many of the results from Cartesian tensor analysis in Chapter 2. This chapter introduces many concepts and tools of use in the remainder of the book.

16.1	Introduction to non-divergent flow . . . . .	336
16.2	Kinematic boundary conditions . . . . .	337
16.3	Kinematic free surface equation . . . . .	337
16.4	Streamfunction for two-dimensional flow . . . . .	338
16.4.1	Streamfunction isolines are streamlines . . . . .	338
16.4.2	Streamfunction is constant on material boundaries . . . . .	339
16.4.3	The streamfunction and fluid transport . . . . .	339
16.4.4	Gauge symmetry . . . . .	340
16.4.5	Exact differential formulation . . . . .	340
16.4.6	Concerning the Helmholtz decomposition . . . . .	341
16.4.7	A caveat: transport with curl-free + divergent flow . . . . .	342
16.5	Vector streamfunction for three-dimensional flow . . . . .	342
16.5.1	Gauge symmetry . . . . .	342
16.5.2	Vector streamfunction in the vertical gauge . . . . .	343

<sup>1</sup>A somewhat trivial example of a non-divergent flow is given by  $\mathbf{v}(x, y, z) = u(y, z)\hat{\mathbf{x}} + v(x, z)\hat{\mathbf{y}} + w(x, y)\hat{\mathbf{z}}$ . However, there are far less trivial flows that are non-divergent, such as realized by the oceanic Boussinesq fluid studied in Chapter 23.

<sup>2</sup>In some presentations,  $\nabla \cdot \mathbf{v} = 0$  is referred to as a *solenoidal velocity*, in analog to the non-divergent or solenoidal magnetic field occurring in classical electrodynamics.

16.5.3	The streamfunction and transport through a surface . . . . .	344
16.5.4	Scalar streamfunctions and transport . . . . .	344
16.5.5	Concerning a harmonic velocity potential . . . . .	345
16.6	Evolution of volume and area . . . . .	<b>346</b>
16.6.1	Material volumes and areas . . . . .	346
16.6.2	Arbitrary volume and area . . . . .	346
16.7	Meridional-depth overturning circulation . . . . .	<b>347</b>
16.8	Exercises . . . . .	<b>349</b>

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## 16.1 Introduction to non-divergent flow

For many purposes in fluid mechanics, we can make the simplifying assumption regarding the fluid kinematics whereby the volume of a fluid element is approximated as a constant. In particular, this situation holds for fluid flow satisfying the oceanic Boussinesq approximation (see Chapter 23). Recalling the expression

$$\frac{1}{\delta V} \frac{D(\delta V)}{Dt} = \nabla \cdot \mathbf{v} \quad (16.1)$$

from Section 13.5.1, we see that a constant volume for a fluid element constrains the velocity field to be non-divergent

$$\frac{1}{\delta V} \frac{D(\delta V)}{Dt} = 0 \implies \nabla \cdot \mathbf{v} = 0. \quad (16.2)$$

Flow satisfying  $\nabla \cdot \mathbf{v} = 0$  is said to be *incompressible* since the volume of a fluid element is materially invariant. We illustrate this situation in Figure 16.1.

A slightly less onerous constraint arises from the anelastic approximation, whereby

$$\nabla \cdot (\rho \mathbf{v}) = 0. \quad (16.3)$$

The anelastic approximation is sometimes motivated for the atmosphere. However, it is less commonly used for atmospheric dynamics than the Boussinesq approximation is used for the ocean. We thus focus on the Boussinesq case here, whereby  $\nabla \cdot \mathbf{v} = 0$ .

The non-divergence constraint (16.2) reduces by one the number of functional degrees of freedom possessed by the velocity field. What that means in practice is that we need one fewer velocity component to determine the flow. That is, one velocity component is specified by the other components. This property manifests by our ability to introduce a streamfunction to specify the velocity. We further develop this point in the following.

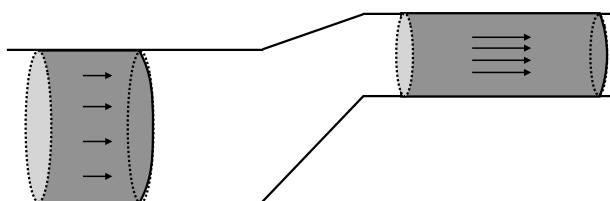


FIGURE 16.1: Illustrating volume continuity for an incompressible liquid flowing in a pipe. On the left the pipe has a relatively large diameter whereas on the right the pipe is narrower. A plug of water on the left moves through the pipe and becomes longer when it moves into the narrower region so that the volume of the plug remains the same. Correspondingly, the speed of the flow increases when moving into the narrower portion of the pipe.

## 16.2 Kinematic boundary conditions

For incompressible flow, there are slight modifications to the compressible boundary conditions detailed in Section 14.4. Whereas the material conditions remain identical, the non-material conditions are applied with a constant reference density,  $\rho_0$ , rather than the local *in situ* density,  $\rho$ . The reason is that we switch from specifying a mass transport condition as per equation (14.63) to a volume transport condition

$$\rho_0 (\mathbf{v} - \mathbf{v}^{(s)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = -Q_m d\mathcal{S} = -Q_m dA \quad \text{moving non-material boundary condition, (16.4)}$$

where the second equality introduced the mass flux per unit horizontal area,  $Q_m$ , according to equation (14.73c). Correspondingly, the kinematic boundary condition (14.79) applied at the ocean free surface takes on the form

$$\rho_0 \frac{D(z - \eta)}{Dt} = -Q_m \implies w + \frac{Q_m}{\rho_0} = \frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla \eta. \quad (16.5)$$

## 16.3 Kinematic free surface equation

We here derive the volume budget over a column of fluid. This budget provides a kinematic expression for the free surface evolution in an incompressible flow. For this purpose, we vertically integrate the non-divergence constraint,  $\nabla \cdot \mathbf{v} = 0$ , over the depth of an ocean column, from  $z = \eta_b(x, y)$  at the bottom to  $z = \eta(x, y, t)$  at the free surface and use the bottom and surface kinematic boundary conditions. This calculation yields

$$0 = \int_{\eta_b}^{\eta} \nabla \cdot \mathbf{v} dz \quad (16.6a)$$

$$= w(\eta) - w(\eta_b) + \int_{\eta_b}^{\eta} \nabla \cdot \mathbf{u} dz \quad (16.6b)$$

$$= w(\eta) - w(\eta_b) + \nabla \cdot \left[ \int_{\eta_b}^{\eta} \mathbf{u} dz \right] - \mathbf{u}(\eta) \cdot \nabla \eta + \mathbf{u}(\eta_b) \cdot \nabla \eta_b \quad (16.6c)$$

$$= [w(\eta) - \mathbf{u}(\eta) \cdot \nabla \eta] - [w(\eta_b) - \mathbf{u}(\eta_b) \cdot \nabla \eta_b] + \nabla \cdot \left[ \int_{\eta_b}^{\eta} \mathbf{u} dz \right], \quad (16.6d)$$

where we made use of Leibniz's Rule to move the horizontal divergence outside of the integral. We now make use of the surface kinematic boundary condition (16.5) and the bottom no-flow condition

$$w(\eta) - \mathbf{u} \cdot \nabla \eta = -\frac{Q_m}{\rho_0} + \frac{\partial \eta}{\partial t} \quad z = \eta \quad (16.7a)$$

$$w = \mathbf{u} \cdot \nabla \eta_b \quad z = \eta_b \quad (16.7b)$$

to render the free surface equation for a fluid with a non-divergent flow

$$\frac{\partial \eta}{\partial t} = \frac{Q_m}{\rho_0} - \nabla \cdot \mathbf{U}, \quad (16.8)$$

where

$$\mathbf{U} = \int_{\eta_b}^{\eta} \mathbf{u} dz \quad (16.9)$$

is the depth integrated horizontal transport. For the special case of a steady state with zero boundary mass flux, the depth integrated flow is non-divergent

$$\nabla \cdot \mathbf{U} = 0 \quad \text{if } Q_m = 0 \text{ and } \partial\eta/\partial t = 0. \quad (16.10)$$

Comparing the incompressible free surface quation (16.8) to the compressible free surface equation (14.84) indicates that the incompressible case is missing a contribution from the material changes in density. These changes arise from mixing and boundary fluxes of buoyancy. The absence of an impact from surface buoyancy fluxes means that the free surface in a Boussinesq fluid is not impacted by global thermal expansion, such as that arising from ocean warming. [Greatbatch \(1994\)](#) and [Griffies and Greatbatch \(2012\)](#) provide a recipe for diagnostically addressing this formulational limitation, thus enabling the study of global mean sea level with Boussinesq ocean models.

## 16.4 Streamfunction for two-dimensional flow

Vertical stratification of buoyancy plus the effects from planetary rotation inhibit vertical motion in geophysical flows. Therefore, as an idealization it is sometimes useful to assume the geophysical fluid flow is horizontal (two-dimensional) as well as non-divergent. The incompressible constraint for two-dimensional flow can be satisfied by writing the horizontal velocity in the form

$$\mathbf{u} = \nabla \times (z \nabla \psi) = \hat{\mathbf{z}} \times \nabla \psi = -\hat{\mathbf{x}} \frac{\partial \psi}{\partial y} + \hat{\mathbf{y}} \frac{\partial \psi}{\partial x}, \quad (16.11)$$

where

$$\nabla_z = \hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y \quad (16.12)$$

is the horizontal gradient operator. The constraint  $\nabla_z \cdot \mathbf{u} = 0$  is satisfied since the partial derivative operators commute

$$\frac{\partial^2 \psi}{\partial x \partial y} = \frac{\partial^2 \psi}{\partial y \partial x}. \quad (16.13)$$

We refer to  $\psi$  as the *streamfunction*, with this name motivated by the following considerations.

Note that in this section we could relax notation by dispensing with the  $z$  subscript on the horizontal gradient operator,  $\nabla_z$ , since we are here concerned only with two-dimensional horizontal flow. However, it is useful to be a bit pedantic to distinguish the two-dimensional formulations in this section from the analogous three-dimensional case considered in Section 16.5.

### 16.4.1 Streamfunction isolines are streamlines

At any fixed time, the total differential of the streamfunction is

$$d\psi = \frac{\partial \psi}{\partial x} dx + \frac{\partial \psi}{\partial y} dy = v dx - u dy, \quad (16.14)$$

where the second equality follows from equation (16.11). Instantaneous lines along which  $\psi$  is a constant satisfy

$$d\psi = 0 \implies \frac{dx}{u} = \frac{dy}{v}. \quad (16.15)$$

Furthermore, the normal direction to constant  $\psi$  lines

$$\hat{\mathbf{n}} = \frac{\nabla_z \psi}{|\nabla_z \psi|} = \frac{v \hat{\mathbf{x}} - u \hat{\mathbf{y}}}{|\mathbf{u}|} \quad (16.16)$$

is normal to the velocity

$$\mathbf{u} \cdot \nabla_z \psi = u v - v u = 0. \quad (16.17)$$

Consequently, at each time instance, lines of constant  $\psi$  are streamlines (see Section 12.8.2 for discussion of streamlines). This property motivates the name *streamfunction*. Furthermore, through each point of a two-dimensional non-divergent flow and at any particular instance in time, there is one and only one streamline passing through that point.

### 16.4.2 Streamfunction is constant on material boundaries

As a corollary to the results from Section 16.4.1, we know that the streamfunction is a spatial constant when evaluated along material boundaries where  $\mathbf{u} \cdot \hat{\mathbf{n}} = 0$ . This property follows from equation (16.17). We can also see it from

$$0 = \mathbf{u} \cdot \hat{\mathbf{n}} = (\hat{\mathbf{z}} \times \nabla_z \psi) \cdot \hat{\mathbf{n}} = (\hat{\mathbf{n}} \times \hat{\mathbf{z}}) \cdot \nabla_z \psi = \hat{\mathbf{t}} \cdot \nabla_z \psi, \quad (16.18)$$

where  $\hat{\mathbf{t}}$  a unit vector pointing tangent to the boundary. The operator  $\hat{\mathbf{t}} \cdot \nabla_z \psi$  is the derivative of  $\psi$  computed along the boundary tangent at any given point along the boundary. Hence,  $\hat{\mathbf{t}} \cdot \nabla_z \psi = 0$  means that  $\psi$  is a spatial constant along the boundary. Even though spatially constant,  $\psi$  along the boundary is generally a function of time.

### 16.4.3 The streamfunction and fluid transport

Consider an arbitrary curve in the fluid with endpoints  $\mathbf{x}_1$  and  $\mathbf{x}_2$  as depicted in Figure 16.2. At any particular time instance, the difference in streamfunction between these two points is given by

$$\psi(\mathbf{x}_2) - \psi(\mathbf{x}_1) = \int_{\mathbf{x}_1}^{\mathbf{x}_2} d\psi = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \left[ dx \frac{\partial \psi}{\partial x} + dy \frac{\partial \psi}{\partial y} \right] = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \nabla_z \psi \cdot d\mathbf{x} = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \nabla_z \psi \cdot \hat{\mathbf{t}} ds. \quad (16.19)$$

For the final equality we wrote

$$d\mathbf{x} = \hat{\mathbf{t}} ds, \quad (16.20)$$

where

$$ds = |\mathbf{d}\mathbf{x}| \quad (16.21)$$

is the element of arc-length along the curve, and  $\hat{\mathbf{t}}$  is a unit tangent vector that points in the direction along the curve from  $\mathbf{x}_1$  to  $\mathbf{x}_2$ . Now introduce the normal vector along the curve according to

$$\hat{\mathbf{t}} = \hat{\mathbf{n}} \times \hat{\mathbf{z}}, \quad (16.22)$$

where  $\hat{\mathbf{n}}$  points to the left when facing in the  $\hat{\mathbf{t}}$  direction. We thus have

$$\psi(\mathbf{x}_2) - \psi(\mathbf{x}_1) = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \nabla_z \psi \cdot (\hat{\mathbf{n}} \times \hat{\mathbf{z}}) ds = \int_{\mathbf{x}_1}^{\mathbf{x}_2} (\hat{\mathbf{z}} \times \nabla_z \psi) \cdot \hat{\mathbf{n}} ds = \int_{\mathbf{x}_1}^{\mathbf{x}_2} \mathbf{u} \cdot \hat{\mathbf{n}} ds, \quad (16.23)$$

with the final equality an expression for the net area transport of fluid normal to the curve (dimensions of area per time). As the chosen curve connecting the points is arbitrary, we conclude that the difference in streamfunction values between two points measures the transport across any

curve connecting the points. Correspondingly, the stronger the gradient in the streamfunction, the larger the transport since

$$|\mathbf{u}| = |\nabla_z \psi|. \quad (16.24)$$

The connection between the transport between two points and the value of the streamfunction at those two points sometimes prompts the name *transport streamfunction*. More specifically, this term is used when the streamfunction is computed for the depth integrated flow (16.9), in the special case when that flow has no divergence,  $\nabla \cdot \mathbf{U} = 0$ . In this case we can write

$$\mathbf{U} = \nabla \times (z \nabla \Psi) = \hat{\mathbf{z}} \times \nabla \Psi, \quad (16.25)$$

where  $\Psi$  is known as the *transport streamfunction* and it has dimensions  $L^3 T^{-1}$ .

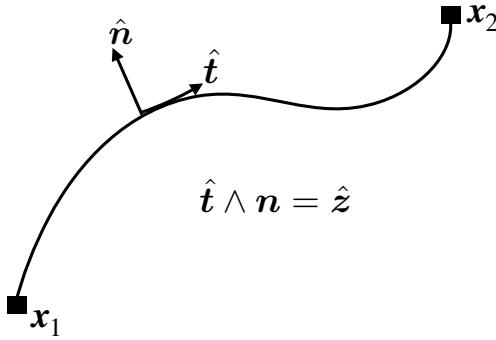


FIGURE 16.2: Depicting the transport between two points in a two-dimensional fluid. The transport is the line integral,  $\int_{x_1}^{x_2} \mathbf{u} \cdot \hat{\mathbf{n}} ds$ , from point  $x_1$  to  $x_2$ , with the normal direction  $\hat{\mathbf{n}}$  pointing to the left when facing in the direction of the local tangent vector,  $\hat{\mathbf{t}}$ . By construction,  $\hat{\mathbf{t}} \times \hat{\mathbf{n}} = \hat{\mathbf{z}}$ , where  $\hat{\mathbf{z}}$  points vertically out of the page. For a two-dimensionally incompressible flow,  $\nabla_z \cdot \mathbf{u} = 0$ , the transport between any two points is the difference in the streamfunction computed at these points,  $\int_{x_1}^{x_2} \mathbf{u} \cdot \hat{\mathbf{n}} ds = \psi(x_1) - \psi(x_2)$ . This result holds regardless the path taken between these two points, so long as the path remains simple; i.e., it does not intersect itself.

#### 16.4.4 Gauge symmetry

For a two-dimensional non-divergent flow, the constraint  $\nabla_z \cdot \mathbf{u} = 0$  reduces the functional degrees of freedom from two (the two velocity components ( $u, v$ )) to one (the streamfunction). However, the streamfunction is arbitrary up to a constant,  $k$ , since

$$\psi' = \psi + k \Rightarrow \mathbf{u}' = \mathbf{u}. \quad (16.26)$$

So the value of the streamfunction at a particular point has no unambiguous physical meaning. Rather, only the difference in streamfunction between two points is physically relevant. The ability to add a constant to the streamfunction is termed a *gauge symmetry*. We return to gauge symmetry for the three dimensional flow in Section 16.5.1.

#### 16.4.5 Exact differential formulation

We here connect our discussion of velocity streamfunction to the discussion of exact differentials in Section 2.8. For that purpose introduce the differential

$$\mathbf{A} \cdot d\mathbf{x} \equiv (\mathbf{u} \times \hat{\mathbf{z}}) \cdot d\mathbf{x} = v dx - u dy. \quad (16.27)$$

By construction

$$\hat{\mathbf{z}} \cdot (\nabla_z \times \mathbf{A}) = 0 \quad \text{since} \quad \nabla_z \cdot \mathbf{u} = 0, \quad (16.28)$$

which means that  $\mathbf{A} \cdot d\mathbf{x}$  is an exact differential (Section 2.8.1). Consequently, we can write

$$\mathbf{A} \cdot d\mathbf{x} = (\mathbf{u} \times \hat{\mathbf{z}}) \cdot d\mathbf{x} = \nabla_z \psi \cdot d\mathbf{x} = d\psi, \quad (16.29)$$

which then leads to the results derived earlier in this section where  $\psi$  is the transport streamfunction.

### 16.4.6 Concerning the Helmholtz decomposition

We close our discussion in this section by tidying up some mathematical niceties concerning the Helmholtz decomposition introduced in Section 2.9. For two-dimensional flows the decomposition takes the form

$$\mathbf{u} = \hat{\mathbf{z}} \times \nabla_z \Gamma + \nabla_z \Phi, \quad (16.30)$$

for some functions  $\Gamma$  and  $\Phi$ . For non-divergent flows,  $\Phi$  is constrained to be harmonic<sup>3</sup>

$$\nabla \cdot \mathbf{u} = 0 \implies \nabla_z^2 \Phi = \nabla_z \cdot \nabla_z \Phi = 0. \quad (16.31)$$

As summarized in Table 16.1, it is sufficient to make use of just a streamfunction,  $\psi$ , for vortical flow and just a *velocity potential*,  $\phi$ , for irrotational flow.<sup>4</sup> In the following we verify why it is sufficient to make use of this truncated version of the Helmholtz decomposition for non-divergent two-dimensional flows.

NON-DIVERGENT VORTICAL FLOW	NON-DIVERGENT IRROTATIONAL FLOW
$\nabla_z \cdot \mathbf{u} = 0$	$\nabla_z \cdot \mathbf{u} = 0$
$\nabla_z \times \mathbf{u} \neq 0$	$\nabla_z \times \mathbf{u} = 0$
$\mathbf{u} = \hat{\mathbf{z}} \times \nabla_z \psi$	$\mathbf{u} = \nabla_z \phi$
$\hat{\mathbf{z}} \cdot (\nabla_z \times \mathbf{u}) = \nabla_z^2 \psi$	$\nabla_z^2 \phi = 0.$

TABLE 16.1: Summarizing some mathematical properties of non-divergent two-dimensional velocity fields,  $\nabla \cdot \mathbf{u} = 0$ . The streamfunction is  $\psi$  whereas the harmonic velocity potential is  $\phi$ .

#### Non-divergent vortical flow

Return to the exact differential formulation from Section 16.4.5. In that formulation we noted that  $\nabla_z \cdot \mathbf{u} = 0$  means that the differential  $\mathbf{A} \cdot d\mathbf{x} = (\mathbf{u} \times \hat{\mathbf{z}}) \cdot d\mathbf{x}$  is exact. Making use of the Helmholtz decomposition (16.30) renders

$$\mathbf{A} \cdot d\mathbf{x} = (\mathbf{u} \times \hat{\mathbf{z}}) \cdot d\mathbf{x} \quad (16.32a)$$

$$= [(\hat{\mathbf{z}} \times \nabla_z \Gamma) \times \hat{\mathbf{z}} + \nabla_z \Phi \times \hat{\mathbf{z}}] \cdot d\mathbf{x} \quad (16.32b)$$

$$= [\nabla_z \Gamma + \nabla_z \Phi \times \hat{\mathbf{z}}] \cdot d\mathbf{x}. \quad (16.32c)$$

To reveal the exactness of the right hand side requires the harmonic property of  $\Phi$  so that we can write

$$\hat{\mathbf{z}} \cdot [\nabla_z \times (\nabla_z \Phi \times \hat{\mathbf{z}})] = -\nabla_z^2 \Phi = 0 \implies \nabla_z \Phi \times \hat{\mathbf{z}} \equiv \nabla_z \Upsilon, \quad (16.33)$$

in which case

$$\mathbf{A} \cdot d\mathbf{x} \equiv v dx - u dy = d(\Gamma + \Upsilon) \equiv d\psi. \quad (16.34)$$

<sup>3</sup>Recall our discussion of harmonic functions in Sections 2.2.2 and 3.5.1.

<sup>4</sup>The vorticity,  $\nabla_z \times \mathbf{u}$ , is a measure of the spin in the fluid and is the focus of Part VI of this book.

We conclude that for non-divergent vortical flow, we lose no generality by working just with the streamfunction,  $\psi$ , of Section 16.4.3. There is no need to also include a harmonic function.

#### *Non-divergent irrotational flow*

The discussion is analogous for non-divergent and irrotational flow, with the irrotational condition holding so long as  $\Gamma$  is harmonic

$$\hat{z} \cdot [\nabla_z \times (\hat{z} \times \nabla_z \Gamma)] = \nabla_z^2 \Gamma = 0. \quad (16.35)$$

Consequently, we can write

$$\hat{z} \times \nabla_z \Gamma = \nabla_z \gamma, \quad (16.36)$$

in which case

$$\mathbf{u} = \hat{z} \times \nabla_z \Gamma + \nabla_z \Phi = \nabla_z (\gamma + \Phi) \equiv \nabla_z \phi. \quad (16.37)$$

Hence, for non-divergent irrotational flow, it is sufficient to work just with the harmonic velocity potential,  $\phi$ .

#### 16.4.7 A caveat: transport with curl-free + divergent flow

Consider a horizontal velocity that has a non-zero divergence,  $\nabla \cdot \mathbf{u} \neq 0$ , and yet it has a zero curl,  $\nabla \times \mathbf{u} = 0$ . The zero curl allows us to write  $\mathbf{u} = \nabla_z \phi$ , with  $\phi$  the velocity potential. Hence,  $d\Phi = \nabla_z \phi \cdot d\mathbf{x}$  is an exact differential and so its closed loop integral vanishes:  $\oint d\Phi = 0$ . However, there is no connection between velocity potential and transport. That is, we cannot conclude anything about the net transport across a closed curve based on properties of  $\phi$ .

## 16.5 Vector streamfunction for three-dimensional flow

A three-dimensional non-divergent velocity,  $\nabla \cdot \mathbf{v} = 0$ , can be specified by a vector streamfunction

$$\mathbf{v} = \nabla \times \Psi. \quad (16.38)$$

The constraint  $\nabla \cdot \mathbf{v} = 0$  is trivially satisfied since the divergence of the curl vanishes

$$\nabla \cdot (\nabla \times \Psi) = 0. \quad (16.39)$$

As we will see, the non-divergence condition reduces the three functional degrees of freedom for  $\mathbf{v}$  from two plus a gauge function.

#### 16.5.1 Gauge symmetry

For three-dimensional non-divergent flow, the constraint  $\nabla \cdot \mathbf{v} = 0$  reduces the three functional degrees of freedom down to the two available from the vector streamfunction,  $\mathbf{v} = \nabla \times \Psi$ . Gauge symmetry manifests through the ability to add the gradient of an arbitrary function to  $\Psi$  without altering  $\mathbf{v}$ :

$$\Psi' = \Psi + \nabla \lambda \Rightarrow \mathbf{v}' = \mathbf{v}, \quad (16.40)$$

which follows since  $\nabla \times \nabla \lambda = 0$ . Hence, the vector streamfunction has no absolute physical meaning since we can always modify the streamfunction by adding an arbitrary gauge function. Even so, we find it useful to consider certain vector streamfunctions that have direct connection to fluid transport, as discussed above in Section 16.5.3.

### 16.5.2 Vector streamfunction in the vertical gauge

We here exploit gauge symmetry to determine the transport streamfunction that is related to the horizontal volume transport of fluid beneath a chosen depth. For this purpose, write the component expression for the velocity

$$u = \frac{\partial \Psi_3}{\partial y} - \frac{\partial \Psi_2}{\partial z} \quad \text{and} \quad v = \frac{\partial \Psi_1}{\partial z} - \frac{\partial \Psi_3}{\partial x} \quad \text{and} \quad w = \frac{\partial \Psi_2}{\partial x} - \frac{\partial \Psi_1}{\partial y}, \quad (16.41)$$

where the Cartesian components to the vector streamfunction are

$$\Psi = \hat{x} \Psi_1 + \hat{y} \Psi_2 + \hat{z} \Psi_3. \quad (16.42)$$

We follow studies of ocean mesoscale eddy parameterizations (e.g., see Sections 46.7.1 and 48.1) by choosing the *vertical gauge*. In this gauge we set  $\nabla \lambda$  to precisely cancel the third component of the vector streamfunction so that

$$\Psi_3 = 0 \iff \text{vertical gauge}, \quad (16.43)$$

which then renders

$$u = -\frac{\partial \Psi_2}{\partial z} \quad \text{and} \quad v = \frac{\partial \Psi_1}{\partial z} \quad \text{and} \quad w = \frac{\partial \Psi_2}{\partial x} - \frac{\partial \Psi_1}{\partial y}. \quad (16.44)$$

Vertically integrating the  $u, v$  equations from the bottom at  $z = \eta_b(x, y)$  up to an arbitrary geopotential leads to

$$\Psi = \int_{\eta_b}^z \mathbf{u} dz' \times \hat{z} \equiv \mathbf{U}(z) \times \hat{z}, \quad (16.45)$$

where  $\mathbf{U}(z) = \int_{\eta_b}^z \mathbf{u} dz'$  is the horizontal transport of fluid beneath a chosen vertical position. By construction,  $u = -\partial \Psi_2 / \partial z$  and  $v = \partial \Psi_1 / \partial z$ . We verify that this streamfunction also renders  $w$  through noting that

$$\frac{\partial \Psi_2}{\partial x} = u(\eta_b) \partial_x \eta_b - \int_{\eta_b}^z \partial_x u dz' \quad \text{and} \quad \frac{\partial \Psi_1}{\partial y} = \int_{\eta_b}^z \partial_y v dz' - v(\eta_b) \partial_y \eta_b, \quad (16.46)$$

so that

$$\frac{\partial \Psi_2}{\partial x} - \frac{\partial \Psi_1}{\partial y} = \mathbf{u}(\eta_b) \cdot \nabla \eta_b - \int_{\eta_b}^z \left[ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right] dz' = w(\eta_b) + \int_{\eta_b}^z \frac{\partial w}{\partial z'} dz' = w(z), \quad (16.47)$$

where we used the bottom kinematic boundary condition (14.41) to write  $w - \mathbf{u} \cdot \nabla \eta_b = 0$  at  $z = \eta_b(x, y)$ . Hence, knowledge of the vector streamfunction (16.45) offers a means to compute the three velocity components. Of course, the velocity is needed to compute the vector streamfunction! Even though the logic is circular, we are satisfied that the circle closes to reveal self-consistency of the formalism. Furthermore, in some contexts it is more suitable to first compute the transport than the velocity, such as in ocean mesoscale eddy parameterizations (e.g., Chapter 9 of Griffies (2004)). We also note that the transport is a smoother field than the velocity given that it is computed as an integral of the velocity.

We close by noting that the transport through the solid-earth bottom at  $z = \eta_b(x, y)$  vanishes according to equation (16.50). We can trivially verify this result for the vertical gauge since

$$\Psi(z = \eta_b) = 0, \quad (16.48)$$

so that  $\oint_{\partial\mathcal{S}} \Psi \cdot \hat{\mathbf{t}} \, ds = 0$  on the bottom.

### 16.5.3 The streamfunction and transport through a surface

The volume transport (volume per time) of fluid crossing a surface is defined by the area integral

$$\mathcal{T}(\mathcal{S}) = \int_{\mathcal{S}} \mathbf{v} \cdot \hat{\mathbf{n}} \, d\mathcal{S}, \quad (16.49)$$

where  $\hat{\mathbf{n}}$  is the outward unit normal vector on the surface. Introducing the vector streamfunction and making use of Stokes' Theorem (Section 2.6) then leads to

$$\mathcal{T}(\mathcal{S}) = \int_{\mathcal{S}} \mathbf{v} \cdot \hat{\mathbf{n}} \, d\mathcal{S} = \int_{\mathcal{S}} (\nabla \times \Psi) \cdot \hat{\mathbf{n}} \, d\mathcal{S} = \oint_{\partial\mathcal{S}} \Psi \cdot \hat{\mathbf{t}} \, ds, \quad (16.50)$$

where  $\hat{\mathbf{t}} \, ds$  is the oriented arc distance increment along the boundary of  $\mathcal{S}$ , and  $\oint_{\partial\mathcal{S}}$  is the oriented line integral around the boundary  $\partial\mathcal{S}$ . Hence, the volume transport of fluid through the surface depends only on the vector streamfunction on the perimeter of the surface. Furthermore, if the transport through the surface vanishes (e.g., no-flux material surface such as a solid earth boundary), then on the surface the vector streamfunction can be written as the gradient of an arbitrary scalar field,  $\Psi = \nabla\chi$ , since

$$\oint_{\partial\mathcal{S}} \Psi \cdot \hat{\mathbf{t}} \, ds = \oint_{\partial\mathcal{S}} \nabla\chi \cdot \hat{\mathbf{t}} \, ds = \oint_{\partial\mathcal{S}} \nabla\chi \cdot d\mathbf{x} = \oint_{\partial\mathcal{S}} d\chi = 0. \quad (16.51)$$

Because  $\Psi$  has a connection to fluid transport, we sometimes refer to it as the *transport streamfunction*, just as for the streamfunction  $\psi$  in two-dimensional non-divergent flows (Section 16.4.3).

### 16.5.4 Scalar streamfunctions and transport

We can expose the two degrees of freedom of the vector streamfunction by writing it as the product

$$\Psi = \gamma \nabla\psi \quad (16.52)$$

so that the velocity is given by

$$\mathbf{v} = \nabla \times \Psi = \nabla\gamma \times \nabla\psi. \quad (16.53)$$

By construction the velocity satisfies

$$\mathbf{v} \cdot \nabla\gamma = \mathbf{v} \cdot \nabla\psi = 0, \quad (16.54)$$

so that the velocity is parallel to surfaces of constant  $\gamma$  and  $\psi$ . Correspondingly, the velocity streamlines are intersections of the  $\gamma$  and  $\psi$  isosurfaces, as depicted in Figure 16.3. We thus refer to  $\gamma$  and  $\psi$  as the two *scalar streamfunctions* for the three dimensional non-divergent flow. However, note that  $\gamma$  and  $\psi$  have different dimensions. By convention, we choose  $\gamma$  to have dimensions of length, so that it is not a traditional streamfunction, whereas  $\psi$  to has the typical streamfunction dimensions of squared length per time.

As a check that the formalism is sensible, consider the special case of two-dimensional flow so that all streamlines are in the horizontal  $x$ - $y$  plane. Taking  $\gamma = z$  then renders

$$\Psi = z \nabla\psi \quad \text{and} \quad \mathbf{v} = \nabla \times \Psi = \hat{z} \times \nabla\psi, \quad (16.55)$$

which agrees with the scalar streamfunction in equation (16.11) for two dimensional non-divergent

flow.

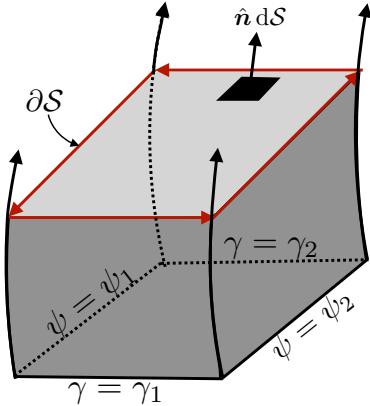


FIGURE 16.3: Isosurfaces of constant scalar streamfunctions,  $\gamma$  and  $\psi$ , for a three dimensional non-divergent flow. Streamlines are defined by the intersections of the  $\gamma$  and  $\psi$  isosurfaces, as shown by four streamlines along the corners of this particular volume. The volume transport of fluid through the surface,  $\mathcal{S}$ , is determined by the line integral,  $\oint_{\partial\mathcal{S}} \gamma \, d\psi = - \oint_{\partial\mathcal{S}} \psi \, d\gamma = (\gamma_1 - \gamma_2)(\psi_2 - \psi_1)$ , around the boundary circuit.

The volume transport through a surface defined by the two streamfunction isosurfaces takes the form

$$\mathcal{T}(\mathcal{S}) = \int_{\mathcal{S}} \mathbf{v} \cdot \hat{\mathbf{n}} \, d\mathcal{S} = \oint_{\partial\mathcal{S}} \Psi \cdot \hat{\mathbf{t}} \, ds = \oint_{\partial\mathcal{S}} \gamma \nabla \psi \cdot \hat{\mathbf{t}} \, ds = \oint_{\partial\mathcal{S}} \gamma \, d\psi = - \oint_{\partial\mathcal{S}} \psi \, d\gamma. \quad (16.56)$$

To reach the penultimate step we set

$$d\psi = \nabla \psi \cdot d\mathbf{x} = \nabla \psi \cdot \hat{\mathbf{t}} \, ds, \quad (16.57)$$

and for the final step we used the identity

$$\oint_{\partial\mathcal{S}} \gamma \, d\psi = \oint_{\partial\mathcal{S}} d(\gamma \psi) - \oint_{\partial\mathcal{S}} \psi \, d\gamma = - \oint_{\partial\mathcal{S}} \psi \, d\gamma, \quad (16.58)$$

which follows since  $\oint_{\partial\mathcal{S}} d(\gamma \psi) = 0$ . The volume transport for the particular surface shown in Figure 16.3 is given by

$$\mathcal{T}(\mathcal{S}) = \oint_{\partial\mathcal{S}} \gamma \, d\psi = \gamma_1 (\psi_2 - \psi_1) + \gamma_2 (\psi_1 - \psi_2) = (\gamma_1 - \gamma_2)(\psi_2 - \psi_1). \quad (16.59)$$

Hence, the volume transport through a streamtube defined by isosurfaces of  $\gamma$  and  $\psi$  is given by the product of the difference between the isosurfaces.

### 16.5.5 Concerning a harmonic velocity potential

As for the two-dimensional case discussed in Section 16.4.6, we consider the relevance of an arbitrary harmonic velocity potential,  $\chi$ , so that the velocity takes the form

$$\mathbf{v} = \nabla \times \boldsymbol{\Gamma} + \nabla \chi \quad \text{with} \quad \nabla^2 \chi = 0. \quad (16.60)$$

Since  $\nabla \cdot \nabla \chi = 0$  we can write  $\nabla \chi$  as the curl of another vector

$$\nabla \cdot \nabla \chi = 0 \implies \nabla \chi = \nabla \times \boldsymbol{\Lambda}, \quad (16.61)$$

in which case the velocity takes the form

$$\mathbf{v} = \nabla \times \boldsymbol{\Gamma} + \nabla \phi = \nabla \times (\boldsymbol{\Gamma} + \boldsymbol{\Lambda}) \equiv \nabla \times \boldsymbol{\Psi}. \quad (16.62)$$

Consequently, just as for the two-dimensional case, we are at liberty to work with the transport streamfunction  $\boldsymbol{\Psi}$  if that suits our needs. Otherwise, we can work with the harmonic potential,  $\chi$ , which is commonly used when the velocity is both non-divergent and irrotational.

## 16.6 Evolution of volume and area

In this section we develop kinematic equations for the evolution of volume and area within a non-divergent flow. We start by considering a material region and then study an arbitrary region.

### 16.6.1 Material volumes and areas

As shown by equation (16.2), the volume of a material parcel remains materially constant in a non-divergent flow. Correspondingly, a material fluid region maintains a constant volume

$$\frac{d}{dt} \int_{\mathcal{R}(\mathbf{v})} dV = \int_{\mathcal{R}(\mathbf{v})} \frac{D(\delta V)}{Dt} = \int_{\mathcal{R}(\mathbf{v})} (\nabla \cdot \mathbf{v}) dV = 0. \quad (16.63)$$

The appearance of a material time derivative on the inside of the integral arises since the integral is computed following material fluid particles whose trajectories define integral curves of the flow (see Section 15.3.7). Likewise, following from the material area element equation (13.68), the area of a material region in a two-dimensional incompressible flow remains materially constant

$$\frac{d}{dt} \int_{\mathcal{S}(\mathbf{v})} d\mathcal{S} = \int_{\mathcal{S}(\mathbf{v})} \frac{D(\delta \mathcal{S})}{Dt} = \int_{\mathcal{S}(\mathbf{v})} (\nabla \cdot \mathbf{u}) d\mathcal{S} = 0. \quad (16.64)$$

This area preservation property is illustrated in Figure 16.4, in which a two-dimensional flow is seen to deform an initially square patch of fluid.



FIGURE 16.4: Illustrating the stretching and straining of an initially square patch of fluid in a two-dimensional non-divergent flow field. As discussed in Section 16.6, the area of a material region remains fixed in this flow field.

### 16.6.2 Arbitrary volume and area

We make use of the Leibniz-Reynolds transport theorem from Section 15.3.4 to develop the evolution equation for the volume of an arbitrary region. In particular equation (15.44) gives

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} dV \right] = \oint_{\partial \mathcal{R}} \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (16.65)$$

This result holds for both compressible and incompressible flows. But for incompressible flows we can go one step further by noting that

$$0 = \int_{\mathcal{R}} \nabla \cdot \mathbf{v} dV = \oint_{\partial \mathcal{R}} \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (16.66)$$

Importantly, this result holds only when integrating around the boundary of the closed volume,  $\mathcal{R}$ . It does not necessarily mean that  $\mathbf{v} \cdot \hat{\mathbf{n}} = 0$  holds at every point along the boundary. Indeed, when the boundary is time dependent  $\mathbf{v} \cdot \hat{\mathbf{n}} \neq 0$  generally holds everywhere along the boundary.

Making use of equation (16.66) allows us to write

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} dV \right] = \oint_{\partial\mathcal{R}} \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} dS = - \oint_{\partial\mathcal{R}} (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} dS = - \int_{\mathcal{R}} \nabla \cdot (\mathbf{v} - \mathbf{v}^{(b)}) dV. \quad (16.67)$$

This result is identical to the mass budget equation (15.46) for the special case of a constant reference density appropriate for a Boussinesq fluid. The dia-surface transport,  $(\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} dS$ , measures the volume per time crossing the boundary of the region, whether that region has a static or moving boundary. For example, if the boundary is the ocean free surface, then we can make use of the surface kinematic boundary condition (16.4).

## 16.7 Meridional-depth overturning circulation

Geophysical fluid flow is generally three-dimensional. However, it is sometimes useful to summarize aspects of that flow by integrating the mass transport over one of the directions. A common approach is to integrate over the zonal direction either between two solid-wall boundaries (as in an ocean basin) or over a periodic domain (as in the atmosphere or within the Southern Ocean). Doing so leaves a two-dimensional transport in the  $(y, z)$  plane known as the meridional-depth overturning circulation

$$V^\rho = \int_{x_1}^{x_2} \rho v dx \quad \text{and} \quad W^\rho = \int_{x_1}^{x_2} \rho w dx. \quad (16.68)$$

We can go even further for incompressible flow, or for steady state compressible flow, in which case we introduce a streamfunction for the meridional-depth circulation.

### *Creating the overturning streamfunction*

To see how to create an overturning streamfunction, consider the zonal integrated area transport for an incompressible flow<sup>5</sup>

$$V = \int_{x_1}^{x_2} v dx \quad \text{and} \quad W = \int_{x_1}^{x_2} w dx. \quad (16.69)$$

For a non-periodic basin domain (e.g., North Atlantic Ocean), let the zonal bounds,  $x_1$  and  $x_2$ , be well within rock (where the velocity vanishes) so that we encompass the full basin without having any meridional or depth dependence to the zonal bounds. Taking the meridional derivative of the

---

<sup>5</sup>The case for a steady compressible flow follows analogously through use of  $(\rho v, \rho w)$  rather than  $(v, w)$ .

meridional transport leads to

$$\frac{\partial V}{\partial y} = \frac{\partial}{\partial y} \left[ \int_{x_1}^{x_2} v \, dx \right] \quad (16.70a)$$

$$= \int_{x_1}^{x_2} \frac{\partial v}{\partial y} \, dx \quad (16.70b)$$

$$= - \int_{x_1}^{x_2} \left[ \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} \right] dx \quad (16.70c)$$

$$= - \int_{x_1}^{x_2} \frac{\partial w}{\partial z} \, dx \quad (16.70d)$$

$$= - \frac{\partial}{\partial z} \left[ \int_{x_1}^{x_2} w \, dx \right] \quad (16.70e)$$

$$= - \frac{\partial W}{\partial z}. \quad (16.70f)$$

These results show that the two-dimensional zonally integrated transport is non-divergent

$$\frac{\partial V}{\partial y} + \frac{\partial W}{\partial z} = 0. \quad (16.71)$$

As a consequence of the non-divergence condition (16.71), we can introduce a meridional-depth streamfunction

$$\Psi(y, z, t) = - \int_{\eta_b^{\max}}^z V \, dz' = - \int_{\eta_b^{\max}}^z \left[ \int_{x_1}^{x_2} v \, dx \right] dz', \quad (16.72)$$

to specify the zonally integrated flow. The lower limit of  $z = \eta_b^{\max}$  is a constant that is deeper than the maximum depth in the full domain and with the convention that there is zero transport for any region below the fluid bottom. This convention follows that taken for the zonal bounds,  $x_1$  and  $x_2$ , which are constants that we well within the solid earth when the domain is not periodic. We verify that  $\Psi$  is a streamfunction by computing

$$\frac{\partial \Psi}{\partial z} = -V \quad (16.73a)$$

$$\frac{\partial \Psi}{\partial y} = - \frac{\partial}{\partial y} \left[ \int_{\eta_b^{\max}}^z V \, dz' \right] = - \int_{\eta_b^{\max}}^z \frac{\partial V}{\partial y} \, dz' = \int_{\eta_b^{\max}}^z \frac{\partial W}{\partial z} \, dz' = W. \quad (16.73b)$$

To reach this result, we made use of the non-divergent condition (16.71), and set

$$W(z = \eta_b^{\max}) = 0. \quad (16.74)$$

Also, we are able to move the derivative across the lower limit of the integral since  $\eta_b^{\max}$  is a constant. An idealized version of the meridional-depth circulation is shown in Figure 16.5.

### *The overturning streamfunction at the ocean surface*

To evaluate the overturning streamfunction (16.72) at the ocean surface,  $z = \eta(x, y, t)$ , we follow a method similar to how we deal with the bottom. Namely, introduce a constant  $\eta^{\max}$  that is larger than any value of  $\eta(x, y, t)$  and with the convention that the transport is zero in regions above the ocean surface. In this case the streamfunction computed across the full depth of the domain

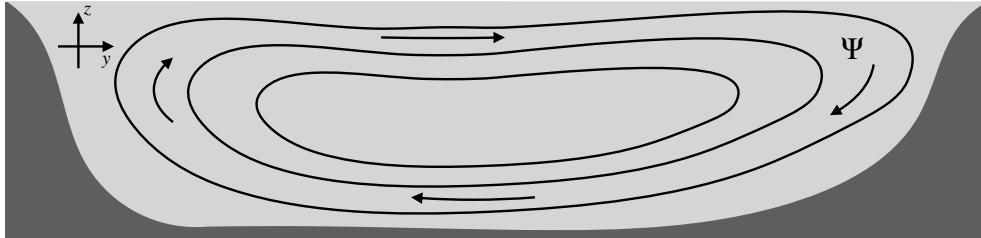


FIGURE 16.5: An idealized depiction of a steady meridional-depth overturning circulation. Shown here are streamlines (isolines of constant  $\Psi$ ) for the zonally integrated flow between two solid boundaries or over a zonally periodic domain. The flow is assumed to be non-divergent, as per equation (16.71). In the upper reaches of the fluid, flow moves northward (positive  $y$ ), with downward motion as it reaches the northern boundary, then southward motion at depth and eventual return towards the surface near the southern boundary.

is given by minus the net meridional transport across the chosen latitude

$$\Psi(y, z = \eta^{\max}, t) = - \int_{\eta_b^{\max}}^{\eta^{\max}} V \, dz' = - \int_{\eta_b^{\max}}^{\eta^{\max}} \left[ \int_{x_1}^{x_2} v \, dx \right] \, dz', \quad (16.75)$$

Volume conservation means that this transport vanishes in the steady state but it is generally nonzero due to transients.



## 16.8 Exercises

### EXERCISE 16.1: STREAMLINES FOR CELLULAR FLOW

Sketch the velocity field for this streamfunction

$$\psi(x, y) = A \sin(kx) \sin ly, \quad (16.76)$$

where  $(k, l)$  are the zonal and meridional wavenumbers, respectively. Hint: assume any convenient value for the wavenumbers  $k, l$  and the amplitude,  $A$ , but indicate what values were chosen. Furthermore, show vectors so that the sense of the flow is clear.

### EXERCISE 16.2: ZERO NET AREA TRANSPORT THROUGH STATIC CLOSED CURVE

For a two-dimensional non-divergent flow, show that there is zero net transport of fluid crossing an arbitrary static and simply connected closed curve. Note that in two space dimensions, the transport of fluid across a line has dimensions  $L^2 T^{-1}$ , thus representing an area transport.

### EXERCISE 16.3: ZERO NET VOLUME TRANSPORT THROUGH STATIC CLOSED SURFACE

For a three-dimensional non-divergent flow, show that there is zero net transport of fluid crossing an arbitrary static and simply connected closed surface within the fluid interior. Note that in three space dimensions, the transport of fluid across a surface has dimensions  $L^3 T^{-1}$ , thus representing a volume transport.

### EXERCISE 16.4: NET FLUID TRANSPORT ACROSS AN ARBITRARY SURFACE

Consider flow in a container with static sides/bottom. Draw an arbitrary static surface,  $\mathcal{S}$ , within the fluid from one side of the container to the other as in Figure 16.6. Integrate the fluid transport over the surface,  $\int_{\mathcal{S}} \mathbf{v} \cdot \hat{\mathbf{n}} \, d\mathcal{S}$ .

- (a) For an incompressible flow, show that the transport  $\int_{\mathcal{S}} \mathbf{v} \cdot \hat{\mathbf{n}} \, d\mathcal{S}$  vanishes. That is, the net transport across the surface is zero.

- (b) Specialize the above result to a horizontal surface so that we see there is zero integrated vertical transport across the surface,  $\int_S w \, dx \, dy = 0$ . Discuss these results. Note: see Section 42.4.8 for the more general case of a non-static surface.
- (c) Rework part (a) for the case of a compressible fluid. That is, derive an equation for the net fluid transport across the surface if the fluid is compressible.

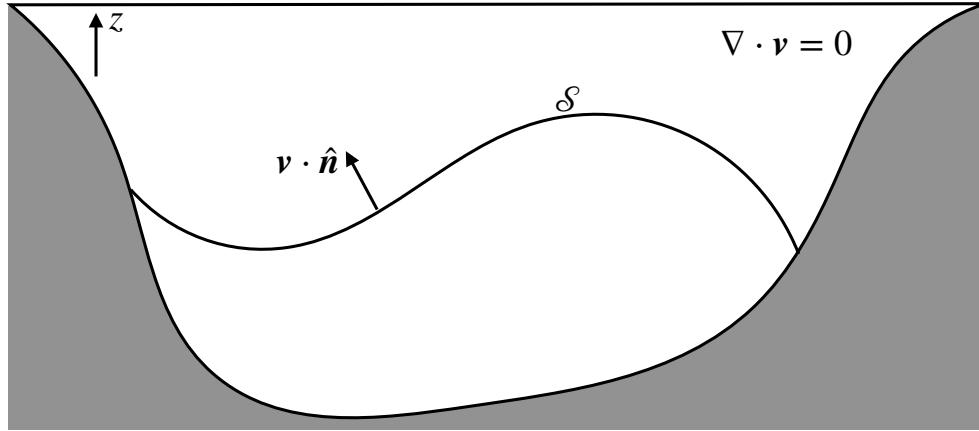


FIGURE 16.6: Schematic for exercise 16.4, whereby we show that the net flow vanishes across a static surface,  $\mathcal{S}$ , that extends from one boundary to the other within an incompressible flow.

#### EXERCISE 16.5: SOLID BODY ROTATION

Consider a velocity field corresponding to a time-independent solid-body rotation on a plane

$$\mathbf{u} = \Omega \hat{\mathbf{z}} \times \mathbf{x} = \Omega (-y \hat{\mathbf{x}} + x \hat{\mathbf{y}}), \quad (16.77)$$

where  $\Omega > 0$  is a constant rotation rate.

- (a) Compute the relative vorticity,  $\boldsymbol{\omega} = \nabla \times \mathbf{u}$ .
- (b) Compute the streamfunction  $\mathbf{u} = \hat{\mathbf{z}} \times \nabla \psi$ . Draw streamfunction contours; i.e., lines of constant streamfunction. Put arrows to orient the flow along the streamlines.
- (c) Describe the geometry of material lines. Hint: since the velocity field is time-independent, material parcel trajectories are coincident with streamlines.

#### EXERCISE 16.6: ALTERNATIVE FORM OF MERIDIONAL-DEPTH STREAMFUNCTION

In equation (16.72), we introduced the meridional-depth overturning streamfunction

$$\Psi(y, z, t) = - \int_{-H_{\max}}^z V \, dz'. \quad (16.78)$$

Show that an alternative streamfunction is given by

$$\Gamma(y, z, t) = \int_{y_s}^y W \, dy', \quad (16.79)$$

where  $y_s$  is a constant latitude just south of the southern-most latitude in the domain.

## EXERCISE 16.7: VOLUME TRANSPORT THROUGH STREAMTUBE ENDS

Recall our discussion of streamtubes in Section 12.8.2 (see in particular Figure 12.5). For a steady non-divergent three-dimensional flow, show that the volume transport (volume per time) through the two streamtube ends balances

$$\int_{\mathcal{S}_1} \mathbf{v} \cdot \hat{\mathbf{n}}_1 d\mathcal{S} + \int_{\mathcal{S}_2} \mathbf{v} \cdot \hat{\mathbf{n}}_2 d\mathcal{S} = 0, \quad (16.80)$$

where  $\hat{\mathbf{n}}_1$  and  $\hat{\mathbf{n}}_2$  are the outward normals at the two end caps  $\mathcal{S}_1$  and  $\mathcal{S}_2$ . Since the end caps have oppositely directed outward normals, equation (16.80) says that the volume transport entering one streamtube end equals to that leaving the other end. Furthermore, the area of the streamtube is inversely proportional to the local normal velocity, so that flow speeds up when moving through a narrower region of the tube.

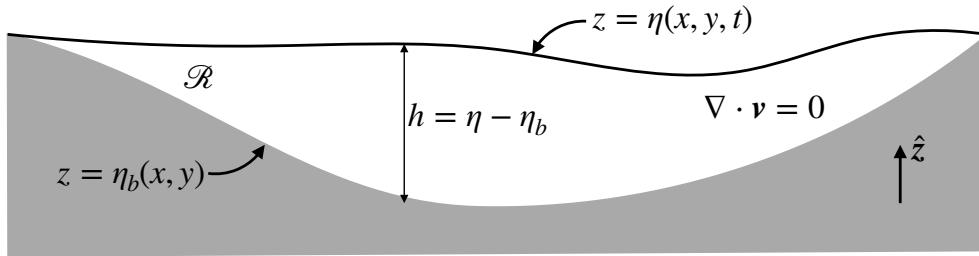


FIGURE 16.7: Schematic for exercise 16.8 with  $z = \eta(x, y, t)$  the free surface at the top of the fluid. This exercise shows that the area integrated time tendency for the free surface vanishes in the absence of mass transport across the free surface.

## EXERCISE 16.8: AREA AVERAGE OF FREE SURFACE TIME TENDENCY

Consider an incompressible ocean flow bounded by a free upper surface and a solid bottom. Let  $z = \eta_b(x, y)$  be the vertical position of the static bottom, and  $z = \eta(x, y, t)$  be the position of the transient free surface, so that the thickness of the layer is  $h = -\eta_b + \eta$  (see Figure 16.7). The horizontal extent of the layer is a function of time, and is defined by a vanishing thickness  $h = -\eta_b + \eta = 0$  (e.g., ocean water reaching the shoreline). Assume no material crosses either the surface or bottom boundaries, so that both boundaries are material surfaces. Show that the free surface has a time derivative,  $\partial\eta/\partial t$ , whose area average vanishes. Discuss this result.

## EXERCISE 16.9: VOLUME INTEGRAL OF THE NON-DIVERGENT CARTESIAN VELOCITY FIELD

Consider an incompressible ocean flow in Cartesian coordinates bounded by a free upper surface and a solid bottom over a domain  $\mathcal{R}$ . Let  $z = \eta_b(x, y)$  be the vertical position of the static bottom, and  $z = \eta(x, y, t)$  be the position of the transient free surface as in Figure 16.7. Prove that the domain integral of the velocity is given by

$$\int_{\mathcal{R}} \mathbf{v} dV = \int_{z=\eta} \mathbf{x} (\mathbf{v} \cdot \hat{\mathbf{n}}) d\mathcal{S} = \int_{z=\eta} \mathbf{x} (\partial_t \eta - Q_m / \rho_0) dx dy. \quad (16.81)$$

Hint: make use of the results from Section 2.7.6 and then use the kinematic boundary conditions from Section 16.2. Note that to enable this exercise we assume Cartesian coordinates, which is required when integrating a vector.





**Part IV**

**Dynamics of geophysical fluid flows**

Dynamics is the area of mechanics that examines the causes of motion. For a Newtonian system, such as a geophysical fluid, the cause of motion is understood when we understand the forces. In this part of the book, we encounter a suite of theoretical concepts that form the foundations of geophysical fluid mechanics. Our presentation moves largely from the general to the specific, with each chapter written in a manner that allows it to be picked up without relying too much on other chapters. The “general to specific” route also allows us to establish general principles based on foundational principles and concepts and to then see how they manifest in specific contexts.

Forces of concern in geophysical fluid mechanics include the body force acting on a fluid element from the earth’s gravity field along with the contact forces from pressure and friction that act between adjacent fluid elements. Additionally, by choosing to work in a non-inertial rotating terrestrial reference frame, we encounter body forces from the Coriolis and planetary centrifugal accelerations, just as encountered for geophysical particle mechanics in Part II. Each of these forces play important roles in determining the diversity of geophysical fluid motion, and their analysis leads to dynamical insights into the nature and causes of fluid motion. We observe that forces in fluids are commonly inferred from kinematic properties of the motion, thus making use of the fluid kinematics from Part III.

#### SUMMARY OF THE DYNAMICS CHAPTERS

We start the development of dynamics by formulating the equations of motion (linear momentum and angular momentum) in Chapter 17. In subsequent chapters we study the forces appearing in these equations, including friction (Chapter 18), pressure (Chapter 19), and buoyancy (Chapter 24). Buoyancy is the vertical pressure force, arising from density inhomogeneities, that are not balanced by gravity. As such, our study of buoyancy focuses on vertical forces, which contrasts to our study of pressure form stresses in Chapter 19, which focus on horizontal forces.

When studying buoyancy in Chapter 24, we make use of an equation of state that provides the mass density of a fluid element as a function of thermodynamical properties such as temperature, pressure, and matter concentration. This role for thermodynamics prompts the development in Chapter 20 of selected topics in equilibrium thermodynamics. In Chapter 21 we extend these equilibrium thermodynamic relations to linear irreversible thermodynamics relevant for a moving geophysical fluid where we assume that each fluid element is in a local thermodynamic equilibrium. This extension to moving fluids allows us to study how mechanical energy is exchanged with internal energy in the presence of work done by pressure and heat generated by friction.

Chapters 22 and 23 introduce a variety of approximate equations that allow us to focus on selected dynamical regimes by filtering away uninteresting phenomena. It is here that we encounter the hydrostatic approximation and the Boussinesq approximation, both of which are commonly used for large-scale models of the ocean and atmosphere. Additionally, we simplify the spherical geometry by making the tangent plane approximation, with the  $f$ -plane and  $\beta$ -plane commonly used in idealized theoretical studies. Approximate balances are further examined in Chapter 25, where we study the mechanics of a rapidly rotating fluid. We here encounter the geostrophic balance, which is a diagnostic balance appropriate for describing large-scale geophysical flows in which the horizontal pressure acceleration is balanced by the Coriolis acceleration. Geostrophic balance is one of the variety of balances considered in Chapter 26, which introduces balanced flow regimes pertaining to horizontal motions. We close this part of the book in Chapter 27, which examines the physics of an Ekman boundary layer in which the Coriolis acceleration balances vertical friction.

Throughout the previous chapters we assumed a constant effective gravitational acceleration. However, much of the observed motion of the ocean arises from the spatial-temporal variations of the gravity field that give rise to tides, thus motivating our brief look at the subject in Chapter 28.

Finally, in Chapter 29 we briefly visit the topic of gravity waves on the surface of a homogenous and non-hydrostatic fluid. Such waves have a vertical extent that decays exponentially, thus leading to the transport of particles through Stokes drift. Stokes drift appears in many guises in fluid mechanics, with the presentation in this chapter rather standard but helping to support the later view in Chapter 47 from the basis of the generalized Lagrangian mean.



# Chapter 17

## Momentum dynamics

We here formulate the fluid mechanical equations for linear and axial angular momentum relevant to geophysical fluid motions. These equations of geophysical fluid dynamics (GFD) are based on Newton's laws of motion applied to a stratified fluid continuum moving on a rotating spherical planet where the rotation rate is constant in time. Relative to the point particle, the new dynamical feature afforded to the continuum concerns contact forces between fluid elements, which lead to pressure and frictional forces from mechanical interactions.

### READER'S GUIDE TO THIS CHAPTER

We make liberal use of results from point particle mechanics studied in Part II as well as fluid kinematics from Part III. Much of the material in this chapter is introductory, with further details and elaboration offered in later chapters.

17.1	Linear momentum equation . . . . .	358
17.1.1	Body forces . . . . .	358
17.1.2	Contact forces . . . . .	358
17.1.3	Equation of motion . . . . .	360
17.1.4	Euler equation for perfect fluid motion . . . . .	361
17.1.5	Further study . . . . .	361
17.2	Special forms for the momentum equation . . . . .	361
17.2.1	Spherical coordinates . . . . .	362
17.2.2	Vector-invariant velocity equation . . . . .	363
17.2.3	Dynamic pressure and the Magnus acceleration . . . . .	363
17.3	Exact hydrostatic balance . . . . .	364
17.3.1	Properties of exact hydrostatic balance . . . . .	365
17.3.2	Comparison to approximate hydrostatic balance . . . . .	365
17.4	Axial angular momentum . . . . .	366
17.4.1	Axial angular momentum conserving motion of a ring of air . . . . .	367
17.4.2	Sketching the atmospheric angular momentum budget . . . . .	368
17.4.3	Further study . . . . .	369
17.5	Acoustic waves . . . . .	369
17.5.1	Rudiments of acoustic waves . . . . .	370
17.5.2	Further study . . . . .	371
17.6	Exercises . . . . .	371

## 17.1 Linear momentum equation

We here summarize elements of classical continuum mechanics and in turn apply Newton's second law to derive the linear momentum budget for a fluid continuum. We present the momentum budget over both a finite volume region of the fluid (weak formulation) and for an infinitesimal fluid element (strong formulation).

### 17.1.1 Body forces

Forces acting on an arbitrary volume,  $\mathcal{R}$ , of a continuous media are of two general kinds. The first kind involves *external* or *body* forces, such as gravitation (including astronomical tidal forces), Coriolis, planetary centrifugal, and electromagnetic forces. These forces act throughout the extent of the media. Consequently, the total body force acting on a volume of fluid is the integral of the body force per unit mass,  $\mathbf{f}_{\text{body}}$ , multiplied by the mass of the media

$$\mathbf{F}_{\text{body}} = \int_{\mathcal{R}} \mathbf{f}_{\text{body}} \rho dV. \quad (17.1)$$

For example, the effective gravitational force (combination of central gravity plus planetary centrifugal) acting on a volume of fluid is given by

$$\mathbf{F}_{\text{effective gravity}} = \int_{\mathcal{R}} \mathbf{g} \rho dV, \quad (17.2)$$

where  $\mathbf{g} = -\nabla\Phi$  is the effective acceleration of gravity with  $\Phi$  the geopotential (Section 9.12.4). Likewise, the Coriolis force is given by

$$\mathbf{F}_{\text{Coriolis}} = -2 \int_{\mathcal{R}} (\boldsymbol{\Omega} \times \mathbf{v}) \rho dV. \quad (17.3)$$

These body forces have the same appearance as for the point particle in Chapter 9, with the only difference being the material is now a continuous media rather than a point mass.

### 17.1.2 Contact forces

The second kind of forces are *internal* or *contact* forces, such as pressure forces and frictional forces. These forces act on a region of a continuous media through the area integrated stresses acting on the boundary enclosing the region. Mathematically, we compute the contact force exerted on the region through its boundaries through the area integral of the *stress tensor* projected onto the normal direction

$$\mathbf{F}_{\text{contact}} = \oint_{\partial\mathcal{R}} \mathbb{T} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (17.4)$$

where  $\hat{\mathbf{n}}$  is the outward normal direction orienting the domain boundary with  $d\mathcal{S}$  the associated area element, and  $\mathbb{T}$  is the second order stress tensor. We have more to say about the stress tensor in the following as well as in Chapter 18.

Contact forces affect continuous media and they do so through the nonzero spatial extent of elements within the media, with this spatial extent allowing for interactions between adjacent fluid elements. Point particles (Part II) do not experience contact forces since point particles have no spatial extent. Hence, contact forces represent a fundamentally new feature, conceptually and operationally, to the fluid dynamical equations relative to the equations of point particles.

### Stresses from friction and pressure

As studied in detail in Chapter 18, there are two types of stress that concern us: diagonal stresses associated with reversible momentum exchange through pressure, and stresses associated with the irreversible exchange of momentum through friction. Hence, it is convenient to decompose the stress tensor components according to

$$\mathbb{T}^{ab} = \tau^{ab} - p g^{ab}. \quad (17.5)$$

In this equation,  $p$  is the pressure, which is a force per unit area acting in a compressive manner on the area of a surface. The second order tensor,  $g^{ab}$ , is a chosen coordinate representation of the inverse metric tensor and it equals to the Kronecker or unit tensor when choosing Cartesian coordinates in Euclidean space (Section 7.1). The frictional stress tensor is written  $\tau^{ab}$ . It is also known as the *deviatoric* stress tensor as it represents deviations from the static case when stress is due solely to pressure. The friction stress tensor generally has zero trace, with pressure comprising the trace portion of the full stress tensor.

Substitution of the stress tensor (17.5) into the contact force expression (17.4) leads to

$$\mathbf{F}_{\text{contact}} = \oint_{\partial\mathcal{R}} (\tau \cdot \hat{\mathbf{n}} - p \hat{\mathbf{n}}) dS, \quad (17.6)$$

where the integral is taken over the bounding surface of the domain whose outward normal is  $\hat{\mathbf{n}}$ . Given this expression for contact forces acting on the boundary of a fluid domain, it is seen that positive pressure ( $p > 0$ ) acts in the direction opposite to the surface's outward normal so that pressure always acts in a compressive manner. Deviatoric stresses create more general forces on the bounding surface, which can have compressive, expansive, shearing, and/or rotational characteristics.

### Exchange of momentum between fluid elements

We mathematically represent the exchange of momentum between fluid elements via a symmetric stress tensor, with symmetry implied by statements about angular momentum conservation (detailed in Section 18.3). The divergence of the stress tensor then leads to a force acting on the fluid element. The forces arising from molecular viscosity provide an irreversible exchange of momentum that reduce the kinetic energy of fluid elements (Section 21.3.2). This process is dissipative and thus referred to as friction. Furthermore, when averaging over turbulent realizations of a fluid, the impacts on the mean flow are generally far larger than those associated with molecular viscosity, with these exchanges commonly parameterized via a symmetric stress tensor.

### A gauge symmetry of pressure force

The contribution from pressure in the contact force (17.6) remains invariant if pressure is shifted by an arbitrary function of time

$$p(\mathbf{x}, t) \rightarrow p(\mathbf{x}, t) + F(t). \quad (17.7)$$

We see this invariance by noting that

$$\oint_{\partial\mathcal{R}} F(t) \hat{\mathbf{n}} dS = F(t) \oint_{\partial\mathcal{R}} \hat{\mathbf{n}} dS = 0, \quad (17.8)$$

where the final equality follows from a corollary of the divergence theorem as discussed in Section 2.7.3. Briefly, through the divergence theorem in Section 2.7.2 we know that

$$\oint_{\partial\mathcal{R}} p \hat{\mathbf{n}} d\mathcal{S} = \int_{\mathcal{R}} \nabla p dV, \quad (17.9)$$

so that if pressure is shifted by a spatial constant then the pressure gradient body force remains unchanged, as will the pressure contact force.

We refer to this invariance of the pressure force as a *gauge symmetry*. It means that motion of the fluid remains unchanged if pressure is modified by a spatial constant that can generally be a function of time.

### 17.1.3 Equation of motion

The linear momentum of a fluid region is given by

$$\mathbf{P} = \int_{\mathcal{R}} \mathbf{v} \rho dV. \quad (17.10)$$

Applying Newton's law of motion to the continuum leads to the finite volume equation of motion

$$\frac{d}{dt} \int_{\mathcal{R}} \mathbf{v} \rho dV = \int_{\mathcal{R}} \rho \mathbf{f}_{\text{body}} dV + \oint_{\partial\mathcal{R}} \mathbb{T} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (17.11)$$

The time derivative can be material, as for a constant mass fluid region moving with the barycentric velocity, Eulerian, as for a fixed region in space (see Section 15.3), or otherwise. Applying the divergence theorem (Section 2.7.2) to the area integral yields

$$\frac{d}{dt} \int_{\mathcal{R}} \rho \mathbf{v} dV = \int_{\mathcal{R}} (\rho \mathbf{f}_{\text{body}} + \nabla \cdot \mathbb{T}) dV, \quad (17.12)$$

where we brought the contact forces into the volume integral through exposing the divergence of the stress tensor.

#### *General form of the equation of motion for a fluid element*

Since the volume under consideration is arbitrary, the integral relation (17.12) is satisfied for an arbitrary region. We apply the result to an infinitesimal fluid element moving with the flow so that

$$\frac{D(\rho \mathbf{v} \delta V)}{Dt} = \delta V (\rho \mathbf{f}_{\text{body}} + \nabla \cdot \mathbb{T}). \quad (17.13)$$

Assuming the mass for the fluid element is constant then leads to the equation of motion

$$\rho \frac{D\mathbf{v}}{Dt} = \rho \mathbf{f}_{\text{body}} + \nabla \cdot \mathbb{T} \iff \rho \frac{Dv_a}{Dt} = \rho f_a + \partial_b \mathbb{T}_{ba}. \quad (17.14)$$

This equation is a continuum expression of Newton's equation of motion, and it is sometimes referred to as *Cauchy's equation of motion* in honor of the work Cauchy did in its formulation. The right expression exposes the Cartesian tensor labels, with the “body” label dropped for brevity.

### Momentum equation for a rotating fluid in a gravitational field

We now specialize the momentum equation (17.14) to suit the needs of geophysical fluid mechanics. We first write the stress tensor in terms of the deviatoric component from friction and a diagonal component from pressure (equation (17.6))

$$\rho \frac{D\mathbf{v}}{Dt} = \rho \mathbf{f}_{\text{body}} - \nabla p + \nabla \cdot \boldsymbol{\tau}. \quad (17.15)$$

Next, move to a rotating terrestrial reference frame and thus expose the Coriolis acceleration and the effective gravitational force (Section 9.13)

$$\rho \frac{D\mathbf{v}}{Dt} + 2\rho \boldsymbol{\Omega} \times \mathbf{v} = -\rho \nabla \Phi - \nabla p + \nabla \cdot \boldsymbol{\tau}. \quad (17.16)$$

This form of the equation of motion arises from extracting the solid-body motion of the basis vectors to define the Coriolis acceleration (see Section 9.11). Any remaining changes to the basis vectors arise from motion of the fluid relative to the solid-body rotating reference frame, and thus appear when expanding the material time derivative. The form (17.16) for the equation of motion offers a suitable starting point for studies of geophysical fluid dynamics. It sometimes goes by the name of *Navier-Stokes* equation. However, that name is more commonly applied to the non-rotating case with a specific form for the friction operator (see Section 18.7.7). We thus refer to equation (17.16) as Newton's law of motion for a rotating fluid.<sup>1</sup>

#### 17.1.4 Euler equation for perfect fluid motion

This inviscid form of the momentum equation (17.15) is known as the *Euler equation* of perfect fluid mechanics

$$\rho \frac{D\mathbf{v}}{Dt} = \rho \mathbf{f}_{\text{body}} - \nabla p, \quad (17.17)$$

where the body force is conservative. That is, the Euler equation is concerned just with fluid motion in the absence of dissipative processes. The inviscid form of the momentum equation (17.16) leads to the Euler equation in the presence of rotation and gravitation

$$\rho \frac{D\mathbf{v}}{Dt} + 2\rho \boldsymbol{\Omega} \times \mathbf{v} = -\rho \nabla \Phi - \nabla p. \quad (17.18)$$

We have many occasions in this book to ignore dissipation, in which case we work with a particular form of the Euler equation of motion. We further comment on the Euler equation in Section 18.7.7.

#### 17.1.5 Further study

Chapter 5 of [Aris \(1962\)](#) offers an insightful discussion of continuum mechanics as applied to a fluid. Section 2.2 [Vallis \(2017\)](#) provides a thorough derivation of the dynamical equations of motion for the atmosphere and ocean. We offer further discussion of the mathematics and physics of stress in fluids in Chapters 18 and 19.

## 17.2 Special forms for the momentum equation

We here display some special forms of the momentum equation that will be of use in our studies.

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<sup>1</sup>The Navier-Stokes equations were first derived by Claude-Louis Navier in 1822 and later independently derived by George Stokes in 1845.

### 17.2.1 Spherical coordinates

Geophysical fluids move on a rotating planet with the planet commonly assumed to have an oblated spherical geometry, though with the equations approximated by their spherical form using the geopotential vertical coordinate. To display the equations of motion, we make use of the acceleration as derived in Section 9.13.3 for the point particle, using the geopotential coordinate to measure radial distances from the center of the sphere (equation (21.143)), as well as the longitude and latitude angular coordinates defined by Figure 8.1. The point particle time derivative, which is computed following the particle, translates into a material time derivative for fluid elements. We are thus led to the spherical equations of motion in their full glory

$$\frac{Du}{Dt} + \frac{u(w - v \tan \phi)}{r} + 2\Omega(w \cos \phi - v \sin \phi) = -\frac{1}{\rho r \cos \phi} \frac{\partial p}{\partial \lambda} + F^\lambda \quad (17.19)$$

$$\frac{Dv}{Dt} + \frac{v w + u^2 \tan \phi}{r} + 2\Omega u \sin \phi = -\frac{1}{\rho r} \frac{\partial p}{\partial \phi} + F^\phi \quad (17.20)$$

$$\frac{Dw}{Dt} - \frac{u^2 + v^2}{r} - 2\Omega u \cos \phi = -g - \frac{1}{\rho} \frac{\partial p}{\partial r} + F^r, \quad (17.21)$$

where we introduced the spherical components to the friction acceleration

$$\mathbf{F} = F^\lambda \hat{\lambda} + F^\phi \hat{\phi} + F^r \hat{r}, \quad (17.22)$$

which is determined by the divergence of the frictional stress tensor. We also note the spherical coordinate form for the gradient operator (Section 8.2.8)

$$\nabla = \frac{\hat{\lambda}}{r \cos \phi} \frac{\partial}{\partial \lambda} + \frac{\hat{\phi}}{r} \frac{\partial}{\partial \phi} + \hat{r} \frac{\partial}{\partial r}, \quad (17.23)$$

as well as the material time derivative operator

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla = \frac{\partial}{\partial t} + \frac{u}{r \cos \phi} \frac{\partial}{\partial \lambda} + \frac{v}{r} \frac{\partial}{\partial \phi} + w \frac{\partial}{\partial r}. \quad (17.24)$$

We can write the spherical momentum equations in a bit more compact form by introducing the spherical coordinate velocity field (see equation (9.80))

$$\mathbf{v} = \mathbf{u} + \hat{r} w = u \hat{\lambda} + v \hat{\phi} + w \hat{r} \quad (17.25)$$

and the corresponding spherical coordinate acceleration

$$\mathbf{A}_{\text{sphere}} = \frac{Du}{Dt} \hat{\lambda} + \frac{Dv}{Dt} \hat{\phi} + \frac{Dw}{Dt} \hat{r}. \quad (17.26)$$

We also introduce the expression (9.117c) for the metric acceleration to render

$$\rho \frac{D\mathbf{v}}{Dt} + 2\rho \boldsymbol{\Omega} \times \mathbf{v} = -\rho \nabla \Phi - \nabla p + \rho \mathbf{F}, \quad (17.27)$$

where we have the acceleration relative to the rotating frame

$$\frac{D\mathbf{v}}{Dt} = \mathbf{A}_{\text{sphere}} + \frac{1}{r} [u \tan \phi (\hat{r} \times \mathbf{v}) + w \mathbf{u} - \hat{r} \mathbf{u} \cdot \mathbf{u}]. \quad (17.28)$$

For some purposes it is convenient to combine one piece of the metric acceleration to the Coriolis

acceleration to yield

$$\mathbf{A}_{\text{sphere}} + \frac{1}{r} [w \mathbf{u} - \hat{\mathbf{r}} \mathbf{u} \cdot \mathbf{u}] + \left[ 2\boldsymbol{\Omega} + \frac{u \tan \phi \hat{\mathbf{r}}}{r} \right] \times \mathbf{v} = - \left[ \frac{\rho \nabla \Phi + \nabla p}{\rho} \right] + \mathbf{F}. \quad (17.29)$$

### 17.2.2 Vector-invariant velocity equation

The metric terms appearing in the momentum equation (17.29) are those terms proportional to  $r^{-1}$  that arise from spatial dependence of the spherical unit vectors. An alternative formulation removes these terms in favor of the vorticity and kinetic energy. For that purpose we make use of the identity (equation (2.39)) for the nonlinear self-advection term

$$(\mathbf{v} \cdot \nabla) \mathbf{v} = \boldsymbol{\omega} \times \mathbf{v} + \nabla(\mathbf{v} \cdot \mathbf{v})/2, \quad (17.30)$$

where  $\boldsymbol{\omega} = \nabla \times \mathbf{v}$  is the vorticity from Part VI of this book. We derive the corresponding *vector-invariant* form of the velocity equation using Cartesian coordinates and then invoke general coordinate invariance (Section 6.1) to extend the result to arbitrary coordinates.<sup>2</sup> Making use of equation (17.30) thus leads to the material acceleration

$$\frac{D\mathbf{v}}{Dt} = \frac{\partial \mathbf{v}}{\partial t} + \boldsymbol{\omega} \times \mathbf{v} + \nabla(\mathbf{v} \cdot \mathbf{v})/2 \quad (17.31)$$

so that the momentum equation (17.16) becomes the vector-invariant velocity equation

$$\frac{\partial \mathbf{v}}{\partial t} + (2\boldsymbol{\Omega} + \boldsymbol{\omega}) \times \mathbf{v} = -\nabla(\Phi + \mathbf{v} \cdot \mathbf{v}/2) + (1/\rho) (-\nabla p + \nabla \cdot \mathbf{v}). \quad (17.32)$$

### 17.2.3 Dynamic pressure and the Magnus acceleration

The *velocity equation* (17.32) is mathematically equivalent to the momentum equation (17.16). Even so, it provides a more convenient means to derive Bernoulli's theorem in Section 21.6.2 and the vorticity equation in Chapter 35. Furthermore, it highlights certain physical processes affecting accelerations that are not obviously seen from the momentum equation. We here consider two such processes.

#### Dynamic pressure

The velocity equation (17.32) reveals that kinetic energy gradients contribute a *dynamic pressure gradient* that accelerates the fluid down the kinetic energy gradient, from regions of high kinetic energy to low. To help understand this process, consider a Boussinesq fluid (Chapter 23), in which case the density factor is a constant so that we can write the accelerations from pressure and kinetic energy as

$$-(1/\rho) \nabla p - \nabla(\mathbf{v} \cdot \mathbf{v}/2) = -\rho^{-1} \nabla(p + \rho \mathbf{v} \cdot \mathbf{v}/2) \equiv -\rho^{-1} \nabla p_{\text{stagnation}}. \quad (17.33)$$

In this equation we defined the *stagnation pressure*

$$p_{\text{stagnation}} \equiv p + \rho \mathbf{v} \cdot \mathbf{v}/2, \quad (17.34)$$

which is the sum of the mechanical pressure,  $p$ , plus the dynamic pressure,  $\rho \mathbf{v} \cdot \mathbf{v}/2$ .

<sup>2</sup>See Section 4.4.4 of [Griffies \(2004\)](#) for a detailed derivation using general coordinates.

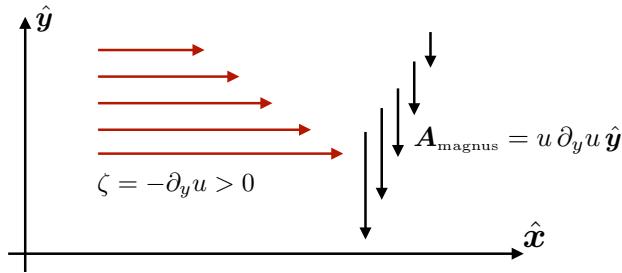


FIGURE 17.1: The Magnus acceleration,  $\mathbf{A}_{\text{magnus}} = -\boldsymbol{\omega} \times \mathbf{v}$ , acting on a fluid element with nonzero vorticity. In this case the fluid element has a zonal velocity with a linear meridional shear,  $\mathbf{v} = u(y) \hat{x}$ , so that the relative vorticity is  $\boldsymbol{\omega} = \zeta \hat{z} = -(\partial_y u) \hat{z}$  and the Magnus acceleration is  $\mathbf{A}_{\text{magnus}} = u \partial_y u \hat{y}$ . When the fluid has a negative meridional shear,  $\partial_y u < 0$ , its relative vorticity is positive (cyclonic),  $\zeta = -\partial_y u > 0$ , so that the Magnus acceleration deflects the fluid element to the right of the motion, just as for the Coriolis acceleration in the northern hemisphere.

The stagnation pressure is the pressure required to keep the local acceleration unchanged if the dynamic pressure is set to zero as per a stagnant fluid. This situation arises in practice in a device known as a *Pitot tube* used to measure the speed of flow in a pipe, with the Pitot tube making use of the Bernoulli theorem formulated in Section 21.6. Stagnation points also arise at special points along solid objects within a moving fluid, such as wings. The dynamic pressure,  $\rho \mathbf{v} \cdot \mathbf{v}/2$ , provides an isotropic force per area in addition to mechanical pressure,  $p$ . Hence, the stagnation pressure is the total isotropic contact force per area, thus motivating some treatments to refer the stagnation pressure as the *total pressure*.<sup>3</sup>

### Magnus acceleration

The acceleration  $-\boldsymbol{\omega} \times \mathbf{v}$  appearing in the velocity equation (17.32) couples vorticity and velocity. This acceleration is known as the *Magnus effect* or *Magnus acceleration*. Since it acts only when there is both motion and vorticity, it is sometimes referred to as a *vortex force*, with the force increasing in magnitude where the velocity and/or vorticity are larger in magnitude. As discussed in Chapter 32, vorticity is a measure of the spin of a fluid element, so that the Magnus acceleration deflects a spinning fluid element in a direction perpendicular to its trajectory just like the Coriolis acceleration. We illustrate a particular case in Figure 17.1 for a zonal flow with a negative meridional shear that creates a positive vertical relative vorticity. Besides causing a moving and spinning fluid element to deflect, the Magnus acceleration provides the mechanism whereby a solid spinning body immersed in a moving fluid is deflected, such as commonly experienced by spinning balls used for baseball, tennis, and cricket. Notably, as per Newton's third law, the spinning ball is deflected in a direction opposite to that of the spinning fluid element.

## 17.3 Exact hydrostatic balance

We are mostly interested in moving fluids within this book. Even so, it is useful to expose the signature of a static fluid supporting the trivial solution,  $\mathbf{v} = 0$ . The equation of motion (17.16) has an exact static solution so long as the pressure gradient force balances the effective gravitational force

$$\nabla p = -\rho \nabla \Phi, \quad (17.35)$$

<sup>3</sup>In many engineering applications, the mechanical pressure,  $p$ , is referred to as the *static pressure* so that the total/stagnation pressure is the sum of the static plus dynamic pressures. See section 4.9 of [Kundu et al. \(2016\)](#) for more discussion.

and where the frictional stress tensor has zero divergence. Equation (17.35) constitutes the *exact hydrostatic balance*. As justified in Section 22.2, the hydrostatic balance is a very good approximation for the vertical momentum equation in large-scale geophysical fluids even when those fluids are moving. We will thus commonly make the *hydrostatic approximation* for moving fluids. For the current considerations, we are interested in a static fluid, in which case the hydrostatic balance (17.35) is an exact solution to the equation of motion.

### 17.3.1 Properties of exact hydrostatic balance

We make the following observations of the exact hydrostatic balance.

- Since  $\nabla p$  is directly proportional to  $\nabla\Phi$ , surfaces of constant pressure in a static fluid correspond to surfaces of constant geopotential.
- Since the curl of the pressure gradient vanishes, a static fluid maintains its density gradients parallel to geopotential gradients

$$\nabla\rho \times \nabla\Phi = 0, \quad (17.36)$$

which in turn means that density surfaces are parallel to geopotentials so that

$$\rho = \rho(\Phi) \quad \text{static fluid.} \quad (17.37)$$

For the geopotential  $\Phi = g z$ , a static fluid is realized if the density has no horizontal (on the sphere) gradients so that

$$\rho = \rho(z) \quad \text{static fluid with } \Phi = g z. \quad (17.38)$$

If the density gradient has any component perpendicular to  $\nabla\Phi$ , then pressure forces will affect fluid flow thus implying that the fluid is not in exact hydrostatic balance.

- Projecting both sides of equation (17.35) onto an infinitesimal space increment,  $d\mathbf{x}$ , renders

$$d\mathbf{x} \cdot \nabla p = -\rho d\mathbf{x} \cdot \nabla\Phi \implies \frac{dp}{d\Phi} = -\rho. \quad (17.39)$$

Hence, the difference in hydrostatic pressure between any two geopotentials is given by the integral

$$p(\Phi_2) - p(\Phi_1) = - \int_{\Phi_1}^{\Phi_2} \rho(\Phi) d\Phi. \quad (17.40)$$

If  $\Phi = g z$  then we recover

$$p(z_2) - p(z_1) = -g \int_{z_1}^{z_2} \rho(z) dz, \quad (17.41)$$

so that the difference in hydrostatic pressure between two geopotentials is given by the weight per horizontal area of fluid between the two geopotentials. This relation is illustrated for an infinitesimally thin layer in Figure 17.2.

### 17.3.2 Comparison to approximate hydrostatic balance

A static fluid in a gravitational field exhibits hydrostatic balance whereby pressure at a point is a function solely of the geopotential, in which case  $p = p(z)$  when  $\Phi = g z$ . Correspondingly,

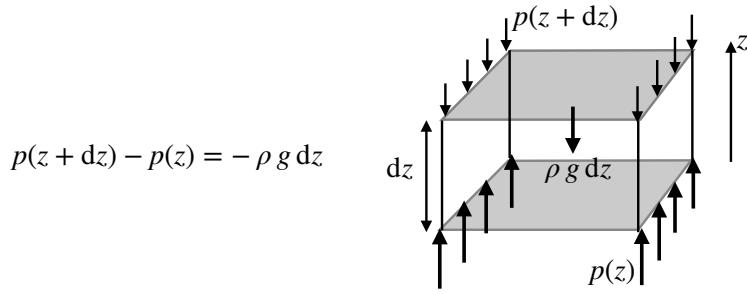


FIGURE 17.2: Illustrating the forces acting in a hydrostatically balanced fluid layer placed in a geopotential field  $\Phi = g z$  with  $g$  constant. The layer has an infinitesimal thickness  $dz > 0$ , density  $\rho$ , and horizontal cross-sectional area  $dA$ . The pressure force acting on the top and bottom of the layer are compressive. Hence, the pressure force at the top of the layer acts downward,  $\mathbf{F}^{\text{press}}(z + dz) = -\hat{z} p(z + dz) dA$ , whereas the pressure force at the bottom of the layer acts upward,  $\mathbf{F}^{\text{press}}(z) = +\hat{z} p(z) dA$ . In a hydrostatically balanced fluid, the difference in pressure across the layer is exactly balanced by the weight per area of fluid within the layer. Consequently,  $p(z + dz) - p(z) = -g \rho(z) dz$ , so that pressure at the top of the layer is less than that at the bottom.

$dp/dz = -\rho z$ , which means that we determine hydrostatic pressure at a point by computing the weight per horizontal area of fluid above that point. Likewise, density is just a function of geopotential since  $\nabla \rho \times \nabla \Phi = 0$ .

For an approximate hydrostatic fluid, pressure is a function of space and time,  $p = p(\mathbf{x}, t)$ , as is density,  $\rho = \rho(\mathbf{x}, t)$ . However, an approximate hydrostatic fluid satisfies  $\partial p / \partial z = -\rho g$ . Hence, column by column, the pressure at a point in an approximate hydrostatic fluid is determined by the weight per horizontal area of fluid above that point. This key property is thus shared between fluids in exact and approximate hydrostatic balance. We have more to say regarding approximate hydrostatic balance in Section 22.2.

## 17.4 Axial angular momentum

Following our discussion of a point particle in Section 10.7, the axial angular momentum of a fluid element is given by

$$L^z = (\rho \delta V) r_{\perp} (u + r_{\perp} \Omega) \equiv (\rho \delta V) l^z \quad (17.42)$$

where

$$l^z = r_{\perp} (u + r_{\perp} \Omega) \quad (17.43)$$

is the axial angular momentum per unit mass, and the distance to the polar rotation axis,

$$r_{\perp} = r \cos \phi \quad (17.44)$$

is the moment-arm for determining the torques acting on a fluid element. Making use of the zonal momentum equation (17.19) we find the material time change

$$\frac{Dl^z}{Dt} = (u + 2\Omega r_{\perp}) \frac{Dr_{\perp}}{Dt} + r_{\perp} \frac{Du}{Dt} \quad (17.45a)$$

$$= (u + 2\Omega r_{\perp}) \frac{Dr_{\perp}}{Dt} + (u + 2\Omega r_{\perp}) (v \sin \phi - w \cos \phi) - \frac{1}{\rho} \frac{\partial p}{\partial \lambda} \quad (17.45b)$$

$$= (u + 2\Omega r_{\perp}) \left[ \frac{Dr_{\perp}}{Dt} + v \sin \phi - w \cos \phi \right] - \frac{1}{\rho} \frac{\partial p}{\partial \lambda} \quad (17.45c)$$

$$= -\frac{1}{\rho} \frac{\partial p}{\partial \lambda}, \quad (17.45d)$$

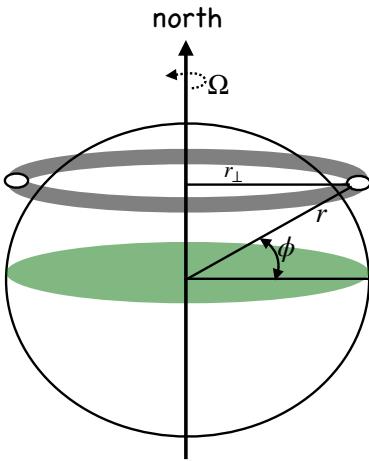


FIGURE 17.3: A ring of inviscid air circulating around a constant latitude circle over a smooth planet. This ring conserves is axial angular momentum. Consequently, axial angular momentum conserving motion of the ring induces a zonal acceleration if the ring alters its distance from the rotation axis,  $r_{\perp}$ , by moving meridionally or vertically.

so that

$$\rho \frac{Dl^z}{Dt} = -\frac{\partial p}{\partial \lambda} \implies \frac{\partial(\rho l^z)}{\partial t} + \nabla \cdot (\rho l^z \mathbf{v}) = -\frac{\partial p}{\partial \lambda}. \quad (17.46)$$

It is only in the absence of a zonal pressure gradient that the axial angular momentum for a fluid element is materially invariant just like for the point particle discussed in Section 10.7. The physical constraints for motion of the point particle, as described in Section 10.8, also hold for the fluid element. In particular, we can equate the zonal Coriolis acceleration to the zonal acceleration induced by axial angular momentum conservation. For example, a fluid element initially at rest in a fluid with zero zonal pressure gradient will zonally accelerate when moved meridionally (e.g., as from a meridional pressure gradient) according to the needs of axial angular momentum conservation.

### 17.4.1 Axial angular momentum conserving motion of a ring of air

Atmospheric and oceanic flows rarely experience a zero zonal pressure gradient. However, on a smooth spherical planet without meridional boundaries there is a zero zonally integrated zonal pressure gradient

$$\int_{\text{ring}} \frac{\partial p}{\partial \lambda} d\lambda = 0. \quad (17.47)$$

Hence, a constant mass ring of fluid circling the smooth planet (Figure 17.3) will preserve its axial angular momentum in the absence of friction

$$\frac{d}{dt} \oint_{\text{ring}} \rho l^z dV = \oint_{\text{ring}} \rho \frac{Dl^z}{Dt} dV = - \oint_{\text{ring}} \frac{\partial p}{\partial \lambda} dV = 0. \quad (17.48)$$

For example, consider a latitudinal ring of constant mass inviscid fluid circling around the equator at radius  $R_e$ , and assume it is at rest relative to the rotating earth. The angular momentum per mass for this ring is  $l^z = \Omega R_e^2$ . Moving the ring vertically to  $r \neq R_e$  while maintaining constant axial angular momentum induces a zonal velocity given by

$$u = \frac{\Omega(R_e^2 - r^2)}{r}. \quad (17.49)$$

Movement downward to  $r < R_e$  leads to an eastward flow,  $u > 0$ , (westerly winds), whereas upward motion leads to the opposite. Likewise, moving the ring latitudinally while keeping  $r = R_e$  leads to the zonal velocity

$$u = \frac{\Omega R_e \sin^2 \phi}{\cos \phi}. \quad (17.50)$$

Since  $\cos \phi \geq 0$  on the sphere, latitudinal motion away from the equator while preserving axial angular momentum leads to eastward flow ( $u > 0$ ) whether the ring is moved northward or southward.

### 17.4.2 Sketching the atmospheric angular momentum budget

How realistic is it to have coherent rings of inviscid air circulating around the planet at all latitudes? To answer this question we insert some numbers for a ring of radius  $R_e$  that starts with zero relative velocity at the equator. Equation (17.50) says that the westerly winds induced by axial angular momentum conserving motion have the following speeds at a selection of latitudes

$$u(10^\circ) = 14 \text{ m s}^{-1} \quad u(20^\circ) = 58 \text{ m s}^{-1} \quad u(30^\circ) = 134 \text{ m s}^{-1}. \quad (17.51)$$

The values at higher latitudes grow unbounded since  $\cos \phi \rightarrow 0$  as the poles are approached. So there is a problem with an idealized theory of atmospheric circulation based on axial angular momentum conserving rings of air. It turns out that inviscid axial angular momentum conserving ideas extend only so far as the Hadley circulation is concerned, with the latitude extents of the Hadley Cell extending only to the middle latitudes. There are two missing ingredients to a more realistic theory: (i) frictional dissipation between the atmosphere and land; (ii) baroclinic eddies that contribute to poleward transport of angular momentum. It is outside of our scope to detail these physical processes and the corresponding atmospheric circulation. Instead, we here simply sketch the scene following Section 10.3 of [Holton \(1992\)](#) and Section 8.2 of [Marshall and Plum \(2008\)](#).

Given that the earth has a near constant rotation rate, we can examine a zonally integrated axial momentum budget for the atmosphere and assume that the axial angular momentum of the earth is fixed.<sup>4</sup> Rather than an inviscid fluid, we consider the dissipation due to boundary layer friction and/or vertical eddy form stress from baroclinic eddies (we study form stress in Chapter 19). In the tropical atmosphere, the atmosphere generally has less angular momentum than the earth given that the winds are predominantly easterly (lower branch of the Hadley Cell). In this region, boundary layer interactions transfer angular momentum from the earth to the atmosphere. In contrast, the presence of middle latitude westerlies aloft (upper branch of the Hadley Cell) signal that the atmosphere has more angular momentum than the earth at these latitudes. There is an implied transfer of angular momentum from the atmosphere to the earth, largely mediated through vertical form stresses due to baroclinic eddies.

As sketched in Figure 17.4, a steady state axial angular momentum budget is realized through a meridional transport of axial angular momentum from the lower latitude atmosphere to the middle latitudes. This transport is mediated partly through an atmospheric overturning circulation (Hadley Cell) and partly through the vertical transfer of momentum via synoptic scale baroclinic eddies (see Section 48.3.5). Furthermore, dissipation by eddies and boundary layer interactions is crucial to realize the observed zonal wind profile. Namely, as seen above, a non-dissipative angular momentum conserving atmosphere exhibits winds that are far larger in magnitude than observed, particularly when moving to higher latitudes.

<sup>4</sup>In fact, the length of a day fluctuates by roughly  $10^{-3}$  s over a seasonal cycle due to transfer of axial angular momentum between the atmosphere and land.

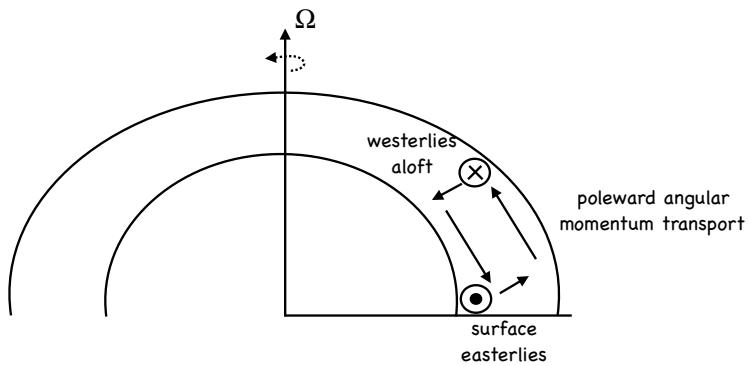


FIGURE 17.4: A sketch of the Hadley circulation. At the low latitudes, low level winds are predominantly easterly (blowing to the west) and so the atmosphere gains positive axial angular momentum from the earth via frictional boundary layer processes. As air rises and moves poleward it zonally accelerates according to conservation of axial angular momentum, thus becoming the mid-latitude westerlies (blowing to the east). The westerlies are generally unstable thus producing baroclinic eddies that vertically transfer axial angular momentum via form stress, thus depositing axial angular momentum back to the earth to close the axial angular momentum cycle.

### 17.4.3 Further study

In Section 19.5 we consider the zonally integrated axial angular momentum budget for the ocean with sloping solid-earth bottom boundary as well as the upper surface (ocean) boundary. In particular, we see how boundary form stresses (Section 19.1) affect the angular momentum in addition to boundary frictional stresses. That analysis is analogous to that for the atmosphere given in Section 10.3 of [Holton \(1992\)](#).

## 17.5 Acoustic waves

In building up our understanding of geophysical fluid dynamics, it is useful to focus on selected pieces of the dynamical equations to see what sorts of phenomena they encompass. In that spirit, we here temporarily discard all portions of the momentum equation (17.16) having to do with geophysics. Namely, we consider a homogeneous perfect fluid in free space, so that the only acceleration arises from pressure gradients

$$\rho \frac{D\mathbf{v}}{Dt} = -\nabla p. \quad (17.52)$$

Mass remains materially conserved, so that this form of the Euler equation is coupled to the mass continuity equation

$$\partial_t \rho + \nabla \cdot (\mathbf{v} \rho) = 0, \quad (17.53)$$

with an assumed equation of state

$$\rho = \rho(p) \quad (17.54)$$

providing a relation between pressure and density.<sup>5</sup> Although highly simplified relative to their geophysically more complete form, these equations are coupled nonlinear partial differential equations that are tough to solve in general. When faced with such complexity it is generally useful to examine the linearized form of the equations. As we now show, the linearized equations supports acoustic waves.

<sup>5</sup>We study equations of state, including the ideal gas equation, in Chapters 20 and 24. Furthermore, as discussed in Chapter 35, an equation of state with  $\rho = \rho(p)$  leads to a barotropic fluid.

### 17.5.1 Rudiments of acoustic waves

Consider a motionless base state and examine small amplitude fluctuations about that state. Since we are ignoring gravity, the pressure and density of the base state are uniform constants,  $p_0$  and  $\rho_0$ . Linearizing the Euler equation (17.52) and mass continuity equation (17.53) leads to the linear system

$$\rho_0 \frac{\partial \mathbf{v}}{\partial t} = -\nabla p \quad (17.55a)$$

$$\frac{\partial p}{\partial t} + c_s^2 \rho_0 \nabla \cdot \mathbf{v} = 0. \quad (17.55b)$$

In the continuity equation we introduced the inverse squared acoustic (sound) speed of the base state

$$c_s^{-2} = \left[ \left( \frac{\partial \rho}{\partial p} \right)_S \right]_{p=p_0}, \quad (17.56)$$

where the pressure derivative is computed with a fixed entropy,  $S$  (matter concentration is also held fixed when considering sound speeds in a non-homogeneous fluid). We assume the entropy is fixed when computing the density derivative since the frequency of acoustic oscillations are so high that there is no time for heat to flow. Hence, sound waves are reversible adiabatic waves, which accords with our use of the perfect fluid equations. We offer further discussion of the sound speed in Sections 20.8.4 and 20.12.8, as part of the thermodynamics chapter.<sup>6</sup>

The velocity,  $\mathbf{v}$ , in equation (17.55a) and pressure,  $p$  in equation (17.55b) are fluctuations relative to the base state. Taking the divergence of the velocity equation (17.55a) and making use of the continuity equation (17.55b) leads to

$$(\partial_{tt} - c_s^2 \nabla^2) p = 0, \quad (17.57)$$

which is the canonical wave equation discussed in Section 3.7. The solutions to this equation are linear and non-dispersive *acoustic waves* or *sound waves* with phase speed  $c_s$ . Since the waves are non-dispersive, their group speed equals to their phase speed. Additionally, the linear velocity equation (17.55a) reveals that pressure fluctuations and fluid particle fluctuations are in the same direction, with such waves known as *longitudinal waves*. Waves encountered later in this book appearing in incompressible flows are *transverse waves*, where  $\mathbf{k} \cdot \mathbf{v} = 0$ , so that fluid particle motion is perpendicular to the wave direction.

Acoustic waves propagate in all directions and they carry information about pressure fluctuations. Their squared speed is determined by isentropic compressibility of the base state. For example, a more compressible media, such as the atmosphere, has a smaller sound speed ( $c_s \approx 350 \text{ m s}^{-1}$ ) than a less compressible media, such as the ocean ( $c_s \approx 1500 \text{ m s}^{-1}$ ). Indeed, acoustic waves have infinite phase speed when the media is incompressible, with the infinite phase speed a signature that the hyperbolic wave system has converted to an elliptic system (see Chapter 3).

The *Mach number* is the ratio of the fluid particle speed to the sound speed. If a fluid is moving with Mach number greater than unity (super-sonic), then there can be discontinuities (shocks) that break the continuum approximation (Chapter 11). In this case, the continuous fluid equations must be supplemented by other physical conditions such as those afforded by molecular dynamics. We have no occasion to study super-sonic flows in this book.

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<sup>6</sup>On first encounter, one may incorrectly compute the sound speed as the density derivative holding temperature fixed rather than entropy, thus leading to the incorrect speed of sound. This mistake was also made by Newton in his original studies of sound.

## 17.5.2 Further study

Our treatment of acoustic waves is very terse, largely since we only wish to expose their role in propagating pressure fluctuations rather than embark on the rather interesting, yet sizable, job of studying the kinematics and dynamics of sound in the atmosphere and ocean. That topic is outside our scope. There are many pedagogical treatments that one can find, such as the physics treatment give in Section 16.5 of [Thorne and Blandford \(2017\)](#) and the oceanographic treatment in Chapter 7 of [Apel \(1987\)](#). [Vallis \(2017\)](#) discusses acoustic-gravity waves for an ideal gas in his Section 7.8, with these waves feeling both compressibility and gravity. See also his Chapter 6 for a lucid summary of wave kinematics.

## 17.6 Exercises

### EXERCISE 17.1: THEOREM OF STRESS MEANS ([Aris \(1962\)](#)) EXERCISE 5.12.2

Make use of Cauchy's equation of motion (17.14) and the divergence theorem to prove the *theorem of stress means*

$$\oint_{\partial\mathcal{R}} \Psi \mathbb{T}_{pq} \hat{n}_q d\mathcal{S} = \int_{\mathcal{R}} \left[ \mathbb{T}_{pq} \partial_q \Psi + \rho \Psi \left( \frac{Dv_p}{Dt} - f_p \right) \right] dV, \quad (17.58)$$

where  $\Psi$  is an arbitrary differentiable function, and  $\hat{n}_q$  is the  $q$ 'th component of the outward normal vector on  $\partial\mathcal{R}$ . This theorem finds use in certain formulations of continuum mechanics. Assume Cartesian tensors.

### EXERCISE 17.2: TIME SYMMETRY OF THE EULER EQUATION

In Section 10.3 we studied the needs for time reversal symmetry in the equations of a point particle. Here we ask the same question for the Euler equation (17.18) in a rotating reference frame. Consider a solution,  $\mathbf{v}(\mathbf{x}, t)$ , to the Euler equation (17.18) in a rotating reference frame in either free space (i.e., no boundaries) or with fixed material boundaries. What transformation properties are needed for  $p(\mathbf{x}, t)$ ,  $\rho(\mathbf{x}, t)$ ,  $\Phi(\mathbf{x}, t)$ , and  $\boldsymbol{\Omega}$  to ensure that  $\mathbf{v}^*(\mathbf{x}, t^*) = -\mathbf{v}(\mathbf{x}, -t)$  is also a solution? That is, what time symmetry properties ensure that the velocity is reversible so that if  $\mathbf{v}(\mathbf{x}, t)$  is a solution then so is  $-\mathbf{v}(\mathbf{x}, -t)$ ? Discuss your answer.

### EXERCISE 17.3: AREA OF A STEADY 1D LAMINAR JET EMANATING FROM A DOWNWARD NOZZLE

Consider a steady state laminar jet of constant density and inviscid water emanating from a downward facing nozzle with a constant prescribed volume flow rate,  $Q$  (dimensions volume per time). Ignore surface tension and assume the air pressure acting on the surface of the jet is constant all along the jet. You can solve this exercise by making use of the steady vertical momentum equation and the steady mass continuity equation.

- (a) Explain why we can set  $dp/dz = 0$  within the jet once it leaves the nozzle.
- (b) Determine an expression for the area of the jet,  $A(z)$ , as a function of distance,  $z$ , from the nozzle, with the nozzle placed at  $z = 0$  and  $z < 0$  a position beneath the nozzle. In addition to  $z$ , your expression will contain  $Q$ ,  $g$ , and  $A(0)$ .
- (c) Is the area of the jet getting smaller or larger as the water moves downward away from the nozzle? Does this answer agree with your experience?
- (d) If the downward speed of water at the nozzle is  $w(0) = 0.5 \text{ m s}^{-1}$ , then at what vertical position,  $z$ , is the area of the jet four times different than at  $z = 0$ ?





# Chapter 18

## Stress in fluids

As an extended continuous region of matter, a fluid element experiences two kinds of forces: *external* or *body* forces and *internal* or *contact* forces. Body forces act throughout the fluid element and arise from sources external to the matter acted upon. The accumulated effects from body forces within a fluid region result from volume integrating the body forces over the region. In geophysical fluid mechanics, we are concerned with body forces from the effective gravitational acceleration (central gravity plus planetary centrifugal) plus the body force from the Coriolis acceleration. Body forces are also experienced by the point particles studied in Part II in this book.

Contact forces act on a fluid element due to local intermolecular forces within the fluid media. Contact forces signal a fundamental distinction between the dynamics of a fluid element (an infinitesimal portion of a continuous media) and the dynamics of a point particle. Contact forces give rise to the local exchange of dynamical properties between fluid elements. Dividing the contact force by the area upon which it acts leads to the stress vector acting on the surface. As a force per unit area, stresses are associated with two directions: the direction of the force and the direction normal to the area acted upon by the force. Correspondingly, stresses acting on a fluid element are naturally organized into a second order *stress tensor*. Contact forces, which are given by the stress times an area element, satisfy Newton's third law, also known as the action/reaction law. Hence, the net contact force acting on a finite region arises just from the contact forces acting at the region boundary. This property of contact forces means that a mechanically isolated region of a continuous media (i.e., a region unaffected by external forces or boundary contact forces) does not spontaneously translate its center of mass.

*Surface tension* is a rather unique kind of stress acting on fluid boundaries such as oil and water or air and water. As shown in Section 18.10, surface tension is generally negligible for length scales larger than a few centimeters. It is for this reason that surface tension is commonly absent from books on geophysical fluid mechanics, where most concern is with larger length scales. Nevertheless, the effects are important if studying physical processes associated with air-sea interactions, such as tracer, heat, and momentum exchange through bubbles, droplets, and capillary-gravity waves.

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## CHAPTER GUIDE

We introduced contact forces in Chapter 17 when deriving the fluid equations of motion. In this chapter we dive deeper into contact forces and their corresponding stresses. We also discuss conditions placed on stress and velocity at boundaries. The material in this chapter builds from our study of forces, acceleration, and Newton's laws as applied to a fluid continuum in Chapter 17. Fluid stresses can be organized into a second order tensor and further decomposed into pressure stresses and viscous/frictional stresses. Understanding the mathematical and physical aspects of stress is important for the suite of fluid models studied in this book. Because the material involves vectors and tensors it can require a bit more patience from the reader than analogous chapters that discuss scalar fields. To make the formalism less mathematically intense, we employ Cartesian tensors as discussed in Chapters 1 and 2. Results can be generalized to arbitrary coordinates through the general tensor analysis detailed in Chapter 7.

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18.1	Cauchy's stress principle and Newton's laws . . . . .	375
18.1.1	Cauchy's stress principle . . . . .	375
18.1.2	Newton's third law and local equilibrium of stresses . . . . .	375
18.1.3	Comments on the local equilibrium relation . . . . .	376
18.2	The stress tensor . . . . .	377
18.3	Angular momentum and stress tensor symmetry . . . . .	380
18.3.1	Basic formulation . . . . .	381
18.3.2	Physical interpretation . . . . .	381
18.3.3	Symmetry of the stress tensor . . . . .	382
18.4	Forces and torques in a static fluid . . . . .	383
18.4.1	Force balance . . . . .	383
18.4.2	Pressure force balance for a homogeneous fluid . . . . .	384
18.4.3	Torque balance . . . . .	385
18.5	Flux-form Eulerian momentum equation . . . . .	387
18.6	Linear momentum for arbitrary regions . . . . .	388
18.7	Constitutive relation between stress and rate of strain . . . . .	389
18.7.1	Thermodynamic pressure and mechanical pressure . . . . .	389
18.7.2	Couette flow and the viscous tensor . . . . .	389
18.7.3	d'Alembert's theorem for perfect fluids . . . . .	390
18.7.4	Guidance from Galilean invariance . . . . .	391
18.7.5	A comment on Rayleigh drag . . . . .	391
18.7.6	Constitutive relation for Newtonian fluids . . . . .	391
18.7.7	Navier-Stokes and Euler equations . . . . .	393
18.7.8	Laplacian friction in terms of vorticity and divergence . . . . .	394
18.7.9	Frictional stresses in a sheared flow . . . . .	395
18.7.10	The net stress tensor . . . . .	396
18.7.11	Comments and further study . . . . .	396
18.8	Reynolds number and flow regimes . . . . .	396
18.8.1	Non-dimensional Navier-Stokes . . . . .	396
18.8.2	Ratio of inertial to frictional accelerations . . . . .	397
18.8.3	Reynolds numbers for some example flows . . . . .	397
18.9	Stress on an interface . . . . .	398
18.9.1	General formulation . . . . .	399
18.9.2	Solid material boundary . . . . .	400
18.9.3	No-slip boundary condition . . . . .	400
18.9.4	Lagrangian interface . . . . .	401
18.9.5	Permeable interface . . . . .	401

18.9.6 Summary comments . . . . .	402
18.9.7 Comments on boundary layers . . . . .	402
18.10 Surface tension . . . . .	<b>402</b>
18.10.1 Force balance on an air-water interface . . . . .	403
18.10.2 Young-Laplace formula . . . . .	405
18.10.3 Some oceanographic examples . . . . .	407
18.10.4 Further study . . . . .	408
18.11 Exercises . . . . .	<b>408</b>

## 18.1 Cauchy's stress principle and Newton's laws

We here develop some general properties of contact forces and the associated stresses. For that purpose, consider an arbitrary smooth closed region,  $\mathcal{R}$ , of fluid with volume  $V = \int_{\mathcal{R}} dV$  and mass  $M = \int_{\mathcal{R}} \rho dV$  (Figure 18.1). Furthermore, let  $\partial\mathcal{R}$  be the bounding surface for the region, and let  $\hat{\mathbf{n}}$  be the outward normal at a point on the boundary.

### 18.1.1 Cauchy's stress principle

The bounding surface of the region experiences mechanical interactions with the surrounding fluid continuum and these interactions lead to contact forces acting on the boundary. Let  $\boldsymbol{\tau}$  be the stress vector (force per unit area) acting at a point on  $\partial\mathcal{R}$ . Cauchy's stress principle asserts that the stress vector is a function of the position, time, and boundary normal

$$\boldsymbol{\tau} = \boldsymbol{\tau}(\mathbf{x}, t, \hat{\mathbf{n}}). \quad (18.1)$$

The dependence on boundary normal means that the stress acting on a surface is generally a function of the orientation of that surface. This form of the stress trivially holds for an exactly hydrostatic fluid where the stress vector is proportional to the pressure (Section 17.3). Furthermore, the stress from pressure is oriented along the inward normal, thus reflecting the purely compressive nature of pressure

$$\boldsymbol{\tau} = -p(\mathbf{x}, t) \hat{\mathbf{n}} \quad \text{static fluid in hydrostatic balance.} \quad (18.2)$$

Cauchy's stress principle is sensible for points within the fluid media, and its relevance has been supported by experimental studies over the time since Cauchy made this assertion in the year 1823. Furthermore, it holds for pressure and viscous stresses at the interface between fluid media or at solid-earth boundaries. However, Cauchy's stress principle does not hold for surface tension, which is proportional to the curvature of the surface separating two fluid media (e.g., atmosphere and ocean), where curvature involves spatial gradients of the normal vector. As discussed in Section 18.10, surface tension effects are important for relatively small scales (order centimeters), and as such play a minor role in this book. Hence, with the single exception of surface tension, we rely on Cauchy's stress principle to formulate the fluid dynamical equations.

### 18.1.2 Newton's third law and local equilibrium of stresses

Newton's second law says that in an inertial reference frame, unbalanced forces acting on a physical system affect a time change to the linear momentum. Consider a region,  $\mathcal{R}(\mathbf{v})$ , whose fluid elements follow the barycentric velocity. Newton's law then states that the material time

evolution of the region's linear momentum is given by

$$\frac{d}{dt} \int_{\mathcal{R}(\mathbf{v})} \mathbf{v} \rho dV = \int_{\mathcal{R}(\mathbf{v})} \mathbf{f} \rho dV + \oint_{\partial\mathcal{R}(\mathbf{v})} \boldsymbol{\tau} d\mathcal{S}, \quad (18.3)$$

where  $\int_{\mathcal{R}(\mathbf{v})} \mathbf{f} \rho dV$  is the domain integrated body force (from central gravity, planetary centrifugal, and Coriolis). To develop a general property for the contact forces, consider this balance for a region whose size gets infinitesimally small. Assuming the integrands for the two volume integrals are well behaved (i.e., smooth and bounded) as the region size goes to zero, we see that the volume integrals are proportional to  $L^3$ , where  $L$  is a length scale measuring the size of the region (e.g., side for a cubical region or diameter for a spherical region). In the same manner, we assume the stresses are well behaved in the case of an infinitesimal region. However, the integral of the contact forces goes to zero at the slower rate that is proportional to  $L^2$ . Self-consistency for the balance (18.3) over a region of infinitesimal size thus requires the contact forces to satisfy the limiting behavior

$$\lim_{L \rightarrow 0} \frac{1}{L^2} \oint_{\partial\mathcal{R}(\mathbf{v})} \boldsymbol{\tau} d\mathcal{S} = 0. \quad (18.4)$$

This behavior means that contact forces at a point in the fluid must be in local equilibrium. Equation (18.4) is sometimes referred to as *Cauchy's fundamental lemma*.

A direct implication of the local equilibrium statement is that stress vectors that respect Cauchy's principle (18.1) satisfy

$$\boldsymbol{\tau}(\mathbf{x}, t, \hat{\mathbf{n}}) = -\boldsymbol{\tau}(\mathbf{x}, t, -\hat{\mathbf{n}}). \quad (18.5)$$

For example, the stress vector on one side of a surface is equal and oppositely directed to the stress vector acting on the other side. This equation is an expression of Newton's third law of mechanics (the action/reaction law), here written in terms of the stresses acting in a continuous media. It is of fundamental importance throughout our study of contact forces and their associated stresses acting within the fluid and at boundaries. We thus see how an application of Newton's second law, the linear momentum principle (18.3) for a continuous media, leads to a statement of Newton's third law, (18.5), for contact forces.

As an example of the above ideas, the simplest stress we consider in this chapter is that from pressure, with pressure acting solely in a compressive manner so that the stress vector takes the form

$$\boldsymbol{\tau}^{\text{press}}(\mathbf{x}, t, \hat{\mathbf{n}}) = -p(\mathbf{x}, t) \hat{\mathbf{n}}. \quad (18.6)$$

This stress trivially satisfies the Newton's third law relation (18.5) since

$$\boldsymbol{\tau}^{\text{press}}(\mathbf{x}, t, \hat{\mathbf{n}}) = -\boldsymbol{\tau}^{\text{press}}(\mathbf{x}, t, -\hat{\mathbf{n}}). \quad (18.7)$$

### 18.1.3 Comments on the local equilibrium relation

The local equilibrium relation (18.4), and the corresponding expression of Newton's third law, (18.5), might suggest that stresses cannot lead to motion. However, that suggestion is incorrect since stresses integrated over a finite region can lead to a net force that causes motion. Since contact forces within the domain interior cancel pointwise, the local equilibrium relation (18.4) says that the net contact force acting on the region arises only from the area integrated stresses acting on the region boundary. Local or pointwise mechanical equilibrium does not imply mechanical equilibrium for finite regions.

To further emphasize the above point, consider an ocean region bounded at its bottom by the

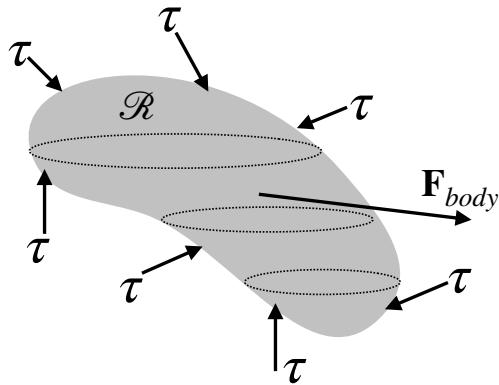


FIGURE 18.1: Schematic of the net body force,  $\mathbf{F}_{body}$ , acting on a finite region of fluid, plus the accumulation of stress vectors,  $\tau$ , acting on the region boundaries. The net body force is determined by a volume integral of the body force (gravity, centrifugal, and Coriolis) at each point within the volume. In contrast, since the stresses are in local equilibrium, the volume integral of the stress divergence reduces to an area integral of the stress over the region boundary. Stress arises from pressure (compressive and normal) and strains (which then lead to viscous stresses when there is viscosity). The area integrated contribution from pressure to horizontal accelerations is referred to as *form stress*. The form stress coming from the bottom boundary is called the *topographic form stress*. The form stress appearing at the air-sea boundary is the *atmospheric form stress* if considering ocean dynamics and *oceanic form stress* if considering atmospheric dynamics. We study form stress in Chapter 19.

solid earth and its upper surface by a massive atmosphere. Variations (divergences) in stresses over finite regions within the ocean fluid lead to accelerations; e.g., ocean circulation. However, when integrated over the full ocean domain, all stresses cancel pointwise. Consequently, the net contact force acting on the full ocean domain reduces to the contact force acting just on the ocean boundaries. The boundary contact forces arise from mechanical interactions with the solid-earth and the overlying atmosphere. The center of mass for the ocean basin remains static if the accumulation of forces sum to zero, which includes the contact forces acting over its boundaries plus the volume integrated body forces from effective gravity (central gravity plus planetary centrifugal) and Coriolis.

In Figure 18.2 we illustrate the net pressure force acting on an arbitrary fluid domain. Pressure acts solely in a compressive manner as directed along the inward normal to the domain. Area integration over a domain boundary renders the net pressure force acting on the domain

$$\mathbf{F}^{\text{pressure}} = - \oint_{\partial\mathcal{R}} p \hat{\mathbf{n}} d\mathcal{S} = - \int_{\mathcal{R}} \nabla p dV, \quad (18.8)$$

where the second equality follows from application of Gauss's divergence theorem for a scalar field (Section 2.7.2). When decomposed according to coordinate axes, the pressure force acting on the boundary has a component in both the vertical and horizontal directions, thus contributing to both vertical and horizontal accelerations. The vertical accelerations are closely balanced by the weight of fluid, with exact balance in the case of a hydrostatic fluid. The horizontal stresses from pressure are known as *form stress*. This name arises since the stress depends on the form, or shape, of the interface on which pressure acts.

## 18.2 The stress tensor

Cauchy's stress principle reduces the mathematical complexity of describing stress vectors. A further implication of this principle leads to *Cauchy's theorem*, which states that the stress vector,

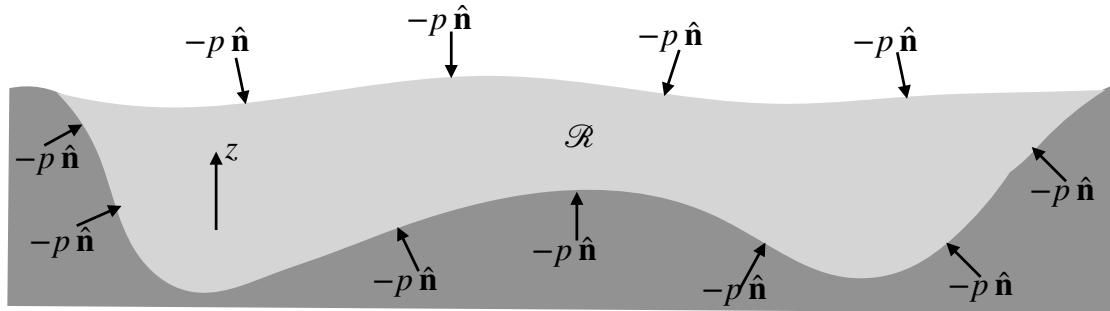


FIGURE 18.2: Schematic of contact forces from pressure acting on the boundaries to an ocean domain. Pressure forces are directed according to minus the local normal since pressure is a compressive force aligned with the inward normal direction. As with all contact forces, the pressure forces acting in the interior of the ocean are locally in mechanical equilibrium. Hence, when integrated over the global domain the net pressure forces only arise at the domain boundaries. That is, the net pressure force acting on the full ocean domain arises only at the interface between the solid-earth and the ocean, plus the interface between the atmosphere and the ocean. Note that the pressure force has a component in both the vertical and horizontal directions as per the orientation of the local normal vector. Further boundary stresses arise from viscous exchange, which generally have components perpendicular to the boundary normal; i.e., tangential to the boundary. Such stresses also satisfy Newton's third law.

which is a function of space, time, and normal direction, can be expressed in terms of a stress tensor (a function of space and time) projected into the direction of the normal. The purpose of this section is to provide arguments supporting this theorem.

For this purpose, consider the tetrahedron fluid region shown in Figure 18.3, where three of the four sides are aligned according to the Cartesian coordinate axes and the fourth side has an outward normal,  $\hat{n} = (\hat{n}_1, \hat{n}_2, \hat{n}_3)$ , projecting into all three directions. The results developed for this rather contrived region hold for an arbitrary region using arbitrary coordinates. The reason for this generality is that once we derive a tensorially correct result using one choice of coordinates, such as Cartesian used here, we can make use of general tensor analysis (Chapters 6 and 7) to move from specific coordinates to arbitrary coordinates.

In the limit that the tetrahedron size goes to zero, local equilibrium of the contact forces means that

$$-\sum_{m=1}^3 \tau_{(m)} dA_m + \tau_{\hat{n}} dA = 0, \quad (18.9)$$

where we use the shorthand expression for the outward normal directed stress vector

$$\tau(\mathbf{x}, t, \hat{n}) = \tau_{\hat{n}}. \quad (18.10)$$

In equation (18.9),  $\tau_{(m)} dA_m$  (no implied summation) is the contact force vector acting on the face with outward normal parallel to the corresponding coordinate axis and  $\tau_{\hat{n}} dA$  is the contact force acting on the slanted face with outward normal  $\hat{n}$ . The minus sign arises for the summation term since the outward normals for these three faces point in the negative coordinate directions, and our convention is for  $\tau_{(m)}$  to align with the positive coordinate directions. The areas for each face are related to the slanted face area through

$$dA_m = \hat{n}_m dA, \quad (18.11)$$

so that the local equilibrium relation (18.9) becomes

$$\boldsymbol{\tau}_{\hat{n}} = \sum_{m=1}^3 \hat{n}_m \boldsymbol{\tau}_{(m)}. \quad (18.12)$$

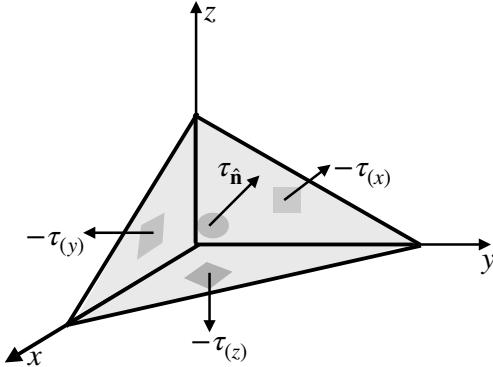


FIGURE 18.3: Tetrahedron region of fluid with stresses acting on the four faces. Note that the stresses are not necessarily directed normal to the faces. Local equilibrium of stresses means that the accumulation of these four stresses around the region volume adds to zero as the region volume goes to zero.

Equation (18.12) can be organized into a matrix-vector equation

$$\begin{bmatrix} (\tau_{\hat{n}})_1 \\ (\tau_{\hat{n}})_2 \\ (\tau_{\hat{n}})_3 \end{bmatrix} = [\hat{n}_1 \quad \hat{n}_2 \quad \hat{n}_3] \begin{bmatrix} \tau_{(1)1} & \tau_{(1)2} & \tau_{(1)3} \\ \tau_{(2)1} & \tau_{(2)2} & \tau_{(2)3} \\ \tau_{(3)1} & \tau_{(3)2} & \tau_{(3)3} \end{bmatrix}, \quad (18.13)$$

where each matrix element is the  $n$ -component of the  $m$ -stress  $\boldsymbol{\tau}_{(m)}$ . We introduce a less cumbersome notation by writing

$$\begin{bmatrix} (\tau_{\hat{n}})_1 \\ (\tau_{\hat{n}})_2 \\ (\tau_{\hat{n}})_3 \end{bmatrix} = [\hat{n}_1 \quad \hat{n}_2 \quad \hat{n}_3] \begin{bmatrix} \mathbb{T}_{11} & \mathbb{T}_{12} & \mathbb{T}_{13} \\ \mathbb{T}_{21} & \mathbb{T}_{22} & \mathbb{T}_{23} \\ \mathbb{T}_{31} & \mathbb{T}_{32} & \mathbb{T}_{33} \end{bmatrix}, \quad (18.14)$$

so that  $\mathbb{T}_{mn}$  measures the force per area in the  $n$ -direction along a surface whose outward normal points in the  $m$ -direction, as depicted in Figure 18.4. Making use of  $\mathbb{T}_{mn}$  in the expression (18.12) leads to

$$(\boldsymbol{\tau}_{\hat{n}})_n = \sum_{m=1}^3 \hat{n}_m \mathbb{T}_{mn}, \quad (18.15)$$

which can be written more succinctly as

$$\boldsymbol{\tau}_{\hat{n}} = \hat{n} \cdot \mathbb{T}. \quad (18.16)$$

We thus see that the stress vector acting on a surface oriented according to a normal vector,  $\hat{n}$ , equals to the projection of the *stress tensor*,  $\mathbb{T}$ , onto the normal vector. Exposing functional dependence reveals

$$\boldsymbol{\tau}_{\hat{n}}(\mathbf{x}, t, \hat{n}) = \hat{n} \cdot \mathbb{T}(\mathbf{x}, t), \quad (18.17)$$

which manifests Cauchy's theorem. Namely, the stress vector  $\boldsymbol{\tau}_{\hat{n}}$ , which is a function of  $(\mathbf{x}, t, \hat{n})$ , has been decomposed into a stress tensor,  $\mathbb{T}$ , which is a function of  $(\mathbf{x}, t)$ , as well as the projection

of the stress tensor into a direction  $\hat{n}$ .

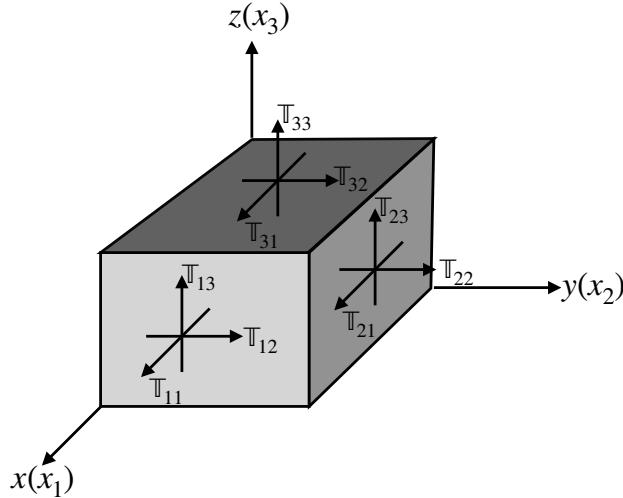


FIGURE 18.4: Illustrating the components to the stress tensor,  $T_{mn}$  and how they are organized according to the coordinate axes. The component  $T_{mn}$  is the stress that points in the  $n$ -direction along the face with outward normal in the  $m$ -direction.

How do we know that  $T_{mn}$  form the components to a tensor rather than just being elements of a  $3 \times 3$  matrix? To answer this question we note that each component of  $T$  is a force per area, with force a vector and area orientable by its outward normal. As it is built from vectors, which are first order tensors, we suspect that  $T$  should be a proper second order tensor. This suspicion is supported by the quotient rule from tensor analysis (Section 6.1.1). Namely, the quotient rule means that equation (18.15) indeed yields  $T_{mn}$  that are components to a second order tensor. As components to a second order tensor, the tensor components,  $T_{mn}$ , transform under a coordinate transformation according to the rules developed in Chapter 1 for Cartesian tensors and in Chapter 7 for general tensors. Through the power of tensor analysis, we thus see that our considerations, based on the rather contrived tetrahedron region in Figure 18.3, hold for an arbitrary region described by an arbitrary coordinate system.

## 18.3 Angular momentum and stress tensor symmetry

The linear momentum principle afforded by Newton's law of motion allowed us to deduce the local equilibrium property (18.4) of the stress. We here derive a constraint placed on the stress tensor that is imposed by studying angular momentum. Phenomenologically, we observe that geophysical fluids, as with most common fluids, experience torques only as the moments of body forces acting throughout the volume of a fluid region, or as moments of contact forces acting on the surface bounding the fluid region. We now make use of this observation to deduce symmetry of the stress tensor.<sup>1</sup>

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<sup>1</sup>Page 11 of [Batchelor \(1967\)](#) and Section 5.13 of [Aris \(1962\)](#) offer brief discussions of fluids in which internal force couples lead to torques distinct from those considered here, and in which the stress tensor has an anti-symmetric component. [Dahler and Scriven \(1961\)](#) provide a more thorough account.

### 18.3.1 Basic formulation

Consider a constant mass fluid element that has a Cartesian position  $\mathbf{x}$  relative to an arbitrary origin. The angular momentum of the fluid element with respect to the origin is

$$\mathbf{L} = \rho \delta V (\mathbf{x} \times \mathbf{v}), \quad (18.18)$$

and its material time evolution is

$$\frac{D\mathbf{L}}{Dt} = \rho \delta V \mathbf{x} \times \frac{D\mathbf{v}}{Dt}, \quad (18.19)$$

which follows since  $D(\rho \delta V)/Dt = 0$ ,  $D\mathbf{x}/Dt = \mathbf{v}$ , and  $\mathbf{v} \times \mathbf{v} = 0$ . Making use of Cauchy's form for the equation of motion (17.14)

$$\rho \frac{D\mathbf{v}}{Dt} = \rho \mathbf{f} + \nabla \cdot \mathbb{T} \quad (18.20)$$

allows us to write the angular momentum evolution as

$$\frac{D\mathbf{L}}{Dt} = \delta V \mathbf{x} \times (\rho \mathbf{f} + \nabla \cdot \mathbb{T}). \quad (18.21)$$

The first term arises from body forces (e.g., central gravity, planetary centrifugal, and Coriolis) and the second term arises from the divergence of stresses. Expanding the stress divergence term renders

$$\left[ \frac{D\mathbf{L}_m}{Dt} \right]_{\text{stress}} = \delta V \epsilon_{mnp} x_n (\nabla \cdot \mathbb{T})_p \quad (18.22a)$$

$$= \delta V \epsilon_{mnp} x_n \partial_q \mathbb{T}_{pq} \quad (18.22b)$$

$$= \delta V \epsilon_{mnp} [\partial_q (x_n \mathbb{T}_{pq}) - (\partial_q x_n) \mathbb{T}_{pq}] \quad (18.22c)$$

$$= \delta V \epsilon_{mnp} [\partial_q (x_n \mathbb{T}_{pq}) - \mathbb{T}_{pn}], \quad (18.22d)$$

where the final equality follows since  $\partial_q x_n = \delta_{qn}$ . Bringing this result back into the full expression (18.21) leads to

$$\frac{D\mathbf{L}_m}{Dt} = \delta V \epsilon_{mnp} [\rho x_n f_p + \partial_q (x_n \mathbb{T}_{pq}) - \mathbb{T}_{pn}]. \quad (18.23)$$

### 18.3.2 Physical interpretation

To facilitate a physical interpretation of the terms appearing in equation (18.23), integrate over an arbitrary Lagrangian region (region moving with the barycentric velocity,  $\mathbf{v}$ ) so that

$$\frac{d}{dt} \int_{\mathcal{R}(\mathbf{v})} L_m = \int_{\mathcal{R}(\mathbf{v})} \epsilon_{mnp} [\rho x_n f_p + \partial_q (x_n \mathbb{T}_{pq}) - \mathbb{T}_{pn}] dV. \quad (18.24)$$

As noted earlier, the first term on the right hand side arises from torques due to body forces acting over the region

$$\int_{\mathcal{R}(\mathbf{v})} \epsilon_{mnp} (\rho x_n f_p) dV = \int_{\mathcal{R}(\mathbf{v})} (\mathbf{x} \times \mathbf{f})_m \rho dV. \quad (18.25)$$

The second term on the right hand side of equation (18.24) can be transferred into a surface integral using the divergence theorem

$$\int_{\mathcal{R}(\mathbf{v})} \epsilon_{mnp} \partial_q (x_n \mathbb{T}_{pq}) dV = \int_{\partial \mathcal{R}(\mathbf{v})} \epsilon_{mnp} x_n \mathbb{T}_{pq} \hat{n}_q dS = \int_{\partial \mathcal{R}(\mathbf{v})} (\mathbf{x} \times \boldsymbol{\tau})_m dS, \quad (18.26)$$

where  $\hat{n}_q$  is the  $q'$ th component of the normal vector on the region boundary,  $\partial\mathcal{R}(\mathbf{v})$ , and

$$\tau_p = \mathbb{T}_{pq} \hat{n}_q \quad (18.27)$$

is the  $p'$ th component to the stress vector that is normal to  $\hat{\mathbf{n}}$  (see equation (18.16)). Hence, the second term is the contribution to angular momentum evolution due to torques arising from the moment of contact forces acting on the region boundary.

### 18.3.3 Symmetry of the stress tensor

As noted at the start of this section, geophysical fluids have their angular momentum affected by torques arising from the moment of body forces acting throughout the fluid region, plus the moment of contact forces acting on the region boundary. There is a third term in equation (18.23) that does not fit into either category, and it is given by the volume integral

$$-\int_{\mathcal{R}(\mathbf{v})} \epsilon_{mnp} \mathbb{T}_{pn} dV = \int_{\mathcal{R}(\mathbf{v})} \epsilon_{mpn} \mathbb{T}_{pn} dV \equiv \int_{\mathcal{R}(\mathbf{v})} T_m^x dV, \quad (18.28)$$

where we defined

$$T_m^x = \epsilon_{mpn} \mathbb{T}_{pn}. \quad (18.29)$$

This term contributes a volume source to angular momentum and yet it is *not* associated with body forces. We might refer to it as a *torque density* (torque source per volume). As already noted, such torque sources are *not* relevant for geophysical fluids, in which case we conclude that geophysical fluids are affected only by symmetric stress tensors

$$\mathbb{T}_{mn} = \mathbb{T}_{nm} \implies \epsilon_{mnp} \mathbb{T}_{np} = 0. \quad (18.30)$$

Symmetry of the stress tensor is a central property of the stresses acting on most fluids, including geophysical fluids. We thus only consider symmetric stress tensors throughout this book.

To further support the above conclusion concerning a symmetric stress tensor, consider a particular component of the torque density, such as the vertical

$$T_3^x = \epsilon_{3pn} \mathbb{T}_{pn} = \mathbb{T}_{12} - \mathbb{T}_{21}, \quad (18.31)$$

with the corresponding torque applied to a fluid element given by

$$T_3^x \delta V = (\mathbb{T}_{12} - \mathbb{T}_{21}) \delta x \delta y \delta z. \quad (18.32)$$

What sort of angular acceleration is induced by this torque when computed relative to the fluid element center? To answer this question, assume the fluid element is moving as a rigid body so that we can compute its angular acceleration by dividing the torque by the moment of inertia for the fluid element. The moment of inertia depends on the shape of the element, which is unspecified. Even so, we can estimate the moment of inertia computed relative to a vertical axis through the center of the element

$$I_3 = \alpha [(\delta x)^2 + (\delta y)^2] \rho \delta x \delta y \delta z, \quad (18.33)$$

where  $\alpha$  is a dimensionless geometric factor. Dividing the torque (18.32) by the moment of inertia thus leads to an estimate of the angular acceleration

$$\text{angular acceleration} \approx \frac{T_3^x}{I_3} \approx \frac{\mathbb{T}_{12} - \mathbb{T}_{21}}{[(\delta x)^2 + (\delta y)^2] \rho \alpha}. \quad (18.34)$$

Now consider the continuum limit, found as  $\delta x$  and  $\delta y$  are reduced to zero. In the absence of an unspecified counteracting torque, a finite angular acceleration in the continuum limit (where  $(\delta x)^2 + (\delta y)^2 \rightarrow 0$ ) is ensured only if the stress tensor is symmetric so that the numerator vanishes.

## 18.4 Forces and torques in a static fluid

In this section we return to the study of a static fluid in a gravitational field originally considered in Section 17.3. The exact solution is known as *exact hydrostatic balance*, which distinguishes it from the approximate hydrostatic balance appropriate for moving geophysical fluids under certain scaling regimes (Section 22.2). For a static fluid, all forces and all torques sum to zero at any point. Similarly, the integrated forces and integrated torques acting on any finite fluid region also vanish. The static fluid, although trivial dynamically, offers useful practice in applying the formalism of continuum mechanics to a system where we know the answer. Furthermore, there are interesting and important applications of these ideas, such as in the building of dams and underwater structures, both of which we certainly hope will remain static!

### 18.4.1 Force balance

The force balance in an exact hydrostatic fluid was addressed in Section 17.3 where we deduced the following relation between the pressure gradient and geopotential gradient

$$\nabla p = -\rho \nabla \Phi. \quad (18.35)$$

This equality holds at every point within the fluid, and as such it is a strong form of the hydrostatic balance.<sup>2</sup> Integrating over a finite fluid region,  $\mathcal{R}$ , and using the divergence theorem for scalar fields, (2.67), renders the finite volume or weak form of hydrostatic balance

$$\int_{\mathcal{R}} \rho \nabla \Phi \, dV = - \int_{\mathcal{R}} \nabla p \, dV = - \oint_{\partial \mathcal{R}} p \hat{\mathbf{n}} \, dS. \quad (18.36)$$

Expanding the above relations for the special case of  $\Phi = g z$  leads to the differential statements

$$0 = \hat{\mathbf{x}} \cdot \nabla p = \hat{\mathbf{y}} \cdot \nabla p \quad \text{and} \quad \rho g = -\hat{\mathbf{z}} \cdot \nabla p, \quad (18.37)$$

with the first two equations implying that the exact hydrostatic pressure is only a function of  $z$ . The corresponding weak form of hydrostatic balance reads

$$g M = - \int_{\mathcal{R}} \nabla p \cdot \hat{\mathbf{z}} \, dV = - \oint_{\partial \mathcal{R}} p (\hat{\mathbf{n}} \cdot \hat{\mathbf{z}}) \, dS, \quad (18.38)$$

where  $M = \int_{\mathcal{R}} \rho \, dV$  is the mass in the fluid region, and the weak form of horizontal balances are

$$0 = \int_{\mathcal{R}} \nabla p \cdot \hat{\mathbf{x}} \, dV = \oint_{\partial \mathcal{R}} p (\hat{\mathbf{n}} \cdot \hat{\mathbf{x}}) \, dS \quad (18.39a)$$

$$0 = \int_{\mathcal{R}} \nabla p \cdot \hat{\mathbf{y}} \, dV = \oint_{\partial \mathcal{R}} p (\hat{\mathbf{n}} \cdot \hat{\mathbf{y}}) \, dS. \quad (18.39b)$$

We emphasize that these finite volume balances hold for any arbitrarily shaped fluid region.

---

<sup>2</sup>Recall the discussion of weak and strong formulation in Section 12.1. In brief, the weak formulation provides integral relations whereas the strong formulation provides differential relations.

### 18.4.2 Pressure force balance for a homogeneous fluid

To further our understanding of the pressure force balances in a static fluid, consider a constant density static ocean sitting under a massless atmosphere, in which case the hydrostatic pressure is

$$p = -\rho g z, \quad (18.40)$$

where  $z < 0$  for the ocean. Now examine the pressure forces acting on the three sides of the triangle in Figure 18.5. This geometry is simple enough to explicitly compute the pressure forces, thus confirming the general properties in equations (18.38), (18.39a), and (18.39b).

The outward normal vectors along the three triangle faces are given by

$$\hat{\mathbf{n}}_A = +\hat{\mathbf{y}} \quad \text{and} \quad \hat{\mathbf{n}}_B = -\hat{\mathbf{z}} \quad \text{and} \quad \hat{\mathbf{n}}_C = \hat{\mathbf{z}} \cos \varphi - \hat{\mathbf{y}} \sin \varphi, \quad (18.41)$$

where

$$\tan \varphi = \frac{z_2 - z_1}{y_2 - y_1} = \frac{\Delta z}{\Delta y} \quad (18.42)$$

is the slope of the hypotenuse relative to the horizontal. The integrated pressure force along the vertical face is thus given by

$$\mathbf{F}_A^{\text{press}} = - \int p \hat{\mathbf{n}}_A dS = \hat{\mathbf{y}} \Delta x \int_{z_1}^{z_2} \rho g z dz = \hat{\mathbf{y}} (\rho g / 2) (z_2 + z_1) \Delta z \Delta x, \quad (18.43)$$

where  $\Delta x$  is the thickness of the triangle in the  $\hat{\mathbf{x}}$  direction into the page. Note that  $\mathbf{F}_A^{\text{press}}$  points in the  $-\hat{\mathbf{y}}$  direction since  $z_2 + z_1 < 0$ . Likewise, the integrated pressure force along the horizontal face is given by

$$\mathbf{F}_B^{\text{press}} = - \int p \hat{\mathbf{n}}_B dS = -\hat{\mathbf{z}} \Delta x \int_{y_1}^{y_2} \rho g z_1 dy = -\hat{\mathbf{z}} \rho g z_1 \Delta y \Delta x, \quad (18.44)$$

which points upward since  $z_1 < 0$ .

The integrated pressure force along the sloped hypotenuse face,  $C$ , requires a bit of trigonometry. For this purpose we make use of the formalism from Section 14.4.3, in which the vertical position along the hypotenuse is written

$$z = \eta(y) = z_2 - (y_2 - y) \tan \varphi, \quad (18.45)$$

so that the horizontal projection of the surface area is given by equation (19.4)

$$dS = |\nabla(z - \eta)| dx dy = \frac{dx dy}{|\cos \varphi|}. \quad (18.46)$$

Hence, the integrated pressure force on the hypotenuse is given by

$$\mathbf{F}_C^{\text{press}} = - \int p \hat{\mathbf{n}}_C dS \quad (18.47a)$$

$$= \frac{\hat{\mathbf{n}}_C}{\cos \varphi} \Delta x \int_{y_1}^{y_2} \rho g \eta(y) dy \quad (18.47b)$$

$$= (\hat{\mathbf{z}} - \hat{\mathbf{y}} \tan \varphi) \rho g \Delta x [z_2 \Delta y - y_2 \Delta z - (1/2)(y_1 + y_2) \Delta y \tan \varphi] \quad (18.47c)$$

$$= (\hat{\mathbf{z}} - \hat{\mathbf{y}} \tan \varphi) \rho g \Delta x [z_2 \Delta y - y_2 \Delta z + (y_1 + y_2) \Delta z / 2] \quad (18.47d)$$

$$= (\hat{\mathbf{z}} - \hat{\mathbf{y}} \tan \varphi) \rho g \Delta x \Delta y (z_1 + z_2) / 2. \quad (18.47e)$$

Bringing these results together renders the net pressure forces in the two directions

$$\hat{y} \cdot (\mathbf{F}_A^{\text{press}} + \mathbf{F}_B^{\text{press}} + \mathbf{F}_C^{\text{press}}) = (\rho g \Delta x / 2) [(z_1 + z_2) \Delta z - \tan \varphi (z_1 + z_2) \Delta y] = 0 \quad (18.48\text{a})$$

$$\hat{z} \cdot (\mathbf{F}_A^{\text{press}} + \mathbf{F}_B^{\text{press}} + \mathbf{F}_C^{\text{press}}) = \rho g \Delta x \Delta y \Delta z / 2 = M g, \quad (18.48\text{b})$$

where the mass of the triangle is given by

$$M = \rho \Delta x \Delta y \Delta z / 2. \quad (18.49)$$

We thus see that the area integrated horizontal pressure forces vanish, whereas the area integrated vertical pressure force balances the weight of the fluid. Again, these results are expected given the general expressions (18.38), (18.39a), and (18.39b) of force balance. Even so, being able to explicitly compute the pressure forces acting around a region, and to confirm the general force balances, is a useful means to become familiar with hydrostatic pressure.

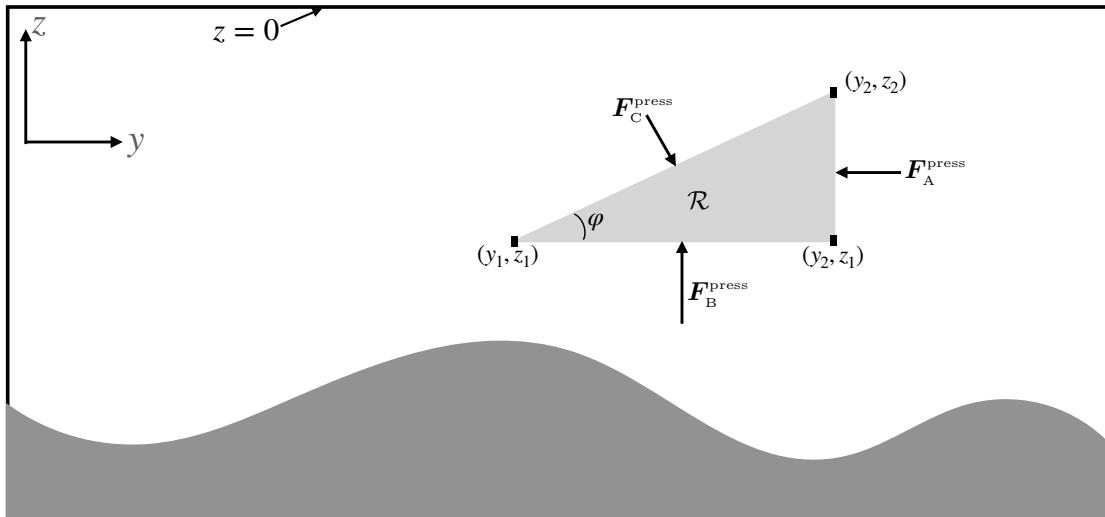


FIGURE 18.5: A right triangle region of fluid in a static ocean where  $z < 0$ . The positions for the three corners are shown as  $(y_1, z_1)$ ,  $(y_2, z_1)$ , and  $(y_2, z_2)$ , along with the pressure forces acting on the three sides. In exact hydrostatic balance, the area integrated pressure force acting over the triangle boundary vanishes,  $-\oint_{\partial\mathcal{R}} p \hat{n} d\mathcal{S} = 0$ . If the density of the fluid is assumed constant, then we can analytically compute the force balance as detailed in Section 18.4.2.

### 18.4.3 Torque balance

Torques arise in the presence of force *couplets*, which in turn lead to time changes in the angular momentum. In our discussion of the stress tensor in Section 18.3, we saw that a symmetric stress tensor removes volume sources of torque; i.e., there are no internal sourced force couplets. So the only means to impart a nonzero torque is for force couplets to arise from body forces (forces originating outside of the fluid region) and from contact forces that act between fluid elements within the region. The aim of this section is to show that for a static fluid with a static angular momentum, then the net torque vanishes both at a point and on an arbitrary fluid region.

*Strong form: zero torques acting on a fluid element*

The torque is the moment of a force computed about a chosen origin. For a static geophysical fluid, the torque acting on a fluid element is given by the moment of the pressure force plus the

moment of the effective gravity force (central gravity plus planetary centrifugal)

$$\mathbf{x} \times \mathbf{f} \rho \delta V = \mathbf{x} \times (-\rho^{-1} \nabla p - \nabla \Phi) \rho \delta V. \quad (18.50)$$

As seen in Section 18.4.1, the pressure and effective gravitational forces exactly balance at each point with a static fluid so that  $\nabla p = -\rho \nabla \Phi$ . Hence, there can be no torques at each point since there are no net forces at each point.

*Weak form: zero torques acting on a finite fluid region*

To show that the torque vanishes for a finite fluid region, we can merely integrate the fluid element result (18.50) over the finite region. Since the integral of zero is still zero, there are no torques on the region. An alternative approach makes use of the weak formulation by following the discussion in Section 18.3.2. In this approach, we start by writing the time change in angular momentum acting on a static fluid region

$$\frac{d}{dt} \int_{\mathcal{R}} \mathbf{L} = \int_{\mathcal{R}} [\mathbf{x} \times (-\rho \nabla \Phi)] dV + \oint_{\partial \mathcal{R}} [\mathbf{x} \times (-\hat{\mathbf{n}} p)] dS. \quad (18.51)$$

Note that although the discussion in Section 18.3.2 focused on a Lagrangian region,  $\mathcal{R}(\mathbf{v})$ , there is no distinction here between Lagrangian and Eulerian since the fluid is static.

The pressure contribution in equation (18.51) is written in its contact force form, which is appropriate for a weak formulation. However, to compare its contribution to the torque with that from effective gravity requires us to convert the area integral to a volume integral. For that purpose we use Cartesian tensor notation and expose full details for clarity

$$\oint_{\partial \mathcal{R}} (\hat{\mathbf{n}} \times \mathbf{x})_a p dS = \epsilon_{abc} \oint_{\partial \mathcal{R}} \hat{n}_b x_c p dS \quad \text{permutation symbol (Section 1.4.1)} \quad (18.52a)$$

$$= \epsilon_{abc} \int_{\mathcal{R}} \partial_b (x_c p) dV \quad \text{divergence theorem} \quad (18.52b)$$

$$= \epsilon_{abc} \int_{\mathcal{R}} (\delta_{bc} p + x_c \partial_b p) dV \quad \text{product rule} \quad (18.52c)$$

$$= \epsilon_{abc} \int_{\mathcal{R}} x_c \partial_b p dV \quad \epsilon_{abc} \delta_{bc} = 0 \quad (18.52d)$$

$$= -\epsilon_{acb} \int_{\mathcal{R}} x_c \partial_b p dV \quad \epsilon_{abc} = -\epsilon_{acb} \quad (18.52e)$$

$$= - \int_{\mathcal{R}} (\mathbf{x} \times \nabla p)_a dV \quad \text{vector cross product notation.} \quad (18.52f)$$

This result then brings the angular momentum equation (18.51) to the form

$$\frac{d}{dt} \int_{\mathcal{R}} \mathbf{L} = \int_{\mathcal{R}} [\mathbf{x} \times (-\rho \nabla \Phi - \nabla p)] dV. \quad (18.53)$$

At this point we can invoke the strong form force balance in equation (18.35), thus revealing that the integrand on the right hand side vanishes at each point in the fluid. However, this approach is no different than starting from the strong formulation of the torques in equation (18.50) and integrating over a finite region. An alternative approach, remaining fully within the weak formulation, states that if the region's angular momentum remains constant, then that defines a region experiencing zero net torque. This approach is the same as taken for the force balance, whereby we say that a fluid region experiencing no acceleration is one that has zero net

forces acting on it. Hence, for a region with constant angular momentum we are led to the finite volume (weak form) torque balance

$$\int_{\mathcal{R}} [\mathbf{x} \times (\rho \nabla \Phi + \nabla p)] dV = 0 \implies \int_{\mathcal{R}} \mathbf{x} \times \rho \nabla \Phi dV = - \int_{\partial \mathcal{R}} \mathbf{x} \times \hat{\mathbf{n}} p dS, \quad (18.54)$$

with this balance the direct analog for torques of the weak form of the force balances given by equations (18.38), (18.39a), and (18.39b).

## 18.5 Flux-form Eulerian momentum equation

We often find it useful to consider Cauchy's form of the momentum equation (18.20) in its flux-form Eulerian expression. Making use of Cartesian tensors, we expand the material time derivative acting on the velocity and introduce the mass conservation equation (14.6) so that

$$\rho \frac{D\mathbf{v}}{Dt} = \rho [\partial_t \mathbf{v} + (\mathbf{v} \cdot \nabla) \mathbf{v}] \quad (18.55a)$$

$$= \rho [\partial_t \mathbf{v} + (\mathbf{v} \cdot \nabla) \mathbf{v}] + \mathbf{v} (\partial_t \rho + \nabla \cdot (\rho \mathbf{v})) \quad (18.55b)$$

$$= \partial_t (\rho \mathbf{v}) + \nabla \cdot [\rho \mathbf{v} \otimes \mathbf{v}], \quad (18.55c)$$

where  $\mathbf{v} \otimes \mathbf{v}$  is the outer product of the velocity vector and it has Cartesian tensor components written as

$$(\mathbf{v} \otimes \mathbf{v})_{mn} = v_m v_n. \quad (18.56)$$

Consequently, the momentum equation (18.20) takes on the flux-form Eulerian expression

$$\partial_t (\rho \mathbf{v}) + \nabla \cdot [\rho \mathbf{v} \otimes \mathbf{v}] = \rho \mathbf{f} + \nabla \cdot \mathbb{T}. \quad (18.57)$$

Alternatively, we can move the advection of momentum term onto the right hand side so that

$$\partial_t (\rho \mathbf{v}) = \rho \mathbf{f} + \nabla \cdot [\mathbb{T} - \rho \mathbf{v} \otimes \mathbf{v}], \quad (18.58)$$

which takes on the component form

$$\partial_t (\rho v_m) = \rho f_m + \partial_n [\mathbb{T}_{mn} - \rho v_m v_n]. \quad (18.59)$$

In this form we see that momentum advection can be interpreted as a stress that modifies the linear momentum per volume at a point in space. We refer to the stress,

$$\mathbb{T}_{mn}^{\text{kinetic}} = -\rho (\mathbf{v} \otimes \mathbf{v})_{mn} = -\rho v_m v_n, \quad (18.60)$$

as the *mechanical stress* or *kinetic stress*, which arises from the mechanical interactions between moving fluid elements. The turbulent contribution to the mechanical stress is known as the *Reynolds stress*.

For a rotating fluid in a gravity field we set the body force to

$$\rho \mathbf{f} = -2 \rho \boldsymbol{\Omega} \times \mathbf{v} - \rho \nabla \Phi, \quad (18.61)$$

and the divergence of the stress tensor is

$$\nabla \cdot \mathbb{T} = -\nabla p + \rho \mathbf{F}, \quad (18.62)$$

with  $\mathbf{F}$  the frictional acceleration (see Section 18.7). In this case, Cauchy's equation (18.57) takes on the form

$$\frac{\partial(\rho \mathbf{v})}{\partial t} + \nabla \cdot (\rho \mathbf{v} \otimes \mathbf{v}) + 2\rho \boldsymbol{\Omega} \times \mathbf{v} = -\nabla p - \rho \nabla \Phi + \rho \mathbf{F}. \quad (18.63)$$

## 18.6 Linear momentum for arbitrary regions

Consider the budget of linear momentum for an arbitrary region,  $\mathcal{R}$ , moving in an arbitrary manner within the fluid. For this purpose we make use of the Leibniz-Reynolds Transport Theorem (15.34)

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \varphi dV \right] = \int_{\mathcal{R}} \frac{\partial \varphi}{\partial t} dV + \oint_{\partial \mathcal{R}} \varphi \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} dS, \quad (18.64)$$

where  $\mathbf{v}^{(b)}$  is the velocity of the region boundary,  $\partial \mathcal{R}$ , with  $\hat{\mathbf{n}}$  the outward normal along the boundary. Applying this result to a component of the linear momentum per volume,  $\varphi = \rho v_m$ , and making use of the flux-form Eulerian momentum equation (18.59) leads to

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho v_m dV \right] = \int_{\mathcal{R}} \partial_t(\rho v_m) dV + \oint_{\partial \mathcal{R}} (\rho v_m) \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} dS \quad (18.65a)$$

$$= \int_{\mathcal{R}} [\rho f_m + \partial_n(\mathbb{T}_{mn} - \rho v_m v_n)] dV + \oint_{\partial \mathcal{R}} (\rho v_m) \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} dS \quad (18.65b)$$

$$= \int_{\mathcal{R}} \rho f_m dV + \oint_{\partial \mathcal{R}} (\mathbb{T}_{mn} - \rho v_m v_n) \hat{\mathbf{n}}_n dS + \oint_{\partial \mathcal{R}} (\rho v_m) \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} dS \quad (18.65c)$$

$$= \int_{\mathcal{R}} \rho f_m dV + \oint_{\partial \mathcal{R}} [\mathbb{T}_{mn} + \rho v_m (v_n^{(b)} - v_n)] \hat{\mathbf{n}}_n dS. \quad (18.65d)$$

We can write this relation in the more elegant geometric form as

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho \mathbf{v} dV \right] = \int_{\mathcal{R}} \rho \mathbf{f} dV + \oint_{\partial \mathcal{R}} [\mathbb{T} + \rho \mathbf{v} \otimes (\mathbf{v}^{(b)} - \mathbf{v})] \cdot \hat{\mathbf{n}} dS. \quad (18.66)$$

As a relation between geometric objects (vectors and tensors), the momentum budget (18.66) is independent of coordinate representation. We conclude that the evolution of linear momentum over an arbitrary region is affected by the volume integrated body force acting over the region, plus the impacts from stresses acting on the region boundary. Notably, the stresses have a contribution from the advection of linear momentum across the region boundary, with advection computed relative to motion of the boundary. In Section 18.9 we specialize the budget (18.66) to an infinitesimally thin interface. That analysis is then used to develop stress conditions for a surface within a single fluid media, and the stress condition at the boundary between two fluids.

We refer to a *Lagrangian region* as one that moves with the barycentric velocity so that  $\mathbf{v}^{(b)} = \mathbf{v}$ , in which case the mechanical stress is eliminated from the finite volume momentum budget (18.66). In fact, to eliminate the mechanical stress only requires the normal components of the boundary velocity to equal that of a fluid element,  $(\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = 0$ . In either case we distinguish a Lagrangian region by writing  $\mathcal{R}(\mathbf{v})$  to emphasize that the region moves with the barycentric fluid velocity,  $\mathbf{v}$ . For this case the linear momentum is only affected by body forces as well as stresses contained in the stress tensor

$$(\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = 0 \implies \frac{d}{dt} \left[ \int_{\mathcal{R}(\mathbf{v})} \rho \mathbf{v} dV \right] = \int_{\mathcal{R}(\mathbf{v})} \rho \mathbf{f} dV + \oint_{\partial \mathcal{R}(\mathbf{v})} \mathbb{T} \cdot \hat{\mathbf{n}} dS. \quad (18.67)$$

This relation is Reynold's transport theorem (Section 15.3.6) as applied to linear momentum.

## 18.7 Constitutive relation between stress and rate of strain

Thus far we have offered a rather general treatment of stress, developing its properties according to the conservation of linear momentum and angular momentum. We now develop *constitutive relations*, which relate stress to properties of the fluid as well as properties of the fluid flow.

### 18.7.1 Thermodynamic pressure and mechanical pressure

Consider a fluid in which the stress on an area element is always normal to the area element and is independent of the orientation. This fluid is in hydrostatic balance and the corresponding stress tensor and stress vector are written

$$\mathbb{T}_{mn} = -p \delta_{mn} \iff \mathbb{T} \cdot \hat{\mathbf{n}} = -p \hat{\mathbf{n}}, \quad (18.68)$$

where  $p$  is the hydrostatic pressure field. Since the pressure introduced here arises from purely mechanical considerations, we refer to it as the *mechanical pressure*. For a compressible fluid at rest, we can identify the mechanical pressure with the *thermodynamic pressure* encountered in our study of equilibrium thermodynamics (Chapter 20). Furthermore, if we assume that local thermodynamic equilibrium is maintained for fluid elements within a moving fluid, then we are motivated to continue making this identification between mechanical pressure and thermodynamical pressure (see Section 4.5 of [Kundu et al. \(2016\)](#) or Section 1.10 of [Salmon \(1998\)](#)). However, we note that there is no fully deductive theory supporting this equality of pressures. The reader in search of a deductive theory likely will need to penetrate nonequilibrium statistical mechanics, which is outside our scope.

When the fluid flow is non-divergent (Chapter 16), we lose the equality between mechanical pressure and thermodynamical pressure, even when the fluid is at rest. The reason is that a non-divergent fluid flow is unable to do pressure work on a fluid element since the flow cannot change the fluid element's volume. Hence, for non-divergent flow there is no connection between pressure and changes to internal energy as per the first law of thermodynamics (Section 20.2). A non-divergent flow only has access to the mechanical pressure as revealed through the measurement of stresses. Furthermore, the mechanical pressure instantaneously conforms to the needs of non-divergence throughout the fluid (see Section 23.3 and Section 33.4). Correspondingly, energetic consistency requires us to make use of the geopotential in the equation of state for *in situ* density in an oceanic Boussinesq fluid (in which the velocity is non-divergent), rather than the thermodynamic pressure. We explore this point in Section 23.7.

### 18.7.2 Couette flow and the viscous tensor

*Couette flow* arises when fluid is placed between two long and straight concentric cylinders that can rotate. Relative motion between the two cylinders leads to fluid motion. For example, if the inner surface rotates, then fluid next to the cylinder wall will move with the cylinder. Any normal stresses on the fluid imparted by the cylinders are directed toward the cylinder axis and so cannot render any tangential motion. This elegant experiment proves that fluid motion can be induced by purely tangential stresses. Furthermore, the tangential stress imparted by the inner cylinder transfers through the fluid to the outer cylinder. Indeed, if the inner cylinder rotates at a constant rate, then eventually the whole fluid-cylinder system rotates as a solid body. Couette flow thus exhibits how real fluids can support tangential stresses in response to tangential strains, thus providing a clear distinction from a perfect fluid where only normal stresses (i.e., pressure) are supported.

As evidenced by the Couette flow, a moving fluid has a more complex stress relation than a static fluid. In particular, the presence of tangential stresses in the fluid provides evidence for an additional piece to the stress tensor that we write as

$$\mathbb{T}_{mn} = -p \delta_{mn} + \tau_{mn} \iff \mathbb{T} = -p \mathbb{I} + \tau. \quad (18.69)$$

The pressure term remains isotropic as for a fluid at rest, thus imparting normal stresses. The additional tensor,  $\tau$ , is referred to as the *friction tensor* or *viscous tensor*. The viscous tensor captures the irreversible exchanges of momentum between moving (relative to one another) fluid elements, such as in Couette flow, with the irreversible momentum exchange supported by fluid viscosity. Viscosity is assumed to be identically zero in a perfect fluid, so that a perfect fluid can only support normal stresses from pressure even when the perfect fluid has relative motion.

As noted above, we assume the viscous tensor vanishes when there is zero relative motion within the fluid.<sup>3</sup> The physical idea is that fluid strains are needed to generate friction between fluid elements to support the transfer of momentum through the presence of viscosity. The determination of frictional stresses from kinematic properties (such as strain) requires a constitutive relation. The constitutive relation commonly used for geophysical fluids follows that for a *Newtonian fluid*, which is a particular type of *Stokesian fluid* whose frictional stresses are assumed to be linearly proportional to the rate of strain.

The diagonal stresses,  $\mathbb{T}_{11}$ ,  $\mathbb{T}_{22}$ , and  $\mathbb{T}_{33}$ , are known as the *direct stresses* or *normal stresses*, whereas the off-diagonal stresses are *shear stresses*. The sum of the direct stresses forms the trace of the stress tensor and is given by

$$\mathbb{T}_{qq} = \mathbb{T}_{11} + \mathbb{T}_{22} + \mathbb{T}_{33} = -3p + \tau_{qq}. \quad (18.70)$$

If  $\tau_{qq} = 0$  then it is known as the *deviatoric friction tensor*. As argued in Section 18.7.6, a deviatoric friction tensor is consistent with the assumption of equal mechanical and thermodynamical pressures.

### 18.7.3 d'Alembert's theorem for perfect fluids

Consider a finite impermeable solid body placed in a steady fluid flow, with the flow assumed to be uniform upstream and downstream. A particular realization is an arbitrarily long pipe flow with a solid object in the middle of the pipe. *d'Alembert's theorem* says that the force exerted by a perfect fluid on the solid body has no component along the direction of the pipe's central axis. A proof of this theorem, as provided in Section 13 of [Meyer \(1971\)](#), makes use of basic insights into momentum balances. Remarkably, d'Alembert's theorem suggests a behavior that is contrary to common experience, whereby an object placed in a real fluid flow experiences a net force in the direction of the flow, so that there is a transfer of momentum between the fluid and the solid body. Consequently, d'Alembert's theorem became known as *d'Alembert's paradox*, thus motivating research during the 19th and early 20th centuries to understand stresses acting between a fluid and solid. It further put into question the ability to approximate a fluid with arbitrarily small, but nonzero, viscosity with a perfect fluid where the viscosity identically vanishes. Namely, a real fluid supports tangential stresses, through the action of viscosity, in addition to normal (pressure) stresses. It is the tangential stresses, no matter how small in magnitude but nonzero, that lead to a net force on the solid body.

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<sup>3</sup>This assumption follows those for a Stokes fluid as discussed in Section 5.21 of [Aris \(1962\)](#).

### 18.7.4 Guidance from Galilean invariance

Consider a fluid in uniform motion in free space. Boosting the reference frame allows us to move to a reference frame where the fluid is static. Through Galilean invariance (Section 12.6) we expect the dynamics to remain unchanged. Since we assume friction vanishes when the fluid is static (as per a Stokesian fluid), Galilean invariance implies that the frictional stresses vanish when the fluid undergoes uniform motion in any direction.

Uniform motion of fluid elements is reflected in zero velocity gradients, which offers a key insight into how friction depends on strains. Namely, these considerations suggest that the friction tensor is a function of gradients in the velocity field,  $\partial_m v_n$ . Furthermore, as the stress tensor must be symmetric (Section 18.3), the simplest expression for the friction tensor is one that is linearly proportional to the rate of strain tensor introduced in Section 13.3.5. Fluids that satisfy this linear stress-rate of strain constitutive relation are known as *Newtonian fluids*. Furthermore, this constitutive relation takes the same mathematical form as *Hooke's Law* used in the study of elastic materials.

### 18.7.5 A comment on Rayleigh drag

Rayleigh drag is a particular form of friction that makes use of the acceleration

$$\mathbf{F}_{\text{Rayleigh}} = -\gamma \mathbf{v}, \quad (18.71)$$

where  $\gamma > 0$  is an inverse time scale. Rayleigh drag does *not* satisfy the Galilean principle since it decelerates all flows, even uniformly moving flows, towards rest where rest is defined by the laboratory frame. Furthermore, Rayleigh drag is not equal to the divergence of a frictional stress tensor, and so it does not arise from a contact stress. Even so, it has found some use for rudimentary purposes, particularly when aiming to derive analytic expressions for how friction acts on flows in a bulk sense. We provide one example in our discussion of Ekman dynamics in Section 27.2.3.

### 18.7.6 Constitutive relation for Newtonian fluids

There are many details involved with deriving the Newtonian fluid constitutive relation, with discussions provided in Chapter 5 of [Aris \(1962\)](#), Section 3.1 of [Segel \(1987\)](#), and Section 4.5 of [Kundu et al. \(2016\)](#) for general fluids, and Chapter 17 and 18 of [Griffies \(2004\)](#) for stratified fluids with particular focus on the ocean. We here offer a taste of these considerations by starting with the constitutive relation

$$\tau_{mn} = \rho (2\nu \mathbb{S}_{mn} + \lambda \nabla \cdot \mathbf{v} \delta_{mn}), \quad (18.72)$$

with  $\mathbb{S}_{mn}$  the components to the rate of strain tensor introduced in Section 13.3.7 and whose trace equals to the velocity divergence

$$\mathbb{S}_{qq} = \nabla \cdot \mathbf{v}. \quad (18.73)$$

The first contribution to the frictional stress (18.72) includes the strain tensor multiplied by the *first kinematic viscosity*,  $\nu > 0$  (dimensions of squared length per time). The second contribution arises just from flow divergence as scaled by a *second kinematic viscosity*,  $\lambda$ . The sum

$$\nu_{\text{bulk}} = \rho (\lambda + 2\nu/3) \quad (18.74)$$

is known as the *bulk viscosity*, which, as discussed in the following, will be set to zero. Finally, one sometimes finds it more convenient to work with the *dynamic viscosity*

$$\mu_{\text{vsc}} = \rho \nu. \quad (18.75)$$

Note that we set  $\rho$  to the constant Boussinesq reference density,  $\rho_0$  (Chapter 23), when working with a Boussinesq fluid.

### *Deviatoric friction tensor*

As noted in Section 18.7.1, the pressure appearing in the stress tensor is a mechanical pressure that equals to minus one-third the trace of the stress tensor when the fluid is at rest

$$\mathbb{T}_{qq}^{\text{static}} = -3 p. \quad (18.76)$$

We assume that the friction stress tensor does *not* alter this trace, so that the friction tensor has zero trace and is known as a *deviatoric friction tensor*<sup>4</sup>

$$\tau_{qq} = 0 = 3 \nu_{\text{bulk}} \nabla \cdot \mathbf{v} \implies \lambda = -2 \nu / 3, \quad (18.77)$$

so that the total stress tensor is given by

$$\mathbb{T}_{mn} = -\delta_{mn} p + 2 \mu_{\text{vsc}} \mathbb{S}_{mn}^{\text{dev}} \quad \text{with} \quad \mathbb{S}_{mn}^{\text{dev}} = \mathbb{S}_{mn} - \delta_{mn} \mathbb{S}_{qq} / 3, \quad (18.78)$$

where  $\mathbb{S}^{\text{dev}}$  is the *deviatoric rate of strain tensor*. We next offer arguments for why the friction tensor used for geophysical flows should have zero trace.

### *Equality of the mechanical and thermodynamic pressures*

The frictional stress tensor (18.72) is not the precise form typically used in geophysical fluid modeling. Instead, the velocity divergence term is generally dropped even for compressible flows, and the viscosity is anisotropic and more generally takes the form of a fourth order tensor (see Chapter 17 and 18 of [Griffies \(2004\)](#) for the ocean). Furthermore, what is generally respected in most geophysical applications is the deviatoric nature of the friction tensor. That property is maintained since it is consistent with our assumption in Section 18.7.1 that the mechanical pressure equals to the thermodynamic pressure.

To see this equality between the pressures, introduce the mechanical pressure,  $p^{\text{mech}}$ , according to the trace of the stress tensor

$$\mathbb{T}_{qq} = -3 p^{\text{mech}}. \quad (18.79)$$

That is, mechanical pressure is minus one-third the trace of the stress tensor whether the fluid is at rest or in motion. We can, in principle, measure this pressure by measuring the stresses. If we now return to the general form of the stress tensor

$$\mathbb{T}_{mn} = -\delta_{mn} p + \rho (\lambda \nabla \cdot \mathbf{v} \delta_{mn} + 2 \nu \mathbb{S}_{mn}), \quad (18.80)$$

with  $p$  here given by the thermodynamic pressure, then the trace is

$$\mathbb{T}_{qq} = -3 p + \rho (3 \lambda + 2 \nu) \nabla \cdot \mathbf{v}. \quad (18.81)$$

---

<sup>4</sup>A second order tensor in 3-dimensions,  $\mathbb{D}$ , has a *deviator* with components given by  $\mathbb{D}_{mn}^{\text{dev}} = \mathbb{D}_{mn} - (1/3) \delta_{mn} \mathbb{D}_{qq}$ . By construction, the trace of the deviator vanishes:  $\mathbb{D}_{qq}^{\text{dev}} = 0$ .

Setting the two traces (18.79) and (18.81) equal then leads to

$$p - p^{\text{mech}} = \nu_{\text{bulk}} \nabla \cdot \mathbf{v}. \quad (18.82)$$

In principle, one can measure the difference in pressures, but in practice this measurement is rather difficult. Stokes assumed  $p - p^{\text{mech}} = 0$  by taking a zero bulk viscosity, and he used arguments from kinetic theory of gases to support that choice. This choice is generally taken for geophysical fluid applications, largely based on the assumption of local thermodynamic equilibrium mentioned in Section 18.7.1.

Local thermodynamical equilibrium is not a good assumption in supersonic flows, in which case  $p - p^{\text{mech}} \neq 0$  and the bulk viscosity is nonzero. Correspondingly, the divergence term and the second kinematic viscosity,  $\lambda \neq -2\nu/3$ , are important. Additionally, the second viscosity is important when concerned with the damping of acoustic waves. Neither topics are considered in this book so that we have no further concern for the second viscosity.

#### *Frictional force per volume*

The viscous force per volume is given by the divergence of the frictional stress tensor

$$\rho F_n = \partial_m \tau_{mn} = 2 \partial_m (\mu_{\text{vsc}} \mathbb{S}_{mn}^{\text{dev}}). \quad (18.83)$$

For a Boussinesq fluid this friction simplifies to

$$\rho_0 F_n = 2 \rho_0 \partial_m (\nu \mathbb{S}_{mn}), \quad (18.84)$$

where we set the dynamic viscosity to  $\mu_{\text{vsc}} = \rho_0 \nu$ , with  $\rho_0$  the constant Boussinesq reference density. Finally, for the case of a constant kinematic viscosity, such as for molecular viscous effects, we have the Boussinesq result reducing to the Laplacian form

$$\mathbf{F} = \nu \nabla^2 \mathbf{v}. \quad (18.85)$$

This form is commonly used in scale analysis, such as when determining the Reynolds number in Section 18.8.

### 18.7.7 Navier-Stokes and Euler equations

The *Navier-Stokes* equation is a special form of the momentum equation found by assuming a Newtonian fluid constitutive relation. In this case the Navier-Stokes momentum equation (17.16), in the presence of rotation and gravity, takes on the form

$$\rho \frac{D\mathbf{v}}{Dt} + 2\rho \boldsymbol{\Omega} \times \mathbf{v} = -\rho \nabla \Phi - \nabla p + \nabla \cdot (2\mu_{\text{vsc}} \mathbb{S}^{\text{dev}}), \quad (18.86)$$

where we set the friction tensor equal to  $\tau = 2\mu_{\text{vsc}} \mathbb{S}^{\text{dev}}$ . Quite often when examining the mathematical properties of the Navier-Stokes equation, one assumes the flow to be non-divergent, in which case  $\mathbb{S}^{\text{dev}} = \mathbb{S}$  since  $\mathbb{S}_{qq} = \nabla \cdot \mathbf{v} = 0$ . A further simplification occurs by assuming a constant density,  $\rho$ , and constant kinematic viscosity,  $\nu$ , in which case the friction tensor reduces to the Laplacian form 18.85 so that the Navier-Stokes equation becomes

$$\frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla \Phi - \rho^{-1} \nabla p + \nu \nabla^2 \mathbf{v}. \quad (18.87)$$

This form, or even simpler when ignoring rotation and gravity, is commonly studied by mathematicians concerned with existence and uniqueness properties of fluid flow solutions (e.g., see [Doering and Gibbon \(2004\)](#)). When assuming the fluid to be perfect, so that there are no viscous forces, the momentum equation is referred to as the *Euler equation*<sup>5</sup>

$$\frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla\Phi - \rho^{-1}\nabla p. \quad (18.88)$$

It is tempting to consider the Euler equations to be a continuous limit of the Navier-Stokes equation as the viscosity goes to zero. However, there is a key distinction between the two equations. Namely, the Navier-Stokes equations admit solutions that display statistically equilibrated turbulent motions, whereby energy cascades to the small scales through vortex stretching in three dimensional flows. This energy is ultimately dissipated by viscosity at the small spatial scales, and this mechanism holds no matter how small the viscosity, so long as it is nonzero. In contrast, for the Euler equations, with identically zero viscosity, energy cannot be dissipated at the small scales so that an equilibrium turbulent flow is not available.

Another fundamental distinction between the Euler equation and Navier-Stokes equation concerns the boundary conditions. For the Navier-Stokes equations, the presence of a second order operator (the Laplacian), weighted by the viscosity, signals a very distinct behavior of the flow next to boundaries. The Euler equation can only maintain a no-normal flow condition at a boundary, with the kinematics detailed in Section 14.4. The viscous fluid described by the Navier-Stokes equation must satisfy an additional boundary condition. Evidence based on research in the 19th and 20th centuries suggests that that fluids, such as air and water, adhere to solid boundaries and thus satisfy the *no-slip* boundary condition. This boundary condition has basic implications for how stress acts between fluids and solids. We have more to say concerning this boundary condition in Section 18.9.<sup>6</sup>

### 18.7.8 Laplacian friction in terms of vorticity and divergence

The Laplacian friction operator with a constant viscosity is afforded the following decomposition

$$\nu^{-1} F_n = \partial_m (\partial_m v_n) \quad (18.89a)$$

$$= \partial_m (\partial_m v_n - \partial_n v_m + \partial_n v_m) \quad (18.89b)$$

$$= \partial_m (\partial_m v_n - \partial_n v_m) + \partial_n (\partial_m v_m) \quad (18.89c)$$

$$= -2 \partial_m \mathbb{A}_{mn} + \partial_n \nabla \cdot \mathbf{v} \quad (18.89d)$$

$$= \epsilon_{nmp} \partial_m \omega_p + \partial_n \nabla \cdot \mathbf{v} \quad (18.89e)$$

$$= (\nabla \times \boldsymbol{\omega})_n + \partial_n \nabla \cdot \mathbf{v}. \quad (18.89f)$$

In the fourth equality we introduced the rotation tensor (13.42)

$$\mathbb{A}_{mn} = (1/2) (\partial_n v_m - \partial_m v_n), \quad (18.90)$$

which is related to the vorticity,  $\boldsymbol{\omega} = \nabla \times \mathbf{v}$ , via equation (13.44)

$$\mathbb{A}_{mn} = -\epsilon_{mnp} \omega_p / 2. \quad (18.91)$$

---

<sup>5</sup>Note that some authors refer to the Euler equations only in the case of a perfect fluid that has no body force, so that both rotation and gravitation vanish.

<sup>6</sup>See also the comments and footnote on page 86 of [Seigel \(1987\)](#) as well as pages 83-84 of [Meyer \(1971\)](#).

These manipulations have served to decompose the Laplacian viscous acceleration, with a constant viscosity, into the two terms

$$\mathbf{F} = \nu [\nabla \times \boldsymbol{\omega} + \nabla(\nabla \cdot \mathbf{v})]. \quad (18.92)$$

The Laplacian friction acceleration is thus due to the curl of the vorticity plus gradients in the velocity divergence. Many geophysical flows are dominated by vorticity since the divergence is quite small. Indeed, the Boussinesq fluids discussed in Chapter 23 have  $\nabla \cdot \mathbf{v} = 0$ , in which case frictional acceleration arises only when the vorticity has a nonzero curl. Correspondingly, irrotational flows (where  $\boldsymbol{\omega} = 0$ ) that are also non-divergent have zero Laplacian frictional acceleration.

### 18.7.9 Frictional stresses in a sheared flow

As a means to connect the above ideas in this section to the Couette flow discussed in Section 18.7.2, consider a non-divergent velocity that only has a zonal component with a vertical shear (Figure 18.6)

$$\mathbf{v} = u(z) \hat{x}. \quad (18.93)$$

In this case the only nonzero components to the rate of strain tensor are due to the vertical shear,  $S_{13} = S_{31} = \partial_z u / 2$ . Now consider a horizontal area whose outward normal is parallel to the  $\hat{z}$  direction. The frictional force acting on that area is given by the area integral of the frictional stress

$$\mathbf{F}_{\text{area}} = \int \tau \cdot \hat{n} dS = \int \tau \cdot \hat{z} dx dy = \rho_0 \frac{\hat{x}}{2} \nu A \frac{\partial u}{\partial z}, \quad (18.94)$$

where  $A = \int dx dy$  is the horizontal area, and where we used the constant reference density,  $\rho_0$ , for a Boussinesq fluid. Hence, the zonal stress arises from the nonzero vertical shear.

Momentum is deposited in regions where there is a divergence in the stress, in which case momentum is transferred from regions of high vertical shear to low vertical shear. At a point, the momentum is affected by the divergence of the viscous stress at that point. For  $\mathbf{v} = u(z) \hat{x}$  we have

$$\left[ \frac{\partial(\rho v_m)}{\partial t} \right]_{\text{viscous}} = \partial_n \tau_{nm} \implies \left[ \frac{\partial(\rho u)}{\partial t} \right]_{\text{viscous}} = \partial_z (\mu_{\text{vsc}} \partial_z u), \quad (18.95)$$

so that zonal momentum is preferentially deposited to or removed from regions with high vertical curvature in the zonal velocity. Spatial variations in the dynamic viscosity,  $\mu_{\text{vsc}} = \rho_0 \nu$ , also contribute to friction.

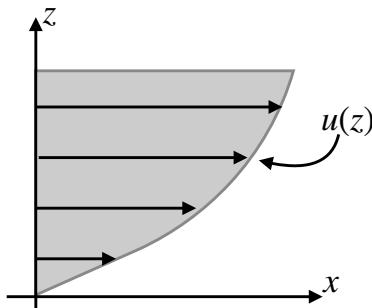


FIGURE 18.6: Sample profile of zonal velocity possessing a vertical shear:  $\mathbf{v} = u(z) \hat{x}$  and with a no-slip boundary condition at  $z = 0$ . The resulting zonal frictional stress arises from the nonzero vertical shear and viscosity.

### 18.7.10 The net stress tensor

Combining the frictional stress tensor with pressure and kinetic stress yields the flux-form momentum equation (18.63)

$$\frac{\partial(\rho \mathbf{v})}{\partial t} + 2\rho \boldsymbol{\Omega} \times \mathbf{v} + \rho \nabla \Phi = \nabla \cdot \mathbb{T}^{\text{net}}, \quad (18.96)$$

where we introduced the net stress tensor

$$\mathbb{T}^{\text{net}} = -p \mathbb{I} - \rho \mathbf{v} \otimes \mathbf{v} + \tau = \begin{bmatrix} -p - \rho u^2 + \tau_{11} & -\rho u v + \tau_{12} & -\rho u w + \tau_{13} \\ -\rho u v + \tau_{12} & -p - \rho v^2 + \tau_{22} & -\rho v w + \tau_{23} \\ -\rho u w + \tau_{13} & -\rho v w + \tau_{23} & -p - \rho w^2 + \tau_{33} \end{bmatrix}. \quad (18.97)$$

The left hand side of the momentum equation (18.96) includes the local time tendency plus the body forces from Coriolis and effective gravity. The right hand side is the divergence of the net stress tensor, with this tensor combining the pressure stress, kinetic stress, and frictional stress. Varieties of the net stress tensor appear in subsequent chapters of this book, with details dependent on the chosen approximations.

### 18.7.11 Comments and further study

There are more elaborate relations between the frictional stress and rate of strain tensors than those considered here. The most general form for a Newtonian fluid introduces a fourth-order viscosity tensor as in Section 4.5 of [Kundu et al. \(2016\)](#) and Chapter 17 in [Griffies \(2004\)](#). We also suggest the treatment of stress in Chapter 5 of [Aris \(1962\)](#).

Geophysical fluids such as air and water are generally well treated using Newtonian constitutive relations. However, there are some geophysical turbulence theories that propose a non-Newtonian constitutive relation for part of their closures, whereby the constitutive relation makes use of products of the rate of strain tensor for computing stress. [Anstey and Zanna \(2017\)](#) offer a compelling approach with a subgrid scale stress tensor that is non-Newtonian and furthermore contains a non-zero trace, thus resulting in a modification to the mechanical pressure. Additional nonlinear relations can arise when the viscous tensor is a function of the flow, such as with the Smagorinsky scheme commonly used for Large Eddy Simulations (LES) (see [Smagorinsky \(1993\)](#) or Chapter 18 of [Griffies \(2004\)](#)).

## 18.8 Reynolds number and flow regimes

How important is friction relative to other terms in the momentum equation? In particular, how does it compare to the material acceleration? We consider that question in the context of the non-rotating and constant density Navier-Stokes equations with a constant viscosity

$$\frac{\partial \mathbf{v}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{v} = -\rho^{-1} \nabla p + \nu \nabla^2 \mathbf{v}, \quad (18.98)$$

with  $\rho$  the constant density.

### 18.8.1 Non-dimensional Navier-Stokes

We non-dimensionalize the Navier-Stokes equation (18.98) to garner an understanding of relative magnitudes of the various terms. For that purpose, introduce the dimensional scales and

corresponding non-dimensional fields

$$L = \text{length scale} \quad U = \text{velocity scale} \quad P = \text{pressure scale} \quad T = \text{time scale}, \quad (18.99)$$

so that equation (18.98) takes the form

$$\frac{\partial \hat{\mathbf{v}}}{\partial \hat{t}} + \frac{V T}{L} (\hat{\mathbf{v}} \cdot \hat{\nabla}) \hat{\mathbf{v}} = -\frac{T P}{\rho V L} \hat{\nabla} \hat{p} + \frac{T \nu}{L^2} \hat{\nabla}^2 \hat{\mathbf{v}}, \quad (18.100)$$

where the hat fields are non-dimensional and defined according to

$$\nabla = L \hat{\nabla} \quad \partial_t = T^{-1} \partial_{\hat{t}} \quad \mathbf{v} = U \hat{\mathbf{v}} \quad p = P \hat{p} \quad (18.101)$$

### 18.8.2 Ratio of inertial to frictional accelerations

We are concerned with three dimensional flows with only a single length and velocity scale,  $L$  and  $U$ . For the time scale we assume that it is determined by fluid particle time scale; i.e., the advective time

$$T \sim L/U. \quad (18.102)$$

Furthermore, we assume that the scale of mechanical pressure is comparable to the stress induced by the flow itself

$$P \sim \rho U^2. \quad (18.103)$$

These assumed scales for time and pressure bring the non-dimensional Navier-Stokes equation (18.100) into the rather tidy form

$$\frac{\partial \hat{\mathbf{v}}}{\partial \hat{t}} + (\hat{\mathbf{v}} \cdot \hat{\nabla}) \hat{\mathbf{v}} = -\hat{\nabla} \hat{p} + \frac{1}{\text{Re}} \hat{\nabla}^2 \hat{\mathbf{v}}. \quad (18.104)$$

Flow regimes of the non-dimensional Navier-Stokes equation are specified by the non-dimensional number,  $\text{Re} = L U / \nu$ , which is the *Reynolds number*. By definition, the Reynolds number is the ratio of scales for material (inertial) acceleration to frictional acceleration

$$\text{Re} = \frac{\text{inertial accelerations}}{\text{frictional accelerations}} = \frac{U/T}{\nu U/L^2} = \frac{L^2/T}{\nu} = \frac{L U}{\nu}. \quad (18.105)$$

### 18.8.3 Reynolds numbers for some example flows

Laboratory experiments with flow around and within various objects indicates the following regimes of flow as a function of the Reynolds number:

$$\text{Re} \sim \begin{cases} \leq 10^2 & \text{laminar} \\ 10^2 - 10^3 & \text{quasi-periodic flow} \\ 10^3 - 10^4 & \text{transition to turbulence} \\ \geq 10^4 & \text{fully turbulent.} \end{cases} \quad (18.106)$$

These numbers are fuzzy given dependence on the geometry of the objects placed in the flow and their characteristic length scale. What is more general concerns the behavior of the flow, with a transition from laminar to turbulent typically occurring as the flow moves from relatively low to high Reynolds number.

For a given molecular kinematic viscosity, the Reynolds number is dependent on the velocity and length scales. Let us consider some examples. First, put your finger into a flowing stream

of water, such as in a gentle mountain creek. Let the length scale for the finger be  $10^{-2}$  m and the stream flow at a speed of  $U \approx 0.1 - 1$  m s $^{-1}$ . With the kinematic viscosity of water given by (page 75 of [Gill \(1982\)](#))

$$\nu_{\text{water}} = 10^{-6} \text{ m}^2 \text{ s}^{-1}, \quad (18.107)$$

we see that our finger poking into the mountain stream is associated with a flow Reynolds number on the order of

$$\text{Re}_{\text{finger in stream}} = 10^3 - 10^4. \quad (18.108)$$

Hence, mountain stream flow around a finger is at the lower end of the turbulent regime. Hence, we might expect to see slightly turbulent whirls and eddies downstream from our finger.

Now consider an oceanographic length scale given by a Gulf Stream ring (see Figure 25.1) in which  $L \approx 10^5$  m. Assuming the flow speed is on the same order as the mountain stream (good assumption) leads to a huge Reynolds number for Gulf Stream flow

$$\text{Re}_{\text{Gulf Stream}} = 10^{10} - 10^{11}. \quad (18.109)$$

For the atmosphere, we take  $L = 10^6$  m for a typical atmospheric weather system,  $U = 10$  m s $^{-1}$  for the speed, and

$$\nu_{\text{air}} = 1.4 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}, \quad (18.110)$$

for the kinematic viscosity of air at standard pressure (page 75 of [Gill \(1982\)](#)). Given the larger length and velocity scales, the Reynolds number for large-scale atmospheric circulation features is

$$\text{Re}_{\text{weather system}} = 10^{12}. \quad (18.111)$$

These values for the Reynolds number are huge relative to typical values found in engineering flows. They signal the minor role that molecular friction plays in large-scale geophysical fluid flows. Even so, molecular friction is the process leading to mechanical energy dissipation at the small scales. A fundamental feature of large Reynolds number flow is the presence of turbulent motions. Turbulent flows are highly nonlinear and affect a transfer of mechanical energy across length and time scales. This cascade leads to the dissipation of mechanical energy at the small scales. It is at the small scales that flow curvature can be large enough for the relatively tiny values of molecular viscosity to dissipate the energy, thus preventing an *ultraviolet catastrophe*; i.e., preventing the unbounded pile up of mechanical energy at the smallest scales.<sup>7</sup>

The ocean and atmosphere exhibit a huge variety of turbulent regimes, from the macroturbulence of quasi-geostrophic eddies to the microturbulence of boundary layers. Turbulence is not directly considered in this book. However, certain of its implications are identified in various places given that it is so basic to the ocean and atmosphere flows. [Vallis \(2017\)](#) offers a pedagogical entry point for the physics and maths of geophysical turbulence.

## 18.9 Stress on an interface

In this section we study the stress acting on an interface. This analysis applies to an arbitrary surface within a single media as well as for the boundary interface separating a liquid and a gas (air-sea boundary) or between a fluid and a rigid boundary (air-land or ocean-land). We ignore the effects from surface tension discussed in Section 18.10 since we are interested in length scales larger than the capillary-gravity waves where surface tension is important, with equation (18.141) indicating that these wavelengths are roughly  $\lambda_{\text{cap-grav}} \approx 17$  cm.

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<sup>7</sup>Ultraviolet refers to the high wavenumber end of the flow spectrum, as in the violet part of the visible electromagnetic spectrum.

### 18.9.1 General formulation

Formulation of the stress boundary conditions follows from applying the finite volume momentum equation (18.66) to a cylindrical region straddling a moving interface such as that shown in Figure 18.7. The sides of the cylinder have thickness  $h$  and the top and bottom have area  $\delta\mathcal{S}$ . In the limit that the cylinder thickness goes to zero, the volume integrals in equation (18.66) vanish under the assumption of a smooth velocity field on both sides of the interface as well as smooth body forces. We are thus left with the constraint that the area integrated contact forces must vanish when integrated around the cylinder boundary

$$\oint_{\partial\text{cylinder}} [\mathbb{T} + \rho \mathbf{v} \otimes (\mathbf{v}^{(b)} - \mathbf{v})] \cdot \hat{\mathbf{n}} d\mathcal{S} = \oint_{\partial\text{cylinder}} [-p \mathbb{I} + \tau + \rho \mathbf{v} \otimes (\mathbf{v}^{(b)} - \mathbf{v})] \cdot \hat{\mathbf{n}} d\mathcal{S} = 0. \quad (18.112)$$

The end-caps on the cylinder vanish as  $h \rightarrow 0$ , in which case we have no constraint based on the stresses acting on the end-caps. Instead, the  $h \rightarrow 0$  limit leads us to conclude that the contact force on one side of the interface is equal and opposite to that on the other side. This condition is a direct statement of the Newton's third law as manifest via the local equilibrium of stresses discussed in Section 18.1.2. For the stresses acting on the interface in Figure 18.7 we have

$$[-p_A \mathbb{I} + \tau_A + \rho_A \mathbf{v}_A \otimes (\mathbf{v}^{(b)} - \mathbf{v}_A)] \cdot \hat{\mathbf{n}}_A + [-p_B \mathbb{I} + \tau_B + \rho_B \mathbf{v}_B \otimes (\mathbf{v}^{(b)} - \mathbf{v}_B)] \cdot \hat{\mathbf{n}}_B = 0. \quad (18.113)$$

Setting  $\hat{\mathbf{n}} = \hat{\mathbf{n}}_B = -\hat{\mathbf{n}}_A$  leads to

$$[-p_A \mathbb{I} + \tau_A + \rho_A \mathbf{v}_A \otimes (\mathbf{v}^{(b)} - \mathbf{v}_A)] \cdot \hat{\mathbf{n}} = [-p_B \mathbb{I} + \tau_B + \rho_B \mathbf{v}_B \otimes (\mathbf{v}^{(b)} - \mathbf{v}_B)] \cdot \hat{\mathbf{n}}, \quad (18.114)$$

which is an expanded expression of Newton's third law given in equation (18.5). Recall that we are ignoring surface tension, which means there is no pressure jump across the interface (see Section 18.10). Hence, setting  $p_A = p_B$  allows us to cancel pressure thus leaving an interface stress condition involving just the frictional stress and kinetic stress

$$[\tau_A + \rho_A \mathbf{v}_A \otimes (\mathbf{v}^{(b)} - \mathbf{v}_A)] \cdot \hat{\mathbf{n}} = [\tau_B + \rho_B \mathbf{v}_B \otimes (\mathbf{v}^{(b)} - \mathbf{v}_B)] \cdot \hat{\mathbf{n}}. \quad (18.115)$$

We now consider a variety of examples to illustrate this condition.

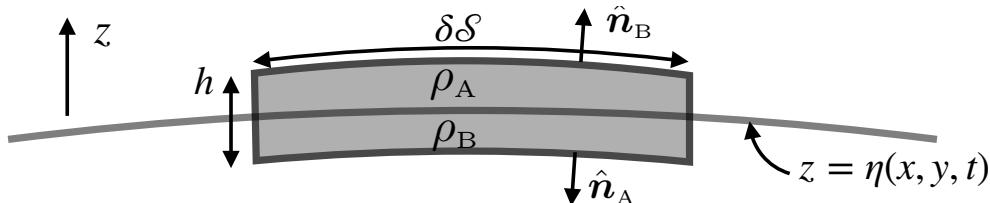


FIGURE 18.7: An infinitesimal cylindrical region used in formulating the stress boundary condition at an interface. The interface can be one that separates two fluid regions with densities  $\rho_A$  and  $\rho_B$ . It can also represent the boundary between a fluid (region A) and solid (region B). The interface generally moves with velocity  $\mathbf{v}^{(b)}$ . We orient the interface through the outward normals according to  $\hat{\mathbf{n}} = \hat{\mathbf{n}}_B = -\hat{\mathbf{n}}_A$ . The outward normal for region A points into region B whereas the outward normal for region B points into region A. For this particular interface, the normal direction has a nonzero projection in the vertical,  $\hat{\mathbf{n}} \cdot \hat{\mathbf{z}} \neq 0$ , thus allowing us to define the interface vertical position according to  $z = \eta(x, y, t)$ . This interface represents an idealized geometry useful to formulate the stress condition at the boundary between fluid media, such as the air-sea interface, fluid-land interface, or interior fluid interface (e.g., buoyancy surface). The single geometric assumption is that there are no overturning motions so that  $\hat{\mathbf{n}} \cdot \hat{\mathbf{z}} \neq 0$ , with this assumption based on convenience. The stress condition is general and so does not require this assumption.

### 18.9.2 Solid material boundary

Consider a solid material boundary through which no matter crosses. Let region  $B$  be the solid side of the interface and region  $A$  the fluid side (region  $A$  is either the ocean or atmosphere). The material nature of the boundary means that no matter crosses it, in which case (see Section 14.4.2)

$$(\mathbf{v}_A - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = (\mathbf{v}_B - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = 0. \quad (18.116)$$

A nonzero  $\mathbf{v}^{(b)}$  corresponds here to a moving solid boundary, such as the region next to the grounding line of an ice-shelf. More commonly, in geophysical fluid applications we have  $\mathbf{v}^{(b)} = 0$  for solid boundaries. Since there is no contribution from the kinetic stress, the stress condition (18.115) reduces to

$$\tau_A \cdot \hat{\mathbf{n}} = \tau_B \cdot \hat{\mathbf{n}}. \quad (18.117)$$

This identity is consistent with

$$\tau_A \cdot \hat{\mathbf{n}} = \boldsymbol{\tau}^{\text{friction } A}(\mathbf{x}, t, \hat{\mathbf{n}}) = -\boldsymbol{\tau}^{\text{friction } A}(\mathbf{x}, t, -\hat{\mathbf{n}}) = \tau_B \cdot \hat{\mathbf{n}} = \boldsymbol{\tau}^{\text{friction } B}(\mathbf{x}, t, \hat{\mathbf{n}}), \quad (18.118)$$

which expresses Newton's third law in the form of equation (18.5). Hence, the frictional force imparted by the land on the fluid is equal and opposite to that imparted by the fluid on the land.

### 18.9.3 No-slip boundary condition

At solid boundaries, the kinematic boundary condition from Section 14.4.1 sets the normal component of the velocity to zero

$$\mathbf{v} \cdot \hat{\mathbf{n}} = 0 \quad \text{kinematic no-flux condition on static material boundary.} \quad (18.119)$$

However, no place have we specified the tangential component of the velocity along a solid boundary. What is it?

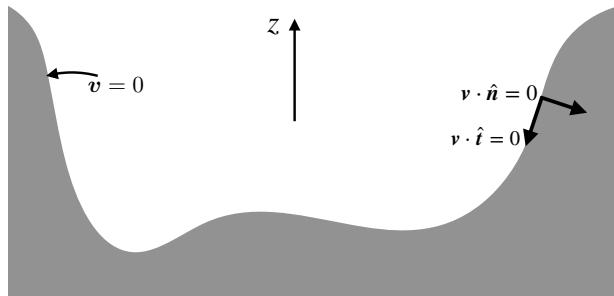


FIGURE 18.8: The no-slip boundary condition means that fluid exhibits zero relative motion at the solid-fluid boundary,  $\mathbf{v} \cdot \hat{\mathbf{t}} = 0$ . That is, the fluid sticks to the solid boundary. The kinematic no-normal flow boundary condition,  $\mathbf{v} \cdot \hat{\mathbf{n}} = 0$ , plus the dynamic no-slip boundary condition together mean that both the normal and tangential components of the velocity vanish at solid boundaries. For both the normal and tangential components of the velocity to vanish at a solid boundary requires the velocity to fully vanish at this boundary.

Laboratory experiments over the 19th and 20th centuries indicate that there is no relative motion of molecules at solid-fluid interfaces.<sup>8</sup> That is, a fluid at the solid-fluid interface has a velocity matching that of the solid so that the fluid sticks to the solid boundary as depicted

<sup>8</sup>As discussed in the historical essay by [Anderson \(2005\)](#), it was the work of Prandtl in 1905 that first exposed the fundamental nature of the no-slip boundary condition, and its role in establishing boundary layers around solid bodies immersed in a fluid flow.

in Figure 18.8. The no-slip boundary condition means that both the normal and tangential components of the fluid velocity vanish next to static solid boundaries

$$\mathbf{v} \cdot \hat{\mathbf{n}} = \mathbf{v} \cdot \hat{\mathbf{t}} = 0 \quad \text{no-slip condition on static solid boundaries.} \quad (18.120)$$

The no-slip boundary condition gives rise to an exchange of momentum between the solid and fluid, with this exchange mediated by viscosity. This boundary condition is the origin of the tangential stresses found in the Couette flow discussed in Section 18.7.2. In the absence of viscous friction, as per an inviscid perfect fluid, the no-slip boundary condition cannot be imposed since doing so would mathematically over-specify the flow. Consequently, for inviscid fluids the tangential component of the velocity remains unspecified at solid boundaries.

#### 18.9.4 Lagrangian interface

Consider a Lagrangian interface within the fluid, with this interface defined so that

$$(\mathbf{v}_A - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = (\mathbf{v}_B - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = 0. \quad (18.121)$$

Again the kinetic stress contribution to equation (18.115) vanishes. We thus have the frictional stress condition (18.117) and a Newton's third law interpretation (18.118), yet now the frictional transfer takes place between two regions of the same fluid.

#### 18.9.5 Permeable interface

Now allow for the interface to be permeable and introduce the dia-surface transport defined by equation (42.41)

$$(\mathbf{v}_A - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = (\mathbf{v}_B - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = w^{\text{dia}}, \quad (18.122)$$

where we assumed continuous dia-surface transport across the interface; i.e., what leaves one side enters the other. The kinetic stress thus adds to the frictional contribution in the stress boundary condition (18.115), with the kinetic stress providing a transfer of momentum across the interface through the dia-surface advection of fluid elements

$$\tau_A \cdot \hat{\mathbf{n}} + \rho_A \mathbf{v}_A w^{\text{dia}} = \tau_B \cdot \hat{\mathbf{n}} + \rho_B \mathbf{v}_B w^{\text{dia}}. \quad (18.123)$$

We consider two cases.

##### *Single continuous fluid media*

If the interface is within a single continuous fluid media, then  $\rho_A = \rho_B$  and  $\mathbf{v}_A = \mathbf{v}_B$ , in which case the advection of momentum from region  $A$  to  $B$  is equal to that from region  $B$  to  $A$ . Consequently, the frictional condition (18.117) again holds.

##### *Air-sea boundary interface*

Consider now the air-sea boundary where region  $B$  is the ocean and region  $A$  the atmosphere. Introduce the dia-surface mass flux according to equation (14.63)

$$\rho_A w^{\text{dia}} = \rho_B w^{\text{dia}} = -\mathcal{Q}_m, \quad (18.124)$$

where  $\mathcal{Q}_m$  is the mass per time per surface area crossing the boundary. The minus sign is implied by the convention that  $\mathcal{Q}_m > 0$  means that mass enters the ocean side of the interface and leaves

the atmosphere side. Even though the densities and velocities on the two sides of the interface are unequal, mass conservation means that the mass transport entering the ocean must leave the atmosphere, and vice versa. Consequently, the stress boundary condition (18.123) takes the form

$$\tau_{\text{atm}} \cdot \hat{\mathbf{n}} - \mathbf{v}_{\text{atm}} \mathcal{Q}_m = \tau_{\text{ocean}} \cdot \hat{\mathbf{n}} - \mathbf{v}_{\text{ocean}} \mathcal{Q}_m \implies (\tau_{\text{atm}} - \tau_{\text{ocean}}) \cdot \hat{\mathbf{n}} = (\mathbf{v}_{\text{atm}} - \mathbf{v}_{\text{ocean}}) \mathcal{Q}_m. \quad (18.125)$$

There is generally a jump in the frictional stress in the presence of mass transport across the air-sea interface. However, when introducing the dia-surface transport (18.122) we see that  $\mathbf{v}_A \cdot \hat{\mathbf{n}} = \mathbf{v}_B \cdot \hat{\mathbf{n}}$  at the interface. So a nonzero  $\mathbf{v}_{\text{atm}} - \mathbf{v}_{\text{ocean}}$  arises just from differences in the tangential velocities at the air-sea interface. If those velocities are equal so that  $(\mathbf{v}_{\text{atm}} - \mathbf{v}_{\text{ocean}}) \mathcal{Q}_m = 0$ , then we are again left with the friction boundary condition (18.117).

### 18.9.6 Summary comments

There are three terms in the general expression for the stress boundary condition (18.114), with contributions from pressure, friction, and kinetic stress. In the absence of surface tension, pressure is continuous at the interface; i.e., its value is the same on both sides of the interface. In the absence of mass transport across the interface, then we find a continuous kinetic stress at the interface that then leads to a continuous frictional stress. However, mass transport crossing the interface leads to a jump in the friction for those case where the tangential velocity has a jump across the interface. Assuming no such jump then leads again to a continuous frictional stress.

### 18.9.7 Comments on boundary layers

A fundamental advance in the relevance of fluid mechanics for describing observed flows came from the 20th century work of Prandtl and others who noted the central role of viscosity, even the tiny molecular values, in forming boundary layers when fluids flow next to rigid bodies.<sup>9</sup> Prandtl's work focused on flows around airplane wings, thus supporting the development of aerodynamics as a scientific and engineering discipline. The key ideas transfer to geophysical flows where boundary layers form in the atmosphere and ocean as these fluids interact with the solid earth. Boundary layers also form where the atmosphere and ocean interact with one another.

A key facet of geophysical boundary layers concerns the dominance of turbulence in producing an eddy viscosity that is many orders larger than molecular viscosity. Indeed, molecular viscosity plays a role only in a very small region (the *laminar subregion*) immediately adjacent to the boundary, where as the bulk of the boundary layer is dominated by turbulence. The study of boundary layers is well outside our scope, as it is largely a topic of turbulence. However, in Chapter 27 we dive into the details of geophysical boundary layers that are affected by pressure, Coriolis, and turbulence induced friction. The leading role of rotation distinguishes geophysical boundary layers from engineering applications. The associated *Ekman boundary layers* are crucial for understanding circulation and transport in both the atmosphere and ocean.

## 18.10 Surface tension

Surface tension is present on surfaces that separate two immiscible liquids or between a liquid and gas. It has many consequences, such as allowing certain insects to walk on water even though their body density is greater than water, and for the predominantly spherical shape of rain drops.

<sup>9</sup>For a historical treatment of boundary layer theory see [Anderson \(2005\)](#), or for a pedagogical study see [Tennekes and Lumley \(1972\)](#). The associated mathematical methods of singular perturbation theory and matched asymptotic expansions (e.g., [Dyke \(1975\)](#)) offer an example of how the study of physical systems can spawn the development of new mathematical methods.

A molecular dynamics understanding of surface tension involves tools from physical chemistry that are outside of our scope. Instead, we develop heuristics sufficient to determine when one needs to be concerned with surface tension in the study of geophysical fluid mechanics. As shown in this section, surface tension can be safely ignored when concerned with length scales on the order of meters or larger.

As an introduction to surface tension, consider that atmospheric pressure at the earth's surface is roughly  $p_{\text{atm}} = 10^5 \text{ N m}^{-2}$ . As we saw in Section 18.7, pressure acts normal to a surface regardless the surface orientation. So fill a container of water whose weight per horizontal area is less than the atmospheric pressure,  $\rho g h < p_{\text{atm}}$  and turn the container upside-down as in Figure 18.9. Does the water spill from the container? Common experience with drinking glasses indicate that water will spill. But what about containers with a very small cross-sectional area such as the pipettes used in chemistry laboratories? Pipettes, or more generally capillary tubes, hold the liquid regardless the orientation. They do so since their cross-sectional area is small enough to allow forces from surface tension to overcome gravitational instabilities acting at the liquid-gas interface. In the remainder of this section we discuss elements of surface tension with the goal to develop intuition as well as to determine the length scales where it becomes important.

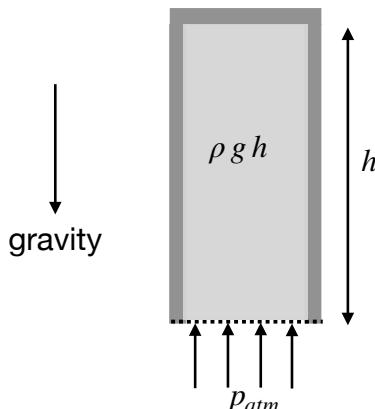


FIGURE 18.9: A container of water with density  $\rho$  and height  $h$  is placed upside-down. Atmospheric pressure,  $p_{\text{atm}}$ , will support water with thickness  $h < p_{\text{atm}}/(\rho g) \approx 10 \text{ m}$  if the cross-sectional area of the container is small enough to allow for surface tension to overcome the gravitationally unstable waves that otherwise allow water to spill from the container. The liquid-gas interface supports both gravity waves (as in Section 31.8.3) and capillary waves. If the wavelength is small enough then surface tension suppresses the growth of unstable gravity waves so that the liquid remains within the *capillary tube*. However, for longer waves allowed by increasing the cross-sectional area, then any fluctuation will allow the gravitational instability to overcome surface tension, thus breaking the interface and releasing water.

### 18.10.1 Force balance on an air-water interface

Consider two fluids with distinct densities. Air and water provide one example of special importance to understanding physics at the ocean-atmosphere boundary. Another example concerns two immiscible layers of water within the ocean or two layers of air within the atmosphere. For molecules well within either of the fluid regions, the intermolecular forces are statistically isotropic. In contrast, intermolecular forces are not isotropic for molecules within a mean free path distance from the interface.<sup>10</sup> Attractive (cohesive) intermolecular (van der Waals) forces dominate within a liquid whereas gas molecules generally feel more repulsive forces. Hence, a liquid molecule

<sup>10</sup>As discussed in Section 11.2, the mean free path is a statistical measure of the distance a molecule moves before hitting another molecule.

within the liquid-gas interface preferentially experiences an attractive force towards the liquid side of the interface, as depicted in Figure 18.10. Surface tension arises from the cohesive force per area acting between molecules in a direction that parallels the interface, with surface tension acting to resist perturbations to the interface shape.

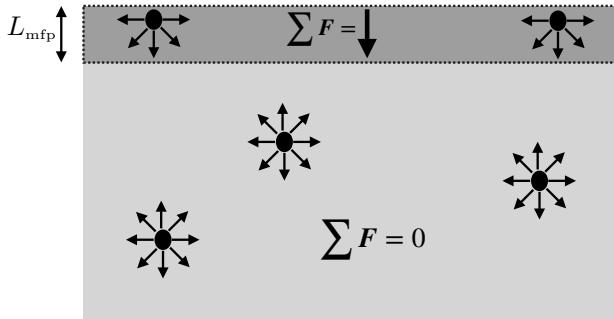


FIGURE 18.10: Surface tension at a liquid-gas interface arises from the anisotropic cohesive forces acting on liquid molecules within a mean-free-path distance,  $L_{\text{mfp}}$ , from the interface, which contrasts to the isotropic cohesive forces acting away from the interface. The net intermolecular force vanishes for interior molecules, whereas the net force acts inward on molecules at the interface. Surface tension refers to the cohesive force per area acting between molecules in a direction that is parallel to the interface.

Anisotropic attractive intermolecular forces cause the interface between the two fluids to behave as a stretched membrane that experiences a tensile force resisting any stretching of the interface. The magnitude of the tensile force per unit length is the *surface tension*,  $\gamma$  (units  $\text{N m}^{-1}$ ). The surface tension is a property of the two fluids, including their temperature, as well as any impurities that might be included on the interface; e.g., oil on the surface of water effects properties of the capillary waves found on the air-sea interface. In the following we focus on the liquid-gas example to be specific and to expose issues that arise in studies of the air-sea interface. For a liquid-gas interface surrounding a liquid drop, the tensile force acts to curve the interface towards the liquid into a spherical shape.

The tensile force along a line segment is directed normal to the line and tangent to the interface

$$\mathbf{f}_{\text{interface}} = -\gamma \hat{\mathbf{n}} \times \delta \mathbf{x}, \quad (18.126)$$

where  $\hat{\mathbf{n}}$  is a normal vector pointing towards the center of the curved interface, and  $\delta \mathbf{x}$  is a line element oriented so that the normal  $\hat{\mathbf{n}}$  points to the left facing in the direction of the line increment. Figure 18.11 depicts the surface tensile forces acting on the surface of a spherical bubble of water. Note that it is sometimes useful to consider the product  $\gamma d\mathcal{S}$  as the work (units of  $\text{N m}^{-1} = \text{Joule}$ ) required to create an area,  $d\mathcal{S}$ , on the interface. We make use of this energetic perspective in Section 18.10.2.

To develop an expression for the pressure jump across the liquid-gas interface, consider a spherical droplet of radius  $R$  shown in Figure 18.11 and focus on the circular cross-section cut through the center of the sphere. The net tensile force acting on the circumference of the circle is

$$\mathbf{F}_{\text{circle}} = \oint_{\text{circle}} \mathbf{f}_{\text{interface}} = - \oint_{\text{circle}} \gamma \hat{\mathbf{n}} \times \delta \mathbf{x} = -2\pi R \gamma \hat{\mathbf{z}}. \quad (18.127)$$

Equilibrium of the spherical droplet is realized by a pressure jump across the circular cross-sectional area

$$\pi R^2 (p_{\text{in}} - p_{\text{out}}) = 2\pi R \gamma \implies (p_{\text{in}} - p_{\text{out}}) = 2\gamma/R. \quad (18.128)$$

Hence, the pressure jump is determined by the surface tension (a property of the two fluids) and the curvature of the sphere,  $R$ , which is also the radius of curvature for the sphere. Pressure is higher inside of the sphere, with this pressure required to balance the pressure outside the sphere plus the surface tension. Notably, equilibrium for smaller bubbles requires a larger pressure difference than for larger bubbles.

The pressure jump is known as the *capillary pressure*. It arises from surface tension and curvature of the interface. The relation (18.128) is a special case of the Young-Laplace formula, specialized here to a sphere.

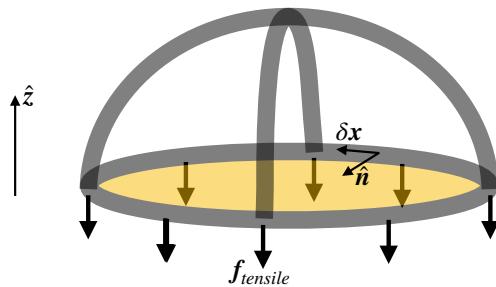


FIGURE 18.11: Surface tension on a spherical water droplet, with water on the inside of the sphere and air on the outside. The tensile forces act parallel to the spherical interface between the water and air. When cutting a circular cross-section as shown here, the surface tensile force acts downward. In equilibrium, the net tensile forces acting downward along the circumference of the hemisphere ( $2\pi R \gamma$ ) are balanced by a pressure jump across the droplet, with the interior pressure larger than the exterior pressure. Focusing on the circular cross-section, this area remains static so long as  $2\pi R \gamma = \pi R^2 (p_{in} - p_{out})$ , leading to a pressure jump across the droplet interface  $p_{in} - p_{out} = 2\gamma/R$ .

## 18.10.2 Young-Laplace formula

We garner added insight into the physics of surface tension by considering the energetics required to enable a virtual displacement of a surface through a pressure field along with the work required to change the area of the surface. The resulting equation for the pressure jump across the surface is referred to as the *Young-Laplace formula*, which expresses the pressure jump in terms of the surface tension and the principle radii of curvature for the surface.

Consider a horizontal surface depicted in Figure 18.12 that represents the interface separating fluid-A from fluid-B, with  $\hat{n}$  a unit normal vector oriented from fluid-A to fluid-B. Now consider a virtual displacement of each point along the interface by an infinitesimal distance,  $\delta h$ , with  $\hat{n} \delta h$  connecting points on the initial position of the interface to the displaced position, where  $\delta h > 0$  if the displacement is directed towards fluid-B and  $\delta h < 0$  if directed towards fluid-A. The (signed) volume swept out by an infinitesimal area  $dA$  is given by  $\delta h dA$ , with this volume realized by applying the pressure work to the surface

$$W_{volume} = (p_B - p_A) \delta h dA. \quad (18.129)$$

For example, if  $p_B > p_A$  and the displacement is into fluid-B ( $\delta h > 0$ ), then  $W_{volume} > 0$ , thus indicating the need to apply positive work to the surface to move it into the fluid region with higher pressure. Conversely, the required pressure work is negative if displacing the interface into a region with lower pressure.

In the presence of surface tension, work must overcome the surface area energy in order to change to the interface area

$$W_{area} = \gamma \delta A, \quad (18.130)$$

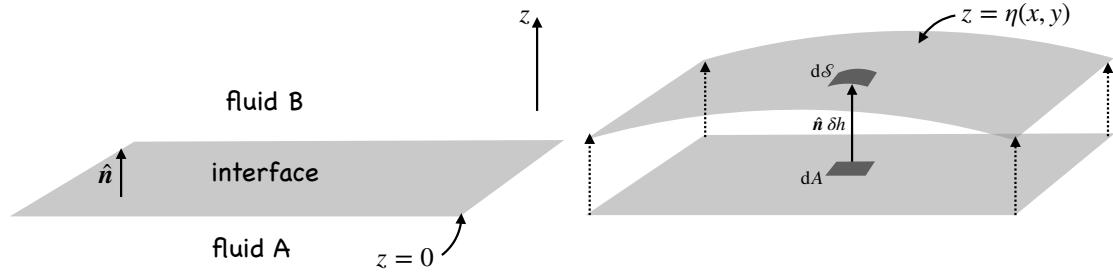


FIGURE 18.12: Left panel: initial position of an interface separating two fluid regions, fluid-A and fluid-B. Right panel: infinitesimal displacement of the interface sweeps out a volume in space. To determine the volume, extend a unit normal vector,  $\hat{n}$ , from the initial interface position and pointing towards fluid-B. Let  $\delta h$  be the distance along that normal to the new position, with  $\delta h > 0$  if the displacement moves towards fluid-B and  $\delta h < 0$  for displacements pointing to fluid-A. We assume that displacements at each interface point can move independently of adjacent points, so that the interface area generally changes.

where  $\delta A$  is the change in area of an infinitesimal element on the interface

$$\delta A = d\mathcal{S} - dA \quad (18.131a)$$

$$= dA \left[ \sqrt{1 + (\nabla \delta h)^2} - 1 \right] \quad (18.131b)$$

$$\approx dA (\nabla \delta h)^2 / 2. \quad (18.131c)$$

To reach this result we made use of equation (5.30) that relates the area of an infinitesimal element on a curved surface to the area of its horizontal projection (see Section 5.3.1). We next make use of the surface curvature detailed in Section 5.3.2, where equation (5.35) shows that the vertical displacement is given, for small displacements, by

$$\delta h \approx \frac{1}{2} R_1^{-1} (\mathbf{x} \cdot \mathbf{e}_1)^2 + \frac{1}{2} R_2^{-1} (\mathbf{x} \cdot \mathbf{e}_2)^2. \quad (18.132)$$

$R_1^{-1}, R_2^{-1}$  are the eigenvalues and  $\mathbf{e}_1, \mathbf{e}_2$  are the corresponding eigenvectors of the matrix of second partial derivatives of  $\delta h(x, y)$ , whereas the inverse eigenvalues,  $R_1, R_2$ , are the radii of curvature of the displaced surface. Orienting the Cartesian axes along the eigenvector directions renders

$$(\nabla \delta h)^2 \approx (x/R_1)^2 + (y/R_2)^2 = \delta h \left[ \frac{1}{R_1} + \frac{1}{R_2} \right], \quad (18.133)$$

where we set

$$\delta h/R_1 = (x/R_1)^2 \quad \text{and} \quad \delta h/R_2 = (y/R_2)^2. \quad (18.134)$$

We are thus led to the area difference

$$\delta A \approx dA \delta h \left[ \frac{1}{R_1} + \frac{1}{R_2} \right]. \quad (18.135)$$

Note that  $\delta A > 0$  whether displacing the surface into a concave or convex direction, since the sign of  $\delta h$  accounts for the sign of the radii of curvature.

The total work for the interface displacement is given by the sum of the area work and volume work

$$W_{\text{area}} + W_{\text{volume}} = dA \delta h [\gamma (R_1^{-1} + R_2^{-2}) + p_B - p_A] \quad (18.136)$$

and equilibrium results if the work vanishes

$$p_A - p_B = \gamma (R_1^{-1} + R_2^{-2}). \quad (18.137)$$

This equation is the Young-Laplace formula, which reduces to equation (18.128) if  $R_1 = R_2$  as for a sphere. It says that there is a pressure jump, known as the *capillary pressure*, across an interface as given by the surface tension times the sum of the inverse principle radii of curvature. Pressure is higher on the concave side of the interface, such as fluid-A depicted in Figure 18.12 or the inside of a bubble/droplet.

### 18.10.3 Some oceanographic examples

We close this section with examples relevant to the ocean.

#### *Soluble gas bubbles inside water*

The previous considerations hold whether there is liquid or gas inside the spherical droplet/bubble. As an example, consider a spherical gas bubble of radius  $R = 10^{-6}$  m inside water and make use of the air-water surface tension  $\gamma = 0.072$  N m<sup>-1</sup>

$$p_{\text{in}} - p_{\text{out}} = 2\gamma/R \approx 144 \times 10^3 \text{ N m}^{-2} = 1.42 p_{\text{atm}}, \quad (18.138)$$

where  $p_{\text{atm}} = 101 \times 10^3$  N m<sup>-2</sup> is standard atmospheric pressure. If the gas inside the bubble is water soluble, then the enhanced pressure inside the bubble will induce more gas to dissolve in the water, which in turn will cause the bubble to shrink and thus increase the pressure inside the bubble. Small bubbles of soluble gases can thus be squeezed towards zero radius by the effects of surface tension induced pressure.

#### *Length scale for capillary waves*

Capillary waves exist along the air-sea interface due to the restorative effects from surface tension. When present within a gravity field, the capillary waves appear along with gravity waves. We see capillary waves when there is a very slight breeze on the ocean surface. Capillary waves also arise when a tiny stone is thrown into a still pond, whereas gravity waves dominate when a larger stone is used. This phenomenology arises from the following considerations of the dispersion relation.

The dispersion relation for capillary-gravity waves (e.g., Section 54 of [Fetter and Walecka \(1980\)](#)) is given by

$$\omega^2 = k g \left[ 1 + \frac{k^2 \gamma}{g \rho} \right], \quad (18.139)$$

where  $\rho$  is the density of water,  $k = 2\pi/\lambda$  is the wave number, and  $\omega$  is the radial frequency. The non-dimensional parameter  $k^2 \gamma / (g \rho)$  provides a regime boundary where capillary waves are important ( $k^2 \gamma > g \rho$ ) and negligible ( $k^2 \gamma < g \rho$ ). To deduce a correspondingly length scale we introduce the wavelength

$$\lambda_{\text{cap-grav}} = 2\pi \sqrt{\frac{\gamma}{\rho g}}, \quad (18.140)$$

with  $\lambda < \lambda_{\text{cap-grav}}$  the capillary wave regime and  $\lambda > \lambda_{\text{cap-grav}}$  the gravity wave regime. Using  $\gamma = 0.072$  N m<sup>-1</sup> and  $\rho = 1000$  kg m<sup>-3</sup> leads to

$$\lambda_{\text{cap-grav}} = 2\pi \sqrt{\frac{\gamma}{\rho g}} \approx 0.017 \text{ m} = 17 \text{ cm}. \quad (18.141)$$

Since this book is mostly concerned with length scales larger than  $\lambda_{\text{cap-grav}}$ , we generally ignore the dynamics of capillary waves for our study of geophysical fluid mechanics.

#### 18.10.4 Further study

Although we have no further concern for surface tension in this book, its study forms an important aspect of air-sea interaction physics. There are many places to continue its study, with the following offering treatments similar to the physical ideas given here.

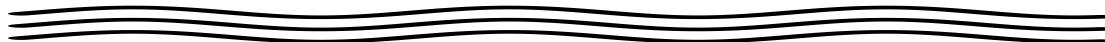
This [30-minute video](#) from Prof. L. Trefethen provides a pedagogical summary of surface tension. The upside-down container of water in Figure 18.9 is based on a discussion of capillary-gravity waves in Section 3.1.3 of [Falkovich \(2011\)](#). Section 1.9 of [Batchelor \(1967\)](#) discusses how surface tension acts between two fluid media, with that discussion extended into his Section 3.3 to develop boundary conditions for velocity and stress. The bubble example in Section 18.10.3 is taken from Section 1.3 of [Kundu et al. \(2016\)](#). Section 4.10 of [Kundu et al. \(2016\)](#) provides a detailed accounting of the force balance at an interface, offering more details than found in [Batchelor \(1967\)](#). The energetic arguments used to derive the Young-Laplace formula follows Section 61 of [Landau and Lifshitz \(1987\)](#). Section 46 of [Fetter and Walecka \(1980\)](#) discuss the dynamics of membranes under tension, and Section 54 considers surface capillary-gravity waves.

### 18.11 Exercises

#### EXERCISE 18.1: FORCE BALANCE FOR A NON-ACCELERATING OCEAN

Consider an ocean basin,  $\mathcal{R}$ , as in Figure 18.2 with bottom interface separating the ocean fluid from the solid-earth, and upper interface separating the ocean fluid from the atmosphere, and where the atmosphere has a nonzero mass.<sup>11</sup> Assume no matter crosses the ocean boundaries; i.e., no evaporation, precipitation, nor river runoff. However, assume there is a horizontal stress over the ocean surface with a stress vector  $\tau^{\text{surf}}$ , thus imparting a net surface stress that drives motion. Allow for the ocean bottom to exchange momentum with the solid-earth through a bottom stress,  $\tau^{\text{bott}}$ .

- What is the force balance for the full ocean domain if the center of mass experiences no acceleration? Express this force balance in words and in equations. The answer should be generally stated, with no need for specific details. Hint: consider Figure 18.2 and include the missing forces to this diagram. Mathematically express the force balance as an integral expression as per the weak formulation.
- Express the vertical component of the force balance assuming the fluid is in an approximate hydrostatic balance, meaning that pressure and gravity forces balance.<sup>12</sup>
- Assume motion on a flat plane with a constant rotation rate  $\Omega = \hat{z}\Omega = \hat{z}(f/2)$  as per an *f*-plane (Section 22.3). Also assume that the center of mass motion vanishes,  $\int \rho \mathbf{v} dV = 0$ . Discuss the resulting zonal and meridional force balance. Hint: one of the forces appearing in part (a) now vanishes.



<sup>11</sup>In some applications it is suitable to assume a zero mass atmosphere. For this exercise, however, we do not make that assumption.

<sup>12</sup>In Section 22.2 we provide a discussion of when this approximation is appropriate for moving fluids. That discussion is not needed for the current exercise. Instead, we merely assume the vertical momentum balance is hydrostatic.

# Chapter 19

## Pressure form stress

As introduced in our discussion of Cauchy's stress principle in Section 18.1, pressure form stress is the horizontal stress arising from pressure that acts on a sloped surface or interface. As a contact force per area, Newton's third law describes how form stress renders a transfer of pressure forces across interfaces, with pressure form stress affecting a vertical transfer of horizontal pressure forces. Hence, it provides an inviscid/reversible mechanism for the vertical transfer of horizontal momentum, thus complementing the vertical transfer associated with viscosity in the presence of tangential shear stresses (Section 18.7.2).

In this chapter we study pressure form stresses encountered on the variety of interfaces encountered in geophysical fluids. We then develop two case studies to expose the role of pressure form stress in the force balances affecting motion of an ocean fluid column. The first case study is concerned with the evolution of vertically integrated horizontal linear momentum per mass. The second case study focuses on the axial angular momentum budget as a framework to study the dominant force balances in ocean channel flow and ocean gyre flows.

### CHAPTER GUIDE

In this chapter we study how form stresses act on the variety of interfaces encountered in geophysical fluids. We build from the study of stresses in Chapter 18, with an understanding of pressure form stress greatly enhancing our understanding of horizontal forces acting in geophysical fluids. The focus on horizontal forces in this chapter complements our studies in Chapter 24, whereby the net vertical acceleration from pressure and gravitational forces is repackaged into the buoyancy force.

19.1	Pressure form stresses at an interface . . . . .	410
19.1.1	Concerning the sign of a form stress . . . . .	411
19.1.2	Mathematical expression for form stress . . . . .	411
19.1.3	Comments . . . . .	413
19.2	Form stresses on the ocean boundaries . . . . .	413
19.2.1	Zonally symmetric ridge . . . . .	413
19.2.2	Form stress transfer between the fluid and its boundaries . . . . .	413
19.2.3	Decomposing topographic form stress . . . . .	415
19.3	Interfacial form stress . . . . .	416
19.3.1	Interfacial form stresses transferred between layers . . . . .	416
19.3.2	Zonally integrated interfacial form stress . . . . .	418
19.3.3	Comments . . . . .	419

19.4	Evolution of depth integrated horizontal momentum . . . . .	419
19.4.1	Flux-form horizontal momentum equation . . . . .	419
19.4.2	Leibniz's rule for the inertial and Coriolis accelerations . . . . .	420
19.4.3	External and internal decomposition of the kinetic stress . . . . .	420
19.4.4	Depth integrated horizontal pressure gradient . . . . .	421
19.4.5	Depth integrated momentum equation . . . . .	421
19.4.6	Balances when $\nabla \cdot \mathbf{U}^p = 0$ . . . . .	422
19.5	Axial angular momentum budget for an ocean domain . . . . .	423
19.5.1	Anticipating the budget . . . . .	424
19.5.2	Axial angular momentum . . . . .	424
19.5.3	Depth integrated budget . . . . .	424
19.5.4	Atmospheric and topographic form stresses . . . . .	425
19.5.5	Turbulent stresses at the surface and bottom . . . . .	425
19.5.6	Summary budget for column integrated axial angular momentum .	426
19.5.7	Zonal domain topology/geometry and zonal integration . . . . .	427
19.5.8	Steady domain integrated balance . . . . .	428
19.5.9	Form stress versus dual form stress . . . . .	428
19.5.10	Steady zonal and depth integrated budget . . . . .	429
19.5.11	Southern Ocean balances . . . . .	429
19.5.12	Topographic form stress and ocean gyres . . . . .	430
19.5.13	Further study . . . . .	430

## 19.1 Pressure form stresses at an interface

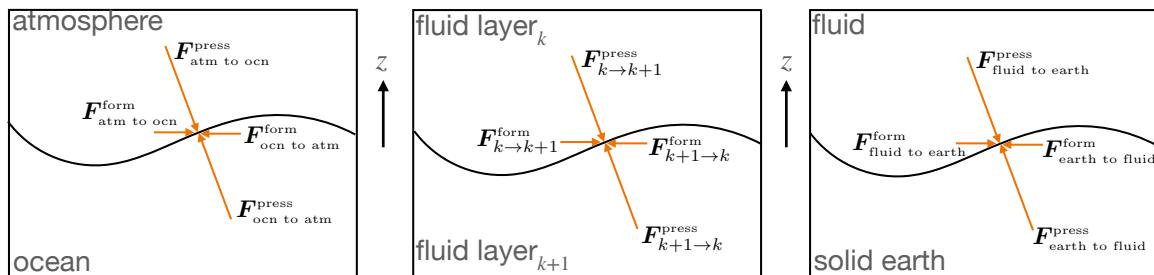


FIGURE 19.1: Illustrating the three interfaces of concern in geophysical fluid mechanics for the discussion of form stresses. Continuity of pressure at the interface, through Newtons' third law, means that the form stress on one side of the interface is equal and opposite to that acting on the other side. Left panel: a curved atmosphere-ocean interface leads to an atmospheric form stress acting on the ocean,  $\mathbf{F}_{\text{atm to ocn}}^{\text{form}}$ , and its equal and opposite oceanic form stress acting on the atmosphere,  $\mathbf{F}_{\text{ocn to atm}}^{\text{form}} = -\mathbf{F}_{\text{atm to ocn}}^{\text{form}}$ . Middle panel: a curved interior ocean interface (e.g., a buoyancy surface) leads to an interfacial form stress acting on the lower layer,  $\mathbf{F}_{k \rightarrow k+1}^{\text{form}}$ , and its equal and opposite interfacial form stress acting on the upper layer,  $\mathbf{F}_{k+1 \rightarrow k}^{\text{form}} = -\mathbf{F}_{k \rightarrow k+1}^{\text{form}}$ . Right panel: a curved fluid solid earth interface leads to a fluid form stress acting on the solid earth,  $\mathbf{F}_{\text{fluid to earth}}^{\text{form}}$ , and its equal and opposite oceanic form stress acting on the fluid,  $\mathbf{F}_{\text{earth to fluid}}^{\text{form}} = -\mathbf{F}_{\text{fluid to earth}}^{\text{form}}$ . The magnitude of the form stresses is a function of the slope of the interface (steeper slopes lead to larger magnitude) and the pressure acting at the interface.

As depicted in Figure 19.1, there are three surfaces or interfaces across which we commonly study form stresses in geophysical fluids.

- **ATMOSPHERE-OCEAN FORM STRESS:** A form stress occurs at the air-sea interface. From the perspective of the ocean, the nonzero sea level pressure from the atmosphere provides a pressure acting on the sloped upper ocean free surface, thus rendering an *atmospheric form stress* acting on the ocean. Through Newton's third law, this form stress is met by the equal in magnitude but oppositely directed *ocean form stress* acting on the atmosphere.

- **INTERIOR FLUID INTERFACIAL FORM STRESS:** A form stress occurs on an internal interface within the fluid, and we study such *interfacial form stresses* in Section 19.3. Although the interface is arbitrary, it is dynamically very interesting to study form stresses acting on buoyancy isosurfaces. The reason is that buoyancy interfaces are directly connected to the geostrophic motion studied in Chapter 25. In particular, in Section 25.7 we study form stresses associated with buoyancy interfaces found in geostrophic flows.
- **FLUID-TOPOGRAPHY FORM STRESS:** A form stress exists at a solid/fluid boundary, at which the ocean or atmosphere impart a pressure force on the solid earth. Through Newton's third law, the pressure force imparted by the fluid on the solid earth is met equally in magnitude but oppositely in direction by a force provided by the solid earth onto the fluid. The horizontal projection of this force from the earth to the fluid is the *topographic form stress* and it is considered in Section 19.2.

### 19.1.1 Concerning the sign of a form stress

As a vector, pressure form stress has a direction and a magnitude, with three examples depicted in Figure 19.1. Even so, keeping track of the direction can be confusing if it is unclear who is the giver of the form stress and who is the receiver. To help in understanding the sign, imagine pushing against a rigid wall: you exert a force on the wall in one direction whereas, through Newton's third law, the wall exerts an equal and opposite force on you. One simply must specify the origin of the force in order to determine its sign. For example, as illustrated in Figure 19.2, is one concerned with the force applied by the ocean bottom pressure onto the earth (liquid ocean is giver and solid earth is receiver), or instead with the force from the earth applied onto the ocean fluid (earth is giver and ocean is receiver)? These forces have equal magnitude but opposite direction. Knowing the direction requires knowing the force giver and/or the force receiver.

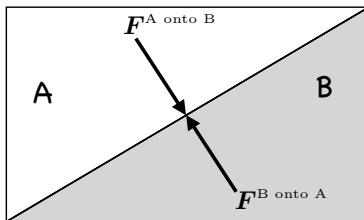


FIGURE 19.2: Contact forces, such as pressure, satisfy Newton's third law. Hence, the contact force at a point imparted by region A onto region B,  $\mathbf{F}^A \text{ onto } B$ , is equal and opposite to the force imparted by region B onto region A so that  $\mathbf{F}^A \text{ onto } B = -\mathbf{F}^B \text{ onto } A$ . In the case where A=fluid (ocean or atmosphere) and B=solid earth, we generally refer to the horizontal portion of  $\mathbf{F}^{\text{earth onto fluid}}$ , per horizontal area, as the *topographic form stress*.

### 19.1.2 Mathematical expression for form stress

To expose the mathematics of form stress, consider a surface,  $\mathcal{S}$ , such as that shown in Figure 19.3. To develop a kinematic decomposition of the pressure force, we assume the surface has no vertical section, with this assumption commonly satisfied by surfaces of interest for geophysical flows.

Assuming the surface has no vertical sections allows us to write the vertical position of a point on the surface as<sup>1</sup>

$$z = \eta(x, y, t). \quad (19.1)$$

<sup>1</sup>See the geometry discussion in Chapter 5 for more on the maths of such surfaces. Also see the discussion of generalized vertical coordinates in Chapters 41 and 42.

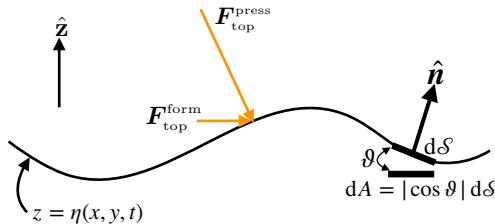


FIGURE 19.3: The pressure force acting on an arbitrary surface is given by  $\mathbf{F}^{\text{press}} = -p \hat{n} dS$ , where  $dS$  is the surface area element. We here depict the pressure acting on the top side of a surface,  $\mathbf{F}_{\text{top}}^{\text{press}}$ . Through Newton's third law, the pressure force vector acting on the top side of the interface is equal and opposite to the pressure force acting on the bottom side:  $\mathbf{F}_{\text{top}}^{\text{press}} = -\mathbf{F}_{\text{b}}^{\text{press}}$ . The horizontal component of this force vector arises from the slope; i.e., the geometric *form* of the surface. We thus refer to the horizontal pressure force per area as the *form stress*,  $\mathbf{F}_{\text{top}}^{\text{form}} = -\mathbf{F}_{\text{b}}^{\text{form}}$ . The area element on the surface,  $dS$ , has a horizontal projection given by  $dA = dx dy = \cos \vartheta dS$ , with the angle assumed to be within the range  $-\pi/2 < \vartheta < \pi/2$  so that the surface is nowhere vertical.

The outward normal pointing away from the top side of the surface is given by

$$\hat{n}_{\text{top}} = \frac{\nabla(z - \eta)}{|\nabla(z - \eta)|} = \frac{\hat{z} - \nabla\eta}{\sqrt{1 + |\nabla\eta|^2}}. \quad (19.2)$$

Multiplying the pressure times the horizontal area element on the surface,  $dS$ , leads to the net pressure force acting at a point on the top side of the surface

$$\mathbf{F}^{\text{press}} = -p \hat{n}_{\text{top}} dS = -p(\hat{z} - \nabla\eta) dA = -p(-\partial_x \eta \hat{x} - \partial_y \eta \hat{y} + \hat{z}) dA. \quad (19.3)$$

In this equation we used the identity<sup>2</sup>

$$dS = |\nabla(z - \eta)| dA = \sqrt{1 + |\nabla\eta|^2} dA, \quad (19.4)$$

with

$$dA = dx dy \quad (19.5)$$

the horizontal projection of the surface area element (see Figure 19.3). We identify the form stress acting on the top side of this interface as

$$\text{pressure form stress acting on top side of interface} \equiv p \nabla\eta. \quad (19.6)$$

The name follows since the stress is determined by the “form” of the surface as measured by its slope,  $\nabla\eta$ . We can thus write the pressure force acting on the top side of the surface as the sum of a vertical pressure force plus a horizontal pressure form stress

$$\mathbf{F}_{\text{top}}^{\text{press}} = \hat{z} [\hat{z} \cdot \mathbf{F}_{\text{top}}^{\text{press}}] + \mathbf{F}_{\text{top}}^{\text{form}} = p(-\hat{z} + \nabla\eta) dA \quad \text{pressure force on top of interface.} \quad (19.7)$$

Newton's third law, as manifested by Cauchy's Stress principle (Section 18.1) says that there is a local mechanical equilibrium of pressure contact forces within a fluid. Additionally, as seen in our discussion of stress on an interface in Section 18.9, this local equilibrium holds for pressure forces acting on interfaces separating two fluids, such as the atmosphere and ocean, as well as a fluid and the solid earth. Thus, the contact pressure force acting on the bottom side of the interface is equal in magnitude but oppositely directed to the contact force acting on the top side

<sup>2</sup>The identity (19.4) follows from trigonometry summarized in Figure 19.3. See further details in the kinematic boundary conditions of Section 14.4 and the analogous dia-surface transport in Section 42.4.

(see Section 18.7.2)

$$\mathbf{F}_{\text{bot}}^{\text{press}} = \hat{\mathbf{z}} [\hat{\mathbf{z}} \cdot \mathbf{F}_{\text{bot}}^{\text{press}}] + \mathbf{F}_{\text{bot}}^{\text{form}} = p (+\hat{\mathbf{z}} - \nabla \eta) \, dA \quad \text{pressure force on bottom of interface. (19.8)}$$

### 19.1.3 Comments

Consider a container filled with water at rest. The horizontal pressure forces acting on the container sides are pressure form stresses between the water and the container. As discussed in Section 18.4, without motion we know that the form stresses balance over the whole of the fluid-container boundary, whereas horizontal motion occurs if the form stresses are out of balance. Quite generally, when concerned with fluid motion, we are interested in processes that lead to unbalanced form stresses. For example, when studying bottom topographic form stresses in the ocean, the bulk of the form stress acts to support the ocean water within the ocean basin. The dynamically active portion of the topographic form stress, associated with the fluid motion, is a small residual of the total form stress. Careful analysis is required to diagnose dynamically relevant patterns, with [Molemaker et al. \(2015\)](#) and [Gula et al. \(2015\)](#) presenting one method, and we explore their method as part of Exercise 35.11.

Notably, form stress, particularly interfacial form stress, can appear mysterious in some presentations. Part of the reason is that it sometimes appears seemingly without prior motivation as part of mathematical manipulations of the momentum equation. We illustrate these manipulations in Sections 19.2, 19.3, and 19.5, yet aim to offer sufficient physical motivation to help guide the maths. Another reason for the mystery is that the signs ascribed to form stress are often not clearly specified, with such ambiguities motivating the somewhat pedantic discussion in Section 19.1.1.

## 19.2 Form stresses on the ocean boundaries

In this section we focus on form stress arising from the shape of the solid earth interface with the atmosphere and ocean; i.e., the *fluid-topographic form stress*. As we are normally interested in the form stress applied to the fluid, we focus on the *topographic form stress*. We also encounter the form stress associated with undulations in the ocean free surface and the atmospheric pressure at that interface, with the *atmospheric form stress* the stress imparted to the ocean from the atmosphere.

### 19.2.1 Zonally symmetric ridge

In Figure 19.4 we depict an idealized ridge with an example oceanic pressure field to illustrate the nature of topographic form stress acting on a fluid. Rather than assuming exact hydrostatic equilibrium as in Figure 18.5, with zero horizontal pressure gradients, we here consider pressure to be higher to the west of the ridge than to the east. Since the ridge is assumed to be symmetric in the zonal direction, we conclude that the topographic form stress, which acts just at the fluid-solid interface, is higher on the west side of the ridge than on the east. In turn, the net topographic form stress acting on the fluid is to the west, whereas the net oceanic form stress acting on the solid earth is to the east. We encounter this situation in Section 19.5.11 when studying the force balances for steady circulation in a zonally periodic channel.

### 19.2.2 Form stress transfer between the fluid and its boundaries

We now illustrate how topographic form stress commonly appears in the study of momentum balances acting on a fluid. For definiteness, consider a column of ocean fluid extending from

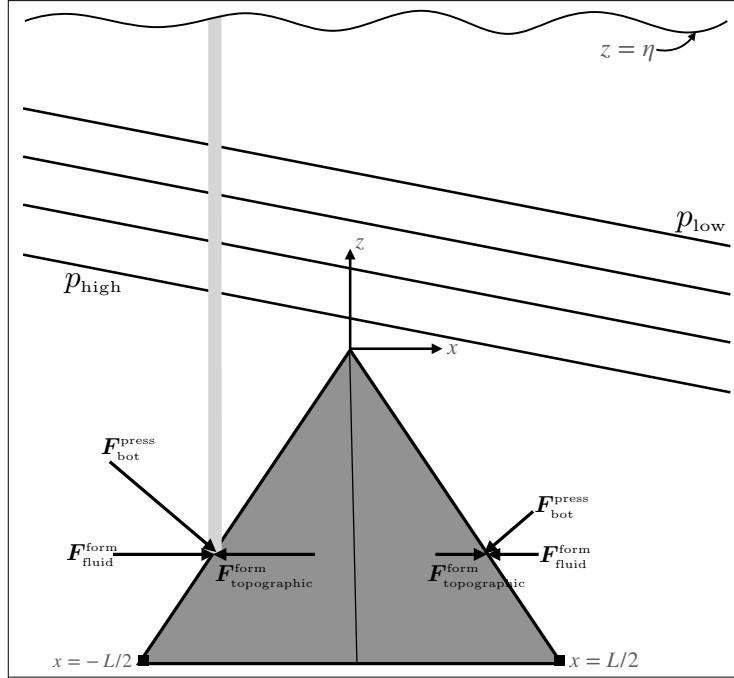


FIGURE 19.4: Depicting contact forces acting at a fluid-solid interface. The topographic form stress acts on the fluid and the equal in magnitude but oppositely directed fluid form stress acts on the solid earth. In this illustration the topography is assumed to be a ridge in the shape of an equilateral triangle. We also assume there is higher pressure to the west of the ridge than to the east as per the zonal balance discussed in Figure 19.8 for a Southern Ocean ridge. Hence, the topographic form stress has a larger magnitude on the western side of the ridge than on the eastern side. When integrated over the full ridge, there will be a net westward topographic form stress acting on the fluid and a net eastward fluid form stress acting on the solid earth. If the ridge was free to move, it would move to the east. The thin gray column extends from the solid earth bottom to the ocean free surface. As this column sits on the western side of the ridge, topographic form stress provides a westward acceleration at the column bottom. The net acceleration of the column is determined by integrating the contact forces around the column boundary and body forces throughout the column interior. We study the axial angular momentum budget for a fluid column in Section 19.5, with form stresses appearing in that budget.

the bottom at  $z = \eta_b(x, y)$  to the free surface at  $z = \eta(x, y, t)$ , and focus on the zonal force balance such as depicted in Figure 19.4. In computing the acceleration acting on this column at a particular horizontal position, we need to determine the depth integrated zonal pressure gradient

$$\text{depth integrated zonal pressure gradient} = - \int_{\eta_b}^{\eta} \frac{\partial p}{\partial x} dz. \quad (19.9)$$

We expose the contact force version of the pressure force by making use of Leibniz's Rule (Section 14.5) to write

$$-\int_{\eta_b}^{\eta} \frac{\partial p}{\partial x} dz = \underbrace{-\frac{\partial}{\partial x} \int_{\eta_b}^{\eta} p dz}_{\text{zonal deriv depth integrated pressure}} + \underbrace{\frac{\partial \eta}{\partial x} p_a}_{\text{atmospheric form stress}} - \underbrace{\frac{\partial \eta_b}{\partial x} p_b}_{\text{topographic form stress}}, \quad (19.10)$$

where  $p_a$  is the pressure applied to the ocean at its surface,  $z = \eta$ , and  $p_b$  is the pressure at the ocean bottom,  $z = \eta_b$ . The decomposition identifies the following three pressure contributions to the pressure force acting on the fluid column.

- **ZONAL DERIVATIVE OF THE COLUMN INTEGRATED PRESSURE:** The first term arises from the zonal derivative of pressure across the vertical sides of the column

$$\text{zonal derivative of layer integrated pressure} = -\frac{\partial}{\partial x} \int_{\eta_b}^{\eta} p \, dz. \quad (19.11)$$

This term leads to a net eastward acceleration if the depth integrated pressure is higher to the west than the east.

- **ATMOSPHERIC FORM STRESS AT THE FREE SURFACE:** In the presence of a sloping free surface interface,  $\partial\eta/\partial x \neq 0$ , the atmospheric pressure,  $p_a$ , imparts an atmospheric form stress onto the ocean

$$\text{zonal atmospheric form stress acting on ocean} = \frac{\partial\eta}{\partial x} p_a. \quad (19.12)$$

For example, if the free surface slopes up to the east,  $\partial\eta/\partial x > 0$ , then the atmosphere provides a positive (eastward) zonal form stress onto the ocean. In turn, through Newton's third law, the ocean provides a westward zonal form stress to the atmosphere.

- **TOPOGRAPHIC FORM STRESS ON OCEAN:** The bottom pressure,  $p_b$ , present at  $z = \eta_b$  imparts an oceanic form stress to the solid earth

$$\text{zonal oceanic form stress acting on solid earth} = \frac{\partial\eta_b}{\partial x} p_b. \quad (19.13)$$

In turn, through Newton's third law, the topographic form stress acting on the ocean is equal in magnitude but oppositely directed

$$\text{zonal topographic form stress acting on ocean} = -\frac{\partial\eta_b}{\partial x} p_b. \quad (19.14)$$

For example, if the bottom rises to the east, so that  $\partial\eta_b/\partial x > 0$ , then the oceanic form stress acting on the solid earth is eastward whereas the topographic form stress acting on the ocean is westward. As a check, we verify that the signs of these form stresses are consistent with those in Figure 19.4.

### 19.2.3 Decomposing topographic form stress

Assuming the fluid maintains an approximate hydrostatic balance, and focusing on the oceanic case, allows us to decompose the bottom pressure into the following terms

$$p_b = p_a + g \int_{\eta_b}^{\eta} \rho \, dz \quad (19.15a)$$

$$= \underbrace{g \rho_0 [\eta + p_a / (g \rho_0)]}_{\text{external}} - \underbrace{g \rho_0 \eta_b}_{\text{topog}} + \underbrace{g \int_{\eta_b}^{\eta} (\rho - \rho_0) \, dz}_{\text{internal}} \quad (19.15b)$$

$$\equiv p_{\text{ext}} + p_{\text{topog}} + p_{\text{int}}. \quad (19.15c)$$

We refer to the contribution from applied surface pressure plus surface height undulations as *external*, whereas those arising from density deviations relative to a constant reference density are termed *internal*. There is a final contribution from bottom topography itself. Multiplying this pressure by the bottom topography slope renders an expression for the various contributions to

topographic form stress

$$-p_b \nabla \eta_b = -p_{\text{ext}} \nabla \eta_b - p_{\text{topog}} \nabla \eta_b - p_{\text{int}} \nabla \eta_b. \quad (19.16)$$

The topographic term is static whereas the other two terms are time dependent. External contributions arise from undulations in the free surface as well as the applied pressure. This contribution fluctuates due to motions occurring on the relatively rapid time scales associated with external gravity waves or atmospheric pressure fluctuations such as through synoptic weather patterns. Internal contributions arise from the relatively slow internal movements of density surfaces, such as from internal gravity waves or even slower motions due to advection and diffusion. The study from [McCabe et al. \(2006\)](#) pursue this decomposition of the topographic form stress as part of their analysis of flow around a headland.

## 19.3 Interfacial form stress

In this section we focus on the form stress acting at an interface within the fluid itself, which is known as the *interfacial form stress*. As part of this discussion we expose some of the common manipulations found when considering finite volume integrated momentum budgets, whereby we decompose the horizontal pressure gradient acceleration acting on an infinitesimal column of fluid within the layer, as depicted in Figure 19.5. These manipulations are analogous to those considered in Section 19.2 for the topographic and atmospheric form stresses.

### 19.3.1 Interfacial form stresses transferred between layers

When studying the momentum of a column of fluid within a chosen layer, we need to compute the depth integrated zonal pressure gradient over a layer at a particular horizontal point

$$\text{layer integrated zonal pressure gradient} = - \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} \frac{\partial p}{\partial x} dz, \quad (19.17)$$

where  $z = \eta_{k-1/2}(x, y, t)$  is the vertical position for the interface at the top of the fluid layer and  $z = \eta_{k+1/2}(x, y, t)$  is the vertical position for the bottom interface. If the layer integrated pressure gradient points downgradient to the east, then pressure accelerates the column to the east.

Although the depth integrated pressure gradient expression (19.17) is straightforward to understand, we also find it useful to consider the complementary perspective by studying the contact force version of the pressure acceleration. Proceeding as in Section 19.2 for topographic and atmospheric form stresses, we make use of Leibniz' Rule for a fluid layer

$$-\int_{\eta_{k+1/2}}^{\eta_{k-1/2}} \frac{\partial p}{\partial x} dz = \underbrace{-\frac{\partial}{\partial x} \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} p dz}_{\text{zonal deriv layer integrated pressure}} + \underbrace{\frac{\partial \eta_{k-1/2}}{\partial x} p_{k-1/2}}_{\text{IFS at } k-1/2 \text{ interface}} - \underbrace{\frac{\partial \eta_{k+1/2}}{\partial x} p_{k+1/2}}_{\text{IFS at } k+1/2 \text{ interface}}, \quad (19.18)$$

where we introduced the pressures acting at a point on the interfaces

$$p_{k-1/2} = p(x, y, z = \eta_{k-1/2}, t) \quad \text{and} \quad p_{k+1/2} = p(x, y, z = \eta_{k+1/2}, t). \quad (19.19)$$

The decomposition identifies the following three pressure contributions, analogous to the decomposition in Section 19.2 for the topographic and atmospheric form stresses.

- **ZONAL DERIVATIVE OF THE COLUMN INTEGRATED PRESSURE:** The first term arises from

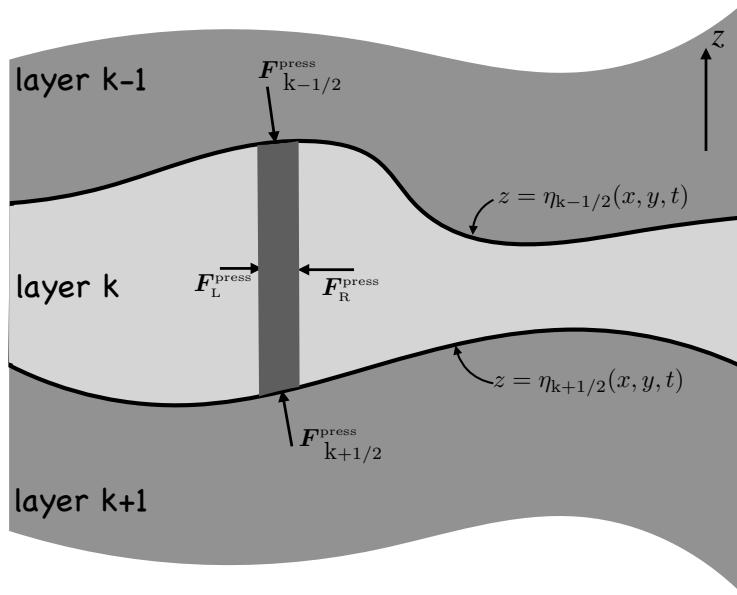


FIGURE 19.5: A schematic of the contact pressure force per area acting on the boundaries of a vertical column region within a fluid layer. The horizontal cross-sectional area of the column is depth independent. The interface at the lower boundary is at the vertical position  $z = \eta_{k+1/2}$ , and the upper interface is at  $z = \eta_{k-1/2}$ . In accordance with Newton's third law, pressures are continuous across each of the  $\eta_{k\pm 1/2}$  layer interfaces so that the pressure forces are equal in magnitude yet oppositely directed on the opposite sides to the interfaces. The boundaries of the dark gray columnar region feel a contact pressure force acting inward. The left side of the column experiences a pressure  $p_L$ ; the right side experiences  $p_R$ ; the upper interface has a pressure  $p_{k-1/2}$  acting between the layer  $k-1$  and layer  $k$ , and the lower interface has a pressure  $p_{k+1/2}$  acting between the layer  $k+1$  and layer  $k$ . The interfacial form stress (IFS) is the name given to the horizontal pressure stress acting on the upper and lower layer interfaces. Through Newton's third law, the IFS imparted to layer  $k$  at the  $z = \eta_{k-1/2}$  interface is equal and opposite to the IFS imparted to layer  $k-1$  at this same interface. The same holds for the IFS at the  $k+1/2$  interface. It is common to define the layers according to buoyancy (see Section 25.7) given its direct connection to pressure and dynamics. Even so, the ideas of pressure contact forces are generic and thus hold for layers defined arbitrarily.

the zonal derivative of pressure across the vertical sides of the column within the layer

$$\text{zonal derivative of layer integrated pressure} = -\frac{\partial}{\partial x} \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} p \, dz. \quad (19.20)$$

- **INTERFACIAL FORM STRESS AT UPPER INTERFACE:** The pressure at the  $z = \eta_{k-1/2}$  interface is given by  $p_{k-1/2}$ . In the presence of a sloping interface,  $\partial\eta_{k-1/2}/\partial x \neq 0$ , this pressure imparts the following interfacial form stress (IFS) to layer-k:

$$\text{IFS on layer-}k \text{ from the } \eta_{k-1/2} \text{ interface} = \frac{\partial\eta_{k-1/2}}{\partial x} p_{k-1/2}. \quad (19.21)$$

For example, if the upper layer interface slopes up to the east,  $\partial\eta_{k-1/2}/\partial x > 0$ , then the interfacial form stress provides a positive (eastward) zonal force to layer-k. In turn, through Newton's third law, the layer above, labelled  $k-1$ , feels an interfacial form stress accelerating this layer to the west.

- **INTERFACIAL FORM STRESS AT LOWER INTERFACE:** The pressure,  $p_{k+1/2}$  present at the

$z = \eta_{k+1/2}$  interface imparts an interfacial form stress to layer-k given by

$$\text{IFS on layer-}k \text{ from } \eta_{k+1/2} \text{ interface} = -\frac{\partial \eta_{k+1/2}}{\partial x} p_{k+1/2}. \quad (19.22)$$

For example, if the layer slopes down to the east,  $\partial \eta_{k+1/2} / \partial x < 0$ , then the interfacial form stress accelerates layer-k to the east. In turn, through Newton's third law, the interfacial form stress acts to accelerate the layer below, labelled k + 1, to the west.

Now apply the above to a column of ocean fluid, and extending the integration to include the full ocean column from the free upper surface to the solid earth bottom. Note that all the intermediate interfacial form stresses vanish in the depth integral, with this cancellation a result of Newton's third law. Hence, accumulation of the interfacial form stresses throughout the ocean column leaves only the interfacial form stress at the top and at the bottom, with those boundary form stresses arising from mechanical interactions with the atmosphere and solid earth as discussed in Section 19.2. This result was already encountered in a more general context of contact forces in Section 18.1. It will also be found in our analysis of the depth integrated axial angular momentum budget in Section 19.5.

### 19.3.2 Zonally integrated interfacial form stress

Besides studying the force acting on a column at a particular horizontal position, it is interesting to study the net zonal force acting on the layer. For pressure, we thus need to consider the zonal integral of the layer integrated zonal pressure gradient

$$-\int \left[ \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} \frac{\partial p}{\partial x} dz \right] dx = \int \left[ -\frac{\partial}{\partial x} \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} p dz + \frac{\partial \eta_{k-1/2}}{\partial x} p_{k-1/2} - \frac{\partial \eta_{k+1/2}}{\partial x} p_{k+1/2} \right] dx. \quad (19.23)$$

If the domain is zonally periodic or is bounded by sloping shorelines (see Figure 19.7 discussed in Section 19.5.7), then the first term vanishes so that the zonally integrated pressure acting on the layer arises just from the interfacial form stresses

$$-\int \left[ \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} \frac{\partial p}{\partial x} dz \right] dx = \int \left[ \frac{\partial \eta_{k-1/2}}{\partial x} p_{k-1/2} - \frac{\partial \eta_{k+1/2}}{\partial x} p_{k+1/2} \right] dx. \quad (19.24)$$

This zonal integral is only affected by zonal anomalies for the layer vertical positions and pressures

$$-\int \left[ \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} \frac{\partial p}{\partial x} dz \right] dx = \int \left[ \frac{\partial \eta'_{k-1/2}}{\partial x} p'_{k-1/2} - \frac{\partial \eta'_{k+1/2}}{\partial x} p'_{k+1/2} \right] dx \quad (19.25a)$$

$$= \int \left[ -\eta'_{k-1/2} \frac{\partial p'_{k-1/2}}{\partial x} + \eta'_{k+1/2} \frac{\partial p'_{k+1/2}}{\partial x} \right] dx, \quad (19.25b)$$

where primes denote deviations from the zonal mean. We spend some time in Section 19.5.10 to prove that it is only the anomalies that matter for the zonally periodic channel, or for domains with sloping shorelines. Furthermore, note that for the second equality we introduced the alternative expressions for the form stresses afforded by zonal periodicity or zonal sloped shorelines. We offer some cautionary remarks in Section 19.5.9 regarding this second equality.

### 19.3.3 Comments

Interfacial form stress acts on any arbitrary surface drawn in a fluid. Interfaces defined by buoyancy surfaces make the connection between the general concepts presented here to geostrophic mechanics, and they do so given the connection between buoyancy slopes and thermal wind (Section 25.4.4). Most studies of interfacial form stress are thus concerned with isopycnal interfacial form stress, with a discussion given in Section 25.7.

## 19.4 Evolution of depth integrated horizontal momentum

In this section we develop the evolution equation for the depth integrated horizontal momentum per volume in a column of ocean fluid

$$\mathbf{U}^\rho = \int_{\eta_b}^{\eta} \rho \mathbf{u} dz, \quad (19.26)$$

extending from the ocean bottom at  $z = \eta_b(x, y)$  to the ocean surface at  $z = \eta(x, y, t)$ . The evolution equation exposes how form stresses acting at the ocean surface and ocean bottom contribute to the column force balance. A study of the depth integrated momentum equation is commonly considered when the ocean fluid maintains an approximate hydrostatic balance, so that we assume such in this section. We discussed the exact hydrostatic fluid in Section 17.3, which is realized by a static fluid in a gravity field. The approximate hydrostatic fluid, as studied in Sections 23.2 and 22.2, is more general since it applies to a moving fluid whose vertical momentum equation is well approximated by the hydrostatic balance.

### 19.4.1 Flux-form horizontal momentum equation

Our starting point is the flux-form horizontal momentum equation (18.63) as specialized to a simple geopotential,  $\Phi = g z$ ,

$$\frac{\partial(\rho \mathbf{u})}{\partial t} + \nabla \cdot [\rho \mathbf{v} \otimes \mathbf{u}] + f \hat{\mathbf{z}} \times (\rho \mathbf{u}) = -\nabla_z p + \rho \mathbf{F}. \quad (19.27)$$

In this equation,  $\rho \mathbf{F}$  is the horizontal friction vector, and the outer product provides components to the kinetic stress (Section 18.5)

$$\rho [\mathbf{v} \otimes \mathbf{u}]_{mi} = \rho v_m u_i = -\mathbb{T}_{mi}^{\text{kinetic}}, \quad (19.28)$$

with  $m = 1, 2, 3$  (for the full velocity vector,  $\mathbf{v}$ ) extending over the full range whereas  $i = 1, 2$  (for the horizontal velocity vector,  $\mathbf{u}$ ) extending just over the horizontal range.

### 19.4.2 Leibniz's rule for the inertial and Coriolis accelerations

Leibniz's rule (Section 15.3.4) renders the following expressions for the depth integrated inertial acceleration and Coriolis acceleration

$$\int_{\eta_b}^{\eta} \frac{\partial(\rho \mathbf{u})}{\partial t} dz = \partial_t \mathbf{U}^\rho - [\rho \mathbf{u} \partial_t \eta]_{z=\eta} \quad (19.29a)$$

$$\int_{\eta_b}^{\eta} \frac{\partial(w \rho \mathbf{u})}{\partial z} dz = [w \rho \mathbf{u}]_{z=\eta} - [w \rho \mathbf{u}]_{z=\eta_b} \quad (19.29b)$$

$$\int_{\eta_b}^{\eta} \nabla_z \cdot [\rho \mathbf{u} \otimes \mathbf{u}] dz = \nabla_z \cdot \left[ \int_{\eta_b}^{\eta} \rho \mathbf{u} \otimes \mathbf{u} dz \right] - [\mathbf{u} \cdot \nabla \eta (\rho \mathbf{u})]_{z=\eta} + [\mathbf{u} \cdot \nabla \eta_b (\rho \mathbf{u})]_{z=\eta_b} \quad (19.29c)$$

$$\int_{\eta_b}^{\eta} f \hat{\mathbf{z}} \times (\rho \mathbf{u}) dz = f \hat{\mathbf{z}} \times \mathbf{U}^\rho. \quad (19.29d)$$

Use of the surface and bottom kinematic boundary conditions from Section 14.4

$$\partial_t \eta + \mathbf{u} \cdot \nabla \eta = w + \rho^{-1} Q_m \quad \text{for } z = \eta \quad (19.30a)$$

$$\mathbf{u} \cdot \nabla \eta_b = w \quad \text{for } z = \eta_b \quad (19.30b)$$

leads to the depth integrated inertial and Coriolis accelerations

$$\begin{aligned} & \int_{\eta_b}^{\eta} [\partial_t(\rho \mathbf{u}) + \nabla \cdot [\mathbf{v} \otimes (\rho \mathbf{u})] + f \hat{\mathbf{z}} \times \rho \mathbf{u}] dz \\ &= (\partial_t + f \hat{\mathbf{z}} \times) \mathbf{U}^\rho - \mathbf{u}(\eta) Q_m - \nabla_z \cdot \int_{\eta_b}^{\eta} \mathbb{T}_{\text{hor}}^{\text{kinetic}} dz, \end{aligned} \quad (19.31)$$

where we introduced the horizontal kinetic stress tensor

$$\mathbb{T}_{\text{hor}}^{\text{kinetic}} = -\rho \mathbf{u} \otimes \mathbf{u}. \quad (19.32)$$

### 19.4.3 External and internal decomposition of the kinetic stress

For some applications it can be useful to introduce the density weighted depth averaged horizontal velocity

$$\bar{\mathbf{u}} = \frac{\int_{\eta_b}^{\eta} \rho \mathbf{u} dz}{\int_{\eta_b}^{\eta} \rho dz} = \frac{\mathbf{U}^\rho}{(p_b - p_a)/g}, \quad (19.33)$$

where  $p_b$  is the hydrostatic pressure at the ocean bottom, and  $p_a$  is the pressure applied to the ocean surface. The depth averaged velocity is referred to as the *external velocity*, whereas the deviation from the depth average

$$\mathbf{u}' = \mathbf{u} - \bar{\mathbf{u}}, \quad (19.34)$$

is referred to it as the *internal velocity*.<sup>3</sup> It follows by its definition that the internal velocity has a zero density weighted vertical integral

$$\int_{\eta_b}^{\eta} \rho \mathbf{u}' dz = \int_{\eta_b}^{\eta} \rho (\mathbf{u} - \bar{\mathbf{u}}) dz = 0. \quad (19.35)$$

---

<sup>3</sup>It is also common in the oceanography literature to refer to  $\mathbf{u}'$  as the *baroclinic velocity* and  $\bar{\mathbf{u}}$  as the *barotropic velocity*. We avoid that nomenclature since we prefer to use baroclinic and barotropic in reference to vorticity mechanics in Section 35.5.

Consequently, by making use of  $\mathbf{u} = \bar{\mathbf{u}} + \mathbf{u}'$  we find the depth integrated kinetic stress

$$\int_{\eta_b}^{\eta} \mathbb{T}_{\text{hor}}^{\text{kinetic}} dz = -g^{-1} (p_b - p_a) [\bar{\mathbf{u}} \otimes \bar{\mathbf{u}} + \bar{\mathbf{u}}' \otimes \bar{\mathbf{u}}']. \quad (19.36)$$

Note that absence of cross-terms (i.e., no internal-external correlation terms) appearing in the depth integrated stress (19.36). In this manner we have separated the contributions from kinetic stresses due to depth averaged horizontal velocities from those arising from depth-dependent horizontal velocities.

#### 19.4.4 Depth integrated horizontal pressure gradient

We find it useful to decompose the depth integrated horizontal pressure gradient by writing

$$\int_{\eta_b}^{\eta} p dz = \int_{\eta_b}^{\eta} [d(pz) - z dp] = p_a \eta - p_b \eta_b + \mathcal{P}, \quad (19.37)$$

where we used the hydrostatic balance for a vertical fluid column to write<sup>4</sup>  $dp = -g \rho dz$ , and introduced the potential energy per horizontal area of a fluid column

$$\mathcal{P} = \int_{\eta_b}^{\eta} g \rho z dz. \quad (19.38)$$

These results then lead to the depth integrated horizontal pressure gradient

$$\int_{\eta_b}^{\eta} \nabla_z p dz = \nabla_z P - p_a \nabla_z \eta + p_b \nabla_z \eta_b \quad (19.39a)$$

$$= \nabla_z [p_a \eta - p_b \eta_b + \mathcal{P}] - p_a \nabla_z \eta + p_b \nabla_z \eta_b \quad (19.39b)$$

$$= \nabla_z \mathcal{P} + \eta \nabla_z p_a - \eta_b \nabla_z p_b, \quad (19.39c)$$

where we introduced the depth integrated pressure field

$$P = \int_{\eta_b}^{\eta} p dz. \quad (19.40)$$

Equation (19.39a) exposes contributions from surface and bottom form stresses,  $-p_a \nabla_z \eta + p_b \nabla_z \eta_b$ , along with the horizontal gradient of the depth integrated pressure. As a complement, equation (19.39c) exposes the *dual form stress*,  $\eta \nabla_z p_a - \eta_b \nabla_z p_b$ , plus the gradient of the potential energy. The role of these accelerations is further studied for the axial angular momentum budget in Section 19.5, and then within the column vorticity balance in Section 35.10.

#### 19.4.5 Depth integrated momentum equation

Bringing the pieces together leads to the depth integrated horizontal momentum equation for an approximate hydrostatic fluid

$$(\partial_t + f \hat{\mathbf{z}} \times) \mathbf{U}^\rho = \mathbf{u}(\eta) Q_m - \eta \nabla_z p_a + \eta_b \nabla_z p_b - \nabla_z \mathcal{P} + \nabla_z \cdot \left[ \int_{\eta_b}^{\eta} \mathbb{T}_{\text{hor}}^{\text{kinetic}} dz \right] + \int_{\eta_b}^{\eta} \rho \mathbf{F} dz. \quad (19.41)$$

---

<sup>4</sup>Specializing to a vertical column allows for the transformation,  $dp = -g \rho dz$ , between pressure and geopotential in the approximate hydrostatic fluid of Section 22.2. When also allowing for horizontal deviations then  $dp = \nabla p \cdot d\mathbf{x}$ .

For many applications we focus on the vertical divergence of horizontal frictional stress plus a term arising from horizontal strains, in which case

$$\int_{\eta_b}^{\eta} \rho \mathbf{F} dz = \int_{\eta_b}^{\eta} (\rho \mathbf{F}_{\text{horz}} + \partial_z \boldsymbol{\tau}) dz = \mathbf{D} + \boldsymbol{\tau}^{\eta} - \boldsymbol{\tau}^{\eta_b} \equiv \mathbf{D} + \Delta \boldsymbol{\tau}, \quad (19.42)$$

where  $\boldsymbol{\tau}^{\eta}$  is the horizontal stress at the surface,  $\boldsymbol{\tau}^{\eta_b}$  is the horizontal stress at the bottom, and

$$\mathbf{D} = \int_{\eta_b}^{\eta} \rho \mathbf{F}_{\text{horz}} dz \quad (19.43)$$

is the depth integrated friction arising from horizontal stresses within the fluid interior. In this case the horizontal momentum equation (19.41) takes on the form

$$(\partial_t + f \hat{z} \times) \mathbf{U}^{\rho} = \mathbf{u}(\eta) Q_m - \eta \nabla_z p_a + \eta_b \nabla_z p_b - \nabla_z \mathcal{P} + \mathbf{A} + \mathbf{D} + \Delta \boldsymbol{\tau}. \quad (19.44)$$

where we introduced the shorthand for the nonlinear kinetic stress term

$$\mathbf{A} \equiv \nabla_z \cdot \left[ \int_{\eta_b}^{\eta} \mathbb{T}_{\text{hor}}^{\text{kinetic}} dz \right] = -\nabla_z \cdot \left[ \int_{\eta_b}^{\eta} \rho \mathbf{u} \otimes \mathbf{u} dz \right]. \quad (19.45)$$

### 19.4.6 Balances when $\nabla \cdot \mathbf{U}^{\rho} = 0$

There are many occasions in which the depth integrated flow is close to non-divergent,  $\nabla \cdot \mathbf{U}^{\rho} = 0$ . Such occurs particularly at the large scale and for cases where we neglect the mass transport across the ocean surface,  $Q_m = 0$ . Following the kinematics from Section 16.4, we introduce a *transport streamfunction* so that

$$\mathbf{U}^{\rho} = \hat{z} \times \nabla \Psi, \quad (19.46)$$

with  $\Psi$  having dimensions of mass per time. Use of the transport streamfunction brings the Coriolis contribution to the form

$$f \hat{z} \times \mathbf{U}^{\rho} = f \hat{z} \times (\hat{z} \times \nabla \Psi) = -f \nabla \Psi, \quad (19.47)$$

so that the momentum equation (19.44) becomes

$$\partial_t \mathbf{U}^{\rho} = f \nabla_z \Psi - \eta \nabla_z p_a + \eta_b \nabla_z p_b - \nabla_z \mathcal{P} + \mathbf{A} + \mathbf{D} + \Delta \boldsymbol{\tau} \quad (19.48a)$$

$$= f \nabla_z \Psi + p_a \nabla_z \eta - p_b \nabla_z \eta_b - \nabla_z P + \mathbf{A} + \mathbf{D} + \Delta \boldsymbol{\tau}. \quad (19.48b)$$

#### Zonal integral of the depth integrated zonal momentum equation

For many purposes, we wish reduce the number of processes contributing to the momentum equations (19.48a) and (19.48b) by forming horizontal integrals along selected contours. For example, a zonal integral of the zonal equation, computed around a periodic domain, eliminates the Coriolis term as well as  $\partial_x P$  and  $\partial_x \mathcal{P}$ , in which case

$$\partial_t \oint U^{\rho} dx = \oint [-\eta \partial_x p_a + \eta_b \partial_x p_b + \hat{x} \cdot (\mathbf{A} + \mathbf{D} + \Delta \boldsymbol{\tau})] dx \quad (19.49a)$$

$$= \oint [p_a \partial_x \eta - p_b \partial_x \eta_b + \hat{x} \cdot (\mathbf{A} + \mathbf{D} + \Delta \boldsymbol{\tau})] dx. \quad (19.49b)$$

As discussed in Section 19.5, this equation, or its analog for the axial angular momentum, provides a valuable framework for studies of the Southern Ocean momentum balances.

### Steady balance

As another example, consider a steady balance in which

$$-f \nabla_z \Psi = p_a \nabla_z \eta - p_b \nabla_z \eta_b - \nabla_z P + \mathbf{A} + \mathbf{D} + \Delta\boldsymbol{\tau}. \quad (19.50)$$

Note that by projecting into the horizontal direction perpendicular to the bottom topography

$$\hat{\mathbf{n}}_b = \frac{\nabla \eta_b}{|\nabla \eta_b|} \quad (19.51)$$

we eliminate the  $p_b \nabla_z \eta_b$  term to have

$$-f \hat{\mathbf{n}}_b \cdot \nabla_z \Psi = \hat{\mathbf{n}}_b \cdot (p_a \nabla_z \eta - \nabla_z P + \mathbf{A} + \mathbf{D} + \Delta\boldsymbol{\tau}). \quad (19.52)$$

## 19.5 Axial angular momentum budget for an ocean domain

We here develop the column integrated budget for axial angular momentum for a region of the ocean, such as shown in Figure 19.6. We then further specialize the budget by zonally integrating. The analysis shares features with the depth integrated linear momentum balance developed in Section 19.4. Similarity arises largely due to the connection between the axial angular momentum and the zonal linear momentum, with details provided in our study of geophysical particle dynamics in Sections 10.7 and 10.8. We choose to study axial angular momentum since it has a slightly simpler budget (equation (19.53) discussed below) than corresponding budget equation (19.44) for zonal linear momentum. The simpler budget follows since axial angular momentum is directly connected to the axial symmetry of the rotating spherical planet (Sections 10.7 and 17.4).

To add a bit more generality to the analysis, we make use of spherical coordinates, though doing so offers only a modest degree of extra details beyond Cartesian coordinates. Although here focused on the ocean, many of the concepts and methods are directly relevant to a study of atmospheric axial angular momentum as introduced in Section 17.4 and lucidly discussed in Section 10.3 of [Holton \(1992\)](#).

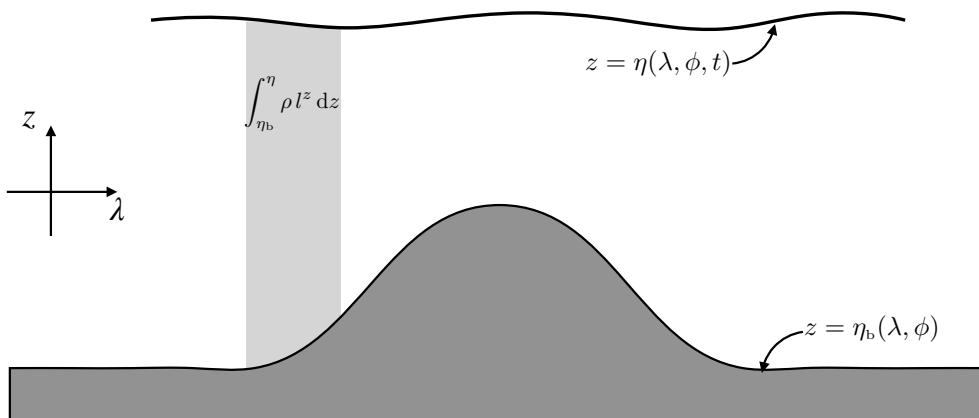


FIGURE 19.6: Schematic of the axial angular momentum for a fluid column, here depicted moving in an ocean with a topographic bump. In Section 19.5 we develop the budget for the depth and zonal integrated axial angular momentum in the ocean, where we see that the axial angular momentum is affected by a variety of boundary processes as well as interior transports and pressures.

### 19.5.1 Anticipating the budget

Before diving into the mathematical formulation, let us use some of the understanding gleaned from earlier sections of this chapter to anticipate the basic results. Doing so offers us a framework to guide the maths, and to double check that the maths indeed renders a physically sensible budget.

For this purpose, consider a column of fluid such as shown in Figure 19.6. The forces acting on that column arise from contact forces (pressure, kinetic, and frictional stresses) acting on the boundary (sides, top, and bottom), and body forces acting throughout the column (from effective gravity and Coriolis). There are further avenues for momentum to be transported across the ocean surface as part of the mass transported by rain, evaporation, and rivers. Each of these forces contribute a torque to the fluid column computed relative to the earth's rotational axis, thus modifying the axial angular momentum of the fluid column. In the following development, we mathematically express the variety of forces and corresponding torques, thus building up the axial angular momentum budget.

### 19.5.2 Axial angular momentum

The axial angular momentum budget for a fluid element follows that developed in Section 17.4, here written with zonal friction

$$\rho \frac{Dl^z}{Dt} = -\frac{\partial p}{\partial \lambda} + r_{\perp} \rho F^{\lambda}, \quad (19.53)$$

where

$$l^z = r_{\perp} (u + r_{\perp} \Omega) \quad (19.54)$$

is the axial angular momentum per unit mass, and

$$r_{\perp} = r \cos \phi \quad (19.55)$$

is the distance to the polar rotation axis (the moment arm). Use of the Eulerian form of mass conservation (equation (14.6)) leads to the Eulerian flux-form budget

$$\frac{\partial(\rho l^z)}{\partial t} + \nabla \cdot (\rho \mathbf{v} l^z) = -\frac{\partial p}{\partial \lambda} + r_{\perp} \rho F^{\lambda}, \quad (19.56)$$

with  $l^z \rho dz$  the angular momentum per unit horizontal area. We use this form for the budget to develop the depth integrated axial angular momentum budget.

### 19.5.3 Depth integrated budget

Vertically integrating equation (19.56) over a column of ocean fluid renders a budget for the column-integrated axial angular momentum. As in Section 19.4.2, we here make use of Leibniz's Rule to reach the following identities that expose boundary contributions

$$\int_{\eta_b}^{\eta} \frac{\partial(\rho l^z)}{\partial t} dz = \frac{\partial}{\partial t} \left[ \int_{\eta_b}^{\eta} \rho l^z dz \right] - \left[ \rho l^z \frac{\partial \eta}{\partial t} \right]_{z=\eta} \quad (19.57a)$$

$$\int_{\eta_b}^{\eta} \nabla_z \cdot (\rho \mathbf{u} l^z) dz = \nabla_z \cdot \left[ \int_{\eta_b}^{\eta} \rho \mathbf{u} l^z dz \right] - [\rho l^z \mathbf{u} \cdot \nabla \eta]_{z=\eta} + [\rho l^z \mathbf{u} \cdot \nabla \eta_b]_{z=\eta_b} \quad (19.57b)$$

$$\int_{\eta_b}^{\eta} \frac{\partial(\rho w l^z)}{\partial z} dz = [w \rho l^z]_{z=\eta} - [w \rho l^z]_{z=\eta_b}. \quad (19.57c)$$

The surface kinematic boundary condition (14.79) and bottom kinematic boundary condition (14.41) allow us to reach a reasonably tidy expression

$$\frac{\partial}{\partial t} \left[ \int_{\eta_b}^{\eta} l^z \rho dz \right] = [l^z Q_m]_{z=\eta} - \nabla_z \cdot \left[ \int_{\eta_b}^{\eta} l^z \mathbf{u} \rho dz \right] + \int_{\eta_b}^{\eta} \left[ -\frac{\partial p}{\partial \lambda} + r_{\perp} \rho F^{\lambda} \right] dz. \quad (19.58)$$

The budget (19.58) says that the depth integrated axial angular momentum per horizontal area in a horizontally fixed fluid column has a time tendency (left hand side) arising from the convergence of horizontal advection of axial angular momentum plus torques due to surface boundary mass fluxes, depth integrated zonal pressure gradients, and depth integrated irreversible stresses. This mathematical expression of the budget meets our expectations based on our understanding of the physical principles discussed in Section 19.5.1.

#### 19.5.4 Atmospheric and topographic form stresses

We can further unpack the contribution from pressure in the budget (19.58) by making use of Leibniz's rule to write

$$\int_{\eta_b}^{\eta} \frac{\partial p}{\partial \lambda} dz = \frac{\partial P}{\partial \lambda} - p_a \frac{\partial \eta}{\partial \lambda} + p_b \frac{\partial \eta_b}{\partial \lambda}, \quad (19.59a)$$

where  $P$  is the depth-integrated pressure given by equation (19.40). We studied this decomposition of the pressure force in Section 19.2 and encountered it in Section 19.4.4. Again, we see that the depth integrated zonal pressure gradient has been decomposed into three terms: (i) zonal pressure differences integrated across the depth of the column, (ii) form stress imparted to the ocean from the atmospheric pressure, (iii) form stress imparted by the solid earth bottom topography onto the ocean.

#### 19.5.5 Turbulent stresses at the surface and bottom

For turbulent stresses, we focus on the vertical transfer of zonal momentum arising from the vertical shear of horizontal stresses

$$\rho F^{\lambda} = \frac{\partial \tau^{\lambda}}{\partial z}, \quad (19.60)$$

where  $\tau^{\lambda}$  is the zonal component to the stress vector.<sup>5</sup> When integrated vertically over an ocean column,  $\int_{\eta_b}^{\eta} \rho F^{\lambda} dz$ , this friction arises from stresses acting in the ocean surface and bottom boundary/Ekman layers (Chapter 27), where the stress arises from turbulent motions that transfer momentum vertically through these layers.

To slightly simplify the contribution from friction, we assume that the axial moment-arm is well approximated by its value at the ocean surface

$$r_{\perp} = r \cos \phi = (z + R) \cos \phi \approx R \cos \phi = R_{\perp}, \quad (19.61)$$

with this assumption holding for the shallow fluid approximation built into the hydrostatic primitive equations discussed in Section 22.1. This assumption allows us to write the frictional con-

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<sup>5</sup>As seen in equation (19.43), there are other turbulent terms associated with interior Reynolds stresses arising from horizontal shears. We omit these terms for the present analysis since they are generally smaller than stresses arising from vertical strains, and smaller than the turbulent stresses associated with surface and bottom boundary processes.

tribution to the angular momentum budget (19.58) in the form

$$\int_{\eta_b}^{\eta} r_{\perp} \rho F^{\lambda} dz \approx R_{\perp} \int_{\eta_b}^{\eta} \rho F^{\lambda} dz = R_{\perp} (\tau_a^{\lambda} - \tau_b^{\lambda}). \quad (19.62)$$

The final expression introduced  $\tau_a^{\lambda}$ , which is the zonal component to the stress acting on the ocean surface imparted through interactions between the ocean and the overlying atmosphere and/or ice. The signs are such that  $\tau_a^{\lambda} > 0$  transfers an eastward momentum to the ocean such as via a westerly wind stress. Likewise, the stress  $\tau_b^{\lambda}$  is the zonal stress at the ocean bottom imparted through interactions between the ocean and the solid-earth. The signs are such that  $\tau_b^{\lambda} > 0$  reflects the transfer of eastward momentum from the ocean to the solid-earth, or conversely the transfer of westward momentum from the earth to the ocean. The net contribution from vertical friction is thus given by the moment arm,  $R_{\perp}$ , multiplied by the difference in boundary stresses.

### 19.5.6 Summary budget for column integrated axial angular momentum

Bringing all the pieces together leads to the depth integrated axial angular momentum budget

$$\frac{\partial}{\partial t} \left[ \int_{\eta_b}^{\eta} l^z \rho dz \right] = -\nabla_z \cdot \left[ \int_{\eta_b}^{\eta} l^z \mathbf{u} \rho dz \right] - \frac{\partial P}{\partial \lambda} + [l^z Q_m]_{z=\eta} + p_a \frac{\partial \eta}{\partial \lambda} - p_b \frac{\partial \eta_b}{\partial \lambda} + R_{\perp} (\tau_a^{\lambda} - \tau_b^{\lambda}). \quad (19.63)$$

Other than assuming the approximate form (19.61) for the moment-arm, and choosing a specific form of the frictional stress given by equation (19.60), this result is an exact budget for the axial angular momentum of a column of ocean fluid.

#### *Removing zonal means*

We further isolate the processes contributing to the budget (19.63) by introducing the zonal mean operator

$$\bar{A} \equiv \frac{1}{L(\phi)} \int A d\lambda, \quad (19.64)$$

where

$$L(\phi) = (R \cos \phi) \Delta \lambda = R_{\perp} \Delta \lambda \quad (19.65)$$

is the zonal length of the domain as a function of latitude,  $\phi$ , and  $\Delta \lambda$  is the zonal extent of the domain in radians. For a domain that circles the planet, then  $\Delta \lambda = 2\pi$ . Other domains are possible when considering idealized theoretical models as in Figure 19.7. The corresponding zonal anomalies to the depth integrated pressure, sea surface height, and bottom topography are thus given by

$$P' = P - \bar{P} \quad \text{and} \quad \eta' = \eta - \bar{\eta} \quad \text{and} \quad \eta'_b = \eta_b - \bar{\eta}_b, \quad (19.66)$$

in which case equation (19.63) takes the form

$$\frac{\partial}{\partial t} \left[ \int_{\eta_b}^{\eta} l^z \rho dz \right] = -\nabla_z \cdot \left[ \int_{\eta_b}^{\eta} l^z \mathbf{u} \rho dz \right] - \frac{\partial P'}{\partial \lambda} + [l^z Q_m]_{z=\eta} + p_a \frac{\partial \eta'}{\partial \lambda} - p_b \frac{\partial \eta'_b}{\partial \lambda} + R_{\perp} (\tau_a^{\lambda} - \tau_b^{\lambda}). \quad (19.67)$$

#### *Steady state balance*

Steady state balances are of particular interest when studying the large-scale low frequency circulation. A steady state holds for the angular momentum budget (19.67) so long as the following

balance is maintained

$$\nabla_z \cdot \left[ \int_{\eta_b}^{\eta} l^z \mathbf{u} \rho dz \right] = -\frac{\partial P'}{\partial \lambda} + [l^z Q_m]_{z=\eta} + p_a \frac{\partial \eta'}{\partial \lambda} - p_b \frac{\partial \eta'_b}{\partial \lambda} + R_{\perp} (\tau_a^{\lambda} - \tau_b^{\lambda}). \quad (19.68)$$

Consequently, a steady state is realized if the horizontal divergence of depth integrated axial angular momentum advection (left hand side) is balanced by torques created by the variety of physical processes on the right hand side. We further examine these physical processes by studying the zonally integrated budget.

### 19.5.7 Zonal domain topology/geometry and zonal integration

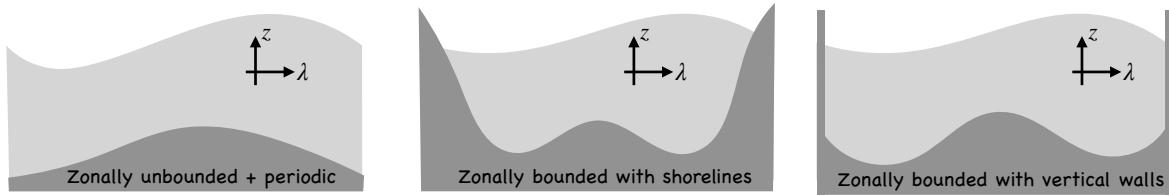


FIGURE 19.7: Three canonical zonal topologies/geometries considered in the study of fluid flow, particularly ocean flows. The light portion of each panel represents the fluid whereas the darker portion is the solid earth bottom topography. Left panel: zonally unbounded and periodic channel. Here, the topography, surface boundary forcing, and flow are zonally periodic. Middle panel: zonally bounded region where the zonal bounds occur along sloping shorelines at which the fluid thickness vanishes. The horizontal position of the vanishing thickness is time dependent since the fluid can move up and down the shoreline. Right panel: zonally bounded region where the fluid encounters a vertical sidewall so that the horizontal position of the fluid boundary is fixed, and so that there is no horizontal position where the fluid thickness vanishes. Fixed vertical sidewall boundaries are commonly found in numerical model simulations and yet they are uncommon in Nature.

Zonal integration and zonal averaging offer a common means to filter the three dimensional equations, particularly in the atmosphere where zonal motions are much stronger than meridional given the earth's rotation and the differential solar heating of the planet. Additionally, zonal averaging is of particular interest in the Southern Ocean, where the Drake Passage latitudes offer a zonally unbounded domain for ocean circulation. Even for zonally bounded ocean domains where gyre circulations occur, it is of interest to zonally integrate across the domain to study balances leading to meridional motion across the chosen latitude.

We are thus motivated to integrate zonally across the full extent of the domain, with the resulting boundary contributions dependent on the geometry and topology of the domain. We illustrate three canonical domains in Figure 19.7. For the zonally periodic domain, the zonal integral of any zonal derivative vanishes so that

$$\oint \frac{\partial P}{\partial \lambda} d\lambda = 0, \quad (19.69)$$

where we write  $\oint d\lambda$  for integration over a zonally periodic domain. Additionally, zonal derivatives vanish for a zonally bounded domain with sloping shorelines

$$\int_{\text{shorelines}} \frac{\partial P}{\partial \lambda} d\lambda = 0. \quad (19.70)$$

The reason this integral vanishes is that quantities such as  $P$  are depth integrated, and so  $P = 0$  at the shoreline edge merely since the layer thickness vanishes at the shoreline edge. The same result holds for any other depth integrated quantity, such as the axial angular momentum.

It is only for the zonally bounded domain with vertical sidewalls (third panel in Figure 19.7) that we are unable to drop the zonal integral of zonal derivatives. We observe that vertical sidewalls are common for numerical models and many theories of the ocean circulation. However, vertical sidewalls are the exception in Nature. For this reason, in the following we focus on the more geophysically relevant periodic configuration and the sloping shoreline configuration.

### 19.5.8 Steady domain integrated balance

Consider the area integral of the steady state balance (19.68) over the full ocean domain that is either periodic and/or has sloping side boundaries. In this case the divergence of the angular momentum transport integrates to zero, so that we are left with the balance

$$\int_{\phi_s}^{\phi_n} \left( \int_{\lambda_w(\phi)}^{\lambda_e(\phi)} \left[ [l^z Q_m]_{z=\eta} + p'_a \frac{\partial \eta'}{\partial \lambda} - p'_b \frac{\partial \eta'_b}{\partial \lambda} + R_\perp (\tau_a^\lambda - \tau_b^\lambda) \right] d\lambda \right) R^2 \cos \phi d\phi = 0. \quad (19.71)$$

In computing the area integral, we chose to first integrate over the longitudinal domain,  $\lambda_w(\phi) \leq \lambda \leq \lambda_e(\phi)$ , which is a function of latitude, and then to integrate over the full latitudinal domain,  $\phi_s \leq \phi \leq \phi_n$ . In most applications the surface mass term,  $[l^z Q_m]_{z=\eta}$ , is smaller than the other terms, in which case the balance is between the boundary form stresses and the boundary turbulent stresses.

In the above balance, we introduced the zonal anomalies for the applied surface pressure and the bottom pressure

$$p'_a(\lambda, \phi) = p_a(\lambda, \phi) - \bar{p}_a(\phi) \quad \text{and} \quad p'_b(\lambda, \phi) = p_b(\lambda, \phi) - \bar{p}_b(\phi). \quad (19.72)$$

We can introduce these anomalous fields since their zonal averages do not contribute to the budgets in either the periodic or sloping shoreline domains. To verify this property, note that

$$\int \bar{p}_a \frac{\partial \eta'}{\partial \lambda} d\lambda = \int \frac{\partial (\bar{p}_a \eta')}{\partial \lambda} d\lambda = 0. \quad (19.73)$$

For a periodic domain this term vanishes by inspection. For a zonally bounded domain with a sloping shoreline, it also vanishes since  $\eta' = 0$  at the edge of the shoreline. Likewise, the bottom pressure term satisfies

$$\int \bar{p}_b \frac{\partial \eta'_b}{\partial \lambda} d\lambda = \int \frac{\partial (\bar{p}_b \eta'_b)}{\partial \lambda} d\lambda = 0, \quad (19.74)$$

which follows either by periodicity or since  $\eta'_b = 0$  along the edge of a sloping shoreline. In conclusion, we see that it is only the zonal anomalies of the atmospheric and bottom pressures, and free surface and bottom topography, that impact the zonal mean zonal momentum balance (19.76) for the periodic and sloping shoreline domains.

### 19.5.9 Form stress versus dual form stress

We can further exploit the symmetries of the periodic and sloping shoreline domains by writing the form stresses in equation (19.76) in the alternative form that makes use of the dual form stress

$$\int \left[ p'_a \frac{\partial \eta'}{\partial \lambda} - p'_b \frac{\partial \eta'_b}{\partial \lambda} \right] d\lambda = \int \left[ -\frac{\partial p'_a}{\partial \lambda} \eta' + \frac{\partial p'_b}{\partial \lambda} \eta'_b \right] d\lambda. \quad (19.75)$$

Diagnostics of zonally integrated form stress can be more convenient using one form or the other, depending on dataset or numerical model framework. We have a choice since the zonal integral is

the same, and that freedom is afforded since the spatial integral removes local information that appears as a total zonal derivative. However, we offer two caveats in this regard.

- The identity (19.75) does not hold for the bounded domain with vertical sidewalls (third panel of Figure 19.7). If working in such a domain and if one chooses to study patterns based on the right hand side dual form stress, then its zonal integral will not agree with that of the form stress on the left hand side. Correspondingly, physical interpretations based on the dual form stress are questionable.
- Although the zonal integrals in equation (19.75) agree for the periodic domain and sloping shoreline domain, there is no local identity between terms on the left hand side and right hand side. So if one wishes to make a statement about patterns of local form stresses acting on the depth integrated axial angular momentum, then it is necessary to return to the form stress appearing on the left hand side of equation (19.75).

### 19.5.10 Steady zonal and depth integrated budget

Now consider just a zonal integral, again over a domain that is either periodic or has sloping shorelines (Figure 19.7). In both of these cases, we are left with the zonal and depth integrated steady angular momentum budget

$$\frac{1}{R \cos \phi} \int \frac{\partial}{\partial \phi} \left[ \int_{\eta_b}^{\eta} l^z v \rho dz \right] d\lambda = \int \left[ [l^z Q_m]_{z=\eta} + p'_a \frac{\partial \eta'}{\partial \lambda} - p'_b \frac{\partial \eta'_b}{\partial \lambda} + R_{\perp} (\tau_a^{\lambda} - \tau_b^{\lambda}) \right] d\lambda. \quad (19.76)$$

The meridional divergence of the advective transport of angular momentum is balanced, in the steady state, by the boundary terms on the right hand side.

### 19.5.11 Southern Ocean balances

Under certain cases the primary balance in equation (19.76) is between the form stress and boundary turbulent stress, whereby

$$\oint \left[ p'_a \frac{\partial \eta'}{\partial \lambda} + R_{\perp} \tau_a^{\lambda} \right] d\lambda \approx \oint \left[ +p'_b \frac{\partial \eta'_b}{\partial \lambda} + R_{\perp} \tau_b^{\lambda} \right] d\lambda. \quad (19.77)$$

For much of the large-scale Southern Ocean circulation, the primary balance is even simpler: it is a balance between surface wind stress and topographic form stress

$$\oint \tau_a^{\lambda} d\lambda \approx \oint p'_b \frac{1}{R_{\perp}} \frac{\partial \eta'_b}{\partial \lambda} d\lambda = - \oint \eta'_b \frac{1}{R_{\perp}} \frac{\partial p'_b}{\partial \lambda} d\lambda, \quad (19.78)$$

with this balance exemplified in Figure 19.8. We now state in words what this balance means in the presence of a net eastward wind stress,  $\oint \tau_a^{\lambda} d\lambda > 0$ . The equivalent expressions on the right hand side allow complementary perspectives.

- For the first equality we see that balance is realized if on the upwind side of a topographic bump there is an anomalously high bottom pressure, with the opposite on the downwind side. Correspondingly, there is a net westward topographic form stress imparted by the solid earth onto the ocean that balances the eastward surface wind stress imparted by the atmosphere onto the ocean.
- The second equality in equation (19.78) reveals that for  $\eta'_b > 0$  (topographic ridge), a steady angular momentum balance is maintained so long as the bottom pressure decreases across the ridge from west to east, just as depicted in Figure 19.8.

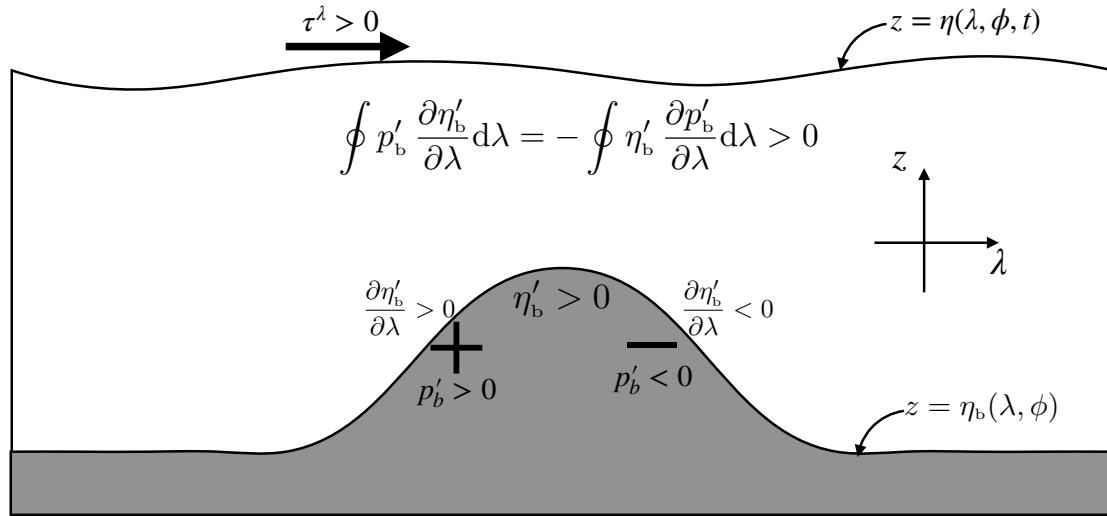


FIGURE 19.8: Depicting the balance between zonal wind stress and topographic form stress for a southern hemisphere zonally periodic ocean channel. For an eastward wind stress, the flow reaches a steady state if the upwind side of a topographic bump sees an anomalously high bottom pressure whereas on the downwind side it is anomalously low. The form stress imparted by the ocean onto the solid earth is eastward since the bottom pressure is higher in the west and lower in the east. Conversely, Newton's third law tells us that the topographic form stress imparted by the solid earth onto the ocean is westward. In this manner, the eastward force imparted by the atmosphere onto the ocean through wind stress is balanced by a westward topographic form stress imparted by the solid earth onto the ocean. Furthermore, the eastward bottom pressure gradient leads to a northward depth integrated geostrophic transport above the southern hemisphere ridge. Signs are swapped when flow moves over a depression, in which a westward bottom pressure gradient leads to southward geostrophic transport over the depression. We revisit these dynamical processes for the shallow water fluid in Figure 31.8.

### 19.5.12 Topographic form stress and ocean gyres

*Hughes and de Cueves* (2001) are notable for having emphasized the importance of bottom topographic form stress, and the associated bottom pressure torque appearing in the vorticity equation (detailed in see Section 35.10). The key role for topographic form stress is well appreciated for channel flows since the work of *Munk and Palmén* (1951) who studied the Southern Ocean force balances. However, *Hughes and de Cueves* (2001) showed that it is central even for steady ocean gyre circulations when allowing for sloping sides rather than vertical sides. Hence, sloping sides for the gyre domain allow for a steady momentum balance to occur between bottom form stress and wind stress, and a steady vorticity balance to occur between bottom pressure torque and wind stress curl. As a result, topographic form stress and bottom pressure torques allow for a mostly inviscid balance in ocean gyres much like for the zonally re-entrant Southern Ocean.

The critical role of sloping sides was not appreciated by the pioneering studies of ocean gyres from *Stommel* (1948) and *Munk* (1950), who used vertical sidewalls and relied on friction to close the vorticity budget. That is, vertical sides hide the role of topographic form stresses, thus requiring frictional stresses to balance the wind stress. We return to these points in Section 34.9, in particular in Section 34.9.5, when studying gyre circulations in a shallow water fluid.

### 19.5.13 Further study

Elements of this section are based on *Hughes and de Cueves* (2001) and the analogous discussion of the global atmospheric axial angular momentum budget developed in Section 10.3 of *Holton* (1992). *Straub* (1993) provides an analogous analysis with a focus on the Southern Ocean. The

physical processes establishing the balances noted for the Southern Ocean remain under investigation, with further resources to the literature including Section 21.7 of [Vallis \(2017\)](#), and the reviews by [Rintoul et al. \(2001\)](#), [Rintoul and Naveira Garabato \(2013\)](#), and [Rintoul \(2018\)](#). We further revisit this balance in Section 31.6 for the shallow water system.





# Chapter 20

## Equilibrium thermodynamics

Thermodynamics is a phenomenological discipline focused on relations between macroscopic properties of physical systems. In this chapter we develop elements of equilibrium thermodynamics relevant to a multi-component fluid in or near thermodynamic equilibrium. We limit concern to a single phase of matter (liquid or gas), noting that a more complete treatment considers multiple phases and transitions between them. Thermodynamics is a necessary ingredient for understanding the stability, evolution, and transformation of macroscopic systems, with such topics at the heart of geophysical fluid mechanics.

The name “thermodynamics” suggests that it is the study of how heat moves through a system. Indeed, that topic formed the focus of the subject in the 19th century, as exemplified by [Maxwell \(1872\)](#). However, more recent treatments, largely following the formulation from Gibbs, generally focus on energy and entropy, from which temperature is derived. Energy and entropy are logically distinct concepts that together form the basis for thermodynamics. Energy is a concept borrowed from mechanics, with the energy of concern in this chapter mostly related to microscopic degrees of freedom; i.e., the *internal energy*. Extensions to include the mechanical energy of macroscopic motion is the subject of Chapter 21. Entropy provides a measure what is unknown about a system. A deductive understanding of entropy comes through the study of statistical mechanics, whereas in classical thermodynamics we must accept entropy’s basic properties as given.

In this chapter we explore ideas from classical thermodynamics, so that we are generally concerned with macroscopic states of a fluid system; i.e., a macrostate. Hence, a macrostate is synonymous with *thermodynamic state*. This nomenclature must be modified when discussing statistical mechanics and quantum mechanics, whereby the complementary notion of a microstate takes on a far more central role than considered in this chapter.

We offer the following reflections from two 20th century giants of physics on the enduring, and often confusing, nature of thermodynamics.

Thermodynamics is a funny subject. The first time you go through it, you do not understand it at all. The second time you go through it, you think you understand it, except for one or two points. The third time you go through it, you know you do not understand it, but by that time you are so used to the subject it does not bother you anymore. *Attributed to Arnold Sommerfeld, unknown source*

A theory is the more impressive the greater the simplicity of its premises, the more different kinds of things it relates, and the more extended is its area of applicability. Therefore the deep impression which classical thermodynamics made upon me. It is the only physical theory of universal content concerning which I am convinced that, within the framework of the applicability of its basic concepts, it will never be overthrown. [Einstein \(1949\)](#)

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## CHAPTER GUIDE

This chapter develops the rudiments of equilibrium thermodynamics as applied to geophysical fluid mechanics. Our treatment follows *Callen* (1985), *Reif* (1965), chapter 2 of *Landau and Lifshitz* (1980), and chapter 2 of *Ebeling and Feistel* (2011). We make use of this chapter when studying energetics of fluid flow in Chapter 21. The mathematical tools required for thermodynamics include the basics of partial differential calculus from Chapter 2. Conceptually, the subject is rather subtle, thus making this chapter long on words and relatively brief on equations.

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20.1	Conceptual basics . . . . .	435
20.1.1	Thermodynamic equilibrium versus steady state . . . . .	435
20.1.2	Exchanges between thermodynamic systems . . . . .	436
20.1.3	Quasi-static processes . . . . .	437
20.1.4	Extensive and intensive properties . . . . .	437
20.1.5	Thermodynamic configuration space . . . . .	438
20.1.6	Internal energy and total energy . . . . .	438
20.1.7	Postulates of thermodynamics . . . . .	439
20.2	Materially closed systems . . . . .	440
20.2.1	First law of thermodynamics . . . . .	440
20.2.2	The nature of working and heating . . . . .	440
20.2.3	Mechanical work from pressure . . . . .	441
20.2.4	Entropy and the quasi-static transfer of internal degrees of freedom . . . . .	442
20.2.5	Gibbs' fundamental thermodynamic relation . . . . .	442
20.2.6	Partial derivatives . . . . .	443
20.2.7	Entropy and reversible/irreversible processes . . . . .	444
20.2.8	Thermodynamic equilibrium . . . . .	445
20.2.9	Thermodynamic equilibrium with macroscopic motion . . . . .	446
20.3	Characterizing materially open systems . . . . .	447
20.3.1	Euler's theorem for homogeneous functions . . . . .	447
20.3.2	Homogeneous functions of degree one . . . . .	448
20.3.3	Chemical potential and the Euler form . . . . .	449
20.3.4	Molar mass and molar chemical potential . . . . .	449
20.3.5	Chemical work and the Gibbs-Duhem relation . . . . .	450
20.3.6	Gibbs potential . . . . .	451
20.3.7	Extensive functions of $(T, p, M_n)$ . . . . .	451
20.4	Materially open single-component systems . . . . .	452
20.5	Thermodynamic equilibrium with a geopotential . . . . .	453
20.5.1	The first law . . . . .	454
20.5.2	Thermodynamic equilibrium . . . . .	454
20.5.3	Further study . . . . .	455
20.6	Materially open systems with fixed total mass . . . . .	455
20.6.1	Matter concentrations . . . . .	456
20.6.2	Fundamental thermodynamic relation per unit mass . . . . .	456
20.6.3	Seawater as a binary fluid . . . . .	456
20.6.4	Further study . . . . .	457
20.7	Thermodynamic potentials . . . . .	457
20.7.1	Equations of state . . . . .	457
20.7.2	Internal energy . . . . .	458
20.7.3	Entropy . . . . .	458
20.7.4	Enthalpy . . . . .	459
20.7.5	Helmholtz free energy . . . . .	460

---

20.7.6 Gibbs potential . . . . .	461
20.7.7 Chemical potential and the Gibbs potential . . . . .	461
20.8 Response functions . . . . .	<b>462</b>
20.8.1 Heat capacities . . . . .	463
20.8.2 Thermal expansion coefficient . . . . .	463
20.8.3 Haline contraction coefficient . . . . .	464
20.8.4 Sound speed . . . . .	464
20.9 Maxwell relations for homogeneous fluids . . . . .	<b>464</b>
20.9.1 Maxwell relation from internal energy . . . . .	464
20.9.2 Summary of the Maxwell relations . . . . .	465
20.10 Adiabatic lapse rate . . . . .	<b>465</b>
20.10.1 Isentropic rearrangement . . . . .	465
20.10.2 Thermodynamic formulation . . . . .	466
20.10.3 Adiabatic lapse rate for pressure changes . . . . .	466
20.10.4 Adiabatic lapse rate for height changes . . . . .	467
20.10.5 Further study . . . . .	467
20.11 Potential temperature . . . . .	<b>467</b>
20.11.1 Motivating the definition of potential properties . . . . .	468
20.11.2 Temperature changes from pressure changes . . . . .	468
20.11.3 Defining the potential temperature . . . . .	468
20.11.4 Potential temperature and specific entropy . . . . .	469
20.12 A simple ideal gas atmosphere . . . . .	<b>471</b>
20.12.1 Equation of state . . . . .	471
20.12.2 Internal energy . . . . .	472
20.12.3 Heat capacity . . . . .	472
20.12.4 Enthalpy . . . . .	473
20.12.5 Thermal expansion coefficient . . . . .	473
20.12.6 Fundamental thermodynamic relations . . . . .	473
20.12.7 Isothermal compressibility . . . . .	474
20.12.8 Sound speed . . . . .	474
20.12.9 Adiabatic lapse rate . . . . .	474
20.12.10 Geopotential thickness . . . . .	475
20.12.11 Potential temperature . . . . .	476
20.12.12 Further study . . . . .	477
20.13 Exercises . . . . .	<b>477</b>

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## 20.1 Conceptual basics

In our study of thermodynamics, we are concerned with macroscopic fluid systems whose evolution tends toward states in which its properties are determined by intrinsic factors rather than depending on memory of previous external influences. These particular *macrostates* are known as *thermodynamic equilibria*. One aim for thermodynamics is the determination of a new thermodynamic equilibrium after the removal of a constraint. When a constraint is removed, the system moves through a sequence of macrostates as it evolves towards its new equilibrium, with the time evolution through such macrostates referred to as a *process*. Any macrostate is comprised of a huge number of microscopic degrees of freedom; i.e., *microstates*. The allure of thermodynamics is that we can describe macroscopic systems, and the process of moving from one equilibria to another, using just a handful of macroscopically measurable properties.

### 20.1.1 Thermodynamic equilibrium versus steady state

Equilibrium thermodynamics is the study of systems in *thermodynamic equilibrium* and how they transit from one thermodynamic equilibrium state to another through quasi-static processes.

We explore the defining characteristics of thermodynamic equilibrium within this chapter. At a basic level, a system in thermodynamic equilibrium will remain in that state for all time, with equilibrium dependent on the constraints imposed on the system. When such constraints are removed, then a system generally transitions to another equilibrium state. Note that “for all time” is a loaded term. More precisely, we mean “for a time extremely long compared to any time scale relevant to the physical system under consideration”, with such time scales considered in Section 20.1.3.

A system in thermodynamic equilibrium is a steady state since there are no time changes to macroscopic properties. However, a general steady state need not be a thermodynamic equilibrium. For example, consider a region of fluid with nonzero heat fluxes yet with no heat flux convergence so the temperature of the region does not change. As we see in this chapter, a temporally constant temperature is a signature of a steady state whereas the flow of heat is the sign of thermodynamic disequilibrium. The distinction is sometimes subtle and always important.

### 20.1.2 Exchanges between thermodynamic systems

In the study of thermodynamics it is important to characterize how a physical system interacts with its surrounding environment through mechanical, thermal, and material interactions and exchanges. Infinitesimal fluid elements, and their accumulation into finite fluid regions, constitute the physical systems we are concerned with in this book<sup>1</sup> We are concerned with systems that routinely interact mechanically with their surroundings so that the systems are mechanically open. However, it is useful to distinguish how a physical system interacts thermally and materially with its surroundings, as well as to consider the time scales over which these interactions take place.

- **THERMALLY OPEN (DIABATIC) AND MATERIALLY OPEN:** An open physical system exchanges matter, thermodynamic properties, and mechanical forces with its surrounding environment. All naturally occurring fluid systems are open in this manner.
- **THERMALLY OPEN (DIABATIC) AND MATERIALLY CLOSED:** We have occasion to consider a thermodynamic system that is mechanically and thermally open yet materially closed. Such systems maintain a fixed matter content yet exchange thermal and mechanical energy with their surrounding environment.
- **THERMALLY CLOSED (ADIABATIC) AND MATERIALLY CLOSED:** We sometimes consider a thermodynamic system that is both materially and thermally closed and yet mechanically open. In fluid mechanics, such systems constitute *material fluid parcels* (Section 12.2), defined as infinitesimal regions that maintain fixed matter and thermal properties yet move according to mechanical forces. A *perfect fluid* is a continuum of infinitesimal material fluid parcels.
- **ISOLATED SYSTEM:** An isolated system does not exchange heat, matter, or mechanical forces with its surroundings.

Each of the above interactions is mechanically open, so that the thermodynamic system is exposed to mechanical forces, either contact forces such as pressure and friction or body forces such as gravity and Coriolis. For pedagogical purposes we first study the thermodynamics of fluid elements that are thermally open yet materially closed and then extend to fluid elements that are both thermally and materially open. As a somewhat overloaded terminology, “adiabatic” in fluid mechanics is often used for a system that is *both* thermally closed *and* materially closed. However, we maintain the distinction in our treatment to maintain consistency with the physics literature.

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<sup>1</sup>See Section 12.2.4 for a reminder of infinitesimal fluid elements.

### 20.1.3 Quasi-static processes

When extending equilibrium thermodynamics to the linear irreversible thermodynamics of moving fluid systems in Chapter 21, we make use of the huge time scale separation between molecular degrees of freedom and macroscopic degrees of freedom. We are led to define a *quasi-static process* as one that proceeds via an arbitrary number of intermediate equilibrium states. In fact, as formally defined (e.g., Section 4.2 of [Callen \(1985\)](#)), a quasi-static process is a locus of equilibrium states that can only be approximated by realistic processes occurring through steps that are each arbitrarily close to thermodynamic equilibrium. By formulating the notion of a quasi-static process, we are afforded a precise definition for intensive properties such as its temperature, pressure, and chemical potential, whereas intensive properties are fuzzy concepts for systems out of thermodynamic equilibrium.

A quasi-static process is a relevant idealization for our study of macroscopic fluid motion. We recognize this relevance by considering the time scale separation between macroscopic and microscopic motions. Recall from Section 11.3.5 that the time between molecular collisions is on the order of  $t_{\text{collision}} \approx 10^{-9}$  s, with this time scale setting the time scale for molecular equilibration. In contrast, typical macroscopic processes occur on time increments on the order of  $\Delta\tau_{\text{macro}} \sim 1$  s. Hence, we can safely assume that any macroscopic process arising in fluid flows, even turbulent flows, evolves through time increments that are much longer than the molecular collision time

$$\Delta\tau_{\text{macro}} \gg t_{\text{collision}} \approx 10^{-9} \text{ s.} \quad (20.1)$$

We are thus led to the following conceptual framework for our treatment of fluid motion. Namely, we assume that the macroscopic motion of a fluid is comprised of the motion of a continuum of fluid elements that are, individually, in a thermodynamically equilibrated state so that each fluid element evolves quasi-statically. So although any finite region of fluid is not necessarily in thermodynamic equilibrium (e.g., its temperature can be nonuniform), the individual fluid elements comprising the finite region are in thermodynamic equilibrium. The justification for this foundational assumption is that the relevant time scales for macroscopic fluid motion are many orders of magnitude longer than the molecular time scales that bring about local thermodynamic equilibrium.

Some authors do not make a distinction between a quasi-static process and a reversible process. Our treatment follows [Callen \(1985\)](#) (see his sections 4.2 and 4.3) and [Reif \(1965\)](#) (see his sections 2.9 and 2.10), whereby reversible processes are subsets of quasi-static processes. Namely, a reversible process is a quasi-static process that occurs without net entropy change (see Section 20.2.7), and yet not all quasi-static processes are reversible.

### 20.1.4 Extensive and intensive properties

In describing thermodynamic systems we characterize properties according to whether they are *extensive* or *intensive*. Extensive properties scale with the size of the system, with examples including mass, internal energy and entropy. Since we can count the amount of an extensive property, we can form budget equations for extensive quantities such as detailed in Section 15.3. That is, when combining two systems then the extensive property of the combined system equals to the sum of the extensive property of the individual systems. Correspondingly, extensive properties scale with a power 1 with the size of the system.

A *homogeneous fluid* is one in which all *intensive properties* are identical, with temperature, pressure, and chemical potential the canonical examples. This characteristic of intensive properties contrasts to extensive properties, which are additive. Hence, intensive properties do not scale with the size of a system. That is, intensive properties are scale invariant and thus scale with power

0 as the size of the system changes. Intensive properties describe possible gradients within a thermodynamic system. In the absence of an externally imposed force field such as gravity, intensive properties are uniform for systems in thermodynamic equilibrium (we show this property in Sections 20.2.8 and 20.5.2). However, as discussed in Section 20.5, hydrostatic balance is realized in thermodynamic equilibrium for a fluid in an externally imposed gravity field, in which case pressure and chemical potential are not uniform.

Extensive and intensive properties come as conjugate pairs in thermodynamics whereby intensive properties always multiply their conjugate extensive property (e.g., pressure-volume and temperature-entropy) when appearing in the various forms of the first law of thermodynamics. In this chapter, extensive properties are labeled with a superscript  $e$  (except for the mass and volume), with this label *not* a tensor index. In Section 20.6 we introduce the internal energy per mass and entropy per mass, as doing so is most convenient when studying thermodynamic systems of fixed mass. In this manner we can convert the extensive properties to their specific (per mass) form in which case we drop the  $e$  superscript. It is the specific form of extensive properties that provides a straightforward transfer to the study of constant mass fluid elements.

### 20.1.5 Thermodynamic configuration space

Equilibrium thermodynamics is not concerned with points in geographical space. Rather, it characterizes a physical system through specifying a suite of continuous thermodynamic properties, and studying how those processes change under changes in the constraints. Thermodynamic properties define coordinates for a point within *thermodynamic configuration space*. Even though one commonly encounters thermodynamic diagrams with orthogonal axes specifying values of thermodynamic properties, there is no notion of distance or angle between points in thermodynamic configuration space since there is no metric structure. Mathematically, we say that thermodynamic configuration space comprises a *differentiable manifold*. A summary of the mathematical structure of equilibrium thermodynamics can be found in [this online tutorial from Salamon et al.](#)<sup>2</sup>

### 20.1.6 Internal energy and total energy

As discussed in Chapter 11, there are a huge number of microscopic (molecular) degrees of freedom that are averaged over when describing a fluid as a continuous media. *Internal energy* embodies the energy of microscopic degrees of freedom not explicitly considered in a macroscopic continuum treatment. Internal energy is not readily accessed or harnessed, which contrasts to the mechanical energy of the macroscopic motion.

For a simple ideal gas (Section 20.12), internal energy arises from the translational kinetic energy of molecular motion, as well as degrees of freedom associated with rotation and vibration. Kinetic theory studies of a simple ideal gas suggests that we conceive of internal energy as *thermal energy*. That is, we idealize molecules as point masses whose kinetic energy is directly related to temperature, and with the internal energy of an ideal gas directly proportional to temperature. However, for a general fluid, particularly for liquids, the internal energy is far more than a measure of the kinetic energy of molecules, as real molecules exhibit intermolecular potential energy arising from molecular interactions. In general, the concept of internal energy is rather slippery. We are thus motivated to sidestep internal when getting serious about quantitative notions, such as when studying energetics of fluid flow in Chapter 21. We do so by appealing to the conservation of

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<sup>2</sup>There are some formulations of thermodynamics that do introduce a metric through properties of the entropy. In so doing, these formulations transform the differentiable manifold to a Riemannian manifold. There are tradeoffs when doing so, with [Andresen et al. \(1988\)](#) offering a survey of the tradeoffs. Here, we follow the traditional approach of Gibbs as articulated in the books by [Callen \(1985\)](#) and [Reif \(1965\)](#).

*total energy* as postulated in Section 20.1.7. Even so, to lay the foundations we largely focus on internal energy in this chapter.

### 20.1.7 Postulates of thermodynamics

Thermodynamics is not a first principles theory, though it does have its roots in statistical mechanics. We follow [Callen \(1985\)](#) by building thermodynamics from a set of postulates from which deductive results are derived. The following postulates render a logical basis for the subject, with the bulk of this chapter exemplifying these postulates and developing implications.

- ★ THERMODYNAMIC EQUILIBRIUM: There exists states of thermodynamic equilibrium that are completely characterized macroscopically by a few extensive properties, including internal energy, volume, and mass (or mole number). For each thermodynamic equilibrium there exists a scalar intensive property, called the *thermodynamic temperature*, or more briefly the temperature, that is uniquely defined. Furthermore, the temperature has the same value for two systems in thermodynamic equilibrium with one another.
- ★ ZEROTH LAW OF THERMODYNAMICS: When two systems,  $A$  and  $B$ , are each separately in thermodynamic equilibrium with a third system,  $C$ , then the systems  $A$  and  $B$  are also in thermodynamic equilibrium with one another.
- ★ MAXIMUM ENTROPY: *Entropy* is an extensive property of a macrostate. The values assumed by the other extensive properties are those that maximize the entropy over the manifold of constrained thermodynamic equilibrium states. This postulate is fundamental to how we determine properties of thermodynamic equilibria.
- ★ ENTROPY INCREASES: The entropy of a composite macroscopic system is additive over the constituent subsystems. Furthermore, entropy is a continuous and differential function that is a monotonically increasing function of the internal energy. This postulate is fundamental to how we use thermodynamics for composite systems such as a fluid.
- ★ TOTAL ENERGY IS CONSERVED: The total energy of a thermodynamic system is locally (in space and time) conserved while undergoing a thermodynamic process. This property constitutes the *first law of thermodynamics*. For a macroscopic fluid, total energy is the sum of the internal energy arising from microscopic degrees of freedom plus the mechanical energy of macroscopic degrees of freedom. In this chapter we are mostly concerned with internal energy, with Chapter 21 extending the discussion to include mechanical energy. Space and time locality of total energy conservation is far more consequential than a global conservation property. Namely, it means that physical processes are not allowed in which total energy disappears from one point in space or time only to reappear at a distant point. As a corollary, we are afforded a local budget equation for total energy whereby energy transferred from one form to another, with particular forms of this budget equation a topic of Chapter 21. Note that energy is well defined for both microstates and macrostates, whereas entropy is only defined for macrostates.
- ★ THIRD LAW OF THERMODYNAMICS: Internal energy and entropy are extensive scalar quantities that are finite for finite systems and bounded from below. In the limit of zero thermodynamic temperature for single-phase (single state of matter) systems, the derivatives of entropy with respect to extensive variables disappear asymptotically. Many take the zero temperature limit to have zero entropy, though statistical fluctuations break this assumption (see page 51 of [Ebeling and Feistel \(2011\)](#) for discussion). We have little direct use for

this postulate, though it takes on an important role when considering quantum statistical mechanics.

The two postulates concerning entropy (entropy maximum and entropy increasing) constitute the *second law of thermodynamics*. Statistical mechanics reveals the fundamentally statistical nature of entropy and the second law. In Sections 20.2.8 and 20.5.2, we see how it provides the basis for determining properties at thermodynamic equilibrium, and for how systems approach equilibrium. We make further use of the second law in Chapter 21 to constrain fundamental processes acting in a multi-component fluid.

## 20.2 Materially closed systems

We are now ready to apply the above foundational concepts by studying the thermodynamics of a physical system that is closed materially.

### 20.2.1 First law of thermodynamics

The first law of thermodynamics for a materially closed system establishes a relationship between infinitesimal changes of internal energy of a physical system, the work done to or by the system, and the thermal energy transferred between the system and its surrounding environment. The first law takes on the mathematical form

$$dJ^e = dW + dQ \quad \Longleftarrow \text{materially closed.} \quad (20.2)$$

In this equation,  $dJ^e$  is the infinitesimal increment (an exact differential) of the internal energy;  $dW$  is the change in internal energy due to work applied to the system (*working*); and  $dQ$  is the internal energy change due to thermal energy transferred to the system (*heating*). We only have occasion to study mechanical work in this book, though note that there are other forms such as those arising from electromagnetic forces.

The first law of thermodynamics is a statement of energy conservation for a physical system, where energy changes arise from working and heating applied to the system or by the system. We are only interested in changes to the energy, with the absolute value of the energy of no concern. For the present consideration, the relevant energy is just the internal energy since we here ignore mechanical energy associated with moving fluids. But that limitation is not suitable for a moving fluid, where mechanical energy exchanges are of direct interest. We thus take up the topic of mechanical energy in Chapter 21, where we add mechanical energy to internal energy to form the total energy of a moving fluid system (Section 21.5).

### 20.2.2 The nature of working and heating

Working and heating are both path-dependent thermodynamic processes that transform a system from one thermodynamic state to another. That is, working and heating represent *path functions* whose value depends on their history. They are mathematically represented by inexact differentials as denoted by the  $d$  symbol. It is remarkable that the first law in equation (20.5) shows that the sum of two inexact differentials equals to an exact differential which, in the absence of macroscopic motion, is the exact differential of the internal energy. The internal energy is a *state function* that is a property of the thermodynamic state of a system and not a function of the path history taken to reach that state. The term *thermodynamic potential* is synonymous with state function. It follows that if the internal energy change occurs in the absence of heating then the working process must occur as a path independent process. The converse holds if internal energy changes

without any working. Furthermore, the first law (20.5) allows us to decompose changes to internal energy according to mechanical and thermal contributions. However, it is not possible to perform that decomposition for the internal energy itself.

Working and heating denote actions applied to a system (verbs) rather than properties of a system (nouns). They are energy *in transition* that arise at the boundary of a thermodynamic system. We raise this somewhat pedantic yet subtle point since the terms “work” and “heat” are often used instead of “working” and “heating”. Indeed, we will often make use of that language in this book. However, such usage should be used with care as it can spuriously lead one to seek information concerning the “work content” or “heat content” of a physical system; i.e., to incorrectly consider work and heat as state properties (i.e., nouns). Rather, in thermodynamics we only consider the work imparted to change a system’s energy (working), or likewise the thermal energy used to change a system (heating).

These conceptual points are particularly relevant when asking questions about the heat transported by a fluid (with dimensions energy per time and SI units of Watt = Joule per second). In the analysis of a heat budget, it is tempting to define the “heat content” of a fluid element or fluid region according to its temperature, mass, and heat capacity. But the notion of heat content spuriously conflates a thermodynamic process whereby a system moves from one state to another (heating) with a thermodynamic state property (e.g., enthalpy, which is a property of the state; see Section 20.7.4). Furthermore, any definition of heat content is ambiguous due to the arbitrariness of the temperature scale; i.e., heat content based on the Celsius scale is distinct from that based on the Kelvin scale. Therefore, when working with heat transport, care should be exercised if also including the notion of heat content. One way to detect an error is to ask whether a particular conclusion is modified by changing the temperature scale. If so, then one should revisit assumptions of the analysis since the results might be unphysical.

### 20.2.3 Mechanical work from pressure

As forces do work on a physical system they change its internal energy and mechanical energy. We are here concerned only with the effects on internal energy, though note that mechanical changes that alter internal energy are generally balanced by compensating changes to mechanical energy (see Section 21.5). One way to perform mechanical work is via changes to the volume of a fluid element through the action of pressure (a contact force per area) on the boundary of the fluid element. For example, if a fluid element increases its volume, it must do work against the surrounding environment to overcome the compressive force from pressure.

When volume changes occur quasi-statically, then we can write the *pressure work* in the mathematical form

$$dW = -p dV, \quad (20.3)$$

where  $p$  is the pressure that acts on the boundaries of the fluid element. The assumption that the mechanical process is quasi-static allows us to unambiguously define pressure acting on the system, and thus to write equation (20.3) for the work. The negative sign arises since the compression of a fluid element into a smaller volume,  $dV < 0$ , requires positive mechanical work be applied to the fluid element,  $dW > 0$ . The mathematical form of pressure work derives from the general form of mechanical work given by

$$\text{work} = \text{force} \times \text{distance} = \text{force}/\text{area} \times \text{distance} \times \text{area} = \text{force}/\text{area} \times \text{volume}. \quad (20.4)$$

Stated alternatively, we note that pressure is a force per unit area acting on a surface, and the product of the surface area and its normal displacement is the volume swept out during a time increment.

We offer the following points in regards to this form of mechanical work.

- Pressure is an intensive property that measures the *intensity* of a force (per area) that is conjugate to the extensive property,  $V$ . In general, work applied to a thermodynamic system, thus leading to a change in the internal energy, takes on the form of an intensive property multiplying the change of an extensive property.
- From a mathematical perspective, pressure is the *integrating factor* that connects the inexact (path dependent) differential  $dW$  to the exact differential  $dV$ . We studied the mathematics of inexact differentials in Section 2.8.
- For a quasi-static process, pressure changes the internal energy of a fluid through the pressure work according to equation (20.3). As seen in Section 21.3.1, pressure also changes the kinetic energy of a moving fluid by changing the fluid speed. When combining the internal energy and mechanical energy budgets in Section 21.5, we see how pressure affects the total energy of a fluid element.
- Surface tension acting on fluid interfaces can give rise to mechanical work. However, we generally ignore surface tension in this book since it is negligible for scales larger than a few centimeters (see Section 18.10).

#### 20.2.4 Entropy and the quasi-static transfer of internal degrees of freedom

The internal energy of a thermodynamic system can change when the molecular degrees of freedom are energized. For a materially closed system whose internal energy changes in a quasi-static manner, we consider the thermal energy change as relates to entropy changes via

$$dQ = T dS^e \quad \text{materially closed system.} \quad (20.5)$$

$T$  is the thermodynamic temperature (measured relative to absolute zero) and it is an intensive variable whereas  $S^e$  is the extensive form of entropy. Entropy is an extensive state function so that  $T$  provides the integrating factor connecting the inexact differential  $dQ$  to the exact differential  $dS^e$ . A nonzero  $dQ$  in a geophysical fluid can arise from radiative fluxes external to the fluid element; internal sources from friction; and the exchange of thermal energy through the mixing of fluid properties. Since heating has dimensions of energy, the entropy has dimensions of energy per temperature.

#### 20.2.5 Gibbs' fundamental thermodynamic relation

We summarize the discussion of this section by writing the first law for quasi-static materially closed processes

$$dJ^e = -p dV + T dS^e \iff \text{quasi-static materially closed processes.} \quad (20.6)$$

This equation is known as the *Gibbs relation* or more commonly the *fundamental thermodynamic relation* for quasi-static materially closed processes moving from one thermodynamic equilibrium state to another. This relation suggests that we interpret minus the pressure as the amount of internal energy required to add one unit of volume to the system while holding entropy fixed. Likewise, temperature is the internal energy required to add one unit of entropy to the system while holding volume fixed.

The fundamental thermodynamic relation (20.6) is an integrable differential equation, with a solution found by performing a path integral within thermodynamic configuration space. The

solution provides one of the extensive properties, such as internal energy or entropy, as a function of the other extensive properties. However, we generally do not require this solution since it is the differential increments, as determined by the Gibbs relation, that are sufficient for determining practical thermodynamic properties such as temperature, pressure, and chemical potential.

All differentials within the fundamental thermodynamic relation (20.6) are exact differentials of state functions. This property is a result of assuming the thermodynamic processes are quasi-static, in which case we can determine the integrating factors pressure and temperature to thus replace the inexact differentials  $dW$  and  $dQ$  with exact differentials. Even with the quasi-static restriction, equation (20.6) offers great utility (with its extension to materially open systems given in Section 20.6). Since we are only concerned with quasi-static changes to fluid elements in this book, the fundamental thermodynamic relation (20.6) provides the central expression of the first law of thermodynamics for our purposes.

It follows from the first law expression in equation (20.6) that the internal energy is a natural function of volume and entropy

$$dJ^e = -p dV + T dS^e \implies J^e = J^e(V, S^e). \quad (20.7)$$

Conversely, the entropy for a materially closed system is naturally a function of volume and internal energy

$$T dS^e = dJ^e + p dV \implies S^e = S^e(V, J^e). \quad (20.8)$$

We see that both of the extensive state functions,  $J^e$  and  $S^e$ , are functions of extensive properties, with such dependence having implications for the scaling discussed in Section 20.3.2. Furthermore, we note that both  $J^e$  and  $S^e$  are functions of the volume of a system, but not of the shape. This behavior is strictly only appropriate for fluids, and it ignores effects from interfaces. Both of these assumptions are suitable for our study of geophysical fluids.

### 20.2.6 Partial derivatives

The fundamental thermodynamic relation (20.7) appears in terms of internal energy, which is written as a natural function of the extensive properties volume and entropy. We arrive at two partial derivative identities by expanding the exact derivative of internal energy

$$dJ^e = \left[ \frac{\partial J^e}{\partial V} \right]_{S^e, M} dV + \left[ \frac{\partial J^e}{\partial S^e} \right]_{V, M} dS^e \quad (20.9)$$

and then identifying this expression with the fundamental thermodynamic relation (20.7) to reveal

$$\left[ \frac{\partial J^e}{\partial S^e} \right]_{V, M} = T \quad (20.10)$$

$$\left[ \frac{\partial J^e}{\partial V} \right]_{S^e, M} = -p. \quad (20.11)$$

Each equation relates an intensive property (right hand side) to the partial derivative of internal energy with respect to an extensive property. Furthermore, since each of the extensive properties is a homogeneous function of degree one, then it follows that the intensive properties are homogeneous functions of degree zero. That is, the intensive properties,  $T$  and  $p$ , do not scale with the size of the system. Rather, intensive properties are scale invariant. We arrive at analogous partial derivative identities for entropy,  $S^e(V, J^e)$ , by expanding its exact differential and then comparing

to equation (20.8)

$$\left[ \frac{\partial S^e}{\partial \mathcal{I}^e} \right]_{V,M} = \frac{1}{T} \quad (20.12)$$

$$\left[ \frac{\partial S^e}{\partial V} \right]_{\mathcal{I}^e,M} = \frac{p}{T}. \quad (20.13)$$

Recall that partial derivatives are defined with the complement variables held fixed during the differentiation. Hence, so long as we are clear about functional dependence, extra subscripts such as those exposed in equations (20.10)-(20.11) are not needed for the partial derivatives. Nonetheless, traditional thermodynamic notation exposes all of the subscripts in order to remain explicit about the dependent and independent variables. Such notation, though clumsy, can be essential when in the midst of manipulations with thermodynamic potentials and their derivatives.

### 20.2.7 Entropy and reversible/irreversible processes

A *reversible process* can, at each stage, go either forward or backward in time so that there is symmetry in time. In the absence of non-conservative forces (e.g., dissipation such as friction), Newton's dynamical laws are reversible. For example, one observes nothing unphysical about the motion of an ideal pendulum with time moving backward rather than forward.

From a thermodynamic perspective, a reversible process does not alter the net entropy of a physical system plus its surrounding environment. Reversible thermodynamic processes are quasi-static and yet not all quasi-static processes are reversible. For example, a process that involves friction can evolve quasi-statically and yet frictional processes, as with any dissipative process, increases entropy. When the net entropy changes, we say the process occurs *irreversibly*, with the second law of thermodynamics stating that the net entropy change is positive. Quasi-static is a property of how a system changes, whereas reversibility is a statement about how both the system and its surrounding environment change. Any natural process is irreversible, with irreversibility providing an arrow for the evolution of physical systems; i.e., it breaks the symmetry between past and future.

The entropy increment for a quasi-static process in a materially closed system is given by  $dS^e = dQ/T$ , with  $T > 0$  (recall  $T$  is the Kelvin thermodynamic temperature) so that the entropy increment has the same sign as the heating increment, and entropy for a materially closed system remains unchanged in the absence of heating. The idealization of a heat bath allows us to perform reversible heating; i.e., heating without change in net entropy for a thermodynamic system plus the heat bath. Heat baths are held at a fixed temperature, which is the idealization of the case when the surrounding environment is arbitrarily larger than the thermodynamic system under consideration. Now imagine exchanging heat between a thermodynamic system and a series of heat baths to progressively alter the system's temperature by differential increments  $dT$ . In each exchange of heat, the entropy of the system plus heat bath is constructed to remain unchanged since we are exchanging an equal magnitude of entropy between them

$$dS_{\text{net}}^e = dS_{\text{system}}^e + dS_{\text{bath}}^e = dQ/T - dQ/T = 0. \quad (20.14)$$

To reverse the process, we merely reverse the heat exchanges between the thermodynamic system and the heat baths.

As noted above, when any thermodynamic process occurs irreversibly there is a net increase in entropy of the universe, which is a statement of the second law of thermodynamics. In statistical mechanics, entropy is computed by counting the number of microstates accessible to any given macrostate. Reversible processes do not modify the number of accessible microstates so there is

zero change in the entropy. In contrast, irreversible processes increase entropy by increasing the number of accessible microstates.

### 20.2.8 Thermodynamic equilibrium

Consider two systems labelled<sup>3</sup> by  $\alpha$  and  $\beta$  that are separately in thermodynamic equilibrium with internal energies,  $\mathcal{I}_\alpha^e$ ,  $\mathcal{I}_\beta^e$ , and volumes,  $V_\alpha$ ,  $V_\beta$ . Allow these two systems to interact mechanically and thermally, but do not allow for any exchange of matter. Furthermore, assume that the interactions conserve the total internal energy and volume of the combined system so that the system maintains the following constraints during the interaction process

$$d(\mathcal{I}_\alpha^e + \mathcal{I}_\beta^e) = 0 \quad \text{and} \quad d(V_\alpha + V_\beta) = 0. \quad (20.15)$$

When the composite system reaches thermodynamic equilibrium, the entropy maximum postulate forming the second law of thermodynamics (Section 20.1.7) means that

$$dS^e = d(S_\alpha^e + S_\beta^e) = 0 \quad (20.16)$$

for the combined composite system. Importantly, this condition holds only at equilibrium, whereas the constraints (20.15) hold throughout the process of reaching equilibrium. From equation (20.8) we know that entropy is naturally a function of volume and internal energy so that

$$dS^e = \left[ \frac{\partial S_\alpha^e}{\partial \mathcal{I}_\alpha^e} \right]_{V_\alpha, M_\alpha} d\mathcal{I}_\alpha^e + \left[ \frac{\partial S_\alpha^e}{\partial V_\alpha} \right]_{\mathcal{I}_\alpha^e, M_\alpha} dV_\alpha + \left[ \frac{\partial S_\beta^e}{\partial \mathcal{I}_\beta^e} \right]_{V_\beta, M_\beta} d\mathcal{I}_\beta^e + \left[ \frac{\partial S_\beta^e}{\partial V_\beta} \right]_{\mathcal{I}_\beta^e, M_\beta} dV_\beta \quad (20.17a)$$

$$= \frac{1}{T_\alpha} d\mathcal{I}_\alpha^e + \frac{p_\alpha}{T_\alpha} dV_\alpha + \frac{1}{T_\beta} d\mathcal{I}_\beta^e + \frac{p_\beta}{T_\beta} dV_\beta \quad (20.17b)$$

$$= \left[ \frac{1}{T_\alpha} - \frac{1}{T_\beta} \right] d\mathcal{I}_\alpha^e + \left[ \frac{p_\alpha}{T_\alpha} - \frac{p_\beta}{T_\beta} \right] dV_\alpha, \quad (20.17c)$$

where we used the partial derivative identities (20.12) and (20.13) for the second equality, and the constraints (20.15) for the final equality. Again,  $dS^e = 0$  at thermodynamic equilibrium, and this condition holds for arbitrary and independent  $d\mathcal{I}_\alpha^e$  and  $dV_\alpha$ . We are thus led to the thermal and mechanical equilibrium conditions

$$T_\alpha = T_\beta \quad \text{and} \quad p_\alpha = p_\beta \quad \text{at thermodynamic equilibrium.} \quad (20.18)$$

That is, the temperature and pressure are uniform when the composite system reaches thermodynamic equilibrium.

To understand how the two systems thermally approach thermodynamic equilibrium, assume the volumes of the two systems are fixed so that there is no mechanical work from pressure. Furthermore, assume the two systems are initially separated by an adiabatic wall with initial temperatures  $T_\alpha^{\text{init}} > T_\beta^{\text{init}}$ . Now allow for the flow of heat by switching from an adiabatic wall to a diathermal wall. Since the temperature differs for the two systems, they are mutually out of equilibrium. Heat flows in a manner to bring the two systems into equilibrium, during which time entropy of the composite system increases. At the new equilibrium, temperature is uniform and entropy has reached its maximum within the constraints imposed on the composite system. At a time instant after the wall changes from adiabatic to diathermal, the infinitesimal entropy

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<sup>3</sup>The labels  $\alpha$  and  $\beta$  are not tensor labels. Instead, they merely label the system under consideration.

change takes the form

$$d\mathcal{S}^e = \left[ \frac{1}{T_\alpha^{\text{init}}} - \frac{1}{T_\beta^{\text{init}}} \right] d\mathcal{J}_\alpha^e > 0, \quad (20.19)$$

where the inequality follows from the second law of thermodynamics (Section 20.1.7). If  $T_\alpha^{\text{init}} > T_\beta^{\text{init}}$ , then an increase in entropy requires  $d\mathcal{J}_\alpha^e < 0$ , which means that heat leaves the system  $\alpha$  and flows to the system  $\beta$ . That is, as the composite system approaches thermodynamic equilibrium, heat flows from the region with higher temperature to the region with lower temperature. This result, deduced from the second law of thermodynamics, accords with common experience.

Further to the time scale for equilibration, we note that mechanical equilibrium (pressure equality) generally arises much sooner than thermal equilibrium (temperature equality). The reason is that mechanical equilibrium is facilitated by force imbalances that lead to macroscopic motion (e.g., acoustic waves), whereas thermal equilibrium arises from microscopic motion (e.g., molecular diffusion).

### 20.2.9 Thermodynamic equilibrium with macroscopic motion

We here ask what kind of macroscopic motion is available that maintains a thermodynamic equilibrium.<sup>4</sup> When a macroscopic system is in motion then its total energy is the sum of the internal energy plus kinetic energy<sup>5</sup>

$$\mathcal{E}^e = \mathcal{I}^e + P^2/(2M), \quad (20.20)$$

where  $\mathbf{P} = M\mathbf{v}$  is the linear momentum of the system with velocity  $\mathbf{v}$  and mass  $M$ , and  $P^2 = \mathbf{P} \cdot \mathbf{P}$  is the squared momentum. If the macroscopic system is materially closed then total energy remains constant, as does the linear momentum and angular momentum. Thermodynamic equilibrium is realized by maximizing the function

$$\Psi = \mathcal{S}^e + \mathbf{A} \cdot \mathbf{P} + \mathbf{B} \cdot (\mathbf{x} \times \mathbf{P}), \quad (20.21)$$

where  $\mathbf{x}$  is the position of the macroscopic system, and the vectors  $\mathbf{A}$  and  $\mathbf{B}$  are constant Lagrange multipliers. Note that for convenience we assume the system to be macroscopically small but microscopically large (e.g., a fluid element) so that we can assign a single position vector to the system.

Should entropy be a function of the total energy (which is a constant of the motion) or remain a function of just the internal energy? To answer this question we appeal to the statistical interpretation of entropy whereby the number of microstates corresponding to a particular macrostate is Galilean invariant.<sup>6</sup> The local rest state, where total energy equals to internal energy, is thus sufficient for defining the functional dependence<sup>7</sup>

$$\mathcal{S}^e = \mathcal{S}^e(V, \mathcal{I}^e) = \mathcal{S}^e[V, \mathcal{E}^e - P^2/(2M)]. \quad (20.22)$$

Hence, maximizing  $\Psi$  with respect to the linear momentum component,  $P_m$ , requires the derivative

$$\left[ \frac{\partial \mathcal{S}^e}{\partial P_m} \right]_V = \left[ \frac{\partial \mathcal{S}^e}{\partial \mathcal{I}^e} \right]_V \frac{\partial \mathcal{I}^e}{\partial P_m} = -\frac{1}{T} \frac{P_m}{M} = -\frac{v_m}{T}, \quad (20.23)$$

<sup>4</sup>The discussion in this subsection follows §10 in [Landau and Lifshitz \(1980\)](#).

<sup>5</sup>We assume there are no external fields such as from gravity.

<sup>6</sup>Recall our discussion of Galilean invariance in Section 12.6.

<sup>7</sup>See footnote on page 36 of [Landau and Lifshitz \(1980\)](#) for more discussion.

so that the macroscopic velocity at equilibrium is

$$\frac{\partial \Psi}{\partial P_m} = 0 \implies \mathbf{v} = T(\mathbf{A} + \mathbf{B} \times \mathbf{x}). \quad (20.24)$$

With temperature uniform throughout the macroscopic system at thermodynamic equilibrium, then we find a velocity decomposed into a uniform translation plus a solid-body rotation. That is, a closed macroscopic system in thermodynamic equilibrium can, at most, exhibit uniform translation plus solid-body rotation. More general macroscopic motion is not possible when the system is in thermodynamic equilibrium. Furthermore, note that each component of the rate of strain tensor vanishes for uniform translation plus a solid-body rotation (see Exercise 13.2). For the Newtonian fluids considered in this book, a zero rate of strain means there are no frictional stresses (Section 18.7.6), thus ensuring no frictionally generated entropy.

To extend the ideas of thermodynamic equilibrium to moving geophysical fluids in Chapter 21, we assume the fluid continuum is decomposed into tiny fluid elements that are macroscopically small but microscopically large, with each fluid element in a local thermodynamic equilibrium at each time instance. The Cauchy-Stokes decomposition from Section 13.3.9 shows that at each time instance, motion of the fluid element can be kinematically decomposed into translation, rotation, and dilation. Dilation occurs through mechanical work. In its absence, and without heating or mixing, the fluid element moves through sequences of translations and rotations that maintain thermodynamic equilibrium. With dilation, heating, and/or matter mixing, we conceive of a moving fluid as a continuum of fluid elements that, on a time scale that is tiny relative to macroscopic processes, adjusts to thermodynamic equilibrium in response to interactions with the surrounding fluid environment.

## 20.3 Characterizing materially open systems

Thermodynamic systems are generally open to the transfer of matter across its boundaries. We here summarize methods used to characterize systems and processes that allow for the movement of matter.

### 20.3.1 Euler's theorem for homogeneous functions

Consider a suite of  $Q$  independent variables,  $X_1, X_2, \dots, X_Q$ , and an arbitrary function of these variables,  $F(X_1, X_2, \dots, X_Q)$ . We say that this function is a *homogeneous function* of degree  $\gamma$  if the following property holds

$$F(\lambda X_1, \lambda X_2, \dots, \lambda X_Q) = \lambda^\gamma F(X_1, X_2, \dots, X_Q), \quad (20.25)$$

with  $\lambda$  an arbitrary scalar. The left hand side is the function evaluated with each of the independent variables scaled by the same number,  $\lambda$ . The right hand side is the function evaluated with the unscaled variables, but multiplied by the scale raised to the power  $\gamma$ . A particularly remarkable and useful property of such functions can be found by taking  $\partial/\partial\lambda$  on both sides of the identity (20.25). The left hand side has the following partial derivative, as found through the

chain rule

$$\begin{aligned}\frac{\partial F(\lambda X_1, \lambda X_2, \dots, \lambda X_Q)}{\partial \lambda} &= \frac{\partial F(X_1, X_2, \dots, X_Q)}{\partial X_1} \frac{\partial(\lambda X_1)}{\partial \lambda} + \dots + \frac{\partial F(X_1, X_2, \dots, X_Q)}{\partial X_Q} \frac{\partial(\lambda X_Q)}{\partial \lambda} \\ &= \sum_{q=1}^Q \left[ \frac{\partial F(X_1, X_2, \dots, X_Q)}{\partial X_q} \right]_{X_r \neq q} X_q\end{aligned}\quad (20.26)$$

The derivative of the right hand side of equation (20.25) is given by

$$\frac{\partial[\lambda^\gamma F(X_1, X_2, \dots, X_Q)]}{\partial \lambda} = \gamma \lambda^{\gamma-1} F(X_1, X_2, \dots, X_Q). \quad (20.27)$$

Bringing these results together leads to *Euler's theorem* for homogeneous functions

$$\sum_{m=1}^Q X_q \left[ \frac{\partial F(X_1, X_2, \dots, X_Q)}{\partial X_q} \right]_{X_r \neq q} = \gamma \lambda^{\gamma-1} F(X_1, X_2, \dots, X_Q). \quad (20.28)$$

Intensive thermodynamic properties are homogeneous functions of degree  $\gamma = 0$ , meaning they are scale invariant. For example, a bucket of homogeneous water has the same temperature whether or not we remove an arbitrary sample of the water. In contrast, as discussed below, extensive thermodynamic properties are homogeneous functions of degree  $\gamma = 1$ .

### 20.3.2 Homogeneous functions of degree one

Both the internal energy,  $\mathcal{I}^e$ , and entropy,  $\mathcal{S}^e$ , are extensive properties of a fluid system. Consequently, the transfer of matter across the system boundaries leads to an additive change in  $\mathcal{I}^e$  and  $\mathcal{S}^e$ . The internal energy and entropy thus have their natural functional dependencies (20.7) and (20.8) extended to include the matter content

$$\mathcal{I}^e = \mathcal{I}^e(V, \mathcal{S}^e, M_n) \quad \text{and} \quad \mathcal{S}^e = \mathcal{S}^e(V, \mathcal{I}^e, M_n), \quad (20.29)$$

where the  $M_n$  argument is shorthand for  $M_1, M_2, \dots, M_N$  for the  $N$  matter constituents.

What happens when we scale the system by an arbitrary parameter  $\lambda$ ? Under this scale operation, the extensive variables,  $\mathcal{I}^e$ ,  $\mathcal{S}^e$ , as well as the volume,  $V$ , and masses,  $M_n$ , scale by the same scale factor. The relation (20.29) thus leads to the scaling

$$\lambda \mathcal{I}^e(V, \mathcal{S}^e, M_n) = \mathcal{I}^e(\lambda V, \lambda \mathcal{S}^e, \lambda M_n) \quad \text{and} \quad \lambda \mathcal{S}^e(V, \mathcal{I}^e, M_n) = \mathcal{S}^e(\lambda V, \lambda \mathcal{I}^e, \lambda M_n), \quad (20.30)$$

thus revealing that  $\mathcal{I}^e(V, \mathcal{S}^e, M_n)$  and  $\mathcal{S}^e(\lambda V, \lambda \mathcal{I}^e, \lambda M_n)$  are homogeneous functions of degree one. Making use of Euler's theorem (20.28) with  $\gamma = 1$  leads to

$$\mathcal{I}^e(V, \mathcal{S}^e, M_n) = V \left[ \frac{\partial \mathcal{I}^e}{\partial V} \right]_{\mathcal{S}^e, M_n} + \mathcal{S}^e \left[ \frac{\partial \mathcal{I}^e}{\partial \mathcal{S}^e} \right]_{V, M_n} + \sum_{n=1}^N M_n \left[ \frac{\partial \mathcal{I}^e}{\partial M_n} \right]_{V, \mathcal{S}^e, M_{m \neq n}} \quad (20.31a)$$

$$\mathcal{S}^e(V, \mathcal{I}^e, M_n) = V \left[ \frac{\partial \mathcal{S}^e}{\partial V} \right]_{\mathcal{I}^e, M_n} + \mathcal{I}^e \left[ \frac{\partial \mathcal{S}^e}{\partial \mathcal{I}^e} \right]_{V, M_n} + \sum_{n=1}^N M_n \left[ \frac{\partial \mathcal{S}^e}{\partial M_n} \right]_{V, \mathcal{I}^e, M_{m \neq n}}. \quad (20.31b)$$

These are very special expressions for the internal energy and entropy that are of great use throughout thermodynamics.

### 20.3.3 Chemical potential and the Euler form

We can further massage the results (20.31a) and (20.31b) by making use of the partial derivative identities from Section 20.2.6 to render

$$\mathcal{I}^e = -pV + T\mathcal{S}^e + \sum_{n=1}^N M_n \left[ \frac{\partial \mathcal{I}^e}{\partial M_n} \right]_{V,\mathcal{S}^e,M_{m \neq n}} \quad (20.32)$$

$$T\mathcal{S}^e = pV + \mathcal{I}^e + \sum_{n=1}^N T M_n \left[ \frac{\partial \mathcal{S}^e}{\partial M_n} \right]_{V,\mathcal{I}^e,M_{m \neq n}}. \quad (20.33)$$

Self-consistency requires

$$\left[ \frac{\partial \mathcal{I}^e}{\partial M_n} \right]_{V,\mathcal{S}^e} = -T \left[ \frac{\partial \mathcal{S}^e}{\partial M_n} \right]_{V,\mathcal{I}^e,M_{m \neq n}}, \quad (20.34)$$

which motivates defining the *chemical potential*

$$\mu_n \equiv \left[ \frac{\partial \mathcal{I}^e}{\partial M_n} \right]_{V,\mathcal{S}^e,M_{m \neq n}} = -T \left[ \frac{\partial \mathcal{S}^e}{\partial M_n} \right]_{V,\mathcal{I}^e,M_{m \neq n}} \quad (20.35)$$

thus leading to

$$\mathcal{I}^e = T\mathcal{S}^e - pV + \sum_{n=1}^N \mu_n M_n \iff T\mathcal{S}^e = \mathcal{I}^e + pV - \sum_{n=1}^N \mu_n M_n. \quad (20.36)$$

These are the *Euler forms* for the internal energy and entropy.

By definition, the chemical potential,  $\mu_n$ , is an intensive property that measures the change in the internal energy,  $\mathcal{I}^e$ , when altering the mass,  $M_n$ , of the constituent  $n$ , while fixing the entropy, volume, and mass of the other components. Equivalently, it is minus the temperature weighted change in the entropy,  $\mathcal{S}^e$ , when altering the mass,  $M_n$  while fixing the volume, internal energy, and mass of the other components. We can define a chemical potential for a single component system, in which it is the change arising from altering the mass of the system. Despite its name, the chemical potential does not necessarily refer to the existence of chemical reactions, though we note that it does appear prominently in the thermodynamics of chemical reactions ([Atkins and de Paula, 2006](#)).

### 20.3.4 Molar mass and molar chemical potential

It is sometimes convenient to write the mass of a constituent as the product of the number of moles,  $N_n$ , and the mass per mole,  $\mathfrak{M}_n$  (the *molar mass*), so that

$$M_n = N_n \mathfrak{M}_n \quad \text{no implied sum.} \quad (20.37)$$

In this way, an infinitesimal mass change is given by

$$dM = \sum_{n=1}^N dM_n = \sum_{n=1}^N d(N_n \mathfrak{M}_n) = \sum_{n=1}^N \mathfrak{M}_n dN_n, \quad (20.38)$$

so that mass changes are signalled by changes in the number of moles. We furthermore note the identity (no implied sum)

$$M_n \mu_n = M_n \left[ \frac{\partial \mathcal{J}^e}{\partial M_n} \right]_{V, S^e, M_m \neq n} = N_n \mathfrak{m}_n \left[ \frac{\partial \mathcal{J}^e}{\partial (N_n \mathfrak{m}_n)} \right]_{V, S^e, N_m \neq n} = N_n \tilde{\mu}_n, \quad (20.39)$$

where we defined the molar chemical potential determined according to mole number

$$\tilde{\mu}_n = \left[ \frac{\partial \mathcal{J}^e}{\partial N_n} \right]_{V, S^e, N_m \neq n} = \mathfrak{m}_n \mu_n. \quad (20.40)$$

We are similarly led to the identities (no implied sum)

$$M_n d\mu_n = N_n d\tilde{\mu}_n \quad \text{and} \quad \mu_n dM_n = \tilde{\mu}_n dN_n. \quad (20.41)$$

### 20.3.5 Chemical work and the Gibbs-Duhem relation

Changes to the matter composition of a system changes the internal energy through *chemical work*, written as  $d\mathcal{C}$ . If the changes to the matter composition occur quasi-statically then the chemical work is written

$$d\mathcal{C} = \sum_{n=1}^N \mu_n dM_n = \sum_{n=1}^N \tilde{\mu}_n dN_n \quad (20.42)$$

so that the chemical potential is the integrating factor connecting the inexact differential measuring the chemical work to the exact differential change in matter content. The chemical potential is the energy absorbed or released due to an infinitesimal change in the matter content. As shown in Section 20.5.2, matter in a mixture tends to move from regions of high chemical potential to lower chemical potential, thus motivating the name “potential” in analog to the gravitational potential.

The inclusion of chemical work brings the first law of thermodynamics to the form

$$d\mathcal{J}^e = d\mathcal{W} + d\mathcal{Q} + d\mathcal{C} \quad \text{materially open} \quad (20.43a)$$

$$d\mathcal{J}^e = -p dV + T dS^e + \sum_{n=1}^N \mu_n dM_n \quad \text{quasi-static and materially open.} \quad (20.43b)$$

Use of the quasi-static form of the first law (20.43b) along with the differential of the result (20.36) leads to the *Gibbs-Duhem* relation<sup>8</sup>

$$S^e dT - V dp + \sum_{n=1}^N M_n d\mu_n = 0. \quad (20.44)$$

As a corollary we see that for processes occurring at constant temperature and pressure that

$$\sum_{n=1}^N M_n d\mu_n = \sum_{n=1}^N N_n d\tilde{\mu}_n = 0 \quad \text{constant } T, p. \quad (20.45)$$

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<sup>8</sup>In Exercise 20.1 we work through the derivation of Gibbs-Duhem (20.44) in a bit more detail.

### 20.3.6 Gibbs potential

We offer a formal study of thermodynamic potentials in Section 20.7. Among those, we find Gibbs potential most useful for geophysical fluid mechanics and thus introduce it here

$$\mathcal{G}^e = \mathcal{I}^e - T \mathcal{S}^e + p V = \sum_{n=1}^N \mu_n M_n. \quad (20.46)$$

The reason that the Gibbs potential is so useful is that it is a natural function of temperature, pressure, and matter content,

$$\mathcal{G}^e = \mathcal{G}^e(T, p, M_n), \quad (20.47)$$

with  $T, p, M_n$  readily measured properties. This convenient functional dependence is confirmed by taking the differential,  $d\mathcal{G}^e$ , and using the fundamental thermodynamic relation (20.43b) to find

$$d\mathcal{G}^e = -\mathcal{S}^e dT + V dp + \sum_{n=1}^N \mu_n dM_n. \quad (20.48)$$

In turn, we can derive the following partial derivatives,

$$\left[ \frac{\partial \mathcal{G}^e}{\partial T} \right]_{p, M_n} = -\mathcal{S}^e \quad \text{and} \quad \left[ \frac{\partial \mathcal{G}^e}{\partial p} \right]_{T, M_n} = V \quad \text{and} \quad \left[ \frac{\partial \mathcal{G}^e}{\partial M_n} \right]_{p, T, M_{m \neq n}} = \mu_n \quad (20.49)$$

along with the second derivative identities

$$\left[ \frac{\partial \mu_n}{\partial p} \right]_{T, M_n} = \frac{\partial}{\partial p} \left[ \frac{\partial \mathcal{G}^e}{\partial M_n} \right]_{p, T, M_{m \neq n}} = \frac{\partial}{\partial M_n} \left[ \frac{\partial \mathcal{G}^e}{\partial p} \right]_{p, T, M_{m \neq n}} = \left[ \frac{\partial V}{\partial M_n} \right]_{p, T, M_{m \neq n}} \quad (20.50a)$$

$$\left[ \frac{\partial \mu_n}{\partial T} \right]_{p, M_n} = \frac{\partial}{\partial T} \left[ \frac{\partial \mathcal{G}^e}{\partial M_n} \right]_{p, T, M_{m \neq n}} = \frac{\partial}{\partial M_n} \left[ \frac{\partial \mathcal{G}^e}{\partial T} \right]_{p, M_n} = - \left[ \frac{\partial \mathcal{S}^e}{\partial M_n} \right]_{p, T, M_{m \neq n}}. \quad (20.50b)$$

The second derivative identities are particular *Maxwell relations*. Maxwell relations result from commutativity of the partial derivative operation.

### 20.3.7 Extensive functions of $(T, p, M_n)$

Just as for the internal energy and entropy, the Gibbs function,  $\mathcal{G}^e(T, p, M_n)$ , is an extensive function. Since the temperature and pressure are both intensive properties, we follow the scale analysis from Section 20.3.2 to arrive at the Euler form of the Gibbs function

$$\mathcal{G}^e(T, p, M_n) = \sum_{n=1}^N M_n \left[ \frac{\partial \mathcal{G}^e}{\partial M_n} \right]_{p, T, M_{m \neq n}} = \sum_{n=1}^N \mu_n M_n, \quad (20.51)$$

which is consistent with the definition (20.46). Indeed, any extensive property written as a function of  $(T, p, M_n)$  can be written in the same fashion. For example, the internal energy,

entropy, and volume take the form

$$\mathcal{I}^e(T, p, M_n) = \sum_{n=1}^N M_n \left[ \frac{\partial \mathcal{I}^e}{\partial M_n} \right]_{p,T,M_{m \neq n}} = \sum_{n=1}^N N_n \left[ \frac{\partial \mathcal{I}^e}{\partial N_n} \right]_{p,T,N_{m \neq n}} \quad (20.52a)$$

$$\mathcal{S}^e(T, p, M_n) = \sum_{n=1}^N M_n \left[ \frac{\partial \mathcal{S}^e}{\partial M_n} \right]_{p,T,M_{m \neq n}} = \sum_{n=1}^N N_n \left[ \frac{\partial \mathcal{S}^e}{\partial N_n} \right]_{p,T,N_{m \neq n}} \quad (20.52b)$$

$$V(T, p, M_n) = \sum_{n=1}^N M_n \left[ \frac{\partial V}{\partial M_n} \right]_{p,T,M_{m \neq n}} = \sum_{n=1}^N N_n \left[ \frac{\partial V}{\partial N_n} \right]_{p,T,N_{m \neq n}}. \quad (20.52c)$$

The partial derivatives,  $[\partial(\mathcal{G}^e, \mathcal{I}^e, \mathcal{S}^e, V)/\partial N_n]_{p,T,N_{m \neq n}}$ , are intensive properties known as the *partial Gibbs potential*, *partial internal energy*, *partial entropy*, and *partial volume*. These relations mean that we can regard each of the extensive quantities as the sum of contributions from each of the material components as determined by their partial properties. For the particular case of a single matter component we have

$$\mathcal{G}^e(T, p, M) = M \left[ \frac{\partial \mathcal{G}^e}{\partial M} \right]_{p,T} = \mu M \quad (20.53a)$$

$$\mathcal{I}^e(T, p, M) = M \left[ \frac{\partial \mathcal{I}^e}{\partial M} \right]_{p,T} = N \left[ \frac{\partial \mathcal{I}^e}{\partial N} \right]_{p,T} \quad (20.53b)$$

$$\mathcal{S}^e(T, p, M) = M \left[ \frac{\partial \mathcal{S}^e}{\partial M} \right]_{p,T} = N \left[ \frac{\partial \mathcal{S}^e}{\partial N} \right]_{p,T} \quad (20.53c)$$

$$V(T, p, M) = M \left[ \frac{\partial V}{\partial M} \right]_{p,T} = N \left[ \frac{\partial V}{\partial N} \right]_{p,T}. \quad (20.53d)$$

## 20.4 Materially open single-component systems

Consider a single-component fluid ( $N = 1$ ) that consists of two regions or systems, labelled by  $\alpha$  and  $\beta$ , with each of these two systems separately in thermodynamic equilibrium. Assume the composite system is enclosed in a container with fixed volume,  $V_\alpha + V_\beta = V$ . Allow the two systems to interact thermally, mechanically, and materially. What are the properties of thermodynamic equilibrium for the composite system,  $\alpha \oplus \beta$ ?

To answer this question, we follow the procedure in Section 20.2.8, only here considering the case where matter flows between the systems, in addition to thermal transfer and mechanical interactions, with such interactions occurring as the composite system approaches thermodynamic equilibrium. Initially, the  $\alpha$  and  $\beta$  systems are separately in thermodynamic equilibrium with internal energies, volumes, and masses given by  $(\mathcal{I}_\alpha^e, \mathcal{I}_\beta^e)$ , volumes,  $(V_\alpha, V_\beta)$ , and  $(M_\alpha, M_\beta)$ . During the process of reaching equilibrium, the internal energy, volume, and mass of the composite system remains constant so that<sup>9</sup>

$$d(\mathcal{I}_\alpha^e + \mathcal{I}_\beta^e) = 0 \quad \text{and} \quad d(V_\alpha + V_\beta) = 0 \quad \text{and} \quad d(M_\alpha + M_\beta) = 0. \quad (20.54)$$

From equation (20.29) we know that entropy is a natural function of volume, internal energy, and

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<sup>9</sup>We assume there is no macroscopic mechanical energy, so that the total energy is the internal energy.

mass of each matter constituent. With only a single matter constituent we have

$$dS^e = \frac{1}{T_\alpha} d\mathcal{I}_\alpha^e + \frac{p_\alpha}{T_\alpha} dV_\alpha - \frac{\mu_\alpha}{T_\alpha} dM_\alpha + \frac{1}{T_\beta} d\mathcal{I}_\beta^e + \frac{p_\beta}{T_\beta} dV_\beta - \frac{\mu_\beta}{T_\beta} dM_\beta \quad (20.55a)$$

$$= \left[ \frac{1}{T_\alpha} - \frac{1}{T_\beta} \right] d\mathcal{I}_\alpha^e + \left[ \frac{p_\alpha}{T_\alpha} - \frac{p_\beta}{T_\beta} \right] dV_\alpha - \left[ \frac{\mu_\alpha}{T_\alpha} - \frac{\mu_\beta}{T_\beta} \right] dM_\alpha, \quad (20.55b)$$

where we used the partial derivative identities (20.12), (20.13), and (20.35). As before,  $dS^e = 0$  at thermodynamic equilibrium, and this condition holds for arbitrary and independent  $d\mathcal{I}_\alpha^e$ ,  $dV_\alpha$ , and  $dM_\alpha$ . We are thus led to the thermal, mechanical, and material conditions for thermodynamic equilibrium

$$T_\alpha = T_\beta \quad \text{and} \quad p_\alpha = p_\beta \quad \text{and} \quad \mu_\alpha = \mu_\beta. \quad (20.56)$$

That is, the temperature, pressure, and chemical potential are uniform when the composite system reaches thermodynamic equilibrium. Note that this condition for thermodynamic equilibrium means that each term in the Gibbs-Duhem relation (20.44) separately vanishes. Furthermore, since the Gibbs potential equals to the mass times the chemical potential for a single component system (equation (20.51)), equality of the chemical potentials at equilibrium means that

$$\mu_\alpha = \mu_\beta \implies \frac{\mathcal{G}_\alpha^e}{M_\alpha} = \frac{\mathcal{G}_\beta^e}{M_\beta}. \quad (20.57)$$

As for the direction of heat flow discussed in Section 20.2.8, we can determine the direction for matter flow as  $\alpha \oplus \beta$  approaches thermodynamic equilibrium. For this purpose, assume the temperature and volumes are already uniform, but the matter content initially differs. At the instance the two systems start interacting, the entropy increment is given by

$$T dS^e = -(\mu_\alpha - \mu_\beta) dM_\alpha > 0, \quad (20.58)$$

where  $T$  is the equilibrium temperature of the two systems, and where the inequality holds according to the second law of thermodynamics (Section 20.1.7). If  $\mu_\alpha > \mu_\beta$ , then this inequality requires  $dM_\alpha < 0$ . Hence, in the process of approaching thermodynamic equilibrium, matter flows from regions of high chemical potential to regions of low chemical potential. This behavior allows us to consider the chemical potential in a manner directly akin to temperature. That is, temperature differences measure the potential for heat to be fluxed, and likewise chemical potential differences measure the potential for matter to be fluxed. The chemical potential is central to the study of changes in matter states (e.g., solid to liquid, liquid to gas), as well as for chemical reactions (e.g., *Guggenheim*, 1967; *Atkins and de Paula*, 2006).

## 20.5 Thermodynamic equilibrium with a geopotential

Geophysical fluids feel the effects from gravity. So what does thermodynamic equilibrium look like in the presence of a gravity field? To answer that question, we here consider a single-component system in the presence of a static gravity field. To further connect to geophysical fluids, we let the geopotential,  $\Phi$ , represent the effects from central gravity plus the planetary centrifugal acceleration (Section 9.12.4). Throughout this analysis, we assume the acceleration from the geopotential is prescribed and is thus not affected by the mass of the thermodynamic system that feels the geopotential. Furthermore, we assume the force from the geopotential is terrestrial, so

that it is weak enough to ignore general relativistic effects.<sup>10</sup>

### 20.5.1 The first law

As seen in Section 20.2.3, a thermodynamic system subjected to a pressure field undergoes pressure work as its volume changes. Analogously, when the mass of a thermodynamic system changes within a geopotential field, then it is subjected to geopotential work, which takes the form

$$dW_{\text{geopotential}} = \Phi dM. \quad (20.59)$$

We thus see that the geopotential is an intensive property with mass its corresponding extensive property. Consequently, the first law for a quasi-static process is modified from equation (20.43b) to now read

$$dJ^e = -p dV + T dS^e + (\mu + \Phi) dM \iff dS^e = T^{-1} [p dV + dJ^e - (\mu + \Phi) dM], \quad (20.60)$$

where  $\mu$  is the chemical potential in the absence of a geopotential

$$\left[ \frac{\partial J^e}{\partial M} \right]_{V, S^e} = \mu + \Phi \quad \text{and} \quad \left[ \frac{\partial J^e}{\partial M} \right]_{V, S^e, \Phi=0} = \mu. \quad (20.61)$$

The corresponding Gibbs-Duhem relation (20.44) now takes on the form

$$-V dp + S^e dT + M d(\mu + \Phi) = 0. \quad (20.62)$$

### 20.5.2 Thermodynamic equilibrium

Following our discussion in Section 20.4, we consider two adjoining fluid regions that are allowed to adjust toward thermodynamic equilibrium in the presence of a geopotential field. The entropy increment in equation (20.55b) now takes on the form

$$dS^e = \left[ \frac{1}{T_\alpha} - \frac{1}{T_\beta} \right] dJ_\alpha^e + \left[ \frac{p_\alpha}{T_\alpha} - \frac{p_\beta}{T_\beta} \right] dV_\alpha - \left[ \frac{\mu_\alpha + \Phi_\alpha}{T_\alpha} - \frac{\mu_\beta + \Phi_\beta}{T_\beta} \right] dM_\alpha, \quad (20.63)$$

which follows from the constraints (20.54) that assume fixed internal energy, mass, and volume for the composite system  $\alpha \oplus \beta$ . Equilibrium is characterized by  $dS^e = 0$ , which leads to a uniform temperature, as for the case with uniform  $\Phi$ . A further naive extension of Section 20.4 suggests that  $dp = 0$  and  $d(\mu + \Phi) = 0$  at equilibrium. However, our understanding of fluid statics leads us to expect pressure to vary according to the hydrostatic balance (Section 17.3). That is, a uniform pressure is not does not arise when there is a nonuniform geopotential.

To recover hydrostatic balance at thermodynamic equilibrium, consider the case with each volume remaining fixed

$$d(J_\alpha^e + J_\beta^e) = 0 \quad \text{and} \quad dV_\alpha = dV_\beta = 0 \quad \text{and} \quad d(M_\alpha + M_\beta) = 0. \quad (20.64)$$

An example consists of two vertically positioned fluid boxes, with  $\nabla\Phi$  defining the local vertical and with adjustment towards equilibrium consisting of mass moving from one box to the other. Note that by fixing each of the region volumes, pressure does no work so that internal energy

<sup>10</sup>The relevant non-dimensional ratio is given by  $\Phi/c^2$ , with  $c$  the speed of light. See [Santiago and Visser \(2018\)](#) for a concise review of how gravity leads to a spatially dependent temperature in thermal equilibrium through Tolman's temperature gradient. These considerations are important when  $\Phi/c^2$  is order unity. For terrestrial purposes,  $\Phi/c^2 \lll 1$ , so that relativistic gravitational effects are entirely negligible.

changes only through entropy and mass changes

$$d\mathcal{I}^e = T dS^e + (\mu + \Phi) dM \iff dS^e = T^{-1} [d\mathcal{I}^e - (\mu + \Phi) dM]. \quad (20.65)$$

Correspondingly, we find that thermodynamic equilibrium results when

$$dT = 0 \quad \text{and} \quad d(\mu + \Phi) = 0. \quad (20.66)$$

To interpret the new equilibrium condition,  $d(\mu + \Phi) = 0$ , take the derivative with respect to geopotential, holding temperature and mass fixed, to render

$$\left[ \frac{\partial \mu}{\partial \Phi} \right]_{T,M} = -1. \quad (20.67)$$

Anticipating the hydrostatic balance, we assume that pressure at thermodynamic equilibrium is a monotonic function of  $\Phi$ , so that

$$\left[ \frac{\partial \mu}{\partial \Phi} \right]_{T,M} = \left[ \frac{\partial \mu}{\partial p} \right]_{T,M} \left[ \frac{dp}{d\Phi} \right]_{T,M} = -1. \quad (20.68)$$

Making use of the Maxwell relation (20.50a) and the identity (20.53d) leads to

$$\left[ \frac{dp}{d\Phi} \right]_{T,M} = -M/V = -\rho, \quad (20.69)$$

where  $\rho = M/V$  is the density. We thus recover the exact hydrostatic balance (Section 17.3)

$$dp = -\rho d\Phi. \quad (20.70)$$

That is, thermodynamic equilibrium in a gravity field consists of a uniform temperature with pressure satisfying the exact hydrostatic balance.

### 20.5.3 Further study

Outside of general relativity (e.g., [Tolman, 1934](#)), there are few presentations of gravity within standard thermodynamic texts. Chapter 9 of [Guggenheim \(1967\)](#) and §25 of [Landau and Lifshitz \(1980\)](#) are notable exceptions, with our presentation following [Landau and Lifshitz \(1980\)](#).

## 20.6 Materially open systems with fixed total mass

In our study of geophysical fluids, we make use of a continuum of fluid elements. Each fluid element is open mechanically, thermally, and materially while maintaining constant mass as it quasi-statically evolves through local thermodynamic equilibrium states. Hence, when formulating the equations of linear irreversible thermodynamics in Chapter 21, we make use of thermodynamic equations written in their “per unit mass” form. Here we present these equations, as well as extend our understanding of the formalism.

### 20.6.1 Matter concentrations

We generally make use of matter or tracer concentration as written

$$C_n = M_n/M \implies \sum_{n=1}^N C_n = 1, \quad (20.71)$$

with the constant mass constraint  $\sum_{n=1}^N C_n = 1$  meaning that only  $N - 1$  of the concentrations are linearly independent. We also introduced tracer concentrations in Section 15.1 when developing the tracer equation.

### 20.6.2 Fundamental thermodynamic relation per unit mass

We scale away the mass of the system by setting the scale factor  $\lambda = M^{-1}$  in our discussion in Section 20.3.2 of how extensive properties scale. The result is the *specific* (per mass) versions of the extensive properties

$$\mathcal{I}^e = M \mathcal{I} \quad (20.72a)$$

$$\mathcal{S}^e = M \mathcal{S} \quad (20.72b)$$

$$V = M \nu_s \quad (20.72c)$$

$$M_n = M C_n, \quad (20.72d)$$

where

$$\nu_s = 1/\rho \quad (20.73)$$

is the specific volume and the total mass,  $M$ , is held fixed. In the equality (20.72d),  $C_n$  is the mass fraction or concentration of species  $n$  in the fluid (Section 20.6.1). Substituting the specific quantities (20.72a)-(20.72d) into the fundamental thermodynamic relation (20.43b) leads to the fundamental thermodynamic relation in terms of specific thermodynamic quantities

$$d\mathcal{I} = T d\mathcal{S} - p d\nu_s + \sum_n \mu_n dC_n. \quad (20.74)$$

This is the form of the fundamental thermodynamic relation most commonly used in this book. Again, this relation holds for quasi-static processes that hold the total mass of the system fixed, thus making it relevant for our study of constant mass fluid elements in Chapter 21.

### 20.6.3 Seawater as a binary fluid

The atmosphere is a multi-component and multi-phase fluid that is well approximated as a mixture of water vapor and dry air. However, we do not consider moist atmospheric processes in this book nor do we consider phases changes. In contrast, there are many occasions in this book that require us to consider seawater as a binary fluid system of salt dissolved in fresh water so that their concentrations satisfy the constraint

$$C_{\text{salt}} + C_{\text{water}} = 1 \implies dC_{\text{water}} = -dC_{\text{salt}}. \quad (20.75)$$

We are thus able to write the Gibbs fundamental thermodynamic relation (20.74) in the form

$$d\mathcal{I} = T d\mathcal{S} - p d\nu_s + \mu_{\text{water}} dC_{\text{water}} + \mu_{\text{salt}} dC_{\text{salt}} \quad (20.76a)$$

$$= T d\mathcal{S} - p d\nu_s + \mu dC, \quad (20.76b)$$

where

$$C = C_{\text{salt}} \quad (20.77)$$

is the concentration of salt (mass of salt per mass of seawater), and

$$\mu = \mu_{\text{salt}} - \mu_{\text{water}} \quad (20.78)$$

is the *relative chemical potential*, often referred to as the *seawater chemical potential*. We return in Section 20.78 to discuss how the chemical potentials are computed according to partial derivatives of the Gibbs potential, which is the preferred method for the ocean and atmosphere.

The *absolute salinity*  $S$ , with units parts per thousand (gram per kilogram), is related to  $C_{\text{salt}}$  via

$$S = 1000 C_{\text{salt}}. \quad (20.79)$$

The range of absolute salinity in the ocean (roughly  $0 \leq S \leq 40$ ) is more convenient than the range of  $C_{\text{salt}}$ , making salinity more commonly used in oceanography.

#### 20.6.4 Further study

Chapters 1 and 2 of [Olbers et al. \(2012\)](#) provide a more complete suite of thermodynamic relations for seawater.

## 20.7 Thermodynamic potentials

Internal energy and entropy are referred to as state functions (functions only of the current state) as well as *thermodynamic potentials*, and they are related by equation (20.36), here written in its specific form as appropriate for constant mass fluid elements

$$\mathcal{I} = T \mathcal{S} - p \nu_s + \sum_{n=1}^N \mu_n C_n \iff T \mathcal{S} = \mathcal{I} + p \nu_s - \sum_{n=1}^N \mu_n C_n. \quad (20.80)$$

Each thermodynamic potential is a natural function of certain other thermodynamic properties, as determined by the fundamental thermodynamic relation.

It is useful to have access to a suite of thermodynamic potentials (internal energy, entropy, enthalpy, Gibbs potential, Helmboltz free energy) that have different functional dependencies, which in turn yield distinct expressions for the fundamental equation of state. Thermodynamic potentials are related mathematically through a *Legendre transformation*. Motivation for their introduction comes from the distinct laboratory and environmental conditions whereby the controlling parameters may differ. In this section we introduce the variety of thermodynamic potentials commonly used for fluid mechanics, and exhibit their natural functional dependencies. We specialize to the case of a binary fluid, which is most commonly the case for the ocean and atmosphere. Generalization to more components is straightforward.

We emphasize the importance of committing to a single choice for the thermodynamic potential when manipulating thermodynamic equations. The reason to adhere to a single choice is that functional dependencies change when switching to a different thermodynamic potential, thus exposing oneself to mistakes when swapping midstream to another formulation.

#### 20.7.1 Equations of state

Equations (20.10), (20.11), and (20.35) provide expressions for intensive properties,  $T$ ,  $p$ , and  $\mu_n$ , in terms of the partial derivatives of the internal energy in terms of extensive functions  $\mathcal{S}^e$ ,  $V$ ,

and  $M_n$ . We thus conclude that we can write  $T$ ,  $p$ , and  $\mu_n$  in the functional form

$$T = T(\mathcal{S}^e, V, M_m) \quad \text{and} \quad p = p(\mathcal{S}^e, V, M_m) \quad \text{and} \quad \mu_n = \mu_n(\mathcal{S}^e, V, M_m). \quad (20.81)$$

These equations are known as *equations of state*. Knowledge of all the equations of state is equivalent to knowledge of the fundamental thermodynamic relation (20.43b). In the following, we develop similar equations of state based on other thermodynamic potentials.

### 20.7.2 Internal energy

Recall the fundamental thermodynamic relation (20.76b) written for a binary fluid<sup>11</sup>

$$d\mathcal{J} = T d\mathcal{S} - p d\nu_s + \mu dC. \quad (20.82)$$

Equation (20.82) identifies the specific internal energy,  $\mathcal{J}$ , as a natural function of specific entropy,  $\mathcal{S}$ , specific volume,  $\nu_s$ , and matter concentration,  $C$

$$\mathcal{J} = \mathcal{J}(\mathcal{S}, \nu_s, C). \quad (20.83)$$

Knowledge of the fundamental thermodynamic relation (20.82) allows us to derive a variety of thermodynamic relations via partial differentiation. For example, we can identify

$$\left[ \frac{\partial \mathcal{J}}{\partial \mathcal{S}} \right]_{\nu_s, C} = T \quad \text{and} \quad \left[ \frac{\partial \mathcal{J}}{\partial \nu_s} \right]_{\mathcal{S}, C} = -p \quad \text{and} \quad \left[ \frac{\partial \mathcal{J}}{\partial C} \right]_{\mathcal{S}, \nu_s} = \mu, \quad (20.84)$$

which are the specific (per mass) forms of equations (20.10), (20.11), and (20.35).

We see that equations (20.84) provide a relation between  $T, p, \mu$  as derivatives of a function, the internal energy, which is itself a function  $\mathcal{J}(\mathcal{S}, \nu_s, C)$ . Hence, we may consider  $T, p, \mu$  each as a function of  $(\mathcal{S}, \nu_s, C)$ , and thus write the equations of state

$$T = T(\mathcal{S}, \nu_s, C) \quad \text{and} \quad p = p(\mathcal{S}, \nu_s, C) \quad \text{and} \quad \mu = \mu(\mathcal{S}, \nu_s, C), \quad (20.85)$$

which are the equations of state (20.81) written in terms of specific (per mass) quantities. In turn, the exact differentials of the intensive properties are

$$dT = \left[ \frac{\partial T}{\partial \mathcal{S}} \right]_{\nu_s, C} d\mathcal{S} + \left[ \frac{\partial T}{\partial \nu_s} \right]_{C, \mathcal{S}} d\nu_s + \left[ \frac{\partial T}{\partial C} \right]_{\mathcal{S}, \nu_s} dC \quad (20.86)$$

$$dp = \left[ \frac{\partial p}{\partial \mathcal{S}} \right]_{\nu_s, C} d\mathcal{S} + \left[ \frac{\partial p}{\partial \nu_s} \right]_{C, \mathcal{S}} d\nu_s + \left[ \frac{\partial p}{\partial C} \right]_{\mathcal{S}, \nu_s} dC \quad (20.87)$$

$$d\mu = \left[ \frac{\partial \mu}{\partial \mathcal{S}} \right]_{\nu_s, C} d\mathcal{S} + \left[ \frac{\partial \mu}{\partial \nu_s} \right]_{C, \mathcal{S}} d\nu_s + \left[ \frac{\partial \mu}{\partial C} \right]_{\mathcal{S}, \nu_s} dC. \quad (20.88)$$

### 20.7.3 Entropy

Rearrangement of the fundamental thermodynamic relation (20.82) leads to the exact differential for specific entropy

$$d\mathcal{S} = \frac{1}{T} d\mathcal{J} + \frac{p}{T} d\nu_s - \frac{\mu}{T} dC. \quad (20.89)$$

<sup>11</sup>If there are more than two matter constituents, then the term  $\mu dC$  appearing in these formula become  $\sum_{n=1}^N \mu_n dC_n$ . Partial derivatives are also modified accordingly. We choose the binary case since it is typically sufficient for the earth's atmosphere and ocean.

In this form, specific entropy has the functional dependence

$$\mathcal{S} = \mathcal{S}(\mathcal{I}, \nu_s, C), \quad (20.90)$$

whose knowledge provides yet another form of the fundamental equation of state. This functional dependence, along with equation (20.89), lead to the following identities

$$\left[ \frac{\partial \mathcal{S}}{\partial \mathcal{I}} \right]_{\nu_s, C} = \frac{1}{T} \quad \text{and} \quad \left[ \frac{\partial \mathcal{S}}{\partial \nu_s} \right]_{\mathcal{I}, C} = \frac{p}{T} \quad \text{and} \quad \left[ \frac{\partial \mathcal{S}}{\partial C} \right]_{\mathcal{I}, \nu_s} = -\frac{\mu}{T}. \quad (20.91)$$

As for internal energy in Section 20.7.2, equation (20.91) provides a relation between  $T, p, \mu$  as derivatives of a function, the entropy, which is itself a function  $\mathcal{S}(\mathcal{I}, \nu_s, C)$ . Hence, we may consider  $T, p, \mu$  as each a function of  $(\mathcal{I}, \nu_s, C)$  to thus write the equations of state

$$T = T(\mathcal{I}, \nu_s, C) \quad \text{and} \quad p = p(\mathcal{I}, \nu_s, C) \quad \text{and} \quad \mu = \mu(\mathcal{I}, \nu_s, C). \quad (20.92)$$

## 20.7.4 Enthalpy

Thus far we have worked only with the fundamental thermodynamic relation (20.82). We now introduce the specific enthalpy

$$\mathcal{H} = \mathcal{I} + p \nu_s = T \mathcal{S} + \sum_{n=1}^N \mu_n C_n, \quad (20.93)$$

where the second equality made use of equation (20.80). Use of the fundamental thermodynamic relation (20.82) leads to the exact differential for enthalpy

$$d\mathcal{H} = d\mathcal{I} + d(p \nu_s) \quad (20.94a)$$

$$= T d\mathcal{S} - p d\nu_s + \mu dC + p d\nu_s + \nu_s dp \quad (20.94b)$$

$$= T d\mathcal{S} + \nu_s dp + \mu dC \quad (20.94c)$$

Recalling that for quasi-static processes,  $T d\mathcal{S}$  equals to the thermal energy added to a fluid element. Hence, for processes occurring at constant pressure and constant matter content, changes in enthalpy are determined by the thermal energy added to the system. This connection motivates the name *heat function* sometimes applied to enthalpy.

Equation (20.94c) provides the fundamental thermodynamic relation with enthalpy rather than internal energy. Consequently, the *Legendre transformation* (20.93) renders a functional dependence for enthalpy

$$\mathcal{H} = \mathcal{H}(\mathcal{S}, p, C), \quad (20.95)$$

which in turn leads to the following partial derivative identities

$$\left[ \frac{\partial \mathcal{H}}{\partial \mathcal{S}} \right]_{p, C} = T \quad \text{and} \quad \left[ \frac{\partial \mathcal{H}}{\partial p} \right]_{\mathcal{S}, C} = \nu_s \quad \text{and} \quad \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{\mathcal{S}, p} = \mu. \quad (20.96)$$

As for internal energy in Section 20.7.2, equations (20.96) provide a relation between  $T, \nu_s, \mu$  as derivatives of a function, the enthalpy, which is itself a function  $\mathcal{H}(\mathcal{S}, p, C)$ . Hence, we may consider  $T, \nu_s, \mu$  as each a function of  $(\mathcal{S}, p, C)$  to thus render the following equations of state

$$T = T(\mathcal{S}, p, C) \quad \text{and} \quad \nu_s = \nu_s(\mathcal{S}, p, C) \quad \text{and} \quad \mu = \mu(\mathcal{S}, p, C). \quad (20.97)$$

Enthalpy's functional dependence (20.95) is more convenient for studies of geophysical fluids than that for internal energy,  $\mathcal{I}(S, \nu_s, C)$ , or for entropy  $S(\mathcal{I}, \nu_s, C)$ .

- In the laboratory or field, we generally have direct mechanical means for measuring pressure in a fluid, whereas specific volume requires indirect methods involving the equation of state for density discussed in Section 24.3.
- Correspondingly, the interaction between fluid elements typically occurs at near constant pressure. Hence, fluid elements exchange both their entropy and enthalpy when the exchange occurs as constant pressure.
- Specific entropy remains constant on a fluid element in the absence of mixing or other irreversible effects. Correspondingly, enthalpy remains constant for constant pressure motion without mixing. Conversely, in the presence of mixing at constant pressure, fluid elements mix their specific enthalpy, specific entropy, and tracer concentration.

### 20.7.5 Helmholtz free energy

The Helmholtz free energy is defined by the Legendre transformation

$$\mathcal{F} = \mathcal{I} - T S = -p \nu_s + \sum_{n=1}^N \mu_n C_n, \quad (20.98)$$

where the second equality made use of equation (20.80). The exact differential of the Helmholtz free energy is given by

$$d\mathcal{F} = d\mathcal{I} - d(T S) \quad (20.99a)$$

$$= d\mathcal{I} - T dS - S dT \quad (20.99b)$$

$$= -S dT - p d\nu_s + \mu dC, \quad (20.99c)$$

where we used the fundamental thermodynamic relation (20.76b) for the final equality. Isothermal and constant concentration processes render the changes to the free energy equal to the pressure work applied to the system.

The Helmholtz free energy has the functional dependence

$$\mathcal{F} = \mathcal{F}(T, \nu_s, C), \quad (20.100)$$

which then leads to the partial derivatives identities

$$\left[ \frac{\partial \mathcal{F}}{\partial T} \right]_{\nu_s, C} = -S \quad \text{and} \quad \left[ \frac{\partial \mathcal{F}}{\partial \nu_s} \right]_{T, C} = -p \quad \text{and} \quad \left[ \frac{\partial \mathcal{F}}{\partial C} \right]_{T, \nu_s} = \mu. \quad (20.101)$$

As for internal energy in Section 20.7.2, equations (20.101) provide a relation between  $S, p, \mu$  as derivatives of a function, the Helmholtz free energy, which is itself a function  $\mathcal{F}(T, \nu_s, C)$ . Hence, we may consider  $S, p, \mu$  each as a function of  $(T, \nu_s, C)$  to render the functional relations

$$S = S(T, \nu_s, C) \quad \text{and} \quad p = p(T, \nu_s, C) \quad \text{and} \quad \mu = \mu(T, \nu_s, C). \quad (20.102)$$

### 20.7.6 Gibbs potential

The Gibbs potential is defined by the Legendre transformation

$$\mathcal{G} = \mathcal{I} + p \nu_s - T \mathcal{S} = \mathcal{H} - T \mathcal{S} = \sum_{n=1}^N \mu_n C_n, \quad (20.103)$$

where the final equality made use of equation (20.80). The exact differential of the Gibbs potential is given by

$$d\mathcal{G} = d\mathcal{H} - d(T \mathcal{S}) \quad (20.104a)$$

$$= T d\mathcal{S} + \nu_s dp + \mu dC - T d\mathcal{S} - \mathcal{S} dT \quad (20.104b)$$

$$= -\mathcal{S} dT + \nu_s dp + \mu dC, \quad (20.104c)$$

where we made use of the fundamental thermodynamic relation (20.94c) written in terms of enthalpy. The Gibbs potential has the functional dependence

$$\mathcal{G} = \mathcal{G}(T, p, C), \quad (20.105)$$

which leads to the partial derivatives identities

$$\left[ \frac{\partial \mathcal{G}}{\partial T} \right]_{p,C} = -\mathcal{S} \quad \text{and} \quad \left[ \frac{\partial \mathcal{G}}{\partial p} \right]_{T,C} = \nu_s \quad \text{and} \quad \left[ \frac{\partial \mathcal{G}}{\partial C} \right]_{T,p} = \mu. \quad (20.106)$$

As for internal energy in Section 20.7.2, equations (20.106) provide a relation between  $\mathcal{S}, \nu_s, \mu$  as derivatives of a function, the Gibbs potential, which is itself a function  $\mathcal{G}(T, p, C)$ . Hence, we may consider  $\mathcal{S}, \nu_s, \mu$  each as a function of  $(T, p, C)$  to render the following functional relations

$$\mathcal{S} = \mathcal{S}(T, p, C) \quad \text{and} \quad \nu_s = \nu_s(T, p, C) \quad \text{and} \quad \mu = \mu(T, p, C). \quad (20.107)$$

The form of the fundamental dependencies (20.105), and the associated equations of state (20.107), are often used in fluid mechanics and physical chemistry. The reason is that temperature, pressure, and concentration are readily measured in the laboratory and the environment. We can thus readily measure the partial derivatives of  $\mathcal{G}$ , and the functional dependence (20.107) provides a convenient means to express  $\mathcal{S}, \nu_s$ , and  $\mu$  (e.g., see the adiabatic lapse rate discussion in Section 20.10).

Given its convenient functional dependence, the Gibbs potential plays a central role in developing the thermodynamics of seawater as formulated by [Feistel \(1993\)](#) and codified by [IOC et al. \(2010\)](#). We thus endeavor to exhibit how quantities (e.g., response functions as in Section 20.8) can be computed based on knowledge of the Gibbs potential and its partial derivatives. For example, use of equation (20.106) renders the expression for the enthalpy

$$\mathcal{H} = \mathcal{G} + T \mathcal{S} = \mathcal{G} - T \left[ \frac{\partial \mathcal{G}}{\partial T} \right]_{p,C}. \quad (20.108)$$

### 20.7.7 Chemical potential and the Gibbs potential

Throughout this section we have displayed equations for the chemical potential of a binary fluid in terms of the partial derivatives of the thermodynamic potentials, such as equation (20.106) using the Gibbs potential. Here we consider some details that lead to further understanding of the partial derivatives. We start by writing the chemical potential of fresh water and salt as

contained within seawater in terms of the partial derivatives of the extensive Gibbs potential

$$\mu_{\text{water}} = \left[ \frac{\partial \mathcal{G}^e}{\partial M_{\text{water}}} \right]_{T,p,M_{\text{salt}}} \quad \text{and} \quad \mu_{\text{salt}} = \left[ \frac{\partial \mathcal{G}^e}{\partial M_{\text{salt}}} \right]_{T,p,M_{\text{water}}}. \quad (20.109)$$

The total mass of a sample of seawater is given by  $M = M_{\text{water}} + M_{\text{salt}}$ . Consequently, to compute these partial derivatives requires us to alter the mass of the sample as we hold the mass of one component fixed while varying the mass of the other component. This sort of partial derivative is less convenient for our purposes since we prefer to work with constant mass samples, such as we encounter with constant mass fluid elements. For that purpose we introduce the specific Gibbs potential, in which case the chemical potential of fresh water is

$$\mu_{\text{water}} = \left[ \frac{\partial \mathcal{G}^e}{\partial M_{\text{water}}} \right]_{T,p,M_{\text{salt}}} = \left[ \frac{\partial(M \mathcal{G})}{\partial M_{\text{water}}} \right]_{T,p,M_{\text{salt}}} = \mathcal{G} + M \left[ \frac{\partial \mathcal{G}}{\partial M_{\text{water}}} \right]_{T,p,M_{\text{salt}}}. \quad (20.110)$$

The specific Gibbs potential is a natural function of  $T, p, C_n$ , and since  $C_{\text{water}} + C_{\text{salt}} = 1$  we can write the Gibbs potential in terms of just one of the concentrations, typically chosen as  $C_{\text{salt}}$ . We are thus led to

$$\mu_{\text{water}} = \mathcal{G} + M \left[ \frac{\partial \mathcal{G}}{\partial M_{\text{water}}} \right]_{T,p,M_{\text{salt}}} \quad (20.111a)$$

$$= \mathcal{G} + M \left[ \frac{\partial \mathcal{G}}{\partial C_{\text{water}}} \right]_{T,p} \left[ \frac{\partial C_{\text{water}}}{\partial M_{\text{water}}} \right]_{M_{\text{salt}}} \quad (20.111b)$$

where the concentration partial derivative is given by

$$\left[ \frac{\partial C_{\text{water}}}{\partial M_{\text{water}}} \right]_{M_{\text{salt}}} = \left[ \frac{\partial}{\partial M_{\text{water}}} \right]_{M_{\text{salt}}} \left[ \frac{M_{\text{water}}}{M_{\text{water}} + M_{\text{salt}}} \right] = \frac{C_{\text{salt}}}{M}, \quad (20.112)$$

thus leading to the chemical potential of fresh water within seawater

$$\mu_{\text{water}} = \mathcal{G} + C_{\text{salt}} \left[ \frac{\partial \mathcal{G}}{\partial C_{\text{water}}} \right]_{T,p} = \mathcal{G} - C_{\text{salt}} \left[ \frac{\partial \mathcal{G}}{\partial C_{\text{salt}}} \right]_{T,p}. \quad (20.113)$$

We are thus able to work with the specific Gibbs function for a constant mass fluid element and compute its concentration partial derivative. Similar manipulations lead to the chemical potential for salt within seawater

$$\mu_{\text{salt}} = \mathcal{G} + C_{\text{water}} \left[ \frac{\partial \mathcal{G}}{\partial C_{\text{salt}}} \right]_{T,p} = \mathcal{G} + (1 - C_{\text{salt}}) \left[ \frac{\partial \mathcal{G}}{\partial C_{\text{salt}}} \right]_{T,p}. \quad (20.114)$$

We are thus led to the seawater chemical potential

$$\mu = \mu_{\text{salt}} - \mu_{\text{water}} = \left[ \frac{\partial \mathcal{G}}{\partial C_{\text{salt}}} \right]_{T,p}, \quad (20.115)$$

which agrees with equation (20.106).

## 20.8 Response functions

*Response functions* measure the change in a thermodynamic property as the system is forced in some manner. We here introduce the heat capacity, thermal expansion coefficient, and haline

contraction coefficient, which are three response functions commonly encountered in ocean and atmospheric fluid mechanics.

### 20.8.1 Heat capacities

The heat capacity measures the change in heat associated with a change in temperature at constant matter composition. There are two distinct heat capacities generally considered in fluid mechanics: one with specific volume held fixed and the other with pressure held fixed

$$c_v \equiv \frac{1}{M} \left[ \frac{dQ}{dT} \right]_{\nu_s, C} \quad \text{SI units m}^2 \text{ s}^{-2} \text{ K}^{-1}. \quad (20.116)$$

$$c_p \equiv \frac{1}{M} \left[ \frac{dQ}{dT} \right]_{p, C} \quad \text{SI units m}^2 \text{ s}^{-2} \text{ K}^{-1}. \quad (20.117)$$

If heating occurs quasi-statically, we can make use of the equation (20.5) that relates heating and entropy, applied here in its specific (per mass) form  $M^{-1} dQ = T dS$ . The result is a state function form of the specific heat capacities

$$c_v = T \left[ \frac{\partial S}{\partial T} \right]_{\nu_s, C} = -T \left[ \frac{\partial}{\partial T} \right]_{\nu_s, C} \left[ \frac{\partial G}{\partial T} \right]_{p, C} \quad (20.118)$$

$$c_p = T \left[ \frac{\partial S}{\partial T} \right]_{p, C} = -T \left[ \frac{\partial}{\partial T} \right]_{p, C} \left[ \frac{\partial G}{\partial T} \right]_{p, C} \quad (20.119)$$

where the second equalities in both of the above equations introduced the Gibbs potential according to equation (20.106). Furthermore, we can make use of the fundamental thermodynamic relation (20.74) with specific volume and matter concentration held fixed to yield

$$c_v = T \left[ \frac{\partial S}{\partial T} \right]_{\nu_s, C} = \left[ \frac{\partial J}{\partial T} \right]_{\nu_s, C}. \quad (20.120)$$

The second form of  $c_v$  motivates the name *internal energy capacity* rather than heat capacity at fixed volume. Likewise, making use of the fundamental thermodynamic relation (20.94c) written in terms of enthalpy leads to the constant pressure heat capacity

$$c_p = T \left[ \frac{\partial S}{\partial T} \right]_{p, C} = \left[ \frac{\partial J}{\partial T} \right]_{p, C} + p \left[ \frac{\partial \nu_s}{\partial T} \right]_{p, C} = \left[ \frac{\partial H}{\partial T} \right]_{p, C}. \quad (20.121)$$

That is, the constant pressure heat capacity is equivalently referred to as the *enthalpy capacity*.

### 20.8.2 Thermal expansion coefficient

The thermal expansion coefficient measures relative changes in density as temperature changes at constant pressure and concentration

$$\alpha_T = -\frac{1}{\rho} \left[ \frac{\partial \rho}{\partial T} \right]_{p, C} = \frac{1}{\nu_s} \left[ \frac{\partial \nu_s}{\partial T} \right]_{p, C} = \frac{1}{(\partial G / \partial p)_{T, C}} \left[ \frac{\partial}{\partial T} \right]_{p, C} \left[ \frac{\partial G}{\partial p} \right]_{T, C} \quad (20.122)$$

where the final equality introduced the Gibbs function according to equation (20.106). The minus sign in the definition is introduced since density typically reduces when temperature increases, so that for most substances  $\alpha_T > 0$ . Freshwater near its freezing point is an important counter-example, with  $\alpha_T < 0$  allowing for solid ice to float on liquid water.

### 20.8.3 Haline contraction coefficient

A similar response function measures changes to density arising from changes in the salt concentration (salinity) in seawater

$$\beta_s = \frac{1}{\rho} \left[ \frac{\partial \rho}{\partial S} \right]_{p,T} = -\frac{1}{\nu_s} \left[ \frac{\partial \nu_s}{\partial S} \right]_{p,T} = -\frac{1}{(\partial \mathcal{G}/\partial p)_{T,S}} \left[ \frac{\partial \mathcal{G}}{\partial S} \right]_{T,p} \left[ \frac{\partial \mathcal{G}}{\partial p} \right]_{T,S} \quad (20.123)$$

where  $S = 1000 C$  is the salinity (20.79). Seawater density typically increases (fluid element volume contracts) when salinity increases, so that  $\beta_s > 0$ .

### 20.8.4 Sound speed

Changes in density with respect to pressure at a fixed entropy define the inverse squared sound speed<sup>12</sup>

$$\frac{1}{c_s^2} = \left[ \frac{\partial \rho}{\partial p} \right]_S = -\frac{1}{(\nu_s)^2} \left[ \frac{\partial \nu_s}{\partial p} \right]_S = -\frac{1}{[(\partial \mathcal{G}/\partial p)_{T,S}]^2} \left[ \frac{\partial \mathcal{G}}{\partial p} \right]_S \left[ \frac{\partial \mathcal{G}}{\partial p} \right]_{T,S}. \quad (20.124)$$

The sound speed is a strong function of pressure, generally increasing with higher pressure, as well as temperature, generally decreasing with lower temperature. For the ocean, these two effects compete when moving into the ocean interior. In the upper 500 m to 1000 m, decreasing temperatures cause the sound speed to reduce whereas at deeper regions the higher pressures overcome the temperature effect thus increasing the sound speed. The result is a sound speed minimum between 500 m and 1000 m. The sound speed minimum and the associated acoustic waveguide play an important role in ocean acoustics, in particular for how certain whales are able to communicate across ocean basins. We consider the sound speed for an ideal gas in Section 20.12.8.

## 20.9 Maxwell relations for homogeneous fluids

Thermodynamics makes use of basic properties of exact differentials for the purpose of developing identities between partial derivatives. Maxwell relations refer to a suite of partial derivative identities that follow from the equality of mixed second partial derivatives of thermodynamic potentials. We already made use of some Maxwell relations in Section 20.3.6 when discussing the Gibbs potential, and we use another in Section 20.10 for expressing the adiabatic lapse rate in terms of readily measurable thermo-mechanical properties. In this section we develop the Maxwell relations encountered with homogeneous fluids, with similar relations holding for multi-component fluids.

### 20.9.1 Maxwell relation from internal energy

As seen from Section 20.7.2, the natural functional dependence for internal energy in a homogeneous fluid is given by its fundamental thermodynamic relation (20.82)

$$d\mathcal{I} = \left[ \frac{\partial \mathcal{I}}{\partial S} \right]_{\nu_s} dS + \left[ \frac{\partial \mathcal{I}}{\partial \nu_s} \right]_S d\nu_s = T dS - p d\nu_s \implies \mathcal{I} = \mathcal{I}(S, \nu_s). \quad (20.125)$$

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<sup>12</sup>We discuss sound waves in Section 17.5.

The mixed second partial derivatives are equal

$$\left[ \frac{\partial}{\partial \nu_s} \right]_{S,C} \left[ \frac{\partial}{\partial S} \right]_{\nu_s,C} \mathcal{J} = \left[ \frac{\partial}{\partial S} \right]_{\nu_s,C} \left[ \frac{\partial}{\partial \nu_s} \right]_{S,C} \mathcal{J}, \quad (20.126)$$

so that, via the fundamental thermodynamic relation (20.125), we have the Maxwell relation

$$\left[ \frac{\partial T}{\partial \nu_s} \right]_S = - \left[ \frac{\partial p}{\partial S} \right]_{\nu_s}. \quad (20.127)$$

### 20.9.2 Summary of the Maxwell relations

The other thermodynamic potentials, and their associated fundamental thermodynamical relations, lead to further Maxwell relations as summarized here

$$d\mathcal{J} = T dS - p d\nu_s \implies \left[ \frac{\partial T}{\partial \nu_s} \right]_S = - \left[ \frac{\partial p}{\partial S} \right]_{\nu_s} \quad (20.128)$$

$$d\mathcal{H} = T dS + \nu_s dp \implies \left[ \frac{\partial T}{\partial p} \right]_S = \left[ \frac{\partial \nu_s}{\partial S} \right]_p \quad (20.129)$$

$$d\mathcal{G} = -S dT + \nu_s dp \implies \left[ \frac{\partial S}{\partial p} \right]_T = - \left[ \frac{\partial \nu_s}{\partial T} \right]_p. \quad (20.130)$$

$$d\mathcal{F} = -S dT - p d\nu_s \implies \left[ \frac{\partial S}{\partial \nu_s} \right]_T = \left[ \frac{\partial p}{\partial T} \right]_{\nu_s}. \quad (20.131)$$

These four Maxwell relations for homogeneous fluids involve permutations on cross derivatives of  $(T, S)$  and  $(p, \nu_s)$ . In statistical mechanics,  $(T, S)$  determine the density of accessible microscopic states forming the thermodynamic system, whereas  $(p, \nu_s)$  involves an external control parameter and its corresponding generalized force.

## 20.10 Adiabatic lapse rate

The temperature of a fluid can change without the transfer of heat. This *adiabatic* temperature change arises when the fluid pressure changes. We here introduce the *adiabatic lapse rate*, which measures the changes in temperature for a static fluid placed in a gravity field. There are two lapse rates commonly considered: one related to height and one related to pressure. We introduce some manipulations commonly performed with thermodynamic state functions and their partial derivatives, with the goal of expressing the lapse rate in terms of commonly measured response functions.

### 20.10.1 Isentropic rearrangement

Consider a finite region of a static fluid in a gravitational field. Assume the fluid is initially in a thin horizontal layer with a uniform temperature. Now rearrange the fluid into a vertical column, and do so without changing the entropy; i.e., without the transfer of heat across the fluid boundary (adiabatically) and without mixing. Performing this rearrangement raises the center of mass of the fluid system and thus increases the gravitational potential energy. This process thus requires mechanical work against the gravitational field.

Gravity makes pressure at the bottom of the vertical fluid column greater than at the top. This pressure difference modifies the temperature in the column. We seek a thermodynamic expression

for how changes in pressure affects changes in temperature for a static fluid, with the pressure changes imparted reversibly and adiabatically so that entropy does not change. Mathematically, we seek an expression for the partial derivative

$$\hat{\Gamma} \equiv \left[ \frac{\partial T}{\partial p} \right]_{C,S}, \quad (20.132)$$

which is known as the *adiabatic lapse rate*. The adiabatic lapse rate can be measured directly, with empirical expressions fit to laboratory measurements. Additionally, it is convenient to express it in terms of other thermodynamic response functions in order to garner further physical insight. The necessary manipulations form the bulk of this section.

### 20.10.2 Thermodynamic formulation

When the matter concentration is held fixed, the equation of state (20.107) allows us to consider entropy as a function of temperature and pressure so that

$$dS = \left[ \frac{\partial S}{\partial T} \right]_p dT + \left[ \frac{\partial S}{\partial p} \right]_T dp. \quad (20.133)$$

Substituting the definition of heat capacity from equation (20.119) leads to

$$T dS = c_p dT + T \left[ \frac{\partial S}{\partial p} \right]_T dp. \quad (20.134)$$

It is useful to eliminate  $(\partial S / \partial p)_T$  in favor of a more easily measurable quantity. For that purpose we make use of the Maxwell relation (20.130) to write

$$\left[ \frac{\partial S}{\partial p} \right]_T = - \left[ \frac{\partial \nu_s}{\partial T} \right]_p. \quad (20.135)$$

Introducing the thermal expansion coefficient (20.122) yields an expression for changes in entropy in terms of changes in temperature and pressure

$$T dS = c_p dT - T \left[ \frac{\partial \nu_s}{\partial T} \right]_p dp = c_p dT - \left[ \frac{T \alpha_T}{\rho} \right] dp. \quad (20.136)$$

Since  $c_p$  and  $\alpha_T$  are readily measurable response functions, the expression (20.136) is a useful means to compute infinitesimal entropy changes when matter concentration is held constant.

### 20.10.3 Adiabatic lapse rate for pressure changes

Equation (20.136) means that the change in temperature associated with motion through a pressure field, with  $dS = 0$  and  $dC = 0$ , can be written

$$\hat{\Gamma} = \left[ \frac{\partial T}{\partial p} \right]_{C,S} = \frac{T \alpha_T}{\rho c_p}. \quad (20.137)$$

Temperature indeed changes when pressure changes, even though there has been no heat exchanged with the environment. With  $\hat{\Gamma}$  so defined, we can write the entropy change in equation (20.136) as

$$T dS = c_p (dT - \hat{\Gamma} dp). \quad (20.138)$$

The term  $dT - \hat{\Gamma} dp$  subtracts from the *in situ* temperature increment the pressure induced changes in temperature. In Section 20.11 we introduce the *potential temperature*, which is defined just for the purpose of removing changes due to pressure.

#### 20.10.4 Adiabatic lapse rate for height changes

A static fluid in a gravity field is in exact hydrostatic balance, whereby the pressure at a point equals to the weight per area above that point (Section 17.3). Hydrostatic balance in a constant gravity field maintains the following relation between the pressure differential increment and the vertical differential increment

$$dp = -g \rho dz. \quad (20.139)$$

Use of the chain rule within the lapse rate expression (20.137) leads to

$$\Gamma = \left[ \frac{\partial T}{\partial z} \right]_{C,S} = \left[ \frac{\partial T}{\partial p} \right]_{C,S} \left[ \frac{\partial p}{\partial z} \right] = -\rho g \left[ \frac{T \alpha_T}{\rho c_p} \right] = -\frac{g T \alpha_T}{c_p}. \quad (20.140)$$

This form for the lapse rates measures the change in temperature (the *lapse*) within a constant composition fluid element as it is isentropically moved vertically through a hydrostatic pressure field.

#### 20.10.5 Further study

In Section 20.12.9 we consider the adiabatic lapse rate for the special case of a simple ideal gas. For this gas, the internal energy of a fluid element is represented entirely by its temperature, and pressure is caused solely by molecular thermal motion. For water, however, molecular interaction energies are important, and pressure arises not only from thermal motion but also from interaction forces of the densely packed molecules. It is these differences between the behavior of water and a perfect gas that were examined by [McDougall and Feistel \(2003\)](#) in terms of molecular dynamics. In particular, they note that the lapse rate, being proportional to the thermal expansion coefficient, can be negative when the thermal expansion is negative. A negative thermal expansion coefficient occurs in cool fresh water, such as the Baltic Sea. Hence, although work is done on the fluid element under increasing pressure, its temperature decreases in these cases.

The addition of water to the atmosphere modifies the lapse rate, as the air is then no longer well approximated by an ideal gas. Chapter 18 of [Vallis \(2017\)](#) offers a pedagogical discussion of the thermodynamics of a moist tropical atmosphere.

### 20.11 Potential temperature

As discussed in Section 20.5, thermodynamic equilibrium of a fluid in a geopotential field sees the hydrostatic pressure balancing the weight of fluid. Thermodynamic equilibrium is also characterized by a uniform *in situ* temperature,  $T$ , which requires removal of the temperature gradient associated with the adiabatic lapse rate discussed in Section 20.10. The molecular diffusive processes (see Section 21.8) that homogenize *in situ* temperature are very slow, so that geophysical fluids are rarely in thermodynamic equilibrium. We here introduce the notion of *potential temperature*, which offers a measure of temperature that removes the adiabatic lapse rate. With some qualifiers discussed below, turbulent mixing processes active in geophysical fluids lead to a nearly homogenous potential temperature. As such, potential temperature is a more practical thermodynamic tracer than *in situ* temperature.

### 20.11.1 Motivating the definition of potential properties

We observe that the processes of heating and cooling of the ocean occur predominantly near the ocean surface. In contrast, transport in the ocean interior is nearly adiabatic and isohaline (i.e., nearly isentropic). The physical picture is suggested whereby the surface ocean boundary layer experiences irreversible processes that set characteristics of water masses that move quasi-reversibly within the ocean interior. As a means to characterize and thus to label these *water masses*, oceanographers prefer to use properties that maintain constant values when moving within the quasi-isentropic ocean interior. Salinity is a good label for this purpose since it is only altered by mixing between waters of varying concentrations, and in turn it is materially constant in the absence of mixing.<sup>13</sup> This behavior constitutes a basic property of material tracers (tracers that measure the mass per mass of a constituent as discussed in Section 15.1). However, it is *not* a property of the *in situ* temperature,  $T$ , which changes even in the absence of mixing due to pressure effects. We are thus motivated to seek a thermodynamic property that evolves analogously to material tracers, so that it can be used as a second material label for fluid elements. A similar motivation stems from the analysis of atmospheric motions.

A thermodynamic property that remains constant when a fluid element is moved from one pressure to another, without the transfer of heat or matter and without any kinetic energy dissipation, is said to be a *potential property*. The *potential temperature* is the example that concerns us in this section. As we will see, in some special cases the potential temperature is directly proportional to the specific entropy. More practically, it offers a means to estimate the heat transport within a geophysical fluid.

*Conservative Temperature*,  $\Theta$ , is another potential property discussed in Section 21.8, with Conservative Temperature defined as the potential enthalpy divided by a constant heat capacity. As detailed in [McDougall \(2003\)](#), Conservative Temperature provides a more convenient and accurate measure of heat transport in a geophysical fluid than potential temperature. As such,  $\Theta$  is now more commonly used in applications than potential temperature,  $\theta$ , ([McDougall et al., 2021](#)).

### 20.11.2 Temperature changes from pressure changes

Motion of a fluid element, without exchange of heat (adiabatic) or matter (constant concentration), generally changes the pressure of the fluid element. In turn, this motion causes the *in situ* temperature to change in proportion to the adiabatic lapse rate given by (Section 20.10)

$$dT = \hat{\Gamma} dp. \quad (20.141)$$

Consequently, and as already noted, the *in situ* temperature is not a useful thermodynamic variable to label fluid elements since it changes even in the absence of irreversible mixing processes. Instead, it is more useful to remove the adiabatic pressure effects. This is the key reason for introducing potential temperature.

### 20.11.3 Defining the potential temperature

Operationally, the potential temperature is based on removing adiabatic pressure effects from *in situ* temperature. That is, potential temperature is defined as the *in situ* temperature that a fluid element of fixed material composition would have if it were isentropically transported

<sup>13</sup>There are nuances concerning what we mean by “salinity”, with details given by [IOC et al. \(2010\)](#) (in particular, see Sections A.8 and A.9). We are not directly concerned with these nuances in this book, though note that they are important for ocean measurements and the interpretation of salinity as used in numerical ocean models ([McDougall et al., 2021](#)).

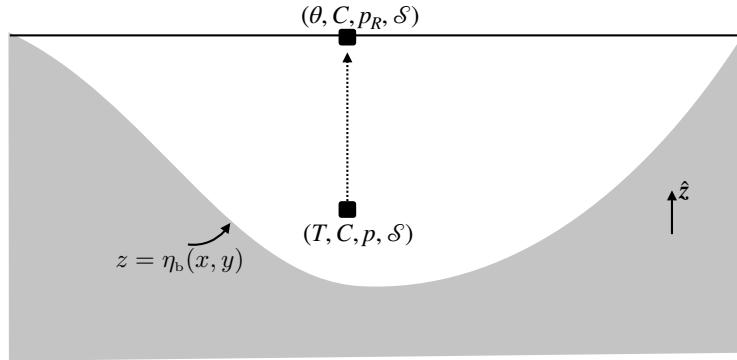


FIGURE 20.1: Potential temperature is the *in situ* temperature that a fluid element of fixed material composition would have if isentropically displaced from its *in situ* pressure to a reference pressure,  $p_R$ . The schematic here depicts that displacement for a seawater fluid element with *in situ* temperature,  $T$ , salinity,  $S = 1000 C$ , pressure,  $p$ , and specific entropy,  $S$ . The element is moved to the ocean surface with the standard sea level atmospheric pressure providing the reference pressure.

from its *in situ* pressure to a reference pressure  $p_R$ , with the reference pressure typically taken at the ocean/land surface (see Figure 20.1). Mathematically, the potential temperature,  $\theta$ , is the reference temperature obtained via integration of  $dT = \hat{\Gamma} dp$  for an isentropic *in situ* temperature change with respect to pressure

$$\int_{\theta}^T dT' = \int_{p_R}^p \hat{\Gamma}(T, p', C) dp' \implies T = \theta(T, p_R, C) + \int_{p_R}^p \hat{\Gamma}(T, p', C) dp', \quad (20.142)$$

with  $\hat{\Gamma}$  the lapse rate defined in terms of pressure changes (equation (20.137)). By definition, the *in situ* temperature,  $T$ , equals the potential temperature,  $\theta$ , at the reference pressure,  $p = p_R$ . Elsewhere, they differ by an amount determined by the adiabatic lapse rate. Furthermore, we see that

$$\left[ \frac{\partial T}{\partial p} \right]_{C,S} = \left[ \frac{\partial \theta}{\partial p} \right]_{C,S} + \hat{\Gamma}. \quad (20.143)$$

However, by definition

$$\left[ \frac{\partial T}{\partial p} \right]_{C,S} = \hat{\Gamma} \quad (20.144)$$

so that

$$\left[ \frac{\partial \theta}{\partial p} \right]_{C,S} = 0. \quad (20.145)$$

That is, by construction, the potential temperature depends explicitly on the concentration,  $C$ , and *in situ* temperature,  $T$ , and has a parametric dependence on the reference pressure. It has no explicit dependence on the *in situ* pressure when holding tracer concentration and entropy fixed. Finally, we emphasize that the potential temperature is a function of tracer concentration,  $C$ . Hence, the potential temperature generally changes if the tracer concentration changes. For example, potential temperature in the ocean changes if the salinity changes.

#### 20.11.4 Potential temperature and specific entropy

An alternative definition of the potential temperature follows by noting that the entropy of a fluid element remains unchanged as it is reversibly moved to the reference pressure. Consequently,

writing entropy as a function of the *in situ* temperature, pressure, and matter concentration as in equation (20.107)

$$\mathcal{S} = \mathcal{S}(T, p, C) \quad (20.146)$$

leads to the defining identity for potential temperature

$$\mathcal{S} = \mathcal{S}(T, p, C) = \mathcal{S}(\theta, p_R, C). \quad (20.147)$$

This relation directly connects changes in entropy to changes in potential temperature

$$d\mathcal{S} = \left[ \frac{\partial \mathcal{S}(\theta, p_R, C)}{\partial \theta} \right]_C d\theta. \quad (20.148)$$

Consequently, the reversible transport of a fluid element with constant matter concentration ( $dC = 0$ ) occurs with both a constant specific entropy and constant potential temperature.

We can go even further than the relation (20.148) by recalling that equation (20.138) relates increments in specific entropy to temperature and pressure

$$T d\mathcal{S} = c_p (dT - \hat{\Gamma} dp), \quad (20.149)$$

where  $\hat{\Gamma}$  is the adiabatic lapse rate defined in terms of pressure changes (equation (20.137)), and we set  $dC = 0$ . To relate  $dT - \hat{\Gamma} dp$  to  $d\theta$  we write the potential temperature equation (20.142) in the form

$$\theta(T, p_R, C) = T - \int_{p_R}^p \hat{\Gamma}(T, p', C) dp' = T - \Psi(T, p, C, p_R), \quad (20.150)$$

so that the differential increments are given by

$$d\theta = dT - d\Psi. \quad (20.151)$$

We evaluate  $d\Psi$  using the chain rule and then specialize to the case of constant composition and with a fixed reference pressure

$$d\Psi = \frac{\partial \Psi}{\partial T} dT + \frac{\partial \Psi}{\partial p} dp + \frac{\partial \Psi}{\partial C} dC + \frac{\partial \Psi}{\partial p_R} dp_R \quad (20.152a)$$

$$= \frac{\partial \Psi}{\partial T} dT + \frac{\partial \Psi}{\partial p} dp \quad (20.152b)$$

$$\equiv \int_{p_R}^p \frac{\partial \hat{\Gamma}(T, p', C)}{\partial T} dp' + \hat{\Gamma}(T, p, C) dp. \quad (20.152c)$$

Evaluating this increment at the reference pressure removes the integral so that

$$d\Psi = \hat{\Gamma}(T, p_R, C) dp, \quad (20.153)$$

in which case the potential temperature increment is

$$d\theta = dT - \hat{\Gamma}(T, p_R, C) dp. \quad (20.154)$$

Making use of this relation in equation (20.149) renders an expression for the entropy increment in terms of the potential temperature increment

$$d\mathcal{S} = c_p \theta^{-1} d\theta \quad p = p_R \text{ and } dC = 0. \quad (20.155)$$

Although evaluated at the reference pressure, as part of exercise 21.6 we see that this relation holds for an ideal gas at all pressures. Furthermore, as part of exercise 21.7 we see that this relation also holds for all pressures in certain liquids.

## 20.12 A simple ideal gas atmosphere

In an ideal gas, intermolecular forces between molecules are ignored. Also, the molecules in an ideal gas are assumed to occupy zero volume (i.e., they are point particles), although they do collide elastically. As a result, the internal energy of an ideal gas is just due to translation, rotation, and vibration of molecules. We refer to a *simple ideal gas* as an ideal gas where the internal energy is a linear function of temperature. In this section we develop a variety of thermodynamic relations for a simple ideal gas atmosphere in exact hydrostatic balance. Although the real atmosphere is moving, and thus not in exact hydrostatic balance, and the real atmosphere is not a simple ideal gas, it turns out that many of the relations established here are rather accurate approximations to the real atmosphere. Furthermore, by exposing these relations for the ideal gas, we further our understanding of the more general thermodynamic relations established earlier in this chapter.

### 20.12.1 Equation of state

An ideal gas satisfies the following equation of state (see Section 11.3.2)

$$PV = n R_g T, \quad (20.156)$$

where  $p$  is the pressure,  $V$  is the volume,  $n$  is the number of moles,

$$R_g = 8.314 \text{ J mole}^{-1} \text{ K}^{-1} = 8.314 \text{ kg m}^2 \text{ s}^{-2} \text{ mole}^{-1} \text{ K}^{-1} \quad (20.157)$$

is the *universal gas constant*, and  $T$  is the absolute temperature in Kelvin (see Section 11.3.2). The number of moles equals to the mass,  $M$ , of the gas divided by the mass per mole,  $M_{\text{mole}}$

$$n = M/M_{\text{mole}}. \quad (20.158)$$

The mass density,  $\rho = M/V$ , is thus given by

$$\rho = \frac{p M_{\text{mole}}}{T R_g} \equiv \frac{p}{T R^M}, \quad (20.159)$$

where

$$R^M = R_g/M_{\text{mole}} \quad (20.160)$$

is the *specific gas constant* as defined by the universal gas constant normalized by the molar mass for the constituent. For air we have (Section 11.3.2)

$$M_{\text{air}} = 28.8 \times 10^{-3} \text{ kg mole}^{-1} \quad (20.161)$$

so that air's specific gas constant is

$$R^{\text{air}} = \frac{R_g}{M_{\text{air}}} = \frac{8.314 \text{ kg m}^2 \text{ s}^{-2} \text{ mole}^{-1} \text{ K}^{-1}}{28.8 \times 10^{-3} \text{ kg mole}^{-1}} = 2.938 \times 10^2 \text{ m}^2 \text{ s}^{-2} \text{ K}^{-1}. \quad (20.162)$$

The relation (20.159) is known as a *thermal equation of state*, or more succinctly just an equation of state (see Section 24.3 for more discussion). It shows that the mass density of an ideal

gas is directly proportional to the pressure: increasing pressure increases density. In contrast, mass density is inversely proportional to the temperature: increases in temperature lead to lower mass density. This behavior for the ideal gas density is reflected in certain real gases and liquids.<sup>14</sup>

### 20.12.2 Internal energy

An ideal gas is comprised of molecules that interact only through elastic collisions. There are no inter-molecular forces. Furthermore, the volume of the individual molecules is ignored in comparison to the volume of empty space between the molecules, so they are approximated as point masses. Consequently, the internal energy for an ideal gas is independent of density and of the matter concentration. It is hence a function only of the temperature, which measures the kinetic energy of the elastic point molecules

$$\mathcal{I} = \mathcal{I}(T) \quad \text{ideal gas.} \quad (20.163)$$

Consequently, the exact differential of internal energy for an ideal gas is

$$d\mathcal{I} = c_v dT. \quad (20.164)$$

The appearance of  $c_v$ , the constant volume specific heat capacity discussed in Section 20.8.1, arises in order for the ideal gas internal energy to satisfy the general equation (20.120). The heat capacity for an ideal gas is generally a function of temperature. However, for many applications it is sufficient to consider a simple ideal gas, in which  $c_v$  is a constant so that

$$\mathcal{I} = c_v T + \text{constant} \quad \text{simple ideal gas.} \quad (20.165)$$

The arbitrary constant of integration is generally set to zero so that the internal energy vanishes at absolute zero.

### 20.12.3 Heat capacity

The heat capacity is a constant for a simple ideal gas (equation 20.165). Results from statistical mechanics show that the thermal/internal energy per molecule equals to  $k_B T/2$  per excited molecular degree of freedom, where

$$k_B = 1.3806 \times 10^{-23} \text{ m}^2 \text{ kg s}^{-2} \text{ K}^{-1} \quad (20.166)$$

is the *Boltzmann constant*. Dry air is mostly comprised of the diatomic molecules  $N_2$  and  $O_2$ . Diatomic molecules at temperatures of the lower atmosphere have two rotational and three translational degrees of freedom,<sup>15</sup> so that  $\mathcal{I}_{\text{molecule}} = 5 k_B T/2$ .

We convert this energy per molecule to an energy per mole of diatomic molecules by multiplying by Avogadro's number (equation (11.9))

$$\mathcal{I}_{\text{mole diatomic}} = 5 A_v k_B T/2 = 5 R_g T/2, \quad (20.167)$$

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<sup>14</sup>A notable counter-example is water near its freezing point, which becomes more dense as temperature rises. This anomalous behavior is why a body of water freezes from the top down rather than from the bottom up.

<sup>15</sup>At high temperatures, two vibrational degrees of freedom are also excited so that  $\mathcal{I}_{\text{molecule}} = 7 k_B T/2$  at high temperatures.

where the gas constant is given by

$$R_g = A_v k_B \quad (20.168a)$$

$$= (6.022 \times 10^{23} \text{ mole}^{-1}) (1.3806 \times 10^{-23} \text{ m}^2 \text{ kg s}^{-2} \text{ K}^{-1}) \quad (20.168b)$$

$$= 8.314 \text{ kg m}^2 \text{ s}^{-2} \text{ mole}^{-1} \text{ K}^{-1}. \quad (20.168c)$$

Finally, dividing by the molar mass for dry air (equation (11.10))

$$M_{\text{air}} = 0.028 \text{ kg mole}^{-1} \quad (20.169)$$

leads to the simple ideal gas approximation to the dry air heat capacity

$$c_v = \frac{5 R_g}{2 M_{\text{air}}} = 742 \text{ m}^2 \text{ s}^{-2} \text{ K}^{-1}. \quad (20.170)$$

The measured heat capacity for dry air at standard temperature (300 K) is  $718 \text{ m}^2 \text{ s}^{-2} \text{ K}^{-1}$ , so the simple ideal gas estimate is only  $(742 - 718)/718 = 3.3\%$  too large.

#### 20.12.4 Enthalpy

The enthalpy is generally given by equation (20.93), which for a simple ideal gas takes the form

$$\mathcal{H} = \mathcal{I} + p/\rho = c_v T + \frac{T R_g}{M_{\text{mole}}} = T (c_v + R^M) \quad (20.171)$$

where  $R^M = R_g/M_{\text{mole}}$  (equation (20.160)) is the specific gas constant for the gas. Recall that the constant pressure heat capacity is given by equation (20.121)

$$c_p = T \left[ \frac{\partial \mathcal{S}}{\partial T} \right]_{p,C} = \left[ \frac{\partial \mathcal{H}}{\partial T} \right]_{p,C}. \quad (20.172)$$

Consequently, for a simple ideal gas we have

$$c_p = c_v + R^M \quad \text{and} \quad \mathcal{H} = c_p T. \quad (20.173)$$

#### 20.12.5 Thermal expansion coefficient

The thermal expansion coefficient for an ideal gas is given by

$$\alpha_T = -\frac{1}{\rho} \frac{\partial \rho}{\partial T} = \frac{1}{T}, \quad (20.174)$$

so that as temperature increases the thermal expansion decreases.

#### 20.12.6 Fundamental thermodynamic relations

The fundamental thermodynamic relation, written in terms of internal energy (equation (20.76b)) and enthalpy (equation (20.93)), are given by

$$d\mathcal{I} = T d\mathcal{S} - p d\nu_s + \mu dC \quad (20.175)$$

$$d\mathcal{H} = T d\mathcal{S} + \nu_s dp + \mu dC. \quad (20.176)$$

For a simple ideal gas these relations take the form

$$c_v dT = T dS - p d\nu_s + \mu dC \quad (20.177)$$

$$c_p dT = T dS + \nu_s dp + \mu dC. \quad (20.178)$$

### 20.12.7 Isothermal compressibility

The isothermal compressibility measures the change in volume when holding the temperature and matter concentration fixed and it is determined by the partial derivatives

$$-\frac{1}{V} \left[ \frac{\partial V}{\partial p} \right]_{T,C} = \frac{1}{\rho} \left[ \frac{\partial \rho}{\partial p} \right]_{T,C}. \quad (20.179)$$

For an ideal gas the compressibility is given by

$$-\frac{1}{V} \left[ \frac{\partial V}{\partial p} \right]_{T,C} = \frac{1}{p}, \quad (20.180)$$

so that the compressibility decreases when pressure increases.

### 20.12.8 Sound speed

Sound travels through a fluid through compression and expansion (Section 17.5), so we expect the sound speed to be related to the compressibility. But rather than the isothermal compressibility considered above, sound waves are largely adiabatic waves so that the entropy is constant. We are thus in need of the isentropic compressibility to compute the sound speed. That is, as defined by equation (20.124), the sound speed is the pressure derivative of density computed with entropy and matter concentration held fixed. We make use of the fundamental relations (20.177) and (20.178), with  $dS = 0$  and  $dC = 0$  to have

$$\frac{c_v}{c_p} = \frac{p}{\rho} \left[ \frac{\partial \rho}{\partial p} \right]_{S,C} = (p/\rho) c_s^{-2} \implies c_s^2 = (p/\rho)(c_p/c_v) = T R^M (c_p/c_v). \quad (20.181)$$

For an ideal diatomic gas, such as nitrogen and oxygen, the ratio  $c_p/c_v = 7/5$ . Taking  $R^M = 2.938 \times 10^2 \text{ m}^2 \text{ s}^{-2} \text{ K}^{-1}$  for air from equation (20.162) then leads to

$$c_s \approx 350 \text{ m s}^{-1} \quad \text{for } T = 300 \text{ K.} \quad (20.182)$$

### 20.12.9 Adiabatic lapse rate

For an ideal gas, the thermal expansion coefficient is given by (equation (20.174))  $\alpha_T = T^{-1}$  so that the lapse rates are

$$\hat{\Gamma} = \frac{1}{\rho c_p} \quad \text{and} \quad \Gamma = -\frac{g}{c_p}. \quad (20.183)$$

The measured specific heat capacity for a dry atmosphere at standard temperature (300 K) is

$$c_p = 1005 \text{ m}^2 \text{ s}^{-2} \text{ K}^{-1} \quad (20.184)$$

so that the adiabatic lapse rate for a dry atmosphere is roughly

$$\Gamma_d = -9.8 \text{ K}/(1000 \text{ m}). \quad (20.185)$$

Hence, temperature decreases by nearly 10 K when rising 1000 m in a dry and ideal gas atmosphere.

### 20.12.10 Geopotential thickness

We now establish basic relations for a static atmosphere satisfying the hydrostatic balance. These relations also hold to a very good approximation for the large-scale atmosphere given the dominance of approximate hydrostatic balance for these scales (see Section 22.2).

From the hydrostatic equation (17.40) we know that the pressure on a geopotential,  $\Phi_1$ , equals to

$$p(\Phi_1) = \int_{\Phi_1}^{\infty} \rho(\Phi) d\Phi \quad (20.186)$$

where we assumed that  $p(\Phi_2 = \infty) = 0$ . Equation (17.39) allows us to write the integrand as

$$d\Phi = -\rho^{-1} dp = -\frac{TR^{\text{air}} dp}{p}, \quad (20.187)$$

where the second equality assumed an ideal gas atmosphere. Vertical integration of equation (20.187) leads to the *hypsometric equation*, which provides the geopotential thickness between two pressure isosurfaces

$$\Phi(z_2) - \Phi(z_1) = -R^{\text{air}} \int_{p_1}^{p_2} T d(\ln p). \quad (20.188)$$

Recall that  $dp < 0$  if  $dz > 0$  since the hydrostatic pressure decreases when moving up in the atmosphere. We define the *geopotential height* according to

$$Z = \Phi/g, \quad (20.189)$$

where  $g$  is the gravitational acceleration at sea level. The geopotential height is close to the geometric height in the troposphere and lower stratosphere. The hypsometric equation (20.188) says that the geopotential thickness between two isobars is

$$Z_2 - Z_1 = \frac{R^{\text{air}}}{g} \int_{p_2}^{p_1} T d(\ln p). \quad (20.190)$$

Defining the layer mean temperature

$$\langle T \rangle = \frac{\int_{p_2}^{p_1} T d(\ln p)}{\int_{p_2}^{p_1} d(\ln p)} \quad (20.191)$$

and the layer mean *scale height*

$$H = \frac{R^{\text{air}} \langle T \rangle}{g} \quad (20.192)$$

leads to the geopotential thickness

$$Z_2 - Z_1 = -H \ln(p_2/p_1) \quad (20.193)$$

The geopotential thickness is thus directly proportional to the mean temperature within the pressure layer, with thicker layers, for example, with higher mean temperatures.

We can invert the geopotential thickness relation (20.193) for the pressures to render

$$p_1 = p_2 e^{-(Z_1 - Z_2)/H}. \quad (20.194)$$

This relation, or more commonly its simplified version (20.198) discussed below, is sometimes referred to as the *law of atmospheres* or the *barometric law*. The scale height is a function of pressure through its dependence on the layer averaged temperature in equation (20.192). For the special case of an atmosphere with a constant temperature,  $T$ , then the scale height is a constant<sup>16</sup>

$$H_{\text{const}} = \frac{R^{\text{air}} T_{\text{const}}}{g}. \quad (20.195)$$

Setting  $T_{\text{const}} = 300$  K and using the specific gas constant for air from equation (20.162) leads to the scale height

$$H_{\text{const}} = \frac{2.938 \times 10^2 \text{ m}^2 \text{ s}^{-2} \text{ K}^{-1} \times 300 \text{ K}}{9.8 \text{ m s}^{-2}} \approx 9 \times 10^3 \text{ m}. \quad (20.196)$$

It is furthermore convenient to set  $Z_2 = 0$  with  $p_2 = p_{\text{slp}}$  the sea level pressure, whose global average is

$$\langle p_{\text{slp}} \rangle = 101.325 \times 10^3 \text{ N m}^{-2}. \quad (20.197)$$

The pressure in an isothermal atmosphere thus decreases exponentially with geopotential height according to the scale height

$$p(Z) = \langle p_{\text{slp}} \rangle \exp(-Z/H_{\text{const}}). \quad (20.198)$$

### 20.12.11 Potential temperature

The fundamental thermodynamic relation for a simple ideal gas (20.178) takes on the following form for an isentropic change

$$c_p dT = \nu_s dp. \quad (20.199)$$

Dividing both sides by temperature and using the ideal gas relation

$$\frac{\nu_s}{T} = \frac{R^M}{p} \quad (20.200)$$

leads to

$$c_p d(\ln T) = R^M d(\ln p). \quad (20.201)$$

Since  $c_p$  and  $R^M$  are constants, we can integrate this relation from the reference pressure to an arbitrary pressure

$$c_p \int_{\theta}^T d(\ln T) = R^M \int_{p_R}^p d(\ln p), \quad (20.202)$$

which renders the explicit expression for the potential temperature of a simple ideal gas

$$\theta = T \left[ \frac{p_R}{p} \right]^{R^M/c_p} \quad \text{where} \quad c_p = \frac{7 R^M}{2}, \quad (20.203)$$

with  $c_p$  the constant pressure heat capacity of a simple ideal gas of diatomic molecules (Section 20.12.3). In Exercise 20.5 we show that  $\partial\theta/\partial p = 0$  for the ideal gas, thus exemplifying the removal of explicit pressure effects from the potential temperature. Furthermore, it follows from equation (20.203) that increments in potential temperature are related to increments in temperature and

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<sup>16</sup>As we saw earlier in this chapter, a fluid has uniform temperature at thermodynamic equilibrium. However, the effects from turbulent motions, even very modest turbulent motions, readily break thermodynamic equilibrium. This topic was first discussed starting on page 299 by Maxwell (1872), where he also credits input from Lord Kelvin.

pressure via

$$\frac{\delta\theta}{\theta} = \frac{\delta T}{T} - \frac{\delta p}{p}. \quad (20.204)$$

In particular, if the increment is between points in space within a fluid, then we are led to the relationship between gradients

$$\frac{\nabla\theta}{\theta} = \frac{\nabla T}{T} - \frac{\nabla p}{p}. \quad (20.205)$$

### 20.12.12 Further study

Atmospheric sciences and dynamic meteorology books have thorough discussions of ideal gas thermodynamics. Some of the material in section 1.6 of [Holton \(1992\)](#) was used in the present section.



## 20.13 Exercises

### EXERCISE 20.1: DERIVATION OF THE GIBBS-DUHEM RELATION

Show all of the steps leading to the Gibbs-Duhem relation (20.44).

### EXERCISE 20.2: CHEMICAL POTENTIAL IDENTITY

As seen in Section 21.4.7, we have need to consider the partial derivative

$$\left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} \quad (20.206)$$

when determining the chemical work done by mixing within a fluid. Prove the identity

$$\left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} = \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{S,p} - T \left[ \frac{\partial \mu}{\partial T} \right]_{C,p} = \mu - T \left[ \frac{\partial \mu}{\partial T} \right]_{C,p}. \quad (20.207)$$

Hint: as seen in Section 20.7.4, the natural functional dependence for enthalpy is  $\mathcal{H}(S, p, C)$ , whereas in Section 20.7.6 we found the natural function dependence of the Gibbs potential to be  $\mathcal{G}(T, p, C)$ . Equate the exact differential expressions for enthalpy using the two functional dependencies  $\mathcal{H}(S, p, C)$  and  $\mathcal{G}(T, p, C)$ , and then derive a Maxwell relation based on the fundamental thermodynamic relation written in terms of the Gibbs potential.

### EXERCISE 20.3: CONSTANT OF MOTION FOR ADIABATIC FLOW

Show that for a simple ideal gas, isentropic flow (i.e., both adiabatic and of constant matter concentration) maintains

$$p \nu_s^{c_p/c_v} = \text{constant}, \quad (20.208)$$

where  $\nu_s = \rho^{-1}$  is the specific volume.

### EXERCISE 20.4: GEOPOTENTIAL HEIGHT

The *geopotential height* is the height above the earth of a chosen pressure surface.

- (a) Show that an ideal gas atmosphere in exact hydrostatic balance with a uniform lapse rate

$$\frac{dT}{dz} = -|\Gamma| = \text{constant} \quad (20.209)$$

has a geopotential height at a pressure  $p$  given by

$$z = \frac{T_0}{|\Gamma|} \left[ 1 - \left[ \frac{p_0}{p} \right]^{-R^M |\Gamma| / g} \right], \quad (20.210)$$

where  $T_0$  is the temperature at  $z = 0$ .

- (b) For an isothermal atmosphere, obtain an expression for the geopotential height as a function of pressure, and show that this result is consistent with the expression (20.210) in the appropriate limit.

**EXERCISE 20.5: POTENTIAL TEMPERATURE FOR AN IDEAL GAS**

Show that  $\partial\theta/\partial p = 0$  for the potential temperature of an ideal gas given by equation (20.203)

$$\theta = T \left[ \frac{p_R}{p} \right]^{R^M / c_p}. \quad (20.211)$$

Hint: remember that  $\partial T/\partial p \neq 0$ .

**EXERCISE 20.6: THERMODYNAMIC RELATIONS FOR AN ATMOSPHERE**

In this exercise, we establish some relations for an ideal gas atmosphere, and one relation holding for an arbitrary equation of state. We assume that the gravitational acceleration is constant throughout the full depth of the atmosphere. This assumption becomes questionable when integrating to the top of the atmosphere. We furthermore ignore differences in the horizontal cross-sectional area of a fluid column at the bottom and top of the atmosphere arising from the spherical nature of the planet. These two assumptions are sufficient for our purposes.

- (a) **PRESSURE-HEIGHT IDENTITY:** Prove the following identity and state your assumptions

$$\int_0^{p_s} z dp = \int_{z=0}^{z_{top}} p dz. \quad (20.212)$$

This identity will be of use for some of the following questions.

- (b) **IDEAL GAS  $\mathcal{I} + \Phi$  INTEGRATED OVER DEPTH OF A HYDROSTATIC ATMOSPHERE:** For an ideal gas atmosphere in exact hydrostatic balance, show that the integral of the gravitational potential energy plus internal energy from the surface to the top of the atmosphere is equal to the integral of the enthalpy of the atmosphere

$$\int_0^{z_{top}} (\Phi + \mathcal{I}) \rho dz = \int_0^{z_{top}} \mathcal{H} \rho dz, \quad (20.213)$$

where

$$\mathcal{H} = p \alpha + \mathcal{I} \quad (20.214)$$

is the enthalpy per mass,

$$\Phi = g z \quad (20.215)$$

is the simple form of the geopotential, which is also the gravitational potential energy per mass (Section 9.12.4), and  $\mathcal{I}$  is the internal energy per mass. The height integral extends from the surface where  $z = 0$ , to the top of the atmosphere where  $z = z_{top}$ .

- (c) **VERTICAL DERIVATIVE OF DRY STATIC ENERGY:** For an ideal gas atmosphere in hydrostatic

balance, show that

$$\frac{d\sigma}{dz} = \Pi \frac{d\theta}{dz}, \quad (20.216)$$

where

$$\sigma = \mathcal{H} + \Phi \quad (20.217)$$

is the dry static energy and

$$\Pi = \frac{c_p T}{\theta} \quad (20.218)$$

is the *Exner function*.

- (d) FIRST IDENTITY FOR HORIZONTAL PRESSURE GRADIENT: For an ideal gas atmosphere (either hydrostatic or non-hydrostatic), derive the following expression for the pressure gradient force

$$-\frac{1}{\rho} \nabla p = -\theta \nabla \Pi. \quad (20.219)$$

- (e) SECOND IDENTITY FOR HORIZONTAL PRESSURE GRADIENT: For an ideal gas atmosphere (either hydrostatic or non-hydrostatic), derive the following expression for the pressure gradient force

$$-\frac{1}{\rho} \nabla p = -\frac{c_s^2}{\rho \theta} \nabla(\rho \theta), \quad (20.220)$$

where  $c_s$  is the sound speed.

- (f)  $\mathcal{I} + \Phi$  INTEGRATED OVER DEPTH OF A HYDROSTATIC ATMOSPHERE: Show that for a hydrostatic atmosphere with an arbitrary equation of state

$$\int_0^{p_s} (\Phi + \mathcal{I}) dp = \int_0^{p_s} \mathcal{H} dp. \quad (20.221)$$

That is, show that the relation in the first part of this problem holds even without making the ideal gas assumption.

#### EXERCISE 20.7: UNIT KNUDSEN NUMBER

Recall from Section 11.2.2 that the Knudsen number is the ratio  $\text{Kn} = L_{\text{mfp}}/L_{\text{macro}}$ , where  $L_{\text{macro}} \approx 10^{-4}$  m is the macroscopic length scale used in the discussion of the continuum approximation, and  $L_{\text{mfp}}$  is the molecular mean free path (Section 11.3.3). Throughout this exercise make use of  $p_{\text{stand}} = 101.325 \times 10^3$  Pa for standard atmospheric pressure.

- (a) Consider a mole of an isothermal and ideal gas atmosphere of  $T = 300\text{K}$  with a constant gravitational acceleration. At what pressure is the Knudsen number unity? Write your answer as a fraction of standard sea atmospheric pressure,  $p_{\text{stand}}$ .
- (b) Compute the altitude corresponding to the above pressure, assuming the sea level pressure is  $p_{\text{slp}}$  and the geopotential is  $\Phi = g z$ . Hint: make use of results from Section 20.12.10.
- (c) Assuming  $p = p_{\text{stand}}$ , at what temperature is  $\text{Kn} = 1$ ? Hint: assume the ideal gas law holds regardless the temperature.
- (d) Comment on what is the least atmospherically relevant assumption made during this exercise.





# Chapter 21

## Energetics of fluid flow

The energy of a static fluid consists of the potential energy of the fluid within a gravitational field plus the internal energy arising from molecular degrees of freedom. In this chapter, we are concerned with moving fluids, in which the macroscopic motion possesses kinetic energy as well as potential energy. We develop the dynamical equations for mechanical energy (kinetic plus gravitational potential) of this macroscopic motion and examine how it can be exchanged with internal energy. We refer to *thermomechanics* as the study of energy flows between various pieces of mechanical energy and the internal energy. That is, thermomechanics is concerned with energetics of both the macroscopic fluid flow and the microscopic internal degrees of freedom.

As part of this analysis we extend the equilibrium thermodynamics of Chapter 20 to include time dependent moving fluid phenomena. Making this transition requires us to assume that moving fluid elements are in *local thermodynamic equilibrium*. This assumption is based on the quasi-static nature of macroscopic motions (Section 20.1.3) whereby microscopic motions have a much shorter equilibration time relative to the slower macroscopic processes of interest for fluid mechanics such as advection, waves, turbulence, and turbulent mixing. The extremely wide time scale separation between the microscopic and macroscopic allows us to use phenomenological thermodynamic laws to develop evolution equations for continuous thermodynamic properties of moving continuum fluid elements. Consistent with the time scale separation, we can assume that the macroscopic motion of a fluid element does not alter its entropy. That is, advective transport in the absence of mixing is a reversible process. In contrast, mixing of properties between fluid elements, whether through molecular or turbulent processes, is irreversible and thus increases entropy.

The application of thermodynamics to a moving fluid is known as *quasi-equilibrium thermodynamics* or *linear irreversible thermodynamics*, with fundamentals developed in [DeGroot and Mazur \(1984\)](#) and [Landau and Lifshitz \(1987\)](#). The term “linear” refers to an assumption that the system is close to thermodynamic equilibrium throughout its motion. This assumption is very accurate for the atmospheric and oceanic motions studied in this book, whereby local thermodynamic equilibrium is maintained for fluid elements even as those elements move as a result of imbalances in macroscopic forces. Thermodynamic fluxes are thus linear functions of the gradients of the thermodynamic state variables. The assumption of local thermodynamic equilibrium breaks down in the rarefied gas dynamics of the upper atmosphere and is outside the scope of this book.

### READER'S GUIDE FOR THIS CHAPTER

This chapter builds from the momentum dynamics of Chapter 17 and the thermodynamics

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of Chapter 20. We develop a variety of energy budgets and consider their physical content. We also study the heat equation as represented by the equation for potential enthalpy, with variations on the heat equation and the transport of enthalpy of primary importance for large-scale ocean and atmospheric phenomena and climate dynamics.

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21.1	Loose threads . . . . .	483
21.2	Gravitational potential energy . . . . .	483
21.2.1	Material evolution . . . . .	483
21.2.2	Reference geopotential . . . . .	484
21.2.3	Regionally integrated gravitational potential energy . . . . .	484
21.2.4	Potential energy and vertical stratification . . . . .	485
21.2.5	Gravitational potential energy and mixing . . . . .	486
21.3	Kinetic energy and mechanical energy . . . . .	487
21.3.1	Kinetic energy . . . . .	487
21.3.2	Frictional dissipation of kinetic energy . . . . .	488
21.3.3	Mechanical energy budget . . . . .	489
21.3.4	Further study . . . . .	490
21.4	Thermodynamics of a moving fluid . . . . .	490
21.4.1	Concerning the transition to a moving fluid . . . . .	490
21.4.2	Thermodynamic properties as space-time fields . . . . .	491
21.4.3	Thermodynamic relations for steady state flow . . . . .	491
21.4.4	Materially constant specific entropy for a perfect fluid . . . . .	492
21.4.5	First law for a moving fluid element . . . . .	492
21.4.6	Enthalpy budget . . . . .	493
21.4.7	Thermal and chemical processes and fluxes . . . . .	493
21.4.8	First law for homogeneous fluids in terms of potential temperature	494
21.4.9	Further study . . . . .	494
21.5	Budget for total energy . . . . .	495
21.5.1	Postulating the budget for total energy . . . . .	495
21.5.2	Budgets for internal energy and enthalpy . . . . .	495
21.5.3	Joule heating from friction . . . . .	496
21.5.4	Comments on gauge symmetry . . . . .	496
21.5.5	Further study . . . . .	497
21.6	Bernoulli potential . . . . .	497
21.6.1	Bernoulli potential and mechanical injection work . . . . .	497
21.6.2	Bernoulli's theorem for a steady perfect fluid . . . . .	498
21.6.3	Traditional derivation of Bernoulli's theorem . . . . .	498
21.6.4	Steady flow of constant density perfect fluid in a pipe . . . . .	499
21.6.5	Further study . . . . .	500
21.7	Entropy budget for the ocean . . . . .	500
21.7.1	Non-advective entropy flux and entropy source . . . . .	501
21.7.2	Constraints from the second law of thermodynamics . . . . .	502
21.7.3	A summary presentation . . . . .	503
21.7.4	Comments and further study . . . . .	505
21.8	Temperature evolution . . . . .	505
21.8.1	Enthalpy equation again . . . . .	505
21.8.2	Evolution of <i>in situ</i> temperature . . . . .	506
21.8.3	Evolution of potential temperature . . . . .	506
21.8.4	Conservative Temperature for the ocean . . . . .	507
21.8.5	Further study . . . . .	508
21.9	Summary of the ocean-atmosphere equations . . . . .	508
21.10	Conservation laws and potential properties . . . . .	510
21.10.1	Flux-form conservation laws . . . . .	510

---

21.10.2 Conservation laws that are not flux-form . . . . .	511
21.10.3 Non-material or wave-like transport of properties . . . . .	511
21.10.4 Local versus global conservation . . . . .	511
21.10.5 Concerning potential properties . . . . .	512
21.10.6 Further study . . . . .	513
21.11 Exercises . . . . .	<b>513</b>

## 21.1 Loose threads

- Figures needed
- Available internal energy
- Potential energy as per Section 108 of *Landau and Lifshitz* (1980) and possible extention to APE.
- Discuss mixing of  $T$  versus  $\Theta$  in Section 21.8. Section 25 of *Landau and Lifshitz* (1980) seems appropriate.

## 21.2 Gravitational potential energy

Geophysical fluids move within a gravitational field created by the mass of the planet, including the mass of the fluid itself. We typically focus on a rather simple form for the effective gravitational acceleration exemplified by the geopotential  $\Phi = g z$ , where  $g$  is the gravitational acceleration that includes effects from both central gravity plus planetary centrifugal (Section 9.12.4). However, we offer some discussion of astronomical tide producing forces in Chapter 28, whereby the geopotential is a more complicated function of space and time,  $\Phi(\mathbf{x}, t)$ . In this section we study the potential energy of a fluid element due to its presence in a gravitational field, with the geopotential providing the effective gravitational potential energy per mass of fluid elements.<sup>1</sup>

### 21.2.1 Material evolution

The gravitational potential energy per mass of a fluid element is given by the geopotential,  $\Phi$ , so that the gravitational potential energy is  $\Phi \rho \delta V$ . Hence, the evolution of potential energy for a constant mass fluid element is given by

$$\frac{D(\Phi \rho \delta V)}{Dt} = \rho \delta V \frac{D\Phi}{Dt}, \quad (21.1)$$

where  $D(\rho \delta V)/Dt = 0$  since the fluid element has a constant mass. The material time derivative for the geopotential

$$\frac{D\Phi}{Dt} = \frac{\partial \Phi}{\partial t} + \mathbf{v} \cdot \nabla \Phi, \quad (21.2)$$

contains a local time dependence that arises from astronomical tide forcing or movement of mass on the planet (Chapter 28). As further explored in Section 21.3, the advective term represents an exchange of mechanical energy between the kinetic energy contained in fluid motion and the gravitational potential energy due to the fluid being within a gravitational field. This energy exchange arises from fluid motion across constant geopotential surfaces. For example, motion up

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<sup>1</sup>In the following we generally refer to the more concise “gravitational potential energy” or even briefer “potential energy” rather than “potential energy from the effective gravitational field.”

the geopotential gradient,  $\mathbf{v} \cdot \nabla \Phi > 0$ , increases gravitational potential energy and motion down the geopotential gradient decreases potential energy. With the geopotential  $\Phi = g z$ , we have

$$\mathbf{v} \cdot \nabla \Phi = g w, \quad (21.3)$$

so that vertically upward motion ( $w > 0$ ) increases potential energy.

### 21.2.2 Reference geopotential

There is no change to the energetics if we modify the gravitational reference state by modifying the geopotential

$$\Phi \rightarrow \Phi + \Phi_r \quad (21.4)$$

with  $\Phi_r$  an arbitrary constant. In particular, this offset has no effect on the evolution of gravitational potential energy of the constant mass fluid element since

$$\frac{D(\Phi_r \rho \delta V)}{Dt} = \Phi_r \frac{D(\rho \delta V)}{Dt} = 0. \quad (21.5)$$

Hence, as is well known from classical mechanics, it is not the value of the gravitational potential energy that is important, but instead it is the space and time changes that affect energetics.

### 21.2.3 Regionally integrated gravitational potential energy

Now consider the evolution of the gravitational potential energy integrated over a finite region  $\mathcal{R}$ . If the fluid region is closed to mass transport, as per a material boundary, then we can make use of the Leibniz-Reynolds transport theorem in the form of equation (15.49d) to write

$$\frac{d}{dt} \int_{\mathcal{R}} \Phi \rho dV = \int_{\mathcal{R}} \frac{D\Phi}{Dt} \rho dV, \quad (21.6)$$

which is an extension of the material evolution equation (21.1). If the region is open to material mass transport, we make use Leibniz-Reynolds transport theorem in the form of equation (15.34) to find

$$\frac{d}{dt} \int_{\mathcal{R}} \rho \Phi dV = \int_{\mathcal{R}} \left[ \frac{\partial(\rho \Phi)}{\partial t} + \nabla \cdot (\rho \Phi \mathbf{v}^{(b)}) \right] dV \quad (21.7a)$$

$$= \int_{\mathcal{R}} \left[ \rho \frac{D\Phi}{Dt} - \nabla \cdot (\rho \Phi \mathbf{v}) + \nabla \cdot (\rho \Phi \mathbf{v}^{(b)}) \right] dV \quad (21.7b)$$

$$= \int_{\mathcal{R}} \left[ \rho \frac{D\Phi}{Dt} + \nabla \cdot [\rho \Phi (\mathbf{v}^{(b)} - \mathbf{v})] \right] dV \quad (21.7c)$$

$$= \int_{\mathcal{R}} \rho \frac{D\Phi}{Dt} dV + \oint_{\partial\mathcal{R}} \rho \Phi (\mathbf{v}^{(b)} - \mathbf{v}) \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (21.7d)$$

where  $\mathbf{v}^{(b)}$  is the velocity of a point on the boundary of the domain. The evolution thus consists of the mass integrated material time evolution of the geopotential, plus a surface term that contributes to the transport of the geopotential across the regional boundaries.

If the region is a vertical column of ocean fluid with fixed horizontal cross-section, extending from the ocean surface to the ocean bottom, then there is horizontal transport across the vertical column bounds, plus vertical transport of mass across the ocean free surface. For the free surface

we make use of the surface kinematic boundary condition (14.73c) to write

$$\int_{z=\eta} \rho \Phi (\mathbf{v}^{(b)} - \mathbf{v}) \cdot \hat{\mathbf{n}} dS = \int_{z=\eta} Q_m \Phi dA. \quad (21.8)$$

In this equation,  $Q_m$  is the mass per time per horizontal area of matter crossing the ocean free surface at  $z = \eta$  where  $Q_m > 0$  for matter entering the ocean domain, and  $dS$  is the area element on the free surface with  $dA$  its horizontal projection. As noted in Section 21.2.2, we can add a constant to the geopotential without affecting the energetics, which is here seen by noting that mass conservation means that

$$\frac{d}{dt} \int \rho dV = - \int_{\mathcal{R}} \nabla \cdot [\rho (\mathbf{v} - \mathbf{v}^{(b)})] dV, \quad (21.9)$$

which results from setting  $\Phi = 1$  in equation (21.7d). In general, we expect the transfer of mass across the surface boundary to affect the gravitational potential energy both because it adds or removes mass to the ocean domain, and because it affects the geopotential. To help interpret the sign from the boundary term, it is useful to define the reference state geopotential so that  $\Phi > 0$  at the ocean surface, no matter what the value of  $\eta$ . We can do so by defining the reference geopotential at or below the ocean bottom. In this case, adding mass increases the gravitational potential energy and removing mass reduces it.

Consider the special case of a geopotential  $\Phi = g z$ , so returning to a  $z = 0$  reference state, in which case the global ocean potential energy equation is written

$$\frac{d}{dt} \int \rho z dV = \int \rho w dV + \int Q_m \eta dA, \quad (21.10)$$

where we cancelled the constant gravitational acceleration. Now decompose  $Q_m$  and  $\eta$  into their global area means and deviations

$$Q_m = \overline{Q_m} + Q'_m \quad \text{and} \quad \eta = \bar{\eta} + \eta', \quad (21.11)$$

so that

$$g \int Q_m \eta dA = g \overline{Q_m} \bar{\eta} A + g \int Q'_m \eta' dA. \quad (21.12)$$

As before, the  $\overline{Q_m} \bar{\eta}$  term alters potential energy relative to the arbitrary reference state, here taken as  $z = 0$ . The area correlation term increases potential energy in regions where  $Q'_m \eta' > 0$ , which acts to increase the relative deviation of the free surface from its mean value. That is,  $Q'_m \eta' > 0$  in regions where  $Q'_m > 0$  and  $\eta' > 0$  as well as in regions where  $Q'_m < 0$  and  $\eta' < 0$ . Conversely, the correlation term reduces potential energy where  $Q'_m$  and  $\eta'$  are anti-correlated, which acts to decrease the relative deviation of the free surface height.

#### 21.2.4 Potential energy and vertical stratification

Consider the potential energy of a region of horizontally homogeneous fluid centered at a vertical position,  $z = z_c$ , and with constant horizontal cross-sectional area,  $A$ . Assuming we do not move vertically far away from the central position, we can write the density in the linear form

$$\rho(z) = \rho(z_c) + \frac{d\rho(z_c)}{dz} (z - z_c) \equiv \rho_c - K (z - z_c), \quad (21.13)$$

where  $K = -d\rho(z_c)/dz > 0$  is a shorthand for the vertical density gradient at the central point. The potential energy per volume ( $\Delta V = A \Delta z$ ) for fluid in the vertical region  $z \in [z_c - \Delta z/2, z_c + \Delta z/2]$  is given by

$$(g/\Delta z) \int z \rho dz = (g/\Delta z) \int_{z_c - \Delta z/2}^{z_c + \Delta z/2} [\rho_c - K(z - z_c)] z dz \quad (21.14a)$$

$$= g \rho_c z_c - g K (\Delta z)^2 / 12. \quad (21.14b)$$

We thus see that the gravitational potential energy decreases as the vertical stratification,  $K > 0$ , increases, with the maximum potential energy when the stratification vanishes,  $K = 0$ . As seen in Section 21.2.5, potential energy is maximized when  $K = 0$  since the center of mass moves vertically upward as the stratification reduces to zero.

### 21.2.5 Gravitational potential energy and mixing

Consider a fluid in exact hydrostatic balance (Section 17.3) with a gravitationally stable vertical stratification where light fluid is above heavy fluid.<sup>2</sup> Now introduce a physical process, such as vertical mixing associated with a kinetic energy source, that reduces the vertical stratification. Reducing vertical stratification requires mixing to move heavy fluid up and light fluid down. In so doing, the kinetic energy supporting the mixing is converted into gravitational potential energy since the center of mass for the fluid column rises.

We can formulate this thought experiment by considering a column of seawater that is vertically stratified in salinity,  $S$ , and Conservative Temperature,  $\Theta$ , and another column that is vertically unstratified with constant values  $S_m$  and  $\Theta_m$  that result from vertically mixing (to infinite time) the original column.<sup>3</sup> We assume the mass of the two columns is the same so that the bottom pressure is the same. However, the volumes will generally differ since the density differs, so that the two free surfaces,  $\eta$  and  $\eta_m$ , are different. Assuming a geopotential,  $\Phi = g z$ , leads to the difference between the gravitational potential energies per horizontal area in the two columns

$$g \int_{\eta_b}^{\eta_m} \rho(S_m, \Theta_m, p) z dz - g \int_{\eta_b}^{\eta} \rho(S, \Theta, p) z dz = \int_{p_a}^{p_b} (z_m - z) dp \quad (21.15a)$$

$$= (p_b - p_a) (\bar{z}_m - \bar{z}). \quad (21.15b)$$

To reach this result we used the same pressure increment,  $dp$ , when integrating over both columns, which we can do since mass is conserved. Furthermore, we used the hydrostatic balance to convert from a depth integral into a pressure integral

$$dp = -g \rho(S, \Theta, p) dz = -g \rho(S_m, \Theta_m, p) dz_m \implies z \rho(S, \Theta, p) dz = z_m \rho(S_m, \Theta_m, p) dz_m. \quad (21.16)$$

We also introduced the center of mass positions for the vertically homogeneous column,  $\bar{z}_m$ , and the stratified column,  $\bar{z}$

$$\bar{z}_m = \frac{1}{p_b - p_a} \int_{p_a}^{p_b} z_m dp \quad \text{and} \quad \bar{z} = \frac{1}{p_b - p_a} \int_{p_a}^{p_b} z dp. \quad (21.17)$$

---

<sup>2</sup>See Section 24.5 for a more precise discussion of gravitational stability.

<sup>3</sup>See Section 24.3 for discussion of the seawater equation of state. For present purposes it is sufficient to know that seawater density is a function of the material tracer  $S$ , the thermodynamic tracer,  $\Theta$ , and pressure,  $p$ . When a column is vertically homogenized that means  $S$  and  $\Theta$  are constant throughout the column. However, pressure remains hydrostatic and thus is not vertically constant. Since density is a function of pressure, it too retains a vertical gradient.

There are two terms in the potential energy difference in equation (21.15b). The first is the mass per horizontal area, as measured by the difference in bottom pressure and applied surface pressure,  $p_b - p_a$ . The second is the difference between the center of mass for the two columns,  $\bar{z}_m - \bar{z}$ , which is a positive number since mixing moves heavier water up and lighter water down so that  $\bar{z}_m > \bar{z}$ . Hence, we see that the potential energy of the mixed column is larger than the stratified column.

## 21.3 Kinetic energy and mechanical energy

Mechanical energy is a dynamical property formed by adding the energy due to motion of fluid elements (kinetic energy) to the energy arising from the position of a fluid element within the gravitational field (gravitational potential energy). Energy is a scalar field, which often means that its budget is simpler to understand than that for the vector momentum field. In this section we develop the evolution equations for kinetic energy and then mechanical energy of a fluid on a rotating sphere, making use of the momentum equation written in the general form of equation (17.16), repeated here for convenience

$$\rho \frac{D\mathbf{v}}{Dt} + 2\rho \boldsymbol{\Omega} \times \mathbf{v} = -\rho \nabla \Phi + \nabla \cdot (-p \mathbb{I} + \tau) \quad (21.18a)$$

$$= -\rho \nabla \Phi - \nabla p + \rho \mathbf{F}, \quad (21.18b)$$

where we wrote

$$\mathbf{F} = \rho^{-1} \nabla \cdot \tau \quad (21.19)$$

for acceleration due to friction.

### 21.3.1 Kinetic energy

Following our discussion of mechanical energy of a point particle in Section 10.9, consider the kinetic energy per mass of a fluid element

$$\mathcal{K} = \mathbf{v} \cdot \mathbf{v}/2. \quad (21.20)$$

Use of the momentum equation in the form of equations (21.18a) and (21.18b) reveals that the material evolution of the kinetic energy per mass is given by

$$\rho \frac{D\mathcal{K}}{Dt} = -\rho \mathbf{v} \cdot \nabla \Phi - \mathbf{v} \cdot \nabla p + \rho \mathbf{v} \cdot \mathbf{F}. \quad (21.21)$$

We thus see that the kinetic energy of a fluid element is affected by work done by the geopotential,  $-\rho \mathbf{v} \cdot \nabla \Phi$ , along with work done by stresses through both pressure and friction. We detail these processes in the following.

#### *Contribution from the geopotential*

Kinetic energy increases for motion directed down the geopotential gradient

$$\mathbf{v} \cdot \nabla \Phi < 0 \implies \text{increases kinetic energy.} \quad (21.22)$$

For example, with a simple geopotential,  $\Phi = g z$ , kinetic energy increases where the vertical velocity is downward,

$$w < 0 \implies -w g \rho > 0 \longleftrightarrow \text{downward motion increases } \mathcal{K}. \quad (21.23)$$

As seen in Section 21.2.1, this increase in kinetic energy due to motion down the geopotential gradient is exactly balanced by a decrease in gravitational potential energy, with this kinetic to potential energy conversion also seen in Section 10.9 for the point particle.

### Contribution from the pressure force

Kinetic energy increases in regions where the velocity projects down the pressure gradient,

$$\mathbf{v} \cdot \nabla p < 0 \implies \text{increase kinetic energy}, \quad (21.24)$$

thus resulting in an increase in fluid speed imparted by the pressure gradient force. Conversely, kinetic energy is reduced in regions where the flow is directed up the pressure gradient. It is notable that horizontal geostrophic flows (Section 25.4) with

$$\mathbf{v}_g = \frac{\hat{\mathbf{z}} \times \nabla p}{f \rho} \quad (21.25)$$

have the velocity oriented perpendicular to the horizontal pressure gradient ( $\mathbf{v}_g \cdot \nabla p = 0$ ). Consequently, pressure has no impact on the horizontal kinetic energy of a geostrophic fluid.

### Contribution from friction

Kinetic energy is reduced in regions where the velocity has a negative projection onto the direction of the friction vector,  $\rho \mathbf{v} \cdot \mathbf{F} < 0$ . As detailed in Section 21.3.2, the friction arising from a viscous stress tensor appropriate for a Newtonian fluid gives rise to two contributions to kinetic energy: the divergence of a viscous flux plus a sign-definite sink.

#### 21.3.2 Frictional dissipation of kinetic energy

We here detail the role of friction on kinetic energy

$$\text{friction power per volume} = \rho \mathbf{v} \cdot \mathbf{F}, \quad (21.26)$$

where friction is determined by the stress-rate of strain relation (18.78). We interpret  $\rho \mathbf{v} \cdot \mathbf{F}$  as the frictional power (energy per time) per volume acting to alter the kinetic energy per volume of a fluid element. To proceed, we expose Cartesian tensor labels to have

$$\rho \mathbf{v} \cdot \mathbf{F} = v_m \rho F_m \quad (21.27a)$$

$$= v_m \partial_n \tau_{nm} \quad (21.27b)$$

$$= 2 v_m \partial_n (\rho \nu \mathbb{S}_{mn}^{\text{dev}}) \quad (21.27c)$$

$$= 2 \partial_n (\rho \nu v_m \mathbb{S}_{mn}^{\text{dev}}) - 2 \rho \nu \partial_n v_m \mathbb{S}_{mn}^{\text{dev}} \quad (21.27d)$$

$$= 2 \nabla \cdot (\rho \nu \mathbf{v} \cdot \mathbb{S}^{\text{dev}}) - 2 \rho \nu \mathbb{S}_{mn} \mathbb{S}_{mn}^{\text{dev}}, \quad (21.27e)$$

where we recall from Section 18.7.6 that the *deviatoric rate of strain tensor* has elements given by

$$\mathbb{S}_{mn}^{\text{dev}} = \mathbb{S}_{mn} - \delta_{mn} \mathbb{S}_{qq}/3 \quad \text{with} \quad \mathbb{S}_{qq} = \nabla \cdot \mathbf{v}. \quad (21.28)$$

To reach equation (21.27e) required the identity

$$2 \partial_n v_m \mathbb{S}_{mn}^{\text{dev}} = (\partial_n v_m + \partial_m v_n) \mathbb{S}_{mn}^{\text{dev}} + (\partial_n v_m - \partial_m v_n) \mathbb{S}_{mn}^{\text{dev}} = 2 \mathbb{S}_{mn} \mathbb{S}_{mn}^{\text{dev}}, \quad (21.29)$$

where

$$(\partial_n v_m - \partial_m v_n) \mathbb{S}_{mn}^{\text{dev}} = 2 \mathbb{A}_{mn} \mathbb{S}_{mn}^{\text{dev}} = 0 \quad (21.30)$$

due to symmetry of the deviatoric rate of strain tensor,  $\mathbb{S}_{mn}^{\text{dev}} = \mathbb{S}_{nm}^{\text{dev}}$ , and anti-symmetry of the rotation tensor,  $\mathbb{A}_{mn}$  (see Section 13.3.5 as well as Exercise 1.2). We can show that the second term in equation (21.27e) is sign-definite by noting that

$$\mathbb{S}_{mn}^{\text{dev}} \mathbb{S}_{mn}^{\text{dev}} = (\mathbb{S}_{mn} - \delta_{mn} \mathbb{S}_{qq}/3)^2 \quad (21.31\text{a})$$

$$= \mathbb{S}_{mn} \mathbb{S}_{mn} + \delta_{mn} \delta_{mn} \mathbb{S}_{qq} \mathbb{S}_{qq}/9 - 2 \mathbb{S}_{mn} \delta_{mn} \mathbb{S}_{qq}/3 \quad (21.31\text{b})$$

$$= \mathbb{S}_{mn} \mathbb{S}_{mn} + (\mathbb{S}_{qq})^2/3 - 2 (\mathbb{S}_{qq})^2/3 \quad (21.31\text{c})$$

$$= \mathbb{S}_{mn} (\mathbb{S}_{mn} - \delta_{mn} \mathbb{S}_{qq}/3) \quad (21.31\text{d})$$

$$= \mathbb{S}_{mn} \mathbb{S}_{mn}^{\text{dev}}. \quad (21.31\text{e})$$

We are thus left

$$\rho \mathbf{v} \cdot \mathbf{F} = 2 \nabla \cdot (\rho \nu \mathbf{v} \cdot \mathbb{S}^{\text{dev}}) - 2 \rho \nu \mathbb{S}^{\text{dev}} \cdot \mathbb{S}^{\text{dev}}, \quad (21.32)$$

with

$$\mathbb{S}^{\text{dev}} \cdot \mathbb{S}^{\text{dev}} = \mathbb{S}_{mn}^{\text{dev}} \mathbb{S}_{mn}^{\text{dev}}. \quad (21.33)$$

We interpret the two contributions to the frictional power in equation (21.32) as

$$\rho \mathbf{v} \cdot \mathbf{F} = \text{divergence of viscous flux} - \text{kinetic energy dissipation}. \quad (21.34)$$

The divergence theorem means that when integrated over the full domain, the flux divergence becomes a contribution from boundary stresses, and boundary stresses can either increase or decrease kinetic energy according to the boundary processes. In contrast, the sign-definite dissipation term provides a sink to the kinetic energy at each point in the fluid interior. This frictional dissipation is commonly written

$$\epsilon \equiv [\mathbf{v} \cdot \mathbf{F}]_{\text{dissipate}} = 2 \nu \mathbb{S}^{\text{dev}} \cdot \mathbb{S}^{\text{dev}} \geq 0. \quad (21.35)$$

The dimensions of  $\epsilon$  are  $L^2 T^{-3}$ , which in SI units are  $m^2 s^{-3} = W \text{ kg}^{-1}$ . We thus refer to  $\epsilon$  as the kinetic energy dissipation per mass due to viscous effects.

### 21.3.3 Mechanical energy budget

Adding the material time evolution equations for kinetic energy per mass and gravitational potential energy per mass leads to the material form of the mechanical energy per mass

$$\rho \frac{Dm}{Dt} = -\mathbf{v} \cdot \nabla p + 2 \nabla \cdot (\rho \nu \mathbf{v} \cdot \mathbb{S}^{\text{dev}}) + \rho (-\epsilon + \partial_t \Phi) \quad (21.36\text{a})$$

$$= -\nabla \cdot (p \mathbf{v} - 2 \rho \nu \mathbf{v} \cdot \mathbb{S}^{\text{dev}}) + p \nabla \cdot \mathbf{v} + \rho (-\epsilon + \partial_t \Phi) \quad (21.36\text{b})$$

$$= -\nabla \cdot \mathbf{J}_{\text{mech}} + p \nabla \cdot \mathbf{v} + \rho (-\epsilon + \partial_t \Phi), \quad (21.36\text{c})$$

where

$$m = \mathcal{K} + \Phi \quad (21.37)$$

is the mechanical energy per mass for a fluid element. As already anticipated, there is a cancellation of the mechanical energy exchange due to motion through the gravitational field, though the time-dependent geopotential provides a source of mechanical energy. The final equality introduced the mechanical energy flux

$$\mathbf{J}_{\text{mech}} = p \mathbf{v} - 2\rho\nu \mathbf{v} \cdot \mathbb{S}^{\text{dev}} = -\mathbf{v} \cdot (-p \mathbb{I} + \tau) = -\mathbf{v} \cdot \mathbb{T}. \quad (21.38)$$

We see that the material evolution of mechanical energy arises from the convergence of the mechanical energy flux, plus the work done by pressure, effects from frictional dissipation (more discussed in Section 21.5.3), and the time changes to the geopotential.

### 21.3.4 Further study

The physics of mechanical energy dissipation forms a central role in the study of ocean mixing and its measurement. [MacKinnon et al. \(2013\)](#) is a useful place to begin studying this active field of physical oceanography.

As shown in Section 17.8 of [Griffies \(2004\)](#), we can relate the global integral of the kinetic energy dissipation to the friction vector by taking the functional derivative of the dissipation with respect to the velocity field. This connection follows from the self-adjoint nature of the friction operator and it has been found to be a useful framework for numerical discretization of viscous friction (e.g., [Griffies and Hallberg \(2000\)](#)).

## 21.4 Thermodynamics of a moving fluid

Recall the fundamental thermodynamic relation (20.76b) for a two-component fluid such as seawater or the atmosphere

$$dJ = T dS - p d\nu_s + \mu dC. \quad (21.39)$$

This relation is an expression of the first law of thermodynamics for a quasi-static process. It provides an expression for the exact differential of internal energy for a thermodynamic system as it transitions from one thermodynamic equilibrium to another.

Now consider a finite region of fluid comprised of fluid elements. The fluid region generally experiences mechanical and thermal forces that support macroscopic motion. However, we assume that each fluid element is in local thermodynamic equilibrium. This assumption is supported by noting that the equilibrium time scale for the microscopic degrees of freedom within an individual fluid element is tiny compared to the equilibrium time scales of the macroscopic motion. We discussed this extremely large time scale separation in Section 20.1.3 when presenting the notion of a quasi-static process. Within this regime, we are justified in making use of quasi-equilibrium thermodynamics in which we use equilibrium thermodynamics locally yet allow for macroscopic gradients in fluid properties. That is, each fluid element is locally in thermodynamic equilibrium while it is out of equilibrium with its neighbors.

### 21.4.1 Concerning the transition to a moving fluid

For a moving continuous fluid, each of the thermodynamic properties in the equilibrium first law expression (21.39) are continuous functions of space and time. Furthermore, equation (21.39) provides a relation between exact differentials as detailed in Section 2.8. As exact differentials of continuous space-time fields, we can make use of the space-time increments detailed in Section 12.5.1 to write

$$d\Psi = \Psi(\mathbf{x} + d\mathbf{x}, t + dt) - \Psi(\mathbf{x}, t) = dt \partial_t \Psi + d\mathbf{x} \cdot \nabla \Psi, \quad (21.40)$$

where  $\Psi$  is one of the thermodynamic properties,  $dt$  is the infinitesimal time increment, and  $d\mathbf{x}$  is the vector of infinitesimal space increments. Following the discussion in Section 12.5.2, we are thus led to the total time derivative for a property following a trajectory  $\mathbf{x} = \mathbf{X}(t)$

$$\frac{d\Psi}{dt} = \frac{\partial\Psi}{\partial t} + \frac{d\mathbf{X}}{dt} \cdot \nabla\Psi. \quad (21.41)$$

Restricting the trajectory to that defined by a fluid particle, so that  $\mathbf{v} = d\mathbf{X}/dt$ , renders the material time derivative as in Section 12.5.4

$$\frac{D\Psi}{Dt} = \frac{\partial\Psi}{\partial t} + \mathbf{v} \cdot \nabla\Psi. \quad (21.42)$$

We make use of this result in Section 21.4.5 to transition the quasi-static relation (21.39) to a moving fluid.

### 21.4.2 Thermodynamic properties as space-time fields

There is room for confusion when allowing thermodynamic properties to extend to space-time functions. The confusion arises when not being clear on whether a mathematical expression refers to an equilibrium thermodynamic relation between thermodynamic variables, as in the fundamental thermodynamic relation (21.39), or whether it expresses a relation involving space-time field representations of thermodynamic properties. The distinction is important especially when considering derivatives and integrals as it is necessary to know what are the other variables to be held fixed in the process of performing the operations.

For example, consider the middle relation in equation (20.106), which says that the partial derivative of the Gibbs potential with respect to pressure, holding temperature and concentration fixed, equals to the specific volume

$$\left[ \frac{\partial\mathcal{G}}{\partial p} \right]_{T,C} = \nu_s = \rho^{-1}. \quad (21.43)$$

However, if we encounter the Gibbs potential as a space-time function, and we use pressure as a generalized vertical coordinate, then we might find need to compute the distinct partial derivative

$$\left[ \frac{\partial\mathcal{G}}{\partial p} \right]_{x,y,t} \neq \left[ \frac{\partial\mathcal{G}}{\partial p} \right]_{T,C}. \quad (21.44)$$

When appropriate, we offer reminders to help avoid a cascade of misunderstandings. One point where this reminder is particularly useful is when discussing energetics for a Boussinesq fluid in Section 23.6.

### 21.4.3 Thermodynamic relations for steady state flow

Before considering time evolution, let us establish some steady (stationary) state relations defined for flows that have no Eulerian time dependence. In this case, the exact differential for a thermodynamic potential arises just from spatial variations

$$d\Psi = \Psi(\mathbf{x} + d\mathbf{x}) - \Psi(\mathbf{x}) = d\mathbf{x} \cdot \nabla\Psi \quad \Leftarrow \text{steady state.} \quad (21.45)$$

Applying this result to the fundamental thermodynamic expression (21.39) renders the steady state relation

$$d\mathbf{x} \cdot (\nabla\mathcal{I} - T \nabla\mathcal{S} + p \nabla\nu_s - \mu \nabla C) = 0. \quad (21.46)$$

Since the spatial increment  $d\boldsymbol{x}$  is arbitrary, the bracketed term generally vanishes

$$\nabla \mathcal{J} = T \nabla \mathcal{S} - p \nabla \nu_s + \mu \nabla C \quad \Leftarrow \text{steady state.} \quad (21.47)$$

Analogous identities hold for steady state thermodynamic potentials following from the fundamental thermodynamic relations derived in Section 20.7

#### STEADY STATE FLOW

$$\nabla \mathcal{J} = T \nabla \mathcal{S} - p \nabla \nu_s + \mu \nabla C \quad (21.48)$$

$$T \nabla \mathcal{S} = \nabla \mathcal{J} + p \nabla \nu_s - \mu \nabla C \quad (21.49)$$

$$\nabla \mathcal{H} = T \nabla \mathcal{S} + \nu_s \nabla p + \mu \nabla C \quad (21.50)$$

$$\nabla \mathcal{G} = -\mathcal{S} \nabla T + \nu_s \nabla p + \mu \nabla C. \quad (21.51)$$

#### 21.4.4 Materially constant specific entropy for a perfect fluid

Each material fluid parcel within a perfect fluid maintains a constant specific entropy given that it experiences no dissipation (friction is absent), maintains a constant composition (mixing is absent), and encounters no heating (adiabatic). Consequently, specific entropy for each fluid parcel is reversibly stirred through advection

$$\frac{D\mathcal{S}}{Dt} = \frac{\partial \mathcal{S}}{\partial t} + \boldsymbol{v} \cdot \nabla \mathcal{S} = 0. \quad (21.52)$$

Notably, a perfect fluid generally admits nonzero gradients of specific entropy even as each fluid element moves without altering its specific entropy.

#### 21.4.5 First law for a moving fluid element

Section 21.4.1 provides the key operational means for developing the equations of quasi-equilibrium thermodynamics, in which we apply the equilibrium thermodynamic relations to moving and evolving fluid elements. Consequently, the equilibrium relation (21.39), which is the first law for a quasi-static process, takes the form for a moving fluid element

$$\frac{D\mathcal{J}}{Dt} = T \frac{D\mathcal{S}}{Dt} - p \frac{D\nu_s}{Dt} + \mu \frac{DC}{Dt}. \quad (21.53)$$

Exposing the Eulerian space and time derivatives renders

$$\partial_t \mathcal{J} - T \partial_t \mathcal{S} + p \partial_t \nu_s - \mu \partial_t C + \boldsymbol{v} \cdot (\nabla \mathcal{J} - T \nabla \mathcal{S} + p \nabla \nu_s - \mu \nabla C) = 0. \quad (21.54)$$

As discussed in Section 21.4.3, for a steady state flow all Eulerian time derivatives vanish and the spatial gradients reduce to the steady state relation (21.48). For the general case of a time dependent flow, the thermodynamic potentials are changing in both space and time so that the first law takes on the material time evolution expression (21.53).

We can massage the result (21.53) to further reveal its connection to the first law written in the form (21.39). For this purpose, recall that mass conservation as discussed in Section 14.2 means that changes in the volume of a fluid element are related to density changes via

$$\frac{1}{\delta V} \frac{D\delta V}{Dt} = \frac{1}{\nu_s} \frac{D\nu_s}{Dt}, \quad (21.55)$$

where  $\nu_s = \rho^{-1}$  is the specific volume. Hence, equation (21.53) can be written

$$\delta M \frac{D\mathcal{J}}{Dt} = T \delta M \frac{D\mathcal{S}}{Dt} - p \frac{D\delta V}{Dt} + \mu \delta M \frac{DC}{Dt}, \quad (21.56)$$

where  $\delta M = \rho \delta V$  is the mass of the fluid element. Since the mass of the fluid element is constant, equation (21.56) is the fluid element extension of the first law given by equation (21.39). Alternatively, we can use the further result from mass conservation (equation (14.26))

$$\frac{1}{\delta V} \frac{D\delta V}{Dt} = \nabla \cdot \mathbf{v} \quad (21.57)$$

to write

$$\frac{D\mathcal{J}}{Dt} = -p \nu_s \nabla \cdot \mathbf{v} + T \frac{D\mathcal{S}}{Dt} + \mu \frac{DC}{Dt}. \quad (21.58)$$

Processes affecting internal energy that appear on the right hand side are (i) mechanical work from pressure modifying the volume of the fluid element, (ii) entropy production, whose form is developed in Sections 21.5 and 21.7, and (iii) mixing (chemical work) through the exchange of matter constituents between fluid elements. We provide further details for the first law in Section 21.5 when considering the budget for the total energy of a fluid element.

## 21.4.6 Enthalpy budget

Rather than work with internal energy, it is often more convenient to consider the specific enthalpy (Section 20.7.4),

$$\mathcal{H} = \mathcal{I} + p/\rho = \mathcal{I} + p \nu_s. \quad (21.59)$$

The mass continuity equation (14.20) and the internal energy equation (21.58) yield

$$\frac{D\mathcal{H}}{Dt} = \frac{D\mathcal{J}}{Dt} + \frac{1}{\rho} \frac{Dp}{Dt} - \frac{p}{\rho^2} \frac{D\rho}{Dt} \implies \rho \frac{D\mathcal{H}}{Dt} = \frac{Dp}{Dt} + \rho \left[ T \frac{D\mathcal{S}}{Dt} + \mu \frac{DC}{Dt} \right]. \quad (21.60)$$

The specific enthalpy equation (21.60) says that for constant pressure processes, changes to specific enthalpy of a moving fluid element arise just from those processes that give rise to changes in specific entropy and changes in matter concentration

$$\frac{Dp}{Dt} = 0 \implies \frac{D\mathcal{H}}{Dt} = T \frac{D\mathcal{S}}{Dt} + \mu \frac{DC}{Dt}. \quad (21.61)$$

Since many boundary processes occur approximately at near constant pressure (e.g., air-sea fluxes), this result motivates formulating boundary fluxes of matter and thermal energy in terms of enthalpy fluxes rather than internal energy fluxes. Also, the mixing of fluid elements occurs locally in space so that pressure of fluid elements is the same when they mix, again making enthalpy a useful thermodynamic potential when studying mixing.

## 21.4.7 Thermal and chemical processes and fluxes

The internal energy of a fluid element is modified by the diabatic transfer of thermal energy. We are generally concerned with two thermal fluxes, one due to conduction and one due to radiation

$$\mathbf{J}_{\text{therm}} = \mathbf{J}_{\text{cond}} + \mathbf{J}_{\text{rad}}. \quad (21.62)$$

Details of the radiant flux require topics outside our scope so we leave it unspecified. However, we consider forms for heat conduction in Section 21.7, with the simplest form being *Fourier's law*

whereby  $\mathbf{J}_{\text{cond}}$  is directed down the temperature gradient.

The internal energy of a fluid element also changes through changes in the matter concentration. This change occurs when fluid elements mix at constant pressure. As mentioned in Section 21.4.6, enthalpy is the proper thermodynamic potential to consider for examining the mixing of matter concentrations. We thus assume that the transfer of chemical energy associated with a matter flux,  $\mathbf{J}_C$ , leads to a corresponding chemical energy flux given by

$$\mathbf{J}_{\text{chem}} = \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} \mathbf{J}_C. \quad (21.63)$$

The enthalpy partial derivative is computed at constant pressure and temperature so to isolate the energy change associated just with mixing of matter. It is important to distinguish this partial derivative with the distinct derivative that leads to the chemical potential as in equation (20.96)

$$\left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{S,p} = \mu. \quad (21.64)$$

As shown by Exercise 20.2, the two partial derivatives are related by

$$\left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} = \mu - T \left[ \frac{\partial \mu}{\partial T} \right]_{C,p}, \quad (21.65)$$

and we make use of this relation when studying the entropy budget in Section 21.7.

Details of the thermal and chemical fluxes are undetermined at this point. We garner further insights through studying the budget for total energy in Section 21.5 as well as the entropy budget and second law of thermodynamics in Section 21.7. Furthermore, the conductive and chemical fluxes are those that arise from molecular motions rather than turbulent motions. Turbulent fluxes are determined by properties of the flow whereas  $\mathbf{J}_{\text{cond}}$  and  $\mathbf{J}_{\text{chem}}$  are determined by properties of the fluid. Since turbulent fluxes are far larger than molecular fluxes, the constraints detailed in this section have little practical applications for a realistic geophysical fluid. Even so, it is remarkable how far the laws of thermodynamics can be used to constrain these molecular flux laws.

#### 21.4.8 First law for homogeneous fluids in terms of potential temperature

Equation (20.155) says that the change in entropy for a fluid element moving with constant matter concentration and at the reference pressure is given in terms of the potential temperature

$$\frac{D\dot{S}}{Dt} = \frac{c_p}{\theta} \frac{D\theta}{Dt} \quad (21.66)$$

Since the potential temperature equals to the temperature when  $p = p_R$ , we have

$$c_p \frac{D\theta}{Dt} = \theta \frac{D\dot{S}}{Dt} = \dot{Q} \quad \text{at } p = p_R \text{ and } dC = 0. \quad (21.67)$$

In Exercise 21.6 we consider these relations for an ideal gas.

#### 21.4.9 Further study

*DeGroot and Mazur* (1984) provide an authoritative accounting of quasi-equilibrium thermodynamics as applied to continuum matter such as a fluid. *Gregg* (1984) and *Davis* (1994) apply these methods to small-scale mixing in the ocean. Slightly different formulations can be found in *Landau and Lifshitz* (1987) and *Batchelor* (1967).

## 21.5 Budget for total energy

Recall from Section 10.9 that a point particle conserves its mechanical energy in the absence of friction. In contrast, the mechanical energy for a fluid element is not materially constant even when only conservative forces act on the element. The reason is that for the continuum fluid, there is (i) a conversion between mechanical energy and internal energy as pressure does work to alter the volume of fluid elements, and (ii) frictional dissipation of kinetic energy irreversibly converts some kinetic energy to internal energy through Joule heating (Section 21.5.3). In this section we combine the mechanical energy budget from Section 21.3 to the internal energy budget from Section 21.4, thus rendering the budget for total energy of a fluid element. We furthermore postulate that the domain integrated total energy changes only due to boundary effects, as well as possible changes in the geopotential. This assumption then leads to further specifications of the processes contributing to the internal energy and enthalpy budgets.

### 21.5.1 Postulating the budget for total energy

The total energy per mass of a fluid element is the sum of the internal energy plus the mechanical energy,

$$\mathcal{E} = \mathcal{I} + \mathcal{M} = \mathcal{I} + \mathcal{K} + \Phi. \quad (21.68)$$

We postulate that this total energy satisfies a conservation law whereby it is affected only by the convergence of a total energy flux, plus a source due to temporal changes in the geopotential

$$\rho \frac{D\mathcal{E}}{Dt} = -\nabla \cdot \mathbf{J}_{\mathcal{E}} + \rho \partial_t \Phi. \quad (21.69)$$

Correspondingly, the Eulerian flux form equation is

$$\frac{\partial(\rho \mathcal{E})}{\partial t} + \nabla \cdot (\rho \mathbf{v} \mathcal{E} + \mathbf{J}_{\mathcal{E}}) = \rho \partial_t \Phi. \quad (21.70)$$

The flux of total energy is given by

$$\rho \mathbf{v} \mathcal{E} + \mathbf{J}_{\mathcal{E}} = \rho \mathbf{v} \mathcal{E} + \mathbf{J}_{\text{therm}} + \mathbf{J}_{\text{chem}} + \mathbf{J}_{\text{mech}} \quad (21.71a)$$

$$= \rho \mathbf{v} \mathcal{E} + \mathbf{J}_{\text{therm}} + \mathbf{J}_{\text{chem}} - \mathbf{v} \cdot (-p \mathbb{I} + \mathbf{\tau}) \quad (21.71b)$$

$$= \rho \mathbf{v} (\mathcal{E} + p/\rho) + \mathbf{J}_{\text{therm}} + \mathbf{J}_{\text{chem}} - \mathbf{v} \cdot \mathbf{\tau}, \quad (21.71c)$$

where  $\mathbf{J}_{\text{therm}}$  and  $\mathbf{J}_{\text{chem}}$  were discussed in Section 21.4.7, and  $\mathbf{J}_{\text{mech}}$  was derived in Section 21.3.3. We have more to say concerning the flux of total energy in Section 21.6 when studying the Bernoulli potential.

We are led to postulate the total energy equation (21.69) through assuming that  $\int_{\mathcal{R}} \rho \mathcal{E} dV$  remains constant in time for a region,  $\mathcal{R}$ , that is closed to thermal, material, and mechanical interactions, and one where the geopotential is constant in time. This assumption is based on our understanding of molecular and atomic mechanics.

### 21.5.2 Budgets for internal energy and enthalpy

We now have the total energy budget as postulated in the form of equation (21.69), along with the mechanical energy budget derived in equation (21.36c). Subtracting the two yields the internal energy budget

$$\rho \frac{D(\mathcal{E} - \mathcal{M})}{Dt} = \rho \frac{D\mathcal{I}}{Dt} = -\nabla \cdot (\mathbf{J}_{\text{therm}} + \mathbf{J}_{\text{chem}}) - p \nabla \cdot \mathbf{v} + \rho \epsilon. \quad (21.72)$$

This equation provides yet another expression for the first law of thermodynamics for a moving fluid element. It says that the internal energy of a fluid element is modified through the convergence of thermal and chemical fluxes, pressure work that alters the volume of a fluid element, and frictional dissipation through viscosity. Both the pressure work and frictional dissipation are exchanged with mechanical energy, and so they appear with opposite signs in the two budget equations. We further specify the thermal and chemical fluxes in Section 21.7 when studying the entropy budget.

Finally, we make use of the enthalpy equation (21.60) to render the enthalpy budget

$$\rho \frac{D\mathcal{H}}{Dt} - \frac{Dp}{Dt} = -\nabla \cdot (\mathbf{J}_{\text{therm}} + \mathbf{J}_{\text{chem}}) + \rho\epsilon. \quad (21.73)$$

We return to this equation in Section 21.8 when studying the evolution of temperature, where we introduce the potential enthalpy and Conservative Temperature.

### 21.5.3 Joule heating from friction

Frictional dissipation,  $\epsilon > 0$ , measures the conversion of kinetic energy into heat, and it is thus a conversion from mechanical energy to internal energy

$$\dot{Q}_{\text{Joule}} \equiv \epsilon. \quad (21.74)$$

This term is referred to as *Joule heating* in analog to the process that occurs in electrical circuits. The Joule heating of a fluid by molecular viscosity is larger in regions where the fluid strains are larger, signalling a more efficient transfer of power to the microscales where molecular viscosity can act on the flow.

In the ocean interior, measurements indicate that  $\epsilon \approx 10^{-9} \text{ W kg}^{-1}$ . Dividing by  $c_p = 3900 \text{ J kg}^{-1} \text{ K}^{-1}$  leads to a heating rate of less than  $10^{-3} \text{ K century}^{-1}$ , which is a very small rate of ocean heating. Consequently, ocean Joule heating has a negligible role in the ocean heat budget and as such is generally ignored. Atmospheric flows are roughly two orders faster so that the kinetic energy per mass is four orders larger. The larger flow speeds lead to larger shears thus creating larger viscous dissipation that reaches roughly  $\epsilon \approx 2 \text{ W m}^{-2}$  globally averaged. Hence, Joule heating is an important part of the global atmosphere enthalpy budget (Becker, 2003).

### 21.5.4 Comments on gauge symmetry

Consider again the Eulerian flux equation for total energy (21.70). It is notable that the time tendency for the total energy remains unchanged if we shift the flux of total energy by a curl,

$$\rho \mathcal{E} \mathbf{v} + \mathbf{J}_{\mathcal{E}} \rightarrow \rho \mathcal{E} \mathbf{v} + \mathbf{J}_{\mathcal{E}} + \nabla \times \mathbf{G}, \quad (21.75)$$

with  $\mathbf{G}$  referred to as a *gauge function*. This arbitrariness in the definition of total energy flux is ubiquitous in physics; e.g., see the discussion of the electromagnetic field energy flux in Section 27-4 in Volume II of Feynman et al. (1963).<sup>4</sup> It means that the energy flux itself has no unique local physical meaning; only its convergence has a meaning as it gives rise to time changes in the energy at a point in space.

We also encounter such *gauge symmetry* in the potential vorticity flux discussed in Chapter 37, as well as the vector streamfunction for an incompressible fluid in Section 16.5.1. In some cases we can exploit the symmetry to our subjective desires, such as discussed in Section 37.5.6

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<sup>4</sup>The Feynman lectures are available online through the California Institute of Technology.

for potential vorticity. However, we know of no strategic use of gauge symmetry for the study of energy budgets.

### 21.5.5 Further study

The postulate of globally integrated total energy conservation in Section 21.5.1, and the associated discussion of energy budgets, follow that from Chapter 14 of [Callen \(1985\)](#), Sections 49 and 58 of [Landau and Lifshitz \(1987\)](#), Section II.4 of [DeGroot and Mazur \(1984\)](#), Chapters 3 and 4 of [Müller \(2006\)](#), Appendix B of [IOC et al. \(2010\)](#), Section 2.4 of [Olbers et al. \(2012\)](#), Chapter 1 of [Vallis \(2017\)](#), and Section 13.5.5 of [Thorne and Blandford \(2017\)](#).

## 21.6 Bernoulli potential

The total energy equation (21.69) reveals that the material time change for the total energy of a fluid element is affected by the convergence of pressure times velocity. Hence, even in the absence of irreversible processes and with a time-independent geopotential, the total energy of a fluid element is not materially invariant. The energy source term  $p\mathbf{v}$  is fundamental to energy within the continuum. As shown in this section, it is the pressure work required for the fluid element to mechanically exist within the continuum. We refer to it as the mechanical *injection work*.

### 21.6.1 Bernoulli potential and mechanical injection work

Consider the Eulerian flux form equation for the total energy, (21.70), written here in the form

$$\frac{\partial(\rho\mathcal{E})}{\partial t} + \nabla \cdot [\rho\mathbf{v}(\mathcal{E} + p/\rho) + \mathbf{J}_{\text{therm}} + \mathbf{J}_{\text{chem}} - \mathbf{v} \cdot \boldsymbol{\tau}] = \rho \partial_t \Phi. \quad (21.76)$$

The left hand side indicates that total energy of a fluid element is locally modified by the advective transport of the quantity

$$\mathcal{E} + p/\rho = (\mathcal{K} + \Phi) + (\mathcal{J} + p/\rho) = \mathcal{M} + \mathcal{H} \equiv \mathcal{B}, \quad (21.77)$$

where we introduced the *Bernoulli potential*, which is the sum of the mechanical energy per mass plus the enthalpy per mass

$$\mathcal{B} = \mathcal{M} + \mathcal{H} = \mathcal{K} + \Phi + \mathcal{J} + p/\rho. \quad (21.78)$$

For a perfect fluid there is no irreversible transfer of heat, matter, or momentum so that

$$\mathbf{J}_{\text{therm}} = 0 \quad \text{and} \quad \mathbf{J}_{\text{chem}} = 0 \quad \text{and} \quad \boldsymbol{\tau} = 0. \quad (21.79)$$

Hence, we see that integration over a region with zero boundary transfer of  $\mathbf{v}\mathcal{B}$  leads to the conservation of total energy for a perfect fluid with a time independent geopotential.

Why is  $\rho\mathcal{E}$  affected by the convergence of  $\rho\mathbf{v}\mathcal{B}$  rather than the convergence of  $\rho\mathbf{v}\mathcal{E}$ ? To answer this question,<sup>5</sup> again note that the Bernoulli potential is the sum of the total energy per mass of a fluid element,  $\mathcal{E}$ , plus the term  $p/\rho = p\nu_s$ . So what is  $p\nu_s$ ? Imagine carving out a tiny region from within a continuous fluid with pressure  $p$  and specific volume  $\nu_s$ , leaving behind a “hole”. The mechanical work required to carve out this hole is precisely equal to  $p\nu_s$ . Correspondingly, we interpret  $p\nu_s$  as the mechanical work required to inject a unit mass of fluid with specific volume  $\nu_s$  into a region with pressure  $p$ . We thus refer to  $p\nu_s$  as the *injection work*,

<sup>5</sup>This argument follows Section 13.5.4 of [Thorne and Blandford \(2017\)](#) as well as Section 6 of [Landau and Lifshitz \(1987\)](#).

and we in turn see that specific enthalpy,  $\mathcal{H} = \mathcal{I} + p/\rho$  (equation (21.59)), measures the internal energy plus the mechanical work required for a fluid element to exist within a continuum.

We can support the above interpretation by considering the flux,  $\rho \mathbf{v} \mathcal{B}$ , in a perfect fluid that penetrates a static closed fluid region

$$\oint_{\partial\mathcal{R}} \rho \mathbf{v} \mathcal{B} \cdot \hat{\mathbf{n}} dS = \oint_{\partial\mathcal{R}} \rho \mathbf{v} \mathcal{E} \cdot \hat{\mathbf{n}} dS + \oint_{\partial\mathcal{R}} p \mathbf{v} \cdot \hat{\mathbf{n}} dS. \quad (21.80)$$

The first term is the flux of total energy (mechanical plus internal) that penetrates the boundary,  $\partial\mathcal{R}$ . The second term is the mechanical work done by pressure acting on the surface. The pipe flow example in Section 21.6.2 further supports this perspective.

### 21.6.2 Bernoulli's theorem for a steady perfect fluid

Consider a perfect fluid flow in steady state (vanishing Eulerian time derivatives). Steady state mass conservation means that

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot (\rho \mathbf{v}) = 0. \quad (21.81)$$

This relation, along with a steady state energy in equation (21.76) (absent friction, heating, mixing, and with a time-independent geopotential), means that the steady state velocity field is parallel to contours of constant Bernoulli potential

$$\mathbf{v} \cdot \nabla \mathcal{B} = 0. \quad (21.82)$$

We thus see that for the perfect fluid to be in a steady state, the Bernoulli potential is constant along streamlines, which is a result known as *Bernoulli's theorem*. Hence, as the fluid moves along a streamline, there is an exchange between the total energy per mass,  $\mathcal{E}$ , and the injection work,  $p \nu_s$ , such that their sum remains constant.

A constant Bernoulli potential for steady flow is used frequently in engineering fluid dynamics to interpret flow around objects, such as for flow around a wing, in which case the sum  $p + \rho \mathbf{v}^2/2$  is sometimes referred to as the *total pressure* or *stagnation pressure*. It leads to a realization of *Bernoulli's Principle*, whereby in regions of low pressure the energy per mass is relatively large, whereas the converse holds in regions of high pressure. The change in energy is largely due to a change in the kinetic energy, so that flow is fast in regions of low pressure (e.g., top of the wing, flow around a train moving through a tunnel) and slow in regions of high pressure (e.g., bottom of the wing). We revisit Bernoulli's Principle in Section 29.1.2 when studying inviscid and irrotational flow.

### 21.6.3 Traditional derivation of Bernoulli's theorem

For completeness we offer a second derivation of Bernoulli's theorem that follows a more traditional route and reveals some useful manipulations. For this purpose, convert the advective-form momentum equation (17.16) into its vector-invariant form by making use of the vector identity (see Section 2.3.4)

$$\boldsymbol{\omega} \times \mathbf{v} = -\mathcal{K} + (\mathbf{v} \cdot \nabla) \mathbf{v}. \quad (21.83)$$

This identity allows us to eliminate velocity self-advection in favor of the vorticity and kinetic energy per mass

$$\frac{\partial \mathbf{v}}{\partial t} + \boldsymbol{\omega}_a \times \mathbf{v} = -\frac{1}{\rho} \nabla p - \nabla m, \quad (21.84)$$

where

$$\omega_a = \omega + 2\Omega \quad (21.85)$$

is the absolute vorticity (see Chapter 35) and we set the irreversible terms to zero since we are assuming a perfect fluid. The Eulerian time evolution for the kinetic energy per mass is therefore given by

$$\frac{\partial \mathcal{K}}{\partial t} = -\frac{1}{\rho} \mathbf{v} \cdot \nabla p - \mathbf{v} \cdot \nabla m, \quad (21.86)$$

where we set  $\mathbf{v} \cdot (\omega_a \times \mathbf{v}) = 0$ .

For Bernoulli's theorem we are interested in the steady state, with a steady kinetic energy per mass realized by the balance

$$\rho^{-1} \mathbf{v} \cdot \nabla p = -\mathbf{v} \cdot \nabla m. \quad (21.87)$$

We can connect this steady state balance to the Bernoulli potential by noting that for a steady perfect fluid, equation (21.50) relates the pressure gradient force to

$$-\rho^{-1} \nabla p = -\nabla \mathcal{H} + T \nabla \mathcal{S}. \quad (21.88)$$

Combining with equation (21.87) renders

$$\mathbf{v} \cdot (\nabla \mathcal{H} + \nabla m - T \nabla \mathcal{S}) = \mathbf{v} \cdot (\nabla \mathcal{B} - T \nabla \mathcal{S}) = 0. \quad (21.89)$$

A perfect fluid maintains materially constant specific entropy (Section 21.4.4), which in a steady state means that

$$\mathbf{v} \cdot \nabla \mathcal{S} = 0 \quad \text{and} \quad \mathbf{v} \cdot \nabla \mathcal{B} = 0 \quad \iff \text{steady state perfect fluid.} \quad (21.90)$$

That is, for a steady perfect fluid the velocity is aligned with isosurfaces of specific entropy and Bernoulli potential.

#### 21.6.4 Steady flow of constant density perfect fluid in a pipe

To help further understand Bernoulli's theorem and the contribution from the mechanical work provided by pressure forces, consider the steady flow of a constant density perfect fluid in a frictionless pipe as depicted in Figure 21.1. For this system, Bernoulli's theorem says that the following quantity is constant for flow along a streamline

$$\mathbf{v}^2/2 + p/\rho + g z = \text{constant}. \quad (21.91)$$

Note that internal energy dropped out since for a constant density fluid the internal energy is a constant and so plays no role in the energetics. We now show that the statement (21.91) of Bernoulli's theorem can be derived through traditional energetic arguments, whereby the work done on the fluid system equals to the system's change in kinetic energy (see Section 9.1.5 for the particle mechanics version of this *work-energy theorem*).

For this purpose, let the system under examination be a control volume of fluid as described in the caption to Figure 21.1, and examine the work done on the control volume over an arbitrary time increment,  $\Delta t$ . During this time, a mass of fluid given by

$$M = \rho A_1 u_1 \Delta t = \rho A_2 u_2 \Delta t \quad (21.92)$$

moves through the pipe, with  $A_1 u_1 = A_2 u_2$  following from volume conservation, and we assumed that the  $u_{1,2} = \Delta x_{1,2}/\Delta t$  measures the average velocity across the pipe cross-section. Mechanical

work is applied to the fluid in the control volume by pressure acting on the end caps (contact force) and by gravity acting throughout the fluid (body force).

- **PRESSURE WORK:** At the left end cap, pressure from fluid to the left of the control volume does work on the control volume by the amount  $p_1 A_1 \Delta x_1 = p_1 M/\rho$ . On the right end, the control volume does work on the fluid to its right, which means that a negative work is applied to the control volume in the amount  $-p_2 A_2 \Delta x_2 = -p_2 M/\rho$ .
- **GRAVITATIONAL WORK:** Fluid downstream at the right end is higher than fluid upstream on the left end. The control volume must do work against gravity to achieve this altitude increase and this work is given by  $-g M (z_2 - z_1)$ .

As the fluid moves from left to right, the control volume changes its kinetic energy by the amount  $(M/2)(u_2^2 - u_1^2)$ . Equating this kinetic energy change to the work applied to the control volume renders

$$(1/2)(u_2^2 - u_1^2) = (1/\rho)(p_1 - p_2) - g(z_2 - z_1), \quad (21.93)$$

where the mass,  $M$ , dropped out. Rearrangement then leads to

$$u^2/2 + p/\rho + g z = \text{constant}, \quad (21.94)$$

which is a statement of Bernoulli's theorem (21.91). Furthermore, the pressure difference between the left and right end of the pipe is given by

$$p_1 - p_2 = \rho g (z_2 - z_1) + (\rho/2) u_1^2 [1 - (A_1/A_2)^2] > 0. \quad (21.95)$$

We expect  $p_1 > p_2$  given the assumed fluid motion from left to right, whereby pressure on the left end must be larger than the right end to support this flow. This example thus supports our understanding of how pressure provides a mechanical work on fluid control volume boundaries. Indeed, taking the control volume to be a tiny fluid element furthers our interpretation of the  $p/\rho$  contribution to the Bernoulli potential (21.77).

### 21.6.5 Further study

For an examination of Bernoulli's theorem for non-rotating flows, such as flow in laminar boundary layers, see [this video](#) from Prof. Shapiro.

## 21.7 Entropy budget for the ocean

In this section we consider the entropy budget for the ocean and make use of the second law of thermodynamics to infer some specific forms for the thermal and chemical fluxes that were introduced in Section 21.4.7. To start, we note that the entropy budget follows simply by rearranging the enthalpy equation (21.60)

$$\rho T \frac{D\mathcal{S}}{Dt} = \rho \frac{D\mathcal{H}}{Dt} - \frac{Dp}{Dt} - \rho \mu \frac{DC}{Dt}, \quad (21.96)$$

with the enthalpy budget in the form (21.73) yielding

$$T \rho \frac{D\mathcal{S}}{Dt} = -\nabla \cdot (\mathbf{J}_{\text{therm}} + \mathbf{J}_{\text{chem}}) + \rho \epsilon + \mu \nabla \cdot \mathbf{J}_C, \quad (21.97)$$

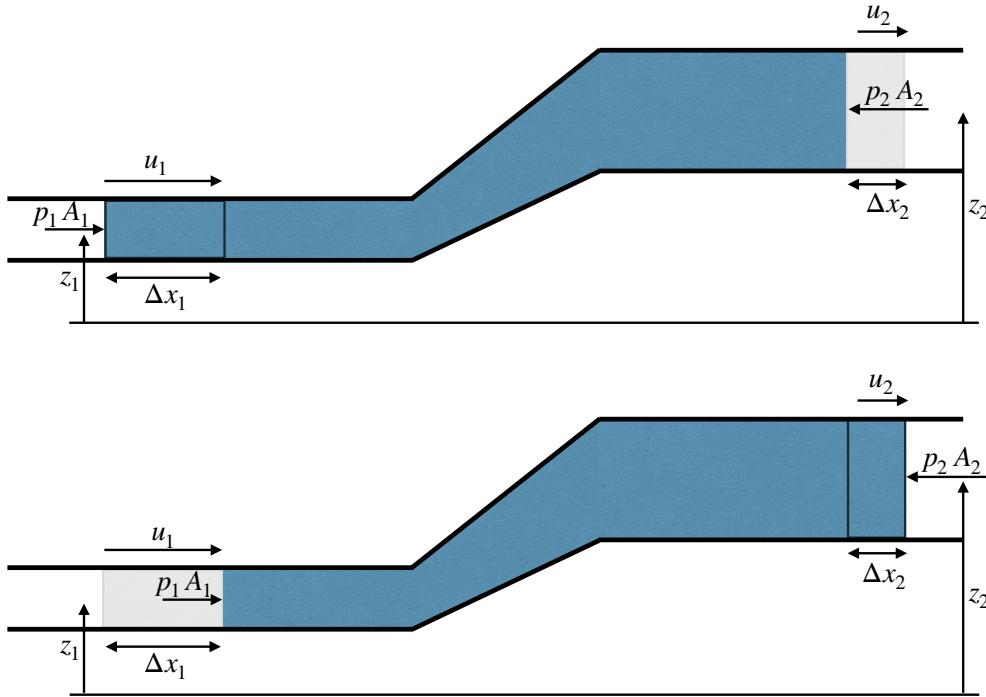


FIGURE 21.1: An example to illustrate the basic physics of Bernoulli's theorem and pressure work, whereby we depict the flow of a perfect and constant density fluid from left to right in a pipe of variable cross-section and variable height. We study the energetics of a control volume (dark blue region) moving with the fluid. The top panel shows the control volume at one time and the lower panel shows the control volume at a time  $\Delta t$  later, after which a mass of fluid,  $M$ , has moved through the system. Volume conservation means that  $(u_1 \Delta t) A_1 = (u_2 \Delta t) A_2$ , where  $\Delta x_{1,2}$  is the horizontal displacement of the fluid plug over time  $\Delta t$ ,  $u_{1,2}$  is the cross-sectional area average velocity,  $A_{1,2}$  is the pipe cross-sectional area, and  $M = \rho \Delta x_1 A_1 = \rho \Delta x_2 A_2$  is the mass of fluid moving over the  $\Delta t$  time increment. Pressure forces,  $p_{1,2}$ , at the end caps point inward (compressive), with pressure on the left larger than that on the right to support the fluid moving to the right. As the fluid moves upward it increases its gravitational potential energy and in so doing the fluid does work against gravity.

where we wrote the tracer equation as

$$\rho \frac{DC}{Dt} = -\nabla \cdot \mathbf{J}_C \quad (21.98)$$

as in Section 15.1.3. Through some manipulations pursued in Section 21.7.1, we identify a non-advection entropy flux and a corresponding entropy source. This form of the entropy budget is useful since we can then invoke the second law to insist that the entropy source is non-negative, and that statement renders some constraints on the thermal and chemical fluxes.

### 21.7.1 Non-advection entropy flux and entropy source

To start the manipulations, divide equation (21.97) by  $T$  and make use of the chemical energy flux in the form

$$\mathbf{J}_{\text{chem}} = \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} \mathbf{J}_C = \left( \mu - T \left[ \frac{\partial \mu}{\partial T} \right]_{C,p} \right) \mathbf{J}_C = (\mu - T \mu_T) \mathbf{J}_C \quad (21.99)$$

where we used the identity (21.65) for the second equality, and introduced a shorthand for the third equality. In this manner we have

$$\rho \frac{D\dot{S}}{Dt} = -\frac{\nabla \cdot (\mathbf{J}_{\text{therm}} + (\mu - T\mu_T) \mathbf{J}_C)}{T} + \frac{\rho\epsilon}{T} + \frac{\mu \nabla \cdot \mathbf{J}_C}{T} \quad (21.100\text{a})$$

$$= -\nabla \cdot (\mathbf{J}_{\text{therm}}/T - \mu_T \mathbf{J}_C) + \frac{\rho\epsilon}{T} + \frac{\nabla T}{T} \cdot (\mu_T \mathbf{J}_C - \mathbf{J}_{\text{therm}}/T) - (\mathbf{J}_C \cdot \nabla \mu)/T \quad (21.100\text{b})$$

$$= -\nabla \cdot (\mathbf{J}_{\text{therm}}/T - \mu_T \mathbf{J}_C) + \frac{\rho\epsilon}{T} - \frac{\nabla T \cdot \mathbf{J}_{\text{therm}}}{T^2} + \frac{\mathbf{J}_C \cdot (\mu_T \nabla T - \nabla \mu)}{T} \quad (21.100\text{c})$$

$$= -\nabla \cdot (\mathbf{J}_{\text{therm}}/T - \mu_T \mathbf{J}_C) + \frac{\rho\epsilon}{T} - \frac{\nabla T \cdot \mathbf{J}_{\text{therm}}}{T^2} - \frac{\mathbf{J}_C \cdot (\mu_C \nabla C + \mu_p \nabla p)}{T}, \quad (21.100\text{d})$$

where we wrote the gradient of the chemical potential,  $\mu(T, p, C)$ , as

$$\nabla \mu = \left[ \frac{\partial \mu}{\partial T} \right]_{p,C} \nabla T + \left[ \frac{\partial \mu}{\partial p} \right]_{T,C} \nabla p + \left[ \frac{\partial \mu}{\partial C} \right]_{T,p} \nabla C = \mu_T \nabla T + \mu_p \nabla p + \mu_C \nabla C. \quad (21.101)$$

We can thus identify the non-advective entropy flux

$$\mathbf{J}_S = \frac{\mathbf{J}_{\text{therm}}}{T} - \left[ \frac{\partial \mu}{\partial T} \right]_{p,C} \mathbf{J}_C, \quad (21.102)$$

and the entropy source

$$\Sigma_S = \frac{\rho\epsilon}{T} - \frac{\nabla T \cdot \mathbf{J}_{\text{therm}}}{T^2} - \frac{\mathbf{J}_C}{T} \cdot \left( \left[ \frac{\partial \mu}{\partial C} \right]_{T,p} \nabla C + \left[ \frac{\partial \mu}{\partial p} \right]_{T,C} \nabla p \right). \quad (21.103)$$

The non-advective entropy flux (21.102) arises from the thermal and chemical fluxes, whereas the entropy source includes contributions from those fluxes as well as the frictional dissipation of mechanical energy.

## 21.7.2 Constraints from the second law of thermodynamics

The second law of thermodynamics states that the entropy source is non-negative

$$\Sigma_S \geq 0 \iff \text{second law of thermodynamics}. \quad (21.104)$$

This condition imposes constraints on the frictional dissipation, thermal flux, and tracer flux. Since frictional dissipation in Newtonian fluids (equation (21.35)) is non-negative,  $\epsilon \geq 0$ , we make use of the second law to constrain just the thermal flux and tracer flux. Furthermore, we split off the radiant flux from the thermal flux, since the radiant flux is generally determined by processes external to the fluid. We thus use the second law to constrain the conductive portion of the thermal flux along with the tracer flux so that

$$-\nabla T \cdot \mathbf{J}_{\text{cond}} - T \mu_C \mathbf{J}_C \cdot \left[ \nabla C + \frac{\mu_p}{\mu_C} \nabla p \right] \geq 0. \quad (21.105)$$

This constraint can be satisfied by assuming the conductive and tracer fluxes are of the form

$$\rho^{-1} \mathbf{J}_{\text{cond}} = -c_p \kappa_T \nabla T - \kappa_{TC} \left[ \nabla C + \frac{\mu_p}{\mu_C} \nabla p \right] \quad (21.106a)$$

$$\rho^{-1} \mathbf{J}_C = -\kappa_C \left[ \nabla C + \frac{\mu_p}{\mu_C} \nabla p \right] - \kappa_{CT} \nabla T. \quad (21.106b)$$

The first term in the conductive thermal flux (21.106a) is known as *Fourier's law of conduction*

$$\mathbf{J}_{\text{cond}}^{\text{Fourier}} = -\rho c_p \kappa_T \nabla T, \quad (21.107)$$

in which case the conductive thermal flux is directed down the gradient of the *in situ* temperature. The second term leads to a conductive thermal flux in the presence of matter concentration gradients and thermal gradients, and this process is known as the *Dufour effect*

$$\mathbf{J}_{\text{cond}}^{\text{Dufour}} = -\rho \kappa_{TC} \left[ \nabla C + \frac{\mu_p}{\mu_C} \nabla p \right]. \quad (21.108)$$

The first term in the matter flux (21.106b) is known as *Fick's law of diffusion*

$$\mathbf{J}_C^{\text{Fick}} = -\rho \kappa_C \nabla C. \quad (21.109)$$

We generally also encounter a matter diffusive flux in the presence of pressure gradients, which accounts for the second contribution to the matter flux in equation (21.106b). Finally, the matter flux has a contribution from temperature gradients, which is known as the *Soret effect*

$$\mathbf{J}_C^{\text{Soret}} = -\rho \kappa_{CT} \nabla T. \quad (21.110)$$

The Onsager reciprocity conditions<sup>6</sup> are now invoked to relate the two off-diagonal coefficients according to

$$T \mu_C \kappa_{CT} = \kappa_{TC}, \quad (21.111)$$

which brings the entropy condition to the form

$$c_p \kappa_T |\nabla T|^2 + \kappa_C \mu_C T \left| \nabla C + \frac{\mu_p}{\mu_C} \nabla p \right|^2 + 2 \kappa_{TC} \nabla T \cdot \left[ \nabla C + \frac{\mu_p}{\mu_C} \nabla p \right] \geq 0. \quad (21.112)$$

This condition then constrains the phenomenological constants  $\kappa_C$ ,  $\kappa_T$  and  $\kappa_{TC}$  so that

$$|\kappa_{TC}|^2 \leq \kappa_T \kappa_C c_p T \mu_S. \quad (21.113)$$

### 21.7.3 A summary presentation

We here summarize the previous material by skipping details for the entropy flux, thermal flux, and matter flux. For this purpose, write the budget for the total energy in the form

$$\rho \frac{D\mathcal{E}}{Dt} = -\nabla \cdot (p \mathbf{v} - \mathbf{v} \cdot \boldsymbol{\tau}) + \rho \left[ -\epsilon + T \frac{D\mathcal{S}}{Dt} + \mu \frac{DC}{Dt} \right] + \rho \partial_t \Phi. \quad (21.114)$$

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<sup>6</sup>See Chapter 14 of [Callen \(1985\)](#) for these conditions and their underlying dynamical connections.

Now assume that the specific entropy and matter concentration satisfy the evolution equations

$$\rho \frac{D\mathcal{S}}{Dt} = -\nabla \cdot \mathbf{J}_S + \Sigma_S \quad \text{and} \quad \rho \frac{D}{Dt} = -\nabla \cdot \mathbf{J}_C, \quad (21.115)$$

thus rendering

$$\rho \left[ T \frac{D\mathcal{S}}{Dt} + \mu \frac{DC}{Dt} \right] = -T \nabla \cdot \mathbf{J}_S + T \Sigma_S - \mu \nabla \cdot \mathbf{J}_C \quad (21.116a)$$

$$= -\nabla \cdot (T \mathbf{J}_S + \mu \mathbf{J}_C) + \nabla T \cdot \mathbf{J}_S + \nabla \mu \cdot \mathbf{J}_C + T \Sigma_S, \quad (21.116b)$$

which then brings the total energy equation (21.114) into the form

$$\rho \frac{D\mathcal{E}}{Dt} = -\nabla \cdot (p \mathbf{v} - \mathbf{v} \cdot \tau + T \mathbf{J}_S + \mu \mathbf{J}_C) + [-\rho \epsilon + \nabla T \cdot \mathbf{J}_S + \nabla \mu \cdot \mathbf{J}_C + T \Sigma_S] + \rho \partial_t \Phi. \quad (21.117)$$

We now postulate that the globally integrated total energy is constant in the absence of boundary processes and with a time independent geopotential. In the presence of mechanical dissipation and matter constituent mixing, a necessary condition for such global energy conservation is for the specific entropy source to take the form

$$T \Sigma_S = \rho \epsilon - \nabla T \cdot \mathbf{J}_S - \nabla \mu \cdot \mathbf{J}_C. \quad (21.118)$$

That is, the entropy source arises from frictional dissipation, entropy mixing, and matter mixing. With this form for the entropy source, the total energy budget (21.117) is given by the material form and the equivalent Eulerian flux-form expressions

$$\rho \frac{D\mathcal{E}}{Dt} = -\nabla \cdot (p \mathbf{v} - \mathbf{v} \cdot \tau + T \mathbf{J}_S + \mu \mathbf{J}_C) + \rho \partial_t \Phi \quad (21.119a)$$

$$\frac{\partial(\rho \mathcal{E})}{\partial t} = -\nabla \cdot (\mathcal{E} \mathbf{v} + p \mathbf{v} - \mathbf{v} \cdot \tau + T \mathbf{J}_S + \mu \mathbf{J}_C) + \rho \partial_t \Phi. \quad (21.119b)$$

The modified form of the internal energy budget (21.58) is found by subtracting the mechanical energy budget (21.36c) from the total energy budget (21.119a)

$$\rho \frac{D\mathcal{I}}{Dt} = \rho \frac{D(\mathcal{E} - \mathcal{M})}{Dt} = -p \nabla \cdot \mathbf{v} - \nabla \cdot (T \mathbf{J}_S + \mu \mathbf{J}_C) + \rho \epsilon. \quad (21.120)$$

The corresponding enthalpy budget (21.60) is given by

$$\rho \frac{D\mathcal{H}}{Dt} - \frac{Dp}{Dt} = -\nabla \cdot (T \mathbf{J}_S + \mu \mathbf{J}_C) + \rho \epsilon = -\nabla \cdot \mathbf{J}_{\mathcal{H}} + \rho \epsilon. \quad (21.121)$$

In the second equatltiy we defined the enthalpy flux

$$\mathbf{J}_{\mathcal{H}} = T \mathbf{J}_S + \mu \mathbf{J}_C \quad (21.122a)$$

$$= \mathbf{J}_{\text{therm}} - T \left[ \frac{\partial \mu}{\partial T} \right]_{p,C} \mathbf{J}_C + \mu \mathbf{J}_C \quad (21.122b)$$

$$= \mathbf{J}_{\text{therm}} + \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} \mathbf{J}_C \quad (21.122c)$$

$$= \mathbf{J}_{\text{therm}} + \mathbf{J}_{\text{chem}}, \quad (21.122d)$$

where we used equation (21.102) for the entropy flux,  $\mathbf{J}_S$ , equation (21.99) for the chemical flux,  $\mathbf{J}_{\text{chem}}$ , and the thermodynamic identity (21.65) for the third equality. Furthermore, recall that the thermal flux,  $\mathbf{J}_{\text{therm}}$ , is the sum of a conductive plus radiative contribution as per equation (21.62).

### 21.7.4 Comments and further study

It is remarkable how the second law of thermodynamics is able to predict new physical processes through considering the various forms that the thermal and matter fluxes can take to ensure a positive entropy source. Even so, for most purposes of oceanography, the fluxes that are considered in this section are far smaller than those induced by turbulent flow processes, in which case the most accurate flux relations reduce to the Fickian and Fourier expressions, thus making the off-diagonal processes (Dufour, Soret, pressure induced diffusion) less important in practice.

Much of our presentation in this section followed that from Sections 2.4 and 2.5 from [Olbers et al. \(2012\)](#). Similar presentations are also found in Appendix B of [IOC et al. \(2010\)](#). The physical ideas underlying the Onsager reciprocity relations are lucidly discussed in Chapter 14 of [Callen \(1985\)](#). The considerations given here are applicable to a laminar ocean, with [Graham and McDougall \(2013\)](#) extending these ideas to a turbulent ocean.

## 21.8 Temperature evolution

In specifying the state of a fluid element it is sensible to make use of the temperature, pressure, and tracer concentration given that these state properties are readily measured in the laboratory and environment. Furthermore, these properties are the natural variables for the Gibbs potential (Section 20.7.6). Hence, given values for  $(T, p, C)$  we can determine the Gibbs potential and then determine all other thermodynamic properties by taking partial derivatives.

How do we specify the evolution of  $(T, p, C)$  for a fluid element? Evolution of the matter concentration follows from the tracer equation (an advection-diffusion equation) as developed in Section 15.1. Pressure measures the compressive stress acting on each fluid element (Section 18.7), with its specification depending on the dominant dynamical balances (see Section 21.9). Temperature reflects the energy of the internal microscopic degrees of freedom within a fluid element, with its evolution the subject of this section. We show how of Conservative Temperature,  $\Theta$ , rather than *in situ* temperature,  $T$ , or potential temperature,  $\theta$ , offers the simplest prognostic equation of the three temperature variables. The key reason is that  $\Theta$  evolves almost precisely like a material tracer, driven by the convergence of fluxes, whereas the equations for  $T$  and  $\theta$  contain extra source terms in addition to flux convergences.

### 21.8.1 Enthalpy equation again

In developing the temperature equation it is useful to start from the prognostic equation for enthalpy as developed in Sections 21.4.6. For that purpose we write the enthalpy equation (21.121) as

$$\rho \frac{D\mathcal{H}}{Dt} = \frac{Dp}{Dt} - \nabla \cdot \mathbf{J}_{\mathcal{H}} + \rho \epsilon, \quad (21.123)$$

with the enthalpy flux,  $\mathbf{J}_{\mathcal{H}}$ , written in terms of the entropy and tracer fluxes as per equation (21.122d).

### 21.8.2 Evolution of *in situ* temperature

To reveal a prognostic equation for temperature, we write enthalpy as a function of  $(T, p, C)$  so that

$$\frac{D\mathcal{H}}{Dt} = \left[ \frac{\partial \mathcal{H}}{\partial T} \right]_{p,C} \frac{DT}{Dt} + \left[ \frac{\partial \mathcal{H}}{\partial p} \right]_{T,C} \frac{Dp}{Dt} + \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} \frac{DC}{Dt}. \quad (21.124)$$

The partial derivatives can be related to response functions via the following. First, the specific heat capacity at constant pressure is given by equation (20.121)

$$\left[ \frac{\partial \mathcal{H}}{\partial T} \right]_{p,C} = c_p. \quad (21.125)$$

Next, we make use of the Gibbs potential identities in Section 20.7.6 to write

$$\left[ \frac{\partial \mathcal{H}}{\partial p} \right]_{T,C} = \left[ \frac{\partial \mathcal{G}}{\partial p} \right]_{T,C} - T \left[ \frac{\partial}{\partial p} \right]_{T,C} \left[ \frac{\partial \mathcal{G}}{\partial T} \right]_{p,C} \quad (21.126a)$$

$$= \nu_s - T \left[ \frac{\partial}{\partial T} \right]_{p,C} \left[ \frac{\partial \mathcal{G}}{\partial p} \right]_{T,C} \quad (21.126b)$$

$$= \nu_s - T \left[ \frac{\partial \nu_s}{\partial T} \right]_{p,C} \quad (21.126c)$$

$$= \nu_s (1 - T \alpha_T), \quad (21.126d)$$

where  $\alpha_T$  is the thermal expansion coefficient given by equation (20.122). Use of these identities in the enthalpy equation (21.124) and rearrangement leads to the *in situ* temperature equation

$$c_p \rho \frac{DT}{Dt} = -\nabla \cdot \mathbf{J}_{\mathcal{H}} + \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} \nabla \cdot \mathbf{J}_C + \alpha_T T \frac{Dp}{Dt} + \rho \epsilon. \quad (21.127)$$

The *in situ* temperature of a fluid element thus evolves according to convergence of the enthalpy fluxes, divergence of matter concentration fluxes, material time changes to pressure, and frictional dissipation. We can massage this expression a bit more by introducing the enthalpy flux (21.122c) so that

$$c_p \rho \frac{DT}{Dt} = -\nabla \cdot \mathbf{J}_{\text{therm}} - \mathbf{J}_C \cdot \nabla \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} + \alpha_T T \frac{Dp}{Dt} + \rho \epsilon, \quad (21.128)$$

where constraints on the conductive portion of the thermal flux were discussed in Section 21.7.2.

### 21.8.3 Evolution of potential temperature

We can convert the *in situ* temperature equation (21.127) into a version of the potential temperature equation by recalling the expression (20.137) for the lapse rate

$$\hat{\Gamma} = \left[ \frac{\partial T}{\partial p} \right]_{C,S} = \frac{T \alpha_T}{\rho c_p} \quad (21.129)$$

so that equation (21.127) takes the form

$$c_p \rho \left[ \frac{DT}{Dt} - \hat{\Gamma} \frac{Dp}{Dt} \right] = -\nabla \cdot \mathbf{J}_{\mathcal{H}} + \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} \nabla \cdot \mathbf{J}_C + \rho \epsilon. \quad (21.130)$$

Making use of the definition (20.142) for potential temperature renders

$$c_p \rho \frac{D\theta}{Dt} = -\nabla \cdot \mathbf{J}_{\mathcal{H}} + \left[ \frac{\partial \mathcal{H}}{\partial C} \right]_{T,p} \nabla \cdot \mathbf{J}_C + \rho \epsilon. \quad (21.131)$$

As expected, pressure changes are removed from the evolution equation for potential temperature.

#### 21.8.4 Conservative Temperature for the ocean

Rather than expressing enthalpy as a function  $\mathcal{H}(T, p, C)$ , we make use of its natural coordinate dependence  $\mathcal{H}(\mathcal{S}, p, C)$  from Section 20.7.4, which leads to the enthalpy equation in the form (21.121)

$$\rho \frac{D\mathcal{H}}{Dt} = \frac{Dp}{Dt} - \nabla \cdot \mathbf{J}_{\mathcal{H}} + \rho \epsilon. \quad (21.132)$$

The pressure term arises just like for *in situ* temperature. Its presence suggests we introduce the *potential enthalpy*.

##### Potential enthalpy and Conservative Temperature

The potential enthalpy is defined to be the enthalpy of a fluid element moved to a reference pressure,  $p_R$ , while maintaining fixed specific entropy and fixed tracer concentration

$$\mathcal{H}^{\text{pot}}(\mathcal{S}, C) = \mathcal{H}(\mathcal{S}, p_R, C). \quad (21.133)$$

As for potential temperature (Section 20.11.3), it is most convenient to take  $p_R$  as the standard atmospheric pressure, thus corresponding to the standard pressure at the air-sea interface. This definition parallels that for potential temperature given by equation (20.147). By construction, the material time derivative of potential enthalpy is given by

$$\rho \frac{D\mathcal{H}^{\text{pot}}}{Dt} = \rho \left[ \frac{\partial \mathcal{H}^{\text{pot}}}{\partial \mathcal{S}} \right]_C \frac{D\mathcal{S}}{Dt} + \rho \left[ \frac{\partial \mathcal{H}^{\text{pot}}}{\partial C} \right]_S \frac{DC}{Dt} \quad (21.134a)$$

$$= \theta (-\nabla \cdot \mathbf{J}_{\mathcal{S}} + \Sigma_{\mathcal{S}}) - \mu_R \nabla \cdot \mathbf{J}_C \quad (21.134b)$$

$$= (\theta/T) [\rho \epsilon - \nabla \cdot \mathbf{J}_H] - [\mu_R - (\theta/T) \mu] \nabla \cdot \mathbf{J}_C, \quad (21.134c)$$

where we set

$$\theta = \left[ \frac{\partial \mathcal{H}^{\text{pot}}}{\partial \mathcal{S}} \right]_C \quad \text{and} \quad \mu_R = \left[ \frac{\partial \mathcal{H}^{\text{pot}}}{\partial C} \right]_S \quad (21.135)$$

and used equation (21.118) for the entropy source,  $\Sigma_{\mathcal{S}}$ . Now define the Conservative Temperature,  $\Theta$ , via

$$c_p^{\text{ref}} \Theta \equiv \mathcal{H}^{\text{pot}}(\mathcal{S}, C) = \mathcal{H}(\mathcal{S}, p_R, C), \quad (21.136)$$

where  $c_p^{\text{ref}}$  is an arbitrary reference specific heat capacity. For the ocean, McDougall (2003) suggested that  $c_p^{\text{ref}}$  be chosen so that  $\Theta = \theta$  at a salinity of 35 parts per thousand. McDougall (2003) furthermore argued that the terms appearing in the potential enthalpy equation (21.134c) are well approximated for the ocean by just the convergence of the enthalpy flux. Hence, the Conservative Temperature satisfies, to a very good approximation, the source-free tracer equation

$$\rho c_p^{\text{ref}} \frac{D\Theta}{Dt} = -\nabla \cdot \mathbf{J}_H. \quad (21.137)$$

### Key points regarding the Conservative Temperature equation

The Conservative Temperature equation (21.137) is mathematically identical to the material tracer equation, and as such it offers an elegant means to prognose thermodynamic properties of the fluid and to perform budget analyses. We further emphasize two points in regards to this equation relative to the potential temperature equation (21.131).

- The source terms (those not associated with flux convergences) on the right hand side of the potential temperature equation are much larger than those in the Conservative Temperature equation. In particular, [McDougall \(2003\)](#) argued that they are roughly 100 times larger in certain regions of the ocean.
- The heat capacity appearing in the Conservative Temperature equation is a fixed constant, by construction. This feature contrasts to the space-time variable heat capacity,  $c_p$ , appearing in both the *in situ* temperature equation (21.127) and potential temperature equation (21.131). The space-time variations of  $c_p$  are not negligible (e.g., order 5% for the global ocean), thus making the non-constant heat capacity required for the  $T$  and  $\theta$  equations very inconvenient for purposes of budget analyses.

We close by noting that the enthalpy flux,  $\mathbf{J}_H$ , is related to the entropy flux and concentration flux as per equation (21.122d). As discussed in Section 2.6 of [Olbers et al. \(2012\)](#), the dominant terms appearing in this flux arise from entropy, which itself is largely due to fluxes of temperature. Consequently, the flux  $\mathbf{J}_H$  is well approximated as a flux just of  $\Theta$ .

#### 21.8.5 Further study

The discussion in this section largely followed the more complete ocean discussion given in Section 2.6 of [Olbers et al. \(2012\)](#), which is itself based on [McDougall \(2003\)](#). Development for a realistic atmosphere must consider phase changes (liquid-vapor and liquid-solid), since the associated latent heat exchanges are leading order contributions to the enthalpy budget. Additionally, the role of frictional dissipation is not negligible in the atmosphere whereas it is negligible in the ocean (see Section 21.5.3).

## 21.9 Summary of the ocean-atmosphere equations

We have now completed the derivation of the full suite of partial differential equations describing rotating and stratified fluids. We thus find it useful to again list these *thermo-hydrodynamical* equations and summarize their content:

$$\rho \frac{D\mathbf{v}}{Dt} + 2\rho \boldsymbol{\Omega} \times \mathbf{v} = -\rho \nabla \Phi - \nabla p + \nabla \cdot \tau \quad \text{momentum} \quad (21.138)$$

$$\frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{v} \quad \text{mass continuity} \quad (21.139)$$

$$\rho \frac{DC}{Dt} = -\nabla \cdot \mathbf{J}(C) \quad \text{matter conservation} \quad (21.140)$$

$$\rho \frac{D\Theta}{Dt} = -\nabla \cdot \mathbf{J}(\Theta) \quad \text{potential enthalpy conservation} \quad (21.141)$$

$$\rho = \rho(C, \Theta, p) \quad \text{equation of state.} \quad (21.142)$$

It is a testament to the success of classical continuum mechanics that these equations are of use for describing fluid phenomena from the millimetre scale to the astrophysical scale. We summarize the following terms in these equations.

- LINEAR MOMENTUM AND VELOCITY: Newton's second law of motion, as developed for a fluid in Chapter 17, provides the prognostic equation for the velocity field,  $\mathbf{v}$ . Each of the three velocity components evolves according to its respective dynamical equation (21.138). As noted at the end of Section 17.1.3, we write the momentum equation in the form (21.138) by separating the time dependence of the basis vectors into a term arising from solid-body rotation (which leads to planetary Coriolis and planetary centrifugal accelerations) and a term arising from the motion of the fluid relative to the rotating sphere (which leads to the metric acceleration when using non-Cartesian coordinates).
- MASS CONSERVATION: Kinematics provides a constraint on the velocity field according to the needs of mass conservation for a fluid element (Section 14.2). This constraint leads to the continuity equation (21.139).
- MATERIAL TRACER CONSERVATION: Kinematic constraints from the conservation of matter (Section 15.1) leads to the material tracer equation (21.140). Evolution is determined by the convergence of tracer fluxes,  $\mathbf{J}$ , with this flux specified by molecular diffusion as discussed in Section 46.3, or through other parameterized processes when sampling flow on scales larger than millimetres (see Chapter 48).
- THERMODYNAMIC TRACER: The Conservative Temperature,  $\Theta$ , (Section 21.8.4), evolves according to the convergence of fluxes, just like a material tracer.
- DENSITY: The *in situ* density can be updated in time via mass continuity (equation (21.139)) or via knowledge of  $(C, \Theta, p)$ . We discussed the many forms of density for the ocean and atmosphere in Section 24.3.
- PRESSURE: There is no prognostic equation for pressure. Rather, pressure is diagnosed based on knowledge of other fields. Here are sketches of how that diagnostic calculation is performed.
  - For an ideal gas, pressure is diagnosed from the ideal gas relation (20.159) using the density and temperature.
  - For fluid flow maintaining an approximate hydrostatic balance (Section 22.2), pressure is diagnosed at a point through knowledge of the weight per area above the point.
  - For an incompressible flow as per the oceanic Boussinesq fluid (Chapter 23), pressure is no longer connected thermodynamically to partial derivatives of the thermodynamic potentials (Section 20.7). Instead, pressure is determined kinematically by the incompressibility constraint. In particular, for a non-hydrostatic Boussinesq fluid, pressure is diagnosed by solving a Poisson equation derived from taking the divergence of the momentum equation (see Section 23.3).
- GEOPOTENTIAL: The geopotential,  $\Phi$ , is specified once the height above an arbitrary reference level is known, as well as the effective gravitational acceleration (Section 9.12.4). For geophysical fluid studies, the reference level is generally taken at the level of a resting sea surface. We thus often write the radial coordinate as

$$r = R_e + z \tag{21.143}$$

where  $R_e = 6.371 \times 10^6$  m is the earth radius (equation (9.147)), and  $z$  is the geopotential coordinate measuring the height above sea level.

- EARTH'S SPIN: The earth's angular velocity,  $\boldsymbol{\Omega}$ , is constant for geophysical fluid studies of concern here. Its value is discussed in Section 9.2.
- FRICTION: The friction vector,

$$\rho \mathbf{F} = \nabla \cdot \tau, \quad (21.144)$$

is the divergence of a symmetric and trace-free deviatoric stress tensor,  $\tau$  (Section 18.7). The stress tensor is determined through a constitutive relation as a function of the strain and viscous properties.

- BOUNDARY CONDITIONS: Boundary conditions consist of the exchange of matter, momentum, and enthalpy with the surrounding media, such as the solid earth or another fluid component (e.g., atmosphere-ocean exchange). We discuss the boundary conditions for matter in Section 14.4; for momentum in Section 18.9; and for ocean buoyancy in Section 49.6.

## 21.10 Conservation laws and potential properties

A central facet of theoretical physics concerns the development of concepts and tools to expose conservation laws and their underlying symmetries.<sup>7</sup> We routinely make use of such laws in geophysical fluid mechanics to provide constraints on the fluid motion and to study budgets of corresponding properties to help understand fundamental processes. As such, conservation laws offer great physical insight and predictive utility. We close this chapter by summarizing some conceptual points concerning conservation laws. In particular, we identify the need to distinguish laws that involve just the convergence of a flux from those that also include non-conservative “source” terms. We also distinguish local or material conservation for a property, as reflected by the property remaining invariant following a fluid element, versus global conservation, whereby a property is invariant only when integrated over a finite region whose boundaries are closed to fluxes that affect the property.

### 21.10.1 Flux-form conservation laws

Certain scalar properties studied in fluid mechanics satisfy Eulerian flux-form conservation laws that are written as

$$\frac{\partial(\rho\psi)}{\partial t} = -\nabla \cdot (\rho \mathbf{v} \psi + \mathbf{J}). \quad (21.145)$$

The right hand side involves a flux that is comprised of an advective term,  $\rho \mathbf{v} \psi$ , plus a non-advective term,  $\mathbf{J}$ . Examples of flux-form conservation laws of this form include the material tracer concentration,  $\psi = C$ , as in equation (21.140); the Conservative Temperature,  $\psi = \Theta$ , as in equation (21.141); the total energy,  $\psi = \mathcal{E}$ , in the absence of astronomical forces, as in equation (21.119b); and the potential vorticity,  $\psi = Q$ , as in equation (36.40). In Chapter 15, we saw how this differential equation leads to finite volume conservation properties for the integral of  $\psi$ -stuff within a region,  $\int_{\mathcal{R}} \psi \rho dV$ , with the evolution of this integral only affected by area integrated fluxes,  $\rho \mathbf{v} \psi + \mathbf{J}$ , penetrating the region boundary (mathematically seen by applying the divergence theorem).

Such conservation laws are a direct consequence of the local conservation of  $\psi$ -stuff within the fluid. That is, the amount of  $\psi$ -stuff changes at a point only through the local convergence of fluxes onto that point, and likewise for a finite region. Conservation laws of the form (21.145)

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<sup>7</sup>See Chapter 10 for the connection between conservation laws and symmetries, as embodied by Noether's theorem.

are consistent with basic notions of causality and locality that appear throughout physics, with a discussion of such conservation laws offered in Section 27-1 of [Feynman et al. \(1963\)](#).

### 21.10.2 Conservation laws that are not flux-form

The presence of source/sinks are relevant for chemical or biogeochemical reactions, whereby matter is converted from one form to another. Such processes are not mathematically represented as the convergence of a flux. As such, they are not contained in the conservation law (21.145) and they are correspondingly referred to as *non-conservative processes*. Even without chemical reactions, not all fluid properties satisfy flux-form conservation laws of the form (21.145). For example, linear momentum of a fluid element is affected by pressure, Coriolis, and effective gravity, and these processes are not represented as the convergence of a flux.

As discussed in Chapter 10, conservation laws are associated with symmetries of the physical system. Correspondingly, non-conservative terms appearing in an evolution equation often reflect the breaking of a symmetry. For example, motion around a sphere does not conserve linear momentum even in the absence of forces, whereas linear momentum is conserved for free motion in a planar geometry.

### 21.10.3 Non-material or wave-like transport of properties

Pressure is of particular note since pressure perturbations travel through a compressible fluid via acoustic waves (Section 17.5), or, in the case of an incompressible flow, a pressure perturbation is felt globally and instantaneously as reflected in the elliptic Poisson equation satisfied by pressure (Section 23.3). More generally, the wave mediated transfer of forces, or other fluid properties such as momentum or mechanical energy, is an example of a non-material transfer; i.e., a transfer of information not arising from the transfer of matter. Non-material wave mediated transfer often occurs much faster than material transfer, with matter transport only mediated through advection and diffusion. Correspondingly, material substances (and potential enthalpy) are not directly affected by wave transport. Rather, waves affect material substances only so far as they affect advection and diffusion.

### 21.10.4 Local versus global conservation

In fluid mechanics we often encounter properties that remain invariant when following a fluid element, such as the mass of a fluid element. Mass invariance for a fluid element reflects matter conservation in classical physics, which in turn motivates the kinematic perspective pursued throughout this book that follows fluid elements whose mass remains constant. A related example concerns the matter content of a fluid element. In the absence of irreversible mixing, the matter content (i.e., tracer concentration) of the fluid element remains invariant so that its tracer concentration is materially constant

$$\rho \frac{D\psi}{Dt} = 0. \quad (21.146)$$

For example, in the absence of mixing, the salt content of seawater and the water content of moist air are invariant, so that the salt concentration and water concentration in a fluid element remains invariant. Such material invariances are termed *local* conservation laws since they hold locally to every fluid element. Correspondingly, in the presence of mixing between two fluid elements, the net material tracer in the combined fluid element equals to the sum of the tracer content in the contributing elements. That is, we can perform local budgets on fields that possess a local conservation law, and it is for this reason we sometimes refer to fluid properties satisfying local conservation laws as *conservative properties*.

But what of fluid properties that satisfy a flux-form conservation law of the form (21.145), and yet do not satisfy the material invariance law (21.146) even in the absence of irreversible processes? For example, consider the total energy,  $\mathcal{E}$ , from Section 21.5. Even in the absence of entropy sources (i.e., no mixing) and astronomical forces (i.e., constant gravity), mechanical work from pressure modifies the internal energy of the fluid element via the energy equation (21.119a)

$$\rho \frac{D\mathcal{E}}{Dt} = -\nabla \cdot (p \mathbf{v}). \quad (21.147)$$

Pressure work means that when two fluid elements are combined, the total energy of the combined fluid,  $\mathcal{E}_{12}$ , is not generally equal to the sum of their separate total energies,

$$\mathcal{E}_{12} \neq \mathcal{E}_1 + \mathcal{E}_2. \quad (21.148)$$

Hence, total energy is not a locally conservative property. This behavior contrasts fundamentally to how material tracers mix, whereby the flux convergence on the right hand side arises from diffusion. However, when integrated globally over a domain that is closed to the fluxes of total energy (i.e., there is no pressure work applied to the domain boundaries), and when there are no time dependent astronomical forces, then the domain integrated total energy,  $\int \rho \mathcal{E} dV$ , remains constant. This *global* conservation law means that the total energy is conserved globally, which is a familiar result from classical physics and was used in Section 21.5 to formulate the budget for total energy and, by inference, the internal energy. Global conservation is a less powerful constraint on fluid motion than local conservation. Even so, global conservation can be of great use when studying energy transformations within a closed domain.<sup>8</sup>

We can summarize the above discussion by noting that for a fluid property to be conservative (i.e., to satisfy a local conservation law), it is necessary but not sufficient that the material derivative of that property to be given by the divergence of a flux. Rather, what is needed is that the material derivative must equal to the divergence of a flux that is zero in the absence of mixing at that point in space and time. A diffusive flux satisfies this property (see Chapter 46 for more on diffusion). In contrast, the pressure flux convergence acting to modify total energy,  $-\nabla \cdot (p \mathbf{v})$ , can be nonzero even in regions where there is no mixing since pressure is transported by waves (Section 21.10.3).

### 21.10.5 Concerning potential properties

As introduced in Sections 20.11 and 21.8.4, to study fluid mixing it is useful to work with scalar fields that are not affected by adiabatic and isentropic pressure work. For this reason, rather than *in situ* temperature, we prefer to work with potential temperature,  $\theta$ , or Conservative Temperature,  $\Theta$ , both of which are potential properties as discussed in Section 20.11.1. Some potential properties are also endowed with the local conservation property discussed above, which makes local budgets available just like for a material tracer. For example, Conservative Temperature is very well approximated as a conservative property, with its non-flux form sources far smaller than potential temperature (Section 21.8.4). In contrast, neither *in situ* temperature nor total energy are potential properties since an adiabatic and isentropic change in pressure alters the total energy and *in situ* temperature of a fluid element. Correspondingly, as noted in Section 21.10.4, total energy and *in situ* temperature are not conservative properties.

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<sup>8</sup>We further encounter these distinctions between local and global conservation laws when studying potential vorticity in Chapter 37.

### 21.10.6 Further study

Much from this section is motivated by the more extensive discussion in Sections A.8 and A.9 of [IOC et al. \(2010\)](#).



## 21.11 Exercises

### EXERCISE 21.1: DYNAMICALLY INCONSISTENT VELOCITY

Consider the two dimensional vector field

$$\mathbf{u} = \Gamma (y^2 \hat{x} + x^2 \hat{y}), \quad (21.149)$$

with  $\Gamma$  a constant of dimensions  $L^{-1} T^{-1}$ .

- (a) Assuming  $\mathbf{u}$  is a velocity field, then determine the pressure field giving rise to this velocity assuming constant density, non-rotating reference frame, zero friction, and no boundary effects. Do so by making use of the Bernoulli theorem in equation (21.91) for horizontal (constant  $z$ ) flow.
- (b) Now make use of the momentum equation and integrating the pressure gradient. You should reach an inconsistency condition. What can you conclude about the physical realizability of the given velocity field? Hint: recall the discussion of exact differentials in Section 2.8.

### EXERCISE 21.2: CROCCO'S THEOREM

Prove that the spatial gradient of the Bernoulli potential for a single-component steady state perfect fluid can be written

$$\nabla \mathcal{B} = T \nabla S + \mathbf{v} \times \boldsymbol{\omega}_a. \quad (21.150)$$

This result is known as Crocco's Theorem ([Crocco, 1937](#)). It means that the velocity for a single-component perfect fluid in steady state is aligned parallel to isosurfaces of both the Bernoulli potential and the specific entropy. We encounter another form of this theorem for the steady state shallow water equations in Exercise 34.6.

Hint: to help formulate the proof, study the discussion in Section 21.6.2 where we showed that the Bernoulli potential is constant along a steady flow streamline in a perfect fluid. Also recall equation (21.50) valid for a steady state and applied here to a single-component fluid.

### EXERCISE 21.3: FRICTIONAL DISSIPATION FROM VISCOSITY

This exercise works through a simple case of the more general considerations from Section 21.3.2. Here, assume the friction in the momentum equation takes the form

$$\rho \mathbf{F} = \nabla \cdot (\rho \nu \nabla \mathbf{v}) = \partial_n (\rho \nu \partial_n \mathbf{v}), \quad (21.151)$$

with  $\nu > 0$  a scalar kinematic viscosity (generally non-constant). Show that when integrated over the full domain

$$\int \mathbf{F} \cdot \mathbf{v} \rho dV < 0, \quad (21.152)$$

where boundary terms are dropped. Hence, the global integrated kinetic energy is dissipated (reduced) through the impacts of viscosity. This dissipation of mechanical energy is converted to an increase in internal energy through Joule heating. Hint: for this exercise, it is sufficient to

assume Cartesian tensors so that

$$\rho \mathbf{F} \cdot \mathbf{v} = \rho F_m v_m = \partial_n(\rho \nu \partial_n v_m) v_m. \quad (21.153)$$

**EXERCISE 21.4: INTEGRATED FRICTIONAL DISSIPATION FOR AN INCOMPRESSIBLE FLUID**

Consider an incompressible fluid ( $\nabla \cdot \mathbf{v} = 0$  and  $\rho$  is constant). Assume the fluid is contained in a region,  $\mathcal{R}$ , whose boundary,  $\partial\mathcal{R}$ , is static. Also assume the velocity satisfies the no-slip condition on  $\partial\mathcal{R}$ , as relevant for a viscous fluid. Show that the frictional dissipation of kinetic energy (Section 21.3.2) has a global integral

$$\int_{\mathcal{R}} \mathbf{v} \cdot \mathbf{F} \rho dV = -\rho \nu \int_{\mathcal{R}} |\boldsymbol{\omega}|^2 dV, \quad (21.154)$$

where  $\boldsymbol{\omega} = \nabla \times \mathbf{v}$  is the vorticity. Hint: derive equation (13.85) from exercise 13.1, and specialize that equation to the case of an incompressible fluid.

**EXERCISE 21.5: CENTER OF MASS TRANSPORT THEOREM**

Consider a field,  $\psi$ , that satisfies the standard conservation law

$$\rho \frac{D\psi}{Dt} = -\nabla \cdot \mathbf{J}, \quad (21.155)$$

within a region,  $\mathcal{R}$ , that moves with the fluid flow. We here derive some results that hold for Cartesian coordinates.

- (a) Prove the transport theorem valid for Cartesian tensors

$$\frac{d}{dt} \int_{\mathcal{R}} \psi \mathbf{x} \rho dV = \int_{\mathcal{R}} (\mathbf{J} + \rho \psi \mathbf{v}) dV - \oint_{\partial\mathcal{R}} \mathbf{x} (\hat{\mathbf{n}} \cdot \mathbf{J}) d\mathcal{S}. \quad (21.156)$$

Hint: multiply both sides of equation (21.155) by  $x_m$ .

- (b) Offer an interpretation of equation (21.156). Hint: first consider the special case that the total  $\psi$ -stuff, defined by  $\Psi \equiv \int_{\mathcal{R}} \psi \rho dV$ , is constant when following the flow. Further hint: consider the more specialized case of  $\psi = 1$  and  $\mathbf{J} = 0$ , and then make use of Exercise 14.2.

**EXERCISE 21.6: THERMODYNAMIC MANIPULATIONS FOR IDEAL GASES**

This question develops some manipulations with the potential temperature.

- (a) Beginning with the expression (20.203) for potential temperature of an ideal gas, show that

$$d\theta = \frac{\theta}{T} \left[ dT - \frac{\nu_s}{c_p} dp \right]. \quad (21.157)$$

- (b) Given the result (21.157), show that an ideal gas satisfies the following relation

$$T d\mathcal{S} = \frac{c_p T}{\theta} d\theta. \quad (21.158)$$

Whereas the relation (20.155) holds for a general fluid only at the reference pressure, this exercise shows that it holds for an ideal gas at all pressures. As a result, a moving fluid of ideal gas satisfies the material time relation

$$T \frac{D\mathcal{S}}{Dt} = \frac{c_p T}{\theta} \frac{D\theta}{Dt} \Rightarrow \frac{c_p T}{\theta} \frac{D\theta}{Dt} = \dot{Q}. \quad (21.159)$$

## EXERCISE 21.7: THERMODYNAMIC MANIPULATIONS FOR A LIQUID

Consider seawater with specific entropy given by (see Section 1.7.2 of [Vallis \(2017\)](#))

$$S(S, T, p) = S_0 + c_{p0} \ln(T/T_o) [1 + \beta_S^*(S - S_o)] - \alpha_o p \left[ \beta_T + \beta_T \gamma^* \frac{p}{2} + \beta_T^* (T - T_o) \right], \quad (21.160)$$

and corresponding specific heat capacity at constant pressure

$$c_p(S, T, p) = c_{p0} [1 + \beta_S^*(S - S_o)] - \alpha_o p \beta_T^* T. \quad (21.161)$$

In these equations,  $T$  is the *in situ* temperature,  $S$  is the salinity, and  $p$  is the *in situ* pressure. All other terms on the right hand side to these expressions are empirical constants. Verify that an infinitesimal change in entropy for a fluid element with constant composition is given by

$$\theta dS = c_p(S, \theta, p_R) d\theta, \quad (21.162)$$

where  $\theta$  is the potential temperature and  $p_R$  is the corresponding reference pressure. Consequently, we can write for a moving fluid element

$$\dot{Q} = \frac{c_p T}{\theta} \frac{D\theta}{Dt}, \quad (21.163)$$

where we evaluate the non-constant heat capacity at  $c_p(S, \theta, p_R)$ . We see that certain liquids have an expression for heating that is analogous to that for an ideal gas, with the ideal gas case discussed in Exercise 21.6. Hint: Make use of the identity (20.147).





# Chapter 22

## Hydrostatic and tangent plane approximations

The ocean and atmosphere thermo-hydrodynamical equations (21.138)-(21.142) explain a huge range of phenomena. Yet by encapsulating so many physical scales of motion and associated dynamical processes, the equations are difficult to manage when studying a focused dynamical regime. Therefore, it is common to approximate or filter the equations to remove scales of little interest, thus enabling a more telescopic view of the dynamics. In this chapter, we develop certain approximations commonly used in geophysical fluid mechanics. In particular we develop the hydrostatic primitive equations as well as the tangent plane approximations.

### READER'S GUIDE TO THIS CHAPTER

The equations developed in this chapter, and their associated approximations, will be used extensively throughout the remainder of this book.

22.1	The hydrostatic primitive equations . . . . .	518
22.1.1	Hydrostatic approximation . . . . .	518
22.1.2	Shallow fluid approximation . . . . .	518
22.1.3	Traditional approximation . . . . .	519
22.1.4	Summary of the hydrostatic primitive equations . . . . .	519
22.1.5	Comments and further study . . . . .	520
22.2	Approximate hydrostatic balance . . . . .	520
22.2.1	Expressions for the hydrostatic pressure . . . . .	520
22.2.2	Evolution of hydrostatic pressure . . . . .	521
22.2.3	Heuristic scaling . . . . .	523
22.2.4	Removal of a dynamically irrelevant background state . . . . .	524
22.2.5	Decomposing the horizontal pressure gradient . . . . .	524
22.2.6	Horizontal hydrostatic pressure gradient in a mass conserving fluid	526
22.2.7	Ocean dynamic topography . . . . .	527
22.2.8	Surfaces of atmospheric geopotential height and pressure . . . . .	529
22.2.9	Concerning vertical motion . . . . .	529
22.2.10	Further study . . . . .	529
22.3	The tangent plane approximation: $f$ -plane and $\beta$ -plane . . . . .	529
22.3.1	Tangent plane approximation . . . . .	530
22.3.2	Traditional approximation and the $f$ -plane . . . . .	530
22.3.3	$\beta$ -plane approximation . . . . .	531
22.4	Homogeneous fluid in a rotating tank . . . . .	531
22.4.1	What about the planet's rotation? . . . . .	531
22.4.2	Formulating the equations of motion . . . . .	532

22.4.3 Solid-body rotation and free surface shape . . . . .	533
22.4.4 Further study . . . . .	534
22.5 Exercises . . . . .	534

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## 22.1 The hydrostatic primitive equations

The hydrostatic *primitive equations* provide a set of approximate equations for use in studying large-scale atmospheric and oceanic phenomena. Indeed, nearly all numerical models of the large-scale atmospheric and oceanic circulation are based on the primitive equations. They make use of the following three approximations.

### 22.1.1 Hydrostatic approximation

As discussed in Section 17.3, a static fluid in a gravity field maintains an exact hydrostatic balance, whereby the pressure at a point equals to the weight per area of fluid above that point. As shown in Section 22.2, the hydrostatic balance is very closely maintained column-by-column for the large scales in a moving geophysical fluid. Hence, it is appropriate for many purposes to take the *hydrostatic approximation* for the vertical momentum equation, with this approximation central to the study of geophysical fluid dynamics.

The hydrostatic approximation results in a balance in the vertical momentum equation (17.21) between the vertical pressure gradient and the effective gravitational force

$$\frac{\partial p}{\partial r} = -\rho g, \quad (22.1)$$

with this balance holding separately for each vertical column. Vertical integration of this equation, while assuming  $g$  is constant, renders a diagnostic expression for the hydrostatic pressure at a point as a function of the weight per horizontal area above the point

$$p(r, \lambda, \phi, t) = p(r_0, \lambda, \phi, t) + g \int_r^{r_0} \rho(r', \lambda, \phi, t) dr'. \quad (22.2)$$

Note that we exposed the horizontal space dependence along with the time dependence for the density and hence the hydrostatic pressure. That is, an approximate hydrostatic fluid has horizontal pressure gradients as well as time dependence.

We emphasize that in making the hydrostatic approximation that we are *not* assuming that vertical motion vanishes. In fact, there is vertical motion. But with the hydrostatic approximation, the vertical motion is not prognosed by the vertical momentum equation. Instead, it must be diagnosed via the constraints imposed on the motion. We have more comment on this point in Section 22.2.9.

### 22.1.2 Shallow fluid approximation

The ocean and atmosphere each form a fluid shell that envelopes the outer portion of the planet. The thickness of these fluids is small relative to the earth's radius. The shallow fluid approximation<sup>1</sup> builds this scale separation into the equations of motion by setting the radial coordinate equal to the earth's radius

$$r = R_e + z \approx R_e. \quad (22.3)$$

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<sup>1</sup>The shallow fluid approximation is distinct from the *shallow water approximation* treated in Part V of this book.

This approximation is made where  $r$  appears as a multiplier, but not as a derivative operator. For example, the spherical coordinate gradient operator (17.23) takes the approximate form

$$\nabla = \frac{\hat{\lambda}}{r \cos \phi} \frac{\partial}{\partial \lambda} + \frac{\hat{\phi}}{r} \frac{\partial}{\partial \phi} + \hat{r} \frac{\partial}{\partial r} \approx \frac{\hat{\lambda}}{R_e \cos \phi} \frac{\partial}{\partial \lambda} + \frac{\hat{\phi}}{R_e} \frac{\partial}{\partial \phi} + \hat{r} \frac{\partial}{\partial r}. \quad (22.4)$$

### 22.1.3 Traditional approximation

The *traditional approximation* comprises three approximations that come as a package.

#### *Coriolis acceleration*

The traditional approximation sets to zero the Coriolis terms in the horizontal momentum equations involving the vertical velocity. We are thus concerned only with the local vertical component of the earth's angular rotation vector (see discussion in Section 9.11.7)

$$\boldsymbol{\Omega} = \Omega \hat{\mathbf{Z}} = \Omega (\hat{\phi} \cos \phi + \hat{r} \sin \phi) \rightarrow \Omega \sin \phi \hat{r} = \mathbf{f}/2, \quad (22.5)$$

where

$$\mathbf{f} = (2 \Omega \sin \phi) \hat{r} \quad (22.6)$$

is the Coriolis parameter and  $\hat{\mathbf{Z}}$  is the spherical earth unit vector pointing out of the north pole (Figure 8.1).<sup>2</sup>

#### *Metric terms*

The traditional approximation also drops the metric terms,  $uw/r$  and  $vw/r$ , associated with the vertical velocity as they appear in the horizontal momentum equations (17.19) and (17.20). These terms are generally smaller than the other terms since  $w$  is much smaller than the horizontal velocity for large-scale geophysical fluid flow.

#### *Self consistency*

The shallow fluid approximation and both parts of the traditional approximation must be taken together in order to maintain a consistent energy and angular momentum conservation principle for the resulting equations. As shown in Exercise 22.1, taking one but not the other leads to an inconsistent set of equations

### 22.1.4 Summary of the hydrostatic primitive equations

The above approximations lead to the primitive equations written in spherical coordinates

$$\frac{Du}{Dt} - \frac{uv \tan \phi}{R_e} - fv = -\frac{1}{\rho R_e \cos \phi} \frac{\partial p}{\partial \lambda} + F^\lambda \quad (22.7)$$

$$\frac{Dv}{Dt} + \frac{u^2 \tan \phi}{R_e} + fu = -\frac{1}{\rho R_e} \frac{\partial p}{\partial \phi} + F^\phi \quad (22.8)$$

$$\frac{\partial p}{\partial z} = -g \rho, \quad (22.9)$$

---

<sup>2</sup>We use the capital  $\hat{\mathbf{Z}}$  to distinguish this north pole unit vector from the local  $\hat{\mathbf{z}} = \hat{r}$  unit vector pointing vertical relative to a tangent plane discussed in Section 22.3.

where the gradient operator is given by equation (22.4). We can write these equations in the succinct form

$$\left[ \frac{D}{Dt} + (f + u \tan \phi / R_e) \hat{z} \times \right] \mathbf{u} = -\rho \nabla \Phi - \nabla p + \mathbf{F}, \quad (22.10)$$

where

$$\mathbf{F} = \hat{\lambda} F^\lambda + \hat{\phi} F^\phi \quad (22.11)$$

is the horizontal friction vector. Furthermore, the material time derivative in this equation signifies the relative acceleration

$$\frac{Du}{Dt} = \hat{\lambda} \frac{Du}{Dt} + \hat{\phi} \frac{Dv}{Dt}. \quad (22.12)$$

### 22.1.5 Comments and further study

The primitive equations make use of the momentum equations, which contrasts to *non-primitive* equation methods that develop evolution equations for the vorticity and divergence. [Smagorinsky \(1963\)](#) was an early proponent of the hydrostatic primitive equations for use in studying the large-scale ocean and atmospheric circulation. These equations form the basis for many general circulation models of the atmosphere and ocean. However, it is notable that even finer resolution simulations are making use of the non-hydrostatic equations. Non-hydrostatic simulations are particularly relevant when studying clouds in the atmosphere and fine-scale mixing in the ocean, with both of these processes involving nontrivial vertical accelerations that break the hydrostatic approximation. These models sometimes also time step the momentum equations, and as such are referred to as *non-hydrostatic primitive equation* models.

## 22.2 Approximate hydrostatic balance

For a static fluid with identically zero net acceleration, the vertical pressure gradient precisely balances the weight of fluid in thus realizing exact hydrostatic balance. We discussed this static solution to the equations of motion in Sections 17.3 and 18.4. For a moving fluid with scales of motion that maintain a small vertical to horizontal aspect ratio, the presentation in this section reveals that the vertical pressure gradient and gravitational acceleration individually remain far larger than other accelerations acting on a fluid element. In this case, the vertical momentum equation, even for the moving fluid, remains approximately in hydrostatic balance column-by-column. We thus have a fluid state whereby each vertical fluid column is in hydrostatic balance, and yet there are horizontal pressure gradients that drive motion. In this section we study aspects of such approximately hydrostatic fluids.

### 22.2.1 Expressions for the hydrostatic pressure

Making the hydrostatic approximation in the vertical momentum equation leads to the local balance

$$\frac{\partial p}{\partial z} = -\rho g. \quad (22.13)$$

Vertically integrating upward from a point within the ocean to the ocean surface leads to the hydrostatic pressure

$$p(x, y, z, t) = p_a(x, y, t) + g \int_z^\eta \rho(x, y, z', t) dz'. \quad (22.14)$$

In this equation we wrote  $p(\eta) = p_a$  for the pressure at the ocean free surface,  $z = \eta(x, y, t)$ , arising from the weight of the overlying atmosphere or sea ice; i.e., this is the applied pressure

acting on the top of the ocean fluid. A similar integration applies to the atmosphere

$$p(x, y, z, t) = g \int_z^{z_{\text{top}}} \rho(x, y, z', t) dz', \quad (22.15)$$

where  $z = z_{\text{top}}$  is the top of the atmosphere, sometimes approximated by  $z_{\text{top}} = \infty$ . For both the ocean and the atmosphere, we assume  $g$  remains a constant over the vertical extent of the fluid, which is a sensible approximation even for the top of the atmosphere.

In both the ocean and atmosphere, the hydrostatic pressure at a vertical position,  $z$ , equals to the weight per horizontal area of matter above that position, with equations (22.14) and (22.15) providing explicit expressions in terms of *in situ* density and boundary contributions. These expressions offer a huge simplification for how we determine pressure, with the remainder of this section providing example implications.

### 22.2.2 Evolution of hydrostatic pressure

We expect that hydrostatic pressure evolves according to the convergence of mass onto the column of fluid above that point. The ocean hydrostatic pressure also changes due to time changes in the applied upper boundary pressure. Here we derive mathematical expressions that support these expectations, with Figure 22.1 providing a schematic.

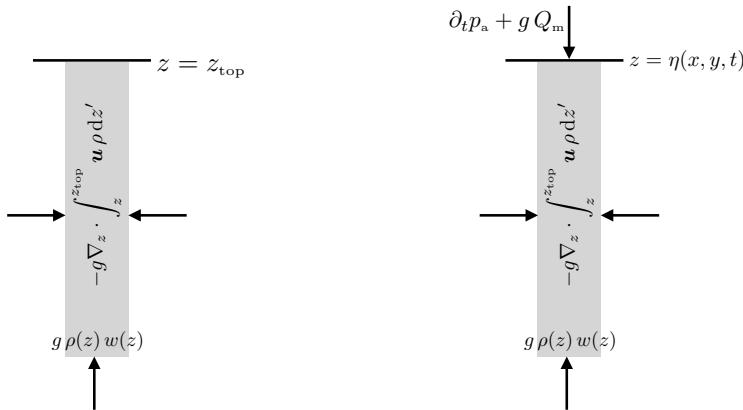


FIGURE 22.1: Evolution of hydrostatic pressure for a vertical position in the atmosphere (left panel) and ocean (right panel) according to equations (22.18) and (22.21a). Hydrostatic pressure at a vertical position,  $z$ , which here is the bottom of the fluid column, arises from the convergence of mass onto the column over the region above  $z$ . The ocean column also has a contribution from the time tendency of applied surface pressure plus the mass of coming across the top boundary. For the atmosphere as assume the top boundary is at  $z_{\text{top}} = \infty$  and so there is no mass coming across that boundary.

#### Hydrostatic pressure in the atmosphere

A time derivative of the atmospheric hydrostatic pressure expression (22.15) renders

$$\partial_t p = g \int_z^{z_{\text{top}}} \partial_t \rho(x, y, z', t) dz'. \quad (22.16)$$

Note the absence of a time derivative on  $z_{\text{top}}$ . We ensure this time derivative is not relevant by setting  $z_{\text{top}}$  to a constant value well above anything of physical relevance; e.g.,  $z_{\text{top}} \approx \infty$ . Now

insert the mass continuity equation (14.6) and make further use of Leibniz's rule to write

$$\partial_t p = -g \int_z^{z_{\text{top}}} \nabla \cdot (\mathbf{v} \rho) dz' \quad (22.17a)$$

$$= g \rho(z) w(z) - g \int_z^{z_{\text{top}}} \nabla_z \cdot (\mathbf{u} \rho) dz', \quad (22.17b)$$

where we set  $w(z_{\text{top}}) \rho(z_{\text{top}}) = 0$ . The first term on the right hand side arises from the vertical mass flux into the fluid column from below. The second term arises from the horizontal convergence of mass as integrated over the column above the position,  $z$ . If the vertical position of the bottom limit on the integral is independent of horizontal position, then we can pull the horizontal divergence operator outside of the integral to render

$$\partial_t p = g \rho(z) w(z) - g \nabla_z \cdot \int_z^{z_{\text{top}}} \mathbf{u} \rho dz'. \quad (22.18)$$

In Exercise 22.3 we derive an expression for the bottom pressure,  $p(x, y, z = \eta_b(x, y), t)$ , where we must use Leibnitz's rule to pull the horizontal derivative outside of the integral.

### *Hydrostatic pressure in the ocean*

The derivation for the ocean requires some more work since the ocean free surface is a permeable space-time dependent function. A time derivative of the ocean pressure expression (22.14) renders

$$\partial_t p = \partial_t p_a + g \rho(\eta) \partial_t \eta + g \int_z^\eta \partial_t \rho(x, y, z', t) dz', \quad (22.19)$$

where we made use of Leibniz's rule to take the time derivative of the upper limit at  $z = \eta(x, y, t)$ , and with the shorthand  $\rho(\eta) = \rho(x, y, z = \eta, t)$ . Now insert the mass continuity equation (14.6) and make further use of Leibniz's rule to write

$$\partial_t(p - p_a) - g \rho(\eta) \partial_t \eta = g \int_z^\eta \partial_t \rho(x, y, z', t) dz' \quad (22.20a)$$

$$= -g \int_z^\eta \nabla \cdot (\mathbf{v} \rho) dz' \quad (22.20b)$$

$$= -g [\rho(\eta) w(\eta) - \rho(z) w(z)] - g \int_z^\eta \nabla_z \cdot (\mathbf{u} \rho) dz' \quad (22.20c)$$

$$= g \rho(z) w(z) + g [(-w + \mathbf{u} \cdot \nabla \eta) \rho]_{z=\eta} - g \nabla_z \cdot \int_z^\eta \mathbf{u} \rho dz' \quad (22.20d)$$

$$= g \rho(z) w(z) + g (Q_m - \rho(\eta) \partial_t \eta) - g \nabla_z \cdot \int_z^\eta \mathbf{u} \rho dz', \quad (22.20e)$$

where the last step made use of the kinematic boundary condition (14.79) for the ocean free surface, with  $Q_m$  the mass flux entering the ocean across the free surface. Rearrangement, and cancellation of the  $\rho(\eta) \partial_t \eta$  term appearing on both sides, leads to

$$\partial_t p = \partial_t p_a + g \rho(z) w(z) + g Q_m - g \nabla \cdot \int_z^\eta \mathbf{u} \rho dz'. \quad (22.21a)$$

The first term on the right hand side arises from time fluctuations of the applied pressure at  $z = \eta$ . The second and third terms measure the vertical convergence of mass onto the column of fluid sitting above the vertical position, with  $\rho(z) w(z)$  the mass flux entering the column from

below and  $Q_m$  the mass flux entering from across the free surface. The final term arises from the vertically integrated horizontal mass transport converging onto the column above the position of interest.

### 22.2.3 Heuristic scaling

We here present a scale analysis to justify the hydrostatic approximation. This analysis serves to introduce a common method used in fluid mechanics to identify those processes that may be dominant for a particular flow regime. In particular, the flow regime of interest here occurs with a small vertical to horizontal aspect ratio

$$\alpha_{\text{aspect}} \equiv \frac{H}{L} \ll 1, \quad (22.22)$$

with  $H$  a typical length scale for vertical motion and  $L$  the horizontal length scale. This regime is fundamental to the large-scale circulation of the ocean and atmosphere. As the hydrostatic approximation is concerned with the force balances in a fluid column, it is sufficient to ignore rotation when performing a scale analysis.

Consider the vertical momentum equation (22.52) from the tangent plane and traditional approximations (Section 22.3), along with the associated scales for the various terms

$$\frac{Dw}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial z} - g \quad (22.23a)$$

$$\frac{W}{T} + \frac{UW}{L} + \frac{WW}{H} = -\frac{1}{\rho} \frac{\partial p}{\partial z} - g. \quad (22.23b)$$

In the second equation we introduced the following scales for the terms appearing on the left hand side of the first equation.

- $L$  is the horizontal scale of the motion.
- $H$  is the vertical scale of the motion.
- $W$  is the vertical velocity scale.
- $U$  is the horizontal velocity scale. For this analysis we do not distinguish between the zonal and meridional velocity scales, writing  $U$  for both. This assumption is not always valid, such as when scaling for jet stream or equatorial flows, both of which have larger zonal speeds than meridional.
- $T$  is the time scale of the motion. We assume that the time scale is determined by horizontal advection<sup>3</sup> so that  $T \sim L/U$ .

To get a sense for the numbers, consider large-scale atmospheric flows with  $W = 10^{-2}$  m s<sup>-1</sup>,  $L = 10^5$  m,  $H = 10^3$  m,  $U = 10$  m s<sup>-1</sup>. These numbers lead to  $T = L/U = 10^4$  s and to the values for the vertical momentum equation

$$10^{-6} \text{ m s}^{-2} \sim -\frac{1}{\rho} \frac{\partial p}{\partial z} - g. \quad (22.24)$$

With  $g \sim 10$  m s<sup>-2</sup>, the only term that can balance the gravitational acceleration is the vertical pressure gradient. A similar analysis holds for large-scale ocean flows where we set  $W =$

---

<sup>3</sup>This assumption for time scale is not always appropriate, such as for studies of waves where we may instead consider time scales according to a wave speed and wave length.

$10^{-3} \text{ m s}^{-1}$ ,  $L = 10^3 \text{ m}$ ,  $H = 10^1 \text{ m}$ ,  $U = 10^{-1} \text{ m s}^{-1}$ . These numbers lead to  $T = L/U = 10^4 \text{ s}$  and to

$$10^{-7} \text{ m s}^{-2} \sim -\frac{1}{\rho} \frac{\partial p}{\partial z} - g. \quad (22.25)$$

In either case, large scale motion maintains an approximate hydrostatic balance whereby  $\partial p/\partial z = -\rho g$ .

We offer a more formal scale analysis in Section 23.2, making use of the oceanic Boussinesq equations derived in Chapter 23. For the remainder of this section we explore certain properties of a fluid maintaining an approximate hydrostatic balance.

### 22.2.4 Removal of a dynamically irrelevant background state

The previous analysis pointed to the dominance of the hydrostatic balance in the vertical momentum equation for large scale motions. However, is that analysis sufficient to understand what causes motion? To help answer that question, consider a density field that is decomposed into a constant,  $\rho_0$ , plus a deviation

$$\rho(\mathbf{x}, t) = \rho_0 + \delta\rho(\mathbf{x}, t), \quad (22.26)$$

with a corresponding decomposition of the pressure field

$$p(\mathbf{x}, t) = p_0(z) + p'(\mathbf{x}, t) \quad \text{with} \quad \frac{dp_0}{dz} = -\rho_0 g. \quad (22.27)$$

That is, the pressure is decomposed into a background static hydrostatic pressure field that is just a function of  $z$ , plus a deviation from the background pressure. In this case, the non-rotating vertical momentum equation takes the form

$$\rho \frac{Dw}{Dt} = -\frac{\partial p'}{\partial z} - \left[ \frac{dp_0}{dz} + \rho_0 g \right] = -\frac{\partial p'}{\partial z}. \quad (22.28)$$

We thus see that the exact hydrostatically balanced background pressure,  $p_0(z)$ , has no dynamical implications. Correspondingly, to garner a more relevant scaling for the hydrostatic balance it is appropriate to ask whether the dynamically active pressure,  $p'$ , is approximately hydrostatic.

For flows with small aspect ratios, the vertical momentum equation remains approximately hydrostatic even when removing the dynamically inactive background pressure field. So our intuition about hydrostatic dominance holds unchanged even for the dynamical pressure. The formal justification of this approximation is nicely framed within the Boussinesq equations of Chapter 23 since the pressure force in these equations exposes just the dynamically active pressure. We thus postpone further discussion of hydrostatic scaling until Section 23.2.

### 22.2.5 Decomposing the horizontal pressure gradient

In contrast to an exact hydrostatic fluid, where there is no motion, there are generally horizontal pressure gradients in an approximate hydrostatic fluid, and these horizontal gradients drive horizontal motion. Such horizontal gradients in the hydrostatic pressure can arise from horizontal differences in the fluid mass density. We refer to such pressure gradients as *internal pressure gradients* since they arise from density gradients internal to the fluid. Horizontal pressure gradients can also arise from horizontal gradients in the total mass of a fluid column, with such pressure gradients referred to as *external pressure gradients*. In developing an understanding of the horizontal pressure gradients in an approximate hydrostatic fluid, it can be useful to examine the mathematical expressions for the pressure gradient. We do so in this section, considering the

specific case of a column of ocean fluid.<sup>4</sup>

Recall equation (22.14), which expresses the hydrostatic pressure at a point within the ocean

$$p(x, y, z, t) = p_a(x, y, t) + g \int_z^\eta \rho(x, y, z', t) dz'. \quad (22.29)$$

In this equation,  $p_a = p[x, y, z = \eta(x, y, t), t]$  is the pressure applied to the ocean free surface at  $z = \eta(x, y, t)$  from any mass above the ocean, such as the atmosphere or cryosphere. In many idealized cases we assume the media above the ocean is massless, in which case  $p_a = 0$ . Nonetheless, we maintain  $p_a \neq 0$  for generality. Now introduce the globally referenced buoyancy (see Chapter 24) as defined by

$$b = -g(\rho - \rho_0)/\rho_0, \quad (22.30)$$

in which case the pressure is

$$p = -g\rho_0 z + g\rho_0 [\eta + p_a/(g\rho_0)] - \rho_0 \int_z^\eta b dz'. \quad (22.31)$$

The first term is a background pressure that increases moving downward. However, this background pressure has no horizontal dependence and so it does not contribute to the horizontal pressure gradients. In contrast, the second and third terms have horizontal gradients and are thus sometimes referred to as the *dynamical pressure*. The second term arises from the free surface height plus the applied surface pressure. This term is uniformly felt throughout the fluid column since it has no vertical dependence. The free surface term is the product of the large number,  $g\rho_0$ , times a small free surface undulation,  $\eta$ . The third term arises from buoyancy within the fluid computed relative to the constant background density,  $\rho_0$ , and this term is a function of vertical position. Furthermore, it is the vertical integral over a generally large depth range of the relatively small buoyancy. In this manner, the second and third terms can generally be of comparable magnitude.

The horizontal gradient of the hydrostatic pressure (22.31) is given by

$$\nabla_z p = \underbrace{\nabla_z p_a + g\rho(\eta)\nabla_z \eta}_{\text{external contribution}} - \underbrace{\rho_0 \int_z^\eta \nabla_z b dz'}_{\text{internal contribution}}. \quad (22.32)$$

Again, the external contribution acts throughout the vertical fluid column since it is only a function of horizontal position and time. Every point within the fluid column instantly feels this term whenever there is a gradient in the applied surface pressure, the surface height, or the surface buoyancy, with  $\rho_0[g - b(\eta)] = g\rho(\eta)$ . The internal term arises from horizontal gradients in the *in situ* buoyancy that are integrated vertically over the region above the point of interest.

We can invert the above formulation by introducing the bottom pressure

$$p_b = p_a + g \int_{\eta_b}^\eta \rho dz, \quad (22.33)$$

in which case

$$p = p_b - g\rho_0(z - \eta_b) + \rho_0 \int_{\eta_b}^z b dz', \quad (22.34)$$

---

<sup>4</sup>Note that some authors refer to *baroclinic* and *barotropic* pressure gradients rather than the *internal* and *external* used here.

so that the corresponding expression for the horizontal hydrostatic pressure gradient is

$$\nabla_z p = \underbrace{\nabla_z p_b + g \rho(\eta_b) \nabla_z \eta_b}_{\text{external contribution}} + \underbrace{\rho_0 \int_{\eta_b}^z \nabla_z b \, dz'}_{\text{internal contribution}}. \quad (22.35)$$

The bottom pressure contribution is dominated by gradients in the bottom topography so that it can be useful to write

$$\nabla_z p_b = -\rho_0 g \nabla_z \eta_b + \nabla_z p'_b, \quad (22.36)$$

in which case the external contribution takes the form

$$\nabla_z p = \underbrace{\nabla_z p'_b - \rho_0 b(\eta_b) \nabla_z \eta_b}_{\text{barotropic contribution}} + \underbrace{\rho_0 \int_{\eta_b}^z \nabla_z b \, dz'}_{\text{baroclinic contribution}}. \quad (22.37)$$

As for the expression (22.32), we have decomposed the horizontal pressure gradient into an external and internal contribution. Here, the external contributions arise from gradients in the bottom pressure, which measures the mass per area of fluid within the column, plus gradients in the bottom topography as weighted by the difference between the gravitational acceleration and bottom buoyancy, with  $\rho_0[g - b(\eta_b)] = g \rho(\eta_b)$ . The internal term arises from gradients in the buoyancy as integrated below the depth of interest.

### 22.2.6 Horizontal hydrostatic pressure gradient in a mass conserving fluid

We here consider a specific example that is emblematic of how one determines the sign for horizontal gradients in a mass conserving fluid that maintains an approximate hydrostatic balance, and thus to determine the direction for the pressure force. In so doing, we further our understanding of the pressure field driving motion in a hydrostatic fluid. The example is posed for a bounded column of fluid, as in the ocean, but analogous considerations hold for the atmosphere where the upper boundary is the top of the atmosphere (i.e., effectively unbounded). Furthermore, the fluid is assumed to be compressible so that fluid elements conserve their mass. In Section 23.2.5 we reconsider this example for a volume conserving oceanic Boussinesq fluid.

#### *Two columns with equal mass yet different densities*

Consider two adjacent columns of seawater with equal mass but with distinct density; assume the density in each column is constant throughout the respective columns; and assume the atmospheric pressure has equal mass above the two water columns. Figure 22.2 offers a schematic, where we make the additional assumption that the two columns sit on a flat bottom. We can imagine setting up this configuration by starting with uniform density water, then warming the water in column B more than column A while maintaining constant mass in the two columns. This process sets up a horizontal density gradient with an associated horizontal gradient in the hydrostatic pressure. Furthermore, the less dense water in column B occupies more volume so that its free surface sits higher

$$\rho_B < \rho_A \implies \eta_B > \eta_A. \quad (22.38)$$

What is the sign of the horizontal hydrostatic pressure gradient? As we show in the following, column B (the low density column) has larger hydrostatic pressure than column A (the high density column) for every point in the column, except at the bottom where the two bottom pressures are identical since the two columns have equal mass.

### Computing pressure starting from the equal bottom pressures

Since the two columns have equal mass and equal cross-sectional area, the hydrostatic pressures (weight per unit area) at the bottom of the two columns are equal and given by

$$p_{\text{bot}} = g \rho_A (\eta_A - \eta_b) = g \rho_B (\eta_B - \eta_b), \quad (22.39)$$

where  $z = \eta_b(x, y)$  is the vertical position at the bottom,  $z = \eta_A(x, y, t)$  is the top of column A, and  $z = \eta_B(x, y, t)$  top of column B. Since the bottom pressures are identical, there is no horizontal pressure gradient at the bottom so that all pressure gradients exist above the bottom.

The hydrostatic pressure at an arbitrary position within column A is given by

$$p_A(z) = g \rho_A (\eta_A - z) = p_{\text{bot}} - g \rho_A (-\eta_b + z). \quad (22.40)$$

The second equality arose by substituting the bottom pressure from equation (22.39) to eliminate the surface height  $\eta_A$ . Likewise, the pressure in column B is given by

$$p_B(z) = g \rho_B (\eta_B - z) = p_{\text{bot}} - g \rho_B (-\eta_b + z). \quad (22.41)$$

We can now take the difference between the two hydrostatic pressures to find

$$p_B(z) - p_A(z) = g (-\eta_b + z) (\rho_A - \rho_B) > 0. \quad (22.42)$$

Since  $\rho_A > \rho_B$  and  $z \geq \eta_b$  we see that at any point above the bottom, the hydrostatic pressure in column B (the lighter column) is greater than that in column A (the denser column). This horizontal difference in the hydrostatic pressure renders a force pointing from column B to column A. Vertically integrating this pressure difference over the thickness of column A leads to the net force per horizontal length

$$F_{\text{pressure B to A}} = \int_{\eta_b}^{\eta_A} [p_B(z) - p_A(z)] dz = (g/2) (\rho_A - \rho_B) (\eta_A - \eta_b)^2 > 0. \quad (22.43)$$

### Inferring pressure gradients starting from the top

Another way to understand why the pressure force points from column B to column A is to note that at the top of both columns the pressures are the same (and equal to the uniform atmospheric pressure). However, since column B sits higher than column A, as we move down from  $z = \eta_B$  the pressure increases in column B immediately, whereas the pressure in column A remains at the atmospheric pressure until entering the water column at  $z = \eta_A < \eta_B$ . So it is clear that the pressure in column B is greater than A starting from the surface and moving down. Since the two bottom pressures are equal, then one can infer the pressure isolines as drawn in Figure 22.2.

### 22.2.7 Ocean dynamic topography

There are occasions in oceanography where it is useful to study the thickness of a layer bounded by isobars. For example, it is often assumed in dynamical oceanography that there is a pressure at which baroclinic currents vanish (*level of no motion*), with the reduced gravity model of Section 30.3 studying the associated dynamical implications.<sup>5</sup> We are thus led to consider the thickness of fluid extending from the ocean free surface to a chosen pressure level in the ocean interior as

<sup>5</sup>Baroclinic refers to a fluid state with pressure and density surfaces distinct, whereas these surfaces are parallel in a *barotropic* fluid state. We discuss *baroclinicity* in the context of vorticity in Section 35.5.

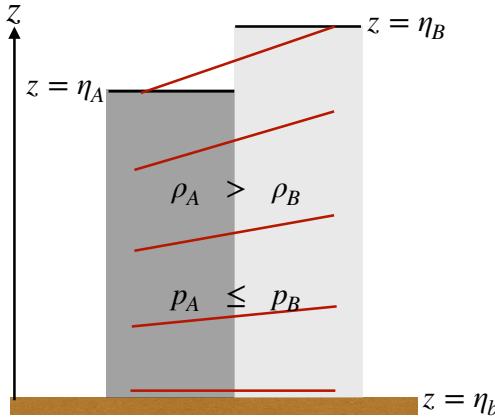


FIGURE 22.2: Two seawater columns on a flat bottom with equal mass but different densities with  $\rho_A > \rho_B$ . We assume the atmosphere above the columns has the same pressure over both columns, thus offering zero horizontal pressure force. Furthermore, the horizontal cross-sectional area of the two columns are the same so that the less dense water in column  $B$  has more volume and thus a greater thickness:  $\eta_B > \eta_A$ . Since the column masses are the same, the hydrostatic pressures (weight per horizontal area) at the bottom of the two columns are equal:  $p_A(z = \eta_b) = p_B(z = \eta_b) = p_{\text{bot}}$ . In oceanographic parlance, the bottom offers a “level of no motion” from which to reference the pressure field. At any position  $z$  above the bottom, equation (22.42) shows that the hydrostatic pressure in column  $B$  is greater than  $A$ :  $p_B(z) - p_A(z) = g(-\eta_b + z)(\rho_A - \rho_B) > 0$ . The horizontal gradient in hydrostatic pressure thus points from column  $B$  towards column  $A$ . The red lines show lines of constant pressure (isobars), which are horizontal next to the bottom but which slope upward to the right moving towards the surface. This configuration provides salient points about hydrostatic pressure relevant for the slightly more complex reduced gravity example in Figure 30.5. Also, it is useful to compare this schematic to Figure 25.4, which discusses the depth dependence of the horizontal gradient in hydrostatic pressure as per  $\partial(\nabla_z p)/\partial z = -g \nabla_z \rho$ .

given by

$$D(p) = \eta - z(p). \quad (22.44)$$

Assuming a hydrostatic balance for each fluid column allows us to relate this expression to the vertical integral between two pressure surfaces of the specific volume,  $\rho^{-1}$

$$D(p) = \int_{z(p)}^{\eta} dz = g^{-1} \int_{p_a}^p \frac{dp'}{\rho}, \quad (22.45)$$

where the second step used the hydrostatic balance and absorbed a minus sign by swapping integral limits. We refer to the thickness  $D(p)$  as the *dynamic topography* with respect to a reference pressure  $p$ . Note that it is sometimes also called the *steric sea level*. Evolution of the dynamic topography arises from changes in the pressure applied to the free surface as well as changes in the specific volume

$$g \frac{\partial D(p)}{\partial t} = -\frac{1}{\rho(\eta)} \frac{\partial p_a}{\partial t} + \int_{p_a}^p \frac{\partial \rho^{-1}}{\partial t} dp. \quad (22.46)$$

Note that the time derivative acts on the specific volume when computed on surfaces of constant pressure. If the depth  $z(p)$  of the constant pressure surface is static, then the evolution of layer thickness,  $D(p)$ , is identical to the sea surface,  $\eta$ . In general, there is no such static pressure level, thus making the time tendencies differ, though certain situations warrant this approximation.

## 22.2.8 Surfaces of atmospheric geopotential height and pressure

In Section 20.12.10 we computed the geopotential height within an exact hydrostatic and ideal gas atmosphere. We here apply those results to the case of approximate hydrostatic and ideal gas columns, making use of equation (20.193) for the difference in geopotential height between two isobars

$$Z_2 - Z_1 = -(R^{\text{atm}} \langle T \rangle / g) \ln(p_2/p_1). \quad (22.47)$$

In this equation,  $\langle T \rangle$  is the mean temperature within the column as computed according equation (20.191), and  $R^{\text{atm}}$  is the specific gas constant for air given by equation (20.162). The geopotential thickness of a column is positive when the isobars have  $p_2 < p_1$ ; i.e.,  $p_2$  is higher in the atmosphere than  $p_1$ . Furthermore, the geopotential thickness of a column is directly proportional to the column mean temperature so that a warmer column is thicker. This result is expected since for a given mass of air, a warmer column is less dense and so isobars are higher over warmer hydrostatic air columns than cooler columns. Correspondingly, when moving horizontally along a constant geopotential surface, we encounter higher pressure when moving into a region of warmer air. This situation is entirely analogous to that in Figure 22.2 when studying the horizontal pressure difference between two hydrostatic and equal mass columns of seawater.

## 22.2.9 Concerning vertical motion

Unbalanced vertical accelerations still exist in an approximate hydrostatic fluid. Yet these vertical accelerations are not needed for the prognostic equations since the vertical momentum equation reduces to a local hydrostatic balance. Hence, rather than compute vertical motion prognostically, vertical motion in an approximate hydrostatic fluid is diagnosed through constraints on the fluid motion.

For example, an important constraint on the large-scale ocean circulation arises from vorticity and potential vorticity conservation, which are topics considered in Part VI of this book. Mass continuity discussed in Section 23.1.4 provides another constraint. In particular, horizontal velocity divergence in an incompressible flow is balanced by vertical velocity convergence as per equation (23.17). The vertical pressure forces required to produce the vertical motion are those precisely needed to maintain volume continuity. In a hydrostatic fluid, we do not directly compute these forces for the purpose of prognosing vertical accelerations. Rather, the vertical acceleration is inferred through kinematic constraints. The associated forces, if desired, can be diagnosed given the velocity and the accelerations.

## 22.2.10 Further study

Section 2.7.4 in [Vallis \(2017\)](#) provides examples of scales over which the hydrostatic relation remains a useful approximation in geophysical fluids. Our discussion of the hydrostatic pressure in Section 22.2.6 is motivated by similar considerations presented in Chapter 2 of the descriptive oceanography text from [Tomczak and Godfrey \(1994\)](#). Further discussion of dynamic topography is given in Appendix B.4 of [Griffies et al. \(2014\)](#) as well as in [Tomczak and Godfrey \(1994\)](#). Finally, this [8-minute video from Prof. Hogg](#) offers an introduction to hydrostatic pressure.

# 22.3 The tangent plane approximation: $f$ -plane and $\beta$ -plane

Spherical coordinates are suited for the study of planetary fluid dynamics for cases where the fluid samples the earth's sphericity. However, spherical coordinates remain more complicated to work with than Cartesian coordinates. We are thus led to consider the utility of an idealized tangent

plane configuration as part of a hierarchy of theoretical models to help understand geophysical fluid motion. This motivation leads to the  $f$ -plane and  $\beta$ -plane approximations, which are the two cases considered as part of the tangent plane approximations. Note that we can consider either hydrostatic or non-hydrostatic flows within these *tangent plane* approximations.

### 22.3.1 Tangent plane approximation

Consider a tangent plane located at latitude  $\phi = \phi_0$  and introduce a Cartesian set of coordinates according to

$$(x, y, z) = (R_e \lambda \cos \phi_0, R_e (\phi - \phi_0), z) \quad (22.48)$$

$$(\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}}) = (\hat{\boldsymbol{\lambda}}, \hat{\boldsymbol{\phi}}, \hat{\mathbf{r}}). \quad (22.49)$$

Use of these Cartesian coordinates leads to the following inviscid (i.e., no friction) equations of motion

$$\frac{Du}{Dt} + 2(\Omega^y w - \Omega^z v) = -\frac{1}{\rho} \frac{\partial p}{\partial x} \quad (22.50)$$

$$\frac{Dv}{Dt} + 2(\Omega^z u - \Omega^x w) = -\frac{1}{\rho} \frac{\partial p}{\partial y} \quad (22.51)$$

$$\frac{Dw}{Dt} + 2(\Omega^x v - \Omega^y u) = -\frac{1}{\rho} \frac{\partial p}{\partial z} - g, \quad (22.52)$$

with rotational vector components

$$\boldsymbol{\Omega} = \Omega (\cos \phi_0 \hat{\mathbf{y}} + \sin \phi_0 \hat{\mathbf{z}}). \quad (22.53)$$

Note the absence of metric terms due to the use of Cartesian coordinates on a flat planar geometry.

The tangent plane approximation originates from the geopotential vertical coordinate system (Section 9.13.3). In that coordinate system, the effective gravitational acceleration (gravity plus planetary centrifugal) is aligned with the local vertical direction. Correspondingly, the resulting tangent plane equations have the effective gravitational force aligned in the  $\hat{\mathbf{z}}$  direction. As seen in Section 22.4, these equations are slightly different from those describing a fluid in a rotating tank, in which the effective gravity is not aligned with the vertical.

### 22.3.2 Traditional approximation and the $f$ -plane

The traditional approximation retains only the local vertical component of the rotation vector, resulting in

$$\frac{Du}{Dt} - fv = -\frac{1}{\rho} \frac{\partial p}{\partial x} \quad (22.54)$$

$$\frac{Dv}{Dt} + fu = -\frac{1}{\rho} \frac{\partial p}{\partial y} \quad (22.55)$$

$$\frac{Dw}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial z} - g. \quad (22.56)$$

The  $f$ -plane makes use of a constant Coriolis parameter

$$f = 2\Omega \sin \phi_0 \equiv f_0. \quad (22.57)$$

The  $f$ -plane approximation is the simplest model for a rotating fluid, and as such it provides an end member in the hierarchy of theoretical models for geophysical fluid flows.

### 22.3.3 $\beta$ -plane approximation

As seen in Section 33.6, *Rossby waves* are planetary scale waves that sample the earth's spherical geometry. The essential ingredient for their existence is the latitudinal dependence of the Coriolis parameter. To capture Rossby waves on a tangent plane requires the meridional gradient of the Coriolis parameter, with a linear dependence sufficient

$$f = f_0 + R_e^{-1} (2\Omega \cos \phi_0) (y - y_0). \quad (22.58)$$

For many purposes the  $\beta$ -plane approximation only depends on the meridional gradient of the Coriolis parameter, in which case we generally set

$$f = f_0 + \beta y \quad (22.59)$$

$$\beta = \partial f / \partial y = (2\Omega / R_e) \cos \phi_0, \quad (22.60)$$

thus ignoring the constant  $-(2\Omega \cos \phi_0) y_0 / R_e$ .

## 22.4 Homogeneous fluid in a rotating tank

As an application of the ideas developed in this chapter and in earlier chapters, we develop the equations for a homogeneous fluid in a rotating tank such as occurs in laboratory studies of rotating fluids. One point of departure from planetary applications concerns the choice of vertical coordinate. Recall we introduced geopotential surfaces in Section 9.12.4, on which the effective gravitational force (sum of central gravity plus planetary centrifugal) is constant. Correspondingly, we introduced geopotential coordinates in Section 9.13.3 to simplify the equations for planetary fluid dynamics. In contrast, for the rotating tank we do not make use of geopotential coordinates. Instead, we expose the centrifugal acceleration (due to rotation of the tank), which allows for a clear display of the parabolic shape for the free surface when the fluid is in solid-body motion.

### 22.4.1 What about the planet's rotation?

Do we need to worry about the planet's rotation? To answer this question, consider a typical record player with an angular speed of 45 revolutions per minute

$$\Omega_{\text{record}} = 0.75 \text{ s}^{-1}. \quad (22.61)$$

This angular speed is roughly  $10^4$  times faster than the earth's angular speed of  $7.29 \times 10^{-5} \text{ s}^{-1}$  (equation (9.33)). For a tank rotating at a rate on the same order as a record player, we are justified ignoring the rotating earth in comparison to the rotating tank. That is, we can safely ignore planetary Coriolis and planetary centrifugal accelerations, allowing us to instead focus on non-inertial accelerations just from the rotating tank.

### 22.4.2 Formulating the equations of motion

In an inertial reference frame, a fluid element feels the gravitational force, pressure force, and friction, thus leading to the Cartesian coordinate equations of motion

$$\frac{Du_I}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + F^x \quad (22.62)$$

$$\frac{Dv_I}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial y} + F^y \quad (22.63)$$

$$\frac{Dw_I}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial z} - g_e + F^z, \quad (22.64)$$

where  $\mathbf{v}_I$  is the inertial velocity,  $\rho$  is the constant density, and we orient the coordinates so that the  $z$ -axis extends vertically upward from the center of the tank and parallel to the gravity acceleration. Correspondingly, the rotation vector for the tank is

$$\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}} = (f/2) \hat{\mathbf{z}}. \quad (22.65)$$

To derive the rotating frame equations, return to some of the kinematics from Chapter 9, in which we write the position of a fluid particle as

$$\mathbf{X}(t) = X \hat{\mathbf{x}} + Y \hat{\mathbf{y}} + Z \hat{\mathbf{z}}. \quad (22.66)$$

We assume that the Cartesian unit vectors are fixed in the rotating frame and thus move as a solid body with the rotating tank. The inertial velocity is thus given by

$$\frac{d\mathbf{X}}{dt} = \left[ \frac{dX}{dt} \right] \hat{\mathbf{x}} + \left[ \frac{dY}{dt} \right] \hat{\mathbf{y}} + \left[ \frac{dZ}{dt} \right] \hat{\mathbf{z}} + \boldsymbol{\Omega} \times \mathbf{X}. \quad (22.67)$$

Correspondingly, the acceleration is given by

$$\frac{d^2\mathbf{X}}{dt^2} = \left[ \frac{d^2X}{dt^2} \right] \hat{\mathbf{x}} + \left[ \frac{d^2Y}{dt^2} \right] \hat{\mathbf{y}} + \left[ \frac{d^2Z}{dt^2} \right] \hat{\mathbf{z}} + 2\boldsymbol{\Omega} \times \mathbf{v} + \boldsymbol{\Omega} \times (\boldsymbol{\Omega} \times \mathbf{X}), \quad (22.68)$$

where we defined the rotating frame Cartesian velocity as

$$\mathbf{v} = \left[ \frac{dX}{dt} \right] \hat{\mathbf{x}} + \left[ \frac{dY}{dt} \right] \hat{\mathbf{y}} + \left[ \frac{dZ}{dt} \right] \hat{\mathbf{z}}. \quad (22.69)$$

Setting the inertial acceleration equal to the inertial force per mass leads to the equations of motion in the rotating frame

$$\frac{Du}{Dt} - 2\Omega v = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \Omega^2 x + F^x \quad (22.70)$$

$$\frac{Dv}{Dt} + 2\Omega u = -\frac{1}{\rho} \frac{\partial p}{\partial y} + \Omega^2 y + F^y \quad (22.71)$$

$$\frac{Dw}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial z} - g_e + F^z, \quad (22.72)$$

which take on the vector form

$$\frac{D\mathbf{v}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{v} = -\nabla [p/\rho + g_e z - \Omega^2 (x^2 + y^2)/2] + \mathbf{F}. \quad (22.73)$$

As expected, we encounter both a Coriolis and centrifugal acceleration due to the rotation of the tank.

### 22.4.3 Solid-body rotation and free surface shape

Consider a fluid at rest in a non-rotating tank, and then start the tank rotating. As in our discussion of Couette flow in Section 18.7.2, viscous effects transfer motion from the outside tank wall (where a no-slip boundary condition makes the fluid move with the wall) into the interior of the fluid. Given sufficient time and a constant rotation rate, the fluid will move as a solid-body. As an application of the above equations of motion, we here determine the shape of the upper free surface for this solid-body motion, offering two related derivations. Note that when the fluid reaches solid-body motion, all strains vanish within the fluid so that frictional stresses vanish (see Section 18.7). Hence, the steady force balance is fully inviscid although the steady state required viscosity to reach it.

#### *Component equations of motion*

The velocity and acceleration in the rotating frame are zero when the fluid is in solid-body rotation. The vertical momentum equation (22.72) thus reduces to hydrostatic balance

$$\frac{\partial p}{\partial z} = -\rho g_e. \quad (22.74)$$

In general we do not have hydrostatic balance for motion in a tank that deviates from solid-body. However, when that motion is close to a solid-body rotation, then the fluid is in an approximate hydrostatic balance. As seen in Section 22.2, this situation corresponds to the large-scale ocean and atmosphere.

Hydrostatic balance with a constant density means that the pressure is a linear function of depth

$$p(x, y, z) = \rho g_e (\eta - z), \quad (22.75)$$

where  $z = \eta(x, y)$  is the vertical position of the free surface. The horizontal momentum equations (22.70)-(22.71) reduce to a balance between the pressure gradient and centrifugal accelerations

$$\frac{\partial p}{\partial x} = \rho x \Omega^2 \quad \text{and} \quad \frac{\partial p}{\partial y} = \rho y \Omega^2. \quad (22.76)$$

Pressure thus increases when moving radially away from the center. Substituting in the pressure as given by the hydrostatic relation (22.75) leads to relations satisfied by the solid-body free surface

$$g_e \frac{\partial \eta}{\partial x} = x \Omega^2 \quad \text{and} \quad g_e \frac{\partial \eta}{\partial y} = y \Omega^2. \quad (22.77)$$

Integration leads to the quadratic expression for the free surface

$$\eta = \eta(0) + \frac{\Omega^2 (x^2 + y^2)}{2 g_e}, \quad (22.78)$$

where  $\eta(0)$  is the free surface at the center of the tank where  $x = y = 0$ . The solid-body rotating fluid thus has a quadratic free surface with the height of the surface increasing away from the center. Notice how the fluid density dropped out from the problem, so that this parabolic shape holds for any fluid in solid-body motion.

### Vector force balance

A more telescopic means to determine the free surface shape is to set the forces to zero on the right hand side of the vector equation of motion (22.73) so that

$$p/\rho + g_e z - \Omega^2 (x^2 + y^2)/2 = p_0/\rho, \quad (22.79)$$

where  $p_0$  is a constant pressure to be specified below. Furthermore, we set friction to zero since the fluid is in solid-body motion. Everywhere along the free surface, with  $z = \eta$ , the pressure equals to that applied to the free surface by the overlying media,  $p = p_a$  (e.g., atmospheric pressure). Hence, setting  $z = \eta$  in equation (22.79) and solving for  $\eta$  yields

$$\eta = \frac{p_0 - p_a}{\rho g_e} + \frac{\Omega^2 (x^2 + y^2)}{2 g_e}. \quad (22.80)$$

For simplicity, assume the applied pressure is spatially constant. Hence, setting  $p_0$  according to the free surface at  $x = y = 0$  brings the free surface to the parabolic form in equation (22.78)

$$\frac{p_0 - p_a}{\rho g_e} = \eta(0) \implies \eta = \eta(0) + \frac{\Omega^2 (x^2 + y^2)}{2 g_e}. \quad (22.81)$$

#### 22.4.4 Further study

We study the angular momentum for the shallow water version of this system in Section 31.7. Refer to Section 6.6.4 of [Marshall and Plumb \(2008\)](#) for more discussion of laboratory rotating tank experiments.

## 22.5 Exercises

### EXERCISE 22.1: PRIMITIVE EQUATIONS AND AXIAL ANGULAR MOMENTUM

The axial angular momentum of a fluid element satisfying the primitive equations is given by

$$L^z = (\rho \delta V) R_\perp (u + R_\perp \Omega) \equiv (\rho \delta V) l^z \quad (22.82)$$

where

$$R_\perp = R_e \cos \phi \quad (22.83)$$

is the distance from the polar rotation axis to a point on the sphere with radius  $R_e$ , and

$$l^z = R_\perp (u + R_\perp \Omega) \quad (22.84)$$

is the angular momentum per unit mass.

- (a) Consider a constant mass fluid element in the absence of friction. Show that the primitive equation zonal momentum equation (22.7) implies that the material evolution of axial angular momentum per mass is given by

$$\frac{Dl^z}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial \lambda}. \quad (22.85)$$

- (b) Assume the zonal pressure gradient vanishes. Move the fluid element vertically while maintaining a fixed latitude. What happens to the zonal momentum of this primitive equation fluid element? Hint: be sure to remain within the “world” of the primitive equations.

- (c) Give a very brief symmetry argument for why the axial angular momentum is materially conserved when  $\partial p / \partial \lambda = 0$ . Hint: recall the discussion of Noether's Theorem in Section 10.2.1.
- (d) Consider the material evolution of primitive equation axial angular momentum per mass in the case where the zonal momentum equation retains the unapproximated form of the Coriolis acceleration. Discuss the resulting material evolution equation. Does this equation make sense based on the symmetry argument given in the previous part of this exercise?

## EXERCISE 22.2: MASS BALANCE FOR A HYDROSTATIC OCEAN COLUMN

Equation (14.88) provides a kinematic expression for the column mass budget. Show that for a hydrostatic fluid the mass balance for a fluid column (equation (14.100)) takes the form

$$\partial_t(p_b - p_a) = -g \nabla \cdot \mathbf{U}^\rho + g Q_m, \quad (22.86)$$

where

$$\mathbf{U}^\rho = \int_{\eta_b}^{\eta} \mathbf{u} \rho dz \quad (22.87)$$

is the depth integrated horizontal mass transport,

$$p_b = p_a + g \int_{\eta_b}^{\eta} \rho dz \quad (22.88)$$

is the hydrostatic pressure at the ocean bottom, and  $p_a(x, y, t)$  is the pressure applied to the ocean surface from the overlying atmosphere or sea ice.

## EXERCISE 22.3: EVOLUTION OF ATMOSPHERIC BOTTOM HYDROSTATIC PRESSURE

In deriving equation (22.18) we assumed the lower limit on the integral to be a horizontal constant. However, when integrating over the full atmospheric column, the lower limit varies horizontally given that the earth boundary is not flat. Return to equation (22.17b) and derive the evolution equation for the bottom pressure

$$\partial_t p_{\text{bot}} = -g \nabla_z \cdot \mathbf{U}^\rho, \quad (22.89)$$

where

$$p_{\text{bot}}(x, y, t) = p[x, y, z = \eta_b(x, y), t] \quad (22.90)$$

is the atmospheric pressure at the solid earth at  $z = \eta_b(x, y)$ ,

$$\mathbf{U}^\rho = \int_{\eta_b}^{z_{\text{top}}} \mathbf{u} \rho dz' \quad (22.91)$$

is the depth integrated horizontal mass transport, and  $z_{\text{top}}$  is the vertical position of the atmospheric top that is assumed to be independent of horizontal position.





# Chapter 23

## Oceanic Boussinesq fluid

In some areas of fluid mechanics the speed of fluid particles can approach the speed of sound. In that case, the *Mach number*, which is the ratio of the fluid speed to the sound speed, reaches unity or larger.<sup>1</sup> In such flows it is important to consider the influence of compressibility since the large flow speeds can lead to nontrivial local density changes through the convergence of advective fluxes. Geophysical flows of interest in this book have Mach numbers well below unity. Nonetheless, even with a small Mach number the impacts of pressure can play a nontrivial role in affecting density changes. Such pressure effects are particularly important in a gas such as the atmosphere, in which case realistic studies of atmospheric flow generally maintain full compressibility.

The flow in many liquids is close to incompressible whereby the velocity is well approximated as non-divergent thus allowing for the volume conserving kinematics from Chapter 16. Even so, a strictly incompressible fluid is one where the density is uniform throughout, with this approximation not suitable for the ocean when aiming to capture physical processes driving large-scale ocean circulation. In this chapter we study how the *seawater or oceanic Boussinesq approximation* finds a middle ground between compressible and incompressible fluids. The oceanic Boussinesq approximation comprises a quasi-compressible fluid in which density materially changes, yet with a non-divergent flow whereby the prognostic velocity is non-divergent. In essence, it achieves a middle ground by measuring the mass of a fluid element by multiplying the volume of the element with a constant reference density,  $\rho_0$ . In contrast, the weight of the fluid element (and hence its gravitational potential energy) is computed with the gravitational acceleration multiplying the space-time dependent *in situ* density,  $\rho(\mathbf{x}, t)$ . Furthermore, the oceanic Boussinesq fluid is energetically consistent so long as the *in situ* density is determined with pressure set according to  $\rho(S, \Theta, p_{\text{eos}} = -\rho_0 \Phi)$  where  $\Phi(\mathbf{x}, t)$  is the geopotential.

### READER'S GUIDE TO THIS CHAPTER

We here derive the oceanic Boussinesq approximation and explore certain of its physical properties including energetics. As part of this discussion we study the available potential energy, which measures that portion of the potential energy available for converting to kinetic energy. Available potential energy is a concept that also holds for compressible non-Boussinesq fluids, but it is more conveniently studied within a Boussinesq fluid. The oceanic Boussinesq fluid has broader application than just to the ocean, with many of its characteristics also holding for atmospheric flow satisfying the anelastic approximation (see Section 2.5 of [Vallis \(2017\)](#)). Furthermore, the oceanic Boussinesq fluid provides the starting point for many of the

<sup>1</sup>When a jet airplane or rocket moves at a speed greater than Mach one, such super-sonic motion generates a spectacularly loud and powerful sonic boom.

geophysical fluid models found later in this book.

23.1	The oceanic Boussinesq approximation . . . . .	538
23.1.1	Isolating the dynamically active pressure field . . . . .	539
23.1.2	Boussinesq momentum equation . . . . .	540
23.1.3	A vorticity motivation to set $\rho_0$ constant . . . . .	541
23.1.4	Mass continuity . . . . .	541
23.1.5	Dependence on reference density . . . . .	542
23.1.6	Version I of the Boussinesq equations . . . . .	542
23.1.7	Version II of the oceanic Boussinesq equations . . . . .	543
23.1.8	Summary points . . . . .	544
23.1.9	Further study . . . . .	546
23.2	Scaling for the hydrostatic approximation . . . . .	546
23.2.1	Stratified non-rotating Boussinesq equations . . . . .	546
23.2.2	Non-dimensionalization . . . . .	547
23.2.3	Specifying scales . . . . .	547
23.2.4	The role of the Froude number . . . . .	548
23.2.5	Horizontal hydrostatic pressure gradient . . . . .	549
23.2.6	Evolution of hydrostatic pressure . . . . .	550
23.3	How pressure enforces non-divergent flow . . . . .	551
23.3.1	Poisson equation for pressure . . . . .	551
23.3.2	Characterizing the pressure sources . . . . .	552
23.3.3	Comments and further study . . . . .	554
23.4	Tracer budgets in Eulerian regions . . . . .	554
23.4.1	Formulating the budget equation . . . . .	554
23.4.2	Interpreting advective tracer contributions . . . . .	555
23.4.3	A rectangular region example . . . . .	555
23.4.4	Comments . . . . .	556
23.5	Subgrid scale processes and boundary conditions . . . . .	556
23.5.1	Material evolution of buoyancy . . . . .	557
23.5.2	Mechanical forcing and dissipation . . . . .	557
23.6	Mechanical energy analysis part I . . . . .	558
23.6.1	Kinetic energy . . . . .	559
23.6.2	Gravitational and mechanical energies . . . . .	560
23.7	Mechanical energy analysis part II . . . . .	561
23.7.1	Boussinesq dynamic enthalpy . . . . .	561
23.7.2	Regionally integrated Boussinesq dynamic enthalpy . . . . .	563
23.7.3	Vertical derivative of density . . . . .	564
23.7.4	Comments . . . . .	566
23.8	Available potential energy (APE) . . . . .	567
23.8.1	Analytic continuation of buoyancy surfaces . . . . .	567
23.8.2	The dual relation between height and buoyancy . . . . .	570
23.8.3	Exact expression for APE . . . . .	572
23.8.4	Approximate expression for APE . . . . .	573
23.8.5	Comments . . . . .	575
23.9	Exercises . . . . .	575

## 23.1 The oceanic Boussinesq approximation

For the ocean, density deviates no more than a few percent relative to the volume mean density. Although small, ocean density deviations act over large distances and are crucial for driving large-scale circulations. Such *thermohaline circulations* derive their driving force from variations

in temperature and salinity that affect density and, in turn, modify the pressure. A key reason that small density changes can be so pivotal is that the density variations are multiplied by the relatively large gravitational acceleration when computing pressure. The oceanic Boussinesq approximation provides a systematic means to ignore small density deviations where it is safe to do so dynamically, while retaining density variations where they are critical such as when multiplied by gravity. In brief, the oceanic Boussinesq approximation makes use of (a slightly modified) compressible thermodynamics plus an incompressible kinematics. The use of compressible thermodynamics allows for thermohaline processes to modify density and thus pressure, while the incompressible kinematics removes sound waves and renders the volume of a fluid element materially invariant in the fluid interior.

### 23.1.1 Isolating the dynamically active pressure field

Pressure in a vertically stratified fluid can be decomposed into a static background hydrostatic pressure plus a deviation from the background pressure. We made use of this decomposition in Section 22.2.4 when developing the scaling for the hydrostatic approximation. The decomposition holds even when the fluid is non-hydrostatic. We consider the background pressure to be a function just of depth and as such it is determined by a static and horizontally homogeneous background density field. We are motivated to introduce this decomposition given that the background hydrostatic pressure field (again, it is just a function of depth) is dynamically inactive (we show this below). It is thus convenient to remove it from the dynamical equations. This decomposition is exact and motivated by the desire to isolate the dynamically active part of the equations of motion.

To achieve the pressure decomposition, start by decomposing density according to

$$\rho(\mathbf{x}, t) = \rho_0(z) + \rho'(\mathbf{x}, t) \quad (23.1)$$

where the deviation density is much smaller than the reference density

$$\rho' \ll \rho_0. \quad (23.2)$$

The following formulation for the momentum equation holds for the general case of  $\rho_0(z)$ . However, we note in Section 23.1.2 that setting  $\rho_0(z) = \rho_0$  is motivated for studies of potential vorticity in Boussinesq fluids. Indeed, a space-time constant reference density is generally synonymous with the oceanic Boussinesq approximation.<sup>2</sup>

The corresponding decomposition of pressure is given by the sum of a static and depth dependent background pressure,  $p_0(z)$ , and a deviation pressure,  $p'(\mathbf{x}, t)$ ,

$$p(\mathbf{x}, t) = p_0(z) + p'(\mathbf{x}, t). \quad (23.3)$$

The background pressure is assumed to be in hydrostatic balance with the reference density

$$\frac{dp_0}{dz} = -\rho_0 g, \quad (23.4)$$

with  $p_0$  and  $\rho_0$  both static. We offer the following points to clarify the decomposition of pressure in equation (23.3).

- Assuming the background pressure,  $p_0(z)$ , to be hydrostatic does *not* imply that the full pressure,  $p(\mathbf{x}, t)$ , is also hydrostatic. Rather, the decomposition merely serves to remove

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<sup>2</sup>Exercise 23.3 offers a modest means to generalize this assumption.

that portion of the pressure field that plays no role in establishing motion (we see this property below). So this decomposition holds whether the full pressure is approximately hydrostatic or fully non-hydrostatic.

- Furthermore, if  $p(\mathbf{x}, t)$  is in an approximate hydrostatic balance (Section 22.2), the decomposition (23.3) does *not* remove all of the hydrostatic pressure from  $p(\mathbf{x}, t)$ . Rather,  $p'(\mathbf{x}, t)$  is generally nonzero whether  $p(\mathbf{x}, t)$  is in an approximate hydrostatic balance or fully non-hydrostatic.

With the above density and pressure decompositions, the momentum equation

$$\rho \left[ \frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} \right] = -\nabla p - \hat{\mathbf{z}} g \rho \quad (23.5)$$

takes the equivalent form

$$(\rho_0 + \rho') \left[ \frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} \right] = -\nabla p' - g \rho' \hat{\mathbf{z}} - \left[ \frac{dp_0}{dz} + \rho_0 g \right] \hat{\mathbf{z}} \quad (23.6a)$$

$$= -\nabla p' - g \rho' \hat{\mathbf{z}}, \quad (23.6b)$$

where we used the hydrostatic balance (23.4) for the second equality. We thus see that the background hydrostatic pressure,  $p_0(z)$ , leads to no motion since it drops out from the momentum equation. Hence, it is a “do nothing” portion of the pressure field. The pressure force is thus determined solely by the gradient of  $p'$ , which serves as the dynamically relevant portion of the pressure field.

### 23.1.2 Boussinesq momentum equation

To develop the Boussinesq momentum equation, divide the momentum equation (23.6b) by the density,  $\rho = \rho_0 + \rho'$ , and write the pressure and gravity terms as

$$\frac{\nabla p' + g \rho' \hat{\mathbf{z}}}{\rho_0 + \rho'} = \frac{\nabla p' + g \rho' \hat{\mathbf{z}}}{\rho_0 + \rho'} \left[ \frac{\rho_0 - \rho'}{\rho_0 - \rho'} \right] = \frac{\nabla p' + g \rho' \hat{\mathbf{z}}}{\rho_0^2 - (\rho')^2} (\rho_0 - \rho') \approx \frac{\nabla p' + g \rho' \hat{\mathbf{z}}}{\rho_0}, \quad (23.7)$$

where the final approximation results from dropping all terms that are second order in deviation quantities. This approximation then leads to the Boussinesq momentum equation

$$\frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\frac{1}{\rho_0} \nabla p' + b \hat{\mathbf{z}}, \quad (23.8)$$

where we introduced the globally referenced *Archimedean buoyancy* (Chapter 24) as defined relative to the constant background density

$$b = -\frac{g \rho'}{\rho_0} = -\frac{g (\rho - \rho_0)}{\rho_0}. \quad (23.9)$$

Hence, the globally referenced Archimedean buoyancy is positive when the *in situ* density is less than the reference density so that  $\rho' = \rho - \rho_0 < 0$ . That is,  $b > 0$  when the fluid element is lighter (more buoyant) than the background reference density. Buoyancy is the product of the gravitational acceleration, which is a relatively large term, and the small number  $\rho'/\rho_0$ . Their product is generally not small so that it generally cannot be neglected from the momentum equation.

In the special case of a space-time constant reference density,  $\rho_0(z) = \rho_0$ , it is convenient to introduce the shorthand for the deviation pressure normalized by the reference density

$$\varphi = \frac{p'}{\rho_0} = \frac{p - p_0(z)}{\rho_0}. \quad (23.10)$$

In this case the Boussinesq momentum equation takes the form

$$\frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla\varphi + b\hat{\mathbf{z}}. \quad (23.11)$$

### 23.1.3 A vorticity motivation to set $\rho_0$ constant

We now anticipate a later discussion of vorticity and potential vorticity to motivate setting  $\rho_0(z)$  to a constant. This paragraph is not critical for the remainder of this chapter, but worth returning to after studying vorticity. For that purpose, we note that the form of the pressure gradient acceleration found in equation (23.11) is particularly useful given that the curl of the right hand side eliminates pressure from the vorticity equation (Section 35.8.1). In contrast, for the more general form with  $\rho_0(z)$  in equation (23.8), the Boussinesq baroclinicity vector (equation (35.112)) has a contribution from both pressure and buoyancy (we derive equation (23.12) in Exercise 35.2)

$$\mathbf{B} = \nabla \left[ b - \frac{p'}{\rho_0^2} \frac{d\rho_0}{dz} \right] \times \hat{\mathbf{z}}. \quad (23.12)$$

The additional pressure contribution complicates the development of potential vorticity whereby we wish to have  $\mathbf{B} \cdot \nabla b = 0$  (see Section 36.5.1). We are thus motivated to use a space-time constant reference density so that  $d\rho_0/dz = 0$ . Following this motivation, we generally assume  $\rho_0$  is a constant in this book. Even so, in Exercise 23.3 we discuss a middle ground by defining a slightly more general buoyancy field while retaining a constant  $\rho_0$ .

### 23.1.4 Mass continuity

When decomposing density according to equation (23.1), the mass continuity equation

$$\frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{v}, \quad (23.13)$$

takes the form

$$\frac{D\rho'}{Dt} = -(\rho_0 + \rho') (\nabla_z \cdot \mathbf{u} + \partial_z w). \quad (23.14)$$

For many geophysical flows, the material time derivative on the left hand side is much smaller than either of the two terms appearing on the right hand side. To help formalize this observation it is useful to introduce a time scale for the various terms in this equation

$$\left| \frac{1}{\rho} \frac{D\rho'}{Dt} \right| \sim \frac{1}{T_\rho} \quad |\partial_x u| \sim T_u^{-1} \quad |\partial_y v| \sim T_v^{-1} \quad |\partial_z w| \sim T_w^{-1}. \quad (23.15)$$

Quite often we find flows in which the time scales associated with the spatial deformations of the flow, in the direction of the flow, are much smaller than time scales for the material changes in density, whereby

$$T_u^{-1}, T_v^{-1}, T_w^{-1} \gg T_\rho^{-1}. \quad (23.16)$$

In this case the only way for the mass balance equation (23.14) to hold is for the three terms contributing to the divergence to balance one another

$$\partial_x u + \partial_y v + \partial_z w \approx 0. \quad (23.17)$$

Taking this balance to the limit motivates setting the velocity field for a Boussinesq fluid to be non-divergent

$$\nabla \cdot \mathbf{v} = 0. \quad (23.18)$$

Note that for stratified flows we generally find the horizontal divergence of the horizontal velocity balancing the vertical convergence of the vertical velocity. For a Boussinesq fluid this balance is exact

$$\nabla_z \cdot \mathbf{u} = -\partial_z w. \quad (23.19)$$

### 23.1.5 Dependence on reference density

How does the solution compare when considering two distinct reference densities, say  $\rho_0 \neq \rho_1$ ? To answer this question, write the inviscid Boussinesq velocity equation in the form

$$(\partial_t + \mathbf{v}_0 \cdot \nabla) \mathbf{v}_0 + 2\boldsymbol{\Omega} \times \mathbf{v}_0 = -\nabla \varphi_0 + b_0 \hat{\mathbf{z}} \quad (23.20a)$$

$$(\partial_t + \mathbf{v}_1 \cdot \nabla) \mathbf{v}_1 + 2\boldsymbol{\Omega} \times \mathbf{v}_1 = -\nabla \varphi_1 + b_1 \hat{\mathbf{z}}. \quad (23.20b)$$

Consider an initial condition in which

$$\rho_0 \mathbf{v}_0 = \rho_1 \mathbf{v}_1, \quad (23.21)$$

and with pressure and buoyancy initialized so that

$$\rho_0 (-\nabla \varphi_0 + b_0 \hat{\mathbf{z}}) = \rho_1 (-\nabla \varphi_1 + b_1 \hat{\mathbf{z}}) = -\nabla p - g \rho \hat{\mathbf{z}}. \quad (23.22)$$

Hence, the difference between equations (23.20a) and (23.20b) takes the form

$$\partial_t (\rho_0 \mathbf{v}_0 - \rho_1 \mathbf{v}_1) = -(\rho_0 \mathbf{v}_0 \cdot \nabla) \mathbf{v}_0 + (\rho_1 \mathbf{v}_1 \cdot \nabla) \mathbf{v}_1 \quad (23.23a)$$

$$= -[(\rho_1 - \rho_0)/\rho_0] (\mathbf{v}_1 \cdot \nabla) \mathbf{v}_1. \quad (23.23b)$$

The difference in reference densities allows for the nonlinear self-advection to evolve the difference  $\rho_0 \mathbf{v}_0 - \rho_1 \mathbf{v}_1$ . This property of the Boussinesq equations must be kept in mind if comparing numerical solutions using distinct reference densities. Namely, an oceanic Boussinesq fluid is dependent on the reference density through the nonlinear advection term.

### 23.1.6 Version I of the Boussinesq equations

The first form of the oceanic Boussinesq equations emphasizes the role of buoyancy computed relative to a reference state of constant density,  $\rho = \rho_0$ . This form facilitates a focus on that portion of the pressure field giving rise to internal or baroclinic pressure gradients; i.e., those pressure gradients that generate motion independent of free surface undulations. The oceanic

Boussinesq equations thus take the form

$$\frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla\varphi + b\hat{z} + \mathbf{F} \quad \text{velocity equation} \quad (23.24a)$$

$$\nabla \cdot \mathbf{v} = 0 \quad \text{continuity equation} \quad (23.24b)$$

$$\frac{Db}{Dt} = \dot{b} \quad \text{buoyancy equation} \quad (23.24c)$$

$$b = -\frac{g\rho'}{\rho_0} = -\frac{g(\rho - \rho_0)}{\rho_0} \quad \text{buoyancy defined} \quad (23.24d)$$

$$\varphi = \frac{p'}{\rho_0} = \frac{p - p_0(z)}{\rho_0} \quad \text{dynamic pressure defined} \quad (23.24e)$$

$$\rho = \rho_0(1 - \alpha\Theta + \beta S) \quad \text{linear equation of state} \quad (23.24f)$$

$$\frac{dp_0}{dz} = -\rho_0 g \quad \text{background hydrostatic pressure.} \quad (23.24g)$$

We offer the following comments on these equations.

- MATERIAL EVOLUTION OF BUOYANCY: The term  $\dot{b}$  on the right hand side of the buoyancy equation (23.24c) is a placeholder for any process leading to a material change in buoyancy. We discuss some explicit examples of  $\dot{b} \neq 0$  in Section 23.5.1.
- EQUATION OF STATE: The equation of state, (23.24f), is written as a linear function of salinity and Conservative Temperature, with the thermal expansion coefficient,  $\alpha$ , and haline contraction coefficient,  $\beta$ , assumed constant. This form of the equation of state eliminates processes such as cabbeling and thermobaricity (see Section 49.3). These processes are important for certain features of the ocean, thus prompting the more general equation set in Section 23.1.7. However, for many studies the linear equation of state is sufficient, and we will at times make use of it, as well as the further simplified form with zero haline contraction,  $\beta = 0$ .
- HYDROSTATIC APPROXIMATION: Most numerical models of the large-scale ocean circulation are hydrostatic. Making the hydrostatic approximation in the velocity equation (23.24a) leads to the split into a horizontal velocity equation plus a vertical hydrostatic balance

$$\frac{D\mathbf{u}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla_z\varphi + \mathbf{F}^h \quad \text{horizontal velocity equation} \quad (23.25a)$$

$$\frac{\partial\varphi}{\partial z} = b \quad \text{hydrostatic balance,} \quad (23.25b)$$

where  $\nabla_z$  is the horizontal gradient operator and  $\mathbf{F}^h$  is the horizontal frictional acceleration.

### 23.1.7 Version II of the oceanic Boussinesq equations

The non-hydrostatic Boussinesq equations (23.24a)-(23.24g) are suited for many purposes in this book. However, we find the following form more convenient when examining the equations used in a realistic non-hydrostatic Boussinesq ocean model, with such models solving prognostic equations for salinity and Conservative Temperature rather than for buoyancy. We are thus motivated to

consider the equations in the form

$$\frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -(1/\rho_0) (\nabla p + \rho \nabla \Phi) + \mathbf{F} \quad \text{velocity equation} \quad (23.26a)$$

$$\nabla \cdot \mathbf{v} = 0 \quad \text{continuity equation} \quad (23.26b)$$

$$\frac{DS}{Dt} = \dot{S} \quad \text{salinity equation} \quad (23.26c)$$

$$\frac{D\Theta}{Dt} = \dot{\Theta} \quad \text{Conservative Temperature equation} \quad (23.26d)$$

$$\rho = \rho(S, \Theta, \Phi) \quad \text{equation of state.} \quad (23.26e)$$

We make the following comments concerning these equations.

- **GEOPOTENTIAL:** The geopotential is here considered to be a function of space and time, as relevant when studying the role of atmospheric tidal forcing or changes to the mass distribution of the planet (see Chapter 28)

$$\Phi = \Phi(\mathbf{x}, t). \quad (23.27)$$

- **EQUATION OF STATE:** The equation of state is a function of salinity, Conservative Temperature, and geopotential, thus allowing for processes such as cabelling and thermobaricity (see Section 49.3). Even so, the pressure dependence in the equation of state is computed as per a homogeneous and resting hydrostatic fluid

$$\rho(S, \Theta, \Phi) = \rho(S, \Theta, p = -\rho_0 \Phi). \quad (23.28)$$

In Section 23.7 we see why it is appropriate to take this functional form rather than the more general form discussed in Section 24.3, in which density is a function of the full *in situ* pressure rather than the geopotential:  $\rho = \rho(S, \Theta, p)$ .

- **HYDROSTATIC APPROXIMATION:** As for version I of the oceanic Boussinesq equations, we here list the equations when making the hydrostatic approximation in the vertical momentum equation, in which case the velocity equation (23.26a) splits into a horizontal velocity equation and hydrostatic balance

$$\frac{D\mathbf{u}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -(1/\rho_0) (\nabla_z p + \rho \nabla_z \Phi) + \mathbf{F}^h \quad \text{horizontal velocity equation} \quad (23.29a)$$

$$\frac{\partial p}{\partial z} = -g \rho \quad \text{hydrostatic balance.} \quad (23.29b)$$

### 23.1.8 Summary points

We close this section by summarizing a number of conceptual points characterizing the oceanic Boussinesq fluid. It is useful to return to this list to help avoid common conceptual confusions.

#### Divergent and non-divergent velocity components

The velocity that results from the Boussinesq momentum equation (i.e., the prognostic Boussinesq velocity) is non-divergent. This is the velocity used for transport as per the material time derivative operator. Additionally, there is a divergent velocity component,  $\mathbf{v}^d$ , that balances the

material evolution of density

$$\frac{1}{\rho'} \frac{D\rho'}{Dt} = -\nabla \cdot \mathbf{v}^d \neq 0. \quad (23.30)$$

The divergent velocity is not used for any of the Boussinesq dynamical equations. Nonetheless,  $\mathbf{v}^d \neq 0$ , as its divergence balances the material evolution of density according to equation (23.30). Consequently, there are acoustic waves (Section 17.5) in an oceanic Boussinesq fluid.

#### *Concerning density evolution and thermohaline circulation*

The use of a non-divergent velocity for the Boussinesq equations does not mean that the material time evolution of  $\rho$  vanishes. Instead, the scaling in Section 23.1.4 focuses just on the mass continuity equation. We must additionally acknowledge that as temperature and salinity evolve, so too does *in situ* density as determined through the equation of state. Indeed, equation (23.30) provides one expression for this evolution. Changes to density translate into changes in pressure, which in turn drive the large-scale *thermohaline circulation*.

The thermodynamic equation for Conservative Temperature or potential temperature is needed to determine density. There are various forms for the relation between temperature and density that depend on thermodynamic assumptions. We discuss the flavors for density in Section 24.3. For purposes of realistic ocean modeling, an accurate expression for density is critical, whereas for idealized modeling it is common to assume density equals to a constant times the temperature.

#### *Buoyancy*

We note the rather trivial point that there is identically zero buoyancy,  $b = -g(\rho - \rho_0)/\rho_0$ , in a fully homogeneous fluid where density is constant everywhere. Hence, for an exactly incompressible fluid, where density is a fixed and uniform constant, there are no buoyancy forces. Such fluids serve many purposes, as exemplified by studies of a single layer of shallow water fluid in Part V of this book. However, buoyancy forces are of primary importance for many other purposes in geophysical fluid mechanics. The oceanic Boussinesq approximation accounts for buoyancy forces, and the changes arising from processes such as heating and freshening, while making use of the more convenient kinematics of an incompressible flow. We have far more to say concerning buoyancy in Chapter 24.

#### *Distinction from traditional Boussinesq*

The oceanic Boussinesq approximation is more general than the Boussinesq approximation considered in other areas of fluid mechanics (e.g., [Chandrasekhar, 1961](#)). In particular, the traditional Boussinesq approximation typically assumes a linear equation of state. However, as we saw in Section 23.1.7, the oceanic Boussinesq approximation does not generally assume a linear equation of state, with a nonlinear equation of state essential for realistic ocean circulation studies.

#### *Mass and weight of a Boussinesq fluid element*

The oceanic Boussinesq fluid element conserves its volume, with this property forming the basis for Boussinesq kinematics. In turn, we measure the mass of an oceanic Boussinesq fluid element by multiplying its volume times the constant reference density,  $\rho_0$ . However, whenever there is a gravitational acceleration multiplying density we retain the full *in situ* density to measure the weight of the fluid element. So in summary, the mass and weight for an oceanic Boussinesq fluid

element are given by

$$\text{mass of Boussinesq fluid element} = \rho_0 \delta V \quad (23.31\text{a})$$

$$\text{weight of Boussinesq fluid element} = g \rho \delta V. \quad (23.31\text{b})$$

This convention enables a realistic calculation of the hydrostatic pressure (Section 23.2.6) and the gravitational potential energy (Sections 23.6 and 23.7), both of which require the *in situ* density, while maintaining the convenience of incompressible flow kinematics.

### *Connection to anelastic atmosphere*

The atmosphere is far more compressible than the ocean, so that density variations cannot be neglected and the divergent nature of the velocity is important. However, there are some cases in which an atmospheric analog to the Boussinesq approximation can be useful. The analog is known as the *anelastic approximation* and it is mathematically isomorphic to the oceanic Boussinesq approximation. Section 2.5 of [Vallis \(2017\)](#) discusses the atmospheric anelastic approximation.

### 23.1.9 Further study

Section 2.4 of [Vallis \(2017\)](#) offers more details to show that density variations are small within the ocean. Further discussion of the oceanic Boussinesq approximation also can be found in Section 9.3 of [Griffies and Adcroft \(2008\)](#). This video from SciencePrimer provides a concise summary of ocean circulation arising from differences in density created by both thermal and haline (salinity) processes.

## 23.2 Scaling for the hydrostatic approximation

Section 22.2 provided the rudiments of a scale analysis justifying the hydrostatic approximation for large-scale ocean and atmospheric flow. However, in that discussion we noted the need to remove a dynamically inactive hydrostatic pressure before addressing the question of whether the dynamically active pressure field is approximately hydrostatic. That decomposition of pressure was performed in Section 23.1.1 as part of deriving the Boussinesq equations. We thus here return to the question of hydrostatic scaling within the context of the perfect non-rotating Boussinesq fluid equations.

### 23.2.1 Stratified non-rotating Boussinesq equations

The stratified non-rotating perfect Boussinesq equations are

$$\frac{Du}{Dt} = -\nabla_z \varphi \quad \text{and} \quad \frac{Dw}{Dt} = -\frac{\partial \varphi}{\partial z} + b \quad \text{and} \quad \nabla \cdot \mathbf{v} = 0 \quad \text{and} \quad \frac{Db}{Dt} = 0. \quad (23.32)$$

To help isolate the dynamically important portion of pressure, we proceed much like in Section 23.1.1 whereby buoyancy is written

$$b = b'(x, y, z, t) + \tilde{b}(z). \quad (23.33)$$

The static buoyancy  $\tilde{b}(z)$  encompasses a background stratification that is in hydrostatic balance with its corresponding portion of the pressure field

$$\frac{d\tilde{\varphi}}{dz} = \tilde{b}(z). \quad (23.34)$$

The Boussinesq equations thus take the form

$$\frac{Du}{Dt} = -\nabla_z \varphi' \quad \text{and} \quad \frac{Dw}{Dt} = -\frac{\partial \varphi'}{\partial z} + b' \quad \text{and} \quad \nabla \cdot \mathbf{v} = 0 \quad \text{and} \quad \frac{Db'}{Dt} = -w N^2, \quad (23.35)$$

where

$$N^2 = \frac{db}{dz} \quad (23.36)$$

is the squared buoyancy frequency from the background vertical stratification. The decomposition into a background stratification helps to isolate the dynamical portion of the horizontal pressure gradient by removing a static depth dependent background. It also allows us to consider the dynamically interesting, but simpler, case in which the background stratification dominates those perturbations around it.

### 23.2.2 Non-dimensionalization

Now introduce the dimensional scales (in uppercase) and corresponding non-dimensional quantities (with hats)

$$(x, y) = L(\hat{x}, \hat{y}) \quad z = H\hat{z} \quad \mathbf{u} = U\hat{\mathbf{u}} \quad w = W\hat{w} \quad (23.37)$$

$$t = T\hat{t} \quad \varphi' = \Phi\hat{\varphi}' \quad b' = B\hat{b}' \quad N^2 = \bar{N}^2\hat{N}^2, \quad (23.38)$$

which yields the equations of motion

$$\frac{U}{T} \frac{\partial \hat{u}}{\partial \hat{t}} + \frac{U^2}{L} \hat{u} \frac{\partial \hat{u}}{\partial \hat{x}} + \frac{U^2}{L} \hat{v} \frac{\partial \hat{u}}{\partial \hat{y}} + \frac{UW}{H} \hat{w} \frac{\partial \hat{u}}{\partial \hat{z}} = -\frac{\Phi}{L} \frac{\partial \hat{\varphi}'}{\partial \hat{x}} \quad (23.39a)$$

$$\frac{U}{T} \frac{\partial \hat{v}}{\partial \hat{t}} + \frac{U^2}{L} \hat{u} \frac{\partial \hat{v}}{\partial \hat{x}} + \frac{U^2}{L} \hat{v} \frac{\partial \hat{v}}{\partial \hat{y}} + \frac{UW}{H} \hat{w} \frac{\partial \hat{v}}{\partial \hat{z}} = -\frac{\Phi}{L} \frac{\partial \hat{\varphi}'}{\partial \hat{y}} \quad (23.39b)$$

$$\frac{W}{T} \frac{\partial \hat{w}}{\partial \hat{t}} + \frac{UW}{L} \hat{u} \frac{\partial \hat{w}}{\partial \hat{x}} + \frac{UW}{L} \hat{v} \frac{\partial \hat{w}}{\partial \hat{y}} + \frac{WW}{H} \hat{w} \frac{\partial \hat{w}}{\partial \hat{z}} = -\frac{\Phi}{H} \frac{\partial \hat{\varphi}'}{\partial \hat{z}} + B\hat{b}' \quad (23.39c)$$

$$\frac{B}{T} \frac{\partial \hat{b}'}{\partial \hat{t}} + \frac{UB}{L} \hat{u} \frac{\partial \hat{b}'}{\partial \hat{x}} + \frac{UB}{L} \hat{v} \frac{\partial \hat{b}'}{\partial \hat{y}} + \frac{WB}{H} \hat{w} \frac{\partial \hat{b}'}{\partial \hat{z}} = -W\bar{N}^2 \hat{w}\hat{N}^2 \quad (23.39d)$$

$$\frac{U}{L} \frac{\partial \hat{u}}{\partial \hat{x}} + \frac{U}{L} \frac{\partial \hat{v}}{\partial \hat{y}} + \frac{W}{H} \frac{\partial \hat{w}}{\partial \hat{z}} = 0. \quad (23.39e)$$

### 23.2.3 Specifying scales

We now impose the following choices based on the flow regimes of interest.

- TIME SCALE: Assume that the time scale is determined by the horizontal velocity and the horizontal length scale

$$T = L/U. \quad (23.40)$$

- VERTICAL VELOCITY: It is common to assume the vertical velocity scales according to the continuity equation

$$\nabla_z \cdot \mathbf{u} + \frac{\partial w}{\partial z} = 0 \implies W = U \frac{H}{L} \equiv U\alpha_{\text{aspect}}, \quad (23.41)$$

where the final equality introduced the vertical to horizontal aspect ratio,  $\alpha_{\text{aspect}}$ . However, vertical stratification acts to suppress vertical motion so that we introduce a non-dimensional

number  $\epsilon$  so that

$$w = W \hat{w} = \epsilon \left[ \frac{HU}{L} \right] \hat{w}. \quad (23.42)$$

In Section 23.2.4 we motivate choosing  $\epsilon$  to be the squared Froude number.

- PRESSURE: Scale the pressure according to the non-rotating balance of the material time change in horizontal velocity and the horizontal pressure gradient

$$\frac{U}{T} + \frac{UU}{L} = \frac{\Phi}{L} \implies \Phi = U^2. \quad (23.43)$$

Note that for rotating flows in near geostrophic balance, we will see how pressure scales with the Coriolis acceleration as in Section 39.2.

- BUOYANCY: Scale buoyancy according to the hydrostatic balance

$$B = \frac{\Phi}{H} = \frac{U^2}{H}. \quad (23.44)$$

With these choices, the equations of motion (23.39a)-(23.39e) take on form

$$\frac{D\hat{\mathbf{u}}}{Dt} = -\hat{\nabla}\hat{\varphi}' \quad (23.45)$$

$$\epsilon \alpha_{\text{aspect}}^2 \frac{D\hat{w}}{Dt} = -\frac{\partial \hat{\varphi}'}{\partial \hat{z}} + \hat{b}' \quad (23.46)$$

$$\left[ \frac{U^2}{N^2 H^2} \right] \frac{\hat{D}\hat{b}'}{Dt} + \epsilon \hat{N}^2 \hat{w} = 0 \quad (23.47)$$

$$\hat{\nabla} \cdot \hat{\mathbf{u}} + \epsilon \frac{\partial \hat{w}}{\partial \hat{z}} = 0 \quad (23.48)$$

where we introduced the non-dimensional material time derivative

$$\frac{D}{Dt} = \frac{\partial}{\partial \hat{t}} + \hat{\mathbf{u}} \cdot \hat{\nabla}_z + \epsilon \hat{w} \frac{\partial}{\partial \hat{z}}. \quad (23.49)$$

### 23.2.4 The role of the Froude number

At this point we make a choice for the parameter  $\epsilon$ , noting that there are many choices that one could consider. For our interests it is suitable to set  $\epsilon$  equal to the squared *Froude number*

$$\epsilon = \text{Fr}^2 = \frac{U^2}{N^2 H^2}. \quad (23.50)$$

The Froude number measures the relative strength of vertical shears of the horizontal velocity,  $U/H$ , versus the buoyancy stratification,  $N$ . Alternatively, it measures the ratio of the horizontal speed for a fluid particle,  $U$ , to an internal gravity wave speed,  $NH$ . Large Froude numbers indicate large fluid particle speeds relative to wave speeds, with  $\text{Fr} > 1$  a common indicator of hydraulic instability (see Exercise 30.2 for a shallow water example). In contrast, a relatively strong stratification ( $N^2$  large) corresponds to a small Froude number and to flow that is stabilized by vertical stratification. Note that the squared Froude number is the inverse of the *Richardson number*

$$\text{Ri} = \text{Fr}^{-2} = \frac{\overline{N}^2 H^2}{U^2}. \quad (23.51)$$

It is a matter of taste whether one works with  $\text{Fr}$  or  $\text{Ri}$ .

The choice (23.50) leads to the vertical velocity scale

$$W = \text{Fr}^2 \left[ \frac{HU}{L} \right]. \quad (23.52)$$

For  $\text{Fr} < 1$ , which is the case for stratified fluids, this result means that stratification reduces the scale for the vertical velocity. The corresponding non-dimensional Boussinesq equations take the form

$$\frac{D\hat{u}}{Dt} = -\hat{\nabla}_z \hat{\varphi}' \quad (23.53)$$

$$\text{Fr}^2 \alpha_{\text{aspect}}^2 \frac{D\hat{w}}{Dt} = -\frac{\partial \hat{\varphi}'}{\partial \hat{z}} + \hat{b}' \quad (23.54)$$

$$\frac{D\hat{b}'}{Dt} + \hat{N}^2 \hat{w} = 0 \quad (23.55)$$

$$\hat{\nabla} \cdot \hat{\mathbf{u}} + \text{Fr}^2 \frac{\partial \hat{w}}{\partial \hat{z}} = 0. \quad (23.56)$$

The condition for hydrostatic balance in a stratified fluid thus takes the form

$$\text{Fr}^2 \alpha_{\text{aspect}}^2 \ll 1. \quad (23.57)$$

This result supports our initial suspicion that stratification suppresses vertical motion, thus reducing the vertical acceleration terms that break hydrostatic balance. That is, hydrostatic balance is more readily achieved for a stratified flow than for an unstratified flow. Note also that the horizontal divergence of the horizontal flow is reduced by the presence of stratification, which thus leads to a nearly horizontally non-divergent flow

$$\left| \hat{\nabla} \cdot \hat{\mathbf{u}} \right| = \left| \text{Fr}^2 \frac{\partial \hat{w}}{\partial \hat{z}} \right| \ll \left| \frac{\partial \hat{w}}{\partial \hat{z}} \right|. \quad (23.58)$$

Finally, this scaling reveals how the hydrostatic approximation becomes less accurate when  $\text{Fr}^2 \alpha_{\text{aspect}}^2 \sim 1$ , which occurs when stratification is weak and/or the aspect ratio large.

### 23.2.5 Horizontal hydrostatic pressure gradient

In Section 23.2.5 we studied the horizontal pressure gradient between two columns of constant density for a hydrostatic fluid. In that example, the two columns were assumed to have equal mass and the fluid non-Boussinesq. Here, we reconsider that example for a Boussinesq fluid. The expression for the hydrostatic pressure at a point within the fluid takes on the same form as that for a compressible fluid (Section 22.2.1)

$$p_h(x, y, z, t) = p_a(x, y, t) + g \int_z^\eta \rho(x, y, z', t) dz', \quad (23.59)$$

and the horizontal pressure gradient is thus given by

$$\nabla_z p_h = \nabla_z p_a + g \rho(\eta) \nabla_z \eta + g \int_z^\eta \nabla_z \rho dz'. \quad (23.60)$$

For many studies with Boussinesq fluids we are interested in the horizontal pressure gradients in the presence of a rigid lid ocean surface whereby  $\eta = 0$ . In this case we compute the *internal pressure gradient*

$$\nabla_z p_h = g \int_z^0 \nabla_z \rho dz' \quad \text{rigid lid ocean.} \quad (23.61)$$

Hence, the internal horizontal pressure gradient at a vertical position  $z$  equals to the horizontal density gradient vertically integrated above that point. For example, if density increases poleward, then so too does the internal hydrostatic pressure.

### 23.2.6 Evolution of hydrostatic pressure

In Section 22.2.2 we developed the Eulerian evolution equation for hydrostatic pressure in a mass conserving non-Boussinesq fluid. Here we discuss the evolution in a Boussinesq fluid, starting with the expression (22.14) for hydrostatic pressure at a point within the ocean

$$p(x, y, z, t) = p_a(x, y, t) + g \int_z^\eta \rho(x, y, z', t) dz', \quad (23.62)$$

and then taking the Eulerian time tendency

$$\partial_t p = \partial_t p_a + g \rho(\eta) \partial_t \eta + \int_z^\eta \partial_t \rho(x, y, z', t) dz'. \quad (23.63)$$

These expressions hold for both the Boussinesq and non-Boussinesq fluids. However, it is only for the mass conserving non-Boussinesq fluid that we can use mass continuity (14.6) to set  $\partial_t \rho = -\nabla \cdot (\mathbf{v} \rho)$ . Use of Leibniz's rule then reveals that the hydrostatic pressure evolves due to the convergence of mass onto the fluid column above that point (see Section 22.2.2 for the derivation). This result is expected since the hydrostatic pressure at a point is the weight per area of fluid above that point.

For a Boussinesq fluid, the volume conserving kinematics means that we cannot replace  $\partial_t \rho$  with  $-\nabla \cdot (\mathbf{v} \rho)$ . Correspondingly, the weight of a fluid column can change merely through *in situ* density changes, so that the weight can change even if the matter content remains fixed; e.g., through heating. We expose details by noting that the energetic consistency ideas from Section 23.7 mean that the *in situ* density in an oceanic Boussinesq fluid has the functional dependence,  $\rho(S, \Theta, \Phi)$ , with  $\Phi$  the geopotential. Hence, the Eulerian time derivative of density is given by

$$\partial_t \rho = (\partial \rho / \partial S) \partial_t S + (\partial \Theta / \partial t) \partial_t \Theta + (\partial \rho / \partial \Phi) \partial_t \Phi. \quad (23.64)$$

With a simple geopotential,  $\Phi = gz$ , we have  $\partial_t \Phi = 0$  since the Eulerian time derivative is computed at fixed  $(x, y, z)$ . This result leads to the time changes in the hydrostatic pressure for a Boussinesq fluid

$$\partial_t p = \partial_t p_a + g \rho(\eta) \partial_t \eta + \int_z^\eta [(\partial \rho / \partial S) \partial_t S + (\partial \Theta / \partial t) \partial_t \Theta] dz'. \quad (23.65)$$

This equation reveals the direct dependence of the hydrostatic pressure on changes in  $S$  and  $\Theta$ . Hence, heating and freshening, which alter the *in situ* density, directly alter the hydrostatic pressure in a Boussinesq fluid by altering the fluid's weight per area. This result contrasts to the mass conserving non-Boussinesq fluid, whose weight per area changes only through changes to its mass per area.

## 23.3 How pressure enforces non-divergent flow

We return now to the case of a non-hydrostatic fluid and consider the Boussinesq velocity equation (23.26a) written in the form

$$\rho_0 (\partial_t + \mathbf{v} \cdot \nabla) \mathbf{v} + f \mathbf{z} \times \rho_0 \mathbf{v} = -\nabla p - \rho g \hat{\mathbf{z}} + \rho_0 \mathbf{F}. \quad (23.66)$$

The non-divergence constraint on the velocity,  $\nabla \cdot \mathbf{v} = 0$ , must be maintained at each point in the fluid and at each time instance. How is that constraint maintained? As we show in this section, pressure is the force that enforces non-divergence of the velocity. Furthermore, pressure is determined through solving an elliptic boundary value problem. As we discussed in Section 3.5, elliptic partial differential equations transfer information instantaneously. Physically, this situation corresponds to the transition from a compressible fluid, in which pressure signals propagate via acoustic waves (Section 17.5), to an incompressible flow, in which pressure adjusts instantaneously just as if the acoustic waves travel at infinite speed. The oceanic Boussinesq fluid sits between the compressible and incompressible fluid. That is, the Boussinesq prognostic velocity is non-divergent, and so it does not support acoustic waves, whereas the full velocity is divergent (Section 23.1.8), and this divergent portion supports, in principle, acoustic waves.

### 23.3.1 Poisson equation for pressure

To derive the pressure equation, we expose Cartesian tensor labels on the momentum equation (23.66) to yield

$$\partial_t v_m + v_n \partial_n v_m + f \epsilon_{mnp} \delta_{3n} v_p = -\partial_m p / \rho_0 - \delta_{3m} g \rho / \rho_0 + F_m. \quad (23.67)$$

We eliminate the time derivative by taking the divergence through contracting with the operator  $\partial_m$ , thus leading to

$$-\nabla^2 p / \rho_0 = \partial_m (v_n \partial_n v_m + f \epsilon_{m3p} v_p + \delta_{3m} g \rho / \rho_0 - F_m), \quad (23.68)$$

where the Laplacian operator is

$$\nabla^2 = \partial_m \partial_m \quad (23.69)$$

and the non-divergence constraint eliminated the time derivative

$$\partial_m \partial_t v_m = \partial_t \partial_m v_m = 0. \quad (23.70)$$

Equation (23.68) can be written as the Poisson equation

$$-\nabla^2 p = \rho_0 \nabla \cdot \mathbf{G}, \quad (23.71)$$

with the vector  $\mathbf{G}$  given by

$$G_m = v_n \partial_n v_m + f \epsilon_{m3p} v_p + \delta_{3m} g \rho / \rho_0 - F_m \quad (23.72a)$$

$$\mathbf{G} = (\mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \mathbf{v} + g (\rho / \rho_0) \hat{\mathbf{z}} - \mathbf{F}. \quad (23.72b)$$

As when studying Green's functions in Chapter 4, it is useful to maintain the minus sign on the left hand side of equation (23.71) so that a positive divergence ( $\nabla \cdot \mathbf{G} > 0$ ) represents a positive source for  $p$ . Equivalently, for a wavelike pressure perturbation we have

$$-\nabla^2 p \propto p, \quad (23.73)$$

so that a positive source,  $-\nabla^2 p = \rho_0 \nabla \cdot \mathbf{G} > 0$ , leads to a local positive pressure anomaly, and conversely for a negative source. Finally, we can integrate the pressure equation (23.71) over the domain and use the divergence theorem to render the Neumann boundary condition

$$-\hat{\mathbf{n}} \cdot \nabla p = \rho_0 \hat{\mathbf{n}} \cdot \mathbf{G}. \quad (23.74)$$

where  $\hat{\mathbf{n}}$  is the outward normal at the domain boundary.

### 23.3.2 Characterizing the pressure sources

There are four sources for the pressure field via the right hand side of the Poisson equation (23.71), and linearity of the Poisson equation allows us to separately study the sources. We here summarize the basics of these sources, borrowing from the treatment given in Section 33.4 for the kinematically simpler non-divergent barotropic fluid. As we will see, three of the pressure sources contribute to non-hydrostatic pressures and one to hydrostatic pressure. Note that these pressure sources are diagnostically related to pressure perturbations. That is, the sources are *associated* with the pressure perturbations rather than *causing* the perturbations. Such is part of the nuance of pressure in a non-divergent flow.

#### Divergence of self-advection

The first source is given by the divergence of self-advection, which can be written

$$\nabla \cdot \mathbf{G}_{\text{self-advect}} = \partial_n(v_m \partial_m v_n) = (\partial_n v_m)(\partial_m v_n) + v_m(\partial_n \partial_m v_n) = (\partial_n v_m)(\partial_m v_n), \quad (23.75)$$

where we set

$$v_m \partial_n \partial_m v_n = v_m \partial_m \partial_n v_n = 0 \quad (23.76)$$

since  $\partial_n v_n = 0$  follows from the non-divergent nature of the flow. Furthermore, introducing the rate of strain tensor (equation (13.33a)) and rotation tensor (equation (13.33b)), renders

$$2 \mathbb{S}_{mn} \mathbb{S}_{mn} = (\partial_m v_n)(\partial_m v_n) + (\partial_m v_n)(\partial_n v_m) \quad (23.77)$$

$$2 \mathbb{A}_{mn} \mathbb{A}_{mn} = (\partial_m v_n)(\partial_m v_n) - (\partial_m v_n)(\partial_n v_m), \quad (23.78)$$

so that

$$\nabla \cdot \mathbf{G}_{\text{self-advect}} = (\partial_n v_m)(\partial_m v_n) = \underbrace{\mathbb{S}_{mn} \mathbb{S}_{mn}}_{\text{splat}} - \underbrace{\mathbb{A}_{mn} \mathbb{A}_{mn}}_{\text{spin}}. \quad (23.79)$$

In this equation,  $\mathbb{S}_{mn}$  are components to the rate of strain tensor and  $\mathbb{A}_{mn}$  are components to the rotation tensor. The vorticity or spin source provides a negative source to  $-\nabla^2 p$ . In contrast, the contribution from strain, sometimes referred to as *splat*, provides a positive source.<sup>3</sup> As detailed in Sections 33.4.3, 33.4.4, and 33.4.5 for non-divergent barotropic flow, we can understand the presence of a negative pressure source from vortical (spinning) motion due to the need for pressure to counteract the centrifugal acceleration associated with curved fluid motion. Likewise, the positive pressure source from straining motion counteracts the convergent acceleration induced by the strains.

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<sup>3</sup>The splat source is so-named since it is large when a fluid element is squashed in a manner increasing fluid strains, akin to how strains appear when a fluid impacts or “splats” against a solid obstacle.

*Divergence of the Coriolis acceleration*

The divergence of the Coriolis acceleration introduces a pressure source given by

$$-\nabla \cdot \nabla p_{\text{coriolis}} = \nabla \cdot \mathbf{G}_{\text{coriolis}} = \nabla \cdot (f \hat{\mathbf{z}} \times \mathbf{v}) = \beta u - f \zeta, \quad (23.80)$$

where  $\zeta = \partial_x v - \partial_y u$  is the vertical component to the relative vorticity, and  $\beta = \partial_y f$  is the planetary vorticity gradient. As an example, consider two-dimensional flow oriented cyclonically around a point as for geostrophic flow around a low pressure center. The cyclonic flow feels an associated centrifugal acceleration directed “outward”. To maintain a non-divergent two-dimensional flow requires an oppositely directed inward pressure force. Hence, such rotating flow induces a low pressure source as a means to counteract the centrifugal acceleration

$$-\nabla \cdot \nabla p_{\text{coriolis}} < 0. \quad (23.81)$$

See section 33.4.6 for more discussion of this source as found in the non-divergent barotropic fluid.

*Divergence of the gravitational force per volume*

The divergence of the gravitational force per volume is given by

$$-\nabla \cdot \nabla p_{\text{gravity}} = \rho_0 \nabla \cdot \mathbf{G}_{\text{gravity}} = \nabla \cdot (g \rho \hat{\mathbf{z}}) = g \partial_z \rho, \quad (23.82)$$

with this pressure source absent in the depth-independent barotropic fluid of Section 33.4. The associated pressure gradient is that arising from the local hydrostatic component of the pressure field in which

$$\nabla \cdot (-\nabla p_{\text{gravity}} + g \rho \hat{\mathbf{z}}) = 0. \quad (23.83)$$

In regions where density decreases upward,  $\partial_z \rho < 0$ , a compressible fluid element that conserves its mass will expand when moving upward into less dense fluid. For a non-divergent flow that conserves the volume of fluid elements, there must be a counteracting force from pressure to halt the expansion of a fluid element. This counteracting force arises from the hydrostatic component to the pressure field that acts inward to squeeze the fluid element, with this pressure force originating from the negative pressure source,  $-\nabla^2 p_{\text{gravity}} = g \partial_z \rho < 0$ .

*Divergence of the friction vector*

The third source arises from the divergence of friction,

$$-\nabla \cdot \nabla p_{\text{friction}} = \rho_0 \nabla \cdot \mathbf{G}_{\text{friction}} = -\rho_0 \nabla \cdot \mathbf{F}. \quad (23.84)$$

With interior fluid friction arising from a nonzero rate of strain (Section 18.7), we expect this pressure source to be most important in regions of large strains. Indeed, for an incompressible flow feeling only molecular viscosity, the friction operator is given by

$$\mathbf{F} = \nu \nabla^2 \mathbf{v}, \quad (23.85)$$

where  $\nu > 0$  is a constant molecular viscosity. In this case  $\nabla \cdot \mathbf{F} = 0$ , so that viscous friction does not contribute a pressure source. More general cases are considered in applications where the molecular viscosity is replaced by a flow dependent eddy viscosity so that  $\nabla \cdot \mathbf{F} \neq 0$ . For the case of a converging frictional acceleration,  $\nabla \cdot \mathbf{F} < 0$ , friction then leads to a positive pressure source to counteract the friction to thus maintain a non-divergent flow.

### 23.3.3 Comments and further study

The gravitational source contributes a local hydrostatic component to the pressure field, whereas the other three sources contribute non-hydrostatic pressure sources. In many applications, such as general circulation modeling of the ocean and atmosphere, the fluid is assumed to be approximately hydrostatic. In this case vertical motion is diagnosed rather than prognosed, and the non-hydrostatic component of pressure is never needed to evolve the fluid motion. Even so, vertical derivatives in the non-hydrostatic pressure provide the vertical force needed for vertical accelerations. We have more to say on vertical motion in Section 24.7.

*Markowski and Richardson (2010)* provide lucid discussions of pressure forces acting in geophysical fluids. In particular their Section 2.5 provided inspiration for much of the current section.

## 23.4 Tracer budgets in Eulerian regions

We are commonly interested in the tracer budget for a fluid region, and we examined a variety of regions in Section 15.3 for a compressible fluid. Here, we expose issues that arise for tracer budgets in a Boussinesq fluid, whereby the flow is non-divergent. We specialize to the study of an Eulerian region,  $\mathcal{R}$ , and emphasize how the non-divergent flow constrains how the advective tracer transport affects changes to the volume integrated tracer content.

### 23.4.1 Formulating the budget equation

Consider a tracer concentration,  $C$ , and compute its net content over an Eulerian region,  $\mathcal{R}$

$$\rho_0 \int_{\mathcal{R}} C \, dV = \rho_0 V \langle C \rangle, \quad (23.86)$$

where  $C$  satisfies the tracer equation

$$\frac{\partial(\rho_0 C)}{\partial t} + \nabla \cdot (\rho_0 C \mathbf{v} + \mathbf{J}) = 0, \quad (23.87)$$

and

$$\langle C \rangle = \frac{\int_{\mathcal{R}} C \, dV}{\int_{\mathcal{R}} dV} = \frac{1}{V} \int_{\mathcal{R}} C \, dV \quad (23.88)$$

is the volume averaged tracer concentration within the region with fixed volume,  $V = \int_{\mathcal{R}} dV$ . Following from the discussion of tracer budgets in Section 15.3, we have

$$\rho_0 \frac{d(V \langle C \rangle)}{dt} = \rho_0 V \frac{d\langle C \rangle}{dt} \quad (23.89a)$$

$$= \rho_0 \frac{d}{dt} \int_{\mathcal{R}} C \, dV \quad (23.89b)$$

$$= \int_{\mathcal{R}} \frac{\partial(\rho_0 C)}{\partial t} \, dV \quad (23.89c)$$

$$= - \int_{\mathcal{R}} \nabla \cdot (\rho_0 C \mathbf{v} + \mathbf{J}) \, dV \quad (23.89d)$$

$$= - \oint_{\partial\mathcal{R}} (\rho_0 C \mathbf{v} + \mathbf{J}) \cdot \hat{\mathbf{n}} \, d\mathcal{S}, \quad (23.89e)$$

where we used the divergence theorem on the final equality with  $\partial\mathcal{R}$  the boundary of  $\mathcal{R}$  and the outward normal  $\hat{\mathbf{n}}$ . Changes in the total tracer contained within the region arise from the

convergence of boundary fluxes due to the non-advection flux,  $\mathbf{J}$ , plus convergence of the advective tracer flux,  $\rho_0 C \mathbf{v}$ . Since the region volume is constant in time, changes in the total tracer content directly affect the volume averaged tracer concentration,  $\langle C \rangle$ .

At any point along the boundary, the tracer content is modified if there is a non-advection flux,  $\mathbf{J}$ , directed across the boundary. There is no *a priori* constraint on  $\mathbf{J}$ , with local properties determining its sign and magnitude. In contrast, contributions from the boundary advective flux are constrained due to the non-divergent nature of the Boussinesq velocity, which we discuss next.

### 23.4.2 Interpreting advective tracer contributions

As seen by equation (23.89e), any advective flux,  $\rho_0 \mathbf{v} C$ , that is directed into the region adds tracer to the region, whereas a flux directed outward reduces the region's tracer content. However, because the velocity is non-divergent, the tracer contained within the region is unaffected if we modify the advective tracer flux along the boundary by adding a number than is constant over the region  $\mathcal{R}$ . We see this property for any closed Eulerian region by writing<sup>4</sup>

$$0 = \int_{\mathcal{R}} \nabla \cdot \mathbf{v} dV = \oint_{\partial\mathcal{R}} \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (23.90)$$

Hence, the velocity is, at each time instance, constrained so that the non-divergent flow cannot lead to the accumulation of fluid within any closed and static region. Correspondingly, the amount of fluid entering  $\mathcal{R}$  exactly and instantaneously balances the amount of fluid leaving  $\mathcal{R}$ . We can thus add any spatial constant,  $k$ , to the advective flux without affecting the net tracer content change

$$\oint_{\partial\mathcal{R}} (C + k) \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S} = \oint_{\partial\mathcal{R}} C \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S} + k \oint_{\partial\mathcal{R}} \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S} = \oint_{\partial\mathcal{R}} C \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (23.91)$$

Boundary advection occurring with  $C = k$  has no affect on the net tracer within a region since an equal amount of fluid enters as leaves.

To help interpret the role of advective fluxes on integrated tracer content, we find it useful to set the arbitrary spatial constant to  $k = -\langle C \rangle$ . In this manner, the advective contribution to the tracer budget takes the form

$$V \left[ \frac{d\langle C \rangle}{dt} \right]_{\text{advective}} = - \oint_{\partial\mathcal{R}} C \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S} = - \oint_{\partial\mathcal{R}} (C - \langle C \rangle) \mathbf{v} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (23.92)$$

Hence, advective transport through the region boundary changes the region integrated  $C$ , and thus the volume mean  $\langle C \rangle$ , only if the boundary transport occurs with  $C$  values that differ from the region average,  $\langle C \rangle$ .

### 23.4.3 A rectangular region example

Consider the rectangular region of Figure 23.1 that is closed along its bottom, northern, eastern, and western boundaries, yet that is open along its top boundary and southern boundary. Specify flow along the southern boundary to be northward and let it bring fluid into the region with  $C_{\text{south}} > \langle C \rangle$ , thus acting to increase  $\langle C \rangle$ . Due to the non-divergent nature of the velocity, the northward transport of fluid through the southern boundary must be precisely balanced by a vertically upward transport of fluid out of the top boundary. What does that vertical transport

<sup>4</sup>We considered property (23.90) in Exercise 16.3.

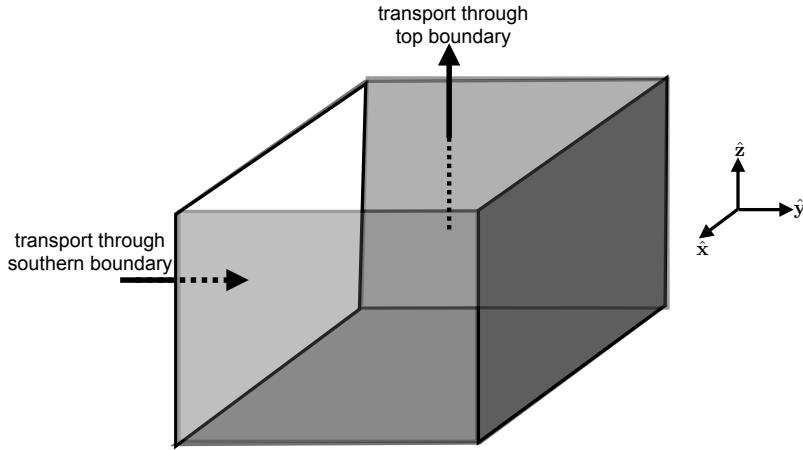


FIGURE 23.1: A rectangular ocean region for considering the tracer budget in a Boussinesq fluid. We assume the only open boundaries of the region are along the southern boundary and top boundary, with the remaining boundaries closed. Note that the top boundary can generally be within the ocean interior, and so does not need to be the top of the ocean. The non-divergent nature of the flow means that any fluid entering through the southern boundary must leave through the top boundary, and conversely. This constraint on the flow impacts on how the advective tracer transport affects changes to the volume integrated tracer within the region.

of fluid imply about changes to  $\langle C \rangle$ ? The answer depends on the tracer concentration on the top boundary.

- If  $C_{\text{top}} > \langle C \rangle$ , then the relatively high values of tracer that leave through the top boundary act to decrease the net  $C$  within the region, thus counteracting the contribution of  $C_{\text{south}} > \langle C \rangle$  that enters through the southern boundary. For the special case of equal  $C$  transports through the two boundaries, then there is no accumulation of  $C$  within the region so that  $\langle C \rangle$  remains unchanged.
- If  $C_{\text{top}} = \langle C \rangle$ , then  $\langle C \rangle$  increases due to the transport of  $C$  through the southern boundary, with no net transport across the top boundary.
- If  $C_{\text{top}} < \langle C \rangle$ , then the vertical transport of  $C_{\text{top}} < \langle C \rangle$  increases  $\langle C \rangle$  acting just like the  $C_{\text{south}} > \langle C \rangle$  fluid that enters through the southern boundary. That is, we can increase  $\langle C \rangle$  in the region by bringing fluid into the domain with  $C$  greater than  $\langle C \rangle$ , or by exporting fluid with  $C$  less than  $\langle C \rangle$ .

#### 23.4.4 Comments

Constraints introduced by the non-divergent nature of the Boussinesq fluid render subtleties to the physical interpretation of how tracer fluxes affect the budget of tracer within a region. These constraints are absent from the compressible fluid, whose flow is generally divergent. The discussion in this section was motivated by Appendix B of [Gregory \(2000\)](#), who studied heat (enthalpy) budgets within a Boussinesq ocean circulation model.

## 23.5 Subgrid scale processes and boundary conditions

The Boussinesq equations from Section 23.1 must be supplemented with boundary conditions as well as subgrid scale parameterizations. We examine boundary stresses in Chapter 18.9; study tracer subgrid scale parameterizations in Chapter 48; and detail the variety of boundary buoyancy

fluxes in Section 49.6. Even so, there is far more to each of these stories than provided in this book. In this section we summarize facets sufficient to help work through exercises at the end of this chapter. One key point to emphasize here is that for all the subgrid scale and boundary conditions, appearances of the *in situ* density are converted to the Boussinesq reference density,  $\rho_0$ .

### 23.5.1 Material evolution of buoyancy

The term  $\dot{b}$  appearing in the buoyancy equation (23.24c) is a shorthand for any process leading to a material change in buoyancy, such as a boundary flux, parameterized turbulent mixing of salinity or Conservative Temperature, or vertical motion through a vertically stratified fluid. With a linear equation of state, we can write the material evolution as the convergence of a subgrid scale buoyancy flux

$$\frac{Db}{Dt} = -\nabla \cdot \mathbf{F}^b. \quad (23.93)$$

A particularly common form for this flux is given by

$$\mathbf{F}^b = -\kappa \frac{\partial b}{\partial z} \hat{z} + \mathbf{v}^* b. \quad (23.94)$$

The first term is a downgradient vertical diffusive flux with the vertical *eddy diffusivity*,  $\kappa > 0$ , a function of the flow state so that

$$\kappa = \kappa(x, y, z, t). \quad (23.95)$$

The second term is an advective flux, where the advective velocity,  $\mathbf{v}^* = (\mathbf{u}^*, w^*)$ , is assumed to be non-divergent

$$\nabla \cdot \mathbf{v}^* = \nabla_z \cdot \mathbf{u}^* + \frac{\partial w^*}{\partial z} = 0. \quad (23.96)$$

The velocity  $\mathbf{v}^*$  is commonly termed the *eddy-induced* velocity, with a particular choice for its parameterization discussed in Exercise 23.10 and further examined in Section 48.1.

Boundary conditions for buoyancy are commonly incorporated through the boundary conditions on the subgrid scale fluxes, with the following representing one form for these boundary conditions

$$\hat{\mathbf{n}} \cdot \mathbf{F}^b = Q_{\text{surf}} \quad \text{at } z = \eta(x, y, t) \quad (23.97a)$$

$$(-\hat{\mathbf{n}}) \cdot \mathbf{F}^b = Q_{\text{bot}} \quad \text{at } z = \eta_b(x, y) \quad (23.97b)$$

$$\mathbf{v}^* \cdot \hat{\mathbf{n}} = 0 \quad \text{all boundaries,} \quad (23.97c)$$

where  $Q_{\text{surf}}$  is the surface buoyancy flux,  $Q_{\text{bott}}$  is the bottom buoyancy flux (e.g., geothermal heating), and  $\hat{\mathbf{n}}$  is the outward normal at the boundaries. Both  $Q_{\text{surf}}$  and  $Q_{\text{bot}}$  are positive upward. In Section 49.6 we detail the plethora of processes leading to boundary fluxes of buoyancy.

### 23.5.2 Mechanical forcing and dissipation

The ocean is a forced-dissipative system, with mechanical and buoyant forcing predominantly at the surface and bottom boundaries and mechanical dissipation via molecular viscosity. We must parameterize mechanical dissipation in the ocean interior arising from subgrid scale processes. A common form for this parameterization is via a vertical transfer of momentum through vertical shears that are weighted by a vertical *eddy viscosity*,  $\nu^{\text{eddy}} > 0$ , in which case the horizontal frictional acceleration in the ocean interior is written as the vertical divergence of a turbulent

stress

$$\mathbf{F}^h = \frac{1}{\rho_0} \frac{\partial \boldsymbol{\tau}}{\partial z} = \frac{\partial}{\partial z} \left[ \nu^{\text{eddy}} \frac{\partial \mathbf{u}}{\partial z} \right], \quad (23.98)$$

where  $\boldsymbol{\tau}$  is a horizontal turbulent stress whose vertical derivative contributes to the vertical transfer of horizontal momentum. The eddy viscosity can be many orders of magnitude larger than the molecular viscosity in regions of strong turbulent mixing. Whereas the molecular viscosity is a function of the fluid composition (Section 18.7), the eddy viscosity is a function of the flow state, which in turn means that

$$\nu^{\text{eddy}} = \nu^{\text{eddy}}(\mathbf{x}, t). \quad (23.99)$$

We parameterize the turbulent mechanical forcing at the ocean boundaries via a boundary stress. This stress is introduced to the governing equations through the following surface and bottom boundary conditions placed on the turbulent stress

$$\boldsymbol{\tau} = \boldsymbol{\tau}^{\text{wind}} \quad \text{at } z = \eta(x, y, t) \quad (23.100)$$

$$\boldsymbol{\tau} = \boldsymbol{\tau}^{\text{bott}} \quad \text{at } z = \eta_b(x, y) \quad (23.101)$$

At the ocean surface,  $z = \eta$ , we introduce the turbulent stress,  $\boldsymbol{\tau}^{\text{winds}}$ , arising from the transfer of momentum between the ocean and atmosphere (or the ocean and ice). In practice, the stress is computed by a boundary layer parameterization that ingests the momentum from the atmosphere and computes a stress that is transferred to the ocean through these boundary conditions. As per Newton's third law (the action/reaction law; see Section 18.9), the stress imparted to the ocean is equal and opposite the stress imparted to the atmosphere at its lower boundary. At the ocean bottom,  $z = \eta_b$ , we often parameterize subgrid scale interactions with bottom topography via a quadratic bottom drag

$$\boldsymbol{\tau}^{\text{bott}} = -C_D \mathbf{u} |\mathbf{u}|, \quad (23.102)$$

where  $C_D > 0$  is a dimensionless *drag coefficient* that is sometimes assumed to be a function of the bottom topographic roughness. This bottom stress acts to drag the ocean bottom velocity towards a state of rest. It is equal and opposite to the frictional stress transferred to the solid earth from the ocean.

## 23.6 Mechanical energy analysis part I

The volume of a fluid element in a non-divergent flow remains materially invariant even as pressure acts on the element, which means that pressure can perform no mechanical work. In turn, non-divergent flow supports no pressure work conversion between internal energy and kinetic energy. We are thus led to formulate a mechanical energy budget for the Boussinesq system that is closed for a perfect fluid with a time-independent geopotential and in the absence of boundary effects. Formulating a closed budget is the topic of this section as well as Section 23.7.

We here develop the mechanical energy budget for an unforced non-hydrostatic Boussinesq fluid assuming density is a function only of salinity and Conservative Temperature,

$$\rho = \rho(S, \Theta). \quad (23.103)$$

The more general pressure-dependent equation of state is considered in Section 23.7. Furthermore,

we choose to work with the velocity, density, and continuity equations in the form

$$\rho_0 \left[ \frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} \right] = -\nabla p - \rho \nabla \Phi \quad (23.104a)$$

$$\frac{D\rho}{Dt} = \frac{\partial \rho}{\partial S} \frac{DS}{Dt} + \frac{\partial \rho}{\partial \Theta} \frac{D\Theta}{Dt} = \dot{\rho} \quad (23.104b)$$

$$\nabla \cdot \mathbf{v} = 0. \quad (23.104c)$$

Note that the geopotential,  $\Phi$ , is generally a function of space and time,  $\Phi = \Phi(\mathbf{x}, t)$ , which is appropriate when studying astronomical tides or mass inhomogeneities creating spatial variations in the gravity field (see Chapter 28).

### 23.6.1 Kinetic energy

To obtain a kinetic energy equation, start by taking the dot product of the velocity,  $\mathbf{v}$ , and the momentum equation (23.190a) and note that the Coriolis acceleration drops out since it is orthogonal to the velocity

$$\mathbf{v} \cdot (2\boldsymbol{\Omega} \times \mathbf{v}) = 0. \quad (23.105)$$

The material time derivative takes the form

$$v_i \left[ \frac{\partial v_i}{\partial t} + v_j \frac{\partial v_i}{\partial x_j} \right] = \frac{\partial \mathcal{K}}{\partial t} + \mathbf{v} \cdot \nabla \mathcal{K} = \frac{D\mathcal{K}}{Dt}, \quad (23.106)$$

where we introduced the kinetic energy per mass

$$\mathcal{K} = \mathbf{v} \cdot \mathbf{v} / 2. \quad (23.107)$$

The equation for the Boussinesq kinetic energy per volume thus takes the form

$$\rho_0 \frac{D\mathcal{K}}{Dt} = -\mathbf{v} \cdot \nabla p - \rho \mathbf{v} \cdot \nabla \Phi \quad (23.108)$$

Alternatively, we can write this equation in the Eulerian flux-form

$$\frac{\partial(\rho_0 \mathcal{K})}{\partial t} + \nabla \cdot [\mathbf{v} (\rho_0 \mathcal{K} + p)] = -\rho \mathbf{v} \cdot \nabla \Phi, \quad (23.109)$$

where we used  $\nabla \cdot \mathbf{v} = 0$  to write  $\mathbf{v} \cdot \nabla p = \nabla \cdot (\mathbf{v} p)$ . Note that in Exercise 23.4 we show that the kinetic energy evolution derived here for the non-hydrostatic fluid holds also for the hydrostatic fluid, yet with the kinetic energy in the hydrostatic fluid determined solely by the horizontal velocity.

The term  $-\rho \mathbf{v} \cdot \nabla \Phi$  in the kinetic energy equation (23.109) is a source/sink that arises from fluid motion crossing surfaces of constant geopotential. Moving a fluid element down the geopotential gradient ( $\mathbf{v} \cdot \nabla \Phi < 0$ ) increases the kinetic energy, and conversely when the fluid moves up the geopotential gradient. We sometimes refer to this process as *buoyancy work*, particularly when considered in the context of a vertically stratified fluid. We can further exemplify this term by taking the simplified form of the geopotential,  $\Phi = g z$ , in which  $\mathbf{v} \cdot \nabla \Phi = \rho g w$ .

### 23.6.2 Gravitational and mechanical energies

A fluid element has a gravitational potential energy per mass given by the geopotential,  $\Phi$ , which has a material time derivative

$$\frac{D\Phi}{Dt} = \partial_t \Phi + \mathbf{v} \cdot \nabla \Phi. \quad (23.110)$$

The time-dependent geopotential provides an external source of potential energy to the system. Additionally, motion moving up the gradient of the geopotential ( $\mathbf{v} \cdot \nabla \Phi > 0$ ) increases the potential energy per mass, and conversely for motion down the geopotential gradient. Adding to the kinetic energy equation (23.108) renders the material evolution

$$\rho_0 \frac{D\mathcal{K}}{Dt} + \rho \frac{D\Phi}{Dt} = -\nabla \cdot (\mathbf{v} p) + \rho \partial_t \Phi. \quad (23.111)$$

Note how the buoyancy work source,  $\rho \mathbf{v} \cdot \nabla \Phi$ , dropped out from this budget. Consequently, this term provides a reversible transfer of mechanical energy between gravitational potential energy per volume and the kinetic energy per volume. We saw the same transfer in Section 21.3.3 when studying the mechanical energy budget for a compressible non-Boussinesq fluid.

Equation (23.111) has nearly the same form as that for the non-Boussinesq fluid given by equation (21.36c). However, for the Boussinesq fluid it does not lead to a flux-form Eulerian conservation law for mechanical energy, even for the perfect fluid. Operationally, the derivations diverge at this point since for the non-Boussinesq fluid we make use of the mass continuity equation (14.6) to write the material evolution of density. In contrast, material density evolution in a Boussinesq fluid is determined by material changes in temperature, salinity, and pressure.

To develop a closed Boussinesq mechanical energy budget, add  $\Phi D\rho/Dt = \Phi \dot{\rho}$  to both sides of equation (23.111) to render the material evolution for the mechanical energy *per volume*

$$\frac{D}{Dt} [\rho_0 \mathcal{K} + \rho \Phi] = -\nabla \cdot (\mathbf{v} p) + \rho \partial_t \Phi + \dot{\rho} \Phi, \quad (23.112)$$

which has the Eulerian flux-form expression

$$\partial_t (\rho_0 \mathcal{K} + \rho \Phi) + \nabla \cdot [\mathbf{v} (\rho_0 \mathcal{K} + \rho \Phi + p)] = \rho \partial_t \Phi + \dot{\rho} \Phi. \quad (23.113)$$

In the absence of boundary processes we have

$$\rho_0 \frac{d}{dt} \left[ \int m dV \right] = \int [\rho \partial_t \Phi + \dot{\rho} \Phi] dV, \quad (23.114)$$

where the Boussinesq mechanical energy per volume is given by

$$\rho_0 m = \rho_0 \mathcal{K} + \rho \Phi. \quad (23.115)$$

Recall we are assuming  $\rho = \rho(S, \Theta)$  in this section, so that

$$\dot{\rho} = (\partial \rho / \partial S) \dot{S} + (\partial \rho / \partial \Theta) \dot{\Theta}. \quad (23.116)$$

Hence, for a time-independent geopotential and in the absence of irreversible mixing then the global integrated Boussinesq mechanical energy is constant.

## 23.7 Mechanical energy analysis part II

In this section we build on the analysis from Section 23.6, here allowing density to be a function of salinity, Conservative Temperature, and pressure so that

$$\frac{D\rho}{Dt} = \frac{\partial\rho}{\partial S} \frac{DS}{Dt} + \frac{\partial\rho}{\partial\Theta} \frac{D\Theta}{Dt} + \frac{\partial\rho}{\partial p} \frac{Dp}{Dt}. \quad (23.117)$$

Density thus materially evolves even in the absence of mixing or diabatic processes since  $Dp/Dt$  is nonzero whenever flow crosses isobars. Hence, the Eulerian flux-form mechanical energy equation (23.113) now takes on the form

$$\partial_t (\rho_0 \mathcal{K} + \rho \Phi) + \nabla \cdot [\mathbf{v} \cdot (\rho_0 \mathcal{K} + \rho \Phi + p)] = \rho \partial_t \Phi + \Phi \left[ \frac{\partial\rho}{\partial S} \dot{S} + \frac{\partial\rho}{\partial\Theta} \dot{\Theta} + \frac{\partial\rho}{\partial p} \dot{p} \right]. \quad (23.118)$$

The right hand side terms provide interior sources that contribute to the evolution of mechanical energy. In the absence of mixing, diabatic processes, and with a time independent geopotential, the sources reduce to a term arising from motion across pressure surfaces. Such motion can occur for either reversible or irreversible processes. This pressure source term is rather awkward since it means the mechanical energy budget is not closed even when the flow is reversible and with time independent astronomical forces. We now follow the approach of [Young \(2010\)](#) to recover a closed Boussinesq mechanical energy budget by making use of a modified form of the gravitational potential energy.

### 23.7.1 Boussinesq dynamic enthalpy

In this section we introduce a new thermodynamic function that, in effect, provides us with an integrating factor to render a closed form to the Boussinesq mechanical energy budget. This function is referred to as the *Boussinesq dynamic enthalpy*. Before considering that function we do a brief warm-up exercise to refamiliarize ourselves with the necessary thermodynamic formalism from Chapter 20.

#### *Material time changes to a pressure integral of density*

Consider a thermodynamic potential,  $\tilde{\Pi}(S, \Theta, p | p_r)$ , defined according to the pressure integral of the *in situ* density

$$\tilde{\Pi}(S, \Theta, p | p_r) \equiv \int_{p_r}^p \rho(S, \Theta, p') dp' \implies \left[ \frac{\partial \tilde{\Pi}}{\partial p} \right]_{S, \Theta} = \rho(S, \Theta, p), \quad (23.119)$$

where  $p_r$  is an arbitrary constant reference pressure. The notation  $\tilde{\Pi}(S, \Theta, p | p_r)$  emphasizes that  $p_r$  is a specified parameter whereas  $S, \Theta, p$  are coordinates in thermodynamic configuration space (see Section 20.1.5). The integration in equation (23.119) is taken over pressure in a thermodynamic configuration space rather than an integral over a region in  $\mathbf{x}$ -space.<sup>5</sup> Accordingly, the infinitesimal

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<sup>5</sup>This is an example where the discussion in Section 21.4.2 is key, whereby we must distinguish between functions in a thermodynamic configuration space versus functions as space-time fields.

increment of  $\tilde{\Pi}$  is given by

$$\delta\tilde{\Pi} = \delta S \left[ \frac{\partial \tilde{\Pi}}{\partial S} \right]_{\Theta,p} + \delta\Theta \left[ \frac{\partial \tilde{\Pi}}{\partial \Theta} \right]_{S,p} + \delta p \left[ \frac{\partial \tilde{\Pi}}{\partial p} \right]_{S,\Theta} \quad (23.120a)$$

$$= \delta S \left[ \frac{\partial \tilde{\Pi}}{\partial S} \right]_{\Theta,p} + \delta\Theta \left[ \frac{\partial \tilde{\Pi}}{\partial \Theta} \right]_{S,p} + \rho(S, \Theta, p) \delta p. \quad (23.120b)$$

If the increment is computed following a moving fluid element then we are led to the material time derivative

$$\frac{D\tilde{\Pi}}{Dt} = \frac{DS}{Dt} \left[ \frac{\partial \tilde{\Pi}}{\partial S} \right]_{\Theta,p} + \frac{D\Theta}{Dt} \left[ \frac{\partial \tilde{\Pi}}{\partial \Theta} \right]_{S,p} + \rho(S, \Theta, p) \frac{Dp}{Dt}. \quad (23.121)$$

### Material time changes to a geopotential integral of density

Using the same formalism as above, now consider a thermodynamic potential that is a function of salinity, Conservative Temperature, and geopotential

$$\Pi(S, \Theta, \Phi | \Phi_r) \equiv \int_{\Phi_r}^{\Phi} \rho(S, \Theta, \Phi') d\Phi' \implies \left[ \frac{\partial \Pi}{\partial \Phi} \right]_{S,\Theta} = \rho(S, \Theta, \Phi), \quad (23.122)$$

where  $\Phi_r$  is an arbitrary constant reference geopotential. We offer the following three comments concerning  $\Pi$ .

- For density that is independent of the geopotential, then  $\Pi dV = (\Phi - \Phi_r) \rho dV$ , which is the gravitational potential energy relative to a reference state. We thus interpret  $\Pi(S, \Theta, \Phi)$  as a generalized gravitational potential energy per volume.
- One might consider  $\Pi$  to be the difference in hydrostatic pressure between  $\Phi$  and  $\Phi_r$  as per equation (17.40). However, the integral in equation (17.40) occurs in  $x$ -space between two geopotentials and holding the  $(x, y)$  coordinates fixed during the integration. This integration generally crosses surfaces of constant  $S$  and  $\Theta$ . In contrast, integration in equation (23.122) is taken from  $\Phi_r$  to  $\Phi$  within thermodynamic configuration space so that  $S$  and  $\Theta$  are fixed while performing the geopotential integral. In this manner, the geopotential, rather than pressure, provides a coordinate within a Boussinesq thermodynamic configuration space along with  $S$  and  $\Theta$ .
- [Young \(2010\)](#) provides motivation for calling  $\Pi$  the *Boussinesq dynamic enthalpy*.

Following the same formalism used to derive  $D\tilde{\Pi}/Dt$  in equation (23.121), we here compute the material time derivative of the Boussinesq dynamic enthalpy

$$\frac{D\Pi}{Dt} = \frac{DS}{Dt} \left[ \frac{\partial \Pi}{\partial S} \right]_{\Theta,\Phi} + \frac{D\Theta}{Dt} \left[ \frac{\partial \Pi}{\partial \Theta} \right]_{S,\Phi} + \rho(S, \Theta, \Phi) \frac{D\Phi}{Dt}. \quad (23.123)$$

We now create a mechanical energy budget in the form

$$\frac{D}{Dt} [\rho_0 \mathcal{K} + \Pi] = -[\mathbf{v} \cdot \nabla p + \rho \mathbf{v} \cdot \nabla \Phi] + \dot{S} \left[ \frac{\partial \Pi}{\partial S} \right]_{\Theta, \Phi} + \dot{\Theta} \left[ \frac{\partial \Pi}{\partial \Theta} \right]_{S, \Phi} + \rho \frac{D\Phi}{Dt} \quad (23.124a)$$

$$= -[\mathbf{v} \cdot \nabla p + \rho \mathbf{v} \cdot \nabla \Phi] + \dot{S} \left[ \frac{\partial \Pi}{\partial S} \right]_{\Theta, \Phi} + \dot{\Theta} \left[ \frac{\partial \Pi}{\partial \Theta} \right]_{S, \Phi} + \rho (\partial_t \Phi + \mathbf{v} \cdot \nabla \Phi) \quad (23.124b)$$

$$= -\mathbf{v} \cdot \nabla p + \rho \partial_t \Phi + \dot{S} \left[ \frac{\partial \Pi}{\partial S} \right]_{\Theta, \Phi} + \dot{\Theta} \left[ \frac{\partial \Pi}{\partial \Theta} \right]_{S, \Phi}, \quad (23.124c)$$

whose Eulerian flux-form expression is given by

$$\partial_t (\rho_0 \mathcal{K} + \Pi) + \nabla \cdot [\mathbf{v} \cdot (\rho_0 \mathcal{K} + \Pi + p)] = \rho \partial_t \Phi + \dot{S} \left[ \frac{\partial \Pi}{\partial S} \right]_{\Theta, \Phi} + \dot{\Theta} \left[ \frac{\partial \Pi}{\partial \Theta} \right]_{S, \Phi}. \quad (23.125)$$

We thus see that in the absence of irreversible effects, and with a time independent geopotential, we have succeeded in deriving a closed (i.e., flux-form) mechanical energy budget for a Boussinesq fluid, with

$$\rho_0 \mathcal{M} = \rho_0 \mathcal{K} + \Pi \xrightarrow{\rho = \rho(S, \Theta)} \rho_0 \mathcal{K} + \rho (\Phi - \Phi_r) \quad (23.126)$$

the appropriate Boussinesq form of the mechanical energy per volume.

### 23.7.2 Regionally integrated Boussinesq dynamic enthalpy

Following the treatment for a compressible non-Boussinesq fluid in Section 21.2.3, we here study the evolution of the gravitational potential energy integrated over a finite region,  $\mathcal{R}$ , that is open to material mass transport. Rather than working with the geopotential as done for the non-Boussinesq fluid, we here follow the discussion in Section 23.7.1 by making use of the Boussinesq dynamic enthalpy, thus ensuring a closed mechanical energy budget.

*Budget with the equation of state:  $\rho = \rho(S, \Theta, \Phi)$*

For this purpose we make use the Leibniz-Reynolds transport theorem in the form of equation (15.34) to find

$$\frac{d}{dt} \int_{\mathcal{R}} \Pi dV = \int_{\mathcal{R}} \left[ \frac{\partial \Pi}{\partial t} + \nabla \cdot (\Pi \mathbf{v}^{(b)}) \right] dV \quad (23.127a)$$

$$= \int_{\mathcal{R}} \left[ \frac{\partial \Pi}{\partial t} + \nabla \cdot (\Pi \mathbf{v}) - \nabla \cdot (\Pi \mathbf{v}) + \nabla \cdot (\Pi \mathbf{v}^{(b)}) \right] dV \quad (23.127b)$$

$$= \int_{\mathcal{R}} \left[ \frac{D\Pi}{Dt} + \Pi \nabla \cdot \mathbf{v} + \nabla \cdot [\Pi (\mathbf{v}^{(b)} - \mathbf{v})] \right] dV \quad (23.127c)$$

$$= \int_{\mathcal{R}} \left[ \frac{D\Pi}{Dt} + \nabla \cdot [\Pi (\mathbf{v}^{(b)} - \mathbf{v})] \right] dV, \quad (23.127d)$$

where  $\mathbf{v}^{(b)}$  is the velocity of a point on the boundary of the domain,  $\partial\mathcal{R}$ , and we set  $\nabla \cdot \mathbf{v} = 0$  as per a Boussinesq fluid. We expose the contributions from irreversible  $S$  and  $\Theta$  processes by making use of the identity (23.123)

$$\frac{d}{dt} \int_{\mathcal{R}} \Pi dV = \int_{\mathcal{R}} \left[ \frac{DS}{Dt} \left[ \frac{\partial \Pi}{\partial S} \right]_{\Theta, \Phi} + \frac{D\Theta}{Dt} \left[ \frac{\partial \Pi}{\partial \Theta} \right]_{S, \Phi} + \rho \frac{D\Phi}{Dt} + \nabla \cdot [\Pi (\mathbf{v}^{(b)} - \mathbf{v})] \right] dV. \quad (23.128)$$

Note that a constant can be added to the dynamic enthalpy without altering the energetics, which is seen by noting that volume conservation means that (equation (16.67))

$$\frac{d}{dt} \int_{\mathcal{R}} dV = - \int_{\mathcal{R}} \nabla \cdot (\mathbf{v} - \mathbf{v}^{(b)}) dV = - \int_{\partial \mathcal{R}} (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (23.129)$$

If the region is a vertical column of fluid with fixed horizontal cross-section, extending from the ocean surface to the ocean bottom, then there is horizontal transport across the vertical boundaries, plus vertical transport of mass across the ocean free surface. For the free surface we make use of the surface kinematic boundary condition (14.73c) to write

$$\int_{z=\eta} (\Pi/\rho) \rho (\mathbf{v}^{(\eta)} - \mathbf{v}) \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{z=\eta} (\Pi/\rho) Q_m dA. \quad (23.130)$$

In this equation,  $Q_m$  is the mass per time per horizontal area of matter crossing the ocean free surface at  $z = \eta$  where  $Q_m > 0$  for matter entering the ocean domain, and  $d\mathcal{S}$  is the area element on the free surface with  $dA$  its horizontal projection.

*Budget with the equation of state:  $\rho = \rho(S, \Theta)$*

For the special case of an equation of state independent of pressure,  $\rho = \rho(S, \Theta)$  (Section 23.6), we have  $\Pi = \rho(\Phi - \Phi_r)$  so that equation (23.128) reduces to

$$\frac{d}{dt} \int_{\mathcal{R}} \rho (\Phi - \Phi_r) dV = \int_{\mathcal{R}} \left[ (\Phi - \Phi_r) \frac{D\rho}{Dt} + \rho \frac{D\Phi}{Dt} + \nabla \cdot [\rho (\Phi - \Phi_r) (\mathbf{v}^{(b)} - \mathbf{v})] \right] dV. \quad (23.131)$$

Note that the reference geopotential,  $\Phi_r$ , drops out since the Boussinesq form of the Leibniz-Reynolds transport theorem (i.e., equation (23.127d) with  $\rho$  replacing  $\Pi$ ) leads to the identity

$$\frac{d}{dt} \int_{\mathcal{R}} \rho dV = \int_{\mathcal{R}} \left[ \frac{D\rho}{Dt} + \nabla \cdot [\rho (\mathbf{v}^{(b)} - \mathbf{v})] \right] dV. \quad (23.132)$$

This equation means that the mass for a region of Boussinesq fluid (left hand side) changes through boundary terms, as for a non-Boussinesq fluid, plus processes that lead to material time changes in  $S$  and  $\Theta$

$$\rho = \rho(S, \Theta) \implies \frac{D\rho}{Dt} = \frac{\partial \rho}{\partial S} \frac{DS}{Dt} + \frac{\partial \rho}{\partial \Theta} \frac{D\Theta}{Dt}. \quad (23.133)$$

We understand the presence of the  $\dot{S}$  and  $\dot{\Theta}$  terms by noting that irreversible processes, such as mixing, do not alter volume in a Boussinesq fluid. Hence, if irreversible processes change density then there must be a corresponding change in mass.

### 23.7.3 Vertical derivative of density

When computing the vertical derivative of density, it is important to note whether the derivative is computed holding  $(\Theta, S)$  fixed or holding  $(x, y)$  fixed. As seen here, this distinction can be confused for the oceanic Boussinesq fluid, especially when the geopotential takes the simple form  $\Phi = g z$ .

*Vertical derivative of in situ density for a non-Boussinesq fluid*

To motivate the discussion, recall the *in situ* density for a non-Boussinesq fluid is a function of the salinity,  $S$ , Conservative Temperature,  $\Theta$ , and *in situ* pressure,  $p$ ,

$$\rho = \rho(S, \Theta, p), \quad (23.134)$$

so that its spatial gradient is

$$\nabla \rho = \left[ \frac{\partial \rho}{\partial S} \right]_{\Theta, p} \nabla S + \left[ \frac{\partial \rho}{\partial \Theta} \right]_{S, p} \nabla \Theta + \left[ \frac{\partial \rho}{\partial p} \right]_{S, \Theta} \nabla p = \left[ \frac{\partial \rho}{\partial S} \right]_{\Theta, p} \nabla S + \left[ \frac{\partial \rho}{\partial \Theta} \right]_{S, p} \nabla \Theta + \frac{1}{c_s^2} \nabla p. \quad (23.135)$$

In the final step we introduced the inverse squared sound speed

$$\frac{1}{c_s^2} = \left[ \frac{\partial \rho}{\partial p} \right]_{S, \Theta}, \quad (23.136)$$

which is the partial derivative of density holding  $S$  and  $\Theta$  fixed. Equation (23.135) says that the spatial gradient of density on the left hand side is determined by the sum of three terms that arise from spatial gradients of  $(S, \Theta, p)$ , each multiplied by their respective functional derivative of the equation of state for density. The vertical component of this equation arises when measuring vertical stratification, in which case

$$\left[ \frac{\partial \rho}{\partial z} \right]_{x, y} = \left[ \frac{\partial \rho}{\partial S} \right]_{\Theta, p} \left[ \frac{\partial S}{\partial z} \right]_{x, y} + \left[ \frac{\partial \rho}{\partial \Theta} \right]_{S, p} \left[ \frac{\partial \Theta}{\partial z} \right]_{x, y} + \frac{1}{c_s^2} \left[ \frac{\partial p}{\partial z} \right]_{x, y}, \quad (23.137)$$

with  $\partial p / \partial z = -\rho g$  for a hydrostatic fluid. Note that we exposed the  $(x, y)$  labels on the left hand side partial derivative. As seen next, these extra labels are especially important for the case of an oceanic Boussinesq fluid.

*Vertical derivative of in situ density for an oceanic Boussinesq fluid*

As seen earlier in this section, the *in situ* density for an energetically consistent Boussinesq fluid has the functional dependence

$$\rho = \rho(S, \Theta, \Phi). \quad (23.138)$$

That is, the geopotential,  $\Phi$ , replaces pressure in the functional dependence, with the equation of state evaluated with a pressure  $p_{eos} = -\rho_0 \Phi$ . Hence, the spatial gradient of *in situ* density for an oceanic Boussinesq fluid is

$$\nabla \rho = \left[ \frac{\partial \rho}{\partial S} \right]_{\Theta, \Phi} \nabla S + \left[ \frac{\partial \rho}{\partial \Theta} \right]_{S, \Phi} \nabla \Theta + \left[ \frac{\partial \rho}{\partial \Phi} \right]_{S, \Theta} \nabla \Phi, \quad (23.139)$$

so that the vertical stratification is measured by

$$\left[ \frac{\partial \rho}{\partial z} \right]_{x, y} = \left[ \frac{\partial \rho}{\partial S} \right]_{\Theta, \Phi} \left[ \frac{\partial S}{\partial z} \right]_{x, y} + \left[ \frac{\partial \rho}{\partial \Theta} \right]_{S, \Phi} \left[ \frac{\partial \Theta}{\partial z} \right]_{x, y} + \left[ \frac{\partial \rho}{\partial \Phi} \right]_{S, \Theta} \left[ \frac{\partial \Phi}{\partial z} \right]_{x, y}. \quad (23.140a)$$

This relation is analogous to the non-Boussinesq expression (23.137). In particular, the inverse squared sound speed for a Boussinesq fluid is given by

$$\left[ \frac{\partial \rho}{\partial \Phi} \right]_{S, \Theta} = -\frac{\rho_0}{c_s^2}. \quad (23.141)$$

Although the prognostic flow is non-divergent for the oceanic Boussinesq fluid, the full velocity field is divergent (Section 23.1.8), thus supporting acoustic waves.

Now consider the special (and common) case of a simple geopotential,  $\Phi = g z$ , whereby the Boussinesq sound speed is given by

$$\left[ \frac{\partial \rho}{\partial z} \right]_{S,\Theta} = -\frac{\rho_0 g}{c_s^2}, \quad (23.142)$$

and the vertical stratification derivative is given by

$$\left[ \frac{\partial \rho}{\partial z} \right]_{x,y} = \left[ \frac{\partial \rho}{\partial S} \right]_{\Theta,z} \left[ \frac{\partial S}{\partial z} \right]_{x,y} + \left[ \frac{\partial \rho}{\partial \Theta} \right]_{S,z} \left[ \frac{\partial \Theta}{\partial z} \right]_{x,y} + \left[ \frac{\partial \rho}{\partial z} \right]_{S,\Theta}. \quad (23.143)$$

We here see why attachment of subscripts to the partial derivatives is essential to avoid confusion, since

$$\left[ \frac{\partial \rho}{\partial z} \right]_{x,y} \neq \left[ \frac{\partial \rho}{\partial z} \right]_{S,\Theta}. \quad (23.144)$$

The left hand side vertical derivative is computed holding the horizontal position fixed, as appropriate for computing the vertical stratification, whereas the right hand side vertical derivative is computed with  $(S, \Theta)$  fixed, as appropriate for computing the sound speed. These two derivatives are conceptually distinct, with equation (23.143) exposing the mathematical distinction.

### 23.7.4 Comments

#### *Decoupling mechanical energy from internal energy*

There are further niceties required to unravel energetics of the oceanic Boussinesq fluid, with details provided by [Young \(2010\)](#). When encountering these details for the first time one may wonder why bother since the compressible energetics discussed in Sections 21.3 and 21.5 are rather straightforward. However, the difficulty with compressible energetics arises from the internal energy. Namely, since many geophysical flows, particularly those in the ocean, have speeds that are tiny compared to molecular speeds (see Section 11.3), the mechanical energy associated with geophysical flow is tiny relative to the internal energy arising from molecular motions. So when studying the total energy budget for a compressible fluid, that energy is dominated by the internal energy. As detailed in [Young \(2010\)](#), the oceanic Boussinesq approximation allows one to focus on the Boussinesq mechanical energy arising just from the fluid flow, and it does so by decoupling mechanical energy from the internal energy.

#### *General form of the geopotential*

The treatments in [Young \(2010\)](#) and Section 2.4.3 of [Vallis \(2017\)](#) focus on the simple form of the geopotential,  $\Phi = g z$ , in which case it appears that density in an energetically consistent Boussinesq fluid can at most have the space-time dependence

$$\rho = \rho[S(\mathbf{x}, t), \Theta(\mathbf{x}, t), p = -\rho_0 g z]. \quad (23.145)$$

However, the formalism from this section allows for a general geopotential, including those that arise from astronomical tidal forcing and from mass redistributions such as near ice shelves. In these cases we retain a consistent Boussinesq energetics with density of the more general form

$$\rho = \rho[S(\mathbf{x}, t), \Theta(\mathbf{x}, t), p = -\rho_0 \Phi(\mathbf{x}, t)]. \quad (23.146)$$

### *Distinct manifestations of irreversible processes*

It is notable that the irreversible terms from  $\dot{S}$  and  $\dot{\Theta}$  that appear in the mechanical energy equations (23.113), (23.124c) and (23.125) are absent from the non-Boussinesq budget in equation (21.36c). Instead, for the non-Boussinesq fluid, the irreversible mixing processes manifest through their effects on flow convergence via the mass continuity equation

$$-\nabla \cdot \mathbf{v} = \rho^{-1} \dot{\rho}. \quad (23.147)$$

Since the Boussinesq fluid has a zero flow divergence, the role of mixing on the potential energy budget appears elsewhere within the mechanical energy budget.

## 23.8 Available potential energy (APE)

As we have seen, the gravitational potential energy per mass of a fluid element as measured relative to the  $z = 0$  geopotential is given by  $g\rho z$ . But how much of that potential energy is convertible to kinetic energy? Clearly not all of it since a state of zero potential energy means all of the fluid sits at  $z = 0$ , which is not generally possible. In Section 23.6 we noted that  $-g^{-1} b\Phi$  is the potential energy per mass relative to the constant density background state. Pursuing this idea one more step, consider a background buoyancy,  $b_{\text{ref}}(z)$ , that has a non-zero depth dependence but with no horizontal dependence. Without any horizontal buoyancy gradients there are zero horizontal internal pressure gradients so that an initially static fluid will remain static. As seen in the discussion of vorticity in Section 35.8.1, a fluid with zero baroclinicity does not generate vorticity since its pressure gradients are perpendicular to buoyancy gradients, which are vertical for a reference state with  $b = b_{\text{ref}}(z)$  (see Section 23.1.2 for the Boussinesq baroclinicity vector). These ideas motivate us to compute the potential energy relative to a depth-dependent background buoyancy profile.

Lorenz (1955) suggested that a particularly relevant background buoyancy state is that obtained by a reversible rearrangement or “sorting” of the original buoyancy to a state that has zero baroclinicity. A reversible rearrangement means there is no mixing when moving between the original state and the background state. The difference in gravitational potential energy between these two states is termed the *available potential energy* (APE), with the APE measuring the potential energy accessible for generating reversible motion. Figure 23.2 illustrates these notions. In the remainder of this section we provide further details to support this conceptual description of APE. We restrict attention to the perfect Boussinesq fluid with a linear equation of state, thus ignoring the role of mixing processes and subtleties associated with the nonlinear equation of state.

### 23.8.1 Analytic continuation of buoyancy surfaces

We use the term *outcrop* to refer to the vanishing of a buoyancy surface at the upper boundary, and *incrop* when it vanishes at the lower boundary. Figure 23.3 illustrates such surfaces. When considering a fluid in a domain with geometric boundaries, and when describing properties of the fluid according to thermodynamic coordinates such as buoyancy, we must decide how to describe these surfaces in regions where they do not exist; i.e., where they are outcropped or incropped. We follow the Lorenz convention described in Lorenz (1955), Andrews (1983), Section 4 of Young (2012), and Appendix A of Ringler et al. (2017).

This goal might appear to be pointless; i.e, if the surface does not exist in a region, then why do we need to specify any of its properties. However, the “analytic continuation” of buoyancy surfaces is very useful when developing their kinematics, with particular use for available potential

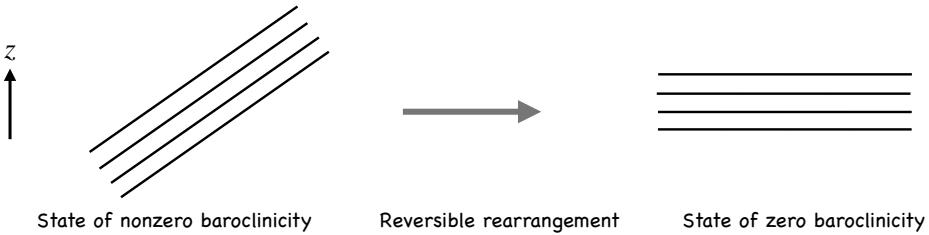


FIGURE 23.2: Isolines of constant buoyancy to illustrate the concept of available potential energy (APE) in a stably stratified Boussinesq fluid. The initial state (left panel) with non-zero baroclinicity is reversibly rearranged to have zero baroclinicity (right panel). The difference in gravitational potential energy between these two states defines the APE in the initial state. As shown in Section 23.8.3, the APE is a non-negative measure of the amount of gravitational potential energy that can, in principle, be reversibly converted to kinetic energy. Due to volume conservation and the absence of irreversible processes, the depth of a buoyancy surface in the background state shown in the right panel equals to the area average depth of the same buoyancy surface in the left panel (see Section 23.8.2).

energy in Section 23.8.3. Such concerns have further applications for studies of water mass transformation arising from boundary buoyancy fluxes (e.g., [Nurser et al. \(1999\)](#) as well as Chapter 50). Additionally, as we will see, the buoyancy frequency along these surfaces is formally infinite since the extended buoyancy surfaces are squeezed into a zero thickness layer. Doing so thus creates an infinite potential vorticity, which corresponds to the potential vorticity *delta sheets* as discussed by [Bretherton \(1966\)](#) and [Schneider et al. \(2003\)](#). In the following we limit our attention to domains with flat bottoms and vertical side-walls to minimize the niceties that arise with more general domains.

#### *Buoyancy-area mean height of a buoyancy surface*

A kinematic property that we make use of when formulating available potential energy is the area mean height of a buoyancy surface. One way to define this mean is to integrate the height over the area of the buoyancy surface and then divide by the area of the buoyancy surface

$$\overline{\eta(\mathcal{B}, t)}^{\text{buoyancy}} = \frac{\int_{\mathcal{B}} \eta(x, y, \mathcal{B}, t) d\mathcal{S}}{\int_{\mathcal{B}} d\mathcal{S}}, \quad (23.148)$$

where  $\int_{\mathcal{B}} d\mathcal{S}$  is the area integral over the  $\mathcal{B}$  buoyancy surface. There are two problems with this area mean. First, the area of a buoyancy surface is rather complicated to compute in practice. Second, the buoyancy surface area is time dependent thus making the area mean also time dependent.

#### *Domain-area mean height of a buoyancy surface*

An alternative method to compute the area mean height is to integrate over the area of the fluid domain

$$\overline{\eta(\mathcal{B})} = \frac{\int \eta(x, y, \mathcal{B}, t) dA}{\int dA}, \quad (23.149)$$

where

$$A = \int dA = \int_{\text{fluid domain}} dx dy \quad (23.150)$$

is the time-independent horizontal area of the fluid domain. However, in choosing the domain area we must specify the height of a buoyancy surface in those horizontal regions where the surface

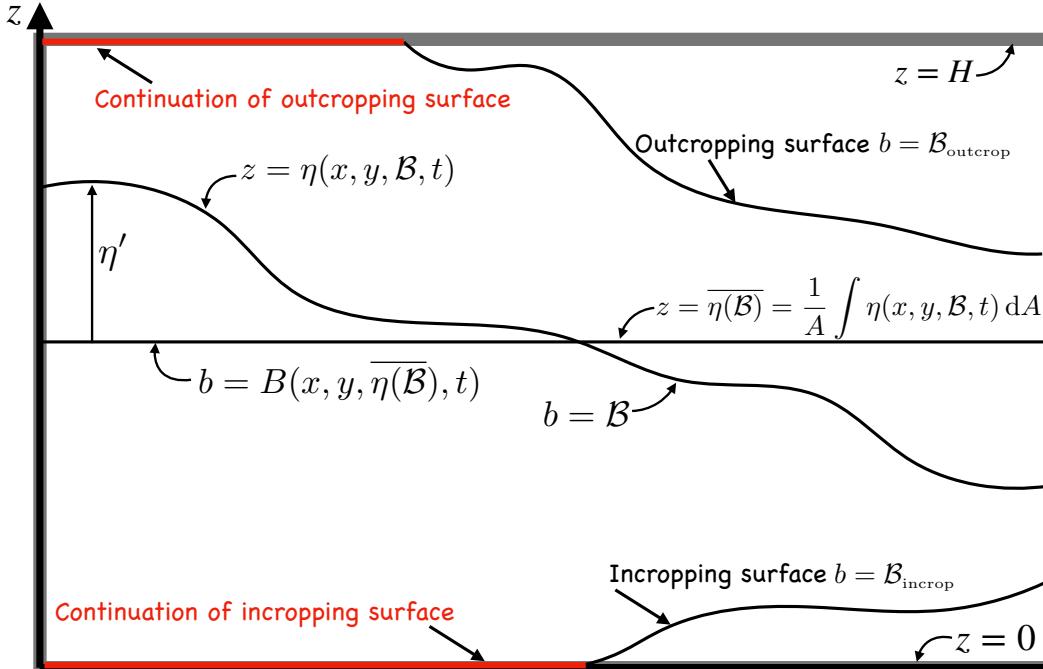


FIGURE 23.3: Geometry of buoyancy surfaces in a flat bottom box of perfect Boussinesq fluid with height  $H$  and horizontal area  $\int dA = A$ . Three representative buoyancy surfaces are shown: one that spans the full domain with  $b = \mathcal{B}$ , one that incrops at the bottom with  $b = \mathcal{B}_{\text{incrop}}$ , and one that outcrops at the surface with  $b = \mathcal{B}_{\text{outcrop}}$ . The vertical height of a buoyancy surface is  $z = \eta(x, y, \mathcal{B}, t)$ ; its area average (which is time independent; see Section 23.8.2) is  $\bar{\eta}(\mathcal{B}) = A^{-1} \int \eta(x, y, \mathcal{B}, t) dA$ ; and its corresponding anomalous height is  $\eta'(x, y, \mathcal{B}, t) = \eta(x, y, \mathcal{B}, t) - \bar{\eta}(\mathcal{B})$ . As a complement, a particular point on the  $z = \bar{\eta}(\mathcal{B})$  height surface has buoyancy  $b = B(x, y, \bar{\eta}(\mathcal{B}), t)$ , which then leads to an anomalous buoyancy  $b'(x, y, \bar{\eta}(\mathcal{B}), t) = B(x, y, \bar{\eta}(\mathcal{B}), t) - \mathcal{B}$ , where  $B(x, y, \bar{\eta}(\mathcal{B}), t) = \mathcal{B}$  (see equation (23.155)). To allow the formalism to be transparent across all buoyancy surfaces, we set  $\eta(x, y, \mathcal{B}_{\text{outcrop}}, t) = H$  in regions where the surface has outcropped, and  $\eta(x, y, \mathcal{B}_{\text{incrop}}, t) = 0$  where the surface has incropped (denoted by the red lines). As a complement, we set  $\partial z / \partial b = 1/N^2 = 0$  for regions where the surface has either incropped or outcropped, thus formally imposing an infinitely stratified extension of the incropped and outcropped surfaces across the top and bottom domain boundaries. Through this analytic continuation of the buoyancy surfaces, we are ensured that the area mean height of all buoyancy surfaces forms a monotonic sequence from 0 to  $H$ , with  $\bar{\eta}(\mathcal{B}_1) > \bar{\eta}(\mathcal{B}_2)$  if  $\mathcal{B}_1 > \mathcal{B}_2$ . When focused on a single buoyancy surface, we can reduce notational clutter by writing, for example,  $\bar{\eta}$  rather than  $\eta(\mathcal{B})$ , as well as  $b'(\bar{\eta}) = B(\bar{\eta}) - \mathcal{B}$ , and  $\eta' = \eta - \bar{\eta}$ .

does not exist; i.e., where the surface outcrops or incrops. By doing so, we see in Section 23.8.2 that the area mean height is time-independent for all buoyancy surfaces. Furthermore, this area mean height satisfies the monotonicity property

$$\bar{\eta}(\mathcal{B}_1) > \bar{\eta}(\mathcal{B}_2) \quad \text{if} \quad \mathcal{B}_1 > \mathcal{B}_2. \quad (23.151)$$

We make use of both the time-independence of the mean height and the monotonicity property when formulating the available potential energy in Section 23.8.3.

#### Analytic continuation of surface height at outcrops and incrops

So how do we specify the height in outcrop regions? Let us motivate a specification by considering a buoyancy surface that sits near the top of the domain; i.e., its buoyancy is near the domain maximum,  $b_{\max}$ . Assume this surface is not horizontal, with the surface  $b = \mathcal{B}_{\text{outcrop}}$  in Figure 23.3 an example. Furthermore, let it cover less horizontal area than the full domain area. If we horizontally integrate just over regions where the surface does not outcrop, but still normalize

by the total horizontal area of the domain, then the area mean height will be less than certain other buoyancy surfaces whose buoyancy is less and yet whose horizontal area is more. As a result we will not satisfy the monotonicity property (23.151). A way to recover monotonicity is to analytically continue the buoyancy surface along the upper boundary so that its height in the outcropped region is set to  $\eta(x_{\text{outcrop}}, y_{\text{outcrop}}, \mathcal{B}_{\text{outcrop}}, t) = H$ . Doing so then ensures that the domain-area mean height for buoyancy surfaces will approach  $H$  as their buoyancy approaches the maximum buoyancy. We provide an analogous continuation of the surface within the bottom boundary so that

$$\eta(x, y, \mathcal{B}, t) = \begin{cases} H & \text{if } (x, y) \in \text{outcrop region} \\ 0 & \text{if } (x, y) \in \text{incrop region} \\ \eta(x, y, \mathcal{B}, t) & \text{otherwise.} \end{cases} \quad (23.152)$$

These two continuations of the buoyancy surfaces ensures that the domain-area mean height of all buoyancy surfaces forms a monotonic sequence and that the sequency extends from  $0 \leq \overline{\eta(\mathcal{B})} \leq H$ .

#### *Analytic continuation of buoyancy stratification at outcrops and incrops*

What does the analytic continuation (23.152) imply for buoyancy? As described, we allow all outcropped buoyancy surfaces to continue along the surface at  $\eta = H$ . All outcropped surfaces are thus squeezed into the infinitesimal upper fluid layer with buoyancy in that layer bounded above by the domain maximum buoyancy,  $b_{\max}$ . Likewise, for the bottom of the domain we squeeze all incropped buoyancy surfaces into an infinitesimal layer bounded below by  $b_{\min}$ , the minimum buoyancy in the domain. Consequently, the upper and lower boundaries are formally capped by infinitely stratified shells in which the inverse squared buoyancy frequency vanishes.

#### 23.8.2 The dual relation between height and buoyancy

In deriving an expression for the APE in Section 23.8.3, we will find it useful to have relations between the unsorted and sorted buoyancy fields. We will also make use of the dual relation between the height of a constant buoyancy surface and the buoyancy of a constant height surface. For this purpose we examine certain kinematic properties of buoyancy surfaces in a stably stratified box of perfect Boussinesq fluid as in Figure 23.3.

##### *Volume beneath a buoyancy surface using height coordinates*

Making use of notation from Figure 23.3, the volume of fluid contained beneath an arbitrary buoyancy surface is

$$V(\mathcal{B}) = \int dA \int_0^{\eta(x,y,\mathcal{B},t)} dz = \int \eta(x, y, \mathcal{B}, t) dA = A \overline{\eta(\mathcal{B})}, \quad (23.153)$$

The following properties result from volume conservation in a perfect non-divergent flow (see Chapter 16).

- The volume of fluid beneath an arbitrary buoyancy surface is time-independent, as is the area mean height of this surface. This property allowed us to drop the time argument from  $V(\mathcal{B})$  and  $\eta(\mathcal{B})$  in equation (23.153).
- The area mean height of a buoyancy surface is identical to the height of the surface when it is reversibly rearranged to be horizontal.

To verify these properties, recall that buoyancy surfaces are material in a perfect fluid so that no fluid crosses them even as they fluctuate. It follows that the volume of fluid beneath an arbitrary buoyancy surface is time-independent. Since the horizontal area of the domain is time-independent, equation (23.153) also means that the area averaged height of the buoyancy surface is time-independent. Furthermore, any motion of a buoyancy surface in a perfect fluid is reversible, including motion that flattens the surface. Since its area mean height remains fixed, the area mean equals to the height of the surface when it is flat.

#### *Area mean buoyancy on a constant depth surface*

As a further realization of the dual relation between height and buoyancy, note that the area average buoyancy,  $b = B(x, y, z, t)$  along a constant height surface is also constant in time

$$\overline{B(z)} = A^{-1} \int B(x, y, z, t) dA = \text{time independent.} \quad (23.154)$$

This property follows since both buoyancy and volume are material constants following a fluid parcel in a perfect Boussinesq fluid. Hence, a fluid parcel carries both its buoyancy and volume unchanged so that the volume integrated buoyancy within any fluid region remains constant. Correspondingly, the area integrated buoyancy along any fixed height surface remains constant. It also follows that the area mean buoyancy at  $z = \overline{\eta(\mathcal{B})}$  is  $\mathcal{B}$

$$\overline{B[\overline{\eta(\mathcal{B})}]} = A^{-1} \int B(x, y, z = \overline{\eta(\mathcal{B})}, t) dA = \mathcal{B}. \quad (23.155)$$

#### *Volume beneath a buoyancy surface using buoyancy coordinates*

Let us return to the volume beneath a buoyancy surface, only now use buoyancy coordinates to write

$$V(\mathcal{B}) = \int dA \int_0^{\eta(x, y, \mathcal{B}, t)} dz = \int dA \int_{b(x, y, 0, t)}^{\mathcal{B}} \frac{\partial z}{\partial b} db = \int dA \int_{b(x, y, 0, t)}^{\mathcal{B}} \frac{db}{N^2} \quad (23.156)$$

where  $b(x, y, 0, t)$  is the buoyancy at the bottom of the domain and

$$N^2 = \frac{\partial b}{\partial z} \quad (23.157)$$

is the squared buoyancy frequency. As noted in Section 23.8.1 and illustrated in Figure 23.3, we analytically continue the buoyancy surfaces into the surface and bottom boundaries so that

$$N^{-2}(x, y, \mathcal{B}) = \begin{cases} = 0 & \text{if } \mathcal{B} > b(x, y, H) \text{ (surface outcrop region)} \\ = 0 & \text{if } \mathcal{B} < b(x, y, 0) \text{ (bottom incrop region)} \\ = N^{-2}(x, y, \mathcal{B}) & \text{if } b(x, y, 0) \leq \mathcal{B} \leq b(x, y, H). \end{cases} \quad (23.158)$$

In this manner we can replace the lower limit in equation (23.156) with a constant buoyancy well below any buoyancy found in the domain, which we write as  $b_{\min}$ , so that

$$V(\mathcal{B}) = \int dA \int_{b_{\min}}^{\mathcal{B}} \frac{db}{N^2} = \int_{b_{\min}}^{\mathcal{B}} db \int \frac{dA}{N^2}. \quad (23.159)$$

Being able to commute the area and buoyancy integrals proves useful in the following.

### 23.8.3 Exact expression for APE

In this section we develop an expression for the APE of the perfect stably stratified Boussinesq fluid in a box. To start, consider the gravitational potential energy of the fluid in Figure 23.3 relative to a constant density background state with  $\rho = \rho_0$

$$\mathcal{P} = - \int dA \int_0^H b z dz = -\frac{1}{2} \int dA \int_0^H b d(z^2). \quad (23.160)$$

Integration by parts leads to the equivalent expression

$$\mathcal{P} = -\frac{1}{2} \int dA \int_0^H d(b z^2) + \frac{1}{2} \int dA \int_{b(x,y,0)}^{b(x,y,H)} \eta^2(x, y, b) db \quad (23.161)$$

$$= -\frac{AH^2}{2} \overline{b(H)} + \frac{1}{2} \int dA \int_{b(x,y,0)}^{b(x,y,H)} \eta^2(x, y, b) db, \quad (23.162)$$

where  $\overline{b(H)}$  is the area averaged buoyancy at the top of the fluid domain,  $z = H$ . As discussed in Section 23.8.1, integration over the finite domain using a buoyancy coordinate leads us to set  $\overline{b(H)} = b_{\max}$ , the domain maximum buoyancy. Likewise, the second expression in equation (23.162) has its buoyancy integral range extended to  $b_{\min}$  and  $b_{\max}$ . By doing so we can swap the area and buoyancy integrals to render

$$\mathcal{P} = \frac{A}{2} \left[ -H^2 b_{\max} + \int_{b_{\min}}^{b_{\max}} \overline{\eta^2(b)} db \right], \quad (23.163)$$

where  $\overline{\eta^2(b)}$  is the area mean of the squared height of a buoyancy surface. The same calculation for the reference buoyancy,  $b_{\text{ref}}(z)$ , leads to

$$\mathcal{P}_{\text{ref}} = \frac{A}{2} \left[ -H^2 b_{\max} + \int_{b_{\min}}^{b_{\max}} \overline{\eta(b)^2} db \right], \quad (23.164)$$

where we noted that the height of a reference buoyancy surface equals to the area mean of the corresponding buoyancy surface

$$\eta(b_{\text{ref}}) = \overline{\eta}(b = b_{\text{ref}}), \quad (23.165)$$

and the reference buoyancy at the surface boundary equals to the maximum buoyancy,  $b_{\text{ref}}(H) = b_{\max}$ .

Subtracting the gravitational potential energy of the reference/background state from the potential energy of the full state renders an expression for the available potential energy

$$\mathcal{P}_{\text{APE}} = \mathcal{P} - \mathcal{P}_{\text{ref}} = \frac{A}{2} \left[ \int_{b_{\min}}^{b_{\max}} [\overline{\eta^2(b)} - \overline{\eta(b)^2}] db \right] = \int_{b_{\min}}^{b_{\max}} \overline{(\eta')^2} db \geq 0, \quad (23.166)$$

where (see Figure 23.3)

$$\eta(x, y, b, t) = \overline{\eta(b)} + \eta'(x, y, b, t). \quad (23.167)$$

The positive definite nature of the APE arises since either a positive or negative buoyancy surface undulation gives rise to motion.

Equation (23.166) is an exact expression for the APE of a perfect Boussinesq fluid in a flat bottom domain. We encounter the same expression when studying the APE in a shallow water fluid in Section 31.3.4. It is the natural expression when working in buoyancy coordinates, whereby the APE is determined by height variations of constant buoyancy surfaces.

### 23.8.4 Approximate expression for APE

When working with geopotential coordinates it is useful to obtain an approximate expression for the APE in terms of buoyancy variations on constant height surfaces. That is the subject of this subsection.

#### *Approximate version of APE in terms of buoyancy fluctuations*

To develop an approximate expression for the APE we write the height of a buoyancy surface  $\eta(\mathcal{B})$  in the form (see caption to Figure 23.3 if confused by signs)

$$\eta(\mathcal{B}) \approx \overline{\eta(\mathcal{B})} + \left[ \frac{\partial z}{\partial b} \right]_{z=\bar{\eta}} [\mathcal{B} - B(\bar{\eta})] = \bar{\eta} - \frac{b'}{N^2} \approx \bar{\eta} - \frac{b'}{N_{\text{ref}}^2}, \quad (23.168)$$

where the final step set  $N^2(x, y, \bar{\eta}) \approx N_{\text{ref}}^2(\bar{\eta})$ , which is valid to the same order as the approximation. We are thus lead to the approximate expression

$$\eta' = \eta - \bar{\eta} \approx -\frac{b'}{N_{\text{ref}}^2} \quad (23.169)$$

so that the APE is given approximately by

$$\mathcal{P}_{\text{APE}} \approx A \left[ \int_0^H \frac{\overline{(b')^2}}{2 N_{\text{ref}}^2} dz \right], \quad (23.170)$$

This approximate expression is commonly used in practical calculations of APE, particularly when making use of field measurements (e.g., [Bishop et al. \(2020\)](#)).

#### *Practical issues related to the sorted buoyancy profile*

Figure 23.4 illustrates how to obtain the sorted buoyancy profile from a discretized version of a stably stratified fluid. The buoyancy of each cell is compared to that of all other cells and vertically stacked according to the relative buoyancy. The vertical position of the sorted grid cell is determined by accumulating the volume per horizontal area of the cell, starting from the bottom and moving up.

It is notable that cells with identical buoyancy lead to regions of zero vertical stratification in the sorted buoyancy profile. Such zero stratification regions commonly arise when sorting stratified fluid layers, where the buoyancy is constant within the layers. One is thus led to perform a vertical smoothing of the sorted profile to remove such unstratified regions, particularly if using the profile to define a background buoyancy frequency as required for the approximate APE calculation given by equation (23.170).

#### *Budget for approximatae APE*

To develop a budget for the approximate form of APE, start by considering the budget for buoyancy as decomposed as

$$b(x, y, z, t) = b_{\text{ref}}(z) + b'(x, y, z, t), \quad (23.171)$$

so that the perfect fluid buoyancy equation takes on the form

$$\frac{Db}{Dt} = 0 \implies \frac{Db'}{Dt} = -w N_{\text{ref}}^2. \quad (23.172)$$

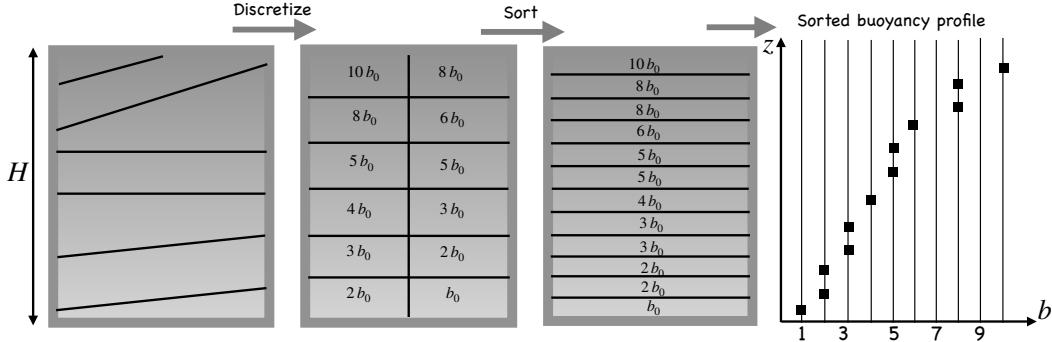


FIGURE 23.4: Illustrating how to sort buoyancy to determine the background or reference profile for computing APE. The first panel on the left shows a sample buoyancy field with black lines representing buoyancy isolines. The second panel shows a discretized version of the field, with  $b_0$  a unit of buoyancy and each cell's buoyancy an integer multiple of  $b_0$ . For simplicity we assume the horizontal area of the domain is depth independent and that each of the discrete grid cells has the same volume and horizontal area. The third panel shows the result of sorting the discrete buoyancy field, with the most buoyant fluid above the less buoyant fluid. During the sort, the cell's volume remains constant (Boussinesq fluid) and the accumulated volume per horizontal area determines the vertical position of the sorted cell. The final panel shows the sorted profile  $b_{\text{ref}}(z)$ . Note that regions of zero lateral buoyancy gradient in the unsorted buoyancy field lead to vertically unstratified regions in the sorted buoyancy.

Multiplying by  $b'$  leads to

$$\frac{D[(b')^2/2]}{Dt} = -w b' N_{\text{ref}}^2, \quad (23.173)$$

and then dividing by  $N_{\text{ref}}^2$  renders

$$\frac{\partial P_{\text{APE}}}{\partial t} + \mathbf{v} \cdot \nabla P_{\text{APE}} = -w b' \left[ 1 - \frac{b'}{2} \frac{\partial(1/N_{\text{ref}}^2)}{\partial z} \right], \quad (23.174)$$

where we defined the approximate APE per unit volume

$$P_{\text{APE}} = (1/2) [b'/N_{\text{ref}}]^2. \quad (23.175)$$

In the case of a depth-independent reference buoyancy frequency, we see that the APE per unit volume materially evolves with a source  $-w b'$ , which is analogous to the potential energy evolution where the source is  $-w b$ . Now adding equation (23.174) to the kinetic energy equation (23.109) with  $\Phi = g z$  leads to

$$\frac{\partial(\mathcal{K} + P_{\text{APE}})}{\partial t} + \mathbf{v} \cdot \nabla(\mathcal{K} + P_{\text{APE}} + p/\rho_0) = -w \left[ g - b_{\text{ref}} - \frac{(b')^2}{2} \frac{\partial(1/N_{\text{ref}}^2)}{\partial z} \right]. \quad (23.176)$$

Note that a global area average on any surface eliminates the  $w(g - b_{\text{ref}})$  term since

$$\bar{w} = A^{-1} \int w \, dA = 0, \quad (23.177)$$

which follows from  $\nabla \cdot \mathbf{v} = 0$  (see Exercise 16.4). Further simplifications arise with depth-independent  $N_{\text{ref}}$ , with the corresponding space-time spectra studied by [Bühler et al. \(2014\)](#).

### 23.8.5 Comments

Elements of this section follow from Section 3.11.1 of [Vallis \(2017\)](#). APE has remained a compelling notion throughout geophysical fluid studies. Unfortunately, for the ocean it has proven very difficult to extend its formalism beyond the perfect fluid Boussinesq system considered here. Particular difficulties arise from the nonlinear equation of state for seawater and the nontrivial ocean geometry with distinct basins and enclosed seas.



## 23.9 Exercises

### EXERCISE 23.1: SYMMETRY UNDER A TIME-DEPENDENT TRANSLATION

In this exercise we consider the Euler equation in free space (no boundaries) where we focus only on the acceleration and the pressure gradient force. That is, we ignore any body forces from gravity and rotation so that the Euler equation takes on the form

$$\rho_0 \frac{D\mathbf{v}}{Dt} = -\nabla p, \quad (23.178)$$

where we assume a Boussinesq fluid so that  $\nabla \cdot \mathbf{v} = 0$ .

Consider a shift in the reference frame used to describe the flow so that a coordinate position shifts according to

$$\mathbf{x} \rightarrow \mathbf{x} + \mathbf{c}(t), \quad (23.179)$$

where the vector  $\mathbf{c}$  is time dependent but has the same value for all points in space.

- (a) Is the shift (23.179) a Galilean transformation? Hint: recall the discussion of Galilean transformation in Section 12.6.
- (b) What happens to pressure in the new reference frame? Hint: consider the elliptic problem for pressure as discussed in Section 23.3.1.
- (c) Write the equation of motion (23.178) in this new reference frame.

### EXERCISE 23.2: STEADY PARALLEL SHEARED FLOW

Consider the non-divergent parallel sheared flow on a tangent plane

$$\mathbf{v} = \hat{\mathbf{x}} u(y). \quad (23.180)$$

That is, the steady velocity is zonal and has a meridional dependence.

- (a) Show that this flow is an exact solution to the  $\beta$ -plane inviscid Boussinesq velocity equation.
- (b) What is the corresponding pressure gradient?
- (c) Show that for an  $f$ -plane the stationary velocity can have an arbitrary orientation. Hint: it is sufficient to show that  $\mathbf{v} = \hat{\mathbf{y}} v(x)$  is a stationary solution.

### EXERCISE 23.3: A GENERALIZED BOUSSINESQ APPROXIMATION

In this exercise we derive a mild generalization to the Boussinesq approximation. This generalization facilitates a more accurate decomposition of pressure by introducing a new reference density,  $\bar{\rho}(z)$ , that is a static function of depth. The new decomposition also leads to a slightly modified buoyancy field.

The derivation starts with the usual decomposition of density using  $\rho_0$  as a space-time constant

$$\rho(\mathbf{x}, t) = \rho_0 + \rho'(\mathbf{x}, t), \quad (23.181)$$

thus leading to the Boussinesq momentum equation

$$\frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\rho_0^{-1} (\nabla p + \hat{\mathbf{z}} g \rho). \quad (23.182)$$

But rather than take the traditional decomposition of the pressure and gravitational terms, we now write

$$\nabla p + \hat{\mathbf{z}} g \rho = \nabla[p - \bar{p}(z) + \bar{p}(z)] + \hat{\mathbf{z}} g [\rho - \bar{\rho}(z) + \bar{\rho}(z)] \quad (23.183a)$$

$$= \nabla[p - \bar{p}(z)] + \hat{\mathbf{z}} g [\rho - \bar{\rho}(z)]. \quad (23.183b)$$

This step introduced the density,  $\bar{\rho}(z)$ , and the corresponding hydrostatically balanced pressure

$$\frac{d\bar{p}(z)}{dz} = -g \bar{\rho}(z). \quad (23.184)$$

- (a) Show that the pressure is decomposed as

$$p(\mathbf{x}, t) = [p(\mathbf{x}, t) - \bar{p}(z)] + \bar{p}(z) = \rho_0 \tilde{\varphi} + \bar{p}(z). \quad (23.185)$$

What is  $\tilde{\varphi}$ ?

- (b) Introduce a buoyancy

$$\tilde{b} = -\frac{g(\rho - \bar{\rho})}{\rho_0}, \quad (23.186)$$

defined relative to the depth-dependent background density,  $\bar{\rho}(z)$ , rather than the globally constant density  $\rho_0$ . Show that the momentum equation is given by

$$\frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla \tilde{\varphi} + \hat{\mathbf{z}} \tilde{b}. \quad (23.187)$$

- (c) Show that the baroclinicity vector appearing in the Boussinesq vorticity equation takes the form

$$\tilde{\mathbf{B}} = \nabla \tilde{b} \times \hat{\mathbf{z}}, \quad (23.188)$$

which is mathematically the same as with the traditional Boussinesq approximation from Section 23.1.2. We have thus succeeded in generalizing the pressure decomposition and buoyancy field, yet without corrupting the familiar Boussinesq vorticity dynamics.

#### EXERCISE 23.4: KINETIC ENERGY FOR A PERFECT HYDROSTATIC BOUSSINESQ FLUID

Consider a perfect *hydrostatic* Boussinesq fluid. Show that the kinetic energy per mass contained in the horizontal velocity,

$$\mathcal{K}_{\text{horz}} = \frac{\mathbf{u} \cdot \mathbf{u}}{2}, \quad (23.189)$$

satisfies the same equation as that for a non-hydrostatic fluid given by equation (23.108). Assume the simple form for the geopotential,  $\Phi = g z$ .

#### EXERCISE 23.5: ENERGETICS FOR A PERFECT BOUSSINESQ FLUID

In Section 23.6 we developed the energetic balances for an ideal Boussinesq fluid in a closed

domain. We here rederive the same energetics but using the the momentum, buoyancy, and continuity equations in the form that exposes buoyancy

$$\frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla\varphi + \hat{\mathbf{z}} b \quad (23.190a)$$

$$\frac{Db}{Dt} = 0 \quad (23.190b)$$

$$\nabla \cdot \mathbf{v} = 0 \quad (23.190c)$$

$$b = b(S, \Theta). \quad (23.190d)$$

Assume the simple form for the geopotential,  $\Phi = g z$ , and assume a closed and static domain (i.e., an Eulerian domain with no boundary contributions). To help physically interpret terms, remember to isolate the total divergence terms and the remainder.

- (a) Derive the material time evolution equation for the kinetic energy.
- (b) Derive the material time evolution equation for the gravitational potential energy. For this purpose it is convenient to introduce  $P^b = -g^{-1} \Phi b$  with  $\Phi = g z$ . Interpret  $P^b$ .
- (c) Derive the mechanical energy equation written in its Eulerian flux-form. Discuss.
- (d) Integrate the mechanical energy equation to derive a global domain budget for mechanical energy. Discuss.

#### EXERCISE 23.6: ENERGETICS FOR A DISSIPATIVE BOUSSINESQ FLUID

We here examine the energy budget for a Boussinesq fluid in a rotating frame under the Traditional approximation and including diabatic forcing, momentum mixing from molecular viscosity, and buoyancy mixing from molecular diffusivity. The equations for this fluid system are

$$\frac{D\mathbf{v}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{v} = -\nabla\varphi + \hat{\mathbf{z}} b + \nu \nabla^2 \mathbf{v} \quad (23.191a)$$

$$\frac{Db}{Dt} = Q^b + \kappa \nabla^2 b \quad (23.191b)$$

$$\nabla \cdot \mathbf{v} = 0. \quad (23.191c)$$

In the above,  $\nu > 0$  is the viscosity leading to irreversible mixing of velocity, and  $\kappa > 0$  is the diffusivity leading to irreversible mixing of buoyancy.

- Assume both  $\nu$  and  $\kappa$  are constant for this exercise; e.g., they are molecular values.
- Assume a linear equation of state so that buoyancy is linearly related to temperature with a constant thermal expansion coefficient (equation (23.24f) with haline contraction coefficient  $\beta = 0$ ).
- Assume the domain has static boundaries so that it has a fixed volume.
- When performing domain integrated budgets, ignore boundary terms that appear as a result of the divergence theorem. Even though boundary terms are generally important, we here are not focused on them.
- Let  $Q^b$  be a three-dimensional buoyancy source and/or boundary term; e.g., surface buoyancy fluxes, geothermal heating, interior sources. That is, we choose to isolate the boundary and source terms in  $Q^b$  so that  $\hat{\mathbf{n}} \cdot \nabla b = 0$  along all boundaries. This construct allows us to contemplate placing buoyancy sources at various places within the fluid column and determining how those sources affect the energy budget.

- Hint: Elements of this exercise are discussed in Chapter 21 of *Vallis (2017)*.
  - To help physically interpret terms, remember to isolate the total divergence terms and the remainder.
- (a) Derive the material evolution of kinetic energy per mass.
- (b) Derive the equation for domain integrated evolution of kinetic energy per mass. Make use of the identity
- $$\nabla^2 \mathbf{v} = -\nabla \times \boldsymbol{\omega} \text{ if } \nabla \cdot \mathbf{v} = 0 \quad (23.192)$$
- to express the viscosity contributions in terms of the vorticity
- $$\boldsymbol{\omega} = \nabla \times \mathbf{v}. \quad (23.193)$$
- (c) Show that the domain integrated kinetic energy per mass is reduced (dissipated) by the viscosity in the presence of a nonzero vorticity. Discuss this result.
- (d) Derive the material evolution equation for  $P^b = -g^{-1}\Phi b$  with  $\Phi = g z$ . Interpret  $P^b$ .
- (e) Derive the equation for domain integrated evolution of gravitational potential energy per mass.
- Discuss how downgradient vertical diffusion of buoyancy impacts on the domain integrated gravitational potential energy.
  - Discuss how diabatic heating impacts on the domain integrated gravitational potential energy.
- (f) Discuss the reversible conversion between kinetic and gravitational potential energy. For example, what happens to the kinetic and gravitational potential energies if a heavy fluid element moves upward?
- (g) Derive the equation for material evolution of mechanical energy per mass.
- (h) Derive the domain integrated evolution of mechanical energy per mass.
- (i) Over a closed volume (no boundary fluxes), show that the dissipation of domain integrated kinetic energy is balanced by the buoyancy source.
- (j) In a steady state (Eulerian time derivative vanishes) and absent buoyancy diffusion, show that diabatic heating from  $Q^b$  must occur at a lower level (lower gravitational geopotential) than cooling if a kinetic energy dissipating circulation is to be maintained.

**EXERCISE 23.7: KINETIC ENERGY AND THE HYDROSTATIC BOUSSINESQ EQUATIONS**

In this exercise we develop some properties of the kinetic energy for the hydrostatic Boussinesq equations listed in Section 23.1.6. We here assume the horizontal frictional acceleration is determined by vertical viscous friction in equation (23.98), and the stress boundary conditions are given by equations (23.100) and (23.102).

- (a) Derive the Eulerian flux-form expression for the kinetic energy budget.
- (b) Why does the kinetic energy only have contributions from the horizontal velocity components?

- (c) Discuss the role of vertical viscosity in transporting kinetic energy in the vertical.
- (d) Discuss the role of vertical viscosity in dissipating kinetic energy.
- (e) Discuss how wind stress and bottom drag impact the globally integrated kinetic energy.  
Assume bottom drag in the form of equation (23.102).

## EXERCISE 23.8: POTENTIAL ENERGY AND THE HYDROSTATIC BOUSSINESQ EQUATIONS

In this exercise we develop some properties of the gravitational potential energy for the hydrostatic Boussinesq equations stated in Section 23.1.6.

- (a) Derive the Eulerian flux-form budget for gravitational potential energy written as  $P^b = -g^{-1} \Phi b$  with  $\Phi = g z$ . Interpret  $P^b$ .
- (b) Discuss the role of the subgrid scale eddy-induced advection in this budget as given by equation (23.94). In particular, discuss its impact on the center of mass of the fluid.
- (c) Discuss the role of vertical diffusion in this budget as given by equation (23.94). In particular, discuss its impact on the center of mass of the fluid.
- (d) Integrate the gravitational potential energy budget over the global ocean. Discuss how the surface boundary buoyancy flux,  $Q_b$ , impacts on the global potential energy budget through impacts on the center of mass of the fluid. Ignore any bottom geothermal heating.

## EXERCISE 23.9: SQUARED BUOYANCY AND THE OCEAN MODEL EQUATIONS

In this exercise we develop some properties of the squared buoyancy for the hydrostatic Boussinesq equations stated in Section 23.1.6 using the subgrid scale buoyancy flux in equation (23.94).

- (a) Write the Eulerian flux-form budget describing the evolution of  $b^2$ , the squared buoyancy.  
Write the budget using the residual mean velocity defined by the sum

$$\mathbf{v}^\dagger = \mathbf{v} + \mathbf{v}^*. \quad (23.194)$$

Hint: start from the buoyancy equation (23.93).

- (b) Discuss the impacts from vertical diffusion on the  $b^2$  budget.

## EXERCISE 23.10: PARAMETERIZED EDDY VELOCITY AND THE OCEAN MODEL EQUATIONS

In this exercise we develop some implications of assuming a specific form for the parameterized eddy velocity for the hydrostatic Boussinesq equations stated in Section 23.1.6. Namely, we consider the specific form for the parameterized eddy-induced velocity proposed by [Gent et al. \(1995\)](#)

$$\mathbf{u}^* = -\partial_z(B \mathbf{S}) \quad (23.195a)$$

$$w^* = \nabla_z \cdot (B \mathbf{S}) \quad (23.195b)$$

$$\mathbf{S} = -\frac{\nabla_z b}{N^2} \quad (23.195c)$$

$$\mathbf{v}^* \cdot \hat{\mathbf{n}} = 0 \quad \text{at all ocean boundaries.} \quad (23.195d)$$

In this expression,  $B > 0$  is an eddy diffusivity. To ensure  $\mathbf{v}^* \cdot \hat{\mathbf{n}} = 0$  at all domain boundaries requires that  $B = 0$  along these boundaries. The horizontal vector  $\mathbf{S} = (S^{(x)}, S^{(y)}, 0)$  measures the slope of the buoyancy surfaces relative to the horizontal. We assume the ocean is stably stratified in the vertical, so that  $\partial b / \partial z = N^2 > 0$ .

- (a) Determine the vector streamfunction  $\Psi^*$  such that

$$\mathbf{v}^* = \nabla \times \Psi^*. \quad (23.196)$$

Choose the gauge with  $\hat{\mathbf{z}} \cdot \Psi^* = 0$ .

- (b) Show that

$$\int_{-H}^{\eta} \mathbf{u}^* dz = 0. \quad (23.197)$$

That is, the parameterized horizontal flow has a zero depth integral.

- (c) At any chosen meridional position  $y$ , the meridional buoyancy transport from advection (resolved plus parameterized) is computed by

$$\mathcal{B}^{(y)}(y, t) = \int_{x_1}^{x_2} dx \int_{-H}^{\eta} b(v + v^*) dz. \quad (23.198)$$

The zonal and vertical integrals are over the full zonal and vertical extent of the ocean domain. Show that the effects from  $v^*$  are to reduce the meridional gradients of buoyancy. That is, if buoyancy decreases poleward, then  $v^*$  will flux buoyancy poleward to reduce the gradient.

- (d) How does the introduction of  $\mathbf{v}^*$  to the buoyancy equation (23.24c) affect the global integrated *gravitational potential energy*? Discuss.
- (e) How does the introduction of  $\mathbf{v}^*$  to the buoyancy equation (23.24c) affect the global integrated *available potential energy*? Discuss.



# Chapter 24

## Buoyancy

A large portion of the vertical pressure force is balanced by the gravitational force, as per a hydrostatic fluid. If there is any unbalanced density-induced pressure force then a fluid element experiences a *buoyant* acceleration that causes vertical motion. More precisely, *buoyancy* is the vertical pressure force acting on a fluid element arising from density inhomogeneities. If these pressure forces are balanced by gravity, then the fluid element is said to be *neutrally buoyant*, whereas if they are unbalanced then the fluid element has a net buoyancy that causes vertical acceleration. Buoyancy is thus a packaging of the vertical forces from gravity and pressure that offers insights into the role of density inhomogeneities in creating vertical fluid motion within a gravitational field.

Our study of buoyancy starts by examining the buoyancy of a *test fluid element* where a test fluid element probes properties of the surrounding fluid environment without altering the environment.<sup>1</sup> We refer to the buoyant force acting on the test fluid element as the *Archimedean buoyancy*, since it offers the natural generalization of the more familiar buoyancy force acting, for example, to keep a ship floating. Examining the buoyancy of test fluid elements throughout a fluid then leads to the notions of gravitational stability and neutral directions.<sup>2</sup>

Most references to buoyancy in the geophysical literature refer to the Archimedean buoyancy. Even so, Archimedean buoyancy is an incomplete rendering of the forces acting in a fluid element arising from density inhomogeneities. A complete description is provided by the *effective buoyancy*, which accounts for the *static forces* creating vertical accelerations of a fluid element. That is, the effective buoyancy is defined as the vertical acceleration acting on a fluid element that remains when setting all velocity dependent accelerations to zero. The effective buoyancy has a contribution from both Archimedean buoyancy acting on a test fluid element, plus the vertical derivative of a pressure perturbation that depends only on the density field. This extra pressure force can be interpreted as the *back-reaction* on a fluid element due to the surrounding fluid environment; i.e., it accounts for the distinction between a test fluid element and a fluid element.

<sup>1</sup> As defined in Section 12.2.5, a test fluid element is directly analogous to the point test mass particles that probe properties of the gravitational field and the point test electrical charges that probe the electromagnetic field, with neither of these test particles altering the fields where they are placed.

<sup>2</sup> Archimedes was a Greek mathematician, inventor, engineer, physicist, and astronomer who lived in Syracuse, Sicily from roughly 287 B.C.E to 212 B.C.E. Hence, Archimedean buoyancy of a test fluid element builds from perhaps the most ancient of physical concepts used in modern fluid mechanics.

## CHAPTER GUIDE

This chapter builds from our study of pressure in Chapters 17, 18, and 19. We also make use of the equations for a Boussinesq fluid as derived in Chapter 23, in particular the Poisson equation satisfied by pressure in a non-divergent flow.

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24.1	Loose threads . . . . .	582
24.2	Archimedes' Principle . . . . .	583
24.2.1	Hydrostatic pressure force . . . . .	584
24.2.2	Archimedean buoyancy force . . . . .	584
24.3	Mass density and its flavors . . . . .	585
24.3.1	Equation of state for the atmosphere and ocean . . . . .	585
24.3.2	Modified temperature variables . . . . .	585
24.3.3	Infinitesimal density increments and material time changes . . . . .	586
24.3.4	Potential density . . . . .	587
24.3.5	Linear equation of state for the ocean . . . . .	588
24.3.6	Further study . . . . .	588
24.4	Archimedean buoyancy of a test fluid element . . . . .	588
24.4.1	Locally referenced Archimedean buoyancy . . . . .	588
24.4.2	Globally referenced Archimedean buoyancy . . . . .	589
24.5	Buoyancy stratification and neutral directions . . . . .	589
24.5.1	General considerations . . . . .	589
24.5.2	Comparing <i>in situ</i> densities . . . . .	590
24.5.3	Neutral directions and the neutrality condition . . . . .	591
24.5.4	Buoyancy frequency and gravitational stability . . . . .	592
24.5.5	Locally referenced potential density . . . . .	593
24.5.6	Gravitational stability of an ideal gas atmosphere . . . . .	594
24.5.7	Comments and further study . . . . .	596
24.6	Neutral helicity . . . . .	596
24.6.1	Mathematical preliminaries . . . . .	596
24.6.2	Helical nature of neutral displacements . . . . .	597
24.6.3	Comments and further study . . . . .	598
24.7	Effective buoyancy and vertical accelerations . . . . .	598
24.7.1	Vertical motion in approximately hydrostatic fluids . . . . .	598
24.7.2	Two decompositions of pressure and gravity forces . . . . .	599
24.7.3	Vertical equation of motion . . . . .	599
24.7.4	Effective buoyancy and motional vertical acceleration . . . . .	600
24.7.5	Poisson equations for the pressures and accelerations . . . . .	601
24.7.6	Thought experiments for effective buoyancy . . . . .	603
24.7.7	Comments and further study . . . . .	604
24.8	Exercises . . . . .	604

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## 24.1 Loose threads

- Provide some examples of  $b_{\text{eff}}$  fields in Section 24.7 as taken from [Tarshish et al. \(2018\)](#).
- More on the mathematics of neutral helicity in Section 24.6.

## 24.2 Archimedes' Principle

The Archimedean buoyancy acting on a massive body immersed in a static fluid is the vertical acceleration due to the gravitational acceleration of the body relative to the gravitational acceleration of the fluid displaced by the body. A body's Archimedean buoyancy is proportional to its density relative to that of the displaced fluid. Hence, there is no Archimedean buoyancy without gravity nor is there a buoyant acceleration without density differences. These statements of *Archimedes' Principle* are a direct consequence of hydrostatics.

Archimedean buoyancy has wide applications for the study of bodies immersed within fluids; e.g. mechanics of marine organisms, ships, submarines, hot air balloons. Our interests concern the buoyancy of the fluid within itself, with this buoyancy fundamentally related to the density field. To extend the notions of Archimedean buoyancy to a fluid, we introduce the conceptual construct of a *test fluid element* originally defined in Section 12.2.5. A test fluid element does not alter the environment into which it is placed, so that it is an imaginary probe that allows us to map the Archimedean buoyancy of the fluid environment without modifying environment.<sup>3</sup>

To help build toward an understanding of the Archimedean buoyancy of a test fluid element, consider an arbitrary finite region,  $\mathcal{R}$ , contained within a static fluid such as shown in Figure 24.1. The region can be occupied by a rigid solid such as a submarine, a semi-rigid region such as a fish, or something else. For our studies, we are interested in an arbitrary region of the fluid itself, such as an infinitesimal fluid element or a finite fluid volume. The mass of the region is given by the integral of the fluid density over the region

$$M_{\text{fluid}} = \int_{\mathcal{R}} \rho dV. \quad (24.1)$$

We seek an understanding of the forces acting on this region from the surrounding fluid.

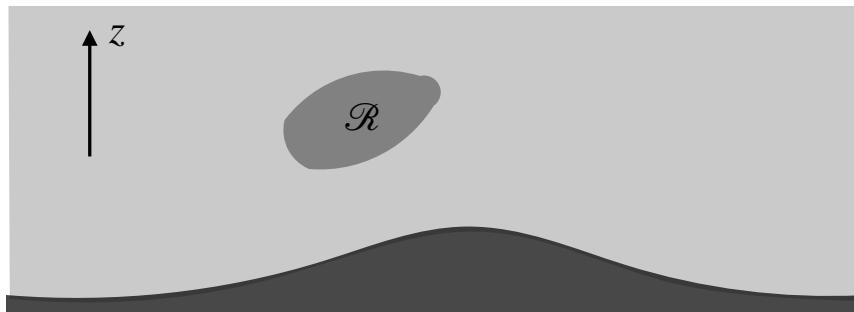


FIGURE 24.1: An arbitrary region,  $\mathcal{R}$ , contained within a fluid experiences a gravitational force acting down and a buoyant force acting up. The region considered here is arbitrary, such as a rigid solid, a swimming creature, an infinitesimal fluid element, or a finite region of the fluid. When the fluid is static, hydrostatics says that the fluid displaced by the body imparts a force equal to the weight of the displaced fluid. This result is *Archimedes' Principle*. The buoyant force acting on the body is determined by the difference in weight between the body and the displaced fluid. A positive buoyancy acts upward on a body that is less dense than the displaced fluid, and a negative buoyancy acts downward on a body that is more dense than the displaced fluid.

<sup>3</sup>We dispense with the “does not alter” assumption when considering the effective buoyancy acting on a fluid element in Section 24.7.

### 24.2.1 Hydrostatic pressure force

As discussed in Chapters 18 and 19, any surface, even an imaginary surface, within a fluid experiences a contact stress due to interactions between the fluid and the surface. For a fluid at rest in a gravitational field, the only contact stress arises from pressure. Pressure is a compressive stress, acting in the direction determined by minus the outward normal along the surface. Integrating the pressure over the closed boundary,  $\partial\mathcal{R}$ , leads to the pressure force acting on the region

$$\mathbf{F}_{\text{pressure}} = - \oint_{\partial\mathcal{R}} p \hat{\mathbf{n}} d\mathcal{S}, \quad (24.2)$$

where  $p$  is the pressure,  $\hat{\mathbf{n}}$  is the outward normal on the boundary, and  $d\mathcal{S}$  is the area element.

If the region is part of the fluid itself, then we can use Gauss's divergence theorem in the form of equation (2.67) to render the equivalent expression in terms of the volume integral of the pressure gradient

$$\mathbf{F}_{\text{pressure}} = - \int_{\mathcal{R}} \nabla p dV. \quad (24.3)$$

Furthermore, since the fluid is at rest, it is in an exact hydrostatic balance and thus only has a dependence on the vertical position within the fluid,  $p = p(z)$ . The hydrostatic pressure equals to the weight per horizontal area of fluid sitting above any point in the fluid so that its vertical derivative given by

$$\frac{dp}{dz} = -\rho g. \quad (24.4)$$

Hence, the force acting on the region is

$$\mathbf{F}_{\text{pressure}} = - \int_{\mathcal{R}} \nabla p dV = - \int_{\mathcal{R}} \hat{\mathbf{z}} (dp/dz) dV = \hat{\mathbf{z}} g \int_{\mathcal{R}} \rho dV = \hat{\mathbf{z}} g M_{\text{fluid}}, \quad (24.5)$$

where we assumed a constant gravitational acceleration over  $\mathcal{R}$ . The hydrostatic pressure acting on the region imparts a vertical upward force equal to the weight of the fluid displaced by the region. This result is a mathematical expression of *Archimedes' Principle*.

Note that there are no net horizontal forces acting over the region. The reason is that there are no horizontal pressure gradients within the fluid since, by assumption, the fluid is at rest and thus experiences no horizontal acceleration. So although the immersed body experiences horizontal compressive pressure forces, these forces balance when integrated over the body (assuming the body can withstand the forces!), thus leaving a zero net horizontal acceleration. We studied such static force balances in Section 18.4.

### 24.2.2 Archimedean buoyancy force

The vertical pressure force (24.6) acts to push the body vertically upward against gravity. Therefore, it reduces the vertical gravitational force when the body is within the fluid. We say that the massive body has a *buoyancy* imparted by the displaced fluid. If the body has a density less than the displaced fluid, then the body experiences a positive buoyancy force relative to the displaced fluid, in which case the body experiences an upward acceleration. The converse holds for a body more dense than the displaced fluid, in which case the body sinks downward. These buoyancy forces arise from pressure acting on the body. If the body is the fluid itself, then the forces arise from non-hydrostatic pressure forces since the vertical acceleration breaks the hydrostatic balance. We further examine these non-hydrostatic pressure forces in Section 24.7. However, for the present section we pursue a study of Archimedean buoyancy, which is computed as a relative force. Namely, we define a *buoyancy force* acting on a massive body relative to the displaced fluid

according to

$$\mathbf{F}_{\text{buoyancy}} = \hat{\mathbf{z}} g \int_{\mathcal{R}} (\rho_{\text{fluid}} - \rho_{\text{body}}) dV = \hat{\mathbf{z}} g (M_{\text{fluid}} - M_{\text{body}}). \quad (24.6)$$

As so defined, the vertical buoyancy force is negative if the mass of the body is larger than that of the fluid it displaces, and conversely if the body is less massive. If the densities are equal, then the body is *neutrally buoyant* and thus experiences no net vertical force; i.e., it floats.

## 24.3 Mass density and its flavors

The density of a fluid element is central to determining its buoyancy. The *thermal equation of state*, or *equation of state* to be more brief (Section 20.12.1), provides an expression for the mass density as a function of pressure, temperature, and material tracer concentration (salinity in the ocean and humidity in the atmosphere). In this section we discuss the equation of state as well as the related flavors of mass density used to study stratified fluids.

### 24.3.1 Equation of state for the atmosphere and ocean

The atmosphere and ocean are commonly approximated as two-component fluids (air and water vapor for the atmosphere; freshwater and salt for ocean). We thus write the *in situ* density as a function

$$\rho = \rho(S, T, p). \quad (24.7)$$

This *equation of state* is a function of the *in situ* temperature,  $T$ , the *in situ* pressure,  $p$ , and the *in situ* salinity,  $S$  (ocean) or humidity (atmosphere).<sup>4</sup> The term *in situ* refers to a property measured locally at a point in the fluid. Such *in situ* properties contrast to *potential* properties, which are based on referencing to a chosen pressure (e.g., potential temperature described in Section 20.11).

Liquids such as seawater have rather complex equations of states obtained from empirical fits to measurements. Part of the complexity arises from the multi-component nature of seawater (salt plus freshwater) as well as the nontrivial inter-molecular forces commonly found in liquids. In contrast, the dry atmosphere can, for many purposes, be well approximated as an ideal gas, which has a rather simple equation of state (see Section 20.12.1). Furthermore, even a moist atmosphere has an equation of state that can be massaged to look like that of an ideal gas (e.g., see Section 18.1 of [Vallis \(2017\)](#)). Hence, much of our discussion in this section is biased toward the ocean, where niceties of the equation of state are most important.

### 24.3.2 Modified temperature variables

As discussed in Section 20.11, the *in situ* temperature of a fluid element changes even if there is no heating applied to the element nor any changes to its material composition. Pressure changes provide the mechanical means for temperature to change even with processes that are adiabatic and constant composition. Is it possible to remove such pressure effects and still have a field that describes the “temperature” of a fluid element? That is, can we define a temperature field that is only modified by irreversible processes such as heating and mixing? This question is answered by defining *potential temperature*,  $\theta$ , as well as potential enthalpy or *Conservative Temperature*,  $\Theta$ , with full discussions given for potential temperature in Section 20.11 and Conservative Temperature in Section 21.8. For now it is sufficient to note that the mass density can be written as

<sup>4</sup>For our purposes when discussing the ocean, we set  $S = 1000 C$  with  $C$  the salt concentration, with this specification referred to as the *absolute salinity* by [IOC et al. \(2010\)](#).  $C$  generally has values around 0.035 so that  $S$  has values around 35.

a function salinity, potential temperature, and pressure

$$\rho = \rho(S, \theta, p), \quad (24.8)$$

or as a function of salinity, Conservative Temperature, and pressure

$$\rho = \rho(S, \Theta, p). \quad (24.9)$$

For our purposes throughout this book, it is not important to distinguish between potential temperature and Conservative Temperature. Hence, we use  $\theta$  for brevity when referring to either of the two temperature fields.

One comment on notation is key here. Namely, the functions  $\rho(S, T, p)$ ,  $\rho(S, \theta, p)$ , and  $\rho(S, \Theta, p)$  have distinct coefficients and as such they are distinct functions. Hence, one may wish to introduce notation to distinguish the functions by writing, say,

$$\rho = \mathcal{F}(S, T, p) = \mathcal{G}(S, \theta, p) = \mathcal{H}(S, \Theta, p). \quad (24.10)$$

However, we choose brevity in notation by allowing the functional dependence to signal the distinction. This overloaded notation is standard in the oceanography literature and yet care is needed to ensure clarity in understanding.

### 24.3.3 Infinitesimal density increments and material time changes

When computing the buoyancy of a fluid element, we compare the density of that element with the density of its local surrounding fluid environment. To support that comparison, we here consider how density changes under infinitesimal changes in spatial position. Given the functional dependence for the equation of state written in terms of  $S, \theta, p$  (equation (24.8)), an infinitesimal density increment is given by

$$d\rho = \left[ \frac{\partial \rho}{\partial S} \right] dS + \left[ \frac{\partial \rho}{\partial \theta} \right] d\theta + \left[ \frac{\partial \rho}{\partial p} \right] dp \equiv \rho \beta dS - \rho \alpha d\theta + c_s^{-2} dp. \quad (24.11)$$

The second equality introduced the following thermodynamic properties of the fluid

$$\beta = \frac{1}{\rho} \left[ \frac{\partial \rho}{\partial S} \right]_{\theta, p} \quad \text{haline contraction coefficient} \quad (24.12)$$

$$\alpha = -\frac{1}{\rho} \left[ \frac{\partial \rho}{\partial \theta} \right]_{S, p} \quad \text{thermal expansion coefficient} \quad (24.13)$$

$$c_s^2 = \left[ \frac{\partial p}{\partial \rho} \right]_{S, \theta} \quad \text{squared sound speed.} \quad (24.14)$$

The haline contraction coefficient,  $\beta$ , is considered for the ocean, where *haline* refers to salinity.<sup>5</sup>

The infinitesimal density increment (24.11) leads to the expression for the material change in the *in situ* density moving along a trajectory

$$\frac{1}{\rho} \frac{D\rho}{Dt} = \beta \frac{DS}{Dt} - \alpha \frac{D\theta}{Dt} + \frac{1}{\rho c_s^2} \frac{Dp}{Dt}. \quad (24.15)$$

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<sup>5</sup>Note that in many chapters of this book,  $\beta = \partial f / \partial y$  is the meridional derivative of the Coriolis parameter. We keep the two usages for  $\beta$  distinct so to avoid confusion.

In the absence of mixing, the potential temperature and salinity are materially constant.<sup>6</sup> In this case, the *in situ* density changes only through adiabatic processes that lead to pressure changes

$$\frac{D\rho}{Dt} = \frac{1}{c_s^2} \frac{Dp}{Dt} \quad \text{adiabatic and isohaline changes.} \quad (24.16)$$

#### 24.3.4 Potential density

As discussed in Section 24.3.2, the reversible motion of a perfect fluid element generally occurs with materially constant potential temperature and materially constant tracer concentration. We thus find it convenient to combine the evolution of salinity and potential temperature into the evolution of a single variable. *Potential density* is one such combination, with it defined as the density a fluid element would have if reversibly moved to a reference pressure

$$\varrho_R \equiv \rho(S, \theta, p = p_R). \quad (24.17)$$

Hence, potential density is found by evaluating the equation of state with the local value for  $S$  and  $\theta$ , but with the pressure set to the reference pressure,  $p = p_R$ . Potential density is parametrically a function of the reference pressure, though we generally drop the R subscript for brevity. As for the potential temperature, the reference pressure is often taken as that at sea level, though this is not necessary.

##### *Material evolution of potential density*

With the definition (24.17), the material evolution of potential density is given by

$$\frac{1}{\rho_R} \frac{D\varrho}{Dt} = \beta_R \frac{DS}{Dt} - \alpha_R \frac{D\theta}{Dt}, \quad (24.18)$$

where

$$\beta_R = \frac{1}{\rho_R} \left[ \frac{\partial \rho(S, \theta, p_R)}{\partial S} \right]_\theta \quad \text{haline contraction at } p = p_R \quad (24.19)$$

$$\alpha_R = -\frac{1}{\rho_R} \left[ \frac{\partial \rho(S, \theta, p_R)}{\partial \theta} \right]_S \quad \text{thermal expansion at } p = p_R \quad (24.20)$$

are the haline contraction and thermal expansion coefficients evaluated at the reference pressure  $p = p_R$ . Since pressure is fixed at the reference value, there is no pressure derivative on the right hand side of equation (24.18). Potential temperature and salinity are materially constant for reversible processes; i.e., adiabatic motion that also maintains constant matter content (e.g., isohaline) for fluid elements. By construction, potential density is also materially constant for reversible processes since both terms on the right hand side of equation (24.18) vanish. This behavior is in contrast to *in situ* density, whose evolution is affected by pressure changes as seen by equations (24.15) and (24.16).

##### *Reference pressures for $\varrho$ and $\theta$*

The reference pressure for the potential density is commonly assumed to be the same as for the potential temperature. This assumption is particularly the norm for the atmosphere, where the reference pressure is generally taken at the sea level. Likewise for the ocean, the potential

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<sup>6</sup>This statement has nuances that are detailed in [IOC et al. \(2010\)](#). For our purposes we can ignore those nuances.

temperature is generally computed using a sea level reference pressure. However, there are many occasions in the ocean to consider potential density with larger reference pressures, such as when considering processes within the ocean interior. Doing so is motivated by the rather strong nonlinear effects associated with the seawater equation of state. In this case, pressure effects prompt one to choose a reference pressure closer to the *in situ* pressure near to the region of analysis. Even though it is common to choose a potential density reference pressure distinct from the surface pressure, the potential temperature reference pressure generally remains at the surface. There is no fundamental problem with the use of distinct reference pressures for  $\varrho$  and  $\theta$ . In particular, all of the above properties of potential density remain unchanged.

### 24.3.5 Linear equation of state for the ocean

For certain purposes, it is useful to approximate the equation of state used to study ocean fluid mechanics. One common idealization is to compute density as a linear function of potential temperature and salinity

$$\varrho = \rho_0 [1 - \alpha(\theta - \theta_0) + \beta(S - S_0)], \quad (24.21)$$

where  $\alpha$ ,  $\beta$ ,  $\theta_0$ , and  $S_0$  are positive constants. An even further simplification is to set salinity to a constant, so that density is just a linear function of potential temperature.

### 24.3.6 Further study

Chapter 1 of [Vallis \(2017\)](#) provides a pedagogical discussion of the equation of state for an ideal gas atmosphere and for seawater, as well as a discussion of the various flavors of density. See also Section 18.1 of [Vallis \(2017\)](#) for the equation of state for an ideal gas with water vapor. The seawater equation of state is detailed by [IOC et al. \(2010\)](#), with a pedagogical overview provided by [McDougall et al. \(2013\)](#).

## 24.4 Archimedean buoyancy of a test fluid element

We now return to the notions of Archimedean buoyancy (in brief, the fluid “buoyancy”) of a test fluid element. Again, buoyancy is the gravitational acceleration that acts on a massive body due to the difference between the density of the body and the density of the local fluid environment. For this section, we consider the massive body to be a test fluid element whose presence does not alter the flow field.

### 24.4.1 Locally referenced Archimedean buoyancy

Consider a local definition of fluid buoyancy according to

$$b_{\text{local}} = -g(\rho_{\text{test}} - \rho_{\text{environ}})/\rho_{\text{environ}} = g(1 - \rho_{\text{test}}/\rho_{\text{environ}}), \quad (24.22)$$

where  $\rho_{\text{environ}}$  is the local density of the fluid environment, and  $\rho_{\text{test}}$  is the density of the test fluid element within that environment. If the fluid element has a density greater than the environment, then it has a negative locally referenced buoyancy, and vice versa.

We determine  $\rho_{\text{test}}$  by specifying its point of origin and specifying how it is moved (e.g., with or without mixing?) to the environment point. Conventional approaches are specified later in this section. A key notion is that buoyancy as defined by equation (24.22) is a function of the path that the test fluid element takes to reach the environment point. This subjectivity lends ambiguity in the definition of buoyancy. We remove this ambiguity by asking specific questions

about local buoyancy. For example, if the fluid element moves an infinitesimal distance while mixing its temperature and salinity with the environment, what direction maintains a neutrally buoyant state for the fluid element? This question forms the basis for defining *neutral directions*.

Working with locally referenced Archimedean buoyancy requires a redefinition of a reference state when moving from point to point within a fluid. The continuum of reference states allows for an accounting of the gravitational stability and neutral directions. However, the re-referencing is not a process that can be seamlessly incorporated to the equations of motion since at each point one needs to redefine the reference state. As an alternative means to garner local information about forces associated with density gradients, we explicitly focus on the pressure force in our discussion of *effective buoyancy* in Section 24.7.

#### 24.4.2 Globally referenced Archimedean buoyancy

The definition (24.22) accepts that buoyancy is a relative field. Hence, at each fluid point we redefine the environment to which to compare the density of the test fluid element. However, there are cases in which it is more convenient, and sufficient, to define a globally constant environment with a constant reference density,  $\rho_{\text{ref}}$ . In this case we consider the global buoyancy as

$$b_{\text{global}} = g(1 - \rho/\rho_{\text{ref}}), \quad (24.23)$$

where we compute  $\rho$  according to the local environmental density. This definition is particularly useful for idealized cases where the *in situ* density is not a function of pressure. In this case buoyancy is a function only of potential temperature and salinity so that we can make use of potential density to measure buoyancy (as explained below).

Although the numerical value of  $b_{\text{global}}$  is a function of the reference density, what is more relevant is the buoyancy of one fluid element relative to another

$$\Delta b_{\text{global}} = -\Delta\rho/\rho_{\text{ref}}. \quad (24.24)$$

The sign of this relative buoyancy does not depend on the reference density, with the sign all that we need to conclude whether one fluid element is more buoyant than another. Furthermore, with a globally constant environmental density, the buoyancy becomes a local function of space. That is, we no longer compare the fluid element density to a changing local density. Instead, we compute the local density and compare it to the reference density. We can thus determine  $b_{\text{global}}$  at a point through information available just at that point. Correspondingly, we can map  $b_{\text{global}}$  and determine the relative buoyancy of fluid elements anywhere in the fluid.

### 24.5 Buoyancy stratification and neutral directions

What are the Archimedean buoyant forces that act on a fluid element? Is the fluid gravitationally stable to small perturbations? We answer these questions by using a test fluid element to probe the local fluid environment without disturbing the environment. We do not consider time changes in this section, instead considering a snapshot of the fluid environment and using test fluid elements to probe the buoyant properties of the environment.

#### 24.5.1 General considerations

As a fluid element moves through the fluid environment it is exposed to a suite of physical processes that can modify its thermal, material, and mechanical properties; i.e., its  $\theta$ ,  $S$ , and  $p$ . Modification of its pressure occurs through contact stresses with other fluid elements (Chapters 18

and 19). Modification of its thermal and material properties occurs through the mixing-induced exchange of heat and matter. The exchange of thermal and material properties occurs in the presence of irreversible processes whereas mechanical exchanges occur either reversibly (pressure exchange) or irreversibly (viscous exchange; Section 18.2).

The *in situ* density of a fluid element generally changes when it moves through the fluid, with the density change determined by how the element interacts with the surrounding environment. We conceive of two complementary interactions for the purpose of examining the local Archimedean buoyancy of the test fluid element.

- **UNMIXED TEST FLUID ELEMENT:** Displace the test fluid element without changing  $\theta$  and  $S$  yet allowing  $p$  to equilibrate with the local environment. We imagine this adiabatic and isohaline displacement to occur by surrounding the test element with a thermally and materially impermeable elastic sack. In this case there is no mixing of the test element with the environment, yet it mechanically equilibrates its pressure with the surrounding fluid. Hence, the test fluid element's *in situ* density changes through the changing pressure of the local environment.
- **MIXED TEST FLUID ELEMENT:** Displace the test fluid element with  $\theta$ ,  $S$ , and  $p$  equilibrating with the local environment. Such equilibration requires a complete mixing of the test fluid element's  $\theta$  and  $S$  with the local environment, as well as the mechanical equilibration of its pressure.

If we displace the unmixed test fluid element to a region where its *in situ* density differs from the local environment, then the fluid element feels a local Archimedean buoyant force. However, there are directions that the test fluid element can move that leave its local Archimedean buoyancy zero; i.e., where the test fluid element retains the same *in situ* density as the local environment and so remains neutrally buoyant. These directions are referred to as *neutral directions*, with a test fluid element displaced along a neutral direction maintaining zero local Archimedean buoyancy. It is as if the test fluid element floats along a neutral direction.

A complementary means to conceive of neutral directions is found by considering the mixed test fluid element that is displaced and equilibrates its  $\theta$ ,  $S$ , and  $p$  with the local environment. An arbitrary displacement leads to a change in the fluid element's *in situ* density due to changes in  $\theta$ ,  $S$ , and  $p$ . However, if the test element is displaced along the neutral direction, the mixing-induced changes from  $\theta$  and  $S$  exactly balance (details given below). In this manner, the only change to the *in situ* density arises from changes to the pressure felt by the test fluid element, with these changes identical to those felt by the unmixed test fluid element.

### 24.5.2 Comparing *in situ* densities

To make the above ideas mathematically precise, consider an infinitesimal displacement,  $d\mathbf{x}$ , of a test fluid element and examine how its *in situ* density,  $\rho = \rho(S, \theta, p)$ , changes under the above two displacements. First consider the mixed fluid element so that it equilibrates  $\theta$ ,  $S$ , and  $p$  with the local environment. The *in situ* density of the test element at the new location equals to that of the local environment,  $\rho(\mathbf{x} + d\mathbf{x})$ . To leading order, the difference in density between the origin

and the displaced position is computed according to the exact differential

$$d\rho = \rho(\mathbf{x} + d\mathbf{x}) - \rho(\mathbf{x}) \quad (24.25a)$$

$$= \rho[S(\mathbf{x} + d\mathbf{x}), \theta(\mathbf{x} + d\mathbf{x}), p(\mathbf{x} + d\mathbf{x})] - \rho[S(\mathbf{x}), \theta(\mathbf{x}), p(\mathbf{x})] \quad (24.25b)$$

$$= d\mathbf{x} \cdot \left[ \frac{\partial \rho}{\partial \theta} \nabla \theta + \frac{\partial \rho}{\partial S} \nabla S + \frac{\partial \rho}{\partial p} \nabla p \right] \quad (24.25c)$$

$$= \rho d\mathbf{x} \cdot \left[ -\alpha \nabla \theta + \beta \nabla S + \frac{1}{\rho c_s^2} \nabla p \right]. \quad (24.25d)$$

For the unmixed test fluid element there is no exchange (mixing) of  $\theta$  and  $S$  with the surrounding environment. Hence, the test element's density changes just from pressure changes

$$(d\rho)_{\text{(no mix)}} = \rho(\mathbf{x} + d\mathbf{x})_{\text{(no mix)}} - \rho(\mathbf{x}) \quad (24.26a)$$

$$= \rho[S(\mathbf{x}), \theta(\mathbf{x}), p(\mathbf{x} + d\mathbf{x})] - \rho[S(\mathbf{x}), \theta(\mathbf{x}), p(\mathbf{x})] \quad (24.26b)$$

$$= \rho d\mathbf{x} \cdot \left[ \frac{1}{\rho c_s^2} \nabla p \right]. \quad (24.26c)$$

Comparing the densities of the two displaced test fluid elements renders

$$\rho(\mathbf{x} + d\mathbf{x}) - \rho(\mathbf{x} + d\mathbf{x})_{\text{(no mix)}} = [\rho(\mathbf{x} + d\mathbf{x}) - \rho(\mathbf{x})] - [\rho(\mathbf{x} + d\mathbf{x})_{\text{(no mix)}} - \rho(\mathbf{x})] \quad (24.27a)$$

$$= \rho[S(\mathbf{x} + d\mathbf{x}), \theta(\mathbf{x} + d\mathbf{x}), p(\mathbf{x} + d\mathbf{x})] - \rho[S(\mathbf{x}), \theta(\mathbf{x}), p(\mathbf{x} + d\mathbf{x})] \quad (24.27b)$$

$$= \rho d\mathbf{x} \cdot [-\alpha \nabla \theta + \beta \nabla S]. \quad (24.27c)$$

We discuss this result in the following.

### 24.5.3 Neutral directions and the neutrality condition

As noted in Figure 24.2, if the density of the displaced unmixed test fluid element is the same as the local environment, then the particular displacement defines a neutral direction. From equation (24.27c) we see a displacement along a neutral direction satisfies

$$d\mathbf{x}_{\text{neutral}} \cdot [-\alpha \nabla \theta + \beta \nabla S] = d\mathbf{x}_{\text{neutral}} \cdot \hat{\gamma} |-\alpha \nabla \theta + \beta \nabla S| = 0, \quad (24.28)$$

where we introduced the *dianeutral direction*

$$\hat{\gamma} = \frac{-\alpha \nabla \theta + \beta \nabla S}{|-\alpha \nabla \theta + \beta \nabla S|}, \quad (24.29)$$

which points in the direction of increasing density.<sup>7</sup> Infinitesimal displacements,  $d\mathbf{x}_{\text{neutral}}$ , that are orthogonal to the dianeutral direction,  $\hat{\gamma}$ , occur along a neutral direction

$$d\mathbf{x}_{\text{neutral}} \cdot \hat{\gamma} = 0 \implies \text{displacement along a neutral direction.} \quad (24.30)$$

These displacements of the unmixed test fluid element lead to no difference in the *in situ* density of the local environment and the fluid element. Hence, neutral displacements retain a vanishing local Archimedean buoyancy for the unmixed test fluid element. In contrast, displacements in the dianeutral direction alter the local buoyancy.

<sup>7</sup>Equation (4) in [McDougall et al. \(2014\)](#) makes use of the opposite convention so that their dianeutral direction points towards decreasing density. We instead follow the water mass transformation convention as in equation (50.38), so that  $\hat{\gamma}$  points in the direction of increasing density.

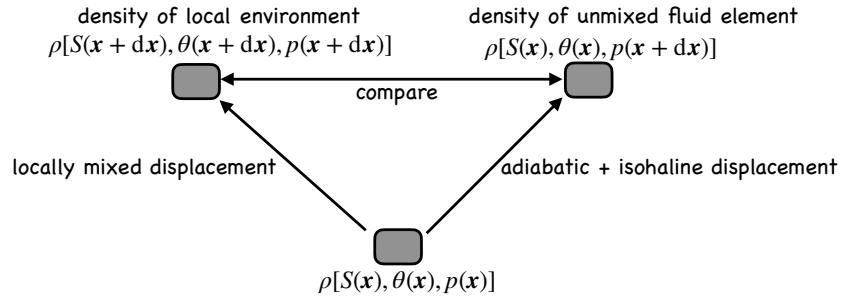
Let us write the neutral displacement in the form

$$dx_{\text{neutral}} = \hat{\mathbf{t}}_{\text{neutral}} ds, \quad (24.31)$$

where  $ds$  is the arc-length along the displacement and  $\hat{\mathbf{t}}_{\text{neutral}}$  is the unit vector pointing along the neutral displacement. We can thus write equation (24.28) as

$$\alpha \hat{\mathbf{t}}_{\text{neutral}} \cdot \nabla \theta = \beta \hat{\mathbf{t}}_{\text{neutral}} \cdot \nabla S, \quad (24.32)$$

which we refer to as the *neutrality condition*. The neutrality condition means that the derivatives of  $\theta$  and  $S$  aligned along a neutral direction, and suitably weighted by  $\alpha$  and  $\beta$ , are precisely balanced. So when considering neutral directions from the perspective of the mixed test fluid element, the mixing-induced changes in  $\theta$  precisely compensate mixing-induced changes in  $S$  as per the neutrality condition (24.32). As a result, the *in situ* density of the mixed test fluid element changes only via changes to the pressure (since  $\theta$  and  $S$  changes are compensated), which is precisely how the unmixed test fluid element changes its *in situ* density.



$$\rho[S(x + dx), \theta(x + dx), p(x + dx)] = \rho[S(x), \theta(x), p(x + dx)] \implies \text{neutral direction}$$

$$\alpha \hat{\mathbf{t}}_{\text{neutral}} \cdot \nabla \theta = \beta \hat{\mathbf{t}}_{\text{neutral}} \cdot \nabla S \implies \text{neutrality condition}$$

FIGURE 24.2: Schematic of the complementary thought experiments used to determine neutral directions. For the right pathway we imagine a test fluid element that is thermally and materially closed but is mechanically open. Hence, as the test fluid element is displaced from its original location,  $x$ , to a new position,  $x + dx$ , it equilibrates to the local pressure but retains the  $\theta$  and  $S$  of the origin. If the *in situ* density of the fluid element is displaced along a direction where it maintains the same density as the local environment, then the locally defined Archimedean buoyancy vanishes and this displacement is aligned along a neutral direction. The complement perspective is shown by the left pathway whereby we follow the mixed test fluid element. If the mixing-induced changes in  $\theta$  precisely compensate mixing-induced changes in  $S$ , according to the neutrality condition (24.32), then the *in situ* density changes for this test fluid element arise only from pressure changes, just like for the unmixed test element on the right pathway.

#### 24.5.4 Buoyancy frequency and gravitational stability

Thus far we have considered a general displacement,  $dx$ , of two test fluid elements, and determined conditions for this displacement to keep the locally defined Archimedean buoyancy at zero. Here we specialize to the case of a vertical displacement (Figure 24.3) in which the difference between the environmental density and the unmixed test element's density is

$$\rho(z + dz) - \rho(z + dz)_{(\text{no mix})} = \rho dz \left[ -\alpha \frac{\partial \theta}{\partial z} + \beta \frac{\partial S}{\partial z} \right]. \quad (24.33)$$

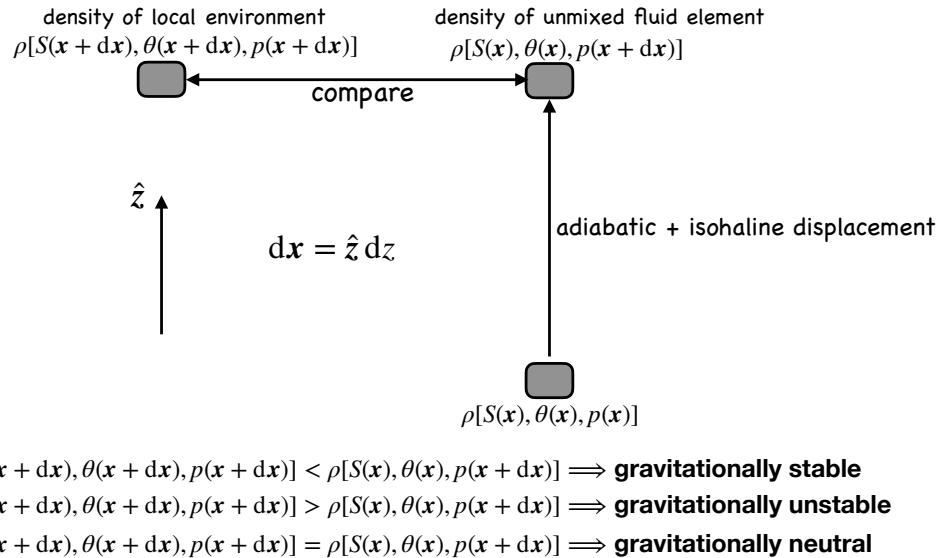


FIGURE 24.3: Schematic of the calculation used to examine whether a fluid column is gravitationally stable under vertical displacement of a test fluid element, here realized by specializing the general displacement in Figure 24.2. A test fluid element is displaced from its original location at a position  $x$  to a position  $x + dx$ , with  $dx = \hat{z} dz$  and  $dz > 0$  in this figure. We compare the density of the displaced unmixed test fluid element with the local environment to determine whether the density stratification of the fluid environment is gravitationally stable, unstable, or neutral.

Now consider a vertically upward displacement so that  $dz > 0$ . If the surrounding environment has a lower density than the adiabatic and isohaline displaced test fluid element,  $\rho(z + dz) < \rho(z + dz)_{(\text{no mix})}$ , then the test element will feel a buoyancy force returning it to the original depth. The restorative buoyancy force per volume is written

$$g [\rho(z + dz) - \rho(z + dz)_{(\text{no mix})}] = g \rho dz \left[ -\alpha \frac{\partial \theta}{\partial z} + \beta \frac{\partial S}{\partial z} \right] \equiv -N^2 \rho dz, \quad (24.34)$$

where we defined the squared buoyancy frequency

$$N^2 = g \left[ \alpha \frac{\partial \theta}{\partial z} - \beta \frac{\partial S}{\partial z} \right]. \quad (24.35)$$

Stable vertical motion results from a background density profile with  $N^2 > 0$ . An unstable profile occurs when  $N^2 < 0$ , in which case motion of the test fluid element results in an exponential growth associated with a *gravitational instability*. That is, when the fluid column is unstably stratified in the vertical, an initially tiny vertical displacement of a test element will lead to an even larger displacement, thus causing the perturbation to grow unbounded, which is the sign of an instability. We illustrate these cases in Figure 24.4 for the case of linear density profiles.

### 24.5.5 Locally referenced potential density

Equation (24.35) defines the squared buoyancy frequency in terms of the vertical temperature and salinity gradients. This expression is identical to the vertical gradient of the potential density (24.17), when the reference pressure for density is taken local to the point where the buoyancy frequency is computed. That is, the vertical gradient of the *locally referenced potential density*

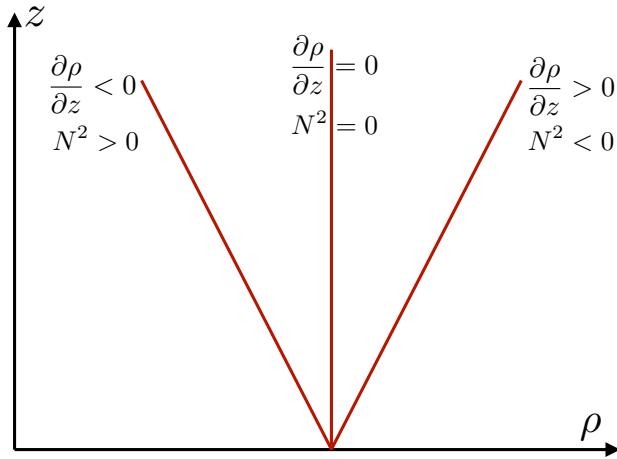


FIGURE 24.4: Sample vertical “soundings” of density in the atmosphere or density profiles in the ocean, with the density assumed to be a linear function of  $z$ . If the density decreases upward, the squared buoyancy frequency is positive,  $N^2 > 0$ , and the fluid is gravitationally stable. If the density does not change when moving vertically, then the fluid is said to be neutrally buoyant with  $N^2 = 0$ . If the density increases moving upward, then the fluid is gravitationally unstable, with this instability signaled by  $N^2 < 0$ .

provides a measure of the vertical stratification

$$N^2 = -g \left[ \frac{\partial \ln \varrho}{\partial z} \right]_{p_R=p} = g \left[ \alpha \frac{\partial \theta}{\partial z} - \beta \frac{\partial S}{\partial z} \right]. \quad (24.36)$$

Note that at a point in the fluid, the locally referenced potential density equals to the *in situ* density. However, when probing nearby points by displacing test fluid elements, and thus to take spatial gradients into account, the two densities have distinct gradients. Namely, the *in situ* density is modified by pressure gradients, whereas spatial gradients of the locally referenced potential density remove pressure effects.

### 24.5.6 Gravitational stability of an ideal gas atmosphere

We introduced the adiabatic lapse rate in Section 20.10 as a measure of how temperature varies as a function of pressure or depth. For an ideal gas atmosphere (Section 20.12), the squared buoyancy frequency can be written (Exercise 24.2)

$$N^2 = \frac{g}{\theta} \frac{\partial \theta}{\partial z}. \quad (24.37)$$

The potential temperature for an ideal gas is given by equation (20.203)

$$\theta = T \left[ \frac{p_R}{p} \right]^\varphi \quad (24.38)$$

where

$$\varphi = R^M/c_p \quad (24.39)$$

is a dimensionless constant for a simple ideal gas. Consequently, the squared buoyancy frequency takes the form

$$g^{-1} N^2 = \frac{\partial \ln \theta}{\partial z} = \frac{\partial \ln T}{\partial z} - \varphi \frac{\partial \ln p}{\partial z}. \quad (24.40)$$

For a hydrostatic fluid with a constant gravitational acceleration, the vertical derivative of pressure is given by (Section 22.2)

$$\frac{\partial p}{\partial z} = -\rho g, \quad (24.41)$$

so that pressure at a point in the fluid equals to the weight per area above that point. Using this result leads to the squared buoyancy frequency

$$g^{-1} N^2 = \frac{\partial \ln T}{\partial z} + \frac{\varphi g \rho}{p} = \frac{1}{T} \frac{\partial T}{\partial z} + \frac{g}{c_p T}, \quad (24.42)$$

where we used the ideal gas relation  $p = \rho T R^M$  for the final step.

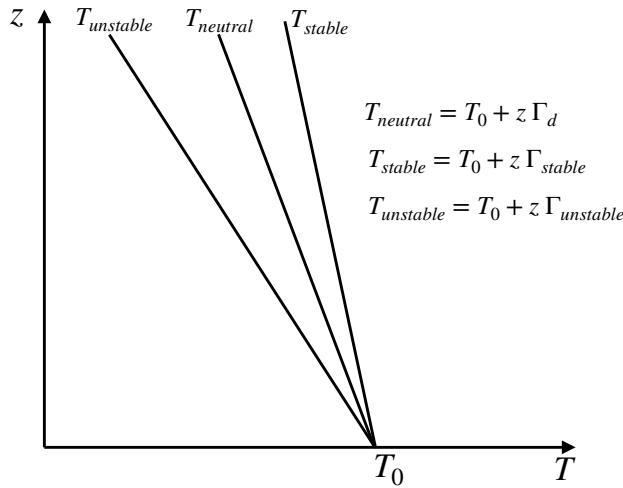


FIGURE 24.5: Three vertical profiles of *in situ* temperature in a dry ideal gas atmosphere. The neutrally stable profile has  $T_{\text{neutral}} = T_0 + z \Gamma_d$ , where  $\Gamma_d = -g/c_p \approx -9.8 \text{ K/(1000 m)}$ . A vertically unstable profile (heavy over light) has  $T_{\text{unstable}} = T_0 + z \Gamma_{\text{unstable}}$  where  $\Gamma_{\text{unstable}} < \Gamma_d = -g/c_p$ . In contrast, the gravitationally stable atmosphere has  $T_{\text{stable}} = T_0 + z \Gamma_{\text{stable}}$  where  $\Gamma_{\text{stable}} > \Gamma_d = -g/c_p$ .

A vanishing buoyancy frequency, or equivalently a vanishing vertical derivative of potential temperature, occurs when the vertical temperature gradient equals to the dry adiabatic lapse rate

$$N^2 = 0 \iff \frac{\partial T}{\partial z} = \Gamma_d, \quad (24.43)$$

where (see equation (20.185))

$$\Gamma_d = -\frac{g}{c_p} \approx -9.8 \text{ K/(1000 m)}. \quad (24.44)$$

That is, if the *in situ* temperature decreases upon ascent more quickly than the dry adiabatic lapse rate, then the vertical column is gravitationally unstable. In effect, the column becomes top heavy and subject to overturning. We summarize this stability criteria as

$$\text{stable} \quad N^2 > 0 \iff -\frac{\partial T}{\partial z} < \frac{g}{c_p} \quad (24.45)$$

$$\text{unstable} \quad N^2 < 0 \iff -\frac{\partial T}{\partial z} > \frac{g}{c_p}, \quad (24.46)$$

with Figure 24.5 providing an illustration for three linear temperature profiles.

### 24.5.7 Comments and further study

Neutral directions were introduced to oceanography by [McDougall \(1987a\)](#) and [McDougall \(1987b\)](#), and they are the basis for how oceanographers think about buoyancy stratification. [McDougall et al. \(2014\)](#) offer another presentation of why neutral directions are relevant for the ocean, taking into account measurements of dianeutral mixing. Our discussion of neutral directions was inspired by the concise presentation in Section 2.7.2 of [Olbers et al. \(2012\)](#).

In deriving an algorithm to compute neutral directions, we have not presented an argument for dynamical processes favoring neutral displacements. That argument requires dynamical principles, such as the equations of motion and associated energetic constraints. Yet there is presently no dynamical argument for why the ocean prefers neutral displacements over arbitrary non-neutral displacements. However, robust empirical measures support the relevance of neutral directions for orienting tracer mixing within the ocean interior. More discussion of these points is given by [McDougall et al. \(2014\)](#).

Our study of vertical gravitational stability follows Section 3.6 of [Gill \(1982\)](#) as well as Section 2.10 of [Vallis \(2017\)](#). In an actual fluid, the movement of any fluid, even a tiny fluid element, modifies the surrounding fluid so that a perfect test fluid element is a fiction. We return to this point in Section 24.7 when studying effective buoyancy.

## 24.6 Neutral helicity

In our study of neutral directions in Section 24.5 we introduced the notion of a neutral displacement. For the test fluid element that mixes with its environment, a neutral displacement results when the mixing of  $\theta$  and  $S$  are balanced according to the neutrality condition (24.32). We here expose a rather remarkable result concerning the topological properties of the surface defined by a series of such neutral displacements.

### 24.6.1 Mathematical preliminaries

Consider a simply connected smooth surface with outward normal written in the form

$$\hat{\mathbf{n}} = |\mathbf{N}|^{-1} \mathbf{N}. \quad (24.47)$$

Likewise, consider a unit vector  $\hat{\mathbf{t}}$  that lives within the surface and is directed tangent to an arbitrary closed loop. Since  $\mathbf{N} \cdot \hat{\mathbf{t}} = 0$  by construction, we can integrate around an arbitrary closed loop within the surface and still maintain the trivial result

$$\oint_{\partial\mathcal{S}} \mathbf{N} \cdot \hat{\mathbf{t}} \, dl = 0. \quad (24.48)$$

We chose a counterclockwise orientation of the loop around the boundary, with  $\partial\mathcal{S}$  denoting the boundary of the area  $\mathcal{S}$  within the surface.

Now apply Stokes' Theorem to the loop integral (24.48) to yield

$$\int_{\mathcal{S}} (\nabla \times \mathbf{N}) \cdot \hat{\mathbf{n}} \, d\mathcal{S} = 0, \quad (24.49)$$

where  $d\mathcal{S}$  is the area element in the surface  $\mathcal{S}$  with outward normal  $\hat{\mathbf{n}}$ . Since the closed path is arbitrary, the area integral (24.49) vanishes only if the integrand is identically zero. We conclude

that for the surface to be simply connected requires that the helicity must vanish

$$\mathcal{H} = \mathbf{N} \cdot (\nabla \times \mathbf{N}) = 0 \implies \text{simply connected surface.} \quad (24.50)$$

The converse also holds so that

$$\mathcal{H} \neq 0 \implies \text{non-simply connected surface.} \quad (24.51)$$

### 24.6.2 Helical nature of neutral displacements

Now apply the above mathematical results to the question of whether a surface with its outward normal parallel to the dianeutral direction,

$$\mathbf{N} = -\alpha \nabla \theta + \beta \nabla S \quad (24.52)$$

is simply connected. We thus consider the *neutral helicity*

$$\mathcal{H}_{\text{neutral}} = (-\alpha \nabla \theta + \beta \nabla S) \cdot \nabla \times (-\alpha \nabla \theta + \beta \nabla S), \quad (24.53)$$

which can be written

$$\mathcal{H}_{\text{neutral}} = (-\alpha \nabla \theta + \beta \nabla S) \cdot \nabla \times (-\alpha \nabla \theta + \beta \nabla S) \quad (24.54a)$$

$$= -\alpha \nabla \theta \cdot (\nabla \times \beta \nabla S) - \beta \nabla S \cdot (\nabla \times \alpha \nabla \theta) \quad (24.54b)$$

$$= -\alpha \nabla \theta \cdot (\nabla \beta \times \nabla S) - \beta \nabla S \cdot (\nabla \alpha \times \nabla \theta). \quad (24.54c)$$

Now expand the gradients of  $\alpha$  and  $\beta$  according to

$$\nabla \alpha = \alpha_\theta \nabla \theta + \alpha_S \nabla S + \alpha_p \nabla p \quad (24.55a)$$

$$\nabla \beta = \beta_\theta \nabla \theta + \beta_S \nabla S + \beta_p \nabla p, \quad (24.55b)$$

where the subscripts are shorthands for partial derivatives. We thus have

$$-\alpha \nabla \theta \cdot (\nabla \beta \times \nabla S) = -\alpha \nabla \theta \cdot (\beta_p \nabla p \times \nabla S) \quad (24.56a)$$

$$-\beta \nabla S \cdot (\nabla \alpha \times \nabla \theta) = -\beta \nabla S \cdot (\alpha_p \nabla p \times \nabla \theta), \quad (24.56b)$$

which brings the neutral helicity to the form

$$-\mathcal{H}_{\text{neutral}} = -\alpha \nabla \theta \cdot (\beta_p \nabla p \times \nabla S) - \beta \nabla S \cdot (\alpha_p \nabla p \times \nabla \theta) \quad (24.57a)$$

$$= -\alpha \beta_p \nabla \theta \cdot (\nabla p \times \nabla S) - \beta \alpha_p \nabla S \cdot (\nabla p \times \nabla \theta) \quad (24.57b)$$

$$= \nabla p \cdot (\nabla S \times \nabla \theta) (\alpha \beta_p - \beta \alpha_p). \quad (24.57c)$$

Introducing the thermobaricity parameter<sup>8</sup>

$$\mathcal{T} = \beta \partial_p (\alpha / \beta) \quad (24.58)$$

renders the tidy result

$$\mathcal{H}_{\text{neutral}} = \beta \mathcal{T} \nabla p \cdot (\nabla S \times \nabla \theta). \quad (24.59)$$

Consequently, a nonzero neutral helicity is fundamentally related to a nonzero thermobaricity parameter  $\mathcal{T}$ . It is also associated with the non-zero volume for a parallelopiped in  $(\theta, S, p)$  space

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<sup>8</sup>We further discuss the thermobaricity parameter in Section 49.3.

(see Section 1.5)

$$\nabla p \cdot (\nabla S \times \nabla \theta) = \nabla \theta \cdot (\nabla p \times \nabla S) = \nabla S \cdot (\nabla \theta \times \nabla p). \quad (24.60)$$

Returning to our discussion of simply connected surfaces in Section 24.6.1, we see that a nonzero  $\mathcal{H}_{\text{neutral}}$  means that a path defined by the accumulation of neutral directions does not close. Hence, the surface defined by neutral paths is not simply connected. Furthermore, as discussed by [McDougall and Jackett \(1988\)](#), neutral paths possess a helical structure, with each loop in  $(S, \theta)$  configuration space displaced vertically in pressure.

### 24.6.3 Comments and further study

Neutral helicity is a property of seawater that is revealed through the neutrally compensated mixing of  $\theta$  and  $S$ . That is, neutral helicity is not a direct property of mixing though mixing is required to determine neutral directions. [McDougall and Jackett \(1988\)](#) first noted the non-trivial topology defined by neutral displacements, and [McDougall and Jackett \(2007\)](#) provide more elaboration and analysis from observational based measurements. [Bennett \(2019\)](#) connects the geometry defined by neutral paths with mathematical properties encountered in a variety of thermodynamic systems. [Stanley \(2019\)](#) offers insights into the topology of neutral directions.

## 24.7 Effective buoyancy and vertical accelerations

We extend our discussion of Archimedean buoyancy in this section by focusing on the vertical forces acting on a fluid element rather than a test fluid element. For this purpose, we find it useful to decompose these forces into *static forces* that remain even when imagining all motion to vanish, plus the *motional forces* that remain when imagining all density gradients to vanish. Motional forces are specific to details of the motion, whereas static forces can generally be deduced just from knowledge of the density field. In analogy with Archimedean buoyancy, we use the term *effective buoyancy* for the static forces acting on a fluid element. Although the effective buoyancy is in part comprised of Archimedean buoyancy, there are distinctions that arise through interactions between the fluid element and its surrounding environment.

### 24.7.1 Vertical motion in approximately hydrostatic fluids

As introduced in Section 22.2 and further detailed in Section 23.2, an approximate hydrostatic fluid is one in which the vertical pressure gradient locally balances the density, with the horizontal gradient of hydrostatic pressure contributing to horizontal accelerations. Although vertical motion can occur in the approximately hydrostatic fluid, that motion is diagnosed rather than prognosed since the vertical momentum equation is reduced to local hydrostatic balance. For example, a diagnostic evaluation of the vertical velocity in a Boussinesq fluid is performed through vertically integrating the continuity equation.

As we see in equation (24.68c) below, the vertical gradient of the non-hydrostatic pressure is the only inviscid force contributing to a vertical acceleration. So even if the fluid is approximately hydrostatic, it is the non-hydrostatic pressure force that enables vertical accelerations. This situation is directly analogous to the oceanic Boussinesq approximation as derived in Section 23.1, whereby the fluid flow is incompressible so that  $\nabla \cdot \mathbf{v} = 0$ , yet the fluid itself is compressible so that  $D\rho/Dt \neq 0$ . For the approximately hydrostatic fluid we have the local hydrostatic balance,  $\partial p/\partial z = -\rho g$ , yet nonzero vertical acceleration,  $Dw/Dt \neq 0$ .

### 24.7.2 Two decompositions of pressure and gravity forces

Consider the momentum equation with the geopotential,  $\Phi = g z$ ,

$$\rho (\partial_t + \mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \rho \mathbf{v} = -\nabla p - \rho g \hat{\mathbf{z}} + \rho \mathbf{F}. \quad (24.61)$$

We are concerned with the pressure and gravity contributions on the right hand side, and we offer two means to organize these terms. The first follows that used to formulate the Boussinesq approximation in Section 23.1.1. Summarizing those steps for completeness, we introduce a constant reference density,  $\rho_0$ , along with a corresponding hydrostatically balanced reference pressure

$$p = p' + p_0 \quad \text{with} \quad dp_0(z)/dz = -\rho_0 g. \quad (24.62)$$

This decomposition brings the pressure and gravity on the right hand side of the momentum equation (24.61) into the form

$$\nabla p + \rho g \hat{\mathbf{z}} = \nabla p' - \rho_0 b \hat{\mathbf{z}} \quad \text{with} \quad b = -g(\rho - \rho_0)/\rho_0, \quad (24.63)$$

where  $b$  is the globally referenced Archimedean buoyancy computed relative to the globally constant reference density,  $\rho_0$ . The second decomposition splits pressure into a local hydrostatic pressure,  $p_h$ , and a non-hydrostatic pressure,  $p_{nh}$ ,

$$p = p_h + p_{nh} \quad \text{with} \quad \partial p_h / \partial z = -\rho g, \quad (24.64)$$

in which case

$$\nabla p + \rho g \hat{\mathbf{z}} = \nabla p_{nh} + \nabla_z p_h = \nabla_z p + \hat{\mathbf{z}} \partial_z p_{nh}. \quad (24.65)$$

The following comments compare and contrast the two decompositions.

- By decomposing pressure as  $p = p_0 + p'$ , we expose the dynamically active portion of the pressure field,  $p'$ , by removing the dynamically irrelevant pressure,  $p_0$ , from the momentum equation. Notably, this decomposition results in a dynamical pressure,  $p'$ , that has both hydrostatic and non-hydrostatic contributions.
- The local hydrostatic plus non-hydrostatic decomposition serves to split the pressure into its two dynamically distinct portions. However, it does not remove the global hydrostatic background pressure from the forcing, which can be seen by the identity

$$\partial p_h / \partial z = dp_0(z)/dz - \rho' g. \quad (24.66)$$

We retain both the global and local pressure decompositions in the following as doing so offers complementary perspectives on how pressure forces lead to vertical accelerations.

### 24.7.3 Vertical equation of motion

To further study how pressure and gravity lead to vertical motion, we make the Boussinesq approximation so that the velocity equation (24.61) takes the form (23.66)

$$\rho_0 (\partial_t + \mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \rho_0 \mathbf{v} = -\nabla p - \rho g \hat{\mathbf{z}} + \rho_0 \mathbf{F} \quad (24.67a)$$

$$= -\nabla p' + \rho_0 b \hat{\mathbf{z}} + \rho_0 \mathbf{F} \quad (24.67b)$$

$$= -\nabla p_{nh} - \nabla_z p_h + \rho_0 \mathbf{F}, \quad (24.67c)$$

with particular attention given to the vertical momentum equation

$$\rho_0 (\partial_t + \mathbf{v} \cdot \nabla) w = -\partial_z p - \rho g + \rho_0 \mathbf{F} \cdot \hat{\mathbf{z}} \quad (24.68a)$$

$$= -\partial_z p' + \rho_0 b + \rho_0 \mathbf{F} \cdot \hat{\mathbf{z}} \quad (24.68b)$$

$$= -\partial_z p_{nh} + \rho_0 \mathbf{F} \cdot \hat{\mathbf{z}}. \quad (24.68c)$$

Equation (24.68c) reveals that vertical acceleration has an inviscid contribution from pressure and gravity arising just from vertical derivatives in the non-hydrostatic pressure,  $p_{nh}$ . Equation (24.68b) has contributions from vertical gradients in the dynamical pressure,  $p'$ , plus the globally referenced Archimedean buoyancy,  $b$ .

#### 24.7.4 Effective buoyancy and motional vertical acceleration

We decompose the vertical acceleration into two conceptually distinct processes. The first is the *effective buoyancy*, which is the vertical acceleration arising from the mass/density field. Operationally, we deduce the effective buoyancy by setting velocity to zero everywhere in the expression for the vertical acceleration

$$b_{\text{eff}} \equiv \left. \frac{Dw}{Dt} \right|_{\mathbf{v}=0}. \quad (24.69)$$

As viscous friction only arises when there is fluid motion, it does not contribute to the effective buoyancy (Section 18.7.6). Hence, equations (24.68b) and (24.68c) show that the effective buoyancy is given by the two equivalent expressions

$$\rho_0 b_{\text{eff}} = \rho_0 b - \partial_z p'|_{\mathbf{v}=0} = -\partial_z p_{nh}|_{\mathbf{v}=0}. \quad (24.70)$$

The first expression identifies the difference between the effective buoyancy and the Archimedean buoyancy

$$\rho_0 (b_{\text{eff}} - b) = -\partial_z p'|_{\mathbf{v}=0}. \quad (24.71)$$

Namely, the difference arises from the nonzero  $(\partial_z p')_{\mathbf{v}=0}$ . This vertical pressure gradient means that the Archimedean buoyancy is an incomplete description of the vertical acceleration. The second expression in equation (24.70) can be thought of as a generalization of the local hydrostatic relation,  $\partial_z p_h = \rho_0 b$ , thus defining the effective buoyancy as minus the vertical gradient of the non-hydrostatic pressure. As a test of the formalism, note that for the special case when  $p'$  is approximated by its hydrostatic component, so that  $\rho_0 b = \partial_z p'$ , then there is no effective buoyancy, which also corresponds to  $\partial_z p_{nh} = 0$ .

If one introduces an Archimedean buoyancy anomaly in a static fluid, then the initial vertical acceleration acting on the anomaly is given by its effective buoyancy. As the anomaly evolves, motion is generated, at which point  $b_{\text{eff}}$  is an incomplete measure of vertical acceleration. In the presence of motion we must also consider the *motional vertical acceleration*. Operationally, we deduce this acceleration by setting the density to a constant within the expression for the vertical acceleration

$$\rho_0 a_{\text{motion}} \equiv \left. \frac{Dw}{Dt} \right|_{\rho=\rho_0}. \quad (24.72)$$

Since the Archimedean buoyancy vanishes when density is uniform, we know that

$$a_{\text{motion}} = -\partial_z p'|_{\rho=\rho_0} + \rho_0 \mathbf{F} \cdot \hat{\mathbf{z}} = -\partial_z p_{nh}|_{\rho=\rho_0} + \rho_0 \mathbf{F} \cdot \hat{\mathbf{z}}, \quad (24.73)$$

so that the vertical pressure gradients of  $p'$  and  $p_{nh}$  are the same when the density field is uniform.

To completely specify the decomposition of vertical acceleration requires boundary conditions for the effective buoyancy and the motional acceleration. Mathematical details are simplified by restricting concern to rigid and flat upper and lower boundaries and no lateral boundaries. At the rigid and flat boundaries we have  $Dw/Dt = 0$ , and this boundary condition holds whether  $\mathbf{v} = 0$  or  $\rho = \rho_0$ , so that  $b_{\text{eff}} = 0$  and  $a_{\text{motion}} = 0$  also hold at these boundaries. In this case we are ensured that the net vertical acceleration is the sum

$$\rho_0 \frac{Dw}{Dt} = \rho_0 (a_{\text{motion}} + b_{\text{eff}}). \quad (24.74)$$

With these special boundary conditions, the conceptual decomposition of the vertical acceleration also serves as an operational decomposition.

### 24.7.5 Poisson equations for the pressures and accelerations

#### *Archimedean buoyancy plus perturbation pressure*

Consider the momentum equation (24.67b) written using the decomposition of pressure and gravity that introduces the Archimedean buoyancy

$$\rho_0 (\partial_t + \mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \rho_0 \mathbf{v} = -\nabla p' + \rho_0 b \hat{\mathbf{z}} + \rho_0 \mathbf{F}. \quad (24.75)$$

As in Section 23.3, we can eliminate the time tendency by taking a divergence to render a Poisson equation for the perturbation pressure

$$-\nabla^2 p' = \rho_0 \nabla \cdot [(\mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \mathbf{v} - b \hat{\mathbf{z}} - \mathbf{F}]. \quad (24.76)$$

The Poisson equation is linear so that we can decompose the source terms and corresponding pressures according to

$$-\nabla^2 p'_{\text{buoy}} \equiv -\rho_0 \partial_z b \quad (24.77a)$$

$$-\nabla^2 p'_{\text{motion}} \equiv \rho_0 \nabla \cdot [(\mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \mathbf{v} - \mathbf{F}], \quad (24.77b)$$

with the buoyancy pressure perturbation,  $p'_{\text{buoy}}$ , sourced by vertical derivatives of the Archimedean buoyancy, and the motional pressure perturbation,  $p'_{\text{motion}}$ , sourced by fluid motion that gives rise to an acceleration through self-advection, Coriolis, and friction.

From the definition (24.70) of the effective buoyancy, the decompositions (24.77a) and (24.77b) allow us to identify the Poisson equation for the effective buoyancy

$$\rho_0 b_{\text{eff}} = \rho_0 b - \partial_z p'_{\text{buoy}} \implies -\nabla^2 b_{\text{eff}} = -\nabla_z^2 b \implies -\nabla^2 (b_{\text{eff}} - b) = \partial_{zz} b. \quad (24.78)$$

Hence, the source for the effective buoyancy is the horizontal Laplacian of the Archimedean buoyancy. Correspondingly, the source for the difference,  $b_{\text{eff}} - b$ , is the vertical curvature of the Archimedean buoyancy,  $\partial_{zz} b$ . The decompositions (24.77a) and (24.77b) also allow us to identify the Poisson equation for the motional acceleration

$$-\nabla^2 a_{\text{motion}} = -\partial_z \nabla \cdot [(\mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \mathbf{v} - \mathbf{F}] - \nabla^2 (\mathbf{F} \cdot \hat{\mathbf{z}}). \quad (24.79)$$

*Local non-hydrostatic plus local hydrostatic pressures*

We can also arrive at the above results by considering the momentum equation (24.67c) written using the decomposition of pressure into local non-hydrostatic and local hydrostatic components

$$\rho_0 (\partial_t + \mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \rho_0 \mathbf{v} = -\nabla p_{nh} - \nabla_z p_h + \rho_0 \mathbf{F}. \quad (24.80)$$

A divergence of this equation leads to the Poisson equation for the non-hydrostatic pressure

$$-\nabla^2 p_{nh} = \nabla_z^2 p_h + \rho_0 \nabla \cdot [(\mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \mathbf{v} - \mathbf{F}]. \quad (24.81)$$

Taking a vertical derivative and use of the hydrostatic relation leads to the Poisson equation for the vertical derivative of the non-hydrostatic pressure

$$-\nabla^2 (\partial_z p_{nh}) = -g \nabla_z^2 \rho + \rho_0 \partial_z \nabla \cdot [(\mathbf{v} \cdot \nabla) \mathbf{v} + f \hat{\mathbf{z}} \times \mathbf{v} - \mathbf{F}]. \quad (24.82)$$

With the motional acceleration given by  $(\partial_z p_{nh})_{\rho=\rho_0}$ , the general expression (24.73) for  $a_{\text{motion}}$ , along with the Poisson equation (24.82) for  $\partial_z p_{nh}$ , renders the Poisson equation (24.79).

Setting  $\mathbf{v} = 0$  in equation (24.81) renders the Poisson equation

$$-(\nabla^2 p_{nh})_{\mathbf{v}=0} = \nabla_z^2 p_h. \quad (24.83)$$

This equation says that the static portion of the non-hydrostatic pressure is sourced by the horizontal Laplacian of the hydrostatic pressure. Equivalently, the convergence of  $(\nabla p_{nh})_{\mathbf{v}=0}$  is balanced by the divergence of the horizontal hydrostatic pressure gradient,  $\nabla_z p_h$ . Furthermore, setting  $\mathbf{v} = 0$  in equation (24.82) yields the Poisson equation for the effective buoyancy

$$-\rho_0 \nabla^2 b_{\text{eff}} = g \nabla_z^2 \rho, \quad (24.84)$$

which accords with equation (24.78).

*Scales for effective buoyancy and Archimedean buoyancy*

One way to emphasize the distinction between the effective buoyancy equation (24.84) and that for the Archimedean buoyancy is to compare their two elliptic equations

$$-\rho_0 \nabla^2 b = g \nabla^2 \rho \longleftrightarrow -\rho_0 \nabla^2 b_{\text{eff}} = g \nabla_z^2 \rho, \quad (24.85)$$

with the first equality following trivially by definition of Archimedean buoyancy,  $b = -(g/\rho_0)(\rho - \rho_0)$ . The different Laplacian operators acting in equation (24.84) on  $b_{\text{eff}}$  and  $b$  means that they scale differently. To see how, consider an Archimedean buoyancy anomaly with a horizontal scale  $D$  and vertical scale  $H$  so that the Laplacian operators scale according to  $\nabla^2 \sim D^{-2} + H^{-2}$  and  $\nabla_z^2 \sim D^{-2}$ . Plugging into the effective buoyancy equation (24.84) leads to

$$B_{\text{eff}} = \frac{B}{1 + D^2/H^2}, \quad (24.86)$$

where  $B_{\text{eff}}$  is the scale for the effective buoyancy and  $B$  is the scale for the Archimedean buoyancy. We see that the effective buoyancy is smaller in scale than the Archimedean buoyancy, with this scale reduction arising from the pressure contribution in the effective buoyancy that is missing from the Archimedean buoyancy.

As a buoyant fluid element moves vertically, it must displace the surrounding environmental fluid. The pressure contribution to the effective buoyancy accounts for the back-reaction of the

environmental fluid on the buoyant fluid element. Since the Archimedean buoyancy ignores the back-reaction, it generally over estimates the magnitude of the vertical acceleration. By accounting for the pressure forces acting on the element from the surrounding fluid, the effective buoyancy offers a more accurate measure of the static vertical forces arising from density inhomogeneities.

### 24.7.6 Thought experiments for effective buoyancy

We here present some thought experiments for the purpose of developing an understanding of effective buoyancy. The thought experiments are somewhat trivial physically and yet they require us to confront basic assumptions, which is generally a useful exercise.

#### *Horizontally unstratified density*

Consider a horizontally unstratified density,  $\rho = \rho(z)$ , on a horizontally periodic domain with the fluid in hydrostatic equilibrium. By construction, the Archimedean buoyancy exactly balances the vertical pressure gradient. In the absence of horizontal density gradients, the effective buoyancy is everywhere a harmonic function since  $\nabla^2 b_{\text{eff}} = 0$ . With vanishing Dirichlet boundary conditions at the rigid bottom and top of the domain,  $z = 0, H$ , then  $b_{\text{eff}} = 0$  everywhere, signaling the absence of any vertical acceleration.

It is notable that this result holds for an arbitrary vertical profile of density, even if the density is gravitationally unstable (Section 24.5). The assumed horizontal symmetry is the key point. This assumption precludes any vertical motion since no fluid element at a single horizontal position can be vertically displaced without breaking horizontal symmetry. The only way to maintain volume conservation ( $\nabla \cdot \mathbf{v} = 0$ ) with vertical motion is for some fluid to move up while other fluid moves down, and for that to happen requires breaking horizontal symmetry. Once a tiny seed of horizontal asymmetry is presented to the fluid, effective buoyancy is sourced by  $\nabla_z^2 \rho \neq 0$ , which in turn allows the gravitational instability to grow.

#### *Vertically unstratified density*

Now consider a vertically unstratified density field,  $\rho = \rho(x, y)$ , so that the Archimedean buoyancy has no depth dependence. This vertically “neutrally buoyant” case commonly means that a fluid element can move vertically without feeling any buoyancy forces. Indeed, such is the case when referring to Archimedean buoyancy. What about effective buoyancy?

If density is a linear function of horizontal position then the effective buoyancy is a harmonic function so that  $b_{\text{eff}} = 0$ . If density is a nonlinear function of the horizontal then the effective buoyancy is nonzero. Yet is there vertical motion? Again we must confront the boundary conditions to answer this question. Here, the rigid top and bottom boundaries preclude movement of fluid across these boundaries by imparting a boundary pressure form stress (Chapter 19) acting throughout the fluid to counteract the effective buoyancy. As a result, the fluid remains static. If instead we allow for a free surface, then the effective buoyancy would cause vertical motion that then leads to horizontal convergences, thus leading to further motion. Alternatively, if we allow for depth dependence of the density, then fluid can move laterally as well as vertically.

#### *Localized source of Archimedean buoyancy*

Although useful to garner some understanding of effective buoyancy, the previous examples are not realistic. More realistic applications are concerned with Archimedean buoyancy sources localized in both the horizontal and vertical directions. In this case the buoyancy source,  $\nabla_z^2 \rho \neq 0$ , and boundary conditions lead to a nontrivial structure for the effective buoyancy through solving

the Poisson equation. Studies listed below offer examples, both analytical and numerical, to further an understanding of how effective buoyancy offers a more complete description of vertical acceleration than Archimedean buoyancy.

### 24.7.7 Comments and further study

Studies from [Davies-Jones \(2003b\)](#), [Doswell and Markowski \(2004\)](#), [Jeevanjee and Romps \(2015a\)](#), [Jeevanjee and Romps \(2015b\)](#), and [Tarshish et al. \(2018\)](#), point to the use of the effective buoyancy and the limitations of Archimedean buoyancy when studying buoyancy dominated motion, such as the early stages of a buoyant thermal. Much of the material in this section was gleaned from these papers, particularly from [Jeevanjee and Romps \(2015a\)](#) and [Jeevanjee and Romps \(2015b\)](#). Chapter 2 of [Markowski and Richardson \(2010\)](#) provides a pedagogical foundation for understanding pressure forces leading to vertical motion.

The structure of  $b_{\text{eff}}$  is distinct from the Archimedean buoyancy,  $b$ , with [Jeevanjee and Romps \(2015a\)](#) and [Tarshish et al. \(2018\)](#) providing examples where  $b$  and  $b_{\text{eff}}$  can even have opposite signs. Furthermore, [Tarshish et al. \(2018\)](#) made use of an elegant analogy between the Poisson equation for  $b_{\text{eff}}$  and the Poisson equation for certain magnetostatics problems. The analogy allowed them to derive analytical expressions for  $b_{\text{eff}}$  from spherical and elliptical Archimedean buoyancy sources.



## 24.8 Exercises

### EXERCISE 24.1: EXAMPLES OF BUOYANCY PERIOD

Using approximate but realistic values for the observed stratification, determine the buoyancy period ( $T_b = 2\pi/N$ ) for

- mid-latitude troposphere
- stratosphere
- ocean thermocline
- ocean abyss.

Provide references for where you obtained the observed stratification. Hint: for both the atmosphere and ocean, it is sufficient to assume stratification is dominated by potential temperature.

### EXERCISE 24.2: BUOYANCY FREQUENCY FOR AN IDEAL GAS

Derive equation (24.37) for the squared buoyancy frequency of an ideal gas. Hint: first derive the expression for the potential density and then take its vertical derivative as per equation (24.36).

### EXERCISE 24.3: VERTICAL INTEGRAL OF $N^2$

The expression for squared buoyancy frequency

$$N^2 = -g \left[ \frac{\partial \ln \varrho}{\partial z} \right]_{p_R=p} \quad (24.87)$$

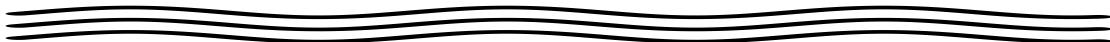
makes it tempting to consider its vertical integral according to

$$-g^{-1} \int_{-H}^{\eta} N^2 dz \stackrel{?}{=} [\ln \varrho]_{\eta} - [\ln \varrho]_{-H}. \quad (24.88)$$

Discuss what is wrong with this equation. Under what conditions is it correct?

**EXERCISE 24.4: WATER LEVEL OF A BOAT WITH AND WITHOUT A STONE**

Consider a boat floating in constant density water,  $\rho_w$ , contained in a tank with vertical sidewalls and cross-sectional area  $A$ . Place a stone of mass  $M_s$  and density  $\rho_s > \rho_w$  in the boat and measure the water level on the tank wall,  $h_1$ . Then throw the stone into the water. What is the new water level,  $h_2$ , as a function of  $h_1$  and the other properties listed above? Does the water level rise or fall along the sides of the tank as a result of throwing the stone over the side? Hint: Watch [this Physics Girl video](#).





# Chapter 25

## Rotating flows

Large-scale and low frequency flows in the atmosphere and ocean are strongly affected by planetary rotation. The inviscid balance for such flows is termed *geostrophic*, in which the planetary Coriolis acceleration balances the pressure gradient acceleration. In this chapter, we introduce salient features of geostrophically balanced flow and the associated *thermal wind balance*. These two diagnostic relations involve no time derivatives, and so cannot be used to predict the fluid flow evolution. However, they provide a very powerful framework for interpreting large-scale and low frequency flow in the atmosphere and ocean.

After studying the basic elements of rotating flow, we examine two case studies. The first concerns *inertial waves*, which are linear fluctuations that vertically mediate information about rotation. In particular, low frequency inertial waves impart a vertically stiffened nature to rotating flows, thus providing the physical mechanism for the *Taylor-Proudman effect*. The second case study concerns the distinctive nature of isopycnal form stresses associated with geostrophically balanced eddy motions. Such form stresses are a key feature of the earth's planetary energy balance, whereby positive buoyancy in the tropics is, in part, transported meridionally through the action of geostrophic eddies.

### READER'S GUIDE TO THIS CHAPTER

This chapter assumes an understanding of the primitive equations from Chapter 22 and the Coriolis acceleration from Chapters 9 and 10. The material in this chapter is fundamental to understanding the nature and mechanisms of large-scale flow in the atmosphere and ocean, so that we make great use of this chapter in the remainder of this book. Throughout the discussion we are not explicitly concerned with sphericity, thus enabling the use of Cartesian vector calculus.

Although the discussion of inertial waves in Section 25.6 is self-contained, the reader will benefit from having a basic understanding of kinematic features of linear waves, most of which will have been seen in an undergraduate physics course. Chapter 6 of [Vallis \(2017\)](#) provides a pedagogical review of wave kinematics for geophysical fluids.

25.1	Loose threads . . . . .	608
25.2	Primitive equations . . . . .	608
25.3	The Rossby number . . . . .	609
25.3.1	Scaling for the Rossby number . . . . .	609
25.3.2	Ratio of material acceleration to Coriolis acceleration . . . . .	610
25.3.3	Ratio of local time tendency to Coriolis acceleration . . . . .	610

25.3.4	Rossby number for a kitchen sink . . . . .	610
25.3.5	Rossby number for a Gulf Stream ring . . . . .	610
25.4	Geostrophic balance . . . . .	<b>611</b>
25.4.1	Geostrophic balance is distinctly fluid mechanical . . . . .	612
25.4.2	Geostrophic relation in geopotential coordinates . . . . .	612
25.4.3	Cyclonic and anti-cyclonic orientation . . . . .	612
25.4.4	Density gradients and thermal wind balance . . . . .	613
25.4.5	Geostrophic relation in pressure coordinates . . . . .	614
25.4.6	Further study . . . . .	614
25.5	Planetary geostrophic mechanics . . . . .	<b>614</b>
25.5.1	Planetary geostrophic equations . . . . .	614
25.5.2	Planetary geostrophic vorticity equation . . . . .	615
25.5.3	Taylor-Proudman and vertical stiffening . . . . .	616
25.5.4	Meridional motion in response to vortex stretching and stress curls	618
25.5.5	Sverdrup balance . . . . .	618
25.5.6	Features of thermal wind balanced flows . . . . .	619
25.5.7	Thermal wind balance for the atmosphere . . . . .	620
25.5.8	Further study . . . . .	622
25.6	Inertial waves . . . . .	<b>623</b>
25.6.1	Inertial oscillations of a fluid ring . . . . .	623
25.6.2	Formulation of the inertial wave equation . . . . .	624
25.6.3	Dispersion relation for inertial waves . . . . .	625
25.6.4	Group velocity . . . . .	626
25.6.5	Relating the velocity components . . . . .	626
25.6.6	“Near” inertial waves with $\varpi \approx \pm f $ . . . . .	627
25.6.7	Near zero frequency inertial waves . . . . .	627
25.6.8	Connecting to Taylor-Proudman . . . . .	628
25.6.9	Concerning other waves depending on Coriolis . . . . .	629
25.6.10	Further study . . . . .	629
25.7	Isopycnal form stress from geostrophic eddies . . . . .	<b>629</b>
25.7.1	Zonal mean zonal form stress on an isopycnal surface . . . . .	630
25.7.2	Zonal mean zonal form stress acting on an isopycnal layer . . . . .	631
25.7.3	Comments and further study . . . . .	633
25.8	Exercises . . . . .	<b>634</b>

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## 25.1 Loose threads

- Connect Section 25.6.1 to the rest of the inertial waves discussion.

## 25.2 Primitive equations

Throughout this chapter we make use of the inviscid hydrostatic primitive equations derived in Section 22.1

$$\partial \mathbf{u} / \partial t + (\mathbf{v} \cdot \nabla) \mathbf{u} + f \hat{\mathbf{z}} \times \mathbf{u} = -\rho^{-1} \nabla_z p \quad (25.1a)$$

$$\partial p / \partial z = -g \rho \quad (25.1b)$$

$$D\rho/Dt = -\rho \nabla \cdot \mathbf{v}, \quad (25.1c)$$

where the velocity vector is written using Cartesian coordinates

$$\mathbf{v} = \mathbf{u} + \hat{\mathbf{z}} w = \hat{\mathbf{x}} u + \hat{\mathbf{y}} v + \hat{\mathbf{z}} w, \quad (25.2)$$

and the horizontal gradient operator is

$$\nabla_z = \hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y. \quad (25.3)$$

For some of the scale analysis in this chapter we assume an oceanic Boussinesq fluid (Section 23.1), in which case the mass continuity equation (25.1c) becomes the non-divergent condition on the velocity

$$\nabla \cdot \mathbf{v} = 0. \quad (25.4)$$

Furthermore,  $\rho$  in the Boussinesq horizontal momentum equation (25.1a) is converted to a constant reference density,  $\rho_0$ , and yet it retains its full form when appearing in the hydrostatic equation since it is there multiplied by the gravitational acceleration.

## 25.3 The Rossby number

Large-scale geophysical fluid flows are strongly influenced by the earth's rotation. Indeed, the earth can be considered a rapidly rotating planet for much of the observed large-scale motion of the ocean and atmosphere. There are two points to emphasize in this regard. First, much of the ocean and atmosphere motion is close to solid-body rotation, in which weather patterns and ocean circulation are best viewed relative to the rotating earth rather than from an inertial frame. Second, human scale horizontal length scales are generally far too small to take a direct notice of the planetary rotation. This point is quantified by considering the *Rossby number*, which includes a horizontal length scale, a velocity scale, and angular rotation speed.

### 25.3.1 Scaling for the Rossby number

The Rossby number measures the ratio of the Coriolis acceleration to the material acceleration (acceleration of a fluid particle). The material acceleration has two contributions: one from local time tendencies and one from advection. We expose typical characteristic scales for the acceleration of a fluid particle by writing

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{u} \sim \frac{U}{T} + \frac{U^2}{L} + \frac{WU}{H}, \quad (25.5)$$

where  $U, W$  are typical horizontal and vertical velocity scales,  $L, H$  are typical horizontal and vertical length scales, and  $T$  is a typical time scale (recall a similar scale analysis for the hydrostatic balance in Section 22.2). Likewise, the Coriolis acceleration scales as

$$f \hat{\mathbf{z}} \times \mathbf{u} \sim f_0 U, \quad (25.6)$$

where  $f_0$  is the scale for the Coriolis parameter. From the continuity equation for non-divergent flow ( $\nabla \cdot \mathbf{v} = 0$ ) we see that the vertical and horizontal velocity scales are related by<sup>1</sup>

$$W/H \sim U/L \implies W \sim U(H/L). \quad (25.7)$$

In either non-divergent or divergent flows, we assume the vertical to horizontal grid aspect ratio is small

$$\alpha_{\text{aspect}} = H/L \ll 1, \quad (25.8)$$

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<sup>1</sup>For divergent flows we can replace  $W$  with the scale for motion across hydrostatic pressure surfaces.

as per the hydrostatic approximation discussed in Section 22.2. Consequently, the vertical velocity scale is much less than the horizontal

$$W \ll U. \quad (25.9)$$

### 25.3.2 Ratio of material acceleration to Coriolis acceleration

Taking the ratio of the advection scale to the Coriolis scale leads to our first expression for the Rossby number

$$\text{Ro} = \frac{U^2/L}{f_0 U} = \frac{U}{f_0 L}. \quad (25.10)$$

Due to the latitudinal variation of the Coriolis parameter, the Rossby number is generally small in magnitude near the poles and large in the tropics. This functional dependence is modified by noting that the length and velocity scales are not constant.

### 25.3.3 Ratio of local time tendency to Coriolis acceleration

A complementary way to understand the Rossby number is to consider it as the ratio of the local time tendency for the horizontal velocity to the Coriolis acceleration

$$\text{Ro} = \frac{U/T}{U f_0} = \frac{1/T}{f_0}. \quad (25.11)$$

Hence, the Rossby number is small for motions that have a frequency,  $T^{-1}$ , that is small compared to the *inertial frequency*,  $f_0$ . In both ways of writing the Rossby number, we associate small Ro with regimes of flow where the earth's rotation plays a crucial role in the dynamics. With small Rossby number, both the local time derivative and the advective acceleration are smaller than the Coriolis acceleration.

### 25.3.4 Rossby number for a kitchen sink

Consider flow in a kitchen sink (left panel of Figure 25.1). Here, the length scale is  $L = 1$  m (sink size) and the velocity scale is  $U = 0.01 - 0.1$  m s<sup>-1</sup>, thus giving a typical time scale for sink motion of  $L/U \approx 10$  s – 100 s. Hence, at 30° latitude, where  $f = 2\Omega \sin \phi = \Omega$ , the Rossby number for fluid motion in a sink is

$$\text{Ro}_{\text{sink}} \approx 10^2 - 10^3. \quad (25.12)$$

The effects from planetary rotation are tiny on these length scales, so that the Coriolis force is negligible for kitchen sink fluid dynamics. Hence, it is extremely difficult to experimentally determine a correlation between the hemisphere (northern or southern) to the rotational direction of water leaving a sink drain.

### 25.3.5 Rossby number for a Gulf Stream ring

For a Gulf Stream ring (right panel of Figure 25.1), the typical length scale is  $L = 10^5$  m and velocity scale is  $U = 0.1 - 1.0$  m s<sup>-1</sup>, thus leading to a time scale  $L/U \approx 10^5 - 10^6$  s. At 30° latitude the Rossby number is

$$\text{Ro}_{\text{ring}} \approx 10^{-2} - 10^{-1}. \quad (25.13)$$

Flow features of such large length scales can feel the planetary rotation so that the Coriolis acceleration is central to dynamics of Gulf Stream rings, as reflected in the small magnitude of the associated Rossby number.

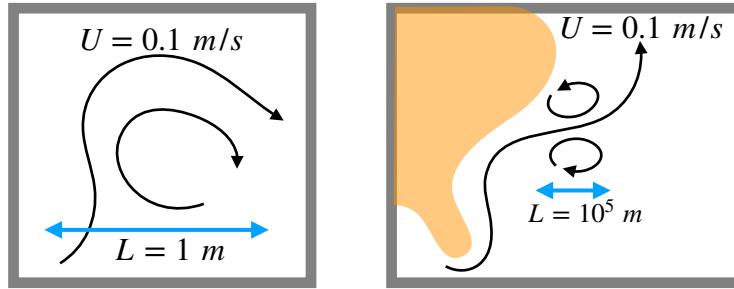


FIGURE 25.1: Estimating the Rossby number for flow in a kitchen sink (left panel) and rings spawned from the Gulf Stream (right panel). The kitchen sink has velocity scales on the order of  $U \sim 0.01 - 0.1 \text{ m s}^{-1}$  whereas Gulf Stream rings have velocity scales on the order  $U \sim 0.1 - 1.0 \text{ m s}^{-1}$ . Their length scales are much more distinct, with the scale for a sink  $L \sim 1 \text{ m}$  whereas for the Gulf Stream rings  $L \sim 10^5 \text{ m}$ . Taking the Coriolis parameter at  $30^\circ$  leads to  $\text{Ro}_{\text{sink}} \sim 10^2 - 10^3$  and  $\text{Ro}_{\text{ring}} \sim 10^{-2} - 10^{-1}$ . The planetary Coriolis acceleration is central to Gulf Stream ring dynamics whereas it is utterly negligible for the kitchen sink.

## 25.4 Geostrophic balance

Under the influence of horizontal pressure forces, a fluid accelerates down the pressure gradient (movement from high pressure to low pressure). In the presence of rotation, a nonzero horizontal velocity couples to the Coriolis parameter,  $f$ , thus giving rise to a nonzero horizontally oriented Coriolis acceleration  $-f \hat{z} \times \mathbf{u}$ . The Coriolis acceleration acts perpendicular to the fluid motion

$$\mathbf{u} \cdot (\hat{z} \times \mathbf{u}) = 0, \quad (25.14)$$

and as such it affects the fluid motion but does not alter kinetic energy; i.e., it does zero work on the fluid.<sup>2</sup> In the northern hemisphere where  $f > 0$ , the Coriolis acceleration acts to the right of the parcel motion, thus causing counter-clockwise motion around low pressure centers and clockwise motion around high pressure centers (Figure 25.3). In the southern hemisphere, where  $f < 0$ , the Coriolis acceleration acts in the opposite direction. So in summary, the geostrophic balance is a diagnostic relation where the pressure gradient acceleration balances the Coriolis acceleration so that the net acceleration acting on a fluid element is zero. In Figure 25.2 we offer a heuristic model to help understand the geostrophic balance and remember its orientation.

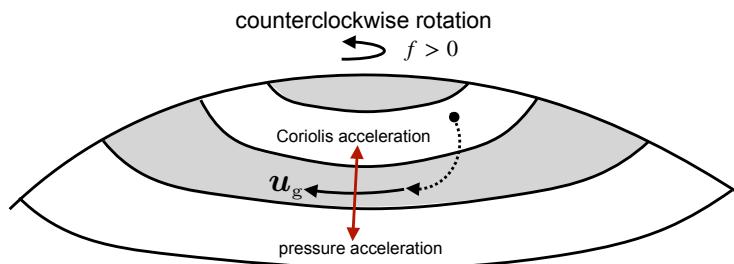


FIGURE 25.2: A particle on a rotating and frictionless hill as a model to help understand geostrophic balance. As the particle moves downhill it picks up a rightward component to its trajectory as a result of the Coriolis acceleration. Equilibrium arises when the downhill pressure gradient acceleration balances the uphill Coriolis acceleration. The downhill gravitational acceleration acting on the particle is the analog of an equatorward pressure acceleration acting on a fluid element.

<sup>2</sup>These characteristics of the Coriolis acceleration are directly analogous to the Lorentz force in electrodynamics (Jackson, 1975).

### 25.4.1 Geostrophic balance is distinctly fluid mechanical

When pressure and Coriolis forces balance, parcel motion is said to be in *geostrophic* balance, whereby large-scale atmospheric winds and ocean currents generally follow isobars (lines of constant pressure). Recall from Chapter 9 that point particles also experience a Coriolis acceleration when viewed in a rotating reference frame. However, geostrophic balance is not afforded to particles since particles do not experience a pressure force that can balance the Coriolis force. Hence, the geostrophic balance is a distinctly fluid mechanical phenomena.

### 25.4.2 Geostrophic relation in geopotential coordinates

The geostrophic balance becomes important when the Rossby number is small. When the Rossby number is small and friction is negligible, the leading order dynamical balance in the horizontal momentum equation (25.1a) is between the Coriolis acceleration and horizontal pressure gradient acceleration

$$f \hat{z} \times \mathbf{u}_g = -\rho^{-1} \nabla_z p, \quad (25.15)$$

or equivalently, we have the expression for the geostrophic velocity<sup>3</sup>

$$\mathbf{u}_g = \frac{\hat{z} \times \nabla p}{f \rho} \implies u_g = -\frac{1}{f \rho} \frac{\partial p}{\partial y} \quad \text{and} \quad v_g = \frac{1}{f \rho} \frac{\partial p}{\partial x}. \quad (25.16)$$

Note that the equator is special since the Coriolis parameter,  $f = 2\Omega \sin \phi$ , vanishes, thus precluding the relevance of geostrophy near the equator. Instead, at the equator flow generally moves down the horizontal pressure gradient since there is no Coriolis acceleration to turn the flow.

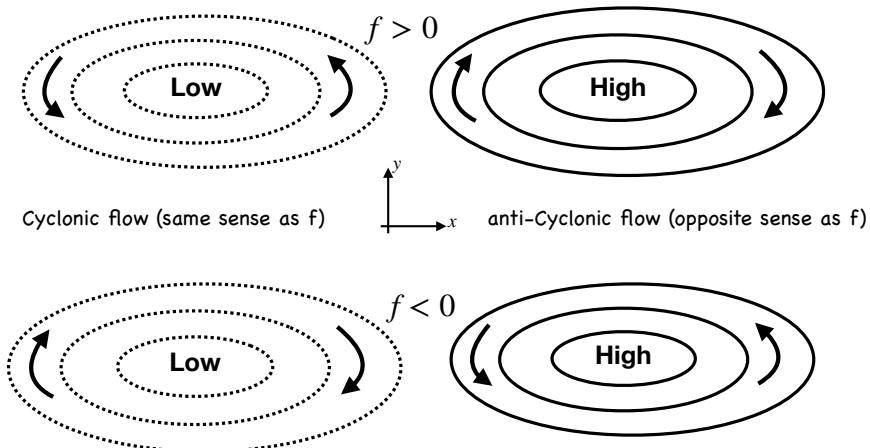


FIGURE 25.3: Geostrophic motion around low and high pressure centers in the northern hemisphere and southern hemisphere ( $f = 2\Omega \sin \phi > 0$  in the north and  $f < 0$  in the south). Upper panel: the counter-clockwise motion around the low pressure center in the northern hemisphere is in the same sense as the planetary rotation, and is thus termed cyclonic. Cyclonic motion in the southern hemisphere occurs in a clockwise direction, again corresponding to the planetary rotation direction as viewed from the south. Geostrophic motion around a high pressure center is counter to the planetary rotation in both hemispheres, and is thus termed anti-cyclonic.

### 25.4.3 Cyclonic and anti-cyclonic orientation

When oriented in the same sense as the earth's rotation (i.e., same sign of the Coriolis parameter) rotational motion is said to be in a *cyclonic* sense. Oppositely oriented motion is *anti-cyclonic*.

<sup>3</sup>We can write either  $\nabla$  or  $\nabla_z$  in equation (25.16). The reason is that the  $\hat{z} \times$  operator selects only the horizontal portion of the gradient.

For example, geostrophic motion around a low pressure center in the northern hemisphere is counter-clockwise (Figure 25.3). Using the right hand rule, this motion represents a positively oriented rotation. Hence, with  $f > 0$  in the north, counter-clockwise motion is cyclonic. In the southern hemisphere, geostrophic motion around a low pressure center is clockwise, which is a negatively oriented rotational motion (again, recall the right hand rule). In the south where  $f < 0$ , clockwise motion around a low pressure center represents cyclonic motion (Figure 25.3).

#### 25.4.4 Density gradients and thermal wind balance

The horizontal momentum is affected by horizontal pressure gradient forces. Furthermore, the hydrostatic balance says that the vertical derivative of the horizontal pressure gradient is determined by horizontal density gradients

$$\frac{\partial(\nabla_z p)}{\partial z} = -g \nabla_z \rho. \quad (25.17)$$

Hence, in the presence of horizontal density gradients, the horizontal pressure gradient forces are depth dependent. Correspondingly, the horizontal velocity field experiences a depth dependent pressure force.

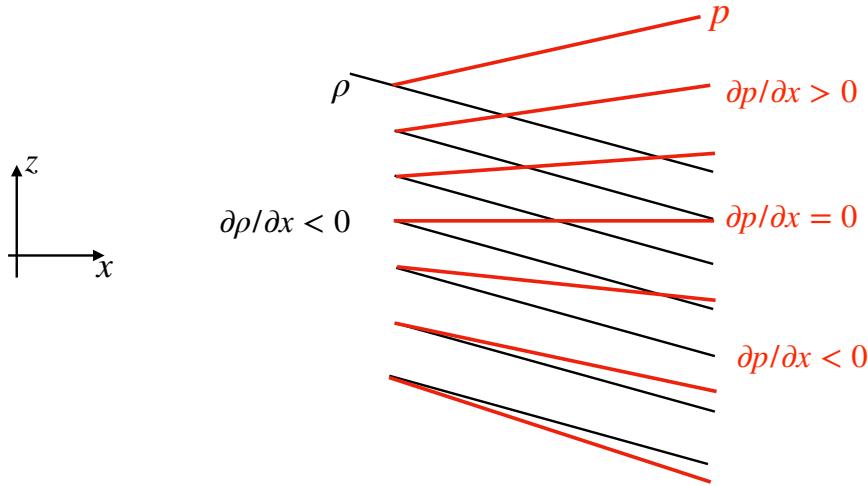


FIGURE 25.4: Horizontal density gradients support a vertical dependence to the horizontal gradient of the hydrostatic pressure via  $\partial(\nabla_z p)/\partial z = -g \nabla_z \rho$ . This figure depicts a constant horizontal density gradient with  $\partial \rho / \partial x < 0$ , thus leading to an increase in the zonal pressure gradient with height,  $\partial(\partial p / \partial x) / \partial z > 0$ . Depending on the thickness of the fluid column, the horizontal pressure gradient can change sign when moving up in the column, as shown here. Compare this figure to Figure 22.2, which discusses how to compute horizontal pressure gradients in a hydrostatic fluid.

We illustrate this depth dependence in Figure 25.4 with a depth independent horizontal density gradient,  $\partial \rho / \partial x = \text{constant} < 0$ , thus leading to a depth dependent horizontal gradient in the hydrostatic pressure. This figure also illustrates how the sign of the horizontal pressure gradient can change when moving in the vertical, depending on the value of the gradient at depth. It also illustrates how horizontal density gradients lead to a nonzero baroclinicity vector

$$\mathbf{B} = \frac{\nabla \rho \times \nabla p}{\rho^2}. \quad (25.18)$$

As shown in Section 35.5, a nonzero baroclinicity imparts a torque on fluid elements that acts as a source for vorticity.

The depth dependence to the horizontal pressure gradient leads to a vertical shear in the

horizontal geostrophic velocity

$$\frac{\partial(\rho f \mathbf{u}_g)}{\partial z} = \hat{\mathbf{z}} \times \nabla(\partial p / \partial z) = -g \hat{\mathbf{z}} \times \nabla \rho. \quad (25.19)$$

This connection between horizontal density gradients and vertical shears in the geostrophic velocity is known as the *thermal wind balance*, which we return to in Section 25.5.6.

### 25.4.5 Geostrophic relation in pressure coordinates

The hydrostatic balance

$$\partial p / \partial z = -\rho g \quad (25.20)$$

can be used to eliminate density from the geostrophic balance (25.15) to render

$$f \hat{\mathbf{z}} \times \mathbf{u}_g = \frac{g \nabla_z p}{\partial p / \partial z}. \quad (25.21)$$

The right hand side is minus the lateral gradient of the geopotential,  $\Phi = g z$ , as computed along surfaces of constant pressure<sup>4</sup>

$$f \hat{\mathbf{z}} \times \mathbf{u}_g = -\nabla_p \Phi \implies f \mathbf{u}_g = \hat{\mathbf{z}} \times \nabla_p \Phi. \quad (25.22)$$

This is a useful expression of geostrophy for the compressible atmosphere.

### 25.4.6 Further study

Visualizations from rotating tank experiments provide very useful illustrations of the Coriolis acceleration and geostrophic balance, such as the experiments shown near the 10 minute mark in [this video from Prof. Fultz](#).

## 25.5 Planetary geostrophic mechanics

We here introduce the planetary geostrophic (PG) equations, which have found great use in describing elements of the large-scale laminar ocean circulation. We state the equations and discuss their physical implications, deferring a systematic derivation for later. In particular, the shallow water PG equations are derived in Section 38.4 and the continuously stratified PG equations are derived in Section 39.3.

### 25.5.1 Planetary geostrophic equations

The governing equations for planetary geostrophy are based on the hydrostatic Boussinesq equations stated in Section 23.1.7, with the assumption of a steady state linear and frictional-/geostrophic balance for the horizontal momentum

$$\rho_0 f (\hat{\mathbf{z}} \times \mathbf{u}) = -\nabla p - \rho g \hat{\mathbf{z}} + \partial \boldsymbol{\tau} / \partial z \quad (25.23a)$$

$$\nabla_z \cdot \mathbf{u} + \partial w / \partial z = 0 \quad (25.23b)$$

$$Db / Dt = \dot{b}. \quad (25.23c)$$

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<sup>4</sup>See Section 41.12.2 for details of computing derivatives using generalized vertical coordinates.

The stress,  $\boldsymbol{\tau}$ , acts just in the horizontal directions so that the vertical component of the momentum equation (25.23a) is the hydrostatic balance

$$\partial p / \partial z = -\rho g. \quad (25.24)$$

We now list some of the key physical attributes captured by these equations.

#### *Velocity is determined by buoyancy*

The only time derivative appearing in the PG equations appears in the buoyancy equation (25.23c). All other equations are diagnostic. As the buoyancy evolves, the hydrostatic pressure changes and so too does the geostrophic velocity. Hence, the velocity is determined by the buoyancy field.

#### *Planetary geostrophy admits no turbulence*

The momentum equation is linear since PG drops the nonlinear advection of momentum. Hence, there is no turbulence in the planetary geostrophic fluid since turbulence relies on the nonlinear momentum advection. Instead, planetary geostrophy is used to describe laminar ocean circulation features at the large-scales.

#### *Vertical transfer of horizontal momentum and subgrid scale parameterizations*

We introduced a horizontal stress (dimensions of force per area) into the momentum equation

$$\boldsymbol{\tau} = (\tau^x, \tau^y, 0). \quad (25.25)$$

This stress is associated with vertical transfer of horizontal momentum in the ocean interior through vertical viscosity, as well as vertical transport of momentum from the atmosphere to the ocean. The vertical stress is enhanced by waves and turbulent features such as mesoscale eddies. However, such transient processes are not represented by planetary geostrophy. Hence, they must be parameterized, which generally leads to an enhanced vertical viscosity relative to that from molecular viscosity. In general, all models (analytic or numerical) of planetary scale circulations are too coarse to resolve the scales over which molecular viscosity dominates the frictional dissipation. Consequently, it is necessary to provide rational *subgrid-scale (SGS) parameterizations* of the variety of physical processes that are unresolved by the model. We have more to say about the parameterization of vertical transfer of horizontal momentum in Section 48.3.5.

### 25.5.2 Planetary geostrophic vorticity equation

The vertical component of relative vorticity is given by

$$\zeta = \partial v / \partial x - \partial u / \partial y, \quad (25.26)$$

with a thorough discussion of vorticity given in Chapter 35. Here, we form the relative vorticity budget for the planetary geostrophic system by taking the curl of the momentum equation.

*Curl of the PG momentum equation*

Taking the curl of the momentum equation (25.23a), and rearranging terms, leads to the planetary geostrophic vorticity equation

$$-\rho_o f \frac{\partial \mathbf{u}}{\partial z} + \hat{z} \rho_o \nabla \cdot (\mathbf{f} \mathbf{u}) = -g \nabla \times (\hat{z} \rho) + \frac{\partial (\nabla \times \boldsymbol{\tau})}{\partial z}. \quad (25.27)$$

Note that  $\nabla \cdot (\mathbf{f} \mathbf{u}) = \nabla_z \cdot (\mathbf{f} \mathbf{u})$  since  $\mathbf{u}$  is the horizontal velocity vector. Introducing the Archimedean buoyancy (Section 23.1.2)

$$b = -g(\rho - \rho_o)/\rho_o \quad (25.28)$$

leads to

$$-\mathbf{f} \frac{\partial \mathbf{u}}{\partial z} + \hat{z} \nabla_z \cdot (\mathbf{f} \mathbf{u}) = \nabla \times (\hat{z} b) + \frac{1}{\rho_o} \frac{\partial (\nabla \times \boldsymbol{\tau})}{\partial z}. \quad (25.29)$$

*Pressure gradients are removed from the vorticity equation*

One of the key reasons to study vorticity is that its evolution equation is not explicitly affected by the pressure gradient since the curl of the pressure gradient vanishes. Eliminating the pressure force affords a simpler evolution equation for vorticity, and we pursue that evolution more thoroughly in Chapter 35. Pressure perturbations are rapidly transferred in a fluid, either by acoustic waves in divergent flows (Section 17.5) or instantaneously in non-divergent flows (Section 23.3). Hence, in the absence of pressure directly affecting the vorticity equation, contributions to vorticity evolution are more localized in space than contributions to velocity evolution.

*Relative vorticity is absent from the PG vorticity equation*

It is notable that there is no appearance of the relative vorticity,  $\zeta = \partial_x v - \partial_y u$ , in the planetary geostrophic vorticity equation (25.23a). The reason is that we dropped the material time derivative of velocity when forming the planetary geostrophic momentum equation (25.23a). By doing so, we drop all expressions of  $\zeta$  in the vorticity equation. Planetary geostrophy is valid for those cases where

$$|\zeta| \ll |f|, \quad (25.30)$$

which means the absolute vorticity (sum of planetary vorticity plus relative vorticity) is dominated by the planetary vorticity. We encounter more complete versions of the vorticity equation in Chapter 35 where we do not make the planetary geostrophic assumption.

Rather than taking the curl of the planetary geostrophic momentum equation, we could have also derived the vorticity equation (25.29) by taking planetary geostrophic scaling in the full vorticity equation. We choose here the path through the planetary geostrophic momentum equation since we have yet to discuss the full vorticity equation (see Chapter 35).

### 25.5.3 Taylor-Proudman and vertical stiffening

Consider the vorticity equation (25.29) on an  $f$ -plane with zero friction, in which the horizontal geostrophic motion is horizontally non-divergent

$$\nabla_z \cdot \mathbf{u} = 0 \quad f\text{-plane geostrophy.} \quad (25.31)$$

Use of continuity (equation (25.23b)) means there is no vertical stretching of a vertical material line element (Section 13.3.6)

$$\partial w / \partial z = 0. \quad (25.32)$$

As shown in Chapter 35, a vortex tube exhibits the same kinematics as a material line element described in Section 13.3. Hence,  $\partial w / \partial z = 0$  means there is no vertical stretching of a vortex tube in the planetary geostrophic fluid. This result has important implications that we now describe.

#### *Flat bottom boundary and columnar motion*

If there is a solid flat bottom to the domain, then the vertical velocity vanishes at that surface. With  $\partial_z w = 0$  in the interior as well, then  $w$  vanishes throughout the domain. Hence, the fluid has zero vertical velocity, and motion occurs on horizontal planes perpendicular to the rotation axis; i.e., the flow is two-dimensional. We furthermore assume zero horizontal buoyancy gradients, so that the vorticity equation (25.29) implies that the horizontal velocity has zero vertical shear

$$\partial \mathbf{u} / \partial z = 0 \quad f\text{-plane and homogeneous density.} \quad (25.33)$$

This result is known as the *Taylor-Proudman effect*, with Figure 25.5 providing an illustration.

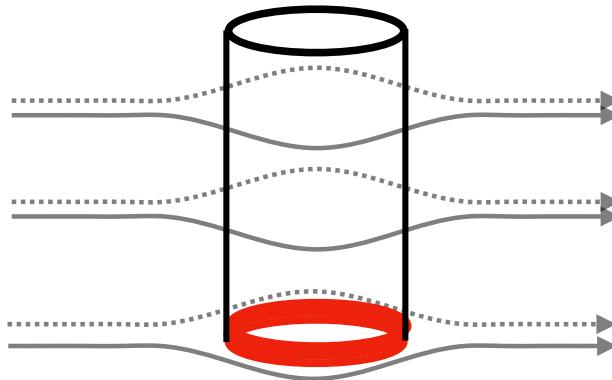


FIGURE 25.5: The Taylor-Proudman effect (25.33) says that horizontal flow in a homogeneous rapidly rotating fluid over a flat bottom (where  $w = 0$ ) is depth-independent. Hence, when flow encounters an obstacle anywhere in the column, such as the red ring shown here at the bottom, then flow throughout the full depth coherently moves around the obstacle. The result is a vertically stiffened motion known as *Taylor columns*.

#### *Relevance to the ocean and atmosphere*

In the ocean and atmosphere, the assumptions leading to the Taylor-Proudman effect are rarely satisfied due to the presence of stratification (i.e., vertical density variations), and a sloping solid earth bottom. Nonetheless, there is a tendency for vertical velocities to be quite small due to the effects of rotation; even smaller than the non-divergent flow scaling  $W/H \sim U/L$  would indicate (see Section 25.3.1). Additionally, for unstratified or linearly stratified fluids, there is a tendency for geostrophic turbulence to cascade energy into the *gravest vertical mode*; i.e., the largest vertical scale. This largest vertical scale mode is termed the *barotropic mode*, and motion of this mode is predominantly horizontal and depth independent. Smaller vertical scales of variation are captured by an infinite hierarchy of *baroclinic modes*. The process of moving energy to the barotropic mode is referred to as *barotropization*.

### 25.5.4 Meridional motion in response to vortex stretching and stress curls

The vertical component to the vorticity balance (25.29) leads to

$$\nabla_z \cdot (f \mathbf{u}) = \frac{1}{\rho_0} \hat{\mathbf{z}} \cdot \partial (\nabla \times \boldsymbol{\tau}) \quad (25.34)$$

which can be written

$$\beta v = -f \nabla_z \cdot \mathbf{u} + \frac{1}{\rho_0} \hat{\mathbf{z}} \cdot \partial (\nabla \times \boldsymbol{\tau}) \quad (25.35)$$

where

$$\beta = \partial f / \partial y \quad (25.36)$$

is the gradient of planetary vorticity. The continuity equation (25.23b) can be used to remove the horizontal divergence, which yields the vorticity balance

$$\beta v = f \frac{\partial w}{\partial z} + \frac{1}{\rho_0} \hat{\mathbf{z}} \cdot \partial (\nabla \times \boldsymbol{\tau}). \quad (25.37)$$

The left hand side is the meridional advection of planetary vorticity. The first term on the right hand side arises from vortex stretching by planetary vorticity; i.e., planetary induction or the  $\beta$ -effect discussed in Section 35.7.2. The second term is the vertical divergence of the curl of the stress.

Reading the vorticity equation (25.37) from right to left indicates that any process leading to a vorticity source via vortex stretching or wind stress curls must be balanced by meridional motion. That is, the fluid responds to vortex stretching and wind curls by moving meridionally through the planet's vorticity field. In a fluid that maintains planetary geostrophic balance, meridional movement is the only means for it to respond to vorticity input since its vorticity is set by planetary vorticity. Conversely, reading the equality (25.37) from the left to the right reveals that any meridional motion itself must be balanced by vortex stretching plus wind stress curls. We study the depth integrated form of this vorticity equation in Section 39.5, where we see how the depth integrated meridional flow is affected by stretching created by boundary torques.

### 25.5.5 Sverdrup balance

Depth integrating the vorticity balance (25.37) over the full depth of an ocean column leads to

$$\beta V = f [(w(\eta) - w(\eta_b))] + \hat{\mathbf{z}} \cdot \nabla \times [\boldsymbol{\tau}(\eta) - \boldsymbol{\tau}(\eta_b)] / \rho_0, \quad (25.38)$$

where

$$V = \int_{\eta_b}^{\eta} v \, dz \quad (25.39)$$

is the depth integrated meridional velocity. For the large-scale we generally assume the surface vertical velocity is small, with  $w(\eta) = 0$  when making the *rigid lid approximation*. Further assuming a flat bottom allows us to drop the vertical velocity at the ocean bottom,  $w(\eta_b) = 0$ . Additionally, the surface turbulent stress is often far larger than the bottom turbulent stress. These assumptions then lead to the *Sverdrup balance*, which is a balance between the depth integrated meridional motion and the curl of the surface turbulent stress

$$\rho_0 \beta V_{\text{Sverdrup}} = \hat{\mathbf{z}} \cdot \nabla \times \boldsymbol{\tau}(\eta) \quad \text{Sverdrup balance.} \quad (25.40)$$

As further discussed in Section 35.10.4, the most problematic aspect of this balance concerns the assumption of vanishing  $w(\eta_b)$ , with  $w(\eta_b)$  generally non-negligible in regions with sloping side boundaries. We also discuss a variant of this balance, known as the *geostrophic Sverdrup balance*, in Section 39.6.

### 25.5.6 Features of thermal wind balanced flows

Horizontal components to the inviscid vorticity equation (equation (25.29) with  $\tau$  set to zero) form the thermal wind balance

$$f \partial \mathbf{u} / \partial z = -\nabla \times (\hat{\mathbf{z}} b) = \hat{\mathbf{z}} \times \nabla b, \quad (25.41)$$

which takes on the component form

$$f \partial u / \partial z = -\partial b / \partial y \quad \text{and} \quad f \partial v / \partial z = \partial b / \partial x. \quad (25.42)$$

As seen already in Section 25.4.4, these relations can also be derived directly from taking the vertical derivative of the horizontal momentum equation (25.23a) and then using the horizontal gradient of the hydrostatic balance (25.24). In either case, the thermal wind balance (25.41) says that the horizontal geostrophic velocity possesses a vertical shear where the buoyancy field has a horizontal gradient. Buoyancy with a horizontal gradient is termed *baroclinic* since it leads to a nonzero baroclinicity vector that provides a source for vorticity (see Section 35.8.2). Correspondingly, it is only the baroclinic (depth dependent) piece of geostrophic velocity that is related to horizontal buoyancy gradients. The depth-independent flow is not constrained by horizontal buoyancy gradients.

#### *Thermal wind, the atmospheric jet stream and the Antarctic Circumpolar Current*

Due to the increased solar radiation reaching the equator relative to the poles, the zonal averaged temperature generally reduces poleward. This poleward reduction in temperature corresponds to a poleward reduction in buoyancy. Also, for a stably stratified fluid, density increases with depth so that buoyancy decreases. Figure 25.6 illustrates this situation.

A zonal average around a zonally symmetric globe, such as in the Antarctic Circumpolar Current, removes all zonal variations, thus putting  $\partial_x \rho = 0$  and so rendering the zonally averaged thermal wind relation

$$f \frac{\partial \bar{u}}{\partial z} = \frac{g}{\rho_o} \frac{\partial \bar{\rho}}{\partial y} = -\frac{\partial \bar{b}}{\partial y} > 0, \quad (25.43)$$

where  $(\bar{\ })$  is the zonal mean operator. In the northern hemisphere,  $\partial_y \bar{b} < 0$ , so that the zonal averaged thermal wind shear is positive,  $\partial_z \bar{u} > 0$ . For example, a westerly zonal wind (blowing to the east) strengthens with height (easterly thermal wind shear). In the Southern Hemisphere,  $f < 0$  with poleward decreasing buoyancy,  $\partial_y \bar{b} > 0$ , means there is also an eastward thermal wind shear. Note that movement towards the poles, where  $|f|$  increases, leads to a smaller thermal wind shear given the same buoyancy gradient.

#### *Diagnosing geostrophic velocity from the buoyancy field*

Vertical integration of the thermal wind relation (25.41) between two constant depth surfaces leads to

$$\mathbf{u}(z) = \mathbf{u}(z_{\text{ref}}) - f^{-1} \nabla \times \hat{\mathbf{z}} \int_{z_{\text{ref}}}^z b \, dz. \quad (25.44)$$

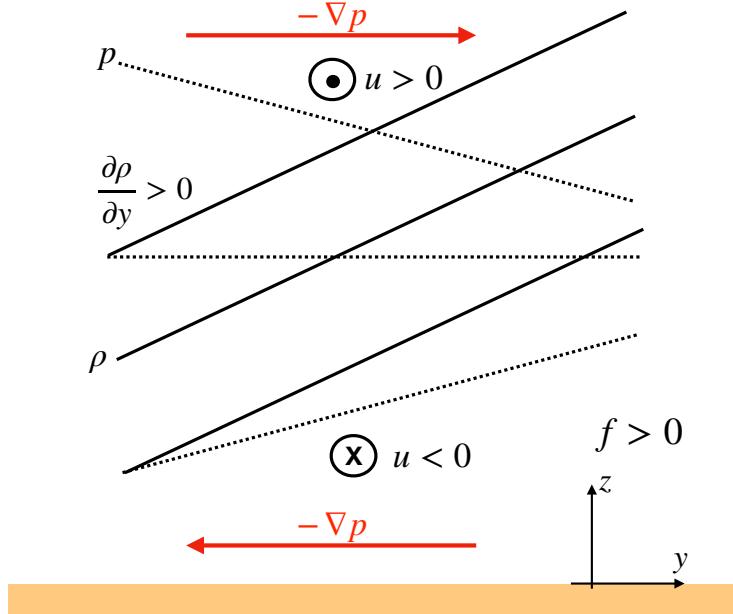


FIGURE 25.6: Schematic of the density and hydrostatic pressure fields and the associated thermal wind balanced flow in the northern hemisphere ( $f > 0$ ) with north to the right and east out of the page. We show surfaces of constant density (solid lines) and constant pressure (isobars; dashed lines). Density increases poleward ( $\partial\rho/\partial y > 0$ ) so that, according to the discussion surrounding Figure 25.4, the meridional pressure gradient decreases when moving upward,  $\partial(\partial p/\partial y)/\partial z = -g \partial_y \rho < 0$ . We illustrate isobars with an equatorward directed down gradient pressure force at lower elevations ( $-\partial p/\partial y < 0$ ) and poleward directed pressure force at higher elevations ( $-\partial p/\partial y > 0$ ). The zonal geostrophic wind is in geostrophic balance with these pressure gradients, with a westward zonal flow at lower elevations (easterly winds) and eastward flow at higher elevations (westerly winds). This flow configuration creates an eastward vertical shear of the zonal geostrophic winds,  $\partial u_g/\partial z > 0$ .

Hence, knowledge of the buoyancy field (e.g., through hydrographic measurements of temperature and salinity in the ocean), along with knowledge of the geostrophic velocity at a single depth, allows for determination of the full geostrophic velocity in terms of density. Unfortunately, specification of the unknown reference velocity is unavailable just from hydrographic measurements. This is the origin of the *depth of no motion* problem in diagnostic oceanography.

### 25.5.7 Thermal wind balance for the atmosphere

The large-scale atmosphere is compressible and approximately in hydrostatic balance. The expression for geostrophic balance (25.22) in pressure coordinates is a suitable starting point to derive thermal wind for the atmosphere. For this purpose, we take the pressure derivative,  $\partial/\partial p$ , of (25.22) to render

$$f \frac{\partial \mathbf{u}}{\partial p} = \hat{\mathbf{z}} \times \nabla_p \left[ \frac{\partial \Phi}{\partial p} \right], \quad (25.45)$$

with  $\Phi = g z$  the geopotential. The hydrostatic relation  $\partial p/\partial z = -\rho g$  takes the form

$$\frac{\partial p}{\partial \Phi} = -\rho \Rightarrow \frac{\partial \Phi}{\partial p} = -1/\rho \quad (25.46)$$

in which case

$$f \frac{\partial \mathbf{u}}{\partial p} = -\hat{\mathbf{z}} \times \nabla_p (1/\rho). \quad (25.47)$$

*Ideal gas atmosphere*

The specific volume takes the following form for an ideal gas atmosphere (see Section 20.12.1)

$$\rho^{-1} = R^M T/p. \quad (25.48)$$

Since the horizontal derivative in the thermal wind relation (25.47) is along pressure surfaces, we have

$$f \frac{\partial \mathbf{u}}{\partial p} = -\frac{R^M}{p} [\hat{\mathbf{z}} \times \nabla_p T]. \quad (25.49)$$

This expression gives rise to the name “thermal wind”, with vertical shears of the horizontal velocity generated by horizontal temperature gradients along isobars.

As for the ocean in equation (25.44), we vertically integrate the thermal wind expression (25.49), here between two pressure levels

$$\mathbf{u}(p_A) - \mathbf{u}(p_B) = f^{-1} R^M \hat{\mathbf{z}} \times \nabla_p \left[ \int_{p_A}^{p_B} \frac{T dp}{p} \right], \quad (25.50)$$

where  $p_A < p_B$ , so that  $p_A$  is at a higher altitude than  $p_B$ . We define the thermal wind shear as the difference between the wind aloft (higher altitude and lower pressure) from that at a lower altitude (greater pressure)

$$\mathbf{u}_T = \mathbf{u}(p_A) - \mathbf{u}(p_B) \quad \text{with } p_A < p_B \quad (25.51)$$

so that

$$\mathbf{u}_T = \frac{R^M}{f} \hat{\mathbf{z}} \times \nabla_p \bar{T}^{\ln p}, \quad (25.52)$$

where we introduced the log-pressure weighted temperature between the two pressure surfaces

$$\bar{T}^{\ln p} = \int_{p_A}^{p_B} \frac{T dp}{p}. \quad (25.53)$$

The relation (25.52) means that on the  $f$ -plane,  $R^M/f$  times the log-pressure weighted temperature serves as a streamfunction for the thermal wind shear. Reconsider the previous example where the polar regions are colder than tropics, so that in the northern hemisphere on pressure surfaces,  $\partial \bar{T}^{\ln p} / \partial y < 0$ . Hence, the zonal westerly winds increase in magnitude with height. We depict this situation in Figure 25.7. Furthermore, the thermal wind shear points to the east. For a more general flow in the northern hemisphere, cold air sits on the left side of the thermal wind shear and warm air on the right. The opposite orientation holds for the southern hemisphere where the Coriolis parameter is negative,  $f < 0$

*Barotropic flow*

Return to the thermal wind equation (25.47)

$$f \frac{\partial \mathbf{u}}{\partial p} = -\hat{\mathbf{z}} \times \nabla_p (1/\rho) = \frac{\hat{\mathbf{z}} \times \nabla_p \rho}{\rho^2}. \quad (25.54)$$

For the special case of density a function just of the pressure,  $\rho = \rho(p)$ , then  $\nabla_p \rho = 0$ . This situation defines a *barotropic* flow, which is characterized here by a horizontal geostrophic velocity with zero vertical variations. Note that we are here only concerned with the geostrophic flow. A density related to pressure through  $\rho = \rho(p)$  can still support vertical variations of the ageostrophic

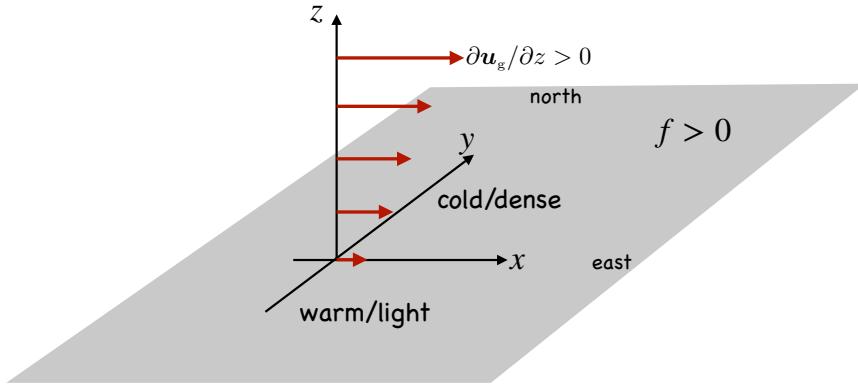


FIGURE 25.7: Thermal wind shear in the northern hemisphere ( $f > 0$ ) middle latitude atmosphere, whereby cold/dense air sits to the north and warm/light air to the south. The zonal geostrophic winds increase to the east when rising in elevation,  $\partial u_g / \partial z > 0$ . We say that the zonal winds have an eastward thermal wind shear. In general, a geostrophic wind in the northern hemisphere atmosphere has cold/dense air to the left when facing downwind, whereas the opposite orientation holds for the southern hemisphere where  $f < 0$ .

flow.

We further discuss barotropic flow in Section 35.3 as part of our study of vorticity. As detailed in that discussion, the general definition of a barotropic flow is one whereby the *baroclinicity* vector vanishes,  $\mathbf{B} = \nabla p \times \nabla(1/\rho) = 0$ . The functional relation  $\rho = \rho(p)$  (equivalently  $p = p(\rho)$ ) is a sufficient condition for vanishing baroclinicity. As seen in Section 35.5, for a barotropic flow there is no generation of vorticity through the torques created when density isosurfaces deviate from pressure isosurfaces (isobars).

### 25.5.8 Further study

Much of the material in this section forms the basis for laminar theories of the large-scale ocean circulation. Many of the concepts are detailed in Chapter 7 of [Marshall and Plumb \(2008\)](#). Chapters 19-22 of [Vallis \(2017\)](#) as well as [Samelson \(2011\)](#) present ocean circulation theory making use of fundamental concepts of geophysical fluid dynamics. A compelling discussion of the cascade of energy from the baroclinic modes to barotropic mode is offered by [Smith and Vallis \(2001\)](#). [Gill \(1982\)](#) provides a discussion of the depth of no motion problem in dynamic oceanography.

Rotating tank laboratory experiments offer a powerful means to explore the variety of rotating fluid mechanics relevant to the atmosphere and oceans. The following resources exemplify the Taylor-Proudman effect (25.33) and the associated vertical stiffening of rotating fluids.

- One means to test Taylor-Proudman is to insert a dye into a rapidly rotating tank of unstratified water. After a few rotation periods the dye forms vertical sheets known as *Taylor curtains* whose center is along the rotation axis. The fluid is said to have a *vertical stiffness* due to the effects of rotation. Vertical stiffening in turn means that flow over a small obstacle is deflected throughout the column rather than just near the bump. This situation is depicted in Figure 25.5 and more vividly illustrated in [this video from the UCLA SpinLab](#).
- Near the 20 minute mark of [this video, also from UCLA](#), we see how vortices in a rotating fluid maintain their coherency much more than in a non-rotating fluid.
- Another laboratory test shown in [this video from Prof. Fultz](#) shows that a buoyant object (a ping pong ball) placed into a rotating tank rises much slower than in a non-rotating tank.

The reason for the slower rise is that the ball must push up against the vertically stiffened fluid column when rotating, thus slowing its rise relative to when in a non-rotating fluid. Later in the same video, near the 16 minute mark, we see Taylor curtains in rotating fluids.

## 25.6 Inertial waves

The vertical stiffness exhibited by the Taylor-Proudman effect (Section 25.5.3) has a somewhat magical appearance. As with any apparent action at a distance in classical physics, the causal mechanism for this effect arises through waves. Here, we study the *inertial waves* that provide the mechanism for mediating vertical stiffening. We expose the basics of inertial waves in a homogeneous and constantly rotating fluid without boundaries. We are somewhat descriptive since a more deductive presentation requires a bit more wave theory than offered in this book.

### 25.6.1 Inertial oscillations of a fluid ring

In Section 10.5 we studied the free motion of a point particle viewed from a rotating reference frame, whereby the particle exhibited anti-cyclonic *inertial oscillations* with period  $2\pi/f$ . Here we extend that study to the case of a fluid. To start the investigation, consider a coherent circular fluid ring within the horizontal plane. Let the plane be rotating about the vertical axis,  $\Omega = \Omega \hat{z}$ , that extends through the center of the ring (Figure 25.8). Now perturb the ring by expanding its radius outward, which then gives the ring a larger moment of inertia as computed relative to the rotational axis. As we saw when studying axial angular momentum in Sections 10.7, 10.8, and 17.4, the constraint imposed by angular momentum computed relative to the  $\hat{z}$  axis requires the ring to rotate anti-cyclonically (clockwise if  $\Omega > 0$ ). As it rotates, each fluid particle within the ring experiences a Coriolis acceleration pointing towards the center of the ring (to the right of the particle motion). This Coriolis acceleration halts the outward perturbation and returns the ring towards its smaller radius, with the inward motion leading to a further Coriolis acceleration that causes the ring to rotate cyclonically (again, to the right of the inward particle motion). The whole process oscillates between radially outward and anti-cyclonic rotation, versus radially inward and cyclonic rotation. These inertial oscillations of a fluid ring illustrate the basic mechanism for inertial waves.

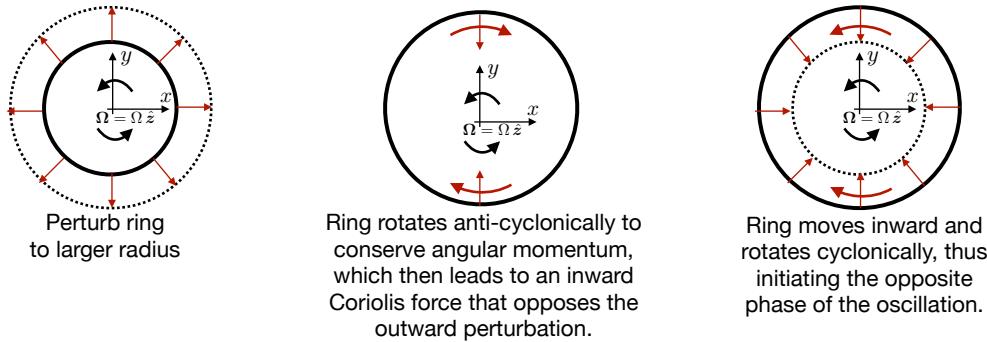


FIGURE 25.8: Schematic of inertial oscillations of a ring of fluid in the horizontal plane in the presence of rotation,  $\Omega = \Omega \hat{z}$  with  $\Omega > 0$ , where the rotation axis extends through the center of the ring. The left panel shows the ring perturbed outward, with this perturbation increasing the ring's moment of inertia about the vertical axis running through the center of the ring. To conserve angular momentum the ring must turn opposite to the sense of the rotating reference frame; that is, it rotates anti-cyclonically, as shown in the middle panel. As it turns anti-cyclonically the ring generates a Coriolis acceleration that points inward (to the right of the motion), thus causing the ring to oscillate back to a smaller radius (right panel), where the oscillation turns around.

### 25.6.2 Formulation of the inertial wave equation

Consider a homogeneous inviscid fluid on a rotating plane governed by the momentum equation

$$[\partial_t + (\mathbf{v} \cdot \nabla)] \mathbf{v} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla p/\rho - \rho g \hat{\mathbf{z}}, \quad (25.55)$$

where  $g$  is the effective gravitational acceleration that arises from central gravity and planetary centrifugal (Section 9.12.4). For the most part, we have in mind the  $f$ -plane case with  $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}} = (f/2) \hat{\mathbf{z}}$ . However, allowing for an arbitrary orientation of  $\boldsymbol{\Omega}$  assists in geometric understanding.

As when formulating the Boussinesq approximation in Section 23.1.1, it is useful to decompose pressure according to

$$p = \rho \varphi + p_0 \quad \text{where} \quad dp_0/dz = -\rho g, \quad (25.56)$$

with  $\rho$  the constant density and  $p_0(z)$  the static background hydrostatic pressure that exactly balances the fluid weight. This decomposition brings the momentum equation 25.55 to the form

$$[\partial_t + (\mathbf{v} \cdot \nabla)] \mathbf{v} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla \varphi. \quad (25.57)$$

Focusing attention on small amplitude fluctuations motivates us to linearize the momentum equation (25.57) by dropping the self-advection term,  $(\mathbf{v} \cdot \nabla) \mathbf{v}$ , thus leading to

$$\partial_t \mathbf{v} + 2\boldsymbol{\Omega} \times \mathbf{v} = -\nabla \varphi. \quad (25.58)$$

With  $\boldsymbol{\Omega}$  independent of time, we see that the velocity projected onto  $\boldsymbol{\Omega}$  satisfies

$$\partial_t(\mathbf{v} \cdot \boldsymbol{\Omega}) = -\boldsymbol{\Omega} \cdot \nabla \varphi. \quad (25.59)$$

Hence, if there is no pressure gradient along the direction of the rotation axis, then the velocity of the linear flow in that direction remains constant in time. For example, if the rotation is around the vertical axis,  $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$ , and there is no vertical dynamic pressure gradient,  $\partial_z \varphi = 0$ , then the vertical velocity is static,  $\partial_t w = 0$ .

Taking the curl of the linear velocity equation (25.58) eliminates the pressure gradient and yields the linearized vorticity equation<sup>5</sup>

$$\partial_t \boldsymbol{\omega} = 2(\boldsymbol{\Omega} \cdot \nabla) \mathbf{v} \quad \text{with} \quad \boldsymbol{\omega} = \nabla \times \mathbf{v}. \quad (25.60)$$

To reach this result requires the identity (2.37h) for the curl of a cross product. We also assumed  $\boldsymbol{\Omega}$  has no spatial dependence so that all of its derivatives vanish. To develop a wave equation, we take a time derivative of the linear vorticity equation (25.60), and make use of the linearized momentum equation (25.58), thus leading to

$$\partial_{tt} \boldsymbol{\omega} = -2(\boldsymbol{\Omega} \cdot \nabla)(2\boldsymbol{\Omega} \times \mathbf{v} + \nabla \varphi). \quad (25.61)$$

To eliminate the pressure gradient we take another curl and again make use of the identity (2.37h) to write

$$\nabla \times \boldsymbol{\omega} = \nabla \times (\nabla \times \mathbf{v}) = \nabla(\nabla \cdot \mathbf{v}) - \nabla^2 \mathbf{v} = -\nabla^2 \mathbf{v}, \quad (25.62)$$

where  $\nabla \cdot \mathbf{v} = 0$  since the fluid density is constant. We also make use of Cartesian tensor calculus

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<sup>5</sup>We study vorticity in Part VI of the book. For now, we only need to know that vorticity is the curl of the velocity.

from Chapter 2 to derive the identity

$$(\nabla \times [(\boldsymbol{\Omega} \cdot \nabla) (\boldsymbol{\Omega} \times \mathbf{v})])_m = \epsilon_{mnp} \partial_n [\Omega_s \partial_s (\boldsymbol{\Omega} \times \mathbf{v})_p] \quad (25.63a)$$

$$= \epsilon_{mnp} \partial_n [\Omega_s \partial_s \epsilon_{pqr} \Omega_q v_r] \quad (25.63b)$$

$$= \epsilon_{mnp} \epsilon_{qrp} \Omega_s \Omega_q \partial_n \partial_s v_r \quad (25.63c)$$

$$= (\delta_{mq} \delta_{nr} - \delta_{mr} \delta_{nq}) \Omega_s \Omega_q \partial_n \partial_s v_r \quad (25.63d)$$

$$= \Omega_s (\Omega_m \partial_r \partial_s v_r - \Omega_n \partial_n \partial_s v_m) \quad (25.63e)$$

$$= -(\boldsymbol{\Omega} \cdot \nabla)^2 v_m, \quad (25.63f)$$

where we made use of the  $\epsilon$ -tensor identity (1.38) as well as  $\nabla \cdot \mathbf{v} = 0$ . We are thus led to the wave equation for inertial waves

$$[\partial_{tt} \nabla^2 + (2 \boldsymbol{\Omega} \cdot \nabla)^2] \mathbf{v} = 0. \quad (25.64)$$

### 25.6.3 Dispersion relation for inertial waves

The inertial wave equation (25.64) provides the starting point for developing the kinematics of inertial waves. Since we are interested in wave fluctuations, we consider a linear wave solution of the form

$$\mathbf{v} = \tilde{\mathbf{v}} \exp[i(\mathbf{k} \cdot \mathbf{x} - \varpi t)] \quad (25.65a)$$

$$\varphi = \tilde{\varphi} \exp[i(\mathbf{k} \cdot \mathbf{x} - \varpi t)], \quad (25.65b)$$

with

$$\mathbf{k} = \hat{\mathbf{x}} k_x + \hat{\mathbf{y}} k_y + \hat{\mathbf{z}} k_z \quad (25.66)$$

the wave vector,  $\tilde{\mathbf{v}}$  and  $\tilde{\varphi}$  the (generally complex) wave amplitudes for the velocity and pressure, and  $\varpi$  the radial frequency.<sup>6</sup> As we are considering free space waves (no boundaries), there is no preferred length scale for inertial waves. Furthermore, since the flow is non-divergent, the constraint  $\nabla \cdot \mathbf{v} = 0$  means that the velocity of fluid particles is perpendicular to the wavevector

$$\mathbf{v} \cdot \mathbf{k} = 0. \quad (25.67)$$

This orientation of wavevector and fluid velocity characterizes *transverse waves*, in which lines of constant wave phase (e.g., wave crests and troughs) are perpendicular to  $\mathbf{k}$ .

Plugging the wave ansatz (25.65a) into the inertial wave equation (25.64) leads to the *dispersion relation*

$$\varpi^2 = (2 \boldsymbol{\Omega} \cdot \mathbf{k})^2 / |\mathbf{k}|^2. \quad (25.68)$$

The radial frequency of inertial waves is thus directly proportional to the orientation of the wave vector relative to the rotation vector. Furthermore, it is independent of the magnitude of the wave vector. To more clearly exhibit these properties we find it useful to write

$$\boldsymbol{\Omega} \cdot \mathbf{k} = |\boldsymbol{\Omega}| |\mathbf{k}| \cos \Lambda, \quad (25.69)$$

where  $\Lambda$  is the angle between  $\boldsymbol{\Omega}$  and  $\mathbf{k}$ . The dispersion relation (25.68) thus takes on the particularly compact form

$$\varpi = \pm 2 |\boldsymbol{\Omega}| \cos \Lambda \quad \text{with} \quad -\pi \leq \Lambda \leq \pi, \quad (25.70)$$

---

<sup>6</sup>We use  $\varpi$  for the radial frequency rather than the more common  $\omega$  in order to distinguish radial frequency from the vorticity,  $\boldsymbol{\omega}$ .

which serves to explicitly remove the wavevector magnitude. Sweeping through the possible orientation angles,  $\Lambda$ , reveals that the radial frequency for free space inertial waves spans the continuum range

$$-2|\Omega| \leq \varpi \leq 2|\Omega|. \quad (25.71)$$

#### 25.6.4 Group velocity

The group velocity determines the speed and direction of wave energy propagation and it is given by

$$\mathbf{c}_g = \nabla_{\mathbf{k}} \varpi = \hat{\mathbf{x}} \frac{\partial \varpi}{\partial k_x} + \hat{\mathbf{y}} \frac{\partial \varpi}{\partial k_y} + \hat{\mathbf{z}} \frac{\partial \varpi}{\partial k_z}. \quad (25.72)$$

Making use of the dispersion relation (25.68) renders

$$\mathbf{c}_g = \frac{\pm \mathbf{k} \times (2\boldsymbol{\Omega} \times \mathbf{k})}{|\mathbf{k}|^3}, \quad (25.73)$$

where we made use of the vector identity (1.40b). This expression leads to a particularly striking feature of the group velocity for inertial waves

$$\mathbf{c}_g \cdot \mathbf{k} = 0. \quad (25.74)$$

We are familiar with the Coriolis force acting perpendicular to the direction of a moving fluid particle. That orientation manifests for inertial waves via  $\mathbf{k} \cdot \mathbf{c}_g = 0$  so that inertial waves carry energy (via the group velocity) in a direction parallel to wave crests (perpendicular to  $\mathbf{k}$ ). A second property of the group velocity is found by projecting it onto the direction of the rotational axis

$$\mathbf{c}_g \cdot \boldsymbol{\Omega} = \pm 2[\Omega^2 \mathbf{k} \cdot \mathbf{k} - (\boldsymbol{\Omega} \cdot \mathbf{k})^2]/|\mathbf{k}|^3 = \pm 2[\Omega^2 - (\varpi/2)^2]/|\mathbf{k}| = \pm 2(\Omega^2/|\mathbf{k}|) \sin^2 \Lambda, \quad (25.75)$$

where we made use of the expressions (25.68) and (25.70) for the dispersion relation.

#### 25.6.5 Relating the velocity components

The velocity amplitude,  $\tilde{\mathbf{v}}$ , is generally a complex number, which allows for there to be a variety of phase shifts between the velocity components. We here determine some general relations between these amplitudes by returning to the linear velocity equation (25.58) and inserting the wave ansatz (25.65a) and (25.65b) to render

$$-\mathrm{i}\varpi \tilde{u} - f \tilde{v} = -\mathrm{i}k_x \tilde{\varphi} \quad (25.76a)$$

$$-\mathrm{i}\varpi \tilde{v} + f \tilde{u} = -\mathrm{i}k_y \tilde{\varphi} \quad (25.76b)$$

$$-\mathrm{i}\varpi \tilde{w} = -\mathrm{i}k_z \tilde{\varphi}. \quad (25.76c)$$

For simplicity we assumed the rotation vector is aligned with the vertical direction so that  $2\boldsymbol{\Omega} = f\hat{\mathbf{z}}$ . Manipulations with the horizontal velocity equations lead to the relations between the horizontal velocity amplitudes

$$\tilde{u}(f^2 - \varpi^2) = -\tilde{\varphi}(k_x \varpi + \mathrm{i}k_y f) \quad (25.77a)$$

$$\tilde{v}(f^2 - \varpi^2) = \tilde{\varphi}(-k_y \varpi + \mathrm{i}k_x f) \quad (25.77b)$$

$$\frac{\tilde{u}}{\tilde{v}} = \frac{-k_x k_y (f^2 - \varpi^2) + \mathrm{i}\varpi f (k_x^2 + k_y^2)}{(k_y \varpi)^2 + (k_x f)^2}. \quad (25.77c)$$

We make use of these relations in the following.

### 25.6.6 “Near” inertial waves with $\varpi \approx \pm|f|$

The inertial wave frequency is at its maximum magnitude when the wavevector is aligned parallel or anti-parallel to the rotation axis,

$$\mathbf{k} \times \boldsymbol{\Omega} = 0 \implies \varpi = \pm 2|\boldsymbol{\Omega}| = \pm|f|. \quad (25.78)$$

Recall that inertial waves are transverse so that  $\mathbf{v} \cdot \mathbf{k} = 0$ . This property, in combination with  $\mathbf{k} \times \boldsymbol{\Omega} = 0$ , means that high frequency inertial waves have fluid particle motion in a plane perpendicular to the rotation axis:  $\mathbf{v} \cdot \boldsymbol{\Omega} = 0$ . For example, if the rotation vector is vertical, then the wavevector only has a vertical component,  $\mathbf{k} = k_z \hat{\mathbf{z}}$ . In oceanography, inertial waves with  $\varpi \approx \pm|f|$  are referred to as *near inertial waves*, which refers to their radial frequency being close to the Coriolis frequency. Since near inertial waves have their wavevector oriented close to the rotation axis, equation (25.73) indicates that they have a vanishingly small group velocity.

For inertial waves with  $\varpi = f$  and  $\mathbf{k} = k_z \hat{\mathbf{z}}$ , the fluid velocity amplitude relation (25.77c) indicates that  $\tilde{u}/\tilde{v} = i$  so that the horizontal velocity of the wave is given by

$$\mathbf{u}/\tilde{u} = \hat{\mathbf{x}} e^{i(k_z z - f t)} + \hat{\mathbf{y}} e^{i(k_z z - f t - \pi/2)}. \quad (25.79)$$

Taking the real part renders

$$\mathbf{u}/\tilde{u} = \hat{\mathbf{x}} \cos(k_z z - f t) + \hat{\mathbf{y}} \sin(k_z z - f t). \quad (25.80)$$

With  $k_x = k_y = 0$  in the velocity equations (25.76a) and (25.76b), we see that there is no coupling between the horizontal velocity components and pressure. Hence, the motion of fluid particles reduces to inertial oscillations in the horizontal plane just as we studied for point particle motion in Section 10.5. As a check, we see that for a fixed vertical position, say  $z = 0$ , the velocity relation (25.80) for near inertial waves is identical the velocity relation (10.15b) for particles undergoing inertial oscillations

$$\mathbf{u}/\tilde{u} = \hat{\mathbf{x}} \cos(f t) - \hat{\mathbf{y}} \sin(f t) \quad \text{for } z = 0. \quad (25.81)$$

### 25.6.7 Near zero frequency inertial waves

Low frequency inertial waves occur when the wavevector is nearly perpendicular to the rotation axis

$$\boldsymbol{\Omega} \cdot \mathbf{k} \approx 0 \implies \varpi/\Omega \approx 0. \quad (25.82)$$

Hence, the wave number parallel to the rotation axis is vanishingly small. For example, if the rotation axis is vertical, then low frequency inertial waves have a vanishingly small vertical wave number,

$$k_z^2 \ll k_x^2 + k_y^2. \quad (25.83)$$

Correspondingly, for the velocity vector in the form (25.65a),  $\boldsymbol{\Omega} \cdot \mathbf{k} \approx 0$  means that

$$(\boldsymbol{\Omega} \cdot \nabla) \mathbf{v} = i(\boldsymbol{\Omega} \cdot \mathbf{k}) \mathbf{v} \approx 0. \quad (25.84)$$

That is, the velocity vector for low frequency inertial waves is coherent in the direction aligned with the rotation axis. Furthermore, when  $\boldsymbol{\Omega} \cdot \mathbf{k} \approx 0$ , the group velocity (25.75) has a magnitude

$$|\mathbf{c}_g| \approx 2|\boldsymbol{\Omega}|/|\mathbf{k}|, \quad (25.85)$$

so that low frequency inertial waves with long wavelength quickly transmit their energy along the rotation axis direction.

### 25.6.8 Connecting to Taylor-Proudman

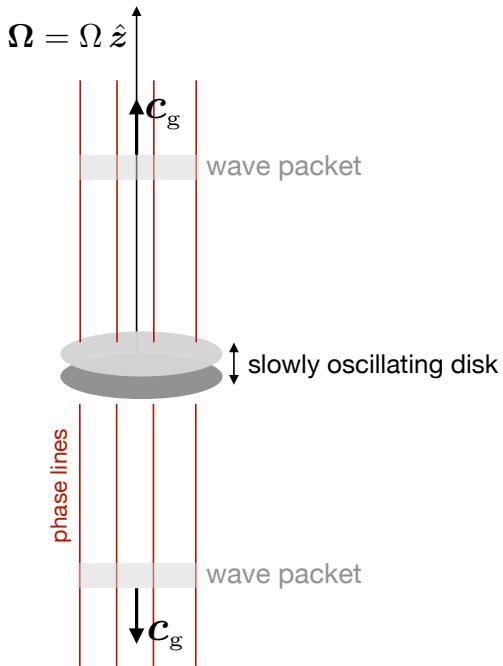


FIGURE 25.9: Schematic of inertial waves generated by a slowly oscillating disk in a rotating homogeneous fluid. The disk moves along the rotation axis in small amplitude oscillations whose radial frequency is much smaller than the rotational frequency,  $|\Omega|$ . The oscillations generate low frequency inertial waves whose phase lines and group velocity are parallel to the rotation axis, and whose wavevector is perpendicular to the rotation axis. We depict two wave packets that send energy vertically away from the disk, with the long wave and low frequency waves having the highest magnitude for the group velocity. Since  $\boldsymbol{\Omega} \cdot \mathbf{k} = 0$ , the fluid particle velocity associated with the inertial waves is constant in the direction along the rotation axis:  $(\boldsymbol{\Omega} \cdot \nabla) \mathbf{v} = 0$ .

We bring the previous notions together to describe a realization of low frequency inertial waves transmitting information about vertical stiffening, with reference to Figure 25.9. For this purpose, imagine a slowly oscillating disk that moves up and down in a direction aligned with the rotation axis. If the oscillation frequency is much slower than the rotation frequency, then the disk generates low frequency inertial waves with frequency of the oscillating disk. The low frequency inertial waves have a wavevector oriented perpendicular to the rotation axis,  $\boldsymbol{\Omega} \cdot \mathbf{k} = 0$ . Since inertial waves have a group velocity that is itself perpendicular to the wavevector, the low frequency inertial waves have a group velocity parallel to the rotation axis:  $\boldsymbol{\Omega} \times \mathbf{c}_g = 0$ . Information about the oscillating disk is most rapidly transmitted by long wavelength low frequency inertial waves. Furthermore, the low frequency inertial waves generate fluid particle motion that is independent of the position along the rotational axis since  $(\boldsymbol{\Omega} \cdot \nabla) \mathbf{v} = 0$ . Hence, the particle motion occurs in the plane perpendicular to the rotational axis, and this motion is coherent in the direction along the rotation axis. That is, inertial waves transmit information about stiffening along the rotation axis.

### 25.6.9 Concerning other waves depending on Coriolis

As we saw in this section, inertial waves rely on the Coriolis force for their existence. There are other waves that share this reliance, such as inertia-gravity waves, Kelvin waves, and Rossby waves. Inertial waves are the most parsimonious since they rely only on the Coriolis force from a constantly rotating homogeneous fluid without boundaries. In contrast, inertia-gravity waves also require continuous stratification or a stratification jump at an interface (as in the shallow water inertia-gravity waves in Chapter 31 or the surface gravity waves in Section 29.1). Likewise, Kelvin waves require a boundary either from a solid wall or an effective boundary due to the sign change of the Coriolis parameter at the equator (Exercise 31.13). And Rossby waves require a spatial gradient in the rotation rate as per the planetary beta effect (Section 33.6).

For much of the ocean and atmosphere, the buoyancy frequency,  $N$  (Section 24.5.4), is larger than  $|f|$ , in which case the radial frequency of inertia-gravity waves is bounded by  $|f| \leq \varpi \leq N$ , such as the shallow water inertia-gravity waves discussed in Section 31.8. These waves are said to be *super-inertial* since their frequency is larger than  $|f|$ . However, when stratification is reduced below  $|f|$ , then the inertia-gravity wave frequency becomes sub-inertial,  $N \leq \varpi \leq |f|$ . In the limit that  $N \rightarrow 0$ , inertia-gravity waves reduce to the inertial waves discussed in this section.

### 25.6.10 Further study

Our discussion of inertial waves was inspired by Section 9.2 of [Davidson \(2015\)](#), who emphasizes the role of inertial waves in forming vertically stiff structures in turbulent rapidly rotating flows. A further pedagogical analysis of inertial waves is provided by [Mory \(1992\)](#). For a visualization of inertial waves, refer to the 18 minute mark from the [rotating tank experiments of Prof. Fultz](#). He illustrates inertial oscillations within a bounded rotating homogeneous fluid, where the presence of boundaries quantizes the frequency of the excited inertial waves.

## 25.7 Isopycnal form stress from geostrophic eddies

As introduced in Section 19.1, form stress is the horizontal stress arising from pressure acting on a sloped surface. The mathematical expression for the form stress acting on the top side of a surface is given by equation (19.6)

$$\Sigma^{\text{form}} = p \nabla \eta, \quad (25.86)$$

with the opposite sign for the form stress on the bottom side of the surface. Here,  $z = \eta(x, y, t)$  is the depth of the surface (see Figure 19.3 or Figure 25.10). The net horizontal force from form stress is the area integral over the surface.

In this section we examine the zonal mean zonal form stress acting on an isopycnal surface (Section 25.7.1) and on an isopycnal layer (Section 25.7.2), each for an adiabatic, Boussinesq, hydrostatic fluid in geostrophic balance and within a zonally periodic channel of length  $L$ . As we show, the zonal mean zonal form stress arising from geostrophically balanced fluctuations provide an eastward acceleration to the fluid. At the same time, these *geostrophic eddies* transport buoyancy and thickness/volume meridionally. Although the channel geometry is rather simple, it has applications to the middle latitude atmospheric circulation as well as for ocean circulation, particularly in the Southern Ocean where there is circumpolar channel-like flow within the Antarctic Circumpolar Current. Furthermore, the discussion exposes key elements of eddy-mean flow interactions, sharing points with the leading order generalized Lagrangian mean of Section 47.3 and the quasi-Stokes transport discussed in Section 48.3.

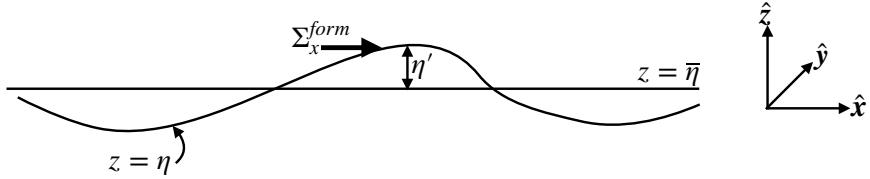


FIGURE 25.10: Schematic of the zonal form stress,  $\Sigma_x^{\text{form}}$ , acting on a surface whose zonal mean vertical position is  $z = \bar{\eta}(y, t)$  and whose vertical position relative to the zonal mean is  $z = \bar{\eta}(y, t) + \eta'(x, y, t)$ .

### 25.7.1 Zonal mean zonal form stress on an isopycnal surface

We are here interested in the form stress acting on an isopycnal surface. Before specializing to an isopycnal, we decompose the form stress according to the zonal mean depth and its deviation from zonal mean (see Figure 25.10). Thereafter, specialization to an isopycnal surface in an adiabatic fluid connects the zonal mean form stress to the meridional eddy flux of buoyancy.

#### *Zonal form stress on an arbitrary surface in a channel*

The zonal mean vertical position of the surface is written

$$\bar{\eta} = \frac{1}{L} \int_0^L \eta \, dx \quad (25.87)$$

and its corresponding zonal fluctuation is

$$\eta' = \eta - \bar{\eta}. \quad (25.88)$$

The zonal component of the form stress is thus given by

$$p \partial_x \eta = p(x, \bar{\eta} + \eta') \partial_x (\bar{\eta} + \eta') \quad (25.89a)$$

$$= p(x, \bar{\eta} + \eta') \partial_x \eta' \quad (25.89b)$$

$$\approx [p(x, \bar{\eta}) + \partial_z p(x, \bar{\eta}) \eta'] \partial_x \eta' \quad (25.89c)$$

$$= p(x, \bar{\eta}) \partial_x \eta' + \mathcal{O}(\eta')^2. \quad (25.89d)$$

Hence, to second order in fluctuations,  $\eta'$ , the zonal form stress acting on the surface equals to  $p(x, \bar{\eta}) \partial_x \eta'$ , where it is important to note that pressure is evaluated at the zonal mean depth,  $z = \bar{\eta}$ .

To within the same accuracy, the zonal integral of the zonal form stress is given by

$$\int_0^L \Sigma_x^{\text{form}} \, dx \approx \int_0^L p(\bar{\eta}) (\partial \eta' / \partial x) \, dx = - \int_0^L \eta' [\partial p(\bar{\eta}) / \partial x] \, dx, \quad (25.90)$$

where the final equality follows from zonal periodicity. Now assume the zonal pressure gradient at  $\bar{\eta}$  is balanced by a meridional geostrophic velocity

$$\partial p(\bar{\eta}) / \partial x = f \rho_0 v(\bar{\eta}), \quad (25.91)$$

where

$$v(\bar{\eta}) = \bar{v}(\bar{\eta}) + v'(\bar{\eta}) \quad (25.92)$$

so that

$$\int_0^L \Sigma_x^{\text{form}} dx = -\rho_0 f \int_0^L \eta' v' dx, \quad (25.93)$$

where we noted that the Coriolis parameter is independent of zonal position. Hence, there is a nonzero zonal mean zonal form stress when there is a nonzero zonal correlation between fluctuations in the meridional velocity and the depth of the surface

$$\bar{\Sigma}_x^{\text{form}} = -\rho_0 f \bar{v'} \bar{\eta'}. \quad (25.94)$$

#### Zonal mean zonal form stress acting on an isopycnal surface

To further unpack the correlation appearing in equation (25.94), specialize to the case of an isopycnal surface in an adiabatic fluid. As shown in our discussion of generalized Lagrangian mean averaging in Sections 47.3.6 and 47.5.7, vertical fluctuations in the position of the isopycnal surfaces, relative to the zonal mean  $\bar{\eta}$ , are related to zonal fluctuations in the density

$$\eta' \approx -\frac{\rho'}{\partial \bar{\rho} / \partial z} = -\frac{b'}{N^2}, \quad (25.95)$$

where we introduced the squared buoyancy frequency of the zonal mean state as well as the fluctuating buoyancy

$$N^2 = -\frac{g}{\rho_0} \frac{\partial \bar{\rho}}{\partial z} \quad \text{and} \quad b' = -\frac{g \rho'}{\rho_0}. \quad (25.96)$$

The zonally averaged zonal form stress thus takes the form

$$\bar{\Sigma}_x^{\text{form}} = \frac{\rho_0 f}{N^2} \bar{v'} \bar{b'}. \quad (25.97)$$

Again, the assumptions rendering the result (25.97) are (i) zonal periodicity, (ii) adiabatic and Boussinesq fluid, (iii) geostrophically balanced flow. Under these assumptions, the zonal mean zonal form stress acting on an isopycnal surface is proportional to the zonal correlation between fluctuations in the meridional velocity and the buoyancy. It is a general statistical property of geostrophic eddies in the atmosphere and ocean to transport positive buoyancy (e.g., warm air/water) poleward and negative buoyancy (e.g., cold air/water) equatorward, thus ameliorating the equator-to-pole buoyancy difference setup by solar radiation that preferentially warms the tropics. In turn, this property of geostrophic eddies leads to a positive zonal mean zonal form stress

$$\bar{\Sigma}_x^{\text{form}} > 0. \quad (25.98)$$

Hence, in addition to transporting buoyancy poleward, geostrophic eddies provide a positive zonal mean force through zonal integrated form stress that accelerates the fluid in the eastward direction. These two properties of geostrophic eddies (poleward flux of positive buoyancy anomalies along with an eastward acceleration from form stress) are fundamental to the middle latitude atmospheric circulation as well as for ocean circulation, particularly within the channel-like Antarctic Circumpolar Current.

#### 25.7.2 Zonal mean zonal form stress acting on an isopycnal layer

We offer yet another means to understand the zonal mean zonal form stress by here examining the form stress acting on a constant density layer of adiabatic Boussinesq fluid such as shown in Figure 25.11. This layered/isopycnal analysis anticipates some of the development considered for

the stacked shallow water model in Chapters 30 and 31 as well as for isopycnal models in Section 44.1.

The net form stress acting on the upper and lower layer interfaces in Figure 25.11 is given by

$$\Sigma^{\text{layer form}} = p_1 \nabla \eta_1 - p_2 \nabla \eta_2 \quad (25.99\text{a})$$

$$= p(\eta + h/2) \nabla(\eta + h/2) - p(\eta - h/2) \nabla(\eta - h/2) \quad (25.99\text{b})$$

$$\approx [p(\eta) - \rho g h/2] \nabla(\eta + h/2) - [p(\eta) + \rho g h/2] \nabla(\eta - h/2) \quad (25.99\text{c})$$

$$= p \nabla h - \rho g h \nabla \eta \quad (25.99\text{d})$$

$$= \nabla(p h) - h \nabla(p + \rho g \eta) \quad (25.99\text{e})$$

$$= \nabla(p h) - \rho_0 h \nabla M. \quad (25.99\text{f})$$

In this relation we set  $z = \eta$  for the vertical position at the center of the layer, introduced the Montgomery potential from Section 44.1.1

$$M \rho_0 = p + \rho g \eta, \quad (25.100)$$

and noted that  $\rho$  is a uniform constant layer density so that it commutes with the horizontal gradient operator computed along  $\rho$  surfaces. We also made use of the hydrostatic balance to approximate the interface pressures as

$$p(\eta + h/2) \approx p(\eta) + \frac{\partial p}{\partial z} \frac{h}{2} = p(\eta) - \rho g h/2 \quad (25.101\text{a})$$

$$p(\eta - h/2) \approx p(\eta) - \frac{\partial p}{\partial z} \frac{h}{2} = p(\eta) + \rho g h/2. \quad (25.101\text{b})$$

The zonal mean of the zonal layer form stress is thus given by the correlation between the layer thickness fluctuations and fluctuations in the zonal derivative of the Montgomery potential

$$\bar{\Sigma}_x^{\text{layer form}} = -\rho_0 \overline{h' \partial M'/\partial x}, \quad (25.102)$$

where we set  $\overline{\partial M/\partial x} = 0$  due to zonal periodicity. As seen in Section 44.1.1, the Montgomery potential is the geostrophic streamfunction in isopycnal coordinates, so that the fluctuating meridional geostrophic velocity is given by

$$f v' = \partial_x M'. \quad (25.103)$$

Consequently, the zonal mean zonal form stress acting on the layer equals to the correlation between the thickness fluctuations and fluctuations in the meridional geostrophic velocity

$$\bar{\Sigma}_x^{\text{layer form}} = -\rho_0 f \overline{v' h'}. \quad (25.104)$$

Hence, as the geostrophic eddies provide a net eastward acceleration to the layer (equation (25.98)), they also move volume meridionally within isopycnal layers, moving positive thickness fluctuations equatorward.

To further understand the physics of the form stress in equation (25.104), parameterize the velocity-thickness eddy correlation,  $\overline{v' h'}$ , by downgradient diffusion of thickness

$$\overline{v' h'} = -\kappa \partial_y \bar{h}, \quad (25.105)$$

where  $\kappa > 0$  is a nonzero kinematic diffusivity (dimensions of squared length per time). This parameterization is suggested by the work of Gent and McWilliams (1990) as discussed in Section 48.3.6. As noted there, thickness diffusion as a parameterization reflects the general tendency of

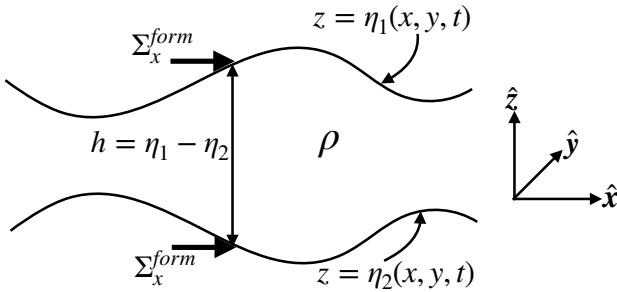


FIGURE 25.11: Schematic of a constant density layer of an adiabatic, hydrostatic, Boussinesq fluid with thickness  $h(x, y, t) = \eta_1(x, y, t) - \eta_2(x, y, t) = (\eta + h/2) - (\eta - h/2)$ , and uniform density  $\rho = \text{constant}$ . East points to the right and north is oriented into the page. The zonal form stress,  $\Sigma_x^{\text{form}}$ , acting on the upper and lower interfaces at a horizontal position  $(x, y)$  are shown by the thick horizontal vectors. The zonal form stress is the horizontal component of the pressure force per area acting on the layer interfaces, with the sign of the form stress determined by the slope of the layer interface. For a zonally periodic fluid layer, the net zonal pressure force acting on the layer arises from the zonal form stress integrated over the layer interfaces.

geostrophic eddies to reduce horizontal gradients in layer thickness as they reduce the available potential energy of the flow. In this case the zonal mean zonal form stress is

$$\bar{\Sigma}_x^{\text{layer form}} = \rho_0 f \kappa \partial_y \bar{h}. \quad (25.106)$$

So in the northern hemisphere in regions where the zonal mean layer thickness increases to the north,  $\partial_y \bar{h} > 0$ , there is a corresponding eastward zonal mean zonal form stress arising from parameterized geostrophic eddies acting on layer thickness. This situation corresponds to the case in Section 25.7.1, where we saw that geostrophic eddies preferentially transport positive buoyancy anomalies poleward and negative buoyancy anomalies equatorward. In the present analysis, meridional changes to the layer thickness correspond to a nonzero thermal wind shear. If layer thickness increases poleward, as for the case of weaker vertical stratification in the high latitudes, then the zonal velocity has a positive vertical shear, thus contributing an eastward zonal mean form stress.

### 25.7.3 Comments and further study

A key feature of geostrophic eddies exposed by this discussion concerns the connection between zonal form stress (providing an eastward force on the zonally periodic channel flow) and meridional eddy transport of buoyancy (positive buoyancy anomalies are transported poleward) and thickness (positive thickness anomalies are transported equatorward). The periodic channel domain is highly idealized. Nonetheless, the basic ideas form the roots for much of how we think about geostrophic eddies in the middle latitude atmosphere and the Southern Ocean. Further generalizations lead to the generalized Lagrangian mean, whose kinematic rudiments are discussed in Section 47.3, as well as the thickness weighted average, discussed in Chapter 45.

The fundamental role of form stress in geostrophic turbulent flows is pedagogically treated by [Vallis \(2017\)](#). See, in particular, his Chapter 21 for a thorough and insightful discussion of circulation in the Southern Ocean. We also return to form stress within the shallow water fluid in Section 31.5. That discussion complements the presentation given here, with a focus on a layer of shallow water fluid. We also touch on the notions of form stress when discussing the [Gent and McWilliams \(1990\)](#) mesoscale eddy parameterization in Section 48.3.

## 25.8 Exercises

### EXERCISE 25.1: SMALL ROSSBY NUMBER AT HUMAN SCALES

Consider motion of a car at a speed  $U \sim 10^5$  m hour $^{-1}$ , a length scale of  $L \sim 10$  m, and moving at 30°N latitude.

- (a) What is the rotation rate of the planet and corresponding rotation period,  $T_{\text{human}} = 2\pi/\Omega_{\text{human}}$ , required to render a unit Rossby number for the given “human” sized scales? Give resulting rotation rate in units of inverse seconds and period in seconds. Hint: since we assume 30°N latitude,  $f_{\text{human}} = 2\Omega_{\text{human}} \sin \phi = \Omega_{\text{human}}$ .
- (b) If the earth rotated at the angular speed  $\Omega_{\text{human}}$ , what would be the solid-body speed for a point at rest on the earth’s surface at the equator? Give result in units of meter per second.
- (c) How does the solid-body speed compare to the speed of sound at standard atmospheric conditions? What about the root-mean-square speed for air molecules? Hint: read Section 11.3.4.
- (d) Discuss an astronomical object that has a very large rotational speed. Hint: 1993 Nobel Prize in physics.

### EXERCISE 25.2: THE BETA SPIRAL

Consider a steady state Boussinesq planetary geostrophic fluid in the absence of mixing. Write the geostrophic velocity as

$$u = |\mathbf{u}| \cos \Delta \quad v = |\mathbf{u}| \sin \Delta, \quad (25.107)$$

where  $\Delta$  is the angle measured counter-clockwise from east. Use thermal wind and the steady state perfect fluid buoyancy equation to determine an expression for  $\partial \Delta / \partial z$ . Show that for  $f > 0$  (northern hemisphere) and  $\partial b / \partial z = N^2 > 0$  (gravitationally stable fluid column), then  $\partial \Delta / \partial z$  has opposite sign from the vertical velocity,  $w$ . This spiralling of the geostrophic velocity is known as the *beta spiral* in oceanography.

### EXERCISE 25.3: ALTERNATIVE FORM OF THERMAL WIND

Consider a fluid with density a function of pressure and potential temperature

$$\rho = \rho(\theta, p). \quad (25.108)$$

A physical realization of this equation of state is a lake. Show that the thermal wind shear for a hydrostatic and *compressible* fluid with this equation of state can be written in the form

$$\frac{\partial \mathbf{u}}{\partial z} = \left[ \frac{N^2}{f \rho g} \right] (\hat{\mathbf{z}} \times \nabla_\theta p), \quad (25.109)$$

where

$$N^2 = -\frac{g}{\rho} \frac{\partial \rho}{\partial \theta} \frac{\partial \theta}{\partial z} = g \alpha_\theta \frac{\partial \theta}{\partial z} > 0 \quad (25.110)$$

is the squared buoyancy frequency, assumed positive so that the fluid is gravitationally stable in the vertical (see Section 24.5.4). The term  $\alpha_\theta$  is the thermal expansion coefficient written in terms of potential temperature (Section 24.3.4),

$$\alpha_\theta = -(1/\rho) \partial \rho / \partial \theta > 0. \quad (25.111)$$

Finally, the horizontal gradient projected onto constant  $\theta$  surfaces is given by (see Section 41.12.2)

$$\nabla_\theta = \hat{\mathbf{x}} \left[ \frac{\partial}{\partial x} \right]_{y,\theta} + \hat{\mathbf{y}} \left[ \frac{\partial}{\partial y} \right]_{x,\theta} \quad (25.112a)$$

$$= \nabla_z - \left[ \frac{\nabla_z \theta}{\partial \theta / \partial z} \right] \frac{\partial}{\partial z}. \quad (25.112b)$$

Hint: This exercise requires careful use of the chain rule and the hydrostatic relation, along with the equations given in the problem statement. Furthermore, assume the fluid is fully compressible.

Hint: Some may wish to “warm-up” by showing that the result holds for the simpler equation of state  $\rho = \rho(\theta)$ . Some of the steps used for the simpler case are relevant for the case with  $\rho = \rho(\theta, p)$ .





# Chapter 26

## Tangent plane flow balances

We here consider a variety of inviscid tangent plane (horizontal) flow regimes characterized by a balance between a subset of terms appearing in the horizontal momentum equation. This discussion allows us to directly compare the geostrophically balanced flow of Chapter 25 to a variety of other balanced flows such as gradient wind, inertial motion, and cyclostrophic balance. We provide a categorization of the flow following *natural coordinates*, where natural coordinates offer a concise means to compare the relative magnitudes of the Coriolis, pressure, and centrifugal accelerations acting on a fluid element moving horizontally.

### READER'S GUIDE TO THIS CHAPTER

We make use of the Boussinesq momentum equation from Section 23.1 and assume an understanding of the geostrophic balance from Chapter 25. We also use of some geometric notions discussed in Chapter 5, though most of the salient points are revisited here so that Chapter 5 is an option rather than a requirement. Throughout this chapter we assume a tangent plane geometry and associated equations from Section 22.3, thus allowing for Cartesian coordinates. Also, we ignore all vertical motion. Some of this material is used in subsequent chapters, in particular Chapter 27 on Ekman dynamics as well as Chapters 38 and 40 on quasi-geostrophy.

26.1	Loose ends	638
26.2	Horizontal flow described by natural coordinates	638
26.2.1	Natural coordinates	638
26.2.2	Material acceleration	639
26.2.3	Centripetal and centrifugal accelerations	640
26.2.4	Coriolis and pressure gradient	640
26.2.5	Horizontal momentum equation and local Rossby number	641
26.2.6	Eulerian decomposition of the acceleration	642
26.2.7	Further study	643
26.3	Exact geostrophic balance	643
26.3.1	Steady $f$ -plane flow	644
26.3.2	Steady $\beta$ -plane flow	644
26.3.3	What about geostrophic balance with curved motion?	645
26.4	Inertial motion	645
26.4.1	Anti-cyclonic circular motion on $f$ -plane	646
26.4.2	Period for inertial motion	646
26.4.3	Observing inertial motion	647

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26.4.4	Inertial motion is Lagrangian . . . . .	647
26.4.5	“Inertial” motion does not refer to an inertial frame . . . . .	647
26.4.6	Inertial motion on a sphere . . . . .	647
26.5	Cyclostrophic balance . . . . .	648
26.6	Gradient wind balance . . . . .	649
26.6.1	Constraints on gradient wind flow . . . . .	650
26.6.2	The variety of gradient wind flows . . . . .	651
26.6.3	Comments . . . . .	652

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## 26.1 Loose ends

- How to determine whether the velocity field is divergent or non-divergent for the cyclostrophic and gradient wind motions?
- Exercises needed for this chapter.

## 26.2 Horizontal flow described by natural coordinates

In this section we decompose the horizontal Boussinesq momentum equation into motion parallel to and motion perpendicular to the instantaneous trajectory of a fluid element moving along a constant geopotential surface. That is, we characterize the velocity and acceleration according to the local flow direction. Furthermore, we are only concerned with motion on a constant geopotential using the tangent plane approximation; i.e., horizontal motion. The *natural coordinates* arising from this description exposes the centripetal/centrifugal acceleration that arises from curvature in the trajectory as measured by the radius of curvature. This non-inertial acceleration is distinct from the centrifugal acceleration that arises from planetary rotation, with planetary centrifugal acceleration already contained within the effective gravitational acceleration that acts in the local vertical direction (see Section 9.10.1). We also decompose the accelerations from pressure, friction, and Coriolis into their natural coordinate components.

### 26.2.1 Natural coordinates

Natural coordinates for horizontal motion are defined by a locally orthogonal set of unit vectors (see Figure 26.1)

$$\hat{z} = \hat{u} \times \hat{n} = \text{vertical direction} \quad (26.1a)$$

$$\hat{u} = \hat{n} \times \hat{z} = \text{tangent to horizontal velocity} \quad (26.1b)$$

$$\hat{n} = \hat{z} \times \hat{u} = \text{normal direction to the left of motion.} \quad (26.1c)$$

The unit vector  $\hat{u}$  is tangent to the velocity vector (which is horizontal), so that

$$\mathbf{u} = |\mathbf{u}| \hat{u} = \frac{Ds}{Dt} \hat{u}, \quad (26.2)$$

where  $s$  is the arc-length measured along the trajectory as introduced in Section 2.4. The unit vector  $\hat{n}$  is perpendicular to the velocity and points to the left of the trajectory facing downstream.

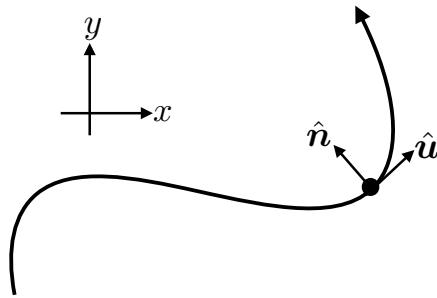


FIGURE 26.1: Illustrating the decomposition of horizontal motion of a fluid element into natural coordinate directions. These directions are defined by a unit tangent vector,  $\hat{u}$ , pointing in the direction of the fluid element motion, and a unit normal vector,  $\hat{n}$ , pointing to the left of the motion facing downstream.

### 26.2.2 Material acceleration

When writing the velocity according to equation (26.2), we decompose the acceleration into the change in speed and change in direction

$$\frac{D\mathbf{u}}{Dt} = \frac{D|\mathbf{u}|}{Dt} \hat{\mathbf{u}} + |\mathbf{u}| \frac{D\hat{\mathbf{u}}}{Dt}. \quad (26.3)$$

Following our discussion of rotation in Section 9.4 (see Figure 9.4), the magnitude of the direction change can be written in terms of the infinitesimal angle swept out by the motion as the fluid element moves along a trajectory

$$|\delta\hat{\mathbf{u}}| = |\delta\vartheta|. \quad (26.4)$$

The infinitesimal angle swept out by the trajectory is related to the radius of curvature,  $R$  (Figure 26.2), and the arc-length increment,  $\delta s$ , traversed by the trajectory

$$\delta\vartheta = \frac{\delta s}{R}. \quad (26.5)$$

Finally, the infinitesimal change in tangent,  $\delta\hat{\mathbf{u}}$ , is directed normal to the motion, which we see by noting

$$\hat{\mathbf{u}} \cdot \hat{\mathbf{u}} = 1 \implies \delta\hat{\mathbf{u}} \cdot \hat{\mathbf{u}} = 0. \quad (26.6)$$

That is,  $\delta\hat{\mathbf{u}}$  is orthogonal to  $\hat{\mathbf{u}}$ , so that it points either parallel or anti-parallel to  $\hat{\mathbf{n}}$ . We detailed this property of rotating unit vectors in Section 2.1.4 (see Figure 2.2). Our convention is that  $\hat{\mathbf{n}}$  points to the left of  $\hat{\mathbf{u}}$ , so that if the trajectory turns to the left, then  $\delta\hat{\mathbf{u}}$  points parallel to  $\hat{\mathbf{n}}$ , whereas if the trajectory turns to the right then  $\delta\hat{\mathbf{u}}$  points anti-parallel to  $\hat{\mathbf{n}}$ . That is,  $\delta\hat{\mathbf{u}}$  always points towards the center of the circle used to compute the radius of curvature as in Figure 26.2.

Bringing these results together leads to the expression for the infinitesimal unit vector change

$$\delta\hat{\mathbf{u}} = \hat{\mathbf{n}} \frac{\delta s}{R}. \quad (26.7)$$

Our sign convention takes  $R > 0$  for a fluid element turning in the direction of  $\hat{\mathbf{n}}$  (to the left facing downstream) and  $R < 0$  when turning opposite to  $\hat{\mathbf{n}}$  (to the right facing downstream). Hence, the material time change is

$$\frac{D\hat{\mathbf{u}}}{Dt} = \frac{D\hat{\mathbf{u}}}{Ds} \frac{Ds}{Dt} = \frac{\hat{\mathbf{n}}}{R} \frac{Ds}{Dt} = \frac{\hat{\mathbf{n}}}{R} |\mathbf{u}|, \quad (26.8)$$

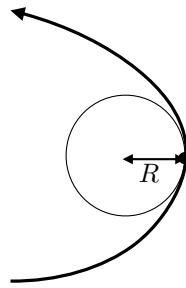


FIGURE 26.2: Illustrating the radius of curvature associated with turning motion of a fluid element. The radius of curvature equals to the radius of a tangent circle (the *curvature circle*) that approximates, to second order accuracy, the trajectory at a particular point. The radius is smaller in magnitude when the trajectory is highly curved, and  $|R| = \infty$  when the trajectory is straight. The radius is positive when the trajectory turns into the normal direction as depicted here (to the left; concave as defined by  $\hat{\mathbf{n}}$ ) and negative when turning in the opposite direction (to the right; convex as defined by  $\hat{\mathbf{n}}$ ). See Section 5.2 for more details on curvature, with Figure 5.4 offering more details for how to determine the radius of curvature.

where the speed is given by the time change of the arc-length along the trajectory

$$|\mathbf{u}| = \frac{Ds}{Dt}. \quad (26.9)$$

Combining these results renders the acceleration

$$\frac{D\mathbf{u}}{Dt} = \frac{D|\mathbf{u}|}{Dt} \hat{\mathbf{u}} + \frac{|\mathbf{u}|^2}{R} \hat{\mathbf{n}}. \quad (26.10)$$

The acceleration has thus been decomposed into the change in speed of the fluid element along the direction of the motion, plus the centripetal acceleration due to curvature of the trajectory. In Section 26.2.3 we justify referring to  $\hat{\mathbf{n}} |\mathbf{u}|^2/R$  as the *centripetal* acceleration.

### 26.2.3 Centripetal and centrifugal accelerations

The centripetal acceleration points towards the concave side of a turning trajectory; “centripetal” means “towards the center.” Its opposing partner, the centrifugal (“away from center”) acceleration points to the convex side (see Figure 26.3). So how do we interpret  $\hat{\mathbf{n}} |\mathbf{u}|^2/R$ ? For motion turning to the left, towards  $\hat{\mathbf{n}}$ , the radius of curvature is positive,  $R > 0$ , so that  $\hat{\mathbf{n}} |\mathbf{u}|^2/R$  points to the concave side of the trajectory (left side). For a trajectory turning to the right then  $R < 0$ , which again means that  $\hat{\mathbf{n}} |\mathbf{u}|^2/R$  points to the concave side (now on the right). We conclude that the acceleration  $\hat{\mathbf{n}} |\mathbf{u}|^2/R$  indeed represents a centripetal acceleration and  $-\hat{\mathbf{n}} |\mathbf{u}|^2/R$  is the centrifugal acceleration.

### 26.2.4 Coriolis and pressure gradient

The Coriolis acceleration takes the following form in natural coordinates

$$-f \hat{\mathbf{z}} \times \mathbf{u} = -(\hat{\mathbf{z}} \times \hat{\mathbf{u}}) f |\mathbf{u}| = -\hat{\mathbf{n}} f |\mathbf{u}|, \quad (26.11)$$

so that the Coriolis acceleration always points to the right of the flow direction for  $f > 0$ . In contrast, the pressure gradient has two components

$$\nabla p = \hat{\mathbf{u}} (\hat{\mathbf{u}} \cdot \nabla p) + \hat{\mathbf{n}} (\hat{\mathbf{n}} \cdot \nabla p) = \hat{\mathbf{u}} \frac{\partial p}{\partial s} + \hat{\mathbf{n}} \frac{\partial p}{\partial n}, \quad (26.12)$$

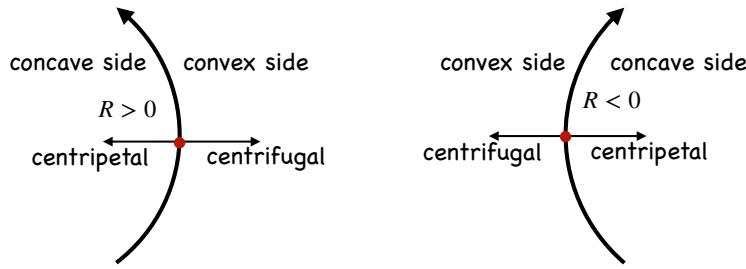


FIGURE 26.3: Centripetal acceleration of a turning fluid element,  $\hat{n}|\mathbf{u}|^2/R$ , points to the concave side of the curve (towards the center) whereas the centrifugal acceleration,  $-\hat{n}|\mathbf{u}|^2/R$ , points to the convex side (away from the center). The centripetal and centrifugal accelerations are paired action/reaction accelerations. The normal unit vector,  $\hat{n}$ , always points to the left of the motion, whereas the radius of curvature,  $R$ , is positive or negative depending on the direction of the turning motion. For a left turning trajectory (in direction of  $\hat{n}$ ), the concave side is on the left and has positive radius of curvature,  $R > 0$ , whereas for the right turning trajectory (opposite direction of  $\hat{n}$ ) the concave side is to the right with  $R < 0$ . To help remember the signs, note that centrifugal means “away from the center” whereas centripetal means “towards the center”. It is the centrifugal acceleration that pulls one away from the center of a merry-go-round whereas one’s arms and hands provide the balancing centripetal acceleration.

one pointing along the flow direction and one normal to the direction.

### 26.2.5 Horizontal momentum equation and local Rossby number

Bringing the above results together leads to the horizontal momentum equation decomposed into natural coordinates

$$\frac{D|\mathbf{u}|}{Dt} = -\frac{1}{\rho_0} \frac{\partial p}{\partial s} + \mathbf{F} \cdot \hat{\mathbf{u}} \quad \text{motion parallel to } \hat{\mathbf{u}} \quad (26.13a)$$

$$\frac{|\mathbf{u}|^2}{R} + f|\mathbf{u}| = -\frac{1}{\rho_0} \frac{\partial p}{\partial n} + \mathbf{F} \cdot \hat{\mathbf{n}} \quad \text{motion perpendicular to } \hat{\mathbf{u}}, \quad (26.13b)$$

where  $\mathbf{F}$  is the frictional acceleration and  $\rho_0$  is the reference density for the Boussinesq fluid. These equations decompose the accelerations into those acting parallel to and normal to the trajectory. It is notable that the normal component is purely diagnostic; there is no time derivative in equation (26.13b). Instead, it is a balance between centrifugal, Coriolis, normal pressure gradient, and normal component of friction. In the next few sections we consider certain limiting cases as revealed by the equations of motion (26.13a) and (26.13b). Friction remains zero in this chapter but is nonzero for the discussion of Ekman mechanics in Chapter 27.

#### *Steady frictionless flow*

The frictionless balanced motions considered in this chapter all occur with a fixed velocity magnitude for the fluid element, so that the along-trajectory component of the momentum equation (26.13a) for frictionless motion reduces to

$$\frac{D|\mathbf{u}|}{Dt} = -\frac{1}{\rho_0} \frac{\partial p}{\partial s} = 0. \quad (26.14)$$

Hence, there is no pressure gradient aligned with the fluid element motion, and correspondingly the frictionless fluid motion preserves its kinetic energy

$$\frac{1}{2} \frac{D(\mathbf{u} \cdot \mathbf{u})}{Dt} = |\mathbf{u}| \frac{D|\mathbf{u}|}{Dt} = 0. \quad (26.15)$$

### Local Rossby number

As discussed in Section 25.3, the Rossby number is the ratio of the velocity advection term to the Coriolis term. In the normal component to the momentum equation (26.13b), we have the advection term manifest as the local centrifugal term. Following Chapter 1 of [van Heijst \(2010\)](#) we define the *local Rossby number* as the ratio of the centrifugal acceleration to the Coriolis acceleration

$$\text{Ro}_{\text{local}} = \frac{|\mathbf{u}|^2/R}{f/|\mathbf{u}|} = \frac{|\mathbf{u}|}{Rf}. \quad (26.16)$$

In this chapter we consider flow regimes as determined by values of the local Rossby number.

### 26.2.6 Eulerian decomposition of the acceleration

The horizontal equations of motion (26.13a) and (26.13b) offer a relatively simple and insightful Lagrangian description of the motion. In contrast, an Eulerian description requires us to expand the material time derivative. Although we focus in this chapter on the Lagrangian perspective, we here consider two decompositions available when using the Eulerian form.

#### Advective form

The standard form of the material time derivative is given by

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = \frac{\text{D}|\mathbf{u}|}{\text{D}t} \hat{\mathbf{u}} + \frac{|\mathbf{u}|^2}{R} \hat{\mathbf{n}}, \quad (26.17)$$

so that

$$\hat{\mathbf{u}} \cdot \left[ \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \right] = \frac{\text{D}|\mathbf{u}|}{\text{D}t} = -\frac{1}{\rho_0} \frac{\partial p}{\partial s} + \mathbf{F} \cdot \hat{\mathbf{u}} \quad (26.18a)$$

$$\hat{\mathbf{n}} \cdot \left[ \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \right] = \frac{|\mathbf{u}|^2}{R} = -f |\mathbf{u}| - \frac{1}{\rho_0} \frac{\partial p}{\partial n} + \mathbf{F} \cdot \hat{\mathbf{n}}. \quad (26.18b)$$

Depending on the information provided by a field measurement or numerical simulation, one might more readily diagnose the kinematic expressions on the left side of these equations or the force balances on the right side. For example, the inverse radius of curvature for the fluid flow can be diagnosed in either of the following ways

$$R^{-1} = \frac{\hat{\mathbf{n}} \cdot [\partial \mathbf{u} / \partial t + (\mathbf{u} \cdot \nabla) \mathbf{u}]}{|\mathbf{u}|^2} = \frac{-f |\mathbf{u}| - \rho_0^{-1} \partial p / \partial n + \mathbf{F} \cdot \hat{\mathbf{n}}}{|\mathbf{u}|^2}. \quad (26.19)$$

#### Vector invariant form

We can transform the self-advection term using the vector identity (see Section 2.3.4)

$$(\mathbf{u} \cdot \nabla) \mathbf{u} = \nabla K - \mathbf{u} \times \zeta \hat{\mathbf{z}}, \quad (26.20)$$

where  $K = \mathbf{u} \cdot \mathbf{u} / 2$  is the kinetic energy per mass in the horizontal flow, and  $\zeta = \partial_x v - \partial_y u$  is the vertical component to the relative vorticity (see Chapter 32). The deflecting acceleration,  $\mathbf{u} \times \zeta \hat{\mathbf{z}}$ , is known as the *Magnus acceleration* and was discussed in Section 17.2.3. Projecting into the  $\hat{\mathbf{u}}$

and  $\hat{\mathbf{n}}$  directions leads to

$$\hat{\mathbf{u}} \cdot \frac{\partial \mathbf{u}}{\partial t} = -\frac{\partial(p/\rho_0 + K)}{\partial s} + \mathbf{F} \cdot \hat{\mathbf{u}} \quad (26.21a)$$

$$\hat{\mathbf{n}} \cdot \frac{\partial \mathbf{u}}{\partial t} = -(f + \zeta) |\mathbf{u}| - \frac{\partial(p/\rho_0 + K)}{\partial n} + \mathbf{F} \cdot \hat{\mathbf{n}}. \quad (26.21b)$$

The gradient acceleration is affected by both pressure and the *dynamic pressure* afforded by the kinetic energy per mass. The Magnus acceleration appears only in the normal component equation, which is expected since it acts just as the Coriolis acceleration to deflect the fluid element perpendicular to its trajectory. Following the example in Figure 17.1, consider a positive relative vorticity,  $\zeta > 0$ . For this case, the Magnus acceleration deflects the fluid element to the right of its trajectory; i.e., opposite to the normal direction, which points to the left as per our convention in Figure 26.1.

### 26.2.7 Further study

Section 3.2 of [Holton \(1992\)](#) details the use of natural coordinates for geophysical flows, with a similar decomposition provided in Section 7.10 of [Gill \(1982\)](#) and Section 2.9 of [Vallis \(2017\)](#). Natural coordinates are also used in describing non-rotating flows as illustrated in [this video](#).

## 26.3 Exact geostrophic balance

Frictionless flow parallel to pressure contours experiences no pressure gradient ( $\partial p / \partial s = 0$ ), so that the speed of a fluid element remains constant. Furthermore, if this motion occurs with an infinite radius of curvature (straight line motion parallel to pressure contours), then the force balance is between the normal pressure gradient and Coriolis. In this case the local Rossby number (26.16) vanishes

$$\text{Ro}_{\text{local}} = \frac{|\mathbf{u}|}{R f} = 0 \quad \text{if } |R| = \infty. \quad (26.22)$$

More precisely, exact geostrophic balance occurs under the following conditions:

- fluid element move on a straight line so that the radius of curvature is infinite,  $|R| = \infty$ , thus making the centripetal acceleration and local Rossby number both vanish;
- fluid elements move along lines of constant pressure so that  $\partial p / \partial s = 0$ ;
- friction vanishes.

In this case the equations of motion (26.13a) and (26.13b) take the form

$$\frac{D|\mathbf{u}|}{Dt} = 0 \quad (26.23a)$$

$$f |\mathbf{u}| = -\frac{1}{\rho_0} \frac{\partial p}{\partial n}. \quad (26.23b)$$

Equation (26.23a) says that the speed of a fluid element is constant, so that the horizontal kinetic energy likewise is constant. Equation (26.23b) says that the pressure gradient normal to the motion balances the Coriolis acceleration. We refer to this flow, depicted in Figure 26.4, as *exact geostrophic balance* since it is an exact solution under the above assumptions.

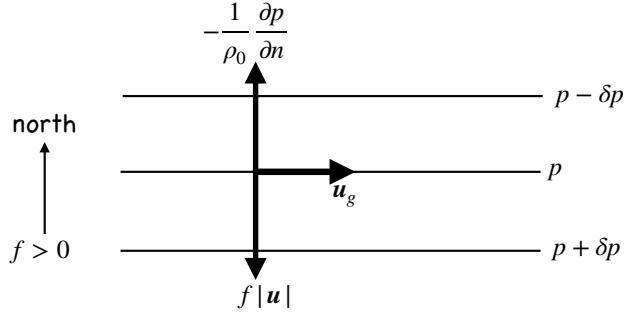


FIGURE 26.4: Exact geostrophic balance on a tangent plane occurs when the flow is horizontal, frictionless, straight, and follows contours of constant pressure. For this case the pressure gradient exactly balances the Coriolis acceleration so that the motion is perpendicular to both of these accelerations. We here depict motion assuming  $f > 0$  as for the northern hemisphere. If flow is on an  $f$ -plane then the exact geostrophic balance is steady for any arbitrary flow direction. On a  $\beta$ -plane, steady exact geostrophic balance holds only for zonal flow.

Writing the horizontal advection of speed in the form

$$\mathbf{u} \cdot \nabla |\mathbf{u}| = |\mathbf{u}| \hat{\mathbf{u}} \cdot \nabla |\mathbf{u}| = |\mathbf{u}| \frac{\partial |\mathbf{u}|}{\partial s}, \quad (26.24)$$

allows us to write the material constancy of the flow speed as

$$\frac{\partial |\mathbf{u}|}{\partial t} + |\mathbf{u}| \frac{\partial |\mathbf{u}|}{\partial s} = 0. \quad (26.25)$$

Hence, a steady flow speed, with  $\partial |\mathbf{u}| / \partial t = 0$ , only holds for the exact geostrophic balance if the flow speed is fixed along each trajectory path

$$\frac{\partial |\mathbf{u}|}{\partial s} = 0 \implies \frac{\partial |\mathbf{u}|}{\partial t} = 0. \quad (26.26)$$

What is required for this condition to hold? We examine two cases, again restricted to a tangent plane.

### 26.3.1 Steady $f$ -plane flow

Geostrophic motion on an  $f$ -plane is horizontally non-divergent (Section 25.4)

$$\nabla \cdot \mathbf{u} = \nabla \cdot (\hat{\mathbf{u}} |\mathbf{u}|) = 0. \quad (26.27)$$

Flow in a straight line, with each trajectory parallel to one another, has the trajectory direction independent of space. Hence, the non-divergent condition means that

$$0 = \nabla \cdot (\hat{\mathbf{u}} |\mathbf{u}|) = (\hat{\mathbf{u}} \cdot \nabla) |\mathbf{u}| = \frac{\partial |\mathbf{u}|}{\partial s}, \quad (26.28)$$

which proves that exact geostrophic flow on an  $f$ -plane is steady.

### 26.3.2 Steady $\beta$ -plane flow

The geostrophic velocity in the presence of a meridional gradient of the Coriolis parameter,  $f = f(y)$ , satisfies (Section 25.4)

$$\nabla \cdot (f \mathbf{u}) = 0. \quad (26.29)$$

Making use of  $\nabla \cdot \hat{\mathbf{u}} = 0$  for straight line trajectories leads to

$$\nabla \cdot (f \mathbf{u}) = \frac{\partial(f |\mathbf{u}|)}{\partial s} = 0. \quad (26.30)$$

We conclude that  $\partial|\mathbf{u}|/\partial s = 0$  holds only for trajectories that are parallel to latitude lines, in which case  $\partial f/\partial s = \partial f/\partial x = 0$ . Therefore, exact geostrophic motion on the  $\beta$ -plane is steady only for trajectories that follow constant latitude lines; i.e., zonal trajectories as depicted in Figure 26.4.

### 26.3.3 What about geostrophic balance with curved motion?

The geostrophically balanced flows discussed in Chapter 25 generally have curvature; i.e., the flows are not straight, such as for the geostrophic motion around a pressure center as shown in Figure 25.3. But as emphasized by the natural coordinate decomposition as per equations (26.13a) and (26.13b), curved motion has an associated centrifugal acceleration. So when speaking of geostrophic balance for flow that has a nonzero curvature, then the local Rossby number (26.16) is not precisely zero. Rather, its magnitude is small but nonzero

$$|\text{Ro}_{\text{local}}| \ll 1 \quad \text{approximate geostrophic flow.} \quad (26.31)$$

In this limit it is accurate to ignore the centrifugal acceleration, which is commonly the case for large-scale flows. Even so, it is an approximation, with the centrifugal acceleration identically zero only for straight line motion on a plane.

## 26.4 Inertial motion

Inertial motion occurs under the following conditions:

- vanishing pressure gradient
- vanishing friction,

so that the equations of motion (26.13a) and (26.13b) take the form

$$\frac{D|\mathbf{u}|}{Dt} = 0 \quad (26.32a)$$

$$\frac{|\mathbf{u}|^2}{R} + f |\mathbf{u}| = 0. \quad (26.32b)$$

Equation (26.32a) says that inertial motion occurs with constant speed, whereas equation (26.32b) says that the motion maintains the balance between Coriolis and centrifugal accelerations

$$f |\mathbf{u}| = -\frac{|\mathbf{u}|^2}{R}. \quad (26.33)$$

Hence, local Rossby number has a unit magnitude

$$|\text{Ro}_{\text{local}}| = \frac{|\mathbf{u}|}{|R| |f|} = 1. \quad (26.34)$$

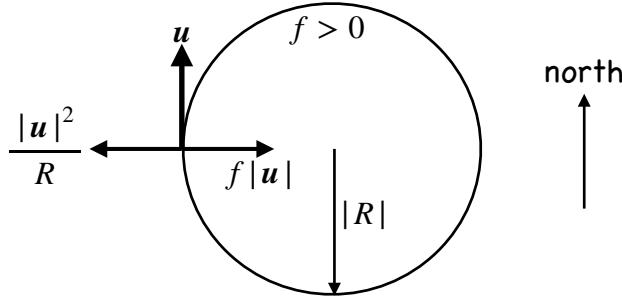


FIGURE 26.5: Inertial motion of a fluid on a plane occurs when the flow is horizontal, frictionless, and the centrifugal acceleration balances the Coriolis in the presence of zero pressure gradient. We here depict motion assuming  $f > 0$  as for the northern hemisphere, revealing that inertial motion is an anti-cyclonic circular motion with radius  $|R| = |\mathbf{u}|/|f|$ . When turning to the right as in the northern hemisphere, the radius of curvature for the inertial circle is negative (see Figure 26.2 for sign convention), so that  $R = -|\mathbf{u}|/f < 0$ .

### 26.4.1 Anti-cyclonic circular motion on $f$ -plane

To further understand inertial motion, rearrange equation (26.33) so that

$$f = -\frac{|\mathbf{u}|}{R}, \quad (26.35)$$

in which case the radius for the inertial circle is

$$R = -|\mathbf{u}|/f. \quad (26.36)$$

Equation (26.35) can be satisfied in the northern hemisphere ( $f > 0$ ) only for motion turning to the right (in which  $R < 0$ ). The opposite orientation occurs in the southern hemisphere, where inertial motion turns to the left so that the radius of curvature is positive,  $R = -|\mathbf{u}|/f > 0$  (see Figure 26.2 for the sign convention on the radius of curvature). Hence, inertial motion is oriented anti-cyclonically (orientated opposite to the earth's rotation). If the Coriolis parameter is constant, then the motion is circular, as depicted in Figure 26.5.

To emphasize the balance, return to equation (26.33) and recall that the Coriolis acceleration in the northern hemisphere points to the right when facing downstream, as per equation (26.11). Hence, the balance (26.33) is between the Coriolis acceleration pointing to the right and the centrifugal acceleration pointing to the left. That is, the Coriolis acceleration provides the centripetal acceleration to balance the centrifugal acceleration.

### 26.4.2 Period for inertial motion

Equation (26.36) says that the speed of a fluid element is given by the radius of curvature times the magnitude of the Coriolis parameter

$$|\mathbf{u}| = R|f|. \quad (26.37)$$

The time for a fluid element to traverse an inertial circle is given by the circumference of the circle,  $2\pi R$ , divided by the constant speed, thus yielding the inertial period

$$T_{\text{inertial}} = \frac{2\pi R}{|\mathbf{u}|} = \frac{2\pi}{|f|}. \quad (26.38)$$

We encountered this inertial period in Section 10.5 when considering inertial oscillations for a point particle.

### 26.4.3 Observing inertial motion

Inertial motion is rarely observed in the atmosphere since fluid motion nearly always occurs in the presence of a pressure gradient. In contrast, surface ocean flow is commonly generated by wind stresses that setup motion even in the absence of pressure gradients. The moving fluid then engenders a Coriolis acceleration, in which case there can be a balance between centrifugal and Coriolis for the moving ocean fluid. As a result, the observed surface ocean currents have nontrivial power within the inertial frequency band, rivaling energy contained in frequencies associated with astronomical tides (e.g., see Figure 3.3 of [Holton \(1992\)](#)).

How large is an inertial circle? Consider a surface ocean current speed of  $|\mathbf{u}| \sim 0.1 \text{ m s}^{-1}$ , which is not atypical of current speeds outside of strong boundary currents or mesoscale eddies, and assume the Coriolis parameter  $f = 10^{-4} \text{ s}^{-1}$ . In this case the inertial radius is

$$R_{\text{inertial}} \approx 10^3 \text{ m.} \quad (26.39)$$

Observations of inertial motion, such as that reproduced in Figure 8.3 of [Gill \(1982\)](#), confirm that the radii are indeed on the order of a few kilometers.

### 26.4.4 Inertial motion is Lagrangian

The analysis in this section concerns a fluid element moving without feeling the impacts from pressure forces. The fluid thus exhibits the same force balance as the point particle discussed in Section 10.5. So although we can measure inertial motion at a fixed point in space, the present considerations are Lagrangian in nature, focusing on motion of fluid elements. Furthermore, the inertial period refers to the time it takes for a fluid element to move around the inertial circle at its constant speed. It does not refer to the period of a wave, for example, and yet there are inertial waves (Section 25.6) with this period as well as inertia-gravity waves that have periods close to the inertial period (Section 31.8),

### 26.4.5 “Inertial” motion does not refer to an inertial frame

We make use of the term “inertial” when referring to inertial motion since both the Coriolis and centrifugal accelerations are nonzero only in the presence of motion; i.e., they require the inertia obtained by a moving massive body. Hence, as noted in Section 10.5.4, “inertial motion” in this context does *not* refer to the motion viewed in the inertial reference frames discussed in Section 9.3.

### 26.4.6 Inertial motion on a sphere

In the analysis thus far, we have assumed an  $f$ -plane so that inertial motion is circular. Without solving the spherical equations for inertial motion we can anticipate what happens when such motion occurs on a sphere. As a fluid element moves to higher latitudes the magnitude of the Coriolis parameter increases, thus decreasing the radius of curvature. The opposite happens when moving equatorward. This effect of planetary sphericity leads to an egg-shaped pattern that does not close but instead drifts to the west. Now consider inertial motion that spans the equator. As the fluid crosses the equator, where  $f = 0$ , the radius of curvature is infinite so that the motion is straight. When moving away from the equator the Coriolis parameter increases, which causes a fluid element to turn and close its path, again with a drift to the west. Motion north of the equator turns to the right whereas motion to the south turns left, so that inertial motion that spans the equator forms a figure-eight path. We illustrate this motion in Figure 26.6.

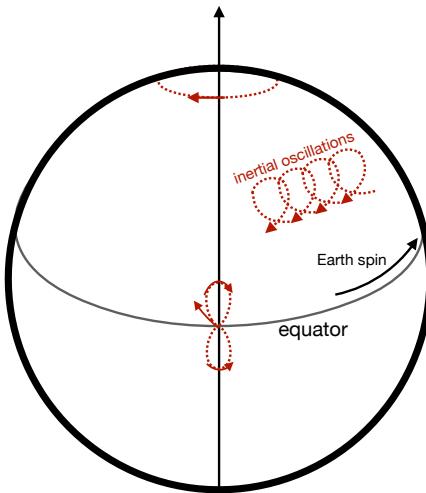


FIGURE 26.6: Depicting inertial motion on a sphere. As the fluid element moves poleward,  $f$  increases so that the radius of curvature decreases. Correspondingly, the fluid motion does not close, but instead the path drifts to the west. This westward drift holds for both hemispheres, where the sense of the motion is anti-cyclonic. The only closed and circular inertial motions are those that encircle the pole. Fluid elements that cross the equator exhibit a figure-eight pattern that also drifts to the west. This figure is taken after Figure 4-14 of [von Arx \(1962\)](#).

## 26.5 Cyclostrophic balance

Cyclostrophic balance occurs under the following conditions:

- fluid element move along lines of constant pressure so that  $\partial p / \partial s = 0$ ;
- vanishing Coriolis acceleration;
- vanishing friction.

The resulting equations of motion (26.13a) and (26.13b) take the form

$$\frac{D|\mathbf{u}|}{Dt} = 0 \quad (26.40a)$$

$$\frac{|\mathbf{u}|^2}{R} = -\frac{1}{\rho_0} \frac{\partial p}{\partial n}. \quad (26.40b)$$

With a vanishing Coriolis acceleration we see that cyclostrophic balance corresponds to local Rossby number that has an infinite magnitude

$$|\text{Ro}_{\text{local}}| = \infty \quad \text{if } f = 0. \quad (26.41)$$

Approximate cyclostrophic balance holds when  $|\text{Ro}_{\text{local}}| \gg 1$ .

Again, equation (26.40a) says that the speed is constant following a material fluid element. Equation (26.40b) says that cyclostrophic flow occurs when the centrifugal acceleration balances the pressure gradient, with the squared speed given by

$$|\mathbf{u}|^2 = -\frac{R}{\rho_0} \frac{\partial p}{\partial n}. \quad (26.42)$$

This equation can be satisfied for either clockwise or counter-clockwise motion around a low pressure center, as shown in Figure 26.7. For clockwise flow, the radius of curvature is negative,  $R < 0$ , whereas  $\partial p / \partial n > 0$ . The signs are swapped for counter-clockwise flow. Cyclostrophic

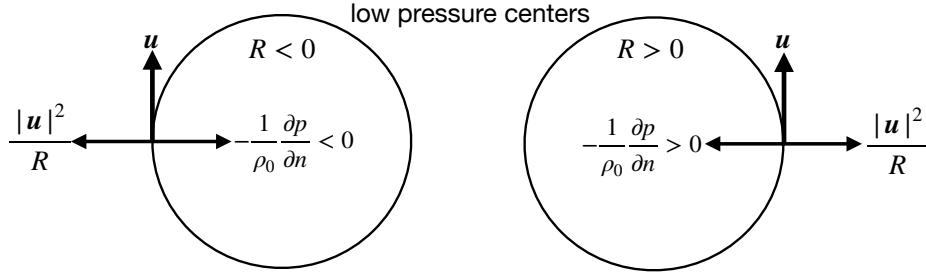


FIGURE 26.7: Cyclostrophic motion of a fluid element on a tangent plane occurs when the flow is horizontal, non-rotating, frictionless, with constant speed, and where the centrifugal acceleration balances the pressure gradient normal to the flow direction. We here depict motion for clockwise and counter-clockwise cyclostrophic flow, both around a low pressure center. Left panel: clockwise motion with radius of curvature,  $R < 0$ , and the pressure gradient pointing in the direction of the normal,  $\frac{1}{\rho_0} \frac{\partial p}{\partial n} > 0$ . Right panel: counter-clockwise motion with radius of curvature,  $R > 0$ , and the pressure gradient pointing opposite to the direction of the normal,  $\frac{1}{\rho_0} \frac{\partial p}{\partial n} < 0$ . Cyclostrophic balance does not occur for flow around a high pressure center. The reason is that if both the pressure and centrifugal accelerations point away from the center, then they are unable to balance one another.

balance cannot be maintained around a high pressure center. The reason is that if both the pressure and centrifugal accelerations point away from the circle's center, then they are unable to balance one another.

Cyclostrophic balance is relevant for scales on the order of a tornado, with a radius on the order of 300 m where tangential speeds are on the order of  $30 \text{ m s}^{-1}$  (see Section 3.2.4 of [Holton \(1992\)](#)). For this flow scale, the Rossby number is on the order of 1000 at middle latitudes, thus justifying neglect of the Coriolis acceleration. Although tornadoes in cyclostrophic balance can rotate either clockwise or counter-clockwise, they are more often observed rotating cyclonically given that they are generally embedded within cyclonic storm systems. In contrast, smaller motions such as dust devils and water spouts are quite often seen rotating in either direction.

## 26.6 Gradient wind balance

Gradient wind balance occurs under the following conditions:

- fluid elements move along lines of constant pressure so that  $\partial p / \partial s = 0$ ;
- vanishing friction.

The resulting equations of motion (26.13a) and (26.13b) take the form

$$\frac{D|\mathbf{u}|}{Dt} = 0 \quad (26.43a)$$

$$\frac{|\mathbf{u}|^2}{R} + f |\mathbf{u}| = -\frac{1}{\rho_0} \frac{\partial p}{\partial n}, \quad (26.43b)$$

Again, equation (26.43a) says that the speed is constant following a material fluid element. Equation (26.43b) says that gradient wind balanced flow occurs when the centrifugal and Coriolis accelerations balance the pressure gradient acting normal to the motion.

The local Rossby number is order unity for the gradient wind balance

$$|\text{Ro}_{\text{local}}| = \frac{|\mathbf{u}|}{|R| |f|} \sim 1, \quad (26.44)$$

meaning that both centrifugal and Coriolis accelerations are both important as they balance the

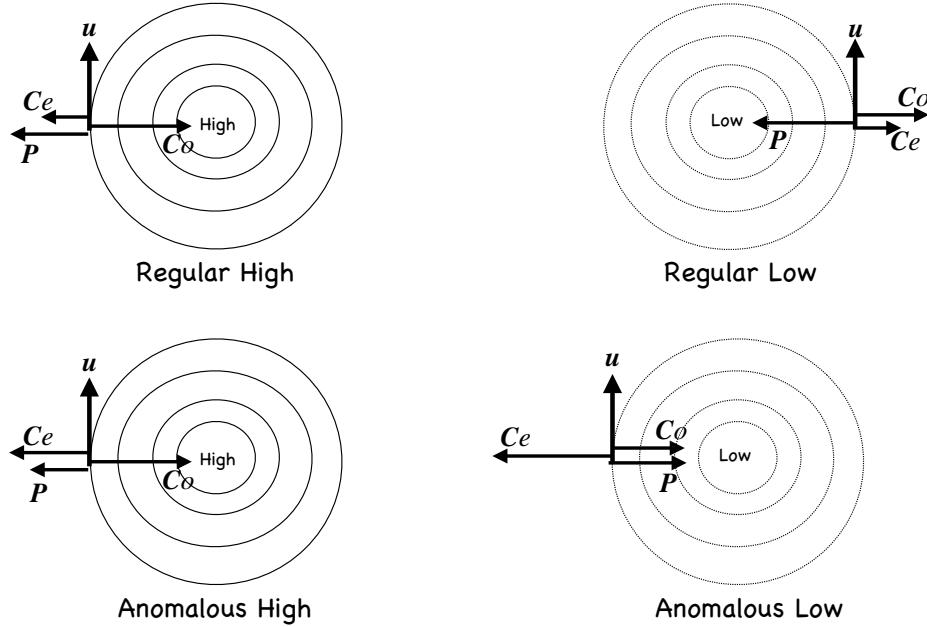


FIGURE 26.8: The variety of gradient wind balances available in the northern hemisphere ( $f > 0$ ). Gradient wind balance occurs when the flow is horizontal, frictionless, with constant speed, and where the centrifugal, pressure, and Coriolis accelerations balance under a variety of magnitudes. To reduce clutter, we use the following shorthand for the accelerations:  $P = -\rho_0^{-1} \partial p / \partial n$ ,  $Co = f |\mathbf{u}|$ , and  $Ce = |\mathbf{u}|^2 / R$ . Upper left panel: motion around a regular high pressure center, whereby the centrifugal acceleration helps the pressure acceleration to balance the Coriolis acceleration. The pressure acceleration is larger in magnitude than the centrifugal. This flow is termed “regular” as it directly corresponds to geostrophic flow around a high pressure center. Lower left panel: motion around an anomalous high pressure center, whereby the centrifugal acceleration helps the pressure acceleration to balance the Coriolis acceleration, with the pressure acceleration smaller in magnitude than the centrifugal. This flow is termed “anomalous” as the pressure acceleration is subdominant to the centrifugal, in contrast to the case of geostrophic flow. Upper right panel: motion around a regular low pressure center, whereby the Coriolis and centrifugal accelerations balance the pressure acceleration. Lower right panel: motion around an anomalous low pressure center, whereby the Coriolis and pressure accelerations balance the centrifugal acceleration. Note the opposite flow orientation between the regular and anomalous lows, whereas the regular and anomalous highs have the same flow orientation.

pressure gradient. Recall that the inertial motion from Section 26.4 has  $|\text{Ro}_{\text{local}}| = 1$ , which arises when the pressure gradient vanishes so that the Coriolis and centrifugal terms have equal but opposite magnitudes. The nonzero pressure gradient makes gradient wind flow fundamentally distinct from inertial motion.

### 26.6.1 Constraints on gradient wind flow

The quadratic formula leads to the following expression for the speed of gradient wind flow

$$|\mathbf{u}| = \frac{R}{2} \left[ f \pm \sqrt{f^2 - \frac{4}{R} \frac{1}{\rho_0} \frac{\partial p}{\partial n}} \right]. \quad (26.45)$$

The speed is a real number if the pressure gradient, Coriolis parameter, and radius of curvature satisfy

$$f^2 > \frac{4}{R} \frac{1}{\rho_0} \frac{\partial p}{\partial n} \implies \frac{1}{\rho_0} \left| \frac{\partial p}{\partial n} \right| \leq \frac{|R| f^2}{4}. \quad (26.46)$$

This relation has direct implications for the structure of the pressure field depending on the sign of the radius of curvature. In particular, as seen in the following, this constraint implies that the pressure gradient at the center of a high pressure region must go to zero as the radius of curvature vanishes, which renders the pressure field relatively flat near the center of highs. In contrast, there is no analogous limit for the magnitude of the pressure gradient approaching a low pressure center. This asymmetry between high and low pressures manifests in atmospheric flow with low pressure centers (cyclonic lows) having stronger magnitude than high pressure centers (anti-cyclonic highs).

### 26.6.2 The variety of gradient wind flows

We now identify the following force balances available with a gradient wind balance, with illustrations provided in Figure 26.8.

#### *Regular high pressure center (right turn with high pressure on right)*

A *regular high pressure* occurs with  $R < 0$  and  $\partial p/\partial n \leq 0$ . This case occurs with the centrifugal and pressure accelerations pointing away from the center, and these balance the Coriolis acceleration pointing to the high pressure center (upper left panel of Figure 26.8).

The inequality (26.46) provides a bound to the size of the pressure gradient since

$$\frac{1}{\rho_0} \frac{\partial p}{\partial n} \leq \frac{R f^2}{4} \quad \text{with } R \leq 0 \quad \text{and} \quad \frac{\partial p}{\partial n} \leq 0 \implies \frac{1}{\rho_0} \left| \frac{\partial p}{\partial n} \right|_{\max} = \frac{|R| f^2}{4}. \quad (26.47)$$

That is, the pressure gradient for a regular high cannot be larger than this bound in order for there to be a gradient wind solution. Since  $R \rightarrow 0$  as the center is approached, the normal pressure gradient,  $\partial p/\partial n$ , in turn must vanish towards the center. Holton (1992) identifies two subcases for this balance depending on the relative size of the pressure and centrifugal accelerations, with the anomalous high the case where the pressure gradient acceleration is weaker than the centrifugal (lower left panel of Figure 26.8).

#### *Regular low (left turn with low pressure on left)*

This flow occurs with  $R \geq 0$  and  $\partial p/\partial n \leq 0$ , so that the inequality (26.46) is always satisfied

$$\frac{1}{\rho_0} \frac{\partial p}{\partial n} \leq \frac{R f^2}{4} \quad \text{with } R \geq 0 \quad \text{and} \quad \frac{\partial p}{\partial n} \leq 0 \implies \text{arbitrary size to } \left| \frac{\partial p}{\partial n} \right|. \quad (26.48)$$

Hence, there is no constraint imposed by gradient wind balance on the size of the pressure gradient magnitude,  $|\partial p/\partial n|$ . So the low pressure center can be arbitrarily strong and still maintain a gradient wind balance. Furthermore, the Coriolis and centrifugal accelerations point away from the low pressure center, and these two accelerations balance the pressure acceleration that points toward the center (upper right panel of Figure 26.8).

#### *Anomalous low (right turn with low pressure on right)*

This flow occurs with  $R < 0$  and  $\partial p/\partial n \geq 0$ . This case occurs with the Coriolis and pressure accelerations pointing toward the low pressure center, and these two accelerations balance the centrifugal acceleration pointing away from the center (lower right panel of Figure 26.8). As with the regular low, the inequality (26.46) provides no bound to the magnitude of the low pressure. Note the opposite orientation for the flow around an anomalous low relative to the regular low.

*Left turn with high pressure on left*

In this case  $R > 0$  and  $\partial p / \partial n > 0$ . There is no solution for the northern hemisphere since all accelerations point to the right of the motion thus disallowing any balance.

### 26.6.3 Comments

As noted in Section 3.2 of [Holton \(1992\)](#), the difference between gradient wind speeds and geostrophic wind speeds is no more than 10% to 20% in middle latitude synoptic atmosphere flow. In the tropics, where geostrophy becomes less relevant, it is important to apply the gradient wind relation to capture the balanced flow states. Furthermore, [van Heijst \(2010\)](#) and Chapter 18 of [Cushman-Roisin and Beckers \(2011\)](#) make use of a gradient wind analysis for the study of ocean vortices. The deviations from geostrophy become important when considering relatively small ocean vortices and/or tropical vortices.



# Chapter 27

## Ekman mechanics

A *boundary layer* is a region of the fluid that is directly affected by boundaries. For geophysical applications we have in mind the solid-earth boundary that interacts with both the ocean and atmosphere, the ocean-atmosphere interface, and the ocean-cryosphere and atmosphere-cryosphere boundaries. The fluid flow in geophysical boundary layers is generally very turbulent, thus causing rapid mixing and the transfer of properties within the boundary layer, along with the transport of properties between the boundary layer and the less turbulent fluid interior. Boundary layer physics is a well developed discipline for geophysical as well as engineering applications. Our treatment is relatively superficial by comparison to the focused treatments given by books such as [Tennekes and Lumley \(1972\)](#), [Stull \(1988\)](#), and [Thorpe \(2005\)](#).

Here, we are particularly focused on the rudiments of *Ekman mechanics*, which is concerned with flow affected by accelerations from horizontal pressure gradients, vertical friction, and Coriolis, with particular attention given to regions near boundaries where friction is especially large and *Ekman boundary layers* form. The leading role for Coriolis acceleration causes Ekman boundary layers to exhibit behaviors quite distinct from their non-rotating cousins mentioned in Section 18.9.7. In particular, Ekman boundary layer flows are horizontally divergent, thus leading to the vertical exchange of mass, tracers, momentum, and vorticity between the boundary layer and the fluid region outside of the boundary layer (i.e., the fluid interior). In so doing, the Ekman layer flow imparts a stretching and squeezing of interior fluid columns that strongly couples the boundary layer to vorticity and circulation of the fluid interior. This role for Ekman layers is especially crucial for the ocean general circulation.

### READER'S GUIDE TO THIS CHAPTER

To introduce the subject we exhibit the role of friction in producing a down pressure gradient component to the flow, making use of natural coordinates from Chapter 26 for this purpose. The remainder of the chapter focuses on the mechanics of Ekman boundary layers, with this study greatly extending our understanding of strongly rotating flows from Chapter 25. Indeed, the addition of friction to an otherwise geostrophically balanced flow provides a surprising level of richness that motivates the variety of perspectives presented in this chapter.

Ekman boundary layers are a key element in the study of ocean circulation, particularly the wind-driven circulation. We here borrow liberally from the material in Section 9.2 of [Gill \(1982\)](#), Section 6.2 of [Apel \(1987\)](#), Section 7.4 of [Marshall and Plumb \(2008\)](#), Chapter 8 of [Cushman-Roisin and Beckers \(2011\)](#), Section 5.7 of [Vallis \(2017\)](#), and materials from [Thorpe](#)

(1988) and Thorpe (2005). A presentation consistent with engineering boundary layers can be found in Section 5.3 of Tennekes and Lumley (1972).

27.1	The dynamical balances . . . . .	654
27.2	Horizontal balances in natural coordinates . . . . .	655
27.2.1	Natural coordinates according to isobars . . . . .	655
27.2.2	Geostrophic and Ekman balances . . . . .	656
27.2.3	Rayleigh drag . . . . .	657
27.2.4	Cross isobar flow driven by Rayleigh drag . . . . .	657
27.2.5	Horizontal spiral plus vertical rising/sinking . . . . .	659
27.2.6	Further study . . . . .	659
27.3	Ekman number and Ekman layer thickness . . . . .	659
27.3.1	Laplacian vertical friction . . . . .	660
27.3.2	Non-dimensionalization . . . . .	660
27.3.3	Defining the Ekman number and layer thickness . . . . .	661
27.3.4	Estimates for the vertical eddy viscosity . . . . .	661
27.4	Ocean surface Ekman layer . . . . .	662
27.4.1	Horizontal mass transport within the Ekman layer . . . . .	662
27.4.2	Example Ekman mass transports . . . . .	663
27.4.3	Mass budget for the Ekman layer . . . . .	664
27.4.4	Ekman layer coupled to the geostrophic interior . . . . .	666
27.4.5	Further study . . . . .	668
27.5	Bottom Ekman layer . . . . .	668
27.5.1	Horizontal mass transport within the Ekman layer . . . . .	669
27.5.2	Mass budget for the bottom Ekman layer . . . . .	669
27.5.3	An analytic bottom Ekman spiral velocity . . . . .	669
27.5.4	Comments . . . . .	672
27.6	Arrested bottom Ekman flows . . . . .	673
27.6.1	Description . . . . .	673
27.6.2	Applications . . . . .	673
27.7	Exercises . . . . .	675

## 27.1 The dynamical balances

Throughout this chapter we make use of a steady, linear, Boussinesq, and hydrostatic fluid maintaining a balance between the horizontal accelerations from Coriolis, pressure, and friction

$$f \hat{z} \times \mathbf{u} = -\frac{1}{\rho_o} \nabla_z p + \mathbf{F}. \quad (27.1)$$

This balance is most relevant over large horizontal length scales as per the planetary geostrophic equations of Section 25.5.

The frictional acceleration,  $\mathbf{F}$ , of interest in this chapter arises from the vertical exchange of horizontal momentum between fluid layers. Turbulence induced viscous exchange is especially large in boundary regions such as the ocean surface and next to the ocean and atmosphere bottom. In such turbulent boundary layer regions we make use of the eddy viscosity, which is much larger than molecular values

$$\nu^{\text{eddy}} \gg \nu. \quad (27.2)$$

We have more to say regarding the frictional operator in Section 27.3.1.

For conceptual and mathematical convenience, we find it useful to separate the horizontal

velocity into two components. The first is the geostrophic velocity defined by a balance between pressure gradient and Coriolis accelerations

$$f \hat{z} \times \mathbf{u}_g = -\frac{1}{\rho_0} \nabla_z p \implies \mathbf{u}_g = \frac{1}{f \rho_0} \hat{z} \times \nabla p. \quad (27.3)$$

In some treatments,  $\mathbf{u}_g$  is referred to as the *pressure driven velocity*. The second is an *ageostrophic* or Ekman component defined by a balance between the frictional and Coriolis accelerations

$$f \hat{z} \times \mathbf{u}_e = \mathbf{F} \implies \mathbf{u}_e = -f^{-1} \hat{z} \times \mathbf{F}, \quad (27.4)$$

so that  $\mathbf{u}_e$  is the *frictional driven velocity*.

This velocity decomposition has the appearance of superposing linearly independent flows, one geostrophic (pressure driven) and one ageostrophic (friction driven). However, the flows are coupled and thus not linearly independent. Namely, ageostrophic motions alter the pressure field which in turn affects the geostrophic flow. So the presence of friction and the associated ageostrophic flows lead to geostrophic flows differing from the inviscid case. Conversely, geostrophic flows affect the level of friction. Hence, the above decomposition does not reflect a physical decoupling of geostrophic and ageostrophic flows. Rather, it is only meant to help in our description of the flow and their force balances.

## 27.2 Horizontal balances in natural coordinates

We here study balances occurring in horizontal flows maintaining a frictional geostrophic balance. As per the definition (27.3), geostrophic motion occurs along lines of constant pressure, with frictionally induced deviations crossing isobars and providing a down pressure gradient component to the fluid trajectory. Motivated by the discussion in Chapter 26, we make use of natural coordinates for the kinematics.

### 27.2.1 Natural coordinates according to isobars

We represent the horizontal flow according to natural coordinates defined along an arbitrary geopotential surface. Instead of defining the natural coordinates according to the flow direction, as done in Section 26.2 for the frictionless case, we here decompose the motion according to pressure contours (isobars). The unit vector  $\hat{s}$  is defined tangent to isobars in the horizontal plane and directed along the direction of geostrophic flow. We define the direction,  $\hat{n}$ , to be perpendicular to isobars and oriented down the horizontal pressure gradient

$$\hat{n} = -\frac{\nabla_z p}{|\nabla_z p|}. \quad (27.5)$$

As illustrated in Figure 27.1, in the northern hemisphere  $\hat{n}$  points to the left of the geostrophic velocity, whereas it is to the right in the southern hemisphere. We thus have the northern hemisphere triplet of unit vectors

NORTHERN HEMISPHERE TRIPLET OF DIRECTIONS

$$\hat{z} = \hat{s} \times \hat{n} = \text{vertical direction} \quad (27.6a)$$

$$\hat{n} = \hat{z} \times \hat{s} = \text{down pressure gradient direction} \quad (27.6b)$$

$$\hat{s} = \hat{n} \times \hat{z} = \text{tangent to isobar in direction of geostrophic flow.} \quad (27.6c)$$

In the southern hemisphere, since  $\hat{\mathbf{n}}$  points to the right of  $\hat{\mathbf{s}}$ , the triplet of directions becomes

## SOUTHERN HEMISPHERE TRIPLET OF DIRECTIONS

$$\hat{\mathbf{z}} = \hat{\mathbf{n}} \times \hat{\mathbf{s}} = \text{vertical direction} \quad (27.7a)$$

$$\hat{\mathbf{n}} = \hat{\mathbf{s}} \times \hat{\mathbf{z}} = \text{down pressure gradient direction} \quad (27.7b)$$

$$\hat{\mathbf{s}} = \hat{\mathbf{z}} \times \hat{\mathbf{n}} = \text{tangent to isobar in direction of geostrophic flow.} \quad (27.7c)$$

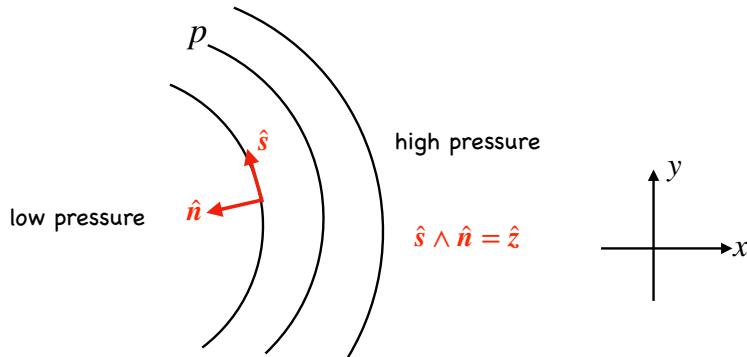


FIGURE 27.1: Natural coordinates defined along an arbitrary geopotential surface according to isobars in the horizontal plane, here depicted for the northern hemisphere. The normal direction,  $\hat{\mathbf{n}} = -\nabla_z p / |\nabla_z p|$ , is oriented down the horizontal pressure gradient so that it points to the left of the geostrophic velocity (facing downstream) in the northern hemisphere and to the right in the southern hemisphere. The tangent direction,  $\hat{\mathbf{s}}$ , points along the isobar in the direction of the geostrophic velocity.

### 27.2.2 Geostrophic and Ekman balances

As found when studying the geostrophic balance in Section 26.3, the geostrophic velocity flows along isobars and so only has a component in the  $\hat{\mathbf{s}}$  direction

$$\hat{\mathbf{s}} \cdot \mathbf{u}_g = -\frac{1}{f\rho_0} \frac{\partial p}{\partial n} \quad \text{and} \quad \hat{\mathbf{n}} \cdot \mathbf{u}_g = 0 \quad (27.8)$$

In contrast, the Ekman velocity has a component both along and across isobars. For the northern and southern hemispheres we have

$$\hat{\mathbf{s}} \cdot \mathbf{u}_e = |f|^{-1} \hat{\mathbf{n}} \cdot \mathbf{F} \quad \text{and} \quad \hat{\mathbf{n}} \cdot \mathbf{u}_e = -|f|^{-1} \hat{\mathbf{s}} \cdot \mathbf{F}. \quad (27.9)$$

As expected, the Ekman velocity vanishes when the frictional acceleration vanishes, in which case the flow reduces to the geostrophic flow that moves along isobars so that  $\hat{\mathbf{s}} = \hat{\mathbf{u}}$ . However, when there is a nonzero friction aligned along isobars, that drives an Ekman velocity across isobars. Conversely, friction aligned across isobars drives Ekman velocities along isobars.

We arrive at a complementary perspective on the origin of cross-isobar flow through the following considerations. Without friction, the Coriolis and pressure gradient accelerations balance when the flow is geostrophic. In the presence of friction, the velocity is slowed so that the Coriolis acceleration weakens. If the pressure gradient acceleration is retained, as occurs if it is determined by large scale balances outside of the Ekman layer, then the Coriolis acceleration no longer balances the pressure gradient. Consequently, flow is diverted from isobars and develops a component down the pressure gradient.

### 27.2.3 Rayleigh drag

The relative simplicity of Rayleigh drag facilitates analytical expressions for the Ekman velocity using natural coordinates, written in terms of the geostrophic velocity (equation (27.8)). In doing so we are afforded an explicit illustration of how the Ekman flow provides a cross-isobar component to the flow in the direction down the pressure gradient. Before developing the Ekman flows we here summarize elements of Rayleigh drag.

In Section 21.3.2 we studied how Rayleigh drag affects the kinetic energy budget. As a reminder, consider a frictional acceleration in the form of a Rayleigh drag acting on the velocity field

$$\mathbf{F} = -\frac{U_{\text{fric}} \mathbf{u}}{\delta} = -\gamma \mathbf{u}, \quad (27.10)$$

where  $\delta$  is a depth scale and  $U_{\text{fric}}$  is a friction velocity scale with dimensions  $L/T$ . The ratio

$$\gamma = \frac{U_{\text{fric}}}{\delta} \quad (27.11)$$

has dimensions  $T^{-1}$  and is an inverse spin-down time. That is, if only Rayleigh drag affected changes to the horizontal momentum,  $\partial_t \mathbf{u} = -\gamma \mathbf{u}$ , then the flow would exponentially come to a halt with an e-folding time  $\gamma^{-1}$ . The drag is relatively large over rough surfaces, thus leading to a small e-folding time. In particular, drag on the lower atmospheric winds is larger over land than over the ocean. The reason is that trees, cities, and mountains dissipate more of the atmosphere's mechanical energy than interactions with the relatively smooth ocean surface (see Section 18.9.7 for a discussion of roughness length).

Rayleigh drag dissipates all flow features regardless of their spatial structure. That is, Rayleigh drag does not prefer any particular length scales in the fluid flow. This lack of scale selectivity contrasts to the Laplacian friction discussed in Section 27.3.1, with Laplacian friction dissipating small spatial scales more strongly than large scales. Correspondingly, Rayleigh drag does not generally provide the means to produce a boundary layer. Hence, when studying physics within the Ekman boundary layer in Section 27.3 we make use of Laplacian friction. But for now, Rayleigh drag provides a very useful means to analytically illustrate the role of friction in producing spiral flows with non-zero horizontal divergence.

### 27.2.4 Cross isobar flow driven by Rayleigh drag

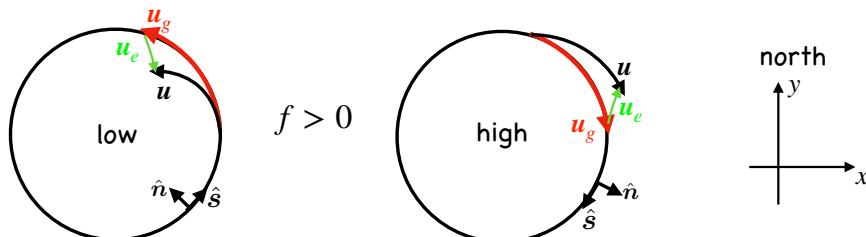


FIGURE 27.2: Illustrating frictional geostrophic flow in the northern hemisphere ( $f > 0$ ). Left panel: geostrophic flow,  $\mathbf{u}_g$ , around a low pressure center is counter-clockwise and aligned with pressure isobars. Friction aligned along the isobars drives Ekman flow,  $\mathbf{u}_e$ , that has a component down the pressure gradient (normal to the geostrophic flow) as well as a component that is directed opposite the geostrophic flow. Consequently, the total velocity,  $\mathbf{u}_g + \mathbf{u}_e$ , spirals into the low pressure center. Right panel: the opposite oriented flow occurs around high pressure centers, where fluid spirals away from the high due to the cross-isobar flow driven by friction. By the definition given by equation (27.6b), the normal direction,  $\hat{n}$ , is directed down the pressure gradient, whereas  $\hat{s}$  is tangent to the isobar and directed along the geostrophic flow direction.

Making use of the Rayleigh drag (27.10) brings the northern hemisphere expressions (27.9) for the Ekman velocity into the form

$$\hat{s} \cdot \mathbf{u}_e = f^{-1} \hat{n} \cdot \mathbf{F} = -(\gamma/f) \hat{n} \cdot \mathbf{u} = -(\gamma/f) \hat{n} \cdot \mathbf{u}_e \quad (27.12a)$$

$$\hat{n} \cdot \mathbf{u}_e = -f^{-1} \hat{s} \cdot \mathbf{F} = (\gamma/f) \hat{s} \cdot (\mathbf{u}_e + \mathbf{u}_g). \quad (27.12b)$$

Similar considerations for the southern hemisphere lead to the general result for both hemispheres

$$\hat{s} \cdot \mathbf{u}_e = -(\gamma/|f|) \hat{n} \cdot \mathbf{u}_e \quad (27.13a)$$

$$\hat{n} \cdot \mathbf{u}_e = (\gamma/|f|) \hat{s} \cdot (\mathbf{u}_e + \mathbf{u}_g). \quad (27.13b)$$

These equations allow us to express the Ekman velocity in terms of the geostrophic velocity (equation (27.8)), with results for both hemispheres given by

$$\hat{n} \cdot \mathbf{u}_e = \hat{s} \cdot \mathbf{u}_g \left[ \frac{\gamma |f|}{f^2 + \gamma^2} \right] \quad (27.14a)$$

$$\hat{s} \cdot \mathbf{u}_e = -\hat{s} \cdot \mathbf{u}_g \left[ \frac{\gamma^2}{\gamma^2 + f^2} \right]. \quad (27.14b)$$

Equation (27.14a) says that the normal component to the Ekman velocity is directed down the pressure gradient. Equation (27.14b) says that the component of the Ekman velocity along the pressure isobar is directed opposite to the geostrophic velocity. We provide an example of an Ekman velocity in Figure 27.2 for the northern hemisphere.

Bringing all pieces together leads to the components for the total velocity,  $\mathbf{u} = \mathbf{u}_g + \mathbf{u}_e$ , and its squared magnitude

$$\hat{s} \cdot \mathbf{u}_g = -\frac{1}{f\rho_0} \frac{\partial p}{\partial n} \quad \text{geostrophic velocity (aligned along isobars)} \quad (27.15a)$$

$$\hat{s} \cdot \mathbf{u} = \hat{s} \cdot \mathbf{u}_g \left[ \frac{f^2}{f^2 + \gamma^2} \right] \quad \text{isobaric velocity component} \quad (27.15b)$$

$$\hat{n} \cdot \mathbf{u} = (\gamma/|f|) \hat{s} \cdot \mathbf{u} \quad \text{normal velocity component} \quad (27.15c)$$

$$(\hat{s} \cdot \mathbf{u})^2 + (\hat{n} \cdot \mathbf{u})^2 = \frac{(\hat{s} \cdot \mathbf{u}_g)^2}{1 + (\gamma/f)^2} \quad \text{horizontal kinetic energy per mass.} \quad (27.15d)$$

The cross-isobar flow (equation (27.15c)) is directly driven by the Rayleigh drag, and it is directed down the pressure gradient so long as the flow has a positive projection onto the tangent direction

$$\hat{s} \cdot \mathbf{u} > 0 \implies \hat{n} \cdot \mathbf{u} > 0. \quad (27.16)$$

When flow is moving counter-clockwise around a low pressure in the northern hemisphere, where  $\hat{n}$  points towards the low pressure center, then Rayleigh drag causes the fluid to spiral into the low pressure center. Conversely, when flow is moving clockwise around a high pressure, with  $\hat{n}$  pointing away from the high pressure center, then Rayleigh drag causes the fluid to spiral away from the high pressure center. We depict these cases in Figure 27.2. Furthermore, equation (27.15d) shows that when  $\gamma \neq 0$  the magnitude of the total flow is reduced relative to the geostrophic flow, thus reflecting the dissipation of kinetic energy arising from Rayleigh drag (Section 21.3.2).

## 27.2.5 Horizontal spiral plus vertical rising/sinking

Thus far, we have focused on the horizontal spiral motion as shown in Figure 27.2. Through continuity we infer a corresponding vertical motion induced by the convergence of mass into the low pressure center and the divergence of mass away from the high pressure center. Figure 27.3 illustrates the vertical motion in a bottom Ekman boundary layer of either the atmosphere or ocean whereby mass rises above a low pressure center in response to the horizontal convergence of mass in the Ekman layer. Conversely, mass diverges from the high pressure Ekman layer, with this divergence inducing a sinking motion over the high pressure to replace the diverging mass. In subsequent sections of this chapter we develop the formalism needed to compute the mass transport into and out of the Ekman boundary layer, with this mass transport playing a particularly important role in how mechanical forcing drives the wind-driven ocean circulation.

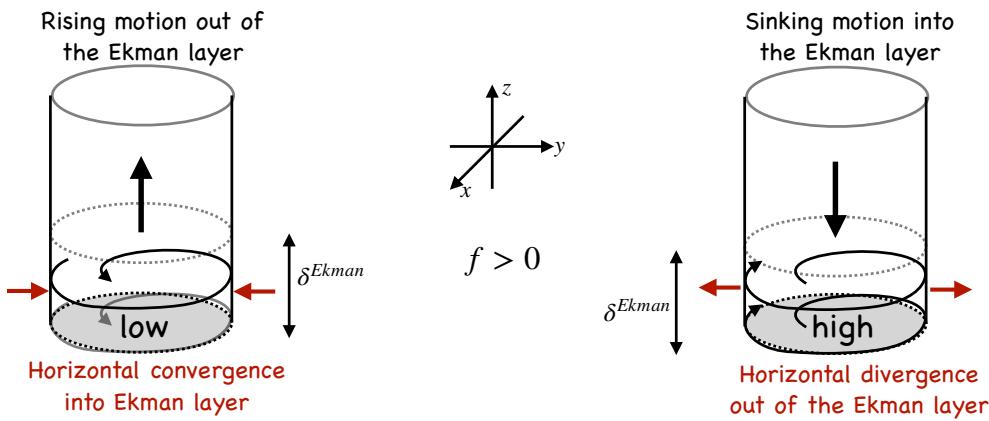


FIGURE 27.3: Illustrating the three-dimensional flow associated with Ekman layers in the northern hemisphere ( $f > 0$ ) next to a bottom boundary. Left panel: flow spiralling into a low pressure center creates convergence of mass into the Ekman layer. Mass continuity means that flow must vertically leave the Ekman layer to thus enter the interior fluid above. Right panel: flow spiralling away from a high pressure center creates divergence of mass away from the Ekman layer. Mass continuity means that flow must vertically sink into the Ekman layer from above. The Ekman layer thickness is denoted by  $\delta^{Ekman}$  (Section 27.3). An analogous picture holds for the surface Ekman layer in the ocean, yet with the Ekman layer at the top of the column rather than the bottom.

## 27.2.6 Further study

The discussion of Ekman velocity arising from Rayleigh drag follows a similar treatment in Section 7.4 of [Marshall and Plumb \(2008\)](#).

## 27.3 Ekman number and Ekman layer thickness

Friction that is most prominent near surface and bottom boundaries arises from vertical shears in the horizontal velocity, with shears leading to flow instabilities and the development of turbulence and associated turbulent friction. There is no deductive theory for turbulent friction so we must rely on empirical expressions. These expressions are typically based on a Laplacian viscous operator, partly motivated by the form arising from kinetic theory of gases briefly mentioned in Chapter 11 (see also equation (18.85)). Most notably, this operator supports the development of a boundary layer through maintenance of both the no-slip (homogeneous Dirichlet) and stress (Neumann) boundary conditions.

### 27.3.1 Laplacian vertical friction

We introduced the Laplacian friction operator in Section 18.7.6 when studying stress in fluids. The Laplacian friction operator considered here is given just in terms of the vertical shears of horizontal stresses

$$\mathbf{F}^{\text{viscous}} = \frac{1}{\rho_0} \frac{\partial \boldsymbol{\tau}}{\partial z} = \frac{\partial}{\partial z} \left[ \nu^{\text{eddy}} \frac{\partial \mathbf{u}}{\partial z} \right], \quad (27.17)$$

with  $\nu^{\text{eddy}} > 0$  a turbulent kinematic viscosity with dimensions  $L^2 T^{-1}$ . This form of the friction operator emulates the Laplacian operator representing molecular viscous friction (equation (18.85)). It is also the form most commonly used in theoretical and numerical models.

Expanding the derivative in equation (27.17) reveals that the Laplacian friction is nonzero where there is curvature in the vertical profile of the horizontal velocity, and where there is depth dependence to the viscosity and velocity

$$\mathbf{F}^{\text{viscous}} = \frac{\partial \nu^{\text{eddy}}}{\partial z} \frac{\partial \mathbf{u}}{\partial z} + \nu^{\text{eddy}} \frac{\partial^2 \mathbf{u}}{\partial z^2}. \quad (27.18)$$

The turbulent viscosity generally has a depth dependence, with larger values in the boundary layer where turbulence is most energetic. This form of the friction preferentially acts on velocity exhibiting nontrivial vertical structure, thus acting to smooth any depth dependent behaviour. In Section 46.4 we discuss further mathematical properties of Laplacian friction.

### 27.3.2 Non-dimensionalization

We non-dimensionalize the equations to isolate important non-dimensional numbers affecting the flow regime. In particular, we identify the Ekman number as a measure of the importance of friction relative to rotation, with friction important where the Ekman number is order unity or larger, and unimportant where the Ekman number is much smaller than unity.<sup>1</sup>

We make use of the following scales and associated non-dimensional quantities

$$(x, y) = L(\hat{x}, \hat{y}) \quad z = H\hat{z} \quad (u, v) = U(\hat{u}, \hat{v}) \quad f = f_0 \hat{f} \quad p = P\hat{p} \quad (27.19)$$

where the hat terms are non-dimensional,<sup>2</sup> and we introduced typical scales for horizontal length ( $L$ ), vertical height ( $H$ ), velocity ( $U$ ), Coriolis parameter ( $f_0$ ), and pressure ( $P$ ). For the pressure scale we assume it follows geostrophic scaling so that it can be written

$$P = f_0 \rho_0 U L. \quad (27.20)$$

Inserting the relations (27.19) into equation (27.1) leads to the non-dimensional frictional geostrophic equation

$$\hat{\mathbf{f}} \times \hat{\mathbf{u}} = -\hat{\nabla} \hat{p} + \frac{\mathbf{F}}{f_0 U}. \quad (27.21)$$

---

<sup>1</sup>For flows unaffected by rotation, the Reynolds number is the key non-dimensional number (Section 18.8) determining where viscous friction is important.

<sup>2</sup>In Section 26.2.1 we defined  $\hat{\mathbf{u}}$  as the unit vector pointing along the trajectory of a fluid element. In contrast, we here let  $\hat{\mathbf{u}}$  be the non-dimensional horizontal velocity.

### 27.3.3 Defining the Ekman number and layer thickness

The *Ekman number* as a non-dimensional measure of the relative importance of the frictional acceleration due to vertical shears versus the Coriolis acceleration

$$\text{Ek} = \frac{\text{frictional acceleration from vertical shears}}{\text{Coriolis acceleration}}. \quad (27.22)$$

The Ekman number increases when there is more boundary layer turbulence, in which case the eddy viscosity,  $\nu^{\text{eddy}}$ , is large relative to its small values in the interior region outside of the boundary layer. Additionally, the Ekman number increases when moving towards the equator, where the Coriolis parameter reduces.<sup>3</sup>

For the viscous stress form of Laplacian vertical frictional acceleration (equation (27.17))

$$\mathbf{F}^{\text{viscous}} = \frac{\nu^{\text{eddy}} U}{H^2} \frac{\partial^2 \hat{\mathbf{u}}}{\partial z^2}, \quad (27.23)$$

the Ekman number is given by

$$\text{Ek} = \frac{\nu^{\text{eddy}}}{f_0 H^2}. \quad (27.24)$$

If we take the vertical scale,  $H$ , equal to the depth scale over which interior flow processes occur, then the Ekman number will be very small, even if the eddy viscosity is relatively large. In this case we conclude that friction is negligible, as indeed it is for many purposes where the boundary layer is not of concern.

However, the Ekman number multiplies the highest derivative in equation (27.21). So setting the Ekman number to zero represents a *singular limit*, whose mathematical meaning is that we change the order of the differential equation when setting  $\text{Ek} = 0$ . Reducing the order of the differential equation then means we can only satisfy a reduced number of boundary conditions relative to the  $\text{Ek} > 0$  case. In particular, with  $\text{Ek} = 0$  we can no longer satisfy the no-slip condition at the solid-fluid boundary. In contrast, with any non-zero value of  $\text{Ek} > 0$ , viscosity will drag the flow to zero towards the boundary within a *boundary layer* where friction is leading order. We expect a boundary layer to form over a boundary layer thickness,  $H = \delta^{\text{Ekman}}$ , in which the Ekman number is order unity where friction is of leading order importance

$$H = \delta^{\text{Ekman}} \implies \text{Ek} = \frac{\nu^{\text{eddy}}}{f_0 (\delta^{\text{Ekman}})^2} = 1. \quad (27.25)$$

Turning this equation around we see that the vertical scale,  $\delta^{\text{Ekman}}$ , defines the viscous Ekman boundary layer thickness as a function of the eddy viscosity and Coriolis parameter

$$\text{Ek} = 1 \implies \delta^{\text{Ekman}} = \delta^{\text{viscous}} = \sqrt{\nu^{\text{eddy}} / f_0}. \quad (27.26)$$

### 27.3.4 Estimates for the vertical eddy viscosity

The eddy viscosity is not readily available from direct measurements or first principles theory. However, measuring the boundary layer thickness provides a means to infer a bulk viscosity for the boundary layer

$$\nu^{\text{eddy}} = f_0 (\delta^{\text{Ekman}})^2. \quad (27.27)$$

---

<sup>3</sup>When getting very close to the equator, our assumption of a frictional geostrophic balance breaks down so that other terms in the momentum equation, such as advection, become important.

In the atmosphere, the boundary layer thickness is order 1000 m, so that at mid-latitudes, with  $f_0 = 10^{-4} \text{ s}^{-1}$ , we expect

$$\nu_{\text{atmos}}^{\text{eddy}} \sim 10^2 \text{ m}^2 \text{ s}^{-1}. \quad (27.28)$$

In the ocean, the upper ocean boundary layer depth, outside of the deep convection regions, is roughly 50 m, in which case

$$\nu_{\text{ocean}}^{\text{eddy}} \sim 0.25 \text{ m}^2 \text{ s}^{-1}. \quad (27.29)$$

## 27.4 Ocean surface Ekman layer

It is possible to establish some integrated mass transport properties of the Ekman layer even without specifying details of the friction (i.e., the viscosity) or the stratification. What is needed is the boundary stress. This stress is commonly estimated for the surface ocean given information about the wind speed and atmospheric stratification. Hence, Ekman theory has found much application to studies of the wind-driven ocean circulation, with the integrated properties the most consequential results from Ekman theory. We here focus on the ocean surface Ekman layer and then consider bottom Ekman boundaries for the atmosphere and ocean in Section 27.5.

### 27.4.1 Horizontal mass transport within the Ekman layer

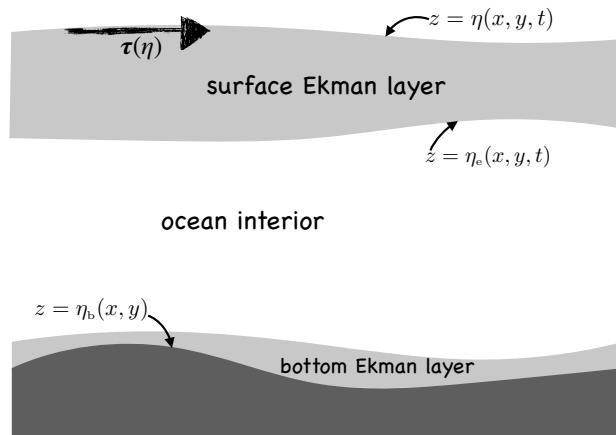


FIGURE 27.4: Ekman layer at the ocean surface, defined for vertical position  $\eta_e(x, y, t) \leq z \leq \eta(x, y, t)$ , with  $\eta_e$  specifying the Ekman layer bottom and  $\eta$  the free surface vertical position. Boundary stress from winds and/or sea ice imparts horizontal momentum to the upper ocean that is transmitted throughout the Ekman layer via the vertical divergence of turbulent horizontal shear stresses. As studied in Section 27.6, there is also a bottom Ekman layer created by stresses active next to the ocean bottom.

We are concerned with the mass budget for the ocean surface Ekman layer sitting between the Ekman layer bottom and the ocean free surface

$$\eta_e(x, y, t) \leq z \leq \eta(x, y, t), \quad (27.30)$$

as depicted in Figure 27.4. Knowledge of the mass budget has implications for how mechanical energy imparted to the boundary layer drives circulation well within the interior of the ocean. This transport and associated circulation are how Ekman mechanics, limited to the boundary layer, affect large-scale ocean circulation throughout the fluid column.

Integrating the horizontal Ekman balance (27.4) over the depth of the Ekman layer leads to

$$\mathbf{M}_e = \int_{\eta_e}^{\eta} \rho_o \mathbf{u}_e dz \implies f \hat{z} \times \mathbf{M}_e = \int_{\eta_e}^{\eta} \rho_o \mathbf{F} dz, \quad (27.31)$$

with  $\mathbf{M}_e$  the depth integrated ageostrophic horizontal mass transport within the Ekman boundary layer. Assuming friction to be in the form of a vertical stress divergence as in equation (27.17) leads to the horizontal Ekman mass transport

$$\mathbf{M}_e = -f^{-1} \hat{z} \times [\boldsymbol{\tau}(\eta) - \boldsymbol{\tau}(\eta_e)]. \quad (27.32)$$

Stress at the bottom of the Ekman layer,  $\boldsymbol{\tau}(\eta_e)$ , matches to the stress in the ocean interior. The stress in the fluid interior is generally much smaller than stress in the turbulent upper ocean surface,  $\boldsymbol{\tau}(\eta)$ , so that we can neglect  $\boldsymbol{\tau}(\eta_e)$  when computing the mass transport. We are thus led to the expression for the surface stress induced ageostrophic horizontal mass transport within the upper ocean Ekman layer

$$\mathbf{M}_e = -f^{-1} \hat{z} \times \boldsymbol{\tau}(\eta). \quad (27.33)$$

The surface stress induced mass transport given by equation (27.33) is very useful in practice. Notably, we do not need to know the depth of the Ekman layer nor details about the boundary layer turbulence. Rather, the mass transport is determined solely by the surface boundary stress. Furthermore, the horizontal mass transport within the Ekman layer is directed at right angles to the surface stress, as depicted in Figure 27.5, with mass transport to the right of the surface stress in the northern hemisphere and to the left in the southern hemisphere.

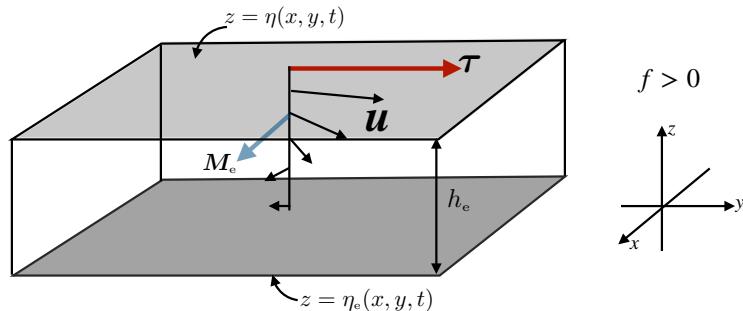


FIGURE 27.5: Horizontal transport integrated over the depth of the surface ocean Ekman layer in the region  $\eta_e(x, y, t) \leq z \leq \eta(x, y, t)$ . The net mass transport is directed perpendicular to the boundary stress, oriented to the right in the northern hemisphere and to the left in the southern hemisphere. Here, the boundary stress,  $\boldsymbol{\tau}$ , is shown directed to the north so that in the northern hemisphere ( $f > 0$ ), the depth integrated horizontal Ekman transport,  $\mathbf{M}_e$ , is to the east. This perpendicular mass transport is the result of the vertically spiralling Ekman flow. The Ekman mass transport resulting from boundary stress is independent of the assumptions made about ocean friction within the ocean boundary layer, and it is independent of the stratification assumed for the Ekman layer.

## 27.4.2 Example Ekman mass transports

A particularly relevant example is when zonal boundary stress is eastward,  $\boldsymbol{\tau}(\eta) = |\tau| \hat{x}$ , in which the Ekman transport is meridional

$$\mathbf{M}_e = -(|\tau|/f) \hat{y}, \quad (27.34)$$

which points equatorward in both hemispheres. Conversely, in the equatorial region winds are generally easterly so that  $\boldsymbol{\tau}(\eta) = -|\tau| \hat{x}$ , in which case the horizontal Ekman mass transport causes waters to move poleward away from the equator. Mass continuity is then satisfied by upwelling

waters along the equator within the Ekman layer. We sketch the elements of this flow in Figure 27.6. Exercise 27.1 considers an analogous situation for a channel in the southern hemisphere, thus illustrating a basic feature of the wind-driven overturning circulation in the Southern Ocean.

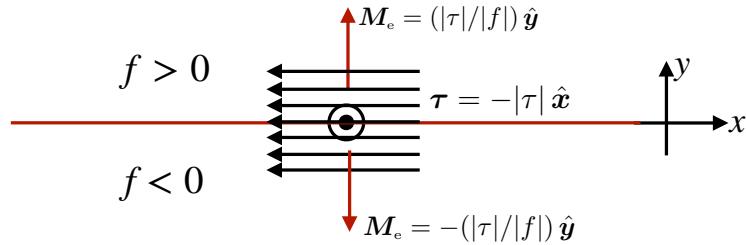


FIGURE 27.6: Easterly winds along the equator drive poleward horizontal mass transport within the upper ocean Ekman layer, as per equation (27.34). Furthermore, as discussed in Section 27.4.3, a steady state Ekman layer mass budget is typically realized by the upwelling of interior waters into the Ekman layer.

A second example concerns the case of a wind stress with a component aligned with a coastline as depicted in Figure 27.7. When the horizontal Ekman mass transport is directed away from the coast, a steady mass balance in the Ekman layer is associated with the upwelling of waters from beneath the Ekman layer. Conversely when the horizontal mass transport is directed toward the coast, steady mass balance is realized by coastal downwelling. This process is very important for coastal physical and biological oceanography.

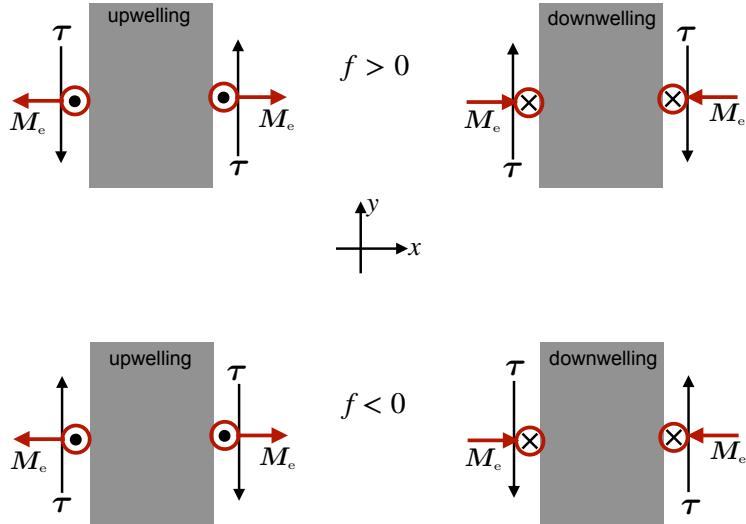


FIGURE 27.7: Wind stresses with a component that is parallel to coastlines lead to horizontal mass transport away from or towards the coast. Mass continuity then leads to coastal upwelling or downwelling of waters into or out of the Ekman layer. Here we depict the various scenarios for the northern hemisphere (top row) and southern hemisphere (bottom row), with the gray regions representing land, the black vectors the wind stresses, and the red arrows the horizontal wind induced mass transports in the Ekman layer. This figure is adapted from Figure 4-24 of [von Arx \(1962\)](#).

### 27.4.3 Mass budget for the Ekman layer

As seen in Figure 27.3, the horizontal transport of fluid within the Ekman layer induces a vertical transport into or out of the Ekman layer. To obtain a mathematical expression for the vertical

transport, integrate the continuity equation  $\nabla \cdot \mathbf{v} = 0$  over the vertical extent of the Ekman layer

$$\frac{\partial}{\partial x} \left[ \int_{\eta_e}^{\eta} u \, dz \right] + \frac{\partial}{\partial y} \left[ \int_{\eta_e}^{\eta} v \, dz \right] + [w(\eta) - \mathbf{u}(\eta) \cdot \nabla \eta] - [w(\eta_e) - \mathbf{u}(\eta_e) \cdot \nabla \eta_e] = 0. \quad (27.35)$$

For a Boussinesq fluid, the kinematic boundary condition at the ocean free surface is given by equation (16.5)

$$w + \frac{Q_m}{\rho_0} = \frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla \eta \quad \text{at } z = \eta(x, y, t). \quad (27.36)$$

Similarly, at the bottom of the Ekman layer we measure the volume transport through this layer by computing the dia-surface transport,  $w^{(\dot{\eta}_e)}$ , according to equation (42.38)

$$w^{(\dot{\eta}_e)} = w - (\partial_t z + \mathbf{u} \cdot \nabla z) \quad \text{at } z = \eta_e(x, y, t). \quad (27.37)$$

The sign convention is such that  $w^{(\dot{\eta}_e)} > 0$  means that mass enters (entrains into) the surface Ekman layer through its base, whereas  $w^{(\dot{\eta}_e)} < 0$  means that mass leaves (detrains from) the surface Ekman layer base.

Using the kinematic boundary conditions (27.36) and (27.37) in the depth integrated volume budget (27.35), and rearranging, leads to the Ekman layer mass budget

$$\rho_0 w^{(\dot{\eta}_e)} + Q_m = \rho_0 \partial h_e / \partial t + \nabla \cdot \mathbf{M}. \quad (27.38)$$

In this equation we wrote

$$h_e = \eta - \eta_e \quad (27.39)$$

for the thickness of the Ekman layer and

$$\mathbf{M} = \rho_0 \int_{\eta_e}^{\eta} \mathbf{u} \, dz \quad (27.40)$$

for the Ekman layer integrated horizontal mass transport. As a check on the above manipulations, let the Ekman layer go to the ocean bottom (so that  $w^{(\dot{\eta}_e)} = 0$  and  $\eta_e = \eta_b$ ), in which case the mass budget equation (27.38) correctly reduces to the kinematic free surface equation for the full ocean column as given by equation (16.8)

$$\rho_0 \frac{\partial \eta}{\partial t} = Q_m - \rho_0 \nabla \cdot \mathbf{U}, \quad (27.41)$$

with  $\mathbf{U} = \int_{\eta_b}^{\eta} \mathbf{u} \, dz$  the depth integrated horizontal velocity.

The horizontal mass transport given by equation (27.40) has a contribution from both the Ekman transport and remaining processes, such as geostrophic flow and ageostrophic flows not associated with Ekman. We write this mass transport in the form

$$\mathbf{M} = \mathbf{M}_e + \mathbf{M}_{\text{other}}. \quad (27.42)$$

The horizontal Ekman transport is determined by the boundary stress according to equation (27.33), with its divergence given by

$$\nabla \cdot \mathbf{M}_e = \hat{z} \cdot [\nabla \times (\boldsymbol{\tau}/f)]. \quad (27.43)$$

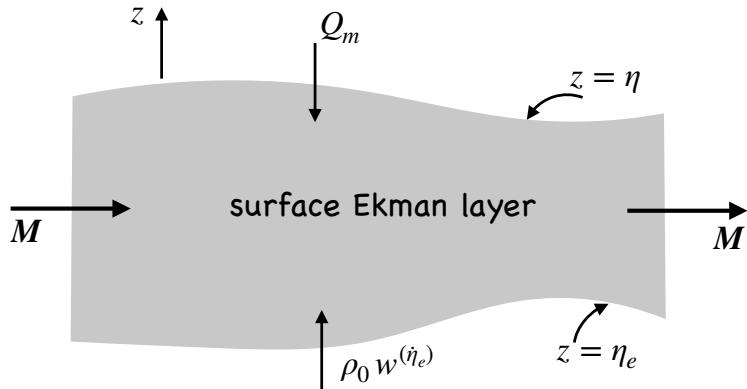


FIGURE 27.8: Mass budget over the surface Ekman layer of the ocean, with contributions from the surface mass flux,  $Q_m$ , flux through the bottom of the layer,  $w^{(\eta_e)}$ , and depth integrated horizontal flux,  $M$ , within the layer. If there are any imbalances then the layer thickness will have a nonzero time tendency,  $\partial h_e / \partial t \neq 0$ . Our sign convention is such as  $w^{(\eta_e)} > 0$  corresponds to water entering (entraining into) the Ekman layer (vertically upward motion) through the Ekman layer base at  $z = \eta_e$ , and likewise  $Q_m > 0$  corresponds to water entering the Ekman layer through the free surface at  $z = \eta$ . Entrainment through the base of the Ekman layer is referred to as *Ekman suction* or *Ekman upwelling*. The opposite case is referred to as *Ekman pumping* or *Ekman downwelling* when water leaves the Ekman layer and enters the ocean interior.

This result brings the Ekman layer mass budget (27.38) into the form

$$\rho_0 w^{(\eta_e)} + Q_m = \rho_0 \frac{\partial h_e}{\partial t} + \nabla \cdot \mathbf{M}_{\text{other}} + \hat{z} \cdot [\nabla \times (\boldsymbol{\tau}/f)]. \quad (27.44)$$

The left hand side measures the mass transport crossing the bottom of the Ekman layer,  $\rho_0 w^{(\eta_e)}$ , plus the transport crossing the free surface,  $Q_m$ . This transport balances a time change in the Ekman layer thickness (first right hand side term) plus the horizontal divergence of mass within the layer. A steady state Ekman layer thickness,  $\partial h_e / \partial t = 0$ , is realized if the horizontal divergence of mass within the Ekman layer is exactly balanced by mass entering the Ekman layer through the top and/or bottom of the layer. We illustrate this budget in Figure 27.8. For example, in the equatorial case of Figure 27.6, the diverging horizontal Ekman layer flow induced by easterly winds (poleward Ekman transport on both sides of the equator) is balanced by water upwelling into the Ekman layer through the base,  $w^{(\eta_e)} > 0$ , along with a generally smaller effects from surface mass fluxes through  $Q_m$  and possible other contributions through  $\nabla \cdot \mathbf{M}_{\text{other}}$ .

#### 27.4.4 Ekman layer coupled to the geostrophic interior

The effects from boundary stress in equation (27.44) warrant particular attention whereby

$$\rho_0 w_{\text{Ekman}}^{(\eta_e)} \equiv \nabla \cdot \mathbf{M}_e = \hat{z} \cdot [\nabla \times (\boldsymbol{\tau}/f)]. \quad (27.45)$$

The stress curl, as well as changes in  $f$  on the sphere, drive vertical motion through the base of the Ekman layer. The flow crossing the Ekman layer boundary acts to stretch or compress vertical fluid columns in the adjoining fluid interior. Interior fluid columns in a rotating fluid are stiffened through the effects of Taylor-Proudman (Section 25.5.3). From our understanding of vorticity (studied in Chapter 35), particularly the notions of vortex stretching, we see that the Ekman induced stretching/compression of interior fluid columns leads to a change in vorticity of the fluid interior, and can then lead to meridional motion due to the beta effect.

Consider an example with  $\nabla \cdot \mathbf{M}_e = \hat{z} \cdot [\nabla \times (\boldsymbol{\tau}/f)] > 0$ , so that winds induce a divergence within the Ekman layer. In a steady state, the interior flow accommodates this Ekman layer mass

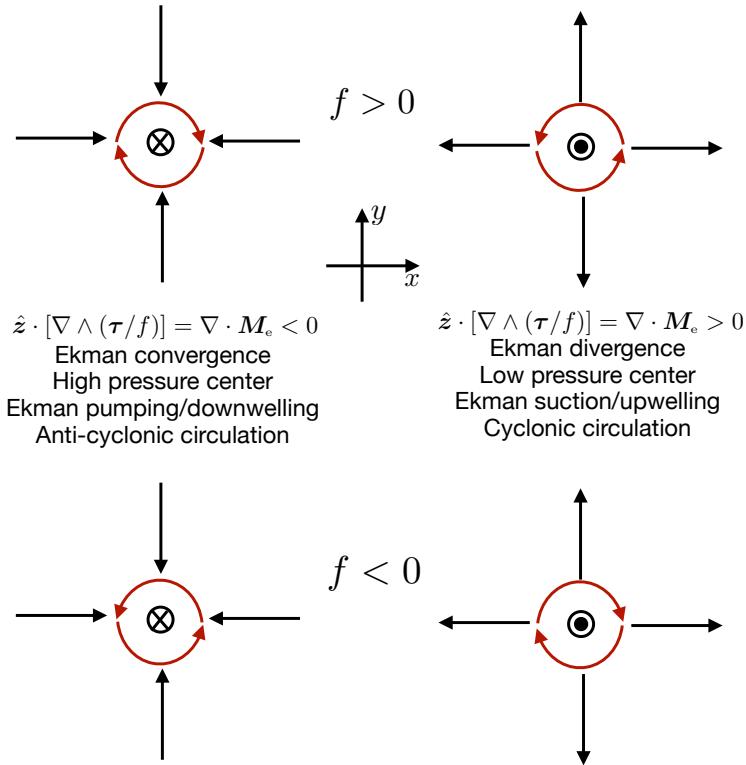


FIGURE 27.9: Plan view depicting the steady state horizontal and vertical transport in the surface Ekman layer (ignoring the possible transport across the ocean surface with  $Q_m$ ). The left column shows horizontal wind-induced convergence in the Ekman layer that induces vertical pumping/downwelling, where  $\nabla \cdot \mathbf{M}_e = \hat{z} \cdot [\nabla \times (\boldsymbol{\tau}/f)] < 0$ . The right column shows the horizontal divergence within the Ekman layer that is balanced by suction/upwelling, where  $\nabla \cdot \mathbf{M}_e = \hat{z} \cdot [\nabla \times (\boldsymbol{\tau}/f)] > 0$ . The top row is for the northern hemisphere, with  $f > 0$ , and the bottom row is for the southern hemisphere. The red arrows depict the sense for the induced circulation. Ekman pumping is associated with anti-cyclonic circulation (clockwise in the northern hemisphere and anti-clockwise in southern hemisphere). In contrast, Ekman suction is associated with cyclonic circulation. The circulation is supported by pressure gradients, with high pressure in regions of Ekman convergence,  $\nabla \cdot \mathbf{M}_e < 0$ , due to the accumulation of mass towards the center, thus giving rise to anti-cyclonic geostrophic flow in the interior. The opposite holds for regions of Ekman divergence,  $\nabla \cdot \mathbf{M}_e > 0$ , where water leaves the region thus leaving a low pressure center and inducing a cyclonic interior geostrophic flow.

divergence by upwelling water through the Ekman layer base,  $w^{(\dot{\eta}_e)} > 0$ . This process of entraining interior water into the Ekman layer is known as *Ekman suction* or *Ekman upwelling*. For the opposite case with  $\hat{z} \cdot [\nabla \times (\boldsymbol{\tau}/f)] < 0$ , water leaves (detrains) from the Ekman layer and moves into the interior. Water detraining from the Ekman layer is known as *Ekman pumping* or *Ekman downwelling*. As water diverges it produces a local low pressure so that the induced flow in the geostrophic interior is cyclonic around a region of Ekman divergence/upwelling. Conversely, the induced interior geostrophic flow is anti-cyclonic around a region of Ekman convergence/downwelling. Figure 27.9 provides an illustration for the variety of cases found in the northern and southern hemispheres.

In the language of vorticity, developed in Part VI of this book, Ekman upwelling with  $w^{(\dot{\eta}_e)} > 0$  leads to vortex stretching of interior fluid columns, whereas Ekman downwelling with  $w^{(\dot{\eta}_e)} < 0$  squashes the interior fluid columns. Vertical stiffening through Taylor-Proudman within the geostrophic interior, coupled to Ekman induced vortex stretching/squashing, makes what happens within the Ekman boundary layer of primary importance to the interior geostrophic flow. This boundary-interior coupling forms a key mechanism for how mechanical forcing from surface boundary stress creates the *wind driven* ocean circulation. It is notable that the coupling between

boundary layer and interior flow is absent from non-rotating boundary layer flows. In Figure 27.10 we offer a highly idealized schematic of the circulation implied by Ekman dynamics in a homogeneous fluid on an  $f$ -plane, thus illustrating the coupling of the upper surface Ekman layer to the geostrophic interior and then to the bottom Ekman layer. We also briefly discuss the *geostrophic Sverdrup balance* in Section 27.4.4, which builds on the ideas in this section.

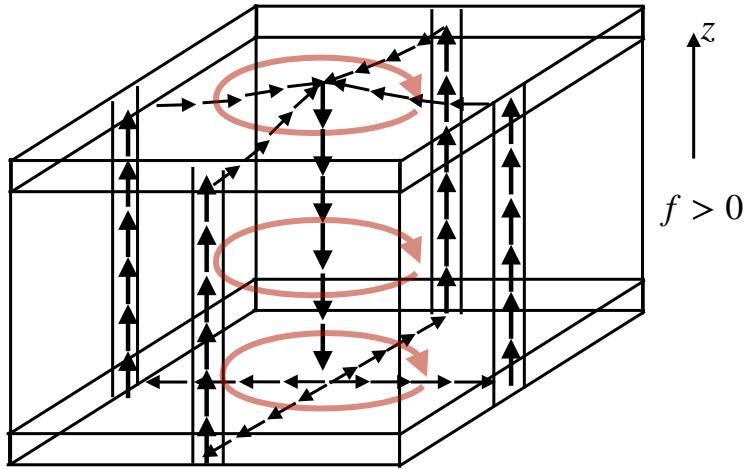


FIGURE 27.10: Schematic Ekman gyre circulation in a rectangular box in the northern hemisphere on an  $f$ -plane as forced by an anti-cyclonic wind stress curl. The wind stress curl causes fluid to pile up in the center of the gyre and develop an anti-cyclonic flow. The horizontal convergence of mass towards the center of the gyre leads to downwelling into the gyre interior below the Ekman layer (as per the upper left panel of Figure 27.9). This downwelling water enters the geostrophic interior and further into the bottom Ekman layer. As discussed in Section 27.5, the downwelling water in the bottom Ekman layer causes a horizontal divergence of mass. Assuming the domain has fixed vertical side walls, continuity requires an upwelling along the outer portion of the gyre. If the wind stress is symmetric about the center of the domain, then so is the flow. However, as studied in Section 34.9, the axial symmetry is broken on the  $\beta$ -plane, in which flow is stronger on the western side of the gyre even if the wind remains symmetric about the domain center. This figure is adapted from Figure 6-15 of [von Arx \(1962\)](#).

#### 27.4.5 Further study

The following videos offer visuals to help develop further intuition for Ekman boundary flows.

- [This 4-minute video from Science Primer](#) provides an overview of how Ekman transport affects ocean circulation features near the coast and in open ocean gyres.
- [This video from MIT Earth, Atmospheric, and Planetary Sciences](#) illustrates the spiral flow found within an Ekman layer as realized in a rotating tank experiment.
- [This video from the UCLA SpinLab](#), near the 18 minute mark, shows how Ekman transport helps to explain the garbage patches found near the center of the ocean's sub-tropical gyres.
- [This video from the University of Chicago](#), starting near the 23 minute mark, provides examples of Ekman layers in a rotating tank. The other portions of this video exhibit many other novel aspects of rotating fluids and is highly recommended.

## 27.5 Bottom Ekman layer

In this section we study the mechanics of a bottom Ekman boundary layer. For the mass transport, we merely translate the results from the upper ocean Ekman layer considered in Section 27.4,

whereby the mass transports are specified by the bottom boundary stress. We go further in this analysis by also providing an analytic expression for the velocity profile within the Ekman layer, with the velocity profile allowing us to diagnose the bottom boundary stress according to the Neumann boundary condition placed on the horizontal velocity (equation (27.58) below).

### 27.5.1 Horizontal mass transport within the Ekman layer

Turning the derivation from Section 27.4.1 upside-down leads to a bottom horizontal Ekman mass transport that is directed to the left of the bottom stress in the northern hemisphere and to the right in the southern hemisphere

$$\mathbf{M}_e = +f^{-1} \hat{z} \times \boldsymbol{\tau}(\eta_b). \quad (27.46)$$

Consider the special case where this bottom Ekman layer is the bottom of the atmosphere sitting over the ocean. Now the stress at the bottom of the atmosphere is equal to that acting on the top of the ocean.<sup>4</sup> Hence, the frictional stress induced mass transport (27.33) for the upper ocean is equal and opposite to the frictional stress induced mass transport in the atmosphere

$$\mathbf{M}_e^{\text{ocn}} = -f^{-1} \hat{z} \times \boldsymbol{\tau}(\eta_b) = -\mathbf{M}_e^{\text{atm}} \implies \mathbf{M}_e^{\text{ocn}} + \mathbf{M}_e^{\text{atm}} = 0. \quad (27.47)$$

Since the density of the atmosphere and ocean are quite different, the equal mass transports correspond to very different volume transports.

### 27.5.2 Mass budget for the bottom Ekman layer

Following the derivation of the Ekman layer mass budget in Section 27.4.3, and assuming no mass enters through the solid earth, we are led to the mass budget for the bottom Ekman boundary layer<sup>5</sup>

$$\rho_0 w^{(\eta_e)} = \rho_0 \frac{\partial h_e}{\partial t} - \nabla \cdot \mathbf{M} \quad (27.48)$$

where  $z = \eta_e(x, y, t)$  is the vertical position for the top of the bottom Ekman layer, and

$$h_e = \eta_e - \eta_b \quad (27.49)$$

is the Ekman layer thickness. For a steady state, the budget equation (27.4.3) says that the horizontal convergence of mass into the bottom Ekman boundary layer leads to a detrainment of mass from the Ekman layer into the interior fluid above (upwelling). Conversely, when fluid horizontally diverges from the bottom Ekman layer there is a balance from an entrainment (downwelling) of fluid from the interior into the Ekman layer. This orientation for the mass transport is illustrated in Figure 27.3 as part of our earlier discussion.

### 27.5.3 An analytic bottom Ekman spiral velocity

When studying the bottom boundary layer for the atmosphere or the surface boundary layer for the ocean, we are generally afforded an estimate of the frictional boundary stress,  $\boldsymbol{\tau}(\eta)$ . In turn, we can estimate the boundary stress induced mass transport and its divergence, and we can do so without making assumptions about the density profile or viscous stresses within the

<sup>4</sup>Recall our discussion of stress in Chapter 18, whereby stress on one side of an interface matches that on the other, which is a result following from Newton's third law.

<sup>5</sup>Note the sign swap in the budget (27.48) in front of the horizontal transport term as compared to the surface boundary layer mass budget (27.38).

boundary layer. However, this estimate is less directly accessible for the ocean bottom Ekman layer, where we need  $\tau(\eta_b)$  to determine the mass transport. We here take an alternative approach that produces an analytic profile for the velocity within the Ekman layer, so long as we know the viscosity within the boundary layer. Knowing the velocity profile then affords an estimate of the boundary stress. This approach requires a few assumptions that are not always met, in particular it requires the viscosity. Even so, it provides physical insights that further our understanding of Ekman mechanics thus motivating the analysis.

### Physical configuration

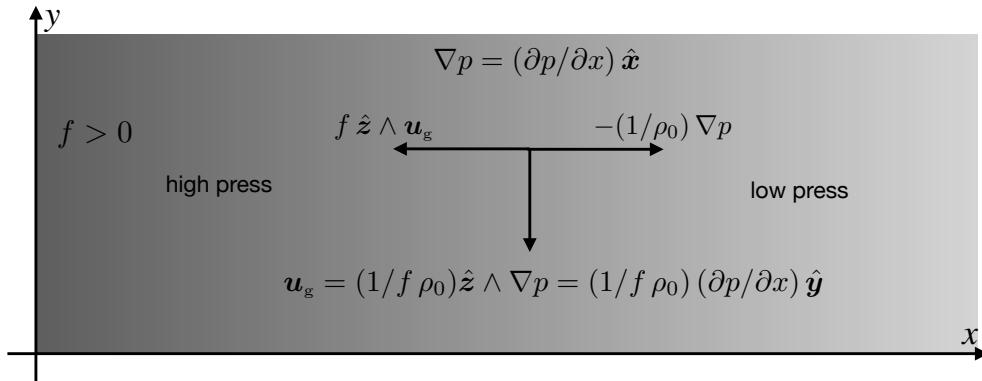


FIGURE 27.11: A southward geostrophic flow in the northern hemisphere ( $f > 0$ ) induced by an eastward pressure gradient acceleration (low pressure to the east;  $\partial p / \partial x < 0$ ) that balances a westward Coriolis acceleration.

We assume flow above the boundary layer is geostrophic and supported by a prescribed depth-independent pressure gradient

$$f \rho_0 \mathbf{u}_g = \hat{\mathbf{z}} \times \nabla p. \quad (27.50)$$

A specific example is given by Figure 27.11, where a southward geostrophic flow in the northern hemisphere has an eastward pressure gradient acceleration (low pressure to the east) balanced by a westward Coriolis acceleration.

For flow within the boundary layer, viscous stresses exchange horizontal momentum vertically between the inviscid interior and the bottom no-slip condition. This viscous exchange slows the boundary layer velocity relative to the interior velocity above the boundary layer. Since the pressure gradient is assumed to be depth-independent and prescribed, the slower velocity within the boundary layer means that the Coriolis acceleration is unable to balance the pressure gradient acceleration. This imbalance between pressure acceleration and Coriolis acceleration leads to a down pressure gradient component to the boundary layer velocity. As a result, the velocity spirals downward toward the bottom.

The key assumptions required to produce an analytic Ekman spiral velocity are: (i) the fluid within the Ekman layer has a constant density,  $\rho_0$ ; (ii) the Coriolis parameter is a constant as per the  $f$ -plane; (iii) the prescribed pressure gradient is depth independent so that the associated geostrophic velocity is depth independent; (iv) the eddy viscosity is constant within the boundary layer and zero in the interior region above the boundary layer; (v) the flow is steady. The homogeneous density assumption is motivated by the rather small vertical scale of the bottom Ekman layer (tens of meters) relative to the horizontal scales over which density varies in the ocean bottom (tens to hundreds of kilometers). A constant viscosity is not always realistic since the turbulent viscosity is generally inhomogeneous within boundary layers. Even so, by assuming sufficient time for statistics to become stationary we can expect to make good use of the time averaged viscosity.

### Velocity profile within the Ekman layer

Bringing the above assumptions into the frictional geostrophic equations (27.1) leads to

$$f \hat{z} \times \mathbf{u} = -(1/\rho_0) \nabla p + \nu^{\text{eddy}} \partial_{zz} \mathbf{u} \quad \text{frictional geostrophic} \quad (27.51\text{a})$$

$$\partial_z (\nabla_z p) = 0 \quad z\text{-independent horizontal pressure gradient} \quad (27.51\text{b})$$

$$\mathbf{u}(\eta_b) = 0 \quad \text{no-slip bottom boundary condition} \quad (27.51\text{c})$$

$$\mathbf{u}(\infty) = \mathbf{u}_g \quad \text{matching to geostrophic interior.} \quad (27.51\text{d})$$

Decomposing the velocity into its geostrophic and ageostrophic components

$$\mathbf{u} = \mathbf{u}_g + \mathbf{u}_e, \quad (27.52)$$

leads to

$$f \hat{z} \times \mathbf{u}_e = \nu^{\text{eddy}} \frac{\partial^2 \mathbf{u}_e}{\partial z^2} \quad (27.53\text{a})$$

$$\mathbf{u}_e(\eta_b) = 0 \quad (27.53\text{b})$$

$$\mathbf{u}_e(\infty) = 0. \quad (27.53\text{c})$$

To reach this result we noted that the geostrophic velocity is depth independent within the boundary layer where the density is constant, so that the geostrophic velocity does not contribute to the viscous friction operator. These coupled second order differential equations are equivalent to the two uncoupled fourth order differential equations

$$(f^2 + \nu^2 \partial_{zzzz}) \mathbf{u}_e = 0 \quad (27.54\text{a})$$

$$\mathbf{u}_e(\eta_b) = 0 \quad (27.54\text{b})$$

$$\mathbf{u}_e(\infty) = 0. \quad (27.54\text{c})$$

A solution to these equations renders the Ekman boundary layer profile

$$u = u_g \left[ 1 - e^{-\Delta z/h_e} \cos(\Delta z/h_e) \right] - v_g e^{-\Delta z/h_e} \sin(\Delta z/h_e) \quad (27.55\text{a})$$

$$v = v_g \left[ 1 - e^{-\Delta z/h_e} \cos(\Delta z/h_e) \right] + u_g e^{-\Delta z/h_e} \sin(\Delta z/h_e) \quad (27.55\text{b})$$

$$h_e^2 = 2 \nu^{\text{eddy}} / |f| \quad (27.55\text{c})$$

$$\Delta z = z - \eta_b. \quad (27.55\text{d})$$

### Properties of the Ekman spiral

The spiral velocity profile (27.55a)-(27.55b) vanishes at the bottom,  $\Delta z = 0$  or  $z = \eta_b$ , reflecting the no-slip bottom boundary condition. It also reduces to the interior geostrophic velocity at  $\Delta z = \infty$ . In moving downward through the boundary layer, the boundary layer current deflects to the left of the interior geostrophic current (deflection is to the right in the southern hemisphere). Making use of the integral identities

$$\int_{\eta_b}^{\infty} e^{-\Delta z/h_e} \cos(\Delta z/h_e) d\Delta z = h_e/2 \quad \text{and} \quad \int_{\eta_b}^{\infty} e^{-\Delta z/h_e} \sin(\Delta z/h_e) d\Delta z = -h_e/2 \quad (27.56)$$

leads to the frictionally induced mass transport within the Ekman layer

$$\mathbf{M}_e = \rho_0 \int_{\eta_b}^{\infty} \mathbf{u}_e dz \quad (27.57a)$$

$$= (h_e \rho_0 / 2) [-\hat{x}(u_g + v_g) + \hat{y}(u_g - v_g)] \quad (27.57b)$$

$$= f^{-1} \hat{z} \times \boldsymbol{\tau}(\eta_b), \quad (27.57c)$$

where we introduced the bottom stress according to equation (27.46). Furthermore, this stress is given by the Neumann boundary condition placed on the horizontal velocity

$$\boldsymbol{\tau}(\eta_b) = \rho_0 \nu^{\text{eddy}} \left[ \frac{\partial \mathbf{u}_e}{\partial z} \right]_{z=\eta_b} = (f h_e / 2) [\hat{x}(u_g - v_g) + \hat{y}(u_g + v_g)]. \quad (27.58)$$

Following from equation (27.48) we see that the bottom stress induced mass transport across the top of the bottom Ekman boundary layer is

$$\rho_0 w_{\text{Ekman}}^{(\eta_e)} = -\nabla \cdot \mathbf{M}_e = -\nabla \cdot [f^{-1} \hat{z} \times \boldsymbol{\tau}(\eta_b)] = (h_e / 2) \zeta_g, \quad (27.59)$$

where we made use of the  $f$ -plane assumption to set  $\nabla \cdot \mathbf{u}_g = 0$  and introduced the relative vorticity of the geostrophic flow

$$\zeta_g = \partial_x v_g - \partial_y u_g. \quad (27.60)$$

Hence, the relative vorticity of the interior geostrophic flow provides a divergence to the horizontal mass transport within the bottom Ekman layer. We illustrate the Ekman mass transport and bottom stress in Figure 27.12.

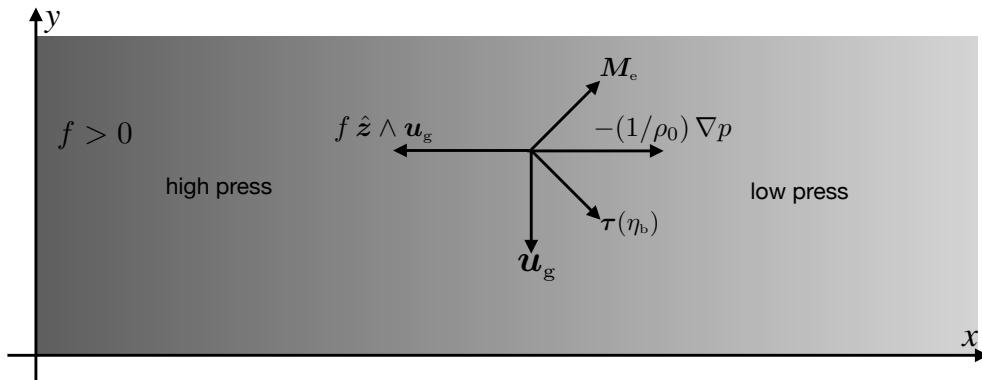


FIGURE 27.12: Mass transport and bottom stress in a homogeneous bottom Ekman layer on an  $f$ -plane in the northern hemisphere. Note how the boundary layer stress is directed  $\pi/4$  radians to the left of the prescribed interior geostrophic velocity. Furthermore, the horizontal Ekman transport is itself  $\pi/2$  radians to the left of the stress, which is then  $3\pi/4$  to the left of the geostrophic velocity.

#### 27.5.4 Comments

The Ekman spiral is a striking solution to the linear frictional geostrophic equations in a homogeneous fluid next to a flat no slip boundary. Section 5.7 of [Vallis \(2017\)](#) provides further discussion of the Ekman spiral solution discussed here. The spiral profile has been measured in the atmosphere and can be produced in the laboratory. However, it has proven difficult to measure in the ocean (see [Gnanadesikan and Weller \(1995\)](#) for an example). Even so, the effects from Ekman transport are robust features of the theory developed in this chapter, with those

results independent of details for the vertical viscosity.

## 27.6 Arrested bottom Ekman flows

When studying the vertical velocity profile within the bottom boundary layer in Section 27.5, we assumed the density to be uniform within the boundary layer. A uniform density is commonly assumed for Ekman layers. However, [MacCready and Rhines \(1991\)](#), [MacCready and Rhines \(1993\)](#), and [Garrett et al. \(1993\)](#) examined that assumption in their study of bottom boundary layers in the presence of a nonzero vertical density stratification next to sloping topography. They point out the remarkable possibility of a vanishing frictional stress within the sloping bottom boundary layer. That is, rather than nonzero friction leading to a zero flow next to the bottom, flow is arrested by a compensation of pressure gradient accelerations. The vanishing frictional stress motivates the term *slippery Ekman layers*, whereas the equivalent term *arrested Ekman layer* refers to the zero boundary layer flow. We here briefly describe the arrested Ekman layer by studying Figure 27.13.

### 27.6.1 Description

In both panels of Figure 27.13 we depict a prescribed barotropic pressure acceleration that acts eastward and has a corresponding southward geostrophic flow ( $f > 0$ ) and westward Coriolis acceleration. This configuration is identical to that shown in Figure 27.11 when studying the bottom Ekman spiral over a flat bottom. As the flow enters the bottom boundary layer it slows so that its Coriolis acceleration no longer balances the barotropic pressure gradient acceleration (we have seen this imbalance throughout this chapter). The bottom Ekman layer flow sends water cross-slope in the direction down the barotropic pressure gradient. In the configuration shown here, the cross-slope flow advects denser water upslope. In so doing, a horizontal baroclinic pressure acceleration develops adjacent to the bottom boundary layer, with the baroclinic pressure acceleration pointing opposite to the barotropic pressure acceleration. A steady state is realized when the two pressure accelerations balance, in which case flow within the boundary layer halts.

It is remarkable that the dynamical balance for the arrested bottom boundary layer flow does not involve friction. Rather, arrest happens when the two pressure gradients balance and the Coriolis acceleration vanishes. That is, referring to the frictional geostrophic equation (27.1), each term separately vanishes in the arrested state.

### 27.6.2 Applications

[MacCready and Rhines \(1991, 1993\)](#) and [Garrett et al. \(1993\)](#) study the transient adjustment leading to the arrested state. They derive the expression for the time scale for adjustment to the arrest state

$$T_{\text{arrest}} = \frac{|f|}{N^2 s^2}, \quad (27.61)$$

where  $s$  is the slope of the bottom and  $N^2$  is the squared buoyancy frequency of the ambient water. The time is less in regions of strong stratification ( $N^2$  relatively large), large topographic slopes ( $s^2$  large), and low latitudes ( $f$  small). Conversely, the infinite time for either  $N^2 = 0$  or  $s^2 = 0$  indicates the need for both stratification and topographic slopes to render an arrest. Finally, we note the absence of any dissipation parameters (e.g., viscosity) from the time scale. Friction is needed to support the Ekman layer where flow crosses isobars, but the time to reach the arrest state is independent of friction.

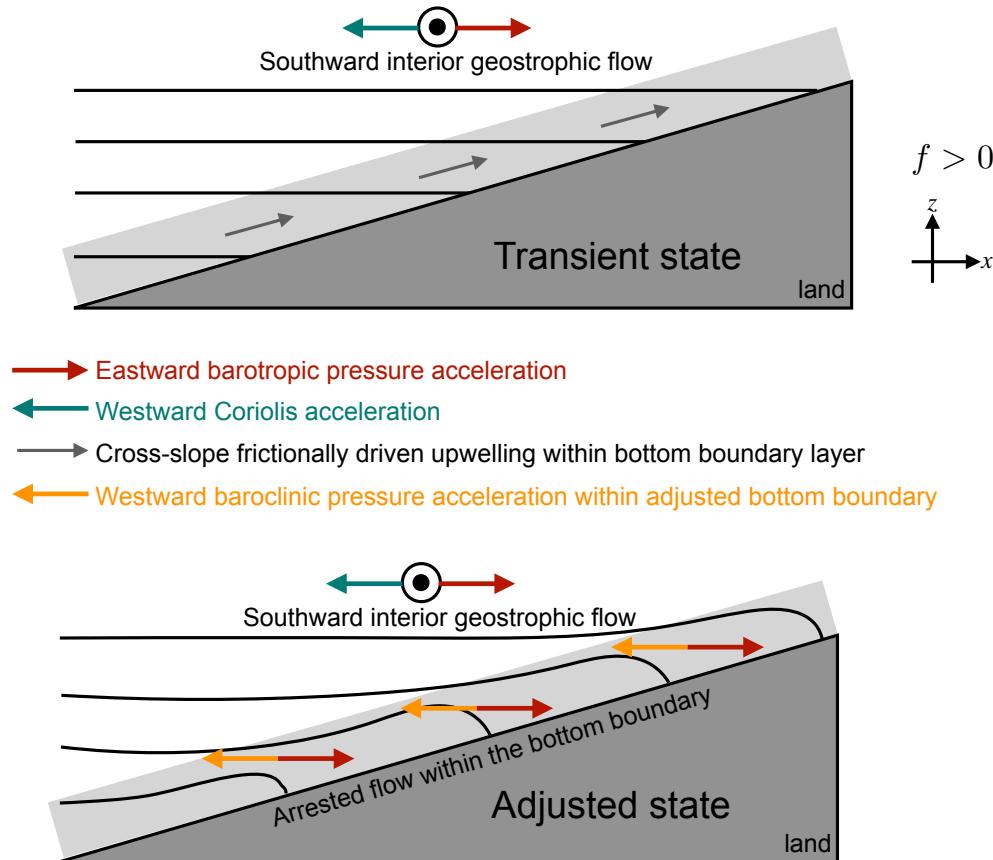


FIGURE 27.13: In both panels we depict a prescribed barotropic pressure acceleration that acts eastward and has a corresponding southward geostrophic flow and westward Coriolis acceleration. The solid lines depict lines of constant buoyancy, also known as isopycnals (see Chapter 24). Top panel: As the flow enters the bottom boundary layer it slows so that its Coriolis acceleration no longer balances the barotropic pressure, thus sending water cross slope in the down pressure gradient direction. Bottom panel: The cross-slope movement of density creates a baroclinic pressure acceleration that counteracts the barotropic pressure acceleration. The steady state is realized when the two pressure accelerations balance, in which case flow within the boundary layer halts. In this halted state there are no frictional stresses since the flow halts due to pressure effects rather than friction. Note that isopycnals are shown intersecting the solid boundary in a perpendicular direction, which is implied by the no-flux bottom boundary condition (in the absence of geothermal heating) as discussed in Section 15.5.2. Geostrophic flow in the opposite direction leads to downwelling along the bottom rather than upwelling. This figure is adapted from Figure 5 of [Wählin et al. \(2012\)](#).

[Wählin et al. \(2012\)](#) interpreted observations from the Amundsen Sea according to the arrested Ekman boundary layer and found  $T_{\text{arrest}}$  to be just a few hours. Additionally, the numerical model studies from [Spence et al. \(2017\)](#) and [Webb et al. \(2019\)](#) point to the ability of barotropic shelf waves around Antarctica to provide an onshore directed barotropic pressure acceleration. Through the arrested Ekman layer mechanism described here, they find that the barotropic pressure is compensated through an upslope transport of relatively warm deep water in regions of the Antarctic Peninsula. Extensions and refinements of these ideas support an active area of ongoing research (e.g., [Ruan et al., 2021](#); [Peterson and Callies, 2022](#)).



## 27.7 Exercises

### EXERCISE 27.1: EKMAN MASS TRANSPORT IN A SOUTHERN CHANNEL

Consider a southern hemisphere channel (e.g., and idealized Southern Ocean) with a zonal wind stress that has a meridional dependence such as shown in Figure 27.14. Following the discussion in Sections 27.4.1 and 27.4.4, sketch the sense for the horizontal and vertical Ekman mass transport arising from this wind stress. Show the transport for regions to the north and to the south of the wind stress maximum. Ignore the  $\beta$  contribution by assuming the channel is not very wide and by noting that  $\beta$  is smaller in the high latitudes (as relevant to the Southern Ocean).

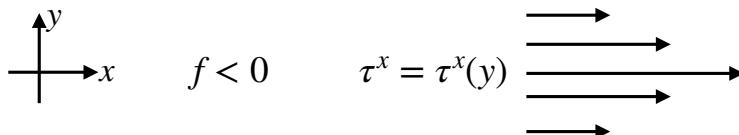


FIGURE 27.14: Zonal wind stress in a southern hemisphere channel with a maximum flanked by lower winds. What is the sense for the associated horizontal and vertical Ekman mass transport following from the discussion in Sections 27.4.1 and 27.4.4?

### EXERCISE 27.2: RELATING EKMAN, ROSSBY, AND REYNOLDS NUMBERS

Under certain scalings, we can connect the Ekman number to the Rossby and Reynolds numbers. In detail, we have

$$\text{Ro} = \frac{U}{f_0 L} \quad \text{and} \quad \text{Ek} = \frac{\nu^{\text{eddy}}}{f_0 H^2} \quad \text{and} \quad \text{Re} = \frac{W H}{\nu^{\text{eddy}}}, \quad (27.62)$$

where

$$H = \text{vertical length scale} \quad (27.63a)$$

$$L = \text{horizontal length scale} \quad (27.63b)$$

$$U = \text{horizontal velocity scale} \quad (27.63c)$$

$$W = \text{vertical velocity scale}. \quad (27.63d)$$

and we defined the Reynolds number (Section 18.8) in terms of the vertical viscosity, vertical length scale, and vertical velocity scale. What is the ratio of the Rossby number to Reynolds if the flow is non-divergent?

### EXERCISE 27.3: EKMAN BOUNDARY LAYERS AND RAYLEIGH DRAG

Rayleigh drag described in Section 27.2.3 allowed us to study the effects of friction on fluid trajectories. However, Rayleigh drag has no spatial derivatives, which contrasts to the Laplacian friction from Section 27.3.1 and used elsewhere in this chapter. Comment on whether Rayleigh drag can support the no-slip boundary condition and the corresponding development of a boundary layer.





# Chapter 28

## Space and time dependent gravity

We here formulate the dynamical equations for a geophysical fluid in the presence of a space and time dependent gravitational acceleration. This formulation has application to the study of astronomical tides in the ocean, thus motivating a discussion of the astronomical tidal forcing that follows the treatment given in Chapter 3 of [Pugh \(1987\)](#) and Section 5.15 of [Apel \(1987\)](#), with Chapter 2 of [Brown \(1999\)](#) and Section 17.4 of [Stewart \(2008\)](#) useful pedagogical supplements. Besides tides, a topic of interest to climate science concerns the study of how ocean sea level responds to changes in mass distributions associated with melting land ice. The nontrivial impact that melting land glaciers has on the earth's geoid and earth's rotation ([Farrell and Clark, 1976](#); [Mitrovica et al., 2001](#); [Kopp et al., 2010](#)) further motivates developing the dynamical equations of a liquid ocean in the presence of a space-time dependent gravity.

### READER'S GUIDE TO THIS CHAPTER

This chapter assumes an understanding of the equations of motion derived in Chapter 17 as well as the gravitational and planetary centrifugal accelerations from Section 9.12. We dispense with tensor notation in this chapter, with subscripts used here as descriptive labels rather than tensor indices. No other chapter depends on the material in this chapter.

28.1	Gravitational potential . . . . .	677
28.1.1	Simple geopotential . . . . .	678
28.1.2	General geopotential . . . . .	678
28.2	Momentum equation . . . . .	678
28.3	Primitive equations . . . . .	679
28.4	Depth independent perturbed geopotential . . . . .	679
28.5	Forces contributing to ocean tides . . . . .	680
28.5.1	Tidal acceleration in a spherically symmetric gravity field . . . . .	680
28.5.2	Heuristics of tidal acceleration on the surface of a sphere . . . . .	681
28.5.3	Gravitational potential for an idealized earth-moon system . . . . .	683
28.5.4	Concerning realistic tides . . . . .	687
28.5.5	Comments . . . . .	688

### 28.1 Gravitational potential

In this section we summarize elements of the gravitational force, including the case with a non-constant gravitational acceleration such as occurs from astronomical tidal forcing and changes to

the mass distribution of the planet.

### 28.1.1 Simple geopotential

As detailed in Section 9.12, the effective gravitational field incorporates the effects from the planetary centrifugal acceleration. The effective gravitational field is conservative, so that the gravitational acceleration of a fluid element can be represented as the gradient of a scalar (see Section 9.12.4),

$$\mathbf{g} = -\nabla \Phi, \quad (28.1)$$

with  $\Phi$  the geopotential. In most applications of this book, the local vertical direction is denoted by

$$z = r - R_e, \quad (28.2)$$

with  $z = 0$  the geopotential surface corresponding to a resting ocean and  $R_e = 6.367 \times 10^6$  m the average radius of the earth (Section 9.2). The geopotential in this case is given by

$$\Phi = \Phi_0 = g z, \quad (28.3)$$

with  $g \approx 9.8 \text{ m s}^{-2}$  the typical value used for the gravitational acceleration at the earth's surface.

### 28.1.2 General geopotential

Consider a generalized geopotential written in the form

$$\Phi = \Phi_0(r) + \Phi_1(r, \lambda, \phi, t), \quad (28.4)$$

where  $\Phi_0(r)$  is the geopotential given by equation (28.3), and  $\Phi_1$  incorporates perturbations to the geopotential. For the study of ocean tides, the structure of  $\Phi_1$  arises from astronomical perturbations to the earth's gravity field. The calculation of ocean tides arising from astronomical forcing is formulated with a space-time dependent geopotential as in equation (28.4), with the radial dependence of  $\Phi_1$  neglected (e.g., Section 9.8 in [Gill, 1982](#)). [Arbic et al. \(2004\)](#) provide a discussion of global tide modelling.

Nontrivial  $\Phi_1$  variations also arise from perturbations in terrestrial masses, such as the melting of land ice such as that occurring on Greenland or Antarctica due to climate warming. These mass distribution changes lead to changes in the earth's gravitational field, its rotational moment of inertia, and the deformation of the crust (GRD as in [Gregory et al. \(2019\)](#)). Each of these effects lead to modifications in the *static equilibrium sea level*. In contrast to ocean tides, GRD perturbations associated with melting land ice are not periodic nor readily predictable. Furthermore, as evidenced by Figure 1 in [Mitrovica et al. \(2001\)](#), the amplitude of static equilibrium sea level changes can be far greater than typical open ocean tide fluctuations.

## 28.2 Momentum equation

As detailed in Section 17.1.3, the inviscid momentum equation for a rotating fluid in a gravitational field is given by

$$\rho \frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \rho \mathbf{v} = -\nabla p - \rho \nabla \Phi. \quad (28.5)$$

In writing the momentum equation in the form (28.5), we have chosen to retain an orientation afforded by the unperturbed geopotential,  $\Phi_0(r)$ , which are surfaces of constant  $z$ . This approach reflects that commonly used to study ocean tides. In the presence of a perturbed geopotential,  $\Phi_1$ ,

the “horizontal” directions defined by surfaces of constant  $z$  are no longer parallel to geopotential surfaces. We thus may interpret the sum  $\nabla_z p + \rho \nabla_z \Phi$  as an orientation of the pressure gradient along surfaces of constant geopotential, where the geopotential is determined by  $\Phi = \Phi_0 + \Phi_1$ , rather than just the unperturbed geopotential  $\Phi_0$ .

## 28.3 Primitive equations

As detailed in Section 22.1, the primitive equations reduce the vertical momentum equation to its static inviscid form, which is the hydrostatic balance

$$\frac{\partial p}{\partial z} = -\rho \frac{\partial \Phi}{\partial z} = -\rho(g + \partial_z \Phi_1). \quad (28.6)$$

The hydrostatic balance is modified from its traditional form for cases where the perturbation geopotential  $\Phi_1$  exhibits nontrivial depth dependence. Correspondingly, the horizontal momentum equation (making the Traditional Approximation from Section 22.1) takes the form

$$\rho \frac{D\mathbf{u}}{Dt} + \hat{\mathbf{z}} f \times \rho \mathbf{u} = -(\rho \nabla_z \Phi_1 + \nabla_z p) \quad (28.7)$$

where  $\nabla_z$  is the horizontal gradient taken on surfaces of constant  $z$ . In their oceanic Boussinesq form (Chapter 23), the inviscid horizontal momentum equation becomes

$$\frac{D\mathbf{u}}{Dt} + \hat{\mathbf{z}} f \times \mathbf{u} = -(1/\rho_0) (\rho_0 \nabla_z \Phi_1 + \nabla_z p) \quad (28.8)$$

where  $\rho_0$  is the constant reference density for a Boussinesq fluid. The Boussinesq form makes the addition of a perturbed geopotential quite straightforward, in which it is gradients in  $\rho_0 \Phi_1 + p$  that take the place of gradients in pressure  $p$ .

## 28.4 Depth independent perturbed geopotential

A particularly simple form of  $\Phi_1$  occurs when it is depth independent,

$$\Phi_1 = \Phi_1(\lambda, \phi, t), \quad (28.9)$$

in which case the hydrostatic balance (28.6) returns to its traditional form  $\partial_z p = -\rho g$ . This form is motivated by the scale analysis in Section 28.5.3 where we find that the radial component of the earth’s gravitational field greatly exceeds that from the moon or other celestial bodies, so that it is the lateral variation in the gravitational acceleration that drive tidal motions. In this case it is convenient to write the geopotential as

$$\Phi_1 = -g h, \quad (28.10)$$

with  $h = h(\lambda, \phi, t)$  the perturbed geopotential height field. The full geopotential is thus written

$$\Phi = g(z - h), \quad (28.11)$$

with this form revealing that the zero of the geopotential is now set by  $z = h$  rather than  $z = 0$ . In the study of ocean tides,  $h$  is referred to as the *equilibrium tide*. In geodesy,  $h$  is referred to as the *static equilibrium sea level*.

Since the perturbed geopotential is depth independent, it only affects the depth integrated horizontal momentum, and it does so through the term

$$-\int_{\eta_b}^{\eta} \nabla_z \Phi_1 dz = g \int_{\eta_b}^{\eta} \nabla_z h dz = g (-\eta_b + \eta) \nabla_z h. \quad (28.12)$$

Hence, modifications to the geopotential as embodied by the perturbed geopotential height field,  $h = h(\lambda, \phi, t)$ , are isolated to their impacts on the horizontal pressure gradients acting on the depth integrated horizontal momentum.

## 28.5 Forces contributing to ocean tides

We here describe the rudiments of forces that contribute to ocean tides as well as solid-earth tides. For simplicity we focus just on the earth-moon system, though note that the sun also plays an analogous role for observed tidal motion.

### 28.5.1 Tidal acceleration in a spherically symmetric gravity field

Before considering the earth-moon system, we introduce the notion of *tidal acceleration*, which arises on a finite sized body placed within a non-uniform gravitational field. Figure 28.1 depicts this situation where the finite sized body is a narrow rod whose axis points towards the center of a spherically symmetric massive body. One end of the rod experiences a different gravitational acceleration than the other since the gravitational field falls off as the inverse squared distance from the center of the sphere. It is this differential gravitational acceleration that we refer to as the tidal acceleration. As we will see, its key property is that the tidal acceleration falls off as the inverse cube of the distance rather than the more familiar inverse square.

To develop a mathematical expression for the tidal acceleration, focus on the spherically symmetric gravitational field in which the gravitational acceleration at a point is given by (Section 9.12.2)

$$\mathbf{g} = -\frac{GM}{r^2} \hat{\mathbf{r}}, \quad (28.13)$$

where  $r$  is the distance from the sphere's center,  $G$  is Newton's gravitational constant,  $M$  is the mass of the sphere, and  $\hat{\mathbf{r}}$  is the radial unit vector. The minus sign indicates that the gravitational acceleration points toward the center of the sphere. For the rod in Figure 28.1, the difference between the gravitational acceleration acting at a point nearest to the sphere (point B) and a point furthest from the sphere (point A) is given by

$$\mathbf{g}(r_B) - \mathbf{g}(r_A) = \mathbf{g}(r_0 - L/2) - \mathbf{g}(r_0 + L/2), \quad (28.14)$$

where  $r_0$  is the distance from the sphere's center to the center of the rod. Assuming the rod is not long, we can expand this difference in a Taylor series about the rod center at  $r_0$ , thus leading to an expression for the tidal acceleration

$$\mathbf{g}(r_B) - \mathbf{g}(r_A) \approx -L \frac{\partial \mathbf{g}}{\partial r} = -2L \frac{GM}{r_0^3} \hat{\mathbf{r}} = (2L/r_0) \mathbf{g}(r_0). \quad (28.15)$$

The key point to conclude from this example is that the tidal acceleration is proportional to the inverse cube of the distance to the center of the sphere. We see this property again when considering in Section 28.5.3 the gravitational acceleration generated from a remote body (e.g., the moon) acting on the surface of a sphere (e.g., the earth).

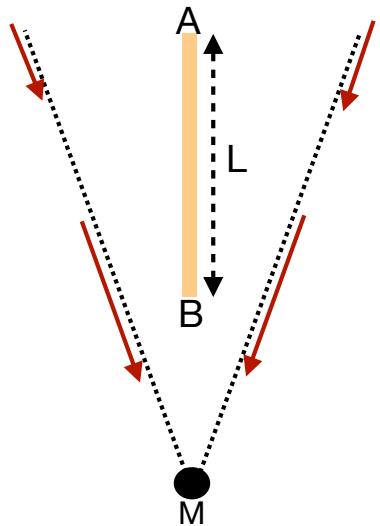


FIGURE 28.1: *Tidal acceleration* is the acceleration that acts on a finite sized object placed in a non-uniform gravitational field. The finite object is here depicted as a narrow rod of length  $L$  placed in the gravity field of a spherically symmetric body of mass  $M$ . That portion of the rod closer to the gravitating sphere (end B) experiences a stronger gravitational acceleration than the end that is further away (end A). The gradient in the gravitational acceleration constitutes the tidal acceleration acting on the rod.

### 28.5.2 Heuristics of tidal acceleration on the surface of a sphere

We now consider the tidal acceleration acting on the surface of a smooth massive sphere due to a spherically symmetric gravitational field generated by a neighboring massive body. Figure 28.2 depicts this system, which we consider an idealized earth-moon system where each body is assumed homogeneous and spherical. Given that they gravitationally attract one another, it is not astronomically possible for the two bodies to remain spatially fixed. Instead, they orbit around their common center of mass while conserving their angular momentum.

A central question of tidal studies is why there are generally two ocean tides per day (semi-diurnal tides) rather than just one (diurnal tides). We here offer two complementary arguments. The first is based on extending the tidal acceleration discussion of Section 28.5.1, whereas the second follows the more traditional account by considering a balance between gravitational and centrifugal accelerations.

#### *General ideas*

Every point on the surface of the earth is attracted to the earth's center by the earth's gravitational field. For a spherical earth, this attractive force is purely radial, so that it cannot lead to lateral motion on the surface of the perfect sphere. We thus conclude that the radial gravitational field is not the cause of tidal motion. Instead, tidal motion arises from a non-radial gravitational field.

The earth-moon gravitational field accelerates the earth and moon toward one another along the axis connecting their centers. Additionally, the spatial dependence of the moon's gravitational field over the earth leads to lateral forces along the earth's surface, thus providing the ingredient for ocean tidal motion. To capture the essence of this force, we examine how the moon's gravitational field acts on a point on the earth relative to its action at the center of the earth.

#### *Sample tidal accelerations on the sphere*

Again, we are tasked with computing the tidal acceleration from the moon's gravitational field for selected points on the earth, and we are computing these accelerations relative to the earth

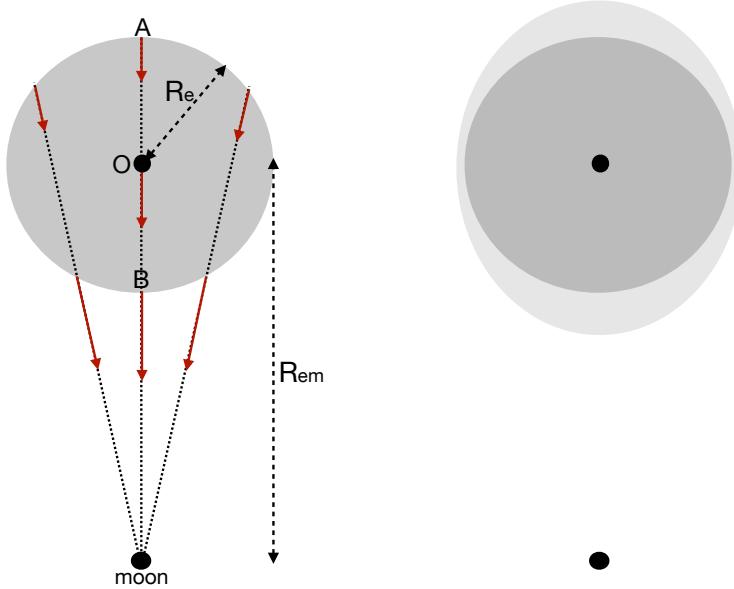


FIGURE 28.2: Illustrating the tidal force on the surface of a sphere. The sphere is an ideal depiction of the earth and the smaller massive object is the moon. The distance between the center of the earth and moon is  $R_{\text{em}}$ , and the radius of the earth is  $R_e$ . The left panel shows representative moon-generated gravitational field lines. Two points along these field lines on the surface of the earth represent the two ends of an imaginary rod as depicted in Figure 28.1. The tidal acceleration acting at point B, relative to the earth's center, points toward the moon (equation (28.16)). In contrast, the tidal acceleration at point A, relative to the earth's center, points in the opposite direction (equation (28.17)). Points on the earth surface between A and B have tidal accelerations with a non-zero component directed along the surface of the earth. Symmetry of the configuration allows us to conclude that a layer of water on the surface of the sphere will accumulate to produce two bulges as shown in the right panel. It is the lateral component of the gravitational acceleration that causes the water to accumulate to produce tidal bulges at points A and B. In contrast, the radial component to the moon's gravitational field has no contribution to the tides. Note that as shown in Section 28.5.3, the bulge shown in the right panel is greatly exaggerated.

center. As for the rod in Figure 28.1, the tidal acceleration at point  $B$  relative to the center of the earth is given by

$$\mathbf{g}(r_B) - \mathbf{g}(R_{\text{em}}) = (2R_e/R_{\text{em}}) \mathbf{g}(R_{\text{em}}). \quad (28.16)$$

This acceleration points towards the moon. In contrast, the tidal acceleration at point  $A$  relative to the center of the earth is given by

$$\mathbf{g}(r_A) - \mathbf{g}(R_{\text{em}}) = -(2R_e/R_{\text{em}}) \mathbf{g}(R_{\text{em}}), \quad (28.17)$$

which is of equal magnitude but points away from the moon.

The tidal accelerations at points  $A$  and  $B$  act radially away from the earth's center. Hence, as noted above, these radial forces do not directly lead to tidal motion at those points. However, through symmetry of the configuration, points on the surface of the sphere between  $A$  and  $B$  have a tidal acceleration from the moon's gravitational field with a nonzero lateral component. These lateral forces lead to the accumulation of water at points  $A$  and  $B$ . We can compute the gravitational acceleration at intermediate points. However, the trigonometry is somewhat complex and we prefer to compute the forces in Section 28.5.3 through use of the gravitational potential. For the current discussion we appeal to symmetry to conclude that the lateral tidal accelerations act to pile up water at both points  $A$  and  $B$  as depicted in the second panel of Figure 28.2. This argument, though heuristic, provides the means to understand how a water covered spherical planet has two bulges, rather than one, due to spatial gradients in the moon's gravitational field. We confirm this argument in Section 28.5.3 by explicitly computing the gravitational potential

for this idealized earth-moon system and then taking the gradient to compute the gravitational acceleration (see Figure 28.4).

### Including orbital motion

Thus far we have ignored the orbital motion of the earth-moon system around their common center of mass. As we will see, there are no fundamental changes to the above arguments when allowing for orbital motion.

In the absence of dissipation, as assumed here, the earth-moon distance remains constant due to their angular momentum conserving orbital motion. From a force-balance perspective, the two spherical bodies remain in a fixed orbit since the gravitational acceleration acting at their centers is balanced by their respective centrifugal accelerations, where the centrifugal acceleration is computed relative to the center of mass of the two-body system. The gravitational acceleration from the moon, acting at the center of the earth, is given by the *free fall* value  $\mathbf{g}(R_{\text{em}})$ , which has magnitude  $GM_{\text{m}}/R_{\text{em}}^2$  and is directed along the axis connecting the earth and moon centers.

Furthermore, when a body exhibits orbital motion, each point on the body exhibits the same orbital motion and has the same linear velocity. Consequently, each point on the earth possess the same centrifugal acceleration

$$\mathbf{a}_{\text{orbital centrifugal}} = -\mathbf{g}(R_{\text{em}}). \quad (28.18)$$

This property of orbital motion is distinct from the spinning motion of a planet rotating about its axis, whereby points further from the rotational axis have larger centrifugal acceleration (see Section 9.12). To help understand orbital motion, move your hand in a circle while maintaining the arm in a single direction so that the hand exhibits an orbital motion rather than a spinning motion. Notice that all parts of the hand move with the same linear velocity and exhibit the same orbital motion. Hence, each point on the hand has the same centrifugal acceleration.

We can now ask about the acceleration felt by a point on the surface of the earth. The acceleration giving rise to tidal motions is the sum of the gravitational acceleration from the moon plus the centrifugal acceleration due to orbital motion. However, this calculation is identical to that considered previously, which led, for example, to the tidal accelerations for points *B* and *A* as given by equations (28.16) and (28.17). We are thus led to the same result as before.

### 28.5.3 Gravitational potential for an idealized earth-moon system

We now perform a more thorough calculation of the gravitational acceleration by computing the gradient of the gravitational potential. First recall the discussion of Newton's gravitational law in Section 9.12.2, whereby the gravitational potential for a point at distance  $r$  from the center of a spherical earth is given by

$$\Phi_{\text{e}}(r) = -\frac{GM_{\text{e}}}{r}, \quad (28.19)$$

where  $M_{\text{e}}$  is the mass of the earth. The corresponding radial gravitational acceleration is given by

$$\mathbf{g}_{\text{e}} = -\nabla\Phi_{\text{e}} = -\frac{GM_{\text{e}}\hat{\mathbf{r}}}{r^2}. \quad (28.20)$$

The same considerations hold for the moon's gravitational potential. Hence, referring to Figure 28.3, the moon's gravitational potential evaluated at a distance  $L$  from the moon's center is given by

$$\Phi_{\text{m}}(L) = -\frac{GM_{\text{m}}}{L}. \quad (28.21)$$

Trigonometry leads to the law of cosines relation

$$L^2 = (R_{\text{em}} - r \cos \psi)^2 + (r \sin \psi)^2 = R_{\text{em}}^2 + r^2 - 2 r R_{\text{em}} \cos \psi, \quad (28.22)$$

where again  $r$  is the distance to the earth's center and  $\psi$  is the polar angle relative to the  $\hat{x}$  axis pointing between the earth and moon centers (see Figure 28.3).

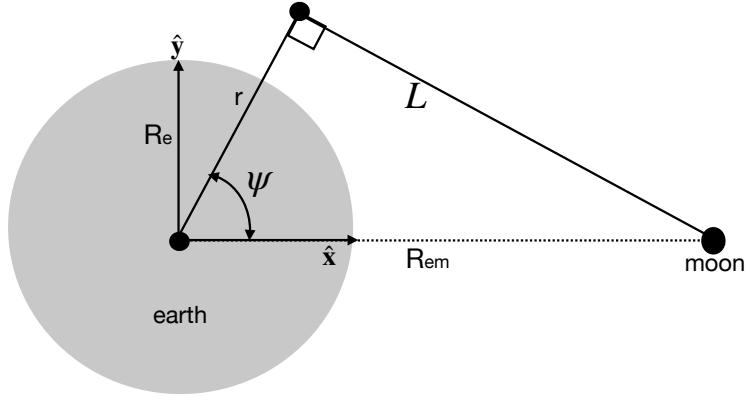


FIGURE 28.3: Geometry of an idealized earth-moon system. The center of the earth is a distance  $R_{\text{em}}$  from the center of the moon; the moon has a mass  $M_m$ ; and the earth has a radius  $R_e$ . An arbitrary test point is shown a distance  $L$  from the center of the moon,  $r$  from the center of the earth, and with a polar angle  $\psi$  relative to the  $\hat{x}$  axis, where the  $\hat{x}$  axis points from the earth center to the moon center. Relative to the earth's center, the test point has Cartesian coordinates  $(x, y) = r(\cos \psi, \sin \psi)$ . See Section 8.3 for details on relating polar and Cartesian coordinates.

### *Identifying the leading order contributions*

Assuming the test point in Figure 28.3 is closer to the earth than to the moon, we can perform a Taylor series expansion in the small parameter  $r/R_{\text{em}}$  to render

$$\Phi_m(L) = -\frac{GM_m}{L} = -\frac{GM_m}{R_{\text{em}}} \left[ 1 + \frac{r \cos \psi}{R_{\text{em}}} + \frac{r^2}{2R_{\text{em}}^2} (3 \cos^2 \psi - 1) + \mathcal{O}(r/R_{\text{em}})^3 \right]. \quad (28.23)$$

We thus identify the leading three terms to the geopotential

$$\Phi_m^{(0)} = -\frac{GM_m}{R_{\text{em}}} \quad (28.24)$$

$$\Phi_m^{(1)} = -\frac{GM_m}{R_{\text{em}}^2} r \cos \psi \quad (28.25)$$

$$\Phi_m^{(2)} = -\frac{GM_m}{2R_{\text{em}}^3} r^2 (3 \cos^2 \psi - 1). \quad (28.26)$$

Assuming the distance between the earth and moon remains fixed, the zeroth order term  $\Phi_m^{(0)}$  is a spatial constant and thus leads to no gravitational acceleration. We now examine the gravitational accelerations from the other two terms.

*Acceleration maintaining the orbiting earth-moon system*

For the first order term,  $\Phi_m^{(1)}$ , we introduce the Cartesian coordinate as in Figure 28.3 to write

$$\Phi_m^{(1)} = -\frac{GM_m x}{R_{em}^2}, \quad (28.27)$$

where  $x = r \cos \psi$  is the distance along  $\hat{x}$ . Hence, the gradient of  $\Phi_m^{(1)}$  leads to the gravitational acceleration

$$\mathbf{g}_m^{(1)} = -\nabla \Phi_m^{(1)} = \hat{x} \frac{GM_m}{R_{em}^2}. \quad (28.28)$$

This gravitational acceleration has a constant magnitude at every point in space and it everywhere points in a direction parallel to the earth-moon axis. Furthermore, the magnitude of  $\mathbf{g}_m^{(1)}$  equals to that of the moon's gravitational acceleration,  $\mathbf{g}_m$ , when evaluated at the earth's center. As seen in Section 28.5.2, the acceleration  $\mathbf{g}_m^{(1)}$  maintains the earth in orbit about the center of mass for the earth-moon system; i.e., this is the free fall acceleration towards the moon. Notably, at the earth's surface, the magnitude of  $\mathbf{g}_m^{(1)}$  is tiny relative to the gravitational acceleration from the earth itself, with their ratios given by

$$\frac{M_m/R_{em}^2}{M_e/R_e^2} \approx 3.4 \times 10^{-6}, \quad (28.29)$$

where we set

$$M_e = 5.97 \times 10^{24} \text{ kg} \quad M_m = 7.35 \times 10^{22} \text{ kg} = (1/81.2) M_e \quad (28.30a)$$

$$R_e = 6.367 \times 10^6 \text{ m} \quad R_{em} = 3.84 \times 10^8 \text{ m} = 60.3 R_e. \quad (28.30b)$$

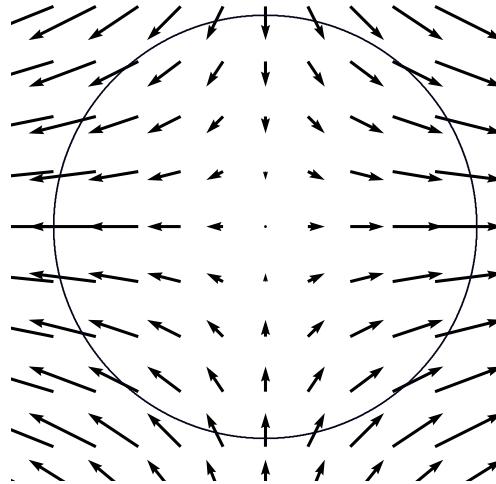


FIGURE 28.4: The tide producing gravitational acceleration  $\mathbf{g}_m^{(2)}$  given by equation (28.34). The moon is assumed to be positioned in the equatorial plane of the earth.

### Tide producing geopotential

The main tide producing acceleration results from  $\Phi_m^{(2)}$ . Introducing the second Cartesian coordinate,  $y = r \sin \psi$ , leads to

$$\Phi_m^{(2)} = -\frac{GM_m}{2R_{em}^3} r^2 (3 \cos^2 \psi - 1) = -\frac{GM_m}{2R_{em}^3} (2x^2 - y^2). \quad (28.31)$$

The corresponding perturbed geopotential height field (see equation (28.11)) is given by

$$h = -\frac{\Phi_m^{(2)}}{g} = \frac{R_e^2}{2R_{em}^3} \frac{M_m}{M_e} r^2 (3 \cos^2 \psi - 1). \quad (28.32)$$

Placing the test point on the earth surface,  $r = R_e$ , renders

$$h = \frac{R_e^4}{2R_{em}^3} \frac{M_m}{M_e} (3 \cos^2 \psi - 1) \approx 2.8 \times 10^{-8} R_e (3 \cos^2 \psi - 1). \quad (28.33)$$

Plugging in numbers for the earth-moon system suggests that the maximum perturbation to the geopotential height arising from the moon's gravity field is roughly 36 cm. Correspondingly, the bulge shown in Figure 28.2 is greatly exaggerated. Note that ocean tidal amplitudes can get much larger (order meters) than this "equilibrium tide" amplitude due to resonances from ocean geometry, with the Bay of Fundy in Nova Scotia a particularly striking example.

### Tide producing acceleration

The gravitational acceleration arising from the tidal potential is determined by the gradient of the tidal geopotential

$$\mathbf{g}_m^{(2)} = -\nabla \Phi_m^{(2)} = \frac{GM_m}{R_{em}^3} (2x \hat{\mathbf{x}} - y \hat{\mathbf{y}}). \quad (28.34)$$

We illustrate the vector field  $\mathbf{g}_m^{(2)}$  in Figure 28.4. Note how the accelerations lead to two bulges on opposite sides of the planet. We can write this acceleration using polar coordinates by introducing the polar unit vectors  $\hat{\mathbf{r}}$  and  $\hat{\psi}$  according to Section 8.3.2

$$\hat{\mathbf{r}} = \hat{\mathbf{x}} \cos \psi + \hat{\mathbf{y}} \sin \psi \quad (28.35a)$$

$$\hat{\psi} = -\hat{\mathbf{x}} \sin \psi + \hat{\mathbf{y}} \cos \psi \quad (28.35b)$$

thus rendering

$$\mathbf{g}_m^{(2)} = \frac{GM_m R_e}{R_{em}^3} \left[ \hat{\mathbf{r}} (3 \cos^2 \psi - 1) - (3/2) \hat{\psi} \sin 2\psi \right], \quad (28.36)$$

where we evaluated the acceleration at the earth surface so that  $r = R_e$ . Evaluating the acceleration at  $\psi = 0, \pi$  verifies the heuristic calculation performed in Section 28.5.2 for points on the earth surface nearest and furthest from the moon. We can further gauge the magnitude of the tidal acceleration by introducing the acceleration due to the earth's gravity field

$$\mathbf{g}_m^{(2)} = g_e \frac{M_m}{M_e} \frac{R_e^3}{R_{em}^3} \left[ \hat{\mathbf{r}} (3 \cos^2 \psi - 1) - (3/2) \hat{\psi} \sin 2\psi \right], \quad (28.37)$$

where  $g_e = GM_e/R_e^2$  is the acceleration at the earth's surface from the earth's gravity field. The dimensional prefactor has magnitude  $\approx 5.6 \times 10^{-8} g_e$ , so that the tidal acceleration is tiny relative to that from the earth's gravity field. It is for this reason that the radial component of the tidal

acceleration is largely irrelevant since it is dominated by the far larger radial component of the earth's gravity field. However, the angular component of the tidal acceleration, although small relative to the earth's radial gravitational acceleration, is able to move water along the surface of the planet as indicated by Figure 28.4, thus leading to tidal motion.

#### 28.5.4 Concerning realistic tides

Our discussion of tides has been rather terse, aiming to identify key aspects of the tidal accelerations but giving little attention to details that impact real ocean tides. Here are a few points that must be considered for these purposes.

- As the earth spins under the tidal bulges, there are two high and two low tides per day. Additional orbital motion of the moon adds roughly 50 minutes per day to the diurnal (daily) tide and 25 minutes to the semi-diurnal (twice daily).
- The moon orbits the earth at a latitude of roughly  $28.5^\circ N$  rather than within the equatorial plane, so that the tidal bulges are offset from the equator. As the earth spins under the bulges, one of the high tides is generally larger than the other due to the offset. This offset in turn introduces a diurnal component to the tides in addition to the semi-diurnal.
- The sun contributes to tides in a manner similar to the moon. The sun is more massive than the moon, yet it is further away, so that the ratio of the magnitudes for the tidal producing accelerations is given by

$$\frac{\text{moon tidal acceleration}}{\text{sun tidal acceleration}} = \frac{M_m/R_{em}^3}{M_s/R_{es}^3} \approx 2.2 \quad (28.38)$$

where we set

$$M_s = 1.99 \times 10^{30} \text{ kg} \quad R_{es} = 23460 R_e. \quad (28.39)$$

Hence, the moon has an impact on tides that is somewhat more than double that of the sun.

- The gravitational acceleration that leads to the tidal bulge moves around the mid-latitudes at roughly  $330 \text{ m s}^{-1}$ , which is faster than the  $\approx 200 \text{ m s}^{-1}$  wave speed for shallow water gravity waves. Hence, the ocean tidal motion is never equilibrated to the *equilibrium tides* defined by the tidal acceleration. In contrast, solid-earth waves are much faster and so the solid-earth tidal motions are mostly equilibrated with the equilibrium tidal acceleration. Solid-earth tides have an amplitude on the order of 10 cm with wavelengths spanning the planet. Hence, an accurate treatment of ocean tides must take into account the solid-earth tides.
- The movement of ocean mass modifies the earth's gravity field, and this modification is referred to as *self-attraction*. Additionally, movement of the ocean mass alters the *loading* felt by the solid-earth and thus causes the crust to compress and expand. These two terms are referred to as the *self attraction and loading* (SAL) terms.
- Geometry of the ocean plays a leading role in determining tides at a particular location. We have incomplete information about the geometry of ocean basins, such as the presence of deep ridges, troughs, and seamounts. In lieu of such information we can garner useful information based on the analysis of past tides, with that information used to fit sinusoidal waves to the measured time series for use in projecting forward in time.

### 28.5.5 Comments

A key feature of the tidal producing forces is that it is the lateral (along-earth) component of the moon's tidal gravitational force that produces the earth's tides. These lateral forces cause water to accumulate at the point nearest to and furthest from the moon (points *A* and *B* in Figure 28.2), thus producing the characteristic double-bulge pattern. Notably, many common literature presentations make it appear that it is the radial (i.e., pointing to the earth's center) component of the moon's gravitational force, and its gradient across the earth, that leads to the earth's tidal bulges. But as discussed in Section 28.5.2, radial gravitational forces cannot lead to tidal motions; what is needed is a force that leads to lateral motion. These key notions are nicely emphasized in [this Space Time video](#).



# Chapter 29

## Surface gravity waves and Stokes drift

In this chapter we consider the ocean surface to be a material interface separating the liquid ocean from the atmosphere above, and we examine its small amplitude fluctuations. These fluctuations manifest as linear surface gravity waves whose existence relies on the restoring force from gravity. In formulating the equations for surface gravity waves, we bring together a number of fluid mechanical principles considered earlier in this book so that this analysis supports our understanding of how basic principles are used to describe motion. Notably, we here ignore rotation, instead focusing on ocean surface waves whose lateral extent is too short to be affected much by the Coriolis force.

Our treatment of surface waves is relatively brief, offering only sufficient details to expose their characteristic exponential decay with depth when moving into the ocean interior. This depth decay leads to a general class of fluid particle motion known as *Stokes drift*, where Stokes drift arises for all waves whose amplitude changes in those directions not parallel to the wave phase direction. So although the surface gravity waves are linear, the depth decay in their amplitude leads to a net drift motion of fluid particles and hence to the transport of matter. The Stokes drift exemplified by surface gravity waves provides an example of how averaging at a fixed point in space (Eulerian average) yields distinct behaviors from averaging on a fixed fluid particle (Lagrangian average). The kinematics of Stokes drift has wide application throughout geophysical fluid mechanics.

### READER'S GUIDE TO THIS CHAPTER

In deriving the basic equations of surface gravity waves we make use of dynamical ideas from Chapter 17 and elements of the filtered equations from Chapter 22. We also make use of ideas from partial differential equations introduced in Chapter 3. The mathematical description of Stokes drift requires an understanding of Eulerian and Lagrangian kinematic descriptions from Chapter 12. Generalizations of Stokes drift appear in Chapter 47 in our study of wave-mean flow interactions, isopycnal averaging, and the corresponding eddy-induced tracer transport. Finally, we ignore surface tension and their associated capillary waves since our interests concern wave motions with far larger wavelengths than capillary waves (a few centimeters; see Section 18.10.3).

29.1	Surface gravity waves . . . . .	690
29.1.1	Harmonic scalar potential . . . . .	690
29.1.2	Equation of motion and Bernoulli's Principle . . . . .	690
29.1.3	Non-hydrostatic pressure and the shallow water limit . . . . .	692
29.1.4	Dynamic boundary condition at the free surface . . . . .	693

29.1.5	Kinematic boundary conditions . . . . .	693
29.1.6	Summary of the linear equation set . . . . .	694
29.2	Surface gravity waves in a flat bottom channel . . . . .	<b>694</b>
29.2.1	Monochromatic wave solution . . . . .	695
29.2.2	Dispersion relation for surface gravity waves . . . . .	695
29.2.3	Heuristics of waves in the shortwave/deep water limit . . . . .	696
29.2.4	Heuristics of waves in the longwave/shallow water limit . . . . .	696
29.2.5	Further study . . . . .	697
29.3	Stokes drift . . . . .	<b>697</b>
29.3.1	General formulation of Stokes drift . . . . .	697
29.3.2	Stokes drift in surface gravity waves . . . . .	699
29.3.3	Comments and further study . . . . .	702
29.4	Exercises . . . . .	<b>703</b>

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## 29.1 Surface gravity waves

We study linear fluctuations of the ocean free surface on a non-rotating plane, with the free surface assumed to be a material interface separating a homogeneous ocean from a homogeneous atmosphere (Figure 29.1). The mass of the atmosphere is horizontally uniform and static so that surface atmosphere pressure does not contribute to oceanic motion. We develop the boundary value problem describing linear wave motions of the free surface, and characterize physical aspects of the waves.

### 29.1.1 Harmonic scalar potential

We are interested in fluctuations that have zero vorticity so that the velocity field has zero curl<sup>1</sup>

$$\nabla \times \mathbf{v} = 0. \quad (29.1)$$

Recall from Section 2.3.2 that vector fields with zero curl can be determined from a scalar potential

$$\mathbf{v} = -\nabla\psi. \quad (29.2)$$

Note that the scalar potential is unspecified up to an arbitrary function of time, since  $\psi$  and  $\psi + F(t)$  yield the same velocity field. We make use of this *gauge* freedom in Section 29.1.2.

Since the ocean is assumed to have uniform density, the velocity field is non-divergent. Consequently, the scalar potential satisfies Laplace's equation (Section 2.3.3)

$$\nabla \cdot \mathbf{v} = -\nabla \cdot \nabla\psi = \nabla^2\psi = 0. \quad (29.3)$$

$\psi$  is termed a *harmonic function*, with salient properties noted in Section 3.5. To fully specify the scalar potential requires boundary conditions, which enter our development via the equation of motion.

### 29.1.2 Equation of motion and Bernoulli's Principle

The vector-invariant equation of motion (17.32) for a non-rotating, irrotational, inviscid, uniform density fluid is given by

$$\frac{\partial \mathbf{v}}{\partial t} = -\nabla(\Phi + \mathcal{K} + p/\rho), \quad (29.4)$$

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<sup>1</sup>We study fluids with nonzero vorticity in Part VI of this book.

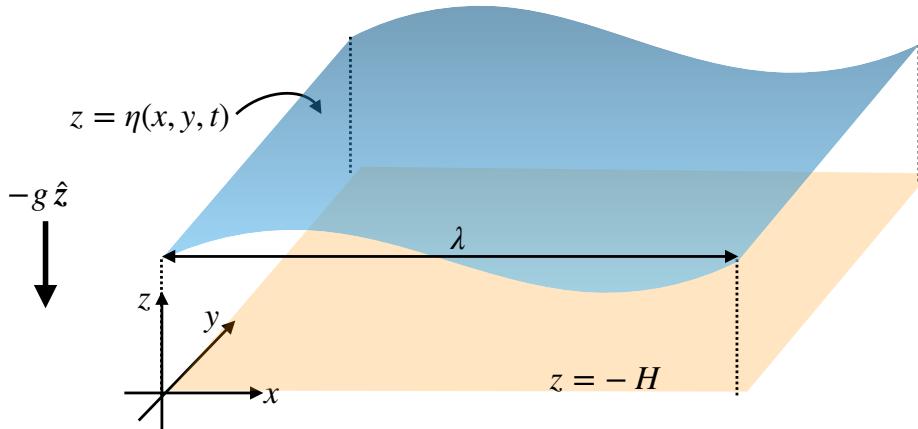


FIGURE 29.1: A depiction of the ocean free surface as a mathematical surface whose linear fluctuations exhibit gravity wave motion due to the restoring effects from a uniform gravitational field,  $\mathbf{g} = -g \hat{\mathbf{z}}$ . The atmosphere applies a pressure to the ocean due to its mass; however, that mass is assumed to be uniform and static so that it does not affect surface motion. Our formulation of surface waves makes no restrictions on the depth of the fluid relative to the wavelength of the waves, with the resulting waves exhibiting dispersion (i.e., the wave speed is a function of the wavelength). However, assuming the depth to be far smaller than the wavelength,  $H \ll \lambda$  recovers the dispersion relation for linear non-dispersive shallow water gravity waves discussed in Section 31.8.3.

with

$$\mathcal{K} = \frac{\mathbf{v} \cdot \mathbf{v}}{2} \quad (29.5)$$

the kinetic energy per mass of a fluid element. In the following we assume the simple form of the geopotential (Section 9.12.4)

$$\Phi = g z \quad (29.6)$$

with  $g$  the constant gravitational acceleration. Inserting the scalar potential,  $\mathbf{v} = -\nabla\psi$ , brings the equation of motion (29.4) to the form

$$\nabla(\Phi + \mathcal{K} + p/\rho - \partial_t\psi) = 0. \quad (29.7)$$

This equation means that everywhere in the fluid the dynamical fields satisfy

$$\Phi + \mathcal{K} + p/\rho - \partial_t\psi = C(t), \quad (29.8)$$

for some arbitrary time dependent function  $C(t)$ . This equation is a particular expression of Bernoulli's theorem encountered in Section 21.6.2.

#### *Removing the time dependent function via a gauge transformation*

We ascribe no physical meaning to the arbitrary function  $C(t)$  appearing in equation (29.8). In fact, it can be completely removed by exploiting the gauge degree of freedom in the scalar potential as noted following equation (29.2). We do so by introducing a modified scalar potential

$$\Psi(\mathbf{x}, t) = \psi(\mathbf{x}, t) + \int^t C(t') dt'. \quad (29.9)$$

Both  $\psi$  and  $\Psi$  lead to the same velocity vector

$$\mathbf{v} = -\nabla\psi = -\nabla\Psi \quad (29.10)$$

and as such they are physically indistinguishable. However,  $\Psi$  has the mathematical advantage of absorbing the arbitrary time dependent function  $C(t)$ , thus rendering the simpler expression for the equation of motion

$$\Phi + \mathcal{K} + p/\rho - \partial_t \Psi = 0. \quad (29.11)$$

This equation provides a balance condition that constrains the flow properties at every point within the fluid.

### *A brief diversion into Bernouilli's Principle for steady flow*

The central focus of this analysis is with transient fluctuations of the free surface. Even so, we here comment on the case of steady flow, in which the constraint (29.11) leads to

$$\Phi + \mathcal{K} + p/\rho = 0. \quad (29.12)$$

Furthermore, assuming motion occurs on a constant geopotential then leads to

$$p + \rho \mathcal{K} = \text{constant}. \quad (29.13)$$

Motion on a geopotential means that all fluid particles feel the same gravitational acceleration. Hence, spatial changes in pressure provide the only force that can lead to spatial changes in fluid speed. That is the physical content of this special form of Bernouilli's Principle given by equation (29.13). It says that in regions of relatively high fluid speed the pressure is relatively low, and vice versa. Correspondingly, if the fluid moves into a region of relatively high pressure then it must slow down, whereas the speed increases when moving to a region of low pressure. This principle helps to explain the basic features of steady state flow around obstacles such as airplane wings.

### 29.1.3 Non-hydrostatic pressure and the shallow water limit

The fluid is non-hydrostatic since

$$\frac{\partial p}{\partial z} = -\rho \frac{\partial \Phi}{\partial z} + \frac{\partial(\partial_t \Psi - \mathcal{K})}{\partial z} = \frac{\partial p_{\text{hydrostatic}}}{\partial z} + \frac{\partial p_{\text{non-hydrostatic}}}{\partial z}. \quad (29.14)$$

Depth variations in the kinetic energy and depth-time variations in the velocity potential lead to deviations from hydrostatic balance. We do not generally expect the flow to be hydrostatically balanced for two reasons: (i) the fluid layer has a uniform density so there is no stratification to suppress vertical accelerations that contribute to non-hydrostatic pressures; (ii) the fluid is nonrotating and so there is no vertical stiffening via the Taylor-Proudman result (Section 25.5.3), with vertical stiffening acting to suppress vertical accelerations that cause deviations from hydrostatic balance.

For the shallow water model we also consider a homogenous density layer. However, as shown in Chapter 30, the hydrostatic balance is fundamental to the dynamics. In particular, in Section 30.2 we see that the hydrostatic balance over a single homogeneous layer leads to horizontal motion that is depth independent throughout the layer. Hence,  $\partial_z(\partial_t \Psi) = 0$  and the kinetic energy in the horizontal motions is depth independent,  $\partial_z(u^2 + v^2) = 0$ . Furthermore, the vertical motion has a linear depth dependence across the shallow water layer (Section 30.2.7) and its magnitude is far smaller than horizontal motions. Therefore, we can drop all contributions to  $\partial_z \mathcal{K}$  for the shallow water layer, in which case equation (29.14) reduces to the hydrostatic limit

$$\frac{\partial p}{\partial z} = -\rho \frac{\partial \Phi}{\partial z} = -\rho g \quad \text{hydrostatic limit.} \quad (29.15)$$

So in summary, a homogeneous layer of fluid can have a depth dependence to its horizontal flow. But that depth dependence is driven only through non-hydrostatic pressure forces. The reason is the hydrostatic pressure has a depth-independent horizontal gradient within a homogeneous layer

$$\partial_z (\nabla_z p_{\text{hydrostatic}}) = -g \nabla_z \rho = 0. \quad (29.16)$$

#### 29.1.4 Dynamic boundary condition at the free surface

Return now to the time dependent expression of the equation of motion (29.11). It is a rather remarkable result that applies to any point within the fluid and at any time. In particular, it applies at the free surface,  $z = \eta(x, y, t)$  where pressure equals to the atmospheric pressure. As stated earlier, we assume that the atmospheric pressure is constant in space and time so that

$$g \eta + \mathcal{K} - \partial_t \Psi = -p_a / \rho = \text{constant}. \quad (29.17)$$

Without loss of generality we can set this constant to zero.<sup>2</sup> We are thus left with the boundary condition

$$g \eta + \mathcal{K} - \partial_t \Psi = 0 \quad \text{at } z = \eta. \quad (29.18)$$

At this point we linearize relative to a state of rest with  $\eta = 0$ ,  $\mathbf{v} = 0$ , and  $\partial_t \Psi = 0$ . Linear fluctuations about this rest state have small velocities and as such the kinetic energy, which is second order in velocity, can be dropped to leave the linearized boundary condition

$$g \eta = \frac{\partial \Psi}{\partial t} \quad \text{linearized dynamic b.c. at } z = \eta. \quad (29.19)$$

This boundary condition directly connects the free surface to time tendencies of the velocity potential. The free surface rises when the velocity potential has a positive tendency, and vice versa.

#### 29.1.5 Kinematic boundary conditions

The free surface is assumed to be a material interface, meaning that we ignore effects from matter transport across this surface. Consequently, following the discussion of kinematic boundary conditions in Section 14.4.2, we have

$$\frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla \eta = w \quad \text{at } z = \eta. \quad (29.20)$$

Linearizing this boundary condition about the state of rest, and introducing the scalar potential, leads to

$$\frac{\partial \eta}{\partial t} = -\frac{\partial \Psi}{\partial z} \quad \text{linearized kinematic b.c. at } z = \eta. \quad (29.21)$$

This is yet another constraint that links the free surface to the velocity potential.

One final kinematic boundary condition applies just to the velocity potential when it intersects with the rigid solid boundaries. Namely, the no normal flow condition from Section 14.4.1 means that

$$\hat{\mathbf{n}} \cdot \nabla \Psi = 0 \quad \text{on rigid solid boundaries}, \quad (29.22)$$

where  $\hat{\mathbf{n}}$  is the outward normal on the solid boundaries.

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<sup>2</sup>Alternatively, make use of a further gauge transformation  $\Psi' = \Psi - t(p_a/\rho)$  to eliminate the constant.

### 29.1.6 Summary of the linear equation set

The boundary value problem for the velocity potential and free surface is given by

$$\nabla^2 \Psi = 0 \quad \text{irrotational and non-divergent velocity throughout domain} \quad (29.23a)$$

$$\frac{\partial \Psi}{\partial t} = g \eta \quad \text{linearized dynamic b.c. at } z = \eta \quad (29.23b)$$

$$\frac{\partial \Psi}{\partial z} = -\frac{\partial \eta}{\partial t} \quad \text{linearized kinematic b.c. at } z = \eta \quad (29.23c)$$

$$\hat{\mathbf{n}} \cdot \nabla \Psi = 0 \quad \text{no-normal flow kinematic b.c. on rigid boundaries.} \quad (29.23d)$$

The first equation holds throughout the fluid whereas the remaining equations hold only at the boundaries.

Although the equations (29.23a)-(29.23d) were derived through linearization, there is an additional nonlinear term to remove in order to allow for analytical treatment of the wave solutions. Namely, when combining the boundary conditions into a single equation we compute the time derivative of equation (29.23b) according to

$$g \frac{\partial \eta}{\partial t} = \left[ \frac{\partial}{\partial t} + \frac{\partial \eta}{\partial t} \frac{\partial}{\partial z} \right] \frac{\partial \Psi}{\partial t} \quad (29.24)$$

and then combine with equation (29.23c) to render

$$\left[ \frac{\partial}{\partial t} + \frac{\partial \eta}{\partial t} \frac{\partial}{\partial z} \right] \frac{\partial \Psi}{\partial t} = -g \frac{\partial \Psi}{\partial z}. \quad (29.25)$$

With  $w \approx \partial \eta / \partial t$  at the free surface, we identify  $(\partial \eta / \partial t) \partial_z$  as a vertical advection operator. The corresponding term  $(\partial \eta / \partial t) \partial_{zt} \Psi$  is nonlinear and second order in perturbation terms. It is therefore dropped when fully linearizing the system. An equivalent means to realize this linearization is to evaluate the free surface boundary condition at  $z = 0$  rather than at  $z = \eta(x, y, t)$ . For this approximation to be self-consistent requires the amplitude of free surface undulations to be much smaller than the typical wavelengths of the fluctuations

$$|\eta|/\lambda \ll 1. \quad (29.26)$$

In summary, the fully linearized equation set takes the form

$$\nabla^2 \Psi = 0 \quad \text{irrotational and non-divergent velocity throughout domain} \quad (29.27a)$$

$$g \eta = \frac{\partial \Psi}{\partial t} \quad \text{linearized dynamic b.c. at } z = 0 \quad (29.27b)$$

$$\frac{\partial \eta}{\partial t} = -\frac{\partial \Psi}{\partial z} \quad \text{linearized kinematic b.c. at } z = 0 \quad (29.27c)$$

$$\hat{\mathbf{n}} \cdot \nabla \Psi = 0 \quad \text{no-normal flow kinematic b.c. on rigid boundaries.} \quad (29.27d)$$

## 29.2 Surface gravity waves in a flat bottom channel

We now derive a wave-like solution to the equations (29.27a)-(29.27d) posed in a flat bottom channel domain as illustrated in Figure 29.1. This analysis provides experience with the *separation of variables* method of use for deriving solutions to certain partial differential equations. We are not interested in the most general wave solution. Instead, we aim to determine a particular solution of sufficient generality to expose the underlying physics of the linear wave fluctuations,

and in particular to expose the exponential decay of the wave amplitude with depth. Furthermore, given linearity, the superposition principle holds whereby the linear sum of particular solutions is also a solution.

### 29.2.1 Monochromatic wave solution

We seek a monochromatic wave solution with the wave moving parallel to the channel with radial frequency  $\omega = 2\pi/\tau$  and wavenumber  $k = 2\pi/\lambda$ , with  $\tau$  the period and  $\lambda$  the wavelength. We furthermore assume the waves appear in the velocity potential in the shape of a cosine with an undetermined vertical structure

$$\Psi(x, y, z, t) = \Gamma(z) \cos(kx - \omega t). \quad (29.28)$$

Note the assumed absence of  $y$  dependence, as motivated by our choice to examine waves moving parallel to the channel and with symmetry across the channel. Furthermore, the cosine and sine functions form a complete set of basis functions for the channel domain, so that they can be superposed to generate any arbitrary wave pattern. This property is the basis for Fourier analysis commonly employed to study waves.

Plugging the ansatz (29.28) into Laplace's equation  $\nabla^2\Psi = \partial_{xx}\Psi + \partial_{zz}\Psi = 0$  leads to the ordinary differential equation satisfied by the vertical structure function

$$\frac{d^2\Gamma}{dz^2} = k^2 \Gamma \quad -H \leq z \leq 0 \quad (29.29a)$$

$$\frac{d\Gamma}{dz} = 0 \quad \text{at } z = -H, \quad (29.29b)$$

where the bottom boundary condition is required to satisfy the no-normal flow condition (29.27d). We write the solution in the form

$$\Psi = \Psi_o \cosh[k(z + H)] \cos(kx - \omega t), \quad (29.30a)$$

$$\Psi_o = \frac{g \eta_o / \omega}{\cosh(kH)} \quad (29.30b)$$

so that the boundary condition (29.27b) renders the free surface height

$$\eta(x, t) = -\eta_o \sin(kx - \omega t). \quad (29.31)$$

The corresponding velocity field,  $\mathbf{v} = -\nabla\Psi$ , is given by

$$u = -\Psi_o k \cosh[k(z + H)] \sin(kx - \omega t) \quad (29.32a)$$

$$w = -\Psi_o k \sinh[k(z + H)] \cos(kx - \omega t). \quad (29.32b)$$

### 29.2.2 Dispersion relation for surface gravity waves

Combining the two  $z = 0$  boundary conditions (29.27b) and (29.27c) yields

$$\frac{\partial^2\Psi}{\partial t^2} + g \frac{\partial\Psi}{\partial z} = 0 \quad z = 0. \quad (29.33)$$

Substituting the wave solution (29.30a) into this relation leads to the constraint

$$\omega^2 = g k \tanh(kH). \quad (29.34)$$

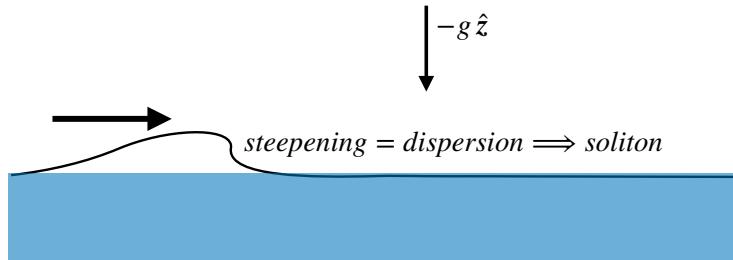


FIGURE 29.2: A soliton in the deep water limit results when the wave dispersion (long waves travel faster than short waves) balances the nonlinear steepening. The result is a soliton, which has an exact analytic expression following from the KdV equation (see [Drazin and Johnson \(1989\)](#)).

This is the *dispersion relation* that constrains values available for the radial frequency,  $\omega$ , and wavenumber,  $k$ . That is, the surface gravity waves only exist if their frequency and wavenumber are related according to the dispersion relation (29.34). The corresponding phase speed for the wave is given by

$$c = \frac{\omega}{k} = \sqrt{(g/k) \tanh(kH)}. \quad (29.35)$$

We emphasize the two limits:  $kH \gg 1$  (shortwaves/deep water) and  $kH \ll 1$  (longwave/shallow water), in which the phase speed satisfies

$$\omega \approx \sqrt{gk} \quad c \approx \sqrt{g/k} \quad kH \gg 1 \quad \text{shortwave/deep water limit} \quad (29.36a)$$

$$\omega \approx k\sqrt{gH} \quad c \approx \sqrt{gH} \quad kH \ll 1 \quad \text{longwave/shallow water limit.} \quad (29.36b)$$

### 29.2.3 Heuristics of waves in the shortwave/deep water limit

The shortwave/deep water waves are notable for having shorter waves travel slower than longer waves. In the event of a perturbation to the fluid, such as from a stone dropped into a pond or a storm on a lake or the ocean, deep water waves are energized. The dispersion relation means that longer waves spread away from the storm center faster than the shorter waves, leading to a self-organization of the wavelengths and corresponding wave packets.

Now imagine a deepwater wave packet (group of waves traveling together) that somehow steepens and takes on a nonlinear form. Fourier decomposing this nonlinear wave into linear deepwater modes requires more shortwave linear modes in the steep region, whereas the less steep portion of the wave requires longer deep water Fourier modes, which travel faster. If the nonlinear steepening on the wave face is exactly balanced by the faster dispersion of the long waves near the wave base and back-side, then the wave pattern remains stable; it does not break. This balance of steepening and dispersion describes the fundamental features of a soliton.

### 29.2.4 Heuristics of waves in the longwave/shallow water limit

The longwave/shallow water limit is notable for the absence of wave dispersion; i.e., shallow water gravity waves of all wavelengths travel at speed  $\sqrt{gH}$ . Tsunamis are the prototypical shallow water waves that travel at speeds well approximated by  $\sqrt{gH}$ .

The dispersion relation also means that shallow water gravity waves slow down when the depth shoals, as when approaching a beach. Consequently, as waves reach the shoreline there is a tendency to accumulate wave energy as the deeper waves pile up behind the shallower waves. Furthermore, the steeper part of the wave, being part of a thicker region of the fluid and thus a larger effective  $H$ , travels slightly faster than the wave trough. As such, the steeper part of the

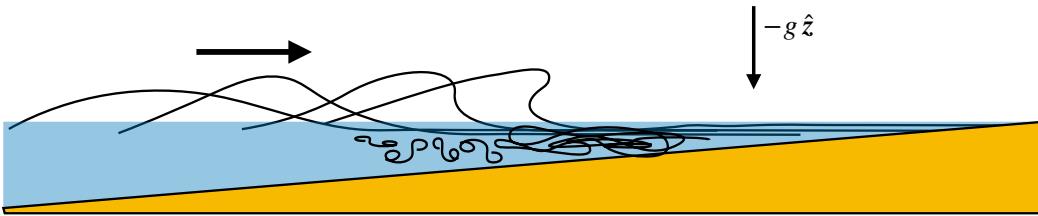


FIGURE 29.3: Shallow water waves approaching a shoreline steepen and eventually break. We can infer this behavior from the dispersion relation,  $\sqrt{gH}$ , whereby waves in deeper water move slightly faster than those in shallower water, so that the wave energy accumulates near the shore. Furthermore, water on the steeper part of the wave moves slightly faster than water in the trough, due to the difference in thickness of the water. This process causes water on the steeper portion of the wave to travel slightly faster than in the trough, leading to steepening of the waves. Nonlinearities eventually invalidate the assumptions made in deriving the linear wave dispersion relation  $c = \sqrt{gH}$ . Even so, the qualitative characterization based on the linear analysis allows for a useful heuristic understanding of shallow water wave breaking on the beach.

wave overtakes the trough and, at some point, the assumptions of linearity breakdown and the shallow water waves break on the shore as depicted in Figure 29.3.

### 29.2.5 Further study

Elements from this section follow Section 54 of the [Fetter and Walecka \(1980\)](#), with their discussion of surface gravity waves also probing topics such as energetics, group velocity, and the inclusion of surface tension as appropriate for deep water waves with wavelengths on the order of centimeters. An accessible development of the theory of solitons can be found in the book by [Drazin and Johnson \(1989\)](#). Ocean surface waves are generally energized by atmospheric winds, in particular large storms. The dynamics of gravity wave breaking in the open ocean and on the beach remains a decades-long problem in fluid mechanics that stretches the limits of theory, experiment, and simulation. [Bühler \(2014a\)](#) offers a thorough treatment of waves and their effects on mean flows

This video from [Prof. A. Hogg](#) provides a pedagogical introduction to shallow water wave breaking as well as deep water solitons realized in a laboratory.

## 29.3 Stokes drift

We here consider a fluid particle moving as part of a wave field. In homogenous linear wave fields, the particle periodically returns to its original position. However, in the presence of wave inhomogeneities, such as the surface gravity waves considered in this chapter, fluid particles generally oscillate between regions where the undulation in one direction does not match that in the other direction. In this case there is a net particle drift or transport known as *Stokes drift*. This drift occurs even though the phase average of the wave at a fixed spatial point vanishes. Formulating the mathematics of Stokes drift offers a means to explore the differences between averages formed at a fixed space point (Eulerian mean) versus averages following fluid particles (Lagrangian mean). We here introduce these notions, which form part of the rudiments for wave-mean flow interaction theory further pursued in Chapter 47.

### 29.3.1 General formulation of Stokes drift

Consider a three-dimensional particle trajectory written in Cartesian coordinates,

$$\mathbf{X}(\mathbf{a}, t) = X(\mathbf{a}, t) \hat{\mathbf{x}} + Y(\mathbf{a}, t) \hat{\mathbf{y}} + Z(\mathbf{a}, t) \hat{\mathbf{z}}. \quad (29.37)$$

In the analysis of waves, it is common to assume the material coordinate,  $\mathbf{a}$ , is the initial position of a fluid particle so we make that assumption here. As discussed in Section 12.8.1, the particle trajectory is determined by time integrating the particle velocity (also known as the “flow map”)

$$\frac{\partial \mathbf{X}(\mathbf{a}, t)}{\partial t} = \mathbf{v}[\mathbf{X}(\mathbf{a}, t), t] \quad (29.38)$$

so that

$$\mathbf{X}(\mathbf{a}, t) = \mathbf{X}(\mathbf{a}, 0) + \int_0^t \mathbf{v}[\mathbf{X}(\mathbf{a}, t'), t'] dt'. \quad (29.39)$$

This equation is a trivial result of time integrating the flow map. Nonetheless, it is useful to express the content of this equation in words. It says that the position at time  $t$  of a fluid particle labelled by the material coordinate  $\mathbf{a}$  is given by the initial position of the particle,  $\mathbf{X}(\mathbf{a}, 0)$ , plus the time integrated movement of the particle following the fluid flow.

We now form a Taylor series computed relative to the initial position of the particle, so that the particle velocity at time  $t$  takes on the approximate form

$$v^n[\mathbf{X}(\mathbf{a}, t), t] \approx v^n[\mathbf{X}(\mathbf{a}, 0), t] + \nabla v^n[\mathbf{X}(\mathbf{a}, 0), t] \cdot [\mathbf{X}(\mathbf{a}, t) - \mathbf{X}(\mathbf{a}, 0)] \quad (29.40a)$$

$$= v^n[\mathbf{X}(\mathbf{a}, 0), t] + \nabla v^n[\mathbf{X}(\mathbf{a}, 0), t] \cdot \int_0^t \frac{d\mathbf{X}(\mathbf{a}, t')}{dt'} dt' \quad (29.40b)$$

$$= v^n[\mathbf{X}(\mathbf{a}, 0), t] + \nabla v^n[\mathbf{X}(\mathbf{a}, 0), t] \cdot \int_0^t \mathbf{v}[\mathbf{X}(\mathbf{a}, t'), t'] dt', \quad (29.40c)$$

where the Taylor series was truncated after terms linear in the particle displacement  $\mathbf{X}(\mathbf{a}, t) - \mathbf{X}(\mathbf{a}, 0)$ . We emphasize two points regarding equation (29.40c).

- How do we interpret  $v^n[\mathbf{X}(\mathbf{a}, 0), t]$ ? This is the  $n$ 'th component of the velocity field evaluated at the initial point of the trajectory,  $\mathbf{X}(\mathbf{a}, 0)$ , at time  $t$ . That is, it is the Eulerian velocity evaluated at the fixed Eulerian point  $\mathbf{X}(\mathbf{a}, 0)$ .
- What determines the accuracy of the Taylor series? A suitable non-dimensional expansion coefficient for the Taylor expansion is the ratio of the particle displacement to the scale,  $\Lambda$ , of inhomogeneities in flow properties

$$\epsilon = \frac{|\mathbf{X}(\mathbf{a}, t) - \mathbf{X}(\mathbf{a}, 0)|}{\Lambda}. \quad (29.41)$$

This ratio is small for the small amplitude waves considered here, whereby the particle displacements are far smaller than inhomogeneities in flow properties.

The integrand on the right hand side of equation (29.40c) is the Lagrangian velocity integrated over the time interval. To within the same order of accuracy as maintained thus far, we can use the Eulerian velocity evaluated at the initial position, thus rendering

$$v^n[\mathbf{X}(\mathbf{a}, t), t] \approx v^n[\mathbf{X}(\mathbf{a}, 0), t] + \nabla v^n[\mathbf{X}(\mathbf{a}, 0), t] \cdot \int_0^t \mathbf{v}[\mathbf{X}(\mathbf{a}, 0), t'] dt', \quad (29.42)$$

with rearrangement leading to

$$v^n[\mathbf{X}(\mathbf{a}, t), t] - v^n[\mathbf{X}(\mathbf{a}, 0), t] \approx \nabla v^n[\mathbf{X}(\mathbf{a}, 0), t] \cdot \int_0^t \mathbf{v}[\mathbf{X}(\mathbf{a}, 0), t'] dt'. \quad (29.43)$$

The left hand side is the difference between the velocity following a fluid particle (the Lagrangian

velocity for the moving fluid particle) from the velocity at the initial particle point (the Eulerian velocity at the initial point of the trajectory). The right hand side terms are all evaluated at the initial position,  $\mathbf{X}(\mathbf{a}, 0)$ . Furthermore, the right hand side is non-zero where the velocity at the initial position has a nonzero gradient (i.e., it is spatially inhomogeneous), with its inhomogeneity projecting onto the time integrated velocity at that point. Equation (29.43) says that the velocity following a fluid particle is modified from the velocity at its initial position if the particle moves through an inhomogeneous velocity field.

The Stokes drift is defined as the difference of the velocities in equation (29.43) when time averaged over a wave period, which we write as

$$v_{(S)}^n[\mathbf{X}(\mathbf{a}, 0), t] = \overline{v^n[\mathbf{X}(\mathbf{a}, t), t] - v^n[\mathbf{X}(\mathbf{a}, 0), t]} \quad (29.44a)$$

$$\approx \nabla v^n[\mathbf{X}(\mathbf{a}, 0), t] \cdot \int_0^t \mathbf{v}[\mathbf{X}(\mathbf{a}, 0), t'] dt'. \quad (29.44b)$$

This expression holds for any arbitrary initial point in the fluid, so that we can write it in a concise Eulerian form that dispenses with trajectories

$$v_{(S)}^n(\mathbf{x}, t) \approx \overline{\nabla v^n(\mathbf{x}, t) \cdot \int_0^t \mathbf{v}(\mathbf{x}, t') dt'}. \quad (29.45)$$

We liken Stokes drift to surfing: the more a particle samples larger amplitude variations in the velocity field (the gradient term), the further it drifts (the integral term). Note that for the case of a transverse wave disturbance, where the particle disturbance is orthogonal to the wavevector, then the Stokes drift vanishes to leading order.

### 29.3.2 Stokes drift in surface gravity waves

The canonical example of Stokes drift occurs in the near surface ocean, where the surface gravity waves discussed in Section 29.1 create particle motion that is larger near the surface than at depth. For this example, consider a monochromatic wave field in the zonal-vertical directions written in the form

$$\frac{dX}{dt} = U \sin(\omega t) \quad (29.46a)$$

$$\frac{dZ}{dt} = U \cos(\omega t), \quad (29.46b)$$

where  $U > 0$  is the speed of the circular particle motion and we use the capital  $X$  and  $Z$  to denote Cartesian components of the particle trajectory. To simplify the mathematics we perform the analysis in a frame where the waves are stationary, hence the  $kx - \omega t$  phase from Section 29.2. Figure 29.4 shows a schematic of the particle trajectories as derived in the following.

#### *Homogeneous flow field*

If the background flow is homogeneous, then the speed is a constant,  $U = U_o > 0$ . Particle trajectories in this case are clockwise in the x-z plane around a circle with radius  $U_o/\omega$

$$X(t) - X_o = -\frac{U_o}{\omega} [\cos(\omega t) - 1] \quad (29.47a)$$

$$Z(t) - Z_o = \frac{U_o}{\omega} \sin(\omega t), \quad (29.47b)$$



FIGURE 29.4: Sketch of Stokes drift in the upper ocean with the wave vector in the horizontal direction and clockwise time integrated fluid particle motion induced by the traveling wave. For the case of a wave amplitude that decreases with depth, lateral motion of the particle is larger when the particle is closer to the surface thus leading to a Stokes drift in the direction of the wave. Note that there is zero Stokes drift for the case of a homogeneous wave, in which the wave amplitude is independent of depth. Additionally, and even more trivially, if the particle motion is purely transverse to the wave vector, in this case purely vertical, then the particle merely retraces its motion along a vertical line and does not undergo any lateral Stokes drift.

where the initial position at time  $t = 0$  is

$$\mathbf{X}(t = t_o) = \mathbf{X}_o, \quad (29.48)$$

and the center of the circle is

$$\mathbf{X}_{\text{center}} = \left[ X_o + \frac{U_o}{\omega} \right] \hat{\mathbf{x}} + Z_o \hat{\mathbf{z}}. \quad (29.49)$$

### Inhomogeneous flow field

In the presence of vertical inhomogeneities of the flow field, the wave amplitude becomes a function of depth,  $U = U(z)$ . The canonical example is where the wave amplitude decreases with depth, as for the surface gravity waves detailed in Section 29.2. In turn, we expect there to be a fluid particle drift in the zonal direction introduced by the vertical wave inhomogeneity. This drift is a particular realization of Stokes drift.

To compute the leading order expression for the Stokes drift, expand  $U$  in a Taylor series about the initial position

$$U \approx U_o + R(Z - Z_o) \quad (29.50)$$

where  $R$  has units of inverse time and is given by

$$R = \left[ \frac{dU}{dZ} \right]_{Z=Z_o}. \quad (29.51)$$

For the surface gravity waves with velocity components (29.32a) and (29.32b), we have

$$U = \Psi_o k \sqrt{\cosh[2k(z + H)]} \quad (29.52)$$

so that with  $Z_o = 0$ ,

$$R = \Psi_o k^2 \frac{\sinh(2kH)}{\sqrt{\cosh(2kH)}}. \quad (29.53)$$

In general, the Taylor series is valid so long as the vertical trajectories maintain the inequality

$$|R| |Z - Z_o| \ll U_o, \quad (29.54)$$

which says that the vertical shear is small

$$|R| \ll \frac{U_o}{|Z - Z_o|}. \quad (29.55)$$

We use the Taylor series expansion (29.50) to solve for the vertical trajectory as determined by

$$\frac{d(Z - Z_o)}{dt} = [U_o + R(Z - Z_o)] \cos(\omega t). \quad (29.56)$$

Rearrangement leads to

$$\int_{Z_o}^Z \frac{d(Z - Z_o)}{U_o + R(Z - Z_o)} = \int_0^t \cos(\omega t) dt. \quad (29.57)$$

The left hand side integral can be computed by changing variables

$$\Sigma = U_o + R(Z - Z_o) \quad (29.58a)$$

$$d\Sigma = R d(Z - Z_o), \quad (29.58b)$$

so that equation (29.57) becomes

$$\int_{U_o}^{\Sigma} \frac{d\Sigma}{\Sigma} = R \int_0^t \cos(\omega t) dt. \quad (29.59)$$

Performing the integrals and evaluating the end points renders

$$\ln \left[ 1 + \frac{R}{U_o} (Z - Z_o) \right] = \frac{R \sin(\omega t)}{\omega}, \quad (29.60)$$

which yields the exponential solution

$$1 + \frac{R}{U_o} (Z - Z_o) = e^{(R/\omega) \sin(\omega t)} \Rightarrow Z - Z_o = \frac{U_o}{R} \left( -1 + e^{(R/\omega) \sin(\omega t)} \right). \quad (29.61)$$

The vertical particle position is seen to oscillate around its initial position  $Z_o$ .

We next consider the zonal particle position, in which case

$$\frac{d(X - X_o)}{dt} = U_o \left[ 1 + \frac{R}{U_o} (Z - Z_o) \right] \sin(\omega t) \quad (29.62a)$$

$$= U_o e^{(R/\omega) \sin(\omega t)} \sin(\omega t) \quad (29.62b)$$

where we used equation (29.61) for the vertical trajectory. To make progress, we expand the exponential assuming the ratio of inverse time scales,  $R/\omega$ , is small

$$|R/\omega| \ll 1. \quad (29.63)$$

In this limit, the vertical trajectory retains its unperturbed form (29.47b), and the zonal trajectory satisfies

$$\frac{d(X - X_o)}{dt} \approx U_o \sin(\omega t) \left[ 1 + \frac{R}{\omega} \sin(\omega t) \right], \quad (29.64)$$

where we dropped terms of order  $(R/\omega)^2$ . We can understand the scaling in equation (29.63) by noting that the period for the circular motion is given by

$$\tau_{\text{circle}} = \frac{2\pi}{\omega}. \quad (29.65)$$

The inverse time  $R$  introduces a time scale for the drift, defined according to

$$\tau_{\text{drift}} = \frac{2\pi}{|R|}. \quad (29.66)$$

A small ratio  $|R/\omega|$  thus implies

$$|R/\omega| = \tau_{\text{circle}}/\tau_{\text{drift}} \ll 1. \quad (29.67)$$

Hence, we are solving for the zonal trajectory in the limit where the time scale for the circular motion is small (i.e., fast oscillations around the circle) relative to the time scale for the drift (i.e., slow drift).

Returning now to the approximate zonal trajectory equation (29.64) yields

$$\frac{d(X - X_o)}{dt} = U_o \sin(\omega t) \left[ 1 + \frac{R}{\omega} \sin(\omega t) \right] \quad (29.68a)$$

$$= U_o \sin(\omega t) + \frac{U_o R}{2\omega} [1 - \cos(2\omega t)], \quad (29.68b)$$

which integrates to

$$X - X_o = \left( \frac{U_o}{\omega} \right) \left[ 1 - \cos(\omega t) - \frac{R \sin(2\omega t)}{4\omega} + \frac{R t}{2} \right] \quad (29.69a)$$

$$= \underbrace{\left( \frac{U_o}{\omega} \right) [1 - \cos(\omega t)]}_{\text{homogeneous}} + \underbrace{\frac{U_o R t}{2\omega}}_{\text{Stokes drift}} - \underbrace{\frac{U_o R \sin(2\omega t)}{4\omega^2}}_{\text{higher harmonic}} + \mathcal{O}(R/\omega)^2. \quad (29.69b)$$

The leading order term is the homogeneous motion given by equation (29.47a). The next term is the Stokes drift, followed by a higher order harmonic and then further terms on the order of  $(R/\omega)^2$ . There is no vertical Stokes drift to this order in  $(R/\omega)$ , so that the Stokes drift velocity is given by

$$\left[ \frac{\mathbf{X} - \mathbf{X}_o}{t} \right]^{\text{drift}} = \frac{R U_o}{2\omega} \hat{\mathbf{x}}. \quad (29.70)$$

The circular motion of the parcels is therefore deformed by the zonal Stokes drift. The drift increases with larger wave amplitude ( $U_o$  large); with larger vertical shear ( $R$  large); and with longer period waves ( $\omega$  small). See Figure 29.5 for an illustration based on a particular choice for the dimensional parameters.

### 29.3.3 Comments and further study

Stokes drift occurs in many guises when studying the motion of fluid particles within wave fields. We revisit elements of Stokes drift in Chapter 47 when studying the rudiments of eddy-induced tracer transport. This video from [Prof. Andy Hogg at Australian National University](#) provides an overview of the discussion in this section along with some laboratory experiments to illustrate Stokes drift.

Is Stokes drift a nonlinear wave phenomena? In answering this question we note that Stokes

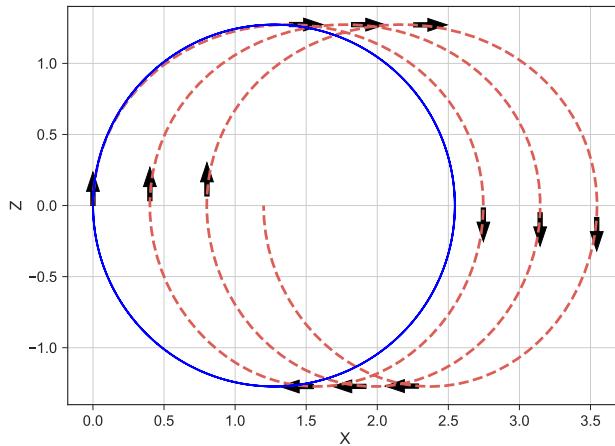


FIGURE 29.5: Example trajectories of fluid particles undergoing Stokes drift for short surface ocean waves. Particle motion is clockwise in the  $x$ - $z$  plane. For homogeneous waves, there is zero Stokes drift with circular trajectories given by equations (29.47a) and (29.47b), as depicted here by the blue trajectory. There is a Stokes drift in the presence of vertical shear in the wave amplitude and thus in the particle velocity, with the trajectories for this example given by equation (29.61) for the vertical component and equation (29.69b) for the horizontal component. We set the parameters as follows:  $T = 2\pi/\omega = 60$  s,  $U_o = 0.1$  m s $^{-1}$ , and  $R = \omega/10$  and exhibit trajectories over four minutes.

drift occurs with particle motion in linear waves, but the waves must be inhomogeneous such as the surface gravity waves studied in this chapter. However, nonlinearity appears in the form of the particle-following averaging, as can be seen by the expression of Stokes drift given by equation (29.45)

$$\dot{v}_{(S)}^n(\mathbf{x}, t) \approx \nabla v^n(\mathbf{x}, t) \cdot \overline{\int_0^t \mathbf{v}(\mathbf{x}, t') dt'}. \quad (29.71)$$

The dot product of the velocity gradient with the time integrated velocity (to give the time integrated position) is nonlinear. So although the waves are linear, the Lagrangian kinematics of particle trajectories introduces nonlinearities.



## 29.4 Exercises

### EXERCISE 29.1: STOKES DRIFT FOR ONE-DIMENSIONAL MONOCHROMATIC WAVE

Consider a one-dimensional monochromatic longitudinal wave with velocity

$$u = u_o \sin(k x - \omega t), \quad (29.72)$$

where  $u_o$  is the wave amplitude,  $k = 2\pi/\lambda$  the wave number,  $\lambda$  the wavelength,  $\omega = 2\pi/T$  the radial frequency,  $T$  the wave period, and  $c = \omega/k = \lambda/T$  the wave speed. A longitudinal wave is one whose particle motions are parallel to the wave vector, which in this exercise are both in the  $\hat{\mathbf{x}}$  direction. Determine the wave period averaged Stokes velocity to first order accuracy in the small parameter

$$\epsilon = \frac{u_o}{c} = \frac{u_o k}{\omega} = \frac{u_o T}{\lambda} \quad (29.73)$$

with this parameter the ratio of the wave amplitude to wave speed, or equivalently the ratio of the length scale of particle displacements to the wavelength. Hint: make use of the general result

given by equation (29.45).



**Part V**

**Shallow water mechanics**

Adiabatic shallow water models consist of constant density homogeneous fluid layers whose interfaces are material (i.e., no matter is transferred between the immiscible layers). Thermodynamic processes are absent from the system, thus allowing us to focus on the dynamics of fluid layers. Pressure is hydrostatic, which means that motion occurs in columns whereby horizontal velocity is independent of the vertical position within a layer, whereas the column can expand and contract so that there is vertical motion within a layer. Horizontal momentum is transferred between shallow water layers via pressure form stresses that act on sloping layer interfaces.

The shallow water system offers a suite of versatile theoretical models of use to deduce impacts on the flow from both rotation and stratification. Consequently, the shallow water model is featured in many areas of geophysical fluid mechanics as well as in ocean and atmosphere applications. In this part of the book, our goal is to develop an understanding of the shallow water model fundamentals and study some basic dynamical features as realized in the model. We have further use of the shallow water model in our study of vorticity in Part VI, balanced flows in Part VII, and generalized vertical coordinates in Part VIII.

We offer an observation concerning the mathematics required for studying the shallow water model. Namely, the shallow water model is a vertically discrete realization of a continuously stratified fluid described by the isopyncal coordinates of Chapter 44. However, the mathematical formalism of generalized vertical coordinates developed in Part VIII is largely unnecessary when working with the shallow water model. The reason for the simplification is that columnar motion within a shallow water layer means that lateral gradients of properties need not be projected along the slope of the layer. In contrast, this projection is needed for a continuously stratified fluid described by generalized vertical coordinates (e.g., see Figure 41.4). So although we appreciate the beauty and power of generalized vertical coordinate mathematics for studying continuously stratified flows, it is liberating to be able to avoid that formalism while still capturing much of the underlying physics associated with stratification (albeit discretely stratified). This feature of the shallow water model greatly adds to its allure and accessibility.

# Chapter 30

## Shallow water models

In this chapter we formulate the kinematic and dynamic equations for a suite of shallow water models. For this purpose we develop the equations describing motion of a single shallow water layer; multiple shallow water layers (stacked shallow water); and reduced gravity models (models with one layer that is dynamically inactive). In formulating these models we also expose their underlying physical basis.

### READER'S GUIDE TO THIS CHAPTER

We make use of fluid kinematics and dynamics described in earlier chapters. Our presentation was inspired by Chapter 3 of [Vallis \(2017\)](#) as well as various sections in [Salmon \(1998\)](#).

The horizontal velocity is vertically uniform within a shallow water layer, whereas the vertical velocity and hydrostatic pressure are linear functions of vertical position within the layer. When acting on a property that is vertically uniform within a layer, the gradient operator,  $\nabla$ , results in a horizontal vector. To minimize notational clutter, we typically write  $\nabla$  for brevity, rather than the more clumsy  $\nabla_k$  or  $\nabla_z$  (with  $k$  the layer index). The meaning of the resulting vector equations will be clear from the functional dependencies of the fields present in the equations.

30.1	Loose threads	708
30.2	A single shallow water layer	708
30.2.1	Pressure gradient force within the fluid layer	708
30.2.2	Further comments on pressure in a homogeneous layer	710
30.2.3	Momentum equation	711
30.2.4	Thickness equation	711
30.2.5	Bottom kinematic boundary condition	713
30.2.6	Surface kinematic boundary condition	714
30.2.7	Column stretching and vertical velocity	715
30.2.8	Tracer concentration equation	716
30.2.9	Summary comments	717
30.3	Reduced gravity model for the upper ocean	718
30.3.1	Momentum and thickness equations for the active layer	718
30.3.2	Relating undulations of the top and bottom layer interfaces	719
30.3.3	Momentum equation with reduced gravity	719
30.3.4	Heuristics for the reduced gravity	720
30.3.5	Further study	720

30.4	Stacked shallow water equations . . . . .	721
30.4.1	Formulation of a 2-layer model . . . . .	721
30.4.2	$N$ -layer model equations . . . . .	724
30.4.3	Rigid lid models . . . . .	725
30.5	Non-conservative processes and boundary stresses . . . . .	725
30.5.1	Dia-surface volume fluxes . . . . .	725
30.5.2	Frictional and boundary stresses . . . . .	726
30.6	Exercises . . . . .	727

## 30.1 Loose threads

- Internal and external mode as per Raymond's notes.

## 30.2 A single shallow water layer

Consider a homogeneous layer of fluid in a uniform effective gravitational field (gravity plus planetary centrifugal as in Section 9.12.4), contained on its side by solid boundaries. If there are no lateral force imbalances, then the fluid remains static. Now perturb the fluid so that it has a nonuniform layer thickness, say with a bump in a particular region. Conservation of fluid mass (which translates into volume conservation for a uniform density layer) means that thicker fluid regions must be exactly compensated by thinner fluid regions. Furthermore, layer thickness gradients create pressure differences (thicker water has larger hydrostatic pressure than thinner water), which in turn drives fluid motion. If the fluid has much larger lateral extent than vertical, then the lateral motion occurs as an expanding and contracting column with no depth dependence to the horizontal pressure forces and thus the horizontal motion is depth independent.

The essence of a perfect fluid (i.e., no irreversible processes such as mixing) shallow water flow concerns the motion of fluid columns accelerated by pressure gradients created by layer thickness undulations, and the associated conservation of mass ensuring that the accumulation of fluid in one region is balanced by the depletion of fluid in another. Pressure gradients act to homogenize the layer thickness. However, rotation allows for layer thickness to be non-constant even in a steady state.

### 30.2.1 Pressure gradient force within the fluid layer

Figure 30.1 shows a single shallow water layer with a generally non-flat bottom and an undulating free surface height. We assume that each column of fluid within the layer is in hydrostatic balance, so that the vertical momentum equation reduces to

$$\frac{\partial p}{\partial z} = -\rho g. \quad (30.1)$$

Recall from Section 22.2 that the hydrostatic balance is consistent with lateral length scales much larger than vertical (small vertical to horizontal aspect ratio), which is satisfied by large-scale geophysical fluid motion. Hence, a shallow water fluid is a relevant idealization if we are considering large horizontal scales relative to the vertical.

Since the fluid density is assumed constant (i.e., the fluid is a homogeneous layer), we can integrate the hydrostatic balance from the surface to an arbitrary vertical position within the layer

$$p(x, y, z, t) = p_a(x, y, t) + g \rho \int_z^\eta dz = p_a(x, y, t) + g \rho [\eta(x, y, t) - z], \quad (30.2)$$

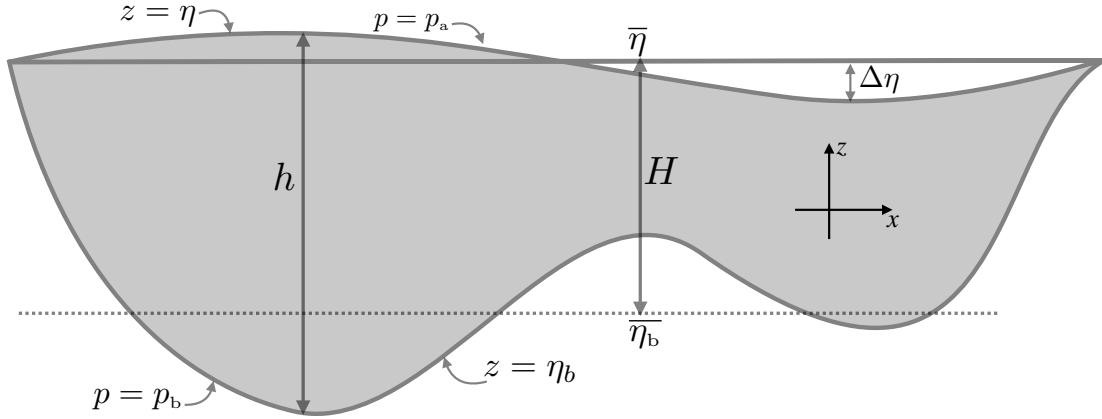


FIGURE 30.1: A single layer of shallow water fluid with thickness  $h = \eta - \eta_b$  that extends from the bottom at  $z = \eta_b$  to the free surface at  $z = \eta$ . The area averaged thickness is defined by  $H = \bar{h} = A^{-1} \int h \, dx \, dy = A^{-1} \int (\eta - \eta_b) \, dx \, dy = \bar{\eta} - \bar{\eta}_b$ , where  $A = \int dx \, dy$  is the horizontal area of the layer. The deviation of the free surface from  $\bar{\eta}$  is given by  $\Delta\eta = \eta - \bar{\eta} = \eta - (\bar{\eta}_b + H)$  so that  $\eta(x, y, t) = \eta_b(x, y) + h(x, y, t) = \bar{\eta}_b + H + \Delta\eta(x, y, t)$ . Likewise, the deviation of the bottom from  $\bar{\eta}_b$  is given by  $\Delta\eta_b = \eta_b - \bar{\eta}_b$ , so that  $h = \eta - \eta_b = H + \Delta\eta - \Delta\eta_b$ . Volume conservation for the layer is maintained in the absence of volume boundary fluxes, in which case  $\bar{\Delta}\eta = 0$ . Note that the position of the reference height,  $z = 0$ , is arbitrary. Atmospheric conventions typically choose  $z = 0$  so that  $\bar{\eta}_b = 0$ ,  $\eta = H + \Delta\eta$ , and  $\bar{\eta} = H$ . Oceanic conventions typically choose  $\bar{\eta} = 0$  so that  $\eta = \Delta\eta$  and  $\bar{\eta}_b = -H$ . We are only concerned with fluctuations that leave the free surface monotonic; i.e., we do not consider overturns or breaking waves. This assumption is implied by assuming that each column extending from  $\eta_b \leq z \leq \eta$  maintains hydrostatic balance. We refer to this figure countless times in this book when discussing shallow water mechanics.

where  $p_a(x, y, t)$  is the pressure applied to the layer free surface, say from the overlying atmosphere. Furthermore, the horizontal pressure gradient thus takes the form

$$\nabla_z p = \nabla_z p_a + g \rho \nabla_z \eta. \quad (30.3)$$

Since  $p_a$  and  $\eta$  are independent of  $z$ , there is no need to expose the  $z$  subscript on the gradient operator on the right hand side. We thus drop the subscript when no ambiguity results, as per our convention noted at the start of the chapter.

### *Effective sea level and inverse barometer responses*

It is common to ignore the applied surface pressure,  $p_a$ , by assuming the fluid above the layer either has zero horizontal variations in pressure, or, more commonly, by assuming the fluid has zero inertia (i.e., zero mass). This assumption must be relaxed if studying the effects of atmospheric pressure variations acting on a single layer ocean. For generality, we sometimes find it useful to introduce an *effective free surface height*

$$\eta^{\text{eff}} = \eta + p_a / (\rho g). \quad (30.4)$$

When the applied pressure is anomalously positive, the free surface is generally depressed under the added weight. A perfect compensation occurs when the free surface exhibits an *inverse barometer response*, whereby the effective sea level remains unchanged. Appendix C to [Griffies and Greatbatch \(2012\)](#) offer a discussion of the inverse barometer response of the ocean to atmospheric loading as well as sea ice loading.

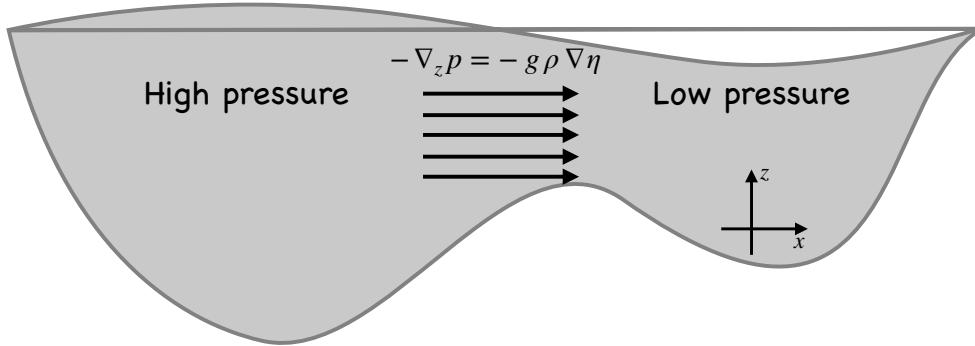


FIGURE 30.2: When there are zero horizontal gradients in the applied surface pressure,  $\nabla p_a = 0$ , the horizontal acceleration from pressure within a single shallow water fluid layer is determined solely by the surface height,  $-\nabla_z p = -g \nabla \eta$ . The acceleration is uniform throughout the layer and points from sea level highs towards sea level lows. Although bottom topography interacts with the flow and thus affects the shape of the free surface, the topography does not appear explicitly in the horizontal pressure gradient. Instead, we only need to know the shape of the free surface (and the applied pressure  $p_a$ ) to know the horizontal pressure force throughout the layer.

### *Layer depth independent pressure gradient force*

We emphasize that although hydrostatic pressure within a shallow water layer is depth dependent as per equation (30.2), the horizontal pressure gradient, as given by equation (30.3), has no depth dependence within the layer. The acceleration from this hydrostatic pressure force points from highs in the effective sea level to lows in the effective sea level (see Figure 30.2).

It is notable that the pressure gradient is solely determined by properties at the upper interface of the layer. That is, we only need to know the shape of the free surface,  $z = \eta$ , and the applied pressure,  $p_a$ , to know the horizontal pressure force acting throughout the layer. But what about the bottom topography? Experience indicates that topography affects the shape of the free surface and thus modifies the pressure field, yet topography does not explicitly appear in the mathematical expression for the horizontal pressure gradient. This characteristic is specific to the use of a pressure gradient body force to describe the role of pressure on the layer momentum. As a complement, we saw in Chapter 19 how to formulate the pressure contact force. It is through the contact force perspective that we see, in Section 31.5, how bottom topography appears in the momentum balance of a shallow water layer. In particular, this perspective exposes the topographic form stresses that mechanically exchange momentum between the layer and the solid earth bottom.

### 30.2.2 Further comments on pressure in a homogeneous layer

The depth independence of the horizontal pressure gradient within the shallow water layer is a direct result of the assumed hydrostatic nature of the pressure within the layer. To emphasize this point, we certainly can imagine a homogeneous fluid layer in which the horizontal velocity has a vertical shear. For example, in Section 29.1 we study surface gravity waves in a homogeneous fluid layer. Such waves have an amplitude that exponentially decays with depth, and so the horizontal and vertical fluid motion associated with the waves have a non-zero vertical shear. Such motion clearly cannot be caused by a hydrostatic pressure gradient since it has no vertical dependence throughout the layer, in which case

$$\partial_z(\nabla_z p_{\text{hydrostatic}}) = 0. \quad (30.5)$$

Hence, in a homogeneous fluid layer, hydrostatic pressure gradients can only drive a horizontal flow that is depth independent within that layer. So if the vertically sheared horizontal flow is found within a homogeneous fluid layer, and if pressure gradients cause this flow, then it can only be through gradients in the *non-hydrostatic pressure*. As discussed in Section 29.1.3, surface gravity waves indeed involve non-hydrostatic pressure forces that drive the vertical dependence to the wave amplitude.

Moving beyond the homogeneous layer assumption, we saw in Section 22.2.6 that a horizontal gradient in the density leads to a vertically dependent hydrostatic pressure gradient  $\partial_z(\nabla_z p_{\text{hydrostatic}}) \neq 0$ . This hydrostatic pressure force can impart vertical shears to the horizontal flow. Thermal wind shear is the canonical example whereby vertical shears in the horizontal velocity are present in geostrophically balanced fluids as driven by horizontal density gradients (Section 25.4.4).

### 30.2.3 Momentum equation

If there is no friction anywhere in the fluid, including at the upper and lower boundaries, then the horizontal momentum is effected only by the Coriolis and pressure forces. Following our discussion of the Traditional Approximation in Section 22.1.3, we retain only the local vertical component to the Coriolis acceleration, which is compatible with the hydrostatic approximation. We are thus led to the horizontal velocity equation

$$\frac{D\mathbf{u}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla(g\eta + p_a/\rho), \quad (30.6)$$

where

$$\mathbf{v} = (\mathbf{u}, w) \quad (30.7)$$

splits out the horizontal velocity vector,  $\mathbf{u}$ , from the vertical velocity component,  $w$ .

The Coriolis parameter,  $f = f \hat{\mathbf{z}}$ , is independent of depth, as is the horizontal pressure force from gradients in the free surface and applied pressure. Consequently, if the horizontal velocity is initially independent of depth, it will remain so for all time. The material time derivative thus only has contributions from the local time derivative and from horizontal advection

$$\frac{D\mathbf{u}}{Dt} = \left[ \frac{\partial}{\partial t} + u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} \right] \mathbf{u} \quad (30.8)$$

so that the shallow water momentum equation (30.6) takes on the form

$$\left[ \frac{\partial}{\partial t} + u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} + f \hat{\mathbf{z}} \times \right] \mathbf{u} = -\nabla(g\nabla\eta + p_a/\rho). \quad (30.9)$$

### 30.2.4 Thickness equation

The mass of a shallow water layer is constant in the absence of sources, sinks, or boundary fluxes. Hence, changes in mass at a particular region in the fluid must arise from mass fluxed across the region boundaries, leaving one region and accumulating in another. For simplicity, we assume that no mass crosses the fluid top (the free surface) or the bottom (the solid earth). We consider the more general case of boundary mass transport in Section 30.5. Note that since the fluid density is constant, mass conservation is the same as volume conservation. Hence, the terms “mass conservation” and “volume conservation” are commonly used interchangeably when working with shallow water models.

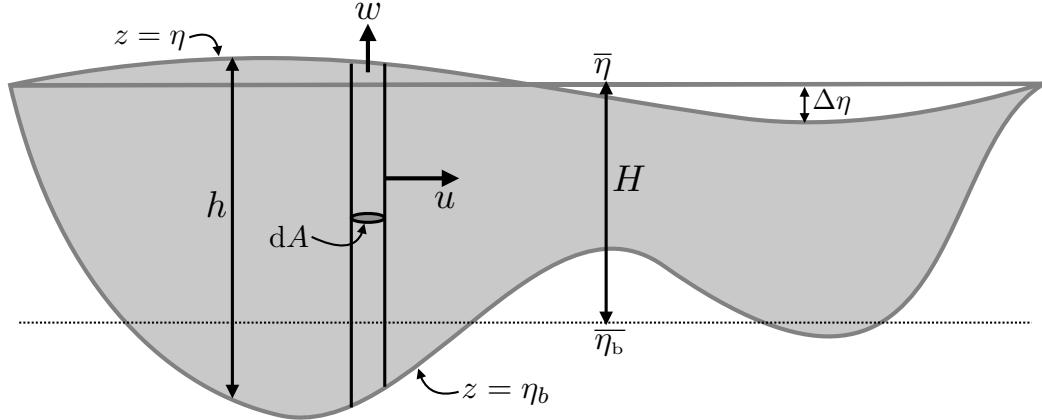


FIGURE 30.3: Mass budget for a column of shallow water fluid with fixed cross-sectional area,  $dA$ , constant density,  $\rho$ , and thickness,  $h$ . The column mass is affected only by horizontal transport (transport within the layer) in the absence of boundary mass fluxes through the top,  $z = \eta$ , or bottom,  $z = \eta_b$ . Note that since the density of the layer is constant, then mass equals to the constant density times the volume.

Consider an infinitesimally thin (in horizontal cross-section) vertical column of shallow water fluid that is fixed in space and extending from  $\eta_b \leq z \leq \eta$ . Let the horizontal cross-sectional area be written as  $dA$  and the thickness be  $h = \eta - \eta_b$  (see Figure 30.3). The total mass of fluid in this column is given by

$$M = \int_{\text{column}} \left[ \int_{\eta_b}^{\eta} \rho dz \right] dA = \rho \int_{\text{column}} (\eta - \eta_b) dA = \rho \int_{\text{column}} h dA. \quad (30.10)$$

Time changes in the column mass thus arise from time changes in the layer thickness integrated over the horizontal area of the column

$$\frac{dM}{dt} = \rho \int_{\text{column}} \frac{\partial h}{\partial t} dA, \quad (30.11)$$

where

$$\frac{\partial h}{\partial t} = \frac{\partial (\eta - \eta_b)}{\partial t} = \frac{\partial \eta}{\partial t}, \quad (30.12)$$

since the bottom topography at  $z = \eta_b(x, y)$  is static.

### General derivation

The mass within a fluid column changes due to mass crossing the vertical column boundaries (again, we assume here that no mass crosses the top or bottom interfaces). The mass flux penetrating the vertical boundary is given by

$$\text{mass per time entering column} = -\rho \oint_{\text{column}} \mathbf{u} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (30.13)$$

where  $\hat{\mathbf{n}}$  is the outward normal at the column boundary, and  $d\mathcal{S}$  is the area element along the column boundary. The area integral is computed over the boundary of the column, which involves a vertical integral and a circumferential line integral

$$\text{mass per time entering column} = -\rho \oint_{\text{column}} \left[ \int \mathbf{u} \cdot \hat{\mathbf{n}} dz \right] dl, \quad (30.14)$$

where  $dl$  is the infinitesimal line element around the column circumference. Since  $\hat{\mathbf{n}} \cdot \mathbf{u}$  is depth independent, we can perform the vertical integral to render

$$-\rho \oint_{\text{column}} \left[ \int \mathbf{u} \cdot \hat{\mathbf{n}} dz \right] dl = -\rho \oint_{\text{column}} h \mathbf{u} \cdot \hat{\mathbf{n}} dl = -\rho \int_{\text{column}} \nabla \cdot (h \mathbf{u}) dA, \quad (30.15)$$

where the second equality follows from the divergence theorem applied to the horizontal cross-sectional area of the column. Equating this result to the mass time tendency (30.11), and noting that the horizontal cross-sectional area is arbitrary, yields an equation for the layer thickness

$$\frac{\partial h}{\partial t} + \nabla \cdot (h \mathbf{u}) = 0. \quad (30.16)$$

This result means that the thickness of fluid at a fixed location increases if there is a convergence of thickness onto that location, and decreases if thickness diverges from the location. We may also write the thickness equation (30.16) in the material time derivative form

$$\frac{Dh}{Dt} = -h \nabla \cdot \mathbf{u}. \quad (30.17)$$

Hence, thickness of a material fluid column increases in regions where the horizontal flow converges.

#### *Special case with a rectangular column*

To further our understanding of the second step in equation (30.15), consider the special case of a rectangular column, for which the mass per time of fluid entering the column is given by

mass per time entering column

$$= -\rho \int_{\text{column}} [(u h)_{\text{east}} - (u h)_{\text{west}}] dy - \rho \int_{\text{column}} [(v h)_{\text{north}} - (v h)_{\text{south}}] dx. \quad (30.18)$$

Taking the limit as the horizontal cross-section of the column becomes infinitesimal leads to

mass per time entering column

$$= -\rho \int_{\text{column}} \left[ \frac{\partial(u h)}{\partial x} + \frac{\partial(v h)}{\partial y} \right] dx dy = -\rho \int_{\text{column}} \nabla \cdot (h \mathbf{u}) dA, \quad (30.19)$$

thus recovering the result (30.15).

### 30.2.5 Bottom kinematic boundary condition

Kinematic boundary conditions arise from geometric constraints placed on the fluid system. We consider here the kinematic boundary condition at the bottom interface in the case where there is no flow through this interface, and follow up in Section 30.2.6 with the surface kinematic boundary condition.<sup>1</sup>

---

<sup>1</sup>From the discussion of fluid kinematics in Part III, we use the term *material surface* for any continuous surface or interface that is impenetrable to the flow of matter or thermal energy (mechanical energy can be transferred via pressure forces). In Section 14.4 we derived the kinematic boundary conditions for a fluid at interfaces. We here apply those ideas to the shallow water system, so that the presentation in Sections 30.2.5 and 30.2.6 offer a review of Section 14.4 as applied to a shallow water layer.

The ocean bottom is located at a vertical position,  $z = \eta_b(x, y)$ . This location can equivalently be specified mathematically by the surface

$$s(x, y, z) = z - \eta_b(x, y) = 0. \quad (30.20)$$

The outward normal (pointing from the fluid into the rock) at this surface is given by

$$\hat{\mathbf{n}} = -\frac{\nabla s}{|\nabla s|} = \frac{\nabla \eta_b - \hat{\mathbf{z}}}{\sqrt{1 + \nabla \eta_b \cdot \nabla \eta_b}}. \quad (30.21)$$

If the bottom is impenetrable to fluid then the velocity field is constrained to satisfy the no-normal flow boundary condition

$$\mathbf{v} \cdot \hat{\mathbf{n}} = 0 \quad \text{at } z = \eta_b. \quad (30.22)$$

Making use of the bottom outward normal (30.21) leads to

$$w = \mathbf{u} \cdot \nabla \eta_b \quad \text{at } z = \eta_b. \quad (30.23)$$

For a flat bottom, with  $\nabla \eta_b = 0$ , the no-normal flow condition means that  $w(\eta_b) = 0$ . For the case of nontrivial bottom topography,  $w(\eta_b) = 0$  remains if flow occurs along lines of constant topography; i.e., along isobaths, in which case  $\mathbf{u} \cdot \nabla \eta_b = 0$ . But more generally, sloping bottoms lead to a nonzero vertical velocity component. Dynamically, a nonzero bottom vertical velocity arises from forces at the bottom that cause the horizontal velocity to cross isobaths,  $\mathbf{u} \cdot \nabla \eta_b \neq 0$ .

The kinematic result (30.23) is written in an Eulerian sense, with the velocity constrained to satisfy this relation at each point along the bottom interface. It has a dual material interpretation based on acknowledging that the bottom interface is a material surface. A fluid element on the bottom at  $s = z - \eta_b = 0$  will thus remain there; it does not cross the bottom interface. Rather, it can at most move tangentially to the bottom.<sup>2</sup> We can ensure the no-normal flow constraint by setting

$$\frac{Ds}{Dt} = \frac{D(z - \eta_b)}{Dt} = 0 \quad \text{at } z = \eta_b. \quad (30.24)$$

Rearrangement of this result leads to the Eulerian constraint (30.23). Equivalently, we can write this boundary condition in the form

$$w = \frac{D\eta_b}{Dt} \quad \text{at } z = \eta_b. \quad (30.25)$$

Since  $\eta_b = \eta_b(x, y)$ , this expression of the kinematic boundary condition is identical to equation (30.23).

### 30.2.6 Surface kinematic boundary condition

We here assume the surface boundary is a material surface to derive the surface kinematic boundary condition, with Section 30.5 considering the slightly more general case of volume crossing this surface. As a material surface, the surface kinematic boundary condition follows analogously to the bottom. However, there is a fundamentally new feature in that the layer's upper free surface is a time dependent moving boundary. We studied such boundaries in Section 14.4.2 when detailing the kinematic boundary conditions for a material surface. We here review some of that discussion.

---

<sup>2</sup>Details of the tangential motion along a material boundary require dynamical information such as boundary stresses (see Chapter 18). We are not concerned with such dynamical information here, rather our concern is solely with kinematics.

The free surface is located at a vertical position  $z = \eta(x, y, t)$ . Equivalently, the free surface can be specified by a surface of constant  $s$ , where

$$s(x, y, z, t) = z - \eta(x, y, t) = 0. \quad (30.26)$$

The outward normal to the free surface is thus given by

$$\hat{\mathbf{n}} = \frac{\nabla s}{|\nabla s|} = \frac{\hat{z} - \nabla \eta}{\sqrt{1 + \nabla \eta \cdot \nabla \eta}}. \quad (30.27)$$

We must account for motion of the surface when formulating the no-normal flow condition. To do so, write this no-normal flow condition as

$$(\mathbf{v} - \mathbf{v}^{(s)}) \cdot \hat{\mathbf{n}} = 0 \quad \text{at } z = \eta(x, y, t), \quad (30.28)$$

where  $\mathbf{v}^{(s)}$  is the velocity of a point on the ocean surface. The velocity of a point fixed on an arbitrary surface with specified  $s$  satisfies

$$\frac{\partial s}{\partial t} + \mathbf{v}^{(s)} \cdot \nabla s = 0. \quad (30.29)$$

As defined,  $\mathbf{v}^{(s)}$  advects a fluid element in a manner to always keep the element fixed on the constant  $s$  surface. With  $\hat{\mathbf{n}} = \nabla s / |\nabla s|$ , we have

$$\mathbf{v}^{(s)} \cdot \hat{\mathbf{n}} = -\frac{\partial_t s}{|\nabla s|} = \frac{\partial_t \eta}{\sqrt{1 + \nabla \eta \cdot \nabla \eta}}. \quad (30.30)$$

Hence, if the surface remains static, then  $\mathbf{v}^{(s)} \cdot \hat{\mathbf{n}} = 0$ . But more generally, the surface is moving, and that movement is fundamental to the surface kinematic boundary condition.

Making use of the result (30.30) in the no-normal flow constraint (30.28) then leads to the surface kinematic boundary condition

$$w - \mathbf{u} \cdot \nabla \eta = \frac{\partial \eta}{\partial t} \quad \text{at } z = \eta. \quad (30.31)$$

As for the bottom kinematic boundary condition written as (30.24), we can interpret the surface kinematic condition (30.31) materially, in which case

$$\frac{Ds}{Dt} = \frac{D(z - \eta)}{Dt} = 0 \quad \text{at } z = \eta. \quad (30.32)$$

That is, in the absence of flow across the surface boundary, that surface remains material. We can write this boundary condition in the equivalent form

$$w = \frac{D\eta}{Dt} = \frac{D\Delta\eta}{Dt} \quad \text{at } z = \eta. \quad (30.33)$$

### 30.2.7 Column stretching and vertical velocity

Since the fluid has constant density, we know that the velocity has zero divergence

$$\nabla \cdot \mathbf{u} + \partial_z w = 0 \implies \partial_z w = -\nabla \cdot \mathbf{u}. \quad (30.34)$$

This result also follows since material fluid elements in the constant density shallow water layer maintain a constant volume (see Section 16.1). Furthermore, since the horizontal velocity has no depth dependence, we can vertically integrate the continuity equation from the bottom to an arbitrary depth within the layer to render

$$w(z) = w(\eta_b) - (z - \eta_b) \nabla \cdot \mathbf{u}, \quad (30.35)$$

so that the vertical velocity is a linear function of depth. Applying this equation at the ocean surface yields

$$w(\eta) = w(\eta_b) - (\eta - \eta_b) \nabla \cdot \mathbf{u}. \quad (30.36)$$

Eliminating the horizontal convergence between equations (30.35) and (30.36) leads to

$$w(z) - w(\eta_b) = \left[ \frac{z - \eta_b}{\eta - \eta_b} \right] [w(\eta) - w(\eta_b)]. \quad (30.37)$$

Making use of the surface kinematic boundary condition (30.33) and bottom kinematic boundary condition (30.25) renders the material form

$$\frac{1}{z - \eta_b} \left[ \frac{D(z - \eta_b)}{Dt} \right] = \frac{1}{\eta - \eta_b} \left[ \frac{D(\eta - \eta_b)}{Dt} \right]. \quad (30.38)$$

Finally, introducing the layer thickness  $h = \eta - \eta_b$  yields the material conservation law

$$\frac{D}{Dt} \left[ \frac{z - \eta_b}{h} \right] = 0. \quad (30.39)$$

Again,  $h = \eta - \eta_b$  is the layer thickness and  $z - \eta_b$  is the height of a fluid element from the bottom interface (see Figure 30.1). Consequently, equation (30.39) means that the ratio of the fluid element height above the bottom to the layer thickness remains constant as the fluid element moves through the shallow water fluid. That is, a column of shallow water fluid stretches or squeezes uniformly within a shallow water layer. Shallow water mechanics thus comprises the mechanics of coherent vertical fluid columns moving within a fluid layer. This constrained behavior results from the linear depth dependence of the vertical velocity, which itself is a result of the depth independence of the horizontal velocity, and which follows from the depth independence of the horizontal gradient of hydrostatic pressure.

### 30.2.8 Tracer concentration equation

Suppose there is a material substance, a tracer, contained within a shallow water layer.<sup>3</sup> We expect the tracer concentration,  $\psi$ , to have a non-uniform vertical structure within the layer, in addition to having horizontal structure:  $\psi = \psi(x, y, z, t)$ . If the tracer is advected through the layer without any diffusion, then the concentration satisfies the perfect fluid tracer equation (i.e., the *advection equation*)

$$\frac{\partial \psi}{\partial t} + \mathbf{u} \cdot \nabla_z \psi + w \partial_z \psi = 0. \quad (30.40)$$

For a shallow water layer, where the horizontal velocity has no depth dependence within a layer, we find it sufficient to study the depth averaged tracer concentration within the layer,

$$C(x, y, t) \equiv \frac{1}{h} \int_{\eta_b}^{\eta} \psi(x, y, z, t) dz. \quad (30.41)$$

---

<sup>3</sup>We developed the theory of material tracers in Chapter 15.

To develop the evolution equation for  $C$ , we vertically integrate the tracer equation (30.40) over the layer and make use of Leibniz's rule (Section 15.3.4)

$$\int_{\eta_b}^{\eta} \frac{\partial \psi}{\partial t} dz = \partial_t(h C) - \psi(\eta) \partial_t \eta \quad (30.42a)$$

$$\int_{\eta_b}^{\eta} \mathbf{u} \cdot \nabla \psi dz = \nabla \cdot (h C \mathbf{u}) - \psi(\eta) \mathbf{u}(\eta) \cdot \nabla \eta + \psi(\eta_b) \mathbf{u}(\eta_b) \cdot \nabla \eta_b - h C \nabla \cdot \mathbf{u} \quad (30.42b)$$

$$\int_{\eta_b}^{\eta} \psi \partial_z w dz = w(\eta) \psi(\eta) - w(\eta_b) \psi(\eta_b) - h C \partial_z w. \quad (30.42c)$$

Use of the kinematic boundary conditions from Sections 30.2.5 and 30.2.6, and the three dimensional continuity equation,  $\nabla \cdot \mathbf{u} + \partial_z w = 0$ , renders the equation for the layer depth averaged tracer concentration

$$\frac{\partial(h C)}{\partial t} + \nabla \cdot (h C \mathbf{u}) = 0 \iff \frac{\partial C}{\partial t} + \mathbf{u} \cdot \nabla C = \frac{DC}{Dt} = 0. \quad (30.43)$$

As a self-consistency check, note that if the tracer concentration has a horizontally uniform value, then the Eulerian flux-form of the tracer equation (30.43) reduces to the thickness equation (30.16).

### 30.2.9 Summary comments

#### *Key physical assumptions for the shallow water fluid*

The shallow water fluid model is based on the following two assumptions.

- The fluid layer has a uniform density, which then means the fluid is incompressible.
- The pressure is hydrostatic.

Since the pressure gradient is depth-independent within the layer, an initial horizontal velocity that is depth independent will remain depth independent. That is, the fluid moves as columns within the layer, with the columns stretching and squashing depending on the divergence or convergence of column towards the column.

The term “shallow” refers to the small vertical to horizontal aspect ratio,  $H/L \ll 1$ , which in turn is consistent with the hydrostatic approximation (Section 22.2). The term “water” refers to the incompressible nature of the fluid, which is a more relevant approximation for the ocean than for the atmosphere (see Section 23.1). Nonetheless, the shallow water model has direct applications to many features of both the atmosphere and ocean circulation, and as such it is widely used across the atmosphere and ocean sciences.

#### *Shallow water fluid columns are not Taylor columns*

The columnar motion of fluid within a shallow water layer is reminiscent of the Taylor columns discussed in Section 25.5.3. However, the columnar motion of fluid within a Taylor column is fundamentally distinct from that of a column of shallow water fluid. Motion in a Taylor column holds for homogeneous fluids undergoing rapid rotation and moving over a flat surface. The horizontal fluid velocity within a Taylor column is non-divergent so that there is no vertical motion of the fluid. These properties allow one to interpret a Taylor column as a fluid mechanical realization of a column of rigid matter much like a solid body.

In contrast, shallow water fluid columns do not rely on rotation, but instead arise from the hydrostatic balance maintained within each homogeneous layer. Additionally, shallow water columns

are not rigid. Rather, they stretch and squash in the presence of nonzero divergence in the horizontal flow, thus leading to vertical motion of fluid within the column. Finally, shallow water columns remain coherent even as they move over topography, and yet, again, they can stretch and squash.

### 30.3 Reduced gravity model for the upper ocean

The *reduced gravity model* describes an active layer of uniform density,  $\rho_1$ , above a stagnant layer of density,  $\rho_2$ , and below a fluid of zero density,  $\rho_0 = 0$ . It is often referred to as the 1.5 layer model. This theoretical model has been used, to some success, as an idealization of the upper ocean circulation whereby an active layer (e.g., the region above the ocean pycnocline), sits above an inactive layer (the abyss) of zero motion. In this way, we introduce the *level of no motion*, below which (baroclinic) currents vanish.

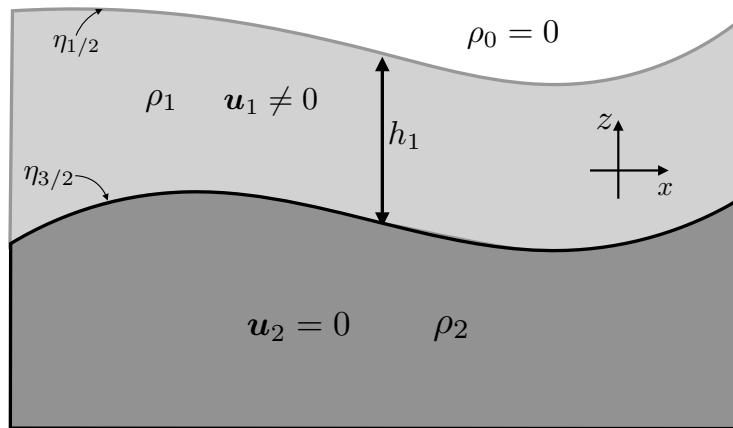


FIGURE 30.4: Reduced gravity model of shallow water fluid. The lower layer with density  $\rho_2$  is dynamically inactive and thus has a zero velocity. The upper layer is dynamically active with thickness  $h = \eta_{1/2} - \eta_{3/2}$  and density  $\rho_1$ . The dynamically active layer is bounded above by a zero density layer,  $\rho_0 = 0$ . The lower inactive layer is assumed to be infinitely deep so that its continuity equation can be ignored; i.e., even though there are zero currents within this layer it can still undulate.

#### 30.3.1 Momentum and thickness equations for the active layer

We develop the momentum equations for the reduced gravity model by making use of the hydrostatic balance, in which pressure at a depth,  $z$ , in the upper layer is computed as (see Figure 30.4)

$$p_1(x, y, z, t) = p_{1/2}(x, y, t) + g \rho_1 [\eta_{1/2}(x, y, t) - z], \quad (30.44)$$

where we denote an interface value by a half-index, so that  $\eta_{1/2}$  and  $p_{1/2}$  are the interface height and pressure at the upper layer interface.<sup>4</sup> Since the fluid above the upper layer is assumed to have zero density, we set

$$p_{1/2} = 0. \quad (30.45)$$

<sup>4</sup>There is no general consensus on this notation, with some treatments, such as [Vallis \(2017\)](#) and [Cushman-Roisin and Beckers \(2011\)](#) using an integer to label an interface quantity, whereas some numerical model papers (e.g., [Griffies et al. \(2020\)](#)) use the half-index. We prefer the half-index since it removes any ambiguity concerning the ordering of the interfaces relative to the layer.

We immediately see that the horizontal momentum equation for the upper (active) layer is written

$$\frac{D\mathbf{u}_1}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u}_1 = -g \nabla \eta_{1/2}. \quad (30.46)$$

The equations for the upper layer are completed by volume conservation in the form of the thickness equation

$$\frac{Dh_1}{Dt} = -h_1 \nabla \cdot \mathbf{u}_1. \quad (30.47)$$

### 30.3.2 Relating undulations of the top and bottom layer interfaces

The pressure in the lower stagnant layer is given by the weight per horizontal area of fluid above it

$$p_2(x, y, z, t) = g \rho_1 (\eta_{1/2} - \eta_{3/2}) + g \rho_2 (\eta_{3/2} - z). \quad (30.48)$$

However, for the reduced gravity model we assume the lower layer is motionless. To maintain zero motion in the lower layer requires the horizontal pressure gradient in this layer to vanish

$$\nabla_z p_2 = g \rho_1 \nabla(\eta_{1/2} - \eta_{3/2}) + g \rho_2 \nabla \eta_{3/2} = 0. \quad (30.49)$$

This relation provides a constraint that links undulations of the top and bottom interfaces of the dynamically active layer

$$\nabla \eta_{1/2} = - \left[ \frac{\rho_2 - \rho_1}{\rho_1} \right] \nabla \eta_{3/2} \implies \eta_{1/2} = -\eta_{3/2} \left[ \frac{\rho_2 - \rho_1}{\rho_1} \right] + \text{constant}. \quad (30.50)$$

The density ratio,  $(\rho_2 - \rho_1)/\rho_1$ , is positive but typically much smaller than unity. Hence, the relation (30.50) means that undulations of the free surface,  $\eta_{1/2}$ , are of opposite sign and of much smaller amplitude than undulations in the lower interface,  $\eta_{3/2}$ . This behavior is typical for undulations of the pycnocline region of the ocean and the free surface as depicted in Figure 30.5.

### 30.3.3 Momentum equation with reduced gravity

Relation (30.50) can be used to write the momentum equation (30.46) in the form

$$\frac{D\mathbf{u}_1}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u}_1 = +g_{3/2}^r \nabla \eta_{3/2}, \quad (30.51)$$

where

$$g_{3/2}^r = g \left[ \frac{\rho_2 - \rho_1}{\rho_1} \right] \ll g \quad (30.52)$$

defines the *reduced gravity* between layer-1 and layer-2. We use the half-integer notation for the reduced gravity since it multiplies the gradient of the interface height,  $\eta_{3/2}$ . It is common to make use of the momentum equation in the form (30.51), rather than the original form (30.46). The reason is that historically, ocean hydrography measurements<sup>5</sup> have allowed for an estimate of the pycnocline slope,  $\nabla \eta_{3/2}$ , whereas it was not until precise satellite altimetry measurements starting in the 1990s that we could estimate the far smaller sea level slope,  $\nabla \eta_{1/2}$ .

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<sup>5</sup>In oceanography, hydrography refers to measurements of temperature, salinity, and pressure; see [Talley et al. \(2011\)](#).

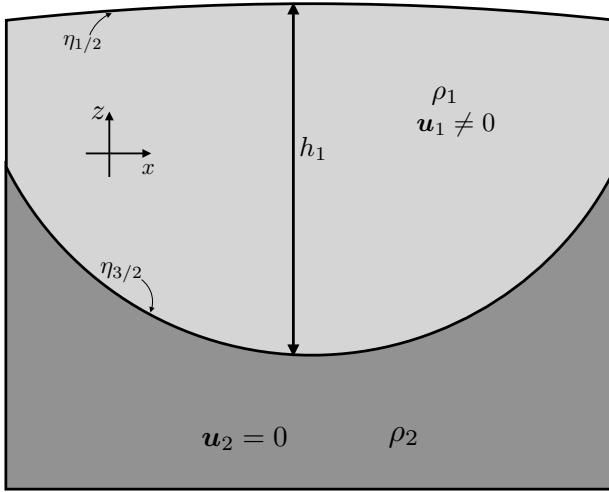


FIGURE 30.5: A vertical slice through a reduced gravity, or 1.5 layer, ocean in hydrostatic balance. Shown here is a plug of dynamically active light water, as may occur in a warm core eddy to the subtropical gyres, sitting on top of heavy water of zero motion. The free surface corresponds to  $\eta_{1/2}$  in Figure 30.4, whereas the pycnocline (heavy black line) corresponds to the lower interface  $\eta_{3/2}$  of Figure 30.4. The sea surface experiences an applied pressure  $p = p_a$ , assumed to be uniform for this idealized situation. Note how sea level is a maximum above the pycnocline minimum, with this geometry reflected in equation (30.50). In the ocean, the slope of the pycnocline is about 100-300 times larger than the slope of the sea level. That is, sea level may show undulations on the order of a metre, whereas the pycnocline undulations are on the order of 100-300 m.

### 30.3.4 Heuristics for the reduced gravity

We here offer some words about the reduced gravity aiming to support further understanding of Figure 30.5. For that purpose, return to relation (30.50), take the spatial gradient and multiply by the gravitational acceleration to yield

$$g \nabla \eta_{1/2} = -g_{3/2}^r \nabla \eta_{3/2}. \quad (30.53)$$

As noted above, since  $g_{3/2}^r \ll g$ , the free surface slopes are much smaller than interior slopes:  $|\nabla \eta_{1/2}| \ll |\nabla \eta_{3/2}|$ . We can understand the large slope differences by recognizing that the gravitational acceleration in the interior is partially compensated by buoyancy forces (Chapter 24). Hence, the interior interface is afforded less resistance to undulations. In contrast, the upper interface,  $\eta_{1/2}$ , directly contacts the atmosphere so that the corresponding reduced gravity felt by the upper interface is much larger. In fact, for the present discussion the upper interface's reduced gravity equals to  $g$  since we assume the atmosphere has zero mass. Even with a massive atmosphere, the upper interface's reduced gravity is close to  $g$  since the atmosphere is roughly 1000 times less dense than seawater. With a larger reduced gravity, the upper interface experiences more resistance to motion than the interior interface so that its slope has a much smaller magnitude.

### 30.3.5 Further study

The material in this section is a summary of that in Section 3.2 of [Vallis \(2017\)](#). [Tomczak and Godfrey \(1994\)](#) make use of the reduced gravity model for interpreting aspects of the observed ocean. Additional use is made by [Griffies et al. \(2014\)](#) for interpreting patterns of sea level in the ocean.

## 30.4 Stacked shallow water equations

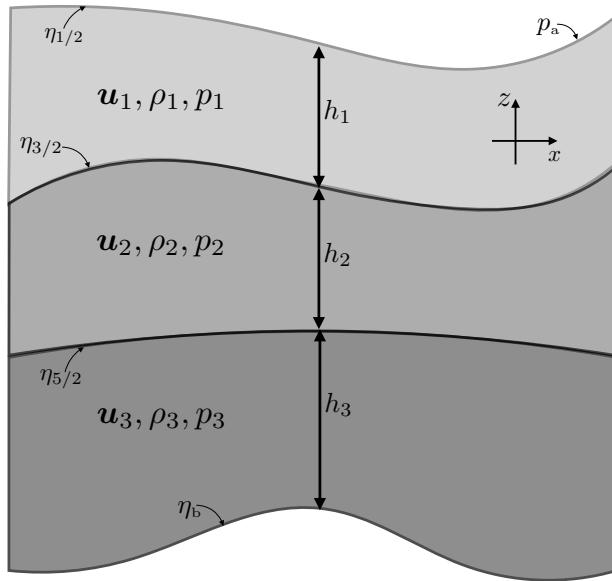


FIGURE 30.6: Three dynamically active layers of stacked shallow water fluid. The notation corresponds to that for the reduced gravity model of Figure 30.4, yet here with three dynamically active layers. The “atmosphere” above the layers is assumed to apply a pressure,  $p_a$ , to the upper surface, and the total thickness of a column is  $h_1 + h_2 + h_3 = \eta_{1/2} - \eta_b$ .

In studies of shallow water fluids, much of the formalism developed for a single layer can be readily extended to an arbitrary number of layers. We here pursue this extension and thereby expose the underlying kinematics and dynamics of stacked shallow water models. We assume the layers are immiscible so that matter and thermal properties are not exchanged between the layers. Instead, the layers couple only through mechanical forces arising from pressure form stress. The notation for our derivations is depicted in Figure 30.6 in the case of three active layers.

In Section 44.1 we develop the equations for a continuously stratified Boussinesq fluid making use of isopycnal vertical coordinates. Although the vertical stratification is continuous in that case, we see in that discussion that the isopycnal equations are isomorphic to the stacked shallow water equations. Hence, besides being of intrinsic interest as a versatile theoretical model, the stacked shallow water model offers a suitable step towards studies of a continuously stratified fluid using isopycnal coordinates.

### 30.4.1 Formulation of a 2-layer model

We here display the equations for two layers, thus offering the seeds for an extenstion to  $N$  layers in Section 30.4.2.

*Thickness and tracer equations*

Each shallow water layer satisfies its own independent thickness equation and tracer equation, representing the conservation of volume and tracer content for each layer

$$\frac{\partial h_1}{\partial t} + \nabla \cdot (h_1 \mathbf{u}_1) = 0 \quad (30.54)$$

$$\frac{\partial h_2}{\partial t} + \nabla \cdot (h_2 \mathbf{u}_2) = 0 \quad (30.55)$$

$$\frac{\partial(h_1 C_1)}{\partial t} + \nabla \cdot (h_1 C_1 \mathbf{u}_1) = 0 \quad (30.56)$$

$$\frac{\partial(h_2 C_2)}{\partial t} + \nabla \cdot (h_2 C_2 \mathbf{u}_2) = 0. \quad (30.57)$$

We emphasize that there is no explicit coupling between these equations, as each layer separately must satisfy volume conservation and tracer conservation. However, the velocities are coupled through the pressure force, as we now discuss.

*Pressure within a layer*

To compute the pressure within a layer, we make use of the hydrostatic balance and integrate down from the surface, which results in the pressure fields

$$p_1 = \rho_1 g (\eta_{1/2} - z) + p_a \quad (30.58)$$

$$p_2 = \rho_1 g (\eta_{1/2} - \eta_{3/2}) + \rho_2 g (\eta_{3/2} - z) + p_a. \quad (30.59)$$

It is convenient to write pressure in layer-two using the reduced gravity, which leads to

$$p_2 - p_a = \rho_1 g (\eta_{1/2} - \eta_{3/2}) + \rho_2 g (\eta_{3/2} - z) \quad (30.60a)$$

$$= g \eta_{3/2} (\rho_2 - \rho_1) + g \rho_1 \eta_{1/2} - g \rho_2 z \quad (30.60b)$$

$$= \rho_1 \left[ g \eta_{1/2} + g \eta_{3/2} \frac{\rho_2 - \rho_1}{\rho_1} \right] - g \rho_2 z \quad (30.60c)$$

$$= \rho_1 (g_{1/2}^r \eta_{1/2} + g_{3/2}^r \eta_{3/2}) - g \rho_2 z, \quad (30.60d)$$

with the reduced gravities given by

$$g_{1/2}^r = g \left[ \frac{\rho_1 - \rho_0}{\rho_1} \right] \approx g \quad \text{and} \quad g_{3/2}^r = g \left[ \frac{\rho_2 - \rho_1}{\rho_1} \right]. \quad (30.61)$$

We here assumed that  $\rho_0 \ll \rho_1$  so that the reduced gravity at the ocean surface,  $g_{1/2}^r$ , is close to the full gravity,  $g_{1/2}^r \approx g$ .

*Horizontal velocity equations*

The horizontal velocity equations for the two layers take the form

$$\rho_1 \left[ \frac{D_1 \mathbf{u}_1}{Dt} + f \hat{z} \times \mathbf{u}_1 \right] = -\nabla p_1 \quad (30.62a)$$

$$\rho_2 \left[ \frac{D_2 \mathbf{u}_2}{Dt} + f \hat{z} \times \mathbf{u}_2 \right] = -\nabla p_2, \quad (30.62b)$$

where we introduced the layer material time derivatives

$$\frac{D_k}{Dt} = \frac{\partial}{\partial t} + \mathbf{u}_k \cdot \nabla \quad \text{for } k = 1, 2. \quad (30.63)$$

Making use of expressions (30.58) and (30.60d) for layer pressures leads to the horizontal momentum equations

$$\frac{D_1 \mathbf{u}_1}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u}_1 = -g \nabla [\eta_{1/2} + p_a / (g \rho_1)] \quad (30.64a)$$

$$\frac{D_2 \mathbf{u}_2}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u}_2 = -\frac{\rho_1}{\rho_2} \nabla \left( g_{1/2}^r \eta_{1/2} + g_{3/2}^r \eta_{3/2} + p_a / \rho_1 \right). \quad (30.64b)$$

Finally, it is convenient to express pressure in terms of layer thicknesses,  $h_1$  and  $h_2$ , since the layer thicknesses are the prognostic fields determined by time stepping the thickness equations (30.54) and (30.55). We thus write

$$\eta_{1/2} = \eta_b + h_1 + h_2 \quad \text{and} \quad \eta_{3/2} = \eta_b + h_2, \quad (30.65)$$

so that

$$p_1 = \rho_1 g (\eta_b + h_1 + h_2) + p_a - g \rho_1 z \quad (30.66a)$$

$$p_2 = \rho_1 \left[ g_{1/2}^r (\eta_b + h_1 + h_2) + g_{3/2}^r (\eta_b + h_2) \right] + p_a - g \rho_2 z, \quad (30.66b)$$

thus resulting in the horizontal momentum equations

$$\frac{D_1 \mathbf{u}_1}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u}_1 = -g \nabla [\eta_b + h_1 + h_2 + p_a / (g \rho_1)] \quad (30.67a)$$

$$\frac{D_2 \mathbf{u}_2}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u}_2 = -\frac{\rho_1}{\rho_2} \nabla \left[ g_{1/2}^r (\eta_b + h_1 + h_2) + g_{3/2}^r (\eta_b + h_2) + p_a / \rho_1 \right]. \quad (30.67b)$$

Notice how layer thickness from one layer appears in the other layer's pressure gradient. In this way, changes in the thickness of one layer have a direct impact on pressure forces and flow in the adjacent layer. Finally, the Boussinesq approximation sets the density ratio  $\rho_1/\rho_2$  to unity so that

$$\frac{D_1 \mathbf{u}_1}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u}_1 = -g \nabla [\eta_b + h_1 + h_2 + p_a / (g \rho_1)] \quad (30.68a)$$

$$\frac{D_2 \mathbf{u}_2}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u}_2 = -\nabla \left[ g_{1/2}^r (\eta_b + h_1 + h_2) + g_{3/2}^r (\eta_b + h_2) + p_a / \rho_1 \right]. \quad (30.68b)$$

#### *Vertical shear in horizontal velocities*

The difference in layer velocities,  $\mathbf{u}_1 - \mathbf{u}_2$ , represents the vertical shear in the layers. Assuming  $g_{1/2}^r = g$  reveals that this difference is affected by a pressure gradient arising just from bottom topography and the interior layer thickness,  $h_2$

$$\frac{D_1 \mathbf{u}_1}{Dt} - \frac{D_2 \mathbf{u}_2}{Dt} + f \hat{\mathbf{z}} \times (\mathbf{u}_1 - \mathbf{u}_2) = g_{3/2}^r \nabla (\eta_b + h_2). \quad (30.69)$$

That is, the vertical shear does not directly feel undulations of the free surface,  $\eta_{1/2}$ , or the applied pressure,  $p_a$ . Rather, it feels these surface undulations only indirectly via nonlinear terms appearing in the advection on the left hand side. We further discuss this result in Section 31.2.2

by introducing thermal wind and the Margules' Relation.

### 30.4.2 $N$ -layer model equations

The 2-layer equations (30.68a) and (30.68b) can be readily generalized to  $N$ -layers. The thickness equation and tracer equation represent volume and tracer conservation for each layer

$$\frac{\partial h_k}{\partial t} + \nabla \cdot (\mathbf{u}_k h_k) = 0 \quad (30.70a)$$

$$\frac{\partial(h_k C_k)}{\partial t} + \nabla \cdot (\mathbf{u}_k h_k C_k) = 0, \quad (30.70b)$$

where  $k = 1, N$  is the discrete layer index and there is no implied summation on this label.<sup>6</sup>

Some work is needed to generalize the pressure gradient appearing in the velocity equation. For that purpose, write the interface height,  $\eta_{k+1/2}$ , as

$$\eta_{k+1/2} = \eta_b + \sum_{j=k+1}^N h_j \quad \text{with } \eta_{N+1/2} = \eta_b \text{ and } \eta_{1/2} = \eta. \quad (30.71)$$

For example, the layer interfaces with  $N = 3$  layers are given by

$$\eta_{1/2} = \eta_b + h_1 + h_2 + h_3 \quad \eta_{3/2} = \eta_b + h_2 + h_3 \quad \eta_{5/2} = \eta_b + h_3 \quad \eta_{7/2} = \eta_b. \quad (30.72)$$

In turn, the hydrostatic pressure within layer- $k$  is given by

$$p_k = -g \rho_k z + p_a + \rho_1 \sum_{j=0}^{k-1} g_{j+1/2}^r \eta_{j+1/2} = p_{k-1/2} + g \rho_k (\eta_{k-1/2} - z), \quad (30.73)$$

where the reduced gravities are

$$g_{j+1/2}^r = g \frac{\rho_{j+1} - \rho_j}{\rho_1} > 0 \quad \text{with} \quad g_{1/2}^r = g \quad \text{if} \quad \rho_0 = \rho_a = 0, \quad (30.74)$$

with  $\rho_a$  the density of the overlying atmosphere. The half-integer pressures are evaluated on the corresponding interface with the hydrostatic balance yielding the pressure difference

$$p_{k+1/2} - p_{k-1/2} = g \rho_k h_k = g \rho_k (\eta_{k-1/2} - \eta_{k+1/2}). \quad (30.75)$$

Since the terms  $g \rho_k z$  appearing in the layer pressures have zero horizontal gradient, they do not contribute to horizontal accelerations. Hence, in some treatments it can be useful to make use of the *dynamic pressures*

$$p_k^{\text{dyn}} \equiv \rho_1 \sum_{j=0}^{k-1} g_{j+1/2}^r \eta_{j+1/2} \implies \nabla p_k = \nabla p_k^{\text{dyn}}. \quad (30.76)$$

The corresponding velocity equation for an arbitrary layer- $k$  is given by

$$\frac{D_k \mathbf{u}_k}{Dt} + f \hat{z} \times \mathbf{u}_k = -\nabla p_k / \rho_1 \iff [\partial_t + (\mathbf{u}_k \cdot \nabla)] \mathbf{u}_k + f \hat{z} \times \mathbf{u}_k = -\nabla p_k / \rho_1. \quad (30.77)$$

---

<sup>6</sup>To help distinguish the layer index,  $k$ , from a tensor index,  $k$ , we write the layer index using an upright Roman font whereas a tensor index is slanted.

### 30.4.3 Rigid lid models

Throughout this section we formulated the equations for an N-layer shallow water model where  $\eta_{1/2}$  is the undulating free surface. For some applications of large-scale oceanography, it is useful to remove the external gravity waves from the model, where these gravity waves are associated with linear fluctuations of the upper free surface.<sup>7</sup> To remove these gravity waves we can, by fiat, set the upper ocean interface to a rigid constant, conventionally taken as  $\eta_{1/2} = 0$ . This assumption is known as the *rigid lid*. If there is no applied pressure,  $p_a = 0$ , then there is no horizontal pressure gradient in the upper layer, much like an inverted reduced gravity model (see Exercise 30.4). A dynamically more interesting case arises when there is an applied pressure,  $p_a \neq 0$ , so that motion is generated in layer one, which in turn induces motion throughout all layers.

Note that velocity in the upper layer remains horizontally divergent since the  $\eta_{3/2}$  interface is not generally rigid. Even so, by fixing the upper ocean to be rigid we remove the relatively fast external gravity waves from the model. We return to the rigid lid assumption when discussing the horizontal non-divergent barotropic model in Chapter 33 (see in particular Section 33.4).

## 30.5 Non-conservative processes and boundary stresses

Much of our focus on shallow water mechanics concerns the adiabatic case in which the layers are immiscible and there are no frictional processes. Even so, we will find occasion to consider non-conservative processes, such as the transfer of volume between layers via dia-surface fluxes, as well as irreversible momentum transfer associated with friction and boundary stresses. In this section we consider these processes for the single shallow water layer, with a straightforward extension to stacked shallow water.

### 30.5.1 Dia-surface volume fluxes

Consider the case of dia-surface transfer as occurs across the ocean surface through evaporation, precipitation, and river runoff, or as occurs for interior layers in the presence of irreversible mixing processes. Let  $w^{(\dot{\eta})}$  measure the volume per time per horizontal area of fluid entering across the surface interface of the shallow water layer, with  $w^{(\dot{\eta})}$  having dimensions of length per time and a sign convention so that  $w^{(\dot{\eta})} > 0$  means volume enters the shallow water layer.<sup>8</sup> For example,  $w^{(\dot{\eta})} > 0$  could represent the addition of rain to the surface layer. To keep the analysis simple, assume the mass contained in  $w^{(\dot{\eta})} \neq 0$  has the same density and same velocity as the shallow water layer. Hence, there is no modification to the layer density. This assumption must be relaxed for realistic layered models.

#### *Surface kinematic boundary condition*

The kinematic boundary condition (30.32) expresses the material nature of the free surface in the absence of boundary volume flux. In the presence of a non-zero boundary flux,  $w^{(\dot{\eta})} \neq 0$ , we follow the formulation of the kinematic boundary condition for the ocean free surface with a mass flux (equation (14.79)), which renders the boundary condition

$$\frac{D(z - \eta)}{Dt} = -w^{(\dot{\eta})} \quad \text{at } z = \eta. \quad (30.78)$$

---

<sup>7</sup>In Section 31.8 we study gravity waves in a single shallow water layer.

<sup>8</sup>This sign convention follows that used for water mass transformation as developed in Chapter 50 and defined by equation (50.38).

In effect, this relation defines the surface boundary flux, and this boundary condition can be written in the equivalent form

$$\frac{D\eta}{Dt} = w(\eta) + w^{(\dot{\eta})}. \quad (30.79)$$

### Stretching of a vertical column

Equation (30.39) shows that in the absence of volume sources, a column of shallow water fluid stretches or squeezes uniformly. What happens when  $w^{(\dot{\eta})} \neq 0$ ? Following through the derivation of the thickness equation in Section 30.2.4, we are trivially led to the following generalization

$$\frac{\partial h}{\partial t} + \nabla \cdot (h \mathbf{u}) = w^{(\dot{\eta})}, \quad (30.80)$$

or equivalently

$$\frac{Dh}{Dt} = -h \nabla \cdot \mathbf{u} + w^{(\dot{\eta})}. \quad (30.81)$$

Equation (30.37) is derived through assuming the horizontal velocity has no depth dependence within a shallow water layer, and the fluid has a three-dimensional non-divergent velocity. It holds whether the ocean surface is material or non-material, and thus forms a suitable starting point for generalization to the case of  $w^{(\dot{\eta})} \neq 0$

$$w(z) - w(\eta_b) = \left[ \frac{z - \eta_b}{\eta - \eta_b} \right] [w(\eta) - w(\eta_b)]. \quad (30.82)$$

We now make use of the new surface kinematic boundary condition (30.79) and the unmodified bottom kinematic boundary condition (30.25) to write the material form

$$\frac{1}{z - \eta_b} \left[ \frac{D(z - \eta_b)}{Dt} \right] = \frac{1}{\eta - \eta_b} \left[ \frac{D(\eta - \eta_b)}{Dt} - w^{(\dot{\eta})} \right]. \quad (30.83)$$

Rearrangement thus leads to the material conservation statement

$$\left[ \frac{z - \eta_b}{h} \right]^{-1} \frac{D}{Dt} \left[ \frac{z - \eta_b}{h} \right] = -\frac{w^{(\dot{\eta})}}{h}, \quad (30.84)$$

where  $h = \eta - \eta_b$  is the layer thickness. This result can be written in the more concise form

$$\frac{D}{Dt} \left[ \ln \left( \frac{z - \eta_b}{h} \right) \right] = -\frac{w^{(\dot{\eta})}}{h}. \quad (30.85)$$

Either way, we see that in the presence of a surface boundary volume flux, a column of shallow water fluid no longer stretches or squeezes uniformly. Instead, for  $w^{(\dot{\eta})} > 0$ , a fluid parcel moves down within the column as more water is added to the top of the layer.

### 30.5.2 Frictional and boundary stresses

As discussed in Chapter 18, accelerations from friction appear in the momentum equation via the divergence of the frictional stress tensor. For a shallow water fluid we may choose to include a frictional stress proportional to lateral shears within each layer much like the friction operators discussed in Section 18.7. Additionally, we may need to include boundary stresses such as those from winds and bottom friction. To incorporate boundary stresses, consider the Boussinesq form (Section 23.5.2) of the vertical stress divergence appearing in the momentum equation as an

acceleration

$$\mathbf{F} = \frac{1}{\rho_0} \frac{\partial \boldsymbol{\tau}}{\partial z}, \quad (30.86)$$

where  $\boldsymbol{\tau}$  is the horizontal stress imparted to the layer interface due to turbulent boundary layer processes. Since a shallow water layer is homogeneous, we can only apply this boundary stress uniformly throughout the layer (as a body stress) and so it appears as

$$\mathbf{F}_k = \frac{1}{\rho_0} \frac{\boldsymbol{\tau}_{k-1/2} - \boldsymbol{\tau}_{k+1/2}}{h_k}, \quad (30.87)$$

where  $h_k$  is the layer thickness,  $\boldsymbol{\tau}_{k-1/2}$  is the stress at the upper interface (e.g., wind stress) and  $\boldsymbol{\tau}_{k+1/2}$  is the stress at the lower interface (e.g., bottom drag).



## 30.6 Exercises

### EXERCISE 30.1: RELATIONS FOR VERTICAL VELOCITY (EXERCISE (3.2) OF *Vallis (2006)*)

Show that the vertical velocity within a shallow water system is given by

$$w = \left[ \frac{z - \eta_b}{h} \right] \frac{Dh}{Dt} + \frac{D\eta_b}{Dt}. \quad (30.88)$$

Interpret the result, showing that it gives sensible answers at the top and bottom of the fluid layer.

### EXERCISE 30.2: NON-ROTATING HYDRAULIC CONTROL

Consider the steady flow in a non-rotating shallow water layer where the flow is purely one-dimensional in the zonal direction.

- (a) Show that the steady flow satisfies the balance

$$\partial_x h [1 - Fr^2] = \partial_x \eta_b \quad (30.89)$$

where the Froude number is given by

$$Fr = \frac{u}{\sqrt{gh}}. \quad (30.90)$$

The Froude number is the ratio of the speed for a fluid particle to the speed of a shallow water gravity wave.

- (b) Discuss the case in which  $\partial_x \eta_b = 0$  yet  $\partial_x h \neq 0$ . This case is known as *hydraulic control*.

### EXERCISE 30.3: SHALLOW WATER EQUATIONS WITH TIDES

In Chapter 28 we derive the equations for a primitive equation ocean in the presence of astronomical forcing that leads to tides. Specialize the general results from that chapter to derive the thickness and momentum equations for a single layer of shallow water fluid in the presence of astronomical tidal forcing. As in Section 28.4, assume the perturbation geopotential is depth independent.

### EXERCISE 30.4: INVERTED REDUCED GRAVITY MODEL

Derive the shallow water equations for a single moving layer of fluid of density  $\rho_2$  above a rigid

floor, with this moving layer below a stagnant fluid of density  $\rho_1$ , with  $\rho_1 < \rho_2$ . Show that as  $\rho_1/\rho_2 \rightarrow 0$  the single layer shallow water equations emerge. Make use of notation from the three-layer system shown in Figure 30.6. This model might be used to study flow in the atmosphere well above the boundary layer, or the abyssal ocean well below the pycnocline. Hint: invert the approach taken in Section 30.3 for the reduced gravity model of the upper ocean.



# Chapter 31

## Shallow water dynamics

In this chapter we further our dynamical understanding of the shallow water fluid model. Our study includes geostrophy, thermal wind (as expressed by Margules' relation), momentum budgets, form stress, mechanical energy, and available potential energy. We also develop three case studies: the steady force balance in a zonally reentrant channel, the angular momentum dynamics of a rotating tank of shallow water fluid, and linear gravity waves in a single shallow water layer.

### READER'S GUIDE TO THIS CHAPTER

This chapter builds from the formulations in Chapter 30 as well as the geostrophic mechanics from Chapter 25 and the pressure form stress from Chapter 19. We make use of the dynamical results in this chapter for many of the subsequent chapters. Notationally, we follow the same convention for the gradient operator noted at the start of Chapter 30.

31.1	Loose threads	730
31.2	Geostrophic balance and thermal wind	730
31.2.1	Geostrophy for a single layer	731
31.2.2	Geostrophy and thermal wind for two layers	731
31.2.3	Geostrophic transport within layers	732
31.2.4	Flow within a geostrophic eddy	734
31.2.5	Comments	735
31.3	Mechanical energy	735
31.3.1	Gravitational potential energy	735
31.3.2	Kinetic energy	736
31.3.3	Mechanical energy	737
31.3.4	Available potential energy	738
31.4	Thickness weighted momentum equation	738
31.4.1	Single layer equations	739
31.4.2	Geostrophic and ageostrophic contributions	740
31.4.3	Form stresses acting on a shallow water column	740
31.4.4	Comments on the two pressure force formulations	742
31.5	Contact pressure forces in shallow water layers	743
31.5.1	Pressure contact force and pressure body force	743
31.5.2	$N$ -layer equations	743
31.5.3	Contact pressure force along vertical sides	744
31.5.4	Contact pressure force along the top and bottom interfaces	745
31.5.5	Form stress	746
31.5.6	Net contact pressure force on a shallow water column	747

31.5.7	Contact pressure force summed over all layers . . . . .	747
31.5.8	Horizontal pressure force with potential energy gradients . . . . .	748
31.5.9	Momentum equation with contact pressure forces . . . . .	748
31.5.10	Further reading . . . . .	751
31.6	Steady momentum balance in a zonal channel . . . . .	751
31.6.1	Volume transport for steady flow . . . . .	752
31.6.2	Steady meridional balances . . . . .	753
31.6.3	Steady zonal balance . . . . .	753
31.6.4	The role of frictional bottom drag . . . . .	754
31.6.5	Correlation between surface height and topographic slope . . . . .	755
31.6.6	Connection to meridional geostrophic transport . . . . .	755
31.6.7	Sinusoidal example . . . . .	756
31.6.8	Comments . . . . .	758
31.7	Angular momentum in a rotating tank . . . . .	759
31.7.1	Angular momentum for a column of shallow water fluid . . . . .	759
31.7.2	Material time evolution of the angular momentum . . . . .	759
31.7.3	Materially invariant angular momentum . . . . .	761
31.7.4	Comments . . . . .	761
31.8	Inertia-gravity waves in a single shallow water layer . . . . .	761
31.8.1	Linearized shallow water equations . . . . .	761
31.8.2	Relative vorticity of linear fluctuations . . . . .	762
31.8.3	Non-rotating gravity waves . . . . .	762
31.8.4	Potential vorticity of linear fluctuations . . . . .	765
31.8.5	Inertia-gravity waves . . . . .	765
31.8.6	Inertia-gravity wave dispersion relation . . . . .	765
31.8.7	Horizontally longitudinal and transverse components . . . . .	768
31.8.8	Comments . . . . .	768
31.9	Inertia-gravity waves generated by topography . . . . .	768
31.9.1	Linearized equations . . . . .	769
31.9.2	Galilean transformation . . . . .	769
31.9.3	Wave equation and relation between amplitudes . . . . .	770
31.10	Exercises . . . . .	771

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## 31.1 Loose threads

- More schematics
- Work through a two-layer example for the zonal channel in Section 31.6 to describe the features exhibited by Olbers and Hughes in their schematic of the Southern Ocean circulation. Discuss topographic form stress.
- Two-layer gravity waves and topographic forcing to show that with two layers one gets a phase shift and thus a nonzero topographic form stress.

## 31.2 Geostrophic balance and thermal wind

As described in Chapter 25, geostrophic balance arises from neglecting the material time derivative in the inviscid horizontal momentum equation, which is a sensible assumption when the Rossby number is small. The resulting balance between Coriolis and pressure accelerations constitutes the geostrophic balance. We consider here the implications of geostrophy for one and two-layer shallow water systems.

### 31.2.1 Geostrophy for a single layer

Ignoring atmospheric pressure ( $p_a = 0$ ) leads to the geostrophic balance for a single shallow water layer

$$f \hat{z} \times \mathbf{u}_g = -g \nabla \eta \implies f \mathbf{u}_g = g \hat{z} \times \nabla \eta, \quad (31.1)$$

or in component form

$$u_g = -\frac{g}{f} \frac{\partial \eta}{\partial y} \quad \text{and} \quad v_g = \frac{g}{f} \frac{\partial \eta}{\partial x}. \quad (31.2)$$

Consequently, the shallow water layer geostrophic current is balanced by the gradient of the free surface (sea level). In the northern hemisphere, where  $f > 0$ , geostrophic shallow water currents flow counter-clockwise around negative sea level anomalies (low pressure) and clockwise around positive sea level anomalies (high pressure). The opposite orientation holds in the southern hemisphere, where  $f < 0$ . Figure 31.1 shows a schematic of geostrophic balance for a single shallow water layer.

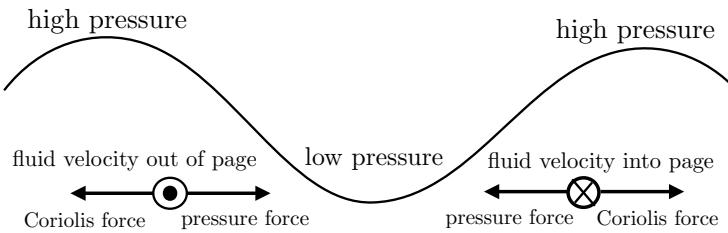


FIGURE 31.1: Side view of geostrophic balance for a single shallow water layer, here shown with two high pressure centers surrounding a low pressure center. The Coriolis force balances the pressure gradient force. In the northern hemisphere, where  $f > 0$ , geostrophic flow is counter-clockwise around a low pressure center and clockwise around a high pressure center.

### 31.2.2 Geostrophy and thermal wind for two layers

Now consider two shallow water layers as in Figure 30.6. Recall the layer pressure equations (30.58) and (30.59), which leads to the pressure difference

$$p_1 - p_2 = g \eta_{3/2} (\rho_1 - \rho_2) + g z (\rho_2 - \rho_1) = g_{3/2}^r \rho_1 (z - \eta_{3/2}), \quad (31.3)$$

where the reduced gravity is given by

$$g_{3/2}^r = g \left[ \frac{\rho_2 - \rho_1}{\rho_1} \right] > 0. \quad (31.4)$$

The density difference  $\rho_2 - \rho_1$  is generally much smaller than either density, so that  $g_{3/2}^r \ll g$ . For a Boussinesq shallow water system, the momentum equations are given by

$$\frac{D_1 \mathbf{u}_1}{Dt} + f \hat{z} \times \mathbf{u}_1 = -\rho_1^{-1} \nabla p_1 \quad (31.5a)$$

$$\frac{D_2 \mathbf{u}_2}{Dt} + f \hat{z} \times \mathbf{u}_2 = -\rho_1^{-1} \nabla p_2, \quad (31.5b)$$

where we used the top layer density as the Boussinesq reference density, and where we introduced the material time derivatives for each layer

$$\frac{D_n}{Dt} = \frac{\partial}{\partial t} + \mathbf{u}_n \cdot \nabla. \quad (31.6)$$

Making use of the pressure difference (31.3) renders

$$\frac{D_1 \mathbf{u}_1}{Dt} - \frac{D_2 \mathbf{u}_2}{Dt} + f \hat{\mathbf{z}} \times \Delta \mathbf{u} = -\rho_1^{-1} \nabla(p_1 - p_2) = g_{3/2}^r \nabla \eta_{3/2}, \quad (31.7)$$

where

$$\Delta \mathbf{u} = \mathbf{u}_1 - \mathbf{u}_2 \quad (31.8)$$

is the vertical difference of the layer horizontal velocities. We see that the difference in the geostrophic velocities for the two layers is proportional to the slope of the interface between the two layers

$$f \hat{\mathbf{z}} \times \Delta \mathbf{u}_g = g_{3/2}^r \nabla \eta_{3/2}, \quad (31.9)$$

which is equivalent to

$$f \Delta \mathbf{u}_g = -\hat{\mathbf{z}} \times g_{3/2}^r \nabla \eta_{3/2} \implies \Delta u_g = +\frac{g_{3/2}^r}{f} \frac{\partial \eta_{3/2}}{\partial y} \quad \text{and} \quad \Delta v_g = -\frac{g_{3/2}^r}{f} \frac{\partial \eta_{3/2}}{\partial x}. \quad (31.10)$$

These equations represent the *Margules' relation*. It applies at any interface between two shallow water fluid layers. It says that the vertical difference between the layer geostrophic velocities is proportional to the interface slope. When the slope is large, the vertical difference in the geostrophic velocity is large. Also, the velocity difference is large when the reduced gravity is large; i.e., when the density difference is large. We illustrate this relation in Figure 31.2. The Margules relation is a discrete (two-layer) version of the thermal wind relation discussed in Section 25.5.6.

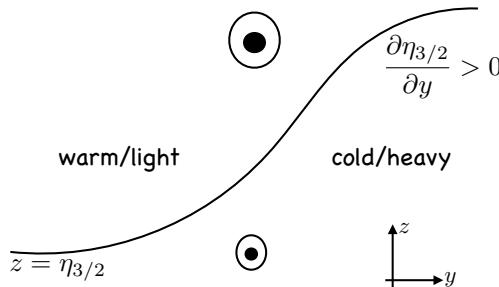


FIGURE 31.2: Illustrating Margules' relation for the northern hemisphere ( $f > 0$ ). Here we show the interface between a two-layer shallow water model with a cold/heavy layer to the right and a warm/light layer to the left. The slope of the interface is positive,  $\partial \eta_{3/2} / \partial y > 0$ , thus leading to an increase in the eastward zonal geostrophic velocity moving upward, as depicted by the circles with a dot. This orientation corresponds to the northern hemisphere atmospheric jet stream, whereby the interface between cold/heavy air to the north and warm/light air to the south leads to a zonal thermal wind jet.

### 31.2.3 Geostrophic transport within layers

We are often interested in computing the net volume transport within a layer of fluid in order to measure how much the fluid is moving across a particular region. For an  $N$ -layer shallow water

fluid this transport is written

$$\mathbf{U} = \int \mathbf{u} dz = \sum_{k=1}^N \mathbf{u}_k h_k, \quad (31.11)$$

where  $\mathbf{u}_k$  is the layer horizontal velocity and  $h_k$  the layer thickness. For many purposes it is sufficient to compute the transport due to the geostrophic motion, in which case

$$\mathbf{u}_k = (\rho_1 f)^{-1} \hat{\mathbf{z}} \times \nabla p_k, \quad (31.12)$$

where  $\rho_1$  is the layer-1 density, which is also used as the reference density for the Boussinesq approximation.

Inserting the geostrophic velocity (31.12) into the depth integrated transport equation (31.11) yields

$$\mathbf{U}_g = \int_{\eta_b}^{\eta} \mathbf{u}_g dz = (\rho_1 f)^{-1} \hat{\mathbf{z}} \times \sum_{k=1}^N h_k \nabla p_k \quad (31.13)$$

As an exercise, let us work through the geostrophic transport for three layers (assuming  $p_a = 0$ ), in which the layer pressures are written (see Section 30.4.2)

$$p_1 = \rho_1 g (\eta_{1/2} - z) \quad (31.14a)$$

$$p_2 = \rho_1 g (\eta_{1/2} - \eta_{3/2}) + \rho_2 g (\eta_{1/2} - z) \quad (31.14b)$$

$$p_3 = \rho_1 g (\eta_{1/2} - \eta_{3/2}) + \rho_2 g (\eta_{3/2} - \eta_{5/2}) + \rho_3 g (\eta_{5/2} - z), \quad (31.14c)$$

which can be written in terms of the reduced gravities according to

$$p_1 = \rho_1 g (\eta_{1/2} - z) \quad (31.15a)$$

$$p_2 = \rho_1 (g_{1/2}^r \eta_{1/2} + g_{3/2}^r \eta_{3/2}) - \rho_2 g z \quad (31.15b)$$

$$p_3 = \rho_1 (g \eta_{1/2} + g_{3/2}^r \eta_{3/2} + g_{5/2}^r \eta_{5/2}) - \rho_3 g z. \quad (31.15c)$$

With  $g_{1/2}^r = g$  (consistent with  $p_a = 0$ ) we can express the geostrophic transport within the three layers as

$$h_1 \mathbf{u}_1 = \frac{h_1}{f} \hat{\mathbf{z}} \times \nabla (g_{1/2}^r \eta_{1/2}) \quad (31.16a)$$

$$h_2 \mathbf{u}_2 = \frac{h_2}{f} \hat{\mathbf{z}} \times (g_{1/2}^r \nabla \eta_{1/2} + g_{3/2}^r \nabla \eta_{3/2}) \quad (31.16b)$$

$$h_3 \mathbf{u}_3 = \frac{h_3}{f} \hat{\mathbf{z}} \times (g_{1/2}^r \nabla \eta_{1/2} + g_{3/2}^r \nabla \eta_{3/2} + g_{5/2}^r \nabla \eta_{5/2}), \quad (31.16c)$$

in which case the depth integrated geostrophic transport is

$$\mathbf{U}_g = \frac{1}{f} \left[ g_{1/2}^r (h_1 + h_2 + h_3) \nabla \eta_{1/2} + g_{3/2}^r (h_2 + h_3) \nabla \eta_{3/2} + g_{5/2}^r h_3 \nabla \eta_{5/2} \right], \quad (31.17)$$

where  $h_1 + h_2 + h_3 = \eta_{1/2} - \eta_b$  is the total depth of a fluid column spanning the three layers. This expression for  $\mathbf{U}_g$  displays the cascade of contributions from each of the layer interfaces. The top interface contributes as a depth-integral along with the full contribution from gravity, whereas the interior layers have successively less thickness weighting along with a weighting by their respective reduced gravities.

### 31.2.4 Flow within a geostrophic eddy

The ocean and atmosphere are highly turbulent fluids, with turbulent features extending from the small scales (millimeters) to large scales (hundreds to thousands of kilometers). The larger scale turbulent features feel the earth's rotation and thus maintain a force balance close to geostrophic.<sup>1</sup> We here outline some features of an ocean *geostrophic eddy* as idealized using the reduced gravity model of Section 30.3. Figure 31.3 shows a vertical-zonal slice through the upper portion of an ocean eddy in the middle latitude northern hemisphere ( $f > 0$ ) ocean. The central region consists of a geostrophic eddy, sometimes also referred to as an *ocean mesoscale eddy*. The signature of the eddy is a depression in the free surface height and upward deformation of the pycnocline. The lateral scale of the eddy is on the order of the internal deformation scale (see Exercise 31.11).

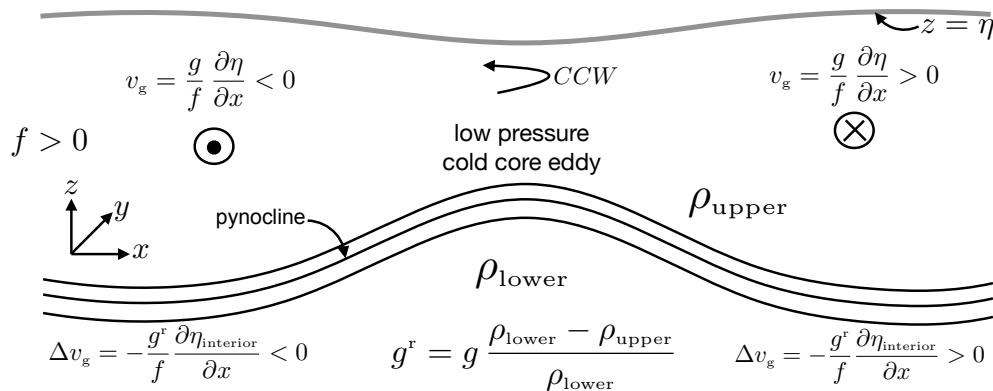


FIGURE 31.3: Vertical-zonal slice through a northern hemisphere mid-latitude cold-core ocean eddy looking from the south to the north (north is into the page). The ocean free surface is depressed down in the middle so that flow is cyclonic (counter-clockwise in north) within the upper portion of the eddy where  $\rho = \rho_{\text{upper}}$ . The pycnocline (region of enhanced vertical density gradient) is deformed upward, and the baroclinic flow implied by Margules' relation (31.10) is indicated, making use of the reduced gravity  $g^r = g(\rho_{\text{lower}} - \rho_{\text{upper}})/\rho_{\text{upper}}$ . Note that  $\Delta v_g = v_{\text{upper}} - v_{\text{lower}}$ , so that  $\Delta v_g > 0$  means that the meridional flow increases in the  $+\hat{y}$ -direction when moving from the lower to upper layer, and conversely when  $\Delta v_g < 0$ .

The ocean eddy in Figure 31.3 is an anomalously dense cyclonic mesoscale eddy with the dense water causing the pycnocline to deviate upward. If density is dominated by temperature, as it typically is within the middle to lower latitude oceans, then the eddy is a *cold core eddy*. Under geostrophic balance, water circulates counter-clockwise in the northern hemisphere within the upper portion of the cold core eddy, in the region where the pressure gradient force is dominated by the free surface undulation. In this case we see say the eddy is cyclonic. According to the reduced gravity model from Section 30.3 (see in particular Figure 30.5), the ratio of the free surface undulation to the pycnocline undulation scales like the reduced gravity, so that a meter undulation of the free surface corresponds to roughly 100 m undulation of the pycnocline. The same ideas hold for a *warm core eddy*, such as that depicted in Figure 31.4, with undulations complementing those in the cold core and thus supporting anti-cyclonic thermal wind flow.

In presenting the idealized rendition of an ocean eddy in Figure 31.3, we are assuming a reduced gravity model is sufficient and that the atmosphere has no significant horizontal pressure gradients over the scale of the eddy. Under these assumptions, we make use of the Margules' relation (31.10) to deduce the thermal wind flow in the upper layer relative to the layer below;

<sup>1</sup>As noted in Section 26.6, the gradient wind balance provides a more accurate approximation to flows in ocean and atmospheric eddies by also including the centrifugal acceleration associated with the curved motion. Even so, the geostrophic balance provides a sufficient approximation for many purposes and it will be used here, along with thermal wind.

i.e., the vertical shear in the geostrophic flow. For the left side of the eddy, where  $\partial\eta_{\text{interior}}/\partial x > 0$ , the vertical shear in the meridional geostrophic velocity is southward, consistent with orientation of the flow implied by the sea surface gradient. Conversely, on the right side of the eddy, where  $\partial\eta_{\text{interior}}/\partial x < 0$ , the vertical shear in the meridional flow is northward.

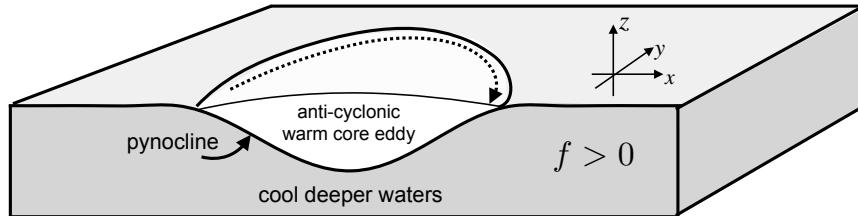


FIGURE 31.4: Schematic of a warm core (light water) geostrophic ocean eddy as idealized by a reduced gravity model. The geostrophic/thermal wind flow is anti-cyclonic within the eddy, which contrasts to the cyclonic flow for a cold core eddy as depicted in Figure 31.3. The eddy is characterized by a slight expansion of the free surface (high pressure) and a relatively larger depression of the pycnocline.

### 31.2.5 Comments

An alternative definition of reduced gravity for the 2-layer system uses the average density,

$$\bar{\rho}^{12} = (\rho_1 + \rho_2)/2, \quad (31.18)$$

in which case the modified reduced gravity is

$$\bar{g}_{3/2} = g \left[ \frac{\rho_2 - \rho_1}{\bar{\rho}^{12}} \right]. \quad (31.19)$$

Correspondingly, the pressure gradient on the right hand side of the momentum equations (31.5a) and (31.5b) have  $1/\rho_1$  replaced by  $1/\bar{\rho}^{12}$ . Even so, the equation for the vertical shear evolution, (31.7), remains unchanged. For more than two layers, it is typical to take the reference density equal to that of the top layer, as done in our three layer example in Section 31.2.3.

## 31.3 Mechanical energy

We here study the mechanical energy for a single shallow water layer sitting on top of a generally non-flat bottom. As part of this discussion we consider the available potential energy (APE).

### 31.3.1 Gravitational potential energy

The gravitational potential energy per horizontal area of a shallow water fluid of constant density is given by

$$\mathcal{P} = g \rho \int_{\eta_b}^{\eta} z \, dz \quad (31.20a)$$

$$= \frac{g \rho}{2} (\eta^2 - \eta_b^2) \quad (31.20b)$$

$$= g \rho h (\eta - h/2). \quad (31.20c)$$

Note how the gravitational potential energy vanishes when  $\eta^2 = \eta_b^2$ . For the case  $\eta = \eta_b$ , there is no fluid so we expect the potential energy to vanish. For the case  $\eta = -\eta_b > 0$ , there is the same amount of fluid above  $z = 0$  as below, in which case the potential energy vanishes since we are computing it relative to the  $z = 0$  reference state. Furthermore, in the flat bottom case,  $\eta_b = 0$  so that  $h = \eta - \eta_b = \eta$ , in which case the potential energy (31.20c) reduces to

$$\mathcal{P}_{\text{flat}} = g \rho h^2 / 2. \quad (31.21)$$

Taking the material time tendency of the potential energy in equation (31.20b) yields

$$\frac{D\mathcal{P}}{Dt} = g \rho \left[ \eta \frac{D\eta}{Dt} - \eta_b \frac{D\eta_b}{Dt} \right] = g \rho (\eta w_\eta - \eta_b w_b), \quad (31.22)$$

where we used equations for the vertical velocity component from Section 30.2.7. This equation states that the potential energy increases if the thickness of the layer increases through vertical motion along the top and bottom interfaces. Making further use of these equations renders

$$\frac{D\mathcal{P}}{Dt} = g \rho (\eta w_\eta - \eta_b w_b) \quad (31.23a)$$

$$= g \rho [\eta (w_b - h \nabla \cdot \mathbf{u}) - \eta_b w_b] \quad (31.23b)$$

$$= g \rho [w_b (\eta - \eta_b) - \eta h \nabla \cdot \mathbf{u}] \quad (31.23c)$$

$$= g \rho h (w_b - \eta \nabla \cdot \mathbf{u}), \quad (31.23d)$$

where we used the definition  $h = \eta - \eta_b$ . We make use of this form of the potential energy change for developing the mechanical energy budget in Section 31.3.3.

### 31.3.2 Kinetic energy

The kinetic energy per horizontal area is

$$\mathcal{K} = \frac{1}{2} \int_{\eta_b}^{\eta} \rho \mathbf{u} \cdot \mathbf{u} dz = \frac{1}{2} \rho h \mathbf{u} \cdot \mathbf{u}, \quad (31.24)$$

which has a material time derivative given by

$$\frac{D\mathcal{K}}{Dt} = \rho h \mathbf{u} \cdot \frac{D\mathbf{u}}{Dt} + \frac{1}{2} \rho \mathbf{u} \cdot \mathbf{u} \frac{Dh}{Dt} \quad (31.25a)$$

$$= -g \rho h \mathbf{u} \cdot \nabla \eta - \frac{\rho h \mathbf{u} \cdot \mathbf{u}}{2} \nabla \cdot \mathbf{u} \quad (31.25b)$$

$$= -g \rho h \mathbf{u} \cdot \nabla \eta - \mathcal{K} \nabla \cdot \mathbf{u}. \quad (31.25c)$$

$$= -g \rho h \mathbf{u} \cdot \nabla \eta + \frac{\mathcal{K}}{h} \frac{Dh}{Dt}, \quad (31.25d)$$

where we made use of the velocity equation (30.6) (with  $p_a = 0$ ) and thickness equation (30.17). The first term on the right hand side is the projection of the horizontal velocity onto the horizontal pressure gradient acceleration, thus indicating that kinetic energy increases if the flow has a component that is directed down the pressure gradient. The second term increases kinetic energy for cases where the thickness increases via the convergence of horizontal velocity.

### 31.3.3 Mechanical energy

The material time derivative of the mechanical energy per horizontal area is given by

$$\frac{D(\mathcal{K} + \mathcal{P})}{Dt} = -g h \rho \mathbf{u} \cdot \nabla \eta - \mathcal{K} \nabla \cdot \mathbf{u} + g h \rho (w_b - \eta \nabla \cdot \mathbf{u}). \quad (31.26)$$

Note there is no internal energy for the shallow water fluid, so the mechanical energy equals to the total energy.

Expanding the material time derivative in equation (31.26) into its Eulerian components leads to

$$\frac{\partial}{\partial t}(\mathcal{K} + \mathcal{P}) + \mathbf{u} \cdot \nabla (\mathcal{K} + \mathcal{P}) = -g h \rho \mathbf{u} \cdot \nabla \eta - \mathcal{K} \nabla \cdot \mathbf{u} + g h \rho (w_b - \eta \nabla \cdot \mathbf{u}), \quad (31.27)$$

with rearrangement rendering

$$\frac{\partial}{\partial t}(\mathcal{K} + \mathcal{P}) + \nabla \cdot [\mathbf{u} (\mathcal{K} + \mathcal{P})] = \mathcal{P} \nabla \cdot \mathbf{u} - g h \rho \mathbf{u} \cdot \nabla \eta + g h \rho (w_b - \eta \nabla \cdot \mathbf{u}) \quad (31.28a)$$

$$= (\mathcal{P} - g h \rho \eta) \nabla \cdot \mathbf{u} + g h \rho (w_b - \mathbf{u} \cdot \nabla \eta) \quad (31.28b)$$

$$= -(g \rho h^2/2) \nabla \cdot \mathbf{u} + g h \rho (w_b - \mathbf{u} \cdot \nabla \eta) \quad (31.28c)$$

$$= -\nabla \cdot (\mathbf{u} g \rho h^2/2) + g \rho h \mathbf{u} \cdot \nabla h + g h \rho (w_b - \mathbf{u} \cdot \nabla \eta) \quad (31.28d)$$

$$= -\nabla \cdot (\mathbf{u} g \rho h^2/2) + g \rho h (\mathbf{u} \cdot \nabla (h - \eta) + w_b) \quad (31.28e)$$

$$= -\nabla \cdot (\mathbf{u} g \rho h^2/2) + g \rho h (-\mathbf{u} \cdot \nabla \eta_b + w_b) \quad (31.28f)$$

$$= -\nabla \cdot (\mathbf{u} g \rho h^2/2), \quad (31.28g)$$

where we used the identity

$$w_b = \frac{D\eta_b}{Dt} = \mathbf{u} \cdot \nabla \eta_b, \quad (31.29)$$

which follows since  $\partial \eta_b / \partial t = 0$ . We are thus left with the conservation law

$$\frac{\partial \mathcal{E}}{\partial t} + \nabla \cdot \mathbf{F} = 0, \quad (31.30)$$

which has the expression

$$\frac{\partial}{\partial t}(\mathcal{K} + \mathcal{P}) + \nabla \cdot [\mathbf{u} (\mathcal{K} + \mathcal{P} + g \rho h^2/2)] = 0, \quad (31.31)$$

where the total mechanical energy is

$$\mathcal{E} = \mathcal{K} + \mathcal{P} = \frac{1}{2} \rho h \mathbf{u} \cdot \mathbf{u} + \frac{1}{2} \rho g (\eta^2 - \eta_b^2), \quad (31.32)$$

and the flux of mechanical energy is

$$\mathbf{F} = \mathbf{u} (\mathcal{K} + \mathcal{P} + g \rho h^2/2) = \mathbf{u} (\mathcal{K} + \rho g \eta h). \quad (31.33)$$

Recall in our discussion of total energy for a continuously stratified fluid in Section 21.6.1, where we identified the mechanical injection work term that appears in the energy flux in addition to the advection of energy. Here, that term is given by  $g \rho h^2/2$  for the shallow water fluid.

### 31.3.4 Available potential energy

As discussed in Section 23.8, a huge portion of the gravitational potential energy is not realizable as kinetic energy, merely because the minimum potential energy state is when the fluid is at rest with some fluid parcels sitting above others. Available potential energy measures that amount of the gravitational potential energy that can be converted to kinetic energy through a reversible rearrangement of the fluid. We here display the available potential energy for a single shallow water layer, thus specializing the more general discussion given in Section 23.8.

The gravitational potential energy for a single shallow water layer is given by

$$P = g \rho \int dA \int_0^\eta z dz = \frac{g \rho}{2} \int \eta^2 dA, \quad (31.34)$$

where  $\int dA$  is the horizontal integral over the full domain of the fluid and we choose to measure the potential energy relative to  $z = 0$ . The background or reference potential energy is realized by relaxing the free surface interface to its uniform area average value,  $z = \bar{\eta}$  (see Figure 30.1), so that

$$P_{\text{ref}} = \frac{g \rho}{2} \int \bar{\eta}^2 dA = \frac{g \rho}{2} \bar{\eta}^2 A. \quad (31.35)$$

The available potential energy is the difference

$$E_{\text{APE}} = P - P_{\text{ref}} = \frac{g \rho}{2} \int (\eta^2 - \bar{\eta}^2) dA = \frac{g \rho}{2} \int (\eta')^2 dA \geq 0, \quad (31.36)$$

where

$$\eta' = \eta - \bar{\eta} \quad (31.37)$$

is the anomalous free surface. Equation (31.36) shows that the APE is non-negative for the shallow water layer. That is, any slope to the shallow water layer represents a store of positive APE. We derive the APE for a single shallow water layer with bottom topography in Exercise 31.8 and for two layers in Exercise 31.9. In both cases we find the APE is non-negative.

## 31.4 Thickness weighted momentum equation

Throughout our discussion of the shallow water model, we have made use of the prognostic equation for the velocity of a layer. Here, we study the momentum equation as determined by the depth integrated velocity in a shallow water layer. This formulation proves particularly useful when studying forces acting on the layer, such as those from pressure form stresses, and is of use for studies of rotating hydraulics such as pursued in the monograph by [Pratt and Whitehead \(2008\)](#).

For a single layer, the shallow water column extends from the surface to the bottom of the layer (see Figure 31.5)

$$\int_{\eta_b}^{\eta} \mathbf{u} dz = \mathbf{u} h, \quad (31.38)$$

so that the column momentum equals to  $\mathbf{u} h \rho dx dy$ . The resulting momentum equation is written in an Eulerian flux form. Doing so facilitates analysis of forces acting on the layer and hence of the layer momentum budget. In Section 31.6 we illustrate the momentum budget for a zonal channel. We also show in Section 31.5.2 that the  $N$ -layer equations are isomorphic to the single layer, thus allowing for concepts developed for a single layer to be readily extended to multiple layers.

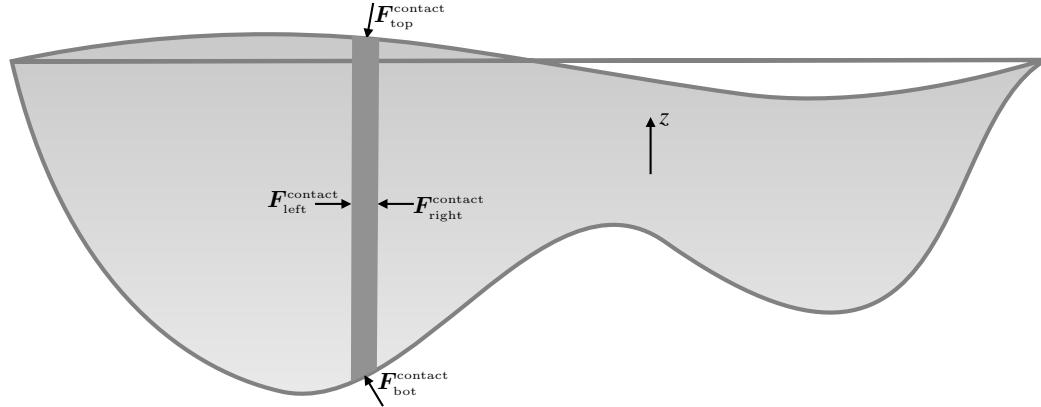


FIGURE 31.5: Momentum of a column of a single layer shallow water fluid is affected by contact forces at the column boundaries (pressure and friction), as well as body forces acting throughout the column (Coriolis and gravity).

### 31.4.1 Single layer equations

Recall the velocity and thickness equations written using the material time operator

$$\frac{D\mathbf{u}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -g \nabla \eta \quad \text{and} \quad \frac{Dh}{Dt} = -h \nabla \cdot \mathbf{u}. \quad (31.39)$$

Combining these two equations allows us to write the thickness weighted material acceleration as

$$h \frac{D\mathbf{u}}{Dt} = h \frac{D\mathbf{u}}{Dt} + \mathbf{u} \left[ \frac{Dh}{Dt} + h \nabla \cdot \mathbf{u} \right] = \frac{\partial(h \mathbf{u})}{\partial t} + \nabla \cdot [h \mathbf{u} \otimes \mathbf{u}], \quad (31.40)$$

so that the thickness weighted equation takes the vector form

$$\frac{\partial(h \mathbf{u})}{\partial t} + \nabla \cdot [h \mathbf{u} \otimes \mathbf{u}] + f \hat{\mathbf{z}} \times (h \mathbf{u}) = -g h \nabla \eta. \quad (31.41)$$

The Cartesian tensor form of the outer product is<sup>2</sup>

$$[\mathbf{u} \otimes \mathbf{u}]_{mn} = u_m u_n \quad \text{for } m, n = 1, 2, \quad (31.42)$$

with  $h \mathbf{u} \otimes \mathbf{u}$  the specialization to the shallow water system of the *kinetic stress* appearing in the continuously stratified momentum equation (18.56). The component form of the thickness weighted momentum equation (31.41) is

$$\frac{\partial(h u)}{\partial t} + \partial_x(h u^2) + \partial_y(h u v) - v h f = -g h \partial_x \eta \quad (31.43a)$$

$$\frac{\partial(h v)}{\partial t} + \partial_x(h u v) + \partial_y(h v^2) + u h f = -g h \partial_y \eta. \quad (31.43b)$$

Note that when the bottom is flat then  $\nabla h = \nabla \eta$  so that we have

$$\frac{\partial(h u)}{\partial t} + \partial_x(h u^2 + g h^2/2) + \partial_y(h u v) - v h f = 0 \quad (31.44a)$$

$$\frac{\partial(h v)}{\partial t} + \partial_x(h u v) + \partial_y(h v^2 + g h^2/2) + u h f = 0. \quad (31.44b)$$

<sup>2</sup>Equation (31.42) is the only place in this chapter where a subscript refers to a tensor label. Otherwise, subscripts refer to a shallow water layer index as in Section 31.5.2.

### 31.4.2 Geostrophic and ageostrophic contributions

Bringing the Coriolis terms to the right hand side of equations (31.43a) and (31.43b) renders

$$\frac{\partial(h u)}{\partial t} + \partial_x(h u^2) + \partial_y(h u v) = h(-g \partial_x \eta + v f) \quad (31.45a)$$

$$\frac{\partial(h v)}{\partial t} + \partial_x(h u v) + \partial_y(h v^2) + u h f = h(-g \partial_y \eta - u f). \quad (31.45b)$$

In the absence of rotation, the right hand side has contributions only from the thickness weighted pressure gradient. For the case of rotation it sometimes proves useful to decompose velocity into its geostrophic and ageostrophic components

$$f u = f(u_a + u_g) = f u_a - g \partial \eta / \partial y \quad (31.46a)$$

$$f v = f(v_a + v_g) = f v_a + g \partial \eta / \partial x, \quad (31.46b)$$

in which case equations (31.45a) and (31.45b) become

$$\frac{\partial(h u)}{\partial t} + \partial_x(h u^2) + \partial_y(h u v) = h f v_a \quad (31.47a)$$

$$\frac{\partial(h v)}{\partial t} + \partial_x(h u v) + \partial_y(h v^2) = -h f u_a. \quad (31.47b)$$

One should be careful *not* to take the  $f = 0$  limit of these equations since one might spuriously conclude there is no free surface contribution. Instead, equations (31.45a) and (31.45b) should be the basis for the  $f = 0$  limit.

### 31.4.3 Form stresses acting on a shallow water column

The kinetic stress contributes to momentum evolution in equations (31.43a) and (31.43b) via its divergence. In contrast, the pressure stress contributes as a thickness weighted pressure gradient body stress. In this subsection, and in all of Section 31.5, we formulate pressure as a contact stress, in which case it also contributes to momentum evolution as a divergence. In so doing, we provide an Eulerian flux-form conservation law for momentum that supports analysis and interpretation.

*Reintroducing atmospheric pressure to symmetrize the forces acting on the layer*

To expose both the surface and bottom form stresses, we reintroduce the atmospheric pressure,  $p_a$ , and thus make use of the effective sea level (30.4)

$$\eta^{\text{eff}} = \eta + p_a / (\rho g) = \eta_b + h + p_a / (\rho g), \quad (31.48)$$

with the corresponding thickness weighted horizontal momentum equation

$$\frac{\partial(h \mathbf{u})}{\partial t} + \nabla \cdot [h \mathbf{u} \otimes \mathbf{u}] + f \hat{z} \times (h \mathbf{u}) = -g h \nabla \eta^{\text{eff}}. \quad (31.49)$$

*Exposing the contact pressure stresses*

The free surface height equals  $\eta = \eta_b + h$ , in which case the momentum equation (31.49) is

$$\frac{\partial(h \mathbf{u})}{\partial t} + \nabla \cdot [h \mathbf{u} \otimes \mathbf{u}] + f \hat{z} \times (h \mathbf{u}) = -(g/2) \nabla h^2 - g h \nabla [\eta_b + p_a / (\rho g)]. \quad (31.50)$$

To help interpret this equation it is convenient to write the boundary terms on the right hand side as

$$-g h \nabla[\eta_b + p_a/(\rho g)] = -\nabla(h p_a/\rho) + (p_a/\rho) \nabla(\eta - \eta_b) - g h \nabla\eta_b \quad (31.51a)$$

$$= -\nabla(h p_a/\rho) + (p_a/\rho) \nabla\eta - (g h + p_a/\rho) \nabla\eta_b \quad (31.51b)$$

$$= -\nabla(h p_a/\rho) + \rho^{-1} (p_a \nabla\eta - p_b \nabla\eta_b), \quad (31.51c)$$

so that

$$-(g/2) \nabla h^2 - g h \nabla[\eta_b + p_a/(\rho g)] = -\nabla[(g/2) h^2 + h p_a/\rho] + \rho^{-1} (p_a \nabla\eta - p_b \nabla\eta_b). \quad (31.52)$$

The first term on the right hand side is the gradient of the layer integrated hydrostatic pressure

$$P \equiv \int_{\eta_b}^{\eta} [p_a + \rho g (\eta - z)] dz = h (\rho g h/2 + p_a), \quad (31.53)$$

and the second term exposes the form stresses acting at the surface and bottom of the layer. With these expressions, the horizontal thickness weighted momentum equation (31.50) becomes

$$\frac{\partial(h \mathbf{u})}{\partial t} + \nabla \cdot [h \mathbf{u} \otimes \mathbf{u} + \mathbb{I} P/\rho] + f \hat{\mathbf{z}} \times (h \mathbf{u}) = (p_a \nabla\eta - p_b \nabla\eta_b)/\rho, \quad (31.54)$$

where  $\mathbb{I}$  is the unit tensor. Exposing the zonal and meridional components renders

$$\frac{\partial(h u)}{\partial t} + \partial_x(h u^2 + P/\rho) + \partial_y(h u v) - v h f = (p_a \partial_x\eta - p_b \partial_x\eta_b)/\rho \quad (31.55a)$$

$$\frac{\partial(h v)}{\partial t} + \partial_x(h u v) + \partial_y(h v^2 + P/\rho) + u h f = (p_a \partial_y\eta - p_b \partial_y\eta_b)/\rho. \quad (31.55b)$$

The horizontal pressure gradient appears as a continuous operator since we assumed an infinitesimal horizontal cross-sectional area for the fluid column. In contrast, the pressure form stresses appear as a vertical finite difference across the layer interfaces, which results since we are integrating over the thickness of a finite layer. Furthermore, note how the depth integrated pressure contributions appear in a flux-form, which contrasts to the body force version that appears as thickness weighted pressure gradient.

#### *Kinetic stresses and contact pressure stresses combined into a momentum flux*

To anticipate the thickness weighted momentum equation for the stacked shallow water model in Section 31.5, write the finite difference of the form stresses as

$$p_a \nabla\eta - p_b \nabla\eta_b = p_{1/2} \nabla\eta_{1/2} - p_{3/2} \nabla\eta_{3/2} \equiv \delta_k(p_{k-1/2} \nabla\eta_{k-1/2}). \quad (31.56)$$

We here introduced the layer interface difference operator

$$\delta_k(\Phi_{k-1/2}) = \Phi_{k-1/2} - \Phi_{k+1/2} = -(\Phi_{k+1/2} - \Phi_{k-1/2}), \quad (31.57)$$

with the backward difference motivated since  $k$  increases downward whereas  $\hat{\mathbf{z}}$  points upward. In the following, we choose to define the difference operator to only act on interface fields. Hence, any layer quantity, such as the layer thickness, commutes with the interface operator

$$\delta_k(h \Phi_{k-1/2}) = h (\Phi_{k-1/2} - \Phi_{k+1/2}). \quad (31.58)$$

With the above notation, the component momentum equations (31.55a) and (31.55b) take on the matrix-vector form

$$\begin{bmatrix} \partial_t(h u) - h f v \\ \partial_t(h v) + h f u \end{bmatrix} = - \begin{bmatrix} \partial_x & \partial_y & h^{-1} \delta_k \end{bmatrix} \begin{bmatrix} D_1^{(u)} & D_1^{(v)} & 0 \\ D_2^{(u)} & D_2^{(v)} & 0 \\ D_3^{(u)} & D_3^{(v)} & 0 \end{bmatrix}. \quad (31.59)$$

The  $3 \times 3$  matrix is a second order tensor with the first and second columns consisting of the momentum fluxes

$$\mathbf{D}^{(u)} = (h u^2 + P/\rho) \hat{\mathbf{x}} + h u v \hat{\mathbf{y}} - (p_{k-1/2} \partial_x \eta_{k-1/2}/\rho) h \hat{\mathbf{z}} \quad (31.60a)$$

$$\mathbf{D}^{(v)} = h u v \hat{\mathbf{x}} + (h v^2 + P/\rho) \hat{\mathbf{y}} - (p_{k-1/2} \partial_y \eta_{k-1/2}/\rho) h \hat{\mathbf{z}}, \quad (31.60b)$$

where we suppressed unnecessary layer indices. The horizontal flux components are given by minus the thickness weighted kinetic stress,  $h \mathbf{u} \otimes \mathbf{u}$ , plus the depth integrated contact pressure acting on the vertical sides of the shallow water column. The vertical flux component contains the pressure form stresses acting on the top and bottom interfaces, with these interfacial form stresses leading to the vertical transfer of horizontal form stresses across the layer boundaries. These fluxes allow us to write the thickness weighted zonal and meridional momentum equations as

$$\frac{\partial(h u)}{\partial t} - v h f = -(\hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y + \hat{\mathbf{z}} h^{-1} \delta_k) \cdot \mathbf{D}^{(u)} \quad (31.61a)$$

$$\frac{\partial(h v)}{\partial t} + u h f = -(\hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y + \hat{\mathbf{z}} h^{-1} \delta_k) \cdot \mathbf{D}^{(v)}. \quad (31.61b)$$

In this form of the momentum equation, contributions from contact stresses (kinetic stresses and form stresses) appear as the convergence of these stresses with the divergence operator built as combination of the continuous horizontal gradient operator along with a finite difference vertical operator. The third column of the tensor (31.59) is identically zero and so it can be readily dropped. However, we include it to connect with the *Eliassen-Palm flux tensor* as detailed by [Maddison and Marshall \(2013\)](#). We return to equations (31.61a) and (31.61b) in Section 31.5.9 for the stacked shallow water model.

#### 31.4.4 Comments on the two pressure force formulations

The momentum equations (31.61a) and (31.61b) are written as a flux-form Eulerian conservation law, with only the Coriolis force appearing as a body force. This formulation follows that for Cauchy's equation of motion as discussed in Section 17.1.3. We make use of these flux-form momentum equations in Section 31.6 when discussing force balances in a zonally periodic channel, as well as in Chapter 45 when formulating the thickness weighted averaged shallow water equations. Before doing so, we focus in Section 31.5 by further unpacking the contact force version of pressure as it appears in the shallow water model.

What has been gained by writing the momentum equation as the thickness weighted forms (31.61a) and (31.61b) versus the non-flux form velocity equation (31.39)? Indeed, the thickness weighted formulation is arguably less elegant and takes more effort to derive. A key reason we consider the thickness weighted equations is that they provide a venue to study how pressure contact forces alter momentum of a shallow water fluid column through interactions with the bottom, the surface, and adjacent vertical columns. We put this perspective to use in Section 31.6 when studying the force balances on a zonally reentrant channel. Additionally, in Section 31.5

we further pursue the contact force perspective by studying how pressure form stresses appear within a stacked shallow water model.

## 31.5 Contact pressure forces in shallow water layers

For a finite region of fluid, if the boundary area integrated contact pressure stress is nonzero, then pressure accelerates the region. In this section we study the physics and maths of contact pressure forces as they appear in the stacked shallow water model. As revealed by this study, the columnar motion of the shallow water fluid is fundamental to the analysis. Namely, the contact pressure approach is realized by studying the thickness weighted velocity equations of motion, which determine evolution of the momentum per horizontal area of a shallow water fluid column. We introduced the thickness weighted approach in Section 31.4 for a single shallow water layer, and it led to the flux-form Eulerian momentum equations (31.61a) and (31.61b). The single layer results are reproduced here for the stacked shallow water model, yet only after furthering our understanding of how pressure forces act to move momentum through shallow water layers.

### 31.5.1 Pressure contact force and pressure body force

As discussed in Section 18.1.3, the connection between the body force and contact force expressions of the pressure force arise through an application of Gauss's divergence theorem to scalar fields (see Section 2.7.2)

$$\mathbf{F}_{\mathcal{R}}^{\text{press}} = - \int_{\mathcal{R}} \nabla p \, dV = - \oint_{\partial\mathcal{R}} p \hat{\mathbf{n}} \, dS. \quad (31.62)$$

The first expression on the right hand side is a volume integral of the pressure gradient over the fluid region,  $\mathcal{R}$ . This expression provides the body force version of the pressure force. The second expression is a surface area integral over the region boundary,  $\partial\mathcal{R}$ , whose outward normal is  $\hat{\mathbf{n}}$ . This second expression provides the contact force version of the pressure force. Neither expression is more or less fundamental. Instead, they offer complementary insights into how pressure acts to modify the momentum of a fluid, with general notions of this complementarity the topic of Chapter 19. We here pursue the contact force perspective as a means to understand the *pressure form stress* or *interfacial form stress* acting between layers of a shallow water fluid. There is also a pressure form stress acting between a fluid layer and the solid earth (topographic form stress), as well as between a fluid layer and the overlying atmosphere when the atmosphere has a non-zero mass (atmosphere form stress).

### 31.5.2 $N$ -layer equations

Our starting point for the development in this section are the  $N$ -layer shallow water thickness and velocity equations derived in Section 30.4.2

$$\frac{\partial h_k}{\partial t} + \nabla \cdot (h_k \mathbf{u}_k) = 0 \quad \text{and} \quad [\partial_t + (\mathbf{u}_k \cdot \nabla)] \mathbf{u}_k + f \hat{z} \times \mathbf{u}_k = -(1/\rho_1) \nabla p_k, \quad (31.63)$$

where  $k = 1, N$  is the layer index with no implied summation over this index,  $\rho_1$  is the top layer density that also serves as the Boussinesq reference density, and equation (30.73) gives the horizontal pressure gradient acceleration. Equations (31.63) are isomorphic to the single layer equations considered in Section 31.4.1. Hence, the thickness weighted velocity equation is a simple generalization of the single layer equation (31.41)

$$\frac{\partial(h_k \mathbf{u}_k)}{\partial t} + \nabla \cdot [h_k \mathbf{u}_k \otimes \mathbf{u}_k] + f \hat{z} \times (h_k \mathbf{u}_k) = -(h_k/\rho_1) \nabla p_k, \quad (31.64)$$

where, again, there is no implied summation over the layer index,  $k$ . We commonly refer to the thickness weighted equation (31.64) as the momentum equation since  $\rho dx dy h_k \mathbf{u}_k$  is the horizontal momentum of a shallow water fluid column,

### 31.5.3 Contact pressure force along vertical sides

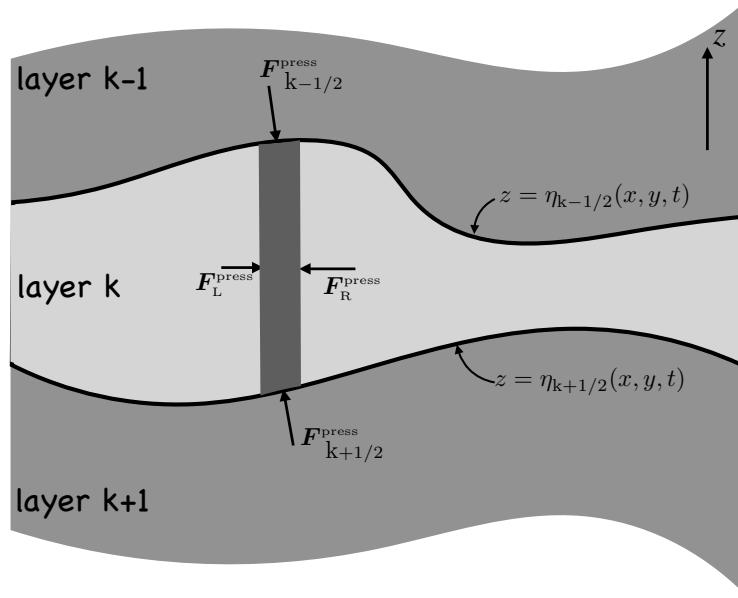


FIGURE 31.6: A schematic of the contact pressure force per area acting on the boundaries of a vertical column region within a shallow water layer of density  $\rho_k$ . Since fluid moves as vertical columns in a shallow water layer, we focus on the pressure forces acting on this column. The horizontal cross-sectional area of the column is depth independent. The interface at the lower boundary is at the vertical position  $z = \eta_{k+1/2}$ , and the upper interface is at  $z = \eta_{k-1/2}$ . In accordance with Newton's third law, pressures are continuous across each of the  $\eta_{k\pm 1/2}$  layer interfaces so that the pressure forces are equal in magnitude yet oppositely directed on the opposite sides to the interfaces. The layer thickness is the difference between the interface positions,  $h_k = \eta_{k-1/2} - \eta_{k+1/2}$ . The boundaries of the columnar region feel a contact pressure force acting inward. The left side of the column experiences a pressure  $p_L$ ; the right side experiences  $p_R$ ; the upper interface has a pressure  $p_{k-1/2}$  acting between the layer  $k-1$  and layer  $k$ , and the lower interface has a pressure  $p_{k+1/2}$  acting between the layer  $k+1$  and layer  $k$ . The net pressure acting on the column is computed as the area integral of the pressure acting around the full extent of the column boundaries. The horizontal components of the stress are known as *interfacial form stresses*. This figure is identical to Figure 19.5 used to discuss the general notions of pressure form stress.

We now build up our understanding of pressure form stresses acting in a stacked shallow water fluid, with the essence of this discussion following that encountered for the single layer in Section 31.4.3. Our interest concerns the pressure acting on the boundaries of a fluid column within a shallow water layer, such as shown in Figure 31.6.

The pressure at a vertical position within the shallow water layer- $k$  is given by

$$p_k(z) = \rho_k g (\eta_{k-1/2} - z) + p_{k-1/2}. \quad (31.65)$$

Integrating this pressure over the layer thickness yields

$$P_k \equiv \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} p_k(z) dz \quad (31.66a)$$

$$= g \rho_k \left[ \eta_{k-1/2} h_k - (1/2) (\eta_{k-1/2}^2 - \eta_{k+1/2}^2) \right] + p_{k-1/2} h_k \quad (31.66b)$$

$$= h_k (g \rho_k h_k / 2 + p_{k-1/2}). \quad (31.66c)$$

Since pressure is a linear function of  $z$  within a layer, the vertically averaged hydrostatic pressure within a layer,  $P_k/h_k$ , equals to the pressure at the upper interface,  $p_{k-1/2}$ , plus one-half the weight per area of the layer,  $g \rho_k h_k / 2$ .

The zonal pressure force acting on the column sides is the difference between the pressure integrated across the left and right zonal faces of the column. Assuming the fluid column to have an infinitesimal horizontal cross-sectional area  $dx dy$ , we find the zonal pressure force is given by

$$dy \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} (p_L - p_R) dz = -dx dy \left[ (g/2) \rho_k \frac{\partial h_k^2}{\partial x} + \frac{\partial (h_k p_{k-1/2})}{\partial x} \right] \quad (31.67a)$$

$$= -dx dy \partial_x [(g/2) \rho_k h_k^2 + h_k p_{k-1/2}] \quad (31.67b)$$

$$= -dx dy \partial_x P_k. \quad (31.67c)$$

The analogous result holds for the meridional direction, thus rendering the net contact pressure force acting on the vertical sides of the column

$$\mathbf{F}_{\text{sides}}^{\text{press}} = -dx dy \nabla P_k. \quad (31.68)$$

Hence, the contact force on the vertical sides of the column is given by the gradient of the layer vertically integrated pressure, with the vertical integral given by equation (31.66c). It is notable that this semi-discrete exercise reveals no more information than already contained within the integral theorem (31.62). Nonetheless, it is useful to see how the integral theorem manifests within discrete shallow water layers.

### 31.5.4 Contact pressure force along the top and bottom interfaces

Now consider the contact pressure force acting on the top interface. This interface is generally sloped, so that the contact force has a component in both the vertical and horizontal directions. The vertical component to the pressure force maintains hydrostatic balance with the contact pressure at the lower boundary interface. The horizontal component provides a horizontal acceleration, with this acceleration (sign and magnitude) determined by the slope of the interface. Following our discussion in Section 19.3, we term the horizontal pressure acting on the sloped interface the *interfacial form stress*.

To mathematically characterize the pressure force on the top interface,  $z = \eta_{k-1/2}$ , requires the outward normal

$$\hat{\mathbf{n}}_{k-1/2} = \frac{\nabla (z - \eta_{k-1/2})}{|\nabla (z - \eta_{k-1/2})|} = \frac{\hat{\mathbf{z}} - \nabla \eta_{k-1/2}}{\sqrt{1 + (\nabla \eta_{k-1/2})^2}}. \quad (31.69)$$

Temporarily assume the interface slope to have a zero projection in the  $\hat{\mathbf{y}}$  direction. In this case,

the outward normal is

$$\hat{\mathbf{n}}_{k-1/2} = \frac{\hat{\mathbf{z}} - \hat{\mathbf{x}} \partial_x \eta_{k-1/2}}{\sqrt{1 + (\partial_x \eta_{k-1/2})^2}} \quad (31.70a)$$

$$= \frac{\hat{\mathbf{z}} - \hat{\mathbf{x}} \tan \varphi_{k-1/2}}{\sqrt{1 + \tan^2 \varphi_{k-1/2}}} \quad (31.70b)$$

$$= (\hat{\mathbf{z}} - \hat{\mathbf{x}} \tan \varphi_{k-1/2}) \cos \varphi_{k-1/2}, \quad (31.70c)$$

where we defined the interface slope as

$$\frac{\partial \eta_{k-1/2}}{\partial x} = \tan \varphi_{k-1/2}, \quad (31.71)$$

with  $\varphi_{k-1/2}$  the angle between the horizontal plane and the interface. Trigonometry leads to an expression for the area of the top of the column<sup>3</sup>

$$d\mathcal{S}_{k-1/2} = \frac{dx dy}{\cos \varphi_{k-1/2}}, \quad (31.72)$$

so that the product of the area and the outward normal is given by

$$\hat{\mathbf{n}}_{k-1/2} d\mathcal{S}_{k-1/2} = dx dy (\hat{\mathbf{z}} - \hat{\mathbf{x}} \partial_x \eta_{k-1/2}). \quad (31.73)$$

This result generalizes to an interface slope that projects into both horizontal directions

$$\hat{\mathbf{n}}_{k-1/2} d\mathcal{S}_{k-1/2} = dx dy (\hat{\mathbf{z}} - \nabla \eta_{k-1/2}), \quad (31.74)$$

so that the contact pressure force acting on layer-k at its top interface is given by

$$\mathbf{F}_{\text{top}}^{\text{press}} = -dx dy (\hat{\mathbf{z}} - \nabla \eta_{k-1/2}) p_{k-1/2}. \quad (31.75)$$

Analogous considerations lead to the contact pressure force acting on layer-k at the bottom of the column

$$\mathbf{F}_{\text{bot}}^{\text{press}} = dx dy (\hat{\mathbf{z}} - \nabla \eta_{k+1/2}) p_{k+1/2}. \quad (31.76)$$

### 31.5.5 Form stress

As noted earlier, form stress is the horizontal projection of the contact pressure acting on the sloped top or bottom interface of the fluid column (Chapter 19). The corresponding forces acting on layer-k is the horizontal area element multiplied by the form stress

$$\mathbf{F}_{\text{top face}}^{\text{form stress}} = dx dy (p_{k-1/2} \nabla \eta_{k-1/2}) \quad (31.77)$$

$$\mathbf{F}_{\text{bot face}}^{\text{form stress}} = -dx dy (p_{k+1/2} \nabla \eta_{k+1/2}). \quad (31.78)$$

These forces render a mechanically reversible vertical exchange of horizontal momentum. This momentum exchange occurs without any exchange of matter. Rather, it is an inviscid exchange that occurs according to Newton's third law principle of action/reaction.

For a specific case, consider a  $k - 1/2$  interface that slopes upward in the  $\hat{\mathbf{x}}$  direction (e.g.,

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<sup>3</sup>Equation (31.72) was also found in Section 14.4.3 when developing the kinematic boundary condition for a material interface.

see Figure 31.6). Form stress acting at the interface provides a  $+\hat{x}$  directed acceleration on the column. For the  $k + 1/2$  interface, a negatively sloped interface also experiences a  $+\hat{x}$  directed acceleration.

### 31.5.6 Net contact pressure force on a shallow water column

Summing the contact pressure forces (31.68), (31.75), and (31.76), and dividing by the horizontal area, leads to the net pressure force per horizontal area acting on a column within layer-k

$$\frac{\mathbf{F}_{\text{net},k}^{\text{press}}}{dx dy} = -\nabla P_k - (\hat{z} - \nabla \eta_{k-1/2}) p_{k-1/2} + (\hat{z} - \nabla \eta_{k+1/2}) p_{k+1/2} \quad (31.79a)$$

$$= \rho_k g \hat{z} - \nabla P_k + p_{k-1/2} \nabla \eta_{k-1/2} - p_{k+1/2} \nabla \eta_{k+1/2}. \quad (31.79b)$$

To reach this result we made use of the hydrostatic relation for the vertical pressure difference across a layer

$$p_{k+1/2} - p_{k-1/2} = \rho_k g h_k, \quad (31.80)$$

and introduced the mass of a column within layer k

$$M_k = g \rho_k h_k dx dy. \quad (31.81)$$

The vertical component of the net contact pressure force balances the weight of the column within the layer, which is expected since the shallow water fluid is in hydrostatic balance. The horizontal contact pressure force arises from a horizontal gradient plus the form stress at the surface and bottom interfaces. The gradient term is removed when integrating horizontally over the full domain given that the thickness of the layer vanishes upon reaching the coastlines (e.g., see Figure 19.7). The resulting net force on the full domain arises just from the weight of the fluid acting in the vertical, plus form stress at the surface and bottom. We discuss this point more in Section 31.5.7.

### 31.5.7 Contact pressure force summed over all layers

Summing the contact pressure force (31.79b) over all layers reveals the contact forces on the interior layer interfaces vanish, as per Newton's third law (see Section 19.1), thus leaving just the form stress at the surface and bottom and the contact pressure force acting on the vertical sides. Dividing by the horizontal area of the column leads to the net pressure force per area

$$\frac{1}{dx dy} \sum_{k=1}^N \mathbf{F}_{\text{net},k}^{\text{press}} = g \hat{z} \sum_{k=1}^N \rho_k h_k + p_a \nabla \eta_{1/2} - p_b \nabla \eta_b - \sum_{k=1}^N \nabla P_k \quad (31.82a)$$

$$= (p_b - p_a) \hat{z} + p_a \nabla \eta_{1/2} - p_b \nabla \eta_b - \sum_{k=1}^N \nabla P_k, \quad (31.82b)$$

where we wrote the total mass per area within the column as the difference between the bottom pressure and applied surface pressure

$$\sum_{k=1}^N \rho_k h_k = (p_b - p_a)/g. \quad (31.83)$$

The horizontal components to the applied and bottom pressure terms in equation (31.82b) arise from pressure form stresses applied to the interfaces at the top and bottom of the column. The

vertical component arises from the net weight per area of the fluid. The summation term is the horizontal gradient of the depth integrated pressure form stress applied along the vertical sides of the column.

### 31.5.8 Horizontal pressure force with potential energy gradients

There is another means to express the horizontal pressure force. Here, we expose the gravitational potential energy per horizontal area for a column of fluid within a shallow water layer

$$\mathcal{P}_k = g \rho_k \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} z dz = (g \rho_k / 2) (\eta_{k-1/2}^2 - \eta_{k+1/2}^2). \quad (31.84)$$

Use of the layer gravitational potential energy brings the layer vertical integral of the hydrostatic pressure from Section 31.5.3 into

$$\int_{\eta_{k+1/2}}^{\eta_{k-1/2}} p_k(z) dz = g \rho_k h_k^2 / 2 + h_k p_{k-1/2} = \mathcal{P}_k - g \rho_k h_k \eta_{k+1/2} + h_k p_{k-1/2}. \quad (31.85a)$$

Making use of this result in equation (31.79b), along with a few lines of algebra, yields the net horizontal contact pressure force acting on a shallow water column

$$-\nabla P_k + \delta_k(p_{k-1/2} \nabla \eta_{k-1/2}) = -\nabla \mathcal{P}_k - \delta_k(\eta_{k-1/2} \nabla p_{k-1/2}). \quad (31.86)$$

To reach the identity (31.86) requires the hydrostatic relation,  $p_{k+1/2} - p_{k-1/2} = g \rho_k h_k$ , and the layer thickness,  $h_k = \eta_{k-1/2} - \eta_{k+1/2}$ . A consistency check notes that the curl of both sides to equation (31.86) are the same. The identity (31.86) suggests we define the form stress and its dual

$$\mathbf{F}^{\text{form}} = p \nabla \eta \quad \text{and} \quad \mathbf{F}^{\text{dual form}} = -\eta \nabla p. \quad (31.87)$$

These two stresses have the same curl, and thus impart the same pressure torque on a column of fluid (Chapter 34)

$$\nabla \times (p \nabla \eta) = \nabla \times (-\eta \nabla p). \quad (31.88)$$

However, these stresses are distinct and as such cannot be arbitrarily interchanged.<sup>4</sup>

### 31.5.9 Momentum equation with contact pressure forces

*Comparing the body force version and the contact force version*

Recall that the thickness weighted velocity equation (31.64), as written in terms of the pressure gradient body force, is given by<sup>5</sup>

$$\frac{\partial(h_k \mathbf{u}_k)}{\partial t} + \nabla \cdot [h_k \mathbf{u}_k \otimes \mathbf{u}_k] + f \hat{z} \times (h_k \mathbf{u}_k) = -(h_k / \rho_1) \nabla_z p_k, \quad (31.89)$$

<sup>4</sup>It is notable that much of the literature refers to  $-\eta \nabla p$  as the form stress rather than the dual form stress. This usage presumably originates from the common application of zonal averages for studying atmospheric motions, whereby  $\eta \partial_x p^x = -p \partial_x \eta^x$ . But this identity does not hold for arbitrary averaging operators so it is generally necessary to distinguish the form stress from the dual form stress.

<sup>5</sup>In equation (31.89) we wrote the gradient on the pressure as  $\nabla_z$  since we are only interested in the horizontal gradient acting on  $p_k(x, y, z)$ . All other objects in equation (31.89) are just a function of horizontal position within a layer, so that  $\nabla$  acting on them reduces to  $\nabla_z$ . Hence, the subscript on the gradient operator,  $\nabla_z$ , is exposed only when it acts on a function of  $z$ , such as for  $p_k(x, y, z)$ . Since  $p_k(x, y, z)$  is a linear function of  $z$ , its horizontal gradient is depth independent within the layer, as illustrated in Figure 30.1.

again with no implied summation over the layer label,  $k$ . Alternatively, we can make use of the net contact pressure force (31.79b) so that

$$\frac{\partial(h_k \mathbf{u}_k)}{\partial t} + \nabla \cdot (h_k \mathbf{u}_k \otimes \mathbf{u}_k + \mathbb{I} P_k / \rho_1) + f \hat{\mathbf{z}} \times (h_k \mathbf{u}_k) = \delta_k(p_{k-1/2} \nabla \eta_{k-1/2}) / \rho_1, \quad (31.90)$$

where  $\mathbb{I}$  is the identity tensor,  $P_k$  is the layer integrated pressure given by equation (31.66c), and  $\delta_k$  is the difference operator defined by equation (31.57). Choosing the contact pressure force as in equation (31.86) to expose the potential energy brings the momentum equation (31.90) into the alternative form

$$\frac{\partial(h_k \mathbf{u}_k)}{\partial t} + \nabla \cdot [h_k \mathbf{u}_k \otimes \mathbf{u}_k + \mathbb{I} \mathcal{P}_k / \rho_1] + f \hat{\mathbf{z}} \times (h_k \mathbf{u}_k) = -\delta_k(\eta_{k-1/2} \nabla p_{k-1/2}) / \rho_1. \quad (31.91)$$

Equations (31.89), (31.90), and (31.91) allow us to identify the body force and contact force versions of the thickness weighted horizontal pressure acceleration

$$-h_k \nabla_z p_k = -\nabla P_k + \delta_k(p_{k-1/2} \nabla \eta_{k-1/2}) = -\nabla \mathcal{P}_k - \delta_k(\eta_{k-1/2} \nabla p_{k-1/2}). \quad (31.92)$$

#### *The balance of pressure torques acting on a shallow water column*

A necessary (but not sufficient) check of the identity (31.92) can be found by verifying that the curl agrees for each expression

$$-\nabla \times \delta_k(\eta_{k-1/2} \nabla p_{k-1/2}) = \nabla \times \delta_k(p_{k-1/2} \nabla \eta_{k-1/2}) \quad (31.93a)$$

$$= \delta_k[\nabla \times (p_{k-1/2} \nabla \eta_{k-1/2})] \quad (31.93b)$$

$$= \delta_k[\nabla p_{k-1/2} \times \nabla \eta_{k-1/2}] \quad (31.93c)$$

$$= \nabla p_{k-1/2} \times \nabla \eta_{k-1/2} - \nabla(p_{k-1/2} + g \rho_k h_k) \times \nabla \eta_{k+1/2} \quad (31.93d)$$

$$= \nabla p_{k-1/2} \times \nabla h_k - g \rho_k \nabla h_k \times \nabla \eta_{k+1/2} \quad (31.93e)$$

$$= \nabla(p_{k-1/2} + g \rho_k \eta_{k+1/2}) \times \nabla h_k \quad (31.93f)$$

$$= \nabla(p_{k-1/2} - g \rho_k h_k + g \rho_k \eta_{k-1/2}) \times \nabla h_k \quad (31.93g)$$

$$= \nabla_z[p_{k-1/2} + g \rho_k (\eta_{k-1/2} - z)] \times \nabla h_k \quad (31.93h)$$

$$= \nabla_z p_k \times \nabla h_k \quad (31.93i)$$

$$= -\nabla \times (h_k \nabla_z p_k), \quad (31.93j)$$

which concurs with the curl of the left hand side of equation (31.92). To reach this result we set  $h_k = \eta_{k-1/2} - \eta_{k+1/2}$  and used equation (31.65) for the pressure within a shallow water layer:  $p_k(z) = \rho_k g (\eta_{k-1/2} - z) + p_{k-1/2}$ .

Anticipating our discussion of vorticity for the shallow water fluid in Section 34.2, we observe that the identity derived above

$$\nabla \times \delta_k(p_{k-1/2} \nabla \eta_{k-1/2}) = -\nabla \times (h_k \nabla_z p_k) \quad (31.94)$$

says that the difference in interfacial pressure torques acting on the top and bottom of a shallow water layer precisely balances minus the torque arising from the thickness weighted horizontal pressure gradient acting within the layer. This rather remarkable fine tuning of the interfacial and interior pressure torques is a direct consequence of assuming that the fluid motion is restricted to extensible vertical columns within each shallow water layer. This balance is not maintained within a three dimensional fluid, where fluid columns can generally tilt and bend (Chapter 35).

*Layer summed momentum equation*

Taking the vertical sum of the layer-k momentum equation (31.90) leads to the column integrated horizontal momentum equation

$$\frac{\partial \mathbf{U}}{\partial t} + f \hat{\mathbf{z}} \times \mathbf{U} + \nabla \cdot \left[ \sum_{k=1}^N (h_k \mathbf{u}_k \otimes \mathbf{u}_k + \mathbb{I} P_k / \rho_1) \right] = [p_a \nabla \eta_{1/2} - p_b \nabla \eta_b] / \rho_1, \quad (31.95)$$

where  $\mathbf{U}$  is the depth integrated horizontal velocity given by equation (31.11). The same vertical sum for equation (31.91) leads to

$$\frac{\partial \mathbf{U}}{\partial t} + f \hat{\mathbf{z}} \times \mathbf{U} + \nabla \cdot \left[ \sum_{k=1}^N (h_k \mathbf{u}_k \otimes \mathbf{u}_k + \mathbb{I} \mathcal{P}_k / \rho_1) \right] = [-\eta_{1/2} \nabla p_a + \eta_b \nabla p_b] / \rho_1. \quad (31.96)$$

The right hand side of equations (31.95) and (31.96) exposes the pressure form stresses (and dual form stresses) acting on the ocean surface and bottom.

*Decomposing into depth averaged and depth deviation velocities*

For detailed analyses of the depth integrated (layer summed) momentum and vorticity budgets, it is of interest to introduce the depth averaged operator and its deviation

$$\bar{\Phi}^z = \frac{\sum_{k=1}^N h_k \Phi_k}{\sum_{k=1}^N h_k} \quad \text{and} \quad \Phi'_k = \Phi_k - \bar{\Phi}^z \quad (31.97)$$

so that the depth integrated kinetic stress in equation (31.95) is

$$\sum_{k=1}^N h_k \mathbf{u}_k \otimes \mathbf{u}_k = D [\bar{\mathbf{u}}^z \otimes \bar{\mathbf{u}}^z + \overline{\mathbf{u}' \otimes \mathbf{u}'^z}] \quad \text{where } D = \sum_{k=1}^N h_k. \quad (31.98)$$

The velocity  $\mathbf{u}'_k$  is the deviation from the layer-k velocity from the depth average velocity, and we refer to it as the *internal velocity*, whereas the depth averaged velocity,  $\bar{\mathbf{u}}^z$ , is the *external velocity*.<sup>6</sup> The identity (31.98) reveals that the depth integrated kinetic stress can be decomposed into a stress arising from internal-internal velocity interactions plus external-external velocity interactions. By construction, there are no cross-terms (i.e., no internal-external terms) appearing in this depth integrated stress.

*Momentum fluxes*

Following the single layer discussion in Section 31.4.3, we write the momentum equation (31.90) in the form

$$\frac{\partial(h u)}{\partial t} - v h f = -(\hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y + \hat{\mathbf{z}} h^{-1} \delta_k) \cdot \mathbf{D}^{(u)} \quad (31.99a)$$

$$\frac{\partial(h v)}{\partial t} + u h f = -(\hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y + \hat{\mathbf{z}} h^{-1} \delta_k) \cdot \mathbf{D}^{(v)}, \quad (31.99b)$$

<sup>6</sup>It is also common in the oceanography literature to refer to  $\mathbf{u}'_k$  as the *baroclinic velocity* and  $\bar{\mathbf{u}}^z$  as the *barotropic velocity*.

where we dropped the  $k$  label for brevity and introduced the layer momentum fluxes

$$\mathbf{D}^{(u)} = (h u^2 + P/\rho_1) \hat{\mathbf{x}} + h u v \hat{\mathbf{y}} - (p_{k-1/2} \partial_x \eta_{k-1/2}/\rho_1) h \hat{\mathbf{z}} \quad (31.100a)$$

$$\mathbf{D}^{(v)} = h u v \hat{\mathbf{x}} + (h v^2 + P/\rho_1) \hat{\mathbf{y}} - (p_{k-1/2} \partial_y \eta_{k-1/2}/\rho_1) h \hat{\mathbf{z}}. \quad (31.100b)$$

Likewise, we can write the momentum equation (31.91) in the component form

$$\frac{\partial(h u)}{\partial t} - v h f = -(\hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y + \hat{\mathbf{z}} h^{-1} \delta_k) \cdot \mathbf{E}^{(u)} \quad (31.101a)$$

$$\frac{\partial(h v)}{\partial t} + u h f = -(\hat{\mathbf{x}} \partial_x + \hat{\mathbf{y}} \partial_y + \hat{\mathbf{z}} h^{-1} \delta_k) \cdot \mathbf{E}^{(v)}, \quad (31.101b)$$

where the dual layer momentum fluxes are given by

$$\mathbf{E}^{(u)} = (h u^2 + \mathcal{P}/\rho_1) \hat{\mathbf{x}} + h u v \hat{\mathbf{y}} + (\eta_{k-1/2} \partial_x p_{k-1/2}/\rho_1) h \hat{\mathbf{z}} \quad (31.102a)$$

$$\mathbf{E}^{(v)} = h u v \hat{\mathbf{x}} + (h v^2 + \mathcal{P}/\rho_1) \hat{\mathbf{y}} + (\eta_{k-1/2} \partial_y p_{k-1/2}/\rho_1) h \hat{\mathbf{z}}. \quad (31.102b)$$

Besides swapping the depth integrated pressure,  $P$ , for the potential energy,  $\mathcal{P}$ , the dual momentum fluxes,  $\mathbf{E}^{(u)}$  and  $\mathbf{E}^{(v)}$ , make use of the dual form stress,  $\eta_{k-1/2} \nabla p_{k-1/2}$ , rather than the form stress,  $-p_{k-1/2} \nabla \eta_{k-1/2}$ . Upon performing an eddy-mean flow decomposition as in Section 45.6, the eddy correlation portion of the fluxes (31.102a) and (31.102b) lead to the shallow water *Eliassen-Palm* fluxes, which are rows in the Eliassen-Palm flux tensor.

### 31.5.10 Further reading

[Ward and Hogg \(2011\)](#) and [Barthel et al. \(2017\)](#) offer pedagogical treatments of the stacked shallow water equations in the context of idealized simulations that lend insight into the dynamical balances. [Maddison and Marshall \(2013\)](#) study the Eliassen-Palm flux tensor for continuously stratified quasi-geostrophy as well as the Boussinesq hydrostatic equations.

## 31.6 Steady momentum balance in a zonal channel

In this section we study the depth integrated steady momentum budget for a shallow water layer in a zonally re-entrant channel as depicted in Figure 31.7. The results hold for a single layer and can be generalized to multiple layers. In theoretical oceanography, such shallow water models have been used to garner insights into the Southern Ocean circulation ( $f < 0$ ), and we keep this application in mind for the following. We are particularly interested in the force balances required to reach a steady state in the presence of a prescribed wind stress acceleration,  $\tau/\rho$ . The channel has arbitrary topography, including northern and southern bounds with sloping shelves and shorelines. Applying a zonal surface stress inserts zonal momentum to the fluid through the ocean surface. For simplicity we set the atmospheric pressure to zero,  $p_a = 0$ , so that the bottom pressure is  $p_b = \rho g h$ , and there is no form stress acting on the layer's upper surface.

A similar analysis was presented in Section 19.5 for the depth integrated axial angular momentum budget in a continuously stratified fluid. Following from that analysis, we ignore the role of internal viscous friction. However, we consider bottom frictional stresses written as a quadratic bottom drag

$$\mathbf{F}^{\text{drag}} = -C_d \mathbf{u} |\mathbf{u}|, \quad (31.103)$$

where  $C_d > 0$  is a dimensionless bottom drag coefficient.

The horizontal areal extent of the domain is a function of space and time since the shallow

water layer rises up and down the northern and southern shorelines as motion occurs. Even so, since layer thickness vanishes at the shoreline edge, the horizontal boundary conditions for the shallow water layer are easy to apply when working with the thickness weighted equations. That is, all thickness weighted fields vanish at the shoreline edge merely since the thickness vanishes at the edge. Indeed, working with thickness weighted fields allows us to handle any degree of vanishing layer thicknesses, including if the topography in the center of the channel becomes an island rather than a submerged seamount. We also made use of this property of thickness weighted budgets in Section 19.5 where we also considered sloping sides rather than the commonly considered, yet less realistic, vertical sides.

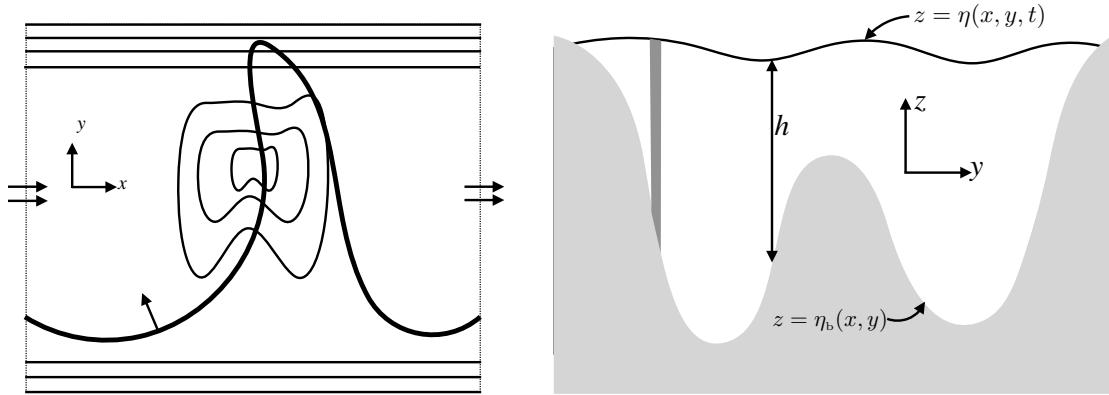


FIGURE 31.7: A zonally periodic/re-entrant southern hemisphere channel with northern and southern shelves and arbitrary seamount topography. Flow that leaves either the east or west boundary is assumed to re-enter the other side, so that the topology is periodic zonally. Left panel: horizontal (plan) view, showing the contours of the shelves and the topography, with flow leaving one of the zonal ends re-entering the other. The arbitrary dark solid contour extends across the zonal extent of the channel and is periodic, with a unit vector,  $\hat{n}$ , depicted normal to a point along the contour. In a steady state, the net fluid transport crossing this contour vanishes:  $\oint h \mathbf{u} \cdot \hat{n} ds = 0$ , meaning that there is no accumulation of fluid within any region of the channel. Right panel: meridional-depth view through an arbitrary longitude, along with a sample vertical column of water extending from the bottom to the surface. The shoreline edges occur where the layer thickness vanishes on the northern and southern shelves. So although the position of the shoreline edge is a function of space and time (since the fluid moves up and down the shoreline slope), the vanishing layer thickness found at the edge renders a simple treatment of boundary conditions for the thickness weighted equations.

### 31.6.1 Volume transport for steady flow

Before considering the steady force balance, we establish a constraint based on volume conservation by considering the steady thickness equation

$$\nabla \cdot (h \mathbf{u}) = 0. \quad (31.104)$$

As discussed for incompressible flow in Chapter 16, this non-divergence condition means that there is zero net steady transport crossing any simply connected closed contour in the fluid. A particularly interesting closed contour is one that is periodic and extends across the full zonal extent of the channel (see Figure 31.7), in which case

$$\oint h \mathbf{u} \cdot \hat{n} ds = 0, \quad (31.105)$$

where  $\oint$  denotes a periodic line integral across the zonal extent of the channel,  $\hat{n}$  is a unit vector normal to the contour, and  $ds$  is the arc-length line element along the contour. The constraint

(31.105) reflects the inability of the steady flow to build up or deplete the fluid on one region of the channel at the expense of another. In particular, if the contour follows a constant latitude line, then we see that for a steady state there is no net meridional transport across a latitude circle

$$\oint h \mathbf{u} \cdot \hat{\mathbf{y}} dx = \oint h v dx = 0 \quad \text{steady flow.} \quad (31.106)$$

In particular, this result means that the depth weighted Coriolis acceleration appearing in the zonal momentum equation vanishes when integrated zonally

$$\oint f h v dx = f \oint h v dx = 0 \quad \text{steady flow.} \quad (31.107)$$

We make use of this result in Section 31.6.3.

### 31.6.2 Steady meridional balances

Consider the meridional thickness weighted momentum equation (31.55b) in the presence of a wind stress and bottom drag

$$\frac{\partial(h v)}{\partial t} + \partial_x(h u v) + \partial_y(h v^2 + g h^2/2) + u h f = -(p_b/\rho) \partial_y \eta_b + \tau^y/\rho - C_d v |\mathbf{u}|. \quad (31.108)$$

Integrating zonally over the channel removes the zonal transport term,  $\partial_x(h u v)$ , due to periodicity

$$\oint \left[ \frac{\partial(h v)}{\partial t} + \partial_y(h v^2 + g h^2/2) + u h f \right] dx = \oint [-(p_b/\rho) \partial_y \eta_b + \tau^y/\rho - C_d v |\mathbf{u}|] dx. \quad (31.109)$$

We can pull the time derivative outside of the zonal integral since the domain is zonally periodic, in which case the time changes to the net meridional transport across a latitude circle are given by

$$\frac{d}{dt} \oint v h dx = \oint [-(\partial_y(h v^2 + g h^2/2) - u h f) - (p_b/\rho) \partial_y \eta_b + \tau^y/\rho - C_d v |\mathbf{u}|] dx. \quad (31.110)$$

Correspondingly, a steady state along a latitude circle is realized by the balance

$$\oint [\partial_y(h v^2 + g h^2/2) + u h f] dx = \oint [-(p_b/\rho) \partial_y \eta_b + \tau^y/\rho - C_d v |\mathbf{u}|] dx. \quad (31.111)$$

The right hand side represents forcing by the topographic form stress, winds, and bottom drag. That forcing, integrated over a latitude circle, balances the left hand side, which is the Coriolis acceleration arising from zonal motion, plus the meridional divergence of meridional momentum advection plus layer integrated pressure.

### 31.6.3 Steady zonal balance

Now consider the zonal momentum equation written in its flux-form (see equation (31.55a))

$$\frac{\partial(h u)}{\partial t} + \partial_x(h u^2 + g h^2/2) + \partial_y(h u v) - v h f = -(p_b/\rho) \partial_x \eta_b + \tau^x/\rho - C_d u |\mathbf{u}|. \quad (31.112)$$

Assuming a steady state and integrating along a latitude circle leads to

$$\rho \oint \partial_y(h u v) dx = \oint [-p_b \partial_x \eta_b + \tau^x - C_d \rho u |\mathbf{u}|] dx, \quad (31.113)$$

where we dropped the Coriolis acceleration as per volume conservation in equation (31.107). For flows that are quasi-linear, the nonlinear term  $\partial_y(h u v)$  will be subdominant to the wind stress and topographic form stress, thus leading to the approximate balance along each latitude circle

$$\oint p_b \partial_x \eta_b dx \approx \oint [\tau^x - C_d \rho u |\mathbf{u}|] dx \quad \text{nonlinear term small.} \quad (31.114)$$

We realize an exact balance over the full channel domain by integrating the latitude balance (31.113) meridionally, which allows us to drop the nonlinear term  $\partial_y(h u v)$  since  $h = 0$  at the northern and southern shoreline edges, thus leading to

$$\int \left[ \oint \tau^x dx \right] dy = \int \left[ \oint [p_b \partial_x \eta_b + C_d \rho u |\mathbf{u}|] dx \right] dy. \quad (31.115)$$

This is an exact steady state balance realized by integrating the zonal thickness weighted momentum equation over the full domain. It is a balance between the momentum input from the winds (left hand side) with the bottom form stress plus bottom frictional drag (right hand side).

### 31.6.4 The role of frictional bottom drag

Consider a flat bottom channel, in which case the area integrated balance (31.115) is between winds and bottom drag

$$\int \left[ \oint \tau^x dx \right] dy = \int \left[ \oint C_d \rho u |\mathbf{u}| dx \right] dy \implies \rho^{-1} \langle \tau^x \rangle = C_d \langle u |\mathbf{u}| \rangle, \quad (31.116)$$

where the angle brackets denote a channel area mean. Typical empirical values for the dimensionless bottom drag coefficient are

$$C_d \approx 2 \times 10^{-3}. \quad (31.117)$$

An area mean eastward zonal wind stress of  $\langle \tau^x \rangle = 0.1 \text{ N m}^{-2}$  leads to a root-mean-square zonal velocity of

$$\sqrt{\langle u |\mathbf{u}| \rangle} \approx \sqrt{\langle u^2 \rangle} \approx 0.2 \text{ m s}^{-1}, \quad (31.118)$$

where the first approximation follows from assuming the zonal velocity dominates over the meridional velocity. How realistic is this number for the Southern Ocean? Field measurements from the Southern Ocean suggest that depth and area averaged velocities are far smaller than this value. Furthermore, if this value occurred in a channel 4000 m deep and 2000 km wide (a rough idealization of the Antarctic Circumpolar Current), then this depth averaged velocity would yield a zonal volume transport of  $\approx 1500 \times 10^6 \text{ m}^3 \text{ s}^{-1}$ , which is about ten times larger than the measured transport through the Drake Passage.

*Munk and Palmén (1951)* identified the problematic aspect of assuming a bottom frictional stress balance for the Southern Ocean. In brief, the field measurements do not support a frictional balance, either from bottom drag or from internal turbulent viscous friction. By inference, they proposed that topographic form stress is the dominant term that balances wind stress in the Southern Ocean. They supported that inference through estimates based on topographic features encountered by the Antarctic Circumpolar Current in its transit of the Southern Ocean. Subsequent studies, using theory, field measurements, and numerical models, support their conclusion. Indeed, in numerical models one finds that so long as there is only a modest degree of bottom slope, the bottom topographic form stress dominates over bottom drag. Given these considerations, we dispense with bottom drag for the remainder of this section.

### 31.6.5 Correlation between surface height and topographic slope

Given the minor role for bottom drag in establishing a steady channel flow in the Southern Ocean, the balance (31.115) says that an eastward wind stress must be balanced, in the area integral over the channel, by a westward topographic form stress

$$\int \left[ \oint \tau^x dx \right] dy = \int \left[ \oint p_b \partial_x \eta_b dx \right] dy. \quad (31.119)$$

What is required to establish a westward topographic form stress? Quite simply, in the area mean, there must be an anomalously large bottom pressure in regions where  $\partial_x \eta_b > 0$  and an anomalously small bottom pressure in regions where  $\partial_x \eta_b < 0$ . Bottom pressure in a shallow water layer is determined by the column thickness. Hence, to establish the anomalous bottom pressures requires an anomalously thick fluid column upstream of topographic bumps and thin fluid column downstream. This situation is illustrated in Figure 31.8 described in Section 31.6.7.

To further reveal the correlation between surface height and bottom topography, write  $p_b = \rho g h$  and use  $\eta = h + \eta_b$  so that

$$p_{\text{bot}} \partial_x \eta_b = \rho g (\eta - \eta_b) \partial_x \eta_b = \rho g \eta \partial_x \eta_b - (g/2) \partial_x \eta_b^2. \quad (31.120)$$

The balance (31.119) thus becomes

$$\langle \tau^x \rangle = \rho g \langle \eta \partial_x \eta_b \rangle. \quad (31.121)$$

Furthermore, due to zonal periodicity, it is only the zonal anomalies in  $\eta$  and  $\eta_b$  that contribute so that

$$\langle \tau^x \rangle = \rho g \langle \eta' \partial_x \eta'_b \rangle, \quad (31.122)$$

where

$$\eta = \eta' + L^{-1} \oint \eta dx \quad \text{and} \quad \eta_b = \eta'_b + L^{-1} \oint \eta_b dx, \quad (31.123)$$

with  $L = \oint dx$  the zonal length of the channel. With  $\langle \tau^x \rangle > 0$ , we see that surface height anomalies must be positively correlated with the bottom slope,  $\int \eta' \partial_x \eta'_b dx dy > 0$ . That is, the surface height is high where topography slopes are positive and low where topography slopes are negative.

As noted above, we must have a positive correlation between surface height anomalies and topographic slope, as in equation (31.122). It follows that a nonzero zonal integrated topographic form stress requires a nonzero phase shift between surface height anomalies and the bottom topography anomalies. That is, if the surface height and bottom topography were perfectly aligned along a latitude circle, then  $\oint \eta' \partial_x \eta'_b dx = 0$ , in which case there is a zero zonal integrated topographic form stress along that latitude. The required phase shift between the free surface and bottom topography has the free surface shifted ahead (i.e., to the west) of the topography. We consider an explicit example in Section 31.6.7 to help in our understanding.

### 31.6.6 Connection to meridional geostrophic transport

Zonal periodicity allows us to write the balance (31.122) as

$$\langle \tau^x \rangle = -\rho g \langle \partial_x \eta' \eta'_b \rangle \quad (31.124)$$

For the large scale flows under consideration here, we can assume that  $g \partial_x \eta'$  is associated with an anomalous meridional geostrophic velocity

$$g \partial_x \eta' = f v'_g \quad (31.125)$$

so that the balance (31.124) is

$$\langle \tau^x \rangle = -\rho \langle f v'_g \eta'_b \rangle. \quad (31.126)$$

Hence, the steady balance is realized with anomalous meridional geostrophic transport correlated with topographic anomalies. Note that periodicity means that the steady meridional geostrophic transport has a zero zonal integral

$$\oint v'_g dx = (g/f) \oint \partial_x \eta' dx = 0, \quad (31.127)$$

which follows from the steady volume balance discussed in Section 31.6.1.

### 31.6.7 Sinusoidal example

To help further our understanding of the balance (31.122), and the phase shift required to develop nonzero zonal integrated topographic form stress, consider a sinusoidal topography that is a function only of the zonal direction. Also assume that the free surface has a sinusoidal shape (though we do not specify the dynamical mechanism for it to reach this shape). With these assumptions the anomalous surface height and bottom topography can be written

$$\eta' = \eta_o \sin(\kappa x + \varphi) \quad \text{and} \quad \eta'_b = D \sin(\kappa x) \quad (31.128)$$

where  $\eta_o > 0$  is a constant amplitude for the free surface undulations,  $D > 0$  is the constant amplitude for the bottom undulations,  $\kappa = 2\pi n/L$  is the wavenumber for the undulations,  $n > 0$  is an integer,  $L$  is the size of the zonal channel, and  $\varphi$  is a phase shift between the topography and the free surface. The corresponding meridional geostrophic flow is given by

$$f v'_g = g \partial_x \eta' = g \kappa \eta_o \cos(\kappa x + \varphi). \quad (31.129)$$

Plugging into the balance (31.122) leads to

$$\sin \varphi = \left[ \frac{L \langle \tau^x \rangle}{D \rho g \eta_o \pi n} \right]. \quad (31.130)$$

For  $\langle \tau^x \rangle > 0$  we see that the free surface undulations are, as expected, shifted to the west of the bottom topography undulations. As an explicit example from an idealized channel configuration, set

$$L = 10^7 \text{ m} \quad D = 10^3 \text{ m} \quad \eta_o = 1 \text{ m} \quad \tau^x = 1 \text{ N m}^{-2}, \quad (31.131)$$

in which case

$$\sin \varphi \approx (\pi n)^{-1}. \quad (31.132)$$

For  $n = 1$ , which corresponds to just one topographic bump, then we have a phase shift of  $\varphi \approx 18^\circ$ , and this case is depicted in Figure 31.8 for the southern hemisphere. If there are two bumps, then the phase shift is reduced to  $\varphi \approx 9^\circ$  since each bump shares half the burden of balancing the wind stress.

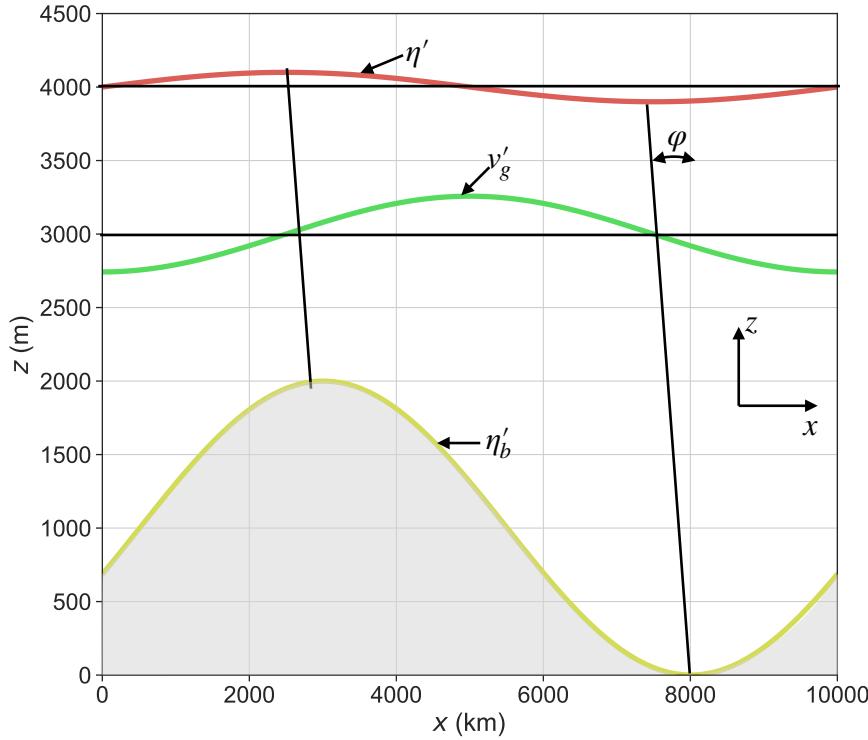


FIGURE 31.8: Zonal-depth view of the wind stress and bottom pressure acting on a steady state layer of shallow water fluid flowing over a sinusoidal bump (north is directed into the page and east is to the right). The eastward surface stress acts in the  $+\hat{x}$  direction and it is balanced by a westward topographic form stress. To establish this form stress when integrated over the zonal extent of the channel requires the sea surface undulations to be phase shifted to the west of the bottom topography undulations, with the phase shift,  $\varphi$ , given by equation (31.130). To better visualize the sea surface, the surface undulations are in units of cm whereas the bottom topography undulations are in units of m. In general, for the topographic form stress to balance the wind stress, the bottom pressure must be anomalously large where  $\partial\eta_b'/\partial x > 0$  and small where  $\partial\eta_b'/\partial x < 0$ , thus leading to the anomalously thick fluid column upstream of the bump and thin column downstream. This correlation also leads to a corresponding meridional geostrophic flow as shown here by the green curve for the southern hemisphere where  $f < 0$ , with  $v_g > 0$  (northward) when shown above the horizontal line and  $v_g < 0$  (southward) when below the line. Compare this figure to the analogous schematic in Figure 19.8.

### Summarizing the dependencies

We here highlight the various dependencies in the phase equation (31.130).

- The phase shift increases with both larger wind stress and larger zonal extent to the domain. This dependency arises since with enhanced wind stress and an enhanced zonal *fetch* (distance over which the winds blow), there is an increase in zonal momentum inserted to the ocean that must be absorbed by the bottom. The larger phase shift increases this topographic form stress, thus enabling the balance.
- Conversely, the phase shift decreases for larger topography  $D$ , and larger undulations in the free surface,  $\eta_o$ , in which case the free surface becomes more aligned with the topographic ridges. This result follows since the topographic form stress is larger for larger topography, thus requiring less phase shift in the surface wave patterns to affect a bottom pressure anomaly.
- Phase shifts decrease when there are more topographic bumps in the channel, with  $n$  the parameter setting the number of bumps. For the Southern Ocean, [Munk and Palmén \(1951\)](#)

identified around four or five large-scale topographic features that provide the dominant balance for the zonal wind stress.

- What if the parameters are such that the right hand side of equation (31.130) has a magnitude larger than unity (e.g., huge winds, very long fetch, small topography, small surface height amplitude)? This situation signals that topographic form stress is insufficient to balance the winds. In a numerical model, one can merely increase the topographic wavenumber,  $n$ , to increase the topographic form stress. Yet where topography is fixed, such as in Nature, then bottom frictional stresses come into play to help reach a force balance (see Section 31.6.4).

#### *Distinguishing steady motion from zero motion*

Why is the phase shift (31.130) independent of the fluid depth? One might suspect that to reach a force balance would require more form stress if there is more fluid. Instead, the force balance, as reflected in the phase shift, depends on the zonal anomalies of the surface height and bottom topography. The depth of the fluid is absent.

The answer to this question is that we are seeking a force balance. When forces are balanced there is no acceleration and thus, as per Newton's second law, the fluid maintains a constant velocity relative to the laboratory reference frame. If we instead wished to stop the fluid, then we would need to decelerate all fluid elements to zero velocity. Determining the forces needed to stop the fluid requires the total fluid mass and thus its depth (as well as the time over which the fluid is to stop). If the fluid is in motion, then halting the motion requires a net force, and that is a very different consideration than the case of zero net force. So in brief, a steady state refers to the absence of time dependence in the fluid from the perspective of an Eulerian (laboratory) observer, with a steady state *not* necessarily a static state.

#### 31.6.8 Comments

The analysis of a single shallow water layer has direct relevance to a stratified flow. The reason is that when integrating over the full depth of the fluid, internal interfacial form stresses cancel pairwise. The resulting net balance for contact forces is concerned with just those acting on the boundaries at the surface and the bottom. We discussed this property of interfacial form stresses in Sections 18.1, 19.3, and 31.5. The direct connection between undulations in the sea surface and bottom pressure provides a particularly simple means to study the phase shift between bottom pressure anomalies and topography required to realize a nonzero zonally integrated form stress. However, this feature of the single layer shallow water system is questionable for a realistic stratified fluid, since stratification breaks the direct connection between sea level undulations and topographic form stress.

The dominance of topographic form stress for the steady Southern Ocean balance contrasts to many of the frictional theories for gyre circulations, such as the classic solutions discussed in Section 34.9. In those theories, based on flat bottom and vertical side configurations, the curl of the wind stress is balanced by torques created by friction.<sup>7</sup> One is thus led to conclude that zonally re-entrant channels exhibit a fundamentally distinct steady force balance from gyres. However, as discussed in Section 19.5.12, *Hughes and de Cueves* (2001) showed how topographic form stresses associated with sloping sides can lead to an inviscid balance for gyres. That is, friction is not needed so long as the bottom can support topographic torques. In this manner, gyres and channels share much in common so long as they both contain topography and sloping sides.

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<sup>7</sup>We will encounter such balances in Chapter 34 when studying vorticity.

## 31.7 Angular momentum in a rotating tank

As our second case study for this chapter, we study angular momentum for a layer of inviscid shallow water fluid in a rotating cylindrical tank. This system was first discussed in Section 22.4, where we developed the horizontal equation of motion

$$\frac{D\mathbf{u}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla (p/\rho + g_e z - \Omega^2 r^2/2), \quad (31.133)$$

where  $r^2 = x^2 + y^2$  is the radial distance from the rotational axis,

$$\Omega = f/2 \quad (31.134)$$

is the constant angular rotation rate, and the vertical component to the right hand side is the hydrostatic balance,  $\partial p / \partial z = -\rho g_e$ . Where convenient, we make use of the polar coordinates (see Chapter 8.3) in the following, whereby

$$x = r \cos \vartheta \quad (31.135a)$$

$$y = r \sin \vartheta, \quad (31.135b)$$

with the polar angle  $\vartheta$  measured counter-clockwise from the positive  $x$ -axis.

### 31.7.1 Angular momentum for a column of shallow water fluid

The angular momentum for a column of shallow water fluid, computed with respect to the vertical rotational axis, is given by (see Sections 10.7 and 17.4)

$$L^z = \delta M [\mathbf{x} \times (\mathbf{u} + \mathbf{U}_{\text{solid}})] \cdot \hat{\mathbf{z}}, \quad (31.136)$$

where  $\mathbf{x} = x \hat{\mathbf{x}} + y \hat{\mathbf{y}} = r \hat{\mathbf{r}}$  is the position vector relative to the rotational axis,  $\delta M = \rho h \delta A$  is the constant mass for the fluid column, and the solid-body rotation velocity is

$$\mathbf{U}_{\text{solid}} = (f/2) \hat{\mathbf{z}} \times \mathbf{x} = r \Omega \hat{\boldsymbol{\theta}}, \quad (31.137)$$

where  $\hat{\mathbf{z}} \times \hat{\mathbf{r}} = \hat{\boldsymbol{\theta}}$  is the azimuthal unit vector pointing counter-clockwise around the origin.

We can further massage the expression for the angular momentum by writing

$$\mathbf{x} \times \mathbf{u} = (x v - y u) \hat{\mathbf{z}} = r^2 \dot{\vartheta} \hat{\mathbf{z}}, \quad (31.138)$$

where  $\dot{\vartheta} = D\vartheta/Dt$  is the angular velocity. Likewise, we have

$$\mathbf{x} \times \mathbf{U}_{\text{solid}} = r^2 \Omega \hat{\mathbf{z}}, \quad (31.139)$$

so that the angular momentum can be written

$$L^z = \delta M [\mathbf{x} \times (\mathbf{u} + \mathbf{U}_{\text{solid}})] \cdot \hat{\mathbf{z}} = \delta M r^2 (\dot{\vartheta} + \Omega). \quad (31.140)$$

### 31.7.2 Material time evolution of the angular momentum

The material time evolution for the angular momentum is given by

$$\frac{DL^z}{Dt} = \delta M [\mathbf{u} \times (\mathbf{u} + \mathbf{U}_{\text{solid}})] \cdot \hat{\mathbf{z}} + \delta M \left[ \mathbf{x} \times \left( \frac{D\mathbf{u}}{Dt} + \frac{D\mathbf{U}_{\text{solid}}}{Dt} \right) \right] \cdot \hat{\mathbf{z}}. \quad (31.141)$$

Note that we set

$$\frac{D(\delta M)}{Dt} = \rho D(h \delta A) Dt = 0 \quad (31.142)$$

since the shallow water fluid columns each have constant volume as they move with the horizontal flow (Section 30.2.4). Using the solid-body rotation velocity given by equation (31.137), and with a constant rotation rate, yields

$$\mathbf{u} \times \mathbf{U}_{\text{solid}} + \mathbf{x} \times \frac{D\mathbf{U}_{\text{solid}}}{Dt} = \mathbf{u} \times (\boldsymbol{\Omega} \times \mathbf{x}) + \mathbf{x} \times (\boldsymbol{\Omega} \times \mathbf{u}) \quad (31.143a)$$

$$= (\mathbf{x} \cdot \mathbf{u}) f \hat{\mathbf{z}}. \quad (31.143b)$$

Making use of the material evolution of the horizontal velocity given by equation (31.133) renders

$$\left[ \mathbf{x} \times \frac{Du}{Dt} \right] \cdot \hat{\mathbf{z}} = (\mathbf{x} \times [-f \hat{\mathbf{z}} \times \mathbf{u} - \nabla(p/\rho + g_e z - \Omega^2 r^2/2)]) \cdot \hat{\mathbf{z}} \quad (31.144a)$$

$$= -f (\mathbf{x} \cdot \mathbf{u}) - (\mathbf{x} \times g \nabla \eta) \cdot \hat{\mathbf{z}}. \quad (31.144b)$$

The centrifugal term dropped out since

$$\mathbf{x} \times \nabla r^2 = 2 \mathbf{x} \times r \hat{\mathbf{r}} = 2 \mathbf{x} \times \mathbf{x} = 0. \quad (31.145)$$

The gravitational term dropped out since

$$(\mathbf{x} \times \nabla z) \cdot \hat{\mathbf{z}} = (\mathbf{x} \times \hat{\mathbf{z}}) \cdot \hat{\mathbf{z}} = 0, \quad (31.146)$$

as does the vertical component to the pressure gradient. We are thus left with

$$\frac{1}{\delta M} \frac{DL^z}{Dt} = -g (\mathbf{x} \times \nabla \eta) \cdot \hat{\mathbf{z}}. \quad (31.147)$$

Consequently, the axial angular momentum for a fluid column is modified by the torque from the horizontal pressure gradient caused by undulations in the free surface height. Note how there is no contribution from the Coriolis acceleration, so that the evolution of angular momentum is the same whether viewed in the laboratory frame or rotating frame.

We can bring the expression (31.147) into a more transparent form by switching to polar coordinates

$$\mathbf{x} \times \nabla \eta = r \hat{\mathbf{r}} \times \left[ \hat{\mathbf{r}} \frac{\partial \eta}{\partial r} + \hat{\vartheta} \frac{1}{r} \frac{\partial \eta}{\partial \vartheta} \right] = \frac{\partial \eta}{\partial \vartheta} \hat{\mathbf{z}}, \quad (31.148)$$

so that

$$\frac{1}{\delta M} \frac{DL^z}{Dt} = -g \frac{\partial \eta}{\partial \vartheta}. \quad (31.149)$$

This result is directly analogous to the angular momentum evolution for a fluid moving around a sphere as derived in Section 17.4. Namely, in the presence of angular pressure gradients, the fluid experiences a torque that in turn leads to a change in the angular momentum relative to the vertical rotation axis.

### 31.7.3 Materially invariant angular momentum

The angular momentum for a fluid column is materially invariant (i.e., a constant on a material fluid parcel) if

$$\frac{DL^z}{Dt} = 0 \iff \frac{\partial \eta}{\partial \vartheta} = 0. \quad (31.150)$$

For a flat bottom, equation (22.81) says that the free surface takes on a radial parabolic shape when the fluid is in solid-body rotation. In this case,  $\nabla \eta$  is in the radial direction, in which case  $\mathbf{x} \times \nabla \eta = 0$ . Consequently, when the fluid is in solid-body rotation, the angular momentum for each fluid column remains materially constant.

### 31.7.4 Comments

The material evolution equation (31.147) also holds for a fluid on the  $f$ -plane tangent to a sphere. The  $f$ -plane formulation is slightly simpler than the tank since the centrifugal term is absorbed into the geopotential (see Section 9.12.4). However, the tank is arguably more pedagogical as it is simpler to visualize and to conduct laboratory experiments. See Section 6.6.4 of [Marshall and Plumbe \(2008\)](#) for more discussion of rotating tank experiments.

## 31.8 Inertia-gravity waves in a single shallow water layer

We here consider linear waves in a single layer of shallow water fluid with a flat bottom on an  $f$ -plane. Waves in this system arise from the gravitational restoring force.<sup>8</sup> To develop the mathematical equations for these shallow water gravity waves, we linearize the equations of motion and then develop constraints that must be satisfied for the existence of nontrivial solutions.

### 31.8.1 Linearized shallow water equations

Recall the shallow water equations of motion are given by the momentum and continuity equations, written here in their Eulerian form

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} + f \hat{z} \times \mathbf{u} = -g \nabla \eta \quad (31.151a)$$

$$\frac{\partial h}{\partial t} + h \nabla \cdot \mathbf{u} + \mathbf{u} \cdot \nabla h = 0. \quad (31.151b)$$

With a flat bottom we assume  $\eta_b = 0$  (see Figure 30.1) so that the surface height equals to the thickness,

$$\eta = h \quad \text{flat bottom with } \eta_b = 0. \quad (31.152)$$

We linearize the momentum and thickness equation relative to a state of rest in which

$$\eta(x, y, t) = H + \eta'(x, y, t) \quad (31.153a)$$

$$\mathbf{u}(x, y, t) = 0 + \mathbf{u}'(x, y, t). \quad (31.153b)$$

Substitution into the thickness equation (31.151b) leads to

$$\frac{\partial \eta'}{\partial t} + (H + \eta') \nabla \cdot \mathbf{u}' + \mathbf{u}' \cdot \nabla \eta' = 0. \quad (31.154)$$

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<sup>8</sup>Rossby waves also arise when considering a non-constant Coriolis parameter. We study Rossby waves for the non-divergent barotropic model in Section 33.6.

The products  $\eta' \nabla \cdot \mathbf{u}'$  and  $\mathbf{u}' \cdot \nabla \eta'$  are second order (and nonlinear) in fluctuating quantities. Dropping these terms leads to the linearized surface height (or thickness) equation

$$\frac{\partial \eta'}{\partial t} + H \nabla \cdot \mathbf{u}' = 0 \quad \text{linearized surface height equation.} \quad (31.155)$$

Similarly, the linearized momentum equation takes the form (dropping the nonlinear advection term  $(\mathbf{u}' \cdot \nabla) \mathbf{u}'$ )

$$\frac{\partial \mathbf{u}'}{\partial t} + f \hat{\mathbf{z}} \times \mathbf{u}' = -g \nabla \eta' \quad \text{linearized momentum equation.} \quad (31.156)$$

### 31.8.2 Relative vorticity of linear fluctuations

We here consider how the vertical component of relative vorticity<sup>9</sup>

$$\zeta = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u}) \quad (31.157)$$

evolves for the small amplitude shallow water fluctuations determined by equations (31.155) and (31.156). Taking the curl of the linearized momentum equation (31.156) leads to

$$\frac{\partial \zeta'}{\partial t} = -\nabla \cdot (f \mathbf{u}'). \quad (31.158)$$

On the  $f$ -plane and with the non-divergence condition  $\nabla \cdot \mathbf{u}' + \partial_z w' = 0$ , we have

$$\frac{\partial \zeta'}{\partial t} = f \frac{\partial w'}{\partial z}. \quad (31.159)$$

We can use the linearized thickness equation (31.155) to render an equivalent result

$$\frac{\partial \zeta'}{\partial t} = \frac{f}{H} \frac{\partial \eta'}{\partial t}. \quad (31.160)$$

In either case, relative vorticity of the linearized shallow water system is modified by vertical stretching in the presence of planetary rotation ( $f \neq 0$ ). In the absence of planetary rotation, the relative vorticity remains static at each point in space. Consequently, if the relative vorticity for a non-rotating system starts with a zero value, it will remain so throughout the linearized evolution.

### 31.8.3 Non-rotating gravity waves

For the non-rotating case ( $f = 0$ ), the linear velocity and thickness equations are

$$\frac{\partial \eta'}{\partial t} = -H \nabla \cdot \mathbf{u}' \quad (31.161a)$$

$$\frac{\partial \mathbf{u}'}{\partial t} = -g \nabla \eta'. \quad (31.161b)$$

Equation (31.161a) reveals that horizontal convergence drives temporal changes in the free surface height. Hence, a nonzero horizontal flow convergence is required for gravity waves to exist.

Take the time derivative of the thickness equation and the divergence of the momentum

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<sup>9</sup>In Chapter 34 we study vorticity within the shallow water system.

equation

$$\frac{\partial^2 \eta'}{\partial t^2} = -H \frac{\partial(\nabla \cdot \mathbf{u}')}{\partial t} \quad (31.162a)$$

$$\frac{\partial(\nabla \cdot \mathbf{u}')}{\partial t} = -g \nabla^2 \eta'. \quad (31.162b)$$

Time changes in the horizontal divergence are thus driven by curvature in the free surface. Substitution then reveals that the perturbation surface height satisfies the linear wave equation

$$\frac{\partial^2 \eta'}{\partial t^2} - g H \nabla^2 \eta' = 0. \quad (31.163)$$

The complement substitution leads to the slightly more general wave equation for the perturbation horizontal velocity

$$\frac{\partial^2 \mathbf{u}'}{\partial t^2} - g H \nabla(\nabla \cdot \mathbf{u}') = 0. \quad (31.164)$$

We discussed the linear wave equation in Section 3.7, revealing it to be the canonical hyperbolic partial differential equation. An appreciation of that discussion is useful though not necessary for the following examination of gravity wave properties.

### Wave ansatz and dispersion relation

The linearized shallow water system (31.161a)-(31.161b) exhibits horizontal spatial symmetry. We are thus motivated to consider the linear wave ansatz<sup>10</sup>

$$(u', v', \eta') = (\tilde{u}, \tilde{v}, \tilde{\eta}) e^{i(\mathbf{k} \cdot \mathbf{x} - \omega t)}, \quad (31.165)$$

where

$$i = \sqrt{-1} \quad (31.166)$$

and where the real part of the right hand side is assumed. The amplitudes  $(\tilde{u}, \tilde{v}, \tilde{\eta})$  are generally *complex* numbers that are independent of space and time. The vector

$$\mathbf{k} = \hat{\mathbf{x}} k + \hat{\mathbf{y}} l \quad (31.167)$$

is the horizontal vector wave-number and  $\omega$  is the radial frequency with

$$\tau_{\text{period}} = 2\pi/\omega \quad (31.168)$$

the wave period.<sup>11</sup>

Making use of the linearized momentum equation (31.161b) allows us to connect the amplitude of the free surface undulation to the velocity

$$\tilde{\mathbf{u}} = \mathbf{k} \frac{g \tilde{\eta}}{\omega} \implies \tilde{\mathbf{u}} \times \mathbf{k} = 0 \quad \text{and} \quad \tilde{\mathbf{u}} \cdot \mathbf{k} = \frac{g \tilde{\eta} |\mathbf{k}|^2}{\omega}. \quad (31.169)$$

These relations mean that the horizontal velocity of a fluid particle within the wave is oriented parallel to the horizontal wave vector. If fluid particle motion is parallel to the wave, then the

<sup>10</sup>Ansatz is a German word meaning “educated guess”. For the linear waves considered here, the wave ansatz (31.165) is a valid solution of the linearized shallow water equations (31.161a)-(31.161b) if the dispersion relation (31.171) is satisfied.

<sup>11</sup>It is important to distinguish the radial frequency,  $\omega$ , from the vector vorticity,  $\boldsymbol{\omega}$ , used elsewhere in this book.

wave is said to be *longitudinal*. However, we recall that a shallow water fluid has a vertical velocity that is a linear function of depth as given by equation (30.35)

$$w(z) = w(\eta_b) - (z - \eta_b) \nabla \cdot \mathbf{u}. \quad (31.170)$$

The presence of vertical motion within the wave means that shallow water gravity waves, which have horizontal wave vectors, are not purely longitudinal; it is just the particle's horizontal motion that is longitudinal.

Substitution of the surface height fluctuation (31.165) into the wave equation (31.163) leads to the relation between frequency and wave-number

$$\omega = \pm c |\mathbf{k}|, \quad (31.171)$$

where

$$c = \sqrt{g H} \quad (31.172)$$

is the shallow water gravity wave speed. We emphasize that the wave ansatz (31.165) is a valid solution of the linearized shallow water equations (31.161a)-(31.161b) only if the *dispersion relation* (31.171) is satisfied.

The dispersion relation (31.171) indicates that each wave vector corresponds to a single wave frequency (mod the sign ambiguity, which corresponds to waves moving in opposite directions). Hence, there is no mixing, or dispersion, between waves of different wavenumber or frequency. Non-rotating shallow water gravity waves are thus a type of *non-dispersive* wave. Furthermore, use of the dispersion relation brings the amplitude relations (31.169) into the form

$$\tilde{\mathbf{u}} = \tilde{\eta} \frac{\mathbf{k}}{|\mathbf{k}|} \sqrt{\frac{g}{H}} \implies \tilde{\mathbf{u}} \cdot \mathbf{k} = \tilde{\eta} \frac{\omega}{H}. \quad (31.173)$$

Since the wave vector is real, this relation means that the velocity and the free surface move in phase as part of the linear wave.

### *Vanishing relative vorticity*

Equation (31.162b) indicates that the linear fluctuations have a horizontal divergence driven by curvature in the surface height. In contrast, because the linearized velocity fluctuation is driven by the gradient of the surface height (see equation (31.161b)), the associated vorticity has a zero time tendency

$$\frac{\partial (\nabla \times \mathbf{u}')}{\partial t} = 0. \quad (31.174)$$

This result follows from the discussion of vorticity for the shallow water waves in Section 31.8.2. Hence, if the initial flow configuration has zero vorticity, the linear gravity waves retain zero vorticity as they propagate. The velocity fluctuation (31.169) indeed has zero vorticity since

$$\hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u}') = i \hat{\mathbf{z}} \cdot (\mathbf{k} \times \tilde{\mathbf{u}}) e^{i(\mathbf{k} \cdot \mathbf{x} - \omega t)} = 0, \quad (31.175)$$

where we used equation (31.169) to set  $\mathbf{k} \times \tilde{\mathbf{u}} = 0$ .

### 31.8.4 Potential vorticity of linear fluctuations

Returning now to the  $f \neq 0$  case, we rearrange the linearized vorticity equation (31.160) to reach the linear conservation law

$$\frac{\partial q}{\partial t} = 0, \quad (31.176)$$

where the linearized shallow water potential vorticity is given by<sup>12</sup>

$$q = \zeta' - \frac{f\eta'}{H}. \quad (31.177)$$

For the rotating case, we see that potential vorticity is locally constant in the presence of linear fluctuations, such as the inertia-gravity waves discussed in Section 31.8.5. We make use of this constraint in Section 34.7 when studying geostrophic adjustment.

### 31.8.5 Inertia-gravity waves

Now let the Coriolis parameter,  $f$ , be a nonzero constant, so that the linearized thickness equation (31.155) and momentum equation (31.156) take the form

$$\frac{\partial \eta'}{\partial t} = -H \nabla \cdot \mathbf{u}' \quad (31.178a)$$

$$\frac{\partial \mathbf{u}'}{\partial t} + f \hat{\mathbf{z}} \times \mathbf{u}' = -g \nabla \eta'. \quad (31.178b)$$

The resulting linear fluctuations are known as *inertia-gravity* or *Poincaré waves*. The name “inertia-gravity” is due to the presence of both the Coriolis frequency  $f$  and gravity  $g$ . Recall our discussion of inertial oscillations in Section 10.5, which describe free particle motion in a rotating reference frame. Inertia-gravity waves arise from the combination of inertial oscillations and non-rotating gravity wave oscillations from Section 31.8.3. That is, both  $f$  and  $g$  play a role as restoring forces for the waves.

The continuity equation, as a kinematic constraint, has the same form for both rotating and non-rotating systems. Hence, its linearized version, equation (31.178a), remains the same as for the non-rotating case in equation (31.161a). Like the non-rotating case, convergence in the horizontal flow drives surface height tendencies. Hence, horizontal flow convergence is required to support gravity waves in both the rotating and non-rotating systems.

### 31.8.6 Inertia-gravity wave dispersion relation

The linearized shallow water system (31.178a)-(31.178b) exhibits horizontal spatial symmetry given that  $f$  is assumed constant. We are thus motivated to consider the linear wave ansatz

$$(u', v', \eta') = (\tilde{u}, \tilde{v}, \tilde{\eta}) e^{i(\mathbf{k} \cdot \mathbf{x} - \omega t)}, \quad (31.179)$$

which is the same as assumed for the non-rotating case in Section 31.8.3. Although the same ansatz, the dispersion relation and amplitude relations differ since  $f \neq 0$ . In particular, we here need to make use of the complex nature of the wave amplitudes  $(\tilde{u}, \tilde{v}, \tilde{\eta})$  to realize nontrivial solutions.

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<sup>12</sup>The linearized potential vorticity (31.177) can be obtained by taking the limit of  $|f| \gg |\zeta|$  and  $H \gg \Delta\eta$  in the shallow water potential vorticity,  $Q = (f + \zeta)/h$ , studied in Section 34.4.

Substituting the wave ansatz (31.179) into equations (31.178a)-(31.178b) renders the homogeneous matrix-vector equation

$$\begin{bmatrix} -i\omega & -f & igk \\ f & -i\omega & igl \\ iHk & iHl & -i\omega \end{bmatrix} \begin{bmatrix} \tilde{u} \\ \tilde{v} \\ \tilde{\eta} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}. \quad (31.180)$$

This equation has a nontrivial solution only when the determinant of the matrix vanishes. The real part of the determinant cancels exactly, thus leaving just the imaginary part. Setting the imaginary part to zero yields the dispersion relation

$$\omega [\omega^2 - f^2 - gH(k^2 + l^2)] = 0. \quad (31.181)$$

There are three solutions to this cubic equation to which we now describe.

### Geostrophic motion

The zero frequency solution,  $\omega = 0$ , corresponds to  $f$ -plane geostrophic motion. Such motion has zero horizontal divergence since the fluid is time dependent, in which case the linearized continuity equation (31.178a) has  $\nabla \cdot \mathbf{u}' = 0$ . We studied shallow water geostrophic motion in Section 31.2. We thus move onto the main focus of this chapter, which is the ageostrophic motion associated with inertia-gravity waves in which the horizontal flow is divergent.

### Inertia-gravity wave solutions

The two  $\omega \neq 0$  solutions to the dispersion relation (31.181) satisfy the quadratic dispersion relation

$$\omega^2 = f^2 [1 + L_d^2(k^2 + l^2)], \quad (31.182)$$

where

$$L_d = \frac{c}{f} = \frac{\sqrt{gH}}{f} \quad (31.183)$$

is the *deformation radius* for the shallow water layer. As seen in the following, scales smaller than the deformation radius are well approximated by non-rotating physics, whereas rotation is central to the dynamics at scales larger than the deformation radius.

The non-zero frequency modes satisfying the dispersion relation (31.182) are inertia-gravity waves and Figure 31.9 depicts this relation. These waves have a frequency,  $\omega$ , whose magnitude is greater than the inertial frequency

$$\omega^2 \geq f^2, \quad (31.184)$$

and are thus said to be *super-inertial waves*.

### Shortwave limit

The short wave limit is in the regime where

$$k^2 + l^2 \gg \frac{f^2}{gH} = \frac{1}{L_d^2}, \quad (31.185)$$

so that the shortwave limit occurs when the wavelength is much shorter than the deformation radius. For a wave moving in the  $\hat{x}$  direction with wavelength  $\lambda = 2\pi/k$ , the shortwave limit

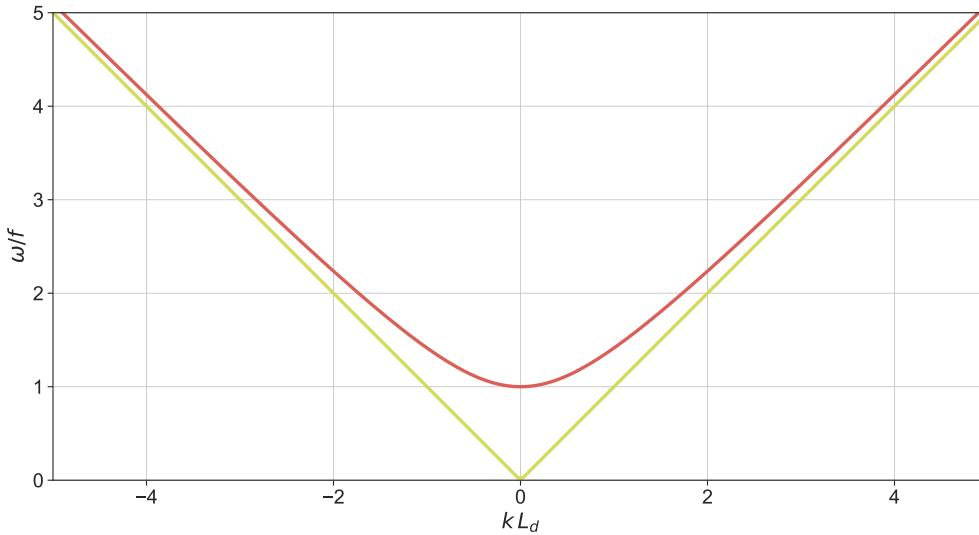


FIGURE 31.9: Illustrating the dispersion relation (31.182) for shallow water inertia-gravity waves (hyperbolic curve). Frequency is scaled by the Coriolis frequency,  $f$ , and horizontal wavenumber magnitude is scaled by the deformation radius  $L_d = \sqrt{gH}/f$ . For small wave numbers ( $|k| L_d \ll 1$  or  $\lambda \gg 2\pi L_d$ ), the inertial-gravity wave frequency approaches the inertia frequency,  $f$ , with this behavior seen at the minimum of the dispersion curve. We expect this result since waves large relative to the deformation radius feel the Coriolis acceleration. At the opposite extreme of high wave numbers ( $\lambda \ll 2\pi L_d$ ), the wave frequency approaches the non-rotating gravity wave frequency, shown here by the linear dispersion relation  $\omega = k \sqrt{gH}$ . Waves small relative to the deformation radius do not feel the Coriolis acceleration and thus converge to non-rotating gravity waves. Since all inertia-gravity waves satisfy  $\omega^2 \geq f^2$ , they are said to be *super-inertial* waves; i.e., waves whose frequency is larger in magnitude than the inertial frequency.

occurs when

$$\lambda \ll 2\pi L_d. \quad (31.186)$$

Note that to remain consistent with the shallow water limit with a small vertical to horizontal aspect ratio (i.e., a hydrostatic fluid layer), the wavelength must be longer than the layer thickness,  $H$ . Finally, for the shortwave limit, the dispersion relation (31.182) reduces to the non-rotating dispersion relation (31.171)

$$\omega \approx \pm |\mathbf{k}| c = \pm |\mathbf{k}| \sqrt{gH}. \quad (31.187)$$

We see that waves smaller than the deformation radius are only weakly affected by the Coriolis acceleration so that their dispersion relation reduces to linear non-rotating gravity waves of Section 31.182.

### Longwave limit

The opposite limit occurs when

$$k^2 + l^2 \ll \frac{1}{L_d^2}, \quad (31.188)$$

so the waves are much longer than the deformation radius. In this limit the dispersion relation is

$$\omega = \pm f. \quad (31.189)$$

This dispersion relation is satisfied by inertial oscillations. As discussed in Section 10.5, inertial oscillations are unaffected by pressure forces otherwise arising from surface height undulations. Instead, they are determined only by the Coriolis frequency. Hence, in this longwave limit the

fluid particles move as inertially oscillating particles.

### 31.8.7 Horizontally longitudinal and transverse components

As discussed in Section 31.8.3, non-rotating gravity waves are horizontally longitudinal, which means that horizontal fluid particle motion induced by the waves is in the same direction as the wave vector. In contrast, we will see that in the presence of rotation, the waves develop a horizontally transverse wave component in addition to the longitudinal component.

Substituting the wave ansatz (31.179) into the linearized continuity equation (31.178a) leads to

$$\mathbf{k} \cdot \tilde{\mathbf{u}} = \tilde{\eta} \frac{\omega}{H}, \quad (31.190)$$

which is the same as for the non-rotating case given by equation (31.173). The wave ansatz (31.179) in the velocity equation (31.178b) gives

$$\hat{\mathbf{z}} \cdot (\mathbf{k} \times \tilde{\mathbf{u}}) = -\tilde{\eta} \frac{i f}{H}, \quad (31.191)$$

which results from the vanishing linearized potential vorticity as per equation (31.177). In reading this equation, it is important to recall that the wave amplitudes,  $(\tilde{\mathbf{u}}, \tilde{\eta})$ , are generally complex numbers.

Making use of equations (31.190) and (31.191) leads to the following decomposition of the wave velocity amplitude

$$\tilde{\mathbf{u}} = \frac{\tilde{\eta}}{H |\mathbf{k}|^2} [\omega \mathbf{k} - i f (\mathbf{k} \times \hat{\mathbf{z}})], \quad (31.192)$$

which in turn leads to the wave velocity

$$\mathbf{u}' = \frac{\tilde{\eta}}{H |\mathbf{k}|^2} \left[ \underbrace{\omega \mathbf{k} \cos(\mathbf{k} \cdot \mathbf{x} - \omega t)}_{\text{horizontally longitudinal}} + \underbrace{f (\mathbf{k} \times \hat{\mathbf{z}}) \sin(\mathbf{k} \cdot \mathbf{x} - \omega t)}_{\text{horizontally transverse}} \right]. \quad (31.193)$$

For the northern hemisphere, where  $f > 0$ , the wave rotates clockwise relative to the direction of the wave, when looking from above, with the wave vector tracing out an ellipse. The horizontally transverse component of the velocity vector is  $\pi/2$  out of phase with the horizontally longitudinal component. Furthermore, the transverse component corresponds to fluid particle motion that is perpendicular to the wave vector, in which case we say that the transverse component is *polarized* perpendicular to the horizontal wave vector.

### 31.8.8 Comments

There is much more to be said about gravity waves, particularly when having more than a single shallow water layer and then when allowing for continuous stratification. Chapter 7 of [Vallis \(2017\)](#) provides a thorough and pedagogical introduction to the subject. For our purposes, we only wished to whet the appetite. Also, we make use of the basic ideas of gravity waves when discussing geostrophic adjustment in Section 34.7.

## 31.9 Inertia-gravity waves generated by topography

In this section we consider a geophysically relevant means to force gravity waves via the flow of fluid over topography.

### 31.9.1 Linearized equations

The physical system consists of flow in a zonally reentrant channel with small amplitude topography,  $\eta_b = \eta'_b$ . We also introduce a constant zonal mean flow,  $U \hat{x}$ . Linear inertia-gravity wave fluctuations are generated as the flow moves over the topography. Our goal is to examine the properties of these waves.

The free surface and velocity take on the assumed form

$$\eta = H + \eta'_b + \eta' \quad \text{and} \quad u = U + u' \quad \text{and} \quad v = 0 + v', \quad (31.194)$$

where primed variables are small so that the product of any two primed variables is neglected. We are unconcerned with how the zonal mean flow is generated, instead focusing on the small amplitude perturbations ( $u', v', \eta'$ ). Substituting the expressions (31.194) into the shallow water equations (31.151a) and (31.151b) leads to the linearized equations

$$\frac{\partial \mathbf{u}'}{\partial t} + U \frac{\partial \mathbf{u}'}{\partial x} + f \hat{z} \times \mathbf{u}' = -g \nabla \eta' \quad (31.195a)$$

$$\frac{\partial(\eta' - \eta'_b)}{\partial t} + U \frac{\partial(\eta' - \eta'_b)}{\partial x} = -H \nabla \cdot \mathbf{u}'. \quad (31.195b)$$

We chose to retain  $\eta'_b$  as part of the time derivative even though the topography is time-independent.

### 31.9.2 Galilean transformation

The background zonal flow is constant in time and zonally symmetric. In this situation it is convenient to introduce a Galilean transformation according to

$$\bar{t} = t \quad \text{and} \quad \bar{x} = x - U t \quad \text{and} \quad \bar{y} = y. \quad (31.196)$$

Following our discussion of Galilean transformations in Section 12.6, we know that the derivative operators transform according to<sup>13</sup>

$$\frac{\partial}{\partial \bar{t}} = \frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \quad \text{and} \quad \frac{\partial}{\partial \bar{x}} = \frac{\partial}{\partial x} \quad \text{and} \quad \frac{\partial}{\partial \bar{y}} = \frac{\partial}{\partial y}. \quad (31.197)$$

With this coordinate transformation the linear equations (31.195a)-(31.195b) take the form

$$\frac{\partial \mathbf{u}'}{\partial \bar{t}} + f \hat{z} \times \mathbf{u}' = -g \nabla \eta' \quad (31.198a)$$

$$\frac{\partial(\eta' - \eta'_b)}{\partial \bar{t}} = -H \nabla \cdot \mathbf{u}'. \quad (31.198b)$$

Note how the  $U \partial_x$  operator has been absorbed into the time derivative,  $\partial_{\bar{t}}$ . The price to pay for that simplification is that the topography that is independent of the time  $t$ , is now a function of the time  $\bar{t}$ . That is, in the reference frame moving with the mean flow with velocity  $U \hat{x}$ , the topography moves in the opposite direction since

$$\eta'_b(x, y) = \eta'_b(\bar{x} + U \bar{t}, \bar{y}). \quad (31.199)$$

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<sup>13</sup>Note that the Galilean transformation considered in Section 12.6 uses the opposite sign for the flow relative to that considered here. There is nothing fundamental about the sign; one merely needs to be careful when translating the earlier results to the current case.

### 31.9.3 Wave equation and relation between amplitudes

Taking  $\partial_{\bar{t}}$  of the continuity equation (31.198b) and then substituting the time derivative of the velocity equation (31.198a) leads to the forced wave equation

$$\frac{\partial^2 \eta'}{\partial \bar{t}^2} - g H \nabla^2 \eta' + f H \zeta' = \frac{\partial^2 \eta'_b}{\partial \bar{t}^2}, \quad (31.200)$$

where

$$\zeta' = \hat{z} \cdot (\nabla \times \mathbf{u}') = \partial_x v' - \partial_y u' \quad (31.201)$$

is the relative vorticity of the waves.

#### Assumptions

To proceed, we make the following simplifying assumptions.

- The topography is a function only of the zonal position

$$\eta'_b = \eta'_b(x) = \eta'_b(\bar{x} + U \bar{t}). \quad (31.202)$$

- Seek a steady solution whereby  $\partial_t = 0$  so that  $\partial_{\bar{t}} = U \partial_x$ .
- Assume zero meridional dependence so that  $\partial_y = 0$ . This assumption in-effect means that we are working on a domain that is either periodic in  $y$  or infinite in  $y$ ; i.e., there are no northern or southern walls to the zonal channel.
- Assume the topography has a wave structure

$$\eta'_b(x) = \tilde{\eta}_b e^{ik_b x} = \tilde{\eta}_b e^{ik_b (\bar{x} + U \bar{t})} = \tilde{\eta}_b e^{i(k_b \bar{x} - \omega_b \bar{t})}, \quad (31.203)$$

where  $\tilde{\eta}_b$  is the specified amplitude of the topography,  $k_b$  is the specified wave number of the topography, and

$$\omega_b = -U k_b \quad (31.204)$$

is the intrinsic frequency of the topography as viewed in the moving reference frame. This monochromatic wave assumption is a strong idealization since realistic topography has many Fourier wave components. Nonetheless, once we obtain the solution for a single wave we can use the principle of superposition available for linear equations to develop a more general solution.

#### Wave ansatz

What sort of waves do we expect to excite? Without any prior notion, we might expect to excite a variety of waves. However, to simplify the analysis we seek wave solutions with the same wave number,  $k_b$ , and intrinsic frequency,  $\omega_b$ , of the topography. These considerations lead us to study the wave ansatz

$$(u', v', \eta') = (\tilde{u}, \tilde{v}, \tilde{\eta}) e^{i(k_b \bar{x} - \omega_b \bar{t})}. \quad (31.205)$$

We are thus not in search of a dispersion relation, since the wave number and frequency are specified. Instead, we wish to determine the relation between the wave amplitudes. In particular, we will see that knowledge of  $\tilde{\eta}$  is sufficient to specify the velocity amplitudes,  $(\tilde{u}, \tilde{v})$ . Furthermore, we express the free surface wave amplitude,  $\tilde{\eta}$ , in terms of the topography amplitude,  $\tilde{\eta}_b$ .

### Relating the amplitudes

Use of the wave ansatz (31.205) in the wave equation (31.200) leads to

$$(-\omega_b^2 + g H k_b^2) \tilde{\eta} = -\omega_b^2 \tilde{\eta}_b - i f H k_b \tilde{v}. \quad (31.206)$$

To simplify this expression, make use of the velocity equation (31.198a) and continuity equation (31.198b), which take on the modal form

$$\omega_b \hat{z} \cdot (\mathbf{k}_b \times \tilde{\mathbf{u}}) = -i f \mathbf{k}_b \cdot \tilde{\mathbf{u}} \quad (31.207a)$$

$$H \mathbf{k}_b \cdot \tilde{\mathbf{u}} = \omega_b (\tilde{\eta} - \tilde{\eta}_b), \quad (31.207b)$$

which, for  $\mathbf{k}_b = \hat{x} k_b$ , leads to

$$i k_b H \tilde{v} = f (\tilde{\eta} - \tilde{\eta}_b). \quad (31.208)$$

Substitution of equation (31.208) into the dispersion relation (31.206) leads to

$$\tilde{\eta} = \left[ \frac{\omega_b^2 - f^2}{\omega_b^2 - f^2 - g H k_b^2} \right] \tilde{\eta}_b = \left[ \frac{(f/k_b)^2 - U^2}{(f/k_b)^2 + (g H - U^2)} \right] \tilde{\eta}_b, \quad (31.209)$$

where the second equality follows by setting  $\omega_b = -U k_b$  for the intrinsic frequency. Since the ratio on the right hand side is a real number, we see that the free surface is in phase with the bottom topography. Furthermore, note that for most cases of interest,  $g H \gg U^2$  since non-rotating gravity wave speeds are typically much larger than the mean flow speeds (except perhaps in very shallow waters). In general, when  $g H \leq U^2$  then the flow can be subject to hydraulic jumps since the particle speed overcomes the wave speed (see Exercise 30.2), with such jumps well outside the linear regime considered here. We thus assume  $g H \gg U^2$ , in which case the amplitude of the free surface undulations are much smaller than the topography undulations

$$|\tilde{\eta}| \ll |\tilde{\eta}_b|. \quad (31.210)$$

From the discussion of topographic form stress in Section 31.6, we know that a net topographic form stress over the extent of the channel requires there to be a nonzero phase shift between the topography and the free surface height. Given the absence of such a phase shift in this example, we see that the waves do not generate a net topographic form stress.



## 31.10 Exercises

### EXERCISE 31.1: POTENTIAL TEMPERATURE SLOPES IN ATMOSPHERE AND OCEAN

Use the two-layer thermal wind relations from Section 31.2.2, also known as Margules' relation, to estimate the slope of the potential temperature surfaces in the atmosphere and ocean. This question is based on exercise 3.2 of [Vallis \(2006\)](#).

- (a) Model the atmosphere as two immiscible shallow water layers of different density stacked one above the other. Using reasonable values for any required physical parameters, estimate the vertical displacement of the interfacial surface associated with a pole-to-equator temperature difference of 40K. You may wish to consult [Wallace and Hobbs \(2006\)](#) or [Marshall and Plumb \(2008\)](#) for physical scales.

- (b) Estimate a vertical interfacial displacement in the ocean thermocline associated with a temperature difference of 20K over a horizontal distance of 4000 km. The interface between the two shallow water layers offers a crude representation of the main oceanic thermocline. Ignore salinity effects so that temperature and density are directly proportional.

Double-check your results by examining some atmosphere and ocean latitude-height profiles for potential temperature (e.g., Figure 5.8 of [Marshall and Plumb \(2008\)](#)).

**EXERCISE 31.2: CIRCULAR STEADY GEOSTROPHIC FLOW**

Consider a single layer of shallow water fluid in steady geostrophic balance on a  $f$ -plane so that

$$f \hat{z} \times \mathbf{u}_g = -g \nabla \eta, \quad (31.211)$$

where  $f > 0$  (northern hemisphere). Assume the free surface has a circular Gaussian shape

$$\eta = \eta_0 e^{-r^2/(2\sigma^2)} \quad (31.212)$$

where  $r^2 = x^2 + y^2$  is the square of the radial position and  $\sigma$  is the standard deviation of the Gaussian.

- (a) Determine the horizontal geostrophic velocity components corresponding to this free surface undulation.
- (b) Determine the streamlines for the flow. Hint: recall the discussion in Section 12.8.2.

**EXERCISE 31.3: STEADY STATE MOMENTUM AND GEOSTROPHY**

Consider a single layer of shallow water fluid with zero boundary mass fluxes through the surface. Assume the lateral boundaries are solid. All boundaries are thus material. The domain integrated horizontal momentum (within the rotating reference frame) is defined by

$$\mathbf{P} = \int \rho \mathbf{u} dV = \int \rho h \mathbf{u} dA. \quad (31.213)$$

Show that for tangent plane motion (Section 22.3)

$$\frac{d\mathbf{P}}{dt} = 0 \quad (31.214)$$

can be realized either by (A) zero flow everywhere, (B) flow that is in geostrophic balance at each point, or (C) flow that is in geostrophic balance as a global integral.

**EXERCISE 31.4: THICKNESS WEIGHTED MOMENTUM FOR TWO LAYERS**

Following the methods from Section 31.4, derive the thickness weighted momentum equation for an inviscid two-layer stacked shallow water fluid. That is, derive the evolution equation for  $h_1 \mathbf{u}_1 + h_2 \mathbf{u}_2$ , thus providing the two-layer version of equation (31.41).

**EXERCISE 31.5: CONTACT PRESSURE FORCE ON A SINGLE LAYER**

As a check on our calculation of the contact pressure force (31.79b), consider a single shallow water layer under a massless atmosphere. Show that the contact pressure force per mass is given by

$$\frac{\mathbf{F}_{\text{net}}^{\text{press}}}{M} = g \hat{z} - g \nabla \eta. \quad (31.215)$$

As expected, the horizontal component of this force equals to the pressure gradient body force per mass detailed in Section 30.2.1. The vertical pressure force balances the weight of the fluid as per the hydrostatic balance.

## EXERCISE 31.6: TOPOGRAPHIC FORM STRESS FOR A RIDGE

As in Section 31.6, apply a constant eastward zonal wind to a zonally reentrant channel with a single shallow water layer. Let the layer flow over a topographic ridge of height  $H$  above the surrounding flat bottom, and let the ridge be a function just of zonal position,  $\eta'_b(x)$ . Furthermore, assume the ridge has a constant slope on both the upstream (west) side,  $S_{\text{up}}$ , and downstream (east) side,  $S_{\text{dn}}$ . An example is depicted in Figure 31.10. Following the force balance (31.122), derive an expression for the free surface height zonally averaged over the upstream side of the ridge, minus the free surface height zonally averaged over the downstream sides of the ridge,

$$\Delta\eta' = (\bar{\eta'})_{\text{up}} - (\bar{\eta'})_{\text{dn}}, \quad (31.216)$$

where

$$(\bar{\eta'})_{\text{up}} = \frac{\int_{x_{\text{up}}}^{x_0} \eta' dx}{L_{\text{up}}} \quad \text{and} \quad (\bar{\eta'})_{\text{dn}} = \frac{\int_{x_0}^{x_{\text{dn}}} \eta' dx}{L_{\text{dn}}}. \quad (31.217)$$

Show that the expression for  $\Delta\eta'$  is independent of the two slopes. Instead, the only geometric property that determines  $\Delta\eta'$  is the ridge height,  $H$ . Discuss this result.

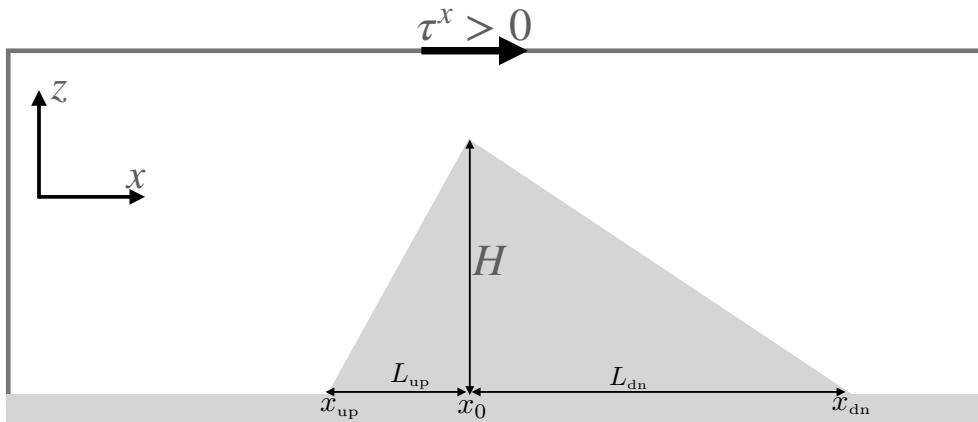


FIGURE 31.10: Zonal-vertical view of a single layer of shallow water fluid moving in a zonally re-entrant channel for use in Exercise 31.6. The domain has a topographic ridge that is a function just of the zonal direction and has constant slopes on its western and eastern sides. There is a constant eastward zonal wind stress.

## EXERCISE 31.7: GEOSTROPHIC TRANSPORT

Consider a zonal-vertical section of shallow water flow in the middle latitude northern hemisphere. Let the section be 1000 m deep and away from side and bottom boundaries. Assume the sea level is 1 cm higher at the eastern end of the section than the western end. Estimate the mass transport (kg/sec) of constant density seawater going through the section. What direction is the transport? Hint: Assume geostrophic balance; choose a representative constant seawater density; and note that the zonal width of the section cancels out so it is not needed.

## EXERCISE 31.8: APE FOR A SINGLE SHALLOW WATER LAYER WITH BOTTOM TOPOGRAPHY

Generalize the APE discussion in Section 31.3.4 to allow for a nonzero bottom topography,  $z = \eta_b(x, y)$ . Show that the APE is non-negative, just as for the flat bottom case. Assume the domain is simply connected.

## EXERCISE 31.9: APE FOR TWO SHALLOW WATER LAYERS

Compute the APE for two shallow water layers using the notation from Figure 30.6 with nontrivial bottom topography,  $z = \eta_b(x, y)$ . Show that the APE is non-negative. Assume the domain is

simply connected.

**EXERCISE 31.10: RATIO OF KE TO APE FOR SINGLE LAYER  $f$ -PLANE GEOSTROPHY**

Consider a single layer of shallow water fluid in geostrophic balance on an  $f$ -plane with a flat bottom. Show that the ratio of kinetic energy to available potential energy scales like

$$\frac{E_{\text{KE}}}{E_{\text{APE}}} \sim \left[ \frac{L_d^{\text{ext}}}{L} \right]^2. \quad (31.218)$$

In this equation,  $L$  is the horizontal length scale for the fluctuation of the free surface  $\eta$  (i.e.,  $\nabla \eta \sim \eta'/L$ ), and

$$L_d^{\text{ext}} = \frac{\sqrt{g H}}{f} \quad (31.219)$$

is the external deformation radius. The scaling (31.218) means that for scales larger than the external deformation radius,  $L_d$ , the available potential energy is larger than the kinetic energy. The converse holds for scales smaller than  $L_d$ .

**EXERCISE 31.11: RATIO OF KE TO APE FOR 1.5 LAYER  $f$ -PLANE GEOSTROPHY**

Consider a reduced gravity system (Section 30.3) in geostrophic balance on an  $f$ -plane. Show that the ratio of kinetic energy to available potential energy scales like

$$\frac{E_{\text{KE}}}{E_{\text{APE}}} \sim \left[ \frac{L_d^{\text{int}}}{L} \right]^2. \quad (31.220)$$

In this equation,  $L$  is the horizontal length scale for the fluctuation of the internal interface  $\eta_{3/2}$  (i.e.,  $\nabla \eta_{3/2} \sim \eta'_{3/2}/L$ ), and

$$L_d^{\text{int}} = \frac{\sqrt{g_{3/2}^r h}}{f} \quad (31.221)$$

is the internal deformation radius with  $g_{3/2}^r = g(\rho_2 - \rho_1)/\rho_1$  the reduced gravity and  $h = A^{-1} \int (\eta_{1/2} - \eta_{3/2}) dA$  the area averaged layer thickness (see Figure 30.4). The scaling (31.220) means that for scales larger than the internal deformation radius,  $L_d^{\text{int}}$ , the available potential energy is larger than the kinetic energy, and conversely for scales smaller than  $L_d^{\text{int}}$ .

To solve this exercise you must make use of the following.

- Derive the APE for two layers with a flat bottom.
- Assume the contribution to the APE from free surface undulations, is much smaller than from the interior interface. So that the APE is roughly due just to undulations of the interior interface. This assumption follows from Figure 30.5.
- The scaling (31.220) is identical to that found for the quasi-geostrophic system in Section 40.6.4. However, to solve this exercise it is not sufficient to merely reproduce the scaling discussed in Section 40.6.4. Instead, use here the expressions for APE and KE appropriate for the shallow water system.

**EXERCISE 31.12: NON-DIMENSIONALIZED LINEAR SHALLOW WATER EQUATIONS**

For the linear equations (31.178a)-(31.178b), introduce

$$\mathbf{x} = L \hat{\mathbf{x}}, \quad \mathbf{u}' = U \hat{\mathbf{u}}, \quad t = \frac{L \hat{t}}{U}, \quad f = \hat{f} T^{-1}, \quad \eta' = H \hat{\eta}, \quad (31.222)$$

where  $L$  is a horizontal length scale,  $T = L/U$  is an advective time scale,  $U$  is a velocity scale, and  $H \ll L$  is the resting layer thickness. All variables with hats are non-dimensional and not to be confused with unit vectors. Substitute into equations (31.178a)-(31.178b) and identify the non-dimensional ratio of the advective velocity scale to the non-rotating gravity wave speed

$$\text{Fr} \equiv \frac{U}{\sqrt{g H}}. \quad (31.223)$$

This non-dimensional number is known as the *Froude number*. When the Froude number is larger than unity, the fluid can experience an instability known as an *hydraulic jump*, with some elements of jumps discussed in Exercise 30.2.

#### EXERCISE 31.13: SHALLOW WATER KELVIN WAVES

This exercise works through the basics of Kelvin waves as presented by Section 3.8.3 of [Vallis \(2017\)](#). The Kelvin wave is an inertia-gravity wave that arises from the presence of a boundary<sup>14</sup> and rotation. To develop the basic Kelvin-wave solution, it is convenient to orient the  $f$  plane with a solid boundary along a line of constant latitude,  $y = y_0$ . The meridional velocity component must vanish at this boundary to satisfy the no-normal flow condition. We are thus motivated to consider an ansatz with  $v' = 0$  everywhere and see whether there are nontrivial solutions maintaining this structure.

1. Derive the linearized equations of motion for the  $f$ -plane shallow water Kelvin wave.
2. Derive the one-dimensional wave equation for the zonal velocity fluctuation.
3. What is the wave speed?
4. Following the discussion in Section 3.7, write the linear wave equation solution in the form

$$u'(x, y, t) = F_1(x + ct, y) + F_2(x - ct, y), \quad (31.224)$$

Verify that this form satisfies the wave equation derived above for any general functions  $F_1$  and  $F_2$ .

5. What is the expression for the surface height displacement,  $\eta'$ ?

From the above we can determine the  $y$ -dependence to the Kelvin wave

$$L_d \frac{\partial F_1}{\partial y} = F_1 \quad \text{and} \quad L_d \frac{\partial F_2}{\partial y} = -F_2, \quad (31.225)$$

where  $L_d = c/f = \sqrt{g H}/f$  is the shallow water deformation radius given by equation (31.183). Solutions to equations (31.225) are given by

$$F_1 = F(x + ct) e^{(y-y_0)/L_d} \quad \text{and} \quad F_2 = G(x - ct) e^{-(y-y_0)/L_d}. \quad (31.226)$$

To ensure boundedness in the region  $y > y_0$  where the fluid is assumed to exist, we drop the  $F_1$  piece of the general solution, thus leaving

$$\mathbf{u}' = \hat{\mathbf{x}} e^{-(y-y_0)/L_d} G(x - ct) \quad \text{and} \quad \eta' = (H/g)^{1/2} e^{-(y-y_0)/L_d} G(x - ct). \quad (31.227)$$

---

<sup>14</sup>Kelvin waves also occur at the equator, which acts as a boundary due to the change in sign of  $f$ . We only consider Kelvin waves that arise from a vertical side wall.

The specific form of the wave signal,  $G(x - ct)$ , is determined by the initial conditions of the pulse. Regardless the form of this wave pulse, these signals are non-dispersive waves that propagate in the positive  $\hat{x}$  direction, in which case the boundary  $y = y_0$  is on the right when facing in the direction of propagation. This orientation holds for any boundary orientation in the northern hemisphere, whereby Kelvin waves propagate with the solid boundary on the right when looking in the direction of wave movement. For the southern hemisphere Kelvin waves propagate with the boundary to the left of the wave motion. Hence, Kelvin waves propagate in a cyclonic direction. This result extends to the equator as well, where  $f = 0$  at the equator acts as a “wall” that supports the equatorial Kelvin waves.

Kelvin waves have an exponential decay in the direction perpendicular to the boundary with an e-folding length scale given by the deformation radius,  $L_d$ . We thus refer to the waves as “trapped waves”, with exponential boundary trapping over a length scale determined by the deformation radius.

**EXERCISE 31.14: DEFORMATION RADIUS**

The deformation radius appears in many contexts within rotating fluid dynamics. Here, we compute this length scale for selective geophysical flow regimes.

- (a) Compute the shallow water deformation radius for an ocean continental shelf of depth 500 m.
- (b) Compute the shallow water deformation radius for the deep ocean with depth 5000 m.
- (c) The deformation radius defined in this chapter is sometimes called the *external deformation radius* as it makes use of the full depth of the fluid and the gravitational acceleration. In contrast, the deformation radius defined in terms of internal layer thickness and reduced gravity  $g'$  leads to the internal deformation radius. The internal deformation radius,  $L_d^{\text{int}} = \sqrt{g' h} / f$  is the appropriate rotational length scale for density layers in the interior of the ocean or isentropic layers in the interior of the atmosphere. Compute the deformation radius for a density layer of thickness  $h = 200$  m and reduced gravity of  $g' = g/1000$ .



## **Part VI**

# **Vorticity and potential vorticity**

Vorticity locally measures the spin of a fluid element. It is the natural extension to continuum kinematics of the angular velocity and angular momentum used in rigid body kinematics. For geophysical flows, external forces, ultimately due to differential heating over the planet, resupply vorticity in the face of dissipation. The addition of planetary vorticity, arising from motion on a rotating spherical planet, also renders a nonzero vorticity to geophysical fluids even when the fluid is at rest in the rotating earth reference frame. Vorticity thus plays a central role in geophysical fluid motions, even for relatively sluggish and laminar flow, since motion on a rotating planet always involves vorticity. Furthermore, potential vorticity is a strategically chosen component of vorticity whose conservation properties are simpler than the full vorticity vector. Indeed, under certain assumptions of balance (considered in Part VII), knowledge of potential vorticity offers the means to deduce all prognostic information about the flow. For these reasons, potential vorticity has found great use for understanding and predicting geophysical fluid flows.

#### OUTLINE OF THIS PART

We start this part of the book by introducing vorticity and circulation in Chapter 32, making use of Stokes' Theorem to show that the area integral of vorticity over a finite region yields the circulation around the region's boundary. Chapter 33 considers the case where the horizontal flow is non-divergent, thus leading to the study of non-divergent barotropic flow. This flow is fully described by the vorticity field, and it offers many insights into large-scale vortical flows in the atmosphere and ocean. Chapter 34 then introduces the mechanics of vorticity and potential vorticity within a shallow water fluid, which builds on the discussion of the simpler non-divergent barotropic model. It was for the shallow water system that [Rossby \(1940\)](#) showed how powerful the notion of potential vorticity conservation is for understanding geophysical fluid flow patterns.

Chapter 35 then dives into the fundamentals of vorticity and circulation. It is here that we encounter Kelvin's Circulation Theorem, which identifies the materially conserved nature of circulation around an arbitrary loop in a perfect barotropic flow. Chapter 36 presents the foundations of potential vorticity, with Chapter 37 closing this part of the book by studying the remarkable impermeability property of the potential vorticity flux and its implications for potential vorticity budgets.

# Chapter 32

## Vorticity and circulation

Vorticity measures the spin of a flow at each point within the fluid. Vorticity is the generalization to continuum kinematics of the angular velocity relevant to rigid body kinematics. Circulation also measures spin, but as defined over a closed line integral (circuit) within the fluid. Helmholtz was an early proponent of vorticity whereas Kelvin was a proponent of circulation. These two properties of fluid motion are connected through Stokes' theorem. In this chapter we introduce the basic kinematic notions of vorticity and circulation with a focus on developing intuition. We also discuss the relation between vorticity, angular momentum, and the rate of strain.

### CHAPTER GUIDE

This chapter makes use of vector calculus identities for Cartesian coordinates as detailed in Chapter 2. The ideas introduced in this brief chapter are fundamental to the remaining chapters in this part of the book.

32.1	Vorticity . . . . .	<b>780</b>
32.1.1	Rotation of line elements . . . . .	781
32.1.2	Rotating reference frame . . . . .	781
32.1.3	There are no vorticity sources . . . . .	782
32.1.4	Further study . . . . .	782
32.2	Irrational flows . . . . .	<b>782</b>
32.2.1	Characterizing irrational flows . . . . .	782
32.2.2	Comments . . . . .	782
32.3	Circulation of the velocity field . . . . .	<b>783</b>
32.4	The free vortex . . . . .	<b>784</b>
32.4.1	Motion of a fluid particle . . . . .	784
32.4.2	Circulation . . . . .	785
32.5	Translation and solid-body rotation . . . . .	<b>786</b>
32.5.1	Absolute vorticity . . . . .	786
32.5.2	Solid-body rotation on a plane . . . . .	786
32.5.3	Circulation for solid-body rotation . . . . .	787
32.5.4	Comments . . . . .	787
32.6	Relative vorticity from curvature and shear . . . . .	<b>787</b>
32.6.1	Circular flow . . . . .	788
32.6.2	Generalization to natural coordinates . . . . .	788
32.6.3	Example vorticities . . . . .	789
32.7	Relating angular momentum to vorticity and strain . . . . .	<b>791</b>
32.7.1	Linear momentum . . . . .	791

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32.7.2	Angular momentum . . . . .	792
32.7.3	Taylor expanding the velocity . . . . .	793
32.7.4	Angular momentum, rate of strain, and vorticity . . . . .	794
32.7.5	Comments and further reading . . . . .	795
32.8	Exercises . . . . .	795

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## 32.1 Vorticity

Vorticity is the curl of the velocity field

$$\boldsymbol{\omega} = \nabla \times \mathbf{v}. \quad (32.1)$$

Vorticity measures the rotation or spin of fluid motion at each point and, unlike angular momentum, it does so without reference to an origin. In addition to writing vorticity as the curl of the velocity, we may choose to use the equivalent expression

$$\boldsymbol{\omega} = [\nabla \cdot (\mathbf{v} \times \hat{\mathbf{x}})] \hat{\mathbf{x}} + [\nabla \cdot (\mathbf{v} \times \hat{\mathbf{y}})] \hat{\mathbf{y}} + [\nabla \cdot (\mathbf{v} \times \hat{\mathbf{z}})] \hat{\mathbf{z}}. \quad (32.2)$$

That is, a vorticity component in a particular coordinate direction is the divergence of the velocity field after being rotated by  $-\pi/2$  around the coordinate axis direction. For example, the vector  $\mathbf{v} \times \hat{\mathbf{z}}$  is the result of rotating the velocity by  $-\pi/2$  radians around the  $\hat{\mathbf{z}}$  axis, with the identity

$$\hat{\mathbf{z}} \cdot (\nabla \times \mathbf{v}) = \nabla \cdot (\mathbf{v} \times \hat{\mathbf{z}}) \quad (32.3)$$

leading to the vertical component of the vorticity in equation (32.2).

Being the curl of a vector, the vorticity transforms as a vector under coordinate rotations. However, vorticity changes sign under mirror symmetry, thus making it a pseudo-vector (Section 1.4.2). A simple means to understand this property is to note that the spinning earth rotates counter clockwise when viewed from above the north pole and clockwise when viewed from below the south pole (see Figure 9.3).

Figure 32.1 provides an example zonal flow with a meridional strain (shear). The vertical component to the vorticity is negative for this flow, as per the right hand rule. Furthermore, an imaginary test “paddle wheel” placed anywhere within this flow spins clockwise about its axis. The nonzero spin of test paddle wheels is a fundamental character of fluid flow with nonzero vorticity.

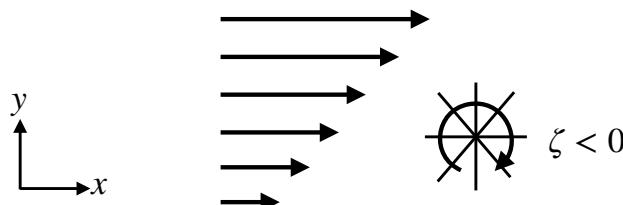


FIGURE 32.1: An example zonal flow with a meridional shear,  $\mathbf{v} = u(y) \hat{\mathbf{x}}$ , and a corresponding vertical vorticity component that is negative:  $\zeta = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{v}) = \partial v / \partial x - \partial u / \partial y = -\partial u / \partial y < 0$ . The clockwise arrow surrounds a test “paddle wheel” that exhibits a clockwise spin about its axis when placed in this flow. Such test paddle wheels only spin when there is nonzero vorticity. The right hand rule determines the sign of the vorticity, which for this example is into the page (negative  $\hat{\mathbf{z}}$ ).

### 32.1.1 Rotation of line elements

In Section 13.3 we considered the kinematic evolution of a line element,  $\delta\mathbf{x}$ , separating two fluid particles, with that evolution provided by equation (13.31)

$$\frac{D(\delta x_m)}{Dt} = \delta x_n \frac{\partial v_m}{\partial x_n} \implies \frac{D(\delta \mathbf{x})}{Dt} = (\delta \mathbf{x} \cdot \nabla) \mathbf{v}. \quad (32.4)$$

This equation says that the material line element evolves according to the velocity gradient tensor  $\partial_n v_m$ . The symmetric portion of this tensor is the rate of strain tensor,

$$\mathbb{S}_{mn} = (\partial_n v_m + \partial_m v_n)/2, \quad (32.5)$$

whose action generates changes in the distance between the fluid particles (Section 13.3.7). The anti-symmetric portion to the velocity gradient tensor is known as the rotation tensor,

$$\mathbb{R}_{mn} = (\partial_n v_m - \partial_m v_n)/2. \quad (32.6)$$

The rotation tensor is related to vorticity via equation (13.44)

$$\mathbb{R}_{mn} = -\epsilon_{mnp} \omega_p/2 \iff \mathbb{R} = \frac{1}{2} \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix}, \quad (32.7)$$

so that

$$2 \mathbb{R}_{mn} \delta x_n = -\epsilon_{mnp} \omega_p \delta x_n \implies 2 \mathbb{R} \cdot \delta \mathbf{x} = \boldsymbol{\omega} \times \delta \mathbf{x}. \quad (32.8)$$

From our discussion of rotation in Section 9.4, this equation means that vorticity in a fluid generates a rigid rotation of a material line element (Section 13.3.8). This result accords with Figure 32.1, whereby vorticity leads to the spin of a test paddle wheel; i.e., the rotation of line elements.

### 32.1.2 Rotating reference frame

As another means to understand the kinematics of vorticity, let us view the flow field from a reference frame that rotates with a constant angular velocity,  $\boldsymbol{\Gamma}$ . Following equation (9.73e), we know that the velocity observed in the non-rotating reference frame,  $\mathbf{v}$ , is related to the rotating reference frame velocity,  $\mathbf{v}_{\text{rot}}$ , via

$$\mathbf{v} = \mathbf{v}_{\text{rot}} + \boldsymbol{\Gamma} \times \mathbf{x}. \quad (32.9)$$

The vorticity in the two reference frames is thus related by

$$\boldsymbol{\omega} = \nabla \times \mathbf{v} = \nabla \times \mathbf{v}_{\text{rot}} + \nabla \times (\boldsymbol{\Gamma} \times \mathbf{x}) = \boldsymbol{\omega}_{\text{rot}} + 2 \boldsymbol{\Gamma}. \quad (32.10)$$

If there is a point in the fluid whereby the rotating reference frame's angular velocity equals to one-half the vorticity at that point,  $\boldsymbol{\Gamma} = \boldsymbol{\omega}/2$ , then the rotating reference frame's vorticity vanishes at that point

$$\boldsymbol{\Gamma} = \boldsymbol{\omega}/2 \implies \boldsymbol{\omega}_{\text{rot}} = 0. \quad (32.11)$$

Hence, we may interpret  $\boldsymbol{\omega}/2$  as the angular velocity of the fluid circulating around any point in the fluid. That is, the vorticity is twice the local angular velocity of the fluid. Furthermore, if the vorticity,  $\boldsymbol{\omega}$ , is spatially constant, then we can move to a rotating reference frame in which the vorticity vanishes everywhere, with such flow referred to as *irrotational*.

### 32.1.3 There are no vorticity sources

Vorticity has zero divergence

$$\nabla \cdot \boldsymbol{\omega} = \nabla \cdot (\nabla \times \mathbf{v}) = 0. \quad (32.12)$$

This property is akin to the non-divergent nature of the velocity vector in an incompressible flow (see Chapter 16). However, vorticity is non-divergent for both compressible and incompressible flow. Consequently, there are no interior sources or sinks of vorticity for any fluid. This very basic property plays an important role in developing some further kinematic properties of vorticity in Chapter 35.

### 32.1.4 Further study

[This video from 3Blue1Brown](#) provides some compelling graphics to help develop intuition for the divergence and curl of a vector, with particular emphasis on fluid flow. In so doing, one learns much about vorticity.

## 32.2 Irrotational flows

Most geophysical flows have nonzero vorticity. Indeed, even when at rest on the earth, a geophysical fluid carries the vorticity of the rotating planet. However, if we can ignore the planetary vorticity component, as when focused on motions too small to feel the Coriolis acceleration, we can find some geophysically relevant flows with vanishing vorticity. Linear gravity waves in the absence of planetary rotation provide a particularly relevant example (Section 31.8.2).

### 32.2.1 Characterizing irrotational flows

Irrotational fluid flow is characterized by a zero vorticity

$$\boldsymbol{\omega} = 0 = \text{irrotational flow}. \quad (32.13)$$

Since the curl of a gradient vanishes, irrotational flow has a velocity field equal to the gradient of a velocity potential

$$\nabla \times \mathbf{v} = 0 \Rightarrow \mathbf{v} = \nabla \Psi. \quad (32.14)$$

Irrotational flow is therefore sometimes called *potential flow*. Figure 32.2 illustrates a two-dimensional flow field generated by taking the gradient of a scalar potential so that the flow has zero vorticity. In this case, the vertical component of the vorticity vanishes at each point since  $\partial v / \partial x = \partial u / \partial y$ .

If the flow is incompressible, as in a Boussinesq fluid (Section 23.1), then the velocity potential is a harmonic function since it satisfies Laplace's equation

$$\nabla \cdot \mathbf{v} = 0 \implies \nabla^2 \Psi = 0. \quad (32.15)$$

The study of harmonic functions is a very mature area of mathematical physics, thus providing a great deal of analytic power towards the study of potential flow for incompressible fluids.

### 32.2.2 Comments

This book does not discuss turbulence in any depth. Nevertheless, we here note that three dimensional turbulence fundamentally relies on vorticity. Hence, irrotational flows, though they may exhibit chaotic motions, are not turbulent since they do not allow for the nonlinear cascade of energy to small spatial scales, with this cascade a fundamental characteristic of three dimensional

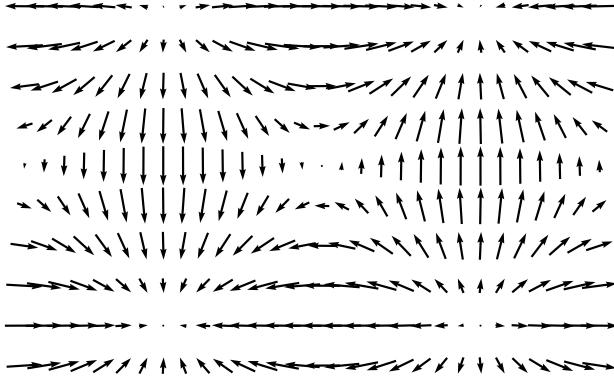


FIGURE 32.2: An example horizontal flow based on a potential,  $\Psi = \sin(x/5) \sin(y/5)$ . The flow has zero vorticity,  $\omega \cdot \hat{z} = \zeta = \partial v / \partial x - \partial u / \partial y = 0$ , since the flow is based on a scalar potential:  $\omega = \nabla \times \mathbf{v} = \nabla \times \nabla \Psi = 0$ . This example illustrates how irrotational flow may have nontrivial structure even though a test paddle wheel will not spin since there is zero vorticity.

turbulence. As we will see in Section 35.4, vorticity evolves from sources that tilt and stretch vortex tubes. Vortex stretching is the key source for the turbulent cascade in three dimensional turbulence. Section 3.3 of [Tennekes and Lumley \(1972\)](#) provides a pedagogical discussion of vorticity in the context of three-dimensional turbulence.

### 32.3 Circulation of the velocity field

The velocity circulation, or more briefly the *circulation*, is defined as the oriented closed loop line integral of velocity as projected onto the unit tangent of the path

$$\mathcal{C} \equiv \oint_{\partial S} \mathbf{v} \cdot d\mathbf{r}, \quad (32.16)$$

with Figure 32.3 offering a schematic. The line element,  $d\mathbf{r}$ , is oriented in the counter-clockwise direction around the circuit  $\partial S$ . More precisely, let  $\mathbf{r}(\varphi)$  be an expression for the position of a point on the circuit, with  $\varphi(x, y, z, t)$  a parameter that measures the distance along the closed circuit (see Section 2.4). The difference between two very close positions along the circuit defines the increment

$$d\mathbf{r} = \mathbf{r}(\varphi + \delta\varphi) - \mathbf{r}(\varphi). \quad (32.17)$$

By construction,  $d\mathbf{r}$  is tangent to the circuit so that  $\mathbf{v} \cdot d\mathbf{r}$  picks out the component of the velocity that is tangent to the path.

Stokes' theorem (Section 2.6) renders the very important identity

$$\mathcal{C} = \oint_{\partial S} \mathbf{v} \cdot d\mathbf{r} = \int_S (\nabla \times \mathbf{v}) \cdot \hat{\mathbf{n}} dS = \int_S \boldsymbol{\omega} \cdot \hat{\mathbf{n}} dS, \quad (32.18)$$

where  $\hat{\mathbf{n}}$  is the outward normal vector orienting the area according to the right-hand rule applied to the bounding circuit. The area integral expression motivates interpreting velocity circulation as the “flux of vorticity” penetrating the area. Stokes' theorem provides the means to connect the vorticity theories promoted by Helmholtz to the circulation theories of Kelvin.

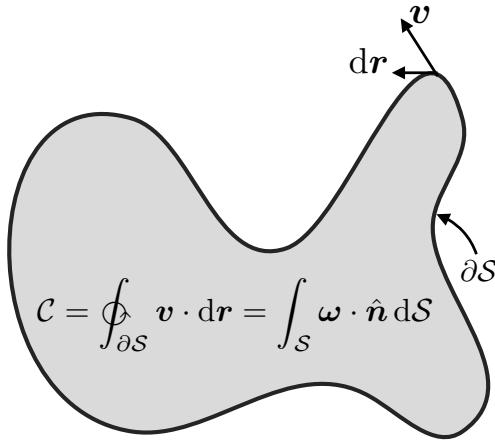


FIGURE 32.3: The velocity circulation around the boundary of a region,  $\partial\mathcal{S}$ , is determined by the line integral of the velocity projected into the direction of the line integral,  $\mathbf{v} \cdot d\mathbf{r}$ . Stokes' theorem shows that the velocity circulation computed as a line integral is identical to the normal projection of the vorticity integrated over the area of the region,  $C = \oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{r} = \int_{\mathcal{S}} \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S}$ .

## 32.4 The free vortex

Consider a two-dimensional rotating fluid in the  $x$ - $y$  plane with angular velocity given by

$$\boldsymbol{\Omega} = \frac{\mathbf{x} \times \mathbf{v}}{r^2} = \frac{K \hat{\mathbf{z}}}{r^2}. \quad (32.19)$$

The constant  $K$  has dimensions  $L^2 T^{-1}$ , and  $r^2 = x^2 + y^2$  is the squared distance from the axis of rotation with  $\hat{\mathbf{z}}$  the unit vector normal to the  $x$ - $y$  plane. The angular velocity falls off as the squared distance from the center, whereas it is singular at the origin. As shown in this section, the fluid flow associated with this *free vortex* has zero vorticity and zero circulation for all points except the origin. Yet the same points with zero vorticity and zero circulation have a constant angular momentum relative to the origin. As shown by Exercise 32.4, and pursued in more detail in Section 32.7, nonzero angular momentum can arise in a fluid with zero circulation so long as there is a nonzero strain within the fluid, such as in the free vortex.

### 32.4.1 Motion of a fluid particle

A fluid particle moves in a circular orbit when in the free vortex flow field. Hence, the particle velocity is perpendicular to its position vector,  $\mathbf{x} = x \hat{\mathbf{x}} + y \hat{\mathbf{y}}$ , with respect to the origin

$$\mathbf{v} \cdot \mathbf{x} = 0. \quad (32.20)$$

The velocity for this pure rotational flow is given by (see Section 9.4)

$$\mathbf{v} = \boldsymbol{\Omega} \times \mathbf{x} = \frac{K(-y \hat{\mathbf{x}} + x \hat{\mathbf{y}})}{r^2} = \frac{K \hat{\vartheta}}{r}, \quad (32.21)$$

where  $\hat{\vartheta}$  is the polar angle unit vector oriented in the counter-clockwise direction (see Section 8.3). Each component of the velocity falls off as  $1/r$  when moving away from the origin. Away from the origin, the vorticity vector vanishes

$$\boldsymbol{\omega} = \nabla \times \mathbf{v} = 0, \quad (32.22)$$

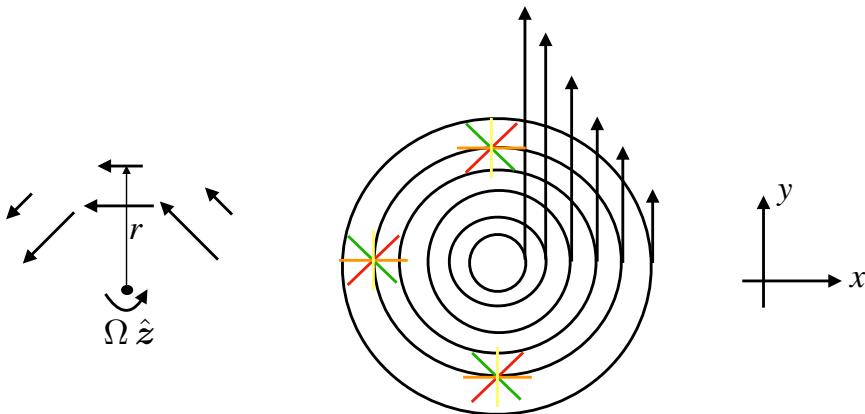


FIGURE 32.4: Irrotational counter-clockwise planar flow in the presence of a free vortex with velocity  $\mathbf{v} = (K/r)\hat{\theta}$ . The tangential velocity decays as  $1/r$  from the origin and the vorticity,  $\nabla \times \mathbf{v}$ , vanishes for all points except the origin. Also, test paddle wheels (colored line segments) do not spin when removed from the center since there is zero vorticity. Notice also that the free vortex has constant angular momentum per mass (computed relative to the origin), since the tangential velocity falls off as  $1/r$  thus canceling the moment-arm distance  $r$ .

whereas it is singular at the origin.

As noted above, although vorticity is zero everywhere (except at the origin), the angular momentum is nonzero, as expected since the fluid is rotating around the vortex center. The angular momentum for this system arises just from the nonzero strain in the flow field (see Exercise 32.4), with the strain causing fluid particles to move relative to one another. The angular momentum per unit mass, relative to the center of the vortex, is constant and pointed vertically

$$\mathbf{r} \times \mathbf{v} = r \hat{\mathbf{r}} \times (K/r) \hat{\theta} = K \hat{\mathbf{z}}. \quad (32.23)$$

This result follows since the velocity falls off as  $1/r$  to cancel the moment-arm distance,  $r$ . Hence, the angular momentum per mass is the same for all fluid particles in the presence of a free vortex, no matter what radial distance the particles have from the vortex center.

We illustrate the free vortex velocity field (32.21) in Figure 32.4 along with test paddle wheels. The paddle wheels remain stationary when placed away from the origin, in the region where the vorticity vanishes. As the paddle wheel centers move counter-clockwise with the flow, the marked paddle wheel blades remain oriented at the same angle. That is, the paddle wheels orbit around the vortex center but they do not spin. The free vortex thus illustrates a fluid flow with non-zero angular momentum yet with zero vorticity (except at the origin).

### 32.4.2 Circulation

The circulation vanishes for any circuit bounded away from the origin, and it does so trivially since vorticity vanishes away from the origin. However, the circulation is nonzero for any circuit enclosing the origin

$$\mathcal{C} = \oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{r} = \int_0^{2\pi} \mathbf{v} \cdot \hat{\theta} r d\theta = 2\pi K. \quad (32.24)$$

To reach this result, we set the line element to

$$d\mathbf{r} = \hat{\theta} r d\theta \quad (32.25)$$

and inserted the velocity (32.21) represented in cylindrical polar coordinates,  $\mathbf{v} \cdot \hat{\boldsymbol{\vartheta}} = K/r$ . Hence, the singular point vortex at  $r = 0$  induces a nonzero circulation for all circuits that enclose the vortex.

## 32.5 Translation and solid-body rotation

Rigid or solid-body fluid motion occurs when all fluid particles are rigidly locked into their relative positions, as if in a rigid solid body. There are two kinds of rigid body motion: translation and rotation. The velocity field for this motion is given by

$$\mathbf{v} = \mathbf{U} + \boldsymbol{\Omega} \times \mathbf{x}, \quad (32.26)$$

where  $\mathbf{x}$  is the position vector relative to the origin,  $\mathbf{U}$  is a translation velocity, and  $\boldsymbol{\Omega}$  is an angular velocity. For rigid body motion, both  $\mathbf{U}$  and  $\boldsymbol{\Omega}$  are spatially uniform, but can in general be time dependent. The rate of strain tensor vanishes for uniform translation or solid-body motion (see Exercise 13.2)

$$S_{mn} = \frac{1}{2}(\partial_m v_n + \partial_n v_m) = 0. \quad (32.27)$$

However, the vorticity is nonzero (see Exercise 32.1)

$$\boldsymbol{\omega} = \nabla \times (\boldsymbol{\Omega} \times \mathbf{x}) = 2\boldsymbol{\Omega}. \quad (32.28)$$

We encountered this vorticity in Section 32.1.2 when connecting vorticity and angular velocity.

### 32.5.1 Absolute vorticity

For planetary fluid dynamics, rotation of the planet imparts *planetary vorticity* to fluids. Hence, the total or *absolute* vorticity of a fluid is the vector sum of the *relative vorticity*,  $\boldsymbol{\omega}$ , plus the planetary vorticity

$$\boldsymbol{\omega}_{\text{absolute}} = \boldsymbol{\omega}_{\text{planet}} + \boldsymbol{\omega}. \quad (32.29)$$

In this equation,

$$\boldsymbol{\omega}_{\text{planet}} = 2\boldsymbol{\Omega}_{\text{planet}} \quad (32.30)$$

is the planetary vorticity associated with solid-body motion of a fluid particle stationary with respect to the planet, and

$$\boldsymbol{\omega} = \nabla \times \mathbf{v} \quad (32.31)$$

is the relative vorticity. The relative vorticity measures the vorticity of the fluid due to motion relative to the rotating sphere, with  $\mathbf{v}$  the velocity relative to the rotating sphere.

### 32.5.2 Solid-body rotation on a plane

Consider the circular solid-body rotation on a plane shown in Figure 32.5, in which the velocity is purely tangential and linearly proportional to the distance from the center

$$\mathbf{v} = \boldsymbol{\Omega} \times \mathbf{x} = |\boldsymbol{\Omega}|(-y \hat{\mathbf{x}} + x \hat{\mathbf{y}}) = |\boldsymbol{\Omega}| r \hat{\boldsymbol{\vartheta}}. \quad (32.32)$$

Assuming the center of mass to be at the circle center, the angular momentum for the flow is the same as that for a solid-body. Even though the motion of each fluid particle is rigidly fixed relative to all other particles, there is a nonzero vorticity in this flow as illustrated by the spin of colored test paddle wheels in Figure 32.5.

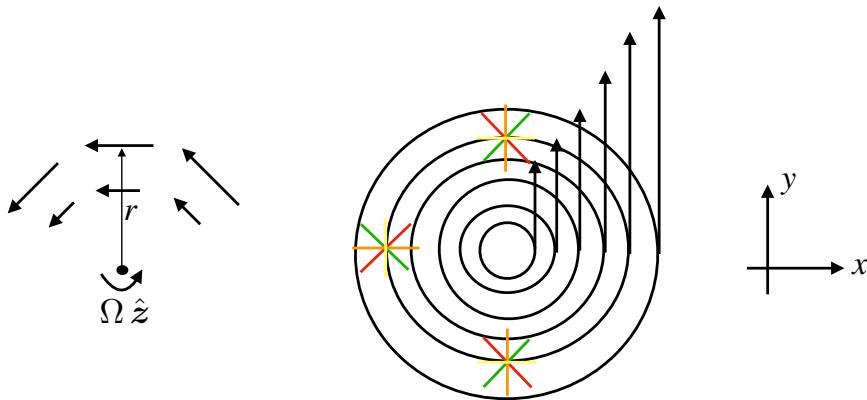


FIGURE 32.5: Rigid body fluid motion, whereby the fluid velocity is: (A) purely tangential and linearly proportional to the radial distance from the vortex center,  $v = |\Omega| r \hat{\vartheta}$ ; (B) fluid particles maintain a fixed relative position; (C) and vorticity is constant and points perpendicular to the page,  $\omega = 2\Omega = 2|\Omega| \hat{z}$ . Test paddle wheels rigidly move around the center, and they exhibit a spin about their axis that manifests the nonzero vorticity.

### 32.5.3 Circulation for solid-body rotation

For solid-body rotation, the velocity circulation around a circular path of radius  $R$  is given by

$$\mathcal{C} = \oint \mathbf{v} \cdot d\mathbf{r} = \oint (\boldsymbol{\Omega} \times \mathbf{r}) \cdot d\mathbf{r} = R^2 |\Omega| \oint d\vartheta = 2\pi R^2 |\Omega| = 2A |\Omega|, \quad (32.33)$$

where  $A = \pi R^2$  is the area of the circle. Hence, the velocity circulation per area for solid-body rotating fluid flow is twice the angular rotation rate, which is the magnitude of the vorticity

$$\mathcal{C}/A = |\omega| = 2|\Omega|. \quad (32.34)$$

### 32.5.4 Comments

As seen in Section 32.4, fluid flow in the presence of a free vortex has zero vorticity for all points except the origin of the vortex. However, the same points also have a constant angular momentum relative to the origin, and they experience a nonzero strain. In contrast, constant solid-body rotating fluid flow has a nonzero vorticity, nonzero angular momentum, yet a zero strain. Section 32.7 details the connection between vorticity, strain, and angular momentum, where we see that angular momentum can be nonzero if either vorticity or strain are nonzero. These ideas are illustrated in [this 3-minute video](#) as well as in this [10 minute video from the Open University](#).

## 32.6 Relative vorticity from curvature and shear

In this section we decompose the vorticity into two terms: one arising from curvature in the flow and another arising from shears in the direction normal to the flow. This decomposition is formulated for horizontal flows, but can be generalized to arbitrary flow. It offers yet another means to understand the kinematic properties of vorticity.

### 32.6.1 Circular flow

Before treating the general case, it is useful to consider a two-dimensional velocity that locally takes the form of an angular flow

$$\mathbf{u} = u^\vartheta(r, \vartheta) \hat{\boldsymbol{\vartheta}}, \quad (32.35)$$

where  $\vartheta$  is the polar angle. Circulation around the circular wedge shown in Figure 32.6 has zero contributions from the two radial segments since these segments are perpendicular to the angular flow. The circulation is thus given by

$$\mathcal{C} = \oint_{\text{wedge}} \mathbf{u} \cdot d\mathbf{r} \quad (32.36a)$$

$$= \int_{\vartheta}^{\vartheta+\delta\vartheta} u^\vartheta(r + \delta r, \vartheta') (r + \delta r) d\vartheta' + \int_{\vartheta+\delta\vartheta}^{\vartheta} u^\vartheta(r, \vartheta') r d\vartheta' \quad (32.36b)$$

$$= \int_{\vartheta}^{\vartheta+\delta\vartheta} [u^\vartheta(r + \delta r, \vartheta') (r + \delta r) - r u^\vartheta(r, \vartheta')] d\vartheta' \quad (32.36c)$$

$$\approx \int_{\vartheta}^{\vartheta+\delta\vartheta} \left[ u^\vartheta(r, \vartheta') \delta r + \frac{\partial u^\vartheta}{\partial r} r \delta r \right] d\vartheta' \quad (32.36d)$$

$$= r \delta r \int_{\vartheta}^{\vartheta+\delta\vartheta} \left[ \frac{u^\vartheta}{r} + \frac{\partial u^\vartheta}{\partial r} \right] d\vartheta', \quad (32.36e)$$

where the approximation holds when  $\delta r \rightarrow 0$ . Taking the further limit  $\delta\vartheta \rightarrow 0$  renders

$$\mathcal{C} \approx \zeta \delta A = \zeta r \delta r \delta\vartheta = \left[ \frac{u^\vartheta}{r} + \frac{\partial u^\vartheta}{\partial r} \right] r \delta r \delta\vartheta \implies \zeta = \frac{u^\vartheta}{r} + \frac{\partial u^\vartheta}{\partial r}. \quad (32.37)$$

The first term in the vorticity arises from the nonzero radius of curvature of the circular flow whereas the second term arises from radial shear.

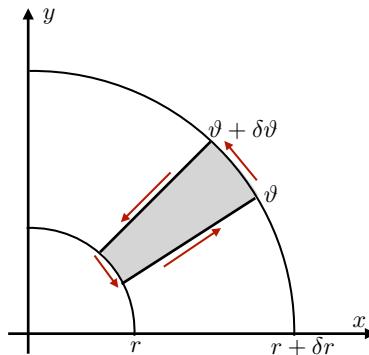


FIGURE 32.6: Circulation around the circular wedge  $[r, r + \delta r] \otimes [\vartheta, \vartheta + \delta\vartheta]$ .

### 32.6.2 Generalization to natural coordinates

The decomposition (32.37) can be generalized to arbitrary horizontal flow by making use of the natural coordinates from Section 26.2. Here, we introduce the locally orthogonal coordinates,  $(s, n)$ , with  $s$  the arc-length defined along the trajectory of a fluid element and  $n$  measuring the distance normal to the trajectory. We make the convention that the unit tangent direction,  $\hat{s}$ , is aligned along the local flow direction whereas the unit normal direction,  $\hat{n}$ , is to the left facing

downstream. Furthermore, the radius of curvature at a point along a trajectory (see Section 5.2.3) is positive if the flow turns into the positive  $\hat{\mathbf{n}}$  direction (left turn) and negative for oppositely curved flow (right turn) (see Figures 26.2 and 26.3). Finally, the radius of curvature is infinite for straight flow.

For the counter-clockwise circuit in Figure 32.6, a left turn occurs with  $\hat{\mathbf{n}} = -\hat{\mathbf{r}}$  so that equation (32.37) takes on the general form

$$\zeta = \underbrace{\frac{|\mathbf{u}|}{R}}_{\text{curvature}} - \underbrace{\frac{\partial |\mathbf{u}|}{\partial n}}_{\text{shear}} = \zeta_{\text{curv}} + \zeta_{\text{shear}}. \quad (32.38)$$

Again, the first term arises from curvature in the flow, with  $R$  the radius of curvature. This *curvature vorticity* is sometimes also called the *orbital vorticity*. A trajectory turning to the left has  $R > 0$  and this curved trajectory contributes to a positive vorticity; conversely for a trajectory turning to the right. The second term in equation (32.38) arises from shears computed normal to the flow direction. If the flow speed decreases in the normal direction (e.g., towards the center of the circle in Figure 32.6), then that too contributes to a positive vorticity. Furthermore, flow with  $\zeta = 0$  arises if there is an exact compensation between the curvature-induced vorticity with the shear-induced vorticity

$$\zeta = 0 \implies \frac{|\mathbf{u}|}{R} = \frac{\partial |\mathbf{u}|}{\partial n}. \quad (32.39)$$

### 32.6.3 Example vorticities

*Rigid body vortex and free vortex*

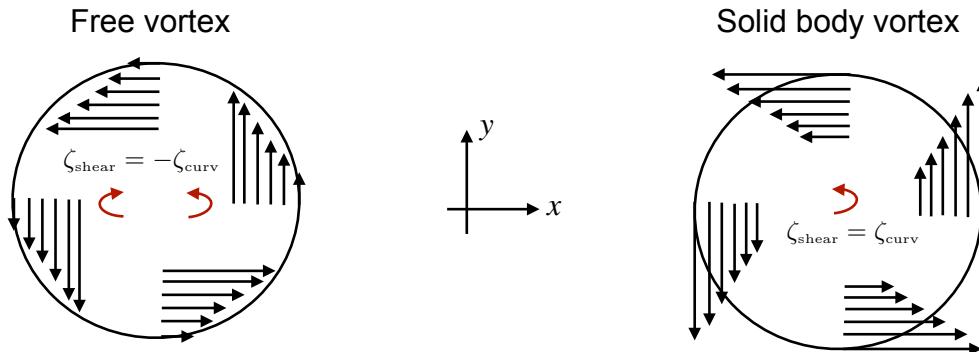


FIGURE 32.7: Decomposing the relative vorticity into its contributions from curvature and normal shear. Left panel: the free vortex from Figure 32.4 has  $\zeta_{\text{curv}} = -\zeta_{\text{shear}} = K/r^2$  so that  $\zeta = \zeta_{\text{curv}} + \zeta_{\text{shear}} = 0$ . Right panel: the solid body vortex from Figure 32.5 has  $\zeta_{\text{curv}} = \zeta_{\text{shear}} = \Omega$  so that  $\zeta = 2\Omega$ .

To help further understand the decomposition (32.38), consider the case of solid body rotation (Figure 32.5) where  $\mathbf{v} = \Omega r \hat{\boldsymbol{\vartheta}}$  and  $\hat{\mathbf{n}} = -\hat{\mathbf{r}}$ . For a circle the radius of curvature equals to the radius of the circle, so that

$$\zeta_{\text{curv}} = \frac{\Omega r}{r} = \Omega \quad \text{and} \quad \zeta_{\text{shear}} = -\partial_n |\mathbf{u}| = \partial_r (\Omega r) = \Omega, \quad (32.40)$$

in which case

$$\zeta = \zeta_{\text{curv}} + \zeta_{\text{shear}} = 2\Omega = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{v}), \quad (32.41)$$

as depicted in Figure 32.7. Likewise, for the free vortex (Figure 32.4) we have  $\mathbf{v} = (K/r) \hat{\boldsymbol{\vartheta}}$  so

that

$$\zeta_{\text{curv}} = K/r^2 \quad \text{and} \quad \zeta_{\text{shear}} = \partial|\mathbf{u}|/\partial r = -K/r^2, \quad (32.42)$$

which yields zero relative vorticity

$$\zeta = \zeta_{\text{curv}} + \zeta_{\text{shear}} = 0. \quad (32.43)$$

### Gaussian jet moving along a line and around a circle

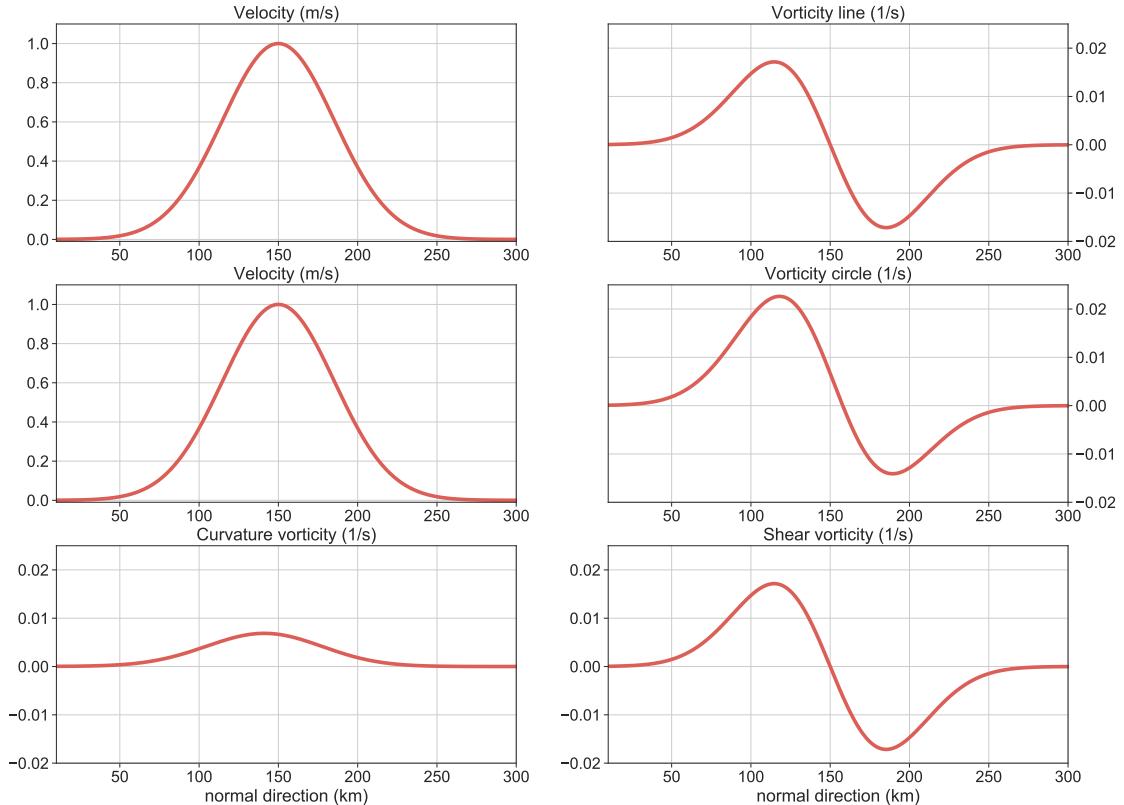


FIGURE 32.8: Top row: velocity and vorticity within a Gaussian jet that is moving along a straight line according to equations (32.44) and (32.45). We set the jet e-folding scale as  $L = 50$  km, jet maximum at  $x_{\max} = 150$  km, and velocity scale as  $v_o = 1$  m s $^{-1}$ . Note the symmetry of the vorticity relative to the jet maximum, with the vorticity extrema corresponding to the inflection points of the Gaussian velocity field. Middle left: the same Gaussian velocity profile only now for a jet that is moving counter-clockwise around a circle so that  $\mathbf{v} = v(r)\hat{\theta}$  according to equation (32.46). To avoid a singularity of the curvature vorticity at  $r = 0$  (infinite curvature) we assume the velocity field vanishes within a small distance from the origin. Middle right: vorticity for the Gaussian jet moving around the circle. Middle right: vorticity for the circular jet,  $\zeta = r^{-1}\partial_r(rv)$ . Notice how the vorticity is not symmetric relative to the jet maximum. Rather, the zero vorticity occurs to the right of the jet maximum, and the vorticity on the inside of the jet maximum is larger in magnitude than the outer vorticity. Lower left: vorticity due to the curvature of the jet as it moves around the circle,  $\zeta_{\text{curve}} = v(r)/r$ . Lower right: vorticity due to the radial shear in the Gaussian jet,  $\zeta_{\text{shear}} = -2(r - r_{\max})v(r)/L^2$ .

Next consider a Gaussian jet moving along a straight line in the meridional direction with velocity field

$$\mathbf{v}(x) = v(x)\hat{\mathbf{y}} = v_o \exp[-(x - x_{\max})^2/L^2]\hat{\mathbf{y}}, \quad (32.44)$$

where  $v_o$  is the velocity scale,  $L$  is the e-folding length scale for the jet, and  $x_{\max}$  is the position

of the jet maximum. The corresponding vorticity of the jet is given by

$$\zeta_{\text{line}} = \partial_x v = -2 [(x - x_{\max})/L^2] v(x). \quad (32.45)$$

We depict the velocity (32.44) and vorticity (32.45) in the top row of Figure 32.8. Note the symmetry of the vorticity around the jet maximum at  $x = x_{\max}$ , with the vorticity extrema corresponding to inflection points of the jet.<sup>1</sup>

Now assume the same jet is moving counter-clockwise around a circle so that the velocity field is given by

$$\mathbf{v}(r) = v(r) \hat{\boldsymbol{\vartheta}} = v_o \exp[-(r - r_{\max})^2/L^2] \hat{\boldsymbol{\vartheta}}, \quad (32.46)$$

where we made use of the polar coordinates from Section 8.3 with  $r^2 = x^2 + y^2$  the squared radial distance from the center, and  $\hat{\boldsymbol{\vartheta}}$  the unit vector pointing in the counter-clockwise direction from the  $\hat{\mathbf{x}}$  axis. Making use of the curl operation in polar coordinates given by equation (8.85c) renders the vorticity

$$\zeta = r^{-1} \partial_r(r v) = \frac{v}{r} - \frac{2(r - r_{\max}) v}{L^2} = \zeta_{\text{curve}} + \zeta_{\text{shear}}. \quad (32.47)$$

We depict these terms in the third row of Figure 32.8. Note how the vorticity,  $\zeta$ , has the amplitude of its maximum increased, whereas the amplitude of its minimum is decreased. Correspondingly, the vorticity is not symmetric about the jet maximum, with its zero crossing to the outside of the jet maximum. Asymmetry of the vorticity arises from the curvature vorticity,  $\zeta_{\text{curve}} = v/r$ , which has its peak inside the jet maximum. So although the shear vorticity,  $\zeta_{\text{shear}}$ , is symmetric around the jet axis, the curvature vorticity causes a movement of vorticity towards the center of the circle.

## 32.7 Relating angular momentum to vorticity and strain

As noted in Section 32.5.4, fluid flow in the presence of a free vortex (Section 32.4) has zero vorticity for all points except the origin of the vortex. However, the same points also have a constant angular momentum relative to the origin, and they experience a nonzero strain. In contrast, solid-body fluid flow (Section 32.5) has a nonzero vorticity, nonzero angular momentum, yet a zero strain. In this section we study the connection between vorticity, rate of strain, and angular momentum for a fluid continuum. We will here see that angular momentum and vorticity are fundamentally distinct in a fluid that has straining motion between fluid elements. In contrast, angular momentum and vorticity are directly proportional (through the moment of inertia tensor) when the fluid exhibits solid body motion in which the rate of strain tensor vanishes.

### 32.7.1 Linear momentum

To start the analysis, consider the velocity and linear momentum of a connected material fluid region denoted by  $\mathcal{R}(\mathbf{v})$ , with each point of the region moving with the local fluid velocity  $\mathbf{v}(\mathbf{x}, t)$ . Let an arbitrary fluid parcel within this region be marked with the material label  $\mathbf{a}$  so that its position vector is  $\mathbf{X}(\mathbf{a}, t)$  and its velocity is

$$\mathbf{V}(\mathbf{a}, t) = \frac{\partial \mathbf{X}(\mathbf{a}, t)}{\partial t}, \quad (32.48)$$

---

<sup>1</sup>Inflection points are where the curvature changes sign.

where the time derivative is computed holding the material label fixed. Since the parcel is within a finite material region, we find it useful to decompose the motion of the parcel into the motion of the region's center of mass plus the motion of the parcel relative to the center of mass

$$\mathbf{V}(\mathbf{a}, t) = \frac{\partial \mathbf{X}(\mathbf{a}, t)}{\partial t} \quad (32.49a)$$

$$= \frac{\partial (\bar{\mathbf{X}} + \mathbf{X}')}{\partial t} \quad (32.49b)$$

$$= \bar{\mathbf{V}}(t) + \mathbf{V}'(\mathbf{a}, t). \quad (32.49c)$$

In this equation, we introduced the velocity  $\mathbf{V}'$  defined relative to the center of mass of the region. Furthermore, the center of mass velocity is given by

$$\bar{\mathbf{V}} = \frac{d\bar{\mathbf{X}}}{dt} \quad (32.50a)$$

$$= \frac{d}{dt} \left[ \frac{\int_{\mathcal{R}(\mathbf{v})} \mathbf{x} \rho dV}{\int_{\mathcal{R}(\mathbf{v})} \rho dV} \right] \quad (32.50b)$$

$$= \frac{1}{M} \int_{\mathcal{R}(\mathbf{v})} \frac{D\mathbf{x}}{Dt} \rho dV \quad (32.50c)$$

$$= \frac{1}{M} \int_{\mathcal{R}(\mathbf{v})} \mathbf{v} \rho dV. \quad (32.50d)$$

The identity (32.50c) follows since the material region maintains a constant mass,

$$M = \int_{\mathcal{R}(\mathbf{v})} \rho dV \implies \frac{dM}{dt} = 0, \quad (32.51)$$

allowing the denominator to come outside the derivative. Additionally, each of the fluid parcels in the region maintains constant mass. As per Reynold's transport theorem (Section 14.3.4), the time derivative moves across the integral to act materially on the position vector. The final equality, (32.50d), follows since the material time derivative of a parcel trajectory when evaluated at a point,  $\mathbf{x}$ , equals to the velocity field at that point

$$\mathbf{v}(\mathbf{x}, t) = \frac{D\mathbf{x}}{Dt}. \quad (32.52)$$

It follows that the linear momentum for the material fluid region is given by

$$\mathbf{P} = \int_{\mathcal{R}(\mathbf{v})} \mathbf{v} \rho dV = M \bar{\mathbf{V}}. \quad (32.53)$$

We conclude that the total linear momentum of an extended body equals to that of a point particle of mass  $M = \int_{\mathcal{R}(\mathbf{v})} \rho dV$  moving with the center of mass velocity,  $\bar{\mathbf{V}}$ .

### 32.7.2 Angular momentum

We here consider angular momentum for a material fluid region, which is determined by the integral over that region of the angular momentum for each fluid parcel

$$\mathbf{L} = \int_{\mathcal{R}(\mathbf{v})} (\mathbf{x} \times \mathbf{v}) \rho dV. \quad (32.54)$$

Our goal is to expose how physically distinct aspects of the fluid motion contribute to the angular momentum. To proceed, decompose the position vector of a point within the region into the center of mass position plus a deviation,  $\mathbf{x} = \bar{\mathbf{x}} + \mathbf{x}'$ , where  $\bar{\mathbf{x}} = \bar{X}$  is the instantaneous position of the moving center of mass. The angular momentum thus takes the form

$$\mathbf{L} = \int_{\mathcal{R}(\mathbf{v})} (\mathbf{x} \times \mathbf{v}) \rho dV \quad (32.55a)$$

$$= \int_{\mathcal{R}(\mathbf{v})} [(\bar{\mathbf{x}} + \mathbf{x}') \times \mathbf{v}] \rho dV \quad (32.55b)$$

$$= \bar{\mathbf{X}} \times \left[ \int_{\mathcal{R}(\mathbf{v})} \mathbf{v} \rho dV \right] + \int_{\mathcal{R}(\mathbf{v})} (\mathbf{x}' \times \mathbf{v}) \rho dV \quad (32.55c)$$

$$= (\bar{\mathbf{X}} \times \mathbf{P}) + \int_{\mathcal{R}(\mathbf{v})} (\mathbf{x}' \times \mathbf{v}) \rho dV. \quad (32.55d)$$

The final equality introduced the linear momentum, (32.53), for the fluid region. The first term in equation (32.55d) is the angular momentum of the region with respect to the position of the center of mass. The second term is associated with deviations of parcel positions relative to the center of mass.

We now focus on how the deviation term,  $\int_{\mathcal{R}(\mathbf{v})} (\mathbf{x}' \times \mathbf{v}) \rho dV$ , contributes to the angular momentum (32.54). As we will see, this analysis exposes how angular momentum of the extended material fluid region is affected by vorticity and rate of strain in the fluid flow. To facilitate some of the manipulations, we make use of basic Cartesian tensor analysis from Chapter 1, including the summation convention whereby repeated indices are summed over their range.

### 32.7.3 Taylor expanding the velocity

We perform a Taylor expansion of the velocity  $\mathbf{v}(\mathbf{x})$  around the instantaneous center of mass position,  $\bar{\mathbf{x}} = \bar{X}$ , and truncate the expansion to the leading order term<sup>2</sup>

$$\mathbf{v}(\mathbf{x}) = \mathbf{v}(\bar{\mathbf{x}} + \mathbf{x}') \approx \mathbf{v}(\bar{\mathbf{x}}) + (\mathbf{x}' \cdot \nabla) \mathbf{v}|_{\mathbf{x}=\bar{\mathbf{x}}}. \quad (32.56)$$

We are thus left with

$$\mathbf{L} = (\bar{\mathbf{X}} \times \mathbf{P}) + \int_{\mathcal{R}(\mathbf{v})} (\mathbf{x}' \times \mathbf{v}) \rho dV \quad (32.57a)$$

$$= (\bar{\mathbf{X}} \times \mathbf{P}) + \int_{\mathcal{R}(\mathbf{v})} [\mathbf{x}' \times \mathbf{v}(\bar{\mathbf{x}})] \rho dV + \int_{\mathcal{R}(\mathbf{v})} [\mathbf{x}' \times (\mathbf{x}' \cdot \nabla) \mathbf{v}(\bar{\mathbf{x}})] \rho dV. \quad (32.57b)$$

The velocity  $\mathbf{v}(\bar{\mathbf{x}})$  can be removed from the integration since it is evaluated at the center of mass point. Hence, the second term in equation (32.57b) vanishes

$$\int_{\mathcal{R}(\mathbf{v})} [\mathbf{x}' \times \mathbf{v}(\bar{\mathbf{x}})] \rho dV = \left[ \int_{\mathcal{R}(\mathbf{v})} \mathbf{x}' \rho dV \right] \times \mathbf{v}(\bar{\mathbf{x}}) = 0, \quad (32.58)$$

---

<sup>2</sup>The velocity field evaluated at the center of mass position,  $\mathbf{v}(\bar{\mathbf{x}})$ , is not equal to the center of mass velocity:  $\mathbf{v}(\bar{\mathbf{x}}) \neq \bar{\mathbf{v}}$ .

where  $\int_{\mathcal{R}(\mathbf{v})} \mathbf{x}' \rho dV = 0$  by definition of the center of mass. The angular momentum is thus given by the two terms

$$\mathbf{L} = (\bar{\mathbf{X}} \times \mathbf{P}) + \int_{\mathcal{R}(\mathbf{v})} [\mathbf{x}' \times (\mathbf{x}' \cdot \nabla) \mathbf{v}(\bar{\mathbf{x}})] \rho dV. \quad (32.59)$$

The  $m'th$  component of the second term can be written

$$\int_{\mathcal{R}(\mathbf{v})} [\mathbf{x}' \times (\mathbf{x}' \cdot \nabla) \mathbf{v}(\bar{\mathbf{x}})]_m \rho dV = \epsilon_{mnp} \int_{\mathcal{R}(\mathbf{v})} x'_n [(\mathbf{x}' \cdot \nabla) \mathbf{v}(\bar{\mathbf{x}})]_p \rho dV \quad (32.60a)$$

$$= \epsilon_{mnp} \int_{\mathcal{R}(\mathbf{v})} x'_n x'_q \partial_q v_p(\bar{\mathbf{x}}) \rho dV \quad (32.60b)$$

$$= \epsilon_{mnp} \left[ \int_{\mathcal{R}(\mathbf{v})} x'_n x'_q \rho dV \right] \partial_q v_p(\bar{\mathbf{x}}). \quad (32.60c)$$

We removed the velocity derivatives

$$\partial_q v_p(\bar{\mathbf{x}}) = \left[ \frac{\partial v_p}{\partial x_q} \right]_{\mathbf{x}=\bar{\mathbf{x}}} \quad (32.61)$$

from the integral, since they are evaluated at the center of mass point and so do not participate in the integration.

### 32.7.4 Angular momentum, rate of strain, and vorticity

Following from the discussion in Section 13.3.5, we know that the velocity derivatives  $\partial_q v_p$  appearing in equation (32.60c) form the components to a second order tensor known as the *velocity gradient tensor*, which can be decomposed into the rate of strain tensor,  $\mathbb{S}$ , and the rotation tensor,  $\mathbb{R}$ . Introducing these two tensors brings the angular momentum for a continuum fluid region into the form

$$L_m = (\bar{\mathbf{X}} \times \mathbf{P})_m + \epsilon_{mnp} \left[ \int_{\mathcal{R}(\mathbf{v})} x'_n x'_q \rho dV \right] \mathbb{S}_{qp} + \epsilon_{mnp} \left[ \int_{\mathcal{R}(\mathbf{v})} x'_n x'_q \rho dV \right] \mathbb{R}_{qp} \quad (32.62a)$$

$$= (\bar{\mathbf{X}} \times \mathbf{P})_m + \epsilon_{mnp} \left[ \int_{\mathcal{R}(\mathbf{v})} x'_n x'_q \rho dV \right] \mathbb{S}_{qp} + \frac{1}{2} \epsilon_{mnp} \epsilon_{sqp} \left[ \int_{\mathcal{R}(\mathbf{v})} x'_n x'_q \rho dV \right] \omega_s \quad (32.62b)$$

$$= \underbrace{(\bar{\mathbf{X}} \times \mathbf{P})_m}_{\text{center of mass}} + \underbrace{\epsilon_{mnp} \left[ \int_{\mathcal{R}(\mathbf{v})} x'_n x'_q \rho dV \right]}_{\text{strain contribution}} \mathbb{S}_{qp} + \underbrace{\frac{1}{2} \left[ \int_{\mathcal{R}(\mathbf{v})} (\mathbf{x}' \cdot \mathbf{x}' \delta_{ms} - x'_m x'_s) \rho dV \right]}_{\text{vorticity contribution}} \omega_s. \quad (32.62c)$$

Since each point in the fluid continuum can be considered the center of mass for an arbitrary material region, the decomposition (32.62c) holds in general.

- **CENTER OF MASS ANGULAR MOMENTUM:** The first term on the right hand side of equation (32.62c) arises from the angular momentum of the material region as measured with respect to the center of mass position. It has the form of that for a point particle (see equation (9.14a)). This term vanishes if the origin of the coordinate system is taken at the center of mass.
- **STRAINS:** The second contribution is proportional to fluid deformations studied in Section 13.3.5. At each point of the fluid, deformations are measured by the rate of strain tensor,

$\mathbb{S}_{qp}$ . A rigid body moves by uniform translations and/or solid-body rotations, with the rate of strain tensor vanishing for rigid body motions (see Section 32.5). The contribution from strains is weighted by an integral of deviations of parcel position from the center of mass position. A closed form expression for this integral is available only for special shapes.

- **VORTICITY:** The third contribution to angular momentum (32.62c) contains the vorticity as weighted by the moment of inertia tensor

$$I_{ms} \equiv \int_{\mathcal{R}(\mathbf{v})} (\mathbf{x}' \cdot \mathbf{x}' \delta_{ms} - x'_m x'_s) \rho dV. \quad (32.63)$$

Since the material region is evolving and is not rigid, the moment of inertia tensor is time dependent. Even so, the contribution

$$L_m^{\text{vorticity}} \equiv \frac{1}{2} I_{ms} \omega_s \quad (32.64)$$

has the same form as angular momentum for a rigid body, with one-half the vorticity playing the role of angular velocity (see equation (9.14c) for the point particle expression). Fluid vorticity hence contributes to angular momentum for a material region via its product with the moment of inertia tensor.

### 32.7.5 Comments and further reading

Angular momentum is computed relative to a chosen origin, whereas vorticity is an intrinsic property measuring the spin of the fluid at a point. So although they both offer measures of the rotational properties of fluid motion, they are distinct when the fluid experiences a nonzero rate of strain. It is only for the special case of a solid-body motion that the rate of strain vanishes, in which case the angular momentum of a fluid region is directly related to vorticity.

Further discussion of the material in this section can be found in [Chatwin \(1973\)](#), Section 2.3.1 of [Davidson \(2015\)](#), and the online notes “The Vorticity Equation and Conservation of Angular Momentum” from A.J. DeCaria.



## 32.8 Exercises

### EXERCISE 32.1: VORTICITY FOR SOLID-BODY ROTATION

Show that a fluid in solid-body rotation with angular velocity

$$\mathbf{v}_{\text{solid-body}} = \boldsymbol{\Omega} \times \mathbf{x}, \quad (32.65)$$

has a vorticity given by

$$\nabla \times \mathbf{v}_{\text{solid-body}} = 2 \boldsymbol{\Omega}. \quad (32.66)$$

### EXERCISE 32.2: PLANETARY ROTATION IS NON-DIVERGENT

Show that a fluid in solid-body rotation with angular velocity

$$\mathbf{v}_{\text{solid-body}} = \boldsymbol{\Omega} \times \mathbf{x}, \quad (32.67)$$

has zero divergence

$$\nabla \cdot \mathbf{v}_{\text{solid-body}} = 0. \quad (32.68)$$

Consequently, rotation of the planet imparts zero divergence to fluid motion. We make use of this result in part to justify our study of non-rotating fluid kinematics in Part III of this book.

**EXERCISE 32.3: VELOCITY POTENTIAL FOR THE FREE VORTEX**

What is the velocity potential (32.14) for the free vortex whose velocity field is given by (32.21)?

Hint: The problem is two-dimensional and rotationally symmetric, so it is convenient to make use of polar coordinates  $x = r \cos \vartheta$  and  $y = r \sin \vartheta$  as in Appendix 8.3.

**EXERCISE 32.4: STRAIN TENSOR FOR THE FREE VORTEX**

Determine all components to the strain tensor

$$S_{pq} = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} = \begin{bmatrix} \frac{\partial u}{\partial x} & \frac{1}{2} \left[ \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right] \\ \frac{1}{2} \left[ \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right] & \frac{\partial v}{\partial y} \end{bmatrix} \quad (32.69)$$

for the free vortex as specified by the velocity field (32.21). Present the answer in the form of a  $2 \times 2$  matrix.

**EXERCISE 32.5: VANISHING VISCOSIVE FRICTION FOR SOLID-BODY MOTION**

As discussed in Section 18.7.6, viscous effects from molecular viscosity in an incompressible fluid appear in the momentum equation as a Laplacian weighted by a constant molecular viscosity

$$\text{viscous force per mass} = \nu \nabla^2 \mathbf{v}, \quad (32.70)$$

where  $\nu > 0$  is the molecular kinematic viscosity, which is a constant that is a property of the fluid. Show that the viscous operator vanishes for a fluid in solid-body rotation. That is, solid-body motion engenders no frictional dissipation. This result reflects the lack of frictional interaction in a fluid absent shears and strains.

**EXERCISE 32.6: VORTICITY FOR A C-GRID NUMERICAL MODEL**

Vorticity is commonly diagnosed in numerical model simulations. In this exercise we consider how one might determine a discrete equation for the vertical vorticity when the horizontal velocity is arranged according to the Arakawa C-grid ([Arakawa and Lamb, 1977](#)) commonly used in ocean models, and as depicted in Figure 32.9. Derive an expression for the area averaged vorticity over the shaded grid cell region centered at the vorticity point,  $q_{i,j}$ . Make use of Stokes' theorem with the surrounding C-grid velocity components and the corresponding grid distances.



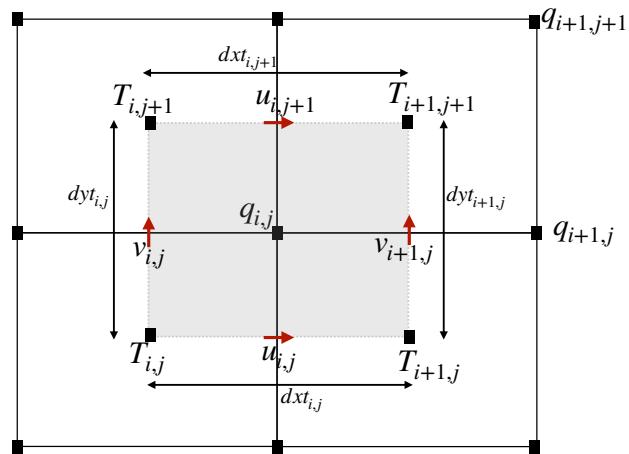


FIGURE 32.9: Layout for velocity on a discrete Arakawa C-grid for use in Exercise 32.6. The central T-point is labeled  $T_{i,j}$  and its corresponding vorticity point,  $q_{i,j}$ , is located to its northeast. This exercise aims to determine the area averaged vorticity for the shaded region. The zonal velocity,  $u_{i,j}$ , is arranged on the east face of the T-cell, whereas the meridional velocity,  $v_{i,j}$ , is on the north face. The zonal and meridional grid distances are indicated, thus measuring distances between adjacent tracer points and so measuring the sides of the shaded region.



# Chapter 33

## Non-divergent barotropic flow

A single layer of homogeneous shallow water fluid is among the simplest models available for the study of fluid motion. In the language of vorticity as described in Chapter 35, a shallow water layer is a barotropic fluid since it has zero baroclinicity (Section 35.5). Consequently, the shallow water model is often referred to as a divergent barotropic model, with divergence referring to the nonzero divergence in the horizontal velocity.

For many purposes, the horizontal flow divergence supported by a shallow water layer can be a distraction. That is, for many geophysical studies one is interested in the low frequency vortical (Rossby wave) motions rather than the divergent and higher frequency gravity wave motions (Section 31.8). The *non-divergent barotropic model* focuses on vortical motion since its horizontal velocity has zero divergence. We study the non-divergent barotropic model with a flat free surface whereby flow is generated by an externally imposed *lid pressure* required to maintain a flat surface. We do not need to explicitly compute the lid pressure since the relative vorticity is the primary dynamical field, whereby knowledge of the vorticity is sufficient to fully determine the streamfunction and the velocity. Furthermore, the absolute vorticity is materially invariant in the absence of irreversible processes such as friction. Hence, meridional motion of the fluid parcel reveals an exact exchange of vorticity between the fluid and the planet. This exchange is manifest in the physical mechanism for Rossby waves, and it offers a key reason to study this model in the vorticity part of the book.

### CHAPTER GUIDE

We develop some of the analytic and semi-analytic properties available for the non-divergent barotropic model, thus providing an entry-point into the vast literature making use of this model. Besides offering a frequently used theoretical model for large-scale dynamics, the non-divergent barotropic model is useful for studies of coherent vortex structures, with Chapter 3 of [McWilliams \(2006\)](#) exploring analytical vortex solutions. The model also served as the basis for the pioneering numerical weather prediction model described by [Charney et al. \(1950\)](#). Since all fields in this chapter are a spatial function only of the horizontal position,  $\nabla\psi = \nabla_z\psi$ .

33.1 Basic equations and their properties . . . . .	800
33.1.1 Velocity equation . . . . .	800
33.1.2 Kinematics of rigid fluid columns . . . . .	801
33.1.3 Vertical velocity . . . . .	802

33.1.4	Velocity self-advection . . . . .	803
33.1.5	Further reading . . . . .	803
33.2	Vorticity . . . . .	<b>803</b>
33.2.1	Vorticity equation . . . . .	804
33.2.2	Absolute vorticity is the potential vorticity . . . . .	804
33.2.3	Jacobian form of vorticity advection . . . . .	805
33.2.4	Taylor-Bretherton identities . . . . .	805
33.2.5	Poisson equation for the streamfunction . . . . .	806
33.2.6	Zonal flow as an exact geostrophic solution . . . . .	807
33.3	Connection to equivalent barotropic flow . . . . .	<b>807</b>
33.3.1	Vorticity equation for the depth averaged flow . . . . .	807
33.3.2	Comments . . . . .	808
33.4	The externally applied lid pressure . . . . .	<b>808</b>
33.4.1	Poisson equation for pressure . . . . .	809
33.4.2	Gradient wind balance . . . . .	809
33.4.3	Pressure source from self-advection . . . . .	810
33.4.4	Pressure source from solid-body flow . . . . .	810
33.4.5	Pressure source from irrotational flow . . . . .	812
33.4.6	Pressure source from Coriolis acceleration . . . . .	812
33.4.7	Pressure source from friction . . . . .	813
33.4.8	Comments and further study . . . . .	813
33.5	Constraints from absolute vorticity invariance . . . . .	<b>814</b>
33.5.1	Relative vorticity from curvature and planetary beta . . . . .	814
33.5.2	Relative vorticity from curvature and normal shears . . . . .	815
33.5.3	Curvature, shear, and planetary contributions . . . . .	816
33.6	Barotropic Rossby waves . . . . .	<b>817</b>
33.6.1	Dispersion relation . . . . .	817
33.6.2	Phase speed . . . . .	818
33.6.3	Group velocity . . . . .	819
33.6.4	Importance of $\beta$ for Rossby waves . . . . .	819
33.7	Exercises . . . . .	<b>820</b>

## 33.1 Basic equations and their properties

The non-divergent barotropic model arises from the following assumptions.

- The flow occurs in a single homogeneous fluid layer, as for the shallow water model from Chapter 30.
- The horizontal velocity is non-divergent:  $\nabla \cdot \mathbf{u} = \partial_x u + \partial_y v = 0$ , which means that the thickness of the layer is fixed.

The second property provides some rather strict constraints on the flow relative to flow in the horizontally divergent shallow water layer. In this section we exhibit the governing equations and derive some of their properties.

### 33.1.1 Velocity equation

The velocity equation for the non-divergent barotropic model follows in a manner akin to the shallow water model from Chapter 30. Namely, the fluid is a homogeneous (uniform and constant density) layer so that the horizontal velocity satisfies

$$\frac{D\mathbf{u}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla \varphi \quad \text{and} \quad \nabla \cdot \mathbf{u} = 0, \quad (33.1)$$

where the pressure is normalized according to

$$\varphi = p/\rho \quad (33.2)$$

with  $\rho$  the constant layer density, and where material evolution occurs with the two-dimensional non-divergent flow

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla. \quad (33.3)$$

All fields are depth independent and there is no vertical motion, so that the flow occurs in rigid fluid columns. Furthermore, the horizontal non-divergent flow can be described by a streamfunction

$$\mathbf{u} = \hat{\mathbf{z}} \times \nabla \psi \implies u = -\frac{\partial \psi}{\partial y} \quad \text{and} \quad v = \frac{\partial \psi}{\partial x}. \quad (33.4)$$

### 33.1.2 Kinematics of rigid fluid columns

Recall the thickness equation (30.17) for a shallow water layer

$$\frac{Dh}{Dt} = -h \nabla \cdot \mathbf{u}, \quad (33.5)$$

where  $h = \eta - \eta_b$  is the column thickness,  $z = \eta(x, y, t)$  is the upper layer interface (the free surface), and  $z = \eta_b(x, y)$  is the lower interface (the bottom topography) (see Figure 30.1). With zero divergence in the horizontal velocity, the thickness of a fluid column is constant when moving with the horizontal flow

$$(\partial_t + \mathbf{u} \cdot \nabla) h = \partial_t(\eta - \eta_b) + \mathbf{u} \cdot \nabla(\eta - \eta_b) = 0. \quad (33.6)$$

We choose to satisfy this equation by setting the upper surface to be static and flat

$$\eta = 0, \quad (33.7)$$

and furthermore by constraining the horizontal flow to follow the bottom topography

$$\mathbf{u} \cdot \nabla \eta_b = (\nabla \psi \times \nabla \eta_b) \cdot \hat{\mathbf{z}} = 0. \quad (33.8)$$

In brief, we are concerned with horizontally non-divergent flow within a homogeneous fluid layer for which a fluid column does not expand or contract and so it only moves along lines of constant topography.

For the case of a flat bottom domain that is bounded on its side by a vertical wall, then the no-flow boundary condition takes the form

$$\mathbf{u} \cdot \hat{\mathbf{n}} = (\hat{\mathbf{z}} \times \nabla \psi) \cdot \hat{\mathbf{n}} = \hat{\mathbf{t}} \cdot \nabla \psi = 0, \quad (33.9)$$

where  $\hat{\mathbf{n}}$  is the horizontal outward unit vector at the boundary, and  $\hat{\mathbf{t}} = \hat{\mathbf{n}} \times \hat{\mathbf{z}}$  is the unit tangent vector along the boundary. The kinematic condition (33.9) means that the streamfunction is a constant along the solid vertical sidewall boundary. We encountered this boundary condition in Section 16.4.2 when studying two-dimensional non-divergent flow. A zonally reentrant channel is an example considered in Section 33.6, whereby  $\psi$  is a constant along the northern and southern walls.

### 33.1.3 Vertical velocity

#### *Vanishing vertical velocity*

Without horizontal divergence and with a flat free surface, there is identically zero vertical motion within the layer

$$w = 0. \quad (33.10)$$

Another manner to deduce this property by noting that the surface kinematic boundary condition for a static and flat free surface leads to

$$w(\eta) = \frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla \eta = 0 + 0, \quad (33.11)$$

so that the vertical velocity at  $z = \eta$  vanishes. With  $w(\eta) = 0$ , and with  $\nabla \cdot \mathbf{u} = 0$  for the horizontal velocity, then  $w = 0$  throughout the layer. Correspondingly, this constraint means that the no-normal flow bottom kinematic condition (Section 14.4.1) renders a horizontal velocity that is aligned with the topography,  $\mathbf{u} \cdot \nabla \eta_b = 0$ , which is a property we already encountered in Section 33.1.2. Since the vertical velocity is zero, the gravitational potential energy is a uniform constant, so that the mechanical energy arises just from kinetic energy.

#### *Non-vanishing vertical velocity*

In Section 33.1.2 we chose to satisfy the thickness equation kinematics by setting  $\partial_t \eta = \nabla \eta = 0$ , in which case the vertical velocity vanishes so long as the horizontal flow follows the bottom topography. However, a static and flat upper boundary is a sufficient condition but it is not necessary.

Another approach to satisfying the thickness equation (33.6) is to consider a static yet non-flat free surface with horizontal flow constrained so that

$$\mathbf{u} \cdot \nabla(\eta - \eta_b) = 0. \quad (33.12)$$

The surface and bottom kinematic boundary conditions then result in a vertical velocity at the surface and bottom

$$w(\eta) = -\mathbf{u} \cdot \nabla \eta \quad \text{and} \quad w(\eta_b) = -\mathbf{u} \cdot \nabla \eta_b. \quad (33.13)$$

Now these two boundary velocities are equal, thus satisfying  $\partial_z w = 0$ . If the bottom topography is flat,  $\nabla \eta_b = 0$ , then  $w(\eta_b) = w(\eta) = 0$ , in which case  $\nabla \eta = 0$ , so that the upper surface is flat. If the bottom is not flat, then the kinematic constraints lead to

$$\nabla \eta = \nabla \eta_b, \quad (33.14)$$

so that the upper ocean surface slope equals to the slope of the bottom topography. In the ocean, it is generally the case that the upper ocean surface undulations are far less than the bottom topography. Hence,  $\nabla \eta = \nabla \eta_b$  is not generally a realistic behavior, though one may study this case particularly with weakly sloping bottom topography.

For the remainder of this chapter we follow the conventional approach whereby  $w = 0$ . Hence, the upper boundary is static and flat. In the presence of a non-flat bottom, then the horizontal flow follows lines of constant bottom topography,  $\mathbf{u} \cdot \nabla \eta_b = 0$ .

### 33.1.4 Velocity self-advection

The velocity self-advection appearing in the velocity equation (33.1) can be written as the divergence of a  $2 \times 2$  symmetric tensor

$$-(\mathbf{u} \cdot \nabla) \mathbf{u} = \nabla \cdot \mathbb{E} \iff -u_m \partial_m u_n = \partial_m \mathbb{E}_{mn}, \quad (33.15)$$

where

$$\mathbb{E} = \begin{bmatrix} -u^2 & -uv \\ -uv & -v^2 \end{bmatrix}, \quad (33.16)$$

thus bringing the momentum equation (33.1) to the Eulerian form

$$\frac{\partial \mathbf{u}}{\partial t} + f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla \varphi + \nabla \cdot \mathbb{E}. \quad (33.17)$$

The tensor,

$$\rho \mathbb{E} = -\rho \mathbf{u} \otimes \mathbf{u} \quad (33.18)$$

is the *kinetic stress tensor*, whose three-dimensional form was introduced in Section 18.5.

In anticipation of our study of vorticity in Section 33.2, we find it useful to decompose the kinetic tensor into its horizontally isotropic and horizontally anisotropic components<sup>1</sup>

$$\mathbb{E} = \begin{bmatrix} -u^2 & -uv \\ -uv & -v^2 \end{bmatrix} = -\mathcal{K} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} -(u^2 - v^2)/2 & -uv \\ -uv & (u^2 - v^2)/2 \end{bmatrix} \equiv -\mathcal{K} \mathbb{I} + \mathbb{F}, \quad (33.19)$$

where we introduced the kinetic energy per mass

$$\mathcal{K} = \mathbf{u} \cdot \mathbf{u}/2 = (u^2 + v^2)/2, \quad (33.20)$$

and the trace-free anisotropic portion of the kinetic stress tensor

$$\mathbb{F} = \mathcal{K} \mathbb{I} + \mathbb{E} = \begin{bmatrix} -(u^2 - v^2)/2 & -uv \\ -uv & (u^2 - v^2)/2 \end{bmatrix} \iff \mathbb{F}_{mn} = \mathcal{K} \delta_{mn} - u_m u_n. \quad (33.21)$$

Making use of the decomposition (33.19) brings the velocity equation (33.22) to the form

$$\frac{\partial \mathbf{u}}{\partial t} + f \hat{\mathbf{z}} \times \mathbf{u} = \nabla \cdot [\mathbb{F} - \mathbb{I}(\mathcal{K} + \varphi)]. \quad (33.22)$$

### 33.1.5 Further reading

As discussed by [Hoskins et al. \(1983\)](#), [Waterman and Hoskins \(2013\)](#) and [Waterman and Lilly \(2015\)](#), the decomposition (33.19) leads to a very insightful kinematic geometric interpretation of eddying flow features.

## 33.2 Vorticity

For the two-dimensional non-divergent flow, the vertical component of the relative vorticity is given by the Laplacian of the streamfunction

$$\zeta = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u}) = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = \nabla^2 \psi. \quad (33.23)$$

<sup>1</sup>Recall our discussion of isotropy in Section 1.8.

We here study the motion of this fluid on a tangent plane in which the Coriolis parameter is given by the  $\beta$ -plane expression

$$f = f_0 + \beta(y - y_0). \quad (33.24)$$

### 33.2.1 Vorticity equation

To form the dynamical equation for the vorticity, take the zonal derivative of the meridional momentum equation (see equation (33.1)) and meridional derivative of the zonal momentum equation

$$\frac{\partial}{\partial t} \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) + \frac{\partial}{\partial x} [\nabla \cdot (\mathbf{u} v)] - \frac{\partial}{\partial y} [\nabla \cdot (\mathbf{u} u)] + f \nabla \cdot \mathbf{u} + \beta v = 0. \quad (33.25)$$

Notice how the pressure gradient dropped out since there is zero baroclinicity for a barotropic flow (see Section 35.5 for a discussion of baroclinicity). We now make use of the identity

$$\frac{\partial}{\partial x} [\nabla \cdot (\mathbf{u} v)] - \frac{\partial}{\partial y} [\nabla \cdot (\mathbf{u} u)] = \frac{\partial \mathbf{u}}{\partial x} \cdot \nabla v - \frac{\partial \mathbf{u}}{\partial y} \cdot \nabla u + \mathbf{u} \cdot \nabla \zeta = \mathbf{u} \cdot \nabla \zeta, \quad (33.26)$$

where we used the non-divergence condition,  $\partial_x u + \partial_y v = 0$ , to write

$$\frac{\partial \mathbf{u}}{\partial x} \cdot \nabla v - \frac{\partial \mathbf{u}}{\partial y} \cdot \nabla u = \frac{\partial u}{\partial x} \frac{\partial v}{\partial x} + \frac{\partial v}{\partial x} \frac{\partial v}{\partial y} - \frac{\partial u}{\partial y} \frac{\partial u}{\partial x} - \frac{\partial v}{\partial y} \frac{\partial u}{\partial y} \quad (33.27a)$$

$$= -\frac{\partial v}{\partial y} \frac{\partial v}{\partial x} + \frac{\partial v}{\partial x} \frac{\partial v}{\partial y} + \frac{\partial u}{\partial y} \frac{\partial v}{\partial y} - \frac{\partial v}{\partial y} \frac{\partial u}{\partial y} \quad (33.27b)$$

$$= 0. \quad (33.27c)$$

We are thus led to the vorticity equation

$$\frac{\partial \zeta}{\partial t} + \nabla \cdot (\mathbf{u} \zeta) = -\beta v \quad \text{and} \quad \frac{D\zeta}{Dt} = -\beta v. \quad (33.28)$$

Hence, the material evolution of relative vorticity in the non-divergent barotropic fluid is only affected by meridional advection of planetary vorticity. Since  $\beta > 0$  over the globe, northward flow ( $v > 0$ ) produces a negative source (clockwise tendency) for relative vorticity following a fluid parcel. This source term is the *beta effect* studied in Section 35.7.

### 33.2.2 Absolute vorticity is the potential vorticity

Since  $f$  is time independent, we can write the vorticity equation (33.28) in the form

$$\frac{\partial \zeta_a}{\partial t} + \mathbf{u} \cdot \nabla \zeta_a = 0, \quad (33.29)$$

where

$$\zeta_a = \zeta + f \quad (33.30)$$

is the vertical component of the absolute vorticity. Hence, there is no stretching or tilting of fluid columns in the non-divergent barotropic fluid. Again, we conceive of the flow as that of rigid fluid columns of constant thickness. Furthermore, the material conservation of  $\zeta_a$  allows us to identify the potential vorticity with the absolute vorticity for the non-divergent barotropic fluid

$$q = \zeta_a = \zeta + f \implies \frac{\partial q}{\partial t} + \mathbf{u} \cdot \nabla q = 0 \implies \frac{Dq}{Dt} = 0. \quad (33.31)$$

To maintain a materially constant absolute vorticity requires the relative vorticity to change oppositely to that of the planetary vorticity. For example, in the northern hemisphere, the relative vorticity must decrease ( $\zeta \downarrow$ ) for fluid particles moving northward. This change in the relative vorticity is needed to counteract the increasing planetary vorticity ( $f \uparrow$ ) when moving northward. This result accords with the  $-\beta v$  source found in the relative vorticity equation (33.28). Furthermore, it is a reflection of the beta effect studied in Section 35.7.2.

The presence of topography adds further richness to the flow. According to the kinematic boundary condition (33.8), horizontal flow is aligned with isobaths (lines of constant bathymetry or topography). Flow moving along constant isobaths generally crosses latitude lines, and in so doing the relative vorticity must change precisely to maintain  $f + \zeta$  materially constant.

### 33.2.3 Jacobian form of vorticity advection

In some contexts it is convenient to write the advection operator acting on relative vorticity as

$$\mathbf{u} \cdot \nabla \zeta = u \partial_x \zeta + v \partial_y \zeta \quad (33.32a)$$

$$= -\partial_y \psi \partial_x \zeta + \partial_x \psi \partial_y \zeta \quad (33.32b)$$

$$= \hat{\mathbf{z}} \cdot (\nabla \psi \times \nabla \zeta) \quad (33.32c)$$

$$\equiv J(\psi, \zeta), \quad (33.32d)$$

where  $J$  is the Jacobian operator

$$J(A, B) = \hat{\mathbf{z}} \cdot (\nabla A \times \nabla B) = \frac{\partial A}{\partial x} \frac{\partial B}{\partial y} - \frac{\partial A}{\partial y} \frac{\partial B}{\partial x}. \quad (33.33)$$

We can also make use of the Jacobian for the advection of absolute vorticity

$$\mathbf{u} \cdot \nabla \zeta_a = \hat{\mathbf{z}} \cdot (\nabla \psi \times \nabla \zeta_a) \equiv J(\psi, \zeta + f). \quad (33.34)$$

The Jacobian operator corresponds to the Poisson bracket used in Hamiltonian mechanics.

### 33.2.4 Taylor-Bretherton identities

An equivalent means to write the vorticity equation is to start from the velocity equation in the form (33.22). Taking the curl and projecting onto the vertical direction then leads to

$$\frac{\partial \zeta}{\partial t} = -\beta v + \hat{\mathbf{z}} \cdot [\nabla \times \nabla \cdot \mathbb{F}]. \quad (33.35)$$

The nonlinear forcing from the anisotropic kinetic stress can be written

$$\hat{\mathbf{z}} \cdot [\nabla \times \nabla \cdot \mathbb{F}] = \hat{\mathbf{z}}_n \epsilon_{npq} \partial_p (\partial_m \mathbb{F}_{mq}) \quad (33.36a)$$

$$= \partial_m \partial_p (\epsilon_{npq} \hat{\mathbf{z}}_n \mathbb{F}_{mq}) \quad (33.36b)$$

$$= -\partial_m \partial_p (\epsilon_{pnq} \hat{\mathbf{z}}_n \mathbb{F}_{qm}) \quad (33.36c)$$

$$= -\partial_m \partial_p (\hat{\mathbf{z}} \times \mathbb{F})_{pm} \quad (33.36d)$$

$$= -\nabla \cdot [\nabla \cdot (\hat{\mathbf{z}} \times \mathbb{F})], \quad (33.36e)$$

where we used symmetry of the anisotropic kinetic tensor,  $\mathbb{F}_{mq} = \mathbb{F}_{qm}$ .

*Taylor-Bretherton identity for relative vorticity*

Comparing to the vorticity equation in the form (33.28) reveals the identity

$$\nabla \cdot (\mathbf{u} \zeta) = \nabla \cdot [\nabla \cdot (\hat{\mathbf{z}} \times \mathbb{F})] \implies \mathbf{u} \zeta = \nabla \cdot (\hat{\mathbf{z}} \times \mathbb{F}). \quad (33.37)$$

This equation says that the advective vorticity flux equals to the divergence of the counter-clockwise rotated anisotropic kinetic stress tensor. Equation (33.37) is a special form of the *Taylor-Bretherton identity* that provides a connection between the vorticity flux and the momentum flux. We encounter the shallow water form of this identity Chapter 45 when studying the decomposition of eddy and mean flows.

*Verifying the Taylor-Bretherton identity*

The divergence expression on the left hand side of equation (33.37) can be satisfied by  $\hat{\mathbf{z}} \times \nabla \Upsilon + \nabla \cdot (\hat{\mathbf{z}} \times \mathbb{F})$ , with  $\Upsilon$  an arbitrary gauge function. However,  $\Upsilon = 0$  is zero for the anisotropic kinetic tensor (33.21), as seen by

$$[\nabla \cdot (\hat{\mathbf{z}} \times \mathbb{F})]_1 = \partial_m (\epsilon_{mnp} \hat{\mathbf{z}}_n \mathbb{F}_{p1}) \quad (33.38a)$$

$$= \epsilon_{m3p} \partial_m \mathbb{F}_{p1} \quad (33.38b)$$

$$= -\epsilon_{3mp} \partial_m \mathbb{F}_{p1} \quad (33.38c)$$

$$= -\epsilon_{312} \partial_1 \mathbb{F}_{21} - \epsilon_{321} \partial_2 \mathbb{F}_{11} \quad (33.38d)$$

$$= -\partial_x \mathbb{F}_{21} + \partial_y \mathbb{F}_{11} \quad (33.38e)$$

$$= \partial_x (u v) + \partial_y (-u^2 + v^2)/2 \quad (33.38f)$$

$$= v \partial_x u + u \partial_x v - u \partial_y u + v \partial_y v \quad (33.38g)$$

$$= u \zeta, \quad (33.38h)$$

and likewise

$$[\nabla \cdot (\hat{\mathbf{z}} \times \mathbb{F})]_2 = \partial_y \mathbb{F}_{12} - \partial_x \mathbb{F}_{22} = v \zeta. \quad (33.39)$$

*Taylor-Bretherton identity for potential vorticity*

Building from the development for relative vorticity, we can readily connect the potential vorticity flux,  $\mathbf{u} q$ , to the anisotropic kinetic stress. We do so by considering the two equivalent forms for the potential vorticity equation

$$\frac{\partial q}{\partial t} = -\nabla \cdot (\mathbf{u} q) \quad \text{and} \quad \frac{\partial q}{\partial t} = -\nabla \cdot [\mathbf{u} f + \nabla \cdot (\hat{\mathbf{z}} \times \mathbb{F})]. \quad (33.40)$$

Hence, the Taylor-Bretherton identity for potential vorticity in the two dimensional non-divergent flow is given by

$$\mathbf{u} q = \mathbf{u} f + \nabla \cdot (\hat{\mathbf{z}} \times \mathbb{F}). \quad (33.41)$$

### 33.2.5 Poisson equation for the streamfunction

Given boundary conditions, the barotropic vorticity equation (33.29) allows us to determine the evolution of vorticity. We can in turn invert the Poisson equation (see Section 3.5 for discussion of the Poisson equation)

$$\nabla^2 \psi = \zeta \quad (33.42)$$

to determine the streamfunction and then the velocity field  $\mathbf{u} = \hat{\mathbf{z}} \times \nabla\psi$ . This inversion requires information about the boundary conditions for the streamfunction, as discussed in Section 33.1.2. By this method, time integration of the absolute vorticity equation is sufficient to fully specify time evolution of the horizontal velocity. Notably, we do not need to explicitly determine pressure to determine the flow.

### 33.2.6 Zonal flow as an exact geostrophic solution

An arbitrary zonal velocity with a meridional shear,  $\mathbf{u} = U(y)\hat{\mathbf{x}}$ , is an exact solution of the perfect fluid non-divergent barotropic model. We see this property by plugging into the velocity equation (33.1) and noting that  $D\mathbf{u}/Dt = 0$ . Hence, this flow is an exact geostrophic solution whose pressure field is itself also just a function of latitude and whose meridional gradient is determined by

$$f\hat{\mathbf{z}} \times \mathbf{u} = -\nabla\varphi \implies \partial_y\varphi = -f(y)U(y). \quad (33.43)$$

Furthermore, each term in the vorticity equation (33.28) identically vanishes, so that the vorticity

$$\zeta = -\partial_y U \quad (33.44)$$

remains constant in time at each point in space.

## 33.3 Connection to equivalent barotropic flow

In many cases, flows respecting the quasi-geostrophic assumptions possess a vertical profile that can be separated from the horizontal. In this case we write the horizontal velocity as

$$\mathbf{u}(x, y, z, t) = \Psi(z)\mathbf{u}^{\text{eb}}(x, y, t), \quad (33.45)$$

where  $\Psi > 0$  is a single-signed non-dimensional structure function that has a unit average,  $\langle \Psi \rangle = 1$ , when computed over the fluid layer thickness, and where  $\mathbf{u}^{\text{eb}}(x, y, t)$  carries the horizontal spatial dependence of the flow. With  $\Psi > 0$ , the horizontal flow remains in the same direction throughout the fluid column; i.e., eastward flow at the top of the column remains eastward at the bottom.

### 33.3.1 Vorticity equation for the depth averaged flow

To connect the very particular form (33.45) for the flow with the non-divergent barotropic model, we anticipate a discussion in Section 40.2.2 in which the quasi-geostrophic vorticity equation is shown to be

$$\frac{\partial \zeta_g}{\partial t} + \mathbf{u}_g \cdot \nabla \zeta_g = -\beta \zeta_g + f_0 \frac{\partial w}{\partial z}, \quad (33.46)$$

where  $\mathbf{u}_g$  is the horizontally non-divergent geostrophic velocity, and  $\zeta_g = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u}_g)$  is the geostrophic relative vorticity. We see that the quasi-geostrophic vorticity is affected by both the beta-effect and by vertical stretching of fluid columns (the  $\partial w / \partial z$  term), whereas vertical stretching is absent from the non-divergent barotropic vorticity equation (33.28). There are occasions in which it is sensible to assume the vertical velocity for a quasi-geostrophic flow vanishes at the top and bottom of the fluid domain, such as when considering flow in the absence of topography. In this case, performing the decomposition (33.45) for the horizontal flow and then taking a vertical average of the quasi-geostrophic vorticity equation (33.46) leads to

$$\frac{\partial \zeta_g^{\text{eb}}}{\partial t} + \langle \Psi^2 \rangle \mathbf{u}_g^{\text{eb}} \cdot \nabla \zeta_g^{\text{eb}} = -\beta v_g^{\text{eb}}. \quad (33.47)$$

This equation motivates us to define

$$\mathbf{u}^* = \langle \Psi^2 \rangle \mathbf{u}_g^{eb} \quad \text{and} \quad \zeta^* = \langle \Psi^2 \rangle \zeta_g^{eb}, \quad (33.48)$$

which are the original geostrophic fields,  $\mathbf{u}_g(x, y, z, t)$  and  $\zeta_g(x, y, z, t)$ , when evaluated at a depth where  $\Psi(z^*) = \langle \Psi^2 \rangle$ . The depth,  $z^*$ , is known as the *equivalent barotropic depth*. Introduction of the starred fields then brings the vorticity equation (33.47) into the form of the non-divergent barotropic vorticity equation

$$\frac{\partial \zeta^*}{\partial t} + \mathbf{u}^* \cdot \nabla \zeta^* = -\beta v^*. \quad (33.49)$$

### 33.3.2 Comments

[Charney et al. \(1950\)](#) justified their study of the non-divergent barotropic vorticity model by noting its connection to the commonly observed equivalent barotropic structure of the large-scale middle latitude atmosphere. The equivalent barotropic model has been a very useful analysis and prediction tool for meteorologists, and it formed the basis of many numerical weather prediction models into the 1980s. Section 7.1 of [Haltiner and Williams \(1980\)](#) offers further details on such numerical models.

One hypothesis for why quasi-geostrophic flows tend towards an equivalent barotropic profile relates to movement of energy in rotationally dominant turbulent flows, whereby energy cascades to the larger scales. As discussed in [Smith and Vallis \(2001\)](#) and [Venaille et al. \(2012\)](#), among others, this *inverse* energy cascade pumps mechanical energy into a vertically uniform or “barotropic” structure. In a realistic flow, including topography, stratification, and variable forcing, this cascade is never realized completely, thus rendering a flow that approaches the equivalent barotropic structure. Conversely, moving to the highly idealized world, the case of  $f = 0$  with flat bottom is commonly referred to as *two-dimensional turbulence* ([Kraichnan and Montgomery, 1980](#)). This model has a long history of key theoretical results that presaged their analog in quasi-geostrophic turbulence.

## 33.4 The externally applied lid pressure

As noted in Section 33.2.5, we do not need to determine the pressure to determine the evolution of the non-divergent barotropic flow. Instead, we can determine the flow by time stepping vorticity and then inverting the elliptic problem to get the streamfunction. Furthermore, the free surface is absolutely flat even in the presence of topography. Hence, there is no pressure generated by undulations of the free surface. So how is there flow in this model?

As we see in this section, the non-divergent barotropic model maintains a flat *rigid lid* upper surface due to an externally imposed *lid pressure*. In turn, it is the lid pressure that provides the force that drives flow in this model. We here expose details to understand the fundamental, yet somewhat hidden, role for the lid pressure.

To further motivate the analysis, we again emphasize the strong constraints placed on the velocity field, which must satisfy the following conditions at each space and time point

$$\nabla \cdot \mathbf{u} = 0 \quad \text{and} \quad \mathbf{u} \cdot \nabla \eta_b = 0 \quad \text{and} \quad w = 0. \quad (33.50)$$

Kinematics of the constrained flow induce a depth-independent pressure that enforces these constraints. Examining the resulting pressure field furthers our understanding of the forces acting in the fluid. This role for pressure as an enforcer of non-divergence is shared by the three-dimensional non-divergent flow found in a Boussinesq fluid (see Section 23.3). It is simpler to visualize fields in

the two dimensional non-divergent barotropic model, thus facilitating understanding and insights that generalize to the three dimensional case.

### 33.4.1 Poisson equation for pressure

We derive the pressure equation by using the two-dimensional non-divergence property of the horizontal flow and then developing a diagnostic relation. We can eliminate the time derivative from equation (33.1) by taking  $\partial/\partial x$  on the zonal equation and  $\partial/\partial y$  on the meridional equation, then adding. The result is a diagnostic relation for the Laplacian of the pressure<sup>2</sup>

$$-\nabla^2\varphi = \partial_x[\nabla \cdot (\mathbf{u} u)] + \partial_y[\nabla \cdot (\mathbf{u} v)] - f\zeta + \beta u, \quad (33.51)$$

where we set

$$\nabla \cdot \partial_t \mathbf{u} = \partial_t \nabla \cdot \mathbf{u} = 0 \implies \partial_x(\partial_t u) = -\partial_y(\partial_t v). \quad (33.52)$$

Making use of the boundary conditions discussed in Section 33.1.2, the elliptic partial differential equation (33.51) can be inverted to find the pressure field (Section 3.5). As for the three-dimensional incompressible case, we see that the pressure is instantaneously constrained to satisfy the non-divergence condition placed on the velocity.

Numerically inverting an elliptic operator in equation (33.51) is straightforward on simple domains, such as flat bottom rectangular regions or a smooth sphere. However, when the bottom is not flat, or when there are islands (i.e., the domain is not simply connected), then the elliptic inversion can be difficult to perform numerically. This algorithmic complexity is one reason numerical barotropic models are less commonly used for realistic numerical experimentation than the more general shallow water models. Even so, as pursued in the remainder of this section, we can make use of idealized configurations to garner insight into how pressure maintains the flow constraints.

### 33.4.2 Gradient wind balance

For two-dimensional non-divergent flow we can write the self-advection in terms of the streamfunction, or equivalently to the Jacobian of the velocity field, through the following manipulations

$$\partial_x[\nabla \cdot (\mathbf{u} u)] + \partial_y[\nabla \cdot (\mathbf{u} v)] = \nabla \cdot (\partial_x \mathbf{u} u) + \nabla \cdot (\mathbf{u} \partial_x u) + \nabla \cdot (\partial_y \mathbf{u} v) + \nabla \cdot (\mathbf{u} \partial_y v) \quad (33.53a)$$

$$= \partial_x \mathbf{u} \cdot \nabla u + \partial_y \mathbf{u} \cdot \nabla v \quad (33.53b)$$

$$= (\partial_x u)^2 + (\partial_y v)^2 + 2 \partial_x v \partial_y u \quad (33.53c)$$

$$= 2 [(\partial_x u)^2 + \partial_x v \partial_y u] \quad (33.53d)$$

$$= 2 [(\partial_{xy}\psi)^2 - \partial_{xx}\psi \partial_{yy}\psi] \quad (33.53e)$$

$$= 2 \hat{\mathbf{z}} \cdot (\partial_x \nabla \psi \times \partial_y \nabla \psi) \quad (33.53f)$$

$$= -2 J(\partial_x \psi, \partial_y \psi), \quad (33.53g)$$

$$= 2 J(v, u), \quad (33.53h)$$

---

<sup>2</sup>We maintain the minus sign on the left hand side of equation (33.51) so that a positive source on the right hand side leads to a positive  $\varphi$ . We can readily understand the sign by taking a Fourier transform, whereby the Laplacian operator picks up a minus sign when converted to Fourier space. We follow the same sign convention when studying the Green's function for the Poisson equation in Chapter 4.

where we introduced the Jacobian operator from equation (33.28). The pressure equation (33.51) thus takes on the form

$$-\nabla^2 \varphi = -2 J(u, v) - \nabla \cdot (f \nabla \psi), \quad (33.54)$$

where we also wrote

$$-\nabla \cdot (f \nabla \psi) = -f \nabla^2 \psi - \beta \partial_y \psi = -f \zeta + \beta u. \quad (33.55)$$

We consider this equation as a *gradient wind balance* in analog to the gradient wind balance discussed in Section 26.6. Here, the Jacobian term accounts for the centrifugal acceleration of the curved fluid motion, and the  $\nabla \cdot (f \nabla \psi)$  term accounts for the Coriolis acceleration, both for the  $f$ -plane and  $\beta$ -plane. Equation (33.54) thus offers a more accurate diagnostic relation for the pressure field than provided by assuming a geostrophically balanced flow.

### 33.4.3 Pressure source from self-advection

We here introduce yet another way to examine the self-advection source appearing in the pressure equation (33.51) by writing it as

$$\partial_x [\nabla \cdot (\mathbf{u} u)] + \partial_y [\nabla \cdot (\mathbf{u} v)] = \mathbb{S}_{mn} \mathbb{S}_{mn} - \mathbb{R}_{mn} \mathbb{R}_{mn}, \quad (33.56)$$

where the rate of strain tensor,  $\mathbb{S}$ , and rotation tensor,  $\mathbb{R}$ , have components given by equations (13.33a) and (13.33b)

$$\mathbb{S}_{mn} = \frac{1}{2} \left[ \frac{\partial v_m}{\partial x_n} + \frac{\partial v_n}{\partial x_m} \right] = \mathbb{S}_{nm} \quad \text{rate of strain tensor} \quad (33.57)$$

$$\mathbb{R}_{mn} = \frac{1}{2} \left[ \frac{\partial v_m}{\partial x_n} - \frac{\partial v_n}{\partial x_m} \right] = -\mathbb{R}_{nm} \quad \text{rotation tensor.} \quad (33.58)$$

For two-dimensional flow the rotation tensor is related to the relative vorticity via

$$\mathbb{R}_{mn} = -\epsilon_{mn} \zeta / 2 = -\epsilon_{mn} \nabla^2 \psi / 2, \quad (33.59)$$

where  $\epsilon_{mn}$  is the anti-symmetric Levi-Civita permutation symbol (see Section 1.4.1)

$$\epsilon_{mn} = \begin{bmatrix} \epsilon_{11} & \epsilon_{12} \\ \epsilon_{21} & \epsilon_{22} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}, \quad (33.60)$$

which leads to

$$\mathbb{R}_{mn} \mathbb{R}_{mn} = \zeta^2 / 2. \quad (33.61)$$

The identity (33.56) indicates that the squared strain (sometimes referred to as the splat) provides a positive source to the Poisson equation (33.51) whereas squared vorticity provides a negative source.

In the following sections, we present two examples to help support understanding of how pressure gradients arise in a 2d-barotropic flow to maintain, at each time instance, a non-divergent two-dimensional velocity field. For simplicity we just consider the non-rotating case so that it is sufficient to examine how pressure responds to self-advection.

### 33.4.4 Pressure source from solid-body flow

Consider a velocity field in a flat domain that is initialized in circular solid-body motion (Figure 33.1)

$$\mathbf{u} = \boldsymbol{\Omega} \times \mathbf{x} = \Omega (-y \hat{x} + x \hat{y}), \quad (33.62)$$

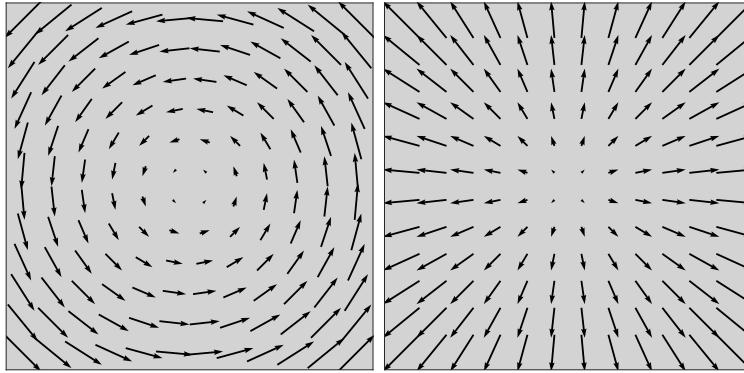


FIGURE 33.1: Left panel: example flow field from solid-body rotation,  $\mathbf{u} = \boldsymbol{\Omega} \times \mathbf{x} = (-y, x)$ , which has vorticity  $\nabla \times \mathbf{u} = 2\boldsymbol{\Omega}$  and zero strain. Right panel: corresponding acceleration from self-advection,  $-(\mathbf{u} \cdot \nabla) \mathbf{u} = \boldsymbol{\Omega}^2 \mathbf{x}$ . The acceleration from self-advection is exactly compensated by the pressure gradient force:  $-(\mathbf{u} \cdot \nabla) \mathbf{u} - \nabla \varphi = 0$ , thus allowing for the solid-body motion to be an exact solution to two-dimensional non-divergent flow. The units are arbitrary.

where  $\boldsymbol{\Omega} = \Omega \hat{\mathbf{z}}$  is a constant angular velocity. This flow has zero strain and non-zero vorticity

$$\hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u}) = \zeta = 2\Omega \implies -\mathbb{R}_{mn} \mathbb{R}_{mn} = -\Omega^2. \quad (33.63)$$

The velocity time tendency from the self-advection acceleration is

$$-(\mathbf{u} \cdot \nabla) \mathbf{u} = \Omega^2 \mathbf{x}, \quad (33.64)$$

which is the outward directed centrifugal acceleration associated with the circular solid-body motion.<sup>3</sup> The centrifugal acceleration generates a velocity field that diverges from the origin. However, the velocity is constrained to remain non-divergent at each instance, so the centrifugal acceleration cannot be the full story. Indeed, to maintain the non-divergent constraint, a pressure gradient is instantaneously established that exactly counteracts the centrifugal acceleration. Hence, there is a low pressure established at the origin so that the pressure gradient force points inward. This example illustrates how vorticity provides a source of low pressure in an incompressible flow. Furthermore, since the pressure gradient exactly counteracts the centrifugal acceleration from the velocity self-advection, the solid-body flow is an exact steady solution for the non-divergent and non-rotating barotropic system.

In the absence of rotation, the pressure field is found by solving the Poisson equation

$$-\nabla^2 \varphi = -\Omega^2. \quad (33.65)$$

Assuming circular symmetry allows us to let  $\varphi$  be a function just of the radial distance from the origin, in which case the pressure field is parabolic and the pressure gradient acceleration is radial

$$\varphi = (\Omega r)^2 / 2 \quad \text{and} \quad -\nabla \varphi = -\Omega^2 \mathbf{x} = (\mathbf{u} \cdot \nabla) \mathbf{u}. \quad (33.66)$$

To reach this result, we used the cylindrical expression for the Laplacian operator (equation (8.83b)) and set  $\varphi(r=0)=0$ . To help understand the physics of this parabolic pressure field, recall the analysis in Section 22.4 of a solid-body rotating homogeneous fluid layer in a cylindrical tank. In contrast to the barotropic system, the horizontal velocity in a homogeneous fluid layer, such as in a shallow water fluid, is divergent so that the layer thickness is not constrained to

<sup>3</sup>We considered the more general case in Section 26.2.2 when decomposing the material acceleration for two-dimensional flow into natural coordinates.

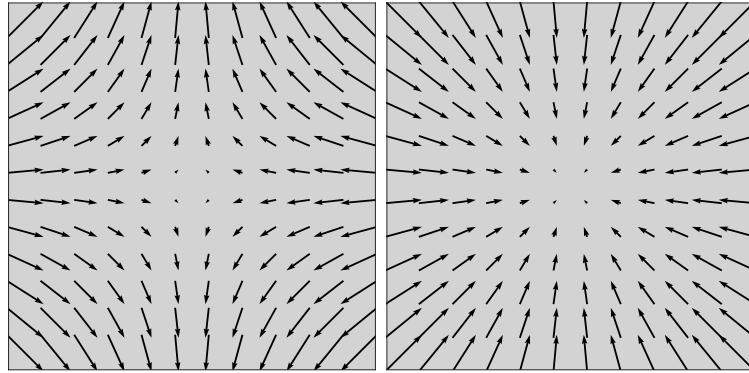


FIGURE 33.2: Left panel: example purely strained flow field with zero vorticity,  $\mathbf{u} = \Omega(-x\hat{\mathbf{x}} + y\hat{\mathbf{y}})$ . Right panel: corresponding converging acceleration from self-advection,  $-(\mathbf{u} \cdot \nabla) \mathbf{u} = -\Omega^2 \mathbf{x}$ . The units are arbitrary.

remain flat. Hence, the centrifugal acceleration causes the velocity to diverge from the center so that the layer thickness increases radially outward, with the layer bounded by the tank wall. At steady state, the homogeneous fluid layer has a parabolic free surface with a minimum at the center (see equation (22.81)). The parabolic free surface creates a pressure field that precisely corresponds to the pressure field (33.66) in the non-divergent barotropic system. The adjustment of a homogeneous fluid layer, such as a shallow water fluid, contains linear fluctuations in the form of gravity waves such as discussed in Chapter 31. In contrast, the adjustment required to reach a steady state occurs instantaneously in the non-divergent barotropic fluid.

### 33.4.5 Pressure source from irrotational flow

Now consider the following pure strain flow (Figure 33.2)

$$\mathbf{u} = \Omega(-x\hat{\mathbf{x}} + y\hat{\mathbf{y}}), \quad (33.67)$$

whose vorticity vanishes and whose self-advection acceleration is given by

$$-(\mathbf{u} \cdot \nabla) \mathbf{u} = -\Omega^2 \mathbf{x} \implies \mathbb{S}_{mn} \mathbb{S}_{mn} = \Omega^2. \quad (33.68)$$

This acceleration is exactly the opposite of that produced by the solid-body motion studied in the previous example. Hence, to maintain the non-divergent nature of the barotropic flow, a pressure (again, assuming  $f = 0$ ) is established with a high pressure at the center that exactly counteracts the converging self-advection acceleration arising in the strained flow

$$\varphi = -(\Omega r)^2/2 \quad \text{and} \quad -\nabla \varphi = \Omega^2 \mathbf{x} = (\mathbf{u} \cdot \nabla) \mathbf{u}. \quad (33.69)$$

This example illustrates how strain provides a source for high pressure in an incompressible flow. Furthermore, we see that this flow is an exact steady solution for non-rotating non-divergent barotropic flow.

### 33.4.6 Pressure source from Coriolis acceleration

In addition to the self-advection source, pressure is affected by a source from the Coriolis acceleration

$$-\nabla^2 \varphi_{\text{geostrophy}} \equiv \nabla \cdot (f \hat{\mathbf{z}} \times \mathbf{u}) = -\nabla \cdot (f \nabla \psi) = \beta u - \zeta f. \quad (33.70)$$

As such, we can write the pressure gradient as<sup>4</sup>

$$-\nabla\varphi_{\text{geostrophy}} = f \hat{\mathbf{z}} \times \mathbf{u}. \quad (33.71)$$

Consider cyclonic flow around an arbitrary point. What is the pressure field induced by this flow? As in our discussion in Section 33.4.4 of the solid body rotating flow, a cyclonic flow has an associated centrifugal acceleration that points outward. To counteract the centrifugal acceleration, and thus to maintain a non-divergent flow, requires an inward pointing pressure force; i.e., a low pressure center. Hence, cyclonic circulation induces, through the Coriolis acceleration, a negative pressure source whereas anti-cyclonic circulation induces a positive pressure source.

### 33.4.7 Pressure source from friction

Consider flow with friction, in which case the velocity equation (33.1) takes the form

$$\frac{D\mathbf{u}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla\varphi + \mathbf{F}, \quad (33.72)$$

with  $\mathbf{F}$  a frictional acceleration. In this case we have yet another source for pressure given by

$$-\nabla^2\varphi_{\text{friction}} \equiv -\nabla \cdot \mathbf{F} \implies -\nabla\varphi_{\text{friction}} = -\mathbf{F}. \quad (33.73)$$

As discussed in Section 18.7, viscous friction is generally associated with a nonzero rate of strain. We see that the frictional acceleration induces a high pressure source in regions where frictional accelerations converge,  $-\nabla \cdot \mathbf{F} > 0$ , with this source acting to maintain non-divergent flow in the presence of converging frictional acceleration.

### 33.4.8 Comments and further study

- The pressure equation (33.51) is elliptic, and elliptic equations need boundary conditions. In the presence of topography the boundary conditions are modified relative to the flat bottom case. Hence, pressure knows about topography through its boundary conditions. The resulting pressure force keeps the flow non-divergent and the flow aligned with topography as per the kinematic conditions in Section 33.1.2.
- The discussion of pressure induced by self-advection in Sections 33.4.4 and 33.4.5 is based on a similar presentation in Appendix B of *Jeevanjee and Romps (2015a)*.
- *Bryan (1969)* provided the first working numerical algorithm to simulate the ocean general circulation. Bryan's method made use of the rigid lid approximation of Section 33.4 so that the depth integrated velocity is non-divergent. However, the vorticity in Bryan's ocean model is affected by more than just the beta-effect. The reason is that the depth integrated velocity equation includes contributions from baroclinic processes, and such processes affect the barotropic vorticity in a baroclinic fluid. We detail such effects in Sections 39.7 and 39.8.

The rigid lid method was generally used for large-scale circulation modeling until the late 1990s. Free surface methods, allowing divergence in the depth integrated flow, have largely displaced the rigid lid as a practical method for time stepping ocean models (e.g., see chapter 12 of *Griffies (2004)*).

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<sup>4</sup>Formally, we can add an arbitrary gauge function to the right hand side of equation (33.71), with this term of the form  $\hat{\mathbf{z}} \times \nabla\chi$ . However, since we derived the pressure Poisson equation from the velocity equation, then we know there is no gauge function arising in equation (33.71).

## 33.5 Constraints from absolute vorticity invariance

We here examine constraints on the flow imposed by material invariance of absolute vorticity, which holds for two-dimensional non-divergent flow when there is no dissipation

$$\frac{D(\zeta + f)}{Dt} = 0. \quad (33.74)$$

These constraints offer insights into the flow behavior and allow us to predict responses to perturbations. We frame the discussion in terms of the decomposition (32.38) of relative vorticity into a curvature (or orbital) term and normal shear term

$$\zeta = \frac{|\mathbf{u}|}{R} - \frac{\partial |\mathbf{u}|}{\partial n} \equiv \zeta_{\text{curv}} + \zeta_{\text{shear}}, \quad (33.75)$$

so that

$$\frac{D(\zeta_{\text{curv}} + \zeta_{\text{shear}} + f)}{Dt} = 0. \quad (33.76)$$

When the flow turns, the curvature term contributes with  $R$  the radius of curvature.<sup>5</sup> If the flow develops shears in the direction normal to the flow, then the shear term contributes. In the presence of  $\beta = \partial_y f$ , meridional motion through the planetary vorticity field requires a compensating response from relative vorticity. In general each of the three terms contribute to the relative vorticity, though in the following we consider cases where one is subdominant.

### 33.5.1 Relative vorticity from curvature and planetary beta

According to the decomposition (33.75), fluid that curves to the left (facing downstream) picks up a positive relative vorticity from flow curvature,  $R > 0 \Rightarrow \zeta > 0$ , as depicted in Figure 33.3. The oppositely curved flow has a negative radius of curvature so flow curving to the right picks up a negative relative vorticity,  $R < 0 \Rightarrow \zeta < 0$ . We focus here on the case where the normal shear induced relative vorticity can be neglected so that we are only concerned with curvature induced vorticity plus planetary vorticity (beta effect).

Consider a flow that is initially zonal with zero relative vorticity. If the flow turns meridionally then it experiences a change in relative vorticity both through the curvature term plus a change in planetary vorticity since  $f$  changes. To maintain constant absolute vorticity, a fluid column that moves meridionally requires the relative vorticity induced by the curved flow path to counteract the change in planetary vorticity. As we now discuss, the constraint of fixed absolute vorticity, in the absence of induced normal shears, means that eastward flow (westerly winds) cannot turn meridionally while maintaining fixed absolute vorticity, whereas westward flow (easterly winds) can turn (see Figure 33.3).

Consider westward flow in the northern hemisphere ( $f > 0$ ). If the flow turns to the north (to the right facing downstream) then this flow picks up a curvature-induced negative relative vorticity,  $\zeta < 0$ , and an increase in the planetary vorticity ( $f$  increases). Likewise, a westward flowing fluid column that turns equatorward (to the left) has a positive curvature-induced relative vorticity ( $\zeta > 0$ ) and a reduction in planetary vorticity ( $f$  decreases). Hence, westward flow in the northern hemisphere can turn either poleward (to the north) or equatorward (to the south) and still maintain constant absolute vorticity, so long as the curved motion induces the proper

<sup>5</sup>As discussed in Section 26.2, we take the convention whereby the normal direction is to the left of flow when facing downstream. Flow turning into the normal direction (to the left) has a positive radius of curvature,  $R > 0$ , and flow turning opposite to the normal direction (to the right) has  $R < 0$ .

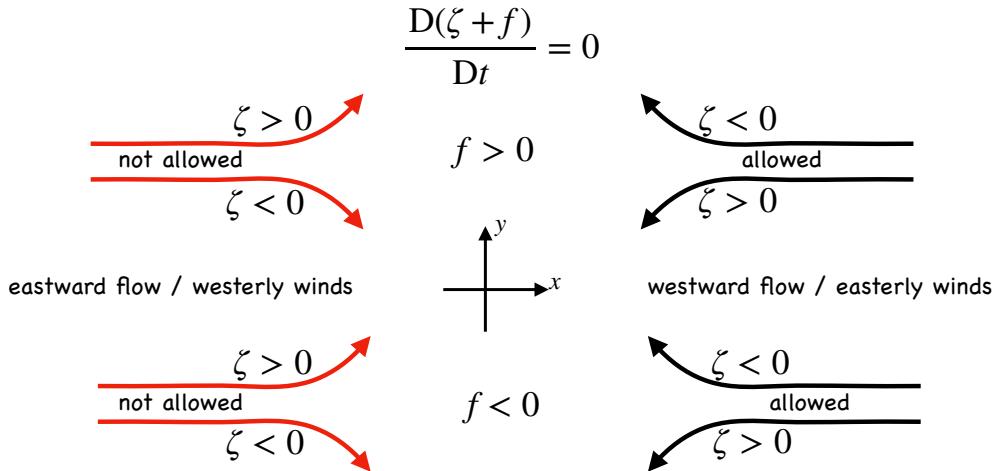


FIGURE 33.3: Illustrating the constraints on a two dimensional non-divergent flow imposed by material invariance of absolute vorticity:  $\zeta + f = \text{constant}$ . We assume flow is over a flat region and assume there is only curvature induced relative vorticity (no shear-induced relative vorticity;  $\partial|\mathbf{u}|/\partial n = 0$ ) as per the decomposition in equation (33.75). In each of the four cases depicted, the entering flow has zero relative vorticity, which means that absolute vorticity must remain constant at the initial Coriolis parameter,  $\zeta + f = f_{\text{initial}}$ . The red eastward flow (westerly winds) that turns meridionally picks up a curvature vorticity that supports the change in planetary vorticity, thus precluding material invariance of absolute vorticity. Hence, the meridional turning of eastward flow is not allowed so that flow must remain zonal for absolute vorticity to remain invariant. In contrast, the oppositely directed westward flow (easterly winds) can deviate either to the north or south and still retain a constant absolute vorticity. We illustrate flows for both the northern and southern hemispheres. This figure is adapted from Figure 4.8 of [Holton \(1992\)](#).

relative vorticity to counteract the changes to  $f$ . The same arguments also hold in the southern hemisphere, so that the general scenarios are depicted in Figure 33.3.

The situation is different for eastward flow. Consider again flow in the northern hemisphere. A poleward (to the left) turning fluid column is associated with a positive curvature-induced relative vorticity,  $\zeta > 0$ , as well as an increase in the planetary vorticity. Hence, this motion changes the absolute vorticity and as such it is not allowed if the absolute vorticity is constrained to remain constant. Likewise, an equatorward (to the right) turning eastward fluid column induces a negative curvature-induced relative vorticity,  $\zeta < 0$ , and a decrease in planetary vorticity, again leading to a change in absolute vorticity. Hence, eastward flow (westerly winds) in either hemisphere must remain zonal to maintain a constant absolute vorticity.

As an application of these results, consider the situation depicted in Figure 33.4, whereby inviscid flow in the interior of an ocean domain moves westward into a frictional western boundary layer. The constraints imposed by absolute vorticity invariance allow for this flow to occur, whereas the opposite is disallowed whereby eastward inviscid flow cannot enter an eastern boundary. We return to this example in Section 34.9 when discussing western intensification of ocean gyres.

### 33.5.2 Relative vorticity from curvature and normal shears

Now consider the case in which the meridional displacements are small so that the beta effect can be neglected. In this case there is an exchange between relative vorticity arising from curvature and relative vorticity from normal shears, thus leaving their sum materially invariant

$$\frac{D(\zeta_{\text{curv}} + \zeta_{\text{shear}})}{Dt} = 0. \quad (33.77)$$

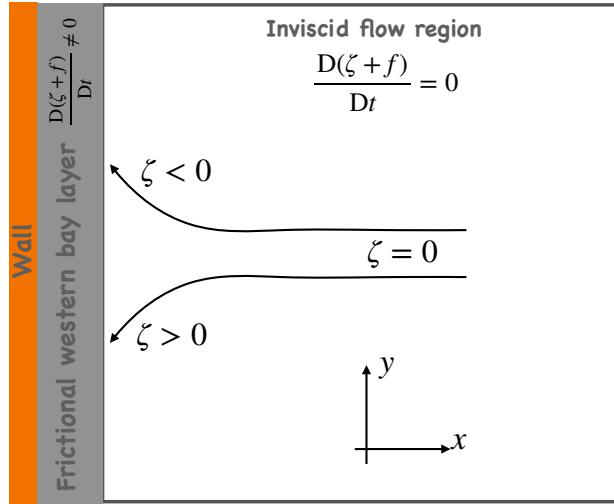


FIGURE 33.4: Illustrating the constraints on a homogeneous and constant thickness fluid layer imposed by material invariance of absolute vorticity:  $\zeta + f = \text{constant}$ . As per the results from Figure 33.3, inviscid flow with initially zero relative vorticity can enter a western boundary layer as depicted here, whereas it cannot enter an eastern boundary layer. This conclusion assumes that there is no shear-induced relative vorticity ( $\partial|\mathbf{u}|/\partial n = 0$ ) that can overcome changes in the vorticity induced by changes to  $f$  and by curvature-induced relative vorticity (see Section 32.6.2). This figure is adapted from Figure 19.12 of [Vallis \(2017\)](#).

We depict an example in Figure 33.5 whereby a vortex undergoes a left turn facing downstream. While on the curve, the relative vorticity of the vortex is in part due to the positive curvature vorticity,  $\zeta_{\text{curv}} > 0$ . If the relative vorticity is positive on the straight portion of the trajectory, then when on the curve the shear vorticity must lose some of its strength in order to compensate for the curvature vorticity. Conversely, if the relative vorticity is negative on the straight portion of the trajectory, then when on the curve the shear vorticity gains in strength to allow for the positive curvature vorticity.

### 33.5.3 Curvature, shear, and planetary contributions

We now consider all three terms appearing in the vorticity equation (33.76). Let us consider again the eastward flow that turns to the north in the northern hemisphere. Such flow is not allowed if the only source for relative vorticity is curvature. However, if the eastward flow, as it turns, picks up a shear that induces a nonzero negative relative vorticity, then such flow can turn so long as the shear-induced negative relative vorticity balances the positive absolute vorticity from increases in  $f$  and the curvature-induced vorticity. Writing this condition for the shear-induced relative vorticity yields

$$\zeta_{\text{shear}} = -\Delta f - \zeta_{\text{curv}} = -(f_{\text{final}} - f_{\text{init}}) - \zeta_{\text{curv}} < 0, \quad (33.78)$$

where  $f_{\text{init}}$  and  $f_{\text{final}}$  are the initial and final Coriolis parameters. Conversely, if the flow deviates towards the equator then it can do so only if there is a positive shear-induced relative vorticity

$$\zeta_{\text{shear}} = -(f_{\text{final}} - f_{\text{init}}) - \zeta_{\text{curv}} > 0. \quad (33.79)$$

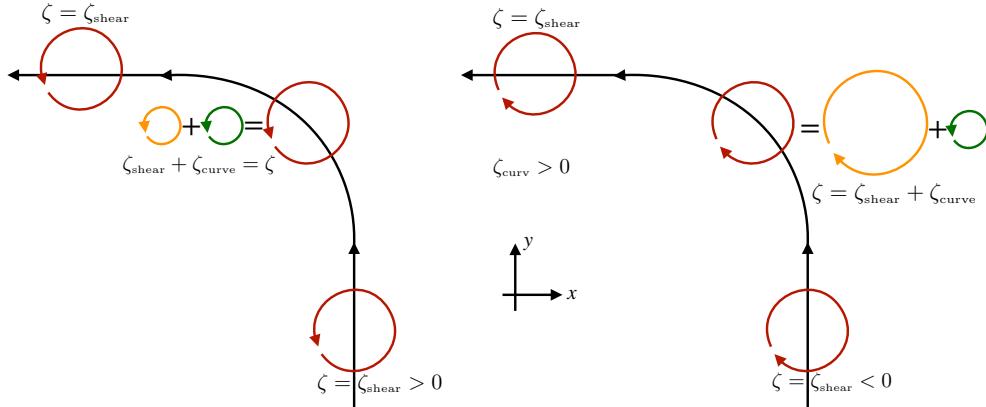


FIGURE 33.5: Material invariance of relative vorticity,  $D\zeta/Dt = D(\zeta_{\text{curv}} + \zeta_{\text{shear}})/Dt = 0$ , means that as a vortex moves around a curve its shear vorticity is modified to keep the total relative vorticity invariant. On the straight portion of these trajectories, the relative vorticity is due only to shear vorticity,  $\zeta = \zeta_{\text{shear}}$  since  $\zeta_{\text{curv}} = 0$ . However, when the vortex enters the curve, maintaining a constant relative vorticity requires an exchange of shear vorticity with the curvature vorticity. In this example we illustrate a steady flow that turns to the left so that the vortex picks up a positive curvature vorticity,  $\zeta_{\text{curv}} > 0$ . Left panel: a vortex that enters the left turn with a positive relative vorticity must give some of its shear vorticity to the curvature vorticity in order to maintain  $\zeta$  constant along the trajectory. Right panel: a vortex that enters the curve with a negative relative vorticity sees its shear vorticity increase in magnitude to compensate for the positive curvature vorticity.

## 33.6 Barotropic Rossby waves

The non-divergent barotropic model has no gravity waves since gravity waves are supported by a nonzero horizontal flow divergence (see discussion of shallow water gravity waves in Section 31.8). We can formally consider the gravity wave speed to be infinite.

However, the non-divergent barotropic model does admit linear wave fluctuations known as *Rossby waves*, and Rossby waves arise from the beta-effect (Section 35.7.2). In this section we illustrate the basic physical attributes of barotropic Rossby waves. We do so by studying linear wave perturbations to uniform mean zonal flow in a zonally re-entrant channel on a beta-plane. We assume some familiarity with wave kinematics as introduced for shallow water gravity waves in Section 31.8. This section is a teaser to a more thorough study of Rossby waves such as that provided in Chapter 6 of [Vallis \(2017\)](#).

### 33.6.1 Dispersion relation

Consider a zonal channel with meridional extent  $y_s \leq y \leq y_n$  where  $y_n - y_s = L$ , and allow for a basic state geostrophic flow to exist with a constant zonal velocity  $U \hat{x}$  and corresponding streamfunction

$$\psi_{\text{basic}} = -U y. \quad (33.80)$$

Now perturb this flow with a wave pattern that leads to a streamfunction of the form

$$\psi = \psi_{\text{basic}} + \psi_o \sin(k x - \omega t) \sin[(y - y_s) l], \quad (33.81)$$

where  $\psi_o$  is the wave amplitude,  $k$  is the zonal wave number, and  $c$  is the wave phase speed. The meridional structure is chosen to satisfy the no-normal flow boundary condition at the northern and southern walls (Section 33.1.2), which leads to  $\partial_x \psi = 0$  at  $y = y_s$  and  $y = y_n$ . The southern boundary condition is trivially satisfied, yet the northern boundary is satisfied only if the

meridional wavenumber,  $l$ , is quantized according to

$$(y_n - y_s) l = L l = 2\pi n \implies l = 2\pi n/L \quad \text{with } n \text{ an integer.} \quad (33.82)$$

The corresponding velocity and relative vorticity are given by

$$u = -\partial_y \psi = U - \psi_o k \sin(kx - \omega t) \cos[(y - y_s) l] \quad (33.83a)$$

$$v = \partial_x \psi = \psi_o k \cos(kx - \omega t) \sin[(y - y_s) l] \quad (33.83b)$$

$$\zeta = \nabla^2 \psi = -\psi_o (k^2 + l^2) \sin(kx - \omega t) \sin[(y - y_s) l], \quad (33.83c)$$

so that terms in the barotropic vorticity equation (33.28) are

$$\partial_t \zeta = \psi_o \omega (k^2 + l^2) \cos(kx - \omega t) \sin[(y - y_s) l] \quad (33.84a)$$

$$\partial_x \zeta = -\psi_o k (k^2 + l^2) \cos(kx - \omega t) \sin[(y - y_s) l] \quad (33.84b)$$

$$\partial_y \zeta = -\psi_o l (k^2 + l^2) \sin(kx - \omega t) \cos[(y - y_s) l] \quad (33.84c)$$

$$\mathbf{u} \cdot \nabla \zeta = -\psi_o k U (k^2 + l^2) \cos(kx - \omega t) \sin[(y - y_s) l]. \quad (33.84d)$$

Plugging into the barotropic vorticity equation leads, without approximation, to the dispersion relation

$$\omega (k^2 + l^2) = k (k^2 + l^2) U - \beta k \implies \omega = U k - \frac{\beta k}{k^2 + l^2}. \quad (33.85)$$

The presence of a constant zonal velocity acts to *Doppler shift* the wave frequency by the amount  $U k$ . Furthermore, it is the presence of  $\beta \neq 0$  that gives rise to these *Rossby waves*, with  $\beta = 0$  rendering a frequency just due to the zonal background flow.

### 33.6.2 Phase speed

Components to the wave phase speed are

$$c_p^x = \frac{\omega}{k} = U - \frac{\beta}{k^2 + l^2} \quad \text{and} \quad c_p^y = \frac{\omega}{l} = \frac{U k}{l} - \frac{\beta k}{l (k^2 + l^2)}. \quad (33.86)$$

It is notable that the zonal phase speed is westward relative to the background zonal velocity. To get a sense for the scales of these waves, consider zero mean flow and set the zonal phase speed equal to the shallow water gravity wave phase speed,  $c_{\text{gravity}} = (g H)^{1/2}$  (Section 31.8), in which case the Rossby wave has a wavenumber

$$(k^2 + l^2)^{1/2} = \beta / \sqrt{g H}. \quad (33.87)$$

Writing  $K = \sqrt{k^2 + l^2} = 2\pi/\lambda$  leads to a wavelength of  $\lambda \approx 2 \times 10^4$  km for  $\phi = 60^\circ\text{S}$  and  $\beta = (2\Omega/R) \cos \phi \approx 1.14 \times 10^{-11} \text{ m}^{-1} \text{ s}^{-1}$ .

*Stationary Rossby waves* are those whose zonal phase speed vanishes due to the Doppler shift from the zonal flow

$$c_p^x = 0 \implies U = \frac{\beta}{k^2 + l^2}, \quad (33.88)$$

in which case the zonal flow speed exactly matches the phase speed of the Rossby wave. Writing  $K = \sqrt{k^2 + l^2} = 2\pi/L$  leads to a length scale for the stationary Rossby waves

$$L_{\text{stationary}} = 2\pi (U/\beta)^{1/2}. \quad (33.89)$$

With a eastward speed of  $U = 1 \text{ m s}^{-1}$  at  $\phi = 60^\circ\text{S}$  we find stationary ocean barotropic Rossby waves have a wavelength of  $\lambda_{\text{stationary}} \approx 1800 \text{ km}$ , whereas for the atmosphere with  $U = 25 \text{ m s}^{-1}$  we find  $\lambda_{\text{stationary}} \approx 9300 \text{ km}$ .

### 33.6.3 Group velocity

Components to the phase speed are not components to a vector, whereas the group velocity is a vector and it measures the velocity that energy moves with the waves

$$\mathbf{c}_g = \hat{\mathbf{x}} \partial_k \omega + \hat{\mathbf{y}} \partial_l \omega \quad (33.90\text{a})$$

$$= \hat{\mathbf{x}} \left[ U + \frac{\beta (k^2 - l^2)}{(k^2 + l^2)^2} \right] + \hat{\mathbf{y}} \frac{2\beta k l}{(k^2 + l^2)^2} \quad (33.90\text{b})$$

$$= \hat{\mathbf{x}} \left[ c_p^x + \frac{2\beta k^2}{(k^2 + l^2)^2} \right] + \hat{\mathbf{y}} \frac{2\beta k l}{(k^2 + l^2)^2}. \quad (33.90\text{c})$$

Note how the zonal component to the group velocity is always eastward relative to the phase speed. Furthermore, the zonal group velocity is westward if the zonal wavenumber is small enough (long zonal Rossby waves)

$$\frac{k^2 - l^2}{(k^2 + l^2)^2} < -U/\beta \iff \text{long zonal Rossby waves have westward group velocity}, \quad (33.91)$$

whereas it is eastward for short zonal Rossby waves

$$\frac{k^2 - l^2}{(k^2 + l^2)^2} > -U/\beta \iff \text{short zonal Rossby waves have eastward group velocity}. \quad (33.92)$$

### 33.6.4 Importance of $\beta$ for Rossby waves

Gravity is the restoring force giving rise to gravity waves (Chapter 31). For Rossby waves, it is the planetary  $\beta$  that gives rise to their existence. We see such to be the case by noting that with  $\beta = 0$  there is no wave disturbance as measured by the dispersion relation (33.85). In Figure 33.6 we illustrate the mechanism for the westward phase propagation of the Rossby waves (with  $U = 0$  for simplicity). As detailed in the figure caption, the constraint of absolute vorticity conservation for fluid parcels, in the presence of  $\beta \neq 0$ , gives rise to the westward phase speed for the Rossby wave.

The argument offered in Figure 33.6 does not consider any forces. Rather, we make use of the constraint imposed by material conservation of absolute vorticity and infer the motion of fluid parcels by noting how the relative vorticity anomaly induces a flow that moves surrounding parcels.<sup>6</sup> These vorticity-based arguments offer a straightforward and insightful means to capture the fundamentals of Rossby waves. An alternative argument, based on examining the pressure force, requires solving the Poisson equation for pressure from Section 33.4. Contrary to the simple examples offered in Section 33.4, the Rossby wave source for the pressure equation is nontrivial, even when linearizing the source by assuming small amplitude waves. We thus find the vorticity arguments to be much more transparent and streamlined.



<sup>6</sup>Analogous arguments hold for a stratified fluid, with material conservation of potential vorticity providing the fundamental constraint. See Chapter 6 of [Vallis \(2017\)](#) for details.

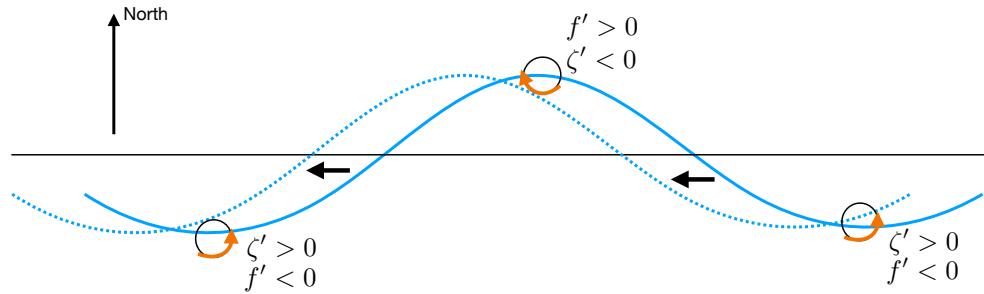


FIGURE 33.6: The westward phase speed of a Rossby wave arises from the presence of  $\beta > 0$  and the constraint that absolute vorticity ( $q = f + \zeta$ ) for a non-divergent and inviscid barotropic flow is materially constant. In this figure we consider a material line within the fluid in either the northern or southern hemispheres, with the solid line the initial position of the fluctuation and the dotted line the position later in time. For a northward perturbation relative to the initial latitude, a fluid parcel moves to a latitude with Coriolis parameter larger than its original value. Absolute vorticity conservation requires the parcel to pick up a negative relative vorticity perturbation,  $\zeta' < 0$ . The opposite occurs for a southward perturbation. The flow induced by the relative vorticity anomaly acts to move the fluctuation westward. In the absence of  $\beta$ , the meridional movement of parcels does not render a change in the planetary vorticity since  $f$  is a constant. In this case there is no induced relative vorticity anomaly so there is no coherent movement of the perturbation. We thus see the central role of  $\beta \neq 0$  for Rossby waves. We also see that the sign of the Coriolis parameter is not relevant; it is only  $\beta > 0$  that determines the wave motion.

## 33.7 Exercises

### EXERCISE 33.1: INTEGRAL PROPERTIES OF THE INVISCID 2D NON-DIVERGENT FLOW

In this exercise, we establish some global conservation properties for inviscid two-dimensional non-divergent flow on a  $\beta$ -plane. Assume the geometry is a flat plane defined over a static region  $\mathcal{S}$ . The region can either be infinite, in which case all fields decay to zero at infinity, or a finite domain surrounded by static material boundaries. It could also be doubly periodic. In any case, there are no boundary fluxes of matter so that the fluid domain is material. Many of the properties derived here are discussed in Section 3.1 of [McWilliams \(2006\)](#).

- (a) Show that the domain integrated kinetic energy per mass remains constant in time

$$\mathcal{K} = \frac{1}{2} \int_{\mathcal{S}} \mathbf{u} \cdot \mathbf{u} \, d\mathcal{S}, \quad (33.93)$$

where the horizontal integral extends over the full fluid domain  $\mathcal{S}$ .

- (b) Why is the mechanical energy budget only associated with kinetic energy? What about the gravitational potential energy?
- (c) Show that the domain integrated relative vorticity (equal also to the relative circulation) is constant in time

$$\mathcal{C} = \int_{\mathcal{S}} \zeta \, d\mathcal{S}. \quad (33.94)$$

- (d) Show that the domain integrated enstrophy is constant in time for  $f$ -plane motion ( $\beta = 0$ )

$$Z^{(\zeta)} = \int_{\mathcal{S}} \zeta^2 \, d\mathcal{S}. \quad (33.95)$$

- (e) Show that the domain integrated potential enstrophy is constant in time even with  $\beta \neq 0$

$$Z^{(q)} = \int_{\mathcal{S}} q^2 \, d\mathcal{S}. \quad (33.96)$$

**EXERCISE 33.2: ALTERNATIVE EXPRESSION FOR THE GLOBALLY INTEGRATED KINETIC ENERGY**  
 For a domain where we can ignore boundary contributions, such as assumed for Exercise 33.1, show that the globally integrated kinetic energy per mass can be written as minus the integrated product of the streamfunction and the vorticity

$$\mathcal{K} = \frac{1}{2} \int_{\mathcal{S}} \mathbf{u} \cdot \mathbf{u} \, d\mathcal{S} = -\frac{1}{2} \int_{\mathcal{S}} \psi \zeta \, d\mathcal{S}, \quad (33.97)$$

where  $\mathbf{u} = \hat{\mathbf{z}} \times \nabla \psi$  is the horizontally non-divergent velocity,  $\psi$  is the streamfunction, and  $\zeta = \nabla^2 \psi$  is the vorticity.

**EXERCISE 33.3: CIRCULATION IN A 2D BAROTROPIC FLOW**

Consider a non-divergent barotropic flow on a  $\beta$ -plane in the presence of a biharmonic friction operator, where the governing vorticity equation is

$$\frac{\partial \zeta}{\partial t} + J(\psi, \zeta + \beta y) = -\nu \nabla^4 \zeta, \quad (33.98)$$

with  $\nu > 0$  a constant biharmonic viscosity with dimensions of  $L^4 T^{-1}$ . Show that the circulation around a fixed material area,  $\mathcal{S}$ , in the fluid evolves according to

$$\frac{d\mathcal{C}}{dt} = - \oint_{\partial\mathcal{S}} \left[ \psi \frac{\partial q}{\partial s} + \nu \frac{\partial(\nabla^2 \zeta)}{\partial n} \right] ds, \quad (33.99)$$

where  $s$  is the arc-length along the boundary of the region and  $n$  is a coordinate normal to the boundary.

**EXERCISE 33.4: DYNAMICS OF VORTICITY GRADIENTS**

For many purposes it is of interest to develop equations describing the evolution of scalar gradients. We developed a general expression in Exercise 12.2. Here, we derive a similar equation for the gradient of relative vorticity in a non-divergent barotropic flow. For this purpose, consider the inviscid barotropic vorticity equation on an  $f$ -plane

$$\frac{\partial \zeta}{\partial t} + J(\psi, \zeta) = 0. \quad (33.100)$$

- (a) Show that the material evolution of the vorticity gradient is given by

$$\frac{D(\nabla \zeta)}{Dt} = -J(\nabla \psi, \zeta). \quad (33.101)$$

- (b) Show that the material evolution of the squared vorticity gradient is given by

$$\frac{D|\nabla \zeta|^2}{Dt} = 2 J(\zeta, \nabla \psi) \cdot \nabla \zeta. \quad (33.102)$$

**EXERCISE 33.5: ANGULAR MOMENTUM FOR BAROTROPIC FLOW IN A BASIN**

The exercise derives some equations presented in [Holloway and Rhines \(1991\)](#), who offer a specialized example of the shallow water angular momentum discussed in Section 31.7.

As in Section 31.7.1, the relative angular momentum for a region of fluid is given by

$$\mathbf{L} = \int d\mathcal{S} \int (\mathbf{x} \times \mathbf{v}) \rho dz, \quad (33.103)$$

where  $\mathbf{x}$  is the position vector and the relative angular momentum is that due to the motion of

the fluid with respect to the solid body. For a barotropic fluid of constant density and constant thickness, and correspondingly a zero vertical velocity, the relative angular momentum reduces to

$$\mathbf{L} = \rho H \int_{\mathcal{S}} (\mathbf{x} \times \mathbf{u}) d\mathcal{S}, \quad (33.104)$$

with  $\mathbf{u}$  the horizontal velocity and  $\mathcal{S}$  the horizontal region. For barotropic motion on a tangent plane we are interested in the vertical component of the relative angular momentum

$$L^z = \rho H \int_{\mathcal{S}} \hat{\mathbf{z}} \cdot (\mathbf{x} \times \mathbf{u}) d\mathcal{S}. \quad (33.105)$$

Show for a simply connected and bounded region,  $L^z$  can be written

$$L^z = 2\rho H \int_{\mathcal{S}} (\psi_b - \psi) d\mathcal{S} \quad (33.106)$$

where  $\psi$  is the streamfunction satisfying  $\mathbf{u} = \hat{\mathbf{z}} \times \nabla \psi$ , and  $\psi_b$  is the value of the streamfunction evaluated on the region boundary. Hint: note that  $\nabla \cdot \mathbf{x} = 2$  for a horizontal position vector. Also recall from Section 16.4.2 that the streamfunction equals to a spatial constant when evaluated along the domain boundary.

#### EXERCISE 33.6: STEADY AXIALLY SYMMETRIC FLOW

Consider a two-dimensional non-divergent velocity

$$\mathbf{v} = \hat{\mathbf{z}} \times \nabla \psi. \quad (33.107)$$

Assume the streamfunction is static and depends only on the radial distance from an arbitrary origin,

$$\psi = \psi(r), \quad (33.108)$$

where  $r = \sqrt{x^2 + y^2}$ , and assume the velocity is a solution to the steady inviscid non-divergent barotropic dynamics on an  $f$ -plane.

- (a) Show that the velocity only has an angular component

$$\mathbf{v} = v^\varphi \hat{\varphi}, \quad (33.109)$$

where  $\hat{\varphi}$  is the angular unit vector oriented counter-clockwise from the  $\hat{\mathbf{x}}$  axis.<sup>7</sup> Express  $v^\varphi$  in terms of the streamfunction  $\psi$ . Hint: see Figure 8.2 and Section 8.3 for a reminder of polar coordinates.

- (b) Write the relative vorticity in terms of the streamfunction using polar coordinates.

- (c) Consider the circulation

$$\mathcal{C} = \oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{r}, \quad (33.110)$$

where  $\mathcal{S}$  is a circular region in the  $x$ - $y$  plane centered at  $r = 0$ . Express the circulation in terms of  $v^\varphi$  and the radius of the circle.

- (d) Write the pressure gradient acceleration in terms of  $v^\varphi$ ,  $f$ , and  $r$ . Hint: remember that  $\hat{\varphi}$  is a function of the polar angle  $\varphi$ .

<sup>7</sup>The azimuthal angular coordinate,  $\varphi$ , that appears in  $\mathbf{v} = v^\varphi \hat{\varphi}$ , is not the same as the density normalized pressure,  $\varphi = p/\rho$ , defined by equation (33.2) and used throughout this chapter.

- (e) Interpret the steady balance of accelerations in terms of the balanced dynamics in Chapter 26.
- (f) Why is this axial symmetric solution only valid for an  $f$ -plane? Hint: show that if  $\beta \neq 0$  that there is an inconsistency in the velocity equation.

**EXERCISE 33.7: GALILEAN TRANSFORMATION OF PV ADVECTION AND THE APV METHOD**

In Section 12.6 we established the invariance of the material time derivative operator under a Galilean transformation

$$\bar{\mathbf{x}} = \mathbf{x} + \mathbf{U} t \quad \text{and} \quad \bar{\mathbf{u}} = \mathbf{u} + \mathbf{U}, \quad (33.111)$$

where  $\mathbf{U}$  is a constant. Here we study the Galilean transformation properties of the non-divergent barotropic model on a  $\beta$ -plane.

- (a) Determine the Galilean transformation properties of the potential vorticity equation (33.31)

$$\frac{\partial q}{\partial t} + \mathbf{u} \cdot \nabla q = \frac{\partial q}{\partial t} + J(\psi, q) = 0, \quad (33.112)$$

where  $q = \zeta + f$ ,  $\hat{\mathbf{z}} \times \psi = \mathbf{u}$ , and  $J$  is the Jacobian operator.

- (b) Determine the Galilean transformation properties of the relative vorticity equation (33.28)

$$\frac{\partial \zeta}{\partial t} + \mathbf{u} \cdot \nabla \cdot \zeta = -\beta v. \quad (33.113)$$

Discuss why there is Galilean invariance *only* for zonal Galilean boosts,  $\mathbf{U} = \hat{\mathbf{x}} U$ .

- (c) An Euler forward time stepping scheme for the PV equation leads to

$$q^{n+1} = q^n - \Delta t \mathbf{u}^n \cdot \nabla q^n, \quad (33.114)$$

where  $\Delta t$  is the discrete time step and the integer  $n$  represents the discrete time label. Inspired by this time discrete expression, [Sadourny and Basdevant \(1985\)](#) proposed the *anticipated potential vorticity* (APV) method for parameterizing subgrid scale processes. The simplest form of APV is given by

$$\frac{\partial q}{\partial t} = -\mathbf{u} \cdot \nabla [q - \tau \mathbf{u} \cdot \nabla q] = -J[\psi, q - \tau J(\psi, q)], \quad (33.115)$$

with  $\tau$  a constant time scale. From the time discrete expression (33.114), we see that the APV method makes use of an estimate for the future value of PV in computing the advection operator, thus motivating the term “anticipated” in the method’s name.

Show that  $\tau \neq 0$  breaks Galilean invariance for the equation (33.115). Provide a discussion of why invariance is broken. Hint: [Vallis and Hua \(1988\)](#) offer a technical reason for why Galilean invariance is broken, making use of the streamfunction and Jacobian form. You do not necessarily need to follow their approach. Rather, it is sufficient to merely note how velocity appears in the APV operator.

**EXERCISE 33.8: ELEMENTS OF THE FOFONOFF GYRE**

A Fofonoff gyre is an unforced inviscid solution in a flat bottom bounded domain with a rigid lid. For a single layer of homogeneous fluid with constant thickness, the absolute vorticity is materially invariant,  $D(\zeta + f)/Dt = 0$ . An explicit solution is derived in Section 19.5.3 of [Vallis \(2017\)](#) for quasi-geostrophic flow using the method of matched asymptotics. We depict elements of a double

Fofonoff gyre in Figure 33.7. Provide a narrative for this flow based on material conservation of absolute vorticity. In particular, discuss how the flow enters and leaves the side boundaries and conversely how it leaves and enters the interior region. We are not concerned with how this flow is established. Instead, assume the flow exists and discuss how its existence is consistent with  $D(\zeta + f)/Dt = 0$ . Hint: recall our discussion of Figure 33.3.

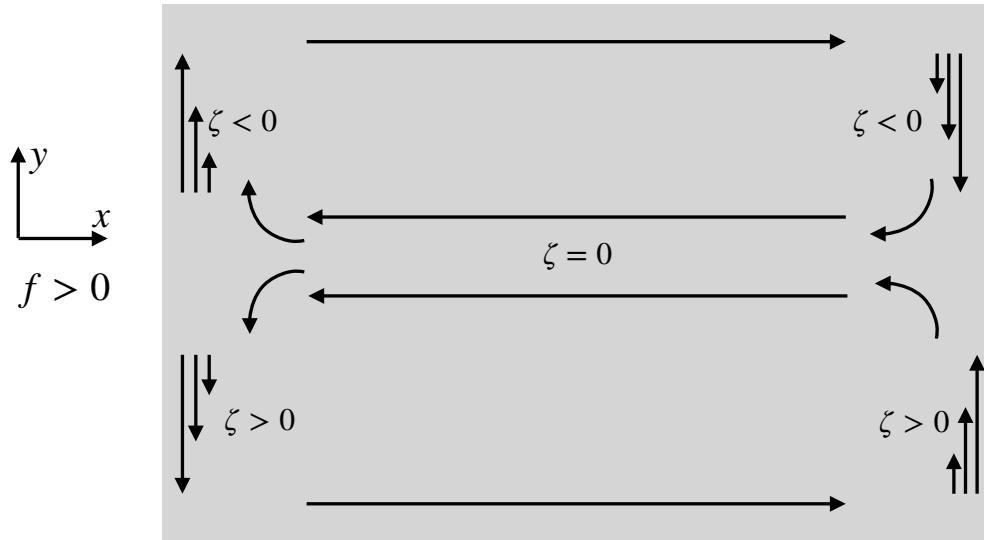


FIGURE 33.7: A Fofonoff gyre is an unforced inviscid flow in a bounded domain where  $D(\zeta + f)/Dt = 0$ . We here depict elements of this double-gyre flow in the northern hemisphere as part of Exercise 33.8.

#### EXERCISE 33.9: PRESSURE EQUATION WITH $w \neq 0$

Equation (33.51) or equation (33.54) provide equivalent expressions for the pressure Poisson equation with  $\nabla \eta = 0$  and, correspondingly, with  $w = 0$ . However, in Section 33.1.3 we considered the possibility of  $\nabla \eta = \nabla \eta_b$ , thus providing a solution with  $w \neq 0$ . In this case, derive the Poisson equation for pressure as decomposed according to  $\varphi = g \eta + \varphi'$ .



# Chapter 34

## Shallow water vorticity and potential vorticity

In this chapter we study vorticity and potential vorticity within the shallow water system. We start by deriving the evolution equation for vorticity by taking the curl of the momentum equation. Combining vorticity evolution with mass continuity then renders the evolution equation for potential vorticity. Potential vorticity is a material invariant for inviscid shallow water motion, thus providing a mechanical constraint on the fluid flow. After developing the basic concepts and equations, we consider a variety of flow regimes and case studies, mostly with an ocean focus, where the study of vorticity, potential vorticity, and circulation enhances our understanding of geophysical fluid mechanics.

### CHAPTER GUIDE

The shallow water fluid offers a fruitful conceptual model to introduce the dynamics of vorticity and potential vorticity while requiring a relatively modest level of mathematical details. Even so, we require vector calculus identities for Cartesian coordinates as detailed in Chapter 2. We also require an understanding of shallow water mechanics from Chapters 30 and 31, as well as the vorticity kinematics introduced in Chapter 32. The concepts and methods developed in this chapter are fundamental to the remaining chapters in this part of the book.

34.1	Vector invariant velocity equation . . . . .	826
34.1.1	Basic manipulations . . . . .	826
34.1.2	Dynamical pressure and the Magnus acceleration . . . . .	827
34.2	Shallow water vorticity equation . . . . .	828
34.2.1	Vorticity equation for a single layer . . . . .	828
34.2.2	Vorticity equation for $N$ -layers . . . . .	829
34.2.3	Vorticity flux divergence and curl of nonlinear advection . . . . .	829
34.3	Potential vorticity for a solid-body rotating cylinder . . . . .	830
34.3.1	Mass conservation . . . . .	830
34.3.2	Angular momentum conservation . . . . .	830
34.3.3	Potential vorticity conservation . . . . .	831
34.3.4	Connecting angular momentum and vorticity . . . . .	832
34.3.5	Comments and further study . . . . .	832
34.4	Shallow water potential vorticity . . . . .	832
34.4.1	Mass conservation plus the vorticity equation . . . . .	832
34.4.2	Motivating the name . . . . .	833
34.4.3	Mass conservation + Kelvin's circulation theorem . . . . .	834

34.4.4 A fluid column with constant $f \neq 0$ . . . . .	835
34.4.5 Material conservation of an arbitrary function of PV . . . . .	836
34.4.6 $N$ -layer potential vorticity . . . . .	837
34.4.7 Further study . . . . .	837
34.5 Potential vorticity with non-conservative processes . . . . .	837
34.5.1 Material time evolution of PV . . . . .	837
34.5.2 The potential vorticity flux . . . . .	838
34.6 Example implications of PV material invariance . . . . .	839
34.6.1 Topographic beta effect . . . . .	839
34.6.2 Planetary geostrophic PV . . . . .	840
34.6.3 Spin up of converging flow . . . . .	840
34.6.4 Further study . . . . .	841
34.7 Geostrophic adjustment . . . . .	841
34.7.1 Potential vorticity inversion . . . . .	842
34.7.2 Posing the initial value problem . . . . .	843
34.7.3 Adjustment in the absence of rotation . . . . .	844
34.7.4 Adjustment with rotation . . . . .	844
34.7.5 Comments . . . . .	846
34.8 Circulation with non-conservative processes . . . . .	846
34.8.1 Circulation around a closed streamline in steady flow . . . . .	848
34.8.2 Circulation from wind stress and Rayleigh drag . . . . .	848
34.9 Western intensification of ocean gyres . . . . .	849
34.9.1 Steady and large-scale vorticity balance . . . . .	849
34.9.2 Planetary geostrophic flow and the Sverdrup balance . . . . .	849
34.9.3 Sverdrup flow in a closed domain with anti-cyclonic wind stress . . . . .	850
34.9.4 Western intensification and the role of beta . . . . .	850
34.9.5 A role for topographic form stress . . . . .	852
34.9.6 Comments and further study . . . . .	854
34.10 Column vorticity . . . . .	854
34.10.1 Formulating the column vorticity equation . . . . .	855
34.10.2 Summary of the column vorticity equation . . . . .	856
34.10.3 Steady linear column vorticity balance and the island rule . . . . .	857
34.10.4 Further study . . . . .	858
34.11 Exercises . . . . .	859

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## 34.1 Vector invariant velocity equation

Prior to deriving the vorticity equation, we massage the momentum equation into its vector invariant form. Doing so exposes the dynamic pressure effects from kinetic energy per mass as well as the Magnus acceleration, both of which were encountered for the continuously stratified fluid in Section 17.2.3.

### 34.1.1 Basic manipulations

To start, introduce vorticity for the full velocity field as well as that just for the horizontal flow

$$\boldsymbol{\omega} = \nabla \times \mathbf{v} \tag{34.1a}$$

$$\boldsymbol{\omega}^* = \nabla \times \mathbf{u} \equiv \zeta \hat{\mathbf{z}}, \tag{34.1b}$$

where

$$\zeta = \hat{\mathbf{z}} \cdot \boldsymbol{\omega} = \hat{\mathbf{z}} \cdot \boldsymbol{\omega}^* = \partial_x v - \partial_y u \tag{34.2}$$

is the vertical component to the relative vorticity. The vector identity (see Section 2.3.4)

$$(\mathbf{u} \cdot \nabla) \mathbf{u} = (1/2) \nabla(\mathbf{u} \cdot \mathbf{u}) - \mathbf{u} \times (\nabla \times \mathbf{u}) = (1/2) \nabla(\mathbf{u} \cdot \mathbf{u}) + \boldsymbol{\omega}^* \times \mathbf{u} \quad (34.3)$$

brings the inviscid shallow water momentum equation (30.6)

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} + f \hat{\mathbf{z}} \times \mathbf{u} = -g \nabla \eta \quad (34.4)$$

into its *vector invariant* form

$$\frac{\partial \mathbf{u}}{\partial t} + (f + \zeta) \hat{\mathbf{z}} \times \mathbf{u} = -\nabla(g \eta + \mathbf{u} \cdot \mathbf{u}/2). \quad (34.5)$$

In the following we sometimes make use of the vertical component to the absolute vorticity

$$\boldsymbol{\omega}_a^* = (\zeta + f) \hat{\mathbf{z}} = \zeta_a \hat{\mathbf{z}} \quad (34.6)$$

which is the sum of the relative vorticity of the horizontal flow,  $\boldsymbol{\omega}^* = \zeta \hat{\mathbf{z}}$ , plus the solid-body vorticity,  $f \hat{\mathbf{z}}$ , due to motion of the rotating reference frame (recall Section 32.5.1).

### 34.1.2 Dynamical pressure and the Magnus acceleration

As for the discussion of vector invariant velocity equation in Section 17.2.2, the velocity equation (34.5) exposes two physical features that lend insight into the motion of a shallow water fluid column.

#### Dynamical pressure from kinetic energy per mass

The kinetic energy per mass,  $\mathbf{u} \cdot \mathbf{u}/2$ , adds a *dynamical pressure* to the mechanical pressure associated with the free surface undulations. Gradients in the kinetic energy thus drive accelerations towards regions of smaller kinetic energy; i.e., down the kinetic energy gradient.

#### Magnus acceleration

As discussed in Sections 17.2.2 and 26.2.6, the Magnus acceleration is a body acceleration defined by the nonlinear term

$$\mathbf{A}_{\text{magnus}} = -\boldsymbol{\omega}^* \times \mathbf{u} = \zeta (\mathbf{u} \times \hat{\mathbf{z}}), \quad (34.7)$$

appearing in the vector-invariant velocity equation (34.5). Hence, there is a non-zero Magnus acceleration when a shallow water fluid column spins while it moves, with this acceleration acting to deflect the spinning column perpendicular to its trajectory. As for the example in Figure 17.1, consider a shallow water fluid column moving zonally, in which case the Magnus acceleration is

$$\mathbf{A}_{\text{magnus}} = u \zeta (\hat{\mathbf{x}} \times \hat{\mathbf{z}}) = -\hat{\mathbf{y}} u \zeta. \quad (34.8)$$

With a positive relative vorticity,  $\zeta > 0$ , the Magnus acceleration is directed to the right of the motion, which is in the same direction as the Coriolis acceleration in the northern hemisphere. For large-scale geophysical flows, the Magnus acceleration is sub-dominant to the Coriolis acceleration. However, the Magnus acceleration is a crucial facet of large (order unity or larger) Rossby number motions in which relative vorticity is sizable.

## 34.2 Shallow water vorticity equation

In this section we formulate the vorticity equation for the shallow water fluid, starting with a single layer and then extending to multiple layers.

### 34.2.1 Vorticity equation for a single layer

We make use of the vector identity from Section 2.3.4 to express the curl of the Magnus acceleration plus Coriolis acceleration in the form

$$\nabla \times (\boldsymbol{\omega}_a^* \times \mathbf{u}) = \boldsymbol{\omega}_a^* (\nabla \cdot \mathbf{u}) + (\mathbf{u} \cdot \nabla) \boldsymbol{\omega}_a^* - \mathbf{u} (\nabla \cdot \boldsymbol{\omega}_a^*) - (\boldsymbol{\omega}_a^* \cdot \nabla) \mathbf{u} \quad (34.9a)$$

$$= \boldsymbol{\omega}_a^* (\nabla \cdot \mathbf{u}) + (\mathbf{u} \cdot \nabla) \boldsymbol{\omega}_a^*, \quad (34.9b)$$

so that

$$\hat{z} \cdot [\nabla \times (\boldsymbol{\omega}_a^* \times \mathbf{u})] = \nabla \cdot (\mathbf{u} \zeta_a) \quad (34.10)$$

Equation (34.9b) required setting

$$\nabla \cdot \boldsymbol{\omega}_a^* = \nabla \cdot \boldsymbol{\omega}^* + \nabla \cdot (f \hat{z}) = 0, \quad (34.11)$$

which follows since this expression involves the divergence of a curl (first right hand side term) and since  $f$  has no  $z$  dependence. We furthermore set

$$(\boldsymbol{\omega}_a^* \cdot \nabla) \mathbf{u} = |\boldsymbol{\omega}_a^*| \partial_z \mathbf{u} = 0, \quad (34.12)$$

which follows since the horizontal velocity in a shallow water fluid is depth independent within a layer (see Section 30.2). Applying the operator  $\hat{z} \cdot (\nabla \times)$  onto the vector-invariant momentum equation (34.5) annihilates the gradient of pressure and kinetic energy, with the identity (34.10) leading to the Eulerian flux-form evolution equation for absolute vorticity

$$\frac{\partial \zeta_a}{\partial t} + \nabla \cdot (\mathbf{u} \zeta_a) = 0. \quad (34.13)$$

This equation says that the vertical component to the absolute vorticity,  $\zeta_a$ , at a point in the inviscid shallow water fluid changes according to the horizontal convergence of vorticity advected to that point

$$\frac{\partial \zeta_a}{\partial t} = -\nabla \cdot (\mathbf{u} \zeta_a). \quad (34.14)$$

We can write the vorticity equation (34.13) in the material form

$$\frac{D \zeta_a}{Dt} = -\zeta_a \nabla \cdot \mathbf{u}, \quad (34.15)$$

where the material time derivative for the shallow water fluid is determined just by the horizontal flow

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla = \frac{\partial}{\partial t} + u \partial_x + v \partial_y. \quad (34.16)$$

The material evolution equation (34.15) means that the absolute vorticity of a shallow water fluid particle, moving with the horizontal flow, changes according to the horizontal convergence of the fluid flow as multiplied by the absolute vorticity.

### 34.2.2 Vorticity equation for $N$ -layers

The previous results for a single layer are readily extended to  $N$ -layers. For that purpose recall the velocity for layer-k evolves according to equation (30.77)

$$[\partial_t + (\mathbf{u}_k \cdot \nabla)] \mathbf{u}_k + f \hat{\mathbf{z}} \times \mathbf{u}_k = -\nabla p_k / \rho_1, \quad (34.17)$$

where there is no implied summation on the layer index k, and where layer pressure,  $p_k$ , is given by equation (30.73). Use of the vector identity (34.3) brings the layer velocity equation (34.17) to the vector invariant form

$$\partial_t \mathbf{u}_k + (f + \zeta_k) \hat{\mathbf{z}} \times \mathbf{u}_k = -\nabla(p_k / \rho_1 + \mathbf{u}_k \cdot \mathbf{u}_k / 2), \quad (34.18)$$

where  $\zeta_k = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u}_k)$  is the vertical component to the layer-k relative vorticity. Taking the curl and making use of the mathematical identities used for single layer in Section 34.2.1 renders the vorticity equation for layer-k

$$\frac{\partial \zeta_{ak}}{\partial t} + \nabla \cdot (\mathbf{u}_k \zeta_{ak}) = 0 \iff \frac{D_k \zeta_{ak}}{Dt} = -\zeta_{ak} \nabla \cdot \mathbf{u}_k \quad (34.19)$$

where

$$\zeta_{ak} = f + \zeta_k \quad (34.20)$$

is the vertical component to the absolute vorticity of layer-k. Hence, the vorticity equation for an arbitrary layer in a stacked shallow water model is isomorphic to that for a single shallow water layer.

### 34.2.3 Vorticity flux divergence and curl of nonlinear advection

We revisit the manipulations from Section 34.2.1 to explicitly identify a connection between the nonlinear terms in the vorticity equation. Start by writing the velocity equation in the advective form and the vector invariant form

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} + f \hat{\mathbf{z}} \times \mathbf{u} = -g \nabla \eta \quad (34.21a)$$

$$\frac{\partial \mathbf{u}}{\partial t} + (f + \zeta) \hat{\mathbf{z}} \times \mathbf{u} = -\nabla(g \eta + \mathbf{u} \cdot \mathbf{u} / 2). \quad (34.21b)$$

Taking their curl yields two expressions of the vorticity equation

$$\frac{\partial \boldsymbol{\omega}^*}{\partial t} + \nabla \times [(\mathbf{u} \cdot \nabla) \mathbf{u}] + \nabla \times [f \hat{\mathbf{z}} \times \mathbf{u}] = 0 \quad (34.22a)$$

$$\frac{\partial \boldsymbol{\omega}^*}{\partial t} + \nabla \times [(f + \zeta) \hat{\mathbf{z}} \times \mathbf{u}] = 0, \quad (34.22b)$$

whose equality leads to

$$\nabla \times [(\mathbf{u} \cdot \nabla) \mathbf{u} - \zeta \hat{\mathbf{z}} \times \mathbf{u}] = 0. \quad (34.23)$$

Making use of the identity

$$\hat{\mathbf{z}} \cdot [\nabla \times (\zeta \hat{\mathbf{z}} \times \mathbf{u})] = \nabla \cdot (\mathbf{u} \zeta) \quad (34.24)$$

renders the relation

$$\hat{\mathbf{z}} \cdot \nabla \times [(\mathbf{u} \cdot \nabla) \mathbf{u}] = \nabla \cdot (\mathbf{u} \zeta). \quad (34.25)$$

We thus see that the divergence of the advective vorticity flux (right hand side) equals to the curl of the nonlinear advection (left hand side). This identity holds for each layer in an  $N$ -layer shallow water model.

### 34.3 Potential vorticity for a solid-body rotating cylinder

To introduce potential vorticity, consider a fluid cylinder of constant mass  $M$ , constant density  $\rho$ , variable radius  $R$ , and variable height  $h$ , and assume the cylinder exhibits solid-body rotation about its central axis. This analysis offers a useful conceptual picture for a rotating column of a shallow water layer, in which time derivatives in the following are interpreted as material derivatives. It also lends intuition for the motion of spinning fluids constrained by mass and angular momentum conservation.

#### 34.3.1 Mass conservation

With a constant density, mass conservation for the cylinder means that its volume is fixed. Hence, mass conservation constrains the relative changes to the radius and height of the cylinder. A materially constant cylinder mass

$$M = \pi R^2 h \rho \quad (34.26)$$

implies

$$\frac{2}{R} \frac{DR}{Dt} = -\frac{1}{h} \frac{Dh}{Dt}. \quad (34.27)$$

That is, mass conservation means that the relative height decreases as twice the relative radius increase. That is, if the cylinder is squashed ( $h$  decreases) it thickens ( $R$  increases) and conversely the cylinder thins ( $R$  decreases) as it extends ( $h$  increases).

#### 34.3.2 Angular momentum conservation

A second constraint arises from angular momentum conservation. Since the cylinder is rotating as a solid-body, angular momentum is straightforward to compute. For simplicity, choose the center of mass coordinate axes through the center of the cylinder, with the  $z$ -axis along the central line of the cylinder and with  $z = 0$  at the cylinder mid-point. The angular rotation vector is thus given by

$$\boldsymbol{\Omega} = \Omega \hat{z}. \quad (34.28)$$

With this axis orientation, the solid-body rotation occurs about the center of mass so that the angular momentum of the center of mass vanishes. The moment of inertia tensor for a cylinder with this axis orientation is given by (e.g., [Marion and Thornton, 1988](#))

$$I_{mn} = \delta_{mn} \frac{MR^2}{2}. \quad (34.29)$$

The moment of inertia is a measure of the rotational inertia of the cylinder, and is seen to be directly related to the cylinder mass (assumed fixed here) and radius (can change). Note that the moment of inertia is not a function of the cylinder height. The angular momentum for the cylinder is thus given by

$$\mathbf{L} = \frac{MR^2}{2} \boldsymbol{\Omega} \hat{z}. \quad (34.30)$$

The familiar *ice skater* example occurs when the cylinder radius changes and thus changes the moment of inertia (e.g., the ice skater's arms are brought in toward the central axis of the

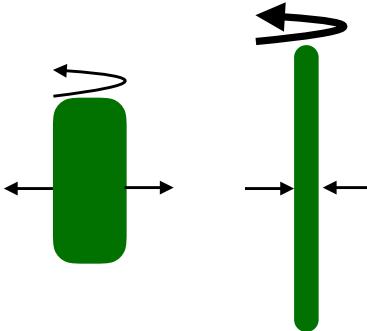


FIGURE 34.1: Illustrating the conservation of angular momentum for a spinning cylinder of constant mass undergoing solid-body rotation around its central axis. The moment of inertia (relative to the central axis) for the left cylinder is larger since more of its mass is distributed away from the central axis than in the right configuration. If the initial spin for the left cylinder is counterclockwise, then for the two configurations to have identical angular momentum means that the right cylinder spins more rapidly since its moment of inertia is smaller. This example exemplifies the familiar ice skater experience, whereby the skater's spin rate increases when bringing arms (mass) inward towards the central axis of the body (depicted by the inward arrows on the right panel), and the skater slows when extending the arms outward (depicted by the outward arrows on the left panel).

body or out away from the body). Maintaining constant angular momentum and constant mass means that the angular velocity,  $\Omega$ , increases in magnitude (rotates faster) when the cylinder radius decreases, and vice versa. Explicitly for the cylinder we have  $d\mathbf{L}/dt = 0$  and  $dM/dt = 0$  thus rendering

$$\frac{2}{R} \frac{DR}{Dt} = -\frac{1}{\Omega} \frac{D\Omega}{Dt}. \quad (34.31)$$

We see that reducing the moment of inertia for a constant mass body by bringing its mass distribution towards the central axis (converging mass) leads, through angular momentum conservation, to an increase in rotation speed. The opposite occurs when mass diverges from a region, thus reducing the rotation speed.

Although the angular momentum constraint means that the spin rate changes when changing the moment of inertia, it does not impose a preferred direction. For example, no matter what direction a skater is rotating, decreasing the moment of inertia increases the spin rate in that particular direction. Yet when placing the spinning column on a rotating planet, the planetary rotation breaks the symmetry and thus prescribes the direction for the spin changes. The reason is that planetary rotation contributes to the spin of the column, even if the column has no spin relative to the rotating planetary reference frame. We encounter this additional part of the story in Section 34.4.

### 34.3.3 Potential vorticity conservation

Combining angular momentum conservation (34.31) with mass conservation (34.27) leads to the conservation law

$$\frac{D}{Dt} \frac{\Omega}{h} = 0. \quad (34.32)$$

Equation (34.32) is a statement of potential vorticity conservation for the material fluid column, with potential vorticity given by

$$Q \equiv \frac{\Omega}{h}. \quad (34.33)$$

For example, if the column thickens then the rotational velocity increases to maintain  $Q = \Omega/h$  constant. Equivalently, if the column cross-sectional area decreases, the column thickness increases

according to volume conservation, which in turn results in an increase in the spin according to angular momentum conservation.

### 34.3.4 Connecting angular momentum and vorticity

When allowing the fluid to exhibit motion that is more general than a solid-body, then the angular rotation rate appearing in the potential vorticity (34.33) is generalized to the absolute vorticity, and we will find this generalization in Section 34.4. Furthermore, as shown in Section 32.5, the vorticity for solid body motion equals to twice the rotation rate,  $2\Omega$ . Hence, the numerator for the potential vorticity of the solid-body rotating cylinder equals to one-half the vorticity. In Section 32.7 we connect angular momentum to vorticity and the rate of strain for arbitrary fluid motion.

### 34.3.5 Comments and further study

The discussion in this section is motivated by Section 2.4 of *Salmon* (1998). The solid-body rotating cylinder succinctly identifies the two mechanical properties contributing to the potential vorticity conservation law (34.32): a kinematic property (mass conservation) and a dynamic property (angular momentum conservation). For the solid-body rotating cylinder, the implications of PV conservation are well gleaned from the separate mass and angular momentum conservation principles. Hence, PV conservation lends little novel insight for the cylinder. However, PV conservation is of fundamental use for studies of rotating and stratified fluids.

We also note that an important element missing from this discussion is the *beta effect*, which accounts for the changes in planetary vorticity when moving on a rotating spherical planet. We encounter this effect in the following sections.

## 34.4 Shallow water potential vorticity

We now consider the potential vorticity for a single layer of shallow water fluid. The result is directly analogous to that derived for the solid-body rotating cylinder in Section 34.3. However, the derivation here makes use of fluid mechanical equations rather than those from rigid body mechanics. We present two derivations: one based on manipulations of the mass and momentum equations, and one based on the small aspect ratio limit of Kelvin's circulation theorem, with Kelvin's theorem more thoroughly studied in Chapter 35. Figure 34.2 summarizes key elements leading to PV conservation for a shallow water fluid layer. Namely, as shown in this section, shallow water PV conservation arises from combining the kinematic constraint of mass conservation (material conservation of  $h A$ ) with either the vorticity equation or Kelvin's circulation theorem for a small aspect ratio fluid.

### 34.4.1 Mass conservation plus the vorticity equation

To derive the potential vorticity equation, we here make use of the vorticity equation (34.15) and combine it with mass conservation.

#### *Shallow water vorticity and vortex stretching*

Mass conservation in the form of the material thickness equation (30.17) leads to the following expression for the divergence of the horizontal velocity

$$\nabla \cdot \mathbf{u} = -\frac{1}{h} \frac{Dh}{Dt}. \quad (34.34)$$

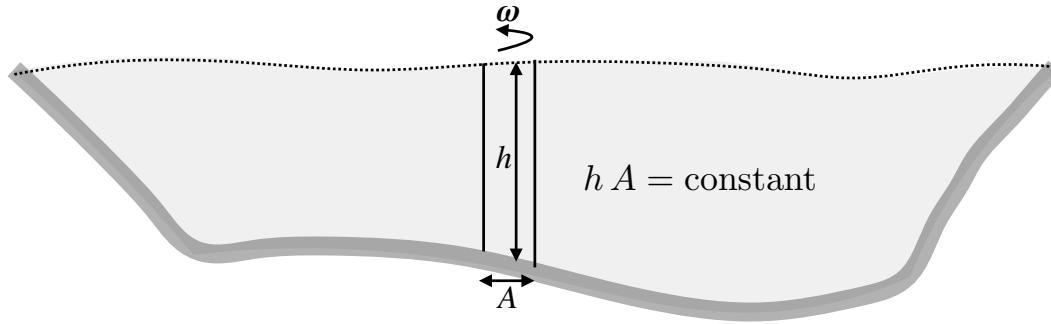


FIGURE 34.2: Illustrating the conservation of PV for a layer of shallow water fluid column. PV conservation results from merging mass conservation (material conservation of the column volume,  $h A$ ), to either the vorticity equation or Kelvin's circulation theorem for a small aspect ratio fluid (material conservation of  $\zeta A$ ).

Making use of this result in the vorticity equation (34.15) allows us to eliminate the horizontal convergence

$$\frac{D\zeta_a}{Dt} = -\zeta_a \nabla \cdot \mathbf{u} = \frac{\zeta_a}{h} \frac{Dh}{Dt}. \quad (34.35)$$

This equation says that material changes in shallow water absolute vorticity arise only from material changes in the layer thickness; i.e., absolute vorticity increases in magnitude if the column stretches and decreases if the column compresses. We refer to this process as *vortex stretching*. We see in Section 35.6.3 that vorticity in more general fluids is affected by vortex stretching as well as *vortex tilting* and torques from baroclinicity. In contrast, equation (34.35) says that the material evolution of absolute vorticity for a shallow water fluid is affected only through vortex stretching. This behavior is a result of the depth independence of the horizontal velocity within a shallow water layer and the associated vertical columnar motion of fluid within the layer.

### Material invariance of PV

Equation (34.35) can be written as an expression of the material invariance of the shallow water potential vorticity

$$\frac{DQ}{Dt} = 0, \quad (34.36)$$

where

$$Q = \frac{\zeta_a}{h} = \frac{\zeta + f}{h} \quad (34.37)$$

is the shallow water potential vorticity. As defined, shallow water potential vorticity is the ratio of absolute vorticity to the thickness of the fluid layer. The material conservation law (34.36) says that this ratio remains constant for the shallow water layer in the absence of irreversible processes. Much of the remainder of this chapter explores the many implications of potential vorticity conservation.

#### 34.4.2 Motivating the name

Material invariance of the shallow water potential vorticity in equation (34.37) is most practically a statement about how the relative vorticity,  $\zeta$ , changes when changing column thickness or latitude. That is, by maintaining  $Q$  fixed,  $\zeta$  must change when either the column thickness,  $h$ , changes or when the column moves meridionally to thus alter the Coriolis parameter,  $f$ . By focusing on relative vorticity we are offered insights into how the fluid motion is constrained and

thus a means to predict changes in that motion. In turn, these changes in  $\zeta$  motivate the name “potential vorticity” as we now see.

Potential vorticity measures the ability for a shallow water fluid column to either spin up or spin down (change its relative vorticity) relative a standard configuration. For example, let the standard configuration be defined by an arbitrary standard thickness,  $h_s$ , at the equator (where  $f = 0$ ). Now move an off-equatorial shallow water fluid column with zero relative vorticity to the equator and stretch/compress the column to the standard thickness. Material invariance of the column’s potential vorticity allows us to deduce the column’s relative vorticity at the equator, given information about the initial column thickness and initial Coriolis parameter (see Figure 34.3). Hence, potential vorticity, as an invariant material property, provides the “potential” for a fluid column to manifest a particular value of the relative vorticity when moved and stretched into a standard configuration. In this manner, the use of “potential” in “potential vorticity” is directly analogous to the use of “potential” in “potential temperature” as described in Section 20.11, or gravitational potential energy as discussed in Section 21.2.

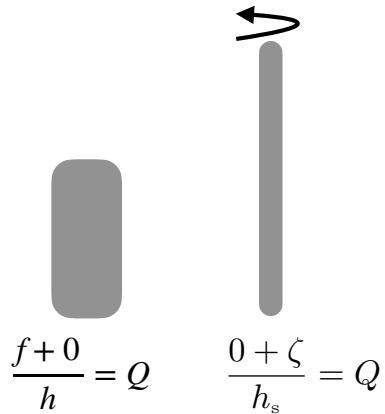


FIGURE 34.3: Left panel: an arbitrary shallow water column with zero relative vorticity and potential vorticity  $Q = f/h$ , with  $f > 0$  assumed for this figure (northern hemisphere). Right panel: the same fluid column moved to the equator (where  $f = 0$ ) and stretched to have the standard thickness,  $h_s > h$ . The relative vorticity of the column at the equator is given by  $\zeta = f(h_s/h)$ , where  $f$  is the Coriolis parameter at the original latitude where  $f > 0$ . Potential vorticity thus provides a means to deduce the relative vorticity that can be realized by moving any particular configuration to a standard location and with a standard thickness. This property motivates the “potential” used in the name.

### 34.4.3 Mass conservation + Kelvin’s circulation theorem

Although we have yet to discuss Kelvin’s theorem (Section 35.3), we here invoke it to illustrate another way to derive shallow water PV conservation. As we will see, this derivation lends itself to direct analog of the rotating cylinder discussed in Section 34.3.

When applied to an infinitesimal circuit in an inviscid and constant density fluid, Kelvin’s theorem says that

$$\frac{D(\boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} \delta \mathcal{S})}{Dt} = 0, \quad (34.38)$$

where  $\boldsymbol{\omega}_a$  is the absolute vorticity

$$\boldsymbol{\omega}_a = \boldsymbol{\omega} + f \hat{\mathbf{z}}, \quad (34.39)$$

$\hat{\mathbf{n}} \delta \mathcal{S}$  is the infinitesimal surface area enclosed by the closed circuit, with  $\hat{\mathbf{n}}$  the outward normal to the surface. Hence, equation (34.38) says that the projection of the absolute vorticity onto the

local normal of an area element, multiplied by that area element, remains materially constant. This identity offers a very strong constraint on the flow.

To make use of equation (34.38) for the shallow water layer, decompose absolute vorticity into

$$\boldsymbol{\omega}_a = \hat{\mathbf{z}}(\zeta + f) + \boldsymbol{\omega}_h, \quad (34.40)$$

where  $\zeta$  is the vertical component to the relative vorticity (equation (34.2)), and

$$\boldsymbol{\omega}_h = \hat{\mathbf{x}} \frac{\partial w}{\partial y} - \hat{\mathbf{y}} \frac{\partial w}{\partial x} \quad (34.41)$$

is the horizontal component to the relative vorticity, making use of the depth independence of the horizontal velocity components for the shallow water fluid ( $\partial u / \partial z = \partial v / \partial z = 0$ ). Inserting the absolute vorticity (34.40) into Kelvin's theorem (34.40) leads to

$$\frac{D}{Dt} [(\zeta + f) \delta A + \boldsymbol{\omega}_h \cdot \hat{\mathbf{n}} \delta \mathcal{S}] = 0, \quad (34.42)$$

where the horizontal area element,  $\delta A$ , is the projection of the surface area element onto the vertical direction

$$\delta A = \hat{\mathbf{z}} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (34.43)$$

Shallow water fluid mechanics arises from considering a constant density fluid layer under the small aspect ratio limit ( $H/L \ll 1$ , with  $H$  the vertical length scale and  $L$  the horizontal length scale). Under this limit, the second term in equation (34.42) is much smaller than the first. Ignoring this small term then leads to

$$\frac{D}{Dt} \left[ \left( \frac{\zeta + f}{h} \right) h \delta A \right] = 0, \quad (34.44)$$

where  $h$  is the layer thickness and  $h \delta A$  is the volume of an infinitesimal fluid column. Given the incompressible nature of the shallow water layer, the column volume is materially constant

$$\frac{D(h \delta A)}{Dt} = 0, \quad (34.45)$$

so that equation (34.44) yields the material invariance of shallow water PV

$$\frac{D}{Dt} \left[ \frac{\zeta + f}{h} \right] = \frac{DQ}{Dt} = 0, \quad (34.46)$$

where  $Q = (\zeta + f)/h$  is the same shallow water potential vorticity derived above in Section 34.4.1.

#### 34.4.4 A fluid column with constant $f \neq 0$

Some of the essential features of shallow water potential vorticity conservation are depicted in Figure 34.4 for the case of a fluid column with constant  $f \neq 0$ . In the left panel, the column thickness increases (column is stretched). Volume conservation means that the column radius decreases. As the material in the column moves radially inward toward the center, it experiences a Coriolis deflection to the right in the northern hemisphere and to the left in the southern. Both of these deflections renders a cyclonic tendency to the relative vorticity, creating a positive relative vorticity tendency in the north and negative relative vorticity tendency in the south.

An equivalent way to understand the cyclonic tendency is to consider the angular momentum

of the fluid column. As the radius of the column decreases so too does its moment of inertia. Angular momentum conservation means that the column picks up a tendency that causes its spin to increase. The direction of this spin increase accords with the background  $f$  of the environment. Returning to the skater analog in Figure 34.1, we consider  $f$  to be the initial spin of the skater so that when the moment of inertia decreases the column picks up a spin in the same direction as  $f$ ; i.e., a cyclonic tendency.<sup>1</sup>

In both hemispheres, the Coriolis deflection, or equivalently angular momentum conservation, creates a cyclonic relative vorticity tendency when the column stretches, thus maintaining  $Q = (f + \zeta)/h$  fixed. Again, the cyclonic relative vorticity adds to the magnitude of the planetary vorticity to ensure that the absolute vorticity magnitude increases in accord with the column thickness increase, thus keeping  $Q = \zeta_a/h$  constant. The converse holds when the column is flattened/squashed, whereby the relative vorticity picks up an anti-cyclonic tendency (negative relative vorticity tendency in the northern hemisphere and positive relative vorticity tendency in the southern). Doing so reduces the magnitude of the absolute vorticity in accord with the reduced column thickness.

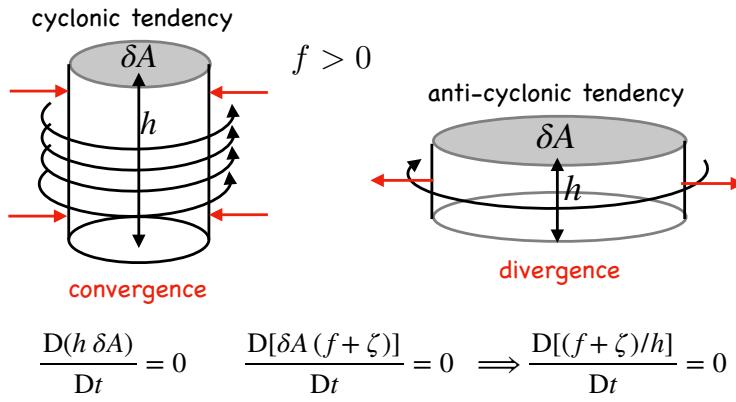


FIGURE 34.4: Material invariance for PV in a shallow water layer results from combining material invariance of the volume of the fluid column with the material invariance of the area weighted absolute vorticity. As the cross-sectional area of the column decreases, as in a converging flow, the thickness of the fluid must increase in order to maintain constant volume. Furthermore, PV invariance can be maintained by changing the fluid spin, as measured by the relative vorticity, or by changing the latitude and thus changing its planetary vorticity (the  $\beta$ -effect discussed in Section 35.7). We here depict the case with  $f > 0$  constant. Flow converging toward the center of the column picks up a Coriolis acceleration that creates a cyclonic tendency in the relative vorticity, just like the spinning cylinder in Figure 34.1. Equivalently, as the radius of the column decreases so too does its moment of inertia so that the column must pick up a cyclonic tendency to conserve angular momentum. Conversely, as the cross-sectional area increases, the diverging flow creates an anti-cyclonic tendency in the relative vorticity.

### 34.4.5 Material conservation of an arbitrary function of PV

The material conservation law for PV, equation (34.36), means that any function,  $F(Q)$  is also materially constant. We see this property through the chain rule

$$\frac{DF}{Dt} = \frac{dF}{dQ} \frac{DQ}{Dt} = 0. \quad (34.47)$$

Since  $F$  is arbitrary, there are an infinite number of material invariants corresponding to distinct functions  $F$ . This result holds for all materially invariant scalar properties of the fluid.

<sup>1</sup>The connection between the Coriolis acceleration and angular momentum conservation was discussed for particle mechanics in Section 10.8.

### 34.4.6 $N$ -layer potential vorticity

The thickness equation (30.70a) and the vorticity equation (34.19) for an  $N$ -layer shallow water model are given by

$$\frac{D_k h_k}{Dt} = -h_k \nabla \cdot \mathbf{u}_k \quad \text{and} \quad \frac{D_k \zeta_{ak}}{Dt} = -\zeta_{ak} \nabla \cdot \mathbf{u}_k, \quad (34.48)$$

where there is no implied summation over the layer index  $k$ . These forms are isomorphic to the single layer equations so that the potential vorticity of layer- $k$  is given by

$$Q_k = \frac{f + \zeta_k}{h_k}, \quad (34.49)$$

and for a perfect fluid this layer potential vorticity is materially constant

$$\frac{D_k Q_k}{Dt} = \frac{\partial Q_k}{\partial t} + \mathbf{u}_k \cdot \nabla Q_k = 0, \quad (34.50)$$

where, again, there is no implied summation over  $k$ .

### 34.4.7 Further study

The shallow water potential vorticity (34.37) was introduced by [Rossby \(1940\)](#) and as such it is sometimes referred to as the *Rossby potential vorticity*. Non-rotating shallow water potential vorticity,  $\zeta/h$ , is illustrated in this [video from Prof. Shapiro at around the 11 minute mark](#). Note that he does not use the term “potential vorticity”, instead invoking mass conservation and angular momentum conservation to describe the motion.

## 34.5 Potential vorticity with non-conservative processes

In this section we consider the role of a non-conservative force per mass,  $\mathbf{F}$ , with this term arising from friction and boundary stresses. Additionally, we allow for the presence of a boundary volume source,  $w^{(\dot{\eta})}$  (as in precipitation minus evaporation), thus changing the volume in the layer. We introduced such processes in Section 30.5, in which case the shallow water equations take on the form

$$\frac{Du}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -g \nabla \eta + \mathbf{F} \quad \text{and} \quad \frac{Dh}{Dt} + h \nabla \cdot \mathbf{u} = w^{(\dot{\eta})}. \quad (34.51)$$

### 34.5.1 Material time evolution of PV

In the presence of friction, the absolute vorticity equation (34.13) takes on the form

$$\frac{\partial \zeta_a}{\partial t} + \nabla \cdot (\mathbf{u} \zeta_a) = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}) \implies \frac{D\zeta_a}{Dt} + \zeta_a \nabla \cdot \mathbf{u} = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}), \quad (34.52)$$

so that vorticity is now affected by the curl of friction. As before, we make use of the thickness equation to replace the horizontal divergence according to

$$\nabla \cdot \mathbf{u} = \frac{1}{h} \left[ -\frac{Dh}{Dt} + w^{(\dot{\eta})} \right]. \quad (34.53)$$

The presence of  $w^{(\dot{\eta})}$  modifies the divergence of the horizontal velocity beyond that for a conservative fluid. We are thus led to the PV equation

$$h \frac{DQ}{Dt} = -Q w^{(\dot{\eta})} + \hat{z} \cdot (\nabla \times \mathbf{F}). \quad (34.54)$$

Hence, with  $w^{(\dot{\eta})} \neq 0$  and/or  $\hat{z} \cdot (\nabla \times \mathbf{F}) \neq 0$ , potential vorticity is no longer materially invariant.

### 34.5.2 The potential vorticity flux

#### *Deriving the Eulerian flux-form equation*

We can convert the potential vorticity equation (34.54) into an Eulerian flux-form conservation equation by making use of the thickness equation

$$h \frac{DQ}{Dt} = h \left[ \frac{\partial Q}{\partial t} + \mathbf{u} \cdot \nabla Q \right] + Q \left[ \frac{\partial h}{\partial t} + \nabla \cdot (h \mathbf{u}) - w^{(\dot{\eta})} \right] = \frac{\partial(hQ)}{\partial t} + \nabla \cdot (h \mathbf{u} Q) - Q w^{(\dot{\eta})}, \quad (34.55)$$

to render

$$\frac{\partial(hQ)}{\partial t} + \nabla \cdot (h \mathbf{u} Q) = \hat{z} \cdot (\nabla \times \mathbf{F}). \quad (34.56)$$

As a final step, make use of the identity

$$\hat{z} \cdot (\nabla \times \mathbf{F}) = -\nabla \cdot (\hat{z} \times \mathbf{F}), \quad (34.57)$$

so that the thickness weighted PV equation (34.56) can be written

$$\frac{\partial(hQ)}{\partial t} = -\nabla \cdot (hQ \mathbf{u} + \hat{z} \times \mathbf{F}). \quad (34.58)$$

Note how the volume source term,  $w^{(\dot{\eta})}$ , does not explicitly appear in the flux-form equation (34.58) since the effects from  $w^{(\dot{\eta})}$  are captured by the divergence,  $\nabla \cdot \mathbf{u}$ , as per equation (34.53).

For the shallow water fluid, the thickness weighted potential vorticity equals to the absolute vorticity

$$hQ = \zeta_a. \quad (34.59)$$

Consequently, the flux-form conservation form of the PV equation (34.58) is identical to equation (34.52) for the absolute vorticity

$$\frac{\partial(hQ)}{\partial t} = -\nabla \cdot (hQ \mathbf{u} + \hat{z} \times \mathbf{F}) \iff \frac{\partial \zeta_a}{\partial t} = -\nabla \cdot (\zeta_a \mathbf{u} + \hat{z} \times \mathbf{F}). \quad (34.60)$$

#### *Potential vorticity flux vector*

It is remarkable that even with non-conservative forcing, the thickness weighted potential vorticity (equivalently, the absolute vorticity) has its Eulerian evolution determined by the convergence of a flux,

$$\mathbf{J}_Q = hQ \mathbf{u} + \hat{z} \times \mathbf{F}. \quad (34.61)$$

The general form for the evolution of “PV-stuff” is not just specific to the shallow water fluid. Rather, it holds for any fluid and it leads to some rather special properties for potential vorticity budgets, with a detailed exploration given in Chapters 37 and 44.

The flux convergence evolution for the potential vorticity equation (34.60) is actually a kine-

matic result of the definition of potential vorticity. Namely,

$$h Q - f = \zeta = \nabla \cdot (\mathbf{u} \times \hat{\mathbf{z}}) \quad (34.62)$$

so that

$$\partial_t(h Q) = \nabla \cdot (\partial_t \mathbf{u} \times \hat{\mathbf{z}}) \equiv -\nabla \cdot \mathbf{J}^{\text{kin}}, \quad (34.63)$$

where we defined the kinematic potential vorticity flux vector

$$\mathbf{J}^{\text{kin}} \equiv -\partial_t \mathbf{u} \times \hat{\mathbf{z}} = \mathbf{J} - \nabla \times (g \eta + \mathbf{u} \cdot \mathbf{u}/2). \quad (34.64)$$

Since the two fluxes differ by a curl; i.e., a rotational term, their divergences are identical

$$\nabla \cdot \mathbf{J}^{\text{kin}} = \nabla \cdot \mathbf{J}, \quad (34.65)$$

so that their convergence leads to the same evolution of  $h Q$ . Stated more formally,  $\mathbf{J}^{\text{kin}}$  and  $\mathbf{J}$  differ by a gauge, with the gauge function here given by  $g \eta + \mathbf{u} \cdot \mathbf{u}/2$ .

## 34.6 Example implications of PV material invariance

The material conservation properties of shallow water PV provide nontrivial constraints on the fluid motion by stating that  $f, h, \zeta$  cannot change independently of the other. Rather, the combination  $Q = (f + \zeta)/h$  must remain materially invariant (in the absence of friction and mixing). There are a huge variety of situations that induce changes in one or two of the terms, with the third term constrained to ensure  $Q$  remains unchanged. We here consider some thought experiments to garner experience with shallow water PV-thinking.

### 34.6.1 Topographic beta effect

Changes in the topography affect the potential vorticity by changing the thickness of a fluid column via (see Figure 30.1)

$$h = H + \Delta\eta - \Delta\eta_b, \quad (34.66)$$

with  $H = \bar{h}$  the area mean layer thickness,  $\Delta\eta = \eta - \bar{\eta}$  the deviation of the free surface from its area mean, and  $\Delta\eta_b = \eta_b - \bar{\eta}_b$  the deviation of the bottom from its area mean. For relative vorticity, we note that spatial changes in the topography act to drive a vertical velocity at the layer bottom as per equation (30.25),

$$w = \frac{D\eta_b}{Dt} \quad \text{at } z = \eta_b, \quad (34.67)$$

which then leads to vortex stretching and hence to a change in relative vorticity. In this subsection we highlight the analog between topographic slopes and planetary beta to thus motivate the term *topographic beta effect*.

To mathematically exhibit the topographic beta effect, consider a fluid column whose vorticity is dominated by planetary vorticity and with bottom topography having a small and linear slope in the meridional direction

$$\Delta\eta_b = \delta y, \quad (34.68)$$

where  $|\delta| \ll 1$  is the topographic slope. Assuming the free surface undulations are small relative

to the resting layer thickness,  $\Delta\eta \ll H$ , we can expand the potential vorticity according to

$$Q = \frac{f + \zeta}{h} \quad (34.69a)$$

$$= \frac{f_0 + \beta y + \zeta}{H + \Delta\eta - \delta y} \quad (34.69b)$$

$$\approx \frac{f_0 + \beta y + \zeta}{H} [1 - H^{-1}(\Delta\eta - \delta y)] \quad (34.69c)$$

$$\approx \frac{f_0 + \beta y + \zeta}{H} - \frac{f_0}{H^2} (\Delta\eta - \delta y). \quad (34.69d)$$

Setting  $DQ/Dt = 0$  and rearranging leads to the material evolution of relative vorticity

$$\frac{D\zeta}{Dt} = -v(\beta + f_0\delta/H) + \frac{f_0 w(\eta)}{H}. \quad (34.70)$$

The second term on the right hand side is the vortex stretching associated with vertical motion at the top of the layer, where  $w(\eta) = D\Delta\eta/Dt = D\eta/Dt$  according to the surface kinematic boundary condition (30.33). The first term on the right hand side is vortex stretching arising from both planetary beta and topographic slopes. It is written in a form revealing the parallels between these two contributions, and it is readily generalized to the following for arbitrary topography

$$\beta_{\text{eff}} = (H - \eta_b) \nabla[f/(H - \eta_b)] \approx \beta \hat{\mathbf{y}} + (f_0/H) \nabla\eta_b. \quad (34.71)$$

One of the more prominent roles for topographic beta is in supporting topographic Rossby waves, which are analogous to the Rossby waves supported by planetary beta (see Section 33.6). We also encounter the topographic beta effect in Section 38.6.1 in our study of the quasi-geostrophic shallow water model.

### 34.6.2 Planetary geostrophic PV

As introduced in Section 25.5, planetary geostrophy (PG) is used to study the large-scale laminar ocean circulation where relative vorticity is ignored. Furthermore, as shown in Section 38.4, the inviscid and adiabatic PG system materially preserves the PG potential vorticity,  $Q = f/h$ , so that

$$\frac{D(f/h)}{Dt} = 0. \quad (34.72)$$

Consequently, fluid particles respecting the inviscid PG equations follow contours of constant  $f/h$ . These contours are referred to as *geostrophic contours* since the flow is under geostrophic balance.

If we furthermore assume the free surface undulations are negligible (a useful assumption for large-scale flow), then shallow water columns follow trajectories of constant  $f/H$ , where  $z = -H(x, y) = \eta_b(x, y)$  is the vertical position of the bottom topography. Figure 34.5 illustrates sample  $f/H$  contours for a topographic seamount (bump) in the southern hemisphere. Fluid columns are steered towards the equator as they encounter the seamount. Those near to the bump are trapped as they circle around the seamount. There are hence two regimes of contours: those that are trapped by the seamount and cannot escape, and those that are untrapped.

### 34.6.3 Spin up of converging flow

Consider the flow shown in Figure 34.6, whereby mass in the shallow water layer converges into a region. Just as described in the PV derivation Figure 34.4, increasing the column thickness, without substantially altering the planetary vorticity (e.g.,  $f$ -plane), requires  $\partial\zeta/\partial t > 0$  in order

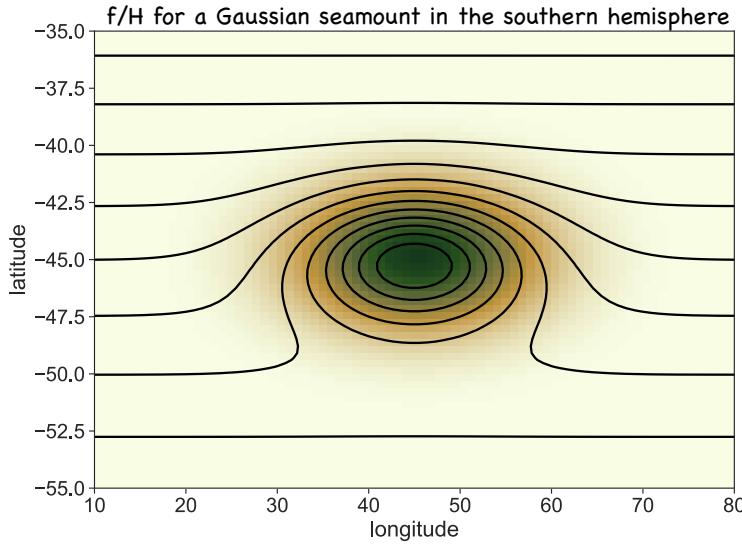


FIGURE 34.5: When a shallow water fluid is governed by the inviscid and adiabatic planetary geostrophic equations, fluid columns maintain fixed planetary geostrophic potential vorticity,  $D(f/h)/Dt = 0$ . Ignoring free surface undulations relative to changes in the bottom depth means that  $f/H$  remains fixed following the inviscid geostrophic flow, where  $z = -H(x, y) = \eta_b(x, y)$  is the bottom topography. We illustrate these *geostrophic contours* for a Gaussian seamount (shaded feature) in the southern hemisphere. Contours of constant  $f/H$  that are far from the seamount follow lines of constant latitude, on which  $f$  is constant. Contours closer to the seamount are diverted according to the requirement of keeping  $f/H$  fixed. When  $H$  decreases, as per a seamount, then the  $f/H$  contours move equatorward. Trajectories near the seamount are trapped as they circle around the bump.

to maintain  $Q = (\zeta + f)/h$  materially constant. Following our discussion of the rotating column in Section 34.3, note that convergence of mass reduces the moment of inertia relative to the center of the region. Angular momentum conservation requires the fluid to rotate faster thus picking up a positive relative vorticity. This dynamical process is embedded in the material invariance of PV. Finally, note that the opposite occurs in a region of diverging fluid, whereby the PV invariance implies that the relative vorticity has a negative tendency ( $\partial\zeta/\partial t < 0$ ) (see also Figure 34.4).

#### 34.6.4 Further study

Section 4.3 of Holton (1992) discusses the case of flow over topography where the full shallow water PV is materially invariant,  $D(f + \zeta)/Dt = 0$ . In that case there is a dramatic difference between easterly and westerly flows. In the northern hemisphere, westerly winds (eastward flow) deflects over the topography and downstream it undulates as topographic leewaves. A rotating tank offers a useful controlled setting to observe leewaves, such as shown near the 20 minute mark in [this video from Prof. Fultz of the University of Chicago](#). Easterly winds (westward flow) do not exhibit a wavelike pattern, instead following a trajectory similar to the  $f/H$  contours of planetary geostrophic case, though modified by relative vorticity. In general, the study of flow near topography, either in the shallow water or continuously stratified, introduces a wealth of dynamical behaviors where material invariance of potential vorticity provides an important tool to help unravel mechanisms.

## 34.7 Geostrophic adjustment

The geostrophic balance presented in Sections 25.4 and 31.2 is very well maintained by the observed large-scale atmosphere and ocean. Hence, geostrophy (and the associated thermal wind)

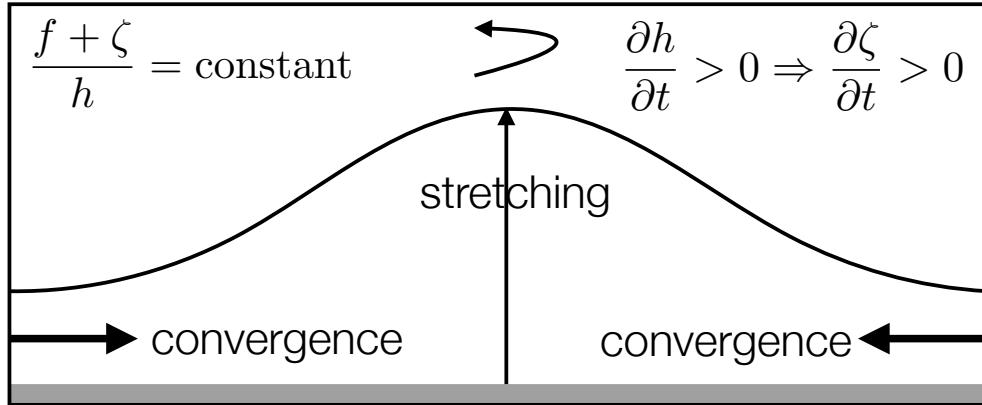


FIGURE 34.6: Illustrating the implications of material PV invariance for a shallow water fluid on an  $f$ -plane. If mass converges into a region, thus stretching the fluid column, then PV invariance implies the relative vorticity increases,  $\partial\zeta/\partial t > 0$ . This result is directly analogous to the rotating cylinder example considered in Figures 34.1 and 34.4. Namely, converging a region of constant mass reduces its moment of inertia so that angular momentum conservation leads to an increase in spin.

is a powerful diagnostic. In this section, we examine how a flow state that is initially not in geostrophic balance evolves towards geostrophy. We thus study the dynamical processes associated with the *geostrophic adjustment* problem.

A single shallow water layer on a flat  $f$ -plane is sufficient to introduce the main physical ideas. Furthermore, we focus on linear perturbations so that the governing equations are those derived in Section 31.8 when studying inertia-gravity waves. The adjustment consists of linear inertia-gravity waves that maintain a locally static potential vorticity (Section 31.8.4). For brevity in notation, we here drop all primes on the linear fluctuating terms.

### 34.7.1 Potential vorticity inversion

Before studying the geostrophic adjustment problem, we offer a few comments about *potential vorticity inversion*, which generally refers to the process of determining the flow field given information about the potential vorticity. In a shallow water layer, the potential vorticity is given by

$$Q = h^{-1} (f + \zeta) = h^{-1} [f + \partial_x v - \partial_y u]. \quad (34.73)$$

If we further assume the flow to be in geostrophic balance (Section 31.2), then

$$Q = \frac{f}{h} + \frac{1}{h} \left[ \frac{\partial}{\partial x} \left( \frac{g}{f} \frac{\partial \eta}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{g}{f} \frac{\partial \eta}{\partial y} \right) \right]. \quad (34.74)$$

Assuming we know  $Q$  throughout the domain; assuming  $f$  and  $Q$  are uniformly of the same sign within the domain; and assuming we know boundary conditions for  $\eta$ , then equation (34.74) is a nonlinear elliptic boundary value problem (Section 3.5) for  $\eta$ . Nonlinearities come from the  $h^{-1} = (\eta - \eta_b)^{-1}$  pre-factor, as well as the boundary conditions discussed below. Linearizing by setting  $h^{-1} \approx H^{-1}$  and simplifying the boundary conditions (see below) allows equation (34.74) to be solved for  $\eta$ . This solution process is referred to as *inverting* the elliptic operator, so that this particular inversion process is referred to as *potential vorticity inversion*.

General boundary conditions for  $\eta$  can be rather complex to handle mathematically. Namely, in a domain with a sloping bottom, such as in Figure 30.1, the free surface vanishes along the domain boundaries since the layer thickness vanishes there. Furthermore, the horizontal position

of the domain boundary is a function of time since the layer moves up and down the sloping bottom. Vanishing layers and the associated moving boundaries are intrinsically nonlinear; i.e., there is no way to linearize this process. Instead, to facilitate the use of linear physics requires us to assume the layer thickness remains nonzero throughout the domain. Furthermore, we assume the layer thickness deviates only a small amount from the layer averaged thickness:  $\eta/H \approx 1$ . These assumptions are made in the following discussion of geostrophic adjustment.

### 34.7.2 Posing the initial value problem

We solve for the  $t > 0$  evolution of surface height and velocity by making use of the linearized equations from Section 31.8

$$\frac{\partial \mathbf{u}}{\partial t} + f \hat{\mathbf{z}} \times \mathbf{u} = -g \nabla \eta \quad (34.75)$$

$$\frac{\partial \eta}{\partial t} + H \nabla \cdot \mathbf{u} = 0 \quad (34.76)$$

$$\zeta - \frac{f\eta}{H} = q(x, y) \quad (34.77)$$

where  $q(x, y)$  is the static potential vorticity determined by the initial conditions (Section 31.8.4). To illustrate the geostrophic adjustment in an analytically tractable manner, consider the following step initial conditions for the surface height

$$\eta(x, t=0) = \begin{cases} +\eta_0 & x < 0 \\ -\eta_0 & x > 0, \end{cases} \quad (34.78)$$

which can be written

$$\eta(x, t=0) = \eta_0 [1 - 2 \mathcal{H}(x)] = -\eta_0 \operatorname{sgn}(x), \quad (34.79)$$

where the sign-function is given by

$$\operatorname{sgn}(x) = \begin{cases} -1 & \text{if } x < 0 \\ 0 & \text{if } x = 0 \\ 1 & \text{if } x > 0, \end{cases} \quad (34.80)$$

which can also be written in terms of the Heaviside step function

$$\operatorname{sgn}(x) = 2 \mathcal{H}(x) - 1, \quad (34.81)$$

where

$$\mathcal{H}(x) = \begin{cases} 0 & \text{if } x < 0 \\ 1/2 & \text{if } x = 0 \\ 1 & \text{if } x > 0. \end{cases} \quad (34.82)$$

The velocity is assumed to be zero initially

$$\mathbf{u}(x, y, t=0) = 0. \quad (34.83)$$

Correspondingly, the initial relative vorticity vanishes so that the linearized potential vorticity (equation (31.177)) is

$$q(x, y) = \frac{f\eta_0}{H} \operatorname{sgn}(x). \quad (34.84)$$

Since  $\partial q/\partial t = 0$  (equation (31.176)), this value of the potential vorticity is maintained at each point throughout the adjustment process. The velocity and surface height adjustment is thus constrained to keep potential vorticity static. This rather basic point is key to determining evolution of the velocity and surface height, and thus in determining the final (equilibrium) state for these fields.

### 34.7.3 Adjustment in the absence of rotation

In the absence of rotation ( $f = 0$ ), relative vorticity is constant at each grid point. With a zero initial velocity, relative vorticity remains zero throughout the adjustment. The adjustment is thus quite simple. Namely, it consists of linear gravity waves (which have zero relative vorticity; see Section 31.8.2) propagating away from the initial step, converting the potential energy of the step into kinetic energy of waves that propagate to infinity. As the linear gravity waves are non-dispersive, they carry the initial pulse out to infinity without distortion in the form<sup>2</sup>

$$\eta(x, t) = -\frac{\eta_0}{2} [\operatorname{sgn}(x + ct) + \operatorname{sgn}(x - ct)], \quad (34.85)$$

where  $c = \sqrt{gH}$  is the speed for non-rotating gravity waves (Section 31.8.3). The meridional velocity remains zero, whereas the zonal velocity

$$\frac{\partial u}{\partial t} = -g \frac{\partial \eta}{\partial x} \quad (34.86)$$

is given by

$$u(x, t) = \frac{g\eta_0}{2c} [\operatorname{sgn}(x + ct) - \operatorname{sgn}(x - ct)]. \quad (34.87)$$

After the transient waves have passed, the steady solution is a flat surface height with zero velocity. This steady solution is familiar from the case of a rock dropped into a still pond. After dropping the rock into the pond, the surface gravity waves radiate outward from the rock and are eventually damped upon reaching the shore. In equilibrium, the pond returns to a state of rest with a flat surface height.<sup>3</sup>

### 34.7.4 Adjustment with rotation

With rotation, the transient solution consists of inertia-gravity waves (Section 31.8) that transmit information about the initial surface height perturbation out to infinity. After the transient waves have passed, the steady solution is either the trivial solution with flat surface height (as for the non-rotating case), or a nontrivial solution that is in geostrophic balance

$$f\hat{z} \times \mathbf{u} = -g \nabla \eta \quad \text{and} \quad \nabla \cdot \mathbf{u} = 0 \quad \text{and} \quad q = H^{-1} f \eta_0 \operatorname{sgn}(x). \quad (34.88)$$

Conservation of potential vorticity constrains the solution so that the steady state surface height is sloped according to a geostrophically balanced state. That is, an equilibrium state of no-motion is not allowed by potential vorticity conservation. This is a profound distinction from the non-rotating case.

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<sup>2</sup>In Section 3.7 we studied the wave solutions that take on the general form of equation (34.85).

<sup>3</sup>For some purposes, a pond is better studied using deep water equations rather than shallow water equations; see Section 29.1. Even so, the key physical points in this example are maintained in either case.

### Computing the equilibrium state

As the flow is geostrophic on an  $f$ -plane, we make use of the geostrophic streamfunction

$$\psi = g \eta / f. \quad (34.89)$$

The equilibrium state is written in terms of the streamfunction according to

$$u = -\partial_y \psi \quad \text{and} \quad v = \partial_x \psi \quad \text{and} \quad \zeta = \nabla^2 \psi. \quad (34.90)$$

Making use of these expressions in the linearized potential vorticity expression (34.84) leads to the elliptic partial differential equation for the streamfunction

$$[\nabla^2 - L_d^{-2}] \psi = q(x, y), \quad (34.91)$$

where we introduced the shallow water *deformation radius*

$$L_d = f^{-1} \sqrt{g H}. \quad (34.92)$$

We motivate the name “deformation radius” in the following.

The initial condition (34.79) has no  $y$ -dependence. Furthermore, there is nothing in the adjustment process that will break this meridional symmetry. Hence, the equilibrium state is a function only of  $x$ , in which case the streamfunction satisfies the ordinary differential equation

$$\frac{d^2 \psi}{dx^2} - L_d^{-2} \psi = \frac{f \eta_0}{H} \operatorname{sgn}(x). \quad (34.93)$$

We solve this equation separately for  $x > 0$  and  $x < 0$  and then match the function and its first derivative at  $x = 0$ . Furthermore, we constrain the streamfunction to vanish at  $\pm\infty$ . The  $x > 0$  streamfunction satisfies

$$\frac{d^2 \psi}{dx^2} - L_d^{-2} \psi = \frac{f \eta_0}{H}. \quad (34.94)$$

The particular solution is

$$\psi_p = -L_d^2 q = -L_d^2 \frac{f \eta_0}{H} = -\frac{g \eta_0}{f} \quad (34.95)$$

and the homogeneous solution is

$$\psi_h = \frac{g \eta_0}{f} e^{-x/L_d} \quad (34.96)$$

so that

$$\psi = -\frac{g \eta_0}{f} \left[ 1 - e^{-x/L_d} \right]. \quad (34.97)$$

The  $x < 0$  solution is found similarly, so that

$$\psi = \frac{g \eta_0}{f} \begin{cases} -\left(1 - e^{-x/L_d}\right) & x > 0 \\ \left(1 - e^{x/L_d}\right) & x < 0, \end{cases} \quad (34.98)$$

which means that the equilibrium surface height is

$$\eta = \eta_0 \begin{cases} -\left(1 - e^{-x/L_d}\right) & x > 0 \\ \left(1 - e^{x/L_d}\right) & x < 0. \end{cases} \quad (34.99)$$

Note that the streamfunction vanishes at  $x = 0$  and has a first derivative of  $-\eta_0 \sqrt{gH}/H$ . Since

the streamfunction only has a zonal dependence, the equilibrium velocity is purely meridional

$$u = 0 \quad \text{and} \quad v = -\frac{g \eta_0}{f L_d} e^{-|x|/L_d}. \quad (34.100)$$

The equilibrium velocity thus consists of a jet that is perpendicular to the surface height front.

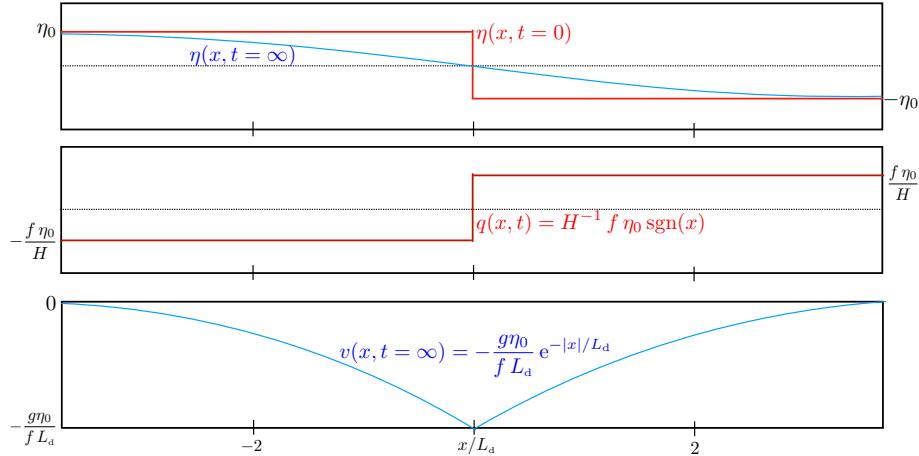


FIGURE 34.7: Depicting solutions to the linear geostrophic adjustment of a rotating shallow water layer on an  $f$ -plane. The top panel shows the initial (step-function) surface height (34.79) and the equilibrium (exponential) surface height (34.99). The second panel shows the static (step-function) potential vorticity (34.88). The third panel shows the equilibrium (exponential) meridional velocity (34.100) comprised of a jet centered at  $x = 0$ . The horizontal axis is scaled according to the shallow water deformation radius,  $L_d = f^{-1} \sqrt{g H}$ . This figure is adapted from figure 3.10 of [Vallis \(2017\)](#).

### 34.7.5 Comments

As illustrated in Figure 34.7, the equilibrium profiles for the surface height and velocity both have an exponential decay, with decay length scale given by the deformation radius. It is this length scale over which the solution is affected or “deformed” by rotation, thus motivating the name “deformation radius”.

A key feature of the rotating case is that some of the potential energy contained within the initial perturbed surface height remains in the equilibrium geostrophic flow. The conservation of potential vorticity constrains the flow so that all of the initial potential energy cannot be converted to kinetic energy. Rather, the adjustment occurs only within a deformation radius distance from the initial perturbation.

Chapter 3 of [Pratt and Whitehead \(2008\)](#) provide a thorough discussion of the geostrophic adjustment problem, both for the linear case and fully nonlinear case.

## 34.8 Circulation with non-conservative processes

We follow the discussion in Section 34.5 to study the evolution of circulation in the presence of non-conservative processes such as dia-surface transport and boundary stresses (Section 30.5). For this purpose, consider the velocity circulation around a closed horizontal area,  $\mathcal{S}$  (see Figure 34.8)

$$\mathcal{C} = \int_{\mathcal{S}} \zeta d\mathcal{S} = \oint_{\partial \mathcal{S}} \mathbf{u} \cdot \hat{\mathbf{t}} d\ell. \quad (34.101)$$

In this equation,  $\hat{\mathbf{t}} d\ell$  is the vector line increment around the contour, and  $\hat{\mathbf{t}}$  is the tangent vector orienting the contour integral in a counterclockwise direction. We assume the circulation contour extends vertically through the layer so that the outward normal,  $\hat{\mathbf{n}}$ , to the contour is strictly horizontal, as is the tangent vector,  $\hat{\mathbf{t}}$ . We now seek an evolution equation for this circulation by making use of the vorticity equation (34.60).

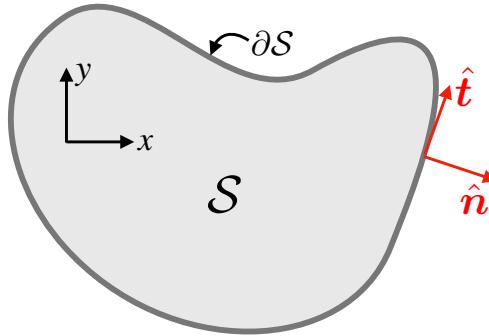


FIGURE 34.8: Illustrating the calculation of circulation around the contour,  $\partial\mathcal{S}$ , of a static horizontal area,  $\mathcal{S}$ , within a layer of shallow water fluid. The circulation theorem (34.105) provides the means to compute the time changes in circulation as a function of the advection of absolute vorticity crossing the contour plus the circulation of friction. Note that the contour has a vertical extent throughout the shallow water layer, so that the unit outward normal,  $\hat{\mathbf{n}}$ , and the unit tangent direction,  $\hat{\mathbf{t}}$ , are both horizontal vectors.

To develop an evolution equation for  $\mathcal{C}$ , integrate the vorticity equation (34.60) over the area  $\mathcal{S}$  to yield

$$\int_{\mathcal{S}} \frac{\partial \zeta}{\partial t} d\mathcal{S} = \int_{\mathcal{S}} [-\nabla \cdot (\zeta_a \mathbf{u} + \hat{\mathbf{z}} \times \mathbf{F})] d\mathcal{S} = - \oint_{\partial\mathcal{S}} [\zeta_a \mathbf{u} + \hat{\mathbf{z}} \times \mathbf{F}] \cdot \hat{\mathbf{n}} d\ell, \quad (34.102)$$

where  $\oint$  symbolizes an integral around the contour. To reach this equation we used the divergence theorem on the right hand side, with  $\hat{\mathbf{n}}$  the *horizontal* outward normal vector along the contour,  $\partial\mathcal{S}$ , and  $d\ell$  is the line increment along the contour. We also set  $\partial f / \partial t = 0$  as part of the time derivative of the absolute vorticity. The non-conservative forcing term can be written

$$(\hat{\mathbf{z}} \times \mathbf{F}) \cdot \hat{\mathbf{n}} = (\hat{\mathbf{n}} \times \hat{\mathbf{z}}) \cdot \mathbf{F} = -\hat{\mathbf{t}} \cdot \mathbf{F}, \quad (34.103)$$

thus leading to

$$\int_{\mathcal{S}} \frac{\partial \zeta}{\partial t} d\mathcal{S} = - \oint_{\partial\mathcal{S}} \zeta_a \mathbf{u} \cdot \hat{\mathbf{n}} d\ell + \oint_{\partial\mathcal{S}} \mathbf{F} \cdot \hat{\mathbf{t}} d\ell, \quad (34.104)$$

where  $\oint$  is the counter-clockwise oriented closed contour integral. We next assume the area  $\mathcal{S}$  is constant in time, so that the Eulerian time derivative can be pulled across the integral to render

$$\frac{d\mathcal{C}}{dt} = - \oint_{\partial\mathcal{S}} \zeta_a \mathbf{u} \cdot \hat{\mathbf{n}} d\ell + \oint_{\partial\mathcal{S}} \mathbf{F} \cdot \hat{\mathbf{t}} d\ell. \quad (34.105)$$

The first term on the right hand side arises from the horizontal advection of absolute vorticity across the contour. This term is not oriented and so the integral sign has no arrow. The second term arises from the counter-clockwise oriented circulation of any non-conservative accelerations. We refer to equation (34.105) as a *circulation theorem*. It has many uses under specific cases, some of which are described in the remainder of this chapter.

### 34.8.1 Circulation around a closed streamline in steady flow

As a particular example of the circulation theorem (34.105), consider a steady flow in the absence of boundary volume sources ( $w^{(\dot{\eta})} = 0$ ). In this case, the thickness equation (30.16) reduces to  $\nabla \cdot (h \mathbf{u}) = 0$  so that we can introduce a streamfunction,  $\Psi$  (with dimensions of  $L^3 T^{-1}$ )

$$h \mathbf{u} = \hat{\mathbf{z}} \times \nabla \Psi. \quad (34.106)$$

In a bounded domain, the contours of constant  $\Psi$ , the streamlines, are closed. Furthermore, the outward normal to a closed streamline is perpendicular to the velocity,  $\mathbf{u} \cdot \hat{\mathbf{n}} = 0$ . We thus see that the steady state form of the circulation theorem (34.105), computed around a closed streamline, leads to the following constraint on the non-conservative forces

$$\oint_{\text{streamline}} \mathbf{F} \cdot \hat{\mathbf{t}} d\ell = \int_{\text{streamline area}} (\nabla \times \mathbf{F}) \cdot \hat{\mathbf{z}} dS = 0, \quad (34.107)$$

where the second equality follows from Stokes' theorem applied over the area bounded by the streamline. Equation (34.107) provides a constraint on the non-conservative forcing that must be satisfied to enable a steady flow. If this constraint is not satisfied, then the flow cannot reach a steady state. Although we may not know explicit details of the streamlines, we can still make use of this constraint if we assume the flow is steady. The analysis in Section 34.9 offers an example application of these ideas for studies of circulation in steady ocean gyres.

### 34.8.2 Circulation from wind stress and Rayleigh drag

A particularly simple form for the non-conservative acceleration is given by

$$\mathbf{F} = -\gamma \mathbf{u} + \boldsymbol{\tau}^{\text{wind}}/(h \rho) \equiv -\gamma \mathbf{u} + \mathbf{F}^{\text{wind}}. \quad (34.108)$$

The first term is referred to as *Rayleigh drag* with  $\gamma > 0$  a constant with dimensions of inverse time.<sup>4</sup> Rayleigh drag damps all flow to rest with  $\gamma^{-1}$  the e-folding time for the damping. The second term in equation (34.108) is the acceleration on the layer from wind stress,  $\mathbf{F}^{\text{wind}} = \boldsymbol{\tau}^{\text{wind}}/(h \rho)$ , with this form following from our discussion in Section 30.5.2. Namely, the homogeneity of the shallow water layer renders the contact stress from winds into a body stress applied throughout the layer.

Plugging the acceleration (34.108) into the time dependent circulation theorem (34.105) leads to

$$\frac{dC}{dt} + \gamma C = - \int_{\partial S} \zeta_a \mathbf{u} \cdot \hat{\mathbf{n}} d\ell + \oint_{\partial S} \mathbf{F}^{\text{wind}} \cdot \hat{\mathbf{t}} d\ell. \quad (34.109)$$

Specializing to a steady state and choosing the contour as a closed streamline (along which  $\mathbf{u} \cdot \hat{\mathbf{n}} = 0$ ), renders

$$C = \gamma^{-1} \oint_{\text{streamline}} \mathbf{F}^{\text{wind}} \cdot \hat{\mathbf{t}} d\ell = (\gamma \rho)^{-1} \oint_{\text{streamline}} (\boldsymbol{\tau}^{\text{wind}}/h) \cdot \hat{\mathbf{t}} d\ell. \quad (34.110)$$

This equation says that velocity circulation around a closed streamline is determined by wind stress circulation around that streamline plus knowledge of the Rayleigh drag damping time scale  $\gamma^{-1}$ . This result supports our intuition that the steady circulation around a closed contour is oriented according to the applied wind stress.

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<sup>4</sup>See Section 27.2.4 for more discussion of Rayleigh drag in the context of Ekman mechanics.

## 34.9 Western intensification of ocean gyres

Ocean gyres are a prominent feature of ocean circulation, with the North Atlantic and North Pacific middle-latitude gyres two canonical examples. A characteristic feature of such gyres is that they are not symmetric in the east-west direction, with a prominent western side where flow is stronger than the more sluggish interior flow. As shown in this section, such asymmetry is not a response to the wind forcing, with the asymmetry found even without any zonal variations in the winds. Instead, it is a manifestation of the beta effect present for flow on a spherical planet (or idealized as the  $\beta$ -plane from Section 22.3). We discuss the beta effect more formally in Section 35.7, but for now it is sufficient to know that it arises from the meridional gradient of the planetary vorticity:  $\beta = \partial_y f$ .

We have the basic tools in hand to understand the physical balances leading to western intensification in steady ocean gyres. For that purpose, we make use of vorticity balances as they offer a more direct path towards western intensification than the linear momentum or axial angular momentum balances used to explore channel flow in Sections 19.5 and 31.6.

### 34.9.1 Steady and large-scale vorticity balance

The steady circulation theorem (34.110) holds regardless the bottom topography or surface height undulations. Again, it says that circulation around a closed streamline is in the same sense as the wind circulation. However, we need more information to see how western intensification emerges as a property of ocean gyres. For that purpose, consider the steady absolute vorticity equation (34.60), again in the presence of wind forcing and Rayleigh drag

$$\nabla \cdot (\mathbf{u} \zeta_a) = -\gamma \zeta + \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}^{\text{wind}}). \quad (34.111)$$

Introducing the shallow water potential vorticity,  $Q = \zeta_a/h$ , allows us to write

$$\nabla \cdot (\mathbf{u} \zeta_a) = \nabla \cdot (h \mathbf{u} Q). \quad (34.112)$$

The steady state thickness equation (30.16) means that  $\nabla \cdot (h \mathbf{u}) = 0$ , so that the vorticity equation (34.111) takes the form

$$h \mathbf{u} \cdot \nabla Q = -\gamma \zeta + \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}^{\text{wind}}). \quad (34.113)$$

This equation says that in the absence of the irreversible terms on the right hand side, the steady horizontal flow follows contours of constant potential vorticity. This result follows directly from the material invariance of PV in the absence of non-conservative processes. However, in the presence of Rayleigh drag and/or wind stress curl, PV is modified when following the flow so that  $\mathbf{u} \cdot \nabla Q \neq 0$ .

### 34.9.2 Planetary geostrophic flow and the Sverdrup balance

For large-scale flow away from lateral boundaries, the flow has an absolute vorticity that is dominated by planetary vorticity so that

$$Q \approx Q_{\text{PG}} = f/h, \quad (34.114)$$

which is the PV for planetary geostrophic flow (Section 25.5 and 38.4). Correspondingly, we assume the Rayleigh drag term is negligible in this region since the relative vorticity is small, so that the PV equation (34.113) takes the form

$$h \mathbf{u} \cdot \nabla Q_{\text{PG}} = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}^{\text{wind}}). \quad (34.115)$$

Expanding the left hand side and introducing the planetary vorticity gradient renders the *shallow water Sverdrup balance*

$$\beta v = Q_{\text{PG}} \mathbf{u} \cdot \nabla h + \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}^{\text{wind}}) \quad \text{shallow water Sverdrup balance.} \quad (34.116)$$

This balance states how horizontal advection of layer thickness (first right hand side term) plus the wind stress curl (second term) lead to meridional motion for flow on a rotating sphere (beta effect on left hand side). Gradients in the layer thickness arise from free surface undulations as well as gradients in the bottom topography (see Figure 30.1). The traditional *Sverdrup balance* arises when we assume the flow takes place over a flat bottom and the free surface undulations are negligible, in which case  $\nabla h \approx 0$  so that

$$\beta v = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}^{\text{wind}}) \quad \text{traditional Sverdrup balance.} \quad (34.117)$$

### 34.9.3 Sverdrup flow in a closed domain with anti-cyclonic wind stress

As a particular example, consider a closed northern hemisphere middle latitude  $\beta$ -plane domain driven by an anti-cyclonic wind stress

$$\hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}^{\text{wind}}) < 0 \quad \text{northern hemisphere anti-cyclonic wind stress.} \quad (34.118)$$

This situation is depicted in Figure 34.9, where we also illustrate a commonly used wind stress profile that is purely zonal and has a co-sinusoidal meridional structure that is symmetric about the central latitude of the domain

$$\mathbf{F}^{\text{wind}} = -\hat{\mathbf{x}} A \cos[\pi(y - y_0 + L/2)/L] \quad (34.119a)$$

$$\hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}^{\text{wind}}) = -(\pi A/L) \sin[\pi(y - y_0 + L/2)/L]. \quad (34.119b)$$

In these equations,  $A > 0$  is the magnitude of the wind stress acceleration applied to the layer, and the domain extends meridionally from  $y_0 - L/2 \leq y \leq y_0 + L/2$  with  $y = y_0$  the central latitude. This wind stress has westerlies on the poleward side of the domain and easterlies (trade winds) on the equatorward side so that  $\hat{\mathbf{z}} \cdot (\nabla \times \boldsymbol{\tau}) < 0$  throughout the domain.

The Sverdrup balance (34.117) indicates that an anti-cyclonic wind stress curl drives an equatorward Sverdrup flow. We emphasize that this flow is *not* the result of meridional winds pushing the fluid to the south. Instead, it arises in response to the constraints of vorticity balance with an anti-cyclonic wind stress curl in the presence of the beta effect. Indeed, for the idealized wind stress (34.119a) there is no meridional wind component. Although water satisfying Sverdrup balance flows south, all the water in the domain cannot be moving to the south. Rather, volume conservation requires a poleward return flow somewhere outside the region of Sverdrup balance.

### 34.9.4 Western intensification and the role of beta

Volume conservation is a kinematic constraint that requires a return flow on either the eastern or western side of the domain, outside the region of Sverdrup balance. But what side? We offer the following arguments for the western side.

#### *Inertial entry into a boundary layer region*

Recall the discussion of Figure 33.4 where we considered how inviscid flow in a homogeneous fluid over a flat bottom region materially preserves absolute vorticity in the presence of a meridional barrier. To materially preserve absolute vorticity (and ignoring free surface undulations relative

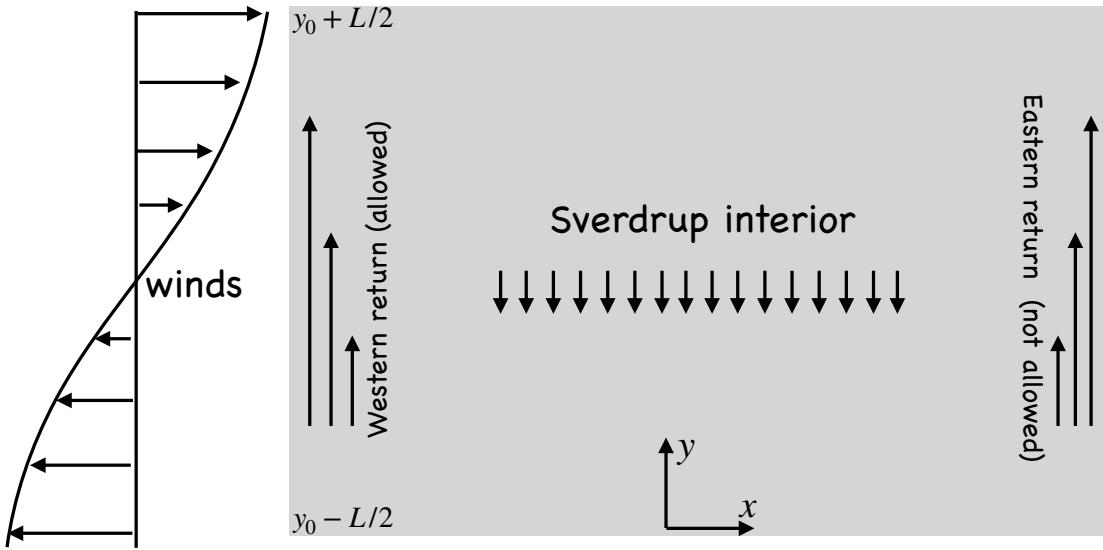


FIGURE 34.9: Illustrating the southward Sverdrup flow in response to an anti-cyclonic wind stress forcing in a bounded northern hemisphere domain. A northward return flow is required to satisfy volume conservation. As seen in Section 34.9.4, a linear vorticity balance between beta, winds, and friction lead to a western boundary return flow and corresponding western intensification.

to the depth of the fluid), the flow can deviate meridionally, either northward or southward, when encountering a western wall. In contrast, such meridional deviation is prohibited for absolute vorticity preserving flow that encounters an eastern wall. So in referring to Figure 34.9, southward flow can make a turn westward towards the western boundary, enter the boundary layer, and move northward within the boundary layer. It cannot do so for the eastern side.

#### *Steady velocity circulation follows wind circulation*

The steady circulation theorem (34.110) means that the flow circulation is in the same sense as the wind circulation. With an anti-cyclonic wind forcing, the circulation also must be anti-cyclonic. This result again leads us to conclude that the western boundary is the region for the return flow, in which case the full gyre circulation will be anti-cyclonic.

#### *Steady vorticity balance and the need for dissipation*

The two previous arguments point to the western side as the return flow region. But we have yet to provide an argument for western intensification. For that purpose, recall that the return flow region is not in traditional Sverdrup balance. To see what terms can break that balance, consider again the steady vorticity balance (34.113). Continuing to assume a flat bottom and rigid lid surface leads to

$$\beta v = -\gamma \zeta + \hat{z} \cdot (\nabla \times \mathbf{F}^{\text{wind}}), \quad (34.120)$$

where we dropped the nonlinear advection term  $\mathbf{u} \cdot \nabla \zeta$  since we wish to determine whether a linear balance can give rise to western intensification. The Rayleigh drag on the right hand side breaks the Sverdrup balance in regions where the relative vorticity is nontrivial. Since we know there must be a return flow somewhere in the domain, we know there must be a region where dissipation is sufficiently strong to break Sverdrup balance.

What is required for the steady and linear dissipative vorticity balance (34.120) to be maintained in the northward return flow region? To answer this question, expose the signs on the

terms in equation (34.120)

$$\underbrace{\beta v}_{\text{positive}} + \underbrace{\gamma \zeta}_{\text{unspecified}} = \underbrace{\hat{z} \cdot (\nabla \times \mathbf{F}^{\text{wind}})}_{\text{negative}}. \quad (34.121)$$

We have  $\beta v > 0$  since we are concerned with the region of northward return flow, and  $\hat{z} \cdot (\nabla \times \mathbf{F}^{\text{wind}}) < 0$  by assumption of anti-cyclonic wind stress over the full domain. Hence, for the balance (34.121) to be realized requires  $\zeta < 0$ , with the value large enough to balance both the winds and the meridional advection of planetary vorticity

$$\underbrace{\gamma \zeta}_{\text{negative}} = \underbrace{-\beta v}_{\text{negative}} + \underbrace{\hat{z} \cdot (\nabla \times \mathbf{F}^{\text{wind}})}_{\text{negative}}. \quad (34.122)$$

For anti-cyclonic gyre flow, as required by the circulation condition (34.110), the only way to realize  $\zeta < 0$  of sufficient magnitude is to have an intensified flow along the western side of the gyre. In this region,  $\zeta \approx \partial v / \partial x < 0$  can become sufficiently large in magnitude. Furthermore, since the wind stress is applied throughout the domain, all streamlines feel the winds and must pass through the western boundary region where vorticity is enhanced and Rayleigh drag is able to balance the winds and planetary advection.

### *The importance of beta*

In the absence of beta, there would be no interior region in Sverdrup balance driving southward flow. The flow would thus only be subject to the circulation condition (34.110) whereby linear flow can symmetrically dissipate the wind stress. Hence, the beta effect is the fundamental element that causes poleward flow to intensify along the western side of the gyre in response to the equatorward interior flow.

#### 34.9.5 A role for topographic form stress

Recall the shallow water Sverdrup balance (34.116), here with the addition of Rayleigh drag

$$\beta v = Q_{\text{PG}} \mathbf{u} \cdot \nabla h - \gamma \zeta + \hat{z} \cdot (\nabla \times \mathbf{F}^{\text{wind}}). \quad (34.123)$$

For the right hand side, we have thus far considered a flat bottom and ignored free surface undulations, in which case  $\nabla h = 0$ . We here sketch the situation with nonzero free surface and topographic variations, thus illustrating how boundary pressure gradients can render flow even in the absence of bottom drag.

### *Curl of the form stresses*

We are just concerned with that portion of  $\mathbf{u} \cdot \nabla h$  due to pressure gradients, in which case we insert the geostrophic flow

$$\mathbf{u} \cdot \nabla h = (g/f) \nabla h \cdot (\hat{z} \times \nabla \eta) = (g/f) \hat{z} \cdot (\nabla \eta \times \nabla h). \quad (34.124)$$

Making use of the hydrostatic relation  $p_b = p_a + \rho g h$ , and the expression for the layer thickness,  $h = \eta - \eta_b$ , leads to

$$\mathbf{u} \cdot \nabla h = (g/f) \hat{\mathbf{z}} \cdot (\nabla \eta \times \nabla h) \quad (34.125a)$$

$$= 1/(\rho f) \hat{\mathbf{z}} \cdot [\nabla \times (p_a \nabla \eta) + \nabla \eta \times \nabla p_b] \quad (34.125b)$$

$$= 1/(\rho f) \hat{\mathbf{z}} \cdot [\nabla \times (p_a \nabla \eta) - \nabla \times (p_b \nabla \eta_b) + \nabla h \times \nabla p_b] \quad (34.125c)$$

$$= 1/(\rho f) \hat{\mathbf{z}} \cdot [\nabla \times (p_a \nabla \eta) - \nabla \times (p_b \nabla \eta_b) + \nabla p_b \times \nabla p_a / (\rho g)]. \quad (34.125d)$$

The first and second terms are the curls of the pressure form stresses applied to the surface (atmospheric) and bottom boundaries (Section 19.2), respectively, which we refer to as the atmospheric and bottom pressure torques. The third term is a torque arising from the misalignment of the applied pressure and bottom pressure. Making use of this result in the vorticity balance (34.123) leads to

$$\beta \rho h v = \hat{\mathbf{z}} \cdot [\nabla \times (p_a \nabla \eta) - \nabla \times (p_b \nabla \eta_b) + \nabla p_b \times \nabla p_a / (\rho g)] + \rho h [-\gamma \zeta + \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}^{\text{wind}})]. \quad (34.126)$$

We consider a few special cases to see how the pressure torques affect the meridional flow in a gyre circulation, with a focus on bottom pressure torque since this term is generally far larger than those involving the atmospheric pressure.

#### *Vanishing topographic form stress curl for geostrophic $f$ -plane motion*

In the absence of friction, wind forcing, and with a uniform atmospheric pressure,  $\beta$  times the depth integrated meridional mass transport in equation (34.126) is balanced by the curl of the topographic form stress

$$\beta \rho h v = -\hat{\mathbf{z}} \cdot (\nabla \times p_b \nabla \eta_b) \quad \text{linear inviscid and unforced.} \quad (34.127)$$

As a corollary of this balance, we see that a linear inviscid and unforced geostrophic flow on an  $f$ -plane satisfies  $\hat{\mathbf{z}} \cdot (\nabla \times p_b \nabla \eta_b) = \hat{\mathbf{z}} \cdot (\nabla p_b \times \nabla \eta_b) = 0$ , so that the isolines of surface height align with isolines of bottom topography since (with  $\nabla p_a = 0$ )  $p_b = g \rho h = g \rho (\eta - \eta_b)$ .

#### *Vanishing integrated topographic form stress curl on closed isobaths*

Consider a closed domain comprised of topography with isobaths closed within the domain. Use of Stokes' theorem reveals that an integral of  $\hat{\mathbf{z}} \cdot (\nabla \times p_b \nabla \eta_b)$  over the area defined by an isobath vanishes

$$\int_{\mathcal{S}} \hat{\mathbf{z}} \cdot (\nabla \times p_b \nabla \eta_b) d\mathcal{S} = \oint_{\partial\mathcal{S}} p_b \nabla \eta_b \cdot \hat{\mathbf{t}} d\ell = 0, \quad (34.128)$$

where  $\partial\mathcal{S}$  is determined by an isobath so that  $\nabla \eta_b \cdot \hat{\mathbf{t}} = 0$ . We can employ the same argument for an area bounded by isobars of bottom pressure. Hence, if there is initially no velocity circulation around an isobar or isobath, then topographic form stress will not spontaneously generate a circulation. This result is sensible because topographic form stress is *not* an external force akin to wind stress. Whereas wind stress curl is not constrained to vanish when integrated over a closed domain, topographic form stress, as it arises only in the presence of flow, is highly constrained.

#### *Local generation of bottom pressure torque*

The beta effect provides an inviscid means to create misalignment between the surface height and the bottom topography, with misalignment required to generate a nonzero topographic form

stress curl, which we refer to as *bottom pressure torque*. We discussed an analogous misalignment in Section 31.6 when studying the force balances in a steady zonally re-entrant channel with bottom topography. Wind stress forcing and dissipation offer another means for  $(\eta, \eta_b)$ -misalignment, as seen merely by rewriting the vorticity balance (34.126) as an expression for the bottom pressure torque

$$\hat{\mathbf{z}} \cdot (\nabla \times p_b \nabla \eta_b) = -\beta \rho h v + \hat{\mathbf{z}} \cdot [\nabla \times (p_a \nabla \eta) + \nabla p_b \times \nabla p_a / (\rho g)] + \rho h [-\gamma \zeta + \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}^{\text{wind}})]. \quad (34.129)$$

In our discussion of western intensification in Section 34.9.4, we ignored the role of bottom pressure torque. However, as seen by this balance, bottom pressure torque plays a role when topography and surface height are misaligned, with that role in some locations more important than friction (see [Hughes and de Cueves \(2001\)](#), [Jackson et al. \(2006\)](#) and [Patmore et al. \(2019\)](#) for examples). Even so, as shown above, the integral of the topographic form stress vanishes over a closed domain bounded by isobaths or isobars, so that friction is ultimately required to balance the input of vorticity from the winds. We contrast this situation to the zonally re-entrant channel from Section 31.6, whereby topographic form stress, of sufficient strength, can balance the momentum input by the winds thus making friction less important for the channel flow.

### 34.9.6 Comments and further study

The study of ocean gyres originates from the pioneering work of Henry Stommel in the 1950s. This video [from SciencePrimer](#) provides a concise summary of the dynamics of ocean gyres and western boundary intensification due to the beta effect. Chapter 19 of [Vallis \(2017\)](#) provides a lucid treatment of ocean gyre dynamics by working through the key features of Stommel's model as well as variants such as that from Walter Munk who considered a viscous closure rather than Rayleigh drag. The Stommel model and its variants are themselves very idealized renditions of the ocean gyres occurring in Nature. Notable further factors become important in studying Nature's gyres, such as topography (briefly discussed in Section 34.9.5), nonlinearities and instabilities, turbulent boundary layers, and coupled air-sea processes. Each of these processes render the study of western boundary currents one of the most complex and timeless areas of physical oceanography.

For the studies of Stommel and Munk, friction plays a key role in the western intensification of wind driven ocean gyres. As described in Chapter 19 of [Vallis \(2017\)](#), there have been attempts to produce an inviscid (and unforced) gyre solution, with the study from Fofonoff of note. We consider elements of the Fofonoff gyre in Exercise 33.8. Additionally, we raised the importance of sloping sides in Section 34.9.5 and in the earlier discussion of axial angular momentum in Section 19.5. Sloping sides enable bottom topographic form stress and bottom pressure torques to dominate over bottom turbulent stresses and turbulent torques. In so doing, sloping sides allow for an inviscid closure of gyres much like that for zonally reentrant channels. The role of sloping sides for gyre circulations was emphasized by [Hughes and de Cueves \(2001\)](#). As Nature eschews vertical sidewalls, the balances of [Hughes and de Cueves \(2001\)](#) are more geophysically compelling than the frictional closures required for vertical sidewalls.

## 34.10 Column vorticity

Throughout this chapter we have focused on vorticity as defined by the curl of the horizontal velocity,  $\zeta = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u})$ . Since flow within a shallow water layer moves in coherent and extensible vertical columns (Section 30.2), the shallow water vorticity measures the spin of a shallow water column. However, we can also measure the column spin by considering the curl of the thickness

weighted velocity

$$\Sigma = \hat{z} \cdot \nabla \times (h \mathbf{u}) = h \zeta + \hat{z} \cdot \nabla h \times \mathbf{u}. \quad (34.130)$$

We refer to  $\Sigma$  as the *column vorticity*. In addition to the thickness weighted relative vorticity,  $\Sigma$  measures the misalignment between the layer thickness gradient and the velocity, with  $\hat{z} \cdot \nabla h \times \mathbf{u}$  generally nonzero especially for geostrophic flows. Hence, the second term offers an extra measure of the spin for the fluid column beyond the relative vorticity measure.<sup>5</sup> As we will see, the layer thickness factor ensures that  $\Sigma$  directly probes stresses acting at the layer interfaces, as well as stresses within the fluid layer. Besides its intrinsic interest, this analysis is motivated by studies of the depth integrated flow commonly pursued in oceanography, with particular examples provided in Chapter 39.

### 34.10.1 Formulating the column vorticity equation

To formulate the dynamical equation for  $\Sigma$ , we start from the momentum equation (31.49)

$$\frac{\partial(h \mathbf{u})}{\partial t} + \nabla \cdot (h \mathbf{u} \otimes \mathbf{u}) + f \hat{z} \times (h \mathbf{u}) = -g h \nabla \eta^{\text{eff}} + \mathbf{f}^{\text{nc}} \quad (34.131)$$

where  $\mathbf{f}^{\text{nc}}$  is the thickness weighted non-conservative accelerations, such as arise from horizontal strains in the presence of viscosity, and the boundary transfer of turbulent momentum such as through winds and bottom drag (see Section 30.5). Taking the vertically projected curl of equation (34.131) leads to

$$\partial_t \Sigma + \hat{z} \cdot \nabla \times [\nabla \cdot (h \mathbf{u} \otimes \mathbf{u})] + \nabla \cdot (f h \mathbf{u}) = -g \hat{z} \cdot (\nabla h \times \nabla \eta^{\text{eff}}) + \hat{z} \cdot (\nabla \times \mathbf{f}^{\text{nc}}). \quad (34.132)$$

Let us now examine each of these terms and offer physical interpretations.

#### Boundary pressure torques and turbulent torques

The term  $\hat{z} \cdot (\nabla \times \mathbf{f}^{\text{nc}})$  in equation (34.132) provides a torque from boundary stresses and interior viscous stresses. The term  $g \nabla h \times \nabla \eta^{\text{eff}}$  provides a torque whenever the thickness gradients are not aligned with the gradients in the effective surface height. We can write this term in the equivalent form based on the following

$$\rho g \nabla h \times \nabla \eta^{\text{eff}} = \rho g \nabla h \times \nabla \eta + \nabla h \times \nabla p_a \quad (34.133a)$$

$$= -\nabla p_a \times \nabla \eta + \nabla p_b \times \nabla \eta + \nabla(p_b - p_a) \times \nabla p_a / (\rho g) \quad (34.133b)$$

$$= -\nabla p_a \times \nabla \eta + \nabla p_b \times \nabla[\eta + p_a / (\rho g)] \quad (34.133c)$$

$$= -\nabla p_a \times \nabla \eta + \nabla p_b \times \nabla[\eta_b + h + p_a / (\rho g)] \quad (34.133d)$$

$$= -\nabla p_a \times \nabla \eta + \nabla p_b \times \nabla \eta_b \quad (34.133e)$$

$$= \nabla \times (-p_a \nabla \eta + p_b \nabla \eta_b), \quad (34.133f)$$

where we made use of the hydrostatic relation  $p_b = p_a + \rho g h$ . We thus see that  $-g \nabla h \times \nabla \eta^{\text{eff}} = \rho^{-1} \nabla \times (p_a \nabla \eta - p_b \nabla \eta_b)$  arises from pressure torques acting on the surface and bottom of the shallow water column. These torques spin the column if there is a misalignment between the boundary pressure gradients and the boundary surface slopes.

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<sup>5</sup>Exercise 34.7 offers a particular example of a geostrophic flow that is aligned perpendicular to  $\nabla h$ , as found in a geostrophic shallow water front.

*Nonlinear transport*

The nonlinear term  $\hat{\mathbf{z}} \cdot \nabla \times [\nabla \cdot (h \mathbf{u} \otimes \mathbf{u})]$  can be written

$$\hat{\mathbf{z}} \cdot \nabla \times [\nabla \cdot (h \mathbf{u} \otimes \mathbf{u})] = \hat{z}_m \epsilon_{mst} \partial_s [\partial_n (h u_n u_t)] \quad (34.134a)$$

$$= \partial_n \partial_s [(h u_n) \epsilon_{mst} \hat{z}_m u_t] \quad (34.134b)$$

$$= \partial_n [\partial_s (h u_n) \epsilon_{mst} \hat{z}_m u_t + h u_n \zeta] \quad (34.134c)$$

$$= -\partial_n [\epsilon_{smt} \hat{z}_m u_t \partial_s (h u_n)] + \nabla \cdot (h \zeta \mathbf{u}), \quad (34.134d)$$

which exposes the divergence of the thickness weighted advective flux of relative vorticity. Further manipulations lead to

$$-\partial_n [\epsilon_{smt} \hat{z}_m u_t \partial_s (h u_n)] = -\partial_n [\epsilon_{smt} \hat{z}_m u_t u_n \partial_s h + \epsilon_{smt} \hat{z}_m u_t h \partial_s u_n] \quad (34.135a)$$

$$= \partial_n [\hat{z}_m (\epsilon_{mst} \partial_s h u_t) u_n - h \epsilon_{smt} \hat{z}_m u_t \partial_s u_n] \quad (34.135b)$$

$$= \nabla \cdot [\hat{\mathbf{z}} \cdot (\nabla h \times \mathbf{u}) \mathbf{u}] - \partial_n [h (\hat{\mathbf{z}} \times \mathbf{u}) \cdot \nabla u_n] \quad (34.135c)$$

$$= \nabla \cdot [\hat{\mathbf{z}} \cdot (\nabla h \times \mathbf{u}) \mathbf{u}] + \nabla \cdot [h (v \partial_x - u \partial_y) \mathbf{u}], \quad (34.135d)$$

so that the nonlinear term takes the form

$$\hat{\mathbf{z}} \cdot \nabla \times [\nabla \cdot (h \mathbf{u} \otimes \mathbf{u})] = \nabla \cdot [\Sigma \mathbf{u} + h (v \partial_x - u \partial_y) \mathbf{u}]. \quad (34.136)$$

The first term is the advective flux of  $\Sigma$ , and the second term is the thickness weighted transport of  $\mathbf{u}$  by the counter-clockwise rotated velocity.

### 34.10.2 Summary of the column vorticity equation

The above manipulations bring the  $\Sigma$  equation (34.132) into the Eulerian flux-form

$$\partial_t \Sigma = -\nabla \cdot \mathbf{J}^\Sigma + \rho^{-1} \hat{\mathbf{z}} \cdot \nabla \times [-p_a \nabla \eta + p_b \nabla \eta_b + \rho \mathbf{f}^{nc}], \quad (34.137)$$

where

$$\mathbf{J}^\Sigma \equiv [\Sigma + h f + h (v \partial_x - u \partial_y)] \mathbf{u} = h \zeta_a \mathbf{u} + [v (\partial_x h + h \partial_x) - u (\partial_y h + h \partial_y)] \mathbf{u} \quad (34.138)$$

is the flux of  $\Sigma$ . The corresponding material time derivative form of equation (34.137) is given by

$$\frac{D\Sigma}{Dt} + \Sigma \nabla \cdot \mathbf{u} + \nabla \cdot [h f \mathbf{u} + h (v \partial_x - u \partial_y) \mathbf{u}] = \rho^{-1} \hat{\mathbf{z}} \cdot \nabla \times [-p_a \nabla \eta + p_b \nabla \eta_b + \rho \mathbf{f}^{nc}], \quad (34.139)$$

with the thickness equation (30.81)

$$\frac{Dh}{Dt} = -h \nabla \cdot \mathbf{u} + w^{(\dot{\eta})}, \quad (34.140)$$

yielding the equivalent expression

$$h \frac{D(\Sigma/h)}{Dt} + \nabla \cdot [h f \mathbf{u} + h (v \partial_x - u \partial_y) \mathbf{u}] = -\frac{\Sigma w^{(\dot{\eta})}}{h} + \rho^{-1} \hat{\mathbf{z}} \cdot \nabla \times [-p_a \nabla \eta + p_b \nabla \eta_b + \rho \mathbf{f}^{nc}]. \quad (34.141)$$

### 34.10.3 Steady linear column vorticity balance and the island rule

To garner experience with the column vorticity equation (34.137), consider the steady state and assume  $\mathbf{J}^\Sigma$  is dominated by the planetary vorticity

$$\mathbf{J}^\Sigma \approx h f \mathbf{u}, \quad (34.142)$$

in which case equation (34.137) reduces to the balance

$$\nabla \cdot (h f \mathbf{u}) = \rho^{-1} \hat{\mathbf{z}} \cdot \nabla \times [-p_a \nabla \eta + p_b \nabla \eta_b + \rho \mathbf{f}^{nc}]. \quad (34.143)$$

Hence, torques due to interface pressures and turbulent stresses are balanced by the divergence of the thickness weighted advective flux of planetary vorticity.

#### *Formulating the integral balance*

The local balance (34.143) leads to an integral balance through an area integral over an arbitrary closed domain

$$\oint_{\mathcal{S}} \nabla \cdot (h f \mathbf{u}) d\mathcal{S} = \rho^{-1} \oint_{\mathcal{S}} \hat{\mathbf{z}} \cdot \nabla \times [-p_a \nabla \eta + p_b \nabla \eta_b + \rho \mathbf{f}^{nc}] d\mathcal{S}. \quad (34.144)$$

Making use of Gauss' divergence theorem on the left hand side and Stokes' theorem on the right hand side renders

$$\oint_{\partial\mathcal{S}} h f \mathbf{u} \cdot \hat{\mathbf{n}} d\ell = \rho^{-1} \oint_{\partial\mathcal{S}} [-p_a \nabla \eta + p_b \nabla \eta_b + \rho \mathbf{f}^{nc}] \cdot \hat{\mathbf{t}} d\ell. \quad (34.145)$$

The left hand side is a contour integral with  $\hat{\mathbf{n}}$  the outward normal along the contour. The right hand side is also a contour integral, yet with  $\hat{\mathbf{t}}$  the tangent along the contour oriented in the counter-clockwise sense. This integral balance says that the advective transport of planetary vorticity leaving the closed region (left hand side) is balanced by the oriented contour integral of the pressure and turbulent stresses.

The integral balance (34.145) is a rather remarkable statement that equates the transport leaving a region to pressure and turbulent stresses integrated along the region boundary. [Godfrey \(1989\)](#) chose a particularly clever contour, such as that depicted in Figure 34.10, and made some assumptions about the stresses that then allowed for an estimate of the transport. We here present the arguments.

#### *Assumptions about the stresses*

A portion of the red contour in Figure 34.10 traverses the eastern boundary on both Island A and Island B. As shown in Section 34.9, friction in the eastern boundary region of an ocean gyre is much less than the western boundary, motivating us to ignore friction (either viscous or bottom drag) along the eastern boundary portions of the contour. Likewise, friction is generally small for the open ocean portion along the two latitudinal lines. Hence, wind stress is the only non-conservative process that affects the right hand side of equation (34.145).

[Godfrey \(1989\)](#) furthermore ignored pressure form stresses and their associated torques. This assumption is reasonable for the atmospheric form stress,  $-p_a \nabla \eta$ , which is generally quite small (it is zero for a rigid lid approximation). However, the bottom form stress,  $p_b \nabla \eta_b$ , and the associated bottom pressure torque, can be larger than the wind stress and wind stress curl, especially near the continental margins and with strong currents. Hence, ignoring bottom pressure torque is perhaps the least satisfying assumption.

### The island rule

The islands are material surfaces so that  $\mathbf{u} \cdot \hat{\mathbf{n}} = 0$  along those portions of the contour that are adjacent to the coasts. Integrating along the northern latitude, with  $\hat{\mathbf{n}} = \hat{\mathbf{y}}$ , yields

$$f_{\text{north}} \int_{y_{\text{north}}} h v dx \equiv f_{\text{north}} \mathcal{T}, \quad (34.146)$$

where  $\mathcal{T}$  is the meridional transport. Ignoring any volume transport through the layer surface (e.g.,  $w^{(\hat{\eta})} = 0$ ), the steady transport crossing the northern boundary equals to that crossing the southern boundary, so that

$$f_{\text{south}} \int_{y_{\text{south}}} h v dx \equiv f_{\text{south}} \mathcal{T}. \quad (34.147)$$

Making use of these results in the integral balance (34.145), and following the above assumptions about the boundary stresses, leads to *Godfrey's island rule*

$$\rho \mathcal{T} = \frac{1}{f_{\text{north}} - f_{\text{south}}} \oint_{\partial S} \boldsymbol{\tau}^{\text{wind}} \cdot \hat{\mathbf{t}} d\ell, \quad (34.148)$$

where  $\boldsymbol{\tau}^{\text{wind}}$  is the wind stress, and where the minus sign on  $f_{\text{south}}$  arises since  $\hat{\mathbf{n}} = -\hat{\mathbf{y}}$  along the southern latitude contour. This expression provides an approximation to the flow around Island A, noting that the only nonzero flow normal to the contour is through the two latitudinal segments.

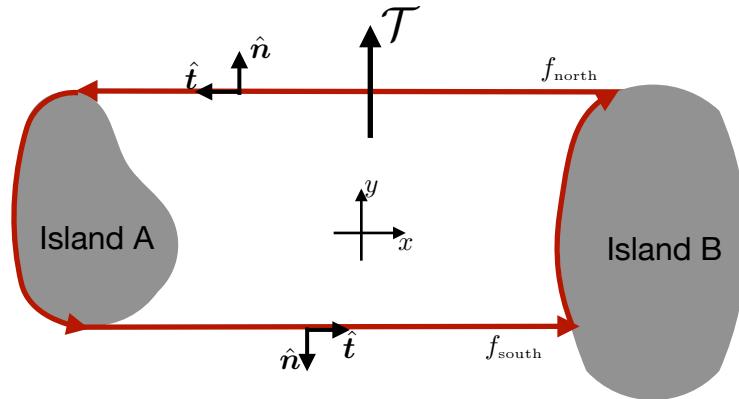


FIGURE 34.10: Illustrating the island rule with two land masses (“islands”). The red contour surrounds all of Island A and traverses along the eastern side of both Island A and Island B. The northern contour extends along a constant latitude line with a corresponding Coriolis parameter  $f_{\text{north}}$ , whereas the southern contour has Coriolis parameter  $f_{\text{south}}$ . Ignoring any precipitation or evaporation crossing the surface, steady state volume conservation means that the same meridional transport,  $\mathcal{T}$ , crosses both the southern and northern contours. Godfrey’s island rule (34.148) provides an estimate for this transport when given the wind stress along the contour.

#### 34.10.4 Further study

[Godfrey \(1989\)](#) applied the island rule (34.148) to estimate transport around Austral-Asia, New Zealand, and Malagasy. Further discussion of Godfrey’s island rule can be found in [Tomczak and Godfrey \(1994\)](#), [Pedlosky et al. \(1997\)](#), and [Klinger and Haine \(2019\)](#).

## 34.11 Exercises

### EXERCISE 34.1: FLOW NEAR A TOPOGRAPHIC BUMP IN A REDUCED GRAVITY MODEL

Elements of this exercise are motivated by Figure 2 from [Adcock and Marshall \(2000\)](#) and Figure 1 from [Marshall et al. \(2012\)](#), where we consider a reduced gravity model with a dynamic lower layer and stagnant upper layer. Place a topographic bump (e.g., seamount or mountain) fully within the lower layer as shown in Figure 34.11.

- Following Exercise 30.4, derive the momentum and thickness equations for a reduced gravity model with a stagnant upper layer. Then derive the potential vorticity equation for the dynamical layer.
- Now assume an  $f$ -plane. If the lower layer potential vorticity is (somehow) horizontally homogenized (e.g., some form of mixing produces a horizontally constant PV), draw the resulting layer interface  $\eta_1$ . Assume the relative vorticity is negligible compared to the planetary vorticity so that the flow satisfies the planetary geostrophic scaling introduced in Section 34.6.2 and further pursued in Section 38.4. Also, ignore any non-steady processes; we are only interested here in the steady flow.
- For the case of horizontally homogenized potential vorticity from the previous part, what is the direction for a geostrophically balanced flow: cyclonic or anti-cyclonic? Hint: make use of Exercise 30.4 for the momentum equation of an inverted reduced gravity model.

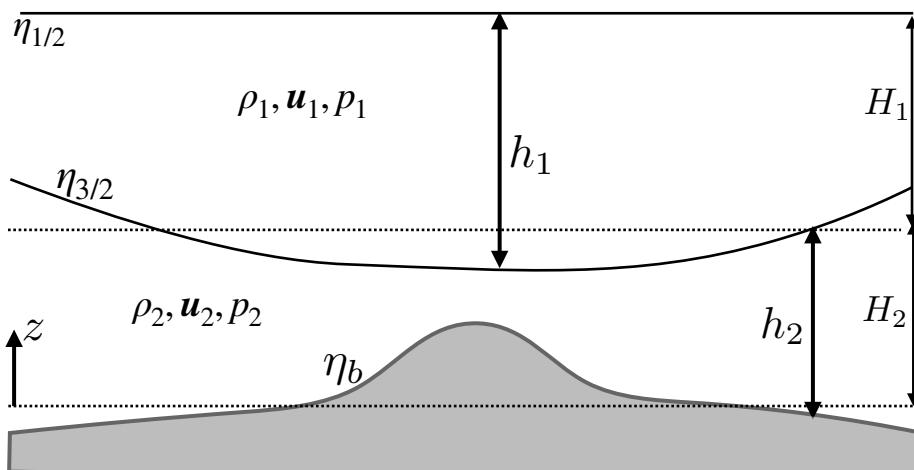


FIGURE 34.11: A reduced gravity model (see Section 30.3) with a stagnant upper layer and a dynamic lower layer as in Exercise 30.4. A seamount sits fully within the lower layer.

### EXERCISE 34.2: PV FOR TWO SHALLOW WATER LAYERS

Consider the inviscid Boussinesq two-layer shallow water model as discussed in Section 30.4. Derive the potential vorticity equation for each layer, showing the mathematical steps used in the derivation. Hint: the answer is given in Section 34.4.6.

### EXERCISE 34.3: AVERAGE VORTICITY IN A SHALLOW WATER LAYER

Consider a single layer of shallow water fluid on a rotating plane with rotation rate  $\Omega = \hat{\mathbf{z}}\Omega$ . Assume the fluid is contained in an arbitrary horizontal region and that it has a constant total

volume given by

$$\mathcal{V} = \int \left[ \int dz \right] d\mathcal{S} = \int h d\mathcal{S} = \int (H + \Delta\eta - \eta_b) d\mathcal{S} = H \mathcal{S}, \quad (34.149)$$

where  $\mathcal{S}$  is the horizontal area of the domain,  $h(x, y, t) = H + \Delta\eta(x, y, t) - \eta_b(x, y)$  is the layer thickness,  $H$  is the resting depth relative to  $z = 0$ ,  $\Delta\eta$  is the sea level deviation from resting, and  $\eta_b$  is the undulation of the bottom topography (see Figure 30.1). Additionally, recall that  $z = 0$  is set according to

$$\int \eta_b d\mathcal{S} = 0, \quad (34.150)$$

and volume conservation ensures that

$$\int \Delta\eta d\mathcal{S} = 0. \quad (34.151)$$

- (a) Determine the volume average of the vorticity  $\hat{\mathbf{z}} \cdot \boldsymbol{\omega}_{\text{solid}}$  arising from the solid-body rotation

$$\langle \hat{\mathbf{z}} \cdot \boldsymbol{\omega}_{\text{solid}} \rangle = \mathcal{V}^{-1} \int \hat{\mathbf{z}} \cdot \boldsymbol{\omega}_{\text{solid}} dV. \quad (34.152)$$

- (b) Determine the area average of the relative vorticity,

$$\bar{\zeta} = \mathcal{S}^{-1} \int \hat{\mathbf{z}} \cdot \boldsymbol{\omega} d\mathcal{S}, \quad (34.153)$$

in terms of the circulation around the boundary of the domain.

- (c) Determine the volume average of the relative vorticity

$$\langle \zeta \rangle = \mathcal{V}^{-1} \int \hat{\mathbf{z}} \cdot \boldsymbol{\omega} dV. \quad (34.154)$$

Write the expression in terms of the area average vorticity,  $\bar{\zeta}$ , and the correlation,  $\overline{\zeta' h'}$ , where primes are deviations from the area mean.

#### EXERCISE 34.4: APPLICATIONS OF SHALLOW WATER PV CONSERVATION

In an adiabatic shallow water fluid in a rotating reference frame, show that the potential vorticity conservation law is

$$\frac{D}{Dt} \left[ \frac{\zeta + f}{\eta - \eta_b} \right] = 0, \quad (34.155)$$

where  $\eta$  is the height of the free surface and  $\eta_b$  is the height of the bottom topography (see Figure 30.1). For both of the following questions, assume constant volume for the fluid column. Also, assume the column rotates about its axis as a solid-body.

- (a) A cylindrical column of air at  $30^\circ$  latitude with radius 100 km expands horizontally to twice its original radius. If the air is initially at rest, what is the mean tangential velocity at the perimeter after the expansion?
- (b) An air column at  $60^\circ\text{N}$  with zero relative vorticity ( $\zeta = 0$ ) stretches from the surface to the tropopause, which we assume is a rigid lid at 10 km. The air column moves zonally onto a plateau 2.5 km high. What is its relative vorticity? Suppose it then moves southward along the plateau to  $30^\circ\text{N}$ , starting from the relative vorticity it obtained from the plateau. What is its new relative vorticity?

## EXERCISE 34.5: APPLICATION OF SHALLOW WATER PV CONSERVATION

An air column at 60°N with  $\zeta = 0$  initially reaches from the surface to a fixed tropopause at 10 km height. If the air column moves across a mountain 2.5 km high at 45°N, what is its absolute vorticity and relative vorticity as it passes the mountaintop? Hint: Use PV conservation for a shallow-water fluid, and assume the top of the column remains at 10 km.

## EXERCISE 34.6: SOME PROPERTIES OF THE STEADY STATE SHALLOW WATER FLUID

Consider a single layer of shallow water fluid in steady state (i.e., all Eulerian time derivatives vanish).

- (a) Show that there exists a streamfunction for the steady state thickness weighted horizontal flow

$$h \mathbf{u} = \hat{\mathbf{z}} \times \nabla \Psi. \quad (34.156)$$

- (b) What are the physical dimensions of  $\Psi$ ?

- (c) Show that the shallow water potential vorticity is a constant along the steady state streamlines of the thickness weighted flow

$$Q = Q(\Psi). \quad (34.157)$$

- (d) Show that the Bernoulli function,

$$B = g \eta + \mathbf{u} \cdot \mathbf{u}/2 \quad (34.158)$$

is also a constant along the same streamlines; i.e.,

$$B = B(\Psi). \quad (34.159)$$

- (e) What is the functional relation between the Bernoulli function and the potential vorticity?

Hint: make use of the physical dimensions for  $Q$ ,  $B$ , and  $\Psi$  to be sure that your solution is dimensionally consistent.

## EXERCISE 34.7: ZONALLY SYMMETRIC SHALLOW WATER FRONT

Consider a single layer of shallow water fluid on a  $\beta$ -plane with a flat bottom. Assume all fields possess zonal symmetry as in the zonal front shown in Figure 34.12. Since the zonal pressure gradient vanishes under the assumption of zonal symmetry, the geostrophic portion of the meridional velocity vanishes. However, there is generally a non-zero ageostrophic component to this velocity, and we retain that possibility throughout this exercise.

- (a) Write the potential vorticity,  $Q$ , assuming the zonal flow is in geostrophic balance. Write  $Q$  terms of meridional derivatives of the layer thickness.
- (b) From the shallow water equations, explicitly show that the PV is materially constant (i.e., it is a Lagrangian invariant). To do so, work through the usual shallow water PV conservation derivation yet make use of the zonally symmetric equations of motion. Allow for a nonzero ageostrophic meridional flow. Show all relevant steps.
- (c) Show that the potential vorticity can be written as  $Q = -(\partial_y M)/h$ , where  $h$  is the layer thickness. What is the expression for  $M$ ? Hint: recall our discussion of potential momentum in Section 10.4.
- (d) Potential vorticity is not the only material constant for this system. Due to the zonal symmetry, Noether's Theorem indicates there is another. Show that  $M$  is materially constant. Again, continue to allow for a nonzero meridional velocity component.

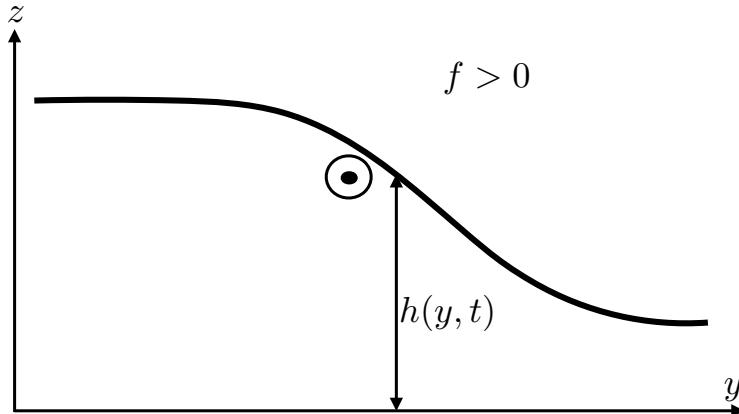


FIGURE 34.12: Schematic of a zonally symmetric front in a shallow water layer in the northern hemisphere ( $f > 0$ ), here used for Exercise 34.7. The thickness decreases to the north. If the zonal flow is in geostrophic balance, then the northward pressure gradient is in geostrophic balance with a southward Coriolis acceleration arising from an eastward (out of the page) geostrophic current (see also Figure 31.1). The geostrophic component of the meridional flow vanishes due to zonal symmetry, but the full meridional flow need not vanish if there are ageostrophic processes. We allow for the possibility of a nonzero meridional velocity throughout this exercise.

#### EXERCISE 34.8: RAYLEIGH DRAG AND GALILEAN INVARIANCE

Recall the discussion of Galilean invariance from Section 12.6. Is the Rayleigh drag used in equation (34.108) Galilean invariant? Why? If not, then should that be of concern for its use in studying flow in a closed and bounded domain?

#### EXERCISE 34.9: GYRES IN THE PRESENCE OF CYCLONIC WINDS

Consider the ocean gyre discussion in Section 34.9. Rather than anti-cyclonic winds, now apply a cyclonic wind stress to the domain. As per the circulation theorem (34.110), the gyre flow will have a cyclonic sense. Will the resulting gyre exhibit eastern intensification or western? Appeal to whatever arguments you wish.

#### EXERCISE 34.10: GEOSTROPHIC ADJUSTMENT (BASED ON EXERCISE 4.6 OF [Vallis \(2019\)](#))

Consider the linear geostrophic adjustment problem on an  $f$ -plane with a single layer of shallow water fluid over a flat bottom. Rather than assume an initial free surface profile, as we did in Section 34.7, here we assume an initial meridional velocity profile given by

$$v(x, t = 0) = v_0 \operatorname{sgn}(x) = v_0 (2 \mathcal{H}(x) - 1), \quad (34.160)$$

where  $v_0$  is a constant,  $\operatorname{sgn}$  is the sign-function (equation (34.80)), and  $\mathcal{H}$  is the Heaviside step function (equation (34.82)). The free surface is assumed to be initially flat.

- (a) Show that the linearized potential vorticity (equation (31.177)) is given by

$$q(x) = 2 v_0 \delta(x), \quad (34.161)$$

where  $\delta(x)$  is the Dirac delta distribution whose dimensions are inverse length.

- (b) As we did in Section 34.7, solve for the geostrophic streamfunction  $\psi = g \eta / f$ .  
(c) Discuss this solution and draw a sketch of  $\psi$  and  $v$ .

Here are some hints.

- We discuss properties of the Dirac distribution in Section 4.2. However, to answer the first part of this question it is sufficient to know that the derivative of the Heaviside step function

(a dimensionless step function) is the Dirac delta distribution

$$\delta(x) = \frac{d\mathcal{H}(x)}{dx}, \quad (34.162)$$

so that the Dirac delta distribution has dimensions of inverse length.

- For the second part, note that the streamfunction is exponentially decaying on either side of the  $x = 0$  according to  $\psi = \psi_0 e^{-|x|/L_d}$ , which then leads to a jump in the derivative approaching the origin from each side. Carefully use equations (34.162) and (34.91) to determine  $\psi_0$ .

#### EXERCISE 34.11: SHALLOW WATER EQUATIONS WITH DIVERGENCE-DAMPING

When breaking the continuous symmetry of the equations of motion, a discretized numerical simulation admits unphysical flow features sometimes referred to as *computational modes*. Some computational modes can evolve in time with energy accumulating at high wave numbers, in which case the numerical simulation produces unphysical grid noise and becomes of little physical use. To suppress grid noise, numerical models commonly introduce numerical dissipation, even if the continuous equations have zero dissipation. The formulation of numerical dissipation is largely an art guided by the dual needs of suppressing grid noise without otherwise damaging physical properties of the simulated flow. We here consider physical properties of a specific form of numerical dissipation known as *divergence-damping*. We work within the framework of the continuous equations so to develop generic physical properties of the divergence-damping operator. No knowledge of numerical methods is required to solve this problem.

Divergence-damping is motivated by the desire to leave the vorticity equation untouched while damping divergent motion that can arise in numerical simulations. This motivation is based on noting that much of the large-scale circulation in a rotating fluid has a nontrivial absolute vorticity yet a relatively small horizontal divergence. For example, geostrophic flow on an  $f$ -plane has vorticity dominated by planetary vorticity  $f$ , while it has zero horizontal divergence (see Section 25.4 or the 2d barotropic equation in Section 33.1). The divergence-damping operator is thus designed to reduce the magnitude of the horizontal divergence while leaving the vorticity untouched.

We here examine the impacts of divergence-damping on mechanical energy and angular momentum. For this purpose, consider a single layer of shallow water fluid with divergence-damping. This system is described by the momentum and thickness equations

$$\frac{D\mathbf{u}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla(g\eta + \alpha\Gamma) \quad (34.163a)$$

$$\frac{Dh}{Dt} = -h\nabla \cdot \mathbf{u}. \quad (34.163b)$$

The parameter  $\alpha > 0$  is a constant and the field  $\Gamma$  is given by the Laplacian of the horizontal flow divergence

$$\Gamma = \nabla^2 \mathcal{D}, \quad (34.164)$$

where

$$\mathcal{D} = \nabla \cdot \mathbf{u}. \quad (34.165)$$

The divergence has physical dimensions of inverse time ( $T^{-1}$ ), so that its Laplacian,  $\Gamma$ , has dimensions of  $L^{-2} T^{-1}$ , and the coefficient  $\alpha$  has dimensions  $L^4 T^{-1}$ .

Divergence damping leads to a modification to the horizontal pressure gradient. We may think

of this modification as arising from the horizontal gradient of a modified free surface height

$$\tilde{\eta} = \eta + \frac{\alpha \Gamma}{g}. \quad (34.166)$$

Notably, mass conservation remains the same since the thickness equation is unchanged. Hence, momentum evolution is modified by changing the pressure gradient, yet the thickness equation remains the same.

- (a) Show that the vorticity equation (34.15) remains unchanged in the presence of divergence-damping.
- (b) Show that the potential vorticity equation (34.36) remains unchanged in the presence of divergence-damping.
- (c) Show that the horizontal divergence evolves according to

$$\frac{\partial \mathcal{D}}{\partial t} = \left[ \frac{\partial \mathcal{D}}{\partial t} \right]_{\alpha=0} - \alpha \nabla^2 \Gamma. \quad (34.167)$$

- (d) Show that the evolution of gravitational potential energy per horizontal area

$$\mathcal{P} = g \rho \int_{\eta_b}^{\eta} z \, dz \quad (34.168)$$

remains unchanged from that determined in Section 31.3.1.

- (e) Show that the kinetic energy per horizontal area evolves according to

$$\frac{\partial \mathcal{K}}{\partial t} + \nabla \cdot (\mathbf{u} \mathcal{K}) = -h \rho g \nabla \tilde{\eta}, \quad (34.169)$$

where

$$\mathcal{K} = \frac{1}{2} \int_{\eta_b}^{\eta} \rho \mathbf{u}^2 \, dz = \rho h \mathbf{u}^2 / 2, \quad (34.170)$$

is the horizontal kinetic energy per area (Section 31.3.2).

- (f) Determine the evolution equation for global integrated kinetic energy

$$\frac{\partial}{\partial t} \left[ \int \mathcal{K} \, dA \right] = \frac{\partial}{\partial t} \left[ \int \int_{\eta_b}^{\eta} (\rho \mathbf{u} \cdot \mathbf{u} / 2) \, dz \, dA \right]. \quad (34.171)$$

Hint: drop all lateral boundary terms by assuming either solid lateral walls or periodicity.

- (g) Consider a single shallow water layer in a rotating tank as in Section 31.7. Show that the material evolution of angular momentum relative to the vertical rotational axis is given by

$$\frac{1}{\delta M} \frac{DL^z}{Dt} = -g \frac{\partial \eta}{\partial \phi} + \mathcal{T}. \quad (34.172)$$

What is the mathematical form for  $\mathcal{T}$ ? Hint: check your answer with the next part of this exercise.

- (h) Show that the domain integrated angular momentum satisfies the equation

$$\frac{\partial}{\partial t} \int L^z = \alpha \rho \int \Gamma \frac{\partial \eta}{\partial \phi} dA. \quad (34.173)$$

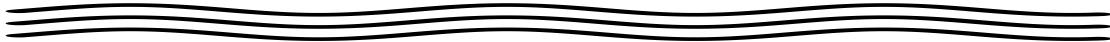
where we assume the bottom topography is flat so that  $h = \eta$ .

- (i) The linearized thickness equation (see Section 31.8) for a flat bottom is given by

$$\frac{\partial \eta}{\partial t} + H \nabla \cdot \mathbf{u} = 0, \quad (34.174)$$

where  $H$  is the thickness of the resting fluid layer. Show that the time change for the global integrated angular momentum is given by

$$\frac{\partial}{\partial t} \int L^z = -\frac{\alpha \rho}{H} \int \left[ \frac{\partial}{\partial t} \nabla^2 \eta \right] \frac{\partial \eta}{\partial \phi} dA. \quad (34.175)$$





# Chapter 35

## Vorticity mechanics

In this chapter we study the kinematics and dynamics of vorticity and circulation, extending the shallow water discussion of Chapter 34 to three-dimensional continuously stratified flows. To ground the conceptual presentation, we include sample applications of particular importance to geophysical flows. An understanding of vorticity mechanics offers many insights into the nature of fluid flow and how that flow is constrained. Hence, vorticity is a central feature in nearly all theories of fluid mechanics, including many arising in geophysical fluids.

In making use of vorticity for geophysical fluids, particularly for the ocean, it is common to move beyond the vorticity of a fluid element as defined by the curl of the velocity field. For example, as a means to summarize facets of the vorticity contained within a three-dimensional fluid, we study the depth integral of the vorticity equation in Section 35.9 for a hydrostatic and Boussinesq fluid and in Section 39.5 for a planetary geostrophic flow. This analysis has its most common application to the ocean where the vertical domain is bounded and with vertical columns extending from the bottom at  $z = \eta_b$  to the surface at  $z = \eta$ . Relatedly, there are occasions to study vorticity of the depth integrated or depth averaged flow, and we do so in Section 35.10. Such studies emphasize the importance of boundary forces and their curls (“torques”) for the vorticity of a fluid column.

### CHAPTER GUIDE

This chapter assumes an understanding of vorticity developed in earlier chapters in this part of the book. We also make use of fluid kinematics from Part III and fluid dynamics from Part IV. As for the shallow water vorticity discussed in Chapter 34, we here make use of vector calculus identities for Cartesian coordinates as detailed in Chapter 2. The concepts and methods developed in this chapter are fundamental to the notions of vorticity and circulation, much of which is encountered in the remainder of this part of the book and elsewhere such as the balanced models considered in Part VII.

Throughout this chapter, when considering spherical geometry, we make use of the planetary Cartesian coordinates from Figure 8.1. Since the sphere is assumed to be embedded in Euclidean space, we can naively perform integrals of vectors over the Euclidean space.

35.1 Loose threads . . . . .	868
35.2 Kinematics of vortex lines and vortex tubes . . . . .	869
35.2.1 Vortex lines and vortex tubes . . . . .	869
35.2.2 Kinematic properties . . . . .	869

35.2.3	Helmholtz's theorems . . . . .	870
35.2.4	Further study . . . . .	872
35.3	Kelvin's circulation theorem . . . . .	<b>872</b>
35.3.1	Formulation . . . . .	872
35.3.2	Barotropic flow . . . . .	873
35.3.3	Pressure gradient force for barotropic fluids . . . . .	874
35.4	Vorticity dynamics . . . . .	<b>874</b>
35.4.1	Vector-invariant velocity equation . . . . .	874
35.4.2	Basic form of the vorticity equation . . . . .	875
35.4.3	Massaged form of the vorticity equation . . . . .	875
35.4.4	Flux-form evolution equation for vorticity components . . . . .	876
35.4.5	Vorticity, angular momentum, and torques . . . . .	877
35.5	Mechanics of baroclinicity . . . . .	<b>877</b>
35.5.1	Curl of the pressure gradient body force . . . . .	878
35.5.2	Kelvin's circulation theorem and contact pressure forces . . . . .	879
35.5.3	Bottom pressure contributions at the solid-earth boundary . . . . .	879
35.5.4	Further study . . . . .	880
35.6	Vorticity filaments and material line elements . . . . .	<b>881</b>
35.6.1	Vortex filaments evolve through the rate of strain . . . . .	881
35.6.2	Frozen-in nature of vorticity . . . . .	882
35.6.3	Stretching and tilting of vortex tubes . . . . .	882
35.6.4	Comments . . . . .	885
35.7	Circulation and vorticity for rotating fluids . . . . .	<b>885</b>
35.7.1	Material evolution of absolute circulation . . . . .	886
35.7.2	The beta effect . . . . .	887
35.7.3	A two-dimensional incompressible fluid . . . . .	889
35.7.4	Further study . . . . .	890
35.8	Vorticity in a hydrostatic and Boussinesq fluid . . . . .	<b>890</b>
35.8.1	Deriving the vorticity equation . . . . .	891
35.8.2	Boussinesq baroclinicity . . . . .	892
35.8.3	Vertical vorticity equation . . . . .	893
35.9	Depth integral of the vertical vorticity equation . . . . .	<b>894</b>
35.9.1	Comments on the baroclinicity source . . . . .	894
35.9.2	Leibniz rule expressions . . . . .	895
35.9.3	Bottom boundary contribution . . . . .	895
35.9.4	Surface boundary contribution . . . . .	897
35.9.5	Comments . . . . .	897
35.10	Vorticity for the depth integrated horizontal flow . . . . .	<b>898</b>
35.10.1	Comparing the two vorticities . . . . .	898
35.10.2	Evolution of vorticity for the depth integrated horizontal flow . . . . .	899
35.10.3	Boundary pressure torques . . . . .	899
35.10.4	Steady state vorticity budget . . . . .	901
35.10.5	Formulation based on the vector invariant velocity equation . . . . .	902
35.10.6	Vorticity of the depth averaged flow . . . . .	903
35.10.7	Comments and further study . . . . .	904
35.11	Exercises . . . . .	<b>904</b>

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## 35.1 Loose threads

- Rewrite Section 35.9 using the full vertical vorticity equation derived in Section 35.4.4. The only difference is the presence of a component of baroclinicity,  $-\hat{z} \times \rho^{-1} \nabla p$ .
- Contour integral around streamline contours as in Styles, Bell, Marshall, Storkey JAMES paper.

## 35.2 Kinematics of vortex lines and vortex tubes

We here develop the basics of vorticity kinematics, with this discussion closely following from the kinematics of material line elements discussed in Section 13.3.3.

### 35.2.1 Vortex lines and vortex tubes

A *vortex line* is a line drawn through the fluid that is tangent, at each instance in time, to the vorticity at each spatial point. A vortex line is mathematically parameterized just like any other line, whereby we write the spatial coordinates along the line as a function of a suitable parameter  $\varphi$  (e.g., the arc-length)

$$\mathbf{x}(\varphi) = x(\varphi) \hat{\mathbf{x}} + y(\varphi) \hat{\mathbf{y}} + z(\varphi) \hat{\mathbf{z}}. \quad (35.1)$$

Correspondingly, the tangent vector for the line is given by

$$\frac{d\mathbf{x}(\varphi)}{d\varphi} = \frac{dx(\varphi)}{d\varphi} \hat{\mathbf{x}} + \frac{dy(\varphi)}{d\varphi} \hat{\mathbf{y}} + \frac{dz(\varphi)}{d\varphi} \hat{\mathbf{z}}. \quad (35.2)$$

The three coordinates of the line are constrained so that the tangent is parallel to vorticity at each point so that

$$\frac{d\mathbf{x}(\varphi)}{d\varphi} \times \boldsymbol{\omega} = 0, \quad (35.3)$$

which is satisfied by the following constraint

$$\frac{dx/d\varphi}{\omega_x} = \frac{dy/d\varphi}{\omega_y} = \frac{dz/d\varphi}{\omega_z}. \quad (35.4)$$

These equations are directly analogous to those satisfied by velocity streamlines (Section 12.8.2)

$$\frac{dx/d\varsigma}{u} = \frac{dy/d\varsigma}{v} = \frac{dz/d\varsigma}{w}, \quad (35.5)$$

where  $\varsigma$  is the parameter along the streamline. Notably, the velocity is not constant along a velocity streamline, nor is vorticity constant along a vortex line. In a steady state, streamlines map the trajectory of a fluid particle (see Section 12.8). However, a vortex line does not offer an interpretation in terms of trajectories.

A *vortex tube* is a bundle of vortex lines that pass through a simple closed curve, with Figure 35.1 illustrating a sample tube. By definition, the sides of the vortex tube are parallel to the vorticity field, since the sides are constructed from vortex lines. We defined a similar notion, the streamtube, for a non-divergent velocity field in Figure 12.5.

### 35.2.2 Kinematic properties

Vorticity has zero divergence

$$\nabla \cdot \boldsymbol{\omega} = \nabla \cdot (\nabla \times \mathbf{v}) = 0, \quad (35.6)$$

which follows since the divergence of a curl vanishes. Integrating the non-divergence relation over an arbitrary closed volume within the fluid leads to

$$\int_{\mathcal{R}} \nabla \cdot \boldsymbol{\omega} dV = \oint_{\partial\mathcal{R}} \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S} = 0, \quad (35.7)$$

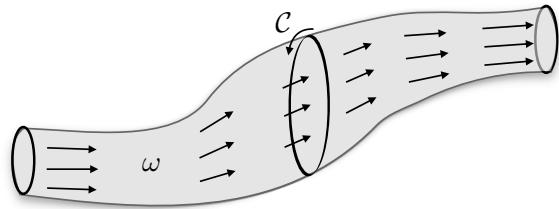


FIGURE 35.1: A vortex line is a line in the fluid that is everywhere tangent to the vorticity vector. A vortex tube is the accumulation of vortex lines passing through a closed loop. A vortex tube is sometimes referred to as a vortex filament. We here depict a vortex tube within the fluid and illustrate the circulation around the tube  $C = \oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{r} = \int \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S}$ . Since vorticity has zero divergence, the circulation is the same for any loop around the vortex tube (Helmholtz's first theorem from Section 35.2.3). A uniform circulation along the tube means that the magnitude of the vorticity is larger in regions where the tube has a small area and conversely where the tube has a large area.

where we made use of Gauss's divergence theorem to reach the surface integral expression, with  $\hat{\mathbf{n}} d\mathcal{S}$  the oriented area element on the boundary of the volume,  $\partial\mathcal{R}$ , and  $\hat{\mathbf{n}}$  the outward normal on the boundary. This result means there is no net vorticity entering or leaving an arbitrary closed region. That is, there is a vanishing net integrated “flux” of vorticity across the closed region. Consequently, there are no sources or sinks of vorticity within the fluid. In turn, there is no accumulation of vorticity within any arbitrary closed region.

Now specialize the surface integral in equation (35.7) to a volume along a chosen vortex tube such as in Figure 35.1.<sup>1</sup> The two ends of the tube generally have different cross-sectional areas. The integral over the sides of the vortex tube vanishes, since the vorticity is parallel to the tube sides. Hence, the surface integral only picks up contributions from the two ends of the tube

$$\int_A \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S}_A + \int_B \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S}_B = 0. \quad (35.8)$$

Note that the outward normals point in the opposite direction, so that we see that the flux of vorticity is independent of position along the tube. Correspondingly, Stoke's theorem transfers the vorticity constraint to a constraint on the circulation around the circumference of the tube, so that

$$\oint_A \mathbf{v} \cdot d\mathbf{r} + \oint_B \mathbf{v} \cdot d\mathbf{r} = 0. \quad (35.9)$$

We thus see that the circulation around the vortex tube is the same no matter where it is computed. The circulation constraints (35.8) and (35.9) are kinematic, holding for any vorticity field. We now consider some consequences of this constraint.

### 35.2.3 Helmholtz's theorems

There are a few basic properties of vorticity that follow from its vanishing divergence. These properties are known as Helmholtz's theorems.

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<sup>1</sup>In Exercise 16.7, we developed a similar set of results for a streamtube in an incompressible fluid.

### Helmholtz's first theorem

Since the cross-sectional slices used to derive the circulation constraint (35.9) are arbitrary, the constraint holds throughout the full extent of the vortex tube. Hence, as noted following equation (35.9), the circulation is the same for any position along the vortex tube; i.e., the strength of a vortex tube is constant along its length (see Figure 35.1). This result is known as *Helmholtz's first theorem*.

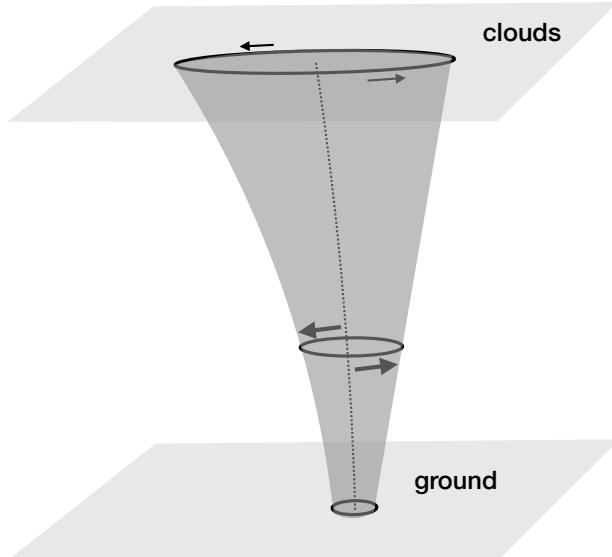


FIGURE 35.2: A vortex tube idealization of a tornado. Since the circulation around the tube is uniform (Helmholtz's first theorem), the tangential velocity of a fluid particle has a larger magnitude in regions where the vortex area is smaller, such as near the ground. As the tornado reaches into the clouds, it generally has a larger cross-sectional area and thus a smaller magnitude for the tangential velocity.

As a corollary, we refer to the vorticity constraint (35.8) to note that changes in the vortex tube cross-sectional area are compensated by changes in vorticity. For example, let the vortex tube shrink over some region. To maintain constant circulation along the tube, the vorticity magnitude must increase where the area decreases, which in turn means that the velocity circulating around the tube increases in magnitude as the area reduces. Think of a tornado as in Figure 35.2, which is a natural expression of a vortex tube. Near the ground, the cross-sectional area of the tornado is small, with the tangential velocity of a fluid particle within the tube relatively large. Near the tornado top, the cross-sectional area is large so the tangential velocity is relatively small.

### Helmholtz's second theorem

The vorticity constraint (35.8) cannot be satisfied by a finite vorticity if the area of a vortex tube vanishes anywhere. Hence, a vortex tube cannot begin or end within the fluid. This result follows from the absence of vortex sources and sinks within the fluid. Hence, a vortex tube can only loop with itself (e.g., a smoke ring as in Figure 35.3), or intersect a boundary (as for a tornado in Figure 35.2, where the ground and clouds form the boundary).

### Helmholtz's third theorem

Helmholtz's third theorem states that an unforced inviscid barotropic fluid that has zero vorticity remains irrotational forever. This theorem is a special case of Kelvin's circulation theorem, which

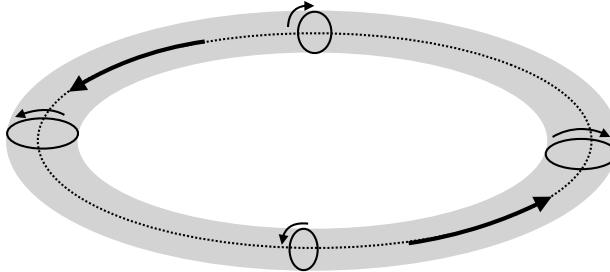


FIGURE 35.3: A vortex ring (torus) is a vortex tube that closes on itself. We here depict a vortex ring with vorticity pointing counter-clockwise around the ring. The tangential velocity is oriented as shown so that the vorticity points according to the right hand rule. That is, orient the fingers on the right hand according to the tangential velocity. The thumb of the right hand then points in the direction of the vorticity vector.

is discussed in Section 35.3.

#### 35.2.4 Further study

A particularly insightful and pedagogical discussion of these ideas can be found in Chapter 5 of [Acheson \(1990\)](#). Additionally, the following videos offer laboratory demonstrations of vorticity in non-rotating and rotating flows.

- Helmholtz's theorems are vividly exhibited [by this video](#) from the *Physics Girl* of flow generated by a paddle in a swimming pool. She also discusses vortex rings in [this video](#).
- Vorticity and Helmholtz's theorems are also described by [this classic video from Prof. Shapiro](#).
- A rotating tank experiment shown near the 15 minute mark of [this video from Prof. Fultz](#) shows how vorticity is affected by vortex stretching.
- [This video](#) offers a classic tutorial on vorticity in non-rotating fluids from Prof. Shapiro.

### 35.3 Kelvin's circulation theorem

Kelvin's circulation theorem is concerned with the evolution of circulation around a closed material loop, or equivalently (through Stokes' theorem) with the change in vorticity penetrating the enclosed area

$$\frac{dC}{dt} = \frac{d}{dt} \oint_{\partial\mathcal{S}(\mathbf{v})} \mathbf{v} \cdot d\mathbf{r} = \frac{d}{dt} \int_{\mathcal{S}(\mathbf{v})} \boldsymbol{\omega} \cdot \hat{\mathbf{n}} dS, \quad (35.10)$$

where  $\mathcal{S}(\mathbf{v})$  designates a surface whose points all move with the fluid flow. We here consider the case of non-rotating flow and extend to the rotating case in Section 35.7.

#### 35.3.1 Formulation

We are here concerned with circulation for material loops. Hence, the time derivative acting on the circulation integral in equation (35.10) moves inside the integral as a material time operator

$$\frac{dC}{dt} = \frac{d}{dt} \oint_{\partial\mathcal{S}(\mathbf{v})} \mathbf{v} \cdot d\mathbf{r} = \oint_{\partial\mathcal{S}(\mathbf{v})} \frac{D(\mathbf{v} \cdot d\mathbf{r})}{Dt}. \quad (35.11)$$

The material evolution of  $\mathbf{v}$  is determined by Newton's law of motion, which for a non-rotating flow is given by (see Section 21.9)

$$\frac{D\mathbf{v}}{Dt} = -\frac{1}{\rho} \nabla p - \nabla \Phi + \mathbf{F}. \quad (35.12)$$

In this equation,  $p$  is the pressure,  $\rho$  is the mass density,  $\Phi$  is the geopotential (and/or the potential for any conservative force), and  $\mathbf{F}$  is the acceleration from any non-conservative forces such as from viscous stresses and/or boundary interactions.

The material time derivative of the differential line element moving around the circuit equals to the differential of the velocity on the circuit

$$\frac{D(d\mathbf{r})}{Dt} = d\mathbf{v}. \quad (35.13)$$

This result follows since all points along the circuit are defined by fluid particles. Consequently, evolution of circulation following a material loop becomes

$$\frac{dC}{dt} = \frac{d}{dt} \oint_{\partial\mathcal{S}(\mathbf{v})} \mathbf{v} \cdot d\mathbf{r} \quad (35.14a)$$

$$= \oint_{\partial\mathcal{S}(\mathbf{v})} \left[ \left( -\frac{1}{\rho} \nabla p - \nabla \Phi + \mathbf{F} \right) \cdot d\mathbf{r} + \frac{1}{2} d\mathbf{v}^2 \right] \quad (35.14b)$$

$$= \oint_{\partial\mathcal{S}(\mathbf{v})} \left[ -\frac{1}{\rho} \nabla p + \mathbf{F} \right] \cdot d\mathbf{r} \quad (35.14c)$$

$$= \int_{\mathcal{S}(\mathbf{v})} \left[ -\nabla \times \left( \frac{1}{\rho} \nabla p \right) + \nabla \times \mathbf{F} \right] \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (35.14d)$$

$$= \int_{\mathcal{S}(\mathbf{v})} (\mathbf{B} + \nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (35.14e)$$

The third equality follows since  $\nabla \Phi \cdot d\mathbf{r} = d\Phi$  has zero integral around a closed circuit, as does  $d\mathbf{v}^2$ . The fourth equality made use of Stokes' theorem. The final equality introduced the *baroclinicity vector*

$$\mathbf{B} = \frac{\nabla \rho \times \nabla p}{\rho^2}, \quad (35.15)$$

which has physical dimensions of inverse squared time,  $T^{-2}$ . Equation (35.14e) says that the circulation around a material loop is affected by two processes: baroclinicity and the curl of any non-conservative (e.g., friction) forces.

### 35.3.2 Barotropic flow

The solenoidal/baroclinicity vector vanishes for a constant density fluid, in which  $\nabla \rho = 0$  such as for a single layer of shallow water fluid. More generally, the baroclinicity vector vanishes for barotropic flow, in which

$$p = p(\rho) \implies \text{barotropic flow.} \quad (35.16)$$

Kelvin's theorem then follows, which states that for inviscid barotropic flow the circulation around any closed material circuit remains constant

$$\frac{dC}{dt} = \frac{d}{dt} \oint_{\partial\mathcal{S}(\mathbf{v})} \mathbf{v} \cdot d\mathbf{r} = \frac{d}{dt} \int_{\mathcal{S}(\mathbf{v})} \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S} = 0 \quad \iff \text{inviscid barotropic flow.} \quad (35.17)$$

That is, the circulation around any vortex tube in a perfect barotropic fluid moves in a manner that keeps the circulation materially constant. This remarkable result greatly constrains the motion of a perfect barotropic fluid.

### 35.3.3 Pressure gradient force for barotropic fluids

As noted above, a barotropic fluid has pressure that is a function just of density, and conversely the density is a function just of the pressure. Hence, the curl of the pressure gradient force vanishes

$$\nabla \times (\rho^{-1} \nabla p) = 0 \quad (35.18)$$

and there is a corresponding scalar potential for the pressure gradient force

$$\nabla \Phi_p = \rho^{-1} \nabla p. \quad (35.19)$$

Integration renders<sup>2</sup>

$$\Phi_p = \int_{p_0}^p \frac{dp'}{\rho(p')}, \quad (35.20)$$

where  $p_0$  is an arbitrary reference pressure. We make use of the scalar potential,  $\Phi_p$ , in Exercise 35.9.

## 35.4 Vorticity dynamics

We now move from the circulation around a macroscopic circuit to the vorticity at a point. In particular, we seek information for how vorticity changes in time. What physical processes lead to these changes? As for Kelvin's theorem, we make use of Newton's law of motion, written here in the form for a rotating fluid (see Section 21.9)

$$\rho \left[ \frac{D}{Dt} + 2\boldsymbol{\Omega} \times \right] \mathbf{v} = -\nabla p - \rho \nabla \Phi + \rho \mathbf{F}, \quad (35.21)$$

where  $\boldsymbol{\Omega}$  is the angular velocity of the rotating reference frame.

### 35.4.1 Vector-invariant velocity equation

As for the shallow water fluid in Section 34.2, we find it useful to convert the advective-form momentum equation to vector-invariant form. For this purpose, make use of the vector identity (see Section 2.3.4)

$$\boldsymbol{\omega} \times \mathbf{v} = -(1/2) \nabla(\mathbf{v} \cdot \mathbf{v}) + (\mathbf{v} \cdot \nabla) \mathbf{v} \quad (35.22)$$

to eliminate velocity self-advection in favor of vorticity

$$\frac{\partial \mathbf{v}}{\partial t} + \boldsymbol{\omega}_a \times \mathbf{v} = -\frac{1}{\rho} \nabla p - \nabla \left[ \frac{1}{2} \mathbf{v}^2 + \Phi \right] + \mathbf{F}. \quad (35.23)$$

We here introduced the absolute vorticity

$$\boldsymbol{\omega}_a = \boldsymbol{\omega} + 2\boldsymbol{\Omega}, \quad (35.24)$$

which is the sum of the relative vorticity and the planetary vorticity (see Section 32.5.1).

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<sup>2</sup>See page 79 of Müller (2006) for more on equation (35.19).

### 35.4.2 Basic form of the vorticity equation

Taking the curl of the vector-invariant momentum equation (35.23) removes the mechanical energy per mass,  $\mathbf{v}^2/2 + \Phi$ , thus leaving

$$\frac{\partial \boldsymbol{\omega}}{\partial t} + \nabla \times (\boldsymbol{\omega}_a \times \mathbf{v}) = \frac{1}{\rho^2} (\nabla \rho \times \nabla p) + \nabla \times \mathbf{F}. \quad (35.25)$$

For geophysical fluids we generally assume that  $\boldsymbol{\Omega}$  has zero time tendency, so that

$$\frac{\partial \boldsymbol{\omega}_a}{\partial t} = \frac{\partial (\boldsymbol{\omega} + 2\boldsymbol{\Omega})}{\partial t} = \frac{\partial \boldsymbol{\omega}}{\partial t}, \quad (35.26)$$

in which case equation (35.25) can be written

$$\frac{\partial \boldsymbol{\omega}_a}{\partial t} + \nabla \times (\boldsymbol{\omega}_a \times \mathbf{v}) = \mathbf{B} + \nabla \times \mathbf{F}, \quad (35.27)$$

where  $\mathbf{B}$  is the baroclinicity vector given by equation (35.15).

### 35.4.3 Massaged form of the vorticity equation

Physical interpretation of the term  $\nabla \times (\boldsymbol{\omega}_a \times \mathbf{v})$  appearing in the prognostic equation (35.27) can be made more transparent by using yet another vector identity

$$\nabla \times (\boldsymbol{\omega}_a \times \mathbf{v}) = (\mathbf{v} \cdot \nabla) \boldsymbol{\omega}_a - (\boldsymbol{\omega}_a \cdot \nabla) \mathbf{v} + \boldsymbol{\omega}_a \nabla \cdot \mathbf{v} - \mathbf{v} \nabla \cdot \boldsymbol{\omega}_a \quad (35.28a)$$

$$= (\mathbf{v} \cdot \nabla) \boldsymbol{\omega}_a - (\boldsymbol{\omega}_a \cdot \nabla) \mathbf{v} - \frac{\boldsymbol{\omega}_a}{\rho} \frac{D\rho}{Dt}. \quad (35.28b)$$

The second equality required the continuity equation

$$\frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{v}, \quad (35.29)$$

and the non-divergent nature of the absolute vorticity

$$\nabla \cdot \boldsymbol{\omega}_a = \nabla \cdot (\nabla \times \mathbf{v} + 2\boldsymbol{\Omega}) = 0. \quad (35.30)$$

Equation (35.27) thus takes the form

$$\frac{D\boldsymbol{\omega}_a}{Dt} - \frac{\boldsymbol{\omega}_a}{\rho} \frac{D\rho}{Dt} = (\boldsymbol{\omega}_a \cdot \nabla) \mathbf{v} + \frac{1}{\rho^2} (\nabla \rho \times \nabla p) + \nabla \times \mathbf{F}, \quad (35.31)$$

which can be written

$$\rho \frac{D(\boldsymbol{\omega}_a/\rho)}{Dt} = (\boldsymbol{\omega}_a \cdot \nabla) \mathbf{v} + \mathbf{B} + \nabla \times \mathbf{F}. \quad (35.32)$$

Each term on the right hand side of the material evolution equation (35.32) represents a distinct physical process that affects the vorticity of a fluid element. The first term,  $(\boldsymbol{\omega}_a \cdot \nabla) \mathbf{v}$ , embodies stretching and twisting and is explored in Section 35.6 in the simplified context of a barotropic fluid. The second term arises from baroclinicity as introduced in equation (35.15) and given a mechanical interpretation in Section 35.5. The third term arises from the curl of the friction vector, which contributes especially in boundary layer regions where frictioncurls are relatively large.

### 35.4.4 Flux-form evolution equation for vorticity components

The terms appearing on the right hand side of the vorticity equation (35.32) provide sources for the vorticity of a fluid element. However, these sources are quite special in that they can be written as the convergence of a flux corresponding to each component of the vorticity. We here expose that property by deriving Eulerian flux-form conservation equations that are separately satisfied by each of the vorticity components.

For this purpose, consider the equation for the vertical component of the absolute vorticity

$$\rho \frac{D(\zeta_a/\rho)}{Dt} = (\boldsymbol{\omega}_a \cdot \nabla) w + \hat{\mathbf{z}} \cdot (\mathbf{B} + \nabla \times \mathbf{F}), \quad (35.33)$$

with

$$\zeta_a = \hat{\mathbf{z}} \cdot \boldsymbol{\omega}_a \quad (35.34)$$

the vertical component to the absolute vorticity. Making use of the identities

$$\rho \frac{D(\zeta_a/\rho)}{Dt} = \frac{\partial \zeta_a}{\partial t} + \nabla \cdot (\mathbf{v} \zeta_a) \quad (35.35a)$$

$$(\boldsymbol{\omega}_a \cdot \nabla) w = \nabla \cdot (\boldsymbol{\omega}_a w) \quad (35.35b)$$

$$\hat{\mathbf{z}} \cdot \mathbf{B} = -\hat{\mathbf{z}} \cdot [\nabla \times (\rho^{-1} \nabla p)] = \nabla \cdot (\hat{\mathbf{z}} \times \rho^{-1} \nabla p) \quad (35.35c)$$

$$\hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}) = -\nabla \cdot (\hat{\mathbf{z}} \times \mathbf{F}), \quad (35.35d)$$

brings equation (35.33) into the Eulerian flux-form

$$\frac{\partial \zeta_a}{\partial t} = -\nabla \cdot \mathbf{J}_\zeta \quad \text{with} \quad \mathbf{J}_\zeta = \mathbf{v} \zeta_a - \boldsymbol{\omega}_a w - \hat{\mathbf{z}} \times \rho^{-1} \nabla p + \hat{\mathbf{z}} \times \mathbf{F}. \quad (35.36)$$

Equation (35.36) says that  $\zeta_a$  evolves at a point according to the convergence of a flux,  $\mathbf{J}_\zeta$ . There are no source terms appearing outside of the flux, even when there are irreversible processes due to friction. This vorticity flux is comprised of an advective flux of vertical vorticity,  $\mathbf{v} \zeta_a$ ; a contribution from absolute vorticity transported vertically,  $-\boldsymbol{\omega}_a w$ ; a contribution from the pressure gradient acceleration rotated clockwise by  $\pi/2$  radians around the vertical axis,  $-\hat{\mathbf{z}} \times \rho^{-1} \nabla p$ ; and the  $\pi/2$  counter-clockwise rotated friction acceleration,  $\hat{\mathbf{z}} \times \mathbf{F}$ . Note that the vertical component to the vorticity flux vanishes

$$\hat{\mathbf{z}} \cdot \mathbf{J}_\zeta = \hat{\mathbf{z}} \cdot [\mathbf{v} \zeta_a - \boldsymbol{\omega}_a w - \hat{\mathbf{z}} \times \rho^{-1} \nabla p + \hat{\mathbf{z}} \times \mathbf{F}] = 0, \quad (35.37)$$

so that  $\zeta_a$  is only affected by the convergence of a purely horizontal flux. We offer a schematic of this property in Figure 35.4.

Mathematically, there is nothing special about the vertical vorticity component. Hence, we readily find that the horizontal vorticity components also satisfy their own respective Eulerian flux-form conservation equations, thus leading to the general result

$$\frac{\partial (\hat{\mathbf{e}} \cdot \boldsymbol{\omega}_a)}{\partial t} = -\nabla \cdot [\mathbf{v} (\hat{\mathbf{e}} \cdot \boldsymbol{\omega}_a) - \boldsymbol{\omega}_a (\hat{\mathbf{e}} \cdot \mathbf{v}) - \hat{\mathbf{e}} \times \rho^{-1} \nabla p + \hat{\mathbf{e}} \times \mathbf{F}], \quad (35.38)$$

where  $\hat{\mathbf{e}}$  is any one of the Cartesian unit vectors  $\hat{\mathbf{x}}, \hat{\mathbf{y}}, \hat{\mathbf{z}}$ . Furthermore, we readily see that the vorticity flux satisfies

$$\hat{\mathbf{e}} \cdot [\mathbf{v} (\hat{\mathbf{e}} \cdot \boldsymbol{\omega}_a) - \boldsymbol{\omega}_a (\hat{\mathbf{e}} \cdot \mathbf{v}) - \hat{\mathbf{e}} \times \rho^{-1} \nabla p + \hat{\mathbf{e}} \times \mathbf{F}] = 0, \quad (35.39)$$

so that the time tendency for  $\hat{\mathbf{e}} \cdot \boldsymbol{\omega}_a$  is affected by a flux in the directions orthogonal to  $\hat{\mathbf{e}}$ . This

$$\partial_t \zeta_a = -\nabla \cdot \mathbf{J}_\zeta$$

$$\hat{z} \cdot \mathbf{J}_\zeta = 0$$

FIGURE 35.4: Tendency for the vertical component to the absolute vorticity arises from the convergence of the vorticity flux,  $\mathbf{J}_\zeta$ , given by equation (35.36), with the vorticity flux strictly horizontal,  $\mathbf{J}_\zeta \cdot \hat{z} = 0$ . This result generalizes for any arbitrary Cartesian component of the absolute vorticity, whereby the corresponding vorticity flux is orthogonal to its vorticity component. It further generalizes to the component of vorticity projected onto the normal direction for an arbitrary surface, thus playing a central role in the impermeability theorem of potential vorticity studied in Section 37.2.

property of the vorticity flux is generalized via the impermeability theorem of potential vorticity studied in Section 37.2, with particular connection to the present discussion given in Section 37.2.3.

### 35.4.5 Vorticity, angular momentum, and torques

Like vorticity, angular momentum provides a measure of the rotational motion of a fluid. However, there are key distinctions as detailed in Section 32.7. Perhaps the most fundamental distinction is that vorticity measures the rotation or spin without reference to an origin, whereas angular momentum is computed relative to a subjectively chosen origin. Vorticity is thus an intrinsic property of the fluid flow, whereas angular momentum depends on the chosen origin and is affected by fluid strains in the region between the point and the origin.

Angular momentum of motion relative to an origin changes in the presence of torques computed about the chosen origin, with the torque equal to the cross product of the position vector of a point and the force vector acting at that point. In contrast, vorticity at a point is affected by the curl of the force per mass acting at the point. Furthermore, angular momentum is a property of any mechanical system, including point particles and rigid bodies, whereas vorticity is a property only of a continuous media where we can compute spatial derivatives.

When the curl of a force per mass is applied to a fluid and thus changes its vorticity, we commonly use the term “torque” in reference to this force curl. For example, in Section 35.5 we explore baroclinicity, which is the key mechanism for how inviscid torques from pressure modify vorticity. That is, baroclinicity provides a vorticity source when the pressure force acting on a fluid element does not pass through the center of mass of that element. When there is baroclinicity, the pressure force spins the fluid element thus affecting vorticity. Analogous inviscid and viscous force curls act on boundaries, such as when a fluid interacts with the solid earth. It is within this context that we use the term “torque” when referring to a vorticity source. Correspondingly, the torques providing a vorticity source have the dimension of force per mass per length, whereas the torques altering angular momentum have the dimension of force times length.

## 35.5 Mechanics of baroclinicity

Baroclinicity is present in most geophysical flows, thus affecting the material evolution of circulation and vorticity. Flow with a nonzero baroclinicity vector is generally referred to as *baroclinic flow*, whereas *barotropic* flows have zero baroclinicity. We illustrate the basic distinction between

barotropic and baroclinic fluids in Figure 35.5. We observe that a baroclinic fluid is associated with fluid motion whereas a barotropic fluid that has its pressure and density surfaces aligned with geopotentials support no motion. We further develop these points in the following as we explore the mechanics of baroclinicity.

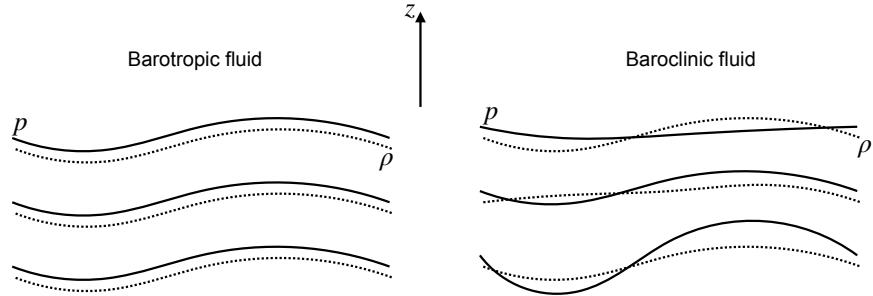


FIGURE 35.5: Left panel: a barotropic fluid, whereby density is a function just of pressure,  $\rho = \rho(p)$ , so that density surfaces (dashed lines) and pressure surfaces (solid lines) are parallel. Horizontal density and pressure surfaces in a barotropic fluid support no motion. Right panel: a baroclinic fluid, whereby density and pressure surfaces generally differ so that density is a function of more than just the pressure. A baroclinic fluid is associated with fluid motion.

### 35.5.1 Curl of the pressure gradient body force

Baroclinicity is the curl of the pressure gradient body force

$$\mathbf{B} = \nabla \times \mathbf{F}_{\text{press}} = \nabla \times (-\rho^{-1} \nabla p) = -\nabla \rho^{-1} \times \nabla p = \frac{\nabla \rho \times \nabla p}{\rho^2}. \quad (35.40)$$

As discussed in Section 35.4.5, the curl of a force provides a torque that spins the fluid, thus rendering a vorticity source. Geometrically, baroclinicity arises when there is nonzero change in pressure along contours of constant density, or conversely changes in density along contours of constant pressure.<sup>3</sup> It can be useful to introduce the notion of a *solenoid*, which is a tube region in the fluid that is perpendicular to both  $\nabla \rho$  and  $\nabla p$ . Solenoids vanish for barotropic flows, whereby  $p = p(\rho)$  (see equation (35.16)). For baroclinic flow, solenoids introduce a torque at each point that affects vorticity.

To further understand the mechanical interpretation of solenoids in terms of a torque, consider the cross product

$$\rho \mathbf{B} = \mathbf{F}_{\text{press}} \times \nabla \rho = (-\rho^{-1} \nabla p) \times \nabla \rho. \quad (35.41)$$

The first term on the right hand side is the pressure gradient force that acts down the pressure gradient. Now consider a tiny fluid element such as shown in Figure 35.6. By construction, the pressure force acts at the geometric center of the element. However, the nonzero density gradient means that the center of mass for the fluid element is not at the geometric center. Since the pressure force does not pass through the center of mass, it imparts a torque to the fluid element. This torque then modifies the vorticity and hence the circulation around the boundary of the element. Only when the pressure force is aligned with the density gradient (barotropic flow), or if the density is spatially uniform (e.g., constant density homogeneous fluid) does the pressure force pass through the center of mass, thus creating no torque and not affecting vorticity.

<sup>3</sup>See Exercise 5.1 for a two-dimensional example of this geometry.

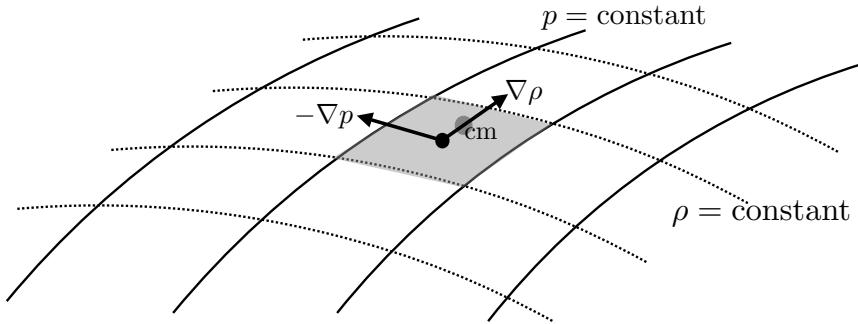


FIGURE 35.6: A mechanical interpretation of the baroclinicity vector. We consider a tiny fluid element bounded by surfaces of constant pressure and density. By construction, the pressure force acts at the geometric center of the element, whereas the center of mass for the element is off-center due to the density gradient across the element. The pressure force thus provides a torque for the fluid element, with the moment-arm for the torque determined by the distance between the geometric center and the center of mass. This torque modifies the vorticity of the fluid element, and in turn modifies the circulation computed around the element's boundary. As depicted here, the baroclinicity vector points into the page (right hand rule for  $(-\rho^{-1} \nabla p) \times \nabla \rho$ ), so that this baroclinicity spins-up a clockwise circulation around the element, or equivalently a clockwise vorticity. This figure is adapted from Figure 14.9 of [Thorne and Blandford \(2017\)](#).

### 35.5.2 Kelvin's circulation theorem and contact pressure forces

We are afforded another means to understand baroclinicity by returning to the formulation of Kelvin's circulation theorem in Section 35.3.1. Focusing just on the baroclinicity contribution in equation (35.14e) we have

$$\left[ \frac{dC}{dt} \right]_{\text{baroclinicity}} = \oint_{\partial S(v)} -\rho^{-1} \nabla p \cdot d\mathbf{r} = \oint_{\partial S(v)} \rho^{-2} (-p \nabla \rho) \cdot d\mathbf{r}, \quad (35.42)$$

which follows since

$$\oint_{\partial S(v)} \nabla(p/\rho) \cdot d\mathbf{r} = 0. \quad (35.43)$$

The term  $-p \nabla \rho$  in equation (35.42) is proportional to the compressive contact pressure force (Section 18.1) acting normal to a constant density surface. Consequently, if the material surface on which we are computing circulation happens to be parallel to a constant density surface, then pressure cannot generate any circulation around that material circuit. The left circuit in Figure 35.7 illustrates this situation. In contrast, in the more general case where a material surface crosses constant density surfaces, pressure modifies circulation around such material circuits (right circuit in Figure 35.7).

### 35.5.3 Bottom pressure contributions at the solid-earth boundary

As an application of the above ideas from Section 35.5.2, consider a fluid region that intersects the solid-earth boundary. The solid-earth boundary is material so that we can apply Kelvin's circulation theorem to a circuit on the boundary. Consider the situation in Figure 35.8, which shows a vertical slice next to a sloping bottom with constant density surface intersecting the bottom. As in our considerations in Section 35.5.2, any material circuit that sits within the bottom boundary crosses density surfaces, in which case circulation is affected by the bottom pressure. Indeed, even if the bottom is flat, so long as density is not constant along the bottom, then a material circuit within the bottom has circulation modified by bottom pressure.

To develop the mathematics of the above ideas, write the differential line element within the

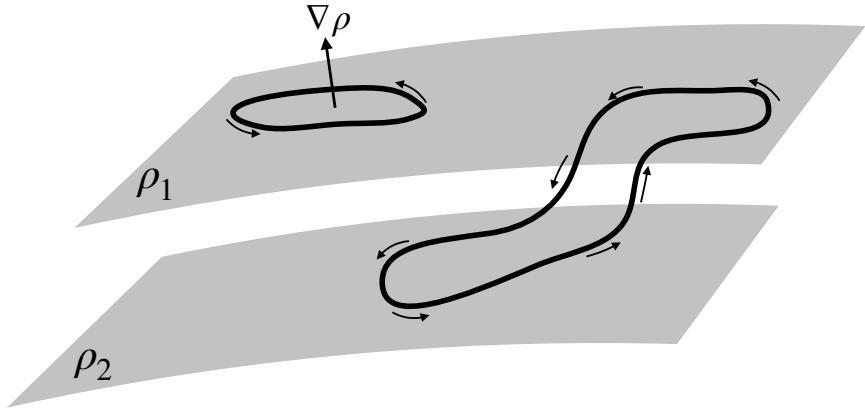


FIGURE 35.7: The material circuit on the left is assumed to be within a constant density surface. In this case,  $\nabla\rho \cdot d\mathbf{r} = 0$  so that pressure cannot modify the circulation around this circuit. If material surfaces are not within constant density surface, such as depicted on the right, then pressure is able to modify the circulation computed around any such material circuits.

bottom circuit as

$$d\mathbf{r} = \hat{\mathbf{x}} dx + \hat{\mathbf{y}} dy + \hat{\mathbf{z}} dz = (\hat{\mathbf{x}} + \hat{\mathbf{z}} \partial_x \eta_b) dx + (\hat{\mathbf{y}} + \hat{\mathbf{z}} \partial_y \eta_b) dy. \quad (35.44)$$

To reach this result we set  $z = \eta_b(x, y)$  since the circuit is along the bottom boundary, which in turn means that

$$dz = d\eta_b = \nabla_z \eta_b \cdot (\hat{\mathbf{x}} dx + \hat{\mathbf{y}} dy). \quad (35.45)$$

Consequently, the projection of the density gradient onto the circuit is given by

$$\nabla\rho \cdot d\mathbf{r} = (\nabla_z \rho + \partial_z \rho \nabla_z \eta_b) \cdot d\mathbf{r}. \quad (35.46)$$

Making use of this result in Kelvin's circulation theorem and focusing on the pressure contribution, as in equation (35.42), leads to

$$\left[ \frac{dC}{dt} \right]_{\text{bottom}} = - \oint_{\partial S_{\text{bottom}}} p \rho^{-2} \nabla\rho \cdot d\mathbf{r} = - \oint_{\partial S_{\text{bottom}}} \frac{p_b}{\rho^2} (\nabla_z \rho + \partial_z \rho \nabla_z \eta_b) \cdot d\mathbf{r}. \quad (35.47)$$

There are two contributions to the circulation changes revealed by equation (35.47). The first arises from the sloped density surfaces next to the bottom, and the second arises from the sloped bottom multiplied by the vertical density gradient. These two contributions are weighted by the bottom pressure,  $p_b$ , which is normalized by the squared density. Circulation modifications are enhanced by increased horizontal density gradients next to the bottom, as well as increased topographic slopes. For the special case of flat topography and flat density there are no bottom pressure-induced changes to the circulation around a bottom material circuit.

#### 35.5.4 Further study

This video from Prof. Shapiro provides a lucid discussion of baroclinicity and its role in affecting vorticity.

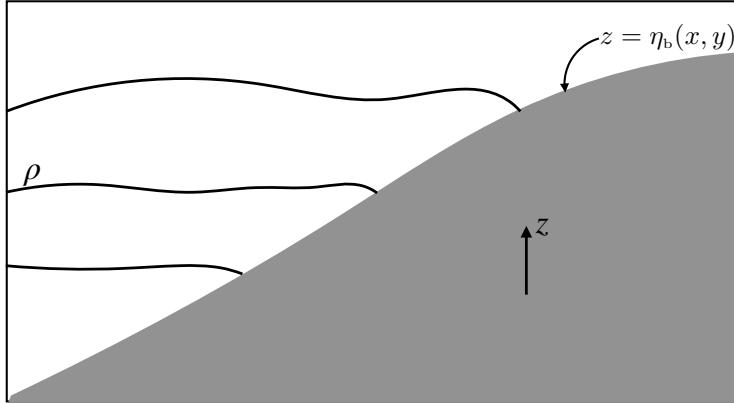


FIGURE 35.8: Constant density surfaces intersecting a sloped solid-earth boundary. Any circuit that sits along the boundary is material since the bottom is material. For circuits that cross density surfaces, the bottom pressure acts to modify circulation computed for this circuit.

## 35.6 Vorticity filaments and material line elements

We here study the physics of the source term

$$(\boldsymbol{\omega}_a \cdot \nabla) \mathbf{v} = f \partial_z \mathbf{v} + (\boldsymbol{\omega} \cdot \nabla) \mathbf{v}. \quad (35.48)$$

The contribution from  $\hat{z} f \partial_z w$  to the first term is further explored when studying the planetary geostrophic equations in Sections 25.5 and 39.4, given its importance for large-scale meridional motion on a spherical planet. It is the second term,  $(\boldsymbol{\omega} \cdot \nabla) \mathbf{v}$ , that is the focus of this section.

### 35.6.1 Vortex filaments evolve through the rate of strain

To help unpack the physics of the source,  $(\boldsymbol{\omega} \cdot \nabla) \mathbf{v}$ , write it in the following form found by exposing Cartesian tensor labels

$$\omega_m \partial_m v_n = (\omega_m / 2) [(\partial_m v_n + \partial_n v_m) + (\partial_m v_n - \partial_n v_m)] \quad (35.49a)$$

$$= \omega_m \mathbb{S}_{mn} - \omega_m \mathbb{R}_{mn}, \quad (35.49b)$$

where  $\mathbb{S}_{mn} = (1/2)(\partial_m v_n + \partial_n v_m)$  are components to the rate of strain tensor and  $\mathbb{R}_{mn} = (1/2)(\partial_n v_m - \partial_m v_n)$  are components to the rotation tensor. These tensors were introduced in Section 13.3 when studying the kinematics of line elements. As shown in that discussion, the rotation tensor is related to the vorticity by the identity (13.44), whose use leads to

$$\omega_m \mathbb{R}_{mn} = -\omega_m \epsilon_{mnp} \omega_p / 2 = 0. \quad (35.50)$$

This identity follows since the outer product  $\omega_m \omega_p$  is symmetric on the labels  $m, p$ , whereas these labels are anti-symmetric in the permutation symbol,  $\epsilon_{mnp}$ . Recalling that the rotation tensor generates rotations about the axis defined by vorticity, we see why  $\boldsymbol{\omega} \cdot \mathbb{R} = 0$ . Namely, there is no rotation generated when a vector is rotated about its own axis. We are thus left just with

$$(\boldsymbol{\omega} \cdot \nabla) \mathbf{v} = \boldsymbol{\omega} \cdot \mathbb{S}. \quad (35.51)$$

That is, the source term in the vorticity equation is determined by the projection of the vorticity onto the rate of strain tensor. This result highlights the fundamental role of flow strains in

affecting vorticity.

### 35.6.2 Frozen-in nature of vorticity

Consider an incompressible, inviscid, non-rotating barotropic fluid, in which case the vorticity equation (35.32) reduces to

$$\frac{D\omega}{Dt} = (\boldsymbol{\omega} \cdot \nabla) \mathbf{v}, \quad (35.52)$$

and recall the evolution equation for a material line element as detailed in Section 13.3

$$\frac{D(\delta\mathbf{x})}{Dt} = (\delta\mathbf{x} \cdot \nabla) \mathbf{v}. \quad (35.53)$$

Now recall from Section 35.2.1 that a vortex line is a line drawn through the fluid that is everywhere parallel to the vorticity. Such a line connects material fluid particles, so that a vortex line constitutes a particular case of a material line. At some initial time,  $t = 0$ , let the vorticity on an infinitesimal vortex line be related to the material line element according to

$$\delta\mathbf{x}(0) = \Gamma \boldsymbol{\omega}(\mathbf{x}, 0), \quad (35.54)$$

where  $\Gamma$  is scalar with dimensions  $LT$  that is determined by the initial vorticity and initial line element. Since the vorticity equation (35.52) has precisely the same mathematical form as the material line element equation (35.53), the difference vector

$$\mathbf{A} \equiv \delta\mathbf{x} - \Gamma \boldsymbol{\omega}, \quad (35.55)$$

evolves according to

$$\frac{D\mathbf{A}}{Dt} = (\mathbf{A} \cdot \nabla) \mathbf{v}. \quad (35.56)$$

But since  $\mathbf{A}$  vanishes at  $t = 0$ , we conclude that it vanishes for all time

$$\frac{D\mathbf{A}}{Dt} = 0. \quad (35.57)$$

Consequently, the relation (35.54) holds for all time with  $\Gamma$  a constant. That is, the vortex filament and its corresponding line element remain parallel as they both evolve according to their projection onto the rate of strain tensor. We thus say that vorticity is a *frozen-in* property as illustrated by Figure 35.9. Although we established this property only for the case of an incompressible, inviscid, barotropic fluid, it offers insight into the more general situation occurring in real fluids.

### 35.6.3 Stretching and tilting of vortex tubes

Vorticity responds when vortex lines or tubes are stretched or bent by the rate of strain tensor. To help understand the response, consider again the perfect fluid barotropic incompressible vorticity equation (35.52) and focus on the material evolution of the vertical vorticity component

$$\frac{D\omega_z}{Dt} = \omega_x \frac{\partial w}{\partial x} + \omega_y \frac{\partial w}{\partial y} + \omega_z \frac{\partial w}{\partial z}. \quad (35.58)$$

Note that since  $\nabla \cdot \boldsymbol{\omega} = 0$ , we can write this equation as

$$\frac{D\omega_z}{Dt} = \nabla \cdot (w \boldsymbol{\omega}), \quad (35.59)$$

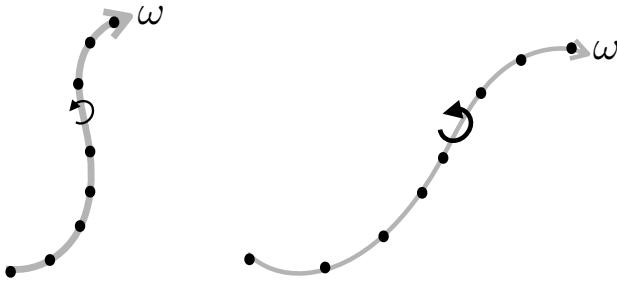


FIGURE 35.9: For the non-divergent flow of a perfect barotropic fluid, vortex lines (also known as vortex filaments) are also material lines. This property means that for an arbitrary vortex line drawn in the fluid, the fluid particles that are initially on the vortex line remain on the line as it moves through the fluid according to the rate of strain tensor. We here show two instances of the same vortex line along with sample test fluid particles. The left configuration stretches into the right configuration, with the vorticity increasing as the vortex line stretches according to the discussion in Section 35.6.3. The material property of vortex lines is known as their *frozen-in nature*. The frozen-in nature of vortex lines strictly holds only for perfect incompressible barotropic fluid, yet it offers useful insights into the vortex dynamics of more general fluids.

though in the following we find it more useful to focus on the form given by equation (35.58). The following discussion closely emulates that given for a material line element in Section 13.3.6.

### Stretching

Consider the vortex tube to be initially aligned with the  $\hat{z}$ -axis, so that  $\omega_x = \omega_y = 0$ , in which case there is only a single term impacting the material evolution of vertical vorticity<sup>4</sup>

$$\frac{D\omega_z}{Dt} = \omega_z \frac{\partial w}{\partial z}. \quad (35.60)$$

Since the fluid is incompressible, the volume of an infinitesimal portion of the vortex tube is materially constant

$$\frac{D(\delta V)}{Dt} = 0, \quad (35.61)$$

which means that the vertical extent,  $\delta z$ , and cross-sectional area,  $\delta A$ , are constrained

$$\frac{1}{\delta z} \frac{D(\delta z)}{Dt} + \frac{1}{\delta A} \frac{D(\delta A)}{Dt} = 0. \quad (35.62)$$

As the tube stretches vertically, its horizontal area reduces, and vice versa. Making use of the expression for the evolution of a material line segment (equation (35.53)) allows us to write

$$\frac{1}{\delta z} \frac{D(\delta z)}{Dt} = \frac{\partial w}{\partial z}, \quad (35.63)$$

so that the vorticity equation (35.60) becomes

$$\frac{D\omega_z}{Dt} = \omega_z \frac{\partial w}{\partial z} = \omega_z \left[ \frac{1}{\delta z} \frac{D(\delta z)}{Dt} \right] = -\omega_z \left[ \frac{1}{\delta A} \frac{D(\delta A)}{Dt} \right]. \quad (35.64)$$

<sup>4</sup>Be mindful to distinguish the symbols for the vertical component of vorticity,  $\omega_z$ , and the vertical component of velocity,  $w$ .

Rearrangement leads to

$$\frac{D(\omega_z \delta A)}{Dt} = 0, \quad (35.65)$$

which is an expression of Kelvin's circulation theorem (equation (35.17)) for a cross-section of the vortex tube.

The above manipulations suggest the following interpretation for the *stretching* term,  $\omega_z (\partial w / \partial z)$ , appearing in the vertical vorticity equation (35.58) and illustrated in Figure 35.10. Namely, as the vortex tube is stretched and its cross-sectional area is compressed, the vorticity magnitude increases so to maintain a constant circulation around the tube, as per Kelvin's theorem (or equivalently as per Helmholtz's first theorem discussed in Section 35.2.3). Stretching a vortex tube increases the magnitude of the vorticity in the direction of the stretching whereas compressing a tube reduces the vorticity magnitude. This result also accords with our understanding of angular momentum conservation as discussed for the rotating cylinder in Section 34.3.2 and depicted by Figure 34.1.

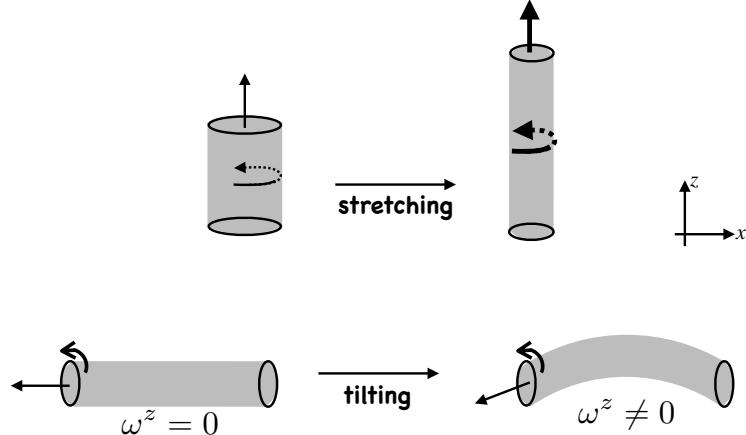


FIGURE 35.10: Illustrating how stretching and tilting of a vortex tube impacts on the vorticity. Top panels: As the cross-sectional area of the vortex tube shrinks, and the vertical extent of the tube stretches, the magnitude of the vorticity along the axis of the tube increases. This result accords with our understanding of angular momentum conservation as discussed for the rotating cylinder in Section 34.3.2 and depicted by Figure 34.1, as well as with Helmholtz's first theorem in Section 35.2.3 and Figure 35.2. Lower panels: The initial vortex tube is assumed to be aligned parallel to the  $x$ -axis, so that it has zero projection in the vertical direction. A horizontal shear of the vertical velocity ( $\partial w / \partial x \neq 0$ ) deforms the vortex tube. Upon deforming (or tilting), the tube picks up a nonzero projection in the vertical, which means that it now has a nonzero vertical component to vorticity.

### Tilting

Now consider an initially horizontal vortex tube as in the lower left panel of Figure 35.10 so that  $\omega_z = 0$ . Furthermore, to focus on just one of the two horizontal directions we set  $\omega_y = 0$  so that equation (35.58) for the vertical vorticity becomes

$$\frac{D\omega_z}{Dt} = \omega_x \frac{\partial w}{\partial x}. \quad (35.66)$$

If there is no horizontal shear in the vertical velocity ( $\partial w / \partial x = 0$ ), then the vortex tube remains horizontal. However, in the presence of  $\partial w / \partial x \neq 0$ , the vorticity vector picks up a nonzero vertical projection. To help visualize this process, recall the frozen-in nature of vortex lines, and consider the evolution of an infinitesimal line segment on the vortex tube. With the vortex tube initially

aligned parallel to the  $x$ -axis, the evolution of a material line segment (equation (35.53)) is given by

$$\frac{D(\delta\mathbf{x})}{Dt} = \delta x \frac{\partial \mathbf{v}}{\partial x}. \quad (35.67)$$

The initially horizontal line segment thus picks up a projection in the vertical so long as  $\partial w / \partial x \neq 0$ . Correspondingly, the vorticity picks up a vertical component. We can think of this process as a tilting or deforming of the initially horizontal vortex tube, with the tilted tube having a nonzero vertical projection.

### 35.6.4 Comments

As a vortex tube is stretched in the presence of straining motion, it spins faster and its radius reduces. Hence, its mechanical energy moves from larger to smaller spatial scales. This process of downscale energy cascade (i.e., the movement of mechanical energy from large to small scales) is a fundamental property of three dimensional turbulence, and vortex stretching is the dominant mechanism for the cascade. In contrast, two dimensional turbulence, which occurs in horizontal non-divergent flows, does not support vortex stretching and consequently does not support the downscale energy cascade. Instead, two dimensional turbulence supports an inverse cascade whereby there is a net flow of energy to larger scales, with that flow related to the material conservation of vorticity in two dimensional non-divergent flows (see Chapter 33). We have little more to say about the turbulent cascade in this book, with the interested reader encouraged to study the presentations given by [Vallis \(2017\)](#).

## 35.7 Circulation and vorticity for rotating fluids

The previous sections focused on circulation and vorticity for non-rotating fluids. The discussion here for rotating fluids is a straightforward extension. Even so, the implications are quite profound for the motion of geophysical fluids.

We start by recalling the expression from Section 9.9.1 for the inertial or absolute velocity (i.e., velocity measured in an inertial frame)

$$\mathbf{v}_a = \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{x}, \quad (35.68)$$

where  $\mathbf{v}$  is the velocity measured in the rotating frame (relative velocity), and  $\mathbf{x}$  is the position vector relative to the origin (e.g., center of earth). The absolute circulation around an arbitrary circuit (a circuit that is not necessarily material) is thus given by

$$\mathcal{C}_a = \oint_{\partial\mathcal{S}} (\mathbf{v} + \boldsymbol{\Omega} \times \mathbf{x}) \cdot d\mathbf{r} = \mathcal{C} + \mathcal{C}_{\text{planet}}, \quad (35.69)$$

where the circulation measured in the rotating frame is

$$\mathcal{C} = \oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{r} \quad (35.70)$$

and the circulation associated with the rotating planet is

$$\mathcal{C}_{\text{planet}} = \oint_{\partial\mathcal{S}} (\boldsymbol{\Omega} \times \mathbf{x}) \cdot d\mathbf{r}. \quad (35.71)$$

Again,  $d\mathbf{r}$  is the differential line element moving around the circuit as mentioned in Section 32.3.

A fluid particle at rest in the rotating frame still has a nonzero absolute circulation as given by the planetary circulation. Making use of Stokes' theorem leads to the equivalent forms for the circulations

$$\mathcal{C} = \oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{r} = \int_{\mathcal{S}} \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S} \quad \text{relative circulation} \quad (35.72a)$$

$$\mathcal{C}_{\text{planet}} = \oint_{\partial\mathcal{S}} (\boldsymbol{\Omega} \times \mathbf{x}) \cdot d\mathbf{r} = \int_{\mathcal{S}} \boldsymbol{\omega}_{\text{planet}} \cdot \hat{\mathbf{n}} d\mathcal{S} \quad \text{planetary circulation} \quad (35.72b)$$

$$\mathcal{C}_a = \oint_{\partial\mathcal{S}} \mathbf{v}_a \cdot d\mathbf{r} = \int_{\mathcal{S}} \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} \quad \text{absolute circulation,} \quad (35.72c)$$

where

$$\boldsymbol{\omega} = \nabla \times \mathbf{v} \quad \text{relative vorticity} \quad (35.73a)$$

$$\boldsymbol{\omega}_{\text{planet}} = \nabla \times (\boldsymbol{\Omega} \times \mathbf{x}) = 2\boldsymbol{\Omega} \quad \text{planetary vorticity} \quad (35.73b)$$

$$\boldsymbol{\omega}_a = \boldsymbol{\omega} + \boldsymbol{\omega}_{\text{planet}} \quad \text{absolute vorticity.} \quad (35.73c)$$

Thus far we have merely substituted in the expression (35.68) for the inertial velocity and then decomposed the vorticity and circulation into its relative and planetary components. Next we consider how circulation evolves, in which case we see how the relative and planetary circulations interact.

### 35.7.1 Material evolution of absolute circulation

We now consider how the absolute circulation evolves for a material circuit that moves with the fluid

$$\frac{d\mathcal{C}_a}{dt} = \frac{d}{dt} \oint_{\partial\mathcal{S}(\mathbf{v})} (\mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}) \cdot d\mathbf{r}, \quad (35.74)$$

where we choose to write  $\mathbf{r} = \mathbf{x}$  for the position of a fluid particle on the circuit, and  $d\mathbf{r}$  is a differential line element around a circuit of material fluid particles. We measure fluid motion in the rotating frame so that the material time derivative contains advection by the velocity  $\mathbf{v}$  rather than the absolute velocity  $\mathbf{v}_a$ . Following the discussion for non-rotating Kelvin's circulation theorem in Section 35.3 leads to

$$\frac{d\mathcal{C}_a}{dt} = \frac{d}{dt} \oint_{\partial\mathcal{S}(\mathbf{v})} (\mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}) \cdot d\mathbf{r} \quad (35.75a)$$

$$= \oint_{\partial\mathcal{S}(\mathbf{v})} \left[ \frac{D\mathbf{v}}{Dt} + \boldsymbol{\Omega} \times \frac{D\mathbf{r}}{Dt} \right] \cdot d\mathbf{r} + \oint_{\partial\mathcal{S}(\mathbf{v})} (\mathbf{v} + \boldsymbol{\Omega} \times \mathbf{r}) \cdot d\mathbf{v} \quad (35.75b)$$

$$= \oint_{\partial\mathcal{S}(\mathbf{v})} \left[ \frac{D\mathbf{v}}{Dt} + \boldsymbol{\Omega} \times \mathbf{v} \right] \cdot d\mathbf{r} + \oint_{\partial\mathcal{S}(\mathbf{v})} (\boldsymbol{\Omega} \times \mathbf{r}) \cdot d\mathbf{v} \quad (35.75c)$$

$$= \oint_{\partial\mathcal{S}(\mathbf{v})} \left[ \frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} \right] \cdot d\mathbf{r}. \quad (35.75d)$$

To reach this result we set

$$\mathbf{v} = \frac{D\mathbf{r}}{Dt}, \quad (35.76)$$

for the velocity of a fluid particle on the circuit. We also used the identity

$$\oint_{\partial\mathcal{S}(\mathbf{v})} \mathbf{v} \cdot d\mathbf{v} = \frac{1}{2} \oint_{\partial\mathcal{S}(\mathbf{v})} d\mathbf{v}^2 = 0 \quad (35.77)$$

as well as

$$\oint_{\partial S(v)} (\boldsymbol{\Omega} \times \mathbf{r}) \cdot d\mathbf{v} = \oint_{\partial S(v)} d[(\boldsymbol{\Omega} \times \mathbf{r}) \cdot \mathbf{v}] - \oint_{\partial S(v)} (\boldsymbol{\Omega} \times d\mathbf{r}) \cdot \mathbf{v} = \oint_{\partial S(v)} (\boldsymbol{\Omega} \times \mathbf{v}) \cdot d\mathbf{r}. \quad (35.78)$$

Now insert the momentum equation (35.21) into equation (35.75d) to yield

$$\frac{dC_a}{dt} = \oint_{\partial S(v)} \left[ \frac{D\mathbf{v}}{Dt} + 2\boldsymbol{\Omega} \times \mathbf{v} \right] \cdot d\mathbf{r}. \quad (35.79a)$$

$$= \oint_{\partial S(v)} \left[ -\frac{1}{\rho} \nabla p - \nabla \Phi + \mathbf{F} \right] \cdot d\mathbf{r}. \quad (35.79b)$$

$$= \oint_{\partial S(v)} \left[ -\frac{dp}{\rho} + \mathbf{F} \cdot d\mathbf{r} \right]. \quad (35.79c)$$

Making use of Stokes' theorem leads to the evolution of absolute circulation around a material loop

$$\frac{dC_a}{dt} = \oint_{\partial S(v)} \left[ -\frac{dp}{\rho} + \mathbf{F} \cdot d\mathbf{r} \right] = \int_{S(v)} (\mathbf{B} + \nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}} dS, \quad (35.80)$$

where  $\mathbf{B} = \rho^{-2} \nabla \rho \times \nabla p$  is the baroclinicity vector from equation (35.40).

The circulation theorem (35.80) is the same as obtained for the non-rotating Kelvin's circulation theorem discussed in Section 35.3 (see equation (35.14e)). This equivalence proves that absolute circulation is an objective (frame invariant) property of the fluid, in which its evolution is unchanged when moving to a non-inertial rotating frame.

### 35.7.2 The beta effect

As given by equation (35.69), the absolute circulation around an arbitrary circuit equals to the circulation of fluid measured in the rotating frame (relative circulation) plus circulation of the rotating frame itself (planetary circulation)

$$C_a = C + C_{\text{planet}} = C + 2 \int_S \boldsymbol{\Omega} \cdot \hat{\mathbf{n}} dS \iff \frac{dC_a}{dt} = \frac{dC}{dt} + \frac{dC_{\text{planet}}}{dt}. \quad (35.81)$$

We can determine the processes that affect the absolute circulation around a material loop by using the circulation equation (35.80)

$$\frac{dC}{dt} = -\frac{dC_{\text{planet}}}{dt} + \frac{dC_a}{dt} \quad (35.82a)$$

$$= -2 \frac{d}{dt} \left[ \int_{S(v)} \boldsymbol{\Omega} \cdot \hat{\mathbf{n}} dS \right] + \int_{S(v)} (\mathbf{B} + \nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}} dS. \quad (35.82b)$$

We generally assume that the planetary rotation is a constant in time and points through the north pole of the sphere<sup>5</sup>  $\boldsymbol{\Omega} = \Omega \hat{\mathbf{Z}}$ , so that

$$\int_{S(v)} \boldsymbol{\Omega} \cdot \hat{\mathbf{n}} dS = \Omega \int_{S(v)} \hat{\mathbf{Z}} \cdot \hat{\mathbf{n}} dS = \Omega A_{\perp}. \quad (35.83)$$

---

<sup>5</sup>We follow the notational conventions of Figure 8.1 with one exception. Here, the vertical Cartesian direction through the north pole is written  $\hat{\mathbf{Z}}$  to avoid confusion with the local vertical direction  $\hat{\mathbf{z}}$  determined by the geopotential.

The area  $A_{\perp}$  is the projection of the spherical area enclosed by the circuit onto the horizontal equatorial plane, with Figure 35.11 illustrating the geometry. This result has profound impact on large scale geophysical fluid motion, whereby relative circulation around a material circuit in the rotating frame changes according to

$$\frac{dC}{dt} = \underbrace{-2\Omega \frac{dA_{\perp}}{dt}}_{\text{beta effect}} + \underbrace{\int_S (\mathbf{B} + \nabla \times \mathbf{F}) \cdot \hat{\mathbf{n}} d\mathcal{S}(\mathbf{v})}_{\text{baroclinicity plus friction}}. \quad (35.84)$$

Equation (35.84) is sometimes referred to as the *Bjerknes circulation theorem* (see Holton (1992) equation (4.5)). The second term, comprised of baroclinicity and friction, also appears in the non-rotating case. It has already been discussed in Sections 35.3 and 35.5.

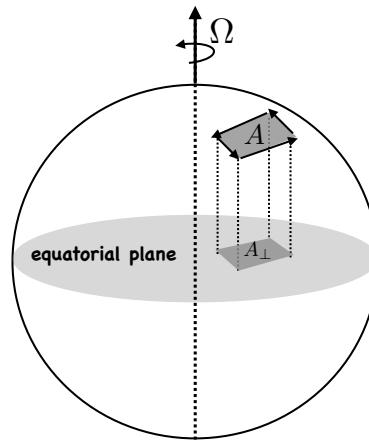


FIGURE 35.11: Geometry of the beta effect. According to the Bjerknes circulation theorem (35.84), the circulation for a material loop on the surface of a rotating sphere is affected by baroclinicity and friction, as for a non-rotating sphere, as well as latitudinal motion of the loop. The latitudinal motion alters the area of the loop as projected onto the equatorial plane, with the projected area increasing as the loop moves poleward. When multiplied by the magnitude of the planetary vorticity,  $2\Omega$ , the area contribution is termed *planetary induction* (i.e., relative circulation is induced by latitudinal motion), or more commonly it is called the *beta effect*. The beta effect requires both rotation ( $2\Omega$ ) and curvature of the sphere ( $\partial_y f = \beta$ ); it is therefore absent on the *f*-plane.

The first term in the circulation theorem (35.84) is fundamentally new. It is nonzero in the presence of both rotation and curvature of the sphere. The spherical effect arises from latitudinal movement of a material circuit, with the area,  $A_{\perp}$ , changing under such motion. When the circuit moves poleward, the projected area  $A_{\perp}$  increases whereas it decreases to zero as it moves equatorward. The material change in  $A_{\perp}$ , when multiplied by the planetary vorticity, modifies the relative circulation around the material circuit. We refer to *planetary induction* as the process whereby relative circulation changes due to latitudinal motion of a material circuit on a rotating sphere. Or more commonly, planetary induction is referred to as the *beta effect*, given its connection to the latitudinal gradient of the Coriolis parameter,  $\beta = \partial_y f$ . Notably, longitudinal motion of the circuit has no impact on  $A_{\perp}$ , so that longitudinal motion imparts no planetary induction of relative circulation.

In theories of large-scale laminar planetary flows, the baroclinicity and friction terms are typically sub-dominant. For these flows, the material evolution of relative circulation is dominated by the beta effect. Planetary geostrophic flow is the canonical example of such flow, as studied in Section 25.5 as well as Chapters 38 and 39. In such flows, forces that lead to meridional motion also give rise to changes in the relative circulation. Conversely, forces that change the circulation around a material loop in turn affect meridional motion of the loop.

### 35.7.3 A two-dimensional incompressible fluid

To garner more insight into the beta effect, consider a perfect incompressible and two-dimensional fluid (zero vertical velocity) on a rotating sphere. In this case there is only a vertical component to vorticity and both baroclinicity and friction have no role in vorticity dynamics. Hence, vorticity is affected only via the beta effect. This *two-dimensional barotropic fluid* system is discussed in more detail in Chapter 33. We here use it as an example that clearly exposes essential features of the beta effect (see also Section 33.2.2).

In the rotating frame, circulation around an infinitesimal closed material loop is

$$\mathcal{C} = A \zeta, \quad (35.85)$$

where  $\zeta$  is the relative vorticity and  $A$  is the area enclosed by the loop. Because the fluid is incompressible, the loop area  $A$  remains constant even as the loop becomes contorted (see Section 16.6). The material evolution of circulation is therefore given by

$$\frac{D\mathcal{C}}{Dt} = A \frac{D\zeta}{Dt} = -2\Omega \frac{DA_{\perp}}{Dt}, \quad (35.86)$$

where the second equality follows from Bjerknes' circulation theorem (35.84). Let the material circuit be at a latitude  $\phi$  so that the projection of the loop area onto the equatorial plane is (see Figure 35.11)

$$A_{\perp} = A \sin \phi. \quad (35.87)$$

Hence, material evolution of the circulation is

$$\frac{D\mathcal{C}}{Dt} = A \frac{D\zeta}{Dt} \quad (35.88a)$$

$$= -2\Omega \frac{DA_{\perp}}{Dt} \quad (35.88b)$$

$$= -2A\Omega \frac{D\sin \phi}{Dt} \quad (35.88c)$$

$$= -2A\Omega \cos \phi \frac{D\phi}{Dt} \quad (35.88d)$$

$$= -A \left[ \frac{2\Omega \cos \phi}{R} \right] \left[ R \frac{D\phi}{Dt} \right] \quad (35.88e)$$

$$= -A\beta v, \quad (35.88f)$$

where we introduced the meridional velocity component

$$v = R \frac{D\phi}{Dt} \quad (35.89)$$

and the meridional derivative of the planetary vorticity

$$\beta = \frac{df}{dy} = \frac{1}{R} \frac{d}{d\phi} (2\Omega \sin \phi) = \frac{2\Omega \cos \phi}{R}. \quad (35.90)$$

The result (35.88f) shows how meridional motion on a rotating sphere induces relative circulation. It furthermore motivates the name *beta effect* for planetary induction of relative vorticity.

### 35.7.4 Further study

The beta effect and its role in vorticity is nicely summarized in [this video from Science Primer](#) in the context of Rossby waves.

## 35.8 Vorticity in a hydrostatic and Boussinesq fluid

In this section we develop the vorticity budget for a hydrostatic Boussinesq fluid in the presence of diabatic sources and frictional forcing. This system is of particular importance for models of the ocean circulation with the governing equations given by (see Section 23.1.6)

$$\frac{Du}{Dt} + \mathbf{f} \times \mathbf{v} = -\nabla_z \varphi + \mathbf{F} \quad (35.91a)$$

$$\frac{\partial \varphi}{\partial z} = b \quad (35.91b)$$

$$\nabla \cdot \mathbf{v} = 0 \quad (35.91c)$$

$$\frac{Db}{Dt} = \dot{b}, \quad (35.91d)$$

with the non-divergent velocity field written

$$\mathbf{v} = (\mathbf{u}, w) = \mathbf{u} + w \hat{\mathbf{z}}. \quad (35.92)$$

The perturbation pressure is given by

$$\rho_0 \varphi = \delta p = p - p_0, \quad (35.93)$$

with the reference pressure,  $p_0 = p_0(z)$ , in hydrostatic balance with the constant reference density

$$\frac{dp_0}{dz} = -g \rho_0 \quad (35.94)$$

and  $p$  the hydrostatic pressure satisfying the hydrostatic balance

$$\frac{\partial p}{\partial z} = -g \rho. \quad (35.95)$$

The globally referenced Archimedean buoyancy is given by

$$b = -g \left[ \frac{\rho - \rho_0}{\rho_0} \right], \quad (35.96)$$

with this field discussed in Section 24.4.2. We assume the Coriolis parameter of the form  $\mathbf{f} = f \hat{\mathbf{z}}$ , in which case

$$\mathbf{f} \times \mathbf{v} = \mathbf{f} \times \mathbf{u}. \quad (35.97)$$

Finally, the horizontal friction acceleration vector is given by

$$\mathbf{F} = (F^x, F^y, 0) \quad (35.98)$$

and the gradient operator is

$$\nabla = \nabla_z + \hat{\mathbf{z}} \partial_z. \quad (35.99)$$

### 35.8.1 Deriving the vorticity equation

*Vector invariant velocity equation*

To derive the vorticity equation, it is useful to combine the horizontal momentum equation with the hydrostatic balance, in which case

$$\frac{Du}{Dt} + \mathbf{f} \times \mathbf{v} = -\nabla \varphi + b \hat{\mathbf{z}} + \mathbf{F}. \quad (35.100)$$

As for the non-hydrostatic case (Section 35.4.1), we rewrite the self-advection operator,  $(\mathbf{v} \cdot \nabla) \mathbf{u}$ , before taking the curl. In turn, we introduce the hydrostatic relative vorticity given by the curl of the horizontal velocity

$$\boldsymbol{\omega}^{\text{hy}} = \nabla \times \mathbf{u} = \hat{\mathbf{z}} \times \partial_z \mathbf{u} + \hat{\mathbf{z}} \zeta = -\hat{\mathbf{x}} \partial_z v + \hat{\mathbf{y}} \partial_z u + \hat{\mathbf{z}} \zeta, \quad (35.101)$$

where  $\zeta = \partial_x v - \partial_y u$  is the vertical component to the relative vorticity, and

$$\nabla \cdot \boldsymbol{\omega}^{\text{hy}} = 0. \quad (35.102)$$

It is then straightforward to show that

$$\boldsymbol{\omega}^{\text{hy}} \times \mathbf{v} = \hat{\mathbf{x}} (w \partial_z u - v \partial_x v + v \partial_y u) + \hat{\mathbf{y}} (w \partial_z v - u \partial_y u + u \partial_x v) - \hat{\mathbf{z}} \partial_z (u^2 + v^2)/2 \quad (35.103a)$$

$$= w \partial_z \mathbf{u} + \zeta (-v \hat{\mathbf{x}} + u \hat{\mathbf{y}}) - \hat{\mathbf{z}} \partial_z (u^2 + v^2)/2, \quad (35.103b)$$

in which case

$$\nabla(\mathbf{u}^2/2) + \boldsymbol{\omega}^{\text{hy}} \times \mathbf{v} = \nabla(u^2 + v^2)/2 - \hat{\mathbf{z}} \partial_z (u^2 + v^2)/2 + w \partial_z \mathbf{u} + \zeta (-v \hat{\mathbf{x}} + u \hat{\mathbf{y}}) \quad (35.104a)$$

$$= (u \partial_x + v \partial_y + w \partial_z) \mathbf{u} \quad (35.104b)$$

$$= (\mathbf{v} \cdot \nabla) \mathbf{u}. \quad (35.104c)$$

The material time derivative of the horizontal velocity can thus be written as

$$\frac{Du}{Dt} = \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{v} \cdot \nabla) \mathbf{u} = \frac{\partial \mathbf{u}}{\partial t} + \boldsymbol{\omega}^{\text{hy}} \times \mathbf{v} + \nabla(\mathbf{u}^2/2), \quad (35.105)$$

which then leads to the vector invariant horizontal velocity equation

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{f} \hat{\mathbf{z}} + \boldsymbol{\omega}^{\text{hy}}) \times \mathbf{v} = -\nabla(\varphi + \mathbf{u}^2/2) + b \hat{\mathbf{z}} + \mathbf{F}, \quad (35.106)$$

which can be written in the equivalent form<sup>6</sup>

$$[\partial_t + w \partial_z + (f + \zeta) \hat{\mathbf{z}} \times] \mathbf{u} = -\nabla_z (\varphi + \mathbf{u}^2/2) - (\partial_z \varphi - b) \hat{\mathbf{z}} + \mathbf{F}. \quad (35.107)$$

*Curl of the velocity equation to render the vorticity equation*

Now take the curl of the vector invariant velocity equation (35.106), and make use of the identity

$$\nabla \times (\boldsymbol{\omega}_{\text{a}}^{\text{hy}} \times \mathbf{v}) = (\mathbf{v} \cdot \nabla) \boldsymbol{\omega}_{\text{a}}^{\text{hy}} - (\boldsymbol{\omega}_{\text{a}}^{\text{hy}} \cdot \nabla) \mathbf{v}, \quad (35.108)$$

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<sup>6</sup>As discussed in Griffies et al. (2020), the form (35.107) is commonly used for Boussinesq and hydrostatic ocean models.

where we introduced the absolute vorticity for a hydrostatic fluid

$$\boldsymbol{\omega}_a^{hy} = f \hat{\mathbf{z}} + \boldsymbol{\omega}^{hy}. \quad (35.109)$$

The result is the vorticity equation

$$\frac{\partial \boldsymbol{\omega}^{hy}}{\partial t} + (\mathbf{v} \cdot \nabla) \boldsymbol{\omega}_a^{hy} = (\boldsymbol{\omega}_a^{hy} \cdot \nabla) \mathbf{v} + \nabla \times \hat{\mathbf{z}} b + \nabla \times \mathbf{F}. \quad (35.110)$$

Since the Coriolis parameter is time independent, we can add it to the time derivative to yield

$$\frac{D \boldsymbol{\omega}_a^{hy}}{Dt} = \underbrace{(\boldsymbol{\omega}_a^{hy} \cdot \nabla) \mathbf{v}}_{\text{stretching + tilting}} + \underbrace{\nabla \times \hat{\mathbf{z}} b}_{\text{baroclinicity}} + \underbrace{\nabla \times \mathbf{F}}_{\text{friction curl}}. \quad (35.111)$$

### 35.8.2 Boussinesq baroclinicity

Equation (35.111) is the vorticity equation for a hydrostatic Boussinesq fluid. We can compare this equation to the vorticity equation for a non-hydrostatic and non-Boussinesq fluid (equation (35.32)). Both equations have a vorticity source due to stretching and tilting, and both have a source due to the curl of friction. However, the baroclinicity vector for the Boussinesq fluid is given by

$$\mathbf{B}_{\text{bouss}} = \nabla \times \hat{\mathbf{z}} b = \nabla b \times \hat{\mathbf{z}}, \quad (35.112)$$

which is simpler than baroclinicity in a compressible fluid

$$\mathbf{B} = (\nabla \rho \times \nabla p) / \rho^2 = -\nabla \times (\rho^{-1} \nabla p) \quad (35.113)$$

(equation (35.40)). We see in Exercise 36.2 that the same baroclinicity vector (35.112) appears for the non-hydrostatic Boussinesq fluid. This form of Boussinesq baroclinicity arises since the pressure gradient acceleration is annihilated by the cross product in the Boussinesq vorticity equation, thus leaving only the buoyancy to affect a baroclinicity source. Consequently, we can diagnose the presence of baroclinicity for the Boussinesq fluid (either non-hydrostatic or hydrostatic) merely by noting whether there is a slope to the buoyancy surfaces relative to the horizontal plane, such as in Figure 35.12. A sloping buoyancy surface provides a vorticity source for the Boussinesq fluid by providing a spin to fluid elements (see Section 35.5).

While the Boussinesq baroclinicity is somewhat simpler than the non-Boussinesq fluid, we lose certain aspects of the physical interpretation offered in Section 35.5 based on baroclinicity as the curl of the pressure acceleration. Since the curl of the non-Boussinesq pressure acceleration has components in all three directions, the non-Boussinesq baroclinicity vector,  $\mathbf{B}$ , affects a source for each of the three vorticity components. In contrast, the Boussinesq baroclinicity is the curl of the Archimedean buoyant acceleration and this acceleration acts only in the vertical. Consequently, the Boussinesq baroclinicity has no direct affect on the vertical component to absolute vorticity

$$\hat{\mathbf{z}} \cdot \mathbf{B}_{\text{bouss}} = \hat{\mathbf{z}} \cdot (\nabla \times \hat{\mathbf{z}} b) = 0. \quad (35.114)$$

That is, Boussinesq baroclinicity only acts directly as a source for horizontal vorticity. Thus, Boussinesq baroclinicity can only indirectly affect vertical vorticity through its effects on vertical velocity and the corresponding vertical stretching.

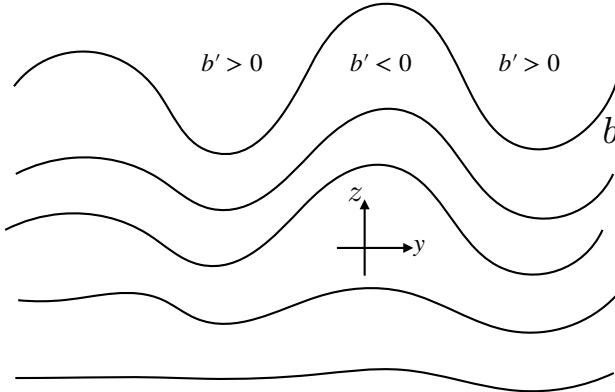


FIGURE 35.12: Baroclinicity in a Boussinesq fluid is manifest by nonzero horizontal gradients in the buoyancy field. Here we depict a region of relatively strong baroclinicity above a region of weaker baroclinicity. A sloping buoyancy surface is therefore synonymous with a nontrivial baroclinic structure. We label anomalously positive (\$b' > 0\$) and negative buoyancy (\$b' < 0\$), where the prime denotes anomalies relative to a horizontal average. Furthermore, as per equation (35.114), baroclinicity in a Boussinesq fluid only acts as a source for horizontal vorticity.

### 35.8.3 Vertical vorticity equation

Following the discussion in Section 35.4.4 for the unapproximated vorticity, we were examine the vertical component of the hydrostatic and Boussinesq vorticity equation (35.111)

$$\frac{D\zeta_a}{Dt} = (\boldsymbol{\omega}_a^{hy} \cdot \nabla) w + \hat{z} \cdot (\nabla \times \mathbf{F}), \quad (35.115)$$

with the absence of baroclinicity noted above in Section 35.8.2. The stretching, tilting, and friction curl appearing on the right hand side provide vorticity sources that affect the left hand side's material time evolution. We see this evolution more fully by expanding the terms to render

$$\frac{\partial \zeta_a}{\partial t} + (\mathbf{v} \cdot \nabla) \zeta + \beta v = \hat{z} \cdot (\partial_z \mathbf{u} \times \nabla_z w) + (\zeta + f) \partial_z w + \hat{z} \cdot (\nabla \times \mathbf{F}). \quad (35.116)$$

#### *Planetary geostrophic limit*

The linearized, inviscid, and steady version of the vorticity equation (35.116) leads to the linear vorticity balance studied in Section 25.5.4 and Chapter 39

$$\beta v = f \partial_z w \quad (35.117)$$

with this relation comprising the inviscid vorticity equation for a flow respecting planetary geostrophic scaling. It represents a kinematic balance since no forces are exposed here to explicitly cause motion, though such forces do appear in the momentum equation. Reading the balance from right to left indicates that any process generating vorticity via vortex stretching must be balanced by meridional motion. That is, the fluid responds to vortex stretching by moving meridionally through the planet's vorticity field. Since the vorticity of a planetary geostrophic fluid is solely determined by planetary vorticity, meridional movement is the only means for the fluid to balance vortex sources. Conversely, reading the equality from left to right reveals that any meridional motion itself must be balanced by vortex stretching.

### Vorticity flux vector

We can write the vorticity equation (35.116) in an alternative form by making use of  $\nabla \cdot \mathbf{v} = \nabla \cdot \boldsymbol{\omega}_a^{hy} = 0$  to yield

$$\frac{\partial \zeta_a}{\partial t} = -\nabla \cdot (\mathbf{v} \zeta_a - w \boldsymbol{\omega}_a^{hy}) + \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}). \quad (35.118)$$

Furthermore, we can write the friction curl in the form

$$\hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}) = \nabla z \cdot (\nabla \times \mathbf{F}) \quad (35.119a)$$

$$= \nabla \cdot [z \nabla \times \mathbf{F}] \quad (35.119b)$$

$$= \nabla \cdot [\nabla \times (z \mathbf{F}) - \nabla z \times \mathbf{F}] \quad (35.119c)$$

$$= -\nabla \cdot (\hat{\mathbf{z}} \times \mathbf{F}). \quad (35.119d)$$

Hence, the vertical component of the Boussinesq vorticity evolves according to the convergence of the vorticity flux

$$\frac{\partial \zeta_a}{\partial t} = -\nabla \cdot \mathbf{J}_\zeta \quad \text{with} \quad \mathbf{J}_\zeta = \mathbf{v} \zeta_a - w \boldsymbol{\omega}_a^{hy} + \hat{\mathbf{z}} \times \mathbf{F}, \quad (35.120)$$

which can be compared to the vorticity flux (35.36) for the compressible nonhydrostatic fluid. Again, the main difference arises from the absence of a baroclinicity contribution for the hydrostatic Boussinesq fluid.

The identity  $\boldsymbol{\omega}_a^{hy} = \hat{\mathbf{z}} \times \partial_z \mathbf{u} + \hat{\mathbf{z}} \zeta_a$  allows us to write

$$\mathbf{v} \zeta_a - w \boldsymbol{\omega}_a^{hy} = \mathbf{u} \zeta_a - w \hat{\mathbf{z}} \times \partial_z \mathbf{u}, \quad (35.121)$$

which is a horizontal vector. Furthermore, note that  $\hat{\mathbf{z}} \times \mathbf{F}$  is a horizontal vector, which then means that there is no vertical contribution to the vorticity flux vector,  $\mathbf{J}_\zeta \cdot \hat{\mathbf{z}} = 0$ . We previously encountered this property in Section 35.4.4 when discussing the vorticity flux for the non-Boussinesq fluid.

## 35.9 Depth integral of the vertical vorticity equation

In this section we study the depth integral of the vertical vorticity equation (35.36)

$$\frac{\partial \zeta_a}{\partial t} = -\nabla \cdot \mathbf{J}_\zeta \quad \text{with} \quad \mathbf{J}_\zeta = \mathbf{v} \zeta_a - \boldsymbol{\omega}_a w - \hat{\mathbf{z}} \times \rho^{-1} \nabla p + \hat{\mathbf{z}} \times \mathbf{F}. \quad (35.122)$$

We perform the depth integral over the full depth of the ocean from its bottom at  $z = \eta_b(x, y)$  to the ocean surface at  $z = \eta(x, y, t)$  (see Figure 30.1). Studies of the depth integrated vorticity equation allow us to focus on the two dimensional budgets with particular attention to how boundary torques alter the budget. This section anticipates analysis of the depth integrated planetary geostrophic vorticity equation in Section 39.5, with that analysis of use for understanding the role of topography in forcing the large-scale ocean circulation. We also consider the vorticity of the depth integrated flow in Section 35.10, which is commonly considered in numerical applications.

### 35.9.1 Comments on the baroclinicity source

Results of this analysis in this section can be readily specialized to the Boussinesq and hydrostatic case given by equation (35.120). The key distinction, as noted in Section 35.8.2, is that Boussinesq baroclinicity does not directly affect changes to the vertical component of the Boussinesq vorticity

(whether hydrostatic or non-hydrostatic; see Exercise 36.2). This property of the Boussinesq baroclinicity means that the boundary pressure torques discussed in Sections 35.9.3 and 35.9.4 play no direct role in the Boussinesq vorticity equation. However, these boundary pressure torques play a direct role in vertical motion next to the boundaries, especially next to the bottom, with such motion affecting a source to vorticity through stretching. We have much to say in Section 39.5 concerning how boundary pressure torques affect vertical motion for vorticity for the planetary geostrophic fluid. Additionally, as seen in Section 35.10, boundary pressure torques do play a direct role in affecting vorticity of the depth integrated flow in both the Boussinesq and non-Boussinesq fluids.

This discussion exemplifies the sometimes subtle differences between vorticity sources depending on the precise nature of the vorticity, whether it be vorticity for a fluid element as discussed in this section, vorticity of the depth integrated flow in Section 35.10, or vorticity of the depth averaged flow in Section 35.10.6. When studying flavors of vorticity, it is important to be clear on details of their evolution equations since the details color the physical interpretations.

### 35.9.2 Leibniz rule expressions

The necessary manipulations are typical for the analysis of depth integrated budgets, such as considered for the depth integrated momentum in Section 19.4 and depth integrated angular momentum in Section 19.5. For vorticity we are interested in manipulating following equation

$$\int_{\eta_b}^{\eta} \frac{\partial \zeta_a}{\partial t} dz = - \int_{\eta_b}^{\eta} \nabla \cdot \mathbf{J}_\zeta dz, \quad (35.123)$$

where  $\mathbf{J}_\zeta$  is the vorticity flux given by equation (35.122). We make use of Leibniz's rule (Section 15.3.4) to move the time and space derivatives from inside the integrals to outside

$$\int_{\eta_b}^{\eta} \frac{\partial \zeta_a}{\partial t} dz = -[\zeta_a \partial_t \eta]_{z=\eta} + \frac{\partial}{\partial t} \int_{\eta_b}^{\eta} \zeta_a dz \quad (35.124)$$

$$- \int_{\eta_b}^{\eta} \nabla_z \cdot \mathbf{J}_\zeta dz = [\nabla_z \eta \cdot \mathbf{J}_\zeta]_{z=\eta} - [\nabla_z \eta_b \cdot \mathbf{J}_\zeta]_{z=\eta_b} - \nabla_z \cdot \int_{\eta_b}^{\eta} \mathbf{J}_\zeta dz \quad (35.125)$$

$$- \int_{\eta_b}^{\eta} \frac{\partial (\hat{\mathbf{z}} \cdot \mathbf{J}_\zeta)}{\partial z} dz = -[\hat{\mathbf{z}} \cdot \mathbf{J}_\zeta]_{z=\eta} + [\hat{\mathbf{z}} \cdot \mathbf{J}_\zeta]_{z=\eta_b}. \quad (35.126)$$

These results then lead to

$$\frac{\partial}{\partial t} \int_{\eta_b}^{\eta} \zeta_a dz = -\nabla_z \cdot \int_{\eta_b}^{\eta} \mathbf{J}_\zeta dz + [\zeta_a \partial_t \eta - \nabla(z - \eta) \cdot \mathbf{J}_\zeta]_{z=\eta} + [\nabla(z - \eta_b) \cdot \mathbf{J}_\zeta]_{z=\eta_b}. \quad (35.127)$$

The time tendency for the depth integrated absolute vorticity for a fluid column (left hand side) is determined by the convergence of the depth integrated vorticity flux (first term on right hand side) plus a suite of boundary contributions due to baroclinicity, vortex stretching and friction. We next massage the boundary contributions to expose their associated physical processes.

### 35.9.3 Bottom boundary contribution

The bottom boundary contribution to the vorticity equation (35.127) takes on the form

$$\nabla(z - \eta_b) \cdot \mathbf{J}_\zeta = \nabla(z - \eta_b) \cdot [\mathbf{v} \zeta_a - \boldsymbol{\omega}_a w - \hat{\mathbf{z}} \times \rho^{-1} \nabla p + \hat{\mathbf{z}} \times \mathbf{F}]_{z=\eta_b} \quad (35.128a)$$

$$= -|\nabla(z - \eta_b)| \hat{\mathbf{n}} \cdot [-\boldsymbol{\omega}_a w - \hat{\mathbf{z}} \times \rho^{-1} \nabla p + \hat{\mathbf{z}} \times \mathbf{F}]_{z=\eta_b}, \quad (35.128b)$$

where we made use of the no-normal flow bottom kinematic boundary condition,  $\hat{\mathbf{n}} \cdot \mathbf{v} = 0$  (Section 14.4.1), and where

$$\hat{\mathbf{n}} = - \left[ \frac{\nabla(z - \eta_b)}{|\nabla(z - \eta_b)|} \right] = - \left[ \frac{\hat{\mathbf{z}} - \nabla_z \eta_b}{\sqrt{1 + \nabla_z \eta_b \cdot \nabla_z \eta_b}} \right] \quad (35.129)$$

is the outward normal at the bottom.

#### *Vortex stretching by vertical flow along a sloping bottom*

The first term in the bottom boundary flux (35.128b) provides an inviscid vertical transport of the normal component of the absolute vorticity at the boundary. This term contributes through the action of vertical motion next to a sloping bottom, thus providing a vertical transfer of the vorticity component that is perpendicular to the bottom. This motion provides a form of vortex stretching that vanishes for a flat bottom, in which case  $w(\eta_b) = 0$ . It also vanishes for flow that parallels the bottom, whereby  $\mathbf{u} \cdot \nabla \eta_b = 0$  so that  $w(\eta_b) = 0$  according to the bottom kinematic boundary condition (14.41).

#### *Bottom pressure torques*

The second term in the bottom boundary flux (35.128b) arises from baroclinicity next to the bottom, and it can be written in the form

$$\hat{\mathbf{n}} \cdot [\hat{\mathbf{z}} \times (\rho^{-1} \nabla p_b)] = \rho^{-1} \nabla p_b \cdot (\hat{\mathbf{n}} \times \hat{\mathbf{z}}) \equiv \rho^{-1} \nabla p_b \cdot \mathbf{t} \quad \text{with} \quad \mathbf{t} = \hat{\mathbf{n}} \times \hat{\mathbf{z}} = \left[ \frac{\nabla \eta_b \times \hat{\mathbf{z}}}{|\nabla(z - \eta_b)|} \right]. \quad (35.130)$$

The vector  $\mathbf{t}$  is horizontal and it points along isolines of constant topography in a direction with land to the left pointing in the direction of  $\mathbf{t}$ , as depicted in Figure 35.13. Since  $\hat{\mathbf{z}}$  and  $\hat{\mathbf{n}}$  are not orthogonal,  $\mathbf{t}$  is not normalized so that it is not adorned with a hat. We thus find the contribution from baroclinicity takes the form

$$\nabla(z - \eta_b) \cdot \mathbf{J}_\zeta^{\text{baroclinicity}} = \rho^{-1} \nabla p_b \cdot (\nabla \eta_b \times \hat{\mathbf{z}}) = \rho^{-1} \hat{\mathbf{z}} \cdot [\nabla \times (p_b \nabla \eta_b)]. \quad (35.131)$$

Hence, the contribution from baroclinicity next to the bottom takes the form of a bottom pressure torque due to bottom pressure isolines that are not parallel to bottom topography isolines. We have more to say concerning boundary pressure torques in Section 35.10.3 as they also affect vorticity of the depth integrated flow.

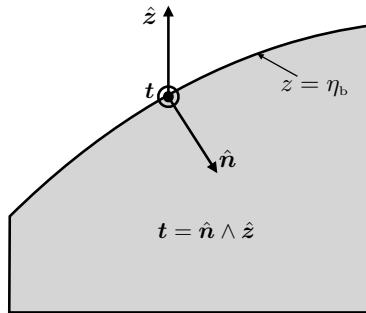


FIGURE 35.13: Orientation of the unit vectors next to the bottom of the fluid. The vertical unit vector,  $\hat{\mathbf{z}}$ , points vertically upward and the outward unit vector,  $\hat{\mathbf{n}}$ , points downward into the rock (shaded gray). The along-topography horizontal vector,  $\mathbf{t} = \hat{\mathbf{n}} \times \hat{\mathbf{z}}$ , points along lines of constant topography with land to the left when facing in the direction of  $\mathbf{t}$ ; in this figure it points out from the page. The vector  $\mathbf{t}$  is not necessarily a unit vector since it is not orthogonal to  $\hat{\mathbf{n}}$ .

### Torques from bottom friction

The third term in the boundary flux (35.128b) is the contribution from friction along the bottom

$$-\hat{\mathbf{n}} \cdot (\hat{\mathbf{z}} \times \mathbf{F}) = -\mathbf{F} \cdot (\hat{\mathbf{n}} \times \hat{\mathbf{z}}) \equiv -\mathbf{F} \cdot \mathbf{t}. \quad (35.132)$$

Hence, contributions to the vertical vorticity evolution arise from the component of friction that projects onto the direction that parallels isobaths. To further our understanding of this result, consider a bottom friction written as a Rayleigh drag (e.g., Section 27.2.3) so that  $\mathbf{F} = -\gamma \mathbf{u}$  and

$$-\mathbf{F} \cdot \mathbf{t} = \gamma \mathbf{u} \cdot \mathbf{t}, \quad (35.133)$$

with  $\gamma$  an inverse time scale. If the flow is oriented with shallow water to the right; e.g., into the page in Figure 35.13, then  $-\mathbf{F} \cdot \mathbf{t} < 0$ , thus contributing a negative vorticity tendency. In general, the bottom friction acts to damp the depth integrated vorticity, which is expected since bottom friction does not spontaneously spin-up the flow.

### 35.9.4 Surface boundary contribution

The surface boundary contribution to the vorticity equation (35.127) takes on a similar form to the bottom, with the new feature that the free surface is both moving and permeable (Section 14.4.3). This boundary term takes on the form

$$\zeta_a \partial_t \eta - \nabla(z - \eta) \cdot \mathbf{J}_\zeta = \zeta_a \partial_t \eta - \nabla(z - \eta) \cdot [\mathbf{v} \zeta_a - w \omega_a^{hy} - \hat{\mathbf{z}} \times \rho^{-1} \nabla p + \hat{\mathbf{z}} \times \mathbf{F}]_{z=\eta} \quad (35.134a)$$

$$= \zeta_a [\partial_t \eta + \mathbf{u} \cdot \nabla_z \eta - w]_{z=\eta} + \nabla(z - \eta) \cdot [w \omega_a^{hy} + \hat{\mathbf{z}} \times \rho^{-1} \nabla p - \hat{\mathbf{z}} \times \mathbf{F}]_{z=\eta} \quad (35.134b)$$

$$= \zeta_a Q_m / \rho + |\nabla(z - \eta)| \hat{\mathbf{n}} \cdot [w \omega_a^{hy} + \hat{\mathbf{z}} \times \rho^{-1} \nabla p - \hat{\mathbf{z}} \times \mathbf{F}]_{z=\eta}, \quad (35.134c)$$

where we made use of the surface kinematic boundary condition (14.79) to introduce the surface mass flux  $Q_m$ , and where

$$\hat{\mathbf{n}} = \frac{\nabla(z - \eta)}{|\nabla(z - \eta)|} = \frac{\nabla_z \eta + \hat{\mathbf{z}}}{\sqrt{1 + \nabla_z \eta \cdot \nabla_z \eta}} \quad (35.135)$$

is the outward normal at the surface. The first term in the surface boundary flux (35.134c) provides transport of boundary vorticity due to the transfer of mass across the boundary. The second term provides an inviscid vertical transport of absolute vorticity at the surface boundary, thus acting as a vortex stretching contribution. The third term provides a torque due to misalignments between the applied pressure isobars and the free surface isolines

$$|\nabla(z - \eta)| \hat{\mathbf{n}} \cdot (\hat{\mathbf{z}} \times \rho^{-1} \nabla p_a) = \rho^{-1} \nabla p_a \cdot (\nabla \eta \times \hat{\mathbf{z}}) = \rho^{-1} \hat{\mathbf{z}} \cdot \nabla \times (p_a \nabla \eta), \quad (35.136)$$

where the density,  $\rho$ , is evaluated at the ocean surface. The fourth term provides the corresponding contribution from the friction along the upper surface, with friction acting to reduce the magnitude of the surface boundary vorticity. For a rigid lid surface,  $w(0) = 0$ ,  $\eta = 0$ , and  $Q_m = 0$  so that the only surface boundary contribution arises from friction.

### 35.9.5 Comments

The depth integrated vorticity budget as derived in this section is perhaps the most physically straightforward of the suite of depth integrated vorticity budgets. However, in the practice of ocean modeling, this budget is generally not used since it requires an online coding of the vorticity equation and then its depth integral. As ocean models generally time step the velocity rather

than the vorticity, it is common to form a vorticity budget based on the depth integrated flow or the depth averaged flow. We develop these budgets in the following sections.

## 35.10 Vorticity for the depth integrated horizontal flow

In this section we develop dynamical equations for vorticity of the depth integrated flow in a hydrostatic fluid. A compelling application of these ideas comes from the study of large-scale ocean circulation. The leading order impacts from bottom pressure torques has emerged from research during recent decades, thus pointing to the fundamental role of bottom topography and flows next to sloping bottom (rather than vertical sidewalls) in affecting the ocean circulation. This recognition contrasts to traditional theories whereby the wind stress curl balances meridional motion through the beta effect. In particular, numerical model studies reveal that wind stress curl is sub-dominant in any region with nontrivial bottom velocities.<sup>7</sup> In this section we introduce the basics and provide more discussion in Sections 39.7 and 39.8 when studying vorticity dynamics for the planetary geostrophic system.

### 35.10.1 Comparing the two vorticities

In Section 35.9 we derived the evolution equation for the depth integral of the vertical component to the absolute vorticity,

$$\int_{\eta_b}^{\eta} \zeta_a dz = \int_{\eta_b}^{\eta} (f + \hat{z} \cdot \nabla \times \mathbf{u}) dz. \quad (35.137)$$

In this section we study the evolution equation for the relative vorticity in the depth integrated horizontal flow

$$\hat{z} \cdot \nabla \times \mathbf{U}^\rho = \hat{z} \cdot \nabla \times \int_{\eta_b}^{\eta} \mathbf{u} \rho dz, \quad (35.138)$$

where we introduced the depth integrated horizontal mass flux

$$\mathbf{U}^\rho = \int_{\eta_b}^{\eta} \rho \mathbf{u} dz. \quad (35.139)$$

For a Boussinesq fluid we set the density to a constant, in which case the difference between the two relative vorticities is

$$\hat{z} \cdot \nabla \times \left[ \int_{\eta_b}^{\eta} \mathbf{u} dz \right] - \int_{\eta_b}^{\eta} \hat{z} \cdot \nabla \times \mathbf{u} dz = \hat{z} \cdot [\nabla \eta \times \mathbf{u}(\eta) - \nabla \eta_b \times \mathbf{u}(\eta_b)]. \quad (35.140)$$

Flows along boundaries generally have a nontrivial projection in the direction parallel to boundary isosurfaces, in which case the cross products are nonzero thus leading to differences in the two relative vorticities.

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<sup>7</sup>The natural ocean has no distinction between side and bottom. Rather, as discussed in Figure 19.7, the ocean has a sloping bottom that reaches to the surface along its boundary at the “beach.” [Hallberg and Rhines \(1996\)](#), [Hughes and de Cueves \(2001\)](#), and many subsequent studies emphasize that theoretical and numerical models using vertical sides and a flat bottom exhibit somewhat unnatural dynamical balances, whereas models with sloping bottoms better capture key effects from topography.

### 35.10.2 Evolution of vorticity for the depth integrated horizontal flow

In Section 19.4 we developed the horizontal momentum equation for a hydrostatic fluid, which takes the form of equation (19.41)

$$(\partial_t + f \hat{z} \times) \mathbf{U}^\rho = \mathbf{u}(\eta) Q_m - \eta \nabla_z p_a + \eta_b \nabla_z p_b - \nabla_z \mathcal{P} + \nabla_z \cdot \left[ \int_{\eta_b}^{\eta} \mathbb{T}_{\text{hor}}^{\text{kinetic}} dz \right] + \int_{\eta_b}^{\eta} \rho \mathbf{F} dz. \quad (35.141)$$

Operating with  $\hat{z} \cdot \nabla \times$  onto this momentum equation leads to

$$\begin{aligned} \hat{z} \cdot \partial_t (\nabla \times \mathbf{U}^\rho) &= -\nabla \cdot (f \mathbf{U}^\rho) \\ &+ \hat{z} \cdot \nabla \times \left[ \mathbf{u}(\eta) Q_m - \eta \nabla_z p_a + \eta_b \nabla_z p_b + \Delta \boldsymbol{\tau} + \mathbf{D} + \nabla_z \cdot \left( \int_{\eta_b}^{\eta} \mathbb{T}_{\text{hor}}^{\text{kinetic}} dz \right) \right], \end{aligned} \quad (35.142)$$

where we wrote friction in the form (19.42), and used the vector identity

$$\hat{z} \cdot \nabla \times (f \hat{z} \times \mathbf{U}^\rho) = \nabla \cdot (f \mathbf{U}^\rho), \quad (35.143)$$

as well as  $\nabla \times \nabla_z \mathcal{P} = 0$ . We now offer some discussion of the various physical processes appearing in the vorticity equation (35.142).

#### Beta effect

The first term on the right hand side of the vorticity equation (35.142) arises from the convergence of mass within a fluid column due to depth integrated horizontal flow. We can further decompose the effects from this term by performing the product rule

$$-\nabla \cdot (f \mathbf{U}^\rho) = -f \nabla \cdot \mathbf{U}^\rho - \beta V^\rho. \quad (35.144)$$

The contribution from  $\beta V^\rho$  arises from the beta effect as discussed in Section 35.7.2. For the first term, the weighting by the Coriolis parameter means that mass convergence at higher latitudes has more impact on vorticity changes than at lower latitudes. We can understand this weighting by noting that vertical fluid columns are more aligned with the planetary rotation at the high latitudes. Hence, when the mass of vertical columns converges at the higher latitudes, there is more impact on changes to the vorticity of the depth integrated flow.

#### Mass transfer, turbulent momentum transfer, and nonlinear effects

The term  $\nabla \times [\mathbf{u}(\eta) Q_m]$  accounts for vorticity crossing the ocean surface as affected by the mass flux. The term  $\nabla \times \Delta \boldsymbol{\tau}$  in equation (35.145) is the torque from turbulent stresses at the ocean surface and bottom, and  $\hat{z} \cdot \nabla \times \mathbf{D}$  is the torque from horizontal frictional stresses in the fluid interior. The final term arises from the nonlinear kinetic stresses,  $\mathbb{T}_{\text{hor}}^{\text{kinetic}}$ , that account for curls in the self-advection operator.

### 35.10.3 Boundary pressure torques

The pressure terms in equation<sup>8</sup> (35.142)

$$\hat{z} \cdot \nabla \times (-\eta \nabla p_a + \eta_b \nabla p_b) = \hat{z} \cdot \nabla \times (p_a \nabla \eta - p_b \nabla \eta_b) \quad (35.145)$$

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<sup>8</sup>Recall that to reduce notational clutter, we can write  $\nabla$  rather than  $\nabla_z$  when operating on functions that are independent of  $z$ , such as  $\eta$ ,  $p_a$ ,  $\eta_b$  and  $p_b$ .

arise from curls of the pressure form stresses (see Chapter 19) at the ocean surface and bottom, and these contributions are referred to as *pressure torques*. When the fluid is a column of ocean water, then the surface pressure contribution is the *atmospheric pressure torque* and the bottom pressure term is the *bottom pressure torque*.

### Geometry of boundary pressure torques

Geometrically, there is a nonzero atmospheric pressure torque when the applied pressure changes when moving along contours of constant free surface. Likewise, there is a nonzero bottom pressure torque when bottom pressure changes along contours of constant bottom topography. Mathematically, we reveal these properties through use of either Exercise 5.1 or 35.11. For example, the bottom pressure torque along an isobath (contour of constant  $\eta_b$ ) can be written

$$\hat{z} \cdot \nabla \eta_b \times \nabla p_b = -(\hat{n} \cdot \nabla \eta_b)(\hat{t} \cdot \nabla p_b), \quad (35.146)$$

where  $\hat{t}$  is a unit tangent vector directed along the isobath, and  $\hat{n}$  is a horizontal unit vector that points to the left of  $\hat{t}$  (see Figure 35.14). Hence,  $\hat{n} \cdot \nabla \eta_b$  measures the slope of the bottom topography in the direction normal to an isobath, and  $\hat{t} \cdot \nabla p_b$  measures the change of the bottom pressure along the isobath. There is a nonzero bottom pressure torque along an isobath so long as there is a slope to the bottom along the isobath, and there is a change in bottom pressure moving along the isobath.

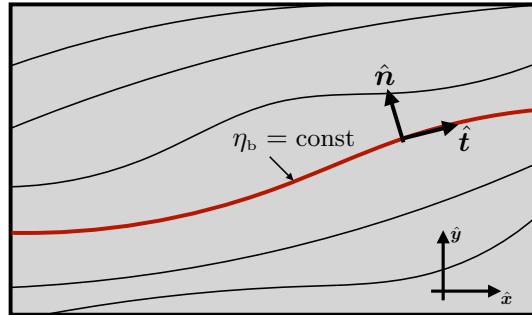


FIGURE 35.14: Geometry depicting a contour along a particular line of constant topography (i.e., an isobath),  $\eta_b(x, y)$ . The along-contour direction is  $\hat{t} = dx/ds$ , with  $s$  the arc length along the contour. The unit direction pointing to the left of  $\hat{t}$  is written  $\hat{n}$ , with  $\hat{n} \cdot \hat{t} = 0$  and  $\hat{t} \times \hat{n} = \hat{z}$ . Both  $\hat{n}$  and  $\hat{t}$  are horizontal unit vectors. There is a nonzero bottom pressure torque if bottom pressure changes when following an isobath.

### Geostrophic velocity associated with the bottom pressure torque

To further our understanding of the pressure torques in equation (35.145), focus on the bottom pressure and introduce a geostrophic velocity

$$\rho_0 f \mathbf{u}_g = \hat{z} \times \nabla p_b, \quad (35.147)$$

so that the bottom pressure torque takes the form

$$\hat{z} \cdot \nabla \times (\eta_b \nabla p_b) = \hat{z} \cdot \nabla \eta_b \times \nabla p_b = \rho_0 f \mathbf{u}_g \cdot \nabla \eta_b. \quad (35.148)$$

This equation is merely a replacement of the bottom pressure gradient with a corresponding geostrophic velocity. However, if this geostrophic velocity is assumed to satisfy the kinematic

boundary condition (14.41), then we reach the equality<sup>9</sup>

$$\hat{z} \cdot \nabla \eta_b \times \nabla p_b = \rho_0 f w_g, \quad (35.149)$$

which links the bottom pressure torque to vertical vortex stretching by the vertical component to the geostrophic velocity.

The equality (35.149) is sometimes used to infer the bottom pressure torque by diagnosing the bottom vertical velocity,  $w(\eta_b)$ . Although this diagnostic is suitable for some studies, there are important caveats. Namely, the bottom vertical velocity is generally affected by bottom frictional effects and thus can have a nontrivial Ekman component.<sup>10</sup> Nonlinear effects can also be important especially when considering motions with sizable Rossby numbers. Neither the Ekman component nor nonlinear terms are directly related to the bottom pressure torque. We thus expect  $\rho_0 f w(\eta_b)$  to be distinct from  $\hat{z} \cdot \nabla \eta_b \times \nabla p_b$  in regions of sizable deep flows where bottom friction and/or nonlinear effects are of leading order importance.<sup>11</sup> The studies from [Gula et al. \(2015\)](#) and [LeCorre et al. \(2020\)](#) illustrate these points from numerical simulations of the subpolar North Atlantic circulation.

### 35.10.4 Steady state vorticity budget

The steady state form of the vorticity budget (35.142) leads to the balance

$$\begin{aligned} \beta V^\rho &= -f \nabla \cdot \mathbf{U}^\rho \\ &+ \hat{z} \cdot \nabla \times \left[ \mathbf{u}(\eta) Q_m - \eta \nabla_z p_a + \eta_b \nabla_z p_b + \Delta \boldsymbol{\tau} + \mathbf{D} + \nabla_z \cdot \left( \int_{\eta_b}^{\eta} \mathbb{T}_{\text{hor}}^{\text{kinetic}} dz \right) \right]. \end{aligned} \quad (35.150)$$

Writing the balance in this manner reveals how the beta affect affords a steady meridional mass transport as a balance with the variety of terms on the right hand side.

Let us further specialize to the case appropriate for many studies of the large-scale circulation, whereby we make the following assumptions.

- Uniform mass atmosphere so that  $p_a$  is a constant.
- The frictional stresses from horizontal strains within the fluid interior,  $\mathbf{D}$ , can be neglected.
- Zero boundary mass transport so that  $Q_m = 0$  and, correspondingly, the steady depth integrated mass budget (14.88) means that  $\nabla \cdot \mathbf{U}^\rho = 0$  when  $Q_m = 0$ .

These simplifications bring the balance (35.150) to the form

$$\beta V^\rho = \hat{z} \cdot \nabla \times \left[ \eta_b \nabla_z p_b + \Delta \boldsymbol{\tau} + \nabla_z \cdot \left( \int_{\eta_b}^{\eta} \mathbb{T}_{\text{hor}}^{\text{kinetic}} dz \right) \right] \quad (35.151a)$$

$$\text{MERIDIONAL TRANSPORT} = \text{BOTTOM PRESS TORQUE} + \text{BOUNDARY STRESS} + \text{NONLINEAR}. \quad (35.151b)$$

This steady balance reveals distinct flow regimes depending on which of the terms dominate, and as such it serves as a useful framework for analysis. In particular, [Jackson et al. \(2006\)](#) and

<sup>9</sup>The velocity,  $\mathbf{v}$ , satisfies the kinematic boundary condition (14.41), in which  $\mathbf{v}(\eta_b) \cdot \hat{\mathbf{n}} = 0$ . Decomposing the velocity into its geostrophic and ageostrophic components,  $\mathbf{v} = \mathbf{v}_g + \mathbf{v}_a$ , does not generally imply that  $\mathbf{v}_g$  and  $\mathbf{v}_a$  separately satisfies the kinematic boundary condition. Rather, we must make that assumption in order to reach the equality (35.149).

<sup>10</sup>Recall our discussion of Ekman boundary layers in Chapter 27.

<sup>11</sup>In addition to the Ekman and nonlinear effects noted here, diagnosing  $w(\eta_b)$  in a numerical model can be fraught with difficulties related to the discrete grid stencil given that grids can be quite coarse in the deep ocean with many ocean model configurations.

*Patmore et al. (2019)* emphasize the importance of the nonlinear term when flows are realistically strong. For the linear regime of planetary geostrophic flow (Chapter 39), the nonlinear term from the kinetic stress is small, so that the balance is between meridional transport, bottom pressure torque, and curl of turbulent boundary stresses. We consider this balance in Sections 39.5, 39.7, and 39.8.

The *Sverdrup balance* is one particular example of a planetary geostrophic balance, with Sverdrup balance ignoring the bottom pressure torque and bottom turbulent stresses, and thus focuses just on the balance between meridional transport with the turbulent surface stresses largely arising from winds

$$\beta V^\rho = \hat{\mathbf{z}} \cdot \nabla \times \boldsymbol{\tau}^\eta \quad \text{Sverdrup balance.} \quad (35.152)$$

However, as emphasized by *Hallberg and Rhines (1996)* and *Hughes and de Cueves (2001)*, as well as more recent studies, contributions from bottom pressure torques are of leading order importance in the presence of sloping side boundaries, thus making the traditional Sverdrup balance mostly relevant in the open ocean away from boundaries.

### 35.10.5 Formulation based on the vector invariant velocity equation

In formulating the budget equation (35.142) for vorticity of the depth integrated flow, we started with the depth integrated momentum in Section 19.4.5. However, many numerical models are formulated using the vector invariant form of the horizontal velocity equation (35.107), here written in the equivalent form for a Boussinesq fluid

$$\underbrace{\partial_t \mathbf{u} + f \hat{\mathbf{z}} \times \mathbf{u} + \nabla_z p / \rho_0 - \mathbf{F}}_{\text{linear terms plus friction}} = \underbrace{-\zeta \hat{\mathbf{z}} \times \mathbf{u} - w \partial_z \mathbf{u} - \nabla_z \mathbf{u}^2 / 2}_{\text{Magnus + vertical advection + kinetic energy}}. \quad (35.153)$$

The three nonlinear terms on the right hand side arise from expanding the nonlinear self-advection term,  $(\mathbf{v} \cdot \nabla) \mathbf{u}$ , following the manipulations in Section 35.8.1. Much of the formulation to follow emulates that considered thus far, with the exception of the nonlinear terms and elements of the boundary contributions.

We take the vertical integral of equation (35.153)

$$\int_{\eta_b}^{\eta} [\partial_t \mathbf{u} + f \hat{\mathbf{z}} \times \mathbf{u} + \nabla_z p / \rho_0 - \mathbf{F}] dz = - \int_{\eta_b}^{\eta} (\zeta \hat{\mathbf{z}} \times \mathbf{u} + w \partial_z \mathbf{u} + \nabla_z \mathbf{u}^2 / 2) dz, \quad (35.154)$$

and then the curl

$$\nabla \times \int_{\eta_b}^{\eta} (\partial_t \mathbf{u} + f \hat{\mathbf{z}} \times \mathbf{u} + \nabla_z p / \rho_0 - \mathbf{F}) dz = - \nabla \times \int_{\eta_b}^{\eta} (\zeta \hat{\mathbf{z}} \times \mathbf{u} + w \partial_z \mathbf{u} + \nabla_z \mathbf{u}^2 / 2) dz. \quad (35.155)$$

Making use of the following identities

$$\hat{\mathbf{z}} \cdot \left[ \nabla \times \int_{\eta_b}^{\eta} \partial_t \mathbf{u} dz \right] = \hat{\mathbf{z}} \cdot \partial_t (\nabla \times \mathbf{U}) - \hat{\mathbf{z}} \cdot \nabla \times [\mathbf{u}(\eta) \partial_t \eta] \quad (35.156a)$$

$$\hat{\mathbf{z}} \cdot \left[ \nabla \times \int_{\eta_b}^{\eta} f \hat{\mathbf{z}} \times \mathbf{u} dz \right] = \nabla \cdot (f \mathbf{U}) \quad (35.156b)$$

$$\hat{\mathbf{z}} \cdot \left[ \nabla \times \int_{\eta_b}^{\eta} \nabla_z p dz \right] = \hat{\mathbf{z}} \cdot \nabla \times (\eta \nabla p_a - \eta_b \nabla p_b) \quad (35.156c)$$

$$\hat{\mathbf{z}} \cdot \left[ \nabla \times \int_{\eta_b}^{\eta} \zeta \hat{\mathbf{z}} \times \mathbf{u} dz \right] = \nabla \cdot \left[ \int_{\eta_b}^{\eta} \zeta \mathbf{u} dz \right] \quad (35.156d)$$

$$\hat{\mathbf{z}} \cdot \left[ \nabla \times \int_{\eta_b}^{\eta} \rho_0 \mathbf{F} dz \right] = \hat{\mathbf{z}} \cdot \nabla \times (\Delta \boldsymbol{\tau} + \mathbf{D}), \quad (35.156e)$$

leads to

$$\begin{aligned} \hat{\mathbf{z}} \cdot \partial_t (\nabla \times \mathbf{U}) &= -\nabla \cdot \left[ f \mathbf{U} + \int_{\eta_b}^{\eta} \zeta \mathbf{u} dz \right] \\ &+ \hat{\mathbf{z}} \cdot \nabla \times \left[ \mathbf{u}(\eta) \partial_t \eta - \eta \nabla p_a + \eta_b \nabla p_b + (\Delta \boldsymbol{\tau} + \mathbf{D})/\rho_0 - \int_{\eta_b}^{\eta} (w \partial_z \mathbf{u} + \nabla_z \mathbf{u}^2/2) dz \right]. \end{aligned} \quad (35.157)$$

The left hand side is the time tendency of the vorticity of the depth integrated horizontal flow, with this time tendency driven by the various linear and nonlinear terms on the right hand side. This evolution equation should be compared to equation (35.142) as derived from the advective form of the momentum equation. Likewise, we derive a steady state balance by setting the time tendencies to zero to yield

$$\begin{aligned} \beta V &= -f \nabla \cdot \mathbf{U} - \nabla \cdot \left[ \int_{\eta_b}^{\eta} \zeta \mathbf{u} dz \right] \\ &+ \hat{\mathbf{z}} \cdot \nabla \times \left[ \mathbf{u}(\eta) \partial_t \eta - \eta \nabla p_a + \eta_b \nabla p_b + (\Delta \boldsymbol{\tau} + \mathbf{D})/\rho_0 - \int_{\eta_b}^{\eta} (w \partial_z \mathbf{u} + \nabla_z \mathbf{u}^2/2) dz \right], \end{aligned} \quad (35.158)$$

which should be compared to equation (35.150).

### 35.10.6 Vorticity of the depth averaged flow

The vorticity of the depth averaged flow is given by  $\hat{\mathbf{z}} \cdot \nabla \times \bar{\mathbf{u}}$ , where  $\bar{\mathbf{u}}$  is given by equation (19.33) for a compressible non-Boussinesq fluid, and which takes on the following form for a Boussinesq fluid

$$\bar{\mathbf{u}} = \frac{\int_{\eta_b}^{\eta} \mathbf{u} dz}{\eta - \eta_b} = \frac{\mathbf{U}}{\eta - \eta_b}. \quad (35.159)$$

The difference is given by

$$\nabla \times \mathbf{U} - (\eta - \eta_b) \nabla \times \bar{\mathbf{u}} = \nabla(\eta - \eta_b) \times \bar{\mathbf{u}}, \quad (35.160)$$

so that the two vorticities are the same in the special case of a depth averaged flow that is parallel to  $\nabla(\eta - \eta_b)$ . Quite trivially,  $\nabla(\eta - \eta_b) \times \bar{\mathbf{u}} = 0$  occurs for a rigid lid and flat bottom ocean, in which  $\nabla \eta = \nabla \eta_b = 0$ . More generally,  $\nabla(\eta - \eta_b) \times \bar{\mathbf{u}} \neq 0$ , particularly in the presence of topography. We further study the budgets for these two vorticities, for planetary geostrophic flow, in Sections 39.7 and 39.8.

### 35.10.7 Comments and further study

The diagnostic budgets derived in this section have appeared in many studies of ocean vorticity. When diagnosing the budget terms in a numerical model, the choice for how to mathematically formulate the diagnostic balances is largely driven by physical transparency as well as by numerical precision. Concerning numerical precision, it is useful to note that vorticity, as the derivative of velocity, has more power at the high spatial wave numbers than does velocity. In a numerical model, such power can manifest as grid scale noise. It is thus of use to perform much of the calculation online to enable the most precise diagnostic available. Further spatial smoothing is generally required, especially in realistic models, to extract physically interpretable signals.



## 35.11 Exercises

### EXERCISE 35.1: STRAIN AND ROTATION FOR STRETCHING AND TILTING

In this exercise we write the  $3 \times 3$  rate of strain tensor,  $\mathbb{S}$ , and rotation tensor,  $\mathbb{R}$ , for the examples of vortex stretching and vortex tilting considered in Section 35.6.3. Recall that elements of  $\mathbb{S}$  are given by equation (13.33a) and  $\mathbb{R}$  have elements given by equation (13.33b). Hint: there is no unique answer for the rate of strain tensors, so offer a simple example that renders the desired behavior of a vortex filament.

- Write a rate of strain tensor corresponding to vortex stretching as per equation (35.60) along with  $\omega^x = \omega^y = 0$ , and write the corresponding vorticity source term  $\boldsymbol{\omega} \cdot \mathbb{S}$ .
- Write the rotation tensor for vortex stretching as per equation (35.60) and verify that  $\omega_m \cdot \mathbb{R}_{mn} = 0$ .
- Write a rate of strain tensor corresponding to vortex tilting as per equation (35.66) along with  $\omega^y = \omega^z = 0$ .
- Write the rotation tensor for vortex tilting as per equation (35.66) and verify that  $\omega_m \mathbb{R}_{mn} = 0$ .

### EXERCISE 35.2: BAROCLINICITY WITH $\rho_0(z)$

Recall the discussion of the Boussinesq momentum equation in Section 23.1.2. The form given by equation (23.8) is written with the reference density,  $\rho_0 = \rho_0(z)$ . We then stated that the form of the baroclinicity vector appearing in the Boussinesq vorticity equation is greatly simplified by setting  $\rho_0$  to a global constant, and thus dropping the  $z$  dependence. Derive the second term in the baroclinicity

$$\mathbf{B} = \nabla \left[ b - \frac{\delta p}{\rho_0^2} \frac{d\rho_0}{dz} \right] \times \hat{\mathbf{z}}, \quad (35.161)$$

so that  $\mathbf{B} = \nabla b \times \hat{\mathbf{z}}$  when  $\rho_0$  is assumed to be a global constant. Hint: write the vector-invariant form of equation (23.8) with  $\rho_0(z)$ . Then take the curl.

### EXERCISE 35.3: FRICTION IN THE VORTICITY EQUATION

Add a viscous term of the form

$$\mathbf{F} = \nu \nabla^2 \mathbf{v}, \quad (35.162)$$

with  $\nu$  a constant molecular kinematic viscosity. How is the vorticity equation modified?

## EXERCISE 35.4: FRICTION FOR NON-DIVERGENT FLOWS

Consider a non-divergent flow with a Laplacian frictional acceleration

$$\mathbf{F} = \nu \nabla^2 \mathbf{v} \quad \text{with} \quad \nabla \cdot \mathbf{v} = 0, \quad (35.163)$$

with  $\nu$  a constant molecular kinematic viscosity. Write this expression in terms of the vorticity. Hint: check that  $\nabla \times \mathbf{F}$  equals to the friction appearing in the vorticity equation derived in exercise 35.3. Further hint: the derivation is given in Section 18.7.8.

## EXERCISE 35.5: GENERATION OF VORTICITY BY BAROCLINICITY

Consider an initially resting body of water with a flat bottom and rigid sides. Let the top surface be at  $z = 0$  and bottom at  $z = -H$ , and assume zero pressure applied at the top surface. Let the density have a horizontal structure given by

$$\rho(x) = \rho_0 (1 - \gamma x) \quad (35.164)$$

where  $\rho_0$  and  $\gamma$  are positive constants (with dimensions of density and inverse length, respectively). We furthermore assume that  $\gamma|x| \ll 1$  so that the density is strictly positive. Note that a study of Figure 35.6 helps with this exercise.

- (a) Compute the density gradient  $\nabla \rho$  and draw a schematic.
- (b) Compute the pressure gradient,  $\nabla p$ , assuming approximate hydrostatic balance so that  $\partial p / \partial z = -\rho g$ . Draw a schematic at  $x = 0$ .
- (c) Compute the baroclinicity/solenoidal vector  $\mathbf{B} = \rho^{-2} (\nabla \rho \times \nabla p)$ . Draw a schematic.
- (d) Describe the vorticity induced by the baroclinicity vector.

## EXERCISE 35.6: GENERATION OF CIRCULATION BY BAROCLINICITY IN AN IDEAL GAS

In this exercise we examine the baroclinicity vector for a simple ideal gas, which is described by the equation of state (20.159)

$$\rho = \frac{p M_{\text{mole}}}{T R_g} \equiv \frac{p}{T R^M}, \quad (35.165)$$

where  $R_g$  is the universal gas constant and  $R^M$  is the specific gas constant. We also assume the atmosphere is in approximate hydrostatic balance (Section 22.2), and we ignore rotation (relatively small lateral region of the atmosphere). For further hints to this exercise, see Section 4.1 of Holton (1992) or Section 2.4.3 of Markowski and Richardson (2010), where they discuss circulation generated by differences in land-sea temperatures, thus leading to a sea breeze.

- (a) Express the baroclinicity vector,  $\mathbf{B}$ , in terms of pressure and temperature gradients.
- (b) Express the baroclinicity vector in terms of pressure and potential temperature gradients.  
Hint: see Section 20.12.11 for potential temperature in an ideal gas.
- (c) Consider an ideal gas atmosphere straddling the ocean and flat land as in Figure 35.15. Let the daytime air be relatively cool over the ocean and relatively warm over the land. Furthermore, assume the sea level pressure is the same value over land and ocean. Ignoring rotation, draw isolines of constant temperature and constant pressure. Assume the horizontal temperature gradient is constant with height. Here are some hints.
  - Temperature decreases from land to ocean and decreases when ascending into the atmosphere.

- Pressure is assumed to be horizontally constant at sea level and it decreases upward. Use the ideal gas law to determine the sense for the horizontal pressure gradient as one ascends. Consult the discussion in Section 20.12.10 for geopotentials in an ideal gas atmosphere.
  - We are only concerned with a qualitative sense for the isolines in the lower atmosphere and over a horizontal region small enough that rotation can be ignored.
- (d) Describe the sense for the circulation induced by the baroclinicity. Does circulation correspond to your experience at a sunny beach day as the air warms over the land faster than over the adjacent ocean? What force causes air to rise and to fall?

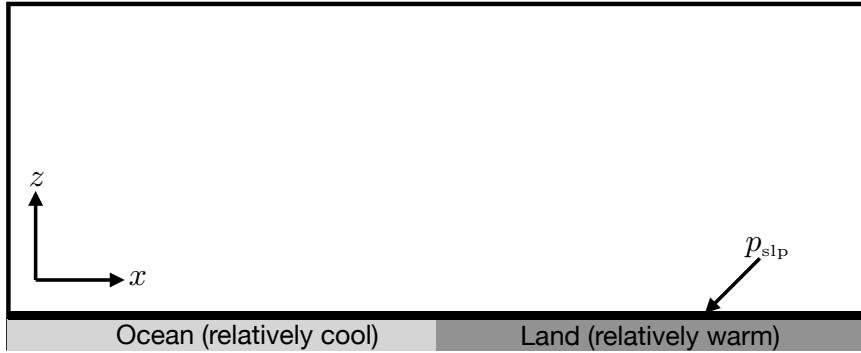


FIGURE 35.15: Setup for the sea breeze Exercise 35.6. We here depict a vertical-zonal crosssection of the atmosphere where the lower boundary straddles the ocean and land. The atmosphere over the ocean is assumed to be cooler than the atmosphere over the land, as typically occurs on a sunny afternoon with solar radiation warming land faster than the ocean.

#### EXERCISE 35.7: CIRCULATION WITH ISLANDS

Our discussion of Stokes' theorem has been thus far restricted to a simply connected domain, in which

$$\oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{r} = \int_{\mathcal{S}} \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (35.166)$$

For a simply connected domain, the closed contour can be shrunk to a point without leaving the domain.

A more general topology consists of a region with holes, whereby closed contours cannot in general be shrunk to a point without leaving the region. In an oceanographic context, the “holes” are islands or continents and the circulation is that for the depth integrated flow. Figure 35.16 shows a region of the ocean containing three arbitrarily shaped impenetrable islands, with the three islands surrounded by a contour. The contour cannot be shrunk to a point without crossing over the islands, thus making this region of the ocean multiply-connected. The presence of islands thus adds a level of complexity to the World Ocean that is absent in an AquaPlanet or the global atmosphere.

Derive the following expression for the circulation in multiply-connected regions

$$\oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{r} = \sum_{n=1}^N \left( \oint_{\partial\mathcal{S}_n} \mathbf{v} \cdot d\mathbf{r} \right) + \int_{\mathcal{S}} \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (35.167)$$

where  $N$  is the number of islands,  $\mathcal{S}_n$  is the contour surrounding each island, and  $\mathcal{S}$  is the region of water that excludes the islands. In words, this result says that the circulation around a region

equals to the circulation around the islands within the region, plus the normal component of the vorticity integrated over the area within the fluid region. Removing the islands allows the island contours to be shrunk to zero size, in which case we recover the simply connected result (35.166).

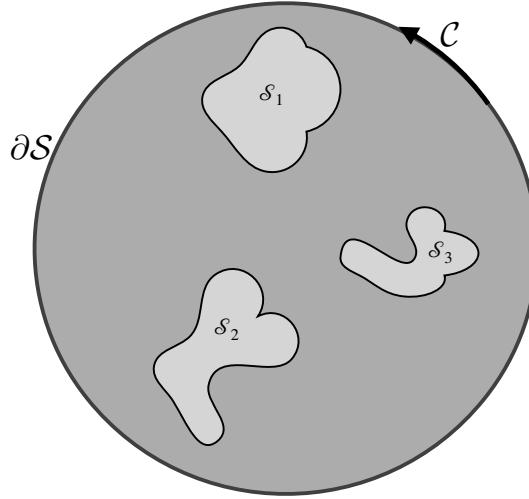


FIGURE 35.16: A region of the ocean consisting of three islands,  $\mathcal{S}_1$ ,  $\mathcal{S}_2$ , and  $\mathcal{S}_3$ , each with boundaries  $\partial\mathcal{S}_n$  and with the closed contour,  $\partial\mathcal{S}$ , drawn around the three islands. The contour  $\partial\mathcal{S}$  cannot be shrunk to a point without crossing over the islands, thus indicating that the domain is multiply connected. Exercise 35.7 is concerned with deriving an expression for the circulation of the depth-integrated flow as defined along the closed contour,  $\partial\mathcal{S}$ .

#### EXERCISE 35.8: EVOLUTION OF CIRCULATION AROUND ISLANDS

The momentum equation for a homogeneous layer of inviscid shallow water on a tangent plane is given by

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} + f \hat{\mathbf{z}} \times \mathbf{u} = -g \nabla \eta. \quad (35.168)$$

In this equation,  $\mathbf{u} = (u, v)$  is the horizontal velocity,  $f$  is the Coriolis parameter,  $g$  is the effective gravitational acceleration, and  $\eta$  is the deviation of the free surface from its horizontal resting position. All spatial derivatives are horizontal, so that

$$\mathbf{u} \cdot \nabla = u \partial_x + v \partial_y. \quad (35.169)$$

Use of a vector identity allows us to write

$$\frac{\partial \mathbf{u}}{\partial t} + (f + \zeta) \hat{\mathbf{z}} \times \mathbf{u} = -\nabla (\mathbf{u}^2/2 + g \eta), \quad (35.170)$$

where

$$\zeta = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u}) \quad (35.171)$$

is the vorticity of the shallow water fluid.

Consider an island, such as one shown in Figure 35.16. Each island is static and impenetrable to fluid flow, which means that

$$\mathbf{u} \cdot \hat{\mathbf{n}} = 0 \quad (35.172)$$

where  $\hat{\mathbf{n}}$  is the outward normal on an island boundary. This no-normal flow constraint means

that the velocity just next to an island is parallel to the island<sup>12</sup>

$$\mathbf{u} \times d\mathbf{r} = 0. \quad (35.173)$$

Equivalently, the island represents a solid material boundary across which no flow passes. Show that the inviscid shallow-water circulation around an island remains constant in time

$$\frac{d}{dt} \oint_I \mathbf{u} \cdot d\mathbf{r} = 0. \quad (35.174)$$

Recall that Kelvin's circulation theorem is formulated for a material contour in an inviscid fluid. This exercise shows that the circulation theorem also holds for a material contour enclosing a static solid boundary.

**EXERCISE 35.9: HELICITY FOR A PERFECT BAROTROPIC FLUID IN A GRAVITY FIELD AND NON-ROTATING REFERENCE FRAME**

Consider a closed material volume,  $\mathcal{R}$ , of a perfect homogenous barotropic fluid ( $\rho = \rho(p)$ ) in a gravity field ( $\mathbf{g} = -\nabla\Phi$ ) and in a non-rotating reference frame ( $\boldsymbol{\Omega} = 0$ ). Let this material volume have a boundary that is always tangent to the fluid vorticity,  $\boldsymbol{\omega}$ . Hence, the outward normal to the region boundary is orthogonal to the vorticity,

$$\hat{\mathbf{n}} \cdot \boldsymbol{\omega} = 0. \quad (35.175)$$

Such volumes define closed vortex tubes, such as a smoke ring or linked smoke rings. The *helicity* of the fluid within the vortex tube volume is defined as the integration of the helicity density,  $\mathbf{v} \cdot \boldsymbol{\omega}$ , over the closed volume

$$\mathbb{H} = \int_{\mathcal{R}(v)} \mathbf{v} \cdot \boldsymbol{\omega} dV, \quad (35.176)$$

where the volume  $\mathcal{R}(v)$  is material. In Cartesian coordinates, the helicity density takes the form

$$\mathbf{v} \cdot \boldsymbol{\omega} = u(\partial_y w - \partial_z v) + v(\partial_z u - \partial_x w) + w(\partial_x v - \partial_y u). \quad (35.177)$$

Although the helicity density vanishes for some common examples, such as for a fluid in solid-body rotation, it need not vanish in general.

- (a) Show that helicity is materially constant following the material volume

$$\frac{d\mathbb{H}}{dt} = 0. \quad (35.178)$$

- (b) Discuss why helicity is not defined for a shallow water fluid.

Use the following hints.

- Make use of  $\Phi_p$  that satisfies equation (35.19).
- The shallow water fluid model is based on the small aspect ratio limit, in which the fluid depth is much smaller than its lateral extent. In this limit, only the vertical component of vorticity is nontrivial.

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<sup>12</sup>This boundary condition is valid only for inviscid fluids such as that considered here. For a real fluid with nonzero viscosity, all components of the velocity vector vanish at solid boundaries due to the no-slip condition.

## EXERCISE 35.10: DISCRETE CALCULATION OF BOTTOM PRESSURE TORQUE

In many diagnostic studies with numerical models it is of interest to compute pressure torques affecting vorticity. One particularly common diagnostic concerns the bottom pressure torque arising in equation (35.145). Derive a discrete expression for the area averaged bottom pressure torque

$$\overline{\text{BPT}} = A^{-1} \int_{\mathcal{S}} \hat{z} \cdot \nabla \times (\eta_b \nabla p_b) d\mathcal{S} = A^{-1} \oint_{\partial\mathcal{S}} \eta_b \nabla p_b \cdot \hat{t} d\ell, = -A^{-1} \oint_{\partial\mathcal{S}} p_b \nabla \eta_b \cdot \hat{t} d\ell, \quad (35.179)$$

over the shaded region depicted in Figure 35.17, with  $A = \int_{\mathcal{S}} d\mathcal{S}$  the horizontal area of this region. Hint: this exercise shares much with the area averaged vorticity in Exercise 32.6, although the final result is distinct. Note: given that the bottom pressure torque is generally the small difference between large numbers, it is very useful to perform the diagnostic calculation online so that full computational precision can be maintained.

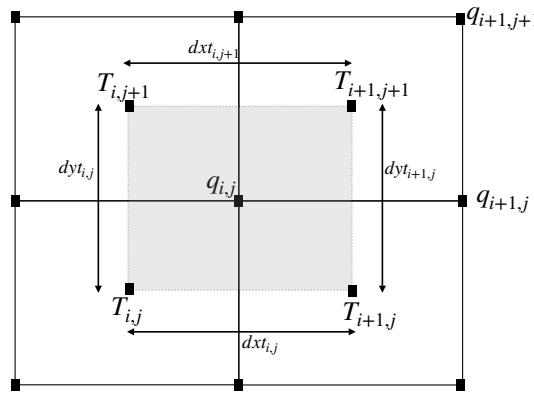


FIGURE 35.17: Discrete grid layout for variables needed to compute the bottom pressure torque as averaged over the shaded vorticity region. The bottom topography and bottom pressure are both known at the tracer points.

## EXERCISE 35.11: DYNAMICAL PORTION OF THE TOPOGRAPHIC FORM STRESS

We discussed bottom topographic form stress in Chapter 19, with its curl leading to the bottom pressure torque in equation (35.145). As noted in Section 19.1.3, the dominant portion of the bottom topographic form stress acting on the ocean has little to do with fluid motion. Rather, it merely holds the ocean fluid within the basin, much as water is held within a drinking container through pressure imparted by the container sides.

- (a) To help isolate the dynamically relevant portion of the bottom bottom pressure, show that we can write the horizontal gradient of the bottom pressure for a hydrostatic fluid according to

$$\nabla_z p_b = g [\rho(\eta) \nabla_z \eta - \rho(\eta_b) \nabla_z \eta_b] + g \int_{\eta_b}^{\eta} \nabla_z \rho dz. \quad (35.180)$$

where we ignore the applied surface pressure,  $p_a$ , for simplicity.

- (b) Hence, show that the bottom pressure torque takes the form

$$\hat{z} \cdot \nabla_z \eta_b \times \nabla_z p_b = g \hat{z} \cdot \nabla_z \eta_b \times \left[ \rho(\eta) \nabla_z \eta + \int_{\eta_b}^{\eta} \nabla_z \rho dz \right] \equiv \hat{z} \cdot \nabla \eta_b \times \nabla p_b^*, \quad (35.181)$$

where

$$\nabla_z p_b^* = g \rho(\eta) \nabla_z \eta + g \int_{\eta_b}^{\eta} \nabla_z \rho dz. \quad (35.182)$$

Note how  $\nabla_z p_b^*$  has no contribution from the potentially very large term,  $-g \rho(\eta_b) \nabla_z \eta_b$ , arising from gradients in the bottom topography.

- (c) *Molemaker et al. (2015)* and *Gula et al. (2015)* assume knowledge of the bottom pressure torque along contours of constant topography. Given that knowledge they then make use of the following diagnostic expression for  $p_b^*$

$$p_b^*(s) - p_b^*(s_0) = - \int_{s_0}^s \frac{\hat{z} \cdot (\nabla \eta_b \times \nabla p_b)}{\hat{n} \cdot \nabla \eta_b} ds, \quad (35.183)$$

with  $p_b^*(s_0)$  the value at the arbitrary starting point for the contour. Derive equation (35.183), with the following information of possible use.

- As depicted in Figure 35.14,  $s$  is the arc length along the chosen contour of constant  $\eta_b$ , with  $s$  increasing in the tangent direction,  $\hat{t}$ . Likewise,  $\hat{n}$  is a unit vector pointing to the left of the contour so that  $\hat{n} \cdot \hat{t} = 0$  and  $\hat{t} \times \hat{n} = \hat{z}$ .
- Along any contour of constant  $\eta_b(x, y)$  we have

$$0 = d\eta_b = \nabla \eta_b \cdot dx = \nabla \eta_b \cdot \frac{dx}{ds} ds = \nabla \eta_b \cdot \hat{t} ds. \quad (35.184)$$

- The main mathematics of this exercise are contained in Exercise 5.1.

Equation (35.183) provides a means to compute the anomalous  $p_b^*$  [anomalous relative to  $p_b^*(s_0)$ ] along a constant topography contour. Mapping  $p_b^*(s) - p_b^*(s_0)$  for a suite of contours then provides the means to determine the dynamically relevant portion of the bottom pressure and then, when multiplying by the bottom slope, compute the dynamically relevant portion of the form stress.



# Chapter 36

## Potential vorticity mechanics

The chapter details the foundational properties of potential vorticity (PV) and its evolution. The PV we encounter is sometimes referred to as the *Ertel* PV, which is the most fundamental form of PV arising in geophysical fluids (*Ertel*, 1942). The barotropic fluid forms a pedagogically useful starting point for the discussion. However, realistic geophysical flows are baroclinic, which are fluids where “PV thinking” is most powerful. The general method exploited for the construction of PV is to choose a scalar field to strategically orient the absolute vorticity. If the scalar is a material invariant, and it annihilates the baroclinicity vector, then PV is a material invariant. As so constructed, PV is a function of the chosen scalar.

For a barotropic fluid, the choice of scalar field is rather arbitrary, with preference given to one that is materially invariant. However, for a baroclinic fluid we are much more restricted since the scalar must orient vorticity in a direction to annihilate the torque from baroclinicity and, ideally, be itself materially invariant. We can only annihilate baroclinicity under certain restricted cases. Nonetheless, even when PV is not materially invariant, it remains a very important fluid property that partially constrains the fluid motion and provides insights into the interpretation of that motion.

### CHAPTER GUIDE

This chapter requires a firm understanding of vorticity from Chapter 35 as well as good skills with vector calculus identities for Cartesian coordinates as detailed in Chapter 2. The concepts and methods developed in this chapter are fundamental to the notions of potential vorticity, much of which is encountered in the remainder of this part of the book as well as when studying balanced models in Part VII.

36.1	Material invariance of PV in perfect fluids . . . . .	912
36.1.1	Perfect barotropic fluid . . . . .	912
36.1.2	Region between two scalar isosurfaces . . . . .	912
36.1.3	Material invariance . . . . .	913
36.1.4	Perfect baroclinic fluid . . . . .	914
36.1.5	Some general remarks . . . . .	914
36.2	PV and the seawater equation of state . . . . .	916
36.2.1	Baroclinicity vector . . . . .	916
36.2.2	PV based on potential density . . . . .	917
36.2.3	An example EOS admitting a materially invariant PV . . . . .	918
36.2.4	Further reading . . . . .	918

36.3	PV evolution with non-conservative processes	918
36.4	Eulerian flux-form PV budget	920
36.4.1	Deriving the Eulerian flux-form PV budget	920
36.4.2	PV-substance and the PV flux	920
36.5	PV budget for a hydrostatic Boussinesq fluid	921
36.5.1	Potential vorticity	921
36.5.2	Potential vorticity flux vector	922
36.5.3	Kinematic derivation of the PV-substance flux	923
36.5.4	Potential vorticity flux vector	924
36.6	Exercises	926

## 36.1 Material invariance of PV in perfect fluids

In this section we derive the material invariance of potential vorticity (PV) for a perfect fluid (i.e., fluid without mixing). We make use of Kelvin's circulation theorem for an infinitesimal loop, in which case the primary object of interest is a particular component of the absolute vorticity. The discussion starts with a barotropic fluid, in which baroclinicity vanishes (Sections 35.3 and 35.5), and then we generalize to a baroclinic fluid.

### 36.1.1 Perfect barotropic fluid

Consider a perfect barotropic fluid. As for the shallow water discussion in Section 34.4.3, we apply Kelvin's circulation theorem (Section 35.3.2) to an infinitesimal material circuit within the fluid

$$\frac{D}{Dt}(\boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} \delta\mathcal{S}) = 0, \quad (36.1)$$

with  $\delta\mathcal{S}$  the area of the circuit. The conservation of PV is built from specializing this result. For that purpose, introduce a materially invariant scalar field

$$\frac{DC}{Dt} = 0. \quad (36.2)$$

### 36.1.2 Region between two scalar isosurfaces

We make use of isosurfaces of  $C$  to orient the material circuit and hence to orient the vorticity. In particular, referring to Figure 36.1, let the circuit bound a small cylinder whose two ends sit on two isosurfaces,  $C - \delta C/2$  and  $C + \delta C/2$ . The tube volume is given by

$$\delta V = \delta\mathcal{S} \delta h, \quad (36.3)$$

where  $\delta h$  is the distance between the isosurfaces. The unit normal direction orienting the area  $\delta\mathcal{S}$  is given by

$$\hat{\mathbf{n}} = \frac{\nabla C}{|\nabla C|}. \quad (36.4)$$

The separation between the two isosurfaces is related to the increment  $\delta C$  through

$$\delta C = \nabla C \cdot \delta \mathbf{x} = |\nabla C| \hat{\mathbf{n}} \cdot \delta \mathbf{x} = |\nabla C| \delta h. \quad (36.5)$$

This result takes on the equivalent expression

$$\delta C = |\nabla C| \delta h = (\hat{\mathbf{n}} \cdot \nabla C) \delta h = \frac{\delta C}{\delta n} \delta h, \quad (36.6)$$

so that the distance (or thickness) between the two isosurfaces is

$$\delta h = \frac{\delta C}{|\nabla C|}. \quad (36.7)$$

This equation has a straightforward geometric interpretation indicated in Figure 36.1. Namely, the geometric separation between the two isosurfaces is reduced in regions of strong scalar gradients and increased in regions of weak gradients.

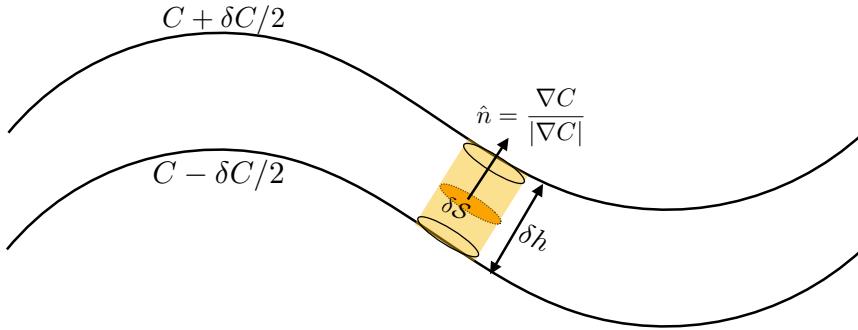


FIGURE 36.1: Illustrating the geometry of a cylindrical region of fluid between two iso-surfaces of a scalar field  $C$ . The volume of the region is  $\delta V = \delta S \delta h$ , with  $\delta h$  the thickness and  $\delta S$  the area. By convention, the normal vector,  $\hat{n}$ , points towards larger values of  $C$ . Notably, if  $C$  is a material invariant so that  $DC/Dt = 0$ , then so is its infinitesimal increment,  $D(\delta C)/Dt = 0$ . As per equation (36.7), the geometric thickness between the isosurfaces is related to the scalar field increment by  $\delta h = \delta C/|\nabla C|$ , so that the larger the magnitude of the gradient in the scalar field, the smaller the layer thickness. For a baroclinic fluid material invariance of PV holds only if we can find a scalar field such that  $\hat{n} \cdot \mathbf{B} = 0$ , with  $\mathbf{B} = (\nabla \rho \times \nabla p)/\rho^2$  the baroclinicity.

### 36.1.3 Material invariance

We now have the necessary pieces in place to write

$$\omega_a \cdot \hat{n} \delta S = \frac{\omega_a \cdot \nabla C}{|\nabla C|} \delta S \quad (36.8a)$$

$$= \frac{\omega_a \cdot \nabla C}{|\nabla C|} \frac{\delta V}{\delta h} \quad (36.8b)$$

$$= (\omega_a \cdot \nabla C) \frac{\delta V}{\delta C} \quad (36.8c)$$

$$= \frac{\omega_a \cdot \nabla C}{\rho} \frac{\rho \delta V}{\delta C}. \quad (36.8d)$$

Mass is materially invariant so that

$$\frac{D(\rho \delta V)}{Dt} = 0. \quad (36.9)$$

Likewise, by assumption  $C$  is materially invariant so that the increment between two  $C$  isosurfaces is materially invariant

$$\frac{D(\delta C)}{Dt} = 0. \quad (36.10)$$

Bringing these elements into Kelvin's circulation theorem (36.1) leads us to conclude that the potential vorticity,  $Q$ , is also materially invariant

$$Q = \frac{\omega_a \cdot \nabla C}{\rho} = \frac{\nabla \cdot (\omega_a C)}{\rho} \implies \frac{DQ}{Dt} = 0. \quad (36.11)$$

This expression for the PV is the most general form and it is often referred to as the *Ertel PV* ([Ertel, 1942](#)). The first expression shows the numerator as the projection of the absolute vorticity into the direction normal to tracer isosurfaces. Conversely, it is a measure of the  $C$  stratification in the direction of the absolute vorticity vector. The second expression follows since the absolute vorticity has zero divergence so that the numerator is a total divergence. We make use of this second form when discussing PV budgets in Section 36.4 and layer integrated PV Section 37.4.

### 36.1.4 Perfect baroclinic fluid

Consider the case of a perfect baroclinic fluid, in which Kelvin's circulation theorem for an infinitesimal circuit takes the form

$$\frac{D}{Dt}(\boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} \delta\mathcal{S}) = \mathbf{B} \cdot \hat{\mathbf{n}} \delta\mathcal{S}, \quad (36.12)$$

where the source on the right hand side arises from the baroclinicity vector discussed in Sections 35.3 and 35.5.

$$\mathbf{B} = \frac{\nabla\rho \times \nabla p}{\rho^2}. \quad (36.13)$$

Now assume there exists a materially invariant scalar,  $\theta$ , that annihilates the baroclinicity vector as in Figure 36.2, so that

$$\mathbf{B} \cdot \hat{\mathbf{n}} = \frac{\mathbf{B} \cdot \nabla\theta}{|\nabla\theta|} = 0. \quad (36.14)$$

In that case, the barotropic derivation detailed earlier in this section follows for the baroclinic case so that PV remains materially invariant

$$\frac{DQ}{Dt} = 0 \quad \text{where} \quad Q = \frac{\boldsymbol{\omega}_a \cdot \nabla\theta}{\rho}. \quad (36.15)$$

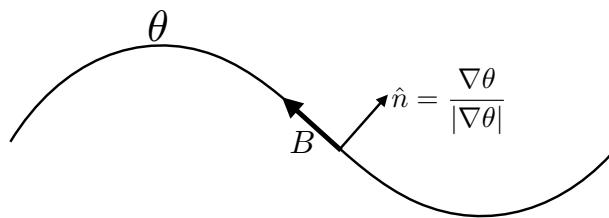


FIGURE 36.2: Material invariance of PV is ensured for perfect fluids that allow for a materially invariant scalar to annihilate baroclinicity, meaning that  $\hat{\mathbf{n}} \cdot \mathbf{B} = 0$  where  $\hat{\mathbf{n}} = \nabla\theta/|\nabla\theta|$ . In this figure we depict the potential temperature field with a baroclinicity vector aligned with isolines of  $\theta$ .

Existence of a materially invariant PV for perfect baroclinic fluids depends on the existence of a materially invariant scalar that annihilates the baroclinicity vector. The most common choice for this scalar in geophysical fluid applications is the buoyancy, which is typically measured by entropy or potential temperature in the atmosphere and potential density in the ocean. We have more to say on the chosen scalar field in the remainder of this chapter as well as in Section 37.3.

### 36.1.5 Some general remarks

*Perfect fluid PV material invariance  $\leftrightarrow$  Kelvin's circulation theorem*

Kelvin's circulation theorem from Section 35.3.2 is at the heart of the derivations presented in this section, with the theorem applied to a strategically chosen infinitesimal loop. Because the

loop is tiny, we convert the line integral expression of Kelvin's theorem into a statement about the material evolution of absolute vorticity projected onto the normal direction of the loop, and multiplied by the loop area. We further specialize the theorem to a cylindrical region between two isosurfaces of a materially invariant scalar field. For the perfect barotropic fluid, we merely require that both mass and scalar to be materially invariant to realize a potential vorticity that is also materially invariant. Material invariance of PV for a baroclinic fluid requires a scalar field that is both materially invariant *and* that annihilates the baroclinicity vector. We have more to say in regards to the availability of such scalar fields when considering entropic PV in the remainder of this chapter, whereby potential temperature is the chosen scalar field.

### *There are numerous forms for PV*

The expression (36.11) is, on first glance, quite distinct from the shallow water potential vorticity,  $Q = (\zeta + f)/h$ , studied in Chapter 34 (see equation (34.37)). However, as shown in Section 44.2, they are closely related for the special case of entropic PV in an incompressible fluid when formulated using isopycnal/isentropic coordinates. Even so, there are a variety of other forms for PV, with the forms (and physical dimensions) depending on the assumptions made in regards to the fluid flow and its thermodynamic properties. We encounter some further forms of PV in the remainder of this chapter, as well as in the oceanic PV discussions of Chapter 44 and in our study of balanced models in Part VII. The review paper by Müller (1995) offers a lucid presentation of PV and its many forms encountered in physical oceanography.

### *Motivating the adjective “potential”*

In Section 34.4.2 we motivated the advective “potential” for the shallow water potential vorticity. We do so here for Ertel's potential vorticity. For that purpose, write PV in the form

$$Q = \frac{\omega_a \cdot \hat{n}}{\rho} |\nabla\theta| \quad \text{with} \quad \hat{n} = \frac{\nabla\theta}{|\nabla\theta|}. \quad (36.16)$$

As noted in Section 2.1 of Müller (1995), in cases where  $\rho$  is roughly a constant, and when  $Q$  is materially invariant, the component of the absolute vorticity in the direction parallel to  $\nabla\theta$  increases when the fluid parcel moves into a region where  $|\nabla\theta|$  decreases. There is hence a “release” of absolute vorticity aligned with  $\nabla\theta$  in regions where  $\theta$  isosurfaces are spread, and a withdrawal of absolute vorticity where  $\theta$  isosurfaces are tightly packed. We thus conceive of PV as the “potential” for releasing absolute vorticity oriented in the direction parallel to  $\nabla\theta$ .

### *PV as a dynamical tracer*

We refer to PV as a *dynamical tracer* since it depends directly on the velocity field through the vorticity. It also depends on the thermodynamic tracer,  $\theta$ , so that PV brings together dynamical and thermodynamical information into a single package. In contrast, material tracers such as salinity, and thermodynamic tracers such as  $\theta$ , are properties of the fluid whose distribution depends on the velocity field but whose local measurement does not require knowledge of velocity.

### *PV is the grand unifier for geophysical fluid mechanics*

Entropic PV provides a connection between vorticity (mechanics) and stratification (thermodynamics). By connecting these two basic facets of geophysical fluid flows, the study of PV and its conservation properties provides a powerful and unique lens to help rationalize the huge variety of

geophysical flow regimes, and to predict their response to changes in forcing. It is for this reason that PV is sometimes considered the grand unifying concept in geophysical fluid mechanics.

### PV as a diagnostic tracer

Suppose we have an initial flow field in which  $Q = 0$  so that the absolute vorticity lives within constant  $\theta$  surfaces. In an inviscid and adiabatic fluid, material conservation of  $Q$  means that  $\omega_a$  remains within constant  $\theta$  surfaces for all time. Hence, if we know the evolution of  $\theta$ , then we know the evolution of vortex lines defined by  $\omega_a$ , which in turn allows for the inference of a number of further flow properties. This particular example offers a hint at the multiple applications of “PV thinking” to understand and predict fluid motion, with [Hoskins \(1991\)](#) providing an elegant survey of such thinking.

### Potential vorticity versus momentum

Momentum is affected by pressure, and pressure fluctuations propagate at the speed of sound (Section 17.5) for compressible flows and oceanic Boussinesq flows, whereas they move infinitely fast for incompressible fluids. In contrast, potential vorticity, when we can remove the full effects of the baroclinicity vector, do not directly feel the impacts from pressure fluctuations. Hence, potential vorticity, much like vorticity in a barotropic fluid, evolves much slower and more locally than momentum. This difference offers a very important reason that potential vorticity offers added insights into fluid flows beyond that afforded by momentum.

## 36.2 PV and the seawater equation of state

As seen in Section 36.1, material invariance of PV for a perfect fluid requires a materially invariant scalar field to annihilate the baroclinicity vector. In the ocean there is generally no such scalar when there is also a realistic seawater equation of state. Hence, the ocean cannot be considered a perfect fluid even in the absence of friction and diabatic processes. Nonetheless, as discussed in this section, there are important approximate cases that allow for material PV invariance.

### 36.2.1 Baroclinicity vector

Recall the baroclinicity vector given by (Sections 35.3 and 35.5)

$$\mathbf{B} = \frac{\nabla\rho \times \nabla p}{\rho^2}. \quad (36.17)$$

If we take the *in situ* density as the scalar field to define PV, then  $\mathbf{B} \cdot \nabla\rho = 0$ . However, *in situ* density is not a conserved scalar in the ocean due to pressure effects. Namely, the material time derivative of  $\rho = \rho(S, \theta, p)$  is

$$\frac{D\rho}{Dt} = \frac{\partial\rho}{\partial S} \frac{DS}{Dt} + \frac{\partial\rho}{\partial\theta} \frac{D\theta}{Dt} + \frac{\partial\rho}{\partial p} \frac{Dp}{Dt}. \quad (36.18)$$

Even when salinity and potential temperature are materially constant,  $DS/Dt = 0$  and  $D\theta/Dt = 0$ , the *in situ* density has a nonzero material time evolution due to pressure changes,  $Dp/Dt \neq 0$ . Material changes in the pressure of a fluid element arise even in the absence of irreversible mixing. In general, such *mechanical changes* arise due to the gradients in the pressure field that the fluid element moves through. Given that pressure effects *in situ* density, with such effects occurring

even in a perfect fluid, we conclude that *in situ* density is not an appropriate scalar for use in developing a materially invariant PV.

### 36.2.2 PV based on potential density

Potential density is commonly used in oceanography (see Section 24.3.4), with potential density the *in situ* density referenced to a chosen pressure.<sup>1</sup> We write potential density as

$$\sigma(S, \theta) = \rho(S, \theta, p = p_R). \quad (36.19)$$

Potential density provides a global measure of buoyancy, with accuracy of the measure compromised in the presence of a nonlinear equation of state.

The material time derivative of potential density is

$$\frac{D\sigma}{Dt} = \frac{\partial\sigma}{\partial S} \frac{DS}{Dt} + \frac{\partial\sigma}{\partial\theta} \frac{D\theta}{Dt}, \quad (36.20)$$

which vanishes in the absence of irreversible material changes to salinity and potential temperature. When using potential density as the scalar field for PV, the baroclinicity vector projects onto the diapycnal direction according to

$$\rho^2 \mathbf{B} \cdot \nabla\sigma = (\nabla\rho \times \nabla p) \cdot \nabla\sigma \quad (36.21a)$$

$$= (\nabla\sigma \times \nabla\rho) \cdot \nabla p \quad (36.21b)$$

$$= [(\sigma_S \nabla S + \sigma_\theta \nabla\theta) \times (\rho_S \nabla S + \rho_\theta \nabla\theta + \rho_p \nabla p)] \cdot \nabla p \quad (36.21c)$$

$$= [(\sigma_S \nabla S + \sigma_\theta \nabla\theta) \times (\rho_S \nabla S + \rho_\theta \nabla\theta)] \cdot \nabla p \quad (36.21d)$$

$$= [\sigma_S \nabla S \times \rho_\theta \nabla\theta + \sigma_\theta \nabla\theta \times \rho_S \nabla S] \cdot \nabla p \quad (36.21e)$$

$$= (\sigma_S \rho_\theta - \sigma_\theta \rho_S) (\nabla S \times \nabla\theta) \cdot \nabla p, \quad (36.21f)$$

where we used the shorthand notation for partial derivatives

$$\rho_S = \frac{\partial\rho}{\partial S} \quad \sigma_S = \frac{\partial\sigma}{\partial S} \quad (36.22a)$$

$$\rho_\theta = \frac{\partial\rho}{\partial\theta} \quad \sigma_\theta = \frac{\partial\sigma}{\partial\theta}. \quad (36.22b)$$

Note that the triple product,  $(\nabla S \times \nabla\theta) \cdot \nabla p$ , also appears in the discussion of neutral helicity in Section 24.6 (see equation (24.59)). Equation (36.21f) allows us to identify cases where the baroclinicity vector is annihilated,  $\mathbf{B} \cdot \nabla\sigma = 0$ , thus yielding a materially invariant PV in the absence of irreversible processes.

- UNIFORM SALINITY OR UNIFORM POTENTIAL TEMPERATURE: If salinity or potential temperature are spatially uniform, then  $\mathbf{B} \cdot \nabla\sigma = 0$ .
- ADDITIVE PRESSURE DEPENDENCE TO THE *in situ* DENSITY: There is an exact PV conservation principle if the thermodynamic pre-factor  $\sigma_S \rho_\theta - \sigma_\theta \rho_S$  vanishes. However, the ocean has a pressure dependent equation of state and this pressure dependence generally means that  $\mathbf{B} \cdot \nabla\sigma \neq 0$ . Nonetheless, the baroclinicity vector is annihilated if the *in situ* density has a pressure dependence that is additive, so that we can write

$$\rho(S, \theta, p) = \sigma(S, \theta) + F(p) - F(p_R) \implies \sigma_S \rho_\theta - \sigma_\theta \rho_S = 0, \quad (36.23)$$

<sup>1</sup>Oceanographers often choose the reference pressure as the standard atmospheric surface pressure. However, that is not required for the following formalism to hold; any reference pressure is suitable.

which then leads to a materially invariant PV. Notably, we did not assume the equation of state to be linear; only that it has the special functional form in equation (36.23). For some cases, we may assume  $F$  to be a constant, in which case there is no pressure dependence; i.e., the *in situ* density is the same as potential density.

### 36.2.3 An example EOS admitting a materially invariant PV

An explicit realization of the equation of state (36.23) can be found by taking a Taylor series expansion of the *in situ* density around the reference pressure, and evaluating the derivatives in the expansion in terms of a chosen reference pressure, reference salinity, and reference potential temperature

$$\rho(S, \theta, p) \approx \sigma(S, \theta) + (p - p_R) \underbrace{\left[ \frac{\partial \rho}{\partial p} \right]_{S=S_R, \theta=\theta_R, p=p_R}}_{F(p)-F(p_R)} + H.O.T. \quad (36.24)$$

where *H.O.T.* symbolizes higher order terms. This approach ignores the salinity and potential temperature dependence of terms in the Taylor series expansion. Ignoring this dependence is a rather good approximation for many purposes since the ocean sound speed is not far from a constant

$$c_s^{-2} = \frac{\partial \rho}{\partial p} \approx \text{constant}. \quad (36.25)$$

In this case, the equation of state takes the form

$$\rho(S, \theta, p) \approx \sigma(S, \theta) + \frac{p - p_R}{c_s^2}, \quad (36.26)$$

where again  $\sigma(S, \theta) = \rho(S, \theta, p_R)$  is the potential density referenced to  $p = p_R$ .

### 36.2.4 Further reading

Straub (1999) presents a discussion of ocean potential vorticity with a focus on the source of potential vorticity arising from a nonzero thermobaricity parameter,  $\mathcal{T} = \partial_p(\alpha/\beta)$  (see Section 49.3.4). The presentation given here follows that given in Section 4.5.4 of Vallis (2017).

## 36.3 PV evolution with non-conservative processes

Thus far we have considered perfect fluids, with the use of Kelvin's circulation theorem a suitable framework to derive the material invariance of PV. In this section we move beyond the perfect fluid by considering a real fluid that contains non-conservative processes. PV is no longer materially invariant when exposed to non-conservative processes. However, as detailed in Chapter 37, there remain some rather remarkable global conservation properties for PV budgets within isentropic layers.

To develop the PV budget in the presence of non-conservative processes, we pursue an algebraic approach that starts from the vorticity equation (35.32)

$$\rho \frac{D(\omega_a/\rho)}{Dt} = (\omega_a \cdot \nabla) \mathbf{v} + \mathbf{B} + \nabla \times \mathbf{F}, \quad (36.27)$$

where  $\mathbf{F}$  is the acceleration from non-conservative forces and  $\mathbf{B}$  the baroclinicity vector. Furthermore, we introduce a non-conservative scalar field

$$\frac{DC}{Dt} = \dot{C}, \quad (36.28)$$

with  $\dot{C}$  arising from diffusion, sources, or other irreversible processes.

As part of the manipulations we make use of the identity

$$(\boldsymbol{\omega}_a \cdot \nabla) \frac{DC}{Dt} = \boldsymbol{\omega}_a \cdot \frac{D(\nabla C)}{Dt} + [(\boldsymbol{\omega}_a \cdot \nabla) \mathbf{v}] \cdot \nabla C, \quad (36.29)$$

which is readily proven by expanding terms and assuming Cartesian coordinates. Rearrangement, and use of the scalar equation (36.28), leads to

$$\boldsymbol{\omega}_a \cdot \frac{D(\nabla C)}{Dt} = (\boldsymbol{\omega}_a \cdot \nabla) \dot{C} - [(\boldsymbol{\omega}_a \cdot \nabla) \mathbf{v}] \cdot \nabla C. \quad (36.30)$$

Now project the vorticity equation (36.27) onto the direction normal to the  $C$  isosurfaces

$$\rho \nabla C \cdot \frac{D(\boldsymbol{\omega}_a / \rho)}{Dt} = \nabla C \cdot [(\boldsymbol{\omega}_a \cdot \nabla) \mathbf{v}] + \nabla C \cdot (\mathbf{B} + \nabla \times \mathbf{F}). \quad (36.31)$$

The sum of equations (36.30) and (36.31) leads to

$$\rho \frac{D(\nabla C \cdot \boldsymbol{\omega}_a / \rho)}{Dt} = (\boldsymbol{\omega}_a \cdot \nabla) \dot{C} + \nabla C \cdot (\mathbf{B} + \nabla \times \mathbf{F}). \quad (36.32)$$

This equation is general so that it applies to any scalar field.

To simplify the source terms on the right hand side of equation (36.32), follow the discussion from Section 36.1.4 by assuming there is a special scalar field that annihilates the baroclinicity vector.<sup>2</sup> We generally denote this scalar field as  $\theta$ , which we use in this chapter as a general designation for potential temperature, specific entropy, buoyancy, or potential density. We thus have

$$\nabla \theta \cdot \mathbf{B} = 0, \quad (36.33)$$

which in turn leads to the potential vorticity equation in the presence of irreversible processes

$$\rho \frac{DQ}{Dt} = (\boldsymbol{\omega}_a \cdot \nabla) \dot{\theta} + \nabla \theta \cdot (\nabla \times \mathbf{F}), \quad (36.34)$$

where the entropic-PV is again given by

$$Q = \frac{\boldsymbol{\omega}_a \cdot \nabla \theta}{\rho}. \quad (36.35)$$

As defined, the material evolution of PV is affected by diabatic processes (heating and cooling) as well as friction. Absent these irreversible processes leaves us with the same PV conservation statement (36.15) derived for the perfect fluid using Kelvin's circulation theorem. In their presence, the PV of a fluid element can be either generated or destroyed depending on details of the irreversible process. Such source/sink regions of potential vorticity are often localized to regions of mixing as well as to boundaries where strong mechanical and/or buoyancy processes are active. The study of how PV is materially modified by irreversible processes forms an important area of

<sup>2</sup>In Section 37.3 we study what happens when no such scalar exists.

research in PV dynamics.

## 36.4 Eulerian flux-form PV budget

The material invariance of PV is an example of a material or Lagrangian conservation property of perfect fluids, with the material conservation statement  $\rho DQ/Dt = 0$  having its Eulerian flux-form expression

$$\frac{\partial(\rho Q)}{\partial t} + \nabla \cdot (\rho \mathbf{v} Q) = 0 \quad \text{perfect fluid.} \quad (36.36)$$

Following the formalism established for material tracers in Section 15.3, the flux-form local conservation law (36.36) leads then to conservation properties over finite regions, which we refer to as *global conservation* laws. In this section we examine the Eulerian flux-form budget in the presence of non-conservative processes. As we will see, the Eulerian evolution of PV will continue to be determined by the convergence of a flux, thus allowing for natural extensions to global conservation laws.

### 36.4.1 Deriving the Eulerian flux-form PV budget

To transform the material evolution equation (36.34) into a flux-form Eulerian equation we make use of the following identities

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \quad \text{relating material and Eulerian time changes} \quad (36.37a)$$

$$\frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{v} \quad \text{mass conservation} \quad (36.37b)$$

$$(\boldsymbol{\omega}_a \cdot \nabla) \dot{\theta} = \nabla \cdot (\boldsymbol{\omega}_a \dot{\theta}) \quad \nabla \cdot \boldsymbol{\omega}_a = 0 \quad (36.37c)$$

$$\nabla \theta \cdot (\nabla \times \mathbf{F}) = \nabla \cdot (\mathbf{F} \times \nabla \theta) \quad \text{divergence of curl vanishes.} \quad (36.37d)$$

The identity (36.37d) follows from

$$\nabla \theta \cdot (\nabla \times \mathbf{F}) = \nabla \cdot (\theta \nabla \times \mathbf{F}) = \nabla \cdot [\nabla \times (\theta \mathbf{F}) - \nabla \theta \times \mathbf{F}] = \nabla \cdot (\mathbf{F} \times \nabla \theta), \quad (36.38)$$

where a vanishing divergence of a curl is needed to reach the first and third equalities. These identities then lead to the material evolution equation

$$\rho \frac{DQ}{Dt} = \nabla \cdot [\boldsymbol{\omega}_a \dot{\theta} + \mathbf{F} \times \nabla \theta]. \quad (36.39)$$

Now converting the material time derivative into its Eulerian expression, and making use of mass conservation, renders the flux-form Eulerian PV budget equation

$$\frac{\partial(\rho Q)}{\partial t} + \nabla \cdot [\rho Q \mathbf{v} - \boldsymbol{\omega}_a \dot{\theta} - \mathbf{F} \times \nabla \theta] = 0. \quad (36.40)$$

### 36.4.2 PV-substance and the PV flux

The budget equation (36.40) says that the density-weighted potential vorticity

$$\rho Q = \boldsymbol{\omega}_a \cdot \nabla \theta \quad (36.41)$$

has a local time tendency determined by the convergence of the PV flux vector

$$\frac{\partial(\rho Q)}{\partial t} = -\nabla \cdot \mathbf{J}_Q \quad \text{with} \quad \mathbf{J}_Q = \rho Q \mathbf{v} - \boldsymbol{\omega}_a \dot{\theta} - \mathbf{F} \times \nabla \theta. \quad (36.42)$$

The budget (36.40) follows a form similar to material tracers detailed in Chapter 15, though with some specific terms in the flux vector,  $\mathbf{J}_Q$ . The correspondence suggests that one consider equation (36.40) as the local budget for *PV-substance*, with  $Q$  the concentration of PV-substance and  $\mathbf{J}_Q$  its flux. This interpretation is pursued further in Chapter 37 when exposing the rather novel properties of budgets for PV-substance when integrated over regions bounded by isentropes.

The first term in the PV-substance flux vector (36.42) arises from the advection of PV-substance; the second contribution arises from diabatic processes; and the third from the curl of the friction vector. Note that there is a nonzero friction contribution only when the frictional acceleration has a component that is not parallel to  $\nabla \theta$ . In this manner we can think of the friction vector as contributing to a “torque” that rotates the  $\theta$  isosurfaces as it contributes to the evolution of PV-substance (see Figure 36.3).

The time tendency for PV-substance,  $\partial_t(\rho Q)$ , is unchanged by adding the curl of a vector to  $\mathbf{J}_Q$ . This ambiguity manifests a *gauge freedom* afforded the PV-substance flux vector. We offer a general discussion of gauge freedom in Section 16.5.1 and provide more specifics for PV in Chapter 37.

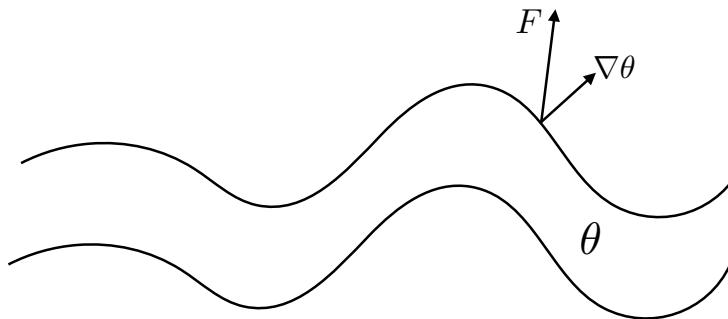


FIGURE 36.3: The contribution from friction to the PV flux is given by  $\mathbf{J}_{\text{friction}} = \nabla \theta \times \mathbf{F}$ , which is nonzero only when the frictional acceleration is not fully aligned with  $\nabla \theta$ . Friction creates PV by acting to rotate  $\theta$  isosurfaces, so if friction is aligned with  $\nabla \theta$ , or when there is no spatial structure to  $\nabla \theta \times \mathbf{F}$  (i.e., zero divergence), then friction does not contribute to PV evolution. This interpretation is analogous to that given to the effects from baroclinicity on vorticity given in Section 35.5.

## 36.5 PV budget for a hydrostatic Boussinesq fluid

Building on the vorticity budget developed in Section 35.8, we here develop the potential vorticity substance budgets for a hydrostatic Boussinesq fluid in the presence of diabatic and frictional forcing. For that purpose, we recall the vorticity equation for a hydrostatic and Boussinesq fluid (35.111)

$$\frac{D\boldsymbol{\omega}_a^{\text{hy}}}{Dt} = \underbrace{(\boldsymbol{\omega}_a^{\text{hy}} \cdot \nabla) \mathbf{v}}_{\text{stretching + tilting}} + \underbrace{\nabla \times \hat{\mathbf{z}} b}_{\text{baroclinicity}} + \underbrace{\nabla \times \mathbf{F}}_{\text{friction curl}}. \quad (36.43)$$

### 36.5.1 Potential vorticity

Potential vorticity evolves in the absence of baroclinicity, which is eliminated from the vorticity equation (36.43) by projecting the absolute vorticity onto the direction normal to buoyancy

surfaces

$$\nabla b \cdot \frac{D\omega_a^{hy}}{Dt} = \nabla b \cdot [(\omega_a^{hy} \cdot \nabla) \mathbf{v}] + \nabla b \cdot (\nabla \times \mathbf{F}), \quad (36.44)$$

where we used

$$\nabla b \cdot (\nabla \times \hat{\mathbf{z}} b) = 0. \quad (36.45)$$

We next make use of the identity

$$\frac{D(\partial b / \partial x^i)}{Dt} = \frac{\partial}{\partial x^i} \left[ \frac{\partial b}{\partial t} \right] - \nabla b \cdot \frac{\partial \mathbf{v}}{\partial x^i} = \frac{\partial \dot{b}}{\partial x^i} - \nabla b \cdot \frac{\partial \mathbf{v}}{\partial x^i}, \quad (36.46)$$

so that

$$\omega_a^{hy} \cdot \left[ \frac{D \nabla b}{Dt} \right] = \omega_a^{hy} \cdot \nabla \dot{b} - \nabla b \cdot [(\omega_a^{hy} \cdot \nabla) \mathbf{v}]. \quad (36.47)$$

Making use of this result in equation (36.44) renders

$$\nabla b \cdot \frac{D\omega_a^{hy}}{Dt} + \omega_a^{hy} \cdot \frac{D \nabla b}{Dt} = \omega_a^{hy} \cdot \nabla \dot{b} + \nabla b \cdot (\nabla \times \mathbf{F}), \quad (36.48)$$

which leads to

$$\frac{DQ}{Dt} = \omega_a^{hy} \cdot \nabla \dot{b} + \nabla b \cdot (\nabla \times \mathbf{F}) \quad (36.49)$$

where

$$Q = \omega_a^{hy} \cdot \nabla b = \omega^{hy} \cdot \nabla b + f \frac{\partial b}{\partial z} \quad (36.50)$$

is the potential vorticity for a rotating hydrostatic Boussinesq fluid. Potential vorticity is materially invariant for the inviscid and adiabatic case, in which  $\mathbf{F} = 0$  and  $\dot{b} = 0$ .

It is sometimes useful to split the hydrostatic vorticity into its vertical and horizontal terms as per equation (35.101). In this way, PV takes on the form

$$Q = \frac{\partial u}{\partial z} \frac{\partial b}{\partial y} - \frac{\partial v}{\partial z} \frac{\partial b}{\partial x} + (\zeta + f) \frac{\partial b}{\partial z} = \hat{\mathbf{z}} \cdot \left[ \frac{\partial \mathbf{u}}{\partial z} \times \nabla b \right] + (\zeta + f) \frac{\partial b}{\partial z}. \quad (36.51)$$

### 36.5.2 Potential vorticity flux vector

The material form of the PV equation (36.49) is converted into its Eulerian flux-form via

$$\frac{\partial Q}{\partial t} + \nabla \cdot (\mathbf{v} Q) = \omega_a^{hy} \cdot \nabla \dot{b} + \nabla b \cdot (\nabla \times \mathbf{F}) \quad (36.52a)$$

$$= \nabla \cdot [\dot{b} \omega_a^{hy} + b (\nabla \times \mathbf{F})] \quad (36.52b)$$

$$= \nabla \cdot [\dot{b} \omega_a^{hy} + \nabla \times (b \mathbf{F}) - \nabla b \times \mathbf{F}] \quad (36.52c)$$

$$= \nabla \cdot [\dot{b} \omega_a^{hy} - \nabla b \times \mathbf{F}], \quad (36.52d)$$

where we used

$$\nabla \cdot \mathbf{v} = 0 \quad (36.53a)$$

$$\nabla \cdot \omega_a^{hy} = 0 \quad (36.53b)$$

$$\nabla \cdot (\nabla \times \mathbf{F}) = 0 \quad (36.53c)$$

$$\nabla \cdot [\nabla \times (b \mathbf{F})] = 0. \quad (36.53d)$$

The conservation equation (36.52d) allows us to identify a potential vorticity flux vector

$$\mathbf{J}_Q = \mathbf{v} Q - \dot{b} \boldsymbol{\omega}_a^{hy} + \nabla b \times \mathbf{F} + \nabla \times \mathbf{A}, \quad (36.54)$$

so that the PV equation takes the form

$$\frac{\partial Q}{\partial t} + \nabla \cdot \mathbf{J}_Q = 0. \quad (36.55)$$

The potential vorticity flux (36.54) is comprised of an advective term

$$\mathbf{J}_{\text{advective}} = \mathbf{v} Q, \quad (36.56)$$

and non-advective terms arising from diabatic and frictional forcing,

$$\mathbf{J}_{\text{non-advective}} = -\dot{b} \boldsymbol{\omega}_a^{hy} + \nabla b \times \mathbf{F}, \quad (36.57)$$

as well as a gauge term,

$$\mathbf{J}_{\text{gauge}} = \nabla \times \mathbf{A}, \quad (36.58)$$

whose form remains unspecified.

### 36.5.3 Kinematic derivation of the PV-substance flux

Following the discussion in Section 37.2.2, we consider a purely kinematic derivation of the PV flux vector. For that purpose write the hydrostatic Boussinesq PV in the form

$$Q = \boldsymbol{\omega}_a^{hy} \cdot \nabla b = \nabla \cdot (b \boldsymbol{\omega}_a^{hy}), \quad (36.59)$$

which follows since  $\nabla \cdot \boldsymbol{\omega}_a^{hy} = 0$ . Taking the Eulerian time derivative then leads to

$$\frac{\partial Q}{\partial t} = \nabla \cdot \left[ \frac{\partial b}{\partial t} \boldsymbol{\omega}_a^{hy} + b \frac{\partial \boldsymbol{\omega}_a^{hy}}{\partial t} \right] = \nabla \cdot \left[ \frac{\partial b}{\partial t} \boldsymbol{\omega}_a^{hy} + \frac{\partial \mathbf{u}}{\partial t} \times \nabla b \right], \quad (36.60)$$

which made use of the identities

$$\frac{\partial \boldsymbol{\omega}_a^{hy}}{\partial t} = \frac{\partial \boldsymbol{\omega}^{hy}}{\partial t} = \frac{\partial (\nabla \times \mathbf{u})}{\partial t} \quad \text{and} \quad \nabla \cdot [\nabla \times (b \mathbf{u})] = 0. \quad (36.61)$$

The PV thus evolves according to

$$\frac{\partial Q}{\partial t} = -\nabla \cdot \tilde{\mathbf{J}}_Q \quad (36.62)$$

where the PV flux is given by

$$\tilde{\mathbf{J}}_Q = -\frac{\partial b}{\partial t} \boldsymbol{\omega}_a^{hy} - \frac{\partial \mathbf{u}}{\partial t} \times \nabla b. \quad (36.63)$$

This form of the PV flux manifests the impermeability property of Chapter 37 since

$$\hat{\mathbf{n}} \cdot (\tilde{\mathbf{J}}_Q / Q) = -\frac{1}{|\nabla b|} \frac{\partial b}{\partial t} = \hat{\mathbf{n}} \cdot \mathbf{v}_{b\perp}, \quad (36.64)$$

where  $\hat{\mathbf{n}} = \nabla b |\nabla b|^{-1}$  is the unit normal for a buoyancy surface, and with  $\mathbf{v}_{b\perp}$  the velocity of a point on the isopycnal that satisfies

$$\frac{\partial b}{\partial t} + \mathbf{v}_{b\perp} \cdot \nabla b = 0. \quad (36.65)$$

### 36.5.4 Potential vorticity flux vector

We introduced the Bernoulli potential and Bernoulli theorem in Section 21.6.2. Schär (1993) provided a generalization of Bernoulli's Theorem, with Marshall (2000), Marshall et al. (2001), and Polton and Marshall (2007) applying this theorem to oceanic contexts. In particular, Marshall (2000) and Polton and Marshall (2007) work with a Boussinesq and hydrostatic ocean. We here consider the details of their analysis, with some of the material in this section building from the more general discussion in Section 37.3.1.

#### Momentum equation

Start by exposing the Boussinesq form of the Bernoulli potential from the vector-invariant velocity equation. For this purpose, return to the horizontal momentum equation (35.106), and expand the expressions for the perturbation pressure and the buoyancy

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{f} + \boldsymbol{\omega}^{\text{hy}}) \times \mathbf{v} = -\nabla(\varphi + |\mathbf{u}|^2/2) + \hat{\mathbf{z}} b + \mathbf{F} \quad (36.66a)$$

$$= -\nabla(|\mathbf{u}|^2/2) - \frac{1}{\rho_0} \nabla(p - p_0) - \hat{\mathbf{z}} \left[ \frac{g(\rho - \rho_0)}{\rho_0} \right] + \mathbf{F} \quad (36.66b)$$

$$= -\nabla(|\mathbf{u}|^2/2) - \frac{1}{\rho_0} \nabla p - \hat{\mathbf{z}} \frac{g\rho}{\rho_0} + \mathbf{F} \quad (36.66c)$$

$$= -\nabla \left[ \frac{|\mathbf{u}|^2}{2} + \frac{p}{\rho_0} \right] - \hat{\mathbf{z}} \left[ \frac{g\rho - g\rho_o + g\rho_0}{\rho_0} \right] + \mathbf{F} \quad (36.66d)$$

$$= -\nabla \left[ \frac{|\mathbf{u}|^2}{2} + \frac{p}{\rho_0} + g z \right] - \hat{\mathbf{z}} \left[ \frac{g(\rho - \rho_o)}{\rho_0} \right] + \mathbf{F} \quad (36.66e)$$

$$= -\nabla \mathcal{B} + \hat{\mathbf{z}} b + \mathbf{F}, \quad (36.66f)$$

where we introduced the Bernoulli potential for a hydrostatic and Boussinesq fluid<sup>3</sup>

$$\mathcal{B} = \frac{|\mathbf{u}|^2}{2} + \frac{p}{\rho_0} + g z. \quad (36.67)$$

#### Potential vorticity flux

The flux-form potential vorticity conservation statement remains as given by equation (36.52d), and the PV-substance flux is given by equation (36.54). However, we can make use of the gauge invariance of the PV-substance flux to write it in a manner conducive to analyzing steady state conditions. For this purpose, operate with  $\nabla b \times$  on the velocity equation (36.66f) to have

$$\nabla b \times \frac{\partial \mathbf{u}}{\partial t} + \nabla b \times (\boldsymbol{\omega}_a^{\text{hy}} \times \mathbf{v}) = -\nabla b \times \nabla \mathcal{B} + \nabla b \times \hat{\mathbf{z}} b + \nabla b \times \mathbf{F}, \quad (36.68)$$

and then make use of the identity

$$\nabla b \times (\boldsymbol{\omega}_a^{\text{hy}} \times \mathbf{v}) = (\nabla b \cdot \mathbf{v}) \boldsymbol{\omega}_a^{\text{hy}} - (\boldsymbol{\omega}_a^{\text{hy}} \cdot \nabla b) \mathbf{v} \quad (36.69)$$

in equation (36.68) to render

$$(\mathbf{v} \cdot \nabla b) \boldsymbol{\omega}_a^{\text{hy}} - (\boldsymbol{\omega}_a^{\text{hy}} \cdot \nabla b) \mathbf{v} = -\nabla b \times \frac{\partial \mathbf{u}}{\partial t} - \nabla b \times \nabla \mathcal{B} + \nabla b \times \hat{\mathbf{z}} b + \nabla b \times \mathbf{F}. \quad (36.70)$$

---

<sup>3</sup>See Section 21.6.1 for the non-Boussinesq Bernoulli potential.

Now write the flux given by equation (36.54) in the form

$$\mathbf{J}_Q = \mathbf{v} Q - \dot{b} \boldsymbol{\omega}_a^{hy} + \nabla b \times \mathbf{F} + \nabla \times \mathbf{A} \quad (36.71a)$$

$$= \mathbf{v} (\boldsymbol{\omega}_a^{hy} \cdot \nabla b) - \left[ \frac{\partial b}{\partial t} + \mathbf{v} \cdot \nabla b \right] \boldsymbol{\omega}_a^{hy} + \nabla b \times \mathbf{F} + \nabla \times \mathbf{A} \quad (36.71b)$$

$$= [\mathbf{v} (\boldsymbol{\omega}_a^{hy} \cdot \nabla b) - (\mathbf{v} \cdot \nabla b) \boldsymbol{\omega}_a^{hy}] - \frac{\partial b}{\partial t} \boldsymbol{\omega}_a^{hy} + \nabla b \times \mathbf{F} + \nabla \times \mathbf{A} \quad (36.71c)$$

$$= \left[ \nabla b \times \frac{\partial \mathbf{u}}{\partial t} + \nabla b \times \nabla \mathcal{B} - \nabla b \times \hat{\mathbf{z}} b - \nabla b \times \mathbf{F} \right] - \frac{\partial b}{\partial t} \boldsymbol{\omega}_a^{hy} + \nabla b \times \mathbf{F} + \nabla \times \mathbf{A} \quad (36.71d)$$

$$= \nabla b \times \frac{\partial \mathbf{u}}{\partial t} - \frac{\partial b}{\partial t} \boldsymbol{\omega}_a^{hy} + \nabla b \times \nabla \mathcal{B} - \nabla b \times \hat{\mathbf{z}} b + \nabla \times \mathbf{A}. \quad (36.71e)$$

$$= \nabla b \times \left[ \frac{\partial \mathbf{u}}{\partial t} + \nabla \mathcal{B} \right] - \frac{\partial b}{\partial t} \boldsymbol{\omega}_a^{hy} + \nabla \times (\mathbf{A} - \hat{\mathbf{z}} b^2 / 2). \quad (36.71f)$$

Choosing the gauge function according to

$$\mathbf{A} = \hat{\mathbf{z}} (b^2 / 2) \quad (36.72)$$

renders the flux vector

$$\mathbf{J}_Q = \nabla b \times \left( \frac{\partial \mathbf{u}}{\partial t} + \nabla \mathcal{B} \right) - \frac{\partial b}{\partial t} \boldsymbol{\omega}_a^{hy} \quad (36.73a)$$

$$= \mathbf{v} Q - \dot{b} \boldsymbol{\omega}_a^{hy} + \nabla b \times \mathbf{F}. \quad (36.73b)$$

The second equality reintroduced the first form of the PV flux given by equation (36.54); made use of the gauge choice (36.72); and furthermore dropped the non-divergent term

$$\nabla b \times b \hat{\mathbf{z}} = (1/2) \nabla b^2 \times \hat{\mathbf{z}} \quad \text{with} \quad \nabla \cdot (\nabla b \times b \hat{\mathbf{z}}) = 0. \quad (36.74)$$

In the steady state, the PV flux (36.73a) reduces to

$$\mathbf{J}_Q^{ss} = \nabla b \times \nabla \mathcal{B}. \quad (36.75)$$

Hence, the steady state potential vorticity flux is aligned with the intersection of surfaces of constant buoyancy and Bernoulli potential

$$\nabla b \cdot \mathbf{J}_Q^{ss} = 0 \quad \text{and} \quad \nabla \mathcal{B} \cdot \mathbf{J}_Q^{ss} = 0. \quad (36.76)$$

This result is the Boussinesq/hydrostatic form of the more general result derived in Section 37.3.3.

## 36.6 Exercises

### EXERCISE 36.1: PV FOR A PERFECT NON-HYDROSTATIC BOUSSINESQ FLUID

Consider a perfect rotating Boussinesq fluid whose governing equations are given by

$$\frac{D\mathbf{v}}{Dt} + f(\hat{\mathbf{z}} \times \mathbf{v}) = -\nabla\varphi + b\hat{\mathbf{z}} \quad (36.77)$$

$$\nabla \cdot \mathbf{v} = 0 \quad (36.78)$$

$$\frac{Db}{Dt} = 0 \quad (36.79)$$

$$b = -\frac{g(\rho - \rho_0)}{\rho_0} = g\alpha\theta, \quad (36.80)$$

where  $\theta$  is the potential temperature and  $\alpha > 0$  is a constant thermal expansion coefficient. Further details are provided in Section 23.1.6. Some of this exercise follows the hydrostatic Boussinesq discussion in Section 36.5, though they differ in important places so be careful!

- (a) Derive the equation for the material time evolution of potential vorticity in this fluid system. Show all steps in the derivation.
- (b) The baroclinicity vector appearing in the Boussinesq vorticity equation is  $\mathbf{B} = \nabla \times \hat{\mathbf{z}} b = \nabla b \times \hat{\mathbf{z}}$  (see Section 35.8.1 to check the derivation in part (a) above). Show that this vector results upon making the Boussinesq approximation to the non-Boussinesq expression  $\mathbf{B} = (\nabla\rho \times \nabla p)/\rho^2$ . Hint: drop the  $\delta\rho$  and  $\delta p$  product given that it is a higher order quantity.
- (c) Show that the vertical portion of  $Q^{\text{bouss}}$  can be written

$$Q_{\text{vert}}^{\text{bouss}} = (\zeta + f) N^2 \quad (36.81)$$

where  $\zeta = \partial_x v - \partial_y u$  is the vertical component to the relative vorticity and  $N^2 = \partial b / \partial z$  is the squared buoyancy frequency (Section 24.5.4). Hint: this is not tough to show; there is no trick here.

- (d) If flow maintains hydrostatic and geostrophic balance, show that the horizontal portion of  $Q^{\text{bouss}}$  can be written

$$Q_{\text{horz}}^{\text{bouss}} = \boldsymbol{\omega} \cdot \nabla_z b \approx -f^{-1} |\nabla_z b|^2. \quad (36.82)$$

Hint: recall that for hydrostatic and geostrophic flow, the vertical velocity is much smaller than horizontal.

### EXERCISE 36.2: PV FOR DIABATIC AND FRICTIONAL NON-HYDROSTATIC BOUSSINESQ FLOW

Reconsider Exercise 36.1 in the presence of irreversible friction and buoyancy sources so that the governing equations are

$$\frac{D\mathbf{v}}{Dt} + f(\hat{\mathbf{z}} \times \mathbf{v}) = -\nabla\varphi + b\hat{\mathbf{z}} + \mathbf{F} \quad (36.83)$$

$$\nabla \cdot \mathbf{v} = 0 \quad (36.84)$$

$$\frac{Db}{Dt} = \dot{b} \quad (36.85)$$

$$b = -\frac{g(\rho - \rho_0)}{\rho_0} = g\alpha\theta, \quad (36.86)$$

where  $\dot{\theta}$  is a diabatic heating source/sink,  $\alpha$  is a constant thermal expansion coefficient, and  $\mathbf{F}$  is a non-conservative acceleration such as from friction or boundary stresses.

- (a) Derive the equation for the material time evolution of potential vorticity in this fluid system, including the irreversible contributions from friction and heating.
- (b) Derive an equation for the potential vorticity time tendency (i.e., Eulerian time derivative), written in the form

$$\frac{\partial Q}{\partial t} = -\nabla \cdot \mathbf{J}_Q. \quad (36.87)$$

What is the PV flux  $\mathbf{J}_Q$ ? Note that your answer is unique up to the curl of an arbitrary vector (gauge symmetry). Also note that for a Boussinesq flow we drop the constant reference density in the definition of  $\mathbf{J}_Q$ .

- (c) A common diabatic process is written in the form of a damping source

$$\dot{b} = -\mu(b - b^*), \quad (36.88)$$

where  $\mu$  is a constant Newtonian damping coefficient (dimensions of inverse time), and  $b^*$  is a specified buoyancy profile. This form of a buoyancy source acts to damp the buoyancy towards a specified profile  $b^*$ . Show that Newtonian damping of buoyancy corresponds to potential vorticity damping towards  $Q^* = \boldsymbol{\omega}_a \cdot \nabla b^*$ .

- (d) A form for the friction operator is given by Rayleigh drag

$$\mathbf{F} = -\gamma \mathbf{v}, \quad (36.89)$$

with  $\gamma$  a constant Rayleigh damping coefficient with dimension of inverse time. Show that Rayleigh drag in the momentum equation, which acts to damp velocity towards zero, corresponds to a damping of potential vorticity towards its planetary geostrophic form,  $Q^{pg} = f N^2$ , where  $N^2 = \partial b / \partial z$  is the squared buoyancy frequency.

- (e) Discuss the balance needed between forcing terms in  $\mathbf{J}_Q$  to arrive at a steady state (i.e., zero Eulerian time tendency). Continue to assume the friction is in the form of Rayleigh drag and heating is in the form of Newtonian damping.





# Chapter 37

## Potential vorticity budgets

The chapter examines a particularly striking property of the flux of potential vorticity substance. Namely, there are forms for this flux (differing by gauge choices) that have identically zero flux of PV-substance crossing an isentrope. This *impermeability theorem* holds even when there are mass and entropy fluxes crossing the isentrope. Isentropes are thus semi-permeable membranes in the sense that they are open to the transport of matter and thermodynamic properties but closed to the transport of PV-substance. This kinematic result offers further understanding for why, as developed in Section 37.4,  $\rho Q$  remains constant within an isentrope unless the isentrope intersects a boundary. These notions are fundamental to how we perform a budget of potential vorticity substance over a region.

### CHAPTER GUIDE

This chapter builds from the potential vorticity mechanics introduced in Chapter 36. It is an essential read for those interested in potential vorticity theory and potential vorticity budgets.

37.1	Loose threads . . . . .	930
37.2	Variations on the impermeability theorem . . . . .	930
37.2.1	Impermeability for the Haynes-McIntyre PV flux . . . . .	930
37.2.2	A kinematic derivation of impermeability . . . . .	931
37.2.3	Impermeability for all components of absolute vorticity . . . . .	933
37.2.4	Comments . . . . .	933
37.3	Impermeability theorem for a realistic seawater EOS . . . . .	934
37.3.1	Ocean PV in terms of potential density . . . . .	934
37.3.2	A modified PV-substance flux . . . . .	934
37.3.3	Integral constraints for steady state . . . . .	936
37.3.4	Further study . . . . .	936
37.4	Integrated potential vorticity . . . . .	936
37.4.1	Region bounded by a buoyancy surface . . . . .	937
37.4.2	Region bounded by two buoyancy surfaces . . . . .	937
37.4.3	Region bounded by land and a buoyancy surface . . . . .	938
37.4.4	An ocean layer that outcrops . . . . .	939
37.5	Layer integrated PV budget . . . . .	939
37.5.1	Layer integrated budget . . . . .	940
37.5.2	Impermeability across interior layer interfaces . . . . .	941
37.5.3	PV flux at the land-sea boundary . . . . .	941

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37.5.4	PV flux at the air-sea boundary . . . . .	942
37.5.5	Thought experiments . . . . .	943
37.5.6	Is there a preferred form of the PV-substance flux? . . . . .	944

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## 37.1 Loose threads

- *Callies and Ferrari (2018)* and bottom mixing induced circulation. Connect the thermal wind next to the bottom, inducing flow counter to Kelvin waves, to the PV boundary fluxes in Section 37.5.3. Discuss the spin up experiment in Section 4 of *Callies and Ferrari (2018)* from a PV perspective. Note the role of bottom friction in enabling the bottom buoyancy mixing to impart PV to the flow. without friction then there would be no way to introduce PV to the flow. That then couples the buoyancy mixing to the friction. *Callies and Ferrari (2018)* also note that to satisfy  $\hat{\mathbf{n}} \cdot \nabla b = 0$  requires friction. I do not understand that fully, but must be related to this PV argument.
- PV near boundaries as in *Benthuysen and Thomas (2012)*.
- Note that all components of vorticity are globally zero when integrated over regions without boundaries intersecting surfaces that define the vorticity.
- Introduce an arbitrary scalar and show that impermeability holds for vorticity projected into the direction normal to isoscalar surfaces.

## 37.2 Variations on the impermeability theorem

In this section we derive the impermeability theorem by making use of a variety of forms for the flux vector of potential vorticity substance. The forms differ by a gauge function, so that the divergence of all the flux forms are the same.

### 37.2.1 Impermeability for the Haynes-McIntyre PV flux

Recall the Eulerian flux-form evolution equation for PV-substance (36.40)

$$\frac{\partial(\rho Q)}{\partial t} + \nabla \cdot \mathbf{J}_Q = 0 \quad \text{with} \quad \mathbf{J}_Q = \rho \mathbf{v} Q - \dot{\theta} \boldsymbol{\omega}_a + \nabla \theta \times \mathbf{F}, \quad (37.1)$$

with the PV-substance flux vector,  $\mathbf{J}_Q$ , here given in the form examined in *Haynes and McIntyre (1987)*. Now decompose the velocity into two components, one oriented parallel to isentropes and one oriented perpendicular

$$\mathbf{v}_{\parallel} = \mathbf{v} - \hat{\mathbf{n}} (\mathbf{v} \cdot \hat{\mathbf{n}}) \quad \text{and} \quad \mathbf{v}_{\perp} = -\frac{\hat{\mathbf{n}} \partial \theta / \partial t}{|\nabla \theta|} \quad \Rightarrow \mathbf{v} = \mathbf{v}_{\parallel} + \mathbf{v}_{\perp} + \frac{\hat{\mathbf{n}} \dot{\theta}}{|\nabla \theta|} \quad (37.2)$$

where  $\hat{\mathbf{n}} = \nabla \theta / |\nabla \theta|$  is the normal vector on an isentrope. The velocity  $\mathbf{v}_{\perp}$ , by construction, satisfies

$$\frac{\partial \theta}{\partial t} + \mathbf{v}_{\perp} \cdot \nabla \theta = 0. \quad (37.3)$$

Hence, according to the kinematics detailed in Section 14.4.2,

$$\mathbf{v}_{\perp} \cdot \hat{\mathbf{n}} = \mathbf{v}_{\theta} \cdot \hat{\mathbf{n}}, \quad (37.4)$$

where  $\mathbf{v}_\theta$  is the velocity of a point fixed on the  $\theta$  isosurface. We make use of this key identity below.

With the velocity decomposition (37.2), the PV-substance flux vector takes the form

$$\mathbf{J}_Q = \rho \mathbf{v} Q - \dot{\theta} \boldsymbol{\omega}_a + \nabla \theta \times \mathbf{F} \quad (37.5a)$$

$$= \left[ \mathbf{v}_{\parallel} + \mathbf{v}_{\perp} + \frac{\dot{\theta} \nabla \theta}{|\nabla \theta|^2} \right] \rho Q - \dot{\theta} \boldsymbol{\omega}_a + \nabla \theta \times \mathbf{F} \quad (37.5b)$$

$$= (\mathbf{v}_{\parallel} + \mathbf{v}_{\perp}) \rho Q - \dot{\theta} [\boldsymbol{\omega}_a - (\boldsymbol{\omega}_a \cdot \hat{\mathbf{n}}) \hat{\mathbf{n}}] + \nabla \theta \times \mathbf{F} \quad (37.5c)$$

$$= (\mathbf{v}_{\parallel} + \mathbf{v}_{\perp}) \rho Q - \dot{\theta} (\boldsymbol{\omega}_a)_{\parallel} + \nabla \theta \times \mathbf{F} \quad (37.5d)$$

$$= \mathbf{v}_{\perp} \rho Q + \left[ \rho Q \mathbf{v}_{\parallel} - \dot{\theta} (\boldsymbol{\omega}_a)_{\parallel} \right] + \nabla \theta \times \mathbf{F} \quad (37.5e)$$

$$\equiv \mathbf{J}_{\perp} + \mathbf{J}_{\parallel}, \quad (37.5f)$$

where

$$(\boldsymbol{\omega}_a)_{\parallel} = \boldsymbol{\omega}_a - (\boldsymbol{\omega}_a \cdot \hat{\mathbf{n}}) \hat{\mathbf{n}} = \boldsymbol{\omega}_a - \left[ \frac{\boldsymbol{\omega}_a \cdot \nabla \theta}{|\nabla \theta|^2} \right] \nabla \theta = \boldsymbol{\omega}_a - \frac{\rho Q}{|\nabla \theta|} \hat{\mathbf{n}}. \quad (37.6)$$

The above results motivate us to write the PV-substance budget equation (37.1) in the alternative form

$$\frac{\partial(\rho Q)}{\partial t} + \nabla \cdot (\mathbf{v}_Q \rho Q) = 0, \quad (37.7)$$

where

$$\mathbf{v}_Q = \frac{\mathbf{J}_Q}{\rho Q} = \mathbf{v}_{\perp} + \mathbf{v}_{\parallel} - \frac{\dot{\theta} (\boldsymbol{\omega}_a)_{\parallel} + \mathbf{F} \times \nabla \theta}{\rho Q} \quad (37.8)$$

is an effective velocity that advects the PV-substance through the fluid. A direct calculation shows that  $\mathbf{v}_Q$  satisfies the following key property

$$\mathbf{v}_Q \cdot \hat{\mathbf{n}} = \mathbf{v}_{\perp} \cdot \hat{\mathbf{n}} = \mathbf{v}_\theta \cdot \hat{\mathbf{n}}, \quad (37.9)$$

where the final equality made use of the identity (37.4). As a result, the velocity  $\mathbf{v}_Q$ , which advects PV-substance, has a normal component that is identical to that of the velocity of a point fixed on the isentrope

$$\frac{\partial \theta}{\partial t} + \mathbf{v}_Q \cdot \nabla \theta = 0. \quad (37.10)$$

We depict this result in Figure 37.1, whereby the PV-substance flux never crosses the isentrope, even as the isentrope moves and even in the presence of irreversible processes that allow for matter and heat to cross the isentrope. This result holds since the  $\theta$ -isosurface moves in a way to precisely track the PV-substance flux. In the presence of non-conservative processes, isentropes are permeable to matter and heat but impermeable to PV-substance. This is a rather remarkable kinematic result that has important implications for budgets of PV-substance, as shown by the discussion in the remainder of this chapter as well as when discussing ocean potential vorticity in Chapter 44.

### 37.2.2 A kinematic derivation of impermeability

We here offer a second derivation of the impermeability theorem that emphasizes its kinematic origins. That is, we make no use of the vorticity equation or the potential temperature equation. Instead, we merely make use of the definition of potential vorticity and, critically, the non-divergence of absolute vorticity.

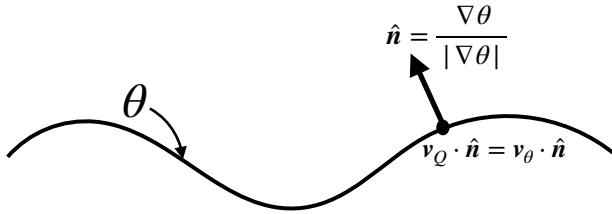


FIGURE 37.1: The flux,  $\mathbf{J}_Q$ , of PV-substance does not penetrate a surface of constant potential temperature (isentrope). This kinematic result follows since the effective velocity of PV-substance,  $\mathbf{v}_Q = \mathbf{J}_Q^{\text{HM}} / (\rho Q)$ , has the same normal component as a point fixed on a potential temperature iso-surface,  $\mathbf{v}_Q \cdot \hat{n} = \mathbf{v}_\theta \cdot \hat{n}$ . Consequently, the potential temperature surface moves in a manner so that no flux of PV-substance crosses the surface, even in the presence of irreversible processes. This result is known as the impermeability theorem since potential temperature surfaces are impermeable to the flux of PV-substance.

The key identity we need is the following

$$\rho Q = \boldsymbol{\omega}_a \cdot \nabla\theta = \nabla \cdot (\boldsymbol{\omega}_a \theta), \quad (37.11)$$

so that  $\rho Q$  is a pure divergence. Taking the Eulerian time derivative then leads to

$$\frac{\partial(\rho Q)}{\partial t} = -\nabla \cdot \mathbf{J}_Q^{\text{kin}}, \quad (37.12)$$

where

$$\mathbf{J}_Q^{\text{kin}} = -\frac{\partial(\boldsymbol{\omega}_a \theta)}{\partial t} \quad (37.13)$$

is the kinematic form of the PV-substance flux. By construction, this flux vanishes in the steady state

$$\mathbf{J}_Q^{\text{kin}} = 0 \quad \text{in steady state}, \quad (37.14)$$

which contrasts to the Haynes-McIntyre form given by equation (37.1). We return to this point in Section 37.3 where we introduce a strategically chosen gauge term (a total curl) to render a nonzero flux in the steady state.

Introducing the velocity seen from an inertial reference frame (also called the absolute velocity; Section 9.9.1)

$$\mathbf{v}_a = \mathbf{v} + \boldsymbol{\Omega} \times \mathbf{x} \quad (37.15)$$

leads to

$$-\frac{\partial \boldsymbol{\omega}_a}{\partial t} \theta = -\frac{\partial(\nabla \times \mathbf{v}_a)}{\partial t} \theta = -\left[ \nabla \times \frac{\partial \mathbf{v}_a}{\partial t} \right] \theta = -\nabla \times \left[ \frac{\partial \mathbf{v}_a}{\partial t} \theta \right] + \nabla\theta \times \frac{\partial \mathbf{v}_a}{\partial t}. \quad (37.16)$$

Dropping the total curl yields the modified kinematic form for the PV-substance flux

$$\tilde{\mathbf{J}}_Q^{\text{kin}} = -\frac{\partial \mathbf{v}_a}{\partial t} \times \nabla\theta - \boldsymbol{\omega}_a \frac{\partial \theta}{\partial t}. \quad (37.17)$$

It follows that

$$\tilde{\mathbf{v}}_Q^{\text{kin}} \cdot \hat{n} = \frac{\tilde{\mathbf{J}}_Q^{\text{kin}} \cdot \hat{n}}{\rho Q} = -\frac{\boldsymbol{\omega}_a \cdot \nabla\theta}{\rho Q} \frac{\partial \theta}{\partial t} \frac{1}{|\nabla\theta|} = -\frac{\partial \theta}{\partial t} \frac{1}{|\nabla\theta|} = \mathbf{v}_\theta \cdot \hat{n}, \quad (37.18)$$

which then leads to the impermeability theorem for  $\tilde{\mathbf{J}}_Q^{\text{kin}}$ . We again emphasize that there has been no use of the dynamical equations for vorticity or potential temperature. Instead, this expression

of impermeability only used the definition of potential vorticity along with the central property  $\nabla \cdot \boldsymbol{\omega}_a = 0$ .

### 37.2.3 Impermeability for all components of absolute vorticity

The above kinematic result suggests that the impermeability theorem is both remarkable and trivial. We support that dual characterization by here showing that all components of absolute vorticity satisfy an impermeability theorem with respect to the direction along which the components are defined. This discussion generalizes that given in Section 35.4.4 when studying the Cartesian components of the absolute vorticity.

Consider an arbitrary smooth scalar field  $\lambda$  and use it to project out that component of absolute vorticity normal to  $\lambda$  isosurfaces

$$\rho Q_\lambda \equiv \boldsymbol{\omega}_a \cdot \nabla \lambda = \nabla \cdot (\boldsymbol{\omega}_a \lambda). \quad (37.19)$$

Following the derivation given in Section 37.2.2 leads to

$$\frac{\partial(\rho Q_\lambda)}{\partial t} = \nabla \cdot \left[ \frac{\partial \mathbf{v}_a}{\partial t} \times \nabla \lambda + \boldsymbol{\omega}_a \frac{\partial \lambda}{\partial t} \right] \equiv -\nabla \cdot \mathbf{J}_{Q_\lambda}. \quad (37.20)$$

It follows that

$$\frac{\mathbf{J}_{Q_\lambda} \cdot \hat{\mathbf{n}}_\lambda}{\rho Q_\lambda} = -\frac{\boldsymbol{\omega}_a \cdot \nabla \lambda}{\rho Q_\lambda} \frac{\partial \lambda}{\partial t} \frac{1}{|\nabla \lambda|} = -\frac{\partial \lambda}{\partial t} \frac{1}{|\nabla \lambda|} = \mathbf{v}_\lambda \cdot \hat{\mathbf{n}}_\lambda, \quad (37.21)$$

where

$$\hat{\mathbf{n}}_\lambda = \frac{\nabla \lambda}{|\nabla \lambda|} \quad \text{and} \quad \frac{\partial \lambda}{\partial t} + \mathbf{v}_\lambda \cdot \nabla \lambda = 0. \quad (37.22)$$

We are thus led to an impermeability theorem for the  $\lambda$ -surface. Hence, *any* scalar field used to project out a component of the absolute vorticity has its iso-surfaces impenetrable to the flux of the corresponding component of absolute vorticity. This result trivializes the impermeability theorem from a mathematical perspective, with Section 5 of [Haynes and McIntyre \(1987\)](#) offering further mathematical insights into the inevitability of the result based on the structure of the vorticity equation (see also Section 35.4.4). Even so, it does not reduce the importance of the entropic PV impermeability theorem for studies of stratified flows, since entropic PV is a special component of the absolute vorticity that has direct connection to dynamics and thermodynamics.

### 37.2.4 Comments

The impermeability theorem was introduced by [Haynes and McIntyre \(1987\)](#), with their paper met by some confusion that prompted [Haynes and McIntyre \(1990\)](#). The impermeability theorem emphasizes the importance of boundary processes when studying how potential vorticity substance changes within a domain bounded by isentropes. We further examine the role of such processes in Sections 37.4 and 37.5. An emphasis on boundary processes is a focus of oceanographic studies of submesoscale instabilities such as [Thomas et al. \(2008\)](#).

Besides exposing the purely kinematic aspects of the impermeability theorem, the presentation in this section reveals that there are multiple PV flux vectors that satisfy the impermeability theorem, with the vectors differing by a gauge transformation. Which vector is preferred depends on the application, with [Bretherton and Schär \(1993\)](#), [Davies-Jones \(2003a\)](#), and [Marshall et al. \(2001\)](#) proposing criteria favoring one form over another. We pursue an example of such considerations in Section 37.3.

### 37.3 Impermeability theorem for a realistic seawater EOS

As seen from Section 37.2.3, impermeability holds for any component of vorticity and the corresponding scalar isosurface. In contrast, material invariance of potential vorticity requires a materially conserved scalar to annihilate the baroclinicity vector (e.g., Section 36.1.4). As shown in Section 36.2, there is no such materially invariant scalar for an ocean with a realistic nonlinear equation of state (EOS). Hence, there is no materially invariant potential vorticity for the ocean even in the absence of irreversible processes. Nevertheless, one can define an ocean potential vorticity according to any scalar field, such as potential density, and still make use of the impermeability theorem when performing a PV budget.

#### 37.3.1 Ocean PV in terms of potential density

The distinction between impermeability and material invariance was emphasized by [Marshall et al. \(2001\)](#), and we here summarize features from that paper. For that purpose, introduce an ocean potential vorticity field according to

$$Q^{\text{ocn}} = \frac{\nabla b \cdot \omega_a}{\rho}, \quad (37.23)$$

where the globally defined buoyancy field,  $b$ , is approximated by a chosen potential density. As shown in Section 36.2, a globally defined buoyancy does not annihilate the baroclinicity vector for a realistic seawater equation of state

$$\mathbf{B} \cdot \nabla b = [-\nabla(1/\rho) \times \nabla p] \cdot \nabla b \neq 0. \quad (37.24)$$

Consequently,  $DQ^{\text{ocn}}/Dt \neq 0$  even in the absence of irreversible processes. Nonetheless, the Eulerian budget for PV-substance satisfies

$$\frac{\partial(\rho Q^{\text{ocn}})}{\partial t} = -\nabla \cdot \tilde{\mathbf{J}}_Q^{\text{ocn}}, \quad (37.25)$$

and  $\tilde{\mathbf{J}}_Q^{\text{ocn}}$  satisfies the impermeability theorem for  $b$ -surfaces. A flux-form budget equation greatly facilitates the study of budgets for PV-substance even within an ocean with a realistic equation of state. Derivation of the flux-form equation (37.25) follows from the discussion in Section 37.2.2, where we know that the kinematic flux

$$\tilde{\mathbf{J}}_Q^{\text{ocn}} = -\frac{\partial \mathbf{v}_a}{\partial t} \times \nabla b - \omega_a \frac{\partial b}{\partial t} = -\frac{\partial \mathbf{v}}{\partial t} \times \nabla b - \omega_a \frac{\partial b}{\partial t} \quad (37.26)$$

satisfies the impermeability theorem for  $b$ -surfaces and whose convergence drives the time tendency for the PV-substance. Note that the second equality in equation (37.26) follows since

$$\frac{\partial \mathbf{v}_a}{\partial t} = \frac{\partial(\mathbf{v} + \boldsymbol{\Omega} \times \mathbf{x})}{\partial t} = \frac{\partial \mathbf{v}}{\partial t}, \quad (37.27)$$

given that the Eulerian time derivative is computed at a fixed position,  $\mathbf{x}$ , and the planetary rotation is assumed constant.

#### 37.3.2 A modified PV-substance flux

The kinematic flux (37.26) vanishes in the steady state. We here motivate a gauge transformed flux that leads to the same flux divergence yet that renders a more physically interesting steady

state flux. For this purpose, make use of the vector-invariant velocity equation (equation (35.23))

$$\frac{\partial \mathbf{v}}{\partial t} + \boldsymbol{\omega}_a \times \mathbf{v} = -\rho^{-1} \nabla p - \nabla m + \mathbf{F}, \quad (37.28)$$

where

$$m = \frac{1}{2} \mathbf{v} \cdot \mathbf{v} + \Phi \quad (37.29)$$

is the mechanical energy per mass of a fluid element. Bringing the pressure term inside of the gradient operator leads to

$$\frac{\partial \mathbf{v}}{\partial t} + \boldsymbol{\omega}_a \times \mathbf{v} = p \nabla(1/\rho) - \nabla(m + p/\rho) + \mathbf{F}. \quad (37.30)$$

Some treatments choose to introduce the Bernoulli function.<sup>1</sup>

$$B = m + p/\rho, \quad (37.31)$$

The vector-invariant velocity equation (37.30) leads to the cross-product

$$\frac{\partial \mathbf{v}}{\partial t} \times \nabla b = -(\boldsymbol{\omega}_a \times \mathbf{v}) \times \nabla b + [p \nabla(1/\rho) - \nabla(m + p/\rho) + \mathbf{F}] \times \nabla b \quad (37.32a)$$

$$= -(\nabla b \cdot \boldsymbol{\omega}_a) \mathbf{v} + (\nabla b \cdot \mathbf{v}) \boldsymbol{\omega}_a + [p \nabla(1/\rho) - \nabla(m + p/\rho) + \mathbf{F}] \times \nabla b \quad (37.32b)$$

$$= -\mathbf{v} \rho Q^{ocn} + (\dot{b} - \partial_t b) \boldsymbol{\omega}_a + [p \nabla(1/\rho) - \nabla(m + p/\rho) + \mathbf{F}] \times \nabla b. \quad (37.32c)$$

Use of this result leads to the flux (37.26)

$$\tilde{\mathbf{J}}_Q^{ocn} = -\frac{\partial \mathbf{v}}{\partial t} \times \nabla b - \boldsymbol{\omega}_a \frac{\partial b}{\partial t} \quad (37.33a)$$

$$= \mathbf{v} \rho Q^{ocn} - \dot{b} \boldsymbol{\omega}_a - \mathbf{F} \times \nabla b + [\nabla(m + p/\rho) - p \nabla(1/\rho)] \times \nabla b \quad (37.33b)$$

$$= \mathbf{J}_Q + [\nabla(m + p/\rho) - p \nabla(1/\rho)] \times \nabla b, \quad (37.33c)$$

where  $\mathbf{J}_Q$  is the Haynes-McIntyre form of the PV-substance flux given by equation (37.1). The term

$$\nabla(m + p/\rho) \times \nabla b = \nabla \times [(m + p/\rho) \nabla b] \quad (37.34)$$

is a total curl and as such it can be moved around without altering the evolution of PV-substance; i.e., it is a “do nothing” flux. Furthermore, since it is parallel to buoyancy isosurfaces it does not alter the impermeability properties of the PV-substance flux.

*Marshall et al. (2001)* focused attention on the flux

$$\mathbf{J}_Q^{\text{marshall}} = \tilde{\mathbf{J}}_Q^{ocn} - \nabla(m + p/\rho) \times \nabla b = -\left[ \frac{\partial \mathbf{v}}{\partial t} + \nabla(m + p/\rho) \right] \times \nabla b - \boldsymbol{\omega}_a \frac{\partial b}{\partial t}. \quad (37.35)$$

Diagnostically desirable features of  $\mathbf{J}_Q^{\text{marshall}}$  include the following

- $\nabla b \cdot \mathbf{J}_Q^{\text{marshall}} / (\rho Q) = \partial_t b$ , thus satisfying the impermeability theorem.
- $\mathbf{J}_Q^{\text{marshall}}$  has no explicit reference to irreversible processes. Consequently, it can in some cases be simpler to diagnose than the Haynes-McIntyre flux,  $\mathbf{J}_Q$ .

<sup>1</sup>The Bernoulli potential,  $\mathcal{B}$ , arises from an analysis of the total energy budget as in equation (21.78), where we see that the Bernoulli potential in a compressible (non-Boussinesq) fluid,  $\mathcal{B} = m + p/\rho + \mathcal{I}$ , also includes the internal energy per mass,  $\mathcal{I}$ . However, the internal energy is missing from equation (37.31), thus motivating our use of the terminology “a Bernoulli function” rather than “the Bernoulli potential”.

- In a steady state, the flux is given by

$$\mathbf{J}_Q^{\text{marshall}} = \nabla b \times \nabla(m + p/\rho) = \nabla \times [b \nabla(m + p/\rho)]. \quad (37.36)$$

Consequently,  $m + p/\rho$  provides a streamfunction for the steady state flux on buoyancy surfaces. As emphasized by [Schär \(1993\)](#), this result holds even when there are irreversible processes, thus providing useful diagnostics even in the presence of dissipation.

### 37.3.3 Integral constraints for steady state

The steady state PV-substance flux in the form (37.36) can be used to develop some integral constraints on the steady flow. For this purpose consider the steady form of  $\mathbf{J}_Q^{\text{marshall}}$  and integrate over an arbitrary simply connected area making use of Stokes' theorem

$$\int_S \nabla \times [b \nabla B] \cdot \hat{\mathbf{n}} dS = \oint_{\partial S} b \nabla B \cdot d\mathbf{r} = \oint_{\partial S} b dB = - \oint_{\partial S} B db. \quad (37.37a)$$

The first equality made use of Stokes' theorem; the second make use of the identity for exact differentials

$$\nabla B \cdot d\mathbf{r} = dB; \quad (37.38)$$

and the final equality made use of

$$b dB = d(b B) - B db \quad (37.39)$$

and noted that

$$\oint_{\partial S} d(B b) = 0. \quad (37.40)$$

If we can find a closed contour where either  $B$  is a constant ( $dB = 0$ ), or the buoyancy is a constant ( $db = 0$ ), then we have the steady state constraint

$$\int_S \mathbf{J}_Q^{\text{marshall}} \cdot \hat{\mathbf{n}} dS = 0 \quad \text{area enclosed by contour with } m + p/\rho \text{ constant or } b \text{ constant.} \quad (37.41)$$

In regions where there are such closed contours, this constraint offers useful insight into the steady state balances. [Marshall \(2000\)](#) and [Polton and Marshall \(2007\)](#) make particular use of closed  $B$  contours on constant depth surfaces (so that  $\hat{\mathbf{n}} = \hat{\mathbf{z}}$ ) in a Boussinesq fluid.

### 37.3.4 Further study

[Marshall et al. \(2001\)](#) builds from the generalized Bernoulli theorem of [Schär \(1993\)](#) and [Bretherton and Schär \(1993\)](#). We also consider these topics for a Boussinesq hydrostatic fluid in Section 36.5.4.

## 37.4 Integrated potential vorticity

In this section we derive some kinematic properties of integrated potential vorticity, with these properties the result of how potential vorticity is defined. We write potential vorticity using a global buoyancy field,  $b$ , as in our discussion of ocean potential vorticity in Section 37.3

$$Q = \frac{\boldsymbol{\omega}_a \cdot \nabla b}{\rho} = \frac{\nabla \cdot (\boldsymbol{\omega}_a b)}{\rho}. \quad (37.42)$$

Notably, the properties exhibited in this section hold even when there is no materially invariant potential vorticity, since they rely solely on the non-divergent nature of the absolute vorticity.

In this section we consider  $Q$  to be an intensive fluid property measuring the amount of PV-substance per unit mass (i.e., the concentration of PV-substance), and correspondingly with  $\rho Q$  the amount of PV-substance per volume.<sup>2</sup> With this interpretation, the amount of PV substance within an arbitrary finite region is determined by the volume integral of  $\rho Q$

$$\mathcal{I} = \int_{\mathcal{R}} Q \rho dV = \int_{\mathcal{R}} \nabla \cdot (\boldsymbol{\omega}_a b) dV = \oint_{\partial\mathcal{R}} \boldsymbol{\omega}_a b \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (37.43)$$

where the final equality used Gauss's divergence theorem. Hence, the volume integrated PV substance in a region is determined solely by values on the region boundary. This property is strikingly distinct from material tracers.

### 37.4.1 Region bounded by a buoyancy surface

Consider a volume of fluid bounded by a single buoyancy surface as shown in the bubble-like region in the left panel of Figure 37.2. Since the outer boundary of the region is set by a constant  $b$ -surface, we can pull  $b$  outside of the surface integral in equation (37.43) so that

$$\mathcal{I} = \oint_{\partial\mathcal{R}} \boldsymbol{\omega}_a b \cdot \hat{\mathbf{n}} d\mathcal{S} = b_2 \oint_{\partial\mathcal{R}} \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (37.44)$$

We can now use the divergence theorem to return to the volume integral, only now with  $b$  outside of the integral

$$\mathcal{I} = b_2 \int_{\mathcal{R}} \nabla \cdot \boldsymbol{\omega}_a dV = 0, \quad (37.45)$$

where  $\nabla \cdot \boldsymbol{\omega}_a = 0$  led to the final equality. Equivalently, we can use Stokes' theorem to convert the closed area integral,  $\oint_{\partial\mathcal{R}} \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S}$ , to a line integral around the boundary. However, there is no boundary for the closed area since it covers the sphere, thus again showing that  $\mathcal{I} = 0$  (see Section 2.7.5).

The remarkable identity (37.45) follows from kinematics alone since no dynamical information was used in its derivation. It says that there is zero integrated PV-substance contained within any region bounded solely by a single buoyancy surface. Hence, within the domain there is just as much positive PV-substance as there is negative PV-substance. So if PV changes locally within the domain, then somewhere else it must experience an oppositely signed change so to leave a net integrated value of zero. The result holds whether there are reversible or irreversible processes acting on the buoyancy surface. The only assumption is that the domain is fully enclosed by a  $b$ -surface.

### 37.4.2 Region bounded by two buoyancy surfaces

The identity (37.45) has a corollary, in which we consider a region bounded by two  $b$ -surfaces such as  $\mathcal{R}_{12}$  shown in the right panel of Figure 37.2. The above arguments hold for that region as well, since we can decompose the surface integral into two integrals separately over  $b_1$  and  $b_2$

$$\mathcal{I} = \int_{\mathcal{R}_{12}} \nabla \cdot (\boldsymbol{\omega}_a b) dV = \int_{\mathcal{R}_2} \nabla \cdot (\boldsymbol{\omega}_a b) dV - \int_{\mathcal{R}_1} \nabla \cdot (\boldsymbol{\omega}_a b) dV, \quad (37.46)$$

---

<sup>2</sup>Recall our discussion of extensive and intensive fluid properties in Section 15.3.1.

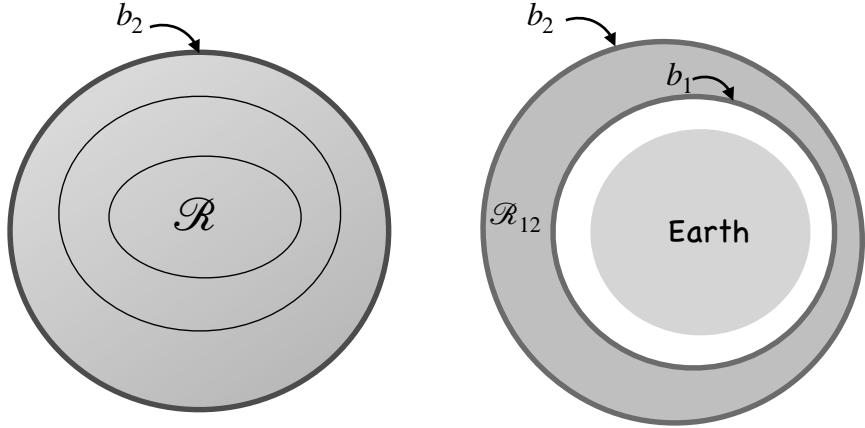


FIGURE 37.2: Integrating PV over regions bounded by potential temperature surfaces that do not intersect the ground. The left panel considers a single buoyancy surface,  $b = b_2$ , bounding the bubble-like fluid region  $\mathcal{R}$ . Notably, the region inside the bubble generally has nontrivial buoyancy distribution, as depicted here by exhibiting a couple of contours inside the  $b_2$ -bounded domain. The only assumption is that it is wholly contained inside the  $b = b_2$  contour. The right panel considers a buoyancy layer or shell,  $\mathcal{R}_{12}$ , bounded by two buoyancy isosurfaces,  $b_1 < b_2$ , surrounding the earth, with neither surface intersecting the ground. There is identically zero domain integrated PV in both  $\mathcal{R}$  and  $\mathcal{R}_{12}$ . Hence, if there is any nontrivial distribution of PV in either domain, there must be as much integrated positive values as there are negative.

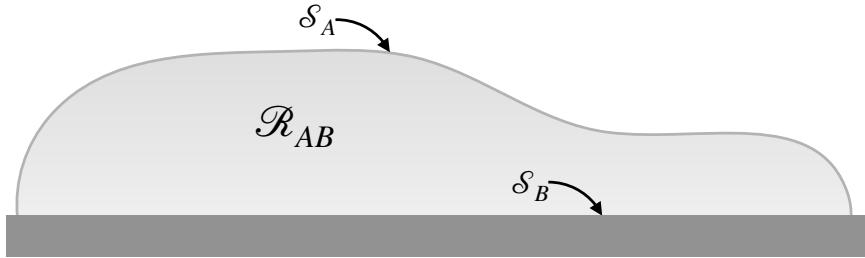


FIGURE 37.3: A fluid region,  $\mathcal{R}_{AB}$ , bounded by two surfaces,  $\mathcal{S}_A$  and  $\mathcal{S}_B$ . The upper surface  $\mathcal{S}_A$  is defined by a buoyancy isosurface,  $b = b_A$ , with this surface intersecting the ground. The lower surface,  $\mathcal{S}_B$ , is along the ground and has a buoyancy that is a function of space and time,  $b_B(\mathbf{x}, t)$ .

where the domain  $\mathcal{R}_1$  extends from the ground up to  $b_1$  and  $\mathcal{R}_2$  extends from the ground up to  $b_2$ . Integration over the region below  $b_1$  cancels through the subtraction. Indeed, the region below  $b_1$  could be anything without changing the result. So let that region be filled with fluid throughout (i.e., ignore the earth) to allow us to extend both integrals throughout the spherical region just like in the single isentrope domain  $\mathcal{R}$  in Figure 37.2. Invoking the single isentrope result we see that both integrals separately vanish. We are thus led to a vanishing integral for the layer

$$\mathcal{I} = \int_{\mathcal{R}_{12}} \nabla \cdot (\boldsymbol{\omega}_a b) dV = 0. \quad (37.47)$$

Again, the key assumption is that no buoyancy surface intersects land, in which case we are able to ignore the presence of land altogether and thus make use of the single isentrope result.

### 37.4.3 Region bounded by land and a buoyancy surface

Now consider a fluid domain bounded by a buoyancy surface that intersects the ground (atmospheric example) or ocean surface (ocean example), as shown in Figure 37.3. The integrated PV

is given by

$$\mathcal{I} = \int_{\mathcal{R}_{AB}} \nabla \cdot (\boldsymbol{\omega}_a b) dV \quad (37.48a)$$

$$= \int_{\mathcal{S}_A} \boldsymbol{\omega}_a b \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{\mathcal{S}_B} \boldsymbol{\omega}_a b \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (37.48b)$$

$$= b_A \int_{\mathcal{S}_A} \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{\mathcal{S}_B} b_B \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (37.48c)$$

$$= b_A \left[ \int_{\mathcal{S}_A} \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{\mathcal{S}_B} \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} \right] + \int_{\mathcal{S}_B} (b_B - b_A) \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (37.48d)$$

$$= b_A \int_{\mathcal{R}_{AB}} \nabla \cdot \boldsymbol{\omega}_a dV + \int_{\mathcal{S}_B} (b_B - b_A) \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (37.48e)$$

$$= \int_{\mathcal{S}_B} (b_B - b_A) \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (37.48f)$$

where we made use  $\nabla \cdot \boldsymbol{\omega}_a = 0$  to reach the final equality. As both the ground and the ocean surface have buoyancy gradients, they contribute to the PV substance within the region they bound.

#### 37.4.4 An ocean layer that outcrops

Figure 37.4 depicts a buoyancy layer in the ocean that outcrops at the ocean surface at both of its ends. Following the derivation in Section 37.4.3 we have the following integrated PV contents

$$\mathcal{I}_A \equiv \int_{\mathcal{S}_A} b \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{\mathcal{S}_1 + \mathcal{S}_2 + \mathcal{S}_3} b \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\mathcal{S}_1 + \mathcal{S}_2 + \mathcal{S}_3} (b - b_A) \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (37.49a)$$

$$\mathcal{I}_B \equiv \int_{\mathcal{S}_B} b \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{\mathcal{S}_2} b \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\mathcal{S}_2} (b - b_B) \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (37.49b)$$

Taking the difference in the integrals leads to the integrated PV within the layer  $\mathcal{R}_{AB}$

$$\mathcal{I}_{AB} \equiv \int_{\mathcal{R}_{AB}} \nabla \cdot (\boldsymbol{\omega}_a b) dV \quad (37.50a)$$

$$= \mathcal{I}_A - \mathcal{I}_B \quad (37.50b)$$

$$= \int_{\mathcal{S}_1} (b - b_A) \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} + (b_B - b_A) \int_{\mathcal{S}_2} \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{\mathcal{S}_3} (b - b_A) \boldsymbol{\omega}_a \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (37.50c)$$

## 37.5 Layer integrated PV budget

In Section 37.4 we developed expressions for the PV-substance integrated over a selection of volumes determined by buoyancy surfaces. That discussion illustrated how the volume integrated potential vorticity has contributions only from boundaries; e.g., where an atmospheric region intersects the ground or ocean, and where an oceanic region intersects the ground or the atmosphere. In this section we further illustrate implications of the impermeability theorem of Section 37.2 by considering a buoyancy (isopycnal) layer within the ocean that intersects the bottom on one side and the atmosphere on the other (Figure 37.5). This discussion aims to expose the physical processes affecting changes to the PV-substance within the layer by unpacking the boundary fluxes.

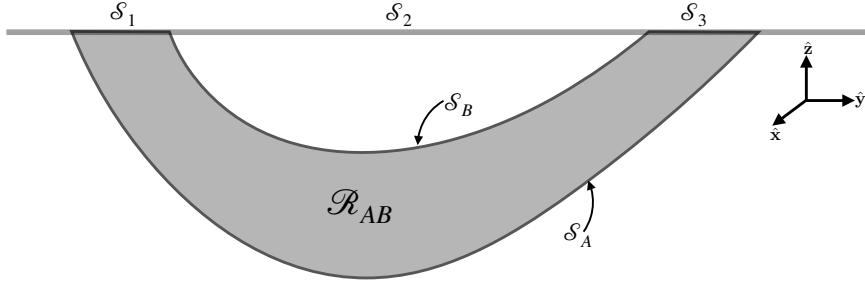


FIGURE 37.4: This figure depicts a buoyancy layer in the ocean that outcrops at both ends of the layer. The bounds the regions are given by the following surfaces. Surfaces  $S_A$  and  $S_B$  are defined by buoyancy isosurfaces with  $b_A < b_B$ . The sea surface is decomposed into three regions,  $S_1$ ,  $S_2$ , and  $S_3$  according to the outcrop locations of  $S_A$  and  $S_B$ .

An isopycnal layer generally moves as it expands and contracts due to both reversible and irreversible processes (waves, currents, mixing). The impermeability theorem means that the total potential vorticity substance for the layer changes only through exchanges at the bottom (boundary between the solid earth and ocean) and air-sea boundaries. Removing interior interfaces from the layer PV budget simplifies the budget analysis, as already revealed in Section 37.4. As per the discussion of Section 37.3, the results in this section apply even when there is no materially invariant potential vorticity. All we require is an Eulerian flux-form budget.

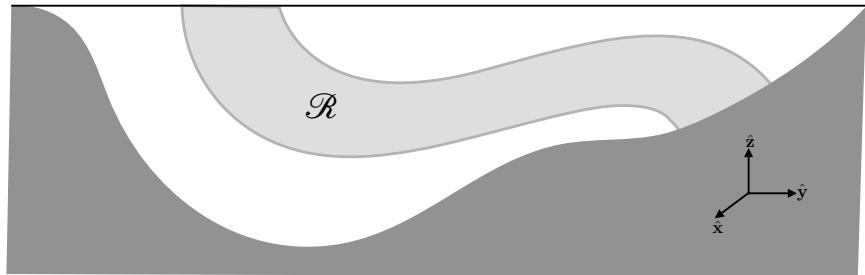


FIGURE 37.5: An isopycnal layer of seawater denoted by  $\mathcal{R}$ , with the layer intersecting bottom topography on one side and the atmosphere on the other.

### 37.5.1 Layer integrated budget

In addition to waves, currents, mixing, and sources affecting the layer interfaces, there is movement of the intersection of the layer with the side boundaries, thus changing the vertical and horizontal extents of these intersections. As a general formulation framework, we derive the isopycnal layer PV budget making use of the Leibniz-Reynolds transport theorem derived in Section 15.3.4. Just as for the layer integrated tracer budget considered in Section 15.5, applying Leibniz-Reynolds to the layer integrated PV budget renders

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho Q dV \right] = \int_{\mathcal{R}} \left[ \frac{\partial(\rho Q)}{\partial t} + \nabla \cdot (\rho Q \dot{x}) \right] dV, \quad (37.51)$$

where  $\mathcal{R}$  is the domain defined by the layer and

$$\dot{x} = \frac{dx}{dt} \quad (37.52)$$

is the velocity for a point on the layer boundary. Making use of the PV equation,  $\partial(\rho Q)/\partial t = -\nabla \cdot \mathbf{J}_Q$ , and the divergence theorem renders

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho Q dV \right] = \int_{\mathcal{R}} \nabla \cdot (-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}) dV = \int_{\partial \mathcal{R}} (-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (37.53)$$

This result holds around the full domain boundary. Now we decompose that boundary into portions defined by isopycnal layer interfaces and those along the air-sea and land-sea boundaries.

### 37.5.2 Impermeability across interior layer interfaces

Rather than invoking the impermeability theorem derived in Section 37.2, we rederive it within the present context to further our confidence in its validity. We thus consider the following for interior layer interfaces, here making use of the Haynes-McIntyre form of the PV flux vector (37.1)

$$[-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}] \cdot \hat{\mathbf{n}} = [\rho Q (\dot{\mathbf{x}} - \mathbf{v}) + \dot{b} \boldsymbol{\omega}_a - \nabla b \times \mathbf{F}] \cdot \hat{\mathbf{n}} \quad (37.54a)$$

$$= [(\boldsymbol{\omega}_a \cdot \nabla b) (\dot{\mathbf{x}} - \mathbf{v}) + \dot{b} \boldsymbol{\omega}_a] \cdot \hat{\mathbf{n}} \quad (37.54b)$$

$$= [(\boldsymbol{\omega}_a \cdot \nabla b) (\dot{\mathbf{x}} - \mathbf{v}) + (\partial b / \partial t + \mathbf{v} \cdot \nabla b) \boldsymbol{\omega}_a] \cdot \hat{\mathbf{n}} \quad (37.54c)$$

$$= [(\boldsymbol{\omega}_a \cdot \nabla b) \dot{\mathbf{x}} + (\partial b / \partial t) \boldsymbol{\omega}_a] \cdot \hat{\mathbf{n}}, \quad (37.54d)$$

where

$$\hat{\mathbf{n}} = \frac{\nabla b}{|\nabla b|} \quad (37.55)$$

is the outward normal direction pointing to regions of higher buoyancy. Now recall that the velocity of a point fixed on an isopycnal interface has a normal component that satisfies equation (37.9) (here applied to isopycnals)

$$\dot{\mathbf{x}} \cdot \hat{\mathbf{n}} = -\frac{\partial b / \partial t}{|\nabla b|}. \quad (37.56)$$

This result then leads to the impermeability statement for isopycnal interfaces in the fluid interior

$$(-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}) \cdot \hat{\mathbf{n}} = 0. \quad (37.57)$$

We thus conclude that changes to the layer integrated PV occur only via transfer across the land-sea boundary and the air-sea boundary

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho Q dV \right] = \int_{\text{land-sea}} [-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}] \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{\text{air-sea}} [-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}] \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (37.58)$$

### 37.5.3 PV flux at the land-sea boundary

We here evaluate the PV flux from equation (37.5a) at the land-sea boundary

$$-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}} = \rho Q (\dot{\mathbf{x}} - \mathbf{v}) + \dot{b} \boldsymbol{\omega}_a + \nabla b \times \mathbf{F}. \quad (37.59)$$

At a solid boundary, the no-normal flow boundary condition means that  $\hat{\mathbf{n}} \cdot \mathbf{v} = 0$ . Likewise, the velocity of a point along the boundary moves along the tangent to the boundary so that  $\dot{\mathbf{x}} \cdot \hat{\mathbf{n}} = 0$ . The bottom boundary condition is thus affected just by irreversible processes

$$(-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}) \cdot \hat{\mathbf{n}} = (\dot{b} \boldsymbol{\omega}_a + \nabla b \times \mathbf{F}) \cdot \hat{\mathbf{n}}. \quad (37.60)$$

In many parts of the ocean, geothermal heating is negligible so that there is no buoyancy input at the bottom, thus leaving just the contribution from friction

$$\text{no geothermal heating} \implies (-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}) \cdot \hat{\mathbf{n}} = (\nabla b \times \mathbf{F}) \cdot \hat{\mathbf{n}} = (\hat{\mathbf{n}} \times \nabla b) \cdot \mathbf{F}. \quad (37.61)$$

Furthermore, in the absence of geothermal heating the buoyancy satisfies a no-flux boundary condition, which can be ensured by having the buoyancy field maintaining

$$\text{no geothermal heating} \implies \hat{\mathbf{n}} \cdot \nabla b = 0. \quad (37.62)$$

Buoyancy isolines thus intersect the bottom parallel to the bottom outward normal, as shown in Figure 37.6. Correspondingly,  $(\hat{\mathbf{n}} \times \nabla b) \cdot \mathbf{F}$  projects out that component of the friction vector pointing parallel to the bottom with constant geopotential,  $z$ . Assuming buoyancy increases upward along the sloping bottom, as per a stably stratified bottom fluid, then  $\hat{\mathbf{n}} \times \nabla b$  points clockwise around bowls and counter-clockwise around bumps (see Figure 37.6).

Within the bottom boundary layer, quadratic bottom drag is a common parameterization of the acceleration associated with turbulent frictional processes

$$\mathbf{F} = -C_d |\mathbf{u}| \mathbf{u}, \quad (37.63)$$

where  $C_d$  is a non-dimensional drag coefficient and  $\mathbf{u}$  is the horizontal velocity. In this case the boundary condition for PV takes the form

$$(\nabla b \times \mathbf{F}) \cdot \hat{\mathbf{n}} = -C_d |\mathbf{u}| (\hat{\mathbf{n}} \times \nabla b) \cdot \mathbf{u}. \quad (37.64)$$

This boundary flux provides a positive PV source in cases where the bottom boundary layer flow is clockwise around abyssal hills and counter-clockwise around abyssal bowls, and conversely for oppositely oriented flow. In contrast, bottom flows that are parallel to  $\nabla b$  (i.e., flows that are orthogonal to buoyancy isosurfaces at the bottom boundary) provide a zero source for PV since  $\nabla b \times \mathbf{F} = 0$ . This result is expected from the discussion in Section 36.4 and Figure 36.3, where we note that friction changes PV by rotating buoyancy surfaces, with that rotation realized only when friction is not aligned with  $\nabla b$ .

#### 37.5.4 PV flux at the air-sea boundary

We make use of the kinematic boundary condition derived in Section 14.4.3 for the permeable air-sea boundary, where the boundary condition (14.63) leads to

$$\rho \hat{\mathbf{n}} \cdot (\dot{\mathbf{x}} - \mathbf{v}) = \mathcal{Q}_m \quad \text{air-sea boundary} \quad (37.65)$$

with  $\mathcal{Q}_m$  the mass per time per surface area crossing the boundary. We are thus led to the air-sea boundary condition

$$(-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}) \cdot \hat{\mathbf{n}} = Q \mathcal{Q}_m + (\dot{b} \boldsymbol{\omega}_a + \nabla b \times \mathbf{F}) \cdot \hat{\mathbf{n}}. \quad (37.66)$$

Besides the irreversible processes, PV is affected at the air-sea interface by the transfer of matter across the boundary via the term  $Q \mathcal{Q}_m$ . We can think of this term as an advection of PV across the boundary via the boundary mass transport. Note that we might choose to approximate the sea surface as nearly flat, so that

$$\hat{\mathbf{n}} \approx \hat{\mathbf{z}}, \quad (37.67)$$

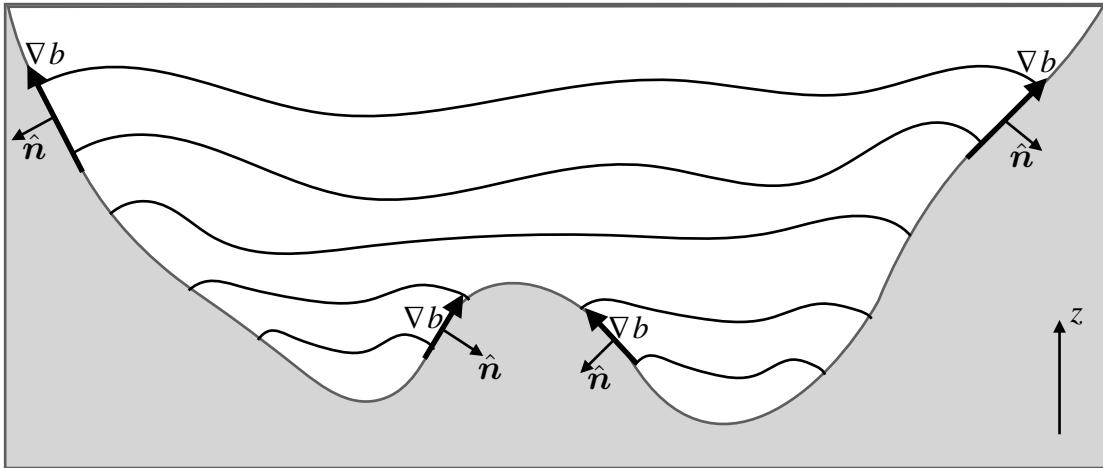


FIGURE 37.6: Buoyancy isosurfaces that intersect the bottom. As discussed in Section 15.5 and depicted in Figure 15.5, in the absence of geothermal heating, a buoyancy isosurface satisfies the no-normal flux bottom boundary condition,  $\hat{\mathbf{n}} \cdot \nabla b = 0$ . This boundary condition requires buoyancy isosurfaces to be orthogonal to the bottom. Assuming buoyancy increases upward along the sloping bottom, then  $\hat{\mathbf{n}} \times \nabla b$  points clockwise around bowls and counter-clockwise around bumps (when viewed from above). This structure for the buoyancy surfaces affects how friction impacts on the layer-integrated PV budget, with details provided in Section 37.5.3.

in which case

$$(-\mathbf{J}_Q + \rho Q \dot{\mathbf{x}}) \cdot \hat{\mathbf{n}} \approx Q \mathcal{Q}_m + \dot{b}(\zeta + f) + (\nabla b \times \mathbf{F}) \cdot \hat{\mathbf{z}}. \quad (37.68)$$

The buoyancy source term appears multiplied by the vertical component to the absolute vorticity, so that modifications to PV appear in proportion to the sign of both  $\dot{b}$  and  $\zeta + f$ . We think of this term as acting to stretch/compress the fluid column so to alter vorticity and hence PV. The friction source arises from the mis-alignment of the horizontal friction vector and the horizontal buoyancy gradient, thus acting like a torque to spin the fluid analogous to the action from baroclinicity described in Section 35.5.

### 37.5.5 Thought experiments

The surface PV flux (37.68) provides an explicit expression for how surface boundary fluxes affect the PV budget within a buoyancy layer outcropping at the ocean surface. It contains a wealth of physics that can be explored via thought experiments.

#### *PV generation in a fluid with zero initial baroclinicity*

Consider a fluid region initially with zero baroclinicity and zero flow so that the initial PV is given by  $f N^2$ , with  $N^2$  the squared buoyancy frequency. The surface PV flux (37.68) creates PV via the mass flux term and through heating/cooling. If this term alone affected the PV, and it did so uniformly in space, then it would alter PV only via changes in the vertical stratification. More generally, both the mass term and the diabatic term create horizontal buoyancy gradients, which then generate currents and vorticity that generate further contributions to the PV flux.

#### *PV generation in a fluid that is initially homogeneous*

Consider an initially homogenous box of seawater with zero PV. In this case it is only the buoyancy term,  $\dot{b} f$ , that contributes to initial changes in PV. Northern hemisphere ( $f > 0$ ) surface cooling ( $\dot{b} < 0$ ) adds negative PV to the box. Cooling also initiates gravitational instability that mixes the water and in turn spreads the negative PV boundary source throughout the fluid. Cooling

adds structure to the buoyancy field by inflating the formerly zero thickness buoyancy layers, with layer inflation originating from the boundary. Once inflated, the impermeability theorem dictates that the layer integrated PV-substance changes only via boundary interactions, whereas stirring and mixing transport PV into the fluid interior. Notably, a region with  $f Q < 0$  is locally unstable to symmetric instability, with the generated symmetric instability acting to locally bring the flow towards a zero PV state. However, the constraints from impermeability mean that the net PV-substance remains unchanged within a buoyancy layer, even in the presence of mixing.

### 37.5.6 Is there a preferred form of the PV-substance flux?

Analysis in this section made use of the Haynes-McIntyre form of the PV-substance flux (equation (37.1))

$$\mathbf{J}_Q = \rho \mathbf{v} Q - \dot{b} \boldsymbol{\omega}_a + \nabla b \times \mathbf{F}. \quad (37.69)$$

We could have instead chosen to work with the Marshall form (equation (37.35))

$$\mathbf{J}_Q^{\text{marshall}} = - \left[ \frac{\partial \mathbf{v}}{\partial t} + \nabla(m + p/\rho) \right] \times \nabla b - \boldsymbol{\omega}_a \frac{\partial b}{\partial t}, \quad (37.70)$$

or the modified kinematic form (equation (37.17))

$$\tilde{\mathbf{J}}_Q^{\text{kin}} = - \frac{\partial \mathbf{v}_a}{\partial t} \times \nabla \theta - \boldsymbol{\omega}_a \frac{\partial \theta}{\partial t}. \quad (37.71)$$

These fluxes differ by a gauge choice and yet they each satisfy the impermeability theorem. Subjective choices determine which one is preferred. Importantly, once chosen, we can use only a single form of the flux throughout the budget analysis in order to remain self-consistent.

The PV-substance budget, though invariant to the choice of flux, has distinct physical pictures depending on the choice of the flux. As a particularly clear example consider a steady state budget in which the fluxes take the form

$$\mathbf{J}_Q = \rho \mathbf{v} Q - (\mathbf{v} \cdot \nabla b) \boldsymbol{\omega}_a + \nabla b \times \mathbf{F} \quad (37.72)$$

$$\mathbf{J}_Q^{\text{marshall}} = -\nabla(m + p/\rho) \times \nabla b \quad (37.73)$$

$$\tilde{\mathbf{J}}_Q^{\text{kin}} = 0. \quad (37.74)$$

The physical picture for  $\tilde{\mathbf{J}}_Q^{\text{kin}}$  is rather trivial, whereby the PV-substance stays constant within buoyancy layers and there are zero PV-substance fluxes across *all* boundaries of the layer. In contrast, a steady state budget when working with  $\mathbf{J}_Q$  or  $\mathbf{J}_Q^{\text{marshall}}$  afford a physical picture of PV-substance entering, leaving, and transported through the buoyancy layers. [Marshall et al. \(2001\)](#) developed a rather elegant analysis framework using  $\mathbf{J}_Q^{\text{marshall}}$  for steady budgets, and we explore facets of that approach in Section 36.5 for the special case of a Boussinesq hydrostatic fluid.

Nevertheless, our use of the Haynes-McIntyre PV-substance flux in the present section is motivated by its utility for describing how boundary forcing can change the sign of the PV. Such forcing exposes the flow to a variety of local instabilities (e.g., symmetric, centrifugal, gravitational). [Thomas et al. \(2008\)](#) offer a pedagogical review for the ocean; [Thomas et al. \(2013\)](#) provides a thorough study of the upper reaches of the Gulf Stream; and [Naveira Garabato et al. \(2019\)](#) provide evidence for such boundary forcing in regions of strong abyssal flows. Each of these studies points to the need to further understand details of the boundary PV flux and to furthermore ensure it is properly formulated within numerical models (e.g., [Hallberg and Rhines \(1996\)](#)).





## **Part VII**

### **Nearly geostrophic balanced flows**

Fluid motion dominated by rotation is characterized by a small Rossby number. To zeroth order in an asymptotic expansion in Rossby number, the flow maintains geostrophic balance, which is a balance between the Coriolis acceleration and pressure gradient acceleration. As seen in Chapter 25, the geostrophic balance is diagnostic so that it offers no means to compute the time evolution of the fluid. To obtain a prognostic equation requires going to next order in Rossby number within the asymptotic expansion. The resulting prognostic equation makes use of ageostrophic motions, though only as an intermediate step towards an evolution equation involving just zeroth order geostrophically balanced fields.

The nuts and bolts of this part of the book involve methods of scaling analysis and asymptotic analysis via perturbation series. In Chapter 38, we use these tools to derive equations for planetary geostrophy (PG) and quasi-geostrophy (QG) within the shallow water system, and then PG and QG for continuously stratified flows in Chapters 39 and 40 . PG and QG are useful theoretical models lending insights into ocean and atmosphere fluid mechanics. In particular, PG is commonly used to study features of the large-scale laminar ocean circulation, and QG is ubiquitous in studies of both oceanic and atmospheric flows at or near the deformation radius.

# Chapter 38

## Shallow water planetary and quasi-geostrophy

In this chapter we develop the mechanical equations for planetary geostrophy (PG) and quasi-geostrophy (QG) within the shallow water fluid. The derivations require elements from dimensional analysis and asymptotic methods. Salient details are introduced and the many mathematical steps exposed.

### READER'S GUIDE FOR THIS CHAPTER

This chapter is largely technical in nature, aiming to provide the necessary tools from dimensional analysis, scale analysis, and asymptotic methods to derive approximate geostrophic equations. We assume an understanding of the equations for a single layer of shallow water fluid as derived in Chapter 30. We follow this work with further studies of the continuously stratified systems in Chapters 39 and 40.

38.1	Loose threads . . . . .	950
38.2	Scaling analysis and the Buckingham-II theorem . . . . .	950
38.3	Shallow water equations . . . . .	950
38.3.1	Dimensional scales . . . . .	951
38.3.2	Physical dimensions . . . . .	952
38.3.3	Number of non-dimensional parameters . . . . .	952
38.3.4	Choosing the non-dimensional parameters . . . . .	952
38.3.5	Assumed values for the non-dimensional parameters . . . . .	954
38.3.6	Deformation radius and the free surface undulation scale . . . . .	955
38.3.7	Non-dimensional shallow water equations . . . . .	956
38.4	Shallow water planetary geostrophy . . . . .	957
38.5	Shallow water quasi-geostrophy . . . . .	958
38.5.1	Quasi-geostrophic scaling . . . . .	958
38.5.2	Outlining the asymptotic method . . . . .	959
38.5.3	Order $\text{Ro}^0$ asymptotic equations . . . . .	961
38.5.4	Order $\text{Ro}^1$ asymptotic equations . . . . .	961
38.6	Physical elements of the theory . . . . .	963
38.6.1	Dimensional potential vorticity and streamfunction . . . . .	963
38.6.2	Contributions to the QG potential vorticity . . . . .	964
38.6.3	Summarizing the equations of quasi-geostrophy . . . . .	965
38.6.4	Connecting quasi-geostrophic PV to shallow water PV . . . . .	966
38.6.5	Considering topography to be $\mathcal{O}(\text{Ro}^0)$ . . . . .	967
38.6.6	Two layer quasi-geostrophy . . . . .	967
38.7	Exercises . . . . .	968

## 38.1 Loose threads

- External and internal modes for QG two layers in Section 38.6.6.

## 38.2 Scaling analysis and the Buckingham-II theorem

Scale analysis is ubiquitous in physics, with the Buckingham-II theorem providing a useful framework. The theorem states that the number of dimensionless parameters in a physical system is a function of the number of dimensional parameters or scales  $K$  (e.g., scales for the velocity, rotation rate, pressure force, friction force, gravitational acceleration) and the number of physical dimensions  $R$  (e.g., time, length, mass). Precisely, Buckingham-II states that the number of dimensionless parameters is

$$N_{\text{dimensionless}} = K - R. \quad (38.1)$$

Different physical systems possessing the same suite of dimensionless parameters are isomorphic. For example, a laboratory study of flow around a cylinder contains two dimensionless parameters: the drag coefficient,  $C_d$ , and the Reynolds number,  $\text{Re}$ . If the problem is scaled up to a building with the same shape, then so long as the values for the dimensionless parameters are the same (e.g., same drag coefficient and same Reynolds number), one can make use of the laboratory analog for determining suitability of the building architecture. Similar isomorphisms exist between flows in a rotating tank and flows in the ocean and atmosphere.

The Buckingham-II theorem does not provide the form of the dimensionless parameters. Nor does the theorem determine their values. This information comes only after introducing physical prejudices surrounding a regime of chosen interest. Additionally, Buckingham-II does not offer information about how the dimensionless parameters might be related. Instead, any such relations are derived from the mechanical and thermodynamical equations describing the system.

We focus in this chapter on the regime of large-scale atmospheric and oceanic flow where the shallow water fluid is close to geostrophic balance. That choice then guides the length and time scales, which in turn determines the size of the dimensionless parameters. In many cases, one is able to identify dimensionless parameters that are large or small in particular regimes, which in turn suggests asymptotic analyses to render equations specific to the regime of interest.

## 38.3 Shallow water equations

A single-layer of inviscid shallow water fluid of thickness  $h$  is governed by the velocity and thickness equations (Chapter 30)

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} + \mathbf{f} \times \mathbf{u} = -g \nabla \eta \quad (38.2a)$$

$$\frac{\partial h}{\partial t} + \nabla \cdot (h \mathbf{u}) = 0, \quad (38.2b)$$

where  $\mathbf{u}$  is the horizontal velocity that is independent of depth within the layer. The geometry of the layer is specified by the free surface height,  $z = \eta(x, y, t)$ , and bottom topography,  $z = \eta_b(x, y)$  (see Figure 30.1). They are related according to

$$\eta = \eta_b + h = H + \bar{\eta}_b + \Delta\eta = \bar{h} + \bar{\eta}_b + \Delta\eta, \quad (38.3)$$

where  $H = \bar{h}$  is the area average layer thickness,  $\bar{\eta}_b$  is the area average of the bottom topography,  $\Delta\eta = \eta - \bar{\eta}$  is the deviation of the surface height from its area average  $\bar{\eta} = \bar{\eta}_b + H$ . We also find occasion to write the layer thickness in the form

$$h = \eta - \eta_b = H + (\bar{\eta}_b - \eta_b) + \Delta\eta = \bar{h} - \Delta\eta_b + \Delta\eta = \bar{h} + \Delta h, \quad (38.4)$$

where  $\Delta\eta_b = \eta_b - \bar{\eta}_b$  is the deviation of the bottom topography from its area mean, and we introduced the thickness deviation from the area mean

$$\Delta h = h - \bar{h} = \Delta\eta - \Delta\eta_b. \quad (38.5)$$

Dexterity with these geometrical relations is assumed in the following.

### 38.3.1 Dimensional scales

We identify nine dimensional parameters for the shallow water system.

- LENGTH SCALES

- ★  $H$  = depth scale of the fluid, which we take equal to the area average layer thickness (see Figure 30.1).
- ★  $L$  = horizontal/lateral length scale of motions under consideration. We assume both horizontal directions to have the same length scale. This assumption is not necessarily valid on a rotating planet, where flows in the zonal (east-west) direction can have length scales longer than meridional (north-south) flow scales. Nonetheless, this choice does not preclude the dynamical emergence of anisotropic length scales.
- ★  $R$  = radius of the planet. We include this scale anticipating that for length scales small compared to the earth's radius, the Coriolis parameter may be approximated by a constant ( $f$ -plane) or linear function of latitude ( $\beta$ -plane).
- ★  $\mathcal{H}$  = scale for deviations of the free surface height,  $\eta$ , relative to its area average,  $\bar{\eta}$ , so that  $\Delta\eta = \eta - \bar{\eta} \sim \mathcal{H}$ .
- ★  $\mathcal{B}$  = scale for deviations of the bottom topography,  $\eta_b$ , relative to its area average,  $\bar{\eta}_b$ , so that  $\Delta\eta_b = \eta_b - \bar{\eta}_b \sim \mathcal{B}$ .

- VELOCITY SCALES

- ★  $U$  = velocity scale for horizontal fluid particle motion; i.e., the speed for horizontal currents or winds.
- ★  $c$  = wave speed scale. For the shallow water model, the wave speed scale is given by the shallow water gravity wave (Section 31.8.3)

$$c = \sqrt{g H}. \quad (38.6)$$

We introduce the wave speed anticipating the presence of distinct flow regimes depending on whether the fluid particle speed is larger or smaller than the wave speed. The ratio of the wave speed to particle speed is known as the *Froude number* (Section 38.3.4).

- BODY FORCES: There are two body forces acting on the fluid; one from gravity and one from Coriolis.

- ★  $g$  = gravitational acceleration.
- ★  $f$  = Coriolis frequency.

If we were interested in other forces, such as electromagnetic or frictional forces, then we would have other dimensional parameters corresponding to these forces.

### 38.3.2 Physical dimensions

There are two physical dimensions in the shallow water system: length,  $L$ , and time,  $T$ . Notably, there is no mass in the shallow water system. The reason is that the fluid density is assumed uniform within a shallow water layer so that mass is described by area times thickness

$$M = \int \rho dV [\equiv] L^2 H \rho, \quad (38.7)$$

where  $[\equiv]$  is read “has dimensions”.

### 38.3.3 Number of non-dimensional parameters

The Buckingham-II theorem then says there are

$$N_{\text{dimensionless}} = 9 - 2 = 7 \quad (38.8)$$

non-dimensional parameters. What if we incorrectly count the physical dimensions or the dimensional scales/parameters? Fortunately, the process of determining the non-dimensional parameters is largely self-correcting. Namely, in the process of non-dimensionalizing the shallow water equations, the seven non-dimensional parameters arise as part of the analysis. Hence, making use of Buckingham-II is useful but it is not essential. If one left out a physical dimension or a physical parameter, then it would appear somewhere in the subsequent analysis, often not until near the end where something mathematically or physically inconsistent appears. One must always be cognizant of the need to self-correct when performing dimensional analysis.

### 38.3.4 Choosing the non-dimensional parameters

There is no unique choice for the non-dimensional parameters. Our choice is guided by experience, interest, and what parameters might be available to experimental control or measurement.

1. VERTICAL TO HORIZONTAL/LATERAL ASPECT RATIO: The ratio of the vertical scale to the horizontal/lateral<sup>1</sup> scale defines the aspect ratio

$$\delta_{\text{vertical/horizontal}} = \frac{\text{vertical depth scale}}{\text{horizontal length scale}} = \frac{H}{L}. \quad (38.9)$$

2. RATIO OF HORIZONTAL/LATERAL SCALE TO PLANETARY SCALE: The ratio of the lateral length scale to the planet radius is

$$\delta_{\text{horizontal/planet}} = \frac{\text{lateral length scale}}{\text{planetary length scale}} = \frac{L}{R}. \quad (38.10)$$

---

<sup>1</sup>The terms “lateral” and “horizontal” are used interchangeably, referring to motion at constant vertical position either on the sphere or on the plane.

3. RATIO OF FREE SURFACE UNDULATION TO DEPTH SCALE: The ratio of the free surface undulation scale to the vertical depth scale is

$$\delta_{\text{free surface/depth}} = \frac{\text{free surface undulation scale}}{\text{vertical depth scale}} = \frac{\mathcal{H}}{H}. \quad (38.11)$$

4. RATIO OF BOTTOM TOPOGRAPHY UNDULATION TO DEPTH: The ratio of the bottom topography undulation scale to the vertical depth scale is

$$\delta_{\text{bottom/depth}} = \frac{\text{bottom topography undulation scale}}{\text{vertical depth scale}} = \frac{\mathcal{B}}{H}. \quad (38.12)$$

5. FROUDE NUMBER: The Froude number is the ratio of the fluid particle speed to the wave speed. For the shallow water system, this ratio is

$$\text{Fr} = \frac{U}{c} = \frac{U}{\sqrt{g H}}. \quad (38.13)$$

6. ROSSBY NUMBER: The Rossby number is the ratio of the fluid particle acceleration scale to the Coriolis acceleration

$$\text{Ro} = \frac{\text{particle acceleration}}{\text{Coriolis acceleration}}. \quad (38.14)$$

The particle acceleration scale is determined by the local time tendency plus advection

$$\text{particle acceleration} = \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \sim \frac{U}{T} + \frac{U^2}{L}. \quad (38.15)$$

The local time tendency and advection generally have distinct scales, thus leading to the potential for two Rossby numbers

$$\text{Ro}^{\text{local}} = \frac{1}{T f} \quad \text{and} \quad \text{Ro}^{\text{adv}} = \frac{U}{L f}. \quad (38.16)$$

In the following we consider these two Rossby numbers to have the same order, which is realized by advective contributions to material time evolution being comparable to local time changes. We refer to this choice as an *advection time scale*, whereby

$$T = \frac{L}{U} \implies \frac{U^2}{L} = \frac{U}{T}, \quad (38.17)$$

so that there is only one Rossby number

$$\text{Ro} = \frac{1}{f T} = \frac{U}{f L}. \quad (38.18)$$

Another interpretation for the Rossby number is the ratio of the relative vorticity to the planetary vorticity

$$\text{Ro} = \frac{\text{relative vorticity}}{\text{planetary vorticity}} \quad (38.19)$$

With the relative vorticity scaling as  $U/L$  and the planetary vorticity scaling as  $f$ , we recover the expression (38.18) for the Rossby number.

7. GEOSTROPHIC NUMBER: We define the geostrophic number as the ratio of the Coriolis

acceleration to the pressure gradient acceleration

$$Ge = \frac{\text{Coriolis acceleration}}{\text{pressure gradient acceleration}}. \quad (38.20)$$

The Coriolis acceleration scales as

$$\text{Coriolis acceleration} \sim f U \quad (38.21)$$

whereas the pressure gradient acceleration,  $-g \nabla \eta$ , scales as

$$\text{pressure gradient acceleration} \sim \frac{g \mathcal{H}}{L}, \quad (38.22)$$

so that

$$Ge = \frac{\text{Coriolis acceleration}}{\text{pressure gradient acceleration}} = \frac{f U}{(g/L) \mathcal{H}}. \quad (38.23)$$

### 38.3.5 Assumed values for the non-dimensional parameters

We now enumerate the assumed values for the non-dimensional parameters.

1. SMALL VERTICAL TO HORIZONTAL ASPECT RATIO: The aspect ratio is generally small for large-scale atmospheric and oceanic fluid systems

$$\delta_{\text{vertical/horizontal}} = H/L \ll 1. \quad (38.24)$$

This assumption was made when formulating the shallow water system, which is based on hydrostatic balance (see Section 30.2). We thus retain this assumption as we further scale the shallow water system.

2. SMALL OR ORDER ONE RATIO OF HORIZONTAL/LATERAL TO PLANETARY SCALES: The ratio of the lateral length scale to the planet radius is small for quasi-geostrophic systems and order unity for planetary geostrophy

$$\delta_{\text{horizontal/planet}} = L/R \ll 1 \quad \text{quasi-geostrophy} \quad (38.25a)$$

$$\delta_{\text{horizontal/planet}} = L/R \sim 1 \quad \text{planetary geostrophy}. \quad (38.25b)$$

3. RATIO OF FREE SURFACE UNDULATION TO DEPTH: The ratio  $\mathcal{H}/H$  is implied by assuming a unit geostrophic number below.

4. RATIO OF BOTTOM TOPOGRAPHY UNDULATION TO DEPTH: For quasi-geostrophy, we assume that undulations in the bottom topography are small relative to the depth, whereas there is no restriction for planetary geostrophy. “Small” in the present context is determined by the Rossby number, in which case

$$\delta_{\text{bottom/depth}} = \mathcal{B}/H = Ro \quad \text{for quasi-geostrophy}. \quad (38.26)$$

5. FROUDE NUMBER: We find that the Froude number is implied by scales assumed for the other non-dimensional numbers.

6. SMALL ROSSBY NUMBER: The Rossby number is assumed small

$$Ro = U/(f L) \ll 1, \quad (38.27)$$

which means that the Coriolis acceleration is a leading order term in the horizontal velocity equation (38.2a).

7. UNIT GEOSTROPHIC NUMBER: The geostrophic number is assumed to be order unity

$$\text{Ge} \sim 1. \quad (38.28)$$

This assumption means that the Coriolis acceleration and pressure gradient acceleration scale together

$$f U \sim (g/L) \mathcal{H}. \quad (38.29)$$

Making use of the velocity equation (38.2a), we see that this scaling is consistent only so long as the Rossby number is small,  $\text{Ro} \ll 1$ . Furthermore, this scaling constrains the scale of the free surface undulation,  $\mathcal{H}$ , as we discuss in Section 38.3.6.

### 38.3.6 Deformation radius and the free surface undulation scale

We determine the scale for the free surface height undulation,  $\mathcal{H}$ , by making use of the assumed order unity geostrophy number. For this purpose, start from the geostrophic scaling of Coriolis and pressure gradient accelerations, (38.29), to express the free surface undulation scale according to

$$\Delta\eta \sim \mathcal{H} = \frac{f U L}{g} = \text{Ro} \frac{f^2 L^2}{g} = \text{Ro} H \frac{f^2 L^2}{g H} = \text{Ro} H \left[ \frac{L}{L_d} \right]^2. \quad (38.30)$$

In the final equality we introduced the *deformation radius*

$$L_d = f^{-1} \sqrt{g H}. \quad (38.31)$$

We previously encountered the deformation radius when discussing geostrophic adjustment in Section 34.7. In Section 38.6.2 we further discuss its role as a regime boundary (between relative vorticity and vortex stretching) for the quasi-geostrophic potential vorticity. The deformation radius decreases toward the poles, so that rotational effects are felt by smaller scales in the high latitudes than in the tropics.

We can use  $L_d$  to rewrite the Froude number as the ratio of the advection speed to the rotational speed

$$\text{Fr} = \frac{U}{\sqrt{g H}} = \frac{U}{f L_d} = \text{Ro} \frac{L}{L_d}. \quad (38.32)$$

Furthermore, the squared ratio of the deformation radius to the lateral length scale is termed the *Burger number*

$$\text{Bu} = \left[ \frac{L_d}{L} \right]^2. \quad (38.33)$$

Use of the Burger number allows us to write the Froude number in terms of the Rossby number and Burger number

$$\text{Fr} = \frac{\text{Ro}}{\sqrt{\text{Bu}}}. \quad (38.34)$$

Likewise, the free surface height undulation scale can be written

$$\mathcal{H} = H \text{Ro} \left[ \frac{L}{L_d} \right]^2 = H \frac{\text{Ro}}{\text{Bu}} = H \frac{\text{Fr}^2}{\text{Ro}}. \quad (38.35)$$

Hence, the ratio of the free surface undulations to the layer thickness (depth) scale is given by

$$\delta_{\text{free surface/depth}} = \frac{\mathcal{H}}{H} = \text{Ro} \left[ \frac{L}{L_d} \right]^2 = \frac{\text{Ro}}{\text{Bu}} = \frac{\text{Fr}^2}{\text{Ro}}. \quad (38.36)$$

Again, this scaling is implied by making the dynamical assumption of a unit geostrophic number, which means that the pressure gradient acceleration scales according to the Coriolis acceleration.

### 38.3.7 Non-dimensional shallow water equations

To non-dimensionalize the shallow water equations we introduce non-dimensional variables for space, time, velocity, and Coriolis parameter as adorned with a widehat<sup>2</sup>

$$t = T \widehat{t} \quad (x, y) = L (\widehat{x}, \widehat{y}) \quad \partial_t = \frac{\partial \widehat{t}}{T} \quad \nabla = \frac{\widehat{\nabla}}{L} \quad (u, v) = U (\widehat{u}, \widehat{v}) \quad f = f_0 \widehat{f}, \quad (38.37)$$

where  $f_0$  is the Coriolis parameter at the central latitude for the  $\beta$ -plane approximation (Section 22.3). We also require non-dimensional variables for the surface and bottom undulations

$$\Delta\eta = \mathcal{H} \widehat{\eta} \quad \Delta\eta_b = \mathcal{B} \widehat{\eta}_b \quad h = H + \Delta\eta - \Delta\eta_b = H + \mathcal{H} \widehat{\eta} - \mathcal{B} \widehat{\eta}_b, \quad (38.38)$$

where we used equation (38.4) for the layer thickness. Importantly, we assume that the non-dimensional variables (the widehat variables) are order unity.

#### *Non-dimensional velocity equation*

Introducing the above variables into the shallow water velocity equation (38.2a) renders

$$\frac{U}{T} \frac{\partial \widehat{\mathbf{u}}}{\partial \widehat{t}} + \frac{U^2}{L} (\widehat{\mathbf{u}} \cdot \widehat{\nabla}) \widehat{\mathbf{u}} + f_0 U (\widehat{\mathbf{f}} \times \widehat{\mathbf{u}}) = - \frac{g \mathcal{H}}{L} \widehat{\nabla} \widehat{\eta}. \quad (38.39)$$

As before, we assume the time scale is given by the advection time

$$T = \frac{L}{U} = \frac{1}{\text{Ro} f_0}, \quad (38.40)$$

so that dividing by  $f_0 U$  leads to

$$\text{Ro} \left[ \frac{\partial \widehat{\mathbf{u}}}{\partial \widehat{t}} + (\widehat{\mathbf{u}} \cdot \widehat{\nabla}) \widehat{\mathbf{u}} \right] + (\widehat{\mathbf{f}} \times \widehat{\mathbf{u}}) = - \left[ \frac{g H}{f_0 L U} \frac{\text{Ro}}{\text{Bu}} \right] \widehat{\nabla} \widehat{\eta}, \quad (38.41)$$

where we set  $\mathcal{H} = H (\text{Ro}/\text{Bu})$  according to equation (38.36). We reduce the factor on the right hand side according to

$$\frac{g H}{f_0 L U} \frac{\text{Ro}}{\text{Bu}} = \frac{g H}{f_0 L U} \frac{U}{f_0 L} \frac{L^2}{L_d^2} = \frac{g H}{f_0 L U} \frac{U}{f_0 L} \frac{L^2 f_0^2}{g H} = 1. \quad (38.42)$$

---

<sup>2</sup>The L<sup>A</sup>T<sub>E</sub>X widehat symbol is used for non-dimensional variables, such as the non-dimensional velocity,  $\widehat{\mathbf{u}}$ . The widehat is distinguished from the hat used for unit vectors, such as for the vertical unit vector,  $\widehat{\mathbf{z}}$ . We also use widehats for thickness weighted means in Chapter 45, but that usage is completely distinct from the non-dimensionalization usage in the present chapter.

Hence, the non-dimensional inviscid shallow water velocity equation takes on the rather elegant form

$$\text{Ro} \left[ \frac{\partial \hat{\mathbf{u}}}{\partial \hat{t}} + (\hat{\mathbf{u}} \cdot \hat{\nabla}) \hat{\mathbf{u}} \right] + \hat{\mathbf{f}} \times \hat{\mathbf{u}} = -\hat{\nabla} \hat{\eta}. \quad (38.43)$$

Introducing the non-dimensional material time derivative

$$\frac{D}{Dt} = \frac{\partial}{\partial \hat{t}} + \hat{\mathbf{u}} \cdot \hat{\nabla} \quad (38.44)$$

brings the velocity equation to

$$\text{Ro} \frac{D \hat{\mathbf{u}}}{Dt} + \hat{\mathbf{f}} \times \hat{\mathbf{u}} = -\hat{\nabla} \hat{\eta}. \quad (38.45)$$

We see that the velocity equation is consistent with a unit geostrophy number (i.e., Coriolis acceleration balances pressure gradient acceleration) if and only if the Rossby number is small, thus eliminating the material acceleration.

#### *Non-dimensional thickness equation*

The thickness (continuity) equation (38.2b) can be written

$$\frac{\partial \Delta \eta}{\partial t} + \nabla \cdot [(H + \Delta \eta - \Delta \eta_b) \mathbf{u}] = 0, \quad (38.46)$$

which takes on the non-dimensional form

$$\frac{\mathcal{H}}{T} \frac{\partial \hat{\eta}}{\partial \hat{t}} + \frac{U H}{L} \hat{\nabla} \cdot [(1 + \hat{\eta} \mathcal{H}/H - \hat{\eta}_b \mathcal{B}/H) \hat{\mathbf{u}}] = 0. \quad (38.47)$$

The advective time scaling  $T = L/U$  brings the thickness equation to

$$\frac{\mathcal{H}}{H} \frac{\partial \hat{\eta}}{\partial \hat{t}} + \hat{\nabla} \cdot [(1 + \hat{\eta} \mathcal{H}/H - \hat{\eta}_b \mathcal{B}/H) \hat{\mathbf{u}}] = 0. \quad (38.48)$$

## 38.4 Shallow water planetary geostrophy

We make use of the non-dimensional equations derived in Section 38.3.7 to derive the dynamical equations for planetary geostrophy. Our presentation is brief since the derivation is technically trivial. In Chapter 39 we develop the theory of planetary geostrophic flows, with this theory of particular use for understanding the large-scale ocean circulation.

Planetary geostrophy is realized by dropping the fluid particle acceleration from the momentum equation (38.45), given that it is one order of Rossby number smaller than the Coriolis and pressure gradient accelerations. This assumption means that the velocity equation reduces to the geostrophic balance

$$\hat{\mathbf{f}} \times \hat{\mathbf{u}} = -\hat{\nabla} \hat{\eta}. \quad (38.49)$$

We furthermore assume that the Rossby number and Burger numbers scale together

$$\text{Ro} \sim \text{Bu} = (L_d/L)^2 \ll 1, \quad (38.50)$$

so that the horizontal length scale for the planetary geostrophic flow is much larger than the deformation radius

$$L \gg L_d. \quad (38.51)$$

This assumption is consistent with dropping the material acceleration term in the velocity equation. Although the velocity equation is greatly simplified, we make no assumption concerning the thickness equation. Consequently, the free surface and bottom undulations are unconstrained with planetary geostrophic flows, so long as the flow maintains the hydrostatic balance.

In summary, the thickness equation for the planetary geostrophic fluid retains its full unapproximated form, whereas the velocity equation reduces to geostrophy. Reintroducing dimensions leads to the planetary geostrophic equations

$$f \hat{z} \times \mathbf{u} = -g \nabla \eta \quad \text{and} \quad \frac{Dh}{Dt} = -h \nabla \cdot \mathbf{u} \quad \text{and} \quad h = \eta - \eta_b. \quad (38.52)$$

Since the Coriolis parameter retains its spatial dependence, and so includes the beta effect, the horizontal velocity field is divergent

$$f \nabla \cdot \mathbf{u} = -\beta (g/f) \partial_x \eta = -\beta v. \quad (38.53)$$

As shown in Exercise 38.1, the shallow water planetary geostrophic equations are equivalent to

$$f \hat{z} \times \mathbf{u} = -g \nabla \eta \quad \text{and} \quad \frac{DQ}{Dt} = 0 \quad \text{with} \quad Q = \frac{f}{h}. \quad (38.54)$$

We encountered this form for the potential vorticity in Section 34.4, in which the shallow water potential vorticity,  $(f + \zeta)/h$ , is approximated by  $f/h$  in the small Rossby number limit.

## 38.5 Shallow water quasi-geostrophy

In this section we develop the quasi-geostrophic equations for a single shallow water fluid layer. Doing so requires more work than for the planetary geostrophic equations. In particular, we use rudimentary asymptotic methods with the Rossby number the small parameter.

### 38.5.1 Quasi-geostrophic scaling

Quasi-geostrophic scaling is based on the following assumptions, with the first and second shared with planetary geostrophy whereas the remaining are distinct.

1. SMALL ROSSBY NUMBER:  $\text{Ro} \ll 1$ , which is fundamental to geostrophic scaling.
2. ADVECTIVE TIME SCALE:  $T \sim L/U$ ; that is, the time scale is determined by advection, which is how time scales throughout this chapter.
3. ORDER ROSSBY NUMBER BETA EFFECT:  $|\beta L| \ll |f_0|$ , which means that the Coriolis frequency does not vary much from its central value. To incorporate this assumption into the asymptotics, we expand the non-dimensional Coriolis parameter in terms of the Rossby number<sup>3</sup>

$$\hat{\mathbf{f}} = \mathbf{f}/f_0 = (1 + \beta y/f_0) \hat{z} \equiv (\hat{f}_0 + \text{Ro} \hat{\beta} \hat{y}) \hat{z}. \quad (38.55)$$

In this equation,  $\hat{z}$  is the unit vector in the vertical, and the time scaling in equation (38.40) renders<sup>4</sup>

$$\hat{\beta} \hat{y} = \beta y/(\text{Ro} f_0) = T \beta y \quad \text{and} \quad \hat{f}_0 = f_0/f_0 = 1. \quad (38.56)$$

<sup>3</sup>One could conceive of another small parameter that scales the beta effect, but the resulting asymptotics would be more difficult to manage given the need to keep track of two small parameters.

<sup>4</sup>Although  $\hat{f}_0 = 1$  in equation (38.56), it is useful to retain this term as a placeholder in the manipulations to follow.

The Coriolis expression (38.55) and the scaling (38.56) are motivated by assuming the horizontal scales of motion are on the same order as the deformation radius, and that the Coriolis frequency does not vary much from its central value. Quasi-geostrophy is thus formulated within the beta plane approximation discussed in Section 22.3.

4. BURGER NUMBER ORDER ONE:  $Bu \sim 1$ , which means that the horizontal scales of motion for the quasi-geostrophic flows are on the order as the deformation radius,  $L \sim L_d$ .
5. ORDER ROSSBY NUMBER FREE SURFACE UNDULATIONS: From equation (38.36), an order unity Burger number means that undulations of the free surface height scale according to the Rossby number:  $\mathcal{H}/H = Ro$ , so that free surface height undulations are small.
6. ORDER ROSSBY NUMBER BOTTOM TOPOGRAPHY UNDULATIONS: As seen in Section 38.6.4, for the quasi-geostrophic potential vorticity to correspond to the small Rossby number version of the shallow water potential vorticity requires the topography undulations to scale as  $\mathcal{B}/H = Ro$ . The assumed scaling for the bottom topography undulation pairs with that for the free surface, so that the layer thickness undulations,  $\Delta h = \Delta\eta - \Delta\eta_b$ , also scale as  $Ro$ . We are thus able to take a sensible  $Ro$  expansion of the  $1/h$  factor appearing in the shallow water potential vorticity (Section 38.6.4). It is useful to maintain a direct connection to the shallow water model as doing so helps to ensure that the resulting asymptotic theory is self-consistent. In particular, it ensures that quasi-geostrophic energetics are physically sensible since there is a direct lineage to the shallow water energetics.

The  $\mathcal{B}/H = Ro$  scaling is consistent with the assumption that the planetary beta effect is small. Together, the two scalings  $\mathcal{B}/H = Ro$  and  $\mathcal{H}/H = Ro$  mean that the effective beta effect (arising from both planetary and topographic variations; see Section 38.6.1 below) are small.

### 38.5.2 Outlining the asymptotic method

To derive the quasi-geostrophic shallow water model, we employ an asymptotic series method with the Rossby number as the small parameter and stop at the first nontrivial order. For this purpose, recall the non-dimensional shallow water equations from Section 38.3.7, and make use of the assumed  $Bu \sim 1$  scaling

$$Ro \frac{D\hat{\mathbf{u}}}{Dt} + (\hat{\mathbf{f}} \times \hat{\mathbf{u}}) = -\hat{\nabla}\hat{\eta} \quad (38.57a)$$

$$Ro \left[ \frac{\partial(\hat{\eta} - \hat{\eta}_b)}{\partial t} + \hat{\nabla} \cdot [(\hat{\eta} - \hat{\eta}_b) \hat{\mathbf{u}}] \right] = -\hat{\nabla} \cdot \hat{\mathbf{u}}. \quad (38.57b)$$

We brought the time independent bottom topography,  $\hat{\eta}_b$ , into the time derivative for the thickness equation to remain symmetric with  $\hat{\eta}$ .

#### *Asymptotic expansion of prognostic fields*

Asymptotic methods are ideally suited for non-dimensional equations since we can unambiguously determine scales via the size of non-dimensional parameters. We here assume the Rossby number to be small, in which case we are led to perform an asymptotic expansion of the prognostic fields in terms of the Rossby number. There are three prognostic fields,  $\hat{u}, \hat{v}, \hat{\eta}$ , and corresponding vertical

velocity,  $\hat{w}$ , which we assume can be written as an asymptotic series

$$\hat{u} = \hat{u}_0 + \text{Ro} \hat{u}_1 + \text{Ro}^2 \hat{u}_2 + \dots \quad (38.58a)$$

$$\hat{v} = \hat{v}_0 + \text{Ro} \hat{v}_1 + \text{Ro}^2 \hat{v}_2 + \dots \quad (38.58b)$$

$$\hat{w} = \hat{w}_0 + \text{Ro} \hat{w}_1 + \text{Ro}^2 \hat{w}_2 + \dots \quad (38.58c)$$

$$\hat{\eta} = \hat{\eta}_0 + \text{Ro} \hat{\eta}_1 + \text{Ro}^2 \hat{\eta}_2 + \dots \quad (38.58d)$$

We thus refer to the zeroth, first, second, etc. “order” of the asymptotic expansion. The velocity field is non-divergent at each order of Rossby number, so that

$$\nabla \cdot \hat{\mathbf{v}}_n = 0 \quad \forall n. \quad (38.59)$$

### *Practical goals*

The practical goal of asymptotic analysis is to develop a closed set of prognostic equations for functions appearing in the asymptotic expansions (38.58a)-(38.58d). For our purposes, we are content to stop at the lowest nontrivial order, meaning the point at which there is a prognostic equation that provides a means to move the system forward in time. Motivation for asymptotic analysis is to produce an equation set offering a means to focus analysis on dynamics most active under the regime determined by the chosen non-dimensional parameters. Each higher order in asymptotic expansion generally requires more complex algebraic manipulations. Hence, pursuit of higher order expansions should be undertaken only after first determining that the lower order equation set remains physically lacking.

### *Enabling the machinery*

At this point we enable the machinery by “turning the crank”. To do so, we insert the asymptotic expansions (38.58a)-(38.58d) into the non-dimensional partial differential equations (38.57a) and (38.57b). Since  $\text{Ro}$  is arbitrarily small, and all non-dimensional fields are order unity regardless their order, the only means to maintain self-consistency is for terms to balance at equal order in Rossby number. Hence, we do not mix terms from different orders of Rossby number. This point is basic to asymptotic methods.

Again, our goal is to establish a set of prognostic equations that allows us to evolve a state that is arbitrarily close to geostrophic balance. We anticipate that at zeroth order the asymptotic method offer just the geostrophic balance, which has no prognostic value. Hence, we need to go at least to order  $\text{Ro}^1$ , and hopefully no further as the algebraic tedium increases with order. With that anticipation and hope, we only keep track of terms of order  $\text{Ro}^0$  and  $\text{Ro}^1$ , in which the momentum and continuity equations become

$$\text{Ro} \frac{D\hat{\mathbf{u}}_0}{Dt} + (\hat{f}_0 + \text{Ro} \beta \hat{y}) \hat{z} \times (\hat{\mathbf{u}}_0 + \text{Ro} \hat{\mathbf{u}}_1) = -\hat{\nabla}(\hat{\eta}_0 + \text{Ro} \hat{\eta}_1) \quad (38.60a)$$

$$\text{Ro} \left[ \frac{\partial \hat{\eta}_0}{\partial t} + \hat{\nabla} \cdot [(\hat{\eta}_0 - \hat{\eta}_b) \hat{\mathbf{u}}_0] + \hat{\nabla} \cdot \hat{\mathbf{u}}_1 \right] = -\hat{\nabla} \cdot \hat{\mathbf{u}}_0. \quad (38.60b)$$

### 38.5.3 Order $\text{Ro}^0$ asymptotic equations

Terms in equations (38.60a) and (38.60b) balancing at order  $\text{Ro}^0$  are given by

$$\hat{\mathbf{f}}_0 \times \hat{\mathbf{u}}_0 = -\hat{\nabla} \hat{\eta}_0 \quad (38.61\text{a})$$

$$\hat{\nabla} \cdot \hat{\mathbf{u}}_0 = 0. \quad (38.61\text{b})$$

The zeroth order velocity equation (38.61a) is the  $f$ -plane geostrophic balance. The curl of this equation leads to the horizontal non-divergence condition

$$\hat{\nabla} \cdot \hat{\mathbf{u}}_0 = 0, \quad (38.62)$$

which is identical to the zeroth order thickness equation (38.61b). Hence, the zeroth order horizontal velocity is given by  $f$ -plane geostrophy.

Given the non-divergence condition (38.61b), the zeroth order velocity field can be written in terms of a *geostrophic streamfunction*

$$\hat{u}_0 = -\frac{\partial \hat{\psi}_0}{\partial \hat{y}} \quad \text{and} \quad \hat{v}_0 = \frac{\partial \hat{\psi}_0}{\partial \hat{x}} \quad \text{and} \quad \hat{\zeta}_0 = \hat{\nabla}^2 \hat{\psi}_0, \quad (38.63)$$

where the zeroth order streamfunction is the ratio of the zeroth order surface height to zeroth order Coriolis parameter

$$\hat{\psi}_0 = \hat{\eta}_0 / \hat{f}_0. \quad (38.64)$$

We also introduced the zeroth order vorticity,  $\hat{\zeta}_0$ , which plays a role in the order  $\text{Ro}^1$  equations. The corresponding dimensionful quantities are

$$\psi = (U L) \hat{\psi}_0 \quad \text{and} \quad \zeta = (U/L) \hat{\zeta}_0. \quad (38.65)$$

We dropped the asymptotic label on the dimensional quantities to reduce clutter and since we only evolve the zeroth order fields. In the following, the higher order fields are referred to as *ageostrophic* fields, whereas the zeroth order fields are the geostrophic fields.

### 38.5.4 Order $\text{Ro}^1$ asymptotic equations

The zeroth order equations do not render a prognostic equation, prompting us to consider equations at order  $\text{Ro}^1$

$$\frac{D_0 \hat{\mathbf{u}}_0}{Dt} + \hat{f}_0 \hat{z} \times \hat{\mathbf{u}}_1 + \hat{\beta} \hat{y} \hat{z} \times \hat{\mathbf{u}}_0 = -\hat{\nabla} \hat{\eta}_1 \quad (38.66\text{a})$$

$$\frac{D_0 (\hat{\eta}_0 - \hat{\eta}_b)}{Dt} = -\hat{\nabla} \cdot \hat{\mathbf{u}}_1. \quad (38.66\text{b})$$

At this order, the material time derivative makes use of *only* the zeroth order geostrophic horizontal velocity

$$\frac{D_0}{Dt} = \frac{\partial}{\partial \hat{t}} + \hat{\mathbf{u}}_0 \cdot \hat{\nabla}. \quad (38.67)$$

The set of first order equations (38.66a) and (38.66b) appear to be unclosed because the evolution equation for zeroth order (geostrophic) terms is dependent on first order (ageostrophic) terms. However, the ageostrophic terms can be eliminated using two steps. First, we produce the vorticity equation from the momentum equation, which removes the ageostrophic pressure gradient  $-\hat{\nabla} \hat{\eta}_1$ . Second, combine the vorticity equation and continuity equation to eliminate the

horizontal convergence of the ageostrophic velocity,  $-\hat{\nabla} \cdot \hat{\mathbf{u}}_1$ . The second step leads to the quasi-geostrophic potential vorticity equation. Although details are specific to our study of shallow water quasi-geostrophy, similar steps are frequently encountered in other balanced geophysical fluid systems.

### The geostrophic vorticity equation

Taking the curl of the momentum equation (38.66a) eliminates the ageostrophic pressure gradient,  $\hat{\nabla} \hat{\eta}_1$ , thus producing the vorticity equation

$$\frac{\partial \hat{\zeta}_0}{\partial \hat{t}} + (\hat{\mathbf{u}}_0 \cdot \hat{\nabla}) (\hat{\zeta}_0 + \hat{\beta} \hat{y}) = -\hat{f}_0 \hat{\nabla} \cdot \hat{\mathbf{u}}_1. \quad (38.68)$$

The right hand side term arises from stretching in the presence of rotation. To this order, stretching arises just from the planetary vorticity, with stretching due to relative vorticity appearing at a higher order. Since  $\hat{\beta} \hat{y}$  is time independent, we can write the vorticity equation using the geostrophic material time derivative

$$\frac{D_0 (\hat{\zeta}_0 + \hat{\beta} \hat{y})}{Dt} = -\hat{f}_0 \hat{\nabla} \cdot \hat{\mathbf{u}}_1. \quad (38.69)$$

### The quasi-geostrophic potential vorticity equation

As anticipated, we need one more step to close the system since the evolution of zeroth order vorticity in equations (38.68) and (38.69) are a function of vortex stretching induced by convergence of the first order velocity. To eliminate  $\hat{\nabla} \cdot \hat{\mathbf{u}}_1$ , we substitute from the thickness equation (38.66b), thus leading to a prognostic equation involving just zeroth order terms

$$\frac{\partial [\hat{\zeta}_0 + \hat{\beta} \hat{y} - \hat{f}_0 (\hat{\eta}_0 - \hat{\eta}_b)]}{\partial \hat{t}} + \hat{\mathbf{u}}_0 \cdot \hat{\nabla} [\hat{\zeta}_0 + \hat{\beta} \hat{y} - \hat{f}_0 (\hat{\eta}_0 - \hat{\eta}_b)] = 0, \quad (38.70)$$

which can be written in the material form

$$\frac{D_0}{Dt} [\hat{\zeta}_0 + \hat{\beta} \hat{y} - \hat{f}_0 (\hat{\eta}_0 - \hat{\eta}_b)] = 0. \quad (38.71)$$

Finally, we introduce the geostrophic streamfunction  $\hat{\psi}_0 = \hat{\eta}_0 / \hat{f}_0$  (equation (38.64)) to render

$$\frac{D_0}{Dt} [\hat{\nabla}^2 \hat{\psi}_0 + \hat{\beta} \hat{y} + \hat{f}_0 \hat{\eta}_b - \hat{f}_0^2 \hat{\psi}_0] = 0. \quad (38.72)$$

Equation (38.72) is a statement of the material conservation of quasi-geostrophic potential vorticity, where material evolution is defined by the horizontal geostrophic currents (equation (38.67)). This equation is the culmination of our quest to derive a prognostic equation for the evolution of geostrophic flow. It enables us to evolve the geostrophic velocity and geostrophic free surface by probing, but not explicitly determining, the leading order ageostrophic motions. Practical use of the quasi-geostrophic method is based on time stepping the quasi-geostrophic potential vorticity, and then inverting the potential vorticity equation to diagnose the streamfunction to then determine the geostrophic velocity and free surface. That inversion requires solving an elliptic boundary value problem.

## 38.6 Physical elements of the theory

The asymptotic analysis of Section 38.5 worked with non-dimensional quantities, which are suitable for determining the scales required for asymptotic methods. Now that we have worked through the details, we can make use of that effort to both further the theory and to understand its physical content. For that purpose we find it essential to reintroduce physical dimensions.

### 38.6.1 Dimensional potential vorticity and streamfunction

To introduce physical dimensions, we invert the relations used in Section 38.3.7, in which we make use of

$$\hat{t} = T^{-1} t \quad (\hat{x}, \hat{y}) = L^{-1} (x, y) \quad \partial_{\hat{t}} = T \partial_t \quad \hat{\nabla} = L \nabla \quad (\hat{u}, \hat{v}) = U^{-1} (u, v) \quad (38.73a)$$

$$\hat{\eta} = \mathcal{H}^{-1} \Delta \eta \quad \hat{\eta}_b = \mathcal{B}^{-1} \Delta \eta_b \quad \mathcal{H} = H \text{Ro} \quad \mathcal{B} = H \text{Ro} \quad (38.73b)$$

$$\hat{f}_0 = f_0 / f_0 \quad \hat{\beta} \hat{y} = \beta y / (Ro f_0) = (L/U) \beta y \quad \hat{\zeta} = (L/U) \zeta = L^2 \nabla^2 \psi. \quad (38.73c)$$

We generally drop asymptotic subscript notation on the dimensional terms to help reduce clutter.

For the potential vorticity we start from the non-dimensional quasi-geostrophic potential vorticity (38.71) and find

$$\hat{q} = \hat{\zeta}_0 + \hat{\beta} \hat{y} + \hat{f}_0 \hat{\eta}_b - \hat{f}_0 \hat{\eta}_0 \quad (38.74a)$$

$$= \frac{L}{U} (\zeta + \beta y) + \frac{\Delta \eta_b}{\mathcal{B}} - \frac{\Delta \eta}{\mathcal{H}} \quad (38.74b)$$

$$= \frac{L}{U} (\zeta + \beta y) + \frac{\Delta \eta_b}{H \text{Ro}} - \frac{\Delta \eta}{H \text{Ro}} \quad (38.74c)$$

$$= \frac{L}{U} \left[ \zeta + \beta y - \frac{f_0 (\Delta \eta - \Delta \eta_b)}{H} \right] \quad (38.74d)$$

$$= \frac{L}{U} \left[ \zeta + \beta y - \frac{g (\Delta \eta - \Delta \eta_b)}{f_0} \frac{1}{L_d^2} \right] \quad (38.74e)$$

$$= \frac{L}{U} [\zeta + \beta y - L_d^{-2} (\psi - \psi_b)], \quad (38.74f)$$

where  $L_d = \sqrt{g H} / f$  is the shallow water deformation radius (equation (38.31)), and we introduced the geostrophic streamfunction<sup>5</sup>

$$\psi = (g/f_0) \Delta \eta. \quad (38.75)$$

We also wrote the contribution from topography as

$$\psi_b = (g/f_0) \Delta \eta_b, \quad (38.76)$$

which is a static field. We are thus led to the dimensionful QG potential vorticity for a single shallow water layer

$$q = f_0 (1 + \text{Ro} \hat{q}) = (\zeta + f) - L_d^{-2} (\psi - \psi_b) = f + \psi_b L_d^{-2} + (\nabla^2 - L_d^{-2}) \psi. \quad (38.77)$$

We took the liberty of adding the constant,  $f_0$ , to the QG potential vorticity, which does not

---

<sup>5</sup> *Vallis* (2017) defines the geostrophic streamfunction in his equation (5.69) as  $\psi_{\text{vallis}} = g \eta / f_0 = \psi + g H / f_0$ , which differs by the constant  $g H / f_0$ . However, there is no difference in the dynamics since a streamfunction is unique only up to a constant.

alter the dynamics but does allow us to introduce the planetary vorticity,  $f = f_0 + \beta y$ . The dynamically relevant portions of  $q$  appear at order  $\text{Ro}$ .

### 38.6.2 Contributions to the QG potential vorticity

The quasi-geostrophic potential vorticity (38.77) has three main contributions

$$q = f + \zeta - f_0 \Delta h / H, \quad (38.78)$$

where we wrote

$$L_d^{-2} (\psi - \psi_b) = f_0^2 / (g H) (g/f_0) (\Delta\eta - \Delta\eta_b) = f_0 \Delta h / H, \quad (38.79)$$

with  $\Delta h$  the undulations in the layer thickness due to undulations in the free surface and bottom topography. Heuristically, we can connect  $q$  to the shallow water  $Q = (f + \zeta)/h$  by

$$(f + \zeta)/h \approx (f + \zeta) (1 - \Delta h / H) \approx H^{-1} (f + \zeta - f_0 \Delta h / H), \quad (38.80)$$

where we assumed  $\beta y$ ,  $\zeta$ , and  $\Delta h$  are order  $\text{Ro}$  whereas  $f_0$  is order unity. We pursue this expansion more formally in Section 38.6.4. But for present purposes we can use it to summarize the various contributions to potential vorticity.

- PLANETARY VORTICITY: The contribution  $f = f_0 + \beta y$  arises from planetary vorticity, with the dynamically relevant contribution for QG arising just from the  $\beta y$  term.
- GEOSTROPHIC RELATIVE VORTICITY:  $\nabla^2 \psi = (g/f_0) \nabla^2 \eta$  is the relative vorticity of the geostrophic flow. Given the Laplacian operator emphasizes small spatial scales, the relative vorticity is most important at scales at or smaller than the deformation radius.
- EFFECTIVE BETA: The contribution from the gradient of planetary vorticity is given by  $\beta y = \mathbf{x} \cdot \nabla f$ . Likewise, the contribution from topography is given by

$$\psi_b L_d^{-2} = f_0 \Delta\eta_b / H = (f_0/H) (\eta_b - \bar{\eta}_b) \approx (f_0/H) \mathbf{x} \cdot \nabla \eta_b, \quad (38.81)$$

where the approximate expression made use of a Taylor series. These two contributions can be combined into an effective beta

$$\beta y + \psi_b L_d^{-2} = \mathbf{x} \cdot \nabla (f + f_0 \eta_b / H) \approx \mathbf{x} \cdot (H - \eta_b) \nabla [f / (H - \eta_b)], \quad (38.82)$$

with the final approximate expression connecting to the effective beta discussed in Section 34.6.1.

- VERTICAL STRETCHING: As discussed in Section 30.2, shallow water fluids move as vertical extensible columns. Hence, the term  $(f_0/H) \Delta h$  accounts for the contribution to potential vorticity from column stretching and squashing. It is most important for scales at or larger than those where the relative vorticity is important; i.e., at or larger than the deformation radius.
- FLOW REGIMES RELATIVE TO THE DEFORMATION RADIUS: As noted above, the term  $(\nabla^2 - L_d^{-2}) \psi$  signals two regimes as determined by the deformation radius. For lateral scales on the order of the deformation radius, both the relative vorticity and vortex stretching make equal contributions to the potential vorticity. For smaller scales relative vorticity is more important whereas for larger scales vortex stretching dominates.

- TWO-DIMENSIONAL TURBULENCE: In the absence of rotation, so that  $f_0 = \beta = 0$ , the QG potential vorticity reduces to the relative vorticity,  $q = \zeta$ , in which case quasi-geostrophy reduces to a non-divergent and non-rotating two-dimensional flow. This model is commonly used to study two dimensional turbulence, which can shed light on quasi-geostrophic turbulence (e.g., Section 11.3 of [Vallis \(2017\)](#)).

### 38.6.3 Summarizing the equations of quasi-geostrophy

The following fields are the key pieces of the single layer shallow water quasi-geostrophic theory

$$\mathbf{u} = \hat{\mathbf{z}} \times \nabla \psi \quad \text{and} \quad \zeta = \hat{\mathbf{z}} \cdot \nabla \times \mathbf{u} = \nabla^2 \psi \quad \text{and} \quad q = f + \zeta - L_d^{-2} (\psi - \psi_b) \quad (38.83a)$$

$$\psi = (g/f_0) \Delta \eta \quad \text{and} \quad \psi_b = (g/f_0) \Delta \eta_b \quad \text{and} \quad L_d = f_0^{-1} \sqrt{g H}. \quad (38.83b)$$

#### *Evolution of the geostrophic flow*

Evolution of the geostrophic flow is determined by material time changes to the QG potential vorticity following the horizontal geostrophic flow

$$\frac{Dq}{Dt} = \frac{\partial q}{\partial t} + \mathbf{u} \cdot \nabla q = \frac{\partial q}{\partial t} + \hat{\mathbf{z}} \cdot (\nabla \psi \times \nabla q) = \frac{\partial q}{\partial t} + J(\psi, q), \quad (38.84)$$

where the final equality introduced the Jacobian operator

$$J(\psi, q) = \partial_x \psi \partial_y q - \partial_y \psi \partial_x q. \quad (38.85)$$

For a perfect fluid, the quasi-geostrophic PV is materially constant, whereas more general flows have forcing and dissipation so that

$$\frac{Dq}{Dt} = \text{forcing} - \text{dissipation}. \quad (38.86)$$

As an algorithm, we first update the potential vorticity to a new time step, then diagnose the streamfunction,  $\psi = g \eta / f_0$ , by solving the elliptic boundary value problem

$$(\nabla^2 - L_d^{-2}) \psi = q - f - \psi_b / L_d^2, \quad (38.87)$$

at which point we know the updated free surface and updated velocity.

#### *Velocity and free surface equations*

In the above algorithm we are not concerned with the velocity and free surface equations, but instead we are concerned with inverting the potential vorticity equation (38.87) to find the streamfunction. Even so, it can be of interest to consider these equations, which are determined by the order  $\text{Ro}^1$  equations in Section 38.5.4

$$\partial_t \mathbf{u}_g + (\mathbf{u}_g \cdot \nabla) \mathbf{u}_g + (f_0 + \beta y) \hat{\mathbf{z}} \times \mathbf{u}_g + f_0 \hat{\mathbf{z}} \times \mathbf{u}_{ag} = -g \nabla (\eta_g + \eta_{ag}) \quad (38.88a)$$

$$\partial_t (\eta_g - \eta_b) + (\mathbf{u}_g \cdot \nabla) (\eta_g - \eta_b) = -\nabla \cdot \mathbf{u}_{ag}. \quad (38.88b)$$

In these equations we temporarily introduced subscripts to distinguish the geostrophic velocity and corresponding surface height

$$f_0 \hat{\mathbf{z}} \times \mathbf{u}_g = -g \nabla \eta_g \quad (38.89)$$

from the ageostrophic free surface height,  $\eta_{\text{ag}}$ , and ageostrophic velocity,  $\mathbf{u}_{\text{ag}}$ . Since the ageostrophic velocity generally has a nonzero horizontal convergence, but it is three dimensionally non-divergent (since the fluid layer has constant density), then we can identify a corresponding vertical component to the ageostrophic velocity that satisfies

$$\mathbf{v}_{\text{ag}} = \mathbf{u}_{\text{ag}} + \hat{\mathbf{z}} w_{\text{ag}} \quad \text{with} \quad \nabla \cdot \mathbf{v}_{\text{ag}} = \partial_x u_{\text{ag}} + \partial_y v_{\text{ag}} + \partial_z w_{\text{ag}} = 0. \quad (38.90)$$

### 38.6.4 Connecting quasi-geostrophic PV to shallow water PV

We here determine how potential vorticity for shallow water quasi-geostrophy relates to the full shallow water potential vorticity studied in Chapter 34. For that purpose, recall that the potential vorticity for a single layer of shallow water fluid is (Section 34.4)

$$Q = \frac{f + \zeta}{h}, \quad (38.91)$$

where  $h = H + \Delta\eta - \Delta\eta_b$  (equation (38.4)) is the thickness of the layer.

To connect to the quasi-geostrophic potential vorticity, we non-dimensionalize the potential vorticity prior to performing an asymptotic expansion to order  $\text{Ro}^1$ . For this purpose, use the scaling relations from Section 38.3.7 to write the geostrophic relative vorticity as

$$\zeta = \nabla^2 \psi = (g/f_0) \nabla^2 \Delta\eta = (g \mathcal{H})/(f_0 L^2) \hat{\nabla}^2 \hat{\eta} = (g H \text{Ro})/(f_0 L^2) \hat{\zeta}_0 = f_0 \text{Ro} (L_d/L)^2 \hat{\zeta}_0 \quad (38.92)$$

as well as

$$h = H + H \text{Ro} (\hat{\eta} - \hat{\eta}_b) \quad (38.93a)$$

$$f = f_0 (\hat{f}_0 + \text{Ro} \hat{\beta} \hat{y}). \quad (38.93b)$$

Taking the ratio and expanding to order  $\text{Ro}^1$  leads to

$$\frac{\zeta + f}{h} = \frac{f_0}{H} \left[ \frac{\hat{f}_0 + \text{Ro} (L_d/L)^2 \hat{\zeta}_0 + \text{Ro} \hat{\beta} \hat{y}}{1 + \text{Ro} (\hat{\eta} - \hat{\eta}_b)} \right] \quad (38.94a)$$

$$\approx \frac{f_0}{H} + \frac{f_0 \text{Ro}}{H} \left[ -\hat{f}_0 (\hat{\eta} - \hat{\eta}_b) + (L_d/L)^2 \hat{\zeta}_0 + \hat{\beta} \hat{y} \right] \quad (38.94b)$$

$$= \frac{f_0}{H} + \frac{f_0 \text{Ro}}{H} \left[ (L_d/L)^2 \hat{\zeta}_0 + \hat{\beta} \hat{y} - \hat{f}_0 (\hat{\eta} - \hat{\eta}_b) \right] \quad (38.94c)$$

$$= \frac{f_0}{H} + \frac{f_0 \text{Ro}}{H} \left[ \frac{\zeta}{f_0 \text{Ro}} + \frac{\beta y}{f_0 \text{Ro}} - \frac{\Delta\eta}{\mathcal{H}} + \frac{\Delta\eta_b}{\mathcal{B}} \right] \quad (38.94d)$$

$$= \frac{1}{H} \left[ \zeta + f_0 + \beta y - \frac{f_0 (\Delta\eta - \Delta\eta_b)}{H} \right] \quad (38.94e)$$

$$= \hat{q} U / (H L) \quad (38.94f)$$

$$= q/H. \quad (38.94g)$$

We are thus led to the relation between the shallow water potential vorticity and the quasi-geostrophic shallow water potential vorticity

$$\frac{f + \zeta}{h} = \frac{q}{H} + \mathcal{O}(\text{Ro}^2). \quad (38.95)$$

As noted in Section 38.5.1, this connection between the potential vorticities only holds when assuming deviations in *both* the bottom topography and free surface scale according to the Rossby

number,  $\Delta\eta = \mathcal{H} \text{Ro}$  and  $\Delta\eta_b = \mathcal{B} \text{Ro}$ , thus allowing us to combine  $\hat{\eta}$  and  $\hat{\eta}_b$  in the thickness equation (38.93a).

The identity (38.95) is a consequence of the asymptotic expansion of the velocity and thickness equations. We could alternatively invert our development of quasi-geostrophy by using the quasi-geostrophic potential vorticity as the basis for deriving the governing equations. We pursue that approach to derive the layered quasi-geostrophic equations in Section 38.6.6.

### 38.6.5 Considering topography to be $\mathcal{O}(\text{Ro}^0)$

We here briefly consider topography to be arbitrarily large, in which case we are no longer ensured asymptotic consistency since we can no longer combine  $\Delta\eta$  and  $\Delta\eta_b$  into an order Rossby number fluctuation of the layer thickness. Even so, it is not uncommon to examine how an asymptotic theory performs when outside of its formal regime of validity, particularly with the advent of numerical codes to facilitate such studies. In many cases the theories continue to provide provocative, and sometimes physically relevant, information.

To see what happens, consider the quasi-geostrophic PV equation

$$(\partial_t + \mathbf{u} \cdot \nabla) [\zeta + \beta y + L_d^{-2} (\psi_b - \psi)] = 0. \quad (38.96)$$

If  $\psi_b$  is order unity whereas the other terms are order Ro, then to leading order the potential vorticity is given by the static term,  $L_d^{-2} \psi_b$ , so that material conservation of potential vorticity reduces to

$$\mathbf{u} \cdot \nabla \psi_b = 0 \implies \mathbf{u} \cdot \nabla \eta_b = 0. \quad (38.97)$$

This constraint means that the  $f$ -plane geostrophic flow is constrained to flow along lines of constant topography (isobaths), in which case the geostrophic streamfunction satisfies

$$(f/g) \mathbf{u} \cdot \nabla \eta_b = \hat{\mathbf{z}} \cdot (\nabla \eta \times \nabla \eta_b) \equiv J(\eta, \eta_b) = 0. \quad (38.98)$$

The order one bottom topography undulations thus provide a strong constraint on the  $f$ -geostrophic flow, making the flow align with the bottom topography and in turn aligning surface height undulations with bottom undulations. We uncovered this constraint in our analysis of topographic form stress in Section 34.9.5. We also discussed this flow as a particular realization of the two-dimensional non-divergent barotropic flow in Section 33.1.3.

### 38.6.6 Two layer quasi-geostrophy

In Section 30.4 we developed the equations for an adiabatic stacked shallow water model. We here specialize those equations to a two-layer quasi-geostrophic model, with extensions to multiple layers following straightforwardly. Rather than pursue the formal asymptotic methods used previously, we here make use of our observation in Section 38.6.4 concerning the connection between shallow water and quasi-geostrophic potential vorticities.

To get started, recall from Section 34.4.6 that the shallow water potential vorticity for an arbitrary layer, labelled by the index  $k$ , is given by

$$Q_k = \frac{f + \zeta_k}{h_k}, \quad (38.99)$$

As in Section 38.6.2, we assume  $\beta y$ ,  $\zeta_k$ , and  $\Delta h_k$  scale as Ro, in which case we have the quasi-geostrophic potential vorticity for each layer

$$q_k = f + \zeta_k - f_0 \Delta h_k / H, \quad (38.100)$$

where  $\zeta_k$  is here the geostrophic relative vorticity.

From our asymptotic analysis earlier in this section, the toughest part of that analysis concerned the derivation of the quasi-geostrophic potential vorticity equation. In the present approach, we already have the potential vorticity for each layer via equation (38.100). What we need is the velocity field to advect it. Again, we know what that velocity is: it is the  $f$ -plane geostrophic velocity for each layer. The 2-layer velocity equations are given by equations (30.68a) and (30.68b), with their geostrophic components determined by

$$f_0 \hat{z} \times \mathbf{u}_1 = -g \nabla(\Delta\eta_b + \Delta h_1 + \Delta h_2) \quad (38.101a)$$

$$f_0 \hat{z} \times \mathbf{u}_2 = -\nabla \left[ g_{1/2}^r (\Delta\eta_b + \Delta h_1 + \Delta h_2) + g_{3/2}^r (\Delta\eta_b + \Delta h_2) \right]. \quad (38.101b)$$

In these equations we set the applied atmospheric pressure to a constant, and made use of the reduced gravities at the layer interfaces are

$$g_{1/2}^r = g(\rho_1 - \rho_a)/\rho_1 \approx g \quad \text{and} \quad g_{3/2}^r = g(\rho_2 - \rho_1)/\rho_1, \quad (38.102)$$

with  $\rho_a \ll \rho_1$  so that the top interface reduced gravity is well approximated by the full gravity. From equations (38.101a) and (38.101b) we can identify the geostrophic streamfunctions

$$\psi_1 = (g/f_0)(\Delta\eta_b + \Delta h_1 + \Delta h_2) \quad (38.103a)$$

$$\psi_2 = (1/f_0) \left[ g_{1/2}^r (\Delta\eta_b + \Delta h_1 + \Delta h_2) + g_{3/2}^r (\Delta\eta_b + \Delta h_2) \right], \quad (38.103b)$$

so that the layer geostrophic velocities are given by

$$\mathbf{u}_1 = \hat{z} \times \nabla \psi_1 \quad \text{and} \quad \mathbf{u}_2 = \hat{z} \times \nabla \psi_2. \quad (38.104)$$

We thus proceed with the usual quasi-geostrophic algorithm, whereby evolution is determined by the material time changes of the potential vorticity with advection given by the layer geostrophic flow

$$(\partial_t + \mathbf{u}_k \cdot \nabla) q_k = 0. \quad (38.105)$$

## 38.7 Exercises

### EXERCISE 38.1: PV CONSERVATION FOR PLANETARY GEOSTROPHY

Show that the planetary geostrophic equations

$$\mathbf{f} \times \mathbf{u} = -g \nabla \eta \quad \text{and} \quad \frac{Dh}{Dt} = -h \nabla \cdot \mathbf{u} \quad \text{with} \quad \eta = \eta_b + h \quad (38.106)$$

are equivalent to

$$\mathbf{f} \times \mathbf{u} = -g \nabla \eta \quad \text{and} \quad \frac{DQ}{Dt} = 0 \quad \text{with} \quad Q = \frac{f}{h}. \quad (38.107)$$

This result shows that the shallow water PG equations may be written as an evolution equation for an approximated version of the shallow water potential vorticity,  $(f + \zeta)/h \approx f/h$ . This limit holds when the Rossby number is small.

### EXERCISE 38.2: CONSTRAINTS ON STEADY STATE PLANETARY GEOSTROPHIC FLOW

Consider a shallow water fluid satisfying the planetary geostrophic equations developed in Section 38.4. Assume the flow is in steady state.

- (a) In what manner does potential vorticity conservation constrain the velocity field?
- (b) Consider an initially zonal geostrophic flow. In what direction (poleward or equatorward) will a fluid parcel deviate when encountering a seamount (i.e., a region of relatively shallow depth)?
- (c) Describe the geostrophic contours (i.e., path of fluid particles following the geostrophic flow) for the case where the ocean sea surface height undulations,  $\Delta\eta$ , are far smaller than undulations in the bottom topography,  $\eta_b$  (see Figure 30.1 for notation).
- (d) For the special case of an  $f$ -plane, show that the velocity is aligned with isolines of bottom topography.
- (e) For the special case of a flat bottom and latitudinally dependent Coriolis parameter,  $f(y)$ , show that there is no meridional geostrophic velocity. That is, the flow is zonally aligned.





# Chapter 39

## Continuously stratified planetary geostrophy

The planetary geostrophic equations consist of linear steady geostrophic balance (commonly also with friction) plus the full nonlinear buoyancy equation. Circulation is thus determined by the mass field given that the flow is diagnostic whereas buoyancy is prognostic. Given that the momentum equation is linear, there is no turbulence in planetary geostrophy. Instead, the equation set allows the analyst to focus on large-scale flow of a stratified laminar fluid feeling the effects from rapid rotation in the presence of planetary and topographic beta.

We already encountered many physical properties of planetary geostrophic flow in Chapter 25, where we studied geostrophy, vorticity, thermal wind, and Taylor-Proudman. We also made use of planetary geostrophy when studying western boundary current intensification for a shallow water layer in Section 34.9. In this chapter we fill in certain of the mathematical details left out from those early discussions by deriving, through non-dimensionalization and scale analysis, the planetary geostrophic equations.

As an application of the planetary geostrophic equations, we examine a variety of vorticity budgets formed from this equation set. We start by examining the potential vorticity budget and studying how the impermeability theorem (Chapter 37.2) manifests. We then discuss a variety of vorticity budgets used to describe the depth integrated or depth averaged flow. Each of these two-dimensional vorticity budgets offers insights into how the large-scale flow is constrained by rapid rotation and the  $\beta$ -effect present on a sphere. In particular, these budgets offer insights into how forces and the curl of forces generate both vertical flow next to the boundaries as well as meridional flow for the full fluid column. The stratified planetary geostrophic equations form the foundation for many theories of the large-scale ocean circulation. Constraints provided by the vorticity theorems developed in this chapter provide the key reasons for why these theories are so physically compelling.

### CHAPTER GUIDE

We here extend the shallow water discussions from Chapter 38 to derive the continuously stratified planetary geostrophic equations. We make use of stratified geophysical fluid dynamics from Chapters 17 and 25, vorticity and the planetary beta effect from Chapter 35, and potential vorticity from Chapter 36. Physical properties of stratified geostrophic mechanics were considered in Chapter 25, with an understanding of that material assumed here. We follow the non-dimensionalization used to derive the shallow water planetary geostrophic equations in Chapter 38, and further extend this material to continuously stratified quasi-geostrophy in Chapter 40.

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39.1	Loose threads	972
39.2	Non-dimensionalizing the stratified Boussinesq equations	972
39.2.1	Dimensional parameters	973
39.2.2	Physical dimensions and non-dimensional parameters	974
39.2.3	Choosing the non-dimensional parameters	974
39.2.4	Relating the buoyancy scale to the Coriolis acceleration scale	976
39.2.5	Richardson number and QG/PG flow regimes	976
39.2.6	The Rossby deformation radius	977
39.2.7	Assumed values for the non-dimensional parameters	977
39.2.8	Non-dimensional Boussinesq equations	979
39.3	Summary equations for planetary geostrophy	980
39.4	Planetary geostrophic potential vorticity	981
39.4.1	Derivation	981
39.4.2	Impermeability theorem	982
39.4.3	Kinematic fluxes satisfying impermeability	983
39.5	Depth integrated vorticity budget	983
39.5.1	The $\beta$ -effect, stretching, and meridional transport	984
39.5.2	Bottom kinematics and dynamics	985
39.5.3	Surface kinematics and dynamics	987
39.5.4	Summary of force curls driving depth integrated meridional flow	988
39.6	Sverdrup balance and geostrophic Sverdrup balance	990
39.7	Vorticity of the depth integrated velocity	991
39.7.1	Depth integrated velocity equation	991
39.7.2	Vorticity budget	992
39.8	Vorticity equation for the depth averaged velocity	992
39.8.1	Relating the depth average velocity to boundary velocities	993
39.8.2	Formulation of the vorticity equation	993
39.8.3	Rigid lid approximation and the role of JEBAR	994
39.8.4	Further study	996

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## 39.1 Loose threads

- Reintroduce the bottom topography to the derivation in Section 39.2 as per the shallow water discussion in Chapter 38.
- More figures throughout the chapter
- Exercises
- Energetics of PG system as per Appendix A of *Callies and Ferrari (2018)*.

## 39.2 Non-dimensionalizing the stratified Boussinesq equations

In this section we non-dimensionalize the continuously stratified Boussinesq equations. As part of this process we identify a variety of non-dimensional numbers that characterize the flow. Planetary geostrophy is a rather simple asymptotic theory. Nonetheless, our work to non-dimensionalize the Boussinesq equations supports the work needed for the more complicated derivations of continuously stratified quasi-geostrophy in Chapter 40.

The starting point is the perfect fluid stratified hydrostatic Boussinesq equations (Section 23.1)

$$\frac{D\mathbf{u}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla_z \varphi \quad (39.1a)$$

$$\frac{\partial \varphi}{\partial z} = b \quad (39.1b)$$

$$\frac{Db}{Dt} = 0 \quad (39.1c)$$

$$\nabla \cdot \mathbf{v} = 0, \quad (39.1d)$$

where  $\mathbf{v} = (\mathbf{u}, w)$  is the three-dimensional velocity written using Cartesian coordinates,  $b = -g(\rho - \rho_0)/\rho_0$  is the Archimedian buoyancy relative to a constant reference density,  $\rho_0$ , with  $\rho$  the density. We also write  $\varphi = \delta p/\rho_0$  for the dynamic pressure (dimensions of  $L^2 T^{-2}$ ), and  $\nabla_z = (\partial_x, \partial_y, 0)$  for the horizontal gradient operator. We separate a background vertical buoyancy profile from a space-time fluctuating buoyancy

$$b = \tilde{b}(z) + b'(x, y, z, t), \quad (39.2)$$

and introduce the corresponding background squared buoyancy frequency

$$N^2 = \frac{d\tilde{b}}{dz}. \quad (39.3)$$

With this decomposition, the buoyancy equation (39.1c) takes the form

$$\frac{Db'}{Dt} + w N^2 = 0. \quad (39.4)$$

We also introduce an associated decomposition of the hydrostatic pressure

$$\varphi = \tilde{\varphi}(z) + \varphi'(x, y, z, t) \quad (39.5)$$

where  $\tilde{\varphi}$  is hydrostatically balanced by  $\tilde{b}$

$$\frac{d\tilde{\varphi}}{dz} = \tilde{b}, \quad (39.6)$$

and the fluctuating pressure,  $\varphi'$ , is hydrostatically balanced by  $b'$

$$\frac{\partial \varphi'}{\partial z} = b'. \quad (39.7)$$

### 39.2.1 Dimensional parameters

Following the shallow water discussion in Section 38.3.1, we have the following dimensional parameters for the perfect Boussinesq fluid.

- LENGTH SCALES

- ★  $H$  = depth scale of a typical vertical structure in the fluid (e.g., the depth of the thermocline).
- ★  $L$  = horizontal/lateral length scale of motions under consideration.
- ★  $R$  = radius of the planet.

- VELOCITY SCALES

- ★  $U$  = horizontal velocity scale for fluid parcel motion.
  - ★  $W$  = vertical velocity scale for fluid parcel motion.

- PRESSURE AND BUOYANCY SCALES: Pressure is a contact force, acting on the boundary of an arbitrary fluid region, and buoyancy arises from the gravitational force that acts to raise or lower a fluid parcel depending on its density relative to the environment. They have scales given by the following.

- ★  $\Phi$  = scale for pressure fluctuations  $\varphi'$  (dimensions of pressure divided by density = length scale  $\times$  acceleration).
  - ★  $B$  = scale of buoyancy fluctuations  $b'$  (dimensions of acceleration).

- BODY FORCES: There are two body forces acting on the fluid, one from gravity and one from Coriolis.

- ★  $g$  = gravitational acceleration
  - ★  $f$  = Coriolis frequency

Contrary to the shallow water discussion in Section 38.3.1, we do not introduce a wave speed since it does not affect the asymptotics. We also dropped the bottom topography scale, assuming it is small for present purposes.

### 39.2.2 Physical dimensions and non-dimensional parameters

There are two physical dimensions in the Boussinesq system: length,  $L$ , and time,  $T$ . As for the shallow water system, there no mass since mass is determined by the density (buoyancy) and volume. The Buckingham-II theorem then says there are

$$N_{\text{dimensionless}} = 9 - 2 = 7 \quad (39.8)$$

non-dimensional parameters.

### 39.2.3 Choosing the non-dimensional parameters

Following the shallow water discussion in Section 38.3.4, we choose the following non-dimensional parameters.

1. VERTICAL TO HORIZONTAL ASPECT RATIO: The ratio of the vertical scale to the horizontal scale defines the aspect ratio

$$\delta_{\text{vertical/horizontal}} = \frac{\text{vertical depth scale}}{\text{horizontal length scale}} = \frac{H}{L}. \quad (39.9)$$

2. RATIO OF HORIZONTAL SCALE TO PLANETARY SCALE: The ratio of the lateral length scale to the planet radius is given by

$$\delta_{\text{horizontal/planet}} = \frac{\text{lateral length scale}}{\text{planetary length scale}} = \frac{L}{R}. \quad (39.10)$$

3. RATIO VERTICAL TO HORIZONTAL VELOCITY SCALE: The ratio of the vertical to horizontal velocity is given by

$$\frac{\text{vertical velocity scale}}{\text{horizontal velocity scale}} = \frac{W}{U}. \quad (39.11)$$

4. HYDROSTATIC NUMBER: The hydrostatic number is the ratio of the pressure gradient scale to the buoyancy scale. For the hydrostatic fluid fluctuations

$$\frac{\Phi}{H} = B, \quad (39.12)$$

where  $B$  is the scale for the buoyancy fluctuations.

5. ROSSBY NUMBER: The Rossby number is the ratio of the fluid parcel acceleration scale to the Coriolis acceleration

$$\text{Ro} = \frac{\text{parcel acceleration}}{\text{Coriolis acceleration}} = \frac{U}{fL}, \quad (39.13)$$

where we again assume time scales advectively

$$T \sim \frac{L}{U} \implies \text{Ro} = \frac{U}{fL} = \frac{1}{fT}. \quad (39.14)$$

6. GEOSTROPHIC NUMBER: The ratio of the Coriolis acceleration to the pressure gradient acceleration defines the geostrophic number

$$\text{Ge} = \frac{\text{Coriolis acceleration}}{\text{pressure gradient acceleration}}. \quad (39.15)$$

The Coriolis acceleration scales as

$$\text{Coriolis acceleration} \sim fU \quad (39.16)$$

whereas the pressure gradient acceleration from the fluctuating pressure,  $\varphi'$ , scales as

$$\text{pressure gradient acceleration} \sim \frac{\Phi}{L}, \quad (39.17)$$

so that

$$\text{Ge} = \frac{\text{Coriolis acceleration}}{\text{pressure gradient acceleration}} = \frac{fU}{(\Phi/L)}. \quad (39.18)$$

7. RATIO OF FLUCTUATING STRATIFICATION TO BACKGROUND STRATIFICATION: The ratio of the buoyancy frequency arising from the fluctuating buoyancy,  $B/H$ , to the background buoyancy frequency,  $N^2$ , is given by

$$\frac{\text{fluctuating buoyancy frequency}}{\text{background buoyancy frequency}} = \frac{B/H}{N^2}. \quad (39.19)$$

### 39.2.4 Relating the buoyancy scale to the Coriolis acceleration scale

The fluctuating buoyancy ( $b'$ ) and fluctuating pressure ( $\varphi'$ ) have scales related through the hydrostatic balance. From equation (39.12) we have

$$B = \frac{\Phi}{H}. \quad (39.20)$$

Additionally, assuming geostrophic scaling, equation (39.18) means that the fluctuating pressure has a scale related to the Coriolis acceleration scale according to

$$\Phi = f U L. \quad (39.21)$$

Hence, the scale for the fluctuating buoyancy is given by

$$B = \frac{f U L}{H}. \quad (39.22)$$

### 39.2.5 Richardson number and QG/PG flow regimes

The *Richardson number* is the non-dimensional ratio of the squared buoyancy frequency to the squared vertical shear of the horizontal velocity

$$\text{Ri} = \frac{N^2}{|\partial_z \mathbf{u}|^2}. \quad (39.23)$$

In regions where  $\text{Ri} \ll 1$ , the vertical shear is stronger than the stabilizing effects from vertical stratification. In regions with small Richardson numbers, there is enough kinetic energy in the vertical shear to extract potential energy from the stratification, and this extraction process occurs via a dynamical instability known as *Kelvin-Helmholtz instability*. In contrast, for large-scale highly stratified flow, the Richardson number is quite large, with  $\text{Ri} \sim 100$  common. Large Richardson number flow regimes are where quasi-geostrophy is relevant (Chapter 40).

In our choice for dimensionless parameters, we could choose one determined by the scale for the Richardson number

$$\text{Ri} = \frac{N^2}{(U/H)^2}, \quad (39.24)$$

where we set the vertical scale equal to  $H$ , the horizontal velocity scale to  $U$ , and the squared buoyancy frequency to a scale  $N^2$ . Alternatively, the Richardson number can be related to the Rossby and Burger numbers through

$$\text{Bu} = \left[ \frac{L_d}{L} \right]^2 = \left[ \frac{N H}{f L} \right]^2 = \frac{U^2 \text{Ri}}{U^2 / (\text{Ro})^2} = (\text{Ro})^2 \text{Ri}. \quad (39.25)$$

One further way to write the Burger number is by introducing the angle  $\varphi$  defined by the vertical and horizontal length scales

$$\tan \varphi \equiv H/L \quad (39.26)$$

in which case

$$\text{Bu} = \left[ \frac{L_d}{L} \right]^2 = \left[ \frac{N H}{f L} \right]^2 = (\text{Ro})^2 \text{Ri} = [(N/f) \tan \varphi]^2. \quad (39.27)$$

When  $\tan^2 \varphi$  is set according to the slope of the ocean bottom, then  $[(N/f) \tan \varphi]^2$  is known as the *slope Burger number* (MacCready and Rhines, 1993; Peterson and Callies, 2022).

For QG flows, the horizontal length scales,  $L$ , are assumed to be on the order of the deformation radius,  $L_d$ , in which case the Burger number is close to unity. The relation (39.25) thus means that the Richardson number scales as

$$\text{Ri} \sim (\text{Ro})^{-2} \quad \text{QG flow regime.} \quad (39.28)$$

For atmospheric flows with a Rossby number order  $1/10$ , QG flow regimes are realized with a Richardson number  $\sim 100$ . For the ocean, the Rossby number can be even smaller, in which case QG flows are characterized by an even larger Richardson number. For planetary geostrophy, the Burger number is small, in which case PG flows are characterized by somewhat smaller Richardson numbers than QG flows.

### 39.2.6 The Rossby deformation radius

The combined effects of buoyancy and rotation yield the richness of continuously stratified planetary geostrophic and quasi-geostrophic motions. Hence, the buoyancy frequency and the Coriolis parameter play central role in characterizing these flow regimes. The ratio of these two frequencies,  $N/f$ , in regions of nontrivial vertical stratification is typically around 100. Hence, rotational inertial oscillations (usually just called *inertial oscillations*) have about 100 times longer period,  $2\pi/f$ , than buoyancy oscillations with period  $2\pi/N$ .

Letting the squared buoyancy frequency  $N^2$  refer to a value typical of a particular flow regime, one can define the Rossby deformation radius

$$L_d = H N/f. \quad (39.29)$$

As defined, the deformation radius is the vertical length scale multiplied by the ratio of the buoyancy frequency to the Coriolis frequency. The ratio  $f/N$  appears frequently in rotating/stratified fluids, and is sometimes called the Prandtl ratio

$$\frac{f}{N} = \text{Prandtl ratio.} \quad (39.30)$$

With  $H \approx 1$  km and  $N/f \approx 100$ , the Rossby deformation radius is roughly 100 km. This length scale measures the relative importance of stratification and rotation. Depending on the ratio  $L/L_d$ , we can have large or small stratification fluctuations relative to the background stratification. Furthermore, it sets the scale for unstable baroclinic waves leading to baroclinically unstable flow (see Chapter 6 of [Vallis \(2017\)](#)). For some context, recall the shallow water deformation radius is given by equation (38.31),  $L_d = \sqrt{gH}/f$ , which is the ratio of the gravity wave speed to Coriolis frequency. With  $N = 100$  f =  $10^{-2}$  s<sup>-1</sup> and  $H = 10^3$  m, the shallow water deformation radius is about an order of magnitude larger than the internal deformation radius. This means that the characteristic length scales, as set by  $L_d$ , are much larger in a shallow water fluid than in a stratified fluid.

### 39.2.7 Assumed values for the non-dimensional parameters

We now enumerate the assumed values for the non-dimensional parameters, again largely following the choices made for the shallow water in Section 38.3.5. These assumptions are guided by the regimes of interest to our analysis. In turn, the assumptions limit the validity of the resulting equations to those regimes.

1. SMALL VERTICAL TO HORIZONTAL ASPECT RATIO: The aspect ratio is generally small for large-scale atmospheric and oceanic fluid systems

$$\delta_{\text{vertical/horizontal}} \ll 1. \quad (39.31)$$

This assumption is part of the hydrostatic approximation (Section 22.2).

2. SMALL OR ORDER ONE RATIO OF HORIZONTAL TO PLANETARY SCALES: The ratio of the lateral length scale to the planet radius is small for quasi-geostrophic systems, and order unity for planetary geostrophy

$$\delta_{\text{horizontal/planet}} \ll 1 \quad \text{quasi-geostrophy} \quad (39.32a)$$

$$\delta_{\text{horizontal/planet}} \sim 1 \quad \text{planetary geostrophy.} \quad (39.32b)$$

3. SMALL RATIO VERTICAL TO HORIZONTAL VELOCITY SCALE: The continuity equation implies

$$\frac{W}{H} = \frac{U}{L}, \quad (39.33)$$

so that

$$W = U \frac{H}{L}. \quad (39.34)$$

As noted above, for a hydrostatic fluid the vertical to horizontal aspect ratio  $H/L$  is small, so that the vertical velocity scale is smaller than the horizontal velocity scale. Furthermore, when the fluid is close to geostrophically balanced, the vertical velocity scale is even smaller, by a factor of  $\text{Ro}$ . We will see that factor emerge in the following scale analysis.

4. UNIT HYDROSTATIC NUMBER: As already noted, the hydrostatic balance (39.1b) means that the scales for a buoyancy fluctuation and pressure fluctuation are related by (see equation (39.12))

$$\Phi = H B. \quad (39.35)$$

5. SMALL ROSSBY NUMBER: The Rossby number is assumed small

$$\text{Ro} = \frac{U}{f L} = \frac{1}{f T} \ll 1, \quad (39.36)$$

where we set the time scale according to advection,  $T = L/U$ .

6. UNIT GEOSTROPHIC NUMBER: The geostrophic number is assumed to be order unity

$$\text{Ge} \sim 1, \quad (39.37)$$

which means that the Coriolis acceleration and pressure gradient acceleration scale together

$$f U \sim \frac{\Phi}{L}. \quad (39.38)$$

This scaling is consistent with the momentum equation (39.1a) so long as the Rossby number is small,  $\text{Ro} \ll 1$ .

7. STRATIFICATION FLUCTUATIONS COMPARED TO BACKGROUND STRATIFICATION: Making use of the assumed unit geostrophic number, the ratio of the buoyancy frequency arising

from the fluctuating buoyancy to the background buoyancy frequency is given by

$$\frac{B/H}{N^2} = \frac{\Phi}{H^2 N^2} = \frac{f U L}{H^2 N^2} = \frac{U}{f L} \frac{L^2 f^2}{H^2 N^2} = \text{Ro} \frac{L^2}{L_d^2}, \quad (39.39)$$

where we introduced the deformation radius (39.29)  $L_d = H N/f$ . It is important to keep the depth dependence of  $N^2$  when returning to dimensional fields, particularly for the QG system in Section 40.3.7.

### 39.2.8 Non-dimensional Boussinesq equations

Following the shallow water approach in Section 38.3.7, we introduce non-dimensional variables according to

$$t = T \hat{t} \quad (x, y) = L(\hat{x}, \hat{y}) \quad \partial_t = \partial_{\hat{t}}/T \quad \nabla_z = \hat{\nabla}_z/L \quad \partial_z = \partial_{\hat{z}}/H \quad f = f_0 \hat{f} \quad (39.40a)$$

$$(u, v) = U(\hat{u}, \hat{v}) \quad w = W \hat{w} \quad \varphi' = f_0 U L \hat{\varphi} \quad b' = B \hat{b} = (f_0 U L / H) \hat{b}. \quad (39.40b)$$

For the second equality in the buoyancy scale, we made use of equation (39.22) to connect the buoyancy fluctuation scale to the Coriolis acceleration scale. We also make use of the following relations between scales

$$T = L/U \quad \text{advective scaling for } T \quad (39.41)$$

$$W = U H / L \quad \text{continuity scaling for } W \quad (39.42)$$

$$\text{Ro} = U/(f_0 L) = (T f_0)^{-1} \quad \text{advective scaling for } T. \quad (39.43)$$

The first relation assumes the time scale is determined by the advection time  $T = L/U$ , which then means that the Rossby number is the ratio of the advective frequency  $1/T$  to the Coriolis frequency  $f_0$ . Furthermore, we assume vertical velocity scales according to the continuity equation,  $w = U(H/L)$ . This continuity scaling for  $W$  will be seen to be an over-estimate in the following, where we find that  $W$  instead scales like  $W = \text{Ro} U (H/L)$ .

#### *Non-dimensional momentum equation*

Introducing the above dimensionless variables and dimensionful scales into the Boussinesq momentum equation (39.1a) renders

$$\frac{U}{T} \frac{\partial \hat{\mathbf{u}}}{\partial \hat{t}} + \frac{U^2}{L} (\hat{\mathbf{u}} \cdot \hat{\nabla}_z) \hat{\mathbf{u}} + \frac{W U}{H} \hat{w} \frac{\partial \hat{\mathbf{u}}}{\partial \hat{z}} + f_0 U (\hat{\mathbf{f}} \times \hat{\mathbf{u}}) = -f_0 U \hat{\nabla}_z \hat{\varphi}. \quad (39.44)$$

Hence, dividing by  $f_0 U$  leads to

$$\text{Ro} \left[ \frac{\partial \hat{\mathbf{u}}}{\partial \hat{t}} + (\hat{\mathbf{u}} \cdot \hat{\nabla}_{\hat{z}}) \hat{\mathbf{u}} + \hat{w} \frac{\partial \hat{\mathbf{u}}}{\partial \hat{z}} \right] + (\hat{\mathbf{f}} \times \hat{\mathbf{u}}) = -\hat{\nabla}_z \hat{\varphi}. \quad (39.45)$$

The momentum equation is consistent with a unit geostrophy number (i.e., Coriolis acceleration balances pressure gradient acceleration) if and only if the Rossby number is small, thus eliminating the acceleration of a fluid parcel. Likewise, the non-dimensional hydrostatic balance is given by

$$\frac{\partial \hat{\varphi}}{\partial \hat{z}} = \hat{b}, \quad (39.46)$$

and the non-dimensional continuity equation is

$$\hat{\nabla} \cdot \hat{\mathbf{v}} = 0. \quad (39.47)$$

#### Non-dimensional buoyancy equation

The buoyancy equation (39.4) requires a bit more work to non-dimensionalize. The material time derivative takes the form

$$\frac{Db'}{Dt} = \frac{B}{T} \frac{D\hat{b}}{Dt} = \frac{U}{L} \frac{f_0 U L}{H} \frac{D\hat{b}}{Dt} = \frac{f_0 U^2}{H} \frac{D\hat{b}}{Dt}, \quad (39.48)$$

where we made use of the advective scaling  $T = L/U$  and continuity scaling  $W = U(H/L)$ . The vertical advection of background stratification is given by

$$N^2 w = N^2 W \hat{w} = N^2 U (H/L) \hat{w} = L_d^2 \frac{U f_0^2}{H L} \hat{w}, \quad (39.49)$$

where we introduced the deformation radius,  $L_d = HN/f$ , from equation (39.29). Bringing these two pieces together leads to

$$\text{Ro} \frac{D\hat{b}}{Dt} + \text{Bu} \hat{w} = 0, \quad (39.50)$$

where we introduced the Burger number  $\text{Bu} = (L_d/L)^2$ .

### 39.3 Summary equations for planetary geostrophy

Just like for the shallow water model in Section 38.4, the planetary geostrophic system for the stratified Boussinesq system is a rather simple asymptotic theory. For this case, we assume the horizontal scales are large compared to the deformation radius, so that

$$\text{Ro}/\text{Bu} \sim 1 \implies \text{Ro} L^2 \sim L_d^2. \quad (39.51)$$

With this scaling, and with a small Rossby number, the momentum equation (39.45) reduces to geostrophic balance. However, the continuity and buoyancy equations retain their unapproximated Boussinesq form. Hence, in dimensional form, the perfect (adiabatic and inviscid) planetary geostrophic equations for a stratified Boussinesq fluid are

$$\frac{Db'}{Dt} + w N^2 = 0 \quad (39.52a)$$

$$f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla_z \varphi' \quad (39.52b)$$

$$\frac{\partial \varphi'}{\partial z} = b' \quad (39.52c)$$

$$\nabla \cdot \mathbf{v} = 0. \quad (39.52d)$$

We could just as well write the above planetary geostrophic equations in terms of the full buoyancy  $b = \tilde{b}(z) + b'$ , and full pressure,  $p = p_0(z) + \rho_0 \varphi$ . Additionally, we can include non-conservative terms such as buoyancy mixing,  $\dot{b}$ , as well as frictional accelerations and/or boundary forcing,  $\mathbf{F}$ . The following form for the frictional and diabatic planetary geostrophic flow will form

the basis for many discussions in this chapter

$$f \hat{z} \times \mathbf{u} = -\rho_0^{-1} \nabla_z p + \mathbf{F} \quad \text{frictional geostrophy} \quad (39.53a)$$

$$\frac{\partial b}{\partial t} + \mathbf{u} \cdot \nabla_z b + N^2 w = \dot{b} \quad \text{diabatic buoyancy equation} \quad (39.53b)$$

$$\frac{\partial p}{\partial z} = -\rho g \quad \text{hydrostatic balance} \quad (39.53c)$$

$$\nabla \cdot \mathbf{v} = \nabla_z \cdot \mathbf{u} + \frac{\partial w}{\partial z} = 0 \quad \text{incompressible flow} \quad (39.53d)$$

$$N^2 = \frac{\partial b}{\partial z} \quad \text{squared buoyancy frequency.} \quad (39.53e)$$

We will also generally assume an equation of state that is independent of pressure, so that changes in buoyancy arise only from changes in potential temperature and/or salinity

$$\dot{b} = \frac{\partial b}{\partial S} \dot{S} + \frac{\partial b}{\partial \Theta} \dot{\Theta}. \quad (39.54)$$

The buoyancy partial derivatives,  $\partial b / \partial \Theta$  and  $\partial b / \partial S$ , will sometimes be assumed constant.

Note that the material time derivative in PG makes use of advection by the three velocity components,  $\mathbf{v} = (\mathbf{u}, w)$ , as seen in the buoyancy equation (39.53b), with the horizontal velocity components determined by the frictional geostrophic balance (39.52b). This situation contrasts to the case of QG, where it is only the horizontal advection by the geostrophic flow that contributes to material time evolution (Section 40.2).

## 39.4 Planetary geostrophic potential vorticity

In Section 36.5 we developed the potential vorticity equation for the hydrostatic Boussinesq system in the presence of horizontal friction in the momentum equation and diabatic terms in the buoyancy equation. Here we specialize that result to the case of planetary geostrophic system written in the form of equations (39.53a)-(39.53e).

### 39.4.1 Derivation

Derivation of the PV equation proceeds much like that for the hydrostatic Boussinesq system. The first step requires the PG vorticity equation as determined by taking the curl of the momentum equation (39.53a). The vertical component of this vorticity equation is given by (see also Section 25.5.2)

$$\beta v = f \frac{\partial w}{\partial z} + \hat{z} \cdot (\nabla_z \times \mathbf{F}) \quad \text{with} \quad \beta = \frac{\partial f}{\partial y}. \quad (39.55)$$

Next make use of the thermal wind relation in the presence of friction

$$f \frac{\partial \mathbf{u}}{\partial z} = \hat{z} \times \nabla_z b - \frac{\partial(\hat{z} \times \mathbf{F})}{\partial z} \quad (39.56)$$

as well as the identities

$$N^2 \frac{Df}{Dt} = N^2 \beta v \quad (39.57a)$$

$$f \frac{DN^2}{Dt} = f \frac{\partial \dot{b}}{\partial z} - f \nabla b \cdot \frac{\partial \mathbf{v}}{\partial z} \quad (39.57b)$$

$$f \nabla b \cdot \frac{\partial \mathbf{v}}{\partial z} = f N^2 \frac{\partial w}{\partial z} - \frac{\partial(\hat{\mathbf{z}} \times \mathbf{F})}{\partial z} \cdot \nabla_z b, \quad (39.57c)$$

to render

$$\frac{D(f N^2)}{Dt} = N^2 \beta v + f \frac{\partial \dot{b}}{\partial z} - f \nabla b \cdot \frac{\partial \mathbf{v}}{\partial z} \quad (39.58a)$$

$$= N^2 \left[ f \frac{\partial w}{\partial z} + \hat{\mathbf{z}} \cdot (\nabla_z \times \mathbf{F}) \right] + f \frac{\partial \dot{b}}{\partial z} - f N^2 \frac{\partial w}{\partial z} + \frac{\partial(\hat{\mathbf{z}} \times \mathbf{F})}{\partial z} \cdot \nabla_z b \quad (39.58b)$$

$$= f \frac{\partial \dot{b}}{\partial z} + \nabla b \cdot (\nabla \times \mathbf{F}) \quad (39.58c)$$

$$= \nabla \cdot (f \dot{b} \hat{\mathbf{z}} + \mathbf{F} \times \nabla b). \quad (39.58d)$$

We thus identify the planetary geostrophic potential vorticity

$$Q_{PG} = f N^2, \quad (39.59)$$

which is materially invariant in the absence of diabatic processes and friction

$$\frac{DQ_{PG}}{Dt} = 0 \quad \text{when } \dot{b} = 0 \text{ and } \mathbf{F} = 0. \quad (39.60)$$

We can write the general budget equation in the form of an Eulerian flux-form expression

$$\frac{\partial Q_{PG}}{\partial t} + \nabla \cdot \mathbf{J}_{PG} = 0, \quad (39.61)$$

where the potential vorticity flux is given by

$$\mathbf{J}_{PG} = \mathbf{v} Q_{PG} - \dot{b} f \hat{\mathbf{z}} + \nabla b \times \mathbf{F} + \nabla \times \mathbf{A}. \quad (39.62)$$

The vector  $\mathbf{A}$  is an arbitrary gauge function that has no impact on the potential vorticity evolution. Comparing to the hydrostatic Boussinesq case from Section 36.5.2, we see that the planetary geostrophic result follows by dropping contributions from the relative vorticity and dropping the inertial acceleration.

### 39.4.2 Impermeability theorem

Following the discussion in Section 37.2.2, we here verify that the potential vorticity flux vector (39.62) satisfies the impermeability theorem for buoyancy isosurfaces. We do so here for the particular case of a zero gauge function ( $\mathbf{A} = 0$ ), in which case

$$\mathbf{v}_{PG} \cdot \nabla b = \frac{\mathbf{J}_{PG} \cdot \nabla b}{Q} = \mathbf{v} \cdot \nabla b - \dot{b} = -\frac{\partial b}{\partial t}, \quad (39.63)$$

so that

$$\frac{\partial b}{\partial t} + \mathbf{v}_{PG} \cdot \nabla b = 0. \quad (39.64)$$

Hence, there is zero flux of PV-substance crossing buoyancy isosurfaces, even in the presence of irreversible processes that allow matter and heat to cross those surfaces. As shown in the next subsection, we identify two more forms of the PV-substance flux vector that also satisfy impermeability, with these alternative forms differing by gauge transformations.

### 39.4.3 Kinematic fluxes satisfying impermeability

Following the discussion of impermeability for the Ertel PV in Section 37.2.2, we expose a purely kinematic means to derive the impermeability theorem for the PG potential vorticity. This derivation follows by computing the time tendency of the PV

$$\frac{\partial Q}{\partial t} = \frac{\partial}{\partial t} \nabla \cdot (f b \hat{z}) = \nabla \cdot \left[ f \frac{\partial b}{\partial t} \hat{z} \right] \equiv -\nabla \cdot \tilde{\mathbf{J}}_{\text{PG}}, \quad (39.65)$$

where

$$\tilde{\mathbf{J}}_{\text{PG}} = -f \frac{\partial b}{\partial t} \hat{z}. \quad (39.66)$$

This form of the PV-substance flux also satisfies impermeability since

$$\tilde{\mathbf{v}}_{\text{PG}} \cdot \nabla b = \frac{\tilde{\mathbf{J}}_{\text{PG}} \cdot \nabla b}{Q} = -\frac{\partial b}{\partial t}, \quad (39.67)$$

so that

$$\frac{\partial b}{\partial t} + \tilde{\mathbf{v}}_{\text{PG}} \cdot \nabla b = 0. \quad (39.68)$$

The flux  $\tilde{\mathbf{J}}_{\text{PG}}$  vanishes in the steady state, whereas the steady state form of  $\mathbf{J}_{\text{PG}}$  does not vanish. Following the discussion in Section 37.3.2, we may choose to introduce a gauge transformation to the kinematic flux  $\tilde{\mathbf{J}}_{\text{PG}}$  so that it does not vanish in the steady state. Taking the small Rossby number limit of the flux (37.35) renders

$$\mathbf{J}_{\text{Q}}^{\text{marshall PG}} = -\nabla(g z + \varphi) \times \nabla b - f \frac{\partial b}{\partial t} \hat{z}. \quad (39.69)$$

This flux differs from  $\tilde{\mathbf{J}}_{\text{PG}}$  by a curl

$$\nabla(g z + \varphi) \times \nabla b = \nabla \times [(g z + \varphi) \nabla b], \quad (39.70)$$

and it also satisfies the impermeability theorem. As discussed in Section 37.5.6, there are a variety of motivations for using one form of the PV-substance flux versus another. Some applications prefer a nonzero steady flux that also does not involve any irreversible processes, with  $\mathbf{J}_{\text{Q}}^{\text{marshall PG}}$  satisfying these desires.

## 39.5 Depth integrated vorticity budget

In a planetary geostrophic flow, vorticity arises just from planetary rotation since relative vorticity is assumed to be negligible. With planetary vorticity a function just of latitude, a budget for the planetary geostrophic vorticity reveals how the curl of forces imparted to the fluid cause meridional motion as the fluid meets the constraints imposed by the vorticity equation. As per our discussion in Section 35.4.5, we commonly refer to a force curl as a “torque” in our study of vorticity sources, with that terminology common in the study of vorticity budgets. However, one must keep in mind that more common usage in physics refers to a torque as affecting changes to angular momentum,

with angular momentum generally distinct from vorticity (see Section 32.7 for a discussion of the distinction).

In this section we study the depth integrated vorticity budget for the planetary geostrophic fluid and derive implications for the meridional flow. For this purpose we focus on frictional and boundary accelerations that take the form of a vertical divergence of horizontal turbulent stresses

$$\mathbf{F} = \frac{\partial \boldsymbol{\tau}}{\partial z}. \quad (39.71)$$

The curl of this stress, as well as pressure forces, provide sources (“torques”) that generate meridional motion as revealed by the planetary geostrophic vorticity budget.

### 39.5.1 The $\beta$ -effect, stretching, and meridional transport

In Section 25.5.2 we derived the vorticity equation for the planetary geostrophic system. We also encountered this equation when deriving the potential vorticity budget in Section 39.4.1. With friction written as a vertical divergence of horizontal turbulent stresses (equation (39.71)), the vertical component of the planetary geostrophic vorticity equation takes the form

$$\rho_0 \beta v = \frac{\partial}{\partial z} [\rho_0 f w + \hat{\mathbf{z}} \cdot (\nabla_z \times \boldsymbol{\tau})]. \quad (39.72)$$

Vertical integration from the ocean bottom at  $z = \eta_b(x, y)$  to sea surface at  $z = \eta(x, y, t)$  leads to

$$\rho_0 \beta V = \underbrace{\rho_0 f [w(\eta) - w(\eta_b)]}_{\text{column stretching}} + \underbrace{\hat{\mathbf{z}} \cdot (\nabla_z \times \Delta \boldsymbol{\tau})}_{\text{boundary stresses}}, \quad (39.73)$$

where

$$\Delta \boldsymbol{\tau} = \boldsymbol{\tau}(\eta) - \boldsymbol{\tau}(\eta_b) \quad (39.74)$$

is the difference in boundary stresses applied at the ocean surface and ocean bottom, and

$$V = \int_{\eta_b}^{\eta} v \, dz \quad (39.75)$$

is the depth-integrated meridional flow. For a planetary geostrophic flow, absolute vorticity is approximated by just the planetary vorticity:  $\zeta_a = \zeta + f \approx f$ . As revealed by the vorticity equation (39.73), vorticity sources in a planetary geostrophic fluid lead to meridional motion since that is the only way the fluid can modify its vorticity in response to the sources.

The first term on the right hand side of equation (39.73) arises from vertical stretching of the depth integrated column as measured by differences in the vertical velocity at the ocean surface and bottom. For example, vertical stretching caused by positive surface velocity,  $w(\eta) > 0$ , or a negative bottom velocity,  $w(\eta_b) < 0$ , lead to poleward motion of the fluid column. Conversely, vertical squashing leads to equatorward motion. We emphasize that the vertical stretching term arises from the difference in the boundary vertical velocity rather than the vertical velocity within the interior of the fluid.

The second term in equation (39.73) arises from differences in the vorticity imparted by surface and bottom boundary stresses. Positive vorticity imparted to the fluid through the curl of wind stresses,  $\hat{\mathbf{z}} \cdot [\nabla_z \times \boldsymbol{\tau}(\eta)] > 0$ , or by the curl of bottom stresses,  $\hat{\mathbf{z}} \cdot [\nabla_z \times \boldsymbol{\tau}(\eta_b)] < 0$ , lead to poleward motion of the fluid column, with opposite motion for the converse curls.

The  $\beta$ -effect (Section 35.7.2) is a fundamental element of the depth integrated vorticity equation (39.73). Namely, as fluid columns are stretched or squashed, they must move meridionally

to maintain vorticity balance for a planetary geostrophic fluid on a rotating spherical earth. The planetary geostrophic vorticity equation restricts attention to vertical stretching through vertical motion (the  $w$  terms) and through the vorticity imparted by the curl of boundary stresses. Notably, the curl of boundary stresses also imparts vertical motion through surface and bottom Ekman layer dynamics (see Chapter 27). Hence, the right hand side of the vorticity equation (39.73) is fundamentally related to vortex stretching.

Equation (39.73) is central to mechanical descriptions of large-scale ocean circulation. For many flow regimes, the curl of the surface wind stress dominates, thus allowing us to ignore the vertical velocity terms as well as bottom frictional stresses. Formally, we isolate the wind stress when studying a flat bottom rigid lid model, whereby  $w(\eta) = w(\eta_b) = 0$ . However, there can be nontrivial impacts from bottom pressure torques when flow interacts with sloping topography, with the North Atlantic and Southern Ocean providing important case studies. Other processes can be important in various flow regimes, thus prompting us to derive a full diagnostic framework to identify where these processes are important. To pursue that framework, we make use of the kinematic boundary conditions and the horizontal momentum equation to unpack the vertical velocity terms. Doing so reveals the forces and their curls that drive vertical motion at the boundaries for a planetary geostrophic flow. By doing so, we capture how these force curls contribute, through the  $\beta$ -effect, to meridional motion of the depth integrated flow.

### 39.5.2 Bottom kinematics and dynamics

The bottom kinematic boundary condition applied at  $z = \eta_b(x, y)$  (Section 14.4.1) is given by

$$w = \mathbf{u} \cdot \nabla_z \eta_b \quad \text{at } z = \eta_b(x, y). \quad (39.76)$$

This relation expresses the no-normal flow condition  $\hat{\mathbf{n}} \cdot \mathbf{v} = 0$  at the ocean bottom, with  $\hat{\mathbf{n}} = -\nabla(z - \eta_b)/|\nabla(z - \eta_b)|$  the outward normal to the bottom. The boundary condition constrains the flow so that any horizontal motion next to a sloping bottom that is oriented either up or down the slope must have an associated vertical motion. As we see in this section, such vertical motion next to the bottom boundary arises from force curls acting to stretch or squash a fluid column. In turn, through the vorticity equation (39.73), vertical motion at the bottom leads to meridional motion of the full fluid column.

#### *Expressions for bottom vertical velocity*

The bottom kinematic boundary condition holds for all dynamical flow regimes. For the particular case of planetary geostrophy, we garner insight into the forces that drive vertical flow near the bottom by making use of the planetary geostrophic momentum equation (39.53a). Evaluating the horizontal components of this equation at the ocean bottom yields

$$\rho_0 f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla_z p_b + \mathbf{F}_b, \quad (39.77)$$

where  $p_b(x, y, t)$  is the bottom pressure and  $\mathbf{F}_b$  is the bottom friction. For the special case of a no-slip bottom, all velocity components vanish at  $z = \eta_b$ . In that case, we consider  $\mathbf{u}$  in equation (39.77) to be the horizontal velocity averaged within the bottom boundary layer, and  $w$  the corresponding vertical velocity leaving the boundary layer.

It is convenient to decompose the bottom horizontal velocity into its geostrophic and Ekman<sup>1</sup> components via

$$\rho_0 f \hat{\mathbf{z}} \times \mathbf{u}_g = -\nabla_z p_b \quad \text{and} \quad \rho_0 f \hat{\mathbf{z}} \times \mathbf{u}_e = \mathbf{F}_b, \quad (39.78)$$

<sup>1</sup>Recall our discussion of Ekman mechanics in Chapter 27.

so that

$$\mathbf{u}_g = \frac{\hat{\mathbf{z}} \times \nabla_z p_b}{\rho_0 f} \quad \text{and} \quad \mathbf{u}_e = -\frac{\hat{\mathbf{z}} \times \mathbf{F}_b}{\rho_0 f}. \quad (39.79)$$

The corresponding bottom vertical velocity components are determined by inserting equations (39.79) into the bottom kinematic boundary condition (39.76)

$$w_g = \frac{\hat{\mathbf{z}} \cdot (-\nabla_z \eta_b \times \nabla_z p_b)}{\rho_0 f} \quad \text{and} \quad w_e = \frac{\hat{\mathbf{z}} \cdot (\nabla_z \eta_b \times \mathbf{F}_b)}{\rho_0 f}. \quad (39.80)$$

These equations reveal how the curl of inviscid pressure forces and boundary frictional forces drive a nonzero vertical motion next to the bottom, all while maintaining the bottom kinematic boundary condition (39.76). As seen by these equations, is only the projection of  $\nabla_z p_b$  and  $\mathbf{F}_b$  onto the isobath direction that contributes to a nonzero vertical velocity. These along-isobath forces are needed to render a horizontal velocity that is itself misaligned with isobaths, thus satisfying the kinematic requirement for vertical motion.

To further understand the bottom pressure term, we write it as

$$w_g = \frac{\hat{\mathbf{z}} \cdot (-\nabla_z \eta_b \times \nabla_z p_b)}{\rho_0 f} = \frac{\hat{\mathbf{z}} \cdot [\nabla_z \times p_b \nabla_z \eta_b]}{\rho_0 f}. \quad (39.81)$$

The numerator is the curl of the horizontal projection of the pressure contact force along the bottom,  $p_b \nabla_z \eta_b$ . This term is the topographic form stress discussed in Section 19.2 for a general fluid and in Section 34.9.5 for the shallow water. We thus conclude that vertical geostrophic motion next to the bottom arises from the curl of the topographic form stress. This is an important result that will appear again within this section as well as in Sections 39.7 and 39.8.

#### *Comments on the bottom vertical geostrophic velocity*

A large part of the bottom pressure gradient driving the horizontal geostrophic flow in equation (39.79) arises from changes in bottom depth. However, that portion of the bottom pressure gradient has no impact on  $w_g$ , since it only drives horizontal flow along isobaths. We see this property by writing

$$p_b = -\rho_0 g \eta_b + p'_b \implies w_g = \frac{\hat{\mathbf{z}} \cdot (-\nabla_z \eta_b \times \nabla_z p'_b)}{\rho_0 f}. \quad (39.82)$$

When there is misalignment between isolines of bottom pressure and bottom topography, the geostrophic flow in a fluid column will cross isobaths. Correspondingly, with the pressure force misaligned with topographic gradients, the fluid column experiences a twisting action akin to how baroclinicity spins a fluid element if the pressure force does not act through the fluid element's center of mass (see Section 35.5).

To illustrate the above, consider the topographic bowl in Figure 39.1, with sides steep enough so that the bottom pressure gradient is dominated by the topographic slopes. Along the bottom the pressure increases moving down (increasing depth) towards the bowl center. The corresponding bottom geostrophic flow is anti-cyclonic within the bowl and largely follows isobaths. As already noted, if the geostrophic flow exactly follows isobaths, then there is no corresponding vertical component to the bottom velocity. A vertical velocity arises only in the presence of an anomalous bottom pressure gradient,  $\nabla_z p'_b$ , that is misaligned with the bottom slope,  $\nabla \eta_b$ . This bottom pressure gradient balances a geostrophic flow that deviates from isobaths thus giving rise to a nonzero  $w_g$ . Similar geometric analysis holds for the bottom friction vector,  $\mathbf{F}_b$ , and how it gives rise to a nonzero vertical Ekman velocity,  $w_e$ .

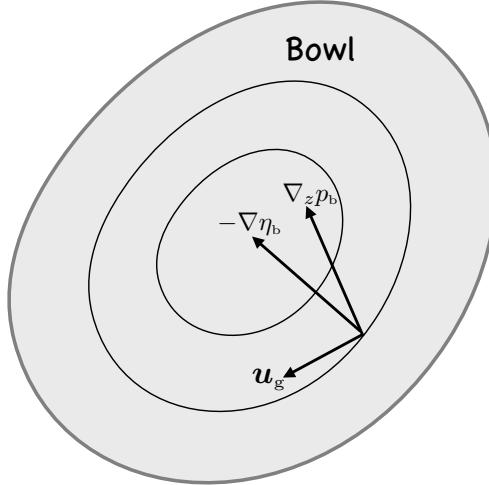


FIGURE 39.1: Depicting how bottom pressure gradients create vertical motion in planetary geostrophic flow next to a sloping bottom according to equations (39.80) and (39.82). Here we show a bowl or depression (local maximum in the depth) with  $-\eta_b$  increasing inward toward the bowl center. Only those portions of  $\nabla_z p_b$  and  $\mathbf{F}_b$  that are aligned parallel to the topographic slope contribute to vertical motion. We illustrate here a case where the bottom pressure gradient leads to  $-\nabla \eta_b \cdot \mathbf{u}_g > 0$  so that  $w_g < 0$  in the northern hemisphere and  $w_g > 0$  in the southern hemisphere (see equations (39.80) and (39.82)).

*What causes misalignment between  $p_b$  and  $\eta_b$ ?*

As we just discussed, misalignment of  $p_b$  and  $\eta_b$  lead to vertical geostrophic motion along the bottom. In Section 39.5.3 we will see a similar relation for vertical geostrophic motion at the ocean surface. But what causes such misalignment? The answer to this question is circular when working within the planetary geostrophic whose momentum equation is diagnostic. Even so, we can offer some insight by returning to the depth-integrated vorticity balance (39.73) and rewriting it as an expression for vertical motion

$$\rho_0 f [w(\eta_b) - w(\eta)] = -\rho_0 \beta V + \hat{\mathbf{z}} \cdot (\nabla_z \times \Delta \boldsymbol{\tau}). \quad (39.83)$$

Hence, vertical motion at the surface and bottom arise from meridional motion in the presence of planetary beta, plus the curl of surface and bottom stresses. The absence of planetary beta, and the absence of boundary stress curls, realizes  $w(\eta_b) = w(\eta)$ , with zero vertical motion the typical case.

### 39.5.3 Surface kinematics and dynamics

For purposes of large-scale circulation studies using the PG equations, it is generally sufficient to assume a rigid lid upper boundary condition, whereby  $w(\eta) = w(0) = 0$ . Even so, we find it revealing to present the results for a free surface in which there is the possibility of nonzero surface mass fluxes. The surface kinematic boundary condition for a Boussinesq fluid (Section 16.2) is given by

$$w = -\frac{Q_m}{\rho_0} + \frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla_z \eta \quad \text{at } z = \eta(x, y, t). \quad (39.84)$$

We retain the sea surface time tendency,  $\partial_t \eta$ , even though for transient solutions the time tendency is many orders of magnitude smaller than the typical vertical velocity under the planetary geostrophic regime.<sup>2</sup> Evaluating the horizontal planetary geostrophic momentum equation

<sup>2</sup>See Section 3.3 of [Samelson \(2011\)](#) for more details on this scaling of the planetary geostrophic system.

(25.23a) at the ocean surface renders

$$\rho_0 f \hat{z} \times \mathbf{u} = -\nabla_z p_a + \mathbf{F}_\eta, \quad (39.85)$$

where  $p_a$  is the pressure applied to the ocean surface and  $\mathbf{F}_\eta$  is the corresponding horizontal friction vector. Like the bottom, we decompose the horizontal velocity into a geostrophic component and an Ekman component via

$$\rho_0 f \hat{z} \times \mathbf{u}_g = -\nabla_z p_a \quad \text{and} \quad \rho_0 f \hat{z} \times \mathbf{u}_e = \mathbf{F}_\eta, \quad (39.86)$$

so that

$$\mathbf{u}_g = \frac{\hat{z} \times \nabla_z p_a}{\rho_0 f} \quad \text{and} \quad \mathbf{u}_e = -\frac{\hat{z} \times \mathbf{F}_\eta}{\rho_0 f}. \quad (39.87)$$

The corresponding vertical velocity components are determined by inserting into the surface kinematic boundary condition (39.84)

$$w_{Q\eta} = -\frac{Q_m}{\rho_0} + \frac{\partial \eta}{\partial t} \quad \text{and} \quad w_g = \frac{\hat{z} \cdot (-\nabla_z \eta \times \nabla_z p_a)}{\rho_0 f} \quad \text{and} \quad w_e = \frac{\hat{z} \cdot (\nabla_z \eta \times \mathbf{F}_\eta)}{\rho_0 f}, \quad (39.88)$$

where we introduced a vertical velocity,  $w_{Q\eta}$ , associated with the boundary mass flux and transient sea level fluctuations. As for the bottom, the second and third of these equations reveal how the curl of inviscid pressure forces and boundary frictional forces drive a nonzero vertical motion at the ocean surface, all while maintaining the surface kinematic boundary condition (39.84). Furthermore, it is only the projection of  $\nabla_z p_a$  and  $\mathbf{F}_\eta$  onto the direction parallel to sea surface height contours that contributes to a nonzero vertical velocity. This orientation of the surface forces is needed to render a horizontal velocity that is itself misaligned with sea surface height contours, thus satisfying the kinematics required to render vertical motion.

### 39.5.4 Summary of force curls driving depth integrated meridional flow

Plugging expressions (39.80), (39.82), and (39.88) into equation (39.73) renders the depth integrated planetary vorticity balance

$$\rho_0 \beta V = f (-Q_m + \rho_0 \partial_t \eta) + \hat{z} \cdot [\nabla_z \eta \times (\mathbf{F}_\eta - \nabla_z p_a) - \nabla_z \eta_b \times (\mathbf{F}_b - \nabla_z p'_b) + \nabla_z \times \Delta \tau]. \quad (39.89)$$

We see how the force curls are symmetrically applied at the surface and bottom, which is part of the motivation for exposing the surface terms even though they are generally subdominant. In general, equation (39.89) shows that the depth integrated meridional flow, within the planetary geostrophic regime, is driven by the following processes.

#### *Surface mass transport plus sea surface fluctuations*

The term  $f (-Q_m + \rho_0 \partial_t \eta)$  arises from mass transport across the ocean surface plus fluctuations in the sea surface height. For example, as sea surface height increases or as water leaves the ocean surface, they impart a positive surface vertical velocity,  $w(\eta) > 0$ , thus causing column stretching and poleward meridional depth integrated flow. In the steady state, where it is just the mass flux term that contributes, the meridional circulation is known as the Goldsbrough-Stommel circulation (see [Huang and Schmitt \(1993\)](#) for a review).

### Curl of turbulent boundary stresses

The term  $\hat{z} \cdot (\nabla_z \times \Delta\boldsymbol{\tau})$  arises from the curl of the turbulent wind stress and turbulent bottom stress. The wind stress term is generally larger than the bottom turbulent stress, with many theories for ocean circulation, particularly those with a flat bottom, almost exclusively focused on the role of surface stress in forcing the planetary geostrophic vorticity budget. We comment more on this case in Section 39.6 where we discuss the *Sverdrup balance*.

### Atmospheric pressure torque

The term

$$\nabla_z p_a \times \nabla_z \eta = \nabla_z \times (p_a \nabla_z \eta) = -\nabla_z \times (\eta \nabla_z p_a) \quad (39.90)$$

arises from differences in lines of constant atmospheric pressure and lines of constant sea surface height. Such misalignments create a torque akin to the baroclinicity detailed in Section 35.5, with these misalignments driving vertical motion and a corresponding depth integrated meridional flow.

### Bottom pressure torque

The term

$$\nabla_z p'_b \times (-\nabla_z \eta_b) = \nabla_z \times (-p'_b \nabla_z \eta_b) = \nabla_z \times (\eta_b \nabla_z p'_b) \quad (39.91)$$

arises from differences in lines of constant bottom pressure and lines of constant bottom topography. As for the atmospheric pressure torques, such misalignments create a torque that drives a depth integrated meridional flow, with this term vanishing when the bottom topography is flat. In many cases with strong flow next to sloping bottoms, this term can contribute more to the vorticity budget than the turbulent bottom stress. Indeed, in some cases it can rival contributions from the surface wind stress. We sketched out such cases for the shallow water when discussing western boundary currents in Section 34.9.5.

### Surface frictional acceleration

The term

$$\hat{z} \cdot (\nabla_z \eta \times \mathbf{F}_\eta) = \hat{z} \cdot \left[ \nabla_z \eta \times \frac{\partial \boldsymbol{\tau}_\eta}{\partial z} \right] \quad (39.92)$$

arises from evaluating the vertical divergence of the frictional stress at the sea surface. A finite volume boundary layer treatment of this term prompts us to integrate the stress divergence over the extent of the surface Ekman layer to render the alternative expression

$$\hat{z} \cdot \int_{-h_{e\text{-surf}}}^{\eta} \left[ \nabla_z \eta \times \frac{\partial \boldsymbol{\tau}}{\partial z} \right] dz = \hat{z} \cdot [\nabla_z \eta \times \boldsymbol{\tau}(\eta)], \quad (39.93)$$

where we assumed  $\boldsymbol{\tau}$  is negligible at the base of the surface Ekman layer,  $z = -h_{e\text{-surf}}(x, y, t)$ . The term  $\hat{z} \cdot [\nabla_z \eta \times \boldsymbol{\tau}(\eta)]$  creates a torque from that component of the surface turbulent stress that is aligned with isolines of the sea surface height.

### Bottom frictional acceleration

The term

$$\hat{z} \cdot (-\nabla_z \eta_b \times \mathbf{F}_b) = \hat{z} \cdot \left[ -\nabla_z \eta_b \times \frac{\partial \boldsymbol{\tau}_b}{\partial z} \right] \quad (39.94)$$

arises from evaluating the vertical divergence of the frictional stress at the ocean bottom. As for the analogous term for the surface, we offer a finite volume Ekman boundary layer treatment to render the alternative expression

$$\hat{\mathbf{z}} \cdot \int_{\eta_b}^{h_{e\text{-bot}}} \left[ -\nabla_z \eta_b \times \frac{\partial \boldsymbol{\tau}}{\partial z} \right] dz = \hat{\mathbf{z}} \cdot [-\nabla_z \eta_b \times \boldsymbol{\tau}(\eta_b)], \quad (39.95)$$

where we assumed  $\boldsymbol{\tau}$  is negligible at the top of the bottom Ekman layer,  $z = -\eta_b + h_{e\text{-bot}}$ . The term  $\hat{\mathbf{z}} \cdot [-\nabla_z \eta_b \times \boldsymbol{\tau}(\eta_b)]$  creates a torque from that component of the bottom turbulent stress that is aligned with isobaths.

## 39.6 Sverdrup balance and geostrophic Sverdrup balance

The balance (39.89) exposes many processes that affect meridional flow in a planetary geostrophic fluid. However, for many purposes, particularly when confronted with minimal information from ocean measurements, we examine just the main contributors to this balance.

The *Sverdrup balance* is a very simplified form of the balance (39.89), and it was first encountered in Section 25.5.5

$$\rho_0 \beta V_{\text{Sverdrup}} = \hat{\mathbf{z}} \cdot \nabla \times \boldsymbol{\tau}(\eta) \quad \text{Sverdrup balance.} \quad (39.96)$$

This balance arises from dropping the vertical velocity at both the surface and bottom; ignoring horizontal frictional stresses, and assuming  $\partial_t \eta = -Q_m / \rho_0$  as per a rigid lid flow in which  $\nabla \cdot \mathbf{U} = 0$ . This relation offers a useful null hypothesis for the large-scale and low frequency meridional ocean circulation away from sloping sides where topographic torques are important.

To derive the Sverdrup balance (39.96), we performed a depth integral of the planetary geostrophic vorticity equation (39.72) from the ocean bottom to the free surface. This integral encompasses both the geostrophic interior and the ageostrophic Ekman flow in the top and bottom Ekman layers. In some treatments we focus exclusively on contributions from the geostrophic interior, in which case the depth integral extends from the top of the bottom Ekman layer,  $z = \eta_{eb}$ , to the bottom of the top Ekman layer,  $z = \eta_{et}$ , thus leading to the depth integrated geostrophic transport

$$V_g \equiv \int_{\eta_{eb}}^{\eta_{et}} v dz. \quad (39.97)$$

Integrating the planetary geostrophic vorticity balance (39.72) over this depth range, and ignoring contributions from friction since we are concerned just with the geostrophic interior, leads to

$$\rho_0 \beta V_g = f [w(\eta_{et}) - w(\eta_{eb})]. \quad (39.98)$$

This equation provides a balance between the depth integrated meridional transport within the geostrophic interior (left hand side), with the vertical vortex stretching within this depth range (right hand side).

We now make use of the Ekman theory from Chapter 27 to approximate the vertical velocities in equation (39.98). For this purpose we neglect both the time tendency for the vertical position of the Ekman layer and the slope of the Ekman layer, in which case the kinematic identity (27.37) is approximated by

$$w^{(\eta_e)} = w - (\partial_t z + \mathbf{u} \cdot \nabla z) \approx w \quad \text{at } z = \eta_e(x, y, t), \quad (39.99)$$

where  $z = \eta_e$  is the vertical position of the Ekman layer. We now make use of the Ekman layer

mass budgets to determine the entrainment velocity,  $w^{(\dot{\eta}_e)}$ . In particular, equation (27.44) is used for  $w(\eta_{\text{et}})$  to give

$$w(\eta_{\text{et}}) \approx w_{\text{Ekman-top}}^{(\dot{\eta}_e)} = (1/\rho_0) \hat{z} \cdot [\nabla \times (\boldsymbol{\tau}(\eta)/f)]. \quad (39.100)$$

with a similar treatment for the bottom leading to

$$w(\eta_{\text{eb}}) \approx w_{\text{Ekman-bot}}^{(\dot{\eta}_e)} = (1/\rho_0) f \hat{z} \cdot [\nabla \times (\boldsymbol{\tau}(\eta_b)/f)]. \quad (39.101)$$

Bringing these results into equation (39.98) leads to

$$\rho_0 \beta V_g = \hat{z} \cdot \nabla \times [\boldsymbol{\tau}(\eta)/f - \boldsymbol{\tau}(\eta_b)/f]. \quad (39.102)$$

Since the bottom turbulent stress is generally much smaller than the surface, it can be readily ignored, in which case we reach the *geostrophic Sverdrup balance*

$$\rho_0 \beta V_g = \hat{z} \cdot \nabla \times [\boldsymbol{\tau}(\eta)/f] \quad \text{geostrophic Sverdrup balance.} \quad (39.103)$$

The geostrophic Sverdrup balance relates the meridional geostrophic transport to the curl of  $\boldsymbol{\tau}/f$  due to upper ocean mechanical stresses from boundary processes; i.e., wind stress and ice-ocean stresses. [Gray and Riser \(2014\)](#) assess the geostrophic Sverdrup balance based on ocean measurements.

## 39.7 Vorticity of the depth integrated velocity

In Section 39.5 we studied the depth integrated vorticity budget for planetary geostrophic flow. We were led to see how boundary torques (i.e., the curl of boundary forces) lead to vertical motion and in turn, through the  $\beta$ -effect, lead to meridional motion of the depth integrated flow. In this section we present another analysis of vorticity in the planetary geostrophic regime, here focusing on vorticity of the depth integrated velocity.

### 39.7.1 Depth integrated velocity equation

The depth integrated horizontal velocity equation (39.53a) is given by

$$\rho_0 f \hat{z} \times \mathbf{U} = - \int_{\eta_b}^{\eta} \nabla_z p \, dz + \Delta \boldsymbol{\tau} \quad (39.104)$$

where

$$\mathbf{U} = \int_{\eta_b}^{\eta} \mathbf{u} \, dz \quad (39.105)$$

is the depth integrated horizontal velocity, and we assumed friction in the form of the vertical divergence of a horizontal turbulent stress as in equation (39.71). For the depth integrated pressure gradient, we follow the decomposition in Section 19.4.4 by writing

$$\int_{\eta_b}^{\eta} p \, dz = \int_{\eta_b}^{\eta} [d(pz) - z \, dp] = p_a \eta - p_b \eta_b + \mathcal{P}, \quad (39.106)$$

where we used the hydrostatic balance to write  $dp = -g \rho dz$ , which is valid for each fluid column. We also introduced the potential energy per horizontal area of a fluid column

$$\mathcal{P} = \int_{\eta_b}^{\eta} g \rho z \, dz = (g \rho_0/2) (\eta^2 - \eta_b^2) + \int_{\eta_b}^{\eta} g \rho' z \, dz, \quad (39.107)$$

where

$$\rho' = \rho - \rho_0 \quad (39.108)$$

is the density deviation from the background reference density. These results then lead to the depth integrated horizontal pressure gradient

$$\int_{\eta_b}^{\eta} \nabla_z p \, dz = \nabla_z \left[ \int_{\eta_b}^{\eta} p \, dz \right] - p_a \nabla_z \eta + p_b \nabla_z \eta_b \quad (39.109a)$$

$$= \nabla_z [p_a \eta - p_b \eta_b + \mathcal{P}] - p_a \nabla_z \eta + p_b \nabla_z \eta_b \quad (39.109b)$$

$$= \eta \nabla_z p_a - \eta_b \nabla_z p_b + \nabla_z \mathcal{P}, \quad (39.109c)$$

which in turn renders the depth integrated planetary geostrophic momentum balance

$$\rho_0 f \hat{z} \times \mathbf{U} = -\eta \nabla_z p_a + \eta_b \nabla_z p_b - \nabla_z \mathcal{P} + \Delta \boldsymbol{\tau}. \quad (39.110)$$

The depth integrated balance is here written in terms of gradients in the surface and bottom pressures, the gradient of the potential energy per area, and the difference in turbulent stresses at the top and bottom boundaries,  $\Delta \boldsymbol{\tau} = \boldsymbol{\tau}(\eta) - \boldsymbol{\tau}(\eta_b)$ .

### 39.7.2 Vorticity budget

Taking the curl of the depth integrated balance (39.110) annihilates the potential energy term, thus leaving

$$\rho_0 \beta V = -\rho_0 f \nabla \cdot \mathbf{U} + \hat{z} \cdot \nabla \times [p_a \nabla \eta + \boldsymbol{\tau}(\eta) - p_b \nabla \eta_b - \boldsymbol{\tau}(\eta_b)]. \quad (39.111)$$

From Section 16.3, we know that the divergence of the depth-integrated flow for a steady Boussinesq fluid is given by

$$\rho_0 \nabla \cdot \mathbf{U} = Q_m, \quad (39.112)$$

so that

$$\rho_0 \beta V = -f Q_m + \hat{z} \cdot \nabla \times [p_a \nabla \eta + \boldsymbol{\tau}(\eta) - p_b \nabla \eta_b - \boldsymbol{\tau}(\eta_b)]. \quad (39.113)$$

This is the vorticity equation for the depth integrated planetary geostrophic fluid. It is quite similar to the vorticity balance for a shallow water fluid as given by equation (34.126) (which considered zero atmospheric pressure). In the presence of  $\beta$ , meridional mass transport for the fluid column is generated by surface mass fluxes,  $Q_m \neq 0$ ; the curl of surface form stresses and surface turbulent stresses; and the curl of topographic form stresses and bottom turbulent stresses. This result follows quite naturally when recognizing that the forces acting on a depth integrated fluid column arise from the depth integrated stresses acting in the column sides plus those acting on the top and bottom boundaries. In the absence of interior friction stresses due to horizontal strains, it is only the depth integrated pressure that acts on the column sides, and this term has zero curl. We are thus left with the curl of the form stresses and turbulent stresses on the surface and bottom boundaries, along with the contribution from mass transport.

## 39.8 Vorticity equation for the depth averaged velocity

In some numerical models, it is more common to have access to the depth averaged velocity

$$\bar{\mathbf{u}} = \frac{1}{D} \int_{\eta_b}^{\eta} \mathbf{u} \, dz \quad \text{with} \quad D = \eta - \eta_b. \quad (39.114)$$

We thus find it useful to derive the budget for the vorticity of the depth averaged velocity. In this discussion we encounter a distinct means for describing how bottom topography, in the presence of baroclinicity, generates meridional flow.

### 39.8.1 Relating the depth average velocity to boundary velocities

Before studying the vorticity equation, we here relate the depth averaged velocity,  $\bar{\mathbf{u}}(x, y, t)$ , to the surface velocity,  $\mathbf{u}(x, y, z = \eta, t)$ , and bottom velocity,  $\mathbf{u}(x, y, z = \eta_b, t)$ . This analysis exposes some general features of how the boundary flows are driven away from the depth average.

The starting point is the identity

$$\int_{\eta_b}^{\eta} \mathbf{u} dz = (\eta - \eta_b) \mathbf{u}(\eta) - \int_{\eta_b}^{\eta} \frac{\partial \mathbf{u}}{\partial z} (z - \eta_b) dz, \quad (39.115)$$

which, along with the analogous identity for the bottom flow, leads to

$$\bar{\mathbf{u}} - \mathbf{u}(\eta) = - \int_{\eta_b}^{\eta} \frac{\partial \mathbf{u}}{\partial z} \left[ \frac{z - \eta_b}{\eta - \eta_b} \right] dz \quad \text{and} \quad \bar{\mathbf{u}} - \mathbf{u}(\eta_b) = \int_{\eta_b}^{\eta} \frac{\partial \mathbf{u}}{\partial z} \left[ \frac{\eta - z}{\eta - \eta_b} \right] dz. \quad (39.116)$$

Note that  $\mathbf{u}(\eta) - \mathbf{u}(\eta_b) = \int_{\eta_b}^{\eta} (\partial \mathbf{u} / \partial z) dz$  serves as a useful check on the manipulations leading to equation (39.116). We see that the difference between the depth averaged flow and the surface flow,  $\bar{\mathbf{u}} - \mathbf{u}(\eta)$ , is determined by the integral of the weighted vertical shear, with the weight linearly decreasing from unity at the surface to zero at the bottom. The minus sign in front of the integral is sensible because if the flow increases in the positive direction from the bottom to the surface, then the depth averaged flow will have a smaller magnitude than the surface flow. The converse weighting holds for computing the difference  $\bar{\mathbf{u}} - \mathbf{u}(\eta_b)$ .

The identities (39.116) hold for arbitrary horizontal velocity fields. Assuming the flow satisfies frictional geostrophy as per equation (39.53a) leads to the frictional thermal wind relation

$$f \mathbf{u} = \rho_0^{-1} \hat{\mathbf{z}} \times \nabla p - \hat{\mathbf{z}} \times \mathbf{F} \implies f \partial_z \mathbf{u} = -(g/\rho_0) \hat{\mathbf{z}} \times \nabla \rho - \hat{\mathbf{z}} \times \partial_z \mathbf{F}, \quad (39.117)$$

so that the velocity differences are given by

$$f [\bar{\mathbf{u}} - \mathbf{u}(\eta)] = \int_{\eta_b}^{\eta} [(g/\rho_0) \hat{\mathbf{z}} \times \nabla \rho - \hat{\mathbf{z}} \times \partial_z \mathbf{F}] \left[ \frac{z - \eta_b}{\eta - \eta_b} \right] dz \quad (39.118a)$$

$$f [\bar{\mathbf{u}} - \mathbf{u}(\eta_b)] = - \int_{\eta_b}^{\eta} [(g/\rho_0) \hat{\mathbf{z}} \times \nabla \rho - \hat{\mathbf{z}} \times \partial_z \mathbf{F}] \left[ \frac{\eta - z}{\eta - \eta_b} \right] dz. \quad (39.118b)$$

Hence, differences between the depth averaged flow and the boundary flows are determined by weighted integrals of the baroclinicity and vertical friction shears.

### 39.8.2 Formulation of the vorticity equation

To develop the vorticity equation, we start by deriving the momentum equation for the depth averaged flow. For that purpose, rearrange the depth integrated momentum budget (39.110) according to

$$\rho_0 f \hat{\mathbf{z}} \times \mathbf{U} = -\eta \nabla_z (p_a - p_b) - D \nabla_z p_b - \nabla_z \mathcal{P} + \Delta \boldsymbol{\tau} \quad (39.119)$$

and then divide by the thickness,  $D = \eta - \eta_b$ , of the ocean column to render

$$\rho_0 f \hat{\mathbf{z}} \times \bar{\mathbf{u}} = -(\eta/D) \nabla_z (p_a - p_b) - \nabla_z p_b + (1/D) (-\nabla_z \mathcal{P} + \Delta \boldsymbol{\tau}). \quad (39.120)$$

Taking the curl then leads to

$$\rho_0 \nabla_z \cdot (f \bar{\mathbf{u}}) = -\hat{\mathbf{z}} \cdot \nabla_z \times [(\eta/D) \nabla_z(p_a - p_b)] + D^{-2} \hat{\mathbf{z}} \cdot [\nabla_z \times (D \nabla_z \mathcal{P})] + \hat{\mathbf{z}} \cdot [\nabla_z \times (D^{-1} \Delta \boldsymbol{\tau})] \quad (39.121a)$$

$$= \hat{\mathbf{z}} \cdot \nabla_z \times [(p_a - p_b) \nabla_z(\eta/D)] - D^{-2} \hat{\mathbf{z}} \cdot [\nabla_z \times (\mathcal{P} \nabla_z D)] + \hat{\mathbf{z}} \cdot [\nabla_z \times (D^{-1} \Delta \boldsymbol{\tau})]. \quad (39.121b)$$

The vorticity budget (39.121) is a bit less tidy than that for the depth integrated budget (39.113). Nonetheless, it offers some useful insights concerning the flow. For that purpose, write the left hand side in the suggestive form

$$\nabla_z \cdot (f \bar{\mathbf{u}}) = \nabla_z \cdot [(f/D) \mathbf{U}], \quad (39.122)$$

with  $f/D$  reminiscent of the shallow water potential vorticity for the planetary geostrophic flow (Section 38.4). Motivated by this analog, we write the vorticity equation (39.121) in the form

$$\begin{aligned} \rho_0 \mathbf{U} \cdot \nabla_z(f/D) &= -\rho_0 (f/D) \nabla_z \cdot \mathbf{U} + \hat{\mathbf{z}} \cdot \nabla_z \times [(p_a - p_b) \nabla_z(\eta/D)] \\ &\quad - D^{-2} \hat{\mathbf{z}} \cdot [\nabla_z \times (\mathcal{P} \nabla_z D)] + \hat{\mathbf{z}} \cdot [\nabla_z \times (D^{-1} \Delta \boldsymbol{\tau})]. \end{aligned} \quad (39.123)$$

Contrary to the shallow water case, we here see that even for a perfect planetary geostrophic fluid, the depth-integrated flow does not generally follow contours of constant  $f/D$ . Even so, it is of interest to examine how the processes on the right hand side contribute to flow deviations from  $f/D$  contours. For that purpose we simplify the flow even more by making the rigid lid approximation.

### 39.8.3 Rigid lid approximation and the role of JEBAR

The rigid lid approximation is commonly made for studies of large-scale circulation. Indeed, it was the basis for many ocean general circulation models following the work of [Bryan \(1969\)](#). A fluid satisfying the rigid lid approximation has a vanishing horizontal divergence for the depth integrated flow

$$\text{rigid lid approximation} \implies \nabla_z \cdot \mathbf{U} = 0. \quad (39.124)$$

Furthermore, as part of the rigid lid approximation we assume the free surface undulations are much smaller than the resting ocean depth so that<sup>3</sup>

$$|\eta| \ll |\eta_b| \implies \eta/D \approx 0 \quad (39.125a)$$

$$1/(\eta - \eta_b) \approx 1/(-\eta_b) = 1/H. \quad (39.125b)$$

Hence, with the rigid lid approximation the vorticity equation (39.123) takes the simplified form

$$\rho_0 \mathbf{U} \cdot \nabla_z(f/H) = \hat{\mathbf{z}} \cdot [\nabla_z \mathcal{P} \times \nabla_z(1/H) + \nabla_z \times (H^{-1} \Delta \boldsymbol{\tau})]. \quad (39.126)$$

---

<sup>3</sup>We use the notation  $\eta_b = -H$  in this subsection to correspond to the literature for rigid lid models and the JEBAR term. Note that  $H$  is the vertical depth scale, which is a constant, and it is distinct from  $H(x, y) = -\eta_b(x, y)$ , which is a function of horizontal position.

*JEBAR drives deviations from f/H aligned flow*

Equation (39.126) indicates that in the absence of boundary stresses, contours of constant  $f/H$  serve as streamlines for flow where the potential energy isolines are parallel to lines of constant  $H$

$$\rho_0 H^2 \mathbf{U} \cdot \nabla_z (f/H) = \hat{\mathbf{z}} \cdot (\nabla_z H \times \nabla_z \mathcal{P}) = \hat{\mathbf{z}} \cdot (\nabla_z \times H \nabla_z \mathcal{P}) = -\hat{\mathbf{z}} \cdot (\nabla_z \times \mathcal{P} \nabla_z H). \quad (39.127)$$

The right hand side offers equivalent expressions for the Joint Effect of Baroclinicity and Relief (JEBAR). This name arises since JEBAR is nonzero only in the presence of non-flat topography (“relief”) and (as shown below) when there are horizontal density gradients (i.e., baroclinicity). Equation (39.127) says that the depth integrated flow does not generally align with  $f/H$  contours. Misalignment of the flow with  $f/H$  contours is driven by misalignments of isobaths and isolines of the depth integrated potential energy, with this misalignment referred to as JEBAR.

Let us show that contributions to JEBAR arise only from the component of the potential energy that deviates from a constant density reference state. For that purpose note that in the rigid lid approximation, the potential energy in a column, as given by equation (39.107), takes the form

$$\mathcal{P} = (1/2) g \rho_0 H^2 + g \int_{-H}^0 \rho' z dz, \quad (39.128)$$

where  $\rho' = \rho - \rho_0$ . With  $\nabla_z H \times \nabla_z (\rho_0 H^2) = 0$ , we are left with just the contribution from  $\rho'$ . Conversely, we see that the depth integrated horizontal flow of a steady, rigid lid, homogeneous fluid, in the absence of turbulent boundary stresses, aligns with  $f/H$  contours, which connects to the case of a single layer of shallow water fluid.

*Relating JEBAR to pressure*

JEBAR as given by the right hand side of equation (39.127) has the appearance of the curl of a form stress, and yet it is not. The reason is that  $\mathcal{P}$  is the potential energy of the fluid column rather than bottom pressure. We make this point explicit by recalling the decomposition (39.106), here specialized to the rigid lid in which

$$\mathcal{P} = H(\bar{p} - p_b) \quad \text{with} \quad \bar{p} = H^{-1} \int_{-H}^0 p dz = (-\eta_b)^{-1} \int_{\eta_b}^0 p dz. \quad (39.129)$$

Plugging into the vorticity equation (39.126) leads to

$$\rho_0 \mathbf{U} \cdot \nabla_z (f/H) = H^{-1} \hat{\mathbf{z}} \cdot [\nabla_z H \times \nabla_z (\bar{p} - p_b)] + \hat{\mathbf{z}} \cdot \nabla_z \times (H^{-1} \Delta \boldsymbol{\tau}). \quad (39.130)$$

The JEBAR term thus arises from deviations of the depth averaged pressure from the bottom pressure. We can go one more step in exposing this pressure difference through use of equation (39.116), here applied to hydrostatic pressure, in which case

$$\bar{p} - p_b = \int_{\eta_b}^0 \frac{\partial p}{\partial z} \frac{z}{\eta_b} dz = (g/H) \int_{-H}^0 z \rho dz = H^{-1} \mathcal{P} \quad (39.131)$$

so that

$$g^{-1} \nabla_z (\bar{p} - p_b) = -\rho(z = \eta_b) \nabla_z H - \int_{-H}^0 \nabla_z (\rho z/H) dz. \quad (39.132)$$

The first term arises from slopes in the bottom topography as weighted by the bottom density, whereas the second term arises from the density integral of the horizontal gradients in the depth-weighted density.

Equation (39.113) provides the budget for vorticity of the depth integrated flow, in which we find the curl of the topographic form stress leads to vortex stretching. For the vorticity of the depth averaged flow, we instead encounter the JEBAR term in equation (39.130), which is not a pure vortex stretching term. Instead, it accounts for the fact that it is the horizontal velocity flowing across isobaths,  $\mathbf{u}(z = \eta_b)$ , rather than depth averaged horizontal velocity,  $\bar{u}$ , that leads to vortex stretching. Hence, when studying vorticity of the depth averaged velocity,  $\bar{u}$ , accounting for the role of vortex stretching requires us to include JEBAR.

### 39.8.4 Further study

Chapter 3 in [Samelson \(2011\)](#) offers more discussion of the large-scale ocean circulation based on planetary geostrophy. [Mertz and Wright \(1992\)](#) discuss the physics of how JEBAR relates to the curl of the topographic form stress as well as other mathematically equivalent forms. [Cane et al. \(1998\)](#) as well a Section 2.5 of [Drijfhout et al. \(2013\)](#) offer critical remarks on JEBAR.



# Chapter 40

## Continuously stratified quasi-geostrophy

Quasi-geostrophy (QG) is the canonical *balanced model* in geophysical fluid mechanics whereby the potential vorticity is the sole prognostic field; all other fields, such as the velocity and buoyancy, are diagnosed from potential vorticity. The process of diagnosing the allied fields requires the inversion of an elliptic operator to compute the geostrophic streamfunction from the potential vorticity. Some authors refer to this connection between potential vorticity and streamfunction as *invertibility*, with the mathematical technology required for inversion shared with many other elliptic problems in mathematical physics (see Section 3.5 for more on elliptic partial differential equations).

Quasi-geostrophy is an elegant theory of mathematical physics offering great physical and mathematical insights into the workings of large-scale geophysical fluid motions. Giving the theory full justice requires a book the size of the current one. Instead, we here aim to provide a taste of its continuously stratified realization, offering a detailed derivation that builds from Chapters 38 and 39, and sampling some of its physical and mathematical content.

### CHAPTER GUIDE

In this chapter we extend to continuously stratified fluids the shallow water discussions of quasi-geostrophy in Chapter 38. Continuously stratified QG is not concerned with the relatively slow processes that affect stratification, but instead with the shorter time scale processes that slightly perturb that stratification. We make use of stratified geophysical fluid dynamics from Chapters 17 and 25, as well as potential vorticity from Chapter 36 and the development of continuously stratified planetary geostrophy in Chapter 39.

40.1	Open threads . . . . .	998
40.2	The quasi-geostrophic PV equation . . . . .	998
40.2.1	Zeroth order asymptotic equations . . . . .	999
40.2.2	First order asymptotic equations . . . . .	1000
40.3	Reintroducing physical dimensions . . . . .	1001
40.3.1	Hydrostatic balance . . . . .	1002
40.3.2	Geostrophic balance . . . . .	1002
40.3.3	Material time derivative . . . . .	1002
40.3.4	Buoyancy equation . . . . .	1003
40.3.5	Vorticity equation . . . . .	1003
40.3.6	Velocity equation . . . . .	1004
40.3.7	Potential vorticity . . . . .	1004

---

40.4	Connecting quasi-geostrophic PV to Ertel PV . . . . .	1005
40.4.1	Non-dimensionalizing the Ertel potential vorticity . . . . .	1005
40.4.2	Material conservation of Ertel PV to order $\text{Ro}^1$ . . . . .	1006
40.5	Mathematical expressions of the theory . . . . .	1007
40.5.1	The Jacobian form of geostropic advection . . . . .	1007
40.5.2	Constant background buoyancy frequency . . . . .	1008
40.5.3	Vertical boundary conditions for $\psi$ . . . . .	1008
40.5.4	Potential vorticity induction and impermeability . . . . .	1009
40.6	Energetics for quasi-geostrophic flow . . . . .	1011
40.6.1	Kinetic energy . . . . .	1011
40.6.2	Available potential energy . . . . .	1012
40.6.3	Energy conversion . . . . .	1013
40.6.4	Scaling APE and KE . . . . .	1013
40.7	Exercises . . . . .	1014

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## 40.1 Open threads

- Finish discussion of impermeability and gauge transformation in Section 40.5.4.
- Rossby waves
- Synoptic development

## 40.2 The quasi-geostrophic PV equation

In deriving the quasi-geostrophic PV equation, we proceed much like for the single layer of shallow water fluid in Section 38.5. In particular, quasi-geostrophic scaling from Section 38.5.1 is relevant for both the shallow water and for the continuously stratified fluid. We employ an asymptotic expansion in the Rossby number and stop at the first nontrivial order, which is  $\text{Ro}^1$ . For this purpose, recall the non-dimensional momentum and continuity equations from Section 39.2.8

$$\text{Ro} \left[ \frac{\partial \hat{\mathbf{u}}}{\partial \hat{t}} + (\hat{\mathbf{u}} \cdot \hat{\nabla}_{\hat{z}}) \hat{\mathbf{u}} + \hat{w} \frac{\partial \hat{\mathbf{u}}}{\partial \hat{z}} \right] + \hat{\mathbf{f}} \times \hat{\mathbf{u}} = -\hat{\nabla}_{\hat{z}} \hat{\varphi} \quad (40.1a)$$

$$\frac{\partial \hat{\varphi}}{\partial \hat{z}} = \hat{b} \quad (40.1b)$$

$$\hat{\nabla} \cdot \hat{\mathbf{v}} = 0 \quad (40.1c)$$

$$\frac{\text{Ro}}{\text{Bu}} \frac{\text{D}\hat{b}}{\text{D}\hat{t}} + \hat{w} = 0. \quad (40.1d)$$

We expand the variables in an asymptotic series in Rossby number

$$\hat{\mathbf{u}} = \hat{\mathbf{u}}_0 + \text{Ro} \hat{\mathbf{u}}_1 + \text{Ro}^2 \hat{\mathbf{u}}_2 + \dots \quad (40.2a)$$

$$\hat{\mathbf{v}} = \hat{\mathbf{v}}_0 + \text{Ro} \hat{\mathbf{v}}_1 + \text{Ro}^2 \hat{\mathbf{v}}_2 + \dots \quad (40.2b)$$

$$\hat{w} = \hat{w}_0 + \text{Ro} \hat{w}_1 + \text{Ro}^2 \hat{w}_2 + \dots \quad (40.2c)$$

$$\hat{b} = \hat{b}_0 + \text{Ro} \hat{b}_1 + \text{Ro}^2 \hat{b}_2 + \dots \quad (40.2d)$$

$$\hat{\varphi} = \hat{\varphi}_0 + \text{Ro} \hat{\varphi}_1 + \text{Ro}^2 \hat{\varphi}_2 + \dots \quad (40.2e)$$

along with the expansion (38.55) for the Coriolis parameter

$$\hat{\mathbf{f}} = \hat{\mathbf{f}}_0 + \text{Ro} \hat{\beta} \hat{\mathbf{y}}, \quad (40.3)$$

and where (equation (38.56))

$$\widehat{\beta} \widehat{y} = \frac{\beta y}{\text{Ro} f_0} = T \beta y. \quad (40.4)$$

As noted in Section 38.5.2, the velocity field is non-divergent at each order of Rossby number, so that

$$\nabla \cdot \widehat{\mathbf{v}}_n = 0 \quad \forall n. \quad (40.5)$$

The Burger number is order unity since the horizontal length scales for the quasi-geostrophic flows of concern here are on the order of the deformation radius

$$\text{Bu} \sim 1 \implies L \sim L_d, \quad (40.6)$$

where we introduced the *internal deformation radius* from Section 39.2.6

$$L_d(z) = H \frac{N(z)}{f_0}. \quad (40.7)$$

It is important to retain the depth dependence of the Burger number through its dependence on the background stratification  $N^2(z)$

$$\text{Bu}(z) = \left[ \frac{L_d}{L} \right]^2 = N(z)^2 \left[ \frac{H}{L f_0} \right]^2. \quad (40.8)$$

Hence, the Burger number does not commute with the vertical derivative operator.

### 40.2.1 Zeroth order asymptotic equations

The zeroth order asymptotic equations are

$$\widehat{\mathbf{f}}_0 \times \widehat{\mathbf{u}}_0 = -\widehat{\nabla}_z \widehat{\varphi}_0 \quad (40.9a)$$

$$\frac{\partial \widehat{\varphi}_0}{\partial \widehat{z}} = \widehat{b}_0 \quad (40.9b)$$

$$\widehat{\nabla}_z \cdot \widehat{\mathbf{u}}_0 + \frac{\partial \widehat{w}_0}{\partial \widehat{z}} = 0 \quad (40.9c)$$

$$\widehat{w}_0 = 0. \quad (40.9d)$$

The first equation represents *f*-plane geostrophy, which means that the horizontal velocity has zero divergence

$$\widehat{\nabla}_z \cdot \widehat{\mathbf{u}}_0 = 0. \quad (40.10)$$

Equation (40.9b) means the zeroth order buoyancy determines the zeroth order hydrostatic pressure. Since the horizontal velocity has zero divergence, the continuity equation (40.9c) means that the vertical velocity is depth independent

$$\frac{\partial \widehat{w}_0}{\partial \widehat{z}} = 0. \quad (40.11)$$

If it vanishes somewhere, such as a solid boundary, then it vanishes everywhere. This is a manifestation of the Taylor-Proudman theorem (see Section 25.5.3). Indeed, a vanishing  $\widehat{w}_0$  is required by the zeroth-order buoyancy equation (40.9d). Hence, the non-dimensional velocity has a nonzero contribution only at order  $\text{Ro}^1$

$$\widehat{w} = \text{Ro} \widehat{w}_1 + \text{Ro}^2 \widehat{w}_2 + \dots, \quad (40.12)$$

thus manifesting the vertical stiffening of fluid columns found in rotating fluids. Correspondingly, the dimensionful vertical velocity has the asymptotic expansion

$$w = W\hat{w} = W\text{Ro}(\hat{w}_1 + \text{Ro}\hat{w}_2 + \dots), \quad (40.13)$$

so that to leading to order  $\text{Ro}^1$

$$\hat{w}_1 = \frac{w}{W\text{Ro}}. \quad (40.14)$$

Since the zeroth-order horizontal velocity is non-divergent, we can introduce a geostrophic streamfunction

$$\hat{u}_0 = -\partial\hat{\psi}_0/\partial\hat{y} \quad \text{and} \quad \hat{v}_0 = \partial\hat{\psi}_0/\partial\hat{x} \quad \text{and} \quad \hat{\zeta}_0 = \hat{\nabla}^2\hat{\psi}_0, \quad (40.15)$$

where the zeroth-order streamfunction is the ratio of the zeroth order pressure to zeroth order Coriolis parameter

$$\hat{\psi}_0 = \hat{\varphi}_0/\hat{f}_0. \quad (40.16)$$

Note also that the zeroth-order system satisfies the thermal wind balance

$$\hat{f}_0 \times \frac{\partial\hat{u}_0}{\partial\hat{z}} = -\hat{\nabla}_z \hat{b}_0. \quad (40.17)$$

Finally, note that the zeroth order buoyancy is determined by the streamfunction through the hydrostatic balance

$$\hat{b}_0 = \frac{\partial\hat{\varphi}_0}{\partial\hat{z}} = \hat{f}_0 \frac{\partial\hat{\psi}_0}{\partial\hat{z}}. \quad (40.18)$$

### 40.2.2 First order asymptotic equations

The zeroth order equations do not render a prognostic equation, for which we need to consider equations at order  $\text{Ro}^1$

$$\frac{D_0\hat{u}_0}{Dt} + \hat{f}_0 \times \hat{u}_1 + \hat{\beta}\hat{y}\hat{z} \times \hat{u}_0 = -\hat{\nabla}_z \hat{\varphi}_1 \quad (40.19a)$$

$$\frac{\partial\hat{\varphi}_1}{\partial\hat{z}} = \hat{b}_1 \quad (40.19b)$$

$$\hat{\nabla}_z \cdot \hat{u}_1 + \frac{\partial\hat{w}_1}{\partial\hat{z}} = 0 \quad (40.19c)$$

$$\frac{1}{Bu} \frac{D_0\hat{b}_0}{Dt} + \hat{w}_1 = 0. \quad (40.19d)$$

The first order terms are often referred to as the *ageostrophic* components, though note that all contributions higher than zeroth order constitute ageostrophic contributions.

At order  $\text{Ro}^1$ , the material time derivative makes use *only* of the zeroth order horizontal geostrophic velocity

$$\frac{D_0}{Dt} = \frac{\partial}{\partial t} + \hat{u}_0 \cdot \hat{\nabla}. \quad (40.20)$$

To close this set of equations, we produce the vorticity equation from the momentum equation, and then combine the vorticity equation and buoyancy equation to produce the QG potential vorticity equation. In Section 38.5, we performed the same procedure for deriving the shallow water quasi-geostrophic equations.

Taking the curl of the momentum equation (40.19a) eliminates the pressure gradient,  $\hat{\nabla}\hat{\varphi}_1$ ,

thus producing the vorticity equation

$$\frac{\partial \hat{\zeta}_0}{\partial \hat{t}} + (\hat{\mathbf{u}}_0 \cdot \hat{\nabla}) (\hat{\zeta}_0 + \hat{\beta} \hat{y}) = -\hat{f}_0 \hat{\nabla}_z \cdot \mathbf{u}_1. \quad (40.21)$$

We make use of the continuity equation (40.19c) to eliminate the horizontal convergence

$$\frac{\partial \hat{\zeta}_0}{\partial \hat{t}} + (\hat{\mathbf{u}}_0 \cdot \hat{\nabla}) (\hat{\zeta}_0 + \hat{\beta} \hat{y}) = \hat{f}_0 \frac{\partial \hat{w}_1}{\partial \hat{z}}. \quad (40.22)$$

The right hand side represents the contribution to vorticity evolution from stretching by the ageostrophic vertical velocity through planetary rotation. We can eliminate the ageostrophic vertical velocity through the buoyancy equation (40.19d). When doing so, it is important to keep the  $Bu(z)$  depth dependence according to equation (40.8), with this depth dependence arising from the background stratification. The resulting vorticity equation is

$$\frac{\partial \hat{\zeta}_0}{\partial \hat{t}} + (\hat{\mathbf{u}}_0 \cdot \hat{\nabla}) (\hat{\zeta}_0 + \hat{\beta} \hat{y}) = -\hat{f}_0 \frac{\partial}{\partial \hat{z}} \left[ \frac{1}{Bu} \frac{D_0 \hat{b}_0}{Dt} \right]. \quad (40.23)$$

We now use the identity

$$\frac{\partial}{\partial \hat{z}} \left[ \frac{1}{Bu} \frac{D_0 \hat{b}_0}{Dt} \right] = \frac{\partial}{\partial \hat{z}} \left[ \frac{1}{Bu} \left( \frac{\partial}{\partial \hat{t}} + \hat{\mathbf{u}}_0 \cdot \hat{\nabla} \right) \hat{b}_0 \right] \quad (40.24a)$$

$$= \frac{D_0}{Dt} \left[ \frac{\partial}{\partial \hat{z}} \left( \frac{\hat{b}_0}{Bu} \right) \right] + \frac{1}{Bu} \frac{\partial \hat{\mathbf{u}}_0}{\partial \hat{z}} \cdot \hat{\nabla}_z \hat{b}_0 \quad (40.24b)$$

$$= \frac{D_0}{Dt} \left[ \frac{\partial}{\partial \hat{z}} \left( \frac{\hat{b}_0}{Bu} \right) \right], \quad (40.24c)$$

where we set

$$\frac{\partial \hat{\mathbf{u}}_0}{\partial \hat{z}} \cdot \hat{\nabla}_z \hat{b}_0 = 0 \quad (40.25)$$

since the zeroth-order velocity maintains thermal wind balance (40.17). Bringing terms together then leads to the material conservation equation for quasi-geostrophic potential vorticity

$$\frac{D_0}{Dt} \left[ \hat{\zeta}_0 + \hat{\beta} \hat{y} + \hat{f}_0 \frac{\partial}{\partial \hat{z}} \left( \frac{\hat{b}_0}{Bu} \right) \right] = 0. \quad (40.26)$$

## 40.3 Reintroducing physical dimensions

To expose the physical elements to the quasi-geostrophic theory, we find it useful, if not essential, to reintroduce physical dimensions much like we did for the shallow water in Section 38.6. For

that purpose, we write

$$\mathbf{u} = \mathbf{u}_g + \mathbf{u}_{ag} = U (\hat{\mathbf{u}}_0 + \text{Ro} \hat{\mathbf{u}}_1) \quad (40.27a)$$

$$w \equiv w_{ag} = \text{Ro} W \hat{w}_1 \quad (40.27b)$$

$$b \equiv b_g + b_{ag} = B (\hat{b}_0 + \text{Ro} \hat{b}_1) \quad (40.27c)$$

$$\varphi \equiv \varphi_g + \varphi_{ag} = f_0 U L (\hat{\varphi}_0 + \text{Ro} \hat{\varphi}_1). \quad (40.27d)$$

The details of reintroducing dimensions are straightforward but can be tedious. We provide full details to help develop experience and confidence working with the theory.

### 40.3.1 Hydrostatic balance

Hydrostatic balance is maintained for terms at each Rossby number order, so that we have the dimensional equations

$$\frac{\partial \varphi_g}{\partial z} = b_g \quad \text{and} \quad \frac{\partial \varphi_{ag}}{\partial z} = b_{ag}. \quad (40.28)$$

### 40.3.2 Geostrophic balance

The non-dimensional geostrophic balance for the zeroth order fields

$$\hat{\mathbf{f}}_0 \times \hat{\mathbf{u}}_0 = -\hat{\nabla}_z \hat{\varphi}_0 \quad (40.29)$$

takes on the dimensional form

$$\hat{\mathbf{z}} \times \mathbf{u}_g / U = -L \nabla_z \varphi_g / (f_0 U L). \quad (40.30)$$

Cancelling factors leads to the expected form of  $f$ -plane geostrophy

$$f_0 \hat{\mathbf{z}} \times \mathbf{u}_g = -\nabla_z \varphi_g. \quad (40.31)$$

### 40.3.3 Material time derivative

For the material time derivative operator we write

$$D/Dt = \partial_t + \mathbf{u} \cdot \nabla + w \partial_z \quad (40.32a)$$

$$= (1/T) \partial_{\hat{t}} + (U/L) \hat{\mathbf{u}} \cdot \hat{\nabla} + (W/H) \hat{w} \partial_{\hat{z}} \quad (40.32b)$$

$$= (1/T) (\partial_{\hat{t}} + \hat{\mathbf{u}} \cdot \hat{\nabla} + \hat{w} \partial_{\hat{z}}) \quad (40.32c)$$

$$= (1/T) (\partial_{\hat{t}} + \hat{\mathbf{u}}_0 \cdot \hat{\nabla}_z) + (\text{Ro}/T) (\hat{\mathbf{u}}_0 \cdot \hat{\nabla}_z + \hat{w}_1 \partial_{\hat{z}}) \quad (40.32d)$$

$$= \partial_t + \mathbf{u}_g \cdot \nabla_z + \mathbf{u}_{ag} \cdot \nabla_z + w_{ag} \partial_z \quad (40.32e)$$

$$\equiv D_g/Dt + \mathbf{u}_{ag} \cdot \nabla_z + w_{ag} \partial_z, \quad (40.32f)$$

where time scales according to advection,  $T = L/U$ , vertical velocity scales according to continuity,  $W = H U / L$ , and we introduced the geostrophic material time derivative operator

$$D_g/Dt \equiv \partial_t + \mathbf{u}_g \cdot \nabla_z. \quad (40.33)$$

### 40.3.4 Buoyancy equation

We split buoyancy into a depth dependent static background and a deviation from the background

$$b = \tilde{b}(z) + b'(x, y, z, t), \quad (40.34)$$

with its vertical derivative

$$\partial_z b = d\tilde{b}/dz + \partial_z b' = N^2 + \partial_z b', \quad (40.35)$$

where  $N^2(z)$  is the squared buoyancy frequency for the background buoyancy field. In this manner, we can write the buoyancy equation for an adiabatic fluid as

$$\frac{\partial b'}{\partial t} + \mathbf{u} \cdot \nabla b' + w(N^2 + \partial_z b') = 0. \quad (40.36)$$

We non-dimensionalize this equation by making use of the following relations between the scales

$$B = f_0 U L / H \quad W = H(U/L) \quad \text{Ro} = U/(f_0 L) \quad \text{Bu} = (N H)^2 / (f_0 L)^2, \quad (40.37)$$

in which case the buoyancy equation takes the form

$$\frac{\partial b'}{\partial t} + \mathbf{u} \cdot \nabla b' + w(N^2 + \partial_z b') = \frac{B}{T} \frac{\partial \hat{b}}{\partial \hat{t}} + \frac{U B}{L} \hat{\mathbf{u}} \cdot \hat{\nabla}_z \hat{b} + W \hat{w} N^2 + \frac{W B}{H} \hat{w} \partial_{\hat{z}} \hat{b} = 0. \quad (40.38)$$

We find it useful to divide by  $f_0 N^2$ , so that

$$\frac{1}{f_0 N^2} \left[ \frac{\partial b'}{\partial t} + \mathbf{u} \cdot \nabla b' + w(N^2 + \partial_z b') \right] = \frac{H \text{Ro}^2}{\text{Bu}} \left[ \frac{\partial \hat{b}}{\partial \hat{t}} + \hat{\mathbf{u}} \cdot \hat{\nabla} \hat{b} + \hat{w} \partial_{\hat{z}} \hat{b} \right] + \text{Ro} \hat{w} = 0. \quad (40.39)$$

The vertical velocity component,  $\hat{w}$ , is nonzero only at order  $\text{Ro}^1$ , so the term  $\text{Ro} \hat{w}$  is order  $\text{Ro}^2$  (recall equation (40.27b)). To the same order, we drop the term,  $\hat{w} \partial_{\hat{z}} \hat{b}$ , that appears within the bracket and retain only the zeroth order buoyancy contribution,  $\hat{b}_0$ . Reintroducing physical dimensions then leads to the dimensional form of the quasi-geostrophic buoyancy equation

$$\partial_t b_g + \mathbf{u}_g \cdot \nabla_z b_g + w_{ag} N^2 = D_g b_g / Dt + w_{ag} N^2 = 0. \quad (40.40)$$

This equation means that the geostrophic transport of the geostrophic buoyancy is affected by a source due to the ageostrophic vertical advection of background buoyancy

$$D_g b_g / Dt = -w_{ag} N^2 \quad (40.41)$$

### 40.3.5 Vorticity equation

Reintroducing dimensions to the vorticity equation (40.22) yields<sup>1</sup>

$$\frac{\partial \hat{\zeta}_0}{\partial \hat{t}} + (\hat{\mathbf{u}}_0 \cdot \hat{\nabla}_z) (\hat{\zeta}_0 + \hat{\beta} \hat{y}) - \hat{f}_0 \frac{\partial \hat{w}_1}{\partial \hat{z}} = T^2 \left[ \frac{\partial \zeta}{\partial t} + \mathbf{u}_g \cdot \nabla_z (\zeta + \beta y) \right] - \frac{H}{W \text{Ro}} \frac{\partial w_{ag}}{\partial z}. \quad (40.42)$$

The identity  $H/(W \text{Ro}) = f_0 T^2$  leads to the order  $\text{Ro}^1$  vorticity equation

$$\frac{\partial \zeta_a}{\partial t} + J(\psi, \zeta_a) = f_0 \frac{\partial w_{ag}}{\partial z}. \quad (40.43)$$

<sup>1</sup>Recall from equation (40.27b) that  $W \hat{w} = \text{Ro} W \hat{w}_1 = w_{ag}$ .

Hence, the absolute geostrophic vorticity is advected by the geostrophic flow, and it has a source (right hand side) due to vertical stretching by the ageostrophic flow.

### 40.3.6 Velocity equation

The prognostic velocity equation arises from the first order asymptotic equation (40.19a)

$$\frac{D_0 \hat{\mathbf{u}}_0}{Dt} + \hat{\mathbf{f}}_0 \times \hat{\mathbf{u}}_1 + \hat{\beta} \hat{\mathbf{y}} \hat{\mathbf{z}} \times \hat{\mathbf{u}}_0 = -\hat{\nabla}_z \hat{\varphi}_1. \quad (40.44)$$

Our skills with reintroducing dimensional quantities should be sufficient to write down the dimensional velocity equation by inspection<sup>2</sup>

$$(\partial_t + \mathbf{u}_g \cdot \nabla) \mathbf{u}_g + \beta y \hat{\mathbf{z}} \times \mathbf{u}_g + f_0 \hat{\mathbf{z}} \times \mathbf{u}_{ag} = -\nabla_z \varphi_{ag}. \quad (40.45)$$

We can also choose to add the geostrophic balanced flow that holds at order  $\text{Ro}^0$ ,  $f_0 \hat{\mathbf{z}} \times \mathbf{u}_g = -\nabla_z \varphi_g$ , so to have the equivalent equation

$$(\partial_t + \mathbf{u}_g \cdot \nabla) \mathbf{u}_g + \beta y \hat{\mathbf{z}} \times \mathbf{u}_g + f_0 \hat{\mathbf{z}} \times (\mathbf{u}_g + \mathbf{u}_{ag}) = -\nabla_z (\varphi_g + \varphi_{ag}). \quad (40.46)$$

### 40.3.7 Potential vorticity

From equation (40.26), we identify the non-dimensional quasi-geostrophic potential vorticity

$$\hat{q} = \hat{\zeta}_0 + \hat{\beta} \hat{\mathbf{y}} + \hat{f}_0 \frac{\partial (\hat{b}_0 / \text{Bu})}{\partial \hat{z}}. \quad (40.47)$$

Introducing dimensional quantities to the right hand side yields<sup>3</sup>

$$\hat{q} = \frac{L}{U} [\zeta_g + \beta y] + \frac{\partial}{\partial z} \left[ \frac{H b_g}{B \text{Bu}} \right] \quad (40.48a)$$

$$= (1/(f_0 \text{Ro}) (\zeta_g + \beta y) + \frac{H}{B} \frac{\partial}{\partial z} \left[ \frac{b_g}{\text{Bu}} \right]). \quad (40.48b)$$

The scale for the fluctuating buoyancy is given by equation (39.22),  $B = f_0 U L / H$ , and the inverse Burger number is given by equation (40.8),  $\text{Bu}^{-1} = [(L f_0) / (H N)]^2$ , so that

$$\hat{q} = (1/(f_0 \text{Ro}) (\zeta_g + \beta y) + \frac{H^2}{f_0 U L} \frac{L^2 f_0^2}{H^2} \frac{\partial}{\partial z} \left[ \frac{b_g}{N^2} \right]) \quad (40.49a)$$

$$= (1/(f_0 \text{Ro}) (\zeta_g + \beta y) + \frac{1}{\text{Ro}} \left[ \frac{\partial}{\partial z} \left( \frac{b_g}{N^2} \right) \right]). \quad (40.49b)$$

Introducing the geostrophic streamfunction,

$$\mathbf{u}_g = \hat{\mathbf{z}} \times \nabla_z \psi \quad \text{and} \quad \zeta = \hat{\mathbf{z}} \cdot (\nabla \times \mathbf{u}_g) = \nabla_z^2 \psi \quad \text{and} \quad b_g = f_0 \partial_z \psi, \quad (40.50)$$

leads to

$$q \equiv f_0 \text{Ro} \hat{q} = \zeta_g + \beta y + \frac{\partial}{\partial z} \left[ \frac{f_0^2}{N^2} \frac{\partial \psi}{\partial z} \right]. \quad (40.51)$$

<sup>2</sup>Recall from equation (40.27d) that  $\varphi_{ag} = f_0 U L \text{Ro} \hat{\varphi}_1 = U^2 \hat{\varphi}_1$ .

<sup>3</sup>Recall  $\hat{f}_0 = 1$  and  $\hat{\beta} \hat{\mathbf{y}} = T \beta y = (L/U) \beta y$ .

Just as for the shallow water case in Section 38.6.1, the potential vorticity (40.51) scales as  $f_0 \text{Ro}$ . We sometimes choose to add the constant  $f_0$  to  $q$ , which has no effect on the dynamics but reveals the beta plane planetary vorticity

$$q = \underbrace{f_0 + \beta y}_{\text{planetary vorticity}} + \underbrace{\nabla_z^2 \psi}_{\text{relative vorticity}} + \underbrace{\frac{\partial}{\partial z} \left[ \frac{f_0^2}{N^2} \frac{\partial \psi}{\partial z} \right]}_{\text{stretching by } f}. \quad (40.52)$$

We identify the following three contributions to the quasi-geostrophic potential vorticity.

- **PLANETARY VORTICITY:** The planetary vorticity contribution,  $f_0 + \beta y$ , arises from rotation of the reference frame. The  $\beta y$  term is the only dynamically relevant contribution, so that we can equally well drop the  $f_0$  contribution.
- **GEOSTROPHIC RELATIVE VORTICITY:** The vertical component of the geostrophic relative vorticity,  $\zeta = \hat{z} \cdot (\nabla \times \mathbf{u}) = \nabla_z^2 \psi$ , acts to bring out the smaller scale features in the streamfunction.
- **VERTICAL STRETCHING:** The final contribution arises from the vertical stretching in the presence of a rotating planet. Equation (40.22) helps to remind us why this term arises from vortex stretching.

## 40.4 Connecting quasi-geostrophic PV to Ertel PV

Following our treatment for the shallow water system in Section 38.6.4, we here determine how quasi-geostrophic potential vorticity relates to the Ertel potential vorticity from Chapter 36. For this purpose, consider the continuously stratified hydrostatic Boussinesq fluid and make use of the Ertel potential vorticity derived in Exercise 36.1

$$Q = (\boldsymbol{\omega} + \hat{z} f) \cdot \nabla b = \frac{\partial u}{\partial z} \frac{\partial b}{\partial y} - \frac{\partial v}{\partial z} \frac{\partial b}{\partial x} + (\zeta + f) \frac{\partial b}{\partial z}. \quad (40.53)$$

In a perfect fluid we have the material conservation

$$(\partial_t + \mathbf{u} \cdot \nabla_z + w \partial_z) Q = 0. \quad (40.54)$$

Our strategy in this section is to non-dimensionalize both  $Q$  and the material time operator, and then to stratify terms in equation (40.54) according to the Rossby number. We will show that material conservation of Ertel potential vorticity, when expanded asymptotically to order  $\text{Ro}^1$ , leads to the geostrophic material conservation of quasi-geostrophic potential vorticity. The continuous stratification makes the derivation more involved than for the shallow water model, prompting us to expose the details for practical experience with the formalism.

### 40.4.1 Non-dimensionalizing the Ertel potential vorticity

As above for the buoyancy, we are led to write the Ertel potential vorticity in the form

$$\frac{Q - f_0 N^2}{f_0 N^2} = \frac{1}{f_0 N^2} \left[ \frac{\partial u}{\partial z} \frac{\partial b'}{\partial y} - \frac{\partial v}{\partial z} \frac{\partial b'}{\partial x} \right] + \frac{1}{N^2} \frac{\partial b'}{\partial z} + \frac{\beta y + \zeta}{f_0} \left[ 1 + \frac{1}{N^2} \frac{\partial b'}{\partial z} \right]. \quad (40.55)$$

with non-dimensionalization leading to

$$\frac{1}{f_0 N^2} \left[ \frac{\partial u}{\partial z} \frac{\partial b'}{\partial y} - \frac{\partial v}{\partial z} \frac{\partial b'}{\partial x} \right] = \frac{B U}{f_0 N^2 H L} \left[ \frac{\partial \hat{u}}{\partial \hat{z}} \frac{\partial \hat{b}}{\partial \hat{y}} - \frac{\partial \hat{v}}{\partial \hat{z}} \frac{\partial \hat{b}}{\partial \hat{x}} \right] = \frac{\text{Ro}^2}{\text{Bu}} \left[ \frac{\partial \hat{u}}{\partial \hat{z}} \frac{\partial \hat{b}}{\partial \hat{y}} - \frac{\partial \hat{v}}{\partial \hat{z}} \frac{\partial \hat{b}}{\partial \hat{x}} \right] \quad (40.56a)$$

$$\frac{1}{N^2} \frac{\partial b'}{\partial z} = \frac{B}{H N^2} \frac{\partial \hat{b}}{\partial \hat{z}} = \frac{\text{Ro}}{\text{Bu}} \frac{\partial \hat{b}}{\partial \hat{z}} \quad (40.56b)$$

$$\frac{\beta y + \zeta}{f_0} = \text{Ro} (\hat{\beta} \hat{y} + \hat{\zeta}). \quad (40.56c)$$

The order  $\text{Ro}^2$  terms appearing in equation (40.56a) are dropped since they do not contribute to the quasi-geostrophic potential vorticity, which involve terms only up to order  $\text{Ro}^1$ . For the order  $\text{Ro}^1$  term, we only retain the zeroth order buoyancy,  $\hat{b}_0 = b_g/B$ , and likewise we just retain the zeroth order vorticity,  $\hat{\zeta}_0 = (L/U) \zeta_g$ . Hence, the Ertel potential vorticity is given by

$$Q = N^2 (f_0 + q_*) + \mathcal{O}(\text{Ro}^2) \quad (40.57)$$

where  $q_*$  is the order  $\text{Ro}^1$  term

$$q_* = \text{Ro} f_0 \left[ \frac{1}{\text{Bu}} \frac{\partial \hat{b}_0}{\partial \hat{z}} + \hat{\beta} \hat{y} + \hat{\zeta}_0 \right] = \frac{f_0}{N^2} \frac{\partial b_g}{\partial z} + \beta y + \zeta_g. \quad (40.58)$$

#### 40.4.2 Material conservation of Ertel PV to order $\text{Ro}^1$

The material conservation of Ertel PV now takes the form

$$(\partial_t + \mathbf{u}_g \cdot \nabla_z + w_{ag} \partial_z) (f_0 N^2 + q_* N^2) = f_0 w_{ag} \partial_z N^2 + N^2 D_g q_* / Dt = 0. \quad (40.59a)$$

We dropped the  $w_{ag} \partial_z$  contribution to the advection of  $q_*$  since ageostrophic vertical advection of  $q_*$  is an order  $\text{Ro}^2$  term. To eliminate the vertical ageostrophic velocity we make use of the buoyancy equation (40.40) so that

$$\frac{D_g q_*}{Dt} + \frac{w_{ag}}{N^2} \frac{\partial N^2}{\partial z} = \frac{D_g q_*}{Dt} - \frac{f_0}{N^4} \frac{D_g b_g}{Dt} \frac{\partial N^2}{\partial z} = 0. \quad (40.60)$$

Writing

$$\frac{\partial}{\partial z} \left[ \frac{1}{N^2} \right] = - \frac{1}{N^4} \frac{\partial N^2}{\partial z} \quad (40.61)$$

leads to

$$\frac{D_g q_*}{Dt} + f_0 \left[ \frac{\partial N^{-2}}{\partial z} \right] \frac{D_g b_g}{Dt} = 0. \quad (40.62)$$

Since the geostrophic material time derivative operator only involves horizontal advection, we can merge these two terms to render

$$\frac{D_g q_*}{Dt} + f_0 \left[ \frac{\partial N^{-2}}{\partial z} \right] \frac{D_g b_g}{Dt} = \frac{D_g}{Dt} \left[ q_* + f_0 b_g \left( \frac{\partial N^{-2}}{\partial z} \right) \right] \quad (40.63a)$$

$$= \frac{D_g}{Dt} \left[ \beta y + \zeta + \frac{f_0}{N^2} \left( \frac{\partial b_g}{\partial z} \right) + f_0 b_g \left( \frac{\partial N^{-2}}{\partial z} \right) \right] \quad (40.63b)$$

$$= \frac{D_g}{Dt} \left[ \beta y + \zeta + f_0 \frac{\partial}{\partial z} \left( \frac{b_g}{N^2} \right) \right] \quad (40.63c)$$

$$= \frac{D_g q}{Dt} \quad (40.63d)$$

$$= 0. \quad (40.63e)$$

In the penultimate step we introduced the quasi-geostrophic potential vorticity given by equation (40.52)

$$q = \beta y + \zeta + f_0 \frac{\partial}{\partial z} \left[ \frac{b_g}{N^2} \right] = q_* + f_0 b_g \frac{\partial N^{-2}}{\partial z}. \quad (40.64)$$

We have thus established how material conservation of Ertel potential vorticity, when expanded asymptotically to order  $\text{Ro}^1$ , leads to the geostrophic material conservation of quasi-geostrophic potential vorticity.

## 40.5 Mathematical expressions of the theory

In this section we sample various mathematical expressions of quasi-geostrophic theory as well as boundary conditions at the top and bottom of the domain.

### 40.5.1 The Jacobian form of geostropic advection

The geostrophic velocity, as a horizontally non-divergent field, can be written in terms of the quasi-geostrophic streamfunction

$$\mathbf{u}_g = \hat{\mathbf{z}} \times \nabla \psi. \quad (40.65)$$

We can thus write the following equivalent forms for the material time derivative of quasi-geostrophic PV

$$\frac{Dq}{Dt} = \frac{\partial q}{\partial t} + \mathbf{u}_g \cdot \nabla q \quad (40.66a)$$

$$= \frac{\partial q}{\partial t} + (\hat{\mathbf{z}} \times \nabla \psi) \cdot \nabla q \quad (40.66b)$$

$$= \frac{\partial q}{\partial t} + (\nabla \psi \times \nabla q) \cdot \hat{\mathbf{z}} \quad (40.66c)$$

$$= \frac{\partial q}{\partial t} + J(\psi, q). \quad (40.66d)$$

The final equality introduced the Jacobian operator  $J(\psi, q) = (\nabla \psi \times \nabla q) \cdot \hat{\mathbf{z}}$ , which is a notation commonly used in the geophysical fluids literature.<sup>4</sup>

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<sup>4</sup>Recall that we also encountered the Jacobian form for horizontally non-divergent two-dimensional advection in Section 33.2.3 when studying the non-divergent barotropic flows.

For a perfect fluid, in which  $Dq/Dt = 0$ , a steady state (zero Eulerian time derivative) is realized when

$$\mathbf{u}_g \cdot \nabla q = (\nabla\psi \times \nabla q) \cdot \hat{\mathbf{z}} = J(\psi, q) = 0. \quad (40.67)$$

Hence, the velocity is parallel to surfaces of constant  $q$ . We are ensured that these equalities hold if the streamfunction is a function only of the potential vorticity

$$\psi = \psi(q) \implies (\nabla\psi \times \nabla q) \cdot \hat{\mathbf{z}} = J(\psi, q) = 0. \quad (40.68)$$

As the steady state is of physical interest, this functional relation between streamfunction and potential vorticity commonly arises in applications.

### 40.5.2 Constant background buoyancy frequency

Consider the quasi-geostrophic potential vorticity for the special case of a constant background buoyancy frequency,  $N^2 = \text{constant}$ , in which the relative potential vorticity (40.51) takes on the form

$$q - \beta y = \nabla_z^2 \psi + \frac{\partial}{\partial z} \left[ \frac{f_0^2}{N^2} \frac{\partial \psi}{\partial z} \right] \quad (40.69a)$$

$$= \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} + \frac{f_0^2}{N^2} \frac{\partial^2 \psi}{\partial z^2} \quad (40.69b)$$

$$= [\partial_{xx} + \partial_{yy} + \partial_{zz}] \psi. \quad (40.69c)$$

For the final equality we introduced the vertical coordinate

$$\tilde{z} = (N/f) z. \quad (40.70)$$

Since  $|N/f| \gg 1$  the stably stratified flows considered in QG,  $\tilde{z}$  is a *stretched* vertical coordinate so that the Laplacian operator acting on  $\psi$  is anisotropic. The linear operator acting on  $\psi$  remains elliptic even in the more general case of a depth dependent stratification, thus warranting the use of elliptical solvers when performing the inversion numerically.

### 40.5.3 Vertical boundary conditions for $\psi$

We need boundary conditions on the geostrophic streamfunction,  $\psi$ , to invert the elliptic quasi-geostrophic PV equation (40.52). For lateral boundaries, one may choose periodicity, whereby the boundaries are absent. Alternatively, we may choose to set the normal component of the flow to zero for the inviscid case, in which case  $\psi$  is a constant along material boundaries as discussed in Section 16.4.2. The top and bottom boundaries require extra considerations as discussed here.

#### Buoyancy equation at the boundaries

To develop the vertical boundary conditions on the streamfunction, consider the quasi-geostrophic buoyancy equation (40.40)

$$D_g b_g / Dt + w_{ag} N^2 = 0. \quad (40.71)$$

Inserting the geostrophic streamfunction,  $b_g = f_0 \partial_z \psi$ , leads to

$$f_0 (\partial_t + \mathbf{u}_g \cdot \nabla_z) \partial_z \psi + w_{ag} N^2 = 0. \quad (40.72)$$

### Rigid top and bottom boundaries

At a rigid lid surface boundary or flat bottom boundary,  $w_{\text{ag}} = 0$ , in which case the boundary condition reduces to geostrophic advection of boundary buoyancy.

$$(\partial_t + \mathbf{u}_g \cdot \nabla_z) \partial_z \psi = 0 \quad \text{at } z = 0, \bar{\eta}_b \quad \text{if } w_{\text{ag}} = 0 \text{ at top and bottom boundaries.} \quad (40.73)$$

That is, the geostrophic buoyancy is materially invariant at the boundaries.

### Sloping bottom boundary condition

With a nonzero slope in the bottom topography,  $\nabla \eta_b \neq 0$ , the bottom kinematic boundary condition (Section 14.4.1) says that velocity is constrained so that

$$\mathbf{v} \cdot \hat{\mathbf{n}} = 0 \implies w = \mathbf{u} \cdot \nabla \eta_b, \quad (40.74)$$

where  $\hat{\mathbf{n}} = -\nabla(z - \eta_b)/|\nabla(z - \eta_b)|$  is the boundary's outward normal. Expanding this kinematic boundary condition leads to

$$w_{\text{ag}} = (\mathbf{u}_g + \mathbf{u}_{\text{ag}}) \cdot \nabla \eta_b, \quad (40.75)$$

which means there is vertical motion so long as the horizontal motion is not aligned with isobaths. To be clear on the implications of this boundary condition, it is useful to examine the asymptotics by non-dimensionalizing<sup>5</sup>

$$\mathbf{u}_g = U \hat{\mathbf{u}}_0 \quad (40.76a)$$

$$w_{\text{ag}} = W \text{Ro} \hat{w}_1 \quad (40.76b)$$

$$\mathbf{u}_{\text{ag}} = U \text{Ro} \hat{\mathbf{u}}_1 \quad (40.76c)$$

$$\nabla \eta_b = (\mathcal{B}/L) \hat{\nabla} \hat{\eta}_b = (H \text{Ro}/L) \hat{\nabla} \hat{\eta}_b, \quad (40.76d)$$

which brings the kinematic boundary condition (40.75) to

$$f_0 H \text{Ro}^2 (\hat{\mathbf{u}}_0 + \text{Ro} \hat{\mathbf{u}}_1) \cdot \hat{\nabla} \hat{\eta}_b = W \text{Ro} \hat{w}_1 \implies (\hat{\mathbf{u}}_0 + \text{Ro} \hat{\mathbf{u}}_1) \cdot \hat{\nabla} \hat{\eta}_b = \hat{w}_1. \quad (40.77)$$

Asymptotic consistency implies that

$$\hat{\mathbf{u}}_0 \cdot \hat{\nabla} \hat{\eta}_b = \hat{w}_1 \implies \mathbf{u}_g \cdot \nabla \eta_b = w_{\text{ag}}. \quad (40.78)$$

Hence, for quasi-geostrophic flow, any projection of the horizontal geostrophic velocity in a direction not aligned with isobaths leads to an ageostrophic vertical velocity component.

Use of the bottom kinematic boundary condition in the buoyancy equation (40.72) leads to the bottom boundary evolution of buoyancy

$$f_0 \partial_t (\partial_z \psi) + \mathbf{u}_g \cdot \nabla_z [f_0 \partial_z \psi + N^2 \eta_b] = 0 \quad \text{at } z = \bar{\eta}_b. \quad (40.79)$$

The boundary condition is evaluated at  $z = \bar{\eta}_b$  since the more precise boundary location,  $z = \eta_b(x, y)$ , is higher order in Rossby number.

#### 40.5.4 Potential vorticity induction and impermeability

The potential vorticity equation is the sole prognostic equation required to evolve the quasi-geostrophic flow. Consequently, one often discards the the quasi-geostrophic velocity and buoy-

<sup>5</sup>The bottom topography slope is non-dimensionalized according to the shallow water discussion in Section 38.3.4.

ancy equations. Even so, we found it useful to use the buoyancy equation in Section 40.3.4 as part of connecting quasi-geostrophic and Ertel potential vorticities. Likewise, there are occasions when it is useful to examine the velocity equation, with a similar discussion provided in Section 38.6.3. In this section we directly connect the velocity and buoyancy equations and then reveal their connection to the potential vorticity equation.

### Combining the velocity and buoyancy equations

Consider the quasi-geostrophic velocity and buoyancy equations derived in Section 40.3

$$(\partial_t + \mathbf{u}_g \cdot \nabla) \mathbf{u}_g + \hat{\mathbf{z}} \times (\beta y \mathbf{u}_g + f_0 \mathbf{u}_{ag}) = -\nabla_z \varphi_{ag} + \mathbf{F} \quad (40.80a)$$

$$(\partial_t + \mathbf{u}_g \cdot \nabla_z) b_g + w_{ag} N^2 = \dot{b} \quad (40.80b)$$

$$f_0 \hat{\mathbf{z}} \times \mathbf{u}_g + \nabla_z \varphi_g = 0 \quad (40.80c)$$

$$\nabla \cdot \mathbf{u}_g = \partial_x u_g + \partial_y v_g = 0 \quad (40.80d)$$

$$\nabla \cdot \mathbf{v}_{ag} = \nabla \cdot \mathbf{u}_{ag} + \partial_z w_{ag} = 0, \quad (40.80e)$$

where we added a non-conservative force per mass,  $\mathbf{F}$  (e.g., friction, wind stress), and irreversible buoyancy source,  $\dot{b}$  (e.g., diffusion, boundary fluxes). Taking  $-\hat{\mathbf{z}} \times$  on the velocity equation and multiplying the buoyancy equation by  $f_0/N^2$  leads to

$$(\partial_t + \mathbf{u}_g \cdot \nabla)(-\hat{\mathbf{z}} \times \mathbf{u}_g) + \beta y \mathbf{u}_g + f_0 \mathbf{u}_{ag} = \hat{\mathbf{z}} \times \nabla_z \varphi_{ag} - \hat{\mathbf{z}} \times \mathbf{F} \quad (40.81a)$$

$$(\partial_t + \mathbf{u}_g \cdot \nabla_z)(f_0 b_g/N^2) + f_0 w_{ag} = f_0 \dot{b}/N^2. \quad (40.81b)$$

Introduce the following vector fields

$$\mathbf{D} \equiv -\hat{\mathbf{z}} \times \mathbf{u}_g + (f_0/N^2) b_g \hat{\mathbf{z}} = \nabla_z \psi + (f_0/N)^2 \partial_z \psi \hat{\mathbf{z}} \quad (40.82a)$$

$$\mathbf{R} \equiv -\hat{\mathbf{z}} \times \mathbf{F} + (f_0/N^2) \dot{b} \hat{\mathbf{z}}, \quad (40.82b)$$

with  $\mathbf{D}$  built from both the velocity and buoyancy fields and  $\mathbf{R}$  built from the corresponding non-conservative tendencies. These vectors combine the velocity and buoyancy equations into a single vector equation

$$(\partial_t + \mathbf{u}_g \cdot \nabla) \mathbf{D} + \beta y \mathbf{u}_g + f_0 \mathbf{v}_{ag} = \hat{\mathbf{z}} \times \nabla_z \varphi_{ag} + \mathbf{R}. \quad (40.83)$$

### Potential vorticity induction

The divergence of  $\mathbf{D}$  yields the relative quasi-geostrophic potential vorticity

$$\nabla \cdot \mathbf{D} = q - \beta y. \quad (40.84)$$

In analogy to Gauss's law of electromagnetism, we refer to  $\mathbf{D}$  as the quasi-geostrophic potential vorticity *induction vector*.<sup>6</sup> Additionally, the potential vorticity equation can be written (see Exercise 40.5)

$$(\partial_t + \mathbf{u}_g \cdot \nabla) q = \nabla \cdot \mathbf{R}, \quad (40.85)$$

so that the quasi-geostrophic potential vorticity flux vector

$$\mathbf{J}_q = \mathbf{u}_g q - \mathbf{R} \quad (40.86)$$

---

<sup>6</sup>This connection between potential vorticity dynamics and electromagnetism was pointed out by [Schneider et al. \(2003\)](#) and further examined by [Maddison and Marshall \(2013\)](#).

allows us to write the potential vorticity equation in the Eulerian flux-form

$$\partial_t q = -\nabla \cdot \mathbf{J}_q. \quad (40.87)$$

### *Kinematic PV flux and impermeability*

Taking the Eulerian time derivative of the potential vorticity induction equation (40.84) renders

$$\partial_t q = \partial_t (\nabla \cdot \mathbf{D}) = \nabla \cdot (\partial_t \mathbf{D}) \equiv -\nabla \cdot \mathbf{J}_q^{\text{kin}}, \quad (40.88)$$

where we introduced the kinematic form of the potential vorticity flux

$$\mathbf{J}_q^{\text{kin}} \equiv -\partial_t \mathbf{D} = \mathbf{J}_q + \nabla \times \mathbf{A}, \quad (40.89)$$

with  $\mathbf{A}$  a gauge function.

which is analogous to the kinematic Ertel PV flux discussed in Section 37.2.2.

## 40.6 Energetics for quasi-geostrophic flow

Consider a quasi-geostrophic fluid configured with flat upper (rigid lid) and lower boundaries, and assume the lateral boundaries are either periodic or constant streamfunction on solid boundaries. These restrictive assumptions allow us to more readily study energetics within the fluid, sans the impacts from boundary effects. For this purpose we make use of the quasi-geostrophic vorticity and buoyancy equations

$$\frac{\partial \zeta}{\partial t} + \mathbf{u} \cdot \nabla \zeta = f_0 \frac{\partial w}{\partial z} \quad (40.90a)$$

$$\frac{\partial b}{\partial t} + \mathbf{u} \cdot \nabla b = -w N^2, \quad (40.90b)$$

where all labels are dropped from the variables to reduce clutter, and where

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla \quad b = f_0 \frac{\partial \psi}{\partial z} \quad u = -\frac{\partial \psi}{\partial y} \quad v = \frac{\partial \psi}{\partial x} \quad \zeta = \nabla_z^2 \psi. \quad (40.91)$$

### 40.6.1 Kinetic energy

The kinetic energy per mass for the total fluid domain is given by the integral

$$\mathcal{K} = \frac{1}{2} \int \mathbf{u} \cdot \mathbf{u} dV = \frac{1}{2} \int \nabla_z \psi \cdot \nabla_z \psi dV, \quad (40.92)$$

and its time derivative is

$$\frac{d\mathcal{K}}{dt} = \int \nabla_z \psi \cdot \nabla_z (\partial \psi / \partial t) dV. \quad (40.93)$$

For this result, we noted that the fluid domain has a constant volume to thus allow the time derivative to move inside the integral without introducing boundary terms. Manipulation renders

$$\frac{d\mathcal{K}}{dt} = \int \nabla_z \psi \cdot \nabla_z (\partial \psi / \partial t) dV \quad (40.94a)$$

$$= \int [\nabla_z \cdot [\psi \nabla_z (\partial \psi / \partial t)] - \psi \partial (\nabla_z^2 \psi) / \partial t] dV \quad (40.94b)$$

$$= - \int \psi (\partial \zeta / \partial t) dV, \quad (40.94c)$$

where we dropped the lateral boundary term and introduced relative vorticity. Use of the vorticity equation (40.90a) yields

$$\frac{d\mathcal{K}}{dt} = - \int \psi (\partial \zeta / \partial t) dV = \int \psi [\mathbf{u} \cdot \nabla_z \zeta - f_0 \partial_z w] dV. \quad (40.95)$$

The first term vanishes since

$$\int \psi (\mathbf{u} \cdot \nabla_z \zeta) dV = \int \psi \nabla_z \cdot (\mathbf{u} \zeta) dV = \int [\nabla_z \cdot (\psi \mathbf{u} \zeta) - \nabla_z \psi \cdot \mathbf{u} \zeta] dV = 0, \quad (40.96)$$

where the boundary term vanishes and  $\mathbf{u} \cdot \nabla_z \psi = 0$  since  $\psi$  is the streamfunction for the horizontal geostrophic flow. We are thus left with the expression for the kinetic energy evolution

$$\frac{d\mathcal{K}}{dt} = - \int \psi f_0 \frac{\partial w}{\partial z} dV. \quad (40.97)$$

Since the top and bottom are assumed flat, the vertical velocity vanishes on these boundaries (rigid lid top and flat bottom), in which case

$$\frac{d\mathcal{K}}{dt} = - \int \psi f_0 \frac{\partial w}{\partial z} dV = - \int f_0 \left[ \frac{\partial(w \psi)}{\partial z} - w \frac{\partial \psi}{\partial z} \right] dV = \int f_0 w \frac{\partial \psi}{\partial z} dV. \quad (40.98)$$

Making use of  $b = f_0 \partial \psi / \partial z$  leads to

$$\frac{d\mathcal{K}}{dt} = \int w b dV. \quad (40.99)$$

Kinetic energy thus increases when vertical motion is positively correlated with anomalous buoyancy. For example, upward motion ( $w > 0$ ) of a positive buoyancy anomaly (relatively light water has  $b > 0$ ) increases kinetic energy, as does downward motion of a negative buoyancy anomaly. This behavior is also reflected in the full fluid system discussed in Section 21.3.

### 40.6.2 Available potential energy

Available potential energy was introduced in Section 23.8 within the context of the Boussinesq fluid. An approximate form of the APE is given by equation (23.170), which we here write in the form

$$\mathcal{A}_{\text{bouss}} \approx \frac{1}{2} \int \left[ \frac{b}{N} \right]^2 dV. \quad (40.100)$$

With  $b = f_0 \partial \psi / \partial z$ , the quasi-geostrophic APE is given by

$$\mathcal{A} = \frac{1}{2} \int \left[ \frac{f_0}{N} \frac{\partial \psi}{\partial z} \right]^2 dV. \quad (40.101)$$

Taking a time derivative leads to

$$\frac{d\mathcal{A}}{dt} = \int \left[ \frac{f_0}{N} \right]^2 \frac{\partial\psi}{\partial z} \frac{\partial}{\partial t} \frac{\partial\psi}{\partial z} dV = \int \frac{f_0}{N^2} \frac{\partial\psi}{\partial z} [-w N^2 - \nabla_z \cdot (\mathbf{u} b)] dV, \quad (40.102)$$

where we used the buoyancy equation (40.90b) for the second equality. The second term vanishes since

$$\int \frac{f_0}{N^2} \frac{\partial\psi}{\partial z} [\nabla_z \cdot (\mathbf{u} b)] dV = \int \left[ \frac{f_0^2}{N^2} \frac{\partial\psi}{\partial z} \right] \mathbf{u} \cdot \nabla_z \left[ \frac{\partial\psi}{\partial z} \right] dV = \frac{1}{2} \int \nabla_z \cdot \left[ \mathbf{u} \left( \frac{f_0}{N} \frac{\partial\psi}{\partial z} \right)^2 \right] dV = 0. \quad (40.103)$$

Consequently, the quasi-geostrophic APE has a time derivative given by

$$\frac{d\mathcal{A}}{dt} = - \int w f_0 \frac{\partial\psi}{\partial z} dV = - \int w b dV, \quad (40.104)$$

so that the APE evolves oppositely to the kinetic energy.

### 40.6.3 Energy conversion

Notice how the evolution of kinetic energy involves the relative vorticity equation, whereas evolution of the APE involves the buoyancy equation. However, their sum remains constant in time since as the kinetic energy increases through buoyancy work, the available potential energy decreases

$$\frac{d(\mathcal{K} + \mathcal{A})}{dt} = 0. \quad (40.105)$$

The buoyancy work conversion term is given by

$$\text{buoyancy work} = \int w f_0 \frac{\partial\psi}{\partial z} dV = \int w b dV, \quad (40.106)$$

which has the same form as that encountered for the conversion between potential and kinetic energy in the unapproximated equations studied in Section 21.3.

### 40.6.4 Scaling APE and KE

The scale for the kinetic energy is given by

$$\mathcal{K} = \frac{1}{2} \int (\nabla_z \psi \cdot \nabla_z \psi) dV \sim L^{-2} \Psi^2 V \quad (40.107)$$

and the scale for the APE is

$$\mathcal{A} = \frac{1}{2} \int \left[ \frac{f_0}{N} \frac{\partial\psi}{\partial z} \right]^2 dV \sim H^{-2} (f_0/N)^2 \Psi^2 V = L_d^{-2} \Psi^2 V, \quad (40.108)$$

where we wrote  $\Psi$  for the streamfunction scale,  $V$  for the domain volume, and  $L_d = H(N/f_0)$  is the deformation radius (see equation (40.7)). Taking the ratio yields

$$\frac{\mathcal{K}}{\mathcal{A}} \sim \left[ \frac{L_d}{L} \right]^2 = \left[ \frac{H}{L} \right]^2 \left[ \frac{N}{f_0} \right]^2 = \text{Bu}. \quad (40.109)$$

Hence, the Burger number is the ratio of the quasi-geostrophic kinetic energy scale to the quasi-geostrophic available potential energy scale. A large Burger number means that the horizontal scales of the flow are smaller than the deformation radius, in which case the QG dynamics is dominated by its kinetic energy. In contrast, for scales larger than the deformation radius (not much larger, as then the flow would not satisfy QG scaling), the Burger number is less than unity, in which case the QG dynamics is dominated by available potential energy.



## 40.7 Exercises

### EXERCISE 40.1: A VARIETY OF POTENTIAL VORTICITIES

Give the mathematical expressions for potential vorticity in the following fluid models. Define all terms in the respective expressions. Give the physical dimensions and/or SI units for the potential vorticity. Hint: the answers can be found somewhere in this book.

- (a) Ertel PV for compressible fluid in a rotating reference frame using potential temperature as the tracer.
- (b) Ertel PV for an incompressible (Boussinesq) fluid in a rotating reference frame using buoyancy as the tracer.
- (c) Single shallow water layer on a beta plane
- (d) Continuously stratified planetary geostrophic flow
- (e) Continuously stratified quasi-geostrophic flow on a beta plane

### EXERCISE 40.2: QUASI-GEOSTROPHIC PV EVOLUTION WITH VERTICAL FRICTION

The first part of this exercise involves elements of the asymptotic method used for deriving the QG equations, only now with the advent of a non-zero friction. Use is made to incorporate the non-dimensionalization detailed in Section 27.1, which provides a detailed discussion of the Ekman number and Ekman layers. The second part of this exercise makes use of the thermal wind balance to connect horizontal buoyancy transfer to the vertical viscous transfer of horizontal momentum.

- (a) Derive the material evolution equation for quasi-geostrophic PV in a continuously stratified Boussinesq fluid in the presence of friction,  $\mathbf{F}$ . Assume the Ekman number is on the order of the Rossby number, so that the zeroth order asymptotic solution satisfies the usual inviscid  $f$ -plane geostrophic balance. Friction only appears in the first order equations.
- (b) Assume friction arises just from vertical shears in the horizontal velocity, so that

$$\mathbf{F} = \frac{\partial}{\partial z} \left[ \nu \frac{\partial \mathbf{u}}{\partial z} \right], \quad (40.110)$$

where  $\nu = \nu(z)$  is a vertical eddy viscosity that is a function of depth (dimensions of squared length per time). Also assume an approximate form of quasi-geostrophic PV in which we drop relative vorticity (i.e., quasi-geostrophic PV is dominated by planetary vorticity and

stretching). Determine the form for the vertical eddy viscosity so that the approximate form of quasi-geostrophic PV is laterally diffused via

$$\frac{Dq^{\text{approx}}}{Dt} = A \nabla_z^2 q^{\text{approx}}, \quad (40.111)$$

where  $A$  is a constant eddy diffusivity for the potential vorticity.

Hint: to leading order, the friction operator is a function just of the geostrophic velocity.

#### EXERCISE 40.3: QUASI-GEOSTROPHIC $\omega$ -EQUATION

As we discovered in this chapter, for quasi-geostrophy the vertical component to the velocity is non-zero only at first order in Rossby number, whereas the zeroth order flow is horizontal and geostrophic. To time step the horizontal geostrophic flow it is not necessary to explicitly compute the ageostrophic vertical velocity. However, there are cases where it is of interest. In this exercise we derive the  $\omega$ -equation for quasi-geostrophic flow, thus providing a diagnostic expression for the ageostrophic vertical velocity. The name for this equation originates from the atmospheric community where  $\omega$  is the common symbol for transport across pressure surfaces. Here, we make use of the Boussinesq system so that the vertical velocity component is across depth surfaces.

An outline for the derivation of the traditional form for the  $\omega$ -equation is given in Section 5.4 of [Vallis \(2017\)](#) for the anelastic version of quasi-geostrophy and for the  $f$ -plane. Here we work with the Boussinesq system and consider a  $\beta$ -plane. Nonetheless, the solution is nearly the same as in [Vallis \(2017\)](#). Hence, your job throughout this exercise is to fully explain the derivation and show each of the relevant steps.

- (a) Cross-multiply the dimensional buoyancy and vorticity equations from Section 40.3 to eliminate the time derivative, thus deriving a diagnostic equation for the ageostrophic vertical velocity that is valid to order  $\text{Ro}^1$ .
- (b) The diagnostic equation you should have derived takes the form

$$\mathcal{L}w = \sigma, \quad (40.112)$$

where

$$\mathcal{L} = N^2 \nabla_z^2 + f_0^2 \frac{\partial^2}{\partial z^2} \quad (40.113)$$

is a linear partial differential operator and

$$\sigma = f_0 \partial_z [J(\psi, \zeta + \beta y)] - \nabla_z^2 J(\psi, b) \quad (40.114)$$

is a source term. The source is a function of the geostrophic flow and the buoyancy field. For vertically stable stratification,  $N^2 > 0$ , characterize the differential operator,  $\mathcal{L}$ , according to the elliptic, hyperbolic, or parabolic classes discussed in Section 3.4. What about when  $N^2 < 0$ ? What new physical phenomena do you expect when  $N^2 < 0$ ?

#### EXERCISE 40.4: HOSKINS' FORM OF THE QUASI-GEOSTROPHIC $\omega$ -EQUATION

We here rederive the  $\omega$ -equation from Exercise 40.3 using methods introduced by [Hoskins et al. \(1978\)](#). It is not necessary to have solved Exercise 40.3 to solve the present exercise.

Hoskins' approach reveals an insightful form for the source function contributing to vertical motion. As in Exercise 40.3, we work with the adiabatic and hydrostatic Boussinesq system (see

Section 39.2)

$$\frac{Du}{Dt} - fv = -\frac{\partial \varphi}{\partial x} \quad (40.115a)$$

$$\frac{Dv}{Dt} + fu = -\frac{\partial \varphi}{\partial y} \quad (40.115b)$$

$$\frac{\partial \varphi}{\partial z} = b \quad (40.115c)$$

$$\frac{Db}{Dt} = 0 \quad (40.115d)$$

$$\nabla \cdot \mathbf{v} = \nabla_z \cdot \mathbf{u} + \frac{\partial w}{\partial z} = 0 \quad (40.115e)$$

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla. \quad (40.115f)$$

In Exercise 40.3, we derived the  $\omega$ -equation making use of the buoyancy equation and vorticity equation. *Hoskins et al.* (1978) worked with the momentum equation rather than the vorticity equation. For this purpose, rather than consider an asymptotic expansion, Hoskins exactly decomposed the horizontal velocity into its geostrophic and ageostrophic components

$$\mathbf{u} = \mathbf{u}_g + \mathbf{u}_{ag}, \quad (40.116)$$

with the geostrophic velocity balancing the horizontal gradient of the full pressure field

$$f\mathbf{u}_g = \hat{\mathbf{z}} \times \nabla \varphi. \quad (40.117)$$

This definition for  $\mathbf{u}_g$  is distinct from that arising from an asymptotic expansion, whereby the geostrophic velocity is the zeroth order term balancing the zeroth order pressure gradient (see Section 40.2.1 or Exercise 40.3). We are generally able to access the full hydrostatic pressure field through knowledge of the buoyancy field, in which case there is no need to make an asymptotic expansion of pressure.

Hoskins' definition for the geostrophic velocity brings the horizontal momentum equations into the rather elegant form

$$\frac{Du}{Dt} + f\hat{\mathbf{z}} \times \mathbf{u}_{ag} = 0, \quad (40.118)$$

with the pressure gradient annihilated since it exactly balances the geostrophic velocity. In this manner, the material evolution of horizontal velocity is determined solely by the ageostrophic Coriolis acceleration. Again, there has been no approximation made thus far. Rather, we have only introduced a strategic decomposition of the velocity field as per Hoskins.

At this point we make the quasi-geostrophic approximation by setting the momentum equation equal to

$$\frac{\partial \mathbf{u}_g}{\partial t} + (\mathbf{u}_g \cdot \nabla_z) \mathbf{u}_g + f\hat{\mathbf{z}} \times \mathbf{u}_{ag} = 0 \quad (40.119)$$

and the buoyancy equation equal to

$$\frac{\partial b}{\partial t} + \mathbf{u}_g \cdot \nabla_z b + N^2 w = 0, \quad (40.120)$$

where  $N^2(z)$  is a prescribed static background stratification. That is, both the horizontal geostrophic velocity and the buoyancy are advected just by the geostrophic velocity. The buoyancy equation is the same as derived to order  $\text{Ro}^1$  using asymptotic methods (Section 40.2.2). However, Hoskins'

momentum equation (40.119) has no pressure gradient on the right hand side, whereas an asymptotic approach has contributions from higher order pressure gradients (Section 40.2.2). Hoskins' approach dispenses with such pressure terms by defining the geostrophic velocity using the full pressure field.

- (a) Show that the evolution of horizontal buoyancy gradients by the horizontal geostrophic currents can be written

$$\left[ \frac{\partial}{\partial t} + \mathbf{u}_g \cdot \nabla_z \right] |\nabla_z b|^2 = \mathbf{Q} \cdot \nabla_z b. \quad (40.121)$$

Hence, horizontal buoyancy gradients grow in magnitude in regions where the horizontal buoyancy gradient projects positively onto the  $\mathbf{Q}$ -vector. Write the expression for the vector  $\mathbf{Q}$ . Hint: A general version of this result was derived in Exercise 12.2.

- (b) Show that the quasi-geostrophic  $\omega$ -equation on an  $f$ -plane can be written

$$N^2 \nabla_z^2 w + f_0^2 \frac{\partial^2 w}{\partial z^2} = 2 \nabla_z \cdot \mathbf{Q}. \quad (40.122)$$

We see that the source for vertical motion is the divergence of the  $\mathbf{Q}$ -vector. This formula offers useful insight into the origin of vertical motion, with [Hoskins et al. \(1978\)](#) offering examples. For this part of the exercise, you are to fully explain the derivation of equation (40.122) and show each of the relevant steps.

- (c) The equation (40.122) for the vertical velocity takes the form

$$\mathcal{L}w = \sigma, \quad (40.123)$$

where

$$\mathcal{L} = N^2 \nabla_z^2 + f_0^2 \frac{\partial^2}{\partial z^2} \quad (40.124)$$

is a linear partial differential operator and

$$\sigma = 2 \nabla_z \cdot \mathbf{Q} \quad (40.125)$$

is a source term. The source term is a function of the geostrophic flow and the buoyancy field. For vertically stable stratification,  $N^2 > 0$ , characterize the differential operator  $\mathcal{L}$  according to the elliptic, hyperbolic, or parabolic classes discussed in Section 3.4. What about when  $N^2 < 0$ ? What new physical phenomena do you expect when  $N^2 < 0$ ?

#### EXERCISE 40.5: QGPV FLUX-FORM EQUATION WITH NON-CONSERVATIVE PROCESSES

Derive the quasi-geostrophic potential vorticity equation (40.85). Show all the relevant steps. Hint: the key step requires showing that

$$\nabla \cdot [(\mathbf{u}_g \cdot) \mathbf{D}] = (\mathbf{u}_g \cdot) \nabla \cdot \mathbf{D}. \quad (40.126)$$

To do so, it is useful to express  $\mathbf{u}_g$  and  $b_g$  in terms of the geostrophic streamfunction.





**Part VIII**

**Generalized vertical coordinates**

*Generalized vertical coordinates (GVCs)* offer a mathematical framework for describing stratified fluid mechanics. Hence, they appear in many guises throughout geophysical fluid mechanics theory and numerical modeling. GVCs were introduced by [Starr \(1945\)](#) for atmospheric modeling and [Bleck \(1978\)](#) for ocean modeling. There is a growing use of GVC-based numerical ocean (e.g., [Griffies et al. \(2020\)](#)) and atmospheric models. This usage prompts the need to master their use for analysis, model formulation, and theory, thus providing motivation for this part of the book.

GVCs are both time dependent and non-orthogonal coordinates, which represents both their strength and their complexity. Both features require extra mathematical care beyond that needed with the more familiar static and orthogonal coordinates considered in Chapter 8. The key reason to favor the use of non-orthogonal GVCs, rather than a locally orthogonal coordinate set, is that gravity plays a dominant role in orienting geophysical fluid motion. Hence, it is strategically useful to decompose the equations of motion so that lateral motions are perpendicular to gravity, just like with familiar Cartesian geopotential vertical coordinates. That is, we orient horizontal motions the same regardless whether we use Cartesian coordinates or GVCs, since doing so removes the vertical pressure force from the horizontal equations of motion.

If we were to locally rotate the components of the velocity vector to be parallel and perpendicular to the surface of constant generalized vertical coordinate, as per a locally orthogonal coordinate description, then that representation would introduce a portion of the vertical pressure gradient into the equations for lateral motion. Having the vertical pressure gradient appear in each of the three components to the equations of motion makes it very difficult to isolate the hydrostatic pressure force. In turn, it makes it difficult to describe nearly all of the basic features of geophysical flows, such as the geostrophic and hydrostatic balances. We thus consider locally orthogonal generalized vertical coordinates to be of minimal use for the dynamical equations of geophysical fluid mechanics. Even so, they are useful for orienting the tracer diffusion operator within the ocean interior, as discussed in Section 48.4.

In this part of the book we develop the mathematics of generalized vertical coordinates, and then build up the kinematics and dynamics of stratified fluid mechanics using these coordinates and then encounter some example applications. These chapters are written in the style of a monograph, with equations derived in detail and concepts explored. Here is a brief summary of these chapters.

- MATHEMATICAL FOUNDATIONS: Chapter 41 initiates our study of the mathematics of generalized vertical coordinates. As noted already, their time dependence and their non-orthogonality present some complexity in both concept and detail. Even so, with some experience, generalized vertical coordinates can become a versatile member of our theoretical and numerical toolkit.
- Chapters 42 and 43 describes elements of fluid kinematics and dynamics using generalized vertical coordinates.
- Chapter 44 formulates the hydrostatic Boussinesq equations using buoyancy as the vertical coordinate. This chapter specializes elements from the previous chapters, and in so doing provides a mathematical and physical basis for *isopycnal* models of the ocean and isentropic models of the atmosphere.
- Chapter 45 provides further insights into eddy and mean flow decomposition, this time making use of thickness weighted averaging (TWA) for the shallow water model. We position this chapter in this part of this book since it makes use of the layered perspective of generalized vertical coordinates, particularly isopycnal coordinates. Indeed, the adiabatic stacked shallow water model is a discrete realization of the perfect fluid isopycnal equations. The

TWA formalism of this chapter offers a technically less difficult rendition of the formalism when applied to the continuously stratified isopycnal coordinates.



# Chapter 41

## Mathematical basics

In this chapter we present the mathematics of generalized vertical coordinates (GVC), with Figure 41.1 offering a schematic of how these coordinates monotonically partition the vertical direction. Such coordinates are of particular use for stratified fluid mechanics, where it is often convenient to make use of a vertical coordinate distinct from, but uniquely related to, the geopotential vertical coordinate,  $z$ .

### CHAPTER GUIDE

We make use of the general tensor analysis detailed in Chapter 7. We mostly consider just the spatial tensors in this chapter, consistent with the Newtonian perspective whereby time is universal. However, since the vertical coordinate is a function of time, we follow the space-time perspective from Section 7.9 for transforming the partial derivative operator. Chapters directly relying on the material from this chapter include the fluid kinematics discussed in Chapter 42, the general vertical coordinate dynamics discussed in Chapter 43, and the tracer equation diffusion and stirring operators discussed in Chapter 48,

41.1	Relating Cartesian and GVCs	1024
41.2	Example generalized vertical coordinates	1026
41.2.1	Pressure coordinates	1026
41.2.2	Terrain following coordinates	1026
41.2.3	Bottom slope oriented coordinates	1026
41.2.4	Isopycnal or buoyancy coordinates	1026
41.3	Spatial basis vectors	1027
41.3.1	More on the transformation matrix	1027
41.3.2	Expressions for the basis vectors	1027
41.4	Basis one-forms	1028
41.4.1	More on the inverse transformation matrix	1028
41.4.2	GVC basis one-forms	1029
41.4.3	Verifying the bi-orthogonality relation	1029
41.5	Triple product identities	1029
41.6	Position vector	1030
41.7	Transforming components of a vector	1032
41.8	Velocity	1033
41.8.1	Contravariant components	1033
41.8.2	Covariant components	1033
41.8.3	Introducing the material time derivative	1033

---

41.8.4	Equivalence to the Cartesian velocity representation . . . . .	1034
41.9	Metric tensor . . . . .	1034
41.9.1	Jacobian of transformation . . . . .	1034
41.9.2	Covariant and contravariant representations . . . . .	1035
41.10	Volume element and the Levi-Civita tensor . . . . .	1035
41.11	Vector cross product of basis vectors . . . . .	1035
41.12	Partial derivative operators . . . . .	1036
41.12.1	Analytical derivation . . . . .	1036
41.12.2	Geometrical derivation . . . . .	1036
41.13	Material time derivative . . . . .	1038
41.14	Divergence of a vector and the divergence theorem . . . . .	1038
41.15	The diffusion operator . . . . .	1038
41.15.1	Continuous expression . . . . .	1039
41.15.2	Layer thickness weighted diffusion operator . . . . .	1039
41.16	Vorticity . . . . .	1040
41.16.1	The components . . . . .	1041
41.16.2	Transforming from Cartesian coordinates . . . . .	1041
41.17	Velocity circulation . . . . .	1041

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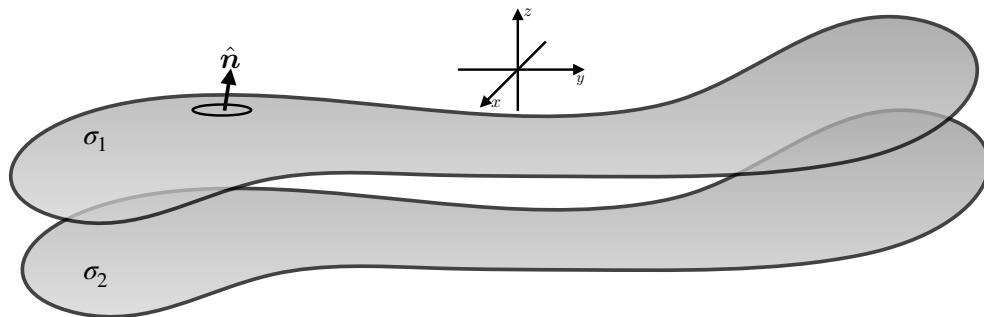


FIGURE 41.1: This stylized schematic illustrates the geometry of two surfaces of constant generalized vertical coordinate  $\sigma(x, y, z, t) = \sigma_1$  and  $\sigma(x, y, z, t) = \sigma_2$ , here showing patches on two such surfaces. The surfaces are generally undulating in space and time yet are assumed to monotonically layer the fluid. Monotonic layering means that the surface normal,  $\hat{n}$ , always has a non-zero projection onto the vertical:  $\hat{n} \cdot \hat{z} \neq 0$ . That is, the surfaces never become vertical nor do they overturn. It also means that there is a 1-to-1 invertible relation between  $\sigma$  and geopotential, so that specifying  $(x, y, \sigma(x, y, z, t))$  is sufficient to yield a unique  $z$ .

## 41.1 Relating Cartesian and GVCs

We make use of the symbol  $\sigma$  for a generalized vertical coordinate. This coordinate is *not* orthogonal to the horizontal spatial coordinates  $x, y$ . This is a central property of GVCs that influences nearly all aspects of their calculus. To help develop the mathematics for transforming between Cartesian coordinates and GVCs, it is important to distinguish the two coordinate systems. For that purpose we write the time coordinate and spatial Cartesian coordinates according to

$$\xi^\alpha = (\xi^0, \xi^a) = (\xi^0, \xi^1, \xi^2, \xi^3) = (t, x, y, z) \quad \text{with } \alpha = 0, 1, 2, 3, \text{ and } a = 1, 2, 3. \quad (41.1)$$

As defined, the tensor label  $a$  runs over the spatial coordinates 1, 2, 3 whereas  $\alpha$  also includes the time coordinate with  $\alpha = 0$ . The corresponding generalized vertical coordinates are denoted with an overbar

$$\bar{\xi}^{\bar{\alpha}} = (\bar{\xi}^{\bar{0}}, \bar{\xi}^{\bar{1}}, \bar{\xi}^{\bar{2}}, \bar{\xi}^{\bar{3}}) = (\bar{t}, \bar{x}, \bar{y}, \sigma). \quad (41.2)$$

The 1-to-1 coordinate transformation between Cartesian and GVC coordinates is written

$$\xi^{\bar{0}} = \xi^0 \iff \bar{t} = t \quad (41.3a)$$

$$\xi^{\bar{1}} = \xi^1 \iff \bar{x} = x \quad (41.3b)$$

$$\xi^{\bar{2}} = \xi^2 \iff \bar{y} = y \quad (41.3c)$$

$$\xi^{\bar{3}} = \sigma(x, y, z, t), \quad (41.3d)$$

with the final relation expressing the generalized vertical coordinate as a function of space and time. We ordered the appearance of independent variables in  $\sigma$  with time in the last position, which is the conventional ordering in this book for functions of space and time even though the zeroth coordinate is time.

The coordinate transformation is invertible so that we can write

$$\xi^0 = \xi^{\bar{0}} \quad (41.4a)$$

$$\xi^1 = \xi^{\bar{1}} \quad (41.4b)$$

$$\xi^2 = \xi^{\bar{2}} \quad (41.4c)$$

$$\xi^3 = \xi^3(\bar{x}, \bar{y}, \sigma, \bar{t}) = \xi^3(x, y, \sigma, t). \quad (41.4d)$$

The relation

$$\xi^3 = \xi^3(\xi^{\bar{a}}) = \xi^3(x, t, \sigma, t) \quad (41.5)$$

provides the vertical position of a given  $\sigma$  surface. Since  $\xi^3 = z$  one commonly writes

$$z = z(x, y, \sigma, t). \quad (41.6)$$

However, this expression is prone to confusion since the meaning of  $z$  is overloaded.<sup>1</sup> Namely, one meaning ascribes  $z$  to a particular value of the vertical position; i.e.,  $z = -100$  m. The other meaning, as on the right hand side, is for  $z$  as the vertical coordinate function of a particular  $\sigma$  surface, with this value a function of space, time, and  $\sigma$ . Learning to distinguish when  $z$  refers to a particular vertical position or as a coordinate function takes some practice, and those who routinely work with generalized vertical coordinates typically find no problem with the overloaded meanings. Indeed, after reading this chapter we should be able to hold the two meanings in our mind without confusion. As a reminder, we commonly write the vertical coordinate function as

$$z = \eta(x, y, \sigma, t), \quad (41.7)$$

where  $\eta$  is used throughout this book to represent the vertical position of a surface, such as the ocean free surface, solid-earth topography, or a generalized vertical coordinate surface. Hence, for example, the vertical position of a pressure surface of chosen value  $p$  is given by the functional relation

$$\xi^3 = z = \eta(\bar{x}, \bar{y}, p, \bar{t}) = \eta(x, y, p, t). \quad (41.8)$$

We make use of the  $\eta$  nomenclature where it seems useful but gradually sprinkle in more use of the  $z(x, y, \sigma, t)$  notation since it is proves to be natural for many of the formulations.

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<sup>1</sup>We use the term *overloaded* as in computer science where a symbol has more than one meaning or usage.

## 41.2 Example generalized vertical coordinates

Before further diving into the mathematics, we here offer some examples of generalized vertical coordinates commonly used to study geophysical fluid flows.

### 41.2.1 Pressure coordinates

Hydrostatic compressible fluids, such as the large-scale atmosphere, pressure is a convenient choice as vertical since it absorbs the appearance of density in many formula such as mass continuity as discussed in Section 42.10.2 and the geostrophic balance given by equation (25.1a). Hence, a natural expression of the compressible hydrostatic equations of motion make use of pressure rather than geopotential for the vertical coordinate, in which case  $\sigma = p(x, y, z, t)$ .

### 41.2.2 Terrain following coordinates

When allowing for a time dependent ocean free surface, the terrain following coordinate in oceanography is given by

$$\sigma = \frac{z - \eta_{\text{surf}}}{-\eta_b + \eta_{\text{surf}}} \quad \text{terrain following ocean coordinate,} \quad (41.9)$$

where  $z = \eta_{\text{surf}}(x, y, t)$  is the vertical position of the ocean surface. The terrain following coordinate is non-dimensional and extends from  $\sigma = 0$  at the ocean surface and  $\sigma = -1$  at the ocean bottom (where  $z = \eta_b(x, y)$ ). For rigid lid ocean models with  $\eta_{\text{surf}} = 0$ , the terrain following coordinate becomes time independent

$$\sigma = -\frac{z}{\eta_b} \quad \text{terrain following rigid lid ocean.} \quad (41.10)$$

Finally, for a compressible ocean, it is more convenient to use pressure to define the terrain following coordinate so that

$$\sigma = \frac{p - p_a}{p_b - p_a} \quad \text{terrain following atmosphere coordinate.} \quad (41.11)$$

In this equation,  $p_a$  is the pressure applied at the ocean surface and  $p_b$  is the pressure at the ocean bottom. For an atmosphere model we might set  $p_a$  as the top of the atmosphere pressure, which is typically assumed to be zero as in [Phillips \(1957\)](#).

### 41.2.3 Bottom slope oriented coordinates

[Peterson and Callies \(2022\)](#) consider an alternative to the traditional terrain following coordinates from Section 41.2.2, here defining a bottom slope oriented coordinate

$$\sigma = z - \mathbf{x} \cdot \nabla \eta_b = z - x \partial \eta_b / \partial x - y \partial \eta_b / \partial y, \quad (41.12)$$

with  $\nabla \eta_b$  the slope of the bottom topography.

### 41.2.4 Isopycnal or buoyancy coordinates

Buoyancy surfaces are material when there is no mixing. Hence, for the study of perfect fluid mechanics it is quite convenient to use the Archimedean buoyancy,  $b$ , as the vertical coordinate,  $\sigma = b(x, y, z, t)$ . Equivalently, one may choose the potential density as the vertical coordinate.

We have more to say about such vertical coordinates in Chapter 44 when developing the equations for isopycnal ocean models.

## 41.3 Spatial basis vectors

Making use of the tensor formalism from Chapter 7, consider the transformation of the Cartesian basis vectors into their corresponding GVC representation. This transformation takes is given by

$$\vec{e}_{\bar{a}} = \Lambda_{\bar{a}}^a \vec{e}_a, \quad (41.13)$$

where the transformation matrix is

$$\Lambda_{\bar{a}}^a = \begin{bmatrix} \partial x / \partial \bar{x} & \partial x / \partial \bar{y} & \partial x / \partial \sigma \\ \partial y / \partial \bar{x} & \partial y / \partial \bar{y} & \partial y / \partial \sigma \\ \partial z / \partial \bar{x} & \partial z / \partial \bar{y} & \partial z / \partial \sigma \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ \partial \eta / \partial \bar{x} & \partial \eta / \partial \bar{y} & \partial \eta / \partial \sigma \end{bmatrix}, \quad (41.14)$$

where the second equality used our preferred notation  $z = \eta(x, y, \sigma, t)$  for the vertical position of a  $\sigma$  surface. The diagonal unit values for the space-space components arise since a horizontal position in Cartesian and GVCs is the same and the horizontal directions are orthogonal. Likewise, the time coordinate does not change when changing  $\bar{x}$ ,  $\bar{y}$ , or  $\sigma$ . Additionally,  $\partial x / \partial \sigma = \partial y / \partial \sigma = 0$  since the horizontal position remains unchanged when moving across a GVC surface. In contrast, a non-zero value for  $\partial \eta / \partial \bar{x}$  and  $\partial \eta / \partial \bar{y}$  arise since we generally change vertical position when moving horizontally along a sloped  $\sigma$  surface. Finally, the element  $\partial \eta / \partial \sigma$  is nonzero due to vertical stratification of the fluid when represented using general vertical coordinates.

### 41.3.1 More on the transformation matrix

To further detail how to produce elements of the transformation matrix (41.14), it is crucial to ensure that the proper variables are held fixed when performing the partial derivatives. For example, consider the top row where we compute

$$\Lambda_{\bar{a}}^1 = [ [\partial x / \partial \bar{x}]_{\bar{y}, \sigma} \quad [\partial x / \partial \bar{y}]_{\bar{x}, \sigma} \quad [\partial x / \partial \sigma]_{\bar{x}, \bar{y}} ] \quad (41.15)$$

Since  $x = \bar{x}$ , all elements vanish except for the first. Namely,  $[\partial x / \partial \bar{y}]_{\bar{x}, \sigma} = 0$  since  $x$  cannot change when  $\bar{x}$  is fixed. The same idea leads to the results for  $y$  derivatives.

### 41.3.2 Expressions for the basis vectors

Use of the transformation matrix (41.14) renders the spatial components of the GVC basis vectors

$$\vec{e}_{\bar{1}} = \hat{\mathbf{x}} + \hat{\mathbf{z}} (\partial \eta / \partial \bar{x}) \quad (41.16a)$$

$$\vec{e}_{\bar{2}} = \hat{\mathbf{y}} + \hat{\mathbf{z}} (\partial \eta / \partial \bar{y}) \quad (41.16b)$$

$$\vec{e}_{\bar{3}} = \hat{\mathbf{z}} (\partial \eta / \partial \sigma). \quad (41.16c)$$

The basis vectors  $\vec{e}_{\bar{1}}$  and  $\vec{e}_{\bar{2}}$  have a vertical component due to sloping GVC surfaces. These basis vectors lie within the tangent plane of the GVC surface. The basis vector  $\vec{e}_{\bar{3}}$  is purely vertical and has a non-unit magnitude due to the inverse vertical stratification,  $\partial \eta / \partial \sigma$ . The left panel of Figure 41.2 illustrates the basis vectors.

As an example, consider the rigid lid terrain following vertical coordinate (41.10), where  $\sigma = -z / \eta_b$ . In this case, the vertical position of a generalized vertical surface is given by  $\eta = -\sigma \eta_b$

so that the basis vectors are

$$\vec{e}_{\bar{1}} = \hat{x} - \hat{z} \sigma (\partial \eta_b / \partial \bar{x}) \quad \text{and} \quad \vec{e}_{\bar{2}} = \hat{y} - \hat{z} \sigma (\partial \eta_b / \partial \bar{y}) \quad \text{and} \quad \vec{e}_{\bar{3}} = -\hat{z} \eta_b. \quad (41.17)$$

Similarly, the bottom slope oriented coordinate (41.12), with  $\sigma = z - \mathbf{x} \cdot \nabla \eta_b$  so that  $\eta = \sigma + \mathbf{x} \cdot \nabla \eta_b$ , has the corresponding basis vectors

$$\vec{e}_1 = \hat{x} + \hat{z} (\partial \eta_b / \partial \bar{x}) \quad \text{and} \quad \vec{e}_2 = \hat{y} + \hat{z} (\partial \eta_b / \partial \bar{y}) \quad \text{and} \quad \vec{e}_3 = \hat{z}. \quad (41.18)$$

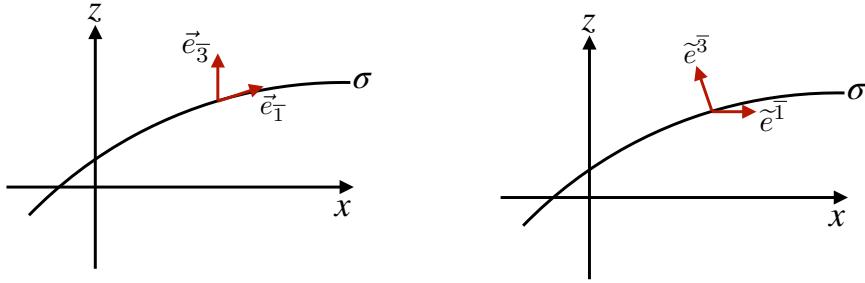


FIGURE 41.2: Illustrating the basis vectors (left panel) and basis one-forms (right panel) for generalized vertical coordinates. The  $\vec{e}_{\bar{3}}$  basis vector is vertical whereas  $\vec{e}_{\bar{1}}$  and  $\vec{e}_{\bar{2}}$  lie within the tangent plane to the  $\sigma$  surface. As a complement, the basis one-form  $\tilde{e}^{\bar{3}}$  is normal to the  $\sigma$  surface whereas the basis one-forms  $\tilde{e}^1$  and  $\tilde{e}^2$  are horizontal.

## 41.4 Basis one-forms

The basis one-forms are obtained by transforming from Cartesian into GVCs through use of the inverse transformation

$$\tilde{e}^{\bar{a}} = \Lambda_{\bar{a}}^{\bar{a}} \tilde{e}^a, \quad (41.19)$$

where the inverse transformation matrix takes the form

$$\Lambda_{\bar{a}}^{\bar{a}} = \begin{bmatrix} \partial \bar{x} / \partial x & \partial \bar{x} / \partial y & \partial \bar{x} / \partial z \\ \partial \bar{y} / \partial x & \partial \bar{y} / \partial y & \partial \bar{y} / \partial z \\ \partial \bar{z} / \partial x & \partial \bar{z} / \partial y & \partial \bar{z} / \partial z \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ \partial \sigma / \partial x & \partial \sigma / \partial y & \partial \sigma / \partial z \end{bmatrix}. \quad (41.20)$$

As for the transformation matrix (41.14), the unit diagonal values arise since a horizontal position in Cartesian and GVCs is the same and the horizontal directions are orthogonal. Likewise,  $\partial \bar{x} / \partial z = \partial \bar{y} / \partial z = 0$  since the horizontal position on a GVC surface remains unchanged when moving across a depth surface. The nonzero values for  $\partial \sigma / \partial x$ ,  $\partial \sigma / \partial y$ , and  $\partial \sigma / \partial z$ , arise in the presence of horizontal and vertical stratification of the generalized vertical coordinate.

### 41.4.1 More on the inverse transformation matrix

When computing elements of the inverse transformation matrix (41.20), it is crucial to ensure that the proper variables are held fixed. For example, consider the top row where we compute

$$\Lambda_{\bar{a}}^{\bar{1}} = [ [\partial \bar{x} / \partial x]_{y,z} \quad [\partial \bar{x} / \partial y]_{x,z} \quad [\partial \bar{x} / \partial z]_{x,y} ]. \quad (41.21)$$

Just as for the transformation matrix (41.15), since  $x = \bar{x}$ , all but the first element vanish in equation (41.21). Namely,  $[\partial \bar{x} / \partial y]_{x,z} = 0$  since the  $\bar{x}$  cannot change when  $x$  is fixed. The same idea holds for the  $\bar{y}$  row.

## 41.4.2 GVC basis one-forms

Use of the inverse transformation matrix (41.20) renders the spatial components of the GVC basis one-forms

$$\tilde{e}^{\bar{1}} = \hat{x} \quad (41.22a)$$

$$\tilde{e}^{\bar{2}} = \hat{y} \quad (41.22b)$$

$$\tilde{e}^{\bar{3}} = \tilde{e}^a \partial_a \sigma = \hat{x} (\partial \sigma / \partial x) + \hat{y} (\partial \sigma / \partial y) + \hat{z} (\partial \sigma / \partial z) = \nabla \sigma. \quad (41.22c)$$

The left panel of Figure 41.2 illustrates the basis one-forms.

As an example, consider again the rigid lid terrain following coordinate (41.10),  $\sigma = -z/\eta_b$ , in which case

$$\tilde{e}^{\bar{3}} = -(1/\eta_b) (\nabla \eta_b + \hat{z}). \quad (41.23)$$

Similarly, the bottom slope oriented coordinate (41.12), with  $\sigma = z - \mathbf{x} \cdot \nabla \eta_b$ , has

$$\tilde{e}^{\bar{3}} = \hat{z} - \nabla \eta_b - \hat{x} (\mathbf{x} \cdot \partial_x \nabla \eta_b) - \hat{y} (\mathbf{x} \cdot \partial_y \nabla \eta_b). \quad (41.24)$$

In the case where the bottom slope is constant in both directions then this result simplifies to

$$\tilde{e}^{\bar{3}} = \hat{z} - \nabla \eta_b. \quad (41.25)$$

## 41.4.3 Verifying the bi-orthogonality relation

The basis one-forms satisfy the bi-orthogonality relation (7.25) with the basis vectors

$$\tilde{e}^{\bar{a}} \cdot \tilde{e}_{\bar{b}} = \delta_{\bar{a}}^{\bar{b}}. \quad (41.26)$$

This identity is trivial to verify for all  $\bar{a} = 1, 2, 3$ .

## 41.5 Triple product identities

We find various occasions to make use of a suite of triple product identities that hold for GVCs. For this purpose we write  $\sigma$  as a composite function as in Section 7.9.3

$$\sigma = \sigma(x, y, z, t) = \sigma[x, y, z(\bar{t}, \bar{x}, \bar{y}, \sigma), t], \quad (41.27)$$

with  $\eta(\bar{x}, \bar{y}, \sigma, \bar{t})$  written as  $z(\bar{x}, \bar{y}, \sigma, \bar{t})$  as it here eases the manipulations. Use of the chain rule leads to the space-time differential increment

$$d\sigma = dt \left[ \frac{\partial \sigma}{\partial t} \right]_{x,y,z} + dx \left[ \frac{\partial \sigma}{\partial x} \right]_{t,y,z} + dy \left[ \frac{\partial \sigma}{\partial y} \right]_{t,x,z} + dz \left[ \frac{\partial \sigma}{\partial z} \right]_{t,x,y}. \quad (41.28)$$

Likewise, writing  $z = z[\bar{t}, \bar{x}, \bar{y}, \sigma]$  leads to the space-time differential increment  $dz$

$$dz = d\bar{t} \left[ \frac{\partial z}{\partial \bar{t}} \right]_{\bar{x}, \bar{y}, \sigma} + d\bar{x} \left[ \frac{\partial z}{\partial \bar{x}} \right]_{\bar{t}, \bar{y}, \sigma} + d\bar{y} \left[ \frac{\partial z}{\partial \bar{y}} \right]_{\bar{t}, \bar{x}, \sigma} + d\sigma \left[ \frac{\partial z}{\partial \sigma} \right]_{\bar{t}, \bar{x}, \bar{y}}. \quad (41.29)$$

We note the identities

$$\left[ \frac{\partial \sigma}{\partial z} \right]_{t,x,y} \left[ \frac{\partial z}{\partial \sigma} \right]_{\bar{t}, \bar{x}, \bar{y}} = 1 \quad d\bar{t} = dt \quad d\bar{x} = dx \quad d\bar{y} = dy, \quad (41.30)$$

which follow since  $t = \bar{t}$ ,  $x = \bar{x}$ , and  $y = \bar{y}$ . Substituting equation (41.29) into equation (41.28) and making use of the identities (41.30) yields

$$0 = dt \left[ \left[ \frac{\partial \sigma}{\partial t} \right]_{x,y,z} + \left[ \frac{\partial \sigma}{\partial z} \right]_{t,x,y} \left[ \frac{\partial z}{\partial \bar{t}} \right]_{\bar{x},\bar{y},\sigma} \right] \\ + dx \left[ \left[ \frac{\partial \sigma}{\partial x} \right]_{t,y,z} + \left[ \frac{\partial \sigma}{\partial z} \right]_{t,x,y} \left[ \frac{\partial z}{\partial \bar{x}} \right]_{\bar{t},\bar{y},\sigma} \right] + dy \left[ \left[ \frac{\partial \sigma}{\partial y} \right]_{t,x,z} + \left[ \frac{\partial \sigma}{\partial z} \right]_{t,x,y} \left[ \frac{\partial z}{\partial \bar{y}} \right]_{\bar{t},\bar{x},\sigma} \right]. \quad (41.31)$$

For this equation to hold with general increments  $dt$ ,  $dx$ , and  $dy$  requires that each bracketed term vanish, which in turn leads to the following set of triple product identities<sup>2</sup>

$$\left[ \frac{\partial \sigma}{\partial z} \right]_{t,x,y} \left[ \frac{\partial z}{\partial \bar{t}} \right]_{\bar{x},\bar{y},\sigma} = - \left[ \frac{\partial \sigma}{\partial t} \right]_{x,y,z} \quad (41.32a)$$

$$\left[ \frac{\partial \sigma}{\partial z} \right]_{t,x,y} \left[ \frac{\partial z}{\partial \bar{x}} \right]_{\bar{t},\bar{y},\sigma} = - \left[ \frac{\partial \sigma}{\partial x} \right]_{t,y,z} \quad (41.32b)$$

$$\left[ \frac{\partial \sigma}{\partial z} \right]_{t,x,y} \left[ \frac{\partial z}{\partial \bar{y}} \right]_{\bar{t},\bar{x},\sigma} = - \left[ \frac{\partial \sigma}{\partial y} \right]_{t,x,z}. \quad (41.32c)$$

If the vertical stratification,  $\partial \sigma / \partial z$ , is non-zero, the triple product identities are equivalent to

$$\left[ \frac{\partial z}{\partial \bar{t}} \right]_{\bar{x},\bar{y},\sigma} = - \frac{[\partial \sigma / \partial t]_{x,y,z}}{[\partial \sigma / \partial z]_{t,x,y}} = - \left[ \frac{\partial \sigma}{\partial t} \right]_{x,y,z} \left[ \frac{\partial z}{\partial \sigma} \right]_{t,x,y} \quad (41.33a)$$

$$\left[ \frac{\partial z}{\partial \bar{x}} \right]_{\bar{t},\bar{y},\sigma} = - \frac{[\partial \sigma / \partial x]_{t,y,z}}{[\partial \sigma / \partial z]_{t,x,y}} = - \left[ \frac{\partial \sigma}{\partial x} \right]_{t,y,z} \left[ \frac{\partial z}{\partial \sigma} \right]_{t,x,y} \quad (41.33b)$$

$$\left[ \frac{\partial z}{\partial \bar{y}} \right]_{\bar{t},\bar{x},\sigma} = - \frac{[\partial \sigma / \partial y]_{t,x,z}}{[\partial \sigma / \partial z]_{t,x,y}} = - \left[ \frac{\partial \sigma}{\partial y} \right]_{t,x,z} \left[ \frac{\partial z}{\partial \sigma} \right]_{t,x,y}. \quad (41.33c)$$

Since  $t = \bar{t}$ ,  $x = \bar{x}$ , and  $y = \bar{y}$  we can write these identities in the more succinct form

$$\left[ \frac{\partial z}{\partial \bar{t}} \right]_\sigma = \left[ \frac{\partial \eta}{\partial \bar{t}} \right]_\sigma = - \frac{[\partial \sigma / \partial t]_z}{[\partial \sigma / \partial z]} \quad (41.34a)$$

$$\left[ \frac{\partial z}{\partial \bar{x}} \right]_\sigma = \left[ \frac{\partial \eta}{\partial \bar{x}} \right]_\sigma = - \frac{[\partial \sigma / \partial x]_z}{[\partial \sigma / \partial z]} \quad (41.34b)$$

$$\left[ \frac{\partial z}{\partial \bar{y}} \right]_\sigma = \left[ \frac{\partial \eta}{\partial \bar{y}} \right]_\sigma = - \frac{[\partial \sigma / \partial y]_z}{[\partial \sigma / \partial z]}, \quad (41.34c)$$

where we reintroduced the notation  $\eta(x, y, \sigma, t) = z(x, y, \sigma, t)$ . These identities are quite useful for manipulating equations involving GVCs. In particular, equations (41.34b) and (41.34c) provide alternate expressions for the slope of  $\sigma$  isosurfaces relative to the horizontal plane (see Section 41.12).

## 41.6 Position vector

We are familiar with locating a point in space using Cartesian coordinates as in Figure 1.1. What about specifying the position using GVCs? We can do so by making use of the basis vectors

<sup>2</sup>These identities are directly analogous to the Maxwell relations from thermodynamics, with an introduction in Section 20.9 and full details in the book by [Callen \(1985\)](#).

(41.16a)-(41.16c) so that the position of an arbitrary point in space is given by

$$\mathcal{P} = \xi^{\bar{a}} \vec{e}_{\bar{a}} \quad (41.35a)$$

$$= \bar{x} [\hat{x} + (\partial\eta/\partial\bar{x}) \hat{z}] + \bar{y} [\hat{y} + (\partial\eta/\partial\bar{y}) \hat{z}] + \sigma (\partial\eta/\partial\sigma) \hat{z} \quad (41.35b)$$

$$= \hat{x} \bar{x} + \hat{y} \bar{y} + \hat{z} [\bar{x} (\partial\eta/\partial\bar{x}) + \bar{y} (\partial\eta/\partial\bar{y}) + \sigma (\partial\eta/\partial\sigma)] \quad (41.35c)$$

$$= \hat{x} \bar{x} + \hat{y} \bar{y} + \hat{z} \xi^{\bar{a}} \partial_{\bar{a}}\eta. \quad (41.35d)$$

We identify the following properties as a means to help understand these expressions, with Figure 41.3 offering a schematic.

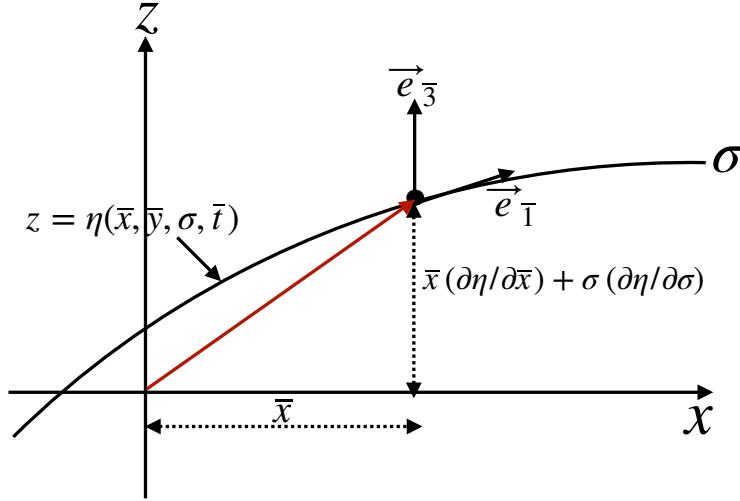


FIGURE 41.3: The position of a point in space as represented using GVCs following equation (41.36a). For this example,  $\bar{y} = 0$  so that the horizontal position is determined by the coordinate  $\bar{x} = x$ , whereas the vertical position is determined by  $\bar{x} (\partial z / \partial \bar{x}) + \sigma (\partial z / \partial \sigma) = \bar{x} (\partial \eta / \partial \bar{x}) + \sigma (\partial \eta / \partial \sigma)$ .

- The expression (41.35b) has horizontal positions  $\bar{x}$  and  $\bar{y}$  multiplying the basis vectors  $\vec{e}_{\bar{x}}$  and  $\vec{e}_{\bar{y}}$ , with these vectors oriented parallel to a surface of constant GVC as in Figure 41.3. Likewise, the third term,  $\sigma (\partial\eta/\partial\sigma) \hat{z}$ , positions the point vertically according to the value of the GVC and its inverse stratification.
- Consider the case of  $\bar{y} = 0$  so that

$$\mathcal{P} = \bar{x} \hat{x} + \hat{z} [\bar{x} (\partial\eta/\partial\bar{x}) + \sigma (\partial\eta/\partial\sigma)] \quad (41.36a)$$

$$= \bar{x} \hat{x} + \hat{z} (\partial\eta/\partial\sigma) [\bar{x} (\partial\sigma/\partial z)_x (\partial\eta/\partial\bar{x})_\sigma + \sigma] \quad (41.36b)$$

$$= \bar{x} \hat{x} + \hat{z} (\partial\eta/\partial\sigma) [-\bar{x} (\partial\sigma/\partial x)_z + \sigma], \quad (41.36c)$$

where we used the triple product identity (41.34b) for the final equality. Consequently, a horizontal position vector is realized using GVC coordinates with  $\sigma = \bar{x} (\partial\sigma/\partial x)$ . That is, a horizontal position vector crosses surfaces of constant GVC when the GVC surface has a nonzero horizontal slope.

- The projection of the position vector onto the basis one-forms leads to

$$\mathcal{P} \cdot \tilde{e}^{\bar{b}} = \xi^{\bar{a}} \vec{e}_{\bar{a}} \cdot \tilde{e}^{\bar{b}} = \xi^{\bar{b}}. \quad (41.37)$$

This result follows from the orthogonality relation (7.25). So the projection of the position vector onto a basis one-form picks out the corresponding coordinate value.

- Equation (41.7) provides the spatial dependence for the vertical position of the surface of constant GVC

$$z = z(\xi^{\bar{a}}) = \eta(\xi^{\bar{a}}). \quad (41.38)$$

At any particular time instance we can perform a Taylor series about a reference geopotential  $\zeta_0 = \eta_0$ , so that

$$\eta(\xi^{\bar{a}}) \approx \eta_0 + \xi^{\bar{a}} \partial_{\bar{a}} \eta. \quad (41.39)$$

We can thus write the position (41.35d) in the form

$$\mathcal{P} = \hat{x} \bar{x} + \hat{y} \bar{y} + \hat{z} [\eta - \eta_0]. \quad (41.40)$$

Taking the reference geopotential as  $\eta_0 = 0$  recovers the Cartesian expression. Since the position vector is a geometric object, it is reassuring that the GVC representation is the same as the Cartesian representation; it is merely a reorganization of the basis vectors and corresponding coordinates.

## 41.7 Transforming components of a vector

Consider a vector field  $\vec{F}$  with Cartesian representation

$$\vec{F} = \mathbf{F} = F^a \vec{e}_a = F^x \hat{x} + F^y \hat{y} + F^z \hat{z}. \quad (41.41)$$

The corresponding GVC components are related through the transformation matrix

$$F^{\bar{a}} = \Lambda_a^{\bar{a}} F^a. \quad (41.42)$$

Making use of the transformation matrix (41.20) yields the relations between GVC components and Cartesian components

$$F^{\bar{1}} = F^1 \quad \text{and} \quad F^{\bar{2}} = F^2 \quad \text{and} \quad F^{\bar{3}} = \nabla \sigma \cdot \mathbf{F}, \quad (41.43)$$

where we wrote

$$\nabla \sigma \cdot \mathbf{F} = (\partial \sigma / \partial x) F^1 + (\partial \sigma / \partial y) F^2 + (\partial \sigma / \partial z) F^3. \quad (41.44)$$

The vector field thus can be represented in GVC coordinates as

$$\vec{F} = F^{\bar{a}} \vec{e}_{\bar{a}} = F^1 \vec{e}_{\bar{1}} + F^2 \vec{e}_{\bar{2}} + (\nabla \sigma \cdot \mathbf{F}) \vec{e}_{\bar{3}}. \quad (41.45)$$

Similarly, the covariant components transform as  $F_{\bar{a}} = \Lambda_a^{\bar{a}} F_a$ , where use of the inverse transformation matrix (41.20) renders

$$F_{\bar{1}} = F_1 + (\partial z / \partial \bar{x}) F_3 = F_1 + (\partial \eta / \partial \bar{x}) F_3 \quad (41.46a)$$

$$F_{\bar{2}} = F_2 + (\partial z / \partial \bar{y}) F_3 = F_2 + (\partial \eta / \partial \bar{y}) F_3 \quad (41.46b)$$

$$F_{\bar{3}} = (\partial z / \partial \sigma) F_3 = (\partial \eta / \partial \sigma) F_3, \quad (41.46c)$$

and the expression for the vector field

$$\vec{F} = F_{\bar{a}} \tilde{e}^{\bar{a}} = [F_1 + (\partial \eta / \partial \bar{x}) F_3] \tilde{e}^{\bar{1}} + [F_2 + (\partial \eta / \partial \bar{y}) F_3] \tilde{e}^{\bar{2}} + (\partial \eta / \partial \sigma) F_3 \tilde{e}^{\bar{3}}. \quad (41.47)$$

Recall also that for Cartesian coordinates the contravariant and covariant components to a vector are identical:  $F^a = F_a$ .

## 41.8 Velocity

As an example of the results from Section 41.7, we here represent the velocity vector, considering both covariant and contravariant representations. As for the position vector detailed in Section 41.6, we are assured that both representations lead to the same velocity vector since the velocity is an objective geometric object (i.e., an arrow with a magnitude). In Section 41.8.4 we verify that the transformation formalism indeed respects this equivalence, with the GVC representations equivalent to the Cartesian representation

$$\vec{v} = u \hat{\mathbf{x}} + v \hat{\mathbf{y}} + w \hat{\mathbf{z}}. \quad (41.48)$$

### 41.8.1 Contravariant components

Following Section 41.7, we have the contravariant velocity components

$$v^{\bar{1}} = u \quad \text{and} \quad v^{\bar{2}} = v \quad \text{and} \quad v^{\bar{3}} = \mathbf{v} \cdot \nabla \sigma. \quad (41.49)$$

Use of the basis vectors (41.16a)-(41.16c) then leads to

$$\vec{v} = v^{\bar{a}} \vec{e}_{\bar{a}} \quad (41.50a)$$

$$= u \vec{e}_{\bar{x}} + v \vec{e}_{\bar{y}} + (\mathbf{v} \cdot \nabla \sigma) \vec{e}_{\sigma} \quad (41.50b)$$

$$= u [\hat{\mathbf{x}} + (\partial \eta / \partial \bar{x}) \hat{\mathbf{z}}] + v [\hat{\mathbf{y}} + (\partial \eta / \partial \bar{y}) \hat{\mathbf{z}}] + (\mathbf{v} \cdot \nabla \sigma) (\partial \eta / \partial \sigma) \hat{\mathbf{z}}. \quad (41.50c)$$

### 41.8.2 Covariant components

The covariant velocity components are given by

$$v_{\bar{1}} = u + (\partial \eta / \partial \bar{x}) w \quad \text{and} \quad v_{\bar{2}} = v + (\partial \eta / \partial \bar{y}) w \quad \text{and} \quad v_{\bar{3}} = (\partial \eta / \partial \sigma) w. \quad (41.51)$$

The one-form basis (41.22a)–(41.22c) thus leads to the velocity vector

$$\vec{v} = v_{\bar{a}} \tilde{e}^{\bar{a}} = [u + (\partial \eta / \partial \bar{x}) w] \hat{\mathbf{x}} + [v + (\partial \eta / \partial \bar{y}) w] \hat{\mathbf{y}} + w (\partial \eta / \partial \sigma) \nabla \sigma. \quad (41.52)$$

### 41.8.3 Introducing the material time derivative

The material evolution for the generalized vertical coordinate can be written

$$\frac{D\sigma}{Dt} = \frac{\partial \sigma}{\partial t} + \mathbf{v} \cdot \nabla \sigma = \dot{\sigma}, \quad (41.53)$$

with  $\dot{\sigma}$  symbolizing any process contributing to motion across  $\sigma$  isosurfaces (as fully explained in Section 42.4). Using the expression (41.53) in the velocity vector expression (41.50c) leads to

$$\vec{v} = u [\hat{\mathbf{x}} + (\partial \eta / \partial \bar{x}) \hat{\mathbf{z}}] + v [\hat{\mathbf{y}} + (\partial \eta / \partial \bar{y}) \hat{\mathbf{z}}] + (\mathbf{v} \cdot \nabla \sigma) (\partial \eta / \partial \sigma) \hat{\mathbf{z}}. \quad (41.54a)$$

$$= u [\hat{\mathbf{x}} + (\partial \eta / \partial \bar{x}) \hat{\mathbf{z}}] + v [\hat{\mathbf{y}} + (\partial \eta / \partial \bar{y}) \hat{\mathbf{z}}] + (\dot{\sigma} - \partial \sigma / \partial t) (\partial \eta / \partial \sigma) \hat{\mathbf{z}} \quad (41.54b)$$

$$= u \hat{\mathbf{x}} + v \hat{\mathbf{y}} + [\partial \eta / \partial \bar{t} + \mathbf{u} \cdot \nabla_{\sigma} z + (\partial \eta / \partial \sigma) \dot{\sigma}] \hat{\mathbf{z}}, \quad (41.54c)$$

where the final equality made use of the triple product (41.33a):  $(\partial \sigma / \partial t) (\partial \eta / \partial \sigma) = -\partial \eta / \partial \bar{t}$ . In the steady state and in the absence of material changes to  $\sigma$ , the three dimensional flow lies within a surface of constant  $\sigma$ , whereby  $\mathbf{v} \cdot \nabla \sigma = 0$  and

$$\vec{v} = u [\hat{\mathbf{x}} + (\partial \eta / \partial \bar{x}) \hat{\mathbf{z}}] + v [\hat{\mathbf{y}} + (\partial \eta / \partial \bar{y}) \hat{\mathbf{z}}] \quad \text{if } \partial_t \sigma = 0 \text{ and } \dot{\sigma} = 0. \quad (41.55)$$

However, in general there are transient fluctuations and material changes to  $\sigma$  so that  $\mathbf{v} \cdot \nabla \sigma \neq 0$ .

#### 41.8.4 Equivalence to the Cartesian velocity representation

Use of the triple product identities (41.34b)-(41.34c) allows us to manipulate both expressions (41.50c) and (41.52) to recover the Cartesian expression

$$\vec{v} = u \hat{\mathbf{x}} + v \hat{\mathbf{y}} + w \hat{\mathbf{z}}. \quad (41.56)$$

Another way to see this identity is to note that in equation (41.54c), the vertical component is an expression for the material time derivative of the vertical position

$$w = \frac{Dz}{Dt} = \frac{\partial \eta}{\partial t} + \mathbf{u} \cdot \nabla_\sigma \eta + \frac{\partial \eta}{\partial \sigma} \dot{\sigma}. \quad (41.57)$$

We derive this identity in Section 42.5 where we discuss further kinematic results using GVCs.

## 41.9 Metric tensor

Recall from Section 7.1 that we make use of a metric tensor to measure the distance between two points in space. The GVC representation of the metric tensor is given by

$$g_{\bar{a}\bar{b}} = \vec{e}_{\bar{a}} \cdot \vec{e}_{\bar{b}} = \begin{bmatrix} 1 + (\partial \eta / \partial \bar{x})^2 & (\partial \eta / \partial \bar{x})(\partial \eta / \partial \bar{y}) & (\partial \eta / \partial \bar{x})(\partial \eta / \partial \sigma) \\ (\partial \eta / \partial \bar{x})(\partial \eta / \partial \bar{y}) & 1 + (\partial \eta / \partial \bar{y})^2 & (\partial \eta / \partial \bar{y})(\partial \eta / \partial \sigma) \\ (\partial \eta / \partial \bar{x})(\partial \eta / \partial \sigma) & (\partial \eta / \partial \bar{y})(\partial \eta / \partial \sigma) & (\partial \eta / \partial \sigma)^2 \end{bmatrix}, \quad (41.58)$$

and the GVC representation of the inverse metric tensor is given by the somewhat simpler form

$$g^{\bar{a}\bar{b}} = \vec{e}^{\bar{a}} \cdot \vec{e}^{\bar{b}} = \begin{bmatrix} 1 & 0 & \partial \sigma / \partial x \\ 0 & 1 & \partial \sigma / \partial y \\ \partial \sigma / \partial x & \partial \sigma / \partial y & |\nabla \sigma|^2 \end{bmatrix}. \quad (41.59)$$

Proof that  $g^{\bar{a}\bar{b}} g_{\bar{b}\bar{c}} = \delta_{\bar{a}}^{\bar{c}}$  requires use of the triple product identities (41.34b) and (41.34c).

### 41.9.1 Jacobian of transformation

The determinant of the GVC representation of the metric tensor (41.58) is

$$\det(g_{\bar{a}\bar{b}}) = (\partial z / \partial \sigma)^2 = (\partial \eta / \partial \sigma)^2 \quad (41.60)$$

so that the Jacobian of transformation (Section 7.5) is the specific thickness

$$\frac{\partial(x, y, z)}{\partial(\bar{x}, \bar{y}, \sigma)} = \frac{\partial z}{\partial \sigma} = \frac{\partial \eta}{\partial \sigma}. \quad (41.61)$$

The coordinate transformation from Cartesian to generalized vertical is invertible only so long as the Jacobian remains nonzero and single-signed, meaning the fluid retains a monotonic vertical stratification of GVC surfaces. The invertible relation between  $z$  and  $\sigma$  means that each point in the vertical can be uniquely specified by either of the two vertical coordinates,  $z$  or  $\sigma$ . For example, the Jacobian for pressure as the generalized vertical coordinate in a hydrostatic fluid is

given by<sup>3</sup>

$$\frac{\partial z}{\partial \sigma} = \frac{\partial z}{\partial p} = -\frac{1}{\rho g}, \quad (41.62)$$

which is indeed single-signed since the mass density is always positive.

### 41.9.2 Covariant and contravariant representations

The metric tensor allows us to convert between the covariant and contravariant representations of a vector via the identity (Section 7.2.3)

$$F_{\bar{a}} = g_{\bar{a}\bar{b}} F^{\bar{b}}. \quad (41.63)$$

We use triple product identities (41.34b)-(41.34c) to verify that this relation agrees with the transformation matrix approach detailed in Section 41.7. For example,

$$F_{\bar{1}} = g_{\bar{1}\bar{b}} F^{\bar{b}} \quad (41.64a)$$

$$= [1 + (\partial\eta/\partial\bar{x})^2] F^{\bar{1}} + (\partial\eta/\partial\bar{x})(\partial\eta/\partial\bar{y}) F^{\bar{2}} + (\partial\eta/\partial\bar{x})(\partial\eta/\partial\sigma) F^{\sigma} \quad (41.64b)$$

$$= [1 + (\partial\eta/\partial\bar{x})^2] F^1 + (\partial\eta/\partial\bar{x})(\partial\eta/\partial\bar{y}) F^2 + (\partial\eta/\partial\bar{x})(\partial\eta/\partial\sigma) \nabla\sigma \cdot \mathbf{F} \quad (41.64c)$$

$$= F^1 + (\partial\eta/\partial\bar{x}) F^3 \quad (41.64d)$$

$$= F_1 + (\partial\eta/\partial\bar{x}) F_3, \quad (41.64e)$$

where the final equality holds since  $F^1 = F_1$  and  $F^3 = F_3$  for Cartesian tensor components.

## 41.10 Volume element and the Levi-Civita tensor

The square root of the determinant of the metric tensor (41.58) is

$$\sqrt{\det(g_{\bar{a}\bar{b}})} = \partial z / \partial \sigma = \partial \eta / \partial \sigma \quad (41.65)$$

so that the volume element (Section 7.5) is

$$dV = (\partial z / \partial \sigma) dx dy d\sigma. \quad (41.66)$$

The covariant Levi-Civita tensor (Section 7.7) has the GVC representations

$$\varepsilon_{\bar{a}\bar{b}\bar{c}} = (\partial z / \partial \sigma) \epsilon_{\bar{a}\bar{b}\bar{c}} \quad \varepsilon^{\bar{a}\bar{b}\bar{c}} = (\partial z / \partial \sigma)^{-1} \epsilon^{\bar{a}\bar{b}\bar{c}} \quad (41.67)$$

where  $\epsilon$  is the permutation symbol introduced in Section 1.4.1 with its components independent of coordinate representation.

## 41.11 Vector cross product of basis vectors

We now verify the relation (7.79) for the cross product of two basis vectors using GVCs

$$\vec{e}_{\bar{a}} \times \vec{e}_{\bar{b}} = \varepsilon_{\bar{a}\bar{b}\bar{c}} \vec{e}^{\bar{c}} \implies \vec{e}_{\bar{a}} \times \vec{e}_{\bar{b}} = (\partial z / \partial \sigma) \epsilon_{\bar{a}\bar{b}\bar{c}} \vec{e}^{\bar{c}}. \quad (41.68)$$

---

<sup>3</sup>We derive the hydrostatic balance in Section 22.2.

Making use of the basis vectors from Section 41.3 and the basis one-forms from Section 41.4 renders

$$\vec{e}_{\bar{x}} \times \vec{e}_{\bar{y}} = \hat{\mathbf{z}} - \hat{\mathbf{x}} (\partial\eta/\partial\bar{x}) - \hat{\mathbf{y}} (\partial\eta/\partial\bar{y}) = (\partial z/\partial\sigma) \nabla\sigma = \varepsilon_{\bar{x}\bar{y}\sigma} \tilde{e}^\sigma \quad (41.69a)$$

$$\vec{e}_{\bar{y}} \times \vec{e}_\sigma = \hat{\mathbf{x}} (\partial z/\partial\sigma) = \varepsilon_{\bar{y}\sigma\bar{x}} \tilde{e}^{\bar{x}} \quad (41.69b)$$

$$\vec{e}_\sigma \times \vec{e}_{\bar{x}} = \hat{\mathbf{y}} (\partial z/\partial\sigma) = \varepsilon_{\sigma\bar{x}\bar{y}} \tilde{e}^{\bar{y}}. \quad (41.69c)$$

## 41.12 Partial derivative operators

We here consider the partial derivative operators and their transformation between coordinate systems. These identities are used throughout GVC calculus. Given the importance of these expressions, we offer two derivations. Notably, the geometric derivation in Section 41.12.2 requires minimal use of the previous tensor formalism.

### 41.12.1 Analytical derivation

The partial derivative operators in GVCs are computed via  $\partial_{\bar{a}} = \Lambda_{\bar{a}}^a \partial_a$ . Including also the time component leads to the relations

$$\partial_{\bar{t}} = \partial_t + (\partial z/\partial\bar{t}) \partial_z = \partial_t + (\partial\eta/\partial\bar{t}) \partial_z \quad (41.70a)$$

$$\partial_{\bar{x}} = \partial_x + (\partial z/\partial\bar{x}) \partial_z = \partial_x + (\partial\eta/\partial\bar{x}) \partial_z \quad (41.70b)$$

$$\partial_{\bar{y}} = \partial_y + (\partial z/\partial\bar{y}) \partial_z = \partial_y + (\partial\eta/\partial\bar{y}) \partial_z \quad (41.70c)$$

$$\partial_\sigma = (\partial z/\partial\sigma) \partial_z = (\partial\eta/\partial\sigma) \partial_z. \quad (41.70d)$$

We can make use of the triple product identities (41.34b) and (41.34c) to express the slope of a constant GVC surface in the equivalent manners

$$\mathbf{S} = \nabla_\sigma \eta = \nabla_\sigma z = -(\partial\sigma/\partial z)^{-1} \nabla_z \sigma \quad (41.71)$$

where we introduced the standard shorthand notation

$$\nabla_\sigma = \hat{\mathbf{x}} \partial/\partial\bar{x} + \hat{\mathbf{y}} \partial/\partial\bar{y} \quad \text{and} \quad \nabla_z = \hat{\mathbf{x}} \partial/\partial x + \hat{\mathbf{y}} \partial/\partial y. \quad (41.72)$$

It is common to transform between the horizontal gradient operators, in which case we write

$$\nabla_\sigma = \nabla_z + (\nabla_\sigma z) \partial_z \equiv \nabla_z + \mathbf{S} \partial_z. \quad (41.73)$$

We emphasize that  $\nabla_\sigma$  is merely a shorthand for the two partial derivative operators and that it only has components in the horizontal directions.

### 41.12.2 Geometrical derivation

We provide a geometric derivation for the lateral derivative operator that complements the previous analytical derivation. This operator is computed by taking the difference of a function along surfaces of constant generalized vertical coordinate, but with the lateral distance computed in the horizontal direction as shown in Figure 41.4. This feature of the horizontal derivative operator is a key aspect of the GVCs' non-orthogonality.

Consider the geometry shown in Figure 41.4, which shows a generalized vertical coordinate

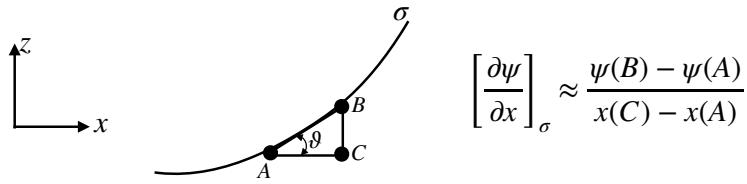


FIGURE 41.4: A surface of constant generalized vertical coordinate,  $\sigma$ , along with a local tangent plane with a slope  $\tan \vartheta$  with respect to the horizontal plane. This figure illustrates the identities (41.75a)-(41.75d), with these identities relating a lateral derivative taken along the GVC surface to horizontal and vertical derivatives taken along orthogonal Cartesian axes.

surface (constant  $\sigma$  surface) along with a sample tangent plane with a slope

$$S^x = \frac{\text{rise}}{\text{run}} = \tan \vartheta = \frac{z(B) - z(C)}{x(C) - x(A)} \approx \left[ \frac{\partial z}{\partial x} \right]_{\sigma} = - \frac{(\partial \sigma / \partial x)_z}{(\partial \sigma / \partial z)} \quad (41.74)$$

relative to the horizontal. We readily verify the following identities based on finite difference operations for an arbitrary function

$$\left[ \frac{\partial \psi}{\partial x} \right]_{\sigma} \approx \frac{\psi(B) - \psi(A)}{x(C) - x(A)} \quad (41.75a)$$

$$= \frac{\psi(C) - \psi(A)}{x(C) - x(A)} + \frac{\psi(B) - \psi(C)}{x(C) - x(A)} \quad (41.75b)$$

$$= \frac{\psi(C) - \psi(A)}{x(C) - x(A)} + \left[ \frac{z(B) - z(C)}{x(C) - x(A)} \right] \frac{\psi(B) - \psi(C)}{z(B) - z(C)} \quad (41.75c)$$

$$= \left[ \frac{\partial \psi}{\partial x} \right]_z + S^x \left[ \frac{\partial \psi}{\partial z} \right]_x. \quad (41.75d)$$

Taking the continuum limit then leads to the relations between horizontal derivatives computed on constant  $\sigma$  surfaces to those computed on constant  $z$  surfaces

$$\left[ \frac{\partial}{\partial x} \right]_{\sigma} = \left[ \frac{\partial}{\partial x} \right]_z + \left[ \frac{\partial z}{\partial x} \right]_{\sigma} \frac{\partial}{\partial z} = \left[ \frac{\partial}{\partial x} \right]_z + \left[ \frac{\partial \eta}{\partial x} \right]_{\sigma} \frac{\partial}{\partial z} \quad (41.76a)$$

$$\left[ \frac{\partial}{\partial y} \right]_{\sigma} = \left[ \frac{\partial}{\partial y} \right]_z + \left[ \frac{\partial z}{\partial y} \right]_{\sigma} \frac{\partial}{\partial z} = \left[ \frac{\partial}{\partial y} \right]_z + \left[ \frac{\partial \eta}{\partial y} \right]_{\sigma} \frac{\partial}{\partial z}, \quad (41.76b)$$

which can be written in the shorthand vector notation

$$\nabla_{\sigma} = \hat{x} \left[ \frac{\partial}{\partial x} \right]_{\sigma} + \hat{y} \left[ \frac{\partial}{\partial y} \right]_{\sigma} = \nabla_z + (\nabla_{\sigma} z) \partial_z = \nabla_z + (\nabla_{\sigma} \eta) \partial_z. \quad (41.77)$$

## 41.13 Material time derivative

Making use of the relations for the partial derivative operators in Section 41.12 allows us to write the material time derivative in the following equivalent forms

$$\frac{D}{Dt} = \left[ \frac{\partial}{\partial t} \right]_z + \mathbf{u} \cdot \nabla_z + w \frac{\partial}{\partial z} \quad (41.78a)$$

$$= \left[ \frac{\partial}{\partial t} \right]_\sigma - (\partial \eta / \partial \bar{t}) \partial_z + \mathbf{u} \cdot [\nabla_\sigma - (\nabla_\sigma \eta) \partial_z] + w \partial / \partial z \quad (41.78b)$$

$$= \left[ \frac{\partial}{\partial t} \right]_\sigma + \mathbf{u} \cdot \nabla_\sigma + [w - \mathbf{u} \cdot \nabla_\sigma \eta - \partial \eta / \partial \bar{t}] (\partial \sigma / \partial z) \partial / \partial \sigma \quad (41.78c)$$

$$= \left[ \frac{\partial}{\partial t} \right]_\sigma + \mathbf{u} \cdot \nabla_\sigma + \frac{D\sigma}{Dt} \frac{\partial}{\partial \sigma} \quad (41.78d)$$

$$= \left[ \frac{\partial}{\partial t} \right]_\sigma + \mathbf{u} \cdot \nabla_\sigma + \frac{\partial z}{\partial \sigma} \frac{D\sigma}{Dt} \frac{\partial}{\partial z}. \quad (41.78e)$$

The equality (41.78d) made use of the identity (41.57), which is itself derived in Section 42.5 where we discuss further kinematic results using GVCs. Besides differences in the spatial operators, it is important to note that the time derivative operators are computed on constant geopotential and constant GVC surfaces, respectively. However, the horizontal velocity component is the *same* for both forms of the material time derivative

$$(u, v) = \frac{D(x, y)}{Dt}. \quad (41.79)$$

## 41.14 Divergence of a vector and the divergence theorem

Making use of the general expression (7.15) for the covariant divergence of a vector renders the GVC expression

$$\nabla_{\bar{a}} F^{\bar{a}} = [\det(g_{\bar{a}\bar{b}})]^{-1/2} \partial_{\bar{a}} \left[ [\det(g_{\bar{a}\bar{b}})]^{1/2} F^{\bar{a}} \right] = (\partial z / \partial \sigma)^{-1} \partial_{\bar{a}} [(\partial z / \partial \sigma) F^{\bar{a}}]. \quad (41.80)$$

Recall that the GVC vector components,  $F^{\bar{a}}$ , are related to the Cartesian components in equation (41.43), and the GVC components of the partial derivative operator,  $\partial_{\bar{a}}$ , are related to the Cartesian operator in equation (41.72).

When making use of the divergence theorem (Section 7.18), we require the product of the volume element and the covariant divergence. For GVCs this product takes on the form

$$(\nabla_{\bar{a}} F^{\bar{a}}) dV = \partial_{\bar{a}} [(\partial z / \partial \sigma) F^{\bar{a}}] d\bar{x} d\bar{y} d\sigma, \quad (41.81)$$

which reduces to a boundary integral when integrating over a volume.

## 41.15 The diffusion operator

As an explicit example of the covariant divergence operator (41.80), we here consider the diffusion operator discussed in Chapter 46. The derivation here recovers much of what we just discussed in Section 41.14, yet we make use of a bit less tensor formalism though at the cost of more algebra.

### 41.15.1 Continuous expression

The diffusion operator is the divergence of the diffusive flux

$$\mathcal{R} = -\nabla \cdot \mathbf{J}, \quad (41.82)$$

where  $\mathbf{J}$  is a vector field. Let us convert the pieces of this operator from Cartesian coordinates into GVC coordinates, making use of the transformation of partial derivative operators given in Section 41.12. Also, we make use of the shorthand  $z(x, y, \sigma, t)$  rather than  $\eta(x, y, \sigma, t)$

$$-\mathcal{R} = \nabla \cdot \mathbf{J} \quad (41.83a)$$

$$= \nabla_z \cdot \mathbf{J}^h + \partial_z J^z \quad (41.83b)$$

$$= (\nabla_\sigma - \nabla_\sigma z \partial_z) \cdot \mathbf{J}^h + (\sigma_z) \partial_\sigma J^z \quad (41.83c)$$

$$= \sigma_z \left[ z_\sigma \nabla_\sigma \cdot \mathbf{J}^h + (\hat{\mathbf{z}} \partial_\sigma - \nabla_\sigma z \partial_\sigma) \cdot \mathbf{J} \right] \quad (41.83d)$$

$$= \sigma_z \left[ \nabla_\sigma \cdot (z_\sigma \mathbf{J}^h) - \mathbf{J}^h \cdot \nabla_\sigma (z_\sigma) + \partial_\sigma J^z - \partial_\sigma (\nabla_\sigma z \cdot \mathbf{J}) + \mathbf{J} \cdot \partial_\sigma (\nabla_\sigma z) \right] \quad (41.83e)$$

$$= \sigma_z \left[ \nabla_\sigma \cdot (z_\sigma \mathbf{J}^h) + \partial_\sigma J^z - \partial_\sigma (\nabla_\sigma z \cdot \mathbf{J}^h) \right] \quad (41.83f)$$

$$= \sigma_z \left( \nabla_\sigma \cdot (\partial_\sigma z \mathbf{J}^h) + \partial_\sigma [(\hat{\mathbf{z}} - \nabla_\sigma z) \cdot \mathbf{J}] \right) \quad (41.83g)$$

$$= \sigma_z \left[ \nabla_\sigma \cdot (z_\sigma \mathbf{J}^h) + \partial_\sigma (z_\sigma \nabla_\sigma \cdot \mathbf{J}) \right], \quad (41.83h)$$

where we used

$$z_\sigma \nabla_\sigma = \hat{\mathbf{z}} - \nabla_\sigma z \quad (41.84)$$

to reach the final equality, and made use of the shorthand

$$z_\sigma = \partial z / \partial \sigma \quad \text{and} \quad \sigma_z = \partial \sigma / \partial z = (z_\sigma)^{-1}. \quad (41.85)$$

The coordinate transformations in Section 41.7 for vector components reveal that the expression (41.83h) is identical to equation (41.80) derived using formal tensor methods. Likewise, multiplying by the volume element

$$dV = dx dy dz = dx dy z_\sigma d\sigma, \quad (41.86)$$

leads to

$$-\mathcal{R} dV = \left[ \nabla_\sigma \cdot (z_\sigma \mathbf{J}^h) + \partial_\sigma (z_\sigma \nabla_\sigma \cdot \mathbf{J}) \right] dx dy d\sigma, \quad (41.87)$$

which is identical to the expression (41.81).

### 41.15.2 Layer thickness weighted diffusion operator

Consider a prescribed increment,  $\delta\sigma$ , separating two  $\sigma$  isosurfaces. This increment commutes with the horizontal operator  $\nabla_\sigma$ , acting within the layer. We can thus formally consider the following

layer-integrated or thickness weighted form of the diffusion operator

$$-\mathcal{R} \delta V = \left[ \nabla_\sigma \cdot (\delta\sigma z_\sigma \mathbf{J}^h) + \delta\sigma \partial_\sigma (z_\sigma \nabla\sigma \cdot \mathbf{J}) \right] \delta x \delta y \quad (41.88a)$$

$$= \frac{1}{\delta z} \left[ \nabla_\sigma \cdot (\delta\sigma z_\sigma \mathbf{J}^h) + \delta\sigma \partial_\sigma (z_\sigma \nabla\sigma \cdot \mathbf{J}) \right] \delta x \delta y \delta z \quad (41.88b)$$

$$= \frac{1}{h} \left[ \nabla_\sigma \cdot (h \mathbf{J}^h) + \Delta_\sigma (z_\sigma \nabla\sigma \cdot \mathbf{J}) \right] \delta x \delta y h, \quad (41.88c)$$

where we introduced the infinitesimal layer thickness

$$h = z_\sigma \delta\sigma \quad (41.89)$$

and the non-dimensional differential operator

$$\Delta_\sigma \equiv \delta\sigma \frac{\partial}{\partial\sigma}. \quad (41.90)$$

Cancelling the volume element on both sides leads to the diffusion operator

$$\mathcal{R} = -\frac{1}{h} \left[ \nabla_\sigma \cdot (h \mathbf{J}^h) + \Delta_\sigma (z_\sigma \nabla\sigma \cdot \mathbf{J}) \right]. \quad (41.91)$$

This form is commonly found in the numerical modeling literature when considering generalized vertical coordinate models.

We make the following comments concerning the diffusion operator in equation (41.91).

- Our introduction of the layer thickness  $h = z_\sigma \delta\sigma$  is treated a bit more formally in Sections 42.10 and 42.11 by considering a vertical integral over a coordinate layer. Even so, the resulting diffusion operator is the same as that derived here.
- The thickness weighted flux,  $h \mathbf{J}^h$ , is oriented within the horizontal plane. However, its contribution to the diffusion operator is computed by taking its convergence using the operator  $\nabla_\sigma$  rather than the horizontal operator  $\nabla_z$ . This distinction is fundamental to how operators, such as advection and diffusion, appear using generalized vertical coordinates.
- The flux  $z_\sigma \nabla\sigma \cdot \mathbf{J}$  is commonly referred to as the dia-surface subgrid scale flux.
- For the special case of a diffusive flux with zero component parallel to  $\nabla\sigma$ , the diffusion operator reduces to

$$\mathcal{R} = -\frac{1}{h} \left[ \nabla_\sigma \cdot (h \mathbf{J}^h) \right] \quad \text{if } \nabla\sigma \cdot \mathbf{J} = 0. \quad (41.92)$$

The neutral diffusion operator of Section 48.4.4 is an example of such an operator, with  $\sigma$  in that case given by the locally referenced potential density.

## 41.16 Vorticity

As detailed in Chapter 35, vorticity is the curl of the velocity

$$\vec{\omega} = \text{curl}(\vec{v}), \quad (41.93)$$

where the curl has components (Section 7.17)

$$\text{curl}(\vec{v}) = \tilde{e}_a \varepsilon^{abc} \partial_b v_c = \tilde{e}_{\bar{a}} \varepsilon^{\bar{a}\bar{b}\bar{c}} \partial_{\bar{b}} v_{\bar{c}}. \quad (41.94)$$

### 41.16.1 The components

We identify the contravariant components of the vorticity via

$$\omega^{\bar{a}} = \varepsilon^{\bar{a}\bar{b}\bar{c}} \partial_{\bar{b}} v_{\bar{c}} = (\partial z / \partial \sigma)^{-1} \epsilon^{\bar{a}\bar{b}\bar{c}} \partial_{\bar{b}} v_{\bar{c}} \quad (41.95)$$

where we made use of equation (41.67) to introduce the permutation symbol. Expanding the components leads to

$$\omega^{\bar{1}} = (\partial \sigma / \partial z) (\partial_{\bar{2}} v_{\bar{3}} - \partial_{\bar{3}} v_{\bar{2}}) \quad (41.96a)$$

$$\omega^{\bar{2}} = (\partial \sigma / \partial z) (\partial_{\bar{3}} v_{\bar{1}} - \partial_{\bar{1}} v_{\bar{3}}) \quad (41.96b)$$

$$\omega^{\bar{3}} = \omega^{\sigma} = (\partial \sigma / \partial z) (\partial_{\bar{1}} v_{\bar{2}} - \partial_{\bar{2}} v_{\bar{1}}). \quad (41.96c)$$

### 41.16.2 Transforming from Cartesian coordinates

The above approach works solely with the GVC coordinates. An alternative approach connects the GVC vorticity components and the Cartesian vorticity components. For that purpose we use the transformation matrix via

$$\omega^{\bar{a}} = \Lambda_a^{\bar{a}} \omega^a, \quad (41.97)$$

where  $\omega^a$  are the Cartesian components

$$\boldsymbol{\omega} = \hat{x} \left( \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) + \hat{y} \left( \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right) + \hat{z} \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right). \quad (41.98)$$

Making use of the transformation matrix  $\Lambda_a^{\bar{a}}$  from equation (41.20) yields (as in Section 41.7)

$$\omega^{\bar{x}} = \omega^x = \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \quad \text{and} \quad \omega^{\bar{y}} = \omega^y = \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \quad \text{and} \quad \omega^{\sigma} = \boldsymbol{\omega} \cdot \nabla \sigma. \quad (41.99)$$

Note that for isopycnal coordinates in a Boussinesq fluid,  $\omega^{\sigma}$  equals to the potential vorticity when the vorticity is the absolute vorticity (Section 44.2). That is, the potential vorticity is the isopycnal component of the absolute vorticity.

## 41.17 Velocity circulation

The velocity circulation (Section 32.3) is given by the closed oriented path integral of the velocity projected into the direction of the path

$$\mathcal{C} \equiv \oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{x} \quad (41.100)$$

where  $d\mathbf{x}$  is the vector line element along the path and  $\partial\mathcal{S}$  is the closed path defining the boundary to a two-dimensional surface  $\mathcal{S}$ . Stokes' Theorem from Section 2.6 leads to the identity

$$\mathcal{C} = \oint_{\partial\mathcal{S}} \mathbf{v} \cdot d\mathbf{x} = \int_{\mathcal{S}} (\nabla \times \mathbf{v}) \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\mathcal{S}} \boldsymbol{\omega} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (41.101)$$

where  $\hat{\mathbf{n}}$  is the outward normal vector orienting the area element  $d\mathcal{S}$  according to the right-hand rule applied to the bounding circuit. These results are all written in a generally covariant manner (Section 6.1) so that they hold for an arbitrary coordinate representation.

As a particular case, consider the circulation around a closed path on a constant  $\sigma$  surface, in which

$$\hat{\mathbf{n}} = \frac{\nabla\sigma}{|\nabla\sigma|} \quad (41.102)$$

is the outward normal and

$$\boldsymbol{\omega} \cdot \hat{\mathbf{n}} = \frac{\omega^\sigma}{|\nabla\sigma|} \quad (41.103)$$

where  $\omega^\sigma = \boldsymbol{\omega} \cdot \nabla\sigma$  (equation (41.99)). So long as the vertical stratification remains non-zero ( $\partial\sigma/\partial z \neq 0$ ) we can write the area factor in the form

$$\frac{dS}{|\nabla\sigma|} = \frac{dS}{\sqrt{(\partial\sigma/\partial x)^2 + (\partial\sigma/\partial y)^2 + (\partial\sigma/\partial z)^2}} \quad (41.104a)$$

$$= \frac{dS}{|\partial\sigma/\partial z| \sqrt{[(\partial\sigma/\partial x)/(\partial\sigma/\partial z)]^2 + [(\partial\sigma/\partial y)/(\partial\sigma/\partial z)]^2 + 1}} \quad (41.104b)$$

$$= \frac{dS}{|\partial\sigma/\partial z| \sqrt{1 + \tan^2 \vartheta}} \quad (41.104c)$$

$$= \left| \frac{\partial z}{\partial \sigma} \right| |\cos \vartheta| dS \quad (41.104d)$$

$$= \left| \frac{\partial z}{\partial \sigma} \right| dA. \quad (41.104e)$$

The equality (41.104c) introduces the angle,  $\vartheta$ , between the boundary surface and the horizontal plane as in Figure 41.4. The squared slope of this surface given by

$$\tan^2 \vartheta = \frac{\nabla_z \sigma \cdot \nabla_z \sigma}{(\partial\sigma/\partial z)^2} = \nabla_\sigma z \cdot \nabla_\sigma z. \quad (41.105)$$

The equality (41.104d) made use of a trigonometric identity, and the equality (41.104e) introduced the horizontal projection of the area,

$$dA = |\cos \vartheta| dS. \quad (41.106)$$

Bringing these results together leads to the expression for circulation around a closed loop on a constant  $\sigma$  surface

$$C_{\sigma-\text{surface}} = \int_S (\boldsymbol{\omega} \cdot \nabla\sigma) |\partial z/\partial\sigma| dA. \quad (41.107)$$



# Chapter 42

## Kinematic equations

In providing a mechanistic description of budgets within the ocean or atmosphere, it is often useful to measure the material or momentum transfer through a surface. This transport is termed the *dia-surface transport*. Our discussion in this chapter unifies ideas developed for kinematic boundary conditions in Section 14.4 with transport across an arbitrary surface in the fluid interior. We do so by making use of the generalized vertical coordinates (GVCs) first introduced in Chapter 41. We make use of the dia-surface transport formulation to express the material time derivative operator using GVCs. This form for the material time derivative allows us to decompose the vertical velocity into motion relative to a moving GVC surface. In turn, we are afforded a means to reinterpret the velocity vector and corresponding particle trajectories. GVC kinematics also provides a means to express the subduction of fluid into the ocean interior beneath the mixed layer base. We close the chapter with derivations of the GVC version of mass continuity and the tracer equation. We also introduce the layer integrated version of the continuity and tracer equations, with the layer integrated equations appropriate for discrete numerical fluid models.

### CHAPTER GUIDE

We introduced mathematical properties of generalized vertical coordinates (GVCs) in Chapter 41, including the calculus using these non-orthogonal coordinates. It is essential to have a working knowledge of that material to understand the present chapter. Later in Chapter 43 we detail the dynamical equations using GVCs, with material in that chapter relying on the kinematics presented here. Following the treatment in Chapter 41, we here use the symbol  $\sigma$  to denote a generalized vertical coordinate.

42.1	Loose threads . . . . .	1044
42.2	Example generalized vertical coordinates . . . . .	1044
42.2.1	Ocean free surface . . . . .	1045
42.2.2	Solid earth boundary . . . . .	1045
42.2.3	Ocean mixed layer base . . . . .	1045
42.2.4	Interior generalized vertical coordinate surfaces . . . . .	1045
42.3	Specific thickness . . . . .	1046
42.4	The dia-surface transport . . . . .	1047
42.4.1	Flow normal to the GVC surface . . . . .	1047
42.4.2	Accounting for movement of the surface . . . . .	1048
42.4.3	We only care about divergent surface motion . . . . .	1049
42.4.4	Cross GVC transport in terms of GVC material evolution . . . . .	1049

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42.4.5 Defining the dia-surface transport . . . . .	1049
42.4.6 Expressions for the dia-surface velocity component . . . . .	1051
42.4.7 An alternative definition of dia-surface velocity component . . . . .	1052
42.4.8 Area integrated dia-surface transport for incompressible flows . . . . .	1052
42.5 Material time derivative . . . . .	1054
42.6 Vertical velocity and dia-surface velocity . . . . .	1054
42.6.1 Decomposing the vertical velocity . . . . .	1055
42.6.2 Another form of the vertical velocity decomposition . . . . .	1055
42.7 The velocity vector and fluid particle trajectories . . . . .	1057
42.8 Subduction across the mixed layer base . . . . .	1058
42.9 Mass continuity . . . . .	1059
42.9.1 Cartesian coordinates . . . . .	1059
42.9.2 Generalized vertical coordinates . . . . .	1060
42.10 Layer integrated mass continuity . . . . .	1060
42.10.1 Compressible fluids . . . . .	1061
42.10.2 Mass continuity using pressure coordinates . . . . .	1062
42.10.3 Incompressible flow . . . . .	1064
42.10.4 Rescaled geopotential coordinates . . . . .	1064
42.11 Layer integrated tracer equation . . . . .	1065

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## 42.1 Loose threads

- Develop the notion of overturning streamfunctions as per Sections 32.2 to 32.4 of the MOM5 elements guide. Work through the issues for both Boussinesq and non-Boussinesq.
- Develop the notion of depth integrated transport as per Sections 32.2 to 32.4 of the MOM5 elements guide. Work through the issues for both Boussinesq and non-Boussinesq.

## 42.2 Example generalized vertical coordinates

We here consider some generalized vertical coordinates that will prove of use for our discussion in this chapter, with Figure 42.1 illustrating the examples.

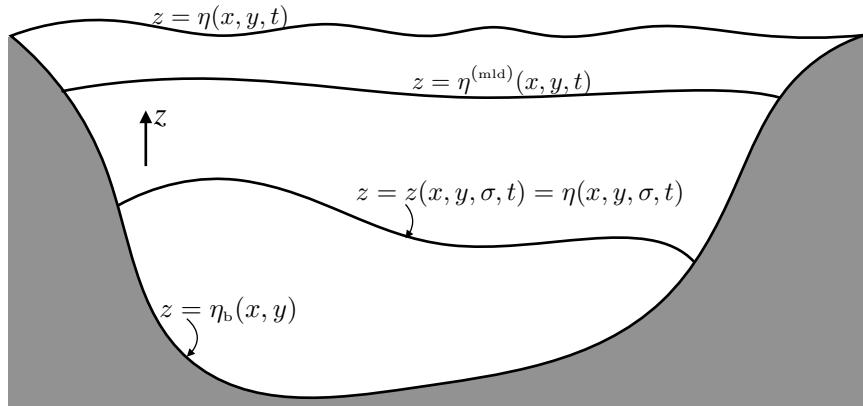


FIGURE 42.1: Example generalized vertical coordinates,  $\sigma(x, y, z, t)$ . The ocean free surface can be represented mathematically by  $\sigma(x, y, z, t) = z - \eta(x, y, t) = 0$ ; the ocean mixed layer base by  $\sigma(x, y, z, t) = z - \eta^{(mld)}(x, y, t) = 0$ ; the position of an interior GVC coordinate  $\sigma$  with depth  $z = z(x, y, \sigma, t) = \eta(x, y, \sigma, t)$ ; and the solid earth bottom  $\sigma(x, y, z) = z - \eta_b(x, y) = 0$ .

### 42.2.1 Ocean free surface

The first surface is the ocean free surface, whose kinematic boundary conditions were derived in Section 14.4.3. Here, water and tracer penetrate this surface through precipitation, evaporation, river runoff (when applied as an upper ocean boundary condition), and sea ice melt. Momentum exchange arises from stresses between the ocean and atmosphere or ice. The ocean free surface can be represented mathematically by the identity

$$\sigma(x, y, z, t) = z - \eta(x, y, t) = 0 \quad \text{ocean free surface.} \quad (42.1)$$

This identity holds so long as we assume the surface height  $\eta$  is smooth and contains no over-turns at the scales of interest. That is, we assume breaking surface waves are filtered from the description.

### 42.2.2 Solid earth boundary

We may describe the solid Earth lower boundary mathematically by using the time independent expression

$$\sigma(x, y, z) = z + H(x, y) = z - \eta_b(x, y) = 0 \quad \text{ocean bottom,} \quad (42.2)$$

where we introduce the two common symbols used for the bottom,  $\eta_b = -H$ . We generally prefer  $\eta_b$  since  $H$  is used elsewhere in this book for vertical scale. As detailed in Section 14.4.1, we typically assume that there is no fluid mass transport through the solid Earth. However, in the case of geothermal heating, we may consider an exchange of heat between the ocean and the solid Earth. Momentum exchange through the action of stresses occur between the solid Earth and ocean fluid.

### 42.2.3 Ocean mixed layer base

Let

$$\sigma = z - \eta^{(\text{mld})}(x, y, t) = 0 \quad (42.3)$$

represent the vertical position of the ocean mixed layer base. The corresponding normal vector is given by

$$\hat{\mathbf{n}}^{(\text{mld})} = \frac{\nabla(z - \eta^{(\text{mld})})}{|\nabla(z - \eta^{(\text{mld})})|} = \frac{\nabla(\hat{z} - \nabla\eta^{(\text{mld})})}{\sqrt{1 + |\nabla\eta^{(\text{mld})}|^2}}. \quad (42.4)$$

This example is relevant for the study of ocean ventilation, whereby we are interested in measuring the transport of fluid that enters the ocean interior across the mixed layer base (see Section 42.8).

### 42.2.4 Interior generalized vertical coordinate surfaces

Within the ocean interior, transport across surfaces of constant generalized vertical coordinate  $\sigma = \sigma(x, y, z, t)$  constitutes the dia-surface transport affecting budgets of mass, tracer, and momentum within layers bounded by two generalized vertical coordinate surfaces. A canonical example is provided by isopycnal layers formed by surfaces of constant potential density (or equivalently constant buoyancy surfaces) as used in isopycnal ocean models as well as theoretical descriptions of adiabatic ocean dynamics. The vertical position of this surface is written in one of two equivalent manners

$$z = z(x, y, \sigma, t) = \eta(x, y, \sigma, t). \quad (42.5)$$

The first expression exposes the functional dependence of the vertical position of the  $\sigma$  surface at a horizontal position and time. In Section 41.1 we discussed the potential for confusion between

writing  $z$  as a particular vertical position versus a function, thus motivating  $z = \eta(x, y, \sigma, t)$ . However, by now we should have sufficient experience with generalized vertical coordinates so that we can well distinguish when  $z$  refers to a particular vertical position versus  $z(x, y, \sigma, t)$  as a coordinate function. For this reason we only infrequently use  $z = \eta(x, y, \sigma, t)$  in this chapter.

## 42.3 Specific thickness

As mentioned in Section 41.9.1, a surface of constant generalized vertical coordinate can be successfully used to partition the vertical so long as the transformation between the generalized vertical coordinate and the geopotential coordinate is invertible. The Jacobian of transformation is given by

$$\frac{\partial z}{\partial \sigma} = z_\sigma, \quad (42.6)$$

which must be single signed for suitable generalized vertical coordinates. This constraint means that we do not allow the surfaces to overturn, which is the same assumption made about the ocean surface,  $z = \eta(x, y, t)$ , and solid earth bottom,  $z = \eta_b(x, y)$ . This restriction places a limitation on the ability of certain GVC models (e.g., isopycnal models) to describe non-hydrostatic processes, such as the overturning common in Kelvin-Helmholtz billows and gravitational convection. Note that for both the solid earth bottom and ocean free surface

$$\frac{\partial z}{\partial \sigma} = 1 \quad \text{ocean free surface and fluid/solid interface.} \quad (42.7)$$

Furthermore, this relation also holds, trivially, for geopotential coordinates in which  $\sigma = z$ .

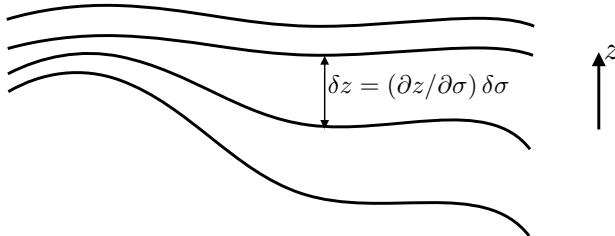


FIGURE 42.2: Illustrating the thickness between surfaces of constant generalized vertical coordinates,  $\delta z = (\partial z / \partial \sigma) \delta \sigma$ . In regions with larger magnitude for the specific thickness,  $\partial z / \partial \sigma$ , or equivalently smaller vertical stratification of the  $\sigma$  surfaces,  $\partial \sigma / \partial z$ , the layer thicknesses are further apart. The converse holds where  $\partial z / \partial \sigma$  is small (equivalently  $\partial \sigma / \partial z$  is large).

We refer to the Jacobian  $z_\sigma$  as the *specific thickness* and sometimes find it useful to write it as

$$h = z_\sigma = \frac{\partial z}{\partial \sigma}. \quad (42.8)$$

This name is motivated by noting that the vertical thickness of an infinitesimal layer of coordinate thickness  $\delta \sigma$  is given by

$$\delta z = \frac{\partial z}{\partial \sigma} \delta \sigma = h \delta \sigma, \quad (42.9)$$

with Figure 42.2 providing an example with finitely thick layers. For example, if  $\sigma = b(x, y, z, t)$  (buoyancy or potential density as in isopycnal models), then the thickness of a buoyancy layer is given by

$$\delta z = \frac{\partial z}{\partial \sigma} \delta b = N^{-2} \delta b, \quad (42.10)$$

with

$$N^2 = \frac{\partial b}{\partial z} \quad (42.11)$$

the squared buoyancy frequency (Section 24.5.4) in a Boussinesq fluid (Chapter 23). For a hydrostatic fluid using pressure as the vertical coordinate, the thickness of a pressure layer is

$$\delta z = \frac{\partial z}{\partial p} \delta p = -\frac{1}{\rho g} \delta p \quad (42.12)$$

where we used the hydrostatic relation (Section 22.2)

$$\frac{\partial p}{\partial z} = -\rho g \quad (42.13)$$

with  $g$  the constant acceleration due to effective gravity. Note that we assume the layer thickness is positive,  $\delta z > 0$ . For this purpose, with hydrostatic pressure we might choose to consider negative pressure increments,  $\delta p < 0$ , as this corresponds to vertically upward movement in a fluid column.

## 42.4 The dia-surface transport

In this section we develop the concept of dia-surface transport and derive its expression in terms of the material time derivative of the GVC surface.

### 42.4.1 Flow normal to the GVC surface

At an arbitrary point on a surface of constant generalized vertical coordinate (see Figure 42.3), the rate at which fluid moves in the direction normal to the surface is given by

$$\text{RATE OF FLUID FLOW IN DIRECTION } \hat{\mathbf{n}} = \mathbf{v} \cdot \hat{\mathbf{n}}, \quad (42.14)$$

where

$$\hat{\mathbf{n}} = \frac{\nabla \sigma}{|\nabla \sigma|}, \quad (42.15)$$

is the surface unit normal. Two examples are useful to ground this expression in common experience. For the ocean free surface,  $\sigma = z - \eta(x, y, t) = 0$ , the unit normal takes the form

$$\hat{\mathbf{n}} = \frac{\nabla(z - \eta)}{|\nabla(z - \eta)|} = \frac{\hat{\mathbf{z}} - \nabla \eta}{\sqrt{1 + |\nabla \eta|^2}}, \quad (42.16)$$

whereas at the solid Earth bottom,  $\sigma = z - \eta_b(x, y) = 0$ ,

$$\hat{\mathbf{n}} = -\frac{\nabla(z - \eta_b)}{|\nabla(z - \eta_b)|} = -\frac{\hat{\mathbf{z}} - \nabla \eta_b}{\sqrt{1 + |\nabla \eta_b|^2}}. \quad (42.17)$$

Introducing the material time derivative

$$\frac{D\sigma}{Dt} = \frac{\partial \sigma}{\partial t} + \mathbf{v} \cdot \nabla \sigma \quad (42.18)$$

to equation (42.14) leads to the identity

$$\mathbf{v} \cdot \hat{\mathbf{n}} = \frac{1}{|\nabla\sigma|} \left[ \frac{D\sigma}{Dt} - \frac{\partial\sigma}{\partial t} \right]. \quad (42.19)$$

Hence, the component to the velocity of a fluid particle that is normal to a GVC surface is proportional to the difference between the material time derivative of the surface coordinate and its partial time derivative.

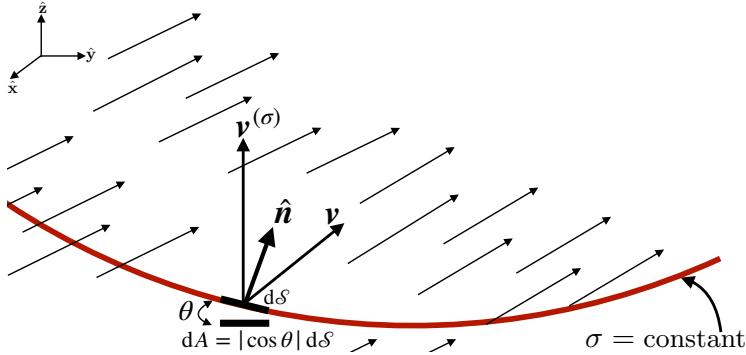


FIGURE 42.3: A surface of constant generalized vertical coordinate,  $\sigma = \text{constant}$ , within a fluid. The normal direction,  $\hat{\mathbf{n}} = \nabla\sigma/|\nabla\sigma|$ , points in the direction of increasing  $\sigma$ . We show an example velocity vector for a fluid particle,  $\mathbf{v}$ , at a point on the surface as well as the velocity,  $\mathbf{v}^{(\sigma)}$ , of a point that lives on the surface. Note that kinematics is only concerned with the normal component to the surface velocity,  $\mathbf{v}^{(\sigma)} \cdot \hat{\mathbf{n}}$ , as per equation (42.25). We require dynamical information to obtain information about the tangential component of  $\mathbf{v}^{(\sigma)}$ , but such information is not required for this chapter. Following equation (42.30), the horizontal projection of the surface area element is given by  $dA = |\cos\vartheta| d\mathcal{S}$ , where  $\vartheta$  is the angle between the surface and the horizontal and  $dA = dx dy$ .

#### 42.4.2 Accounting for movement of the surface

A generalized vertical coordinate surface is generally moving. So to diagnose the net transport of fluid penetrating the surface requires us to subtract the velocity of the surface,  $\mathbf{v}^{(\sigma)}$ , from the velocity of a fluid particle. We are thus led to

$$\text{RATE THAT FLUID CROSSES A MOVING GVC SURFACE} = \hat{\mathbf{n}} \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}). \quad (42.20)$$

We next develop a kinematic property of the surface velocity, or more precisely the normal component to that velocity. For that purpose, consider an infinitesimal increment in both space and time under which  $\sigma$  undergoes an infinitesimal change

$$\delta\sigma = \delta\mathbf{x} \cdot \nabla\sigma + \delta t \partial_t\sigma. \quad (42.21)$$

Now restrict attention to a point fixed on a constant  $\sigma$  surface, in which

$$\delta\sigma = \delta\mathbf{x}^{(\sigma)} \cdot \nabla\sigma + \delta t \partial_t\sigma = 0, \quad (42.22)$$

where  $\delta\mathbf{x}^{(\sigma)}$  is a differential increment following the moving surface. We define the velocity of that point as

$$\mathbf{v}^{(\sigma)} = \frac{\delta\mathbf{x}^{(\sigma)}}{\delta t}, \quad (42.23)$$

in which case equation (42.22) implies that at each point within the fluid,

$$\frac{\partial \sigma}{\partial t} + \mathbf{v}^{(\sigma)} \cdot \nabla \sigma = 0. \quad (42.24)$$

We can likewise write this equation as one for the normal component of the surface velocity

$$\mathbf{v}^{(\sigma)} \cdot \hat{\mathbf{n}} = -\frac{1}{|\nabla \sigma|} \frac{\partial \sigma}{\partial t}. \quad (42.25)$$

Hence, we reach the sensible result that the normal component to the velocity of the surface vanishes when the surface is static.

#### 42.4.3 We only care about divergent surface motion

For the kinematics of fluid motion relative to a surface of constant generalized vertical coordinates, we are only concerned with the normal component to the surface velocity,  $\mathbf{v}^{(\sigma)} \cdot \hat{\mathbf{n}}$ . That is, we are only concerned with divergent motion of the surface, defined as motion parallel to the surface normal direction,  $\hat{\mathbf{n}}$ . We have no concern for rotational or tangential motion, which is motion perpendicular to  $\hat{\mathbf{n}}$ . Even so, some authors, by fiat, choose to set to zero the tangential component of the surface motion. In fact, specification of the tangential surface velocity component is generally not available without extra information about the surface motion, nor is its specification necessary for developing kinematic properties of fluid motion relative to arbitrary generalized vertical coordinate surfaces. Hence, we make no statement about tangential motion of the surface.

#### 42.4.4 Cross GVC transport in terms of GVC material evolution

Using expression (42.25) in equation (42.20) leads to the net flux of fluid crossing the GVC surface

$$\hat{\mathbf{n}} \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}) = \frac{1}{|\nabla \sigma|} \frac{D\sigma}{Dt}. \quad (42.26)$$

The material time derivative of the GVC surface thus vanishes if no fluid crosses the surface. Notably, this result holds for motion of the fluid as defined by the barycentric velocity,  $\mathbf{v}$ , of Section 15.1.2. For multi-component fluids,  $\dot{\sigma} = 0$  can still, in principle, be associated with trace matter exchange across the surface via diffusion so long as the net matter crossing the surface is zero. But this situation is rather fine tuned and thus unlikely. Additionally, matter diffusion also occurs with heat diffusion, in which case  $\dot{\sigma} = 0$  only occurs in the absence of both matter and heat diffusion, which then means that  $\sigma$  is a material surface.

#### 42.4.5 Defining the dia-surface transport

The area normalizing the volume flux in equation (42.26) is the area  $d\delta$  of an infinitesimal patch on the surface of constant generalized vertical coordinate with outward unit normal  $\hat{\mathbf{n}}$ . We now follow the trigonometry discussed in Section 41.17 to introduce the horizontal projection of this area,  $dA$ , which is more convenient to work with for many purposes. So long as the vertical

stratification remains non-zero ( $\partial\sigma/\partial z \neq 0$ ) we can write the area factor in the form

$$\frac{d\mathcal{S}}{|\nabla\sigma|} = \frac{d\mathcal{S}}{\sqrt{(\partial\sigma/\partial x)^2 + (\partial\sigma/\partial y)^2 + (\partial\sigma/\partial z)^2}} \quad (42.27a)$$

$$= \frac{d\mathcal{S}}{|\partial\sigma/\partial z| \sqrt{[(\partial\sigma/\partial x)/(\partial\sigma/\partial z)]^2 + [(\partial\sigma/\partial y)/(\partial\sigma/\partial z)]^2 + 1}} \quad (42.27b)$$

$$= \frac{d\mathcal{S}}{|\partial\sigma/\partial z| \sqrt{1 + \tan^2 \vartheta}} \quad (42.27c)$$

$$= \left| \frac{\partial z}{\partial\sigma} \right| |\cos \vartheta| d\mathcal{S} \quad (42.27d)$$

$$= \left| \frac{\partial z}{\partial\sigma} \right| dA. \quad (42.27e)$$

The equality (42.27c) introduced the angle,  $\vartheta$ , between the boundary surface and the horizontal plane. The squared slope of this surface given by (see Section 41.12)

$$\tan^2 \vartheta = \frac{\nabla_z \sigma \cdot \nabla_z \sigma}{(\partial\sigma/\partial z)^2} = \nabla_\sigma z \cdot \nabla_\sigma z. \quad (42.28)$$

The equality (42.27d) made use of a trigonometric identity so that

$$|\cos \vartheta|^{-1} = |z_\sigma \nabla\sigma|. \quad (42.29)$$

Furthermore, the equality (42.27e) introduced the horizontal projection of the area,

$$dA = |\cos \vartheta| d\mathcal{S}. \quad (42.30)$$

We now introduce the *dia-surface velocity component* for the GVC coordinate

$$w^{(\dot{\sigma})} = \frac{\partial z}{\partial\sigma} \frac{D\sigma}{Dt} = z_\sigma \dot{\sigma}, \quad (42.31)$$

which measures the volume of fluid passing through the surface, per unit horizontal area, per unit time

$$w^{(\dot{\sigma})} \equiv \hat{n} \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}) \frac{d\mathcal{S}}{dA} \quad (42.32)$$

$$= \frac{(\text{VOLUME/TIME}) \text{ FLUID THROUGH SURFACE}}{\text{HORIZONTAL AREA OF SURFACE}}, \quad (42.33)$$

so that

$$w^{(\dot{\sigma})} dA \equiv \hat{n} \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}) d\mathcal{S}. \quad (42.34)$$

The velocity component  $w^{(\dot{\sigma})}$  is referred to as the dia-surface velocity component since it measures flow rate of fluid through the surface. We can think of  $w^{(\dot{\sigma})}$  as the “vertical” velocity which, when multiplied by the horizontal area element, measures the transport of fluid that crosses the surface in the normal direction.

#### 42.4.6 Expressions for the dia-surface velocity component

Making use of various identities derived above, as well as the transformation of partial derivative operators in Section 41.12, allows us to write the dia-surface velocity component in the following equivalent forms

$$w^{(\dot{\sigma})} = \frac{\partial z}{\partial \sigma} \frac{D\sigma}{Dt} \quad (42.35a)$$

$$= \frac{\partial z}{\partial \sigma} |\nabla \sigma| \hat{n} \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}) \quad (42.35b)$$

$$= \frac{\partial z}{\partial \sigma} \nabla \sigma \cdot \mathbf{v} - \frac{\partial z}{\partial \sigma} |\nabla \sigma| \hat{n} \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}) \quad (42.35c)$$

$$= (\hat{z} - \nabla_\sigma z) \cdot \mathbf{v} + \frac{\partial z}{\partial \sigma} \frac{\partial \sigma}{\partial t} \quad (42.35d)$$

$$= (\hat{z} - \nabla_\sigma z) \cdot \mathbf{v} - \frac{\partial z}{\partial t} \quad (42.35e)$$

$$= w - (\partial_t + \mathbf{u} \cdot \nabla_\sigma) z, \quad (42.35f)$$

where  $\partial z / \partial t = (\partial z / \partial t)_\sigma$  is the time derivative for the depth of the  $\sigma$  surface. We also made use of the identity (see equations (41.34b) and (41.34c))

$$\nabla_\sigma z = -z_\sigma \nabla_z \sigma \quad (42.36)$$

to express the slope of the  $\sigma$  surface as projected onto the horizontal direction plane, as well as the corresponding identity (41.34a) for the time derivative

$$\left[ \frac{\partial z}{\partial t} \right]_\sigma = -\frac{[\partial \sigma / \partial t]_z}{[\partial \sigma / \partial z]}. \quad (42.37)$$

The form given by equation (42.35f) directly relates the vertical component to the fluid particle velocity to the dia-surface velocity component

$$w = \frac{Dz}{Dt} \longleftrightarrow w^{(\dot{\sigma})} = \frac{\partial z}{\partial \sigma} \frac{D\sigma}{Dt} = w - (\partial_t + \mathbf{u} \cdot \nabla_\sigma) z. \quad (42.38)$$

When the GVC surface is static, so that it occupies a constant vertical position  $\partial z / \partial t = 0$ , then the dia-surface velocity component reduces to

$$w^{(\dot{\sigma})} = w - \mathbf{u} \cdot \nabla_\sigma z \quad \text{static surface,} \quad (42.39)$$

whereas if the GVC surface is flat, then the dia-surface velocity component measures the flux of fluid moving vertically relative to the motion of the GVC surface. Finally, if the surface is flat and static, the dia-surface velocity component becomes the vertical velocity component

$$w^{(\dot{\sigma})} = w = \frac{Dz}{Dt} \quad \text{GVC surface static and flat,} \quad (42.40)$$

which is the case for the geopotential vertical coordinate. This relation reveals the kinematic distinction between  $w$  and  $w^{(\dot{\sigma})}$ , with the two differing in the presence of GVC transients and horizontal velocities that project onto a non-horizontal GVC surface. Equation (42.35f) thus offers a useful means to distinguish  $w$  from  $w^{(\dot{\sigma})}$ .

#### 42.4.7 An alternative definition of dia-surface velocity component

In some literature presentations, the dia-surface velocity component is taken to be

$$w^{\text{dia}} = \hat{\mathbf{n}} \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}) = \frac{1}{|\nabla\sigma|} \frac{D\sigma}{Dt}. \quad (42.41)$$

For example, [Groeskamp et al. \(2019\)](#) prefer this definition for watermass analysis. As seen in Chapter 50, the reason to prefer expression (42.41) for watermass analysis is that we do not wish to assume vertically stable stratification for surfaces of constant  $\sigma$ . Dropping that assumption allows us to consider transformation between arbitrarily oriented elements of seawater, even those that are gravitationally unstable.

#### 42.4.8 Area integrated dia-surface transport for incompressible flows

We close this section by further emphasizing the distinction in time dependent flows between dia-surface transport and flow normal to a surface. For this purpose consider an incompressible flow whereby  $\nabla \cdot \mathbf{v} = 0$ . Incompressibility means that for any closed surface within the fluid interior, the following identity holds via the divergence theorem

$$0 = \int_{\mathcal{R}} \nabla \cdot \mathbf{v} dV = \oint_{\partial\mathcal{R}} \hat{\mathbf{n}} \cdot \mathbf{v} d\mathcal{S}. \quad (42.42)$$

Notably, only in the case of a static surface do we conclude there is no net flow across the surface (see Exercise 16.4). For surfaces that move, there is generally a nonzero net dia-surface transport. We clarify this rather puzzling statement in the following.

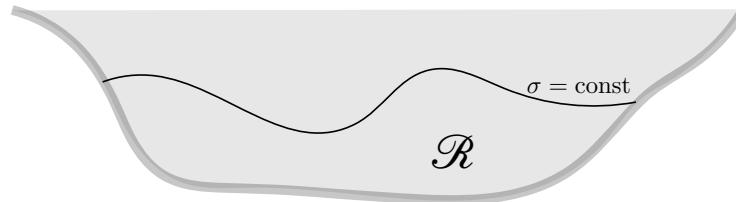


FIGURE 42.4: A constant GVC surface,  $\sigma = \text{constant}$ , within an ocean basin that intersects the bottom. The region  $\mathcal{R}$  is bounded above by the  $\sigma$  surface and below by the solid-earth. Along the constant  $\sigma$  surface an incompressible flow satisfies  $\int_{\sigma=\text{const}} \hat{\mathbf{n}} \cdot \mathbf{v} d\mathcal{S} = 0$ .

As a specific example, consider a fluid region such as shown in Figure 42.4, which is bounded by the solid-earth bottom and a constant GVC surface. Since the solid-earth bottom is static and there is no-normal flow through the bottom, the identity (42.42) means that the area integrated flow normal to the GVC vanishes

$$\int_{\sigma=\text{const}} \hat{\mathbf{n}} \cdot \mathbf{v} d\mathcal{S} = 0. \quad (42.43)$$

But what does this identity imply about the area integrated dia-surface velocity? For the case of a geopotential vertical coordinate,  $\sigma = z$ , it means that the area integrated vertical velocity vanishes across any geopotential surface below the ocean free surface,  $\int_{z=\text{const}} w dA = 0$  (see Exercise 16.4). What about other GVCs?

To address this question consider the general result

$$\int_{\sigma=\text{const}} \hat{\mathbf{n}} \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}) d\mathcal{S} = \int_{\sigma=\text{const}} w^{\text{dia}} d\mathcal{S} = \int_{\sigma=\text{const}} w^{(\dot{\sigma})} dA, \quad (42.44)$$

where again  $dA = dx dy$ . Now make use of the property (42.43) for incompressible flows as well as the identity (42.25) to render

$$\int_{\sigma=\text{const}} w^{(\dot{\sigma})} dA = 0 - \int_{\sigma=\text{const}} \hat{\mathbf{n}} \cdot \mathbf{v}^{(\sigma)} d\mathcal{S} \quad (42.45a)$$

$$= \int_{\sigma=\text{const}} \frac{\partial \sigma / \partial t}{|\nabla \sigma|} d\mathcal{S} \quad (42.45b)$$

$$= \int_{\sigma=\text{const}} \frac{\partial \sigma}{\partial t} \left| \frac{\partial z}{\partial \sigma} \right| dA \quad (42.45c)$$

$$= - \int_{\sigma=\text{const}} \left[ \frac{\partial z}{\partial t} \right]_\sigma dA. \quad (42.45d)$$

The final equality holds if  $\partial z / \partial \sigma > 0$ , whereas we swap signs when the vertical stratification is  $\partial z / \partial \sigma < 0$ . We can go one further step by noting that the time derivative is computed with  $\sigma$  constant, as is the horizontal area integral. Hence, we can pull the time derivative outside the integral to render

$$\int_{\sigma=\text{const}} w^{(\dot{\sigma})} dA = - \left[ \frac{\partial}{\partial t} \right]_\sigma \int_{\sigma=\text{const}} z dA. \quad (42.46)$$

This identity means that for an incompressible flow, the integrated dia-surface transport across the GVC surface equals to minus the time tendency for the area integrated vertical position of that surface. Hence, there is an area integrated dia-surface transport across the GVC surface so long as there is a volume change for the region beneath the surface.

For the case of an isopycnal surface in an adiabatic fluid, there is no change in the volume beneath any interior isopycnal since no flow crosses the isopycnal, in which case we recover the expected result  $\int_{\sigma=\text{const}} w^{(\dot{\sigma})} dA = 0$ . However, this result does not hold for other coordinates, such as the rescaled vertical coordinate,  $\sigma = z^*$  defined by equation (42.112). In this case

$$z^* = H \frac{z - \eta}{H + \eta} \quad (42.47a)$$

$$\frac{\partial z}{\partial z^*} = 1 + H/\eta > 0 \quad (42.47b)$$

$$\left[ \frac{\partial z}{\partial t} \right]_{z^*} = \frac{\partial \eta}{\partial t} (1 + z^*/H), \quad (42.47c)$$

so that

$$\int_{z^*=\text{const}} w^{(z^*)} dA = \int_{z^*=\text{const}} (\partial \eta / \partial t) (1 + z^*/H) dA, \quad (42.48)$$

which is generally nonzero. For example, consider a flat bottom so that

$$\int_{z^*=\text{const}} w^{(z^*)} dA = (1 + z^*/H) \int_{z^*=\text{const}} (\partial \eta / \partial t) dA = (1 + z^*/H) \int_{z^*=\text{const}} (Q_m / \rho_0) dA, \quad (42.49)$$

where  $Q_m$  is the surface mass flux and we made use of the incompressible free surface equation (16.8). In this case the area integrated dia-surface transport across a  $z^*$  surface is proportional to the area integrated surface mass flux.

## 42.5 Material time derivative

The expression (42.31) for  $w^{(\dot{\sigma})}$  brings the material time derivative operator into the following equivalent forms

$$\frac{D}{Dt} = \left[ \frac{\partial}{\partial t} \right]_z + \mathbf{u} \cdot \nabla_z + w \frac{\partial}{\partial z} \quad (42.50a)$$

$$= \left[ \frac{\partial}{\partial t} \right]_\sigma + \mathbf{u} \cdot \nabla_\sigma + \frac{D\sigma}{Dt} \frac{\partial}{\partial \sigma} \quad (42.50b)$$

$$= \left[ \frac{\partial}{\partial t} \right]_\sigma + \mathbf{u} \cdot \nabla_\sigma + w^{(\dot{\sigma})} \frac{\partial}{\partial z}. \quad (42.50c)$$

Note that the chain-rule means that

$$\frac{\partial}{\partial \sigma} = \frac{\partial z}{\partial \sigma} \frac{\partial}{\partial z}, \quad (42.51)$$

thus providing a relationship between the two vertical coordinate partial derivatives. Furthermore, recall that subscripts in the above derivative operators denote variables held fixed when taking the partial derivatives.

We highlight the special case of no fluid particles crossing the generalized coordinate surface. This situation occurs in the case of adiabatic flows with  $\sigma$  equal to the buoyancy or isopycnal coordinate. For adiabatic flow, the material time derivative in equation (42.50c) only has a horizontal two-dimensional advective component,  $\mathbf{u} \cdot \nabla_\sigma$ . This result should not be interpreted to mean that the fluid particle velocity in an adiabatic flow is strictly horizontal. Indeed, it generally is not, as the form given by equation (42.50a) makes clear. Rather, it means that the advective transport of fluid properties occurs along surfaces of constant buoyancy, and such transport is measured by the convergence of horizontal advective fluxes as measured along these constant buoyancy surfaces.

## 42.6 Vertical velocity and dia-surface velocity

Making use of the material time derivative operator (42.50c) affords us an opportunity to emphasize both the differences and similarities between the vertical velocity component and the dia-surface velocity component. Namely, the vertical velocity component takes on the equivalent forms

$$w = \frac{Dz}{Dt} = \left[ \frac{\partial z}{\partial t} \right]_\sigma + \mathbf{u} \cdot \nabla_\sigma z + w^{(\dot{\sigma})} = \frac{\partial z}{\partial \sigma} \left[ -\frac{\partial \sigma}{\partial t} - \mathbf{u} \cdot \nabla_z \sigma + \frac{D\sigma}{Dt} \right], \quad (42.52)$$

and the corresponding expressions for the dia-surface velocity component are given by

$$w^{(\dot{\sigma})} = \frac{\partial z}{\partial \sigma} \frac{D\sigma}{Dt} = \frac{\partial z}{\partial \sigma} \left[ \frac{\partial \sigma}{\partial t} + \mathbf{u} \cdot \nabla_z \sigma + w \frac{\partial \sigma}{\partial t} \right] = - \left[ \frac{\partial z}{\partial t} \right]_\sigma - \mathbf{u} \cdot \nabla_\sigma z + w. \quad (42.53)$$

Whereas the vertical velocity component,  $w$ , measures the transport crossing  $z$  surfaces, which are static and horizontal, the dia-surface velocity component,  $w^{(\dot{\sigma})}$ , measures the transport crossing  $\sigma$  surfaces, which are generally moving and sloped. It is notable that the area normalization used in equation (42.33) for the dia-surface velocity component means that it appears only in the expression for the vertical velocity. However, as we will see in the following, the appearance of  $w^{(\dot{\sigma})}$  in the  $w$  equation does not necessarily mean that  $w^{(\dot{\sigma})}$  corresponds to vertical particle motion. Instead, when it arises from mixing,  $w^{(\dot{\sigma})}$  can lead to vertical motion of the  $\sigma$  surface while maintaining a fixed position for the fluid particle.

### 42.6.1 Decomposing the vertical velocity

The expression

$$w = \left[ \frac{\partial z}{\partial t} \right]_{\sigma} + \mathbf{u} \cdot \nabla_{\sigma} z + w^{(\dot{\sigma})} \quad (42.54)$$

decomposes the vertical velocity of a fluid particle into (i) changes to the vertical position of the  $\sigma$ -surface at a particular horizontal point, (ii) lateral particle motion projected onto a sloped  $\sigma$ -surface, (iii) motion that crosses a  $\sigma$ -surface. Importantly, the three terms are coupled. For example, consider the case of  $\sigma$  defined by isopycnals, in which case irreversible mixing ( $w^{(\dot{\sigma})} \neq 0$ ) changes the configuration of  $\sigma$  surfaces by changing both their height,  $(\partial z / \partial t)_{\sigma}$ , and slope  $\nabla_{\sigma} z$ .

### 42.6.2 Another form of the vertical velocity decomposition

Consider the velocity for a point on the surface,  $\mathbf{v}^{(\sigma)}$ , which satisfies (Section 42.4.2)

$$\frac{\partial \sigma}{\partial t} + \mathbf{v}^{(\sigma)} \cdot \nabla \sigma = 0. \quad (42.55)$$

Making use of the triple product identities from Section 41.5

$$\frac{\partial z}{\partial \sigma} \nabla \sigma = -\nabla_{\sigma} z + \hat{\mathbf{z}} \quad \text{and} \quad \frac{\partial z}{\partial \sigma} \left[ \frac{\partial \sigma}{\partial t} \right]_z = - \left[ \frac{\partial z}{\partial t} \right]_{\sigma} \quad (42.56)$$

brings equation (42.55) into the form

$$\left[ \frac{\partial z}{\partial t} \right]_{\sigma} = (\hat{\mathbf{z}} - \nabla_{\sigma} z) \cdot \mathbf{v}^{(\sigma)} \implies \hat{\mathbf{z}} \cdot \mathbf{v}^{(\sigma)} = \left[ \frac{\partial z}{\partial t} \right]_{\sigma} + \mathbf{u}^{(\sigma)} \cdot \nabla_{\sigma} z, \quad (42.57)$$

where  $\mathbf{u}^{(\sigma)}$  is the horizontal component to the surface velocity  $\mathbf{v}^{(\sigma)}$ . This equation shows that the vertical component to the  $\sigma$ -surface velocity is given by the sum of the changes to the vertical position of the surface plus the projection of the horizontal motion of the surface onto the slope of the surface. Additionally, even if the  $\sigma$ -surface has no component of velocity in the vertical, the depth of the  $\sigma$ -surface measured at a horizontal point generally changes if the surface is sloped and moves horizontally pass that point

$$\left[ \frac{\partial z}{\partial t} \right]_{\sigma} = -\mathbf{u}^{(\sigma)} \cdot \nabla_{\sigma} z \quad \text{if } \hat{\mathbf{z}} \cdot \mathbf{v}^{(\sigma)} = 0. \quad (42.58)$$

Returning to the general result (42.57) allows us to write

$$\left[ \frac{\partial z}{\partial t} \right]_{\sigma} + \mathbf{u} \cdot \nabla_{\sigma} z = \hat{\mathbf{z}} \cdot \mathbf{v}^{(\sigma)} + (\mathbf{u} - \mathbf{u}^{(\sigma)}) \cdot \nabla_{\sigma} z. \quad (42.59)$$

Furthermore, return to the fundamental definition of the dia-surface velocity component detailed in Section 42.4, in which we showed that

$$w^{(\dot{\sigma})} = \frac{\partial z}{\partial \sigma} \frac{D\sigma}{Dt} = \frac{\partial z}{\partial \sigma} \nabla \sigma \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}) = (-\nabla_{\sigma} z + \hat{\mathbf{z}}) \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}). \quad (42.60)$$

This expression, along with equation (42.59), leads to the rather elaborate decomposition of the

vertical velocity component according to motion of a generalized vertical coordinate surface

$$w = \underbrace{\left[ \hat{z} \cdot \mathbf{v}^{(\sigma)} + (\mathbf{u} - \mathbf{u}^{(\sigma)}) \cdot \nabla_{\sigma} z \right]}_{(\partial_t + \mathbf{u} \cdot \nabla_{\sigma}) z} + \underbrace{\left[ \hat{z} \cdot \mathbf{v} - \hat{z} \cdot \mathbf{v}^{(\sigma)} - (\mathbf{u} - \mathbf{u}^{(\sigma)}) \cdot \nabla_{\sigma} z \right]}_{w^{(\dot{\sigma})}}. \quad (42.61)$$

Terms in the first bracket compute vertical particle motion relative to the  $\sigma$ -surface. The dia-surface contribution from the second bracket removes the contribution from  $\sigma$ -surface motion to leave just the vertical motion of the particle. All terms on the right hand side cancel, except for  $\hat{z} \cdot \mathbf{v} = w$ , thus trivially revealing  $w = w$ . The decomposition of  $w$  is rather pedantic when viewed in the unpacked form of equation (42.61). Even so, let us consider some special cases to offer further interpretation.

- NO HORIZONTAL CONTRIBUTION: Consider the case where the horizontal velocity of a fluid particle matches that of the  $\sigma$ -surface:  $\mathbf{u} = \mathbf{u}^{(\sigma)}$ . Alternatively, consider the case with flat  $\sigma$ -surfaces so that  $\nabla_{\sigma} z = 0$ . In either case the vertical velocity is given by

$$w = \underbrace{\left[ \hat{z} \cdot \mathbf{v}^{(\sigma)} \right]}_{(\partial_t + \mathbf{u} \cdot \nabla_{\sigma}) z} + \underbrace{\left[ \hat{z} \cdot (\mathbf{v} - \mathbf{v}^{(\sigma)}) \right]}_{w^{(\dot{\sigma})}}. \quad (42.62)$$

The first contribution is from vertical motion of the  $\sigma$ -surface. The second contribution adjusts for the vertical motion of the particle relative to the  $\sigma$ -surface, leaving behind just the vertical motion of the particle. This rather trivial case exemplifies the contributions from the two pieces of the vertical velocity.

- ZERO VERTICAL PARTICLE MOTION: Consider the case where  $w = 0$  so that

$$w = 0 \quad (42.63a)$$

$$= \left[ \frac{\partial z}{\partial t} \right]_{\sigma} + \mathbf{u} \cdot \nabla_{\sigma} z + w^{(\dot{\sigma})} \quad (42.63b)$$

$$= \underbrace{\left[ \hat{z} \cdot \mathbf{v}^{(\sigma)} + (\mathbf{u} - \mathbf{u}^{(\sigma)}) \cdot \nabla_{\sigma} z \right]}_{(\partial_t + \mathbf{u} \cdot \nabla_{\sigma}) z} + \underbrace{\left[ -\hat{z} \cdot \mathbf{v}^{(\sigma)} - (\mathbf{u} - \mathbf{u}^{(\sigma)}) \cdot \nabla_{\sigma} z \right]}_{w^{(\dot{\sigma})}}. \quad (42.63c)$$

The final expression is trivial since each term in one bracket identically cancels terms in the other bracket. The penultimate expression reveals the balance between dia-surface transport and motion relative to the  $\sigma$  surface

$$-\mathbf{w}^{(\dot{\sigma})} = \left[ \frac{\partial z}{\partial t} \right]_{\sigma} + \mathbf{u} \cdot \nabla_{\sigma} z \quad \text{if } w = 0. \quad (42.64)$$

A particularly simple realization of this balance holds for  $\sigma$  given by isopycnals and where the isosurfaces are horizontal. In the presence of uniform mixing, the flat isopycnals stay flat and there is correspondingly no vertical motion of fluid particles even as the vertical stratification is modified. In contrast, the vertical position of an isopycnal surface changes according to the dia-surface velocity component  $(\partial z / \partial t)_{\sigma} = -w^{(\dot{\sigma})} \neq 0$ . This case illustrates that  $w^{(\dot{\sigma})} \neq 0$  can still occur even when there is zero fluid particle motion since  $w^{(\dot{\sigma})} \neq 0$  can arise from motion of a  $\sigma$ -surface alone.

## 42.7 The velocity vector and fluid particle trajectories

Recall from Section 42.6 the alternative forms for the vertical velocity component given by equation (42.52). We focus on the form

$$w = \left[ \frac{\partial z}{\partial t} \right]_{\sigma} + \mathbf{u} \cdot \nabla_{\sigma} z + w^{(\dot{\sigma})} \quad (42.65)$$

so that the velocity vector is written<sup>1</sup>

$$\mathbf{v} = u \hat{x} + v \hat{y} + w \hat{z} \quad (42.66a)$$

$$= u \hat{x} + v \hat{y} + \left[ (\partial z / \partial t)_{\sigma} + \mathbf{u} \cdot \nabla_{\sigma} z + w^{(\dot{\sigma})} \right] \hat{z} \quad (42.66b)$$

$$= u [\hat{x} + \hat{z} (\partial z / \partial x)_{\sigma}] + v [\hat{y} + \hat{z} (\partial z / \partial y)_{\sigma}] + \left[ (\partial z / \partial t)_{\sigma} + w^{(\dot{\sigma})} \right] \hat{z}. \quad (42.66c)$$

To help further understand these velocity expressions we consider the following three cases, each of which are illustrated in Figure 42.5.

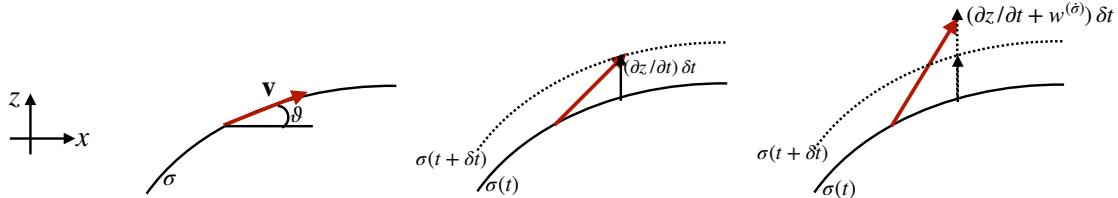


FIGURE 42.5: This schematic shows the various contributions to the fluid particle velocity (red vector) when written relative to motion of a particular generalized vertical coordinate surface. The fluid particle sits at the tail of the velocity vector at time  $t$  and at the head at time  $t + \delta t$ . The left panel is for the case of a static and material  $\sigma$ -surface so that the particle remains on the  $\sigma$ -surface and has a velocity vector given by equation (42.68). The slope of the  $\sigma$ -surface in the  $\hat{x}$ -direction is given by  $\tan \vartheta = (\partial z / \partial x)_{\sigma}$ . The middle panel is for a non-steady material  $\sigma$ -surface whereby the velocity of a particle takes on the form (42.69), with the particle remaining on the moving  $\sigma$ -surface. The right panel shows the case of a non-steady and non-material  $\sigma$ -surface with velocity (42.70). In this final case the particle position departs from the original  $\sigma$ -surface due to the nonzero dia-surface velocity component,  $w^{(\dot{\sigma})} \neq 0$ . However, it is not known *a priori* whether this departure is due to particle motion or motion of the surface. Notably, the horizontal position of the particle remains identical for each of the three cases. It is only the vertical position that is modified according to the slope of the  $\sigma$ -surface (left panel), motion of the  $\sigma$ -surface (middle panel), and motion crossing the  $\sigma$ -surface (right panel).

- STEADY AND MATERIAL  $\sigma$ -SURFACE: The velocity vector is aligned with the instantaneous  $\sigma$ -surface ( $\mathbf{v} \cdot \nabla \sigma = 0$ ) when the  $\sigma$ -surface is steady ( $\partial \sigma / \partial t = 0$ ) and material ( $D\sigma / Dt = 0$ ). Hence, we can diagnose the vertical velocity component in terms of the horizontal via

$$w \partial \sigma / \partial z = -\mathbf{u} \cdot \nabla_z \sigma \implies w = \mathbf{u} \cdot \nabla_{\sigma} z, \quad (42.67)$$

where we used the triple product identities (41.34b) and (41.34c) for the final equality. The velocity vector thus takes on the form

$$\mathbf{v} = u [\hat{x} + \hat{z} (\partial z / \partial x)_{\sigma}] + v [\hat{y} + \hat{z} (\partial z / \partial y)_{\sigma}] \quad \text{if } \partial \sigma / \partial t = 0 \text{ and } D\sigma / Dt = 0. \quad (42.68)$$

<sup>1</sup> As discussed in Section 41.7, we can connect these expressions to the contravariant representation of the velocity vector using GVCs.

In this case, the velocity vector is determined only by the horizontal velocity plus the slope of the  $\sigma$  surface.

- NON-STEADY AND MATERIAL  $\sigma$ -SURFACE: Next consider material  $\sigma$  surfaces ( $D\sigma/Dt = 0$ ) that move ( $\partial_t \sigma \neq 0$ ), in which case the velocity vector is

$$\mathbf{v} = u [\hat{\mathbf{x}} + \hat{\mathbf{z}} (\partial z / \partial x)_\sigma] + v [\hat{\mathbf{y}} + \hat{\mathbf{z}} (\partial z / \partial y)_\sigma] + (\partial z / \partial t)_\sigma \hat{\mathbf{z}} \quad D\sigma/Dt = 0. \quad (42.69)$$

To remain on the moving surface, the fluid particle must move vertically by the extra amount  $(\partial z / \partial t)_\sigma \delta t \hat{\mathbf{z}}$  relative to the case of a static  $\sigma$ -surface.

- NON-STEADY AND NON-MATERIAL  $\sigma$ -SURFACE: The general case with a non-material and non-steady  $\sigma$  also requires the dia-surface velocity component,  $w^{(\dot{\sigma})}$ , which is diagnosed based on the material time derivative of  $\sigma$  and the inverse stratification,  $w^{(\dot{\sigma})} = (\partial z / \partial \sigma) D\sigma/Dt$ :

$$\mathbf{v} = u [\hat{\mathbf{x}} + \hat{\mathbf{z}} (\partial z / \partial x)_\sigma] + v [\hat{\mathbf{y}} + \hat{\mathbf{z}} (\partial z / \partial y)_\sigma] + [(\partial z / \partial t)_\sigma + w^{(\dot{\sigma})}] \hat{\mathbf{z}}. \quad (42.70)$$

The contribution  $w^{(\dot{\sigma})}$  measures the vertical motion of the particle relative to the moving  $\sigma$ -surface. Hence, the sum,  $(\partial z / \partial t)_\sigma + w^{(\dot{\sigma})}$ , measures the vertical motion of the particle relative to a fixed origin. As emphasized in Section 42.6, a non-zero  $w^{(\dot{\sigma})}$  arises from motion of the fluid particle relative to the  $\sigma$ -surface, and this relative motion does not necessarily mean that the particle moves; e.g., recall the example discussed in Section 42.6.2 with a static particle and moving  $\sigma$ -surface.

## 42.8 Subduction across the mixed layer base

Consider the generalized vertical coordinate defined according to the mixed layer base as in equation (42.3). The dia-surface mass transport across this surface leads us to define the subduction

$$-\mathcal{S}^{(\text{subduction})} \equiv \rho dA \left[ \frac{D(z - \eta^{(\text{mld})})}{Dt} \right] \quad \text{at } z = \eta^{(\text{mld})}(x, y, t), \quad (42.71)$$

where the mass transport  $\mathcal{S}^{(\text{subduction})}$  (dimensions of mass per time) is positive for fluid moving downward beneath the mixed layer base into the pycnocline (subduction) and negative for water moving into the mixed layer (obduction). The area element  $dA$  is the horizontal projection of the area on the mixed layer base. Expanding the material time derivative leads to

$$-\left[ \frac{\mathcal{S}^{(\text{subduction})}}{\rho dA} \right] = w - [\partial_t + \mathbf{u} \cdot \nabla] \eta^{(\text{mld})} \quad \text{at } z = \eta^{(\text{mld})}(x, y, t), \quad (42.72)$$

where again we define

$$\mathcal{S}^{(\text{subduction})} > 0 \quad \text{subduction} \quad (42.73)$$

$$\mathcal{S}^{(\text{subduction})} < 0 \quad \text{obduction}. \quad (42.74)$$

We illustrate this definition in Figure 42.6, and note that this definition is consistent with that introduced by [Cushman-Roisin \(1987\)](#).

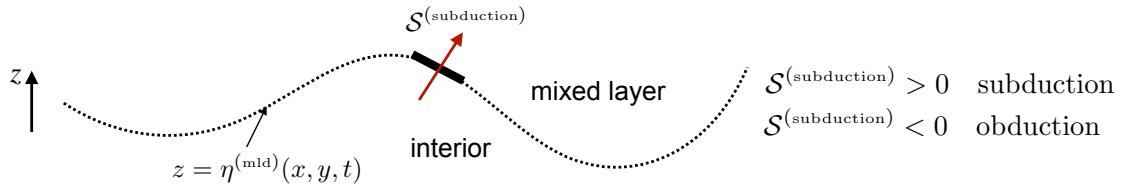


FIGURE 42.6: Illustrating the subduction rate as defined by equation (42.72), which measures the mass transport across the base of the ocean mixed layer. When water enters the ocean interior,  $S^{(\text{subduction})} > 0$ , and we say that water subducts from the mixed layer to the ocean interior. Conversely, when water enters the mixed layer from below,  $S^{(\text{subduction})} < 0$  and we say that water is obducted from the interior to the mixed layer.

## 42.9 Mass continuity

We here derive the Eulerian expression for mass continuity (14.6) using generalized vertical coordinates. We then specialize to incompressible flows, in which mass conservation is converted to volume conservation. To start, recall that mass conservation for a fluid element states that

$$\rho \delta V = \rho \delta x \delta y \delta z = \rho \delta x \delta y z_\sigma \delta \sigma \quad (42.75)$$

is constant following a fluid element.<sup>2</sup> To develop the Eulerian expressions we first consider the case of Cartesian coordinates.

### 42.9.1 Cartesian coordinates

Consider the expression

$$\frac{1}{\rho \delta V} \frac{D(\rho \delta V)}{Dt} = \frac{1}{\rho} \frac{D\rho}{Dt} + \frac{1}{\delta V} \frac{D(\delta V)}{Dt}. \quad (42.76)$$

Now make use of Cartesian coordinates to write the volume

$$\frac{1}{\delta V} \frac{D(\delta V)}{Dt} = \frac{1}{\delta x \delta y \delta z} \frac{D(\delta x \delta y \delta z)}{Dt} \quad (42.77a)$$

$$= \frac{1}{\delta x} \frac{D(\delta x)}{Dt} + \frac{1}{\delta y} \frac{D(\delta y)}{Dt} + \frac{1}{\delta z} \frac{D(\delta z)}{Dt} \quad (42.77b)$$

$$= \frac{\delta u}{\delta x} + \frac{\delta v}{\delta y} + \frac{\delta w}{\delta z} \quad (42.77c)$$

$$= \nabla \cdot \mathbf{v}. \quad (42.77d)$$

Setting  $D(\rho \delta V)/Dt = 0$  leads to the familiar expression for the continuity equation

$$\frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{v}. \quad (42.78)$$

<sup>2</sup>Recall that we write  $\delta$  as an infinitesimal increment following a fluid element.

### 42.9.2 Generalized vertical coordinates

We follow the above procedure but now with generalized vertical coordinates so that

$$\frac{1}{\delta V} \frac{D(\delta V)}{Dt} = \frac{1}{\delta x \delta y z_\sigma \delta \sigma} \frac{D(\delta x \delta y z_\sigma \delta \sigma)}{Dt} \quad (42.79a)$$

$$= \frac{1}{\delta x} \frac{D(\delta x)}{Dt} + \frac{1}{\delta y} \frac{D(\delta y)}{Dt} + \frac{1}{z_\sigma} \frac{D(z_\sigma)}{Dt} + \frac{1}{\delta \sigma} \frac{D(\delta \sigma)}{Dt} \quad (42.79b)$$

$$= \frac{\delta u}{\delta x} + \frac{\delta v}{\delta y} + \frac{1}{z_\sigma} \frac{D(z_\sigma)}{Dt} + \frac{\delta(\dot{\sigma})}{\delta \sigma} \quad (42.79c)$$

$$= \nabla_\sigma \cdot \mathbf{u} + \frac{1}{z_\sigma} \frac{D(z_\sigma)}{Dt} + \frac{\partial \dot{\sigma}}{\partial \sigma} \quad (42.79d)$$

where we introduced the shorthand  $\dot{\sigma} = D\sigma/Dt$ . Note that we set

$$\frac{\delta u}{\delta x} + \frac{\delta v}{\delta y} = \nabla_\sigma \cdot \mathbf{u} \quad (42.80)$$

since we are working with generalized vertical coordinates so that we consider infinitesimal displacements occurring on constant  $\sigma$  surfaces. We are thus led to

$$\frac{1}{\rho \delta V} \frac{D(\rho \delta V)}{Dt} = \nabla_\sigma \cdot \mathbf{u} + \frac{1}{z_\sigma} \frac{Dz_\sigma}{Dt} + \frac{\partial \dot{\sigma}}{\partial \sigma} + \frac{1}{\rho} \frac{D\rho}{Dt} = 0. \quad (42.81)$$

Now use the material time derivative in the form (42.50b) to derive the Eulerian expression of mass conservation

$$\frac{\partial(\rho z_\sigma)}{\partial t} + \nabla_\sigma \cdot (\rho z_\sigma \mathbf{u}) + \frac{\partial(\rho z_\sigma \dot{\sigma})}{\partial \sigma} = 0, \quad (42.82)$$

where the time derivative is computed holding  $\sigma$  fixed. We can furthermore introduce the dia-surface velocity component

$$w^{(\dot{\sigma})} = z_\sigma \dot{\sigma} \quad (42.83)$$

so that mass continuity takes the form

$$\frac{\partial(\rho z_\sigma)}{\partial t} + \nabla_\sigma \cdot (\rho z_\sigma \mathbf{u}) + \frac{\partial(\rho w^{(\dot{\sigma})})}{\partial \sigma} = 0. \quad (42.84)$$

Alternatively, we can reintroduce the material time derivative operator to write the mass continuity equation (42.82) in the form

$$\frac{1}{\rho z_\sigma} \frac{D(\rho z_\sigma)}{Dt} = -(\nabla_\sigma \cdot \mathbf{u} + \partial \dot{\sigma} / \partial \sigma), \quad (42.85)$$

where we used equation (42.50b) to write

$$\frac{D}{Dt} = \left[ \frac{\partial}{\partial t} \right]_\sigma + \mathbf{u} \cdot \nabla_\sigma + \dot{\sigma} \frac{\partial}{\partial \sigma}. \quad (42.86)$$

## 42.10 Layer integrated mass continuity

The formulation thus far has been continuous, with the only assumption made that the specific thickness,  $h = \partial z / \partial \sigma$ , is single signed. We here consider a discrete increment in the generalized

vertical coordinate,

$$\sigma - \delta\sigma/2 \leq \sigma' \leq \sigma + \delta\sigma/2, \quad (42.87)$$

and formulate the mass budget over this layer whose thickness is given by

$$h \equiv \int_{z(\sigma-\delta\sigma/2)}^{z(\sigma+\delta\sigma/2)} dz = \int_{\sigma-\delta\sigma/2}^{\sigma+\delta\sigma/2} \frac{\partial z}{\partial \sigma} d\sigma, \quad (42.88)$$

and whose mass per horizontal area is

$$\delta m = \int_{z(\sigma-\delta\sigma/2)}^{z(\sigma+\delta\sigma/2)} \rho dz = \int_{\sigma-\delta\sigma/2}^{\sigma+\delta\sigma/2} \rho z_\sigma d\sigma = \bar{\rho} h, \quad (42.89)$$

where  $\bar{\rho}$  is the layer averaged density. Note that for Boussinesq fluids the mass per area equals to the layer thickness times the reference density

$$\delta m = \rho_0 h \quad \text{Boussinesq.} \quad (42.90)$$

As defined by equation (42.88) and illustrated in Figure 42.2, the thickness of a layer is relatively large in regions where  $\partial\sigma/\partial z$  is small; i.e., in regions where  $\sigma$  is weakly stratified in the vertical. Conversely, the layer thickness is relatively small where the vertical stratification is large. Furthermore, if the specific thickness is negative, then the layer thickness remains positive by choosing  $\delta\sigma < 0$ . For example, in a stably stratified fluid with  $\sigma$  given by potential density,  $\partial\sigma/\partial z = -(g/\rho_0) N^2 < 0$  so that we take  $\delta\sigma < 0$  to move vertically upward in the water column to regions of lower potential density. The same situation holds when  $\sigma$  is the hydrostatic pressure in which  $\partial p/\partial z = -\rho g$  (Section 42.10.2).

The formulation in this section, and its companion for tracers in Section 42.11, holds across all generalized vertical coordinates, even incorporating the trivial case of geopotential coordinates ( $\sigma = z$ ) whereby the specific thickness is unity. Application of the resulting layer integrated kinematics include the development of discrete equations for numerical layered models (see [Griffies et al. \(2020\)](#) for a review), as well as the shallow water models discussed in Part V of this book.

### 42.10.1 Compressible fluids

Performing a layer integral of the specific thickness equation (42.84) renders

$$\int_{\sigma-\delta\sigma/2}^{\sigma+\delta\sigma/2} \left[ \frac{\partial(\rho z_\sigma)}{\partial t} + \nabla_\sigma \cdot (\rho z_\sigma \mathbf{u}) + \frac{\partial(\rho w^{(\dot{\sigma})})}{\partial \sigma} \right] d\sigma = 0. \quad (42.91)$$

The dia-surface term integrates to a finite difference across the layer

$$\int_{\sigma-\delta\sigma/2}^{\sigma+\delta\sigma/2} \left[ \frac{\partial(\rho z_\sigma)}{\partial t} + \nabla_\sigma \cdot (\rho z_\sigma \mathbf{u}) \right] = -\Delta_\sigma(\rho w^{(\dot{\sigma})}), \quad (42.92)$$

where we introduced the finite difference operator for properties defined at the layer interface

$$\Delta_\sigma(A) = A(\sigma + \delta\sigma/2) - A(\sigma - \delta\sigma/2). \quad (42.93)$$

The time derivative and horizontal space derivative commute with the layer integral, since the limits are specified fixed values for the layer increment,  $\delta\sigma$ , and the derivatives are computed with

$\sigma$  fixed. Hence, layer mass continuity takes the form

$$\left[ \frac{\partial}{\partial t} \right]_{\sigma} \int_{\sigma-\delta\sigma/2}^{\sigma+\delta\sigma/2} \rho z_{\sigma} d\sigma + \nabla_{\sigma} \cdot \int_{\sigma-\delta\sigma/2}^{\sigma+\delta\sigma/2} \rho \mathbf{u} z_{\sigma} d\sigma = -\Delta_{\sigma}(\rho w^{(\dot{\sigma})}). \quad (42.94)$$

The first term involves the layer averaged density times the layer thickness as per equation (42.89). The second term involves the layer averaged density-weighted velocity, which is the layer averaged horizontal mass flux

$$\int_{\sigma-\delta\sigma/2}^{\sigma+\delta\sigma/2} \rho \mathbf{u} z_{\sigma} d\sigma = h \bar{\rho} \bar{\mathbf{u}}. \quad (42.95)$$

We are thus led to the layer integrated continuity equation

$$\left[ \frac{\partial(h \bar{\rho})}{\partial t} \right]_{\sigma} + \nabla_{\sigma} \cdot (h \bar{\rho} \bar{\mathbf{u}}) + \Delta_{\sigma}(\rho w^{(\dot{\sigma})}) = 0. \quad (42.96)$$

When evolving the fields in a discrete numerical model, we have information only about layer averaged fields. So how do we estimate the depth average of the horizontal advective flux,  $\bar{\rho} \bar{\mathbf{u}}$ , appearing in equation (42.96)? One method interprets all fields as their layer averaged values so that  $\bar{\rho} \bar{\mathbf{u}} = \bar{\rho} \bar{\mathbf{u}}$ , thus considering uncomputed sub-layer correlations  $\bar{\rho}' \bar{\mathbf{u}'}$  as part of the truncation error. Alternately, we note that compressible hydrostatic flows can be described by a pressure-based vertical coordinate in which case the layer mass per horizontal area is proportional to a prescribed increment in pressure

$$\delta m = \int_{\sigma-\delta\sigma/2}^{\sigma+\delta\sigma/2} \rho z_{\sigma} d\sigma = \bar{\rho} h = -g^{-1} \delta p. \quad (42.97)$$

Correspondingly, the layer integrated horizontal mass flux equals to the mass increment times the pressure-layer averaged velocity

$$\int_{\sigma-\delta\sigma/2}^{\sigma+\delta\sigma/2} \rho \mathbf{u} z_{\sigma} d\sigma = -g^{-1} \int_{p-\delta p/2}^{p+\delta p/2} \mathbf{u} dp = -g^{-1} \bar{\mathbf{u}} \delta p = h \bar{\rho} \bar{\mathbf{u}}. \quad (42.98)$$

With either of the above two methods, we are led to the same layer integrated continuity equation, which we write in the generic form that drops overbars

$$\left[ \frac{\partial(h \rho)}{\partial t} \right]_{\sigma} + \nabla_{\sigma} \cdot (h \rho \mathbf{u}) + \Delta_{\sigma}(\rho w^{(\dot{\sigma})}) = 0. \quad (42.99)$$

We illustrate contributions to this layer mass budget in Figure 42.7.

### 42.10.2 Mass continuity using pressure coordinates

Let us here consider in some detail the special case of pressure coordinates in a hydrostatic fluid, and thus derive mass continuity using these coordinates.

#### *Method I*

The thickness of a hydrostatic pressure layer (equation (42.88)) takes on the following form

$$h = \int_{p-\delta p/2}^{p+\delta p/2} \frac{\partial z}{\partial p} dp = - \int_{p-\delta p/2}^{p+\delta p/2} \frac{dp}{\rho g}, \quad (42.100)$$

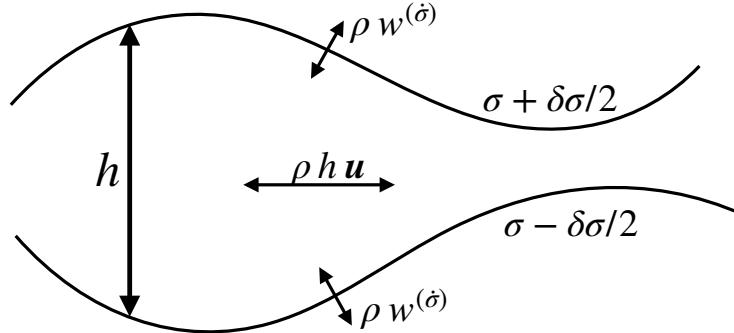


FIGURE 42.7: Illustrating the terms contributing to changes in layer mass according to the layer integrated continuity equation (42.99). The discrete layer is shown here with bounding interfaces at  $\sigma - \delta\sigma/2$  and  $\sigma + \delta\sigma/2$ . Within a layer there is a horizontal redistribution due to horizontal advective transport. Additionally, matter can cross the layer due to dia-surface transport via  $w^{(\delta)}$ .

so that its mass per unit area is

$$\int_{p-\delta p/2}^{p+\delta p/2} \rho \frac{\partial z}{\partial p} dp = -\delta p/g. \quad (42.101)$$

The mass continuity equation (42.99) thus becomes

$$\frac{\partial(\delta p)}{\partial t} + \nabla_p \cdot (\mathbf{u} \delta p) + \Delta_p (\dot{p}) = 0. \quad (42.102)$$

The partial time derivative vanishes since it is computed by holding pressure fixed so that the pressure increment has a zero time tendency

$$\left[ \frac{\partial(\delta p)}{\partial t} \right]_p = 0. \quad (42.103)$$

Likewise,  $\nabla_p(\delta p) = 0$ . Thus, we can divide by  $\delta p$  to render the continuity equation

$$\nabla_p \cdot \mathbf{u} + \frac{\partial \dot{p}}{\partial p} = 0 \quad \text{compressible hydrostatic.} \quad (42.104)$$

This equation is isomorphic to the incompressible continuity equation (for both hydrostatic and non-hydrostatic fluids) written using geopotential coordinates

$$\nabla_z \cdot \mathbf{u} + \frac{\partial \dot{z}}{\partial z} = \nabla_z \cdot \mathbf{u} + \frac{\partial w}{\partial z} 0 \quad \text{incompressible,} \quad (42.105)$$

where  $w = \dot{z}$  is the vertical component to the velocity vector. For both compressible pressure coordinates and incompressible depth coordinates, the continuity equation is a diagnostic relation (i.e., no time derivatives) rather than prognostic (i.e., containing time derivatives).

### Method II

For the second method we make use of the approach detailed in Section 42.9.2, which starts from

$$\frac{D(\rho \delta V)}{Dt} = 0. \quad (42.106)$$

In pressure coordinates the volume of the fluid element takes the form

$$\delta V = \delta x \delta y \delta z = \delta x \delta y \left[ \frac{\partial z}{\partial p} \right] \delta p = -(\rho g)^{-1} \delta x \delta y \delta p. \quad (42.107)$$

Consequently,

$$0 = \frac{D(\rho \delta V)}{Dt} = g^{-1} \left( \frac{D(\delta x \delta y \delta p)}{Dt} \right), \quad (42.108)$$

so that

$$0 = \frac{1}{\delta x \delta y \delta p} \left( \frac{D(\delta x \delta y \delta p)}{Dt} \right) = \nabla_p \cdot \mathbf{u} + \frac{\partial p}{\partial p}. \quad (42.109)$$

The second step made use of the isomorphism between this result and that for equation (13.73) that holds for a geopotential vertical coordinate.

### 42.10.3 Incompressible flow

Specializing to an incompressible volume conserving flow (see Chapters 16 and 23) yields the incompressible layer thickness equation

$$\frac{\partial h}{\partial t} + \nabla_\sigma \cdot (h \mathbf{u}) + \Delta_\sigma w^{(\dot{\sigma})} = 0. \quad (42.110)$$

Further specializing to the case of zero dia-surface transport leads to

$$\frac{\partial h}{\partial t} + \nabla_\sigma \cdot (h \mathbf{u}) = 0 \quad \text{no dia-surface transport.} \quad (42.111)$$

This case is commonly studied for adiabatic fluids using isopycnal coordinates, in which isopycnal surfaces are material (Section 44.1).

### 42.10.4 Rescaled geopotential coordinates

The rescaled geopotential coordinate

$$z^* = \frac{H(z - \eta)}{H + \eta} = \frac{\eta_b(z - \eta)}{\eta_b - \eta} \quad \text{and} \quad \eta_b(x, y) \leq z^* \leq 0, \quad (42.112)$$

is commonly used in Boussinesq ocean models, where  $z = \eta(x, y, t)$  is the ocean free surface and  $z = \eta_b(x, y) = -H(x, y)$  is the ocean bottom. The thickness of a coordinate layer is given by

$$h = dz = \frac{\partial z}{\partial z^*} dz^* = (1 + \eta/H) dz^* = (1 - \eta/\eta_b) dz^*. \quad (42.113)$$

The depth integrated column thickness and depth integrated coordinate thickness are given by

$$\int_{\eta_b}^{\eta} dz = \eta - \eta_b = \eta + H \quad \text{and} \quad \int_{z^*(\eta_b)}^{z^*(\eta)} dz^* = -\eta_b = H. \quad (42.114)$$

Correspondingly, the depth integrated thickness equation is given by the depth integrated volume budget derived in Section 16.3

$$\frac{\partial \eta}{\partial t} + \nabla \cdot \mathbf{U} + [w_{z^*=0}^{(\dot{\sigma})} - w_{z^*=\eta_b}^{(\dot{\sigma})}] = 0. \quad (42.115)$$

We assume no volume flow through the ocean bottom so that  $w_{z^*=\eta_b}^{(\dot{\sigma})} = 0$ , whereas

$$-\rho_0 w_{z^*=0}^{(\dot{\sigma})} = Q_m \quad (42.116)$$

is the mass flux crossing the ocean free surface (Section 14.4.3).

## 42.11 Layer integrated tracer equation

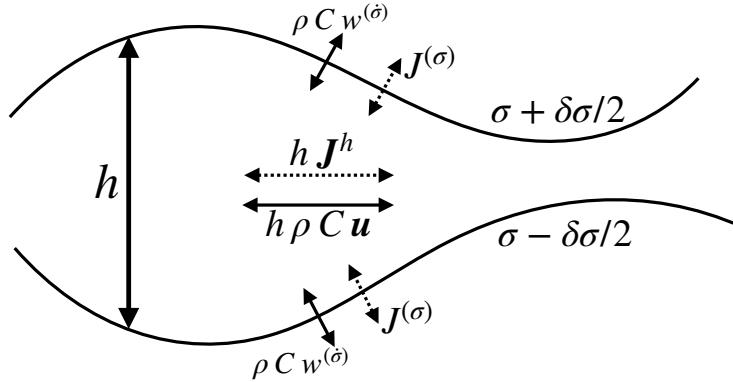


FIGURE 42.8: Illustrating the terms contributing to changes in layer tracer content according to the layer integrated tracer equation (42.121). The layer is shown here with bounding interfaces at  $\sigma - \delta\sigma/2$  and  $\sigma + \delta\sigma/2$ . Within a layer there is a redistribution of tracer due to horizontal advective and subgrid scale tracer fluxes. Additionally, matter can cross the layer due to dia-surface transport via  $\rho C w^{(\dot{\sigma})}$  and subgrid tracer transport  $J^{(\sigma)}$ .

The tracer equation from Section 15.1.3 is given by

$$\rho \frac{DC}{Dt} = -\nabla \cdot \mathbf{J}, \quad (42.117)$$

where  $\mathbf{J}$  is a subgrid scale flux. Now introduce the material time derivative operator in the form (42.50b) to have

$$\rho \left[ \frac{\partial C}{\partial t} + \mathbf{u} \cdot \nabla_\sigma C + \dot{\sigma} \partial_\sigma C \right] = -\nabla \cdot \mathbf{J}, \quad (42.118)$$

Multiplying by the specific thickness and making use of the mass conservation equation (42.84) renders the flux-form Eulerian equation

$$\frac{\partial(z_\sigma \rho C)}{\partial t} + \nabla_\sigma \cdot (z_\sigma \rho C \mathbf{u}) + \frac{\partial(\rho C w^{(\dot{\sigma})})}{\partial \sigma} = - \left[ \nabla_\sigma \cdot (z_\sigma \mathbf{J}^h) + \frac{\partial(z_\sigma \nabla_\sigma \cdot \mathbf{J})}{\partial \sigma} \right], \quad (42.119)$$

where we made use of expression (41.91) for the subgrid scale operator. Now perform a layer integral as detailed in Section 42.10 and use the layer mass continuity equation (42.99) to yield the layer integrated tracer equation

$$\frac{\partial(h \rho C)}{\partial t} + \nabla_\sigma \cdot (h \rho C \mathbf{u}) + \Delta_\sigma(\rho C w^{(\dot{\sigma})}) = - \left[ \nabla_\sigma \cdot (h \mathbf{J}^h) + \Delta_\sigma(z_\sigma \nabla_\sigma \cdot \mathbf{J}) \right]. \quad (42.120)$$

Alternatively, we can bring all terms to the left hand side to yield

$$\frac{\partial(h \rho C)}{\partial t} + \nabla_\sigma \cdot (h \rho C \mathbf{u} + h \mathbf{J}^h) + \Delta_\sigma(\rho C w^{(\dot{\sigma})} + J^{(\sigma)}) = 0 \quad (42.121)$$

where we wrote

$$J^{(\sigma)} = z_\sigma \nabla \sigma \cdot \mathbf{J}. \quad (42.122)$$

We illustrate contributions to the layer tracer budget (42.121) in Figure 42.8. Note that we interpret these layer integrated fields and fluxes as per the discussion in Section 42.10.1.



# Chapter 43

## Dynamical equations

In this chapter we derive the dynamical equations for momentum, vorticity, and potential vorticity using generalized vertical coordinates. These equations provide the foundations for many numerical models of the atmosphere and ocean. Besides being essential for developing methods for numerical simulations, understanding the physical and mathematical basis of these equations supports the analysis of simulations.

### READER'S GUIDE TO THIS CHAPTER

We assume a working knowledge of the mathematics of generalized vertical coordinates as detailed in Chapter 41 and the corresponding kinematics in Chapter 42. We make particular use of the layer integrated notions introduced for mass continuity and the tracer equations in Sections 42.10 and 42.11. We also make use of the dynamical equations derived in Chapter 17. For most purposes in this chapter we find Cartesian horizontal coordinates sufficient. However, we note some places where spherical coordinates warrant special consideration.

43.1	Equations of motion . . . . .	<b>1068</b>
43.1.1	Notation . . . . .	1068
43.1.2	Mass and tracer equations . . . . .	1068
43.1.3	Momentum equation . . . . .	1068
43.1.4	Eulerian flux-form horizontal momentum equation . . . . .	1069
43.1.5	Vector-invariant horizontal momentum equation . . . . .	1069
43.1.6	Hydrostatic balance with constant gravitational acceleration . . . . .	1070
43.2	Concerning the pressure force . . . . .	<b>1071</b>
43.2.1	Computing the horizontal pressure gradient . . . . .	1071
43.2.2	Integrated pressure force on the cell faces . . . . .	1072
43.2.3	Net vertical pressure force . . . . .	1073
43.2.4	Net horizontal pressure force . . . . .	1073
43.2.5	Comments . . . . .	1073
43.3	Hydrostatic vorticity and potential vorticity . . . . .	<b>1074</b>
43.3.1	Basic manipulations . . . . .	1074
43.3.2	Vorticity and potential vorticity equation . . . . .	1075
43.3.3	Boussinesq fluid . . . . .	1076
43.4	Exercise . . . . .	<b>1076</b>

## 43.1 Equations of motion

We here derive the equations of motion based on generalized vertical coordinates. The scalar equations were already discussed in Sections 42.9, 42.10, and 42.11, so our main focus concerns the momentum equation.

### 43.1.1 Notation

For much of this chapter we focus on the continuous formulation of the generalized vertical coordinates. Following the discussion in Section 42.3, we encounter the specific thickness throughout the equations

$$h = \frac{\partial z}{\partial \sigma} = z_\sigma. \quad (43.1)$$

Using this notation we write the dia-surface transport velocity as

$$w^{(\dot{\sigma})} = \frac{\partial z}{\partial \sigma} \dot{\sigma} = h \dot{\sigma}, \quad (43.2)$$

and the dia-surface advection operator is

$$w^{(\dot{\sigma})} \partial_z = \dot{\sigma} \partial_\sigma. \quad (43.3)$$

### 43.1.2 Mass and tracer equations

The mass and tracer equations were derived in Sections 42.9, 42.10, and 42.11, with their continuous vertical coordinate formulation given by

$$\frac{\partial(\rho h)}{\partial t} + \nabla_\sigma \cdot (\rho h \mathbf{u}) + \partial_\sigma(\rho h \dot{\sigma}) = 0 \quad (43.4a)$$

$$\frac{\partial(h \rho C)}{\partial t} + \nabla_\sigma \cdot (h \rho C \mathbf{u} + h \mathbf{J}^h) + \partial_\sigma(\rho h \dot{\sigma} C + h \nabla_\sigma \cdot \mathbf{J}) = 0. \quad (43.4b)$$

Compatibility is maintained between the mass continuity equation (43.4a) and the tracer equation (43.4b) so long as the tracer equation reduces to the mass equation upon setting the tracer concentration to a spatial constant. Hence, for compatibility we must have the subgrid fluxes,  $\mathbf{J}$ , vanish when the tracer is a spatial constant. For example, diffusive fluxes, which are proportional to the tracer gradient, respect this constraint. These properties originate from our discussion of mass budgets and the barycentric velocity in Section 15.1.

### 43.1.3 Momentum equation

From Section 21.9, the horizontal and vertical components to the momentum equation are

$$\rho \frac{D\mathbf{u}}{Dt} + 2\rho \boldsymbol{\Omega} \times \mathbf{u} = -\rho \nabla_z \Phi - \nabla_z p + \rho \mathbf{F}^h \quad (43.5a)$$

$$\rho \frac{Dw}{Dt} = -\rho \frac{\partial \Phi}{\partial z} - \frac{\partial p}{\partial z} + \rho F^z. \quad (43.5b)$$

For the simple form of the geopotential,  $\Phi = g z$  (Section 9.12), so that the horizontal gradient of the geopotential vanishes

$$\Phi = g z \implies \nabla_z \Phi = 0. \quad (43.6)$$

This gradient is nonzero in the presence of astronomical tide forcing (Chapter 28).

*Horizontal momentum equation*

We transform the horizontal derivatives from geopotential coordinates to generalized vertical coordinates according to (see equation (41.73))

$$\nabla_z = \nabla_\sigma - (\nabla_\sigma z) \partial_z \quad (43.7)$$

thus leading to the horizontal momentum equation

$$\rho \frac{D\mathbf{u}}{Dt} + 2\rho \boldsymbol{\Omega} \times \mathbf{u} = -\rho [\nabla_\sigma - (\nabla_\sigma z) \partial_z] \Phi - [\nabla_\sigma - (\nabla_\sigma z) \partial_z] p + \rho \mathbf{F}^h. \quad (43.8)$$

In Section 43.1.6 we present some special cases for this equation that simplify the pressure and geopotential terms.

*Vertical momentum equation*

The vertical momentum equation is transformed into

$$\rho \frac{Dw}{Dt} = -\frac{\partial \sigma}{\partial z} \left[ \rho \frac{\partial \Phi}{\partial \sigma} + \frac{\partial p}{\partial \sigma} \right] + \rho F^z, \quad (43.9)$$

with the hydrostatic form given by

$$\frac{\partial p}{\partial \sigma} = -\rho \frac{\partial \Phi}{\partial \sigma}. \quad (43.10)$$

**43.1.4 Eulerian flux-form horizontal momentum equation**

Using Cartesian horizontal coordinates and generalized vertical coordinates, the horizontal momentum equation includes a contribution from the acceleration that has a form similar to that for a tracer (Section 42.11)

$$\hbar \rho \frac{Du}{Dt} = \left[ \frac{\partial(\hbar \rho u)}{\partial t} \right]_\sigma + \nabla_\sigma \cdot (\hbar \rho u \mathbf{u}) + \partial_\sigma(\hbar \rho u \dot{\sigma}) \quad (43.11a)$$

$$\hbar \rho \frac{Dv}{Dt} = \left[ \frac{\partial(\hbar \rho v)}{\partial t} \right]_\sigma + \nabla_\sigma \cdot (\hbar \rho v \mathbf{u}) + \partial_\sigma(\hbar \rho v \dot{\sigma}). \quad (43.11b)$$

We provide a  $\sigma$  subscript on the time derivative operator to signal that this derivative is taken with  $\sigma$  held fixed. With spherical coordinates there are additional metric terms appearing on the right hand side, as detailed in Section 17.2.1. In particular, there is a metric term that contains the vertical velocity component,  $w = Dz/Dt$ . The appearance of  $w$  is awkward since the vertical velocity is not naturally computed using generalized vertical coordinates. This limitation is overcome through use of the vector-invariant velocity equation derived in Section 43.1.5.

**43.1.5 Vector-invariant horizontal momentum equation**

As noted in Section 17.2.2, the *vector-invariant* form of the momentum equation eliminates the metric terms that appear in the non-Cartesian flux-form equations. The vector-invariant form is also suited for deriving the vorticity equation (see Section 43.3). Here, we start with the material time derivative in the form (42.50c) appropriate for generalized vertical coordinates, in which case

the horizontal acceleration is given by

$$\frac{D\mathbf{u}}{Dt} = \left[ \frac{\partial \mathbf{u}}{\partial t} \right]_{\sigma} + (\mathbf{u} \cdot \nabla_{\sigma}) \mathbf{u} + (\dot{\sigma} \partial_{\sigma}) \mathbf{u}. \quad (43.12)$$

Now make use of the vector identity (see Section 2.3.4)

$$(\mathbf{u} \cdot \nabla_{\sigma}) \mathbf{u} = \nabla_{\sigma} K + (\nabla_{\sigma} \times \mathbf{u}) \times \mathbf{u}, \quad (43.13)$$

where

$$K = \mathbf{u} \cdot \mathbf{u} / 2 \quad (43.14)$$

is the kinetic energy per mass of the horizontal flow. Introducing the GVC version of the relative vorticity (see Section 44.2.1)

$$\tilde{\zeta} \equiv \hat{\mathbf{z}} \cdot (\nabla_{\sigma} \times \mathbf{u}) = \left[ \frac{\partial v}{\partial x} \right]_{\sigma} - \left[ \frac{\partial u}{\partial y} \right]_{\sigma} \quad (43.15)$$

renders

$$\frac{D\mathbf{u}}{Dt} = \left[ \frac{\partial \mathbf{u}}{\partial t} \right]_{\sigma} + \nabla_{\sigma} K + \tilde{\zeta} \hat{\mathbf{z}} \times \mathbf{u} + \dot{\sigma} \partial_{\sigma} \mathbf{u}, \quad (43.16)$$

so that the horizontal momentum equation takes the form

$$\left[ \frac{\partial \mathbf{u}}{\partial t} \right]_{\sigma} + \dot{\sigma} \frac{\partial \mathbf{u}}{\partial \sigma} + (2 \boldsymbol{\Omega} + \hat{\mathbf{z}} \tilde{\zeta}) \times \mathbf{u} = -\nabla_{\sigma} K - \nabla_z \Phi - (1/\rho) \nabla_z p + \mathbf{F}^h, \quad (43.17)$$

where again  $\nabla_z = \nabla_{\sigma} - (\nabla_{\sigma} z) \partial_z$  as per equation (43.7). This equation is form-invariant regardless the horizontal coordinates, thus motivating the name *vector-invariant*.<sup>1</sup>

### 43.1.6 Hydrostatic balance with constant gravitational acceleration

There are many special cases that simplify various terms in the momentum equation. For example, when considering a geopotential in the form  $\Phi = g z$  (Section 9.12) with  $g$  assumed to be a constant effective gravitational acceleration, then the horizontal momentum equation (43.8) becomes

$$\rho \frac{D\mathbf{u}}{Dt} + 2\rho \boldsymbol{\Omega} \times \mathbf{u} = -[\nabla_{\sigma} - (\nabla_{\sigma} z) \partial_z] p + \rho \mathbf{F}^h. \quad (43.18)$$

Furthermore, assuming an approximate hydrostatic balance (and corresponding simplification of the Coriolis acceleration as per Section 22.1.3) allows us to write  $\partial p / \partial z = -g \rho$  so that

$$\rho \frac{D\mathbf{u}}{Dt} + \rho f \hat{\mathbf{z}} \times \mathbf{u} = -[\nabla_{\sigma} p + \rho \nabla_{\sigma} \Phi] + \rho \mathbf{F}^h, \quad (43.19)$$

which also takes on the vector-invariant form

$$\left[ \frac{\partial \mathbf{u}}{\partial t} \right]_{\sigma} + \dot{\sigma} \frac{\partial \mathbf{u}}{\partial \sigma} + (f + \tilde{\zeta}) \hat{\mathbf{z}} \times \mathbf{u} = -\nabla_{\sigma} (K + \Phi) - (1/\rho) \nabla_{\sigma} p + \rho \mathbf{F}^h. \quad (43.20)$$

This form is commonly used for hydrostatic models of the ocean and atmosphere, such as discussed in [Griffies et al. \(2020\)](#).

<sup>1</sup>See Section 4.4.4 of [Griffies \(2004\)](#) for a detailed derivation using arbitrary horizontal coordinates.

## 43.2 Concerning the pressure force

As seen in Section 18.1.3, the pressure force acting on a fluid region is given by the integral

$$\mathbf{F}^{\text{pressure}} = - \oint_{\partial\mathcal{R}} p \hat{\mathbf{n}} d\mathcal{S} = - \int_{\mathcal{R}} \nabla p dV, \quad (43.21)$$

where the second equality follows from Gauss's divergence theorem applied to a scalar field (Section 2.7.2). We refer to the right-most expression as the pressure gradient body force, and this expression is the basis for the discussion in Sections 43.1.6 and 43.2.1. In this formulation, the pressure force at a point is oriented down the pressure gradient, so that the net pressure force acting on a region is the volume integral of pressure gradient.

The middle expression in equation (43.21) formulates the pressure force as the area integrated pressure contact force acting on the region boundaries. In this form, the pressure acting on a region is computed as the integral of pressure over the area bounding the region, with the orientation determined by the inward normal at each point on the boundary. Much of this section is concerned with the contact force expression as a basis for computing the pressure force acting on a finite region as shown in Figure 43.2. The contact force perspective was taken by [Lin \(1997\)](#) and [Adcroft et al. \(2008\)](#) in their finite volume approach to computing the pressure force acting on a numerical model grid cell.

### 43.2.1 Computing the horizontal pressure gradient

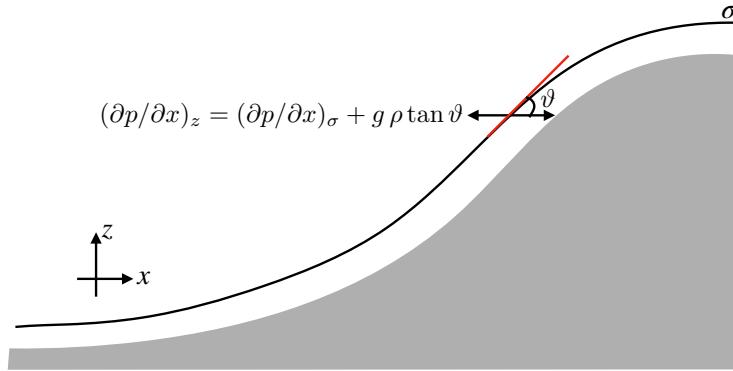


FIGURE 43.1: Illustrating how the horizontal pressure gradient is decomposed into two terms, one aligned with the surface of constant  $\sigma$ , and another associated with the slope of the  $\sigma$ -surface relative to the horizontal,  $\tan \vartheta = (\partial z / \partial x)_{\sigma}$ . We here consider the decomposition using terrain following vertical coordinates, where the vertical coordinate is aligned according to the solid-earth bottom (shaded region). Specifically, for terrain following ocean models we have  $\sigma = (z - \eta) / (-\eta_b + \eta)$ , where  $z = \eta(x, y, t)$  is the ocean free surface and  $z = \eta_b(x, y)$  is the ocean bottom. Terrain-following atmospheric have a similar definition, often using pressure rather than geopotential so that  $\sigma = (p - p_a) / (p_b - p_a)$ , where  $p$  is the pressure,  $p_a = p_a(x, y, t)$  is the pressure applied at the top of the atmosphere (often assumed to be zero), and  $p_b = p_b(x, y, t)$  is the pressure at the bottom of the atmosphere.

The horizontal pressure gradient is aligned perpendicular to the local gravitational direction. It is generally among the dominant horizontal forces acting on a fluid element. Hence, its accurate representation in numerical models is crucial for the physical integrity of a simulation. Unfortunately, decomposition of the horizontal pressure gradient into two terms according to the transformation (43.7) can lead to numerical difficulties. For example, with a simple geopotential and a hydrostatic fluid, equation (43.19) shows that the horizontal pressure gradient takes the

form

$$\nabla_z p = \nabla_\sigma p + \rho \nabla_\sigma \Phi = \nabla_\sigma p + g \rho \nabla_\sigma z, \quad (43.22)$$

with this decomposition illustrated in Figure 43.1 for the case of terrain following vertical coordinates. Numerical difficulties occur when the two terms on the right hand side have comparable magnitude but distinct signs. We are thus confronted with computing the small difference between two large numbers, and that situation generally exposes a numerical simulation to nontrivial truncation errors. Unfortunately, these errors can corrupt the integrity of the computed pressure forces and in turn contribute to spurious flow. An overview of this issue for ocean models is given by [Haney \(1991\)](#), [Mellor et al. \(1998\)](#), [Griffies et al. \(2000\)](#), with advances offered by [Lin \(1997\)](#), [Shchepetkin and McWilliams \(2002\)](#), and [Adcroft et al. \(2008\)](#). In the remainder of this section, we outline a finite volume method for computing the pressure force as proposed by [Lin \(1997\)](#) for atmospheric models and [Adcroft et al. \(2008\)](#) for ocean models. This approach starts from the middle expression in equation (43.21) for the pressure force; i.e., it formulates the pressure force as the area integral of the pressure contact force rather than the volume integral of the pressure gradient force.

### 43.2.2 Integrated pressure force on the cell faces

The inward normal on the grid cell vertical side boundaries points in the horizontal direction. For example, on the left side of Figure 43.2 the pressure force acts in the positive  $\hat{y}$  direction

$$\mathbf{F}_{\text{left}}^{\text{press}} = \hat{y} \int_{\text{left}} p dx dz \quad (43.23)$$

whereas pressure on the right wall acts in the opposite direction

$$\mathbf{F}_{\text{right}}^{\text{press}} = -\hat{y} \int_{\text{right}} p dx dz. \quad (43.24)$$

Similar expressions appear for the front and back vertical boundaries acting in the  $\hat{x}$  direction.

Since the top and bottom boundaries of the grid cell are sloped, there is a pressure force acting on this surface directed in both the horizontal and vertical directions. To unpack the form of this force, write the vertical position of a point on the top interface as  $z = \eta(x, y, t)$  so that the outward normal is given by

$$\hat{\mathbf{n}} = \frac{\nabla(z - \eta)}{|\nabla(z - \eta)|} = \frac{\hat{z} - \nabla\eta}{\sqrt{1 + |\nabla\eta|^2}}. \quad (43.25)$$

Following our discussion of dia-surface transport in Section 42.4.5, we know that the product of the normal direction and the area element can be written

$$\hat{\mathbf{n}} d\mathcal{S} = (\hat{z} - \nabla\eta) dA, \quad (43.26)$$

where  $dA = dx dy$  is the horizontal projection of the area element (see Figure 42.3). Hence, the net pressure force acting on the top face is given by

$$\mathbf{F}_{\text{top}}^{\text{press}} = -\hat{z} \int_{\text{top}} p dx dy + \hat{x} \int_{\text{top}} p (\partial z / \partial x)_\sigma dx dy + \hat{y} \int_{\text{top}} p (\partial z / \partial y)_\sigma dx dy, \quad (43.27)$$

where we set  $z = \eta$  in the second and third terms and placed a  $\sigma$  subscript to emphasize that the horizontal derivative is taken with  $\sigma$  held constant. Notice that the pressure acts in the positive horizontal direction if the top surface slopes upward (surface shoaling) when moving in either of the two horizontal directions. Pressure acting on the bottom face has the same appearance yet

with opposite signs

$$\mathbf{F}_{\text{bott}}^{\text{press}} = \hat{\mathbf{z}} \int_{\text{bott}} p \, dx \, dy - \hat{\mathbf{x}} \int_{\text{bott}} p (\partial z / \partial x)_{\sigma} \, dx \, dy - \hat{\mathbf{y}} \int_{\text{bott}} p (\partial z / \partial y)_{\sigma} \, dx \, dy. \quad (43.28)$$

The pressure acts in the positive horizontal direction if the bottom surface slopes downward (surface deepens) when moving in either of the two horizontal directions. As discussed in Section 18.1.3, the horizontal pressure acting on a sloped surface is known as *form stress*. Here the sloped surface is defined by a constant generalized vertical coordinate.

### 43.2.3 Net vertical pressure force

Bringing the pieces together leads to the net vertical pressure force acting on the grid cell

$$\mathbf{F}_{\text{vertical}}^{\text{press}} = -\hat{\mathbf{z}} \left[ \int_{\text{top}} p \, dx \, dy - \int_{\text{bott}} p \, dx \, dy \right]. \quad (43.29)$$

If the fluid is in hydrostatic balance, then this vertical force is given by the weight of fluid within the cell

$$\mathbf{F}_{\text{vertical}}^{\text{press}} = \hat{\mathbf{z}} M g, \quad (43.30)$$

where  $M$  is the mass of fluid in the grid cell. The net vertical hydrostatic pressure force acts vertically upward since hydrostatic pressure at the cell bottom is greater than at the cell top.

### 43.2.4 Net horizontal pressure force

The net meridional pressure force is given by the forces acting on the sides as well as those acting on the sloped top and bottom boundaries

$$\mathbf{F}_{\text{merid}}^{\text{press}} = \left[ \int_{\text{left}} p \, dx \, dz - \int_{\text{right}} p \, dx \, dz \right] + \left[ \int_{\text{top}} p (\partial z / \partial y)_{\sigma} \, dx \, dy - \int_{\text{bott}} p (\partial z / \partial y)_{\sigma} \, dx \, dy \right]. \quad (43.31)$$

We can write this expression in a more compact form by orienting our integration in a counter-clockwise manner around the cell boundaries, and making use of the identity  $(\partial z / \partial y)_{\sigma} dy = dz$  on the top and bottom faces, so that

$$\mathbf{F}_{\text{merid}}^{\text{press}} = -\oint p \, dx \, dz. \quad (43.32)$$

For some purposes it is more convenient to work with the geopotential,  $\Phi = g z$ , than the pressure. In this case we can write the meridional pressure force as

$$\mathbf{F}_{\text{merid}}^{\text{press}} = -\oint p \, dx \, dz = -\oint dx [d(p z) - z dp] = g^{-1} \oint \Phi \, dx \, dp, \quad (43.33)$$

where  $\oint dx d(p z) = 0$ . This form is useful with compressible / non-Boussinesq models, in which pressure is a natural vertical coordinate (e.g., see the caption to Figure 43.1).

### 43.2.5 Comments

A numerical realization of the integrated contact pressure force requires a representation of pressure along the boundaries of the grid cell. A variety of methods are available with differing accuracies. [Adcroft et al. \(2008\)](#) are notable in proposing an analytic form that allows for an exact integration along the cell faces in special cases, and a highly accurate numerical integration in

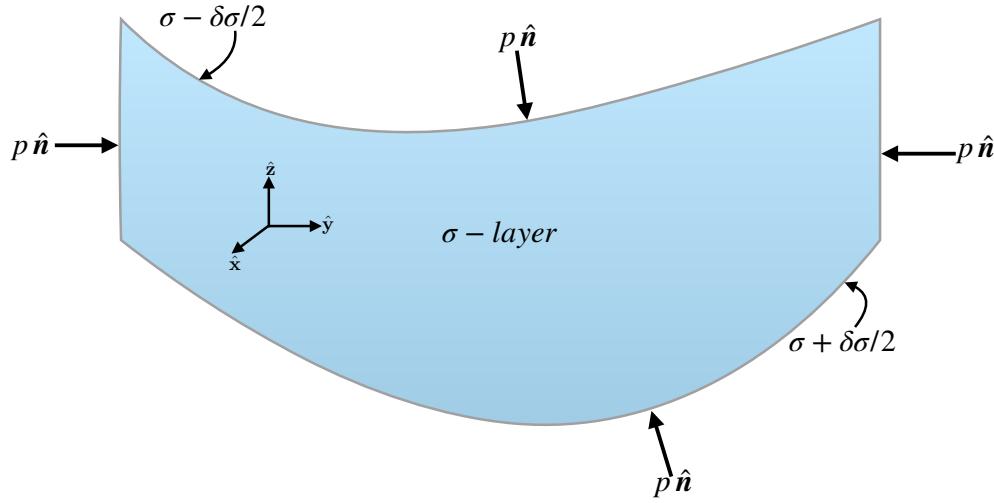


FIGURE 43.2: Schematic of pressure forces acting on the boundaries of a finite region such as a discrete model grid cell. In generalized vertical coordinate models, the side faces are vertical, so that pressure acts only in the horizontal directions. The top and bottom faces are defined by surfaces of constant generalized vertical coordinates with depth  $\sigma(x, y, z, t) = \text{constant}$ . We assume that these surfaces have an outward normal that has a nonzero projection into the vertical so that we can write the depth of a point on these surfaces as  $z = \eta(x, y, t)$ . Because of the slope of the top and bottom surfaces, pressure has both a horizontal and vertical component when acting on these surfaces. The net pressure acting on the grid cell is given by the area integral of the pressures around the grid cell boundary.

other cases. In general, this method for computing pressure forces is highly suited to generalized vertical coordinate grid cells, which was the motivation offered by [Lin \(1997\)](#) in the context of terrain following atmospheric models.

### 43.3 Hydrostatic vorticity and potential vorticity

Generalized vertical coordinates are most commonly used to study hydrostatic fluids. We are thus motivated to develop the equation for the vertical component of vorticity,  $\tilde{\zeta}$ , in a hydrostatic fluid as written using generalized vertical coordinates.

#### 43.3.1 Basic manipulations

Our starting point is the vector-invariant velocity equation given by equation (43.20)

$$\left[ \frac{\partial \mathbf{u}}{\partial t} \right]_\sigma + \dot{\sigma} \frac{\partial \mathbf{u}}{\partial \sigma} + \tilde{\zeta}_a \hat{z} \times \mathbf{u} = -\nabla_\sigma (K + \Phi) - (1/\rho) \nabla_\sigma p + \mathbf{F}^h, \quad (43.34)$$

where  $\tilde{\zeta}_a = \tilde{\zeta} + f$  is the absolute vorticity. Taking the curl of this equation and projecting onto the vertical direction leads to

$$\frac{D\tilde{\zeta}_a}{Dt} = -\tilde{\zeta}_a \nabla_\sigma \cdot \mathbf{u} + \frac{\hat{z} \cdot (\nabla_\sigma \rho \times \nabla_\sigma p)}{\rho^2} + \hat{z} \cdot \left[ \frac{\partial \mathbf{u}}{\partial \sigma} \times \nabla_\sigma \dot{\sigma} + \nabla_\sigma \times \mathbf{F}^h \right] \quad (43.35)$$

where we noted that the planetary vorticity,  $f$ , is independent of time and vertical position.

*Making use of the mass conservation equation*

Mass conservation in the form of equation (42.85)

$$\frac{1}{\rho h} \frac{D(\rho h)}{Dt} = -(\nabla_\sigma \cdot \mathbf{u} + \partial\dot{\sigma}/\partial\sigma), \quad (43.36)$$

renders

$$\rho h \frac{D}{Dt} \left[ \frac{\tilde{\zeta}_a}{\rho h} \right] = \frac{\hat{\mathbf{z}} \cdot (\nabla_\sigma \rho \times \nabla_\sigma p)}{\rho^2} + \tilde{\zeta}_a \frac{\partial \dot{\sigma}}{\partial \sigma} + \hat{\mathbf{z}} \cdot \left[ \frac{\partial \mathbf{u}}{\partial \sigma} \times \nabla_\sigma \dot{\sigma} + \nabla_\sigma \times \mathbf{F}^h \right]. \quad (43.37)$$

*Massaging the  $\dot{\sigma}$  terms*

The terms containing  $\dot{\sigma}$  can be written in the form

$$\tilde{\zeta}_a \partial_\sigma \dot{\sigma} + \hat{\mathbf{z}} \cdot (\partial_\sigma \mathbf{u} \times \nabla_\sigma \dot{\sigma}) = \tilde{\zeta}_a \partial_\sigma \dot{\sigma} + \hat{\mathbf{z}} \cdot [-\nabla_\sigma \times (\dot{\sigma} \partial_\sigma \mathbf{u}) + \dot{\sigma} \nabla_\sigma \times \partial_\sigma \mathbf{u}] \quad (43.38a)$$

$$= \tilde{\zeta}_a \partial_\sigma \dot{\sigma} + \dot{\sigma} \partial_\sigma \tilde{\zeta}_a - \hat{\mathbf{z}} \cdot [\nabla_\sigma \times (\dot{\sigma} \partial_\sigma \mathbf{u})] \quad (43.38b)$$

$$= \partial_\sigma (\dot{\sigma} \tilde{\zeta}_a) - \hat{\mathbf{z}} \cdot [\nabla_\sigma \times (\dot{\sigma} \partial_\sigma \mathbf{u})]. \quad (43.38c)$$

### 43.3.2 Vorticity and potential vorticity equation

The above results allow us to write equation (43.37) in the form

$$\rho h \frac{DQ}{Dt} = \frac{\hat{\mathbf{z}} \cdot (\nabla_\sigma \rho \times \nabla_\sigma p)}{\rho^2} + \partial_\sigma (\dot{\sigma} \tilde{\zeta}_a) + \nabla_\sigma \cdot [\hat{\mathbf{z}} \times \dot{\sigma} \partial_\sigma \mathbf{u} - \hat{\mathbf{z}} \times \mathbf{F}^h], \quad (43.39)$$

where we introduced the potential vorticity defined according to the generalized vertical coordinates

$$Q = \frac{\tilde{\zeta}_a}{h \rho}. \quad (43.40)$$

The potential vorticity equation (43.39) has a generally nonzero baroclinicity contribution (see Section 35.5 for more on baroclinicity)

$$\frac{\hat{\mathbf{z}} \cdot (\nabla_\sigma \rho \times \nabla_\sigma p)}{\rho^2} \quad (43.41)$$

so that the potential vorticity (43.40) is generally not materially invariant even for a perfect fluid.

*Pressure coordinates*

The baroclinicity (43.41) vanishes when choosing  $\sigma = p$ . We already noted this property in our general discussion of baroclinicity in Section 35.5. This choice, however, does not offer us a materially invariant potential vorticity since  $\dot{\sigma} = \dot{p}$  does not generally vanish for a perfect fluid. Namely, a nonzero  $\dot{p}$  merely signals vertical motion, so that  $\dot{p} \neq 0$  for both real and perfect fluids. Hence, even though the baroclinicity vanishes by choosing  $\sigma = p$ , the  $\partial_\sigma (\dot{\sigma} \tilde{\zeta}_a)$  term does not.

*Eulerian flux-form equation*

Expanding the material time derivative in equation (43.39) allows us to cancel the  $\partial_\sigma (\dot{\sigma} \tilde{\zeta}_a)$  term since it appears on both sides of the equation. We are thus led to the Eulerian flux-form potential

vorticity equation written using generalized vertical coordinates

$$\left[ \frac{\partial(\rho h Q)}{\partial t} \right]_\sigma = \frac{\hat{z} \cdot (\nabla_\sigma \rho \times \nabla_\sigma p)}{\rho^2} - \nabla_\sigma \cdot [\rho h \mathbf{u} Q + \hat{z} \times \dot{\sigma} \partial_\sigma \mathbf{u} + \hat{z} \times \mathbf{F}^h], \quad (43.42)$$

which, since  $\tilde{\zeta}_a = h \rho Q$ , is equivalent to the absolute vorticity equation

$$\left[ \frac{\partial \tilde{\zeta}_a}{\partial t} \right]_\sigma = \frac{\hat{z} \cdot (\nabla_\sigma \rho \times \nabla_\sigma p)}{\rho^2} - \nabla_\sigma \cdot [\mathbf{u} \tilde{\zeta}_a + \hat{z} \times \dot{\sigma} \partial_\sigma \mathbf{u} + \hat{z} \times \mathbf{F}^h]. \quad (43.43)$$

As a check, note that setting  $\sigma = z$  so that  $h = 1$  reduces the vorticity equation (43.43) to the vertical component of the vorticity equation (35.32) (see Exercise 43.1).

### 43.3.3 Boussinesq fluid

Recall our discussion of vorticity for the Boussinesq fluid in Section 35.8, where we noted that the vertical component to the absolute vorticity is not affected by baroclinicity. We see this property in the present context by returning to the vector-invariant velocity equation (43.34) and setting the factor  $1/\rho$  multiplying the pressure gradient to  $1/\rho_0$  as part of the Boussinesq approximation

$$(1/\rho) \nabla_\sigma p \longrightarrow (1/\rho_0) \nabla_\sigma p, \quad (43.44)$$

in which  $\rho_0$  is a constant. In this case the  $\nabla_\sigma \times$  operation annihilates pressure and we are left with no vertical component to the baroclinicity. We are thus led to define the Boussinesq potential vorticity

$$Q = \frac{\tilde{\zeta}_a}{h} \quad (43.45)$$

which satisfies the material and Eulerian evolution equations

$$h \frac{DQ}{Dt} = \partial_\sigma(\dot{\sigma} \tilde{\zeta}_a) + \nabla_\sigma \cdot [\hat{z} \times \dot{\sigma} \partial_\sigma \mathbf{u} - \hat{z} \times \mathbf{F}^h] \quad (43.46)$$

$$\left[ \frac{\partial(h Q)}{\partial t} \right]_\sigma = -\nabla_\sigma \cdot [h \mathbf{u} Q + \hat{z} \times \dot{\sigma} \partial_\sigma \mathbf{u} + \hat{z} \times \mathbf{F}^h]. \quad (43.47)$$

If we choose a vertical coordinate that vanishes when there is no mixing, then this potential vorticity is materially invariant for a perfect fluid. The most common choice for this vertical coordinate is buoyancy or potential density, with the corresponding potential vorticity developed in Sections 44.2 and 44.3.

## 43.4 Exercise

### EXERCISE 43.1: CHECKING THE VORTICITY EQUATION

Verify that for  $2\Omega = f\hat{z}$  the choice  $\sigma = z$  reduces the vorticity equation (43.43) to the vertical component of the vorticity equation (35.32).



# Chapter 44

## Isopycnal primitive equations

For stably stratified fluids, buoyancy is a particularly useful generalized vertical coordinate. Most notably, physical processes away from turbulent boundary layers are oriented according to buoyancy surfaces, and horizontal buoyancy gradients give rise to thermal wind shears in a geostrophically balanced flow. For this reason buoyancy (or entropy) plays a key role in theoretical and numerical models of ocean and atmospheric circulation.

In this chapter we study the hydrostatic Boussinesq equations using buoyancy as the vertical coordinate. The resulting primitive equation set forms the basis for *isopycnal* models of the ocean or isentropic models of the atmosphere. We pay particular attention to the needs of vertically integrating the equations over discrete layers, as required to develop discrete numerical models. In the adiabatic limit, the isopycnal equations reduce to the stacked shallow water equations. After deriving the primitive equations using isopycnal coordinates, we derive the corresponding vorticity and potential vorticity equations. Throughout this chapter we expose details for the practitioner interested in the mathematical formalism for the purpose of analyzing ocean momentum, vorticity and potential vorticity budgets using isopycnal models.

### READER'S GUIDE FOR THIS CHAPTER

We assume an understanding of the generalized vertical coordinate mathematics in Chapter 41, kinematics in Chapter 42, and dynamics in Chapter 43. Furthermore, we are concerned with details of vorticity and PV budgets in isopycnal coordinates, with the presentation building from our study of vorticity and potential vorticity in generalized vertical coordinates from Chapter 43.

44.1	Layered isopycnal primitive equations . . . . .	1078
44.1.1	Montgomery potential and the pressure force . . . . .	1078
44.1.2	Material time derivative . . . . .	1080
44.1.3	Layer thickness and specific thickness . . . . .	1080
44.1.4	Ocean equations . . . . .	1081
44.1.5	Vector-invariant horizontal momentum equation . . . . .	1082
44.1.6	Connection to the shallow water equations . . . . .	1083
44.1.7	Diapycnal transfer . . . . .	1083
44.1.8	Momentum transfer . . . . .	1083
44.1.9	Allowing for layers to vanish and reappear . . . . .	1083
44.2	Perfect fluid PV using isopycnal coordinates . . . . .	1084
44.2.1	Derivation of the vorticity equation . . . . .	1084
44.2.2	Derivation of the potential vorticity equation . . . . .	1084

44.2.3	Coordinate transforming vorticity and potential vorticity . . . . .	1085
44.3	Isopycnal coordinate PV with irreversible processes . . . . .	<b>1085</b>
44.3.1	Derivation method I . . . . .	1086
44.3.2	Derivation method II . . . . .	1087
44.3.3	Comments . . . . .	1089

## 44.1 Layered isopycnal primitive equations

Rather than specializing the generalized vertical coordinate equations provided in Section 43.1, we find it pedagogical to start from the equations written using the geopotential vertical coordinate (see Section 23.1.6)

$$\frac{D\mathbf{u}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla_z \varphi + \mathbf{F} \quad \text{horizontal momentum} \quad (44.1a)$$

$$\frac{\partial \varphi}{\partial z} = b \quad \text{hydrostatic} \quad (44.1b)$$

$$\nabla_z \cdot \mathbf{u} + \frac{\partial w}{\partial z} = 0 \quad \text{continuity} \quad (44.1c)$$

$$\frac{Db}{Dt} = \dot{b} \quad \text{thermodynamics} \quad (44.1d)$$

$$\frac{DC}{Dt} = \dot{C} \quad \text{tracers,} \quad (44.1e)$$

where  $\mathbf{v} = (\mathbf{u}, w)$  is the velocity field,  $\mathbf{u}$  is its horizontal component,  $\varphi$  is the dynamic pressure,  $b$  is the buoyancy, and  $C$  is an arbitrary tracer concentration. A discrete realization of the isopycnal layer-integrated form of these equations is depicted in Figure 44.1, with the remainder of this section detailing the formulation using isopycnal coordinates for the vertical.

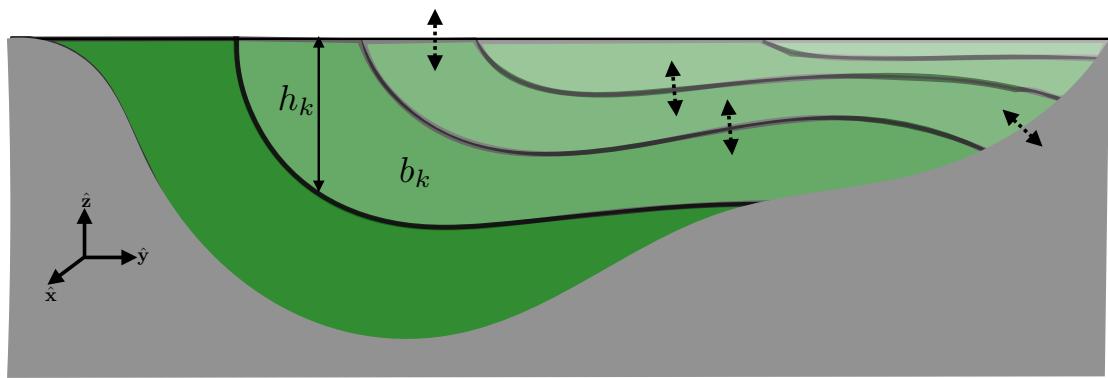


FIGURE 44.1: Schematic of an isopycnal model, formulated as stacked shallow water layers (green layers) that generally allow for the transfer of matter and energy across the layer interfaces as well as across the ocean surface and ocean bottom (as depicted by the double-headed dashed arrows). The dark gray region is land. Discrete layer thicknesses are denoted  $h_k$  with corresponding layer buoyancy,  $b_k$ .

### 44.1.1 Montgomery potential and the pressure force

We here consider the horizontal pressure force appearing in isopycnal models, in which we uncover the importance of the Montgomery potential.

### Horizontal pressure gradient force

Throughout this chapter we make use of the horizontal derivatives on constant buoyancy surfaces (derived in Section 41.12), written here in the form

$$\nabla_b = \hat{\mathbf{x}} \left[ \frac{\partial}{\partial x} \right]_b + \hat{\mathbf{y}} \left[ \frac{\partial}{\partial y} \right]_b. \quad (44.2)$$

Following the discussion in Section 43.1.3, the horizontal pressure thus gradient transforms as

$$\nabla_z \varphi = \nabla_b \varphi - \frac{\partial \varphi}{\partial z} \nabla_b z \quad (44.3a)$$

$$= \nabla_b \varphi - b \nabla_b z \quad (44.3b)$$

$$= \nabla_b (\varphi - b z) \quad (44.3c)$$

$$= \nabla_b M, \quad (44.3d)$$

where

$$M = \varphi - b z \quad (44.4)$$

defines the Montgomery potential. As the contribution to the horizontal pressure force, the Montgomery potential is the geostrophic streamfunction in buoyancy coordinates (see Section 44.1.4).

### The horizontal pressure gradient force for numerical models

It is notable that the horizontal pressure gradient force is determined by the horizontal isopycnal gradient of a single term, the Montgomery potential. Furthermore, as shown below, the Montgomery potential satisfies the buoyancy coordinate form of the hydrostatic balance. Hence, numerical isopycnal models do not suffer from problems with computing the horizontal pressure gradient that can occur with other generalized vertical coordinate models, such as terrain-following models (see Figure 43.1).

Equation (44.3c) is the key step in the formulation, whereby we made use of  $\nabla_b b = 0$ . This step is available only under certain cases that utilize an idealized equation of state for seawater. In more realistic cases, the buoyancy determining the hydrostatic pressure (i.e., the *mass buoyancy*) is defined locally whereas the generalized vertical coordinate must be defined globally. As a result, there are two terms contributing to the pressure gradient in a manner similar to terrain-following models. [Sun et al. \(1999\)](#) and [Hallberg \(2005\)](#) discuss this issue in the context of numerical ocean modeling. For present purposes we ignore this detail and continue to assume a simplified equation of state so that  $\nabla_b b = 0$ .

### Hydrostatic balance

Supporting our use of the Montgomery potential as a pressure field, the hydrostatic balance takes the form

$$\frac{\partial M}{\partial b} = \frac{\partial \varphi}{\partial b} - b \frac{\partial z}{\partial b} - z = \frac{\partial \varphi}{\partial z} \frac{\partial z}{\partial b} - b \frac{\partial z}{\partial b} - z = -z, \quad (44.5)$$

where we made use of the hydrostatic balance  $\partial \varphi / \partial z = b$  (equation (44.1b)). This result means that  $M$  is the buoyancy coordinate version of pressure.

### 44.1.2 Material time derivative

As seen in Section 42.5, there are two equivalent forms for the material time derivative

$$\frac{D}{Dt} = \left[ \frac{\partial}{\partial t} \right]_z + \mathbf{u} \cdot \nabla_z + w \frac{\partial}{\partial z} \quad \text{geopotential form} \quad (44.6a)$$

$$= \left[ \frac{\partial}{\partial t} \right]_b + \mathbf{u} \cdot \nabla_b + w^{(b)} \frac{\partial}{\partial z} \quad \text{isopycnal form,} \quad (44.6b)$$

where

$$w^{(b)} = \frac{\partial z}{\partial b} \frac{Db}{Dt} \quad (44.7)$$

is the diapycnal velocity component that measures the rate of flow crossing buoyancy surfaces (Section 42.4). Besides differences in the spatial operators, it is important to note that the time derivative operators in equations (44.6a) and (44.6b) are computed on constant geopotential and constant buoyancy surfaces, respectively. However, the horizontal velocity component is the *same* for both forms of the material time derivative

$$\mathbf{u} = \hat{\mathbf{x}} u + \hat{\mathbf{y}} v = (D/Dt)(\hat{\mathbf{x}} x + \hat{\mathbf{y}} y). \quad (44.8)$$

### 44.1.3 Layer thickness and specific thickness

The continuity equation,  $\nabla_z \cdot \mathbf{u} + \partial_z w = 0$ , is an expression of volume conservation. We already derived the generalized vertical coordinate version of this equation in Section 42.10.3, and thus quote the isopycnal layer thickness result here

$$\left[ \frac{\partial h}{\partial t} \right]_b + \nabla_b \cdot (h \mathbf{u}) + \Delta_b w^{(b)} = 0. \quad (44.9)$$

The field  $h$  measures the isopycnal layer thickness (dimensions of length) and is given by the vertical integral over a layer

$$h = \int_{z(b-\delta b/2)}^{z(b+\delta b/2)} dz = \int_{b-\delta b/2}^{b+\delta b/2} \frac{\partial z}{\partial b} db = \int_{b-\delta b/2}^{b+\delta b/2} \hbar db = \int_{b-\delta b/2}^{b+\delta b/2} N^{-2} db = \bar{\hbar} db. \quad (44.10)$$

The specific thickness,  $\hbar$ , equals to the inverse squared buoyancy frequency

$$\hbar = \frac{\partial z}{\partial b} = N^{-2}, \quad (44.11)$$

and its layer averaged value is  $\bar{\hbar} = h/\delta b$ . Furthermore, the dia-surface transport velocity is given by

$$w^{(b)} = \hbar \dot{b}. \quad (44.12)$$

Its difference across layer interfaces

$$\Delta_b w^{(b)} = \int_{b-\delta b/2}^{b+\delta b/2} \frac{\partial w^{(b)}}{\partial b} db = w^{(b)}(b + \delta b/2) - w^{(b)}(b - \delta b/2) \quad (44.13)$$

measures the amount of fluid that diverges from the layer through cross-layer transport.

*Specific thickness equation*

Inserting  $h = \bar{h} \delta b$  into the thickness equation (44.9) leads to

$$\left[ \frac{\partial \bar{h}}{\partial t} \right]_b + \nabla_b \cdot (\bar{h} \mathbf{u}) + \partial_b w^{(b)} = 0, \quad (44.14)$$

where we pulled the buoyancy increment,  $\delta b$ , outside of the time and horizontal derivative operators since  $\delta b$  is a fixed number for a chosen layer. We also used the identity relating the difference operator to a differential operator

$$\delta b \partial_b = \Delta_b. \quad (44.15)$$

For a vertically continuous treatment, equation (44.14) can be written with  $h$  rather than the discrete layer averaged value

$$\left[ \frac{\partial h}{\partial t} \right]_b + \nabla_b \cdot (h \mathbf{u}) + \partial_b w^{(b)} = 0. \quad (44.16)$$

It is generally more convenient to use the specific thickness when working with the vertically continuous equations, whereas the finite layer thickness,  $h$ , is more suitable for the layer integrated equations.

*Adiabatic limit*

When  $w^{(b)} \neq 0$ , the three terms in the thickness equation (44.9) or the specific thickness equation (44.14) are coupled. We discussed this coupling in Section 42.6 as part of our broader study of the vertical velocity and the dia-surface velocity. When considering perfect fluids, we can set  $w^{(b)} = h \dot{b} = 0$  since the fluid has no mixing. In this case the layer thickness is altered only through horizontal rearrangements of volume within a layer according to the adiabatic thickness equation

$$\left[ \frac{\partial h}{\partial t} \right]_b + \nabla_b \cdot (h \mathbf{u}) = 0. \quad (44.17)$$

As further discussed in Section 44.1.6, the adiabatic limit brings the discrete isopycnal model into accord with the immiscible stacked shallow water models discussed in Part V of this book.

**44.1.4 Ocean equations**

Bringing the pieces together leads to the isopycnal version of the hydrostatic Boussinesq equations

$$\left[ \frac{\partial \mathbf{u}}{\partial t} \right]_b + (\mathbf{u} \cdot \nabla_b) \mathbf{u} + (w^{(b)} \partial_z) \mathbf{u} + f \hat{z} \times \mathbf{u} = -\nabla_b M + \mathbf{F}^h \quad (44.18a)$$

$$\frac{\partial M}{\partial b} = -z \quad (44.18b)$$

$$\left[ \frac{\partial h}{\partial t} \right]_b + \nabla_b \cdot (h \mathbf{u}) + \Delta_b w^{(b)} = 0 \quad (44.18c)$$

$$\left[ \frac{\partial (h C)}{\partial t} \right]_b + \nabla_b \cdot (h C \mathbf{u} + h \mathbf{J}^h) + \Delta_b (C w^{(b)} + J^{(b)}) = 0, \quad (44.18d)$$

where the tracer equation includes possible subgrid scale flux contributions as well as advective transport. Notice how the advective transport is two-dimensional in the adiabatic case with  $\dot{b} = 0$ ,

in which case layer-integrated scalar properties, such as volume and tracer content, are constant within buoyancy layers. Also note that geostrophic balance in the horizontal momentum equation (44.18a) gives

$$f \hat{z} \times \mathbf{u}_g = -\nabla_b M \implies f u_g = - \left[ \frac{\partial M}{\partial y} \right]_b \quad \text{and} \quad f v_g = \left[ \frac{\partial M}{\partial x} \right]_b. \quad (44.19)$$

Hence, the Montgomery potential is the streamfunction for geostrophic flow as represented using buoyancy coordinates.

#### 44.1.5 Vector-invariant horizontal momentum equation

It is common for isopycnal models to make use of the vector-invariant form of the momentum equation derived in Section 43.1.5. Introducing the isopycnal version of the relative vorticity

$$\hat{z} \tilde{\zeta} \equiv \nabla_b \times \mathbf{u} = \left[ \frac{\partial v}{\partial x} \right]_b - \left[ \frac{\partial u}{\partial y} \right]_b \quad (44.20)$$

renders the vector-invariant horizontal momentum equation

$$\left[ \frac{\partial \mathbf{u}}{\partial t} \right]_b + w^{(b)} \partial_z \mathbf{u} + \tilde{\zeta}_a \hat{z} \times \mathbf{u} = -\nabla_b \mathcal{B} + \mathbf{F}^h, \quad (44.21)$$

where

$$\mathcal{B} = M + \mathbf{u} \cdot \mathbf{u}/2 = \varphi - b z + \mathbf{u} \cdot \mathbf{u}/2 \quad (44.22)$$

is the Bernoulli potential for a hydrostatic Boussinesq fluid (see Section 21.6.2), and

$$\tilde{\zeta}_a = \tilde{\zeta} + f \quad (44.23)$$

is the vertical component to the absolute vorticity using isopycnal coordinates. Note that we can further introduce the isopycnal potential vorticity (Section 44.2.2)

$$h Q = \tilde{\zeta}_a \quad (44.24)$$

to bring the momentum equation to the form

$$\left[ \frac{\partial \mathbf{u}}{\partial t} \right]_b + w^{(b)} \partial_z \mathbf{u} + Q \hat{z} \times (h \mathbf{u}) = -\nabla_b \mathcal{B} + \mathbf{F}^h. \quad (44.25)$$

This form is commonly used as the starting point for certain theoretical analyses, particularly when considering the adiabatic limit in which  $w^{(b)} = 0$ .

### 44.1.6 Connection to the shallow water equations

We can make use of the material time derivative operator (44.6b) to write the material form of the adiabatic and inviscid equations (44.18a)-(44.18c)

$$\frac{D\mathbf{u}}{Dt} + f \hat{\mathbf{z}} \times \mathbf{u} = -\nabla_b M \quad (44.26a)$$

$$\frac{\partial M}{\partial b} = -z \quad (44.26b)$$

$$\frac{Dh}{Dt} + h \nabla_b \cdot \mathbf{u} = 0. \quad (44.26c)$$

These isopycnal momentum and thickness equations are isomorphic to those for a single layer of adiabatic shallow water fluid (see Section 30.2). This isomorphism allows us to derive the vorticity and potential vorticity equations in Section 44.2, making use of the shallow water manipulations from Section 34.4.

### 44.1.7 Diapycnal transfer

At ocean boundaries, the diapycnal term,  $w^{(b)}$ , accounts for the transfer of matter across the ocean boundaries via precipitation, evaporation, ice melt/form, and river runoff. Notably, this matter transfer also generally gives rise to a transfer of trace matter (tracers), heat (evaporation and precipitation carry a heat content), and momentum (precipitation generally has nonzero momentum). In the ocean interior,  $w^{(b)}$  affects the transfer of volume, tracer, and momentum between layers as induced by irreversible processes such as mixing.

### 44.1.8 Momentum transfer

Pressure form stress mechanically couples isopycnal layers even in the absence of diapycnal matter transfer. We discussed the physics of form stress for the shallow water system in Section 31.5 and more generally in Section 19.1. Furthermore, there are a suite of unresolved processes giving rise to lateral and vertical stresses. Typical ocean model treatments incorporate a turbulent friction in the ocean interior, with lateral stresses acting within a layer and diapycnal stresses acting across isopycnal layer interfaces. A bottom drag is typically applied at the ocean bottom and a turbulent stress applied at the ocean surface. Details for the boundary stresses involve the physics of boundary layer turbulence, which is a topic outside of our scope.

### 44.1.9 Allowing for layers to vanish and reappear

Isopycnal layers have a transient existence at any particular horizontal position since a layer can incrop at the ocean bottom and outcrop at the ocean surface (see Figure 44.1). The seasonal cycle of warming and cooling is a canonical example of layer outcropping at the surface ocean. A formulation expedient to handle vanishing layers is to assume that all layers exist everywhere horizontally across the ocean domain, but to allow for zero layer thickness where a layer has zero volume. We made use of this approach when discussing available potential energy in Section 23.8. To admit this feature in a discrete model requires a careful realization of L'Hôpital's rule of differential calculus, thus ensuring the discrete model conserves properties in the presence of layers that can appear and disappear at any particular point in the domain.

## 44.2 Perfect fluid PV using isopycnal coordinates

In Section 36.5, we showed that the absolute vorticity in a Boussinesq hydrostatic fluid with a simplified seawater equation of state (Section 37.3), when projected into the direction normal to constant buoyancy surface,  $\omega_a \cdot \nabla b$ , is not affected by baroclinicity; i.e., that projection annihilates the baroclinicity vector. From that property we conclude that  $\omega_a \cdot \nabla b$  is the potential vorticity for the Boussinesq hydrostatic fluid.

For a Boussinesq hydrostatic fluid, isopycnal coordinates build in the above feature of buoyancy surfaces. Indeed, as shown in Section 43.3.3, the vertical component to baroclinicity vanishes for any generalized vertical coordinate representation of a Boussinesq fluid. Hence, buoyancy coordinates are not special from this perspective. Instead, they are special since in the case of a perfect fluid, the buoyancy based potential vorticity is materially invariant. Deriving this result is one purpose of this section. Note that in Section 43.3, we derived the potential vorticity equation for a hydrostatic fluid represented with generalized vertical coordinates. We could merely specialize that result to the current case. However, we prefer to here work through the maths to help further our experience performing certain of the key manipulations arising with vorticity in rotating and stratified fluids. Hence, consider this section, as well as Section 44.3, to be extended worked exercises.

### 44.2.1 Derivation of the vorticity equation

Acting with the vertical projection of the curl,  $\hat{z} \cdot (\nabla_b \times)$ , onto the adiabatic and inviscid form of the vector-invariant velocity equation (44.21) leads to the isopycnal vorticity equation

$$\left[ \frac{\partial \tilde{\zeta}_a}{\partial t} \right]_b + (\mathbf{u} \cdot \nabla_b) \tilde{\zeta}_a = -\tilde{\zeta}_a \nabla_b \cdot \mathbf{u} \quad (44.27)$$

where

$$\tilde{\zeta}_a = f + \hat{z} \cdot (\nabla_b \times \mathbf{u}) = f + \tilde{\zeta} \quad (44.28)$$

is the absolute vorticity, written as the planetary vorticity plus the isopycnal relative vorticity. The left hand side of equation (44.27) is the material time derivative of absolute vorticity (see equation (44.6b)), so that we can write

$$\frac{D\tilde{\zeta}_a}{Dt} = -\tilde{\zeta}_a \nabla_b \cdot \mathbf{u}. \quad (44.29)$$

As advertised above, there is no baroclinicity vector on the right hand side of this vorticity equation. Again, that property results from our choice to use isopycnal coordinates.

### 44.2.2 Derivation of the potential vorticity equation

We now make use of the thickness equation derived in Section 44.1.3, here realized in its material form to eliminate the convergence  $\nabla_b \cdot \mathbf{u}$  on the right hand side of equation (44.29), thus leading to

$$\frac{D\tilde{\zeta}_a}{Dt} - \frac{\tilde{\zeta}_a}{h} \frac{Dh}{Dt} = 0. \quad (44.30)$$

Introducing the isopycnal potential vorticity

$$Q = \frac{\tilde{\zeta}_a}{h} = \frac{f + \tilde{\zeta}}{h} \quad (44.31)$$

leads to

$$\frac{DQ}{Dt} = 0. \quad (44.32)$$

Expanding the material time derivative into its components according to equation (44.6b), and making use of the adiabatic form of the thickness equation leads to the Eulerian flux-form equation

$$\left[ \frac{\partial(hQ)}{\partial t} \right]_b + \nabla_b \cdot (hQ \mathbf{u}) = 0. \quad (44.33)$$

As noted in Section 44.1.3, when formulating the vertically continuous equations rather than finite thickness layered equations, it is more convenient to make use of the specific thickness,  $\hbar$ , rather than the layer thickness,  $h$ . In this case we are motivated to define the potential vorticity as

$$Q = \frac{\tilde{\zeta}_a}{\hbar} = \frac{f + \tilde{\zeta}}{\hbar}. \quad (44.34)$$

The corresponding PV equation is identical to equation (44.33), only now with  $h$  replaced by  $\hbar$ .

#### 44.2.3 Coordinate transforming vorticity and potential vorticity

As just shown, PV for a hydrostatic Boussinesq fluid can be written in the relatively simple form of a shallow water PV when choosing isopycnal coordinates. Here is a direct transformation from Cartesian to isopyncal coordinates that also reveals this form

$$(\boldsymbol{\omega}^{hy} + f \hat{z}) \cdot \nabla b = -\frac{\partial v}{\partial z} \frac{\partial b}{\partial x} + \frac{\partial u}{\partial z} \frac{\partial b}{\partial y} + \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} + f \right) \frac{\partial b}{\partial z} \quad (44.35a)$$

$$= \frac{\partial b}{\partial z} \left[ f + \left( \frac{\partial v}{\partial x} - \frac{\partial v}{\partial z} \frac{\partial b/\partial x}{\partial b/\partial z} \right) - \left( \frac{\partial u}{\partial y} - \frac{\partial u}{\partial z} \frac{\partial b/\partial y}{\partial b/\partial z} \right) \right] \quad (44.35b)$$

$$= \frac{\partial b}{\partial z} \left[ f + \left( \frac{\partial v}{\partial x} \right)_b - \left( \frac{\partial u}{\partial y} \right)_b \right] \quad (44.35c)$$

$$= \frac{f + (\partial v/\partial x)_b - (\partial u/\partial y)_b}{\partial z/\partial b} \quad (44.35d)$$

$$= \frac{f + \tilde{\zeta}}{\hbar} \quad (44.35e)$$

$$= Q. \quad (44.35f)$$

### 44.3 Isopycnal coordinate PV with irreversible processes

In Section 44.2, we considered the PV equation for an adiabatic, inviscid, hydrostatic, Boussinesq fluid using isopycnal vertical coordinates. We here extend to the case of friction in the momentum equation and diabatic heating in the buoyancy equation. We consider two ways to derive the governing equations. One is to convert the non-hydrostatic PV equation in Exercise 36.2 to isopycnal coordinates, after making the hydrostatic approximation. The second is to start from the equations of motion in isopycnal coordinates and derive the vorticity equation and then the PV equation. We make use of the vertically continuous equations, thus warranting our use of specific thickness,  $\hbar$ , rather than layer thickness,  $h$  (see Section 44.1.3).

Note that much of this section is a specialization of the more general considerations of Section 43.3. Nonetheless, we here revisit some of the earlier derivations as a means to bolster our mathematical manipulation muscle.

### 44.3.1 Derivation method I

As derived earlier in this chapter, the equations of motion with diabatic heating and friction, written using isopycnal (or buoyancy) vertical coordinates, take the form

$$\left[ \frac{\partial \mathbf{u}}{\partial t} \right]_b + (\mathbf{u} \cdot \nabla_b) \mathbf{u} + \dot{b} \frac{\partial \mathbf{u}}{\partial b} + \mathbf{f} \times \mathbf{u} = -\nabla_b M + \mathbf{F} \quad (44.36a)$$

$$\frac{\partial M}{\partial b} = -z \quad (44.36b)$$

$$\left[ \frac{\partial h}{\partial t} \right]_b + \nabla_b \cdot (h \mathbf{u}) = -\frac{\partial (h \dot{b})}{\partial b} \quad (44.36c)$$

$$\frac{D b}{Dt} = \dot{b}. \quad (44.36d)$$

Note that in this section choose to write the dia-surface transport operator in the form

$$w^{(\dot{b})} \partial_z = \dot{b} \partial_b. \quad (44.37)$$

We can make use of the material time derivative operator (44.6b) to write the material form of the equations

$$\frac{D \mathbf{u}}{Dt} + \mathbf{f} \times \mathbf{u} = -\nabla_b M + \mathbf{F} \quad (44.38a)$$

$$\frac{\partial M}{\partial b} = -z \quad (44.38b)$$

$$\frac{D h}{Dt} + h \nabla_b \cdot \mathbf{u} = -h \frac{\partial \dot{b}}{\partial b}. \quad (44.38c)$$

#### Curl of the velocity equation

We start taking the curl,  $\nabla_b \times$ , of the velocity equation (44.36a), thus leading to the isopycnal vorticity equation

$$\left[ \frac{\partial \tilde{\zeta}_a}{\partial t} \right]_b + (\mathbf{u} \cdot \nabla_b) \tilde{\zeta}_a + \dot{b} \left[ \frac{\partial \tilde{\zeta}_a}{\partial b} \right] = -\tilde{\zeta}_a \nabla_b \cdot \mathbf{u} + \hat{z} \cdot \left[ \frac{\partial \mathbf{u}}{\partial b} \times \nabla_b \dot{b} + \nabla_b \times \mathbf{F} \right]. \quad (44.39)$$

The left hand side of equation (44.39) is the material time derivative of absolute vorticity (see equation (44.6b)), so that

$$\frac{D \tilde{\zeta}_a}{Dt} = -\tilde{\zeta}_a \nabla_b \cdot \mathbf{u} + \hat{z} \cdot \left[ \frac{\partial \mathbf{u}}{\partial b} \times \nabla_b \dot{b} + \nabla_b \times \mathbf{F} \right]. \quad (44.40)$$

Now make use of the thickness equation in the material form (44.38c) to eliminate the convergence  $\nabla_b \cdot \mathbf{u}$  on the right hand side, thus leading to

$$\frac{D \tilde{\zeta}_a}{Dt} - \frac{\tilde{\zeta}_a}{h} \left[ \frac{D h}{Dt} - h \frac{\partial \dot{b}}{\partial b} \right] = \hat{z} \cdot \left[ \frac{\partial \mathbf{u}}{\partial b} \times \nabla_b \dot{b} + \nabla_b \times \mathbf{F} \right]. \quad (44.41)$$

Introducing the isopycnal potential vorticity

$$Q = \frac{\tilde{\zeta}_a}{h} = \frac{\tilde{\zeta} + f}{h} \quad (44.42)$$

leads to

$$\hbar \frac{DQ}{Dt} = \zeta_a \frac{\partial \dot{b}}{\partial b} + \hat{z} \cdot \left[ \frac{\partial \mathbf{u}}{\partial b} \times \nabla_b \dot{b} + \nabla_b \times \mathbf{F} \right]. \quad (44.43)$$

### Massaging the diabatic terms

The diabatic terms can be written

$$\zeta_a \frac{\partial \dot{b}}{\partial b} + \hat{z} \cdot \left[ \frac{\partial \mathbf{u}}{\partial b} \times \nabla_b \dot{b} \right] = \zeta_a \frac{\partial \dot{b}}{\partial b} + \dot{b} \frac{\partial \tilde{\zeta}}{\partial b} - \hat{z} \cdot \left[ \nabla_b \times \dot{b} \frac{\partial \mathbf{u}}{\partial b} \right] \quad (44.44a)$$

$$= \zeta_a \frac{\partial \dot{b}}{\partial b} + \dot{b} \frac{\partial \tilde{\zeta}_a}{\partial b} - \hat{z} \cdot \left[ \nabla_b \times \dot{b} \frac{\partial \mathbf{u}}{\partial b} \right] \quad (44.44b)$$

$$= \frac{\partial(\tilde{\zeta}_a \dot{b})}{\partial b} - \hat{z} \cdot \left[ \nabla_b \times \dot{b} \frac{\partial \mathbf{u}}{\partial b} \right] \quad (44.44c)$$

$$= \frac{\partial(\tilde{\zeta}_a \dot{b})}{\partial b} + \nabla_b \cdot \left[ \hat{z} \times \dot{b} \frac{\partial \mathbf{u}}{\partial b} \right], \quad (44.44d)$$

where the second equality follows since the Coriolis parameter is independent of the buoyancy.

### The PV equation

The PV equation takes the material form

$$\hbar \left[ \frac{DQ}{Dt} \right] = \frac{\partial(\tilde{\zeta}_a \dot{b})}{\partial b} + \nabla_b \cdot \left[ \hat{z} \times \dot{b} \frac{\partial \mathbf{u}}{\partial b} - \hat{z} \times \mathbf{F} \right]. \quad (44.45)$$

Expanding the material time derivative into its components (44.6b), and making use of the thickness equation (44.36c), leads to the Eulerian flux-form equation

$$\left[ \frac{\partial(\hbar Q)}{\partial t} \right]_b + \nabla_b \cdot (\hbar Q \mathbf{u}) + \frac{\partial(\hbar Q \dot{b})}{\partial b} = \frac{\partial(\tilde{\zeta}_a \dot{b})}{\partial b} + \nabla_b \cdot \left[ \hat{z} \times \dot{b} \frac{\partial \mathbf{u}}{\partial b} - \hat{z} \times \mathbf{F} \right]. \quad (44.46)$$

Since  $\hbar Q = \tilde{\zeta}_a$ , the  $\partial_b$  terms cancel, thus leaving the flux-form PV equation

$$\left[ \frac{\partial(\hbar Q)}{\partial t} \right]_b = -\nabla_b \cdot \left[ \hbar Q \mathbf{u} - \hat{z} \times \dot{b} \frac{\partial \mathbf{u}}{\partial b} + \hat{z} \times \mathbf{F} \right]. \quad (44.47)$$

#### 44.3.2 Derivation method II

The alternative method to derive the PV equation in isopycnal coordinates is to start from the hydrostatic Boussinesq PV equation in geopotential vertical coordinates, and directly transform to isopycnal coordinates. For this purpose we start from the discussion in Section 36.5.2 to write the material evolution of PV for a hydrostatic and Boussinesq fluid

$$\frac{DQ}{Dt} = \nabla \cdot \left[ (f \hat{z} + \boldsymbol{\omega}_{hy}) \dot{b} + b \nabla \times \mathbf{F} \right], \quad (44.48)$$

where

$$Q = \boldsymbol{\omega}_a^{hy} \cdot \nabla b = \boldsymbol{\omega}^{hy} \cdot \nabla b + f \frac{\partial b}{\partial z} \quad \text{and} \quad \boldsymbol{\omega}_{hy} = -\hat{x} \frac{\partial v}{\partial z} + \hat{y} \frac{\partial u}{\partial z} + \hat{z} \left[ \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right]. \quad (44.49)$$

The simplest term in equation (44.48) to transform to isopycnal coordinates is the curl of the horizontal friction vector

$$\hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}) = \hat{\mathbf{z}} \cdot \nabla \times (F^x, F^y, 0), \quad (44.50)$$

which takes the form

$$\hat{\mathbf{z}} \cdot (\nabla \times \mathbf{F}) = h^{-1} \hat{\mathbf{z}} \cdot (\nabla_b \times \mathbf{F}) = -h^{-1} \nabla_b \cdot (\hat{\mathbf{z}} \times \mathbf{F}). \quad (44.51)$$

The diabatic term requires some more work. Since the vorticity has zero divergence, the diabatic term can be written as

$$\nabla \cdot [(f \hat{\mathbf{z}} + \boldsymbol{\omega}_{hy}) \dot{b}] = (f \hat{\mathbf{z}} + \boldsymbol{\omega}_{hy}) \cdot \nabla \dot{b} \quad (44.52a)$$

$$= f \frac{\partial \dot{b}}{\partial z} - \frac{\partial v}{\partial z} \frac{\partial \dot{b}}{\partial x} + \frac{\partial u}{\partial z} \frac{\partial \dot{b}}{\partial y} + \left[ \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right] \frac{\partial \dot{b}}{\partial z}. \quad (44.52b)$$

We now introduce horizontal derivatives on isopycnal surfaces according to the following relation (see Section 41.12.2)

$$\nabla_z = \nabla_b + \nabla_z b \left[ \frac{\partial z}{\partial b} \right] \frac{\partial}{\partial z} \quad (44.53)$$

Doing so leads to

$$\begin{aligned} \nabla \cdot [(f \hat{\mathbf{z}} + \boldsymbol{\omega}_{hy}) \dot{b}] &= f \frac{\partial \dot{b}}{\partial z} - \frac{\partial v}{\partial z} \frac{\partial \dot{b}}{\partial x} + \frac{\partial u}{\partial z} \frac{\partial \dot{b}}{\partial y} + \left[ \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right] \frac{\partial \dot{b}}{\partial z} \\ &= f \frac{\partial \dot{b}}{\partial z} - \frac{\partial v}{\partial z} \left( \left[ \frac{\partial \dot{b}}{\partial x} \right]_b + \left[ \frac{\partial \dot{b}}{\partial x} \right]_z \frac{\partial z}{\partial b} \frac{\partial \dot{b}}{\partial z} \right) + \frac{\partial u}{\partial z} \left( \left[ \frac{\partial \dot{b}}{\partial y} \right]_b + \left[ \frac{\partial \dot{b}}{\partial y} \right]_z \frac{\partial z}{\partial b} \frac{\partial \dot{b}}{\partial z} \right) \\ &\quad + \frac{\partial \dot{b}}{\partial z} \left( \left[ \frac{\partial v}{\partial x} \right]_b + \left[ \frac{\partial v}{\partial x} \right]_z \frac{\partial z}{\partial b} \frac{\partial v}{\partial z} \right) - \frac{\partial \dot{b}}{\partial z} \left( \left[ \frac{\partial u}{\partial y} \right]_b + \left[ \frac{\partial u}{\partial y} \right]_z \frac{\partial z}{\partial b} \frac{\partial u}{\partial z} \right) \\ &= f \frac{\partial \dot{b}}{\partial z} - \frac{\partial v}{\partial z} \left[ \frac{\partial \dot{b}}{\partial x} \right]_b + \frac{\partial u}{\partial z} \left[ \frac{\partial \dot{b}}{\partial y} \right]_b + \tilde{\zeta} \left[ \frac{\partial \dot{b}}{\partial z} \right] \\ &= \frac{\partial b}{\partial z} \left( \tilde{\zeta}_a \left[ \frac{\partial \dot{b}}{\partial b} \right] - \frac{\partial v}{\partial b} \left[ \frac{\partial \dot{b}}{\partial x} \right]_b + \frac{\partial u}{\partial b} \left[ \frac{\partial \dot{b}}{\partial y} \right]_b \right) \\ &= h^{-1} \left( \tilde{\zeta}_a \left[ \frac{\partial \dot{b}}{\partial b} \right] + \hat{\mathbf{z}} \cdot \left[ \frac{\partial \mathbf{u}}{\partial b} \times \nabla_b \dot{b} \right] \right) \\ &= h^{-1} \left( \tilde{\zeta}_a \left[ \frac{\partial \dot{b}}{\partial b} \right] + \dot{b} \left[ \frac{\partial \tilde{\zeta}_a}{\partial b} \right] + \nabla_b \cdot \left[ \hat{\mathbf{z}} \times \dot{b} \frac{\partial \mathbf{u}}{\partial b} \right] \right) \\ &= h^{-1} \left( \frac{\partial(\dot{b} \tilde{\zeta}_a)}{\partial b} + \nabla_b \cdot \left[ \hat{\mathbf{z}} \times \dot{b} \frac{\partial \mathbf{u}}{\partial b} \right] \right). \end{aligned} \quad (44.54)$$

To reach the penultimate step we noted that  $\partial f / \partial b = 0$  so that we could form the derivative of the absolute vorticity. Bringing the pieces together leads to the PV equation (44.45) derived starting from the isopycnal version of the equations of motion.

### 44.3.3 Comments

The flux-form PV equation (44.47) manifests the impermeability theorem of Chapter 37 since the right hand side is the isopycnal convergence of a flux.





# Chapter 45

## Shallow water thickness weighted averaging

There is a range of mathematical formalisms of use to frame the study of how linear waves, nonlinear waves, eddies, and fully developed turbulence interact with a mean flow. A distinctly geophysical element enters these studies through the primary role of vertical stratification arising from gravitation, with stratification particularly important for large scales flows where motions are approximately hydrostatic. A further specialization to the oceanographic context arises since there are few regions of the ocean where zonal averages apply, which contrasts to the atmospheric case.<sup>1</sup> The *thickness weighted averaging* (TWA) method has emerged as a useful formalism for stratified flows, with particular use for studies of geostrophic eddies and their parameterization. In this chapter, we develop the TWA equations for the adiabatic stacked shallow water model.

As noted in the introduction to Part V of this book, the adiabatic stacked shallow water model exposes key facets of stratified geophysical flows without requiring the mathematics of generalized vertical coordinates developed in Chapters 41, 42, 43, and 44. The core simplification arises by assuming that horizontal fluid motion has no vertical dependence within a shallow water layer, which then means that vertical motion is a linear function of vertical position within each layer. That is, the shallow water fluid moves as extensible vertical columns (Section 30.2.7). It follows that horizontal pressure gradients do not need to be projected along the slope of the layer since they are vertically constant within a layer. In contrast, this projection is needed for a continuously stratified fluid described by generalized vertical coordinates, as illustrated in Figure 41.4. Hence, the shallow water equations for momentum, thickness, and tracers retain their use of Cartesian coordinates even though the layer interfaces undulate and are thus not generally horizontal. This mathematical feature of shallow water fluids aids in our pedagogical development of the TWA method.

[Young \(2012\)](#) offers an elegant application of the TWA to the continuously stratified Boussinesq hydrostatic fluid, with this paper the culmination of many years of prior work (see [Young \(2012\)](#) for citations). Penetrating the TWA approach for continuously stratified fluids requires an understanding of generalized vertical coordinates and the attendant tensor analysis such as that developed in Chapters 41, 42, 43, and 44. In the present chapter, we focus on the TWA equations for the adiabatic shallow water model. Doing so minimizes the mathematical requirements while exposing the key physical concepts. It also offers a useful baseline for those using stacked shallow water models for studies of adiabatic waves and geostrophic turbulence. Digesting the material in this chapter, and then coupling to skills in generalized vertical coordinate tensor analysis, prepares one for penetrating [Young \(2012\)](#). Afterward, the mathematically inclined reader may study the work of [Maddison and Marshall \(2013\)](#), who provide a more general mathematical framework for

<sup>1</sup>The Southern Ocean is a notable ocean exception, as discussed in Sections 19.5 and 31.6.

thickness weighted averaging.

READER'S GUIDE FOR THIS CHAPTER

In this chapter we assume a working knowledge of the shallow water model presented in Chapters 30, 31, and 34, with particular attention given to the pressure force as realized both as a contact force and a body force (see Chapter 19 and Section 31.5). The TWA equations offer a useful framework for eddy parameterizations, with parameterizations for the tracer equation discussed in Chapters 47 and 48. Parameterizations for both the tracer equation and the momentum equation remain a topic of ongoing research. These studies are of particular focus in physical oceanography given the computational expense of resolving quasi-geostrophic eddies in global climate simulations.

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45.1	Loose threads . . . . .	1092
45.2	The unaveraged thickness weighted equations . . . . .	1093
45.3	Thickness transport by the bolus velocity . . . . .	1093
45.3.1	Rectified effects . . . . .	1094
45.3.2	An undulating fluid layer . . . . .	1094
45.3.3	Stokes drift . . . . .	1094
45.3.4	Linearized thickness perturbations . . . . .	1096
45.3.5	Correlation between thickness and velocity . . . . .	1096
45.3.6	Do we need the bolus velocity? . . . . .	1097
45.4	Averaging operators . . . . .	1097
45.4.1	Reynolds average . . . . .	1097
45.4.2	Ensemble average . . . . .	1097
45.4.3	Thickness weighted average . . . . .	1098
45.4.4	Comments . . . . .	1099
45.5	Thickness equation and tracer equation . . . . .	1099
45.5.1	TWA thickness equation . . . . .	1099
45.5.2	Tracer equation . . . . .	1100
45.5.3	Vertical velocity . . . . .	1100
45.6	Horizontal momentum equation . . . . .	1100
45.6.1	Kinetic stress and Reynolds stress . . . . .	1101
45.6.2	Thickness and pressure gradient correlation . . . . .	1101
45.6.3	Zonal and meridional Eliassen-Palm fluxes . . . . .	1103
45.6.4	Interfacial stresses from geostrophic eddies . . . . .	1105
45.7	Vorticity and potential vorticity . . . . .	1105
45.7.1	Derivation . . . . .	1105
45.7.2	Specializing to non-divergent barotropic flow . . . . .	1106

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## 45.1 Loose threads

- Build more into the bolus discussion in Section 45.3 as per Section 4.5 of *McWilliams* (2006).
- More discussion of Taylor-Bretherton relation (45.71).
- Write the EP fluxes for quasi-geostrophic shallow water Rossby waves.
- Write the EP fluxes for 2d non-divergent Rossby waves.
- Formulate the TWA energy equations.
- Is there a gauge that offers good options for parameterization?

## 45.2 The unaveraged thickness weighted equations

The thickness weighted averaging formalism starts from flux-form evolution equations for extensive quantities (per unit horizontal area) rather than intensive quantities. In the context of the shallow water model, this approach means we focus on the thickness equation (30.70a), the thickness weighted tracer equation (30.70b), and the thickness weighted velocity equation (31.64) (also called the momentum equation)

$$\frac{\partial h_k}{\partial t} + \nabla \cdot (h_k \mathbf{u}_k) = 0 \quad (45.1a)$$

$$\frac{\partial(h_k C)}{\partial t} + \nabla \cdot (h_k \mathbf{u}_k C) = 0 \quad (45.1b)$$

$$\frac{\partial(h_k \mathbf{u}_k)}{\partial t} + \nabla \cdot [h_k \mathbf{u}_k \otimes \mathbf{u}_k] + f \hat{\mathbf{z}} \times (h_k \mathbf{u}_k) = -(h_k / \rho) \nabla p_k. \quad (45.1c)$$

The density,  $\rho$ , appearing in the momentum equation (45.1c) is the Boussinesq reference density, normally chosen as the density of the uppermost layer,  $\rho = \rho_1$ . The thickness and tracer equations do not couple to other layers, and as such we can drop the layer index,  $k = 1, N$ , when analyzing these equations. For the momentum equation, we expose the interface indices,  $k \pm 1/2$ , when considering pressure form stresses.

For this chapter, it proves useful to move seamlessly between the thickness weighted pressure gradient body force and its equivalent contact force version studied in Section 31.5. The contact force version of the momentum equation reveals the pressure form stresses acting on the upper and lower interfaces of a shallow water layer. It also brings stresses (kinetic stresses and pressure stresses) together into the divergence of a momentum flux. As such, this formulation follows that of Cauchy as discussed in Section 17.1.3. The eddy correlation portion of the momentum flux is known as the *Eliassen-Palm* flux.<sup>2</sup>

When the dust settles, the TWA equations are isomorphic to the unaveraged equations (45.1a)-(45.1c), yet with the addition of momentum flux convergences to the right hand sides that arise from subgrid correlations (i.e., convergence of the Eliassen-Palm flux). The momentum eddy fluxes are connected to the potential vorticity fluxes, with the connection known as the *Taylor-Bretherton identity*. The isomorphism provides some motivation to favor the TWA approach since properties of the unaveraged equations are directly reflected in the TWA equations. It also provides a suitable framework for parameterizing the subgrid correlations within the context of flux-form conservation laws. Even so, any formalism for an eddy and mean decomposition is subjective since the mean flow and eddying fluctuations are defined by the analyst not by the physics. Hence, arguments concerning what is a preferable framework are subject to the needs of the analyst and have no physically objective foundation.

## 45.3 Thickness transport by the bolus velocity

Prior to diving into the formalism of thickness weighted averaging, we study the eddy-induced volume transport (more precisely, thickness transport) realized by linear waves within a layer of shallow water fluid. This discussion provides a specific example of the thickness transport by the *bolus velocity*, with further discussion offered in Sections 45.5.1 and 47.5.5. Much of our intuition for bolus transport is based on the following relatively simple example of Stokes drift.<sup>3</sup>

<sup>2</sup>See [Bühler \(2014b\)](#) for a historical perspective on the Eliassen-Palm flux, which was introduced by [Eliassen and Palm \(1960\)](#) in their study of stationary mountain waves.

<sup>3</sup>This example is based Section 2 of [Lee et al. \(1997\)](#).

Part of the motivation for TWA is that we do not need to compute the bolus velocity. Even so, understanding the basic physics of the bolus velocity renders useful insights into how eddies, even eddies as simple as linear waves, can provide a rectified transport of properties. We also comment on this point in Section 31.5.

### 45.3.1 Rectified effects

*Rectification* is the conversion of a fluctuating motion into motion in a particular direction. For example, the transformation of an alternating electrical current into a direct electrical current occurs through a rectifier. More generally, rectification arises from the breaking of a symmetry typically through a nonlinear mechanism. The primary example in fluid mechanics is the Stokes drift discussed in Section 29.3 as well as the current section. Stokes drift arises when linear waves have an amplitude that is a function of space, with this spatial dependence giving rise to net particle transport (the Stokes drift) in a preferred direction. Another example concerns the turbulent Stokes drift arising from nonlinear geostrophic waves and eddies in the ocean and atmosphere that lead to a net transport of buoyancy. In Section 31.6 we discuss the meridional transport of buoyancy by eddies in a channel, which is the canonical geophysical example of eddy induced transport.

### 45.3.2 An undulating fluid layer

Figure 45.1 shows a layer of constant density shallow water fluid within an adiabatic stacked shallow water model. Since the layers are immiscible, the total volume of fluid within this layer remains constant. In its unperturbed state with flat layer interfaces, the meridional velocity in the fluid layer is zero and the thickness is a constant,  $h_o$ . When perturbed, the thickness is written

$$h(y, t) = h_o + h'(y, t), \quad (45.2)$$

where we assume the perturbation only depends on  $(y, t)$  for simplicity. The layer thickness changes in time according to the convergence of the advective transport of thickness as found by the thickness equation (45.1a)

$$\frac{\partial h}{\partial t} = -\nabla \cdot (h \mathbf{u}), \quad (45.3)$$

where the convergence is computed within the layer and we drop the k layer index for brevity. As seen by Figure 45.1, undulations of the layer thickness at a point arise from the convergence of thickness advected to that point. Further assuming that there is no zonal dependence ( $\partial_x = 0$ ) leads to the one-dimensional thickness equation

$$\frac{\partial h}{\partial t} = -\frac{\partial (h v)}{\partial y}. \quad (45.4)$$

### 45.3.3 Stokes drift

Consider a linear wave perturbation in the meridional velocity that propagates in the meridional direction

$$v'(y, t) = v_o \sin(k y - \omega t), \quad (45.5)$$

where  $k$  is a constant wave number and  $\omega$  is a constant frequency. This longitudinal wave is depicted in Figure 45.1. We now follow the general formalism developed in Section 29.3 or equivalently in Section 47.3.4 to determine the Stokes drift associated with this wave.

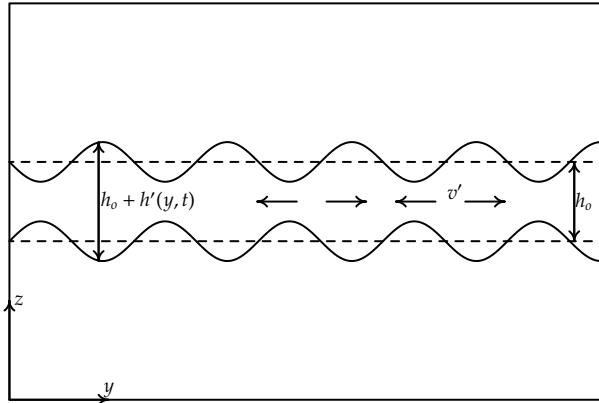


FIGURE 45.1: Shown here is a single layer of constant density fluid, with resting thickness  $h = h_o$  and instantaneous thickness  $h = h_o + h'(y, t)$ . Associated with the undulations in thickness are fluctuations in the meridional velocity  $v' = v_o \sin(k y - \omega t)$ , depicted here by the alternating vectors within the layer. Vertical-meridional axes are shown in the lower left corner for orientation. We are not concerned with boundaries in the meridional direction.

We are only concerned with the meridional component of the velocity, so the fluid particle trajectory equation is given by

$$\frac{dY}{dt} = v_o \sin(k Y - \omega t), \quad (45.6)$$

where  $Y = Y(Y_o, t)$  is the meridional trajectory with initial position  $Y_o$ . Following equation (29.43) we can write the difference between the velocity following a fluid particle (the Lagrangian velocity for the moving fluid particle) from the velocity at the initial particle point (the Eulerian velocity at the initial point of the trajectory)

$$\frac{dY}{dt} - v(y, t) = v_o^2 k \cos(ky - \omega t) \int_0^t \sin(ky - \omega t') dt' \quad (45.7a)$$

$$= \frac{v_o^2 k}{\omega} (\cos^2(ky - \omega t) - \cos(ky - \omega t) \cos(ky)). \quad (45.7b)$$

Time averaging over a single wave period,

$$T = 2\pi/\omega \quad (45.8)$$

leads to the Stokes drift as per the general expression in equation (29.45)

$$V_{\text{Stokes}} = \frac{v_o^2 k}{2\omega}. \quad (45.9)$$

Introducing the phase speed for the wave  $c = \omega/k$  allows us to write the Stokes drift as

$$V_{\text{Stokes}} = \frac{v_o^2}{2c}. \quad (45.10)$$

The Stokes drift becomes small when the phase speed is large, since the fluid particles have only a short time to feel each wave. In this case, there is only a small difference between the Eulerian and Lagrangian velocities. The converse holds for slow phase speeds, where Eulerian and Lagrangian velocities differ more. Note that if we were to consider a more careful asymptotic expansion, then the case of relatively slow phase speeds would require us to keep more terms in the expansion.

### 45.3.4 Linearized thickness perturbations

The velocity and thickness are written in terms of their rest state plus a perturbation due to the wave

$$h = h_o + h' \quad \text{and} \quad v = v', \quad (45.11)$$

where the velocity vanishes when the wave is absent. The thickness equation (45.4) thus takes the form

$$\frac{\partial h'}{\partial t} + h_o \frac{\partial v'}{\partial y} + v' \frac{\partial h'}{\partial y} = 0. \quad (45.12)$$

Linearizing this equation, and using the wave perturbation (45.5), leads to

$$\frac{\partial h'}{\partial t} + h_o v_o k \cos(ky - \omega t) = 0, \quad (45.13)$$

thus yielding the thickness perturbation

$$h' = h_o v'/c. \quad (45.14)$$

Hence, to leading order, the thickness perturbation is directly proportional to and in phase with the velocity perturbation.

### 45.3.5 Correlation between thickness and velocity

Over a single wave period  $T = 2\pi/\omega$ , the temporal correlation between the linear thickness perturbation and velocity perturbation is given by

$$\overline{h' v'} = \frac{1}{T} \int_0^T h' v' dt \quad (45.15a)$$

$$= \frac{h_o}{c T} \int_0^T v' v' dt \quad (45.15b)$$

$$= \frac{v_o^2 h_o}{c T} \int_0^T \sin^2(ky - \omega t) dt \quad (45.15c)$$

$$= \frac{v_o^2 h_o}{2 c} \quad (45.15d)$$

$$= h_o V_{\text{Stokes}}, \quad (45.15e)$$

where we introduced the Stokes drift (45.10) to reach the final equality. A nonzero correlation  $\overline{h' v'}$  means that the thickness has a nonzero tendency when averaged over a wave period.

The nonzero correlation in equation (45.15e) induces a thickness transport from the one-dimensional linear longitudinal waves. This transport arises from the Stokes drift induced by the waves; without Stokes drift there is no eddy thickness transport. This behavior exemplifies that for more general waves and eddies moving through fluid layers. For the general case, a nonzero bolus velocity (Section 45.5.1), determined by velocity-thickness correlations, induces an eddy thickness transport. We see that for the one-dimensional linear longitudinal wave example, the bolus velocity is the Stokes velocity, thus prompting certain authors to make the equality in general.

### 45.3.6 Do we need the bolus velocity?

Although the bolus transport is of fundamental importance for how we think about eddy induced Stokes transport from shallow water waves, more general fluctuations, such as those from turbulent geostrophic eddies, require a parameterization to determine the thickness transport. We considered such in Section 25.7 when studying geostrophic eddies in a zonally reentrant channel. As we see in the remainder of this chapter, the allure of TWA is that it dispenses with the need to parameterize the bolus velocity. Instead, the TWA equations absorb the bolus transport into the residual mean advection operator. Doing so moves the parameterization problem fully into the momentum equation.

## 45.4 Averaging operators

We denote the averaging or mean operator by an overbar

$$\text{average}(\Phi) = \overline{\Phi}, \quad (45.16)$$

where  $\Phi$  is any field such as velocity, thickness, or tracer concentration. Deviations (also called fluctuations) from the mean are denoted by a prime so that the full field can be decomposed as

$$\Phi = \overline{\Phi} + \Phi'. \quad (45.17)$$

There are many averaging operators used in fluid mechanics, such as the wave average from Section 45.3, which is useful when the flow is dominantly linear waves; a long time average (formally an infinitely long time average), which is commonly used for climate studies; a space average, which is appropriate when the spatial sampling is coarse; general space filters or kernels, which are commonly used in large eddy simulations; and ensemble averages, which are generally assumed in traditional studies of turbulence.

### 45.4.1 Reynolds average

A *Reynolds average* is an operator that annihilates any fluctuating quantity, which then means that the average of an average is the identity operator

$$\overline{\Phi'} = 0 \iff \overline{\overline{\Phi}} = \overline{\Phi}, \quad (45.18)$$

which in turn means that

$$\overline{\Phi \Psi} = \overline{(\overline{\Phi} + \Phi') \Psi} = \overline{\Phi} \overline{\Psi}. \quad (45.19)$$

Reynolds averages are commonly used when deriving mean field equations, and yet these assumptions are not satisfied by many operators in practical use. Extra technical issues arise when averaging operators do not satisfy the properties of a Reynolds average, with these issues going beyond our aims. We thus retain the Reynolds average assumption (45.18) for the averaging operator used in this chapter.

### 45.4.2 Ensemble average

A further assumption we make is that the average operator commutes with space-time derivatives and integrals. This assumption does not strictly hold if the operator is a space and/or time average operator, at least not without a bit of work. However, this assumption holds for ensemble

averages. An *ensemble average* is computed over an infinite number of realizations of the fluid flow, with approximations to this average afforded by finite sized ensembles.

Ensemble averages are typically assumed in traditional fluid turbulence studies. However, they are not always very practical nor are they the obvious choice when targeting a framework for parameterization. Even so, we prefer ensemble averages for this chapter in order to dispense with concerns about commutation of the averaging operator with derivative and integral operators. We also make use of ensemble averaging for our discussion of tracer kinematics in Chapter 47.

### 45.4.3 Thickness weighted average

The thickness weighted average of a field is defined as the ensemble average of the thickness weighted field, and then divided by the averaged thickness:

$$\widehat{\Phi} \equiv \frac{\overline{h\Phi}}{\overline{h}} \iff \overline{h}\widehat{\Phi} = \overline{h\Phi}, \quad (45.20)$$

with widehats adorning a thickness weighted average. Deviations from the thickness weighted average are denoted with two primes so that the unaveraged field is decomposed into its average plus fluctuation

$$\Phi = \widehat{\Phi} + \Phi''. \quad (45.21)$$

Since the overline average from Section 45.4.1 satisfies the Reynolds averaging assumption, so too does the thickness weighted average

$$\Phi = \widehat{\Phi} + \Phi'' \implies \widehat{\Phi''} = \frac{\overline{h\Phi''}}{\overline{h}} = 0. \quad (45.22)$$

We are thus able to derive the following related identities

$$\Phi\Psi = (\widehat{\Phi} + \Phi'')(\widehat{\Phi} + \Phi'') \implies \widehat{\Phi\Psi} = \widehat{\Phi}\widehat{\Psi} + \widehat{\Phi''}\widehat{\Psi''} \implies \overline{h\Phi\Psi} = \overline{h}\widehat{\Phi\Psi}. \quad (45.23)$$

We need one final result related to mixed averages and primes, which results from

$$\overline{\overline{h\widehat{\Phi}}} = \overline{h\widehat{\Phi}} = \overline{h}\widehat{\Phi}, \quad (45.24)$$

so that<sup>4</sup>

$$\overline{h\Phi''} = \overline{h}(\overline{\Phi} - \widehat{\Phi}) = \overline{h\Phi} - \overline{h'\Phi'} \neq 0. \quad (45.25)$$

Hence, the ensemble average of a fluctuation relative to thickness weighted mean is generally nonzero.

Derivative operators *do not* commute with the thickness weighted average, so that, for example,

$$\partial_x \widehat{u} \neq \widehat{\partial_x u}. \quad (45.26)$$

Hence, when deriving differential equations for thickness weighted fields, we first derive equations for the unaveraged thickness weighted quantities, and only thereafter do we apply the ensemble mean operator.

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<sup>4</sup>Footnote #4 in [Young \(2012\)](#) is missing the  $\overline{h\Phi}$  term appearing in equation (45.25).

#### 45.4.4 Comments

For the most part, we follow the notation of [Young \(2012\)](#). Nonetheless, we caution that notational clutter and variations on conventions can present a nontrivial barrier to penetrating the TWA literature. Indeed, for our purposes with the stacked shallow water model, there is one additional piece of notation concerning the discrete layer indices. Fortunately, much of the discrete layer notation can be streamlined by exposing just the half-integer indices for fields situated at layer interfaces, along with the layer density.

## 45.5 Thickness equation and tracer equation

In this section we derive the TWA versions of the thickness equation (45.1a) and the tracer equation (45.1b). The derivations involve straightforward applications of the TWA averaging properties (45.22) and (45.23).

### 45.5.1 TWA thickness equation

Taking the ensemble average of the thickness equation (45.1a) renders

$$\partial_t \bar{h} + \nabla \cdot \bar{h} \bar{\mathbf{u}} = 0, \quad (45.27)$$

where we dropped the layer index,  $k$ , to reduce notation. Introducing the thickness weighted average according to equation (45.20) brings the thickness equation to the form

$$\partial_t \bar{h} + \nabla \cdot (\bar{h} \hat{\mathbf{u}}) = 0. \quad (45.28)$$

Consequently, the mean layer thickness,  $\bar{h}$ , evolves at a point in space according to the convergence of the thickness flux,  $-\nabla \cdot (\bar{h} \hat{\mathbf{u}})$ , with the flux determined by the thickness weighted velocity,  $\hat{\mathbf{u}}$ .

We find it useful to introduce the material time derivative operator defined with the thickness weighted velocity<sup>5</sup>

$$\frac{D^\sharp}{Dt} = \frac{\partial}{\partial t} + \hat{\mathbf{u}} \cdot \nabla = \frac{\partial}{\partial t} + \hat{u} \partial_x + \hat{v} \partial_y, \quad (45.29)$$

so that the Eulerian flux-form thickness equation (45.28) can be written in the material time derivative or advective form

$$\frac{D^\sharp \bar{h}}{Dt} = -\bar{h} \nabla \cdot \hat{\mathbf{u}}. \quad (45.30)$$

The isomorphism between the TWA thickness equation (45.28) with the unaveraged thickness equation (45.1a) illustrates a distinct advantage of using the thickness weighted velocity,  $\hat{\mathbf{u}}$ . Even so, for some purposes it is useful to unpack the thickness weighted velocity into its two components

$$\hat{\mathbf{u}} = \bar{u} + \frac{\bar{h}' \mathbf{u}'}{\bar{h}} \equiv \bar{u} + \mathbf{u}^{\text{bolus}}, \quad (45.31)$$

where we defined the bolus velocity as

$$\mathbf{u}^{\text{bolus}} = \frac{\bar{h}' \mathbf{u}'}{\bar{h}}. \quad (45.32)$$

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<sup>5</sup>The  $D^\sharp/Dt$  notation is based on that used by [Young \(2012\)](#). The alternative  $\widehat{D}/Dt$  is less suitable since  $\bar{h}(D/Dt) \neq (D/Dt)\bar{h}$ . In brief, an object adorned with a sharp symbol is consistent with thickness weighted averaging but is itself not the direct result of a thickness weighted average.

We discussed the bolus velocity in Section 45.3 and see it again in Section 47.5.5 when developing the ensemble mean tracer equation in isopycnal coordinates. However, as per our discussion in Section 45.3.6, we do not need to know the bolus velocity if we write the averaged tracer and momentum equations in terms of the thickness weighted velocity.

### 45.5.2 Tracer equation

Taking the ensemble average of the tracer concentration equation (45.1b) for a shallow water fluid layer renders

$$\partial_t(\bar{h} \bar{C}) + \nabla \cdot (\bar{h} \bar{C} \bar{\mathbf{u}}) = 0. \quad (45.33)$$

Making use of the thickness weighted averages from Section 45.4.3 allows us to write

$$\bar{h} \bar{C} = \bar{h} \hat{C} \quad \text{and} \quad \bar{h} \bar{C} \bar{\mathbf{u}} = \bar{h} (\hat{C} \hat{\mathbf{u}} + \widehat{\bar{C}'' \bar{\mathbf{u}}''}), \quad (45.34)$$

thus yielding the TWA tracer equation

$$\partial_t(\bar{h} \hat{C}) + \nabla \cdot (\bar{h} \hat{C} \hat{\mathbf{u}}) = -\nabla \cdot (\bar{h} \widehat{\bar{C}'' \bar{\mathbf{u}}''}). \quad (45.35)$$

The right hand side is the convergence of the thickness weighted eddy tracer flux. As seen in Section 47.6, the isopycnal form of the tracer equation is identical to that given here for a shallow water layer. In that discussion we present methods commonly used to parameterize the eddy flux convergence.

### 45.5.3 Vertical velocity

We generally have no need for the vertical velocity when working with the adiabatic stacked shallow water model. Nonetheless, it is interesting to define a vertical velocity component,  $w^\sharp$ , satisfying the continuity equation

$$\nabla_z \cdot \hat{\mathbf{u}} + \partial_z w^\sharp = 0. \quad (45.36)$$

As for the unaveraged vertical velocity component,  $\partial_z w^\sharp$  is a linear function of  $z$  within the ensemble mean shallow water layers. Note that  $w^\sharp$  is not a thickness weighted velocity. Rather, it is the vertical velocity that is compatible, through the continuity equation, with the thickness weighted horizontal velocity. A vertical velocity is needed for the continuously stratified Boussinesq fluid, and it is defined as done here for the shallow water.

## 45.6 Horizontal momentum equation

Taking the ensemble mean of the horizontal momentum equation (45.1c) renders

$$\partial_t(\bar{h} \bar{\mathbf{u}}) + \nabla \cdot [\bar{h} \bar{\mathbf{u}} \otimes \bar{\mathbf{u}}] + f \hat{\mathbf{z}} \times (\bar{h} \bar{\mathbf{u}}) = -\bar{h} \nabla p / \rho, \quad (45.37)$$

where we dropped the layer interface label,  $k$ , for brevity. Again, we make use of the thickness weighted averages from Section 45.4.3 to write

$$\bar{h} \bar{\mathbf{u}} = \bar{h} \hat{\mathbf{u}} \quad (45.38a)$$

$$\bar{h} \bar{\mathbf{u}} \otimes \bar{\mathbf{u}} = \bar{h} (\hat{\mathbf{u}} \otimes \hat{\mathbf{u}} + \widehat{\bar{\mathbf{u}}'' \otimes \bar{\mathbf{u}}''}), \quad (45.38b)$$

so that equation (45.37) becomes

$$\partial_t(\bar{h}\hat{\mathbf{u}}) + \nabla \cdot [\bar{h}\hat{\mathbf{u}} \otimes \hat{\mathbf{u}}] + f\hat{z} \times (\bar{h}\hat{\mathbf{u}}) = -\nabla \cdot [\bar{h}\widehat{\mathbf{u}'' \otimes \mathbf{u}''}] - \bar{h}\nabla p/\rho. \quad (45.39)$$

The first term on the right hand side is similar to the eddy tracer flux convergence appearing in the TWA tracer equation (45.35). In contrast, the thickness weighted pressure gradient is fundamentally distinct from anything appearing in the tracer equation. Much in the remainder of this section is devoted to developing a physical and mathematical understanding of this term.

### 45.6.1 Kinetic stress and Reynolds stress

Following our discussion in Section 18.5, we introduce the shallow water kinetic stress tensor

$$\mathbb{T}^{\text{sw kinetic}} = -\rho \mathbf{u} \otimes \mathbf{u}. \quad (45.40)$$

The kinetic stress arises from motion of the fluid, with its divergence,  $\nabla \cdot (h\mathbb{T}^{\text{kinetic}})$ , contributing to changes in the momentum of a shallow water fluid column. Decomposing the velocity into the TWA velocity and fluctuation leads to the ensemble mean of the thickness weighted kinetic stress

$$h\mathbb{T}^{\text{kinetic}}(\mathbf{u}) = -\rho \bar{h}\mathbf{u} \otimes \mathbf{u} \quad (45.41a)$$

$$= -\rho \bar{h}[\hat{\mathbf{u}} \otimes \hat{\mathbf{u}} + \widehat{\mathbf{u}'' \otimes \mathbf{u}''}] \quad (45.41b)$$

$$= \bar{h}\mathbb{T}^{\text{kinetic}}(\hat{\mathbf{u}}) + \bar{h}\mathbb{T}^{\text{Reynolds}}, \quad (45.41c)$$

where the eddy correlation is known as the *Reynolds stress*. The divergence of the thickness weighted Reynolds stress provides a rectified effect onto the mean flow due to nonzero eddy correlations.

### 45.6.2 Thickness and pressure gradient correlation

The ensemble mean of the thickness weighted pressure gradient can be written

$$\overline{h_k \nabla p_k} = \bar{h}_k \nabla \bar{p}_k + \overline{h'_k \nabla p'_k}. \quad (45.42)$$

The eddy term is the correlation between layer thickness fluctuations and horizontal pressure gradient fluctuations. We here unpack this term by writing the pressure as a contact force rather than a body force. Doing so exposes the eddy interfacial form stresses that provide a vertical transfer of horizontal momentum. Note that some treatments simply say that  $\overline{h'_k \nabla p'_k}$  is the interfacial form stress. However, that identification is incorrect since, as we will see in this section, there is an additional piece arising from the gradient in the layer depth integrated pressure or, alternatively, the layer potential energy. To proceed we rely on the development given in Section 31.5.9, in which we exposed two equivalent expressions for the contact pressure. As part of the following derivation we make use of relations for pressure within a layer and at an interface

$$p_k(z) = p_{k-1/2} + g\rho_k(\eta_{k-1/2} - z) \quad (45.43a)$$

$$p_{k+1/2} - p_{k-1/2} = g\rho_k h_k = g\rho_k(\eta_{k-1/2} - \eta_{k+1/2}) \quad (45.43b)$$

$$p_{1/2} = p_a, \quad (45.43c)$$

with  $p_a$  the applied (or atmospheric) pressure at the ocean surface.

*Interfacial form stress plus gradient of layer depth integrated pressure*

The first expression for thickness weighted pressure gradient is given by

$$-h_k \nabla p_k = -\nabla P_k + \mathbf{F}_k^{\text{form}}. \quad (45.44)$$

In this equation we introduced the vertically integrated pressure computed over layer-k

$$P_k = \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} p_k(z) dz = h_k (g \rho_k h_k / 2 + p_{k-1/2}), \quad (45.45)$$

with its gradient providing a horizontal acceleration due to imbalances in the contact pressure acting along the vertical sides of a shallow water column. The second stress in equation (45.44) is the pressure form stress acting on the upper and lower layer interfaces

$$\mathbf{F}_k^{\text{form}} = p_{k-1/2} \nabla \eta_{k-1/2} - p_{k+1/2} \nabla \eta_{k+1/2} \equiv \delta_k (p_{k-1/2} \nabla \eta_{k-1/2}), \quad (45.46)$$

where

$$\delta_k \Phi_{k-1/2} = \Phi_{k-1/2} - \Phi_{k+1/2} = -(\Phi_{k+1/2} - \Phi_{k-1/2}) \quad (45.47)$$

is a difference operator acting on interface properties. The use of a backward difference operator is motivated since k increases down whereas  $\hat{z}$  points up. Additionally, we define the difference operator to only act on fields defined at the layer interface, with layer fields commuting with this operator so that, for example,

$$\delta_k (h_k \eta_{k-1/2}) = h_k \delta_k (\eta_{k-1/2}). \quad (45.48)$$

*Dual interfacial pressure form stress plus gradient of layer potential energy*

An alternative formulation uses the dual form stress and potential energy, in which case we write the thickness weighted horizontal pressure gradient as

$$-h_k \nabla p_k = -\nabla \mathcal{P}_k + \mathbf{F}_k^{\text{dual}}. \quad (45.49)$$

In this equation we introduced the layer gravitational potential energy per area

$$\mathcal{P}_k = g \rho_k \int_{\eta_{k+1/2}}^{\eta_{k-1/2}} z dz = (g \rho_k / 2) (\eta_{k-1/2}^2 - \eta_{k+1/2}^2) = (g \rho_k / 2) \delta_k (\eta_{k-1/2}^2), \quad (45.50)$$

and the *dual pressure form stress* (see Section 31.5.8),

$$\mathbf{F}_k^{\text{dual}} = -\delta_k (\eta_{k-1/2} \nabla p_{k-1/2}) = \mathbf{F}_k^{\text{form}} - \nabla [\delta_k (\eta_{k-1/2} p_{k-1/2})]. \quad (45.51)$$

Since they differ by a gradient, the form stress and dual form stress have identical curls and so they contribute the same interfacial pressure torque as part of the layer vorticity evolution

$$-\nabla \times (h_k \nabla p_k) = \nabla \times \mathbf{F}_k^{\text{dual}} = \nabla \times \mathbf{F}_k^{\text{form}}. \quad (45.52)$$

The dual form stress is somewhat more convenient since, when the eddies are geostrophic, we can convert the eddy correlation into an eddy transport of buoyancy. We encountered that feature in Section 25.7 when studying the meridional transport from geostrophic eddies in a zonally reentrant channel.

### *Thickness and pressure gradient correlation*

Making use of the potential energy and dual form stress as given by equation (45.49) allows us to write the ensemble mean thickness weighted pressure gradient as

$$-\overline{h_k \nabla p_k} = -\nabla \overline{\mathcal{P}_k} - \delta_k [\overline{\eta_{k-1/2} \nabla p_{k-1/2}}] \quad (45.53)$$

where minus the potential energy gradient is decomposed as

$$-\nabla \overline{\mathcal{P}_k} = -(g \rho_k / 2) \delta_k [\nabla (\overline{\eta_{k-1/2}})^2 + \nabla (\overline{\eta'_{k-1/2}})^2] \quad (45.54)$$

and the vertical convergence of the dual form stress is

$$-\delta_k [\overline{\eta_{k-1/2} \nabla p_{k-1/2}}] = -\delta_k [\overline{\eta_{k-1/2} \nabla p_{k-1/2}} + \overline{\eta'_{k-1/2} \nabla p'_{k-1/2}}]. \quad (45.55)$$

We are thus led to decompose the thickness weighted pressure gradient correlation as

$$-\overline{h'_k \nabla p'_k} = -(g \rho_k / 2) \nabla [\delta_k (\overline{\eta'_{k-1/2}})^2] - \delta_k [\overline{\eta'_{k-1/2} \nabla p'_{k-1/2}}]. \quad (45.56)$$

Again, the first term on the right hand side arises from the eddy potential energy and the second term from the dual eddy interfacial form stress. For orientation, in Figure 45.2 we illustrate the deviations of the interface positions relative to the ensemble mean.

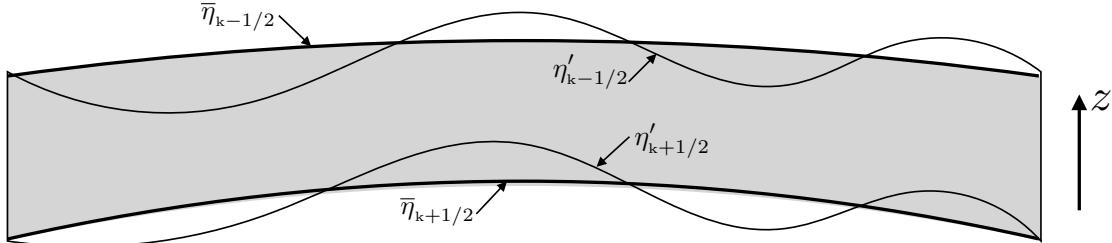


FIGURE 45.2: Schematic of the interface positions for a shallow water layer. The ensemble mean layer interfaces have vertical positions given by  $z = \bar{\eta}_{k\pm 1/2}$ , whereas the fluctuating interfaces are located at  $z = \bar{\eta}_{k\pm 1/2} + \eta'_{k\pm 1/2}$ . As depicted here, the ensemble mean interface positions are not generally horizontal.

### 45.6.3 Zonal and meridional Eliassen-Palm fluxes

Making use of the thickness and pressure gradient correlation in the form of equation (45.56) leads to the thickness weighted momentum equation

$$\begin{aligned} \partial_t (\overline{h} \hat{\mathbf{u}}) + \nabla \cdot (\overline{h} \hat{\mathbf{u}} \otimes \hat{\mathbf{u}}) + f \hat{z} \times \overline{h} \hat{\mathbf{u}} + \overline{h} \nabla \overline{p} / \rho \\ = -\nabla \cdot (\widehat{\overline{h} \mathbf{u}'' \otimes \mathbf{u}''}) - (g \rho_k / 2\rho) \nabla [\delta_k (\overline{\eta'_{k-1/2}})^2] - \delta_k [\overline{\eta'_{k-1/2} \nabla p'_{k-1/2}} / \rho], \end{aligned} \quad (45.57)$$

where we only exposed the interface indices to reduce notational clutter. The subgrid scale correlations on the right hand side can be organized into the divergence of two tensors

$$\nabla \cdot (\bar{h} \widehat{\mathbf{u}'' \otimes \mathbf{u}''}) + (g \rho_k / 2\rho) \nabla [\delta_k \overline{(\eta'_{k-1/2})^2}] + \delta_k \overline{[\eta'_{k-1/2} \nabla p'_{k-1/2}] / \rho} \\ = \begin{bmatrix} \partial_x & \partial_y & \bar{h}^{-1} \delta_k \end{bmatrix} \begin{bmatrix} \bar{h} \widehat{u'' u''} & \bar{h} \widehat{u'' v''} & 0 \\ \bar{h} \widehat{u'' v''} & \bar{h} \widehat{v'' v''} & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad (45.58)$$

$$+ \begin{bmatrix} \partial_x & \partial_y & \bar{h}^{-1} \delta_k \end{bmatrix} \begin{bmatrix} (g \rho_k / 2\rho) [\delta_k \overline{(\eta'_{k-1/2})^2}] & 0 & 0 \\ 0 & (g \rho_k / 2\rho) [\delta_k \overline{(\eta'_{k-1/2})^2}] & 0 \\ (\bar{h}/\rho) \overline{\eta'_{k-1/2} \partial_x p'_{k-1/2}} & (\bar{h}/\rho) \overline{\eta'_{k-1/2} \partial_y p'_{k-1/2}} & 0 \end{bmatrix}. \quad (45.59)$$

The first tensor arises from Reynolds stresses and the second arises from eddy potential energy and eddy dual form stresses. When combined, the columns are the thickness weighted *Eliassen-Palm fluxes* for the zonal (column 1) and meridional (column 2) shallow water momentum equation

$$\mathbf{E}^{(uEP)} = \left[ \bar{h} \widehat{u'' u''} + (g \rho_k / 2\rho) [\delta_k \overline{(\eta'_{k-1/2})^2}] \right] \hat{\mathbf{x}} + \bar{h} \widehat{u'' v''} \hat{\mathbf{y}} + \bar{h} \overline{(\eta'_{k-1/2} \partial_x p'_{k-1/2}) / \rho} \hat{\mathbf{z}} \quad (45.60a)$$

$$\mathbf{E}^{(vEP)} = \bar{h} \widehat{u'' v''} \hat{\mathbf{x}} + \left[ \bar{h} \widehat{v'' v''} + (g \rho_k / 2\rho) [\delta_k \overline{(\eta'_{k-1/2})^2}] \right] \hat{\mathbf{y}} + \bar{h} \overline{(\eta'_{k-1/2} \partial_y p'_{k-1/2}) / \rho} \hat{\mathbf{z}}. \quad (45.60b)$$

We encountered the unaveraged version of these eddy stresses in Sections 31.4.3 and 31.5.9 when studying the shallow water momentum equation. [Maddison and Marshall \(2013\)](#) included the third column of zeros in equation (45.59) to emphasize that the Eliassen-Palm fluxes are the first and second columns to the *Eliassen-Palm flux tensor*. They illustrated the utility of this perspective by considering gauge transformations that result in non-zero elements in the third column.

The Eliassen-Palm fluxes are second order in eddy amplitude; i.e., they are quadratic in eddy fluctuations. Furthermore, they bring together the Reynolds stress, the eddy potential energy, and the dual eddy interfacial form stress. The convergence of the Eliassen-Palm fluxes provides an eddy rectified acceleration on the thickness weighted velocity. To explicitly see this forcing, write the components to the mean field momentum equation (45.57) as<sup>6</sup>

$$\partial_t (\bar{h} \widehat{u}) + \nabla \cdot (\bar{h} \widehat{\mathbf{u}} \widehat{\mathbf{u}}) - f \bar{h} \widehat{v} + \bar{h} \partial_x \bar{p} / \rho = -(\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(uEP)} \quad (45.61a)$$

$$\partial_t (\bar{h} \widehat{v}) + \nabla \cdot (\bar{h} \widehat{\mathbf{u}} \widehat{\mathbf{v}}) + f \bar{h} \widehat{u} + \bar{h} \partial_y \bar{p} / \rho = -(\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(vEP)}. \quad (45.61b)$$

Equations (45.61a) and (45.61b) are isomorphic to the unaveraged horizontal momentum equation (45.1c), yet with the addition of the convergence of the Eliassen-Palm flux on the right hand side that encapsulates rectified effects from eddies. They can be written using the material time derivative (45.29)

$$\frac{D^\sharp \widehat{u}}{Dt} - f \widehat{v} + \partial_x \bar{p} / \rho = -\bar{h}^{-1} (\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(uEP)} \quad (45.62a)$$

$$\frac{D^\sharp \widehat{v}}{Dt} + f \widehat{u} + \partial_y \bar{p} / \rho = -\bar{h}^{-1} (\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(vEP)}. \quad (45.62b)$$

It is notable that these equations only make use of the thickness weighted velocity,  $\widehat{\mathbf{u}}$ , as do the

<sup>6</sup>Recall from equation (45.48) that the operator  $\delta_k$  only acts on interface fields, so that  $\bar{h}^{-1} \delta_k(\bar{h}) = \delta_k$ . This convention thus allows us to unify the horizontal components to the Eliassen-Palm flux with the vertical component, as written in equations (45.60a) and (45.60b).

averaged thickness equation (45.28) and adverged tracer equation (45.35). We advertised this point near the start of this chapter, noting that it greatly facilitates the practical use of the TWA equations. We further this correspondence in Section 45.7 by showing that the vorticity and potential vorticity equations also make use of  $\hat{\mathbf{u}}$ .

#### 45.6.4 Interfacial stresses from geostrophic eddies

In Section 25.7 we studied the rectified effects from geostrophic eddies in a zonally re-entrant channel for a continuously stratified fluid. In that analysis we found that the zonal mean of isopycnal eddy form stresses are equivalent to the meridional eddy flux of buoyancy. We here consider similar questions within the context of the TWA shallow water fluid, here focusing on the interfacial transfer of momentum due to eddy dual form stresses as given by the vertical vectors

$$\mathbf{E}_{\text{form}}^{(\text{uEP})} = \bar{h} (\overline{\eta'_{k-1/2} \partial_x p'_{k-1/2}} / \rho) \hat{\mathbf{z}} \quad (45.63\text{a})$$

$$\mathbf{E}_{\text{form}}^{(\text{vEP})} = \bar{h} (\overline{\eta'_{k-1/2} \partial_y p'_{k-1/2}} / \rho) \hat{\mathbf{z}}. \quad (45.63\text{b})$$

As for the analysis in Section 25.7, we assume the fluctuations are geostrophic. In this manner we introduce an interface geostrophic velocity corresponding to the gradient of the interface pressure fluctuations<sup>7</sup>

$$\partial_x p'_{k-1/2} = f \rho v'_{k-1/2} \quad \text{and} \quad \partial_y p'_{k-1/2} = -f \rho u'_{k-1/2}, \quad (45.64)$$

in which case the dual form stress portion of the Eliassen-Palm fluxes take the form

$$\mathbf{E}_{\text{form}}^{(\text{uEP})} = f \bar{h} (\overline{\eta'_{k-1/2} v'_{k-1/2}}) \hat{\mathbf{z}} \quad (45.65\text{a})$$

$$\mathbf{E}_{\text{form}}^{(\text{vEP})} = -f \bar{h} (\overline{\eta'_{k-1/2} u'_{k-1/2}}) \hat{\mathbf{z}}. \quad (45.65\text{b})$$

For geostrophic eddies, the dual form stress terms take the form of an eddy transport of the area between  $z = \bar{\eta}_{k-1/2}$  and  $z = \eta'_{k-1/2}$  (see Figure 45.2). In a continuously stratified fluid, as in Section 25.7, we can relate the interface fluctuations,  $\eta'$ , to the buoyancy flucutations,  $b'$ , in which case  $\overline{\eta'_{k-1/2} u'_{k-1/2}}$  is proportional to the eddy buoyancy flux. Likewise, the potential energy term can be related to fluctuations in the squared buoyancy.

## 45.7 Vorticity and potential vorticity

We follow the procedure from Chapter 34 to derive the vorticity and potential vorticity for the thickness weighted shallow water equations. In the process, we connect the eddy flux of potential vorticity to the Eliassen-Palm flux.

### 45.7.1 Derivation

Use the vector identities from Sections 34.1 and 34.2 to bring the material evolution equations (45.62a) and (45.62b) into their equivalent vector invariant forms

$$\partial_t \hat{\mathbf{u}} - (f + \hat{\zeta}) \hat{\mathbf{v}} = -\partial_x (\bar{p}/\rho + \hat{\mathbf{u}} \cdot \hat{\mathbf{u}}/2) - \bar{h}^{-1} (\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(\text{uEP})} \quad (45.66\text{a})$$

$$\partial_t \hat{\mathbf{v}} + (f + \hat{\zeta}) \hat{\mathbf{u}} = -\partial_y (\bar{p}/\rho + \hat{\mathbf{u}} \cdot \hat{\mathbf{u}}/2) - \bar{h}^{-1} (\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(\text{vEP})}, \quad (45.66\text{b})$$

<sup>7</sup>Recall that  $\rho$  is the Boussinesq reference density, whereas  $\rho_k$  is the density for layer k.

where we introduced the relative vorticity of the thickness weighted horizontal velocity

$$\hat{\zeta} = \partial_x \hat{v} - \partial_y \hat{u}. \quad (45.67)$$

Taking  $\partial_x$  of the meridional equation (45.66b) and subtracting  $\partial_y$  of the zonal equation (45.66a) renders the evolution equation for absolute vorticity,  $\hat{\zeta}_a = \hat{\zeta} + f$ ,

$$\frac{D^\# \hat{\zeta}_a}{Dt} + \hat{\zeta}_a \nabla \cdot \hat{\mathbf{u}} = \partial_y [\bar{h}^{-1} (\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(uEP)}] - \partial_x [\bar{h}^{-1} (\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(vEP)}]. \quad (45.68)$$

Making use of the thickness equation (45.30) to replace  $\nabla \cdot \hat{\mathbf{u}}$  leads to the potential vorticity equation

$$\bar{h} \frac{D^\# \Pi^\#}{Dt} = -\nabla \cdot \mathbf{F}^\# \quad (45.69)$$

where

$$\Pi^\# = \frac{f + \partial_x \hat{v} - \partial_y \hat{u}}{\bar{h}} = \frac{f + \hat{\zeta}}{\bar{h}} \quad (45.70)$$

is the potential vorticity defined with the thickness weighted velocity and ensemble mean thickness. The corresponding eddy potential vorticity flux is a horizontal vector and given in terms of the divergence of the Eliassen-Palm fluxes

$$\mathbf{F}^\# = \hat{\mathbf{x}} [\bar{h}^{-1} (\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(vEP)}] - \hat{\mathbf{y}} [\bar{h}^{-1} (\nabla_z + \hat{\mathbf{z}} \bar{h}^{-1} \delta_k) \cdot \mathbf{E}^{(uEP)}] + \hat{\mathbf{z}} \times \nabla \Upsilon, \quad (45.71)$$

where  $\Upsilon$  is an arbitrary gauge function.<sup>8</sup> This equation connects the potential vorticity flux to the Eliassen-Palm fluxes and it is known as the *Taylor-Bretherton identity*. Remarkably, the potential vorticity flux also provides the eddy forcing to the thickness weighted velocity equation

$$\partial_t \hat{\mathbf{u}} + (f + \hat{\zeta}) \hat{\mathbf{z}} \times \hat{\mathbf{u}} + \nabla(\bar{p}/\rho + \hat{\mathbf{u}} \cdot \hat{\mathbf{u}}/2) = -\hat{\mathbf{z}} \times (\mathbf{F}^\# - \hat{\mathbf{z}} \times \nabla \Upsilon), \quad (45.72)$$

which can also be written

$$\partial_t \hat{\mathbf{u}} + \hat{\mathbf{z}} \times (\bar{h} \hat{\mathbf{u}} \Pi^\# + \mathbf{F}^\# - \hat{\mathbf{z}} \times \nabla \Upsilon) + \nabla(\bar{p}/\rho + \hat{\mathbf{u}} \cdot \hat{\mathbf{u}}/2) = 0, \quad (45.73)$$

where  $\bar{h} \hat{\mathbf{u}} \Pi^\# + \mathbf{F}^\# - \hat{\mathbf{z}} \times \nabla \Upsilon$  is the net (mean plus eddy plus gauge) potential vorticity flux.

### 45.7.2 Specializing to non-divergent barotropic flow

In Chapter 33 we studied the mechanics of a two dimensional fluid whose horizontal flow is non-divergent. As for the shallow water, the fluid moves as columns. However, since the horizontal flow is non-divergent, each column is rigid and so there is no stretching or squashing of columns. Correspondingly, there are no form stresses acting on these columns. We specialize the shallow water analysis in this section to rigid columnar motion as a means to verify that the Reynolds stresses appearing in the Eliassen-Palm flux formulation correspond to that arising in the non-divergent barotropic model.

For rigid fluid columns, the thickness weighted average reduces to just the ensemble mean since all layer thicknesses are fixed. Correspondingly, there are no form stresses acting at the layer interfaces since interfaces are horizontal. Hence, the Eliassen-Palm fluxes (45.60a) and

<sup>8</sup>Equation (129) in [Young \(2012\)](#) should have a gauge function on its right hand side, which follows from his footnote #3. We provide an example of the need for a gauge function in Section 45.7.2.

(45.60b) reduce to just their Reynold stress contributions

$$h^{-1} \mathbf{E}^{(uEP)} = \overline{u' u'} \hat{\mathbf{x}} + \overline{u' v'} \hat{\mathbf{y}} \quad (45.74a)$$

$$h^{-1} \mathbf{E}^{(vEP)} = \overline{u' v'} \hat{\mathbf{x}} + \overline{v' v'} \hat{\mathbf{y}}. \quad (45.74b)$$

The corresponding eddy potential vorticity flux (45.71), absent the gauge term, is

$$\mathbf{F}^\sharp = \hat{\mathbf{x}} \nabla \cdot [\overline{u' v'} \hat{\mathbf{x}} + \overline{v' v'} \hat{\mathbf{y}}] - \hat{\mathbf{y}} \nabla \cdot [\overline{u' u'} \hat{\mathbf{x}} + \overline{u' v'} \hat{\mathbf{y}}] \quad (45.75a)$$

$$= \hat{\mathbf{x}} [\partial_x(\overline{u' v'}) + \partial_y(\overline{v' v'})] - \hat{\mathbf{y}} [\partial_x(\overline{u' u'}) + \partial_y(\overline{u' v'})]. \quad (45.75b)$$

Does the eddy potential vorticity flux (45.75b) agree, to within a gauge function, with the eddy flux resulting from a direct decomposition into eddy and mean within a two dimensional non-divergent model? To address this question, recall that the advective flux of potential vorticity for the two dimensional non-divergent flow is given by equation (33.41)

$$\mathbf{u} q = \mathbf{u} f + \nabla \cdot (\hat{\mathbf{z}} \times \mathcal{E}), \quad (45.76)$$

where  $\mathcal{E}$  is the trace-free anisotropic portion of the kinetic stress tensor

$$\mathcal{E} = \begin{bmatrix} -(u^2 - v^2)/2 & -uv \\ -uv & (u^2 - v^2)/2 \end{bmatrix}. \quad (45.77)$$

The mean of the potential vorticity flux is (45.76) is given by

$$\overline{\mathbf{u} q} = \overline{\mathbf{u} f} + \overline{\mathbf{u}' q'}, \quad (45.78)$$

where the flux computed from the mean fields is

$$\overline{\mathbf{u} q} = \overline{\mathbf{u}} (f + \bar{\zeta}), \quad (45.79)$$

whereas the eddy potential vorticity flux is

$$\overline{\mathbf{u}' q'} = \nabla \cdot [\hat{\mathbf{z}} \times \overline{\mathcal{E}(\mathbf{u}')}] \quad (45.80a)$$

$$= \hat{\mathbf{x}} [\partial_x(\overline{u' v'}) + \partial_y(\overline{v' v'} - \overline{u' u'})/2] + \hat{\mathbf{y}} [\partial_x(\overline{v' v'} - \overline{u' u'})/2 - \partial_y(\overline{u' v'})] \quad (45.80b)$$

$$= \hat{\mathbf{x}} [\partial_x(\overline{u' v'}) + \partial_y(\overline{v' v'})] - \hat{\mathbf{y}} [\partial_x(\overline{u' u'}) + \partial_y(\overline{u' v'})] + (\hat{\mathbf{x}} \partial_y - \hat{\mathbf{y}} \partial_x) \overline{\mathbf{u}' \cdot \mathbf{u}'}/2 \quad (45.80c)$$

$$= \mathbf{F}^\sharp - \hat{\mathbf{z}} \times \nabla(\overline{\mathbf{u}' \cdot \mathbf{u}'})/2. \quad (45.80d)$$

Hence,  $\overline{\mathbf{u}' q'}$  agrees with  $\mathbf{F}^\sharp$  in equation (45.75b) to within a gauge function given by the rotated gradient of the eddy kinetic energy, so that their divergences are equal

$$\nabla \cdot \mathbf{F}^\sharp = \nabla \cdot \overline{\mathbf{u}' q'}. \quad (45.81)$$

That is, when diagnosing contributions to the potential vorticity flux, the gauge term,  $-\hat{\mathbf{z}} \times \nabla(\overline{\mathbf{u}' \cdot \mathbf{u}'})/2$ , plays no role in forcing potential vorticity.





**Part IX**

**Scalar mechanics**

A scalar field provides a number (e.g., temperature, humidity, density) at every point in the fluid. This property contrasts to a vector field, such as velocity, which provides a vector valued function at each point. In this part of the book, we focus on tracers, density, and Archimedean buoyancy, which are scalar fields that offer fundamental information about the mechanics of fluid motion. Much of the material is relevant to both the atmosphere and ocean, though we also present specialized topics motivated from ocean applications. Our study of *scalar mechanics* complements the mechanics of momentum, vorticity, and energy considered earlier in this book.

Here is a synopsis of the chapters in this part of the book.

- In Chapter 46 we develop the basic maths and physics of advection and diffusion, which are the two processes that affect the evolution of *conservative tracers*.
- In Chapter 47 we introduce the notions of wave-mean flow interactions that give rise to eddy-induced advection (or skew diffusion) as well as diffusion. This chapter makes use of both geopotential coordinates as well as isopycnal coordinate equations from Chapter 44, thus providing an example of the dual roles these coordinates make in describing turbulent geophysical flows.
- Chapter 48 presents elements of standard tracer parameterizations used for coarse resolution models of the ocean circulation. We here study the mathematics of the parameterizations and connect to the basic physics.
- Chapter 49 focuses on ocean density and the study of global sea level. This topic is of growing concern for climate science given the role of the ocean as the dominant sink of anthropogenically induced enthalpy.
- Chapter 50 considers a theoretical study of water mass transformation analysis.

# Chapter 46

## Tracer advection and diffusion

In this chapter we study physical and mathematical aspects of advection and diffusion. These two processes affect matter concentrations through stirring and mixing, and as such we frame the presentation in terms of the tracer equation. Advection and diffusion also affect momentum and vorticity, though both are also affected by other processes such as pressure and Coriolis (for momentum; see Chapter 17) and stretching, twisting, and baroclinicity (for vorticity; see Chapter 35).

In the absence of diffusion, advection imparts a reversible stirring of fluid elements that increases the magnitude of tracer gradients. In contrast, diffusion provides an irreversible mixing of fluid elements that reduces the magnitude of tracer gradients. When acting together, advection is no longer a pure stirring and diffusion is no longer a pure mixing. [Eckart \(1948\)](#) articulated what has become the standard conceptual paradigm for stirring and mixing in geophysical fluids, with elements of that paradigm reflected in this chapter.

### CHAPTER GUIDE

We make use of the tracer equation derived in Section 15.1, with results relevant for matter transport in both the atmosphere and ocean. Notably, results for the oceanic Boussinesq fluid of Chapter 23 are found merely by setting the density factor,  $\rho$ , to a constant where it appears in the non-Boussinesq equations. The discussion of Green's functions in Section 46.10 supplements the [Haine et al. \(2022\)](#) review paper that summarizes many applications of Green's functions for passive ocean tracers. We assume familiarity with the Green's function material presented in Chapter 4.

46.1	Loose threads	1112
46.2	Introduction	1112
46.3	Diffusion physics	1113
46.3.1	Diffusion of matter by random molecular motions	1113
46.3.2	Diffusion of matter by random turbulent motions	1114
46.3.3	Fick's law for matter diffusion	1114
46.3.4	Fourier's law for heat diffusion	1115
46.3.5	Newtonian frictional stress and momentum diffusion	1116
46.3.6	Further study	1117
46.4	Diffusion maths	1117
46.4.1	Sample diffusion tensors	1117
46.4.2	Evolution of tracer concentration powers	1117

46.4.3	Moments of tracer concentration . . . . .	1118
46.4.4	Connecting tracer variance to the diffusion operator . . . . .	1119
46.5	Advection physics . . . . .	<b>1121</b>
46.5.1	The advection equation . . . . .	1122
46.5.2	Eulerian time tendencies from advection . . . . .	1122
46.5.3	Impermeability property of tracer isosurfaces . . . . .	1123
46.6	Advection maths . . . . .	<b>1123</b>
46.6.1	Material constancy of $C^T$ . . . . .	1123
46.6.2	Mass transport . . . . .	1124
46.6.3	Advective tracer fluxes and skew tracer fluxes . . . . .	1124
46.6.4	Skew diffusion . . . . .	1125
46.6.5	A comment about skew fluxes and Lagrangian kinematics . . . . .	1126
46.6.6	Further reading . . . . .	1126
46.7	Advection and skewness . . . . .	<b>1127</b>
46.7.1	Choosing a gauge . . . . .	1127
46.7.2	Vertical gauge . . . . .	1128
46.7.3	Boundary conditions . . . . .	1129
46.8	Finite volume budgets with eddy velocities . . . . .	<b>1129</b>
46.8.1	Advective formulation . . . . .	1130
46.8.2	Skew flux formulation . . . . .	1131
46.8.3	Domain with a tracer boundary . . . . .	1131
46.8.4	Budget for a region with interior sides . . . . .	1133
46.8.5	Budget for a stirred fluid in a region with interior sides . . . . .	1136
46.9	Active tracers and dia-surface flow . . . . .	<b>1138</b>
46.9.1	Adiabatic flow . . . . .	1139
46.9.2	Diabatic processes generating dia-surface transport . . . . .	1139
46.10	Green's function method for passive tracers . . . . .	<b>1140</b>
46.10.1	Concerning time dependent domain boundaries . . . . .	1140
46.10.2	Passive tracer boundary conditions . . . . .	1141
46.10.3	Advection-diffusion initial-boundary value problem . . . . .	1142
46.10.4	The Green's function and its adjoint . . . . .	1143
46.10.5	Reciprocity relation . . . . .	1143
46.10.6	Composition property . . . . .	1147
46.10.7	Integral expression for the tracer concentration . . . . .	1148
46.10.8	Properties of the solution . . . . .	1149
46.10.9	Boundary propagator . . . . .	1150
46.11	Exercises . . . . .	<b>1152</b>

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## 46.1 Loose threads

- Schematic for the boundary propagator.

## 46.2 Introduction

As derived in Section 15.1, the tracer equation takes on the general form

$$\rho \frac{DC}{Dt} = -\nabla \cdot \mathbf{J}(C), \quad (46.1)$$

where  $\mathbf{J}$  is a flux that embodies molecular diffusion as well as subgrid scale advection and subgrid scale diffusion (Chapter 48). Advective transport appears when transforming to an Eulerian or

laboratory reference frame, in which case

$$\rho \frac{DC}{Dt} = \frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\mathbf{v} \rho C), \quad (46.2)$$

with  $\mathbf{v} \rho C$  the advective flux. In the absence of diffusion, advection renders a reversible stirring and stretching of fluid elements that generally increases the magnitude of concentration gradients. Advection does so while maintaining, for each fluid element, a fixed mass for all matter constituents and fixed specific entropy.<sup>1</sup> In contrast, diffusion affects an irreversible exchange, or mixing, of matter, thermodynamic, and mechanical properties between fluid elements. Correspondingly, diffusion reduces the magnitude of property gradients as it irreversibly exchanges properties between fluid elements.

## 46.3 Diffusion physics

The continuum approximation from Chapter 11 proposes that a macroscopic description of fluid motion does not require direct information about the motion of individual molecules. Nonetheless, random molecular motion and properties of the constituent molecules impact on fluid motion through the process of *molecular diffusion* of matter. Analogously, the random motion of fluid elements within a turbulent fluid give rise to *turbulent diffusive transport*.<sup>2</sup> In this section, we explore the basic physical nature of molecular and turbulent diffusion.

### 46.3.1 Diffusion of matter by random molecular motions

Consider a fluid comprised of a single matter constituent, such as a lake of pure  $H_2O$ . As discussed in Section 12.2, for a macroscopic description of this single-component fluid, a constant mass fluid element is identical to a constant mass material fluid parcel. That is, there is no mixing of matter since there is just a single matter component. Now place a dye tracer (Section 15.2) into a corner of the lake so that the lake is comprised of two material components ( $H_2O$  and dye). Even in the absence of ambient macroscopic fluid motion, the random motion of water and dye molecules produces an exchange of matter constituents between fluid elements. Consequently, the dye spreads outward from its initial position; i.e., it *diffuses* into the surrounding water.

We introduced the notion of matter exchange between fluid elements when discussing the tracer equation in Section 15.1. In the present context, matter exchange occurs through the random motion of molecules acting in the presence of a matter concentration gradient. Even though the continuum approximation has removed all explicit concern for details of molecular motion, we confront the underlying molecular nature of matter since molecular motions have a measurable impact on macroscopic fluid properties. This transport of matter by random molecular motions is known as *molecular diffusion*. A statistical description of molecular diffusion was first given by Einstein through his investigations of Brownian Motion ([Einstein, 1905](#)).

Diffusion of matter is a familiar process. For example, the odor from an open perfume bottle will spread throughout a room, even in the absence of macroscopic motion of air in the room. When the ambient macroscopic motion is zero, the spread of the perfume arises from random molecular motions whose properties depend on details of the molecules (e.g., their size, speed, inter-molecular forces). The time scale for molecular diffusion is generally much longer than the analogous *turbulent diffusion* that results if there is random motion in the macroscopic fluid, such as occurs by placing a fan next to the perfume bottle.

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<sup>1</sup>Recall from Chapter 20 that specific entropy remains materially constant on fluid elements in the absence of mixing.

<sup>2</sup>For our purposes, turbulence is characterized by a quasi-random motion of fluid elements.

### 46.3.2 Diffusion of matter by random turbulent motions

It is common for geophysical fluid systems to exhibit some form of turbulent motion. In these systems, the spread of matter by macroscopic turbulent motion is many times more efficient than the spread of matter from molecular motion. In such cases, we are justified in ignoring molecular diffusion since the efficiency of the turbulent diffusive transport is far greater than that from molecular diffusion.

[Taylor \(1921\)](#) described the statistical properties of turbulent diffusion, with many of his insights forming the basis for theories of how turbulent motion impacts on matter concentrations. In Taylor's theory, turbulent diffusion is not concerned with details of the molecular properties of the fluid. Rather, the properties of turbulent diffusion (e.g., the efficiency of the turbulent diffusion) depend just on the nature of the turbulent motion of fluid elements. In this way, turbulent diffusion as described by Taylor is a phenomena that sits fully in the realm of continuum mechanics, whereas molecular diffusion is a subject for the kinetic theory of gases. Correspondingly, each type of turbulent motion gives rise to a distinct form of turbulent diffusion. For example, in a geophysical context, turbulent diffusion associated with the breaking of internal gravity waves is distinct from turbulent diffusion by geostrophic eddies.

### 46.3.3 Fick's law for matter diffusion

Consider a fluid with a non-uniform matter concentration such as that drawn for a one-dimensional case in Figure 46.1. Random motion, due either to molecular motion or turbulent fluctuations, will transfer matter across an arbitrary point, line, or plane. Random motion preferentially moves matter from regions of high concentration to regions of low concentration, thus smoothing gradients. To a good approximation, the mass flux (mass per time per cross-sectional area) of matter is linearly proportional to the concentration gradient, and thus can be written in the form

$$\mathbf{J} = -\kappa \rho \nabla C. \quad (46.3)$$

In this equation, we introduced the positive proportionality factor  $\kappa > 0$ , known as the *kinematic diffusivity*, whereas the product  $\kappa \rho$  is known as the *dynamic diffusivity*

$$\kappa \quad \text{kinematic diffusivity with SI units } \text{m s}^{-2} \quad (46.4)$$

$$\rho \kappa \quad \text{dynamic diffusivity with SI units } \text{kg m}^{-2} \text{ s}^{-2}. \quad (46.5)$$

The kinematic diffusivity has dimensions of squared length per time and it sets the efficiency or strength of the diffusion. The diffusive flux (46.3) is known as Fick's law of matter diffusion. It is the most common mathematical form used to represent the mixing of matter through diffusion. Note that the minus sign in the diffusive flux arises since the flux is directed down the concentration gradient.

The kinematic diffusivity has physical dimensions equal to the product of a length and a speed. For molecular diffusion, the kinematic diffusivity is proportional to the mean free path,  $L_{\text{mfp}}$  (see Section 11.3.3), and the root-mean-square molecular speed,  $v_{\text{rms}}$  (see Section 11.3.4). Each of these properties is a function of the molecules comprising the matter. For air, the mean free path is roughly  $2 \times 10^{-7}$  m and the RMS speed is 500 m s<sup>-1</sup>, so that  $L_{\text{mfp}} v_{\text{rms}} \approx 10^{-4} \text{ m}^2 \text{ s}^{-1}$ . The precise value for the molecular diffusivity depends on the molecular properties of the matter diffusing through air. For turbulent diffusion, Prandtl suggested that we consider a characteristic length and velocity scale determined by properties of the turbulent flow. The turbulent length scale (also called the *mixing length*) is generally much larger than the molecular mean free path, whereas the turbulent velocity scale is much smaller than molecular speeds. Determination of

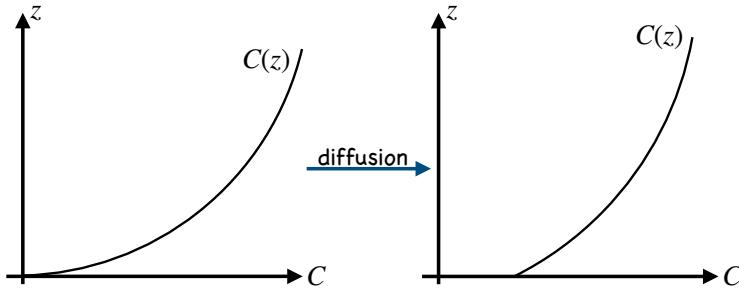


FIGURE 46.1: Shown here is a line graph illustrating the concentration,  $C$ , of a tracer drawn as a function of the space coordinate  $z$ , with the left panel showing the concentration at an earlier time than the right panel. Across any arbitrary point, transport of matter through random motions generally reduces the magnitude of the concentration gradient; i.e., the diffusive transport is down the concentration gradient. For example, where the concentration is relatively high, random motion mixes this high concentration with adjacent lower concentration, acting to lower the concentration in the originally high concentration region and raise the concentration in the originally low concentration region. In this particular example,  $\partial C / \partial z > 0$ , so that random fluid motions (either molecular or turbulent) lead to a diffusive flux directed in the  $-\hat{z}$  direction; i.e., downward. This downward flux brings high concentration fluid into the lower/deeper regions and low concentration fluid into higher/shallower regions. The concentration is uniform in equilibrium, leading to a flat concentration profile.

these turbulent length and velocity scales is subject to large uncertainties and is the topic of much research.

In regions where the diffusive flux is not a constant, there will be a net transport of matter that leads to the reduction of the tracer concentration gradient. At a particular point in space, the concentration changes in time according to the convergence of the diffusive flux

$$\rho \frac{DC}{\partial t} = -\nabla \cdot \mathbf{J} = \nabla \cdot (\kappa \rho \nabla C). \quad (46.6)$$

That is, the concentration increases in regions where the diffusive flux,  $\mathbf{J}$ , converges, and decreases where the flux diverges. Expanding the divergence operator leads to

$$\rho \frac{DC}{\partial t} = \nabla(\kappa \rho) \cdot \nabla C + \rho \kappa \nabla^2 C. \quad (46.7)$$

The first term is nonzero in regions where the dynamic diffusivity,  $\kappa \rho$ , spatially varies. The second term is nonzero in regions where the curvature of the concentration is nonzero. Correspondingly, when the tracer concentration is uniform in space then both terms vanish, whereas the Laplacian term also vanishes when the concentration is linear in space.

#### 46.3.4 Fourier's law for heat diffusion

In the same way that matter concentration gradients lead to diffusion by random motions, temperature gradients lead to diffusion of heat. The corresponding phenomenological relation is known as Fourier's law, with the diffusive flux given by

$$\mathbf{J} = -\gamma \rho \nabla T, \quad (46.8)$$

where  $\gamma > 0$  is the temperature diffusivity. As for the matter diffusivity, the molecular thermal diffusivity can be expressed in terms of fundamental properties of the fluid, and it is different from the matter diffusivity. In general, matter diffuses by molecular processes slower than heat, so that the matter molecular diffusivity is smaller than the heat molecular diffusivity. In contrast, the turbulent thermal diffusivity is roughly the same as the matter diffusivity, since the turbu-

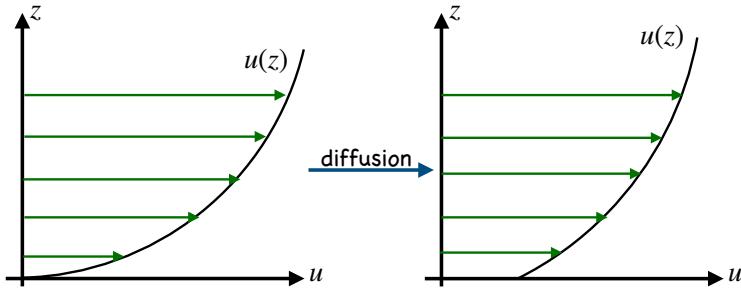


FIGURE 46.2: Shown here is a line graph illustrating the zonal velocity,  $u$ , as a function of the space coordinate  $z$ , with the left panel showing the velocity at an earlier time than the right panel. Across any arbitrary point, transport of momentum through random motions generally reduces the magnitude of the velocity gradient; i.e., the diffusive transport leads to a viscous stress that acts to reduce the velocity shear.

lent diffusion of matter and heat are both mediated by the same turbulent fluctuations of fluid elements.

### 46.3.5 Newtonian frictional stress and momentum diffusion

In the same way that matter concentration and temperature gradients lead to diffusion by random motions, the momentum of fluid elements is exchanged through diffusion in the presence of viscosity. The corresponding phenomenological relation is known as Newton's law of viscous friction. As momentum is a vector, a general treatment of momentum transport through irreversible viscous processes involves a second order stress tensor and a fourth order viscosity tensor. For the specific case shown in Figure 46.2, with shear (i.e., nonzero velocity gradient) in a single direction, Newtonian frictional stress takes the form

$$\tau = \rho \mu \frac{\partial u}{\partial z}, \quad (46.9)$$

where  $\mu > 0$  is the kinematic viscosity. Note the absence of a minus sign, in contrast to diffusive fluxes of scalars. The sign difference arises since it is the divergence of the stress tensor that leads to contact forces on the fluid, whereas it is the convergence of diffusive fluxes that leads to diffusion of matter and heat. We consider these general properties of the stress tensor when exploring the fluid dynamical equations in Chapter 17 and the nature of stress in Chapter 18.

For geophysical fluid mechanics, we are most generally interested in the molecular viscosity of water and air. Quite generally, the dynamic viscosity of water ( $\rho \mu$ ) is about  $10^2$  times larger than that for air. But since the density of water is about  $10^3$  times larger than air, the kinematic viscosity of air is roughly 10 times greater than that of water.

The molecular kinematic viscosity can be expressed in terms of fundamental properties of the fluid, and it is different from the molecular matter diffusivity and molecular thermal diffusivity. For some turbulent processes, the turbulent viscosity is proportional to the scalar diffusivity. In general, the non-dimensional ratio of the viscosity to the diffusivity is known as the *Prandtl* number

$$\text{Pr} = \frac{\mu}{\kappa}. \quad (46.10)$$

Theories for the turbulent Prandtl number are largely empirical in nature, with first principles arguments elusive.

### 46.3.6 Further study

More thorough treatments of molecular diffusion for ideal gases can be found in books that describe the kinetic theory of gases, such as [Reif \(1965\)](#) and [Huang \(1987\)](#). The more terse treatment given in this section largely follows that from Section 1.5 of [Kundu et al. \(2016\)](#). A lucid treatment of Brownian motion in the context of turbulent diffusion is given by [Vallis \(2017\)](#).

## 46.4 Diffusion maths

We now explore various mathematical properties of the diffusion equation, here generalized to allow for distinct behavior in the different directions. Such distinctions are relevant especially in stratified fluids, where turbulent mixing across stratification surfaces is suppressed relative to turbulent mixing parallel to these surfaces (see Section 24.4). For this purpose, introduce the second order symmetric and positive definite diffusion tensor  $\mathbb{K}_{mn} = \mathbb{K}_{nm}$ . The resulting diffusive tracer flux takes the form

$$J_m = -\rho \mathbb{K}_{mn} \frac{\partial C}{\partial x^n}, \quad (46.11)$$

and the corresponding material diffusion equation is

$$\rho \frac{DC}{Dt} = -\nabla \cdot \mathbf{J} = \frac{\partial(\rho \mathbb{K}_{mn} \partial_n C)}{\partial x_m}. \quad (46.12)$$

### 46.4.1 Sample diffusion tensors

For the isotropic case of molecular diffusion considered in equation (46.3), the diffusion tensor takes on the form

$$\mathbb{K}_{mn} = \kappa \delta_{mn} \quad \text{isotropic diffusion.} \quad (46.13)$$

If we rotate the diffusive fluxes to be along surfaces of constant  $\gamma$ , then

$$\mathbb{K}_{mn} = \kappa (\delta_{mn} - \hat{\gamma}_m \hat{\gamma}_n) \quad \text{rotated diffusion,} \quad (46.14)$$

where

$$\hat{\gamma} = \frac{\nabla \gamma}{|\nabla \gamma|} \quad (46.15)$$

is the normal to the surface. The most common case in oceanography is to set  $\gamma$  equal to a measure of the buoyancy, in which case we have *neutral diffusion* (see Section 48.4).

### 46.4.2 Evolution of tracer concentration powers

For certain applications it is of interest to determine how diffusion acts on powers of the tracer concentration. For this purpose consider the material evolution of  $C^\Gamma$ , where  $\Gamma \geq 1$

$$\rho \frac{DC^\Gamma}{Dt} = \Gamma C^{\Gamma-1} \rho \frac{DC}{Dt} \quad (46.16a)$$

$$= -\Gamma C^{\Gamma-1} \nabla \cdot \mathbf{J} \quad (46.16b)$$

$$= -\Gamma \nabla \cdot (C^{\Gamma-1} \mathbf{J}) + \Gamma (\Gamma - 1) C^{\Gamma-2} \nabla C \cdot \mathbf{J} \quad (46.16c)$$

$$= \partial_m \left[ \rho \mathbb{K}_{mn} \frac{\partial C^\Gamma}{\partial x^n} \right] - \rho \Gamma (\Gamma - 1) C^{\Gamma-2} \frac{\partial C}{\partial x^n} \mathbb{K}_{mn} \frac{\partial C}{\partial x^m} \quad (46.16d)$$

$$= -\nabla \cdot \mathbf{J}(C^\Gamma) + \Gamma (\Gamma - 1) C^{\Gamma-2} \mathbf{J} \cdot \nabla C. \quad (46.16e)$$

The first term in equation (46.16e) is the convergence of the diffusive flux defined in terms of  $C^\Gamma$ , and it acts to diffuse  $C^\Gamma$  just like diffusion acts on  $C$ . The second term in equation (46.16e) is negative since the diffusion tensor is symmetric and positive-definite

$$\mathbf{J} \cdot \nabla C = -\rho \mathbb{K}_{mn} \frac{\partial C}{\partial x^m} \frac{\partial C}{\partial x^n} < 0. \quad (46.17)$$

That is, the diffusive flux corresponding to any positive definite and symmetric tensor is oriented down the tracer concentration gradient. Consequently, the second term in equation (46.16e) always acts to reduce the magnitude of  $C^\Gamma$  towards zero. We make use of this result in Section 46.4.3 when considering moments of tracer concentration.

### 46.4.3 Moments of tracer concentration

Consider the evolution of domain integrated tracer concentration and its powers, and focus on impacts just from diffusion. For that purpose, assume the boundaries are insulating so that  $\mathbf{J} \cdot \hat{\mathbf{n}} = 0$  with  $\hat{\mathbf{n}}$  the outward normal at the boundary. Also assume the total fluid mass in the domain remains fixed

$$m = \int \rho dV \iff \frac{dm}{dt} = 0. \quad (46.18)$$

We can thus treat the domain as material given that there is no exchange of mass or tracer across the boundaries.

#### *Domain average tracer concentration*

The domain averaged tracer concentration is given by

$$\bar{C} = \frac{\int C \rho dV}{m}, \quad (46.19)$$

and it follows that its time derivative vanishes since

$$m \frac{d\bar{C}}{dt} = \frac{d}{dt} \int C \rho dV = \int \frac{DC}{Dt} \rho dV = - \int \nabla \cdot \mathbf{J} \rho dV = - \oint \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} = 0, \quad (46.20)$$

where we set  $\mathbf{J} \cdot \hat{\mathbf{n}} = 0$  to reach the last equality. Also note that we brought the time derivative inside the integral as a material derivative since the region is itself material, thus allowing us to make use of Reynold's transport theorem from Section 15.3.6. The result (46.20) follows since there is no change in the total mass of fluid nor is there any exchange of tracer across the boundaries. Hence, the domain averaged tracer concentration remains fixed in time.

#### *Variance of tracer within the domain*

The variance of the tracer concentration is defined by

$$\text{var}(C) \equiv \frac{\int (C - \bar{C})^2 \rho dV}{m} = \bar{C^2} - \bar{C}^2 \geq 0. \quad (46.21)$$

The tracer variance measures the deviation of the tracer concentration relative to the domain averaged concentration. Since the domain average remains fixed in time, the time change of the variance is given by

$$\frac{d[\text{var}(C)]}{dt} = \frac{d\bar{C^2}}{dt}. \quad (46.22)$$

Thus, it is common to refer to  $\overline{C^2}$  as the tracer variance, though strictly speaking only their time derivatives are equal as per equation (46.22). Performing the time derivative, and again noting that the domain is material thus allowing us to use Reynolds transport theorem, renders

$$\frac{d\overline{C^2}}{dt} = \frac{d}{dt} \int C^2 \rho dV = 2 \int C \frac{DC}{Dt} \rho dV = -2 \int C \nabla \cdot \mathbf{J} \rho dV = 2 \int \nabla C \cdot \mathbf{J} \rho dV. \quad (46.23)$$

The final equality again made use of the assumed boundary condition  $\mathbf{J} \cdot \hat{\mathbf{n}} = 0$ . The time change in the tracer variance is thus determined by the integral of the projection of the tracer flux onto the tracer gradient. We already saw from equation (46.17) that diffusive fluxes are oriented down the tracer gradient. Consequently, diffusion of the tracer concentration results in a reduction in tracer variance

$$\frac{d[\text{var}(C)]}{dt} = \frac{d\overline{C^2}}{dt} \leq 0. \quad (46.24)$$

This result further supports our preconceived notions of diffusion as a process that removes differences (i.e., gradients) within the tracer field.

#### *Evolution of arbitrary moments*

Proceeding as before, and dropping boundary contributions, it is straightforward to show that the time derivative of an arbitrary tracer moment is given by

$$\frac{d\overline{C^\Gamma}}{dt} = \Gamma(\Gamma - 1) \int C^{\Gamma-2} \nabla C \cdot \mathbf{J} dV \leq 0. \quad (46.25)$$

For  $\Gamma = 0$  we have an expression of mass conservation for the domain, whereas  $\Gamma = 1$  is an expression of tracer conservation. The case of  $\Gamma = 2$  yields the tracer variance result (46.24). The result for higher powers also holds. Hence, we conclude that the downgradient orientation of diffusive tracer fluxes acts to dissipate all powers of tracer concentration when integrated globally; i.e., all tracer moments are dissipated by diffusion.

#### 46.4.4 Connecting tracer variance to the diffusion operator

We take a slight foray here into linear operator theory, in which we note that with natural boundary conditions (defined below) on the diffusive tracer flux, the diffusion operator is a linear self-adjoint operator.<sup>3</sup> Consequently, the diffusion operator is related to a negative semi-definite functional (e.g., [Courant and Hilbert, 1953, 1962](#)). In the simplest case, the Laplacian operator  $\nabla^2 C$  is equal to the functional derivative  $\nabla^2 C = \delta \mathcal{F} / \delta C$ , where

$$\mathcal{F} \equiv -\frac{1}{2} \int |\nabla C|^2 \rho d^3x \quad (46.26)$$

is the associated functional. In this subsection we prove this result for a general diffusion tensor  $K_{mn}$  acting on an arbitrary tracer concentration,  $C$ , so long as the diffusion tensor is not a function of the tracer concentration. As detailed by [Griffies et al. \(1998\)](#) and Chapter 16 of [Griffies \(2004\)](#), the connection between the diffusion operator and the functional derivative of the diffusion dissipation provides a useful framework for deriving numerical discretizations of the diffusion operator.

---

<sup>3</sup>We discussed the self-adjoint nature of the diffusion operator in Section 4.5.4 in our study of the Green's function for the diffusion equation.

For this subsection it is useful to write

$$d^3x = dV \quad (46.27)$$

for the volume element. The reason will become apparent when reaching equation (46.35).

### Derivative of the diffusion dissipation functional

We introduce the *diffusion dissipation functional*

$$\mathcal{F} = \int \mathcal{L} d^3x \quad (46.28)$$

where the integrand is the negative semi-definite quadratic form

$$2\mathcal{L} = \mathbf{J} \cdot \nabla C = -\rho \partial_m C \mathbb{K}_{mn} \partial_n C \leq 0. \quad (46.29)$$

Our goal is to relate the diffusion operator, given by the convergence of the diffusion flux,  $\mathcal{R} = -\nabla \cdot \mathbf{J}$ , to the functional derivative of  $\mathcal{F}$ . To compute the functional derivative requires us to insert variations to the tracer field  $\delta C$  into the dissipation functional

$$\delta\mathcal{F} = \int \left[ \delta C \frac{\delta\mathcal{L}}{\delta C} + \delta(\partial_m C) \frac{\delta\mathcal{L}}{\delta(\partial_m C)} \right] d^3x. \quad (46.30)$$

Note that functional variations are small perturbations to the form of the function, in which case

$$C \rightarrow C + \delta C \quad \text{with} \quad |\delta C| \ll |C|. \quad (46.31)$$

Integration by parts on the second term leads to

$$\delta\mathcal{F} = \int \left[ \delta C \frac{\delta\mathcal{L}}{\delta C} + \partial_m \left( \delta C \frac{\delta\mathcal{L}}{\delta(\partial_m C)} \right) - \delta C \partial_m \left( \frac{\delta\mathcal{L}}{\delta(\partial_m C)} \right) \right] d^3x. \quad (46.32)$$

The middle term is a total derivative that integrates to a boundary contribution and the associated *natural boundary condition*

$$\hat{\mathbf{n}} \cdot \frac{\delta\mathcal{L}}{\delta\nabla C} = \hat{\mathbf{n}} \cdot \mathbf{J} = \text{boundary flux}, \quad (46.33)$$

with  $\hat{\mathbf{n}}$  the boundary outward normal. This natural boundary condition is the familiar *Neumann boundary condition* from Chapter 4.

To focus on the connection between the diffusion operator and the diffusion dissipation functional, we ignore boundary fluxes so that the functional variation is given by

$$\delta\mathcal{F} = \int \delta C \left[ \frac{\delta\mathcal{L}}{\delta C} - \partial_m \left( \frac{\delta\mathcal{L}}{\delta(\partial_m C)} \right) \right] d^3x. \quad (46.34)$$

Consequently, the functional derivative is given by

$$(d^3y)^{-1} \frac{\delta\mathcal{F}}{\delta C(y)} = \frac{\delta\mathcal{L}}{\delta C} - \partial_m \left[ \frac{\delta\mathcal{L}}{\delta(\partial_m C)} \right], \quad (46.35)$$

where  $d^3y$  is the volume element at the field point  $\mathbf{y}$ . To reach the last step required the identity

$$\frac{\delta C(\mathbf{x})}{\delta C(\mathbf{y})} = d^3y \delta(\mathbf{x} - \mathbf{y}), \quad (46.36)$$

where  $\delta(\mathbf{x} - \mathbf{y})$  is the Dirac delta function satisfying

$$\int \delta(\mathbf{x} - \mathbf{y}) d^3y = 1, \quad (46.37)$$

so long as the integration range includes the singular point  $\mathbf{x} = \mathbf{y}$ . Note that the delta function has dimensions of inverse volume, which necessitates the appearance of the volume factor,  $d^3y$ , on the right hand side of equation (46.36). The reader should be mindful that many treatments in mathematics texts ignore this extra volume factor. However, for physical applications it is important to maintain dimensional consistency, thus requiring us to retain the volume factor.

#### Connection to the diffusion operator

Reintroducing the specific form of the diffusion integrand  $2\mathcal{L} = -\rho \partial_m C \mathbb{K}_{mn} \partial_n C$  leads to

$$(d^3y)^{-1} \frac{\delta \mathcal{F}}{\delta C(\mathbf{y})} = -\partial_m \left[ \frac{\delta \mathcal{L}}{\delta (\partial_m C)} \right] = \partial_m (\rho \mathbb{K}_{mn} \partial_n C). \quad (46.38)$$

The second equality identifies the diffusion operator, thus revealing the connection between the dissipation functional, the diffusion fluxes, and the diffusion operator

$$(d^3y)^{-1} \frac{\delta \mathcal{F}}{\delta C(\mathbf{y})} = -\nabla \cdot \mathbf{J}(\mathbf{y}) = \mathcal{R}. \quad (46.39)$$

#### Why did we assume $\mathbb{K}_{mn}$ is independent of $C$ ?

There are many geophysical applications in which the diffusion tensor is a function of the tracer concentration, in which case the diffusion equation is no longer a linear differential equation. For example, the neutral diffusion of Section 48.4 makes use of a diffusion tensor that is a function of temperature and salinity gradients. In this case the functional derivative in terms of temperature or salinity appearing in equation (46.38) becomes

$$2 \frac{\delta \mathcal{L}}{\delta (\partial_m C)} = -2\rho \mathbb{K}_{mn} \partial_n C - \rho \partial_m C \partial_n C \frac{\delta \mathbb{K}_{mn}}{\delta (\partial_m C)}. \quad (46.40)$$

The specific form of the term  $\delta \mathbb{K}_{mn} / \delta (\partial_m C)$  depends on details of the diffusion tensor. Hence, the general results derived above for the linear diffusion equation no longer hold for this nonlinear diffusion equation. We have more to say about nonlinear advection-diffusion in Section 46.9.

## 46.5 Advection physics

A *perfect* or *ideal* fluid is comprised of material fluid elements whose matter content and thermodynamic properties remain fixed. From the discussion of molecular diffusion in Section 46.3, we know that a perfect fluid can at most consist of a single matter constituent and uniform thermodynamic properties. The reason is that in the presence of multiple constituents with non-uniform concentrations, molecular motions irreversibly exchange matter among fluid elements. This matter exchange, or mixing, breaks the assumption of a perfect fluid. Nonetheless, we find many

occasions to ignore molecular diffusion when focusing on macroscopic motions of the continuum fluid. Such is the case when considering the advection equation in the absence of any mixing.

### 46.5.1 The advection equation

In the absence of mixing or other irreversible processes, the matter content of a fluid element remains fixed as the element moves with the fluid. Since the total mass of the element is also constant, then the tracer concentration remains constant and thus satisfies the reversible (source-free) *advection equation*

$$\frac{DC}{Dt} = \frac{\partial C}{\partial t} + \mathbf{v} \cdot \nabla C = 0. \quad (46.41)$$

The first equality relates the material time derivative to the Eulerian time derivative plus advective transport (see Section 12.5), with  $\mathbf{v}$  the velocity of a fluid element. We can convert the *material* form of the advection equation (46.41) into its flux-form by combining with the mass continuity equation (14.6)

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0, \quad (46.42)$$

which yields

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho C \mathbf{v}) = 0. \quad (46.43)$$

Again, the material form of the advection equation is the trivial statement that tracer concentration remains constant on a fluid element in the absence of sources or mixing. Hence, a general solution to the advection equation is given by

$$C(\mathbf{x}, t) = C[\mathbf{X}(0)], \quad (46.44)$$

where  $\mathbf{X}(0)$  is the initial position of a fluid element that is at the position  $\mathbf{x}$  at time  $t$ . If we know the trajectories for all fluid elements and their initial tracer concentration, we know the tracer concentration for all space and time. For those cases where trajectories are unknown, it is useful to make use of the Eulerian form of the advection equation in order to deduce the evolution of tracer.

### 46.5.2 Eulerian time tendencies from advection

At a point in the fluid, the advection equation (46.41) leads to the Eulerian time tendency for tracer concentration

$$\frac{\partial C}{\partial t} = -\mathbf{v} \cdot \nabla C. \quad (46.45)$$

Geometrically, the tendency arises from the projection of the fluid velocity onto the normal to concentration iso-surfaces. The concentration remains fixed in time (steady) at points where the velocity is parallel to concentration iso-surfaces. From the flux-form advection equation (46.43), the density-weighted tracer concentration (the tracer mass per volume) has an Eulerian time tendency given by the convergence of the advective flux

$$\frac{\partial(\rho C)}{\partial t} = -\nabla \cdot (\rho C \mathbf{v}). \quad (46.46)$$

The tendency vanishes at a point if there is no convergence of tracer mass towards the point.

### 46.5.3 Impermeability property of tracer isosurfaces

We now offer a geometric interpretation of the advection equation

$$\frac{\partial C}{\partial t} + \mathbf{v} \cdot \nabla C = 0, \quad (46.47)$$

following the discussion of dia-surface transport in Section 42.4. For this purpose, introduce the unit normal on a tracer isosurface

$$\hat{\mathbf{n}} = \frac{\nabla C}{|\nabla C|} \quad (46.48)$$

and the normal projection for the velocity of a point on that surface

$$\mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} = -\frac{\partial_t C}{|\nabla C|}. \quad (46.49)$$

The advection equation (46.47) thus can be written as an impermeability condition for a tracer isosurface

$$\rho(\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = 0 \quad \text{on } C \text{ isosurfaces.} \quad (46.50)$$

We encountered this condition in Section 14.4.2 when studying the kinematics of a moving material surface. Hence, in the absence of mixing, tracer isosurfaces are indeed material surfaces since they allow no fluid elements, moving with the fluid velocity  $\mathbf{v}$ , to cross them. This is an important kinematic result that will be extended in Section 46.8.5 to include effects from an eddy induced velocity.

## 46.6 Advection maths

We now explore various mathematical properties of the advection equation. For that purpose, recall the mass continuity equation (46.42) and flux-form tracer advection equation (46.46)

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0 \quad (46.51a)$$

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho C \mathbf{v}) = 0. \quad (46.51b)$$

These equations are manifestly compatible in that the tracer equation (46.51b) reduces to the continuity equation (46.51a) if the tracer concentration is spatially uniform (see Section 15.1.4 for more discussion of compatibility).

### 46.6.1 Material constancy of $C^\Gamma$

A trivial consequence of the material constancy of tracer concentration is that  $C^\Gamma$  is also materially constant, for  $\Gamma$  an arbitrary number. We show this property mathematically by noting that the chain rule holds for a material time derivative, so that

$$\frac{DC^\Gamma}{Dt} = \Gamma C^{\Gamma-1} \frac{DC}{Dt} = 0. \quad (46.52)$$

Likewise, making use of the Eulerian form yields

$$\frac{\partial C^\Gamma}{\partial t} + \mathbf{v} \cdot \nabla C^\Gamma = \Gamma C^{\Gamma-1} \left[ \frac{\partial C}{\partial t} + \mathbf{v} \cdot \nabla C \right] = 0. \quad (46.53)$$

We conclude that advection, in the absence of diffusion, serves to reversibly transport the tracer concentration without altering any of its powers. Correspondingly, all tracer moments are untouched by advection, which contrasts to the case of diffusion considered in Section 46.4.3.

### 46.6.2 Mass transport

The mass density time tendency

$$\frac{\partial \rho}{\partial t} = -\nabla \cdot (\mathbf{v} \rho) \quad (46.54)$$

remains unchanged if the advective mass flux,  $\rho \mathbf{v}$  (dimensions of mass per time per area), is modified by the addition of a total curl

$$\rho \mathbf{v} \rightarrow \rho \mathbf{v}^\dagger = \rho \mathbf{v} + \nabla \times (\rho \Psi^*). \quad (46.55)$$

As in Section 16.5.1, the arbitrariness manifest in equation (46.55) is known as a *gauge symmetry*. The additional mass flux,  $\nabla \times (\rho \Psi^*)$ , leads to no accumulation of mass at a point since it has zero divergence. In the Boussinesq case with  $\rho$  set to a constant  $\rho_0$ , the divergent-free velocity  $\nabla \times \Psi^*$  leads to zero accumulation of volume at a point.

The non-divergent mass flux

$$\rho \mathbf{v}^* \equiv \nabla \times (\rho \Psi^*) \quad (46.56)$$

often arises when we decompose the mass flux into a mean and non-divergent eddy fluctuations. In that context, we make use of the following terminology:

$$\mathbf{v} = \text{Eulerian mean velocity} \quad (46.57a)$$

$$\rho \mathbf{v} = \text{Eulerian mean mass flux} \quad (46.57b)$$

$$\mathbf{v}^* = \text{eddy-induced velocity} \quad (46.57c)$$

$$\rho \Psi^* = \text{eddy-induced mass streamfunction} \quad (46.57d)$$

$$\rho \mathbf{v}^* = \nabla \times (\rho \Psi^*) = \text{eddy-induced mass flux} \quad (46.57e)$$

$$\mathbf{v}^\dagger = \mathbf{v} + \mathbf{v}^* = \text{residual mean velocity} \quad (46.57f)$$

$$\rho \mathbf{v}^\dagger = \rho(\mathbf{v} + \mathbf{v}^*) = \text{residual mean mass flux}. \quad (46.57g)$$

The name “residual mean” is motivated since the sum  $\mathbf{v} + \mathbf{v}^*$  is often smaller than either term individually. That is, the eddy contribution often compensates for the mean, with sum of the mean and eddy representing a residual. We study particular forms of the eddy induced velocity in Chapter 48.

### 46.6.3 Advective tracer fluxes and skew tracer fluxes

Following from the previous discussion, we consider the advection equation with the advective tracer transport determined by the residual mean velocity

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho C \mathbf{v}^\dagger) = 0. \quad (46.58)$$

Given the form (46.56) for the eddy mass flux  $\rho \mathbf{v}^*$ , we can write the *advective tracer flux* as

$$\rho C \mathbf{v}^\dagger = C(\rho \mathbf{v} + \rho \mathbf{v}^*) \quad (46.59a)$$

$$= C \rho \mathbf{v} + C \nabla \times (\rho \Psi^*) \quad (46.59b)$$

$$= C \rho \mathbf{v} + \nabla \times (C \rho \Psi^*) - \nabla C \times \rho \Psi^*. \quad (46.59c)$$

It is the divergence of the tracer flux that determines the time tendency, in which case the total curl plays no role

$$\nabla \cdot (\rho C \mathbf{v}^\dagger) = \nabla \cdot (\rho C \mathbf{v} + \rho C \mathbf{v}^*) \quad (46.60a)$$

$$= \nabla \cdot (\rho C \mathbf{v} - \nabla C \times \rho \Psi^*). \quad (46.60b)$$

That is, the divergence of the advective mass flux equals to the divergence of the *skew tracer flux*

$$\underbrace{\nabla \cdot (\rho C \mathbf{v}^*)}_{\text{advective flux divergence}} = \underbrace{\nabla \cdot (-\nabla C \times \rho \Psi^*)}_{\text{skew flux divergence}} \quad (46.61)$$

since the advective flux and skew flux differ by a rotational flux

$$\mathbf{J}^{\text{adv}} = \mathbf{J}^{\text{skew}} + \mathbf{J}^{\text{rot}} \quad (46.62)$$

where

$$\mathbf{J}^{\text{adv}} = C \rho \mathbf{v}^* \quad \text{and} \quad \mathbf{J}^{\text{skew}} = -\nabla C \times \rho \Psi^* \quad \text{and} \quad \mathbf{J}^{\text{rot}} = \nabla \times (\rho C \Psi^*). \quad (46.63)$$

Notably, the skew tracer flux is neither upgradient nor downgradient. Rather, it is oriented parallel to iso-surfaces of tracer concentration

$$\nabla C \cdot \mathbf{J}^{\text{skew}} = \nabla C \cdot (-\nabla C \times \rho \Psi^*) = 0. \quad (46.64)$$

This orientation serves as motivation for the name “skew.” Figure 46.3 provides a schematic of the skew tracer fluxes.

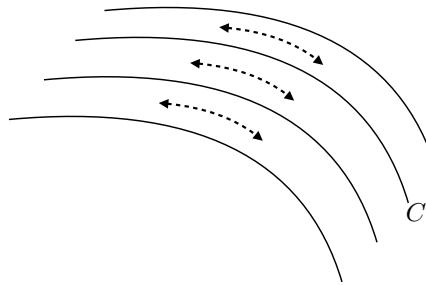


FIGURE 46.3: Skew fluxes (dashed lines with arrows) for a tracer  $C$  are oriented parallel to lines of constant tracer concentration (tracer isolines are the solid lines).

#### 46.6.4 Skew diffusion

Introducing tensor labels brings the skew tracer flux into the form

$$J_m^{\text{skew}} = -(\nabla C \times \rho \Psi^*)_m \quad (46.65a)$$

$$= -\epsilon_{mnp} \frac{\partial C}{\partial x^n} \rho \Psi_p^* \quad (46.65b)$$

$$= -\rho \mathbb{A}_{mn} \frac{\partial C}{\partial x^n}, \quad (46.65c)$$

where we defined the anti-symmetric *skew diffusion* tensor

$$\mathbb{A}_{mn} = \epsilon_{mnp} \Psi_p^* \implies \mathbb{A} = \begin{bmatrix} 0 & \Psi_3^* & -\Psi_2^* \\ -\Psi_3^* & 0 & \Psi_1^* \\ \Psi_2^* & -\Psi_1^* & 0 \end{bmatrix}. \quad (46.66)$$

We thus conclude that advection by a non-divergent mass flux is equivalent to skew-diffusion through the action of an anti-symmetric tensor.

Although leading to the same stirring operator, skew and advective fluxes possess rather complementary properties as listed here.

- **DERIVATIVE OPERATOR:** The skew flux is proportional to the vector streamfunction and the gradient of the tracer, whereas the advective flux is related to the curl of the streamfunction and the value of the tracer concentration. That is, the fluxes in effect swap the placement of the derivative operator. Correspondingly, the advective flux vanishes only if the velocity vanishes, whereas the skew flux vanishes when the tracer gradient vanishes (as for a diffusive flux).
- **FLUX ORIENTATION:** The orientation of the advective flux is determined by the velocity field, which is oriented according to trajectories of fluid particles. This orientation is the same regardless of the tracer. In contrast, a skew tracer flux is directed along lines of constant tracer; i.e., it is neither upgradient nor downgradient. Hence, orientation of the skew flux is directly tied to the tracer field, with each tracer yielding a generally distinct flux orientation. The very distinct orientations of the advective and skew fluxes is the origin of much confusion in regards to these fluxes. We explore many features of these geometric distinctions in Section 47.4 when studying eddy induced tracer fluxes.
- **MATERIAL FLUX:** Fluid elements carry a particular amount of trace matter so that an advective flux of a material tracer measures the passage of matter across an area per unit time (dimensions of mass per area per time), whereas a skew flux is not interpreted as the passage of matter across an area per time. This distinction is particularly important when interpreting boundary conditions discussed in Section 46.7.3.

In Section 46.7 we pursue the above points to further detail the dual relation between advection and skewson.

### 46.6.5 A comment about skew fluxes and Lagrangian kinematics

The advective tracer flux and skew tracer flux are very distinct vectors and we further explore the distinction in Sections 46.7 and 47.4. As detailed in each of those sections, it is a matter of convenience how one chooses to formulate the Eulerian tracer equation since the advective flux and skew flux lead to the same tracer evolution. Furthermore, the choice to formulate the tracer equation in terms of a skew flux in no way eliminates the Lagrangian perspective. That is, fluid particles, or fluid elements, still move through the fluid and transport tracer as part of this motion. The Lagrangian formulation of tracer evolution is naturally connected, via a transformation of reference frames, to the Eulerian advection equation. Even so, we do not somehow eliminate fluid particle motion when choosing to work with skew tracer fluxes. Instead, we merely choose to formulate the tracer equation in terms of the vector streamfunction rather than the velocity.

### 46.6.6 Further reading

The uses of residual-mean transport are many and varied in the ocean and atmospheric literature. [Vallis \(2017\)](#) offers a thorough and pedagogical treatment. Skew diffusion is treated in [Moffatt](#)

(1983), in which he raises the connection to fluids with rotation and/or magnetic fields. *Middleton and Loder* (1989) applied these ideas to ocean gravity waves, tides, and Rossby waves. *Griffies* (1998) applied these ideas to the methods used for parameterizing tracer transport from ocean mesoscale eddies.

## 46.7 Advection and skewson

We introduced skew diffusion in Section 46.6.4 and will again encounter it in Chapterd 47 and 48. Following the terminology of Section 9.2 of *Griffies* (2004), we refer to *skewson* as any process that leads to tracer transport via skew fluxes, with skew diffusion a particular example. There are occasions where it is conceptually and operationally more convenient to use advective fluxes, such as when considering the transport of tracers by the flow field explicitly resolved by a numerical simulation. In contrast, skew fluxes are sometimes more convenient for certain subgrid scale eddy parameterizations, such as the one discussed in Section 48.1. We here consider facets of advection and skewson for those interested in diving deeper into the details.

### 46.7.1 Choosing a gauge

Consider an arbitrary divergent-free mass transport

$$\nabla \cdot (\rho \mathbf{v}^*) = 0, \quad (46.67)$$

where the divergent-free constraint is satisfied by introducing a vector streamfunction

$$\rho \mathbf{v}^* = \nabla \times (\rho \Psi^*). \quad (46.68)$$

The streamfunction is arbitrary up to a gauge transformation

$$\rho \Psi' = \rho \Psi^* + \nabla(\rho \Lambda), \quad (46.69)$$

where  $\Lambda$  is a gauge function.

#### *Changes to the skew flux under a gauge transformation*

Although the velocity is invariant up to an arbitrary gauge function, the skew flux,  $\mathbf{J}^{\text{skew}} = -\nabla C \times \rho \Psi^*$ , changes. Nonetheless, the divergence of the skew flux is invariant, as we see by noting that

$$\nabla C \times [\rho \Psi^* + \nabla(\rho \Lambda)] = \nabla C \times (\rho \Psi^*) + \nabla \times [C \nabla(\rho \Lambda)]. \quad (46.70)$$

and since  $\nabla \cdot \nabla \times [C \nabla(\rho \Lambda)] = 0$ , the flux divergence,  $\nabla \cdot \mathbf{J}^{\text{skew}}$ , remains unchanged.

#### *Coulomb gauge*

We have some freedom in specifying the gauge function. One choice is to set  $\Lambda = 0$ . However, there are occasions in which it is useful to set the gauge function in a manner to cancel unwanted terms. A gauge commonly used in electrodynamics (e.g., *Jackson* (1975)) is the *Coulomb gauge*, in which

$$\nabla \cdot (\rho \Psi^*) = 0 \quad \text{Coulomb gauge.} \quad (46.71)$$

Making use of the curl identity (2.38c) leads to the Poisson equation for the vector potential

$$\nabla^2(\rho \Psi^*) = -\nabla \times (\rho \mathbf{v}^*). \quad (46.72)$$

This equation has a free-space Green's function given by the Coulomb-Ampere expression

$$\rho(\mathbf{x}, t) \Psi^*(\mathbf{x}, t) = \nabla \times \int \frac{\rho(\mathbf{x}', t) \mathbf{v}^*(\mathbf{x}', t)}{4\pi |\mathbf{x} - \mathbf{x}'|} dV', \quad (46.73)$$

where  $dV'$  is the volume element for integration over the test points,  $\mathbf{x}'$ . Although common in electrodynamics, we know of no geophysical fluid application making use of the Coulomb gauge.

### 46.7.2 Vertical gauge

As introduced in Section 16.5.2, a gauge commonly used for eddy parameterizations (Section 48.1) sets to zero one of the three components of the vector streamfunction. This gauge choice is available since there are only two independent functional degrees of freedom available from a divergence-free mass transport field. A common choice is the *vertical gauge* in which

$$\Psi_3^* = 0 \quad \text{vertical gauge.} \quad (46.74)$$

Let us see how we can generally make this gauge choice. Consider a vector streamfunction  $\Phi$  that has all three components nonzero. Now consider the alternative streamfunction  $\rho \Psi^* = \rho \Phi + \nabla(\rho \Lambda)$ , with  $\nabla(\rho \Lambda) = -\hat{\mathbf{z}} \rho \Phi_3$ . This choice in turn means that the third component of  $\Psi^*$  is zero.

To further specify the vertical gauge we invert the relations

$$\rho u^* = -\partial_z(\rho \Psi_2^*) \quad \text{and} \quad \rho v^* = \partial_z(\rho \Psi_1^*) \quad \text{and} \quad \rho w^* = \partial_x(\rho \Psi_2^*) - \partial_y(\rho \Psi_1^*) \quad (46.75)$$

to render the vector streamfunction

$$\rho \Psi^* = \hat{\mathbf{z}} \times \int_{-H}^z \rho \mathbf{u}^* dz' = \hat{\mathbf{z}} \times \underline{\mathbf{U}}^{(*\rho)} \quad (46.76)$$

where

$$\underline{\mathbf{U}}^{(*\rho)}(z) = \int_{-H}^z \rho \mathbf{u}^* dz' \quad (46.77)$$

is the horizontal mass transport associated with  $\mathbf{u}^*$  passing between the bottom and a depth  $z \geq -H$ . The anti-symmetric stirring tensor for the vertical gauge is given by

$$\rho \mathbb{A}_{mn} = \begin{pmatrix} 0 & 0 & \underline{U}^{(*\rho)} \\ 0 & 0 & \underline{V}^{(*\rho)} \\ -\underline{U}^{(*\rho)} & -\underline{V}^{(*\rho)} & 0 \end{pmatrix}, \quad (46.78)$$

and the corresponding skew, rotational, and advective fluxes are

$$\mathbf{J}^{\text{skew}} = -\underline{\mathbf{U}}^{(*\rho)} \partial_z C + \hat{\mathbf{z}} \underline{\mathbf{U}}^{(*\rho)} \cdot \nabla_z C \quad (46.79a)$$

$$\mathbf{J}^{\text{rot}} = \partial_z(C \underline{\mathbf{U}}^{(*\rho)}) - \hat{\mathbf{z}} \nabla_z \cdot (C \underline{\mathbf{U}}^{(*\rho)}) \quad (46.79b)$$

$$\mathbf{J}^{\text{adv}} = C (\partial_z \underline{\mathbf{U}}^{(*\rho)}) - \hat{\mathbf{z}} C \nabla_z \cdot \underline{\mathbf{U}}^{(*\rho)}. \quad (46.79c)$$

Note that the identity  $\mathbf{J}^{\text{adv}} = \mathbf{J}^{\text{skew}} + \mathbf{J}^{\text{rot}}$  is maintained by these expressions. The horizontal components to the skew flux vanish when the tracer is uniform in the vertical, and the vertical skew flux vanishes with a horizontally uniform tracer field. These properties manifest the skewed nature of the fluxes.

### 46.7.3 Boundary conditions

We assume that all external domain boundaries are material in regards to the velocity  $\mathbf{v}^*$ . Furthermore, even for moving domain boundaries, we assume that the suite of kinematic boundary conditions is based on the barycentric velocity  $\mathbf{v}$  (see Section 14.4), so that  $\mathbf{v}^*$  satisfies the no-normal flow condition even on moving boundaries

$$\hat{\mathbf{n}} \cdot \mathbf{v}^* = 0 \quad \text{external domain boundaries.} \quad (46.80)$$

As we discuss in Section 46.8.1, this boundary condition is required for the eddy-induced velocity to have zero impact on the total mass of an arbitrary tracer within the full fluid domain.

Correspondingly, the advective tracer flux also satisfies a no-normal boundary condition on all external boundaries

$$\hat{\mathbf{n}} \cdot \mathbf{J}^{\text{adv}} = \hat{\mathbf{n}} \cdot \mathbf{v}^* \rho C = 0. \quad (46.81)$$

The corresponding boundary condition for the skew flux is found by inserting the relation (46.62) into the advective flux boundary condition (46.81) to render

$$\hat{\mathbf{n}} \cdot \mathbf{J}^{\text{adv}} = \hat{\mathbf{n}} \cdot [\mathbf{J}^{\text{skew}} + \mathbf{J}^{\text{rot}}] = 0. \quad (46.82)$$

Hence, the skew flux generally has a non-zero normal component at the solid boundaries as determined by the rotational flux

$$\hat{\mathbf{n}} \cdot \mathbf{J}^{\text{skew}} = -\hat{\mathbf{n}} \cdot \mathbf{J}^{\text{rot}}. \quad (46.83)$$

Even so, there might be occasions in which  $\hat{\mathbf{n}} \cdot \mathbf{J}^{\text{skew}} = 0$ , which is ensured so long as

$$(-\nabla C \times \rho \Psi^*) \cdot \hat{\mathbf{n}} = -(\rho \Psi^* \times \hat{\mathbf{n}}) \cdot \nabla C = 0. \quad (46.84)$$

A sufficient condition is to have  $\Psi^* \times \hat{\mathbf{n}} = 0$ , in which case the vector streamfunction is parallel to the boundary normal. An alternative sufficient condition is to have the streamfunction vanish at the boundary. Further details for boundary conditions depend on physical properties of the velocity  $\mathbf{v}^*$ . We discuss one example in Section 48.1 as prescribed by the [Gent et al. \(1995\)](#) mesoscale eddy parameterization.

## 46.8 Finite volume budgets with eddy velocities

In this section we examine how an eddy induced velocity modifies the budgets for fluid mass and tracer mass in finite domains. For this purpose, write the local/differential mass and tracer budgets in the form

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}^\dagger) = 0 \quad (46.85a)$$

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho \mathbf{v}^\dagger C + \mathbf{J}^{\text{diff}}) = 0, \quad (46.85b)$$

where (see Section 46.7)

$$\mathbf{v}^\dagger = \mathbf{v} + \mathbf{v}^* \quad \text{and} \quad \nabla \cdot (\rho \mathbf{v}^*) = 0, \quad (46.86)$$

and where  $\mathbf{J}^{\text{diff}}$  is a subgrid scale flux encompassing all processes, such as diffusion and boundary conditions, that are not represented by an eddy-induced advection. Given that  $\nabla \cdot (\rho \mathbf{v}^*) = 0$ , the

mass budget (46.85a) can we written in the equivalent manners

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}^\dagger) = \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0. \quad (46.87)$$

That is, the eddy-induced velocity does not lead to any local sources of fluid mass. This property will prove to be very important in the budget analyses of this section.

As shown in the following, the finite volume budgets for fluid mass and tracer mass also make use of the residual mean velocity,  $\mathbf{v}^\dagger$ . That result is not surprising, since the finite volume budgets are consistent with the differential budgets (46.85a) and (46.85b). Nonetheless, it is useful to expose the details as they appear in many budget analysis applications, such as the water mass and tracer mass analysis of Chapter 50. We furthermore explore how the budgets for tracer mass appear when formulated using advective fluxes versus skew fluxes. As we will see, the finite volume budgets are consistent across the variety of formulations only if the eddy velocity and eddy vector streamfunction satisfy specific boundary conditions as discussed in Section 46.7.3.

### 46.8.1 Advection formulation

Making use of the tracer equation (46.85b) in the Leibniz-Reynolds transport theorem (15.45) renders the finite volume tracer mass budget for an arbitrary domain,  $\mathcal{R}$

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = - \oint_{\partial \mathcal{R}} [\rho C (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) + \mathbf{J}^{\text{diff}}] \cdot \hat{\mathbf{n}} dS, \quad (46.88)$$

where  $\mathbf{v}^{(b)}$  is the velocity of a point on the domain boundary. Appearance of the residual mean velocity,  $\mathbf{v}^\dagger$ , in the finite volume budget (46.88) follows from its appearance in the local tracer budget (46.85b). We thus see that the eddy-induced velocity impacts on the tracer mass budget for an arbitrary domain. However, its impacts disappear when integrating over a closed or periodic fluid domain so long as

$$\mathbf{v}^* \cdot \hat{\mathbf{n}} = 0 \quad \text{on external fluid boundaries.} \quad (46.89)$$

We already encountered this boundary condition in Section 46.7.3. It holds on all boundaries, including those such as the ocean free surface that are time dependent and/or permeable. It is required if we assume the eddy-induced velocity does not modify the mass of any tracer in the full fluid domain. That assumption is generally made for eddy-induced velocities such as those associated with mesoscale and submesoscale eddies in the ocean (see Section 48.3).

Setting the tracer concentration to a constant in equation (46.88) leads to the fluid mass budget

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho dV \right] = - \oint_{\partial \mathcal{R}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} dS, \quad (46.90)$$

where we set the diffusive tracer flux,  $\mathbf{J}^{\text{diff}}$ , to zero since there is no diffusion of fluid mass between fluid elements (Section 15.1). As for the differential form (46.85a), the mass budget for any domain is not changed by the eddy-induced velocity since

$$\nabla \cdot (\rho \mathbf{v}^*) = 0 \implies \oint_{\partial \mathcal{R}} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} dS = 0, \quad (46.91)$$

so that the mass budget is given by

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho dV \right] = - \oint_{\partial \mathcal{R}} [\rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)})] \cdot \hat{\mathbf{n}} dS = - \oint_{\partial \mathcal{R}} [\rho (\mathbf{v} - \mathbf{v}^{(b)})] \cdot \hat{\mathbf{n}} dS \quad (46.92)$$

Hence, the eddy velocity contribution to the mass budget for any finite region vanishes, which is expected since it provides no net mass source to a region. Furthermore, one may choose to diagnose the right hand side of the mass budget in either the residual mean or Eulerian mean form. The choice is based on convenience, such as whether one has easier access to the residual mean velocity or the Eulerian mean velocity. Although the patterns of the fluxes across any particular boundary differs if  $\mathbf{v}^* \neq 0$ , the accumulation of mass within the region are identical for the two formulations.

### 46.8.2 Skew flux formulation

Now consider the complement perspective afforded by the skew flux formulation from Section 46.7. Here we decompose the advective tracer flux according to

$$C \rho \mathbf{v}^\dagger = C \rho \mathbf{v} - \nabla C \times \rho \Psi^* + \nabla \times (C \rho \Psi^*) = C \rho \mathbf{v} + \mathbf{J}^{\text{skew}} + \nabla \times (C \rho \Psi^*), \quad (46.93)$$

where we introduced the skew tracer flux arising from the eddy-induced streamfunction

$$\mathbf{J}^{\text{skew}} = -\nabla C \times (\rho \Psi^*). \quad (46.94)$$

The differential budget for tracer is thus given by

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot [\rho C \mathbf{v} + \mathbf{J}^{\text{skew}} + \mathbf{J}^{\text{diff}}] = 0, \quad (46.95)$$

where the rotational term,  $\nabla \times (C \rho \Psi^*)$ , has zero divergence and thus does not affect the tracer budget. The corresponding finite volume tracer mass budget is

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = - \oint_{\partial \mathcal{R}} \left[ \rho C (\mathbf{v} - \mathbf{v}^{(b)}) - \nabla C \times (\rho \Psi^*) + \mathbf{J}^{\text{diff}} \right] \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.96)$$

In this form, the contribution from the eddies is inside the skew flux rather than in the residual mean advective flux. Setting  $C$  to a constant reveals the mass budget as in the second form of equation (46.92).

### 46.8.3 Domain with a tracer boundary

We now apply the previous general budget discussion to a specific domain that anticipates the more complete budget analysis provided in Section 50.10. Here, we consider the fluid mass and tracer mass within an ocean region with at least one of its bounds determined by an isosurface of constant tracer concentration, as in Figure 46.4.

#### *Advection formulation*

The tracer mass budget written using the advective formulation (46.88) takes the form

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = \int_{\partial \Omega_{\text{surf}}(\tilde{C})} Q_m C dA - \tilde{C} \int_{C=\tilde{C}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \oint_{\partial \mathcal{R}} \mathbf{J}^{\text{diff}} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.97)$$

For the first right hand side term we made use of the surface kinematic boundary condition (14.73c), with  $Q_m dA$  the mass per time crossing the surface interface and where  $dA$  is the horizontal projection of the interface area element  $d\mathcal{S}$ . We also made use of the exterior boundary condition (46.89) for the eddy-induced velocity. For the second term we pulled the tracer concen-

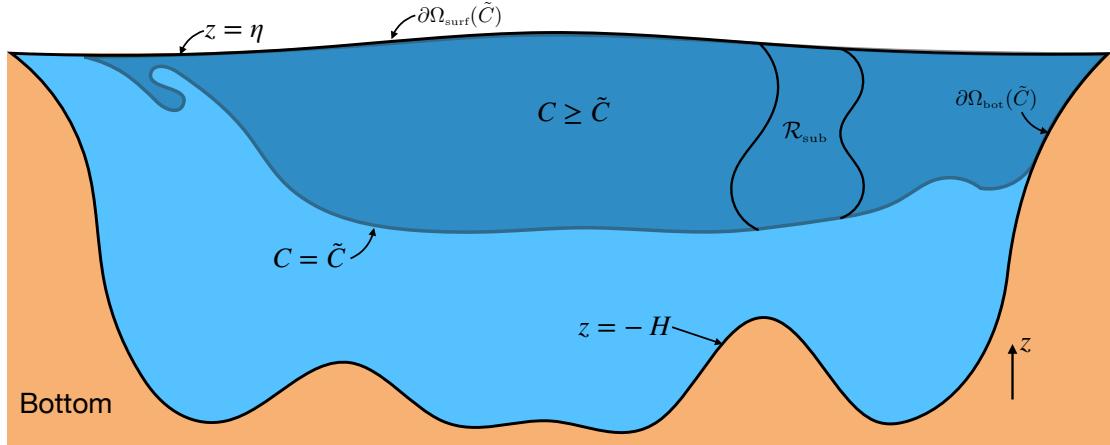


FIGURE 46.4: An ocean region with one of its boundaries set by a surface of constant tracer,  $C = \tilde{C}$ . Note that the region need not be monotonically stratified in the tracer concentration, nor does it need to be simply connected. The region is bounded at the top by  $\partial\Omega_{surf}(\tilde{C})$ ; at the bottom by the  $C = \tilde{C}$  isosurface as well as the solid-earth bottom  $\partial\Omega_{bot}(\tilde{C})$ . The region can generally be multiply connected. A subregion,  $\mathcal{R}_{sub}$ , is also considered where its sides extend from the free surface to the tracer isosurface, and they are assumed to be fully within the fluid domain. We develop the tracer and fluid mass budgets for region  $\mathcal{R}_{sub}$  in Section 46.8.4, whereas the budget in the full region  $C \geq \tilde{C}$  is considered in Section 46.8.3.

tration outside of the boundary integral over the  $C = \tilde{C}$  interface since the concentration is fixed at  $\tilde{C}$  on this interface.

The mass budget for this region, also formulated using advective fluxes, is given by

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho dV \right] = \int_{\partial\Omega_{surf}(\tilde{C})} Q_m dA - \int_{C=\tilde{C}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.98)$$

Combining this budget with the tracer mass budget allows us to write

$$\frac{d}{dt} [M_C - \tilde{C} M] = \int_{\partial\Omega_{surf}(\tilde{C})} Q_m (C - \tilde{C}) dA - \oint_{\partial\mathcal{R}} \mathbf{J}^{\text{diff}} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (46.99)$$

where we introduced the shorthand for the tracer mass and fluid mass in the region

$$M_C = \int_{\mathcal{R}} C \rho dV \quad \text{and} \quad M = \int_{\mathcal{R}} \rho dV. \quad (46.100)$$

In Section 50.10.2 we motivate the name *internal tracer mass* for the quantity  $M_C - \tilde{C} M$ .

### Skew flux formulation

The tracer mass budget formulated using skew tracer fluxes is generally given by equation (46.96). It takes on the following form for the domain in Figure 46.4

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = \int_{\partial\Omega_{surf}(\tilde{C})} Q_m C dA - \tilde{C} \int_{C=\tilde{C}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \oint_{\partial\mathcal{R}} [-\nabla C \times (\rho \Psi^*) + \mathbf{J}^{\text{diff}}] \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (46.101)$$

and the corresponding budget for the fluid mass is

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho dV \right] = \int_{\partial\Omega_{surf}(\tilde{C})} Q_m dA - \int_{C=\tilde{C}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.102)$$

As for the advective formulation, we combine the fluid mass budget equation (46.102) with the tracer mass equation (46.101) to render a budget equation for the internal mass content

$$\frac{d}{dt} \left[ M_C - \tilde{C} M \right] = \int_{\partial\Omega_{\text{surf}}(\tilde{C})} Q_m (C - \tilde{C}) dA - \oint_{\partial\mathcal{R}} \mathbf{J}^{\text{diff}} \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (46.103)$$

which is the same as for the advective formulation given by equation (46.99).

#### *Proving the budgets based on the two formulations are equivalent*

The two tracer budgets, (46.97) and (46.101), must be the same since they measure changes to the tracer mass within the same region. Likewise, the two mass budgets, (46.98) and (46.102), must be the same, as are the two internal tracer mass budgets (46.99) and (46.103). We here expose the manipulations required to verify these equalities.

To prove the  $C = \tilde{C}$  terms in the tracer budget equations (46.97) and (46.101) are the same, consider the identity (46.91) applied to the region under consideration

$$0 = \oint_{\partial\mathcal{R}} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\partial\Omega_{\text{surf}}(\tilde{C})} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{\partial\Omega_{\text{bot}}(\tilde{C})} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{C=\tilde{C}} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.104)$$

The surface and bottom boundary terms vanish due to the external boundary condition (46.89); namely,  $\mathbf{v}^* \cdot \hat{\mathbf{n}} = 0$  for each point along an external fluid boundary. We are thus led to conclude that

$$\int_{C=\tilde{C}} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} = 0. \quad (46.105)$$

This boundary integral means that there is no net accumulation of mass in the region due to action of the eddy velocity. Notably, we generally have  $\mathbf{v}^* \cdot \hat{\mathbf{n}} \neq 0$  at any particular point on the  $C = \tilde{C}$  surface. Given the boundary integral (46.105) we are thus led to conclude

$$\int_{C=\tilde{C}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{C=\tilde{C}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.106)$$

This identity proves that the two mass budgets (46.98) and (46.102) are indeed measuring changes to the same fluid mass, even though one computes the domain boundary fluxes based on the residual mean velocity,  $\mathbf{v}^\dagger$ , whereas the other uses the Eulerian mean,  $\mathbf{v}$ .

Next we need to show that the skew flux term vanishes when integrated around the domain boundary. For the  $C = \tilde{C}$  boundary we have

$$\int_{C=\tilde{C}} [\nabla C \times (\rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S} = 0, \quad (46.107)$$

which follows since  $\hat{\mathbf{n}}$  is parallel to  $\nabla C$  along this boundary. For the external boundaries, equality of the tracer mass budgets (46.97) and (46.101) is satisfied for an arbitrary tracer concentration if one of the boundary conditions discussed in Section (46.7.3) is maintained; i.e., if  $\Psi^*$  vanishes on an external boundary or if it is parallel to the boundary normal direction ( $\hat{\mathbf{n}} \times \Psi^* = 0$ ). Maintenance of either of these two boundary conditions allows us to conclude that the two budgets (46.97) and (46.101) are indeed identical.

#### 46.8.4 Budget for a region with interior sides

Consider the subregion  $\mathcal{R}_{\text{sub}}$  shown in Figure 46.4. This region is bounded above by the free surface and below by the tracer isosurface,  $C = \tilde{C}$ , just like the region  $\mathcal{R}$  encountered in Section

**46.8.3.** Additionally, region  $\mathcal{R}_{\text{sub}}$  is bounded along its sides by surfaces assumed to be within the fluid interior. For much of this discussion we allow the sides to have an arbitrary shape and to move. Towards the end of this section we specialize to the case of static sides, such as might be relevant for a vertical section through the fluid and/or a numerical model grid cell.

### Fluid mass budget

The fluid mass budget for the region  $\mathcal{R}_{\text{sub}}$  can be formulated using either the residual mean velocity or the Eulerian mean velocity

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho dV \right] = \int_{\partial\Omega_{\text{surf}}(\tilde{C})} Q_m dA - \int_{C=\tilde{C}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (46.108a)$$

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho dV \right] = \int_{\partial\Omega_{\text{surf}}(\tilde{C})} Q_m dA - \int_{C=\tilde{C}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.108b)$$

The two budgets are identical since the eddy velocity satisfies  $\oint \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} = 0$  for any domain, as well as  $\mathbf{v}^* \cdot \hat{\mathbf{n}} = 0$  along any external domain boundary. Hence, as already noted in Section 46.8.1, the eddy velocity contribution to the right hand side of equation (46.108a) vanishes; it provides no net mass source to any region. We next show the same equality holds for the tracer mass budgets, with that equality shown with a bit more effort.

### Tracer mass budget

The advective flux formulation of the tracer mass budget is given by

$$\begin{aligned} \frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho C dV \right] &= \int_{\partial\Omega_{\text{surf}}(\tilde{C})} Q_m C dA - \tilde{C} \int_{C=\tilde{C}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \oint_{\partial\mathcal{R}_{\text{sub}}} \mathbf{J}^{\text{diff}} \cdot \hat{\mathbf{n}} d\mathcal{S} \\ &\quad - \int_{\text{sides}} C \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}, \end{aligned} \quad (46.109)$$

and the corresponding skew flux formulation is

$$\begin{aligned} \frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho C dV \right] &= \int_{\partial\Omega_{\text{surf}}(\tilde{C})} Q_m C dA - \tilde{C} \int_{C=\tilde{C}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \oint_{\partial\mathcal{R}_{\text{sub}}} \mathbf{J}^{\text{diff}} \cdot \hat{\mathbf{n}} d\mathcal{S} \\ &\quad - \int_{\text{sides}} C \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} [-\nabla C \times (\rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S}. \end{aligned} \quad (46.110)$$

As for the discussion in Section 46.8.3, we introduce the internal tracer mass and make use of the fluid mass budgets (46.108a) and (46.108b) to write the advective form of the internal mass budget

$$\frac{d}{dt} [M_C - \tilde{C} M] = \int_{\partial\Omega_{\text{surf}}(\tilde{C})} Q_m (C - \tilde{C}) dA - \oint_{\partial\mathcal{R}} \mathbf{J}^{\text{diff}} \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} (C - \tilde{C}) \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (46.111)$$

and the corresponding skew flux form of the same budget

$$\frac{d}{dt} \left[ M_C - \tilde{C} M \right] = \int_{\partial\Omega_{\text{surf}}(\tilde{C})} Q_m (C - \tilde{C}) dA - \oint_{\partial\mathcal{R}} \mathbf{J}^{\text{diff}} \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} (C - \tilde{C}) \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} [-\nabla C \times (\rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.112)$$

We now examine the right hand side of the budgets (46.111) and (46.112) to show they are indeed measuring the same tracer mass budget. For that purpose, consider the skew flux integral in equation (46.112) and note that the integrand vanishes on both the top of the domain, at  $z = \eta$ , and bottom at  $C = \tilde{C}$ , thus allowing us to write

$$-\int_{\text{sides}} [-\nabla C \times (\rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S} = -\oint_{\partial\mathcal{R}_{\text{sub}}} [-\nabla C \times (\rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (46.113)$$

where the right hand side is an integral around the full domain boundaries. Now reintroduce the eddy induced velocity and rotational flux to have

$$-\oint_{\partial\mathcal{R}_{\text{sub}}} [-\nabla C \times (\rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S} = -\oint_{\partial\mathcal{R}_{\text{sub}}} [C \rho \mathbf{v}^* - \nabla \times (C \rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.114)$$

The rotational flux has zero divergence, so that Gauss's divergence theorem means that the rotational flux vanishes when integrated along the domain boundaries

$$\oint_{\partial\mathcal{R}_{\text{sub}}} \nabla \times (C \rho \Psi^*) \cdot \hat{\mathbf{n}} d\mathcal{S} = 0. \quad (46.115)$$

The eddy advection term in equation (46.114) vanishes on the top boundary at  $z = \eta$  due to the boundary condition  $\mathbf{v}^* \cdot \hat{\mathbf{n}} = 0$ , thus yielding

$$\oint_{\partial\mathcal{R}_{\text{sub}}} C \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\text{sides}} C \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} + \int_{C=\tilde{C}} C \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (46.116a)$$

$$= \int_{\text{sides}} C \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} + \tilde{C} \int_{C=\tilde{C}} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.116b)$$

Again make use of the property  $\nabla \cdot (\rho \mathbf{v}^*) = 0$  and  $\hat{\mathbf{n}} \cdot \mathbf{v}^* = 0$  at  $z = \eta$  to write

$$0 = \oint_{\partial\mathcal{R}_{\text{sub}}} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} = \oint_{\text{sides}} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} + \oint_{C=\tilde{C}} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (46.117)$$

which gives us

$$-\int_{\text{sides}} [-\nabla C \times (\rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S} = -\oint_{\partial\mathcal{R}_{\text{sub}}} C \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} = -\int_{\text{sides}} (C - \tilde{C}) \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.118)$$

Making use of this result in the skew flux formulated budget equation (46.112) brings it to the advective flux form found in equation (46.111).

We are thus led to conclude that the right hand side to equation (46.112) does indeed equal to the right hand side of equation (46.111). So although the formulation of the boundary flux contributions is rather distinct between the advective flux and skew flux formulations, the resulting tracer mass budget is the same. The choice for how to formulate the budget is thus a matter of convenience.

### 46.8.5 Budget for a stirred fluid in a region with interior sides

Although contained within the formalism developed in Section 46.8.4, it is revealing to specialize those budgets to the case of zero mixing, in which  $\mathbf{J}^{\text{diff}} = 0$  and there is zero boundary mass flux,  $Q_m = 0$ . In this case the fluid is reversibly stirred. Examining the finite region budgets for this pure stirring case allows us to further reveal the complementary treatments available from advection versus skewson.

#### *Summary of the differential stirring formalism*

As explored in this chapter, an Eulerian description of tracer stirring can arise from either advection or skewson. In the presence of an eddy induced velocity we here consider two representations of tracer stirring, with the first being advection by the residual mean velocity,  $\mathbf{v}^\dagger$

$$\rho \frac{D^\dagger C}{Dt} = \frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho \mathbf{v}^\dagger C) = 0. \quad (46.119)$$

This formulation makes it clear that surfaces of constant  $C$  are material as defined by the residual mean velocity rather than by the Eulerian mean,  $\mathbf{v}$ . That is, tracer isosurfaces satisfy the residual mean impermeability condition

$$\rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = 0 \quad \text{on } C \text{ isosurfaces}, \quad (46.120)$$

with

$$\hat{\mathbf{n}} = \frac{\nabla C}{|\nabla C|} \quad \text{and} \quad \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} = -\frac{\partial_t C}{|\nabla C|}. \quad (46.121)$$

The impermeability condition (46.120) offers a geometric interpretation of the tracer equation (46.119) following from the discussion of dia-surface transport in Section 42.4. Correspondingly, Lagrangian fluid particles moving with the residual mean velocity do not cross tracer isosurfaces even if those isosurfaces move. Furthermore, we observe that the eddy induced velocity has a nonzero projection across tracer isosurfaces

$$(\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = 0 \implies (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = -\mathbf{v}^* \cdot \hat{\mathbf{n}} \quad \text{on } C \text{ isosurfaces}. \quad (46.122)$$

This property of the eddy induced velocity was emphasized by [McDougall and McIntosh \(2001\)](#). It reveals that in the absence of mixing, eddy motion crossing tracer isosurfaces is exactly balanced by Eulerian plus boundary motion, thus leaving a net zero residual mean transfer of matter across the surface. Equation (46.122) is a key kinematic property used for interpreting features of the finite volume budgets detailed below.

Our second means to represent tracer stirring makes use of advection by the Eulerian mean velocity plus skewson by the eddy induced streamfunction

$$\rho \frac{DC}{Dt} + \nabla \cdot [-\nabla C \times (\rho \Psi^*)] = \frac{\partial(\rho C)}{\partial t} + \nabla \cdot [\rho \mathbf{v} C - \nabla C \times (\rho \Psi^*)] = 0. \quad (46.123)$$

In terms of the eddy streamfunction,  $\rho \Psi^*$ , the impermeability condition (46.120) takes on the form

$$[\rho \mathbf{v} + \nabla \times (\rho \Psi^*) - \rho \mathbf{v}^{(b)}] \cdot \hat{\mathbf{n}} = 0 \quad \text{on } C \text{ isosurfaces}. \quad (46.124)$$

### Budgets via residual mean advection

The mass budget formulated in terms of residual mean advection, and the corresponding residual mean advective flux formulation of the tracer mass budget, are given by

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho dV \right] = - \int_{C=\tilde{C}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (46.125a)$$

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho C dV \right] = - \tilde{C} \int_{C=\tilde{C}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} C \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.125b)$$

The residual mean impermeability condition (46.120) for the  $C = \tilde{C}$  surface renders a simplification to the fluid mass and tracer mass budgets

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho dV \right] = - \int_{\text{sides}} \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (46.126a)$$

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho C dV \right] = - \int_{\text{sides}} C \rho (\mathbf{v}^\dagger - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.126b)$$

Hence, in the residual mean formulation, the only fluxes that affect changes to the mass budgets are those that cross the side faces of the region.

### Budgets via Eulerian mean advection plus eddy skewson

The mass budget formulated in terms of Eulerian mean advection, and the corresponding tracer mass budget using eddy skewson, are given by

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho dV \right] = - \int_{C=\tilde{C}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (46.127a)$$

$$\begin{aligned} \frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho C dV \right] &= - \tilde{C} \int_{C=\tilde{C}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} C \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} \\ &\quad - \int_{\text{sides}} [-\nabla C \times (\rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S}. \end{aligned} \quad (46.127b)$$

We already saw in Section 46.8.4 how to bring the right hand side terms into the form realized by the residual mean advective approach. So there is no question concerning the equivalence of the advective and skew flux formulations for the tracer mass budget. Nonetheless, what is here clearly emphasized is that the skew flux approach requires us to account for Eulerian advective transport across the  $C = \tilde{C}$  isosurface, whereas for the advective flux approach the only flux in equation (46.126b) is that crossing the region side boundaries. Even so, as stated earlier, an Eulerian mean transport of tracer across the  $C = \tilde{C}$  isosurface *does not* correspond to material transport across this surface. The reason is that material transport is determined by the residual mean velocity,  $\mathbf{v}^\dagger$ , as per the residual mean impermeability conditions 46.122 and 46.124. So even though there is a contribution to the skew flux formulated budget from Eulerian transport across the  $C = \tilde{C}$  material surface, there remains zero net material crossing that surface.

### Zero Eulerian mean advection and static side walls

One further specialization serves to clearly emphasize the complementary nature of the advective and skew flux approaches. Here, we assume the sides of the region are static and the Eulerian mean velocity vanishes. With a zero Eulerian velocity, the residual mean impermeability condition

(46.122) means that on the  $C = \tilde{C}$  isosurface, the normal component of the eddy velocity is balanced by the boundary velocity as per the impermeability condition (46.128):

$$(\mathbf{v}^* - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} = 0 \quad \text{on } C \text{ isosurfaces and with } \mathbf{v} = 0. \quad (46.128)$$

When formulated using the residual mean advection, the fluid mass budget (46.126a) and tracer mass budget (46.126b) reduce in this case to

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho dV \right] = - \int_{\text{sides}} \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (46.129a)$$

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho C dV \right] = - \int_{\text{sides}} C \rho \mathbf{v}^* \cdot \hat{\mathbf{n}} d\mathcal{S}, \quad (46.129b)$$

so that these budgets are only affected by eddy advection across the side boundaries. The corresponding mass budget written in terms of Eulerian mean advection, (46.127a), and tracer mass budget written in terms of skew fluxes, (46.127b), are given by

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho dV \right] = + \int_{C=\tilde{C}} \rho \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (46.130a)$$

$$\frac{d}{dt} \left[ \int_{\mathcal{R}_{\text{sub}}} \rho C dV \right] = + \tilde{C} \int_{C=\tilde{C}} \rho \mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\text{sides}} [-\nabla C \times (\rho \Psi^*)] \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (46.130b)$$

For the mass budget, (46.130a), there are no contributions to the side walls since they are static and the Eulerian advection is assumed to vanish. The only contribution comes from the eddy term acting on the  $C = \tilde{C}$  isosurface where  $\mathbf{v}^{(b)} \cdot \hat{\mathbf{n}} = \mathbf{v}^* \cdot \hat{\mathbf{n}}$ . For the tracer mass budget, (46.130b), we also have the eddy contribution on the  $C = \tilde{C}$  isosurface, plus skew fluxes that penetrate the side walls.

The right hand sides to the fluid mass budgets (46.129a) and (46.130a), and tracer mass budgets (46.129b) and (46.130b), are remarkably distinct. Even so, they both measure the same budgets. Furthermore, in both cases the  $C = \tilde{C}$  boundary is a material boundary as defined by the residual mean velocity.

## 46.9 Active tracers and dia-surface flow

An *active tracer* is a tracer that impacts the dynamics, with potential temperature and salinity the canonical examples. Active tracers directly impact the buoyancy, which in turn affects pressure and velocity. Hence, the advection-diffusion equation for active tracers is nonlinear since the velocity field is dependent on active tracers. We here write the advection-diffusion equation in terms of the residual mean velocity using potential temperature as an example active tracer

$$\rho \frac{D^\dagger \theta}{Dt} = \rho \left[ \frac{\partial}{\partial t} + \mathbf{v}^\dagger \cdot \nabla \right] \theta = -\nabla \cdot \mathbf{J}^{\text{diff}}(\theta). \quad (46.131)$$

Further nonlinearities arise when the subgrid scale diffusion tensor is itself a function of the buoyancy, as discussed at the end of Section 46.4.4, and/or when the parameterized eddy-induced velocity is a function of the buoyancy, as discussed in Section 48.3.

### 46.9.1 Adiabatic flow

In an adiabatic fluid, potential temperature is materially invariant. When advected by the residual mean velocity this material invariance takes on the form

$$\frac{D^\dagger \theta}{Dt} = \frac{\partial \theta}{\partial t} + \mathbf{v}^\dagger \cdot \nabla \theta = 0 \quad \text{adiabatic.} \quad (46.132)$$

Furthermore, following the kinematics of Section 14.4.2, the adiabatic residual mean flow field does not penetrate surfaces of constant potential temperature ( $\theta$ -isosurfaces are impermeable) since

$$\mathbf{v}^\dagger \cdot \nabla \theta = -\frac{\partial \theta}{\partial t}. \quad (46.133)$$

In this case we say that residual mean advection reversibly stirs the potential temperature field. This property of the residual mean velocity was also considered in the discussion of pure stirring in Section 46.8.4.

### 46.9.2 Diabatic processes generating dia-surface transport

Potential temperature is no longer materially invariant in the presence of diabatic processes such as mixing typically parameterized by diffusion. Correspondingly, the residual mean velocity picks up a component,  $w^{\text{dia}}$ , that crosses the moving potential temperature surface thus making it permeable. Hence, advective transport in the presence of mixing is no longer reversible. We follow the kinematics from Section 42.4 to render the expression (42.26) for  $w^{\text{dia}}$ , which we here write as

$$w^{\text{dia}} \equiv \hat{\mathbf{n}} \cdot (\mathbf{v}^\dagger - \mathbf{v}^{(\theta)}) = \frac{1}{|\nabla \theta|} \frac{D^\dagger \theta}{Dt} \quad (46.134)$$

where

$$\hat{\mathbf{n}} = \frac{\nabla \theta}{|\nabla \theta|} \quad \text{and} \quad \mathbf{v}^{(\theta)} \cdot \nabla \theta = -\frac{\partial \theta}{\partial t}. \quad (46.135)$$

Rearrangement of equation (46.134) renders the kinematic identity

$$\frac{D^\dagger \theta}{Dt} = \frac{\partial \theta}{\partial t} + \mathbf{v}^\dagger \cdot \nabla \theta = w^{\text{dia}} |\nabla \theta|. \quad (46.136)$$

With nonzero  $w^{\text{dia}}$ , we no longer have residual mean advection preserving properties along fluid element trajectories. We offer examples to illustrate the physics underlying this identity.

#### *Diffusion with no fluid motion*

Diffusion is the canonical example of a diabatic process (Section 46.3)

$$\rho \frac{D^\dagger \theta}{Dt} = \nabla \cdot (\kappa \rho \nabla \theta), \quad (46.137)$$

with  $\kappa > 0$  the scalar kinematic diffusivity. Diffusion in turn drives a diabatic transport velocity

$$\rho w^{\text{dia}} = \frac{\nabla \cdot (\kappa \rho \nabla \theta)}{|\nabla \theta|}. \quad (46.138)$$

Consider a horizontally homogeneous potential temperature field. If buoyancy is alone determined by potential temperature then there is no fluid motion since buoyancy surfaces are flat (and we assume the eddy-induced motion is also zero). Yet in the presence of vertical diffusion and vertical

stratification there is a diabatic transport since

$$\rho w^{\text{dia}} = \frac{\partial_z(\kappa \rho \partial_z \theta)}{|\partial_z \theta|} \neq 0. \quad (46.139)$$

In the absence of fluid flow, the dia-surface transport is determined solely by movement of the potential temperature surfaces. Correspondingly, potential temperature evolution is determined only by vertical diffusion since with  $\mathbf{v}^\dagger = 0$  we have

$$\frac{\partial \theta}{\partial t} = \rho^{-1} \frac{\partial}{\partial z} \left[ \kappa \rho \frac{\partial \theta}{\partial z} \right] = w^{\text{dia}} \left| \frac{\partial \theta}{\partial z} \right|. \quad (46.140)$$

#### *Steady state advective-diabatic balance*

A steady state potential temperature field in the presence of diabatic processes is realized when there is an exact balance between advective transport and dia-surface transport enabled by diffusion

$$\rho \mathbf{v}^\dagger \cdot \nabla \theta = \rho w^{\text{dia}} |\nabla \theta| = \nabla \cdot (\kappa \rho \nabla \theta). \quad \text{steady state.} \quad (46.141)$$

That is, maintaining static  $\theta$ -surfaces ( $\partial_t \theta = 0$ ) requires the residual mean advective transport to cross  $\theta$  surfaces (left hand side) by an amount that exactly balances diabatic processes such as diffusion (right hand side). This example illustrates that in the presence of mixing, advection is no longer an adiabatic stirring process. Namely, in the steady state, advection equals diffusion.

## 46.10 Green's function method for passive tracers

Passive tracers (Section 15.2) have no impact on the flow field (and so do not impact the seawater density or diffusion tensor). Hence, passive tracer patterns serve to “trace” the effects from advective and diffusive transport without affecting the transport velocity or diffusion tensor. Correspondingly, the passive tracer advection-diffusion equation is a linear partial differential equation. With some qualifications identified below, we are able to make use of the Green's function methods from Chapter 4 when studying solutions to the passive tracer equation.

In this section we develop the Green's function method for use with the advection-diffusion equation. This section offers a supplement to the review paper from [Haine et al. \(2022\)](#) who synthesize the variety of Green's function methods of use for studying geophysical fluids. Although our formulation is largely based on ocean applications, the Green's function method for the advection-diffusion equation is also applicable to the atmosphere.

### 46.10.1 Concerning time dependent domain boundaries

The ocean free surface is time dependent, so that the domain,  $\mathcal{R}$ , is itself time dependent. Mathematically, this time dependence means that time and space integrations do not commute. In particular, space integration is generally written in the form

$$\int_{\mathcal{R}} dV = \iint \left[ \int_{\eta_b}^{\eta} dz \right] dx dy, \quad (46.142)$$

where  $z = \eta_b(x, y)$  is the static bottom and  $z = \eta(x, y, t)$  is the time dependent free surface. We must, in turn, first compute the space integration over the full domain and then do the time time integration when deriving the reciprocity relation and the Green's function solution.

The free surface undulations make the vertical extent of the domain time dependent. Additionally, in an ocean with sloping sidewalls, the horizontal domain boundaries are also time dependent as the ocean moves up and down the sloping sides. However, allowing for the horizontal domain extent to fluctuate does not introduce any fundamentally new kinematics in our analysis. The reason is that when integrating to the lateral domain boundaries, all terms vanish since the water depth vanishes at the edge of the sloping beaches. We saw this kinematic result when integrating the angular momentum budget in a channel with sloping sidewalls in Section 19.5.

Therefore, we assume the horizontal extent of the domain to be static in order to slightly ease the analysis. We do so by imagining a few meter high vertical seawall placed around the ocean domain edges, and by assuming a minimum depth so that there is nonzero water everywhere in the domain. These assumptions are common in ocean modeling, except in models allowing for wetting and drying of land/ocean cells. So in conclusion, we limit our analysis to time dependence of the vertical extent of the domain, with the horizontal extent static. Such limitation can be removed without much difficulty but doing so adds nothing new fundamentally.

### 46.10.2 Passive tracer boundary conditions

In this section, we are concerned with the evolution of a smooth passive tracer concentration,  $C$ , which is the dimensionless ratio of the tracer mass to seawater mass. Boundary conditions play a key role in the evolution. We here discuss the boundary conditions placed on the passive tracer along the ocean bottom, at  $z = \eta_b(x, y)$ , and the free surface, at  $z = \eta(x, y, t)$ .

#### Ocean bottom

At the static ocean bottom we generically consider a no-flux condition for the diffusive flux

$$\mathbf{J} \cdot \hat{\mathbf{n}} = -\rho \mathbb{K} \cdot \nabla C \cdot \hat{\mathbf{n}} = 0 \quad \text{at } z = \eta_b. \quad (46.143)$$

Along with the kinematic no-normal flow condition,  $\mathbf{v} \cdot \hat{\mathbf{n}} = 0$ , the no-flux condition means that there is zero tracer flux through the bottom.

#### Ocean free surface

At the ocean free surface we use results from Section 14.4.3, which developed the boundary conditions for mass flux  $\mathcal{Q}_m$  (mass per time per area) across a permeable free surface, as well as Section 15.5, which developed the analogous boundary conditions for tracers. In particular, equation (15.79) provides an expression for the net mass flux of tracer crossing the free surface,  $\mathcal{Q}_C$ , written as the sum of an advective flux plus a non-advective flux

$$\mathcal{Q}_C = C \mathcal{Q}_m - \mathbf{J} \cdot \hat{\mathbf{n}} = \underbrace{C \mathcal{Q}_m}_{\text{advective}} + \underbrace{\rho \mathbb{K} \cdot \nabla C \cdot \hat{\mathbf{n}}}_{\text{diffusive}} \quad \text{for } \mathbf{x} \in \partial \mathcal{R}_{\text{surface}}, \quad (46.144)$$

where  $C$  is the concentration at  $z = \eta$ , and we assumed the non-advective flux is given by a diffusive flux. We consider the following prescribed boundary conditions.

- ROBIN CONDITIONS: Prescribing the boundary tracer mass flux,  $\mathcal{Q}_C$ , leads to a Robin or mixed boundary condition

$$\mathcal{Q}_C = \text{prescribed} = C \mathcal{Q}_m + \rho \mathbb{K} \cdot \nabla C \cdot \hat{\mathbf{n}} \quad \text{for } \mathbf{x} \in \partial \mathcal{R}_{\text{surface}}. \quad (46.145)$$

This boundary condition is relevant for enthalpy and salt, with full discussion given in Section 49.5. However, the Robin condition is rarely used for passive tracers along the ocean surface and so it will not be considered further.

- NEUMANN CONDITIONS: Prescribing the diffusive flux leads to the Neumann boundary condition

$$\rho \mathbb{K} \cdot \nabla C \cdot \hat{\mathbf{n}} = \text{prescribed} \equiv \Sigma(\mathbf{x}, t) \quad \text{for } \mathbf{x} \in \partial\mathcal{R}_{\text{surface}}. \quad (46.146)$$

This surface ocean boundary condition is also rarely used for passive tracers, though we will examine it within the following.

- DIRICHLET CONDITIONS: Prescribing the value of the tracer concentration at the boundary leads to the Dirichlet boundary condition

$$C = \text{prescribed} \equiv \sigma(\mathbf{x}, t) \quad \text{for } \mathbf{x} \in \partial\mathcal{R}_{\text{surface}}. \quad (46.147)$$

This boundary condition is the most commonly used condition for passive tracers, and thus will be our favored choice in the following. Note that both the Neumann and Dirichlet conditions generally involve a net transport of tracer,  $\mathcal{Q}_C \neq 0$ , across the ocean boundary.

As we will see in Section 46.10.5, the Neumann boundary condition in the presence of a surface mass flux is problematic due to the associated non-closed reciprocity relation satisfied by the Green's function and its adjoint. The absence of a suitable reciprocity relation makes it difficult to use the Green's function method, since one would need to solve for both the Green's function and its adjoint. In contrast, the Dirichlet condition allows for a simple reciprocity relation, identical to that for the diffusion equation (Section 4.7.4), thus making the Green's function method for the advection-diffusion equation with a Dirichlet condition suitable even in the presence of a surface mass flux (see page 2450 of *Larson* (1999) for a similar point).

### 46.10.3 Advection-diffusion initial-boundary value problem

We study the initial-boundary value problem for a smooth passive tracer concentration,  $C$ , which is the dimensionless ratio of the tracer mass to seawater mass. The tracer is affected by advection and diffusion on a spatial domain,  $\mathcal{R}$ , in the presence of a tracer source,  $\rho \Lambda$  (with dimensions of tracer mass per volume per time), with initial data available for the density and tracer concentration at time  $t = t_{\text{init}}$ . The initial-boundary value problem in the presence of Neumann or Dirichlet boundary conditions is given by

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho \mathbf{v}^\dagger C - \rho \mathbb{K} \cdot \nabla C) = \rho \Lambda \quad \mathbf{x} \in \mathcal{R}, t \geq t_{\text{init}} \quad (46.148a)$$

$$\rho C = \rho I \quad \mathbf{x} \in \mathcal{R}, t = t_{\text{init}} \quad (46.148b)$$

$$\hat{\mathbf{n}} \cdot \rho \mathbb{K} \cdot \nabla C = \rho \Sigma \quad \text{or} \quad \rho C = \rho \sigma \quad \mathbf{x} \in \partial\mathcal{R}, t \geq t_{\text{init}}. \quad (46.148c)$$

The prescribed initial condition data for the tracer concentration at time  $t = t_{\text{init}}$  is given by  $I(\mathbf{x})$ , and the initial density is also prescribed at this time,  $\rho(\mathbf{x}, t_{\text{init}})$ . We consider two options for the boundary condition at  $\mathbf{x} \in \partial\mathcal{R}$ : (i) the Neumann boundary condition with a prescribed flux,  $\hat{\mathbf{n}} \cdot \rho \mathbb{K} \cdot \nabla C = \rho \Sigma$ , or the (ii) Dirichlet boundary condition with a prescribed value,  $\rho C = \rho \sigma$ . Furthermore, we assume the flow field,  $\mathbf{v}(\mathbf{x}, t)$ , the eddy-induced velocity,  $\mathbf{v}^*(\mathbf{x}, t)$ , the seawater density,  $\rho(\mathbf{x}, t)$ , and the diffusivity tensor,  $\mathbb{K}(\mathbf{x}, t)$ , are known functions of space-time that are determined by solving for the dynamics, kinematics, thermodynamics, and active tracers. Finally, we assume the tracer concentration source,  $\Lambda(\mathbf{x}, t)$ , does not itself depend on the tracer concentration,  $C$ , thus ensuring linearity of the partial differential equation (46.148a).

#### 46.10.4 The Green's function and its adjoint

##### *Green's function problem*

The Green's function corresponding to the passive tracer advection-diffusion equations (46.148a)-(46.148c) satisfies the following causal boundary value problem

$$\frac{\partial[\rho G(\mathbf{x}, t|\mathbf{x}_0, t_0)]}{\partial t} + \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger G(\mathbf{x}, t|\mathbf{x}_0, t_0) - \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t|\mathbf{x}_0, t_0)] = \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0) \quad (46.149a)$$

$$G(\mathbf{x}, t < t_0|\mathbf{x}_0, t_0) = 0 \quad (46.149b)$$

$$\hat{\mathbf{n}}_{\mathbf{x}} \cdot \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x} \in \partial\mathcal{R}, t|\mathbf{x}_0, t_0) = 0 \text{ or } G(\mathbf{x} \in \partial\mathcal{R}, t|\mathbf{x}_0, t_0) = 0. \quad (46.149c)$$

The space-time point  $(\mathbf{x}_0, t_0)$  is where the Dirac delta source is located, which is located within the spatial domain,  $\mathcal{R}$ , and occurs after the initial time

$$\mathbf{x}_0 \in \mathcal{R} \quad \text{and} \quad t_0 \geq t_{\text{init}}. \quad (46.150)$$

The Green's function satisfies homogeneous boundary conditions corresponding to those satisfied by the passive tracer concentration in equation (46.148c). Finally, since the Dirac delta source,  $\delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0)$ , has dimensions of inverse volume times inverse time, the Green's function has dimensions of inverse mass. We physically interpret the Green's function as the tracer concentration resulting from an impulsive tracer concentration source, divided by the mass of tracer injected by the source.

##### *Adjoint Green's function problem*

The adjoint Green's function,  $\tilde{G}$ , satisfies the adjoint problem

$$-\frac{\partial[\rho \tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0)]}{\partial t} + \nabla_{\mathbf{x}} \cdot [-\rho \mathbf{v}^\dagger \tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0) - \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t|\mathbf{x}_0, t_0)] = \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0) \quad (46.151a)$$

$$\tilde{G}(\mathbf{x}, t > t_0|\mathbf{x}_0, t_0) = 0 \quad (46.151b)$$

$$\hat{\mathbf{n}}_{\mathbf{x}} \cdot \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x} \in \partial\mathcal{R}, t|\mathbf{x}_0, t_0) = 0 \text{ or } \tilde{G}(\mathbf{x} \in \partial\mathcal{R}, t|\mathbf{x}_0, t_0) = 0. \quad (46.151c)$$

Note the sign change on both the time derivative, as for the diffusion equation in Section 4.7.3, as well as the advection term. The sign change on advection is expected since with time running backwards, so too does the velocity of a fluid particle. Hence, the adjoint advection-diffusion equation is a backwards in time advection-diffusion equation.

#### 46.10.5 Reciprocity relation

We here derive the reciprocity relation satisfied by the Green's function,  $G$ , and its adjoint,  $\tilde{G}$ . The derivation follows that in Section 4.5.4 for the Poisson equation and Section 4.7.4 for the diffusion equation. A new feature here arises from the advection operator, and another arises from allowing the domain boundary to be time dependent as occurs at the ocean free surface. We will see that the reciprocity relation for Neumann boundary conditions (46.149c) and (46.151c) does not “close” when there is mass transport across the ocean free surface (see equation (46.166) below). In contrast, the reciprocity relation closes with Dirichlet boundary conditions, taking the same form as for the diffusion equation in equation (4.129). We have more to say on this distinct behavior after its derivation.

### Notation and setup

We consider the Green's function partial differential equation (46.149a) with a Dirac delta source  $\delta(\mathbf{x} - \mathbf{x}_1) \delta(t - t_1)$ , along with the adjoint Green's function equation (46.151a) with a Dirac delta source,  $\delta(\mathbf{x} - \mathbf{x}_2) \delta(t - t_2)$ , where both sources are within the spatial domain and both occur later than the initial time:

$$\mathbf{x}_1, \mathbf{x}_2 \in \mathcal{R} \quad \text{and} \quad t_{\text{init}} < t_1, t_2. \quad (46.152)$$

We also follow the approach in Section 4.7.4 for the diffusion equation by introducing the arbitrarily large time,  $T$ , such that  $-T < t_1, t_2 < T$ . As for the diffusion problem, causality conditions will ensure that  $T$  drops out from the final expression for the tracer concentration. Additionally, to help ease notational clutter, we make use of the following shorthand where convenient

$$G(\mathbf{x}, t | \mathbf{x}_1, t_1) = G(1) \quad \text{and} \quad \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) = \tilde{G}(2). \quad (46.153)$$

### Cross-multiplication

Multiply the Green's function equation by  $\tilde{G}(2)$  and the adjoint equation by  $G(1)$  to find

$$\tilde{G}(2) \left( \partial_t [\rho G(1)] + \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger G(1) - \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} G(1)] \right) = \tilde{G}(2) \delta(\mathbf{x} - \mathbf{x}_1) \delta(t - t_1) \quad (46.154a)$$

$$G(1) \left( -\partial_t [\rho \tilde{G}(2)] + \nabla_{\mathbf{x}} \cdot [-\rho \mathbf{v}^\dagger \tilde{G}(2) - \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(2)] \right) = G(1) \delta(\mathbf{x} - \mathbf{x}_2) \delta(t - t_2). \quad (46.154b)$$

In the following, we work from the left hand side of equation (46.154a) and bring the differential operators from  $G(1)$  onto  $\tilde{G}(2)$ . The result of this movement will be equation (46.154b) plus some extra terms whose form depends on the causality condition and boundary conditions. Integration over space and time will then render the reciprocity relation.

### Self-adjointness of the generalized Laplacian operator

The generalized Laplacian operator term on the left hand side of equation (46.154a) can be written

$$\begin{aligned} & -\tilde{G}(2) \nabla_{\mathbf{x}} \cdot [\rho \mathbb{K} \cdot \nabla_{\mathbf{x}} G(1)] \\ &= \nabla_{\mathbf{x}} \cdot [-\tilde{G}(2) \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} G(1) + G(1) \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(2)] - G(1) \nabla_{\mathbf{x}} \cdot [\rho \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(2)]. \end{aligned} \quad (46.155)$$

A spatial integration of this equation over the region  $\mathcal{R}$ , and use of the homogeneous boundary conditions in equations (46.148c) or (46.151c) eliminates the divergence term to reveal

$$\begin{aligned} & \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) \nabla_{\mathbf{x}} \cdot [\rho \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_1, t_1)] dV \\ &= \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_1, t_1) \nabla_{\mathbf{x}} \cdot [\rho \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2)] dV. \end{aligned} \quad (46.156)$$

This equality proves that the generalized Laplacian operator with a symmetric diffusion tensor is self-adjoint, which is a result already encountered in Section 4.7.4 when discussing the diffusion equation. This result holds for either Neumann or Dirichlet boundary conditions.

*Time derivative plus advection*

Next write the time derivative and advection portion of equation (46.154a) as

$$\begin{aligned} & \tilde{G}(2) \left( \partial_t[\rho G(1)] + \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger G(1)] \right) \\ &= \partial_t[\tilde{G}(2) \rho G(1)] + \nabla_{\mathbf{x}} \cdot [\tilde{G}(2) \rho \mathbf{v}^\dagger G(1)] - G(1) \rho \left[ \partial_t \tilde{G}(2) + \mathbf{v}^\dagger \cdot \nabla_{\mathbf{x}} \tilde{G}(2) \right] \\ &= \partial_t[\tilde{G}(2) \rho G(1)] + \nabla_{\mathbf{x}} \cdot [\tilde{G}(2) \rho \mathbf{v}^\dagger G(1)] - G(1) \left( \partial_t(\rho \tilde{G}(2)) + \nabla \cdot [\rho \mathbf{v}^\dagger \tilde{G}(2)] \right), \end{aligned} \quad (46.157)$$

where we used the mass continuity equation (14.6) for the final equality. Rearrangement thus leads to

$$\begin{aligned} & \tilde{G}(2) \left( \partial_t[\rho G(1)] + \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger G(1)] \right) - G(1) \left( -\partial_t[\rho \tilde{G}(2)] - \nabla \cdot [\rho \mathbf{v}^\dagger \tilde{G}(2)] \right) \\ &= \partial_t[\tilde{G}(2) \rho G(1)] + \nabla_{\mathbf{x}} \cdot [\tilde{G}(2) \rho \mathbf{v}^\dagger G(1)]. \end{aligned} \quad (46.158)$$

*Space integration*

Now integrate equations (46.154a) and (46.154b) over the spatial domain,  $\mathcal{R}$ , subtract these two equations, and make use of the results (46.156) and (46.158) to reveal

$$\begin{aligned} & \tilde{G}(\mathbf{x}_1, t | \mathbf{x}_2, t_2) \delta(t - t_1) - G(\mathbf{x}_2, t | \mathbf{x}_1, t_1) \delta(t - t_2) \\ &= \int_{\mathcal{R}} \left[ \partial_t[\tilde{G}(2) \rho G(1)] + \nabla_{\mathbf{x}} \cdot [\tilde{G}(2) \rho \mathbf{v}^\dagger G(1)] \right] dV. \end{aligned} \quad (46.159)$$

The divergence term on the right hand side takes the form

$$\int_{\mathcal{R}} \nabla_{\mathbf{x}} \cdot [\tilde{G}(2) \rho \mathbf{v}^\dagger G(1)] dV = \oint_{\partial \mathcal{R}} \tilde{G}(2) G(1) \rho \mathbf{v}^\dagger \cdot \hat{\mathbf{n}}_{\mathbf{x}} d\mathcal{S} \quad \text{divergence theorem} \quad (46.160a)$$

$$= \oint_{\partial \mathcal{R}} \tilde{G}(2) G(1) \rho \mathbf{v} \cdot \hat{\mathbf{n}}_{\mathbf{x}} d\mathcal{S} \quad \hat{\mathbf{n}} \cdot \mathbf{v}^* = 0 \quad (46.160b)$$

$$= \int_{z=\eta} \tilde{G}(2) G(1) \rho \mathbf{v} \cdot \hat{\mathbf{n}}_{\mathbf{x}} d\mathcal{S} \quad \mathbf{v} \cdot \hat{\mathbf{n}} = 0 \text{ for } z = \eta_b \quad (46.160c)$$

$$= \int_{z=\eta} \tilde{G}(2) G(1) \rho \mathbf{v} \cdot \nabla(z - \eta) dA \quad \text{equation (14.76)} \quad (46.160d)$$

$$= \int_{z=\eta} \tilde{G}(2) G(1) \rho (w - \mathbf{u} \cdot \nabla \eta) dA. \quad (46.160e)$$

The time derivative term takes the form

$$\int_{\mathcal{R}} \partial_t[\tilde{G}(2) G(1) \rho] dV = \frac{\partial}{\partial t} \left[ \int_{\mathcal{R}} \tilde{G}(2) G(1) \rho dV \right] - \int_{z=\eta} \left[ \tilde{G}(2) G(1) \rho \partial_t \eta \right] dA, \quad (46.161)$$

where we made use of Leibniz's rule to bring the time derivative across the integral sign and made note of the time dependent free surface,  $z = \eta(x, y, t)$ . Combining equations (46.161) and

(46.160e) leads to

$$\tilde{G}(\mathbf{x}_1, t | \mathbf{x}_2, t_2) \delta(t - t_1) - G(\mathbf{x}_2, t | \mathbf{x}_1, t_1) \delta(t - t_2) \quad (46.162a)$$

$$= \frac{\partial}{\partial t} \left[ \int_{\mathcal{R}} \tilde{G}(2) G(1) \rho dV \right] + \int_{z=\eta} \tilde{G}(2) G(1) [\rho (w - \mathbf{u} \cdot \nabla \eta - \partial_t \eta)] dA \quad (46.162b)$$

$$= \frac{\partial}{\partial t} \left[ \int_{\mathcal{R}} \tilde{G}(2) G(1) \rho dV \right] - \int_{z=\eta} \tilde{G}(2) G(1) Q_m dA, \quad (46.162c)$$

where the final equality follows from the surface ocean kinematic boundary condition (14.79), with  $Q_m$  the mass per time per horizontal area crossing the ocean surface.

### Time integration

We are now ready to integrate equation (46.162c) over time, with its left hand side leading to

$$\begin{aligned} \int_{-T}^T \left[ \tilde{G}(\mathbf{x}_1, t | \mathbf{x}_2, t_2) \delta(t - t_1) - G(\mathbf{x}_2, t | \mathbf{x}_1, t_1) \delta(t - t_2) \right] dt \\ = \tilde{G}(\mathbf{x}_1, t_1 | \mathbf{x}_2, t_2) - G(\mathbf{x}_2, t_2 | \mathbf{x}_1, t_1), \end{aligned} \quad (46.163)$$

which used the sifting property (4.28). There are two terms that appear when time integrating the time derivative from equation (46.162c), with each term vanishing due to the causality conditions (46.149b) and (46.151b)

$$\int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t = T | \mathbf{x}_2, t_2) G(\mathbf{x}, t = T | \mathbf{x}_1, t_1) \rho dV = 0 \iff \tilde{G}(\mathbf{x}, t = T | \mathbf{x}_2, t_2) = 0 \quad (46.164)$$

$$\int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t = t_{\text{init}} | \mathbf{x}_2, t_2) G(\mathbf{x}, t = t_{\text{init}} | \mathbf{x}_1, t_1) \rho dV = 0 \iff G(\mathbf{x}, t = t_{\text{init}} | \mathbf{x}_1, t_1) = 0. \quad (46.165)$$

We are thus left with

$$\tilde{G}(\mathbf{x}_1, t_1 | \mathbf{x}_2, t_2) - G(\mathbf{x}_2, t_2 | \mathbf{x}_1, t_1) = - \int_{t_{\text{init}}}^{t_1} \left[ \int_{z=\eta} \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) G(\mathbf{x}_1, t_1 | \mathbf{x}, t) Q_m dA \right] dt, \quad (46.166)$$

which we refer to as a *non-closed reciprocity relation* between  $G$  and  $\tilde{G}$ . Note that the time limits on the integral follow from causality on the Green's function and its adjoint.

### Closed form reciprocity in special cases

There are two cases in which the relation (46.166) leads to a closed reciprocity relation:

- Zero mass flux across surface:  $Q_m = 0$ .
- Homogeneous Dirichlet boundary conditions:  $\tilde{G}(\mathbf{x} \in \partial \mathcal{R}, t | \mathbf{x}_0, t_0) = G(\mathbf{x} \in \partial \mathcal{R}, t | \mathbf{x}_0, t_0) = 0$ .

In either case we are led to

$$\tilde{G}(\mathbf{x}_1, t_1 | \mathbf{x}_2, t_2) = G(\mathbf{x}_2, t_2 | \mathbf{x}_1, t_1), \quad (46.167)$$

which is the same reciprocity (4.129) satisfied for the diffusion equation Green's functions.

The more nuanced reciprocity for the advection-diffusion equation arises from the advective mass flux at the ocean free surface boundary. The mass flux couples the ocean with its surrounding media (e.g., the atmosphere, rivers, or cryosphere), and in so doing precludes a general closed reciprocity relation. However, the Dirichlet boundary condition closes the surface boundary through the homogeneous Green's function boundary conditions. Most applications of Green's function methods for passive ocean tracers make use of Dirichlet boundary conditions, in which case we are afforded a closed reciprocity relation even with a free surface open to mass transport.

#### 46.10.6 Composition property

We here follow the analysis of Section 4.7.5 to derive the composition property of the Green's function for the advection-diffusion equation. For this purpose, return to the cross-multiplication equations (46.154a) and (46.154b) used to derive reciprocity, here written as

$$\tilde{G}(2) \left( \partial_t [\rho G(1)] + \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger G(1) - \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} G(1)] \right) = \tilde{G}(2) \delta(\mathbf{x} - \mathbf{x}_1) \delta(t - t_1) \quad (46.168a)$$

$$G(1) \left( \partial_t [\rho \tilde{G}(2)] + \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger \tilde{G}(2) + \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(2)] \right) = -G(1) \delta(\mathbf{x} - \mathbf{x}_2) \delta(t - t_2). \quad (46.168b)$$

Adding these two equations and use of mass continuity (14.6) brings the left hand side to

$$\text{LHS} = \partial_t [\rho G(1) \tilde{G}(2)] + \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger G(1) \tilde{G}(2) + \rho G(1) \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(2) - \rho \tilde{G}(2) \mathbb{K} \cdot \nabla_{\mathbf{x}} G(1)]. \quad (46.169)$$

Integration over the domain  $\mathcal{R}$  eliminates the diffusion terms for both the Dirichlet and Neumann boundary conditions. For the time derivative term we use Leibniz's rule to write

$$\int_{\mathcal{R}} \partial_t [\rho G(1) \tilde{G}(2)] dV = \frac{d}{dt} \int_{\mathcal{R}} \rho G(1) \tilde{G}(2) dV - \int_{z=\eta} \rho G(1) \tilde{G}(2) \partial_t \eta dA. \quad (46.170a)$$

For the advection term we follow the manipulations used for equation (46.160e) to derive

$$\int_{\mathcal{R}} \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger G(1) \tilde{G}(2)] dV = \int_{z=\eta} \rho G(1) \tilde{G}(2) \mathbf{v}^\dagger \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (46.171a)$$

$$= \int_{z=\eta} \rho G(1) \tilde{G}(2) (w - \mathbf{u} \cdot \nabla \eta) dA \quad (46.171b)$$

$$= \int_{z=\eta} G(1) \tilde{G}(2) (\rho \partial_t \eta - Q_m) dA. \quad (46.171c)$$

Bringing the pieces together and expanding the arguments leads to

$$\begin{aligned} \frac{d}{dt} \int_{\mathcal{R}} \rho(\mathbf{x}, t) G(\mathbf{x}, t | \mathbf{x}_1, t_1) \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) dV &= \tilde{G}(\mathbf{x}_1, t | \mathbf{x}_2, t_2) \delta(t - t_1) \\ &\quad - G(\mathbf{x}_2, t | \mathbf{x}_1, t_1) \delta(t - t_2) - \int_{z=\eta} G(\mathbf{x}, t | \mathbf{x}_1, t_1) \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) Q_m(\mathbf{x}, t) dA. \end{aligned} \quad (46.172)$$

As for the derivation of reciprocity in Section 46.10.5, we here assume either  $Q_m = 0$  or a homogeneous Dirichlet boundary condition so that

$$\begin{aligned} \frac{d}{dt} \int_{\mathcal{R}} \rho(\mathbf{x}, t) G(\mathbf{x}, t | \mathbf{x}_1, t_1) \tilde{G}(\mathbf{x}, t | \mathbf{x}_2, t_2) dV &= \tilde{G}(\mathbf{x}_1, t | \mathbf{x}_2, t_2) \delta(t - t_1) \\ &\quad - G(\mathbf{x}_2, t | \mathbf{x}_1, t_1) \delta(t - t_2). \end{aligned} \quad (46.173)$$

This equation is directly analogous to equation (4.138) satisfied by the diffusion equation Green's function. Following from that analysis, and making use of reciprocity (46.167), we find the composition property for the advection-diffusion equation in a non-Boussinesq fluid

$$G(\mathbf{x}_2, t_2 | \mathbf{x}_1, t_1) = \int_{\mathcal{R}} \rho(\mathbf{x}, \tau) G(\mathbf{x}_2, t_2 | \mathbf{x}, \tau) G(\mathbf{x}, \tau | \mathbf{x}_1, t_1) dV \quad \text{if } t_1 < \tau < t_2. \quad (46.174)$$

The left hand side of this equation is the response from a Dirac source that is advected-diffused from  $(\mathbf{x}_1, t_1)$  and measured at the space-time point  $(\mathbf{x}_2, t_2)$ . The right hand side is the composition of a Green's function feeling the source at  $(\mathbf{x}_1, t_1)$  but now sampled at an intermediate space-time position,  $(\mathbf{x}, \tau)$ , and then further advective-diffused to  $(\mathbf{x}_2, t_2)$ , with integration over all possible intermediate positions  $\mathbf{x}$ . The intermediate sampling can occur at an arbitrary intermediate time  $\tau$ , so long as  $t_1 < \tau < t_2$ . The composition property (46.174) allows us to conceive of a long-time interval Green's function as the composition of an arbitrary number of shorter time interval Green's functions.

#### 46.10.7 Integral expression for the tracer concentration

We are now ready to express the passive tracer concentration,  $C$ , as a suite of integrals involving the Green's function and the known boundary and initial conditions as well as the known source function. The process for deriving this expression is identical to that used in Section 46.10.5 for reciprocity, with the following steps offered for completeness.

##### *Derivation setup*

The initial-boundary value problem for the passive tracer is given by

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho \mathbf{v}^\dagger C - \rho \mathbb{K} \cdot \nabla C) = \rho \Lambda \quad \mathbf{x} \in \mathcal{R}, t \geq t_{\text{init}} \quad (46.175a)$$

$$\rho C = \rho I \quad \mathbf{x} \in \mathcal{R}, t = t_{\text{init}} \quad (46.175b)$$

$$\rho C = \rho \sigma \quad \mathbf{x} \in \partial \mathcal{R}, t \geq t_{\text{init}} \quad (46.175c)$$

where we only consider the Dirichlet boundary condition to ensure a closed reciprocity relation in the presence of surface mass fluxes (Section 46.10.5). The corresponding adjoint Green's function satisfies

$$-\frac{\partial[\rho \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0)]}{\partial t} + \nabla_{\mathbf{x}} \cdot [-\rho \mathbf{v}^\dagger \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) - \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0)] = \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0) \quad (46.176a)$$

$$\tilde{G}(\mathbf{x}, t > t_0 | \mathbf{x}_0, t_0) = 0 \quad (46.176b)$$

$$\tilde{G}(\mathbf{x} \in \partial \mathcal{R}, t | \mathbf{x}_0, t_0) = 0, \quad (46.176c)$$

with the reciprocity condition (46.167) holding since we chose Dirichlet boundary conditions. Multiplying the adjoint Green's function equation (46.176a) by  $C(\mathbf{x}, t)$  and performing manipulations just like those for reciprocity leads to

$$\begin{aligned} -\partial_t(\rho C \tilde{G}) + \nabla_{\mathbf{x}} \cdot [\tilde{G} \rho \mathbb{K} \cdot \nabla C - C \rho \mathbb{K}(\mathbf{x}, t) \cdot \nabla_{\mathbf{x}} \tilde{G} - C \rho \mathbf{v}^\dagger \tilde{G}] + \tilde{G} \rho \Lambda \\ = C(\mathbf{x}, t) \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0). \end{aligned} \quad (46.177)$$

With the homogeneous Dirichlet conditions satisfied by  $\tilde{G}$  on the spatial boundaries, a space and time integration over  $(\mathbf{x}, t)$  leads to

$$C(\mathbf{x}_0, t_0) = \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t_{\text{init}} | \mathbf{x}_0, t_0) \rho(\mathbf{x}, t_{\text{init}}) I(\mathbf{x}) dV + \int_{t_{\text{init}}}^{t_0} \left[ \int_{\mathcal{R}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \rho(\mathbf{x}, t) \Lambda(\mathbf{x}, t) dV \right] dt - \int_{t_{\text{init}}}^{t_0} \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}, t) \rho(\mathbf{x}, t) \mathbb{K}(\mathbf{x}, t) \cdot \nabla_{\mathbf{x}} \tilde{G}(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}} d\mathcal{S} \right] dt. \quad (46.178)$$

Use of the reciprocity relation (46.167) allows us to write this equation in terms of the Green's function rather than the adjoint Green's function

$$C(\mathbf{x}_0, t_0) = \int_{\mathcal{R}} G(\mathbf{x}_0, t_0 | \mathbf{x}, t_{\text{init}}) \rho(\mathbf{x}, t_{\text{init}}) I(\mathbf{x}) dV + \int_{t_{\text{init}}}^{t_0} \left[ \int_{\mathcal{R}} G(\mathbf{x}_0, t_0 | \mathbf{x}, t) \rho(\mathbf{x}, t) \Lambda(\mathbf{x}, t) dV \right] dt - \int_{t_{\text{init}}}^{t_0} \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}, t) \rho(\mathbf{x}, t) \mathbb{K}(\mathbf{x}, t) \cdot \nabla_{\mathbf{x}} G(\mathbf{x}_0, t_0 | \mathbf{x}, t) \cdot \hat{\mathbf{n}}_{\mathbf{x}} d\mathcal{S} \right] dt. \quad (46.179)$$

Finally, swapping labels  $(\mathbf{x}_0, t_0) \leftrightarrow (\mathbf{x}, t)$  renders

$$C(\mathbf{x}, t) = \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) \rho(\mathbf{x}_0, t_{\text{init}}) I(\mathbf{x}_0) dV_0 + \int_{t_{\text{init}}}^t \left[ \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \rho(\mathbf{x}_0, t_0) \Lambda(\mathbf{x}_0, t_0) dV_0 \right] dt_0 - \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) \rho(\mathbf{x}_0, t_0) \mathbb{K}(\mathbf{x}_0, t_0) \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} d\mathcal{S}_0 \right] dt_0. \quad (46.180)$$

This solution manifests causality since the concentration at time  $t$  is a function only of processes occurring from  $t_{\text{init}}$  up to time  $t$ .

#### 46.10.8 Properties of the solution

The integral solution (46.180) is of the same form as equation (4.150) for the diffusion equation. Properties of this solution, and corresponding properties of the Green's function, follow from those satisfied by the diffusion equation as detailed in Section 4.7.7. We here summarize these properties for completeness.

##### *The role of advection and diffusion at boundaries*

Explicit contributions from the advective flux are absent from the solution (46.180). Namely, there are no advective flux contributions at the surface boundary due to the homogeneous Dirichlet boundary conditions imposed on the Green's function. For the ocean bottom, material and rigid no-flux conditions mean that  $\mathbf{v} \cdot \hat{\mathbf{n}} = 0$  at the bottom. The presence of advection arises only through its effect on the Green's function, which is affected by both advection and diffusion.

Furthermore, notice how in the absence of diffusion (i.e.,  $\mathbb{K} = 0$ ) the Dirichlet boundary data is unable to penetrate into the ocean interior since the surface boundary integral vanishes from equation (46.180). In effect, the surface boundary becomes a material surface when there is no diffusion. That is, diffusive mixing is needed for boundary data to move into the interior. This role for diffusion was also identified when studying the surface flux condition for salt and freshwater in Section 49.5 (see also [Nurser and Griffies \(2019\)](#)).

### *Initial conditions*

When sampling the tracer concentration at the initial time,  $t \rightarrow t_{\text{init}}$ , all the time integrals vanish from the solution (46.180), thus leaving

$$\lim_{t \rightarrow t_{\text{init}}} C(\mathbf{x}, t) = \lim_{t \rightarrow t_{\text{init}}} \int_{\mathcal{R}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) \rho(\mathbf{x}_0, t_{\text{init}}) I(\mathbf{x}_0) dV_0. \quad (46.181)$$

Self-consistency implies that the Green's function satisfies

$$\lim_{t \rightarrow t_{\text{init}}} G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) \rho(\mathbf{x}_0, t_{\text{init}}) = \delta(\mathbf{x} - \mathbf{x}_0) \quad \text{with } \mathbf{x}, \mathbf{x}_0 \in \mathcal{R}, \quad (46.182)$$

so that

$$\lim_{t \rightarrow t_{\text{init}}} \int_{\mathcal{R}} \rho(\mathbf{x}, t_{\text{init}}) G(\mathbf{x}, t | \mathbf{x}_0, t_{\text{init}}) I(\mathbf{x}_0) dV_0 = \int_{\mathcal{R}} \delta(\mathbf{x} - \mathbf{x}_0) I(\mathbf{x}_0) dV_0 = I(\mathbf{x}). \quad (46.183)$$

### *Dirichlet boundary conditions*

Evaluating the Dirichlet solution (46.180) on a spatial boundary,  $\mathbf{x} \in \partial\mathcal{R}$ , eliminates both the volume integrals given that the Green's function satisfies homogeneous Dirichlet boundary conditions. The tracer concentration (46.180) thus takes the form

$$C(\mathbf{x}, t) = - \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) \rho(\mathbf{x}_0, t_0) \mathbb{K}(\mathbf{x}_0, t_0) \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} d\mathcal{S}_0 \right] dt_0 \quad \text{with } \mathbf{x} \in \partial\mathcal{R}. \quad (46.184)$$

Self-consistency with the Dirichlet boundary condition (46.148c) implies that the Green's function, when both spatial points are evaluated on the boundary, satisfies

$$\rho(\mathbf{x}_0, t_0) \mathbb{K}(\mathbf{x}_0, t_0) \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} = -\delta(t - t_0) \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) \quad \text{with } \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}, \quad (46.185)$$

so that

$$C(\mathbf{x}, t) = \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) \delta(t - t_0) \delta^{(2)}(\mathbf{x} - \mathbf{x}_0) d\mathcal{S}_0 \right] dt_0 = \sigma(\mathbf{x}, t) \quad \text{with } \mathbf{x} \in \partial\mathcal{R}. \quad (46.186)$$

### 46.10.9 Boundary propagator

#### *Defining the boundary propagator*

As for the diffusion equation in Section 4.7.8, we here introduce the boundary propagator for the advection-diffusion equation with Dirichlet boundary conditions. For this purpose, consider the special case of a passive tracer with zero interior source and with zero initial condition, thus satisfying the initial-boundary value problem

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho \mathbf{v}^\dagger C - \rho \mathbb{K} \cdot \nabla C) = 0 \quad \mathbf{x} \in \mathcal{R}, t \geq t_{\text{init}} \quad (46.187a)$$

$$\rho C = 0 \quad \mathbf{x} \in \mathcal{R}, t = t_{\text{init}} \quad (46.187b)$$

$$\rho C = \rho \sigma \quad \mathbf{x} \in \partial\mathcal{R}, t \geq t_{\text{init}}, \quad (46.187c)$$

which leads to the simplification of the Green's function solution (46.180)

$$C(\mathbf{x}, t) = - \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) \rho(\mathbf{x}_0, t_0) \mathbb{K}(\mathbf{x}_0, t_0) \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} d\mathcal{S}_0 \right] dt_0. \quad (46.188)$$

The tracer concentration at a point in space-time is determined by the history of the advection and diffusion that transfers boundary information to this point. To manifest this cause-effect relation, it is useful to define the boundary propagator just as for the diffusion equation

$$G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) \equiv -\rho(\mathbf{x}_0, t_0) \mathbb{K}(\mathbf{x}_0, t_0) \cdot \nabla_{\mathbf{x}_0} G(\mathbf{x}, t | \mathbf{x}_0, t_0) \cdot \hat{\mathbf{n}}_{\mathbf{x}_0} \quad \text{with } \mathbf{x}_0 \in \partial\mathcal{R}, \quad (46.189)$$

with  $G^{\text{bp}}$  having dimensions  $\text{L}^{-2} \text{T}^{-1}$ . The boundary propagator thus brings the tracer concentration (46.188) into the rather tidy form

$$C(\mathbf{x}, t) = \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} \sigma(\mathbf{x}_0, t_0) G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) d\mathcal{S}_0 \right] dt_0. \quad (46.190)$$

#### *Inhomogeneous Dirichlet at the surface and homogeneous Neumann at the bottom*

In applications of passive tracers to study ocean circulation, it is common to apply inhomogeneous Dirichlet boundary conditions just at the ocean surface, and homogeneous Neumann boundary conditions (no-flux) at the ocean bottom

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho \mathbf{v}^\dagger C - \rho \mathbb{K} \cdot \nabla C) = 0 \quad \mathbf{x} \in \mathcal{R}, t \geq t_{\text{init}} \quad (46.191a)$$

$$C = 0 \quad \mathbf{x} \in \mathcal{R}, t = t_{\text{init}} \quad (46.191b)$$

$$\rho C = \rho \sigma \quad \mathbf{x} \in \partial\mathcal{R}_{\text{surface}}, t \geq t_{\text{init}} \quad (46.191c)$$

$$\hat{\mathbf{n}}_{\mathbf{x}} \cdot \mathbb{K} \cdot \nabla_{\mathbf{x}} C = 0 \quad \mathbf{x} \in \partial\mathcal{R}_{\text{bottom}}, t \geq t_{\text{init}}. \quad (46.191d)$$

Note that since  $\hat{\mathbf{n}} \cdot \mathbf{v} = 0$  at the solid earth ocean bottom, kinematics imposes no advective flux through the bottom,  $\hat{\mathbf{n}} \cdot \mathbf{v} C = 0$ . Since the bottom boundary conditions are homogeneous, the solution (46.188) also holds for the initial-boundary value problem (46.191a)-(46.191d). The key distinction, however, is that the Green's function now satisfies the following boundary value problem

$$\frac{\partial[\rho G(\mathbf{x}, t | \mathbf{x}_0, t_0)]}{\partial t} + \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger G(\mathbf{x}, t | \mathbf{x}_0, t_0) - \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_0, t_0)] = \delta(\mathbf{x} - \mathbf{x}_0) \delta(t - t_0) \quad (46.192a)$$

$$G(\mathbf{x}, t < t_0 | \mathbf{x}_0, t_0) = 0 \quad (46.192b)$$

$$G(\mathbf{x}, t | \mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \partial\mathcal{R}_{\text{surface}} \quad (46.192c)$$

$$\hat{\mathbf{n}}_{\mathbf{x}} \cdot \mathbb{K} \cdot \nabla_{\mathbf{x}} G(\mathbf{x}, t | \mathbf{x}_0, t_0) = 0 \quad \mathbf{x} \in \partial\mathcal{R}_{\text{bottom}}. \quad (46.192d)$$

#### *Boundary value problem for the boundary propagator*

Following the more detailed presentation in Section 4.7.8 for the diffusion equation, we are led to the following boundary value problem satisfied by the boundary propagator

$$\frac{\partial[\rho G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0)]}{\partial t} + \nabla_{\mathbf{x}} \cdot [\rho \mathbf{v}^\dagger G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) - \rho \mathbb{K} \cdot \nabla_{\mathbf{x}} G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0)] = 0, \quad \mathbf{x} \in \mathcal{R} \quad (46.193a)$$

$$G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) = 0, \quad \mathbf{x} \notin \partial\mathcal{R}, t \leq t_0 \quad (46.193b)$$

$$G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) = \delta(t - t_0) \delta^{(2)}(\mathbf{x} - \mathbf{x}_0), \quad \mathbf{x}, \mathbf{x}_0 \in \partial\mathcal{R}. \quad (46.193c)$$

The boundary propagator acts as the mediator between boundary data,  $\sigma$ , and interior points, with the transfer of information realized through both advection and diffusion. A focus on the boundary propagator rather than the Green's function allows us to dispense with the need to compute the normal gradient of the Green's function at the boundary, with that calculation rather awkward in practice. Also recall our discussion in Section 4.8.5, where we argued that the boundary propagator can be considered the impulse response function for spatially distributed sources. Here, the mediation of the Dirac boundary sources is performed by advection plus diffusion, whereas in Section 4.8 we only considered linear damping and diffusion.

#### *Normalization of the boundary propagator*

As seen in Sections 46.3 and 46.4, diffusion acts to smooth all structure in the tracer field. Hence, if the boundary data is a uniform constant,  $\sigma = \sigma_{\text{const}}$ , then given sufficient time the tracer concentration will equal to this constant,  $C = \sigma_{\text{const}}$ . This steady state result is independent of details for the velocity field and for the diffusivity tensor, with details of advection and the diffusivity acting only to modify the time scale for the equilibration. Assuming we wait long enough, or equivalently that the initial condition occurs infinitely far in the past, then the tracer concentration solution (46.190) leads to the normalization of the boundary propagator

$$\lim_{t_{\text{init}} \rightarrow -\infty} \int_{t_{\text{init}}}^t \left[ \oint_{\partial\mathcal{R}} G^{\text{bp}}(\mathbf{x}, t | \mathbf{x}_0, t_0) d\mathcal{S}_0 \right] dt_0 = 1 \quad \text{for } \mathbf{x} \in \mathcal{R}. \quad (46.194)$$

This normalization holds for all field points,  $\mathbf{x}$ , within the region. Even though this condition was derived by assuming the special case of constant boundary data, it holds in general since the Green's function, and by extension the boundary propagator, are independent of the boundary data prescribed for the tracer concentration.



## 46.11 Exercises

### EXERCISE 46.1: VERTICAL DIFFUSION OF TEMPERATURE IN THE OCEAN ([Vallis, 2017](#))

There is a natural time scale associated with diffusive transport. This time scale can be found from scaling the diffusion equation, which reveals that it takes the form

$$\tau_{\text{diffusion}} = \frac{\Delta^2}{\kappa} \quad (46.195)$$

where  $\Delta$  is the length scale and  $\kappa$  is the kinematic diffusivity (dimensions of squared length per time). We now make use of this time scale to consider the diffusion of temperature in the ocean, with diffusion due solely to molecular processes.

Using the observed value of molecular diffusivity of temperature in water (look it up), estimate the time for a temperature anomaly to mix from the top of the ocean to the bottom, assuming vertical diffusion through the molecular diffusivity is the only means for mixing. This time scale follows from the one-dimensional diffusion equation and is determined by the diffusivity and the depth of the ocean. Comment on whether you think the real ocean has reached equilibrium after the last ice age (which ended about 12Kyr ago).

### EXERCISE 46.2: ANALYTICAL SOLUTION TO ONE-DIMENSIONAL DIFFUSION EQUATION

Consider a one-dimensional diffusion equation

$$\frac{\partial C}{\partial t} = \kappa \frac{\partial^2 C}{\partial z^2}, \quad (46.196)$$

where  $C$  is a tracer concentration (e.g., temperature or salinity),  $\kappa$  is a constant kinematic diffusivity, and  $z$  is the vertical coordinate. Assume the domain has fixed boundaries at  $z = 0$  and  $z = H$ .

- (a) Assume there is a zero flux of tracer at the two boundaries. Mathematically express this no-flux boundary condition.
- (b) Assume that the initial tracer concentration is confined to an area near the center of the domain. Use dimensional analysis to estimate the time scale for the concentration to homogenize throughout the domain.
- (c) Consider the initial-boundary value problem

$$\frac{\partial C}{\partial t} = \kappa \frac{\partial^2 C}{\partial z^2}, \quad (46.197a)$$

$$\text{no-flux boundary condition from part (b)} \quad (46.197b)$$

$$C(z, t = 0) = C_0 \cos(Kz), \quad (46.197c)$$

where  $C_0$  is a constant. What values for the wave-number,  $K$ , satisfy the no-flux boundary condition?

- (d) Solve the diffusion equation analytically for the given initial condition. Hint: consult your favorite partial differential equation book to learn how to solve this linear 1+1 dimensional diffusion equation.
- (e) Explain how the analytical answer you obtained is consistent with the dimensional analysis answer from part (b).

#### EXERCISE 46.3: DISSIPATIVE PROPERTIES OF DIFFUSION

This exercise explores the dissipative property of diffusion when acting on a tracer extrema.

- (a) ONE-DIMENSIONAL DIFFUSION

Consider the diffusion equation in one spatial dimension, and assume a Boussinesq fluid in which case the density factors are all constant and so can be dropped

$$\frac{\partial C}{\partial t} = \frac{\partial}{\partial z} \left[ \kappa \frac{\partial C}{\partial z} \right] \quad (46.198a)$$

$$= \frac{\partial \kappa}{\partial z} \frac{\partial C}{\partial z} + \kappa \frac{\partial^2 C}{\partial z^2}, \quad (46.198b)$$

where  $\kappa(z, t)$  is an *eddy diffusivity* (also *turbulent diffusivity*). The eddy diffusivity is assumed to be a function of  $(z, t)$ , with the spatial dependence determined by the flow. Show that a tracer extrema,  $C^*$ , evolves under diffusion according to

$$\frac{\partial C^*}{\partial t} = \kappa \frac{\partial^2 C^*}{\partial z^2}. \quad (46.199)$$

So what does diffusion do to a local maxima (e.g., a local hot region) in the tracer field? What about a minima (e.g., a local cold region)?

## (b) THREE-DIMENSIONAL DIFFUSION

Generalize the above one dimensional result to three dimensions, whereby the diffusivity  $\kappa$  becomes a symmetric positive-definite diffusion *tensor*, in which case

$$\frac{\partial C}{\partial t} = \frac{\partial}{\partial x^m} \left[ \mathbb{K}^{mn} \frac{\partial C}{\partial x^n} \right]. \quad (46.200)$$

Now consider an extrema in the tracer field, which is defined by

$$\frac{\partial C^*}{\partial x^n} = 0 \quad \forall n = 1, 2, 3. \quad (46.201)$$

Prove that three dimensional diffusion acts to *dissipate* an extrema. Hint: recall some linear algebra properties of a symmetric positive-definite matrix. In particular, note that a symmetric positive-definite matrix has positive eigenvalues.

**EXERCISE 46.4: DIFFUSION INCREASES INFORMATION ENTROPY OF A TRACER CONCENTRATION**  
 Diffusion is an irreversible process. Here we illustrate this property by considering the *information entropy* associated with a non-negative tracer concentration<sup>4</sup>

$$\mathcal{S}_C \equiv - \int (C \ln C) \rho dV. \quad (46.202)$$

Show that

$$\frac{d\mathcal{S}_C}{dt} \geq 0 \quad (46.203)$$

over a material region with  $C > 0$  and diffusion downgradient,  $\mathbf{J} \cdot \nabla C < 0$ . That is, diffusion always increases the information entropy. Hint: follow the discussion of tracer moments in Section 46.4.3.

**EXERCISE 46.5: ONE-DIMENSIONAL ADVECTION**

Consider the advection equation in one space dimension without boundaries

$$\frac{\partial C}{\partial t} + u \frac{\partial C}{\partial x} = 0 \quad (46.204a)$$

$$C(x, z, t = 0) = C_0 \cos(kx) \quad (46.204b)$$

$$u(z, t) = \alpha z \cos(\omega t). \quad (46.204c)$$

The specified zonal velocity is non-divergent, oscillatory in time, and vertically sheared

$$\frac{\partial u}{\partial z} = \alpha \cos(\omega t), \quad (46.205)$$

with  $\omega$  the radial frequency of the temporal oscillations. What is the tracer concentration at times  $t > 0$ ? Hint: make use of the exact solution given by equation (46.44).

**EXERCISE 46.6: SKEW FLUX FOR OCEAN MESOSCALE EDDIES**

Consider a middle-latitude mesoscale ocean eddy respecting geostrophic balance (see Section 25.4) on an *f*-plane (constant Coriolis parameter) and incompressibility. In this case, the horizontal eddy-induced velocity at the ocean surface is non-divergent

$$\mathbf{u}^* = \nabla \times \hat{\mathbf{z}} \psi. \quad (46.206)$$

---

<sup>4</sup>Information entropy is used in statistical physics as a measure of the order/disorder of a probability distribution. We here apply these notions to measure the information entropy of a tracer concentration.

In this equation, the geostrophic streamfunction is given by

$$\psi = -\hat{z} \frac{g \eta}{f}, \quad (46.207)$$

with  $f$  the Coriolis parameter,  $g$  the gravitational acceleration, and  $\eta$  the sea level undulation associated with the eddy. Since the fluid is incompressible, the mass transport equals to the volume transport times a constant reference density,  $\rho_0$ .

- (a) Determine the skew diffusion tensor (46.66).
- (b) Determine the skew tracer flux (46.79a).

#### EXERCISE 46.7: INTEGRATION BETWEEN TWO CLOSED TRACER CONTOURS

This exercise introduces some ideas of use for determining processes affecting the transport of matter across a tracer contour. Note that in general, the tracer concentration is a function of time. However, the present suite of questions concerns the instantaneous geometry of the tracer field, so that time dependence is not considered.

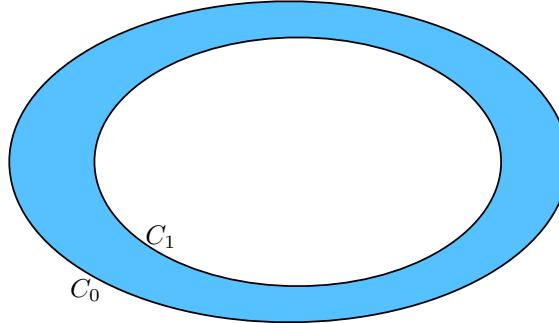


FIGURE 46.5: Illustrating the area contained between two closed tracer contours,  $C_0 \leq C(x, y, t) \leq C_1$ . Exercise 46.7 develops some mathematical expressions for integration within this area, with the resulting expressions of use for the analyses of tracer transport.

- (a) Consider a closed two-dimensional region bounded by two contours of tracer concentration,  $C_0 \leq C(x, y, t) \leq C_1$ , such as shown in Figure 46.5. Derive the following expression for the area enclosed by the two contours

$$\mathcal{A} = \int_{C_0}^{C_1} dC \oint \frac{dl}{|\nabla C|}. \quad (46.208)$$

In this expression,  $dl$  is the line element for a path taken in a counter-clockwise direction along a contour of constant  $C$ . We also assume the tracer concentration is not uniform in the region of interest so that  $\nabla C \neq 0$ .

- (b) As a corollary, show that for

$$\mathcal{A}(C) = \int_{C_0}^C dC' \oint \frac{dl}{|\nabla C'|} \quad (46.209)$$

we have the identity

$$\frac{\partial \mathcal{A}(C)}{\partial C} = \oint \frac{dl}{|\nabla C|}. \quad (46.210)$$

In words, this result means that the area between two tracer contours has a partial derivative, with respect to the tracer contour, equal to the line integral on the right hand side. The area per  $C$  is smaller in regions where the tracer gradient is larger; i.e., there is less area “concentration” in regions of strong tracer gradient.

- (c) Use the above two results to prove the following form of the Fundamental Theorem of Calculus

$$\frac{\partial}{\partial C} \left[ \int \Phi(\mathbf{x}) d\mathcal{A} \right] = \frac{\partial}{\partial C} \left[ \int_{C_0}^C dC' \oint \frac{\Phi dl}{|\nabla C'|} \right] \quad (46.211a)$$

$$= \oint \frac{\Phi dl}{|\nabla C|}, \quad (46.211b)$$

with  $\Phi$  an arbitrary function. This is a remarkable identity with many useful applications such as those in [Marshall et al. \(2006\)](#).

#### EXERCISE 46.8: EVOLUTION OF TRACER CENTER OF MASS IN A STATIC DOMAIN

The exercise introduces us to how the tracer center of mass evolves within a Boussinesq fluid. We define the tracer center of mass as

$$\langle \mathbf{x} \rangle^C = \frac{\int \mathbf{x} C dV}{\int C dV}, \quad (46.212)$$

with  $C$  the tracer concentration,  $\mathbf{x}$  the coordinate of a point in the fluid, and integration is over the full fluid domain. For example, with a spherically symmetric tracer cloud, the center of mass position is at the sphere’s center. The center of mass position is not necessarily where the largest tracer concentration sits, in the same way that the center of mass of a massive object is not necessarily where the object is most dense. For example, a hollow spherical shell has its center of mass at the center of the sphere, even though there is no mass there.

For this exercise, assume the fluid is within a domain whose static boundaries are either material (no normal component to the boundary flux) or periodic. Hence, the total fluid volume and total tracer content remain constant

$$V = \int dV \quad \text{and} \quad C = \int C dV. \quad (46.213)$$

Furthermore, when computing the time derivative acting on the integral, make use of the kinematic results from Section 15.3.3, in which for any integrand  $\varphi$

$$\frac{d}{dt} \int \varphi dV = \int \frac{\partial \varphi}{\partial t} dV, \quad (46.214)$$

which follows since the region boundaries are assumed to be static. Equivalently, since the region under consideration is material (no matter crosses the boundaries), we can make use of Reynold’s transport theorem from Section 15.3.4 to write

$$\frac{d}{dt} \int \varphi dV = \int \frac{D\varphi}{Dt} dV. \quad (46.215)$$

- (a) Consider a tracer concentration whose tendency at a point in space is affected only by advection

$$\frac{DC}{Dt} = 0 \implies \frac{\partial C}{\partial t} + \nabla \cdot (\mathbf{v} C) = 0, \quad (46.216)$$

with  $\mathbf{v}$  a non-divergent velocity,  $\nabla \cdot \mathbf{v} = 0$ . Show that the tracer center of mass position

evolves according to the tracer center of mass velocity

$$\frac{d\langle \mathbf{x} \rangle^C}{dt} = \langle \mathbf{v} \rangle^C, \quad (46.217)$$

where the tracer center of mass velocity is given by

$$\langle \mathbf{v} \rangle^C = \frac{\int \mathbf{v} C dV}{\int C dV} = \frac{1}{C} \int \mathbf{v} C dV. \quad (46.218)$$

- (b) Consider a tracer concentration whose tendency at a point in space affected only by diffusion

$$\frac{\partial C}{\partial t} = \nabla \cdot (K \cdot \nabla C), \quad (46.219)$$

where  $K = K(\mathbf{x}, t) > 0$  is a kinematic diffusivity (physical dimensions of squared length per time), and which is assumed to vanish at the domain boundaries. Show that the tracer center of mass drifts up the diffusivity gradient

$$\frac{d\langle \mathbf{x} \rangle^C}{dt} = \langle \nabla K \rangle^C. \quad (46.220)$$

Hint: use the product rule and drop boundary terms.

- (c) Consider an initial tracer concentration that is a function only of latitude,

$$C(x, y, z, t = 0) = C_0(y), \quad (46.221)$$

and assume a smooth spherical domain. Assume the diffusivity,  $K$ , is a turbulent diffusivity proportional to the eddy kinetic energy of the flow, so that large diffusivity occurs in regions with large eddy activity; i.e., there is a lot of turbulent mixing where turbulence is active. Introduce an stirring from the eddies that breaks the zonal symmetry. Qualitatively discuss the process whereby this turbulent diffusive mixing causes the tracer center of mass to drift towards the turbulent region.

- (d) Generalize the result from part (b) to the case of the diffusion equation

$$\frac{\partial C}{\partial t} = \nabla \cdot (\mathbb{K} \cdot \nabla C) = \partial_p (\mathbb{K}^{pq} \partial_q C), \quad (46.222)$$

where  $\mathbb{K}$  is a second order symmetric diffusion tensor.

#### EXERCISE 46.9: EVOLUTION OF TRACER CENTER OF MASS IN MOVING REGION

Consider a finite region of fluid with fixed mass that is moving with the fluid velocity field,  $\mathcal{R}(\mathbf{v})$ . The fluid is assumed to have a tracer whose concentration is affected by an irreversible process so that

$$\frac{DC}{Dt} = \dot{C} \neq 0. \quad (46.223)$$

For example,  $\dot{C}$  may represent a diffusive process, in which case the tracer content within the region changes due to diffusion of tracer across the region boundary.

Determine the evolution equation for the tracer center of mass position

$$\langle \mathbf{x} \rangle^C = \frac{\int_{\mathcal{R}(\mathbf{v})} \mathbf{x} C \rho dV}{\int_{\mathcal{R}(\mathbf{v})} C \rho dV}. \quad (46.224)$$

Hint: the region under consideration is moving with the fluid and has constant mass. Although the region boundaries are not material, we can make use of Reynold's transport theorem from Section 15.3.6 since the region has a constant mass. Consequently, we can set

$$\frac{d}{dt} \int_{\mathcal{R}(\mathbf{v})} \psi \rho dV = \int_{\mathcal{R}(\mathbf{v})} \frac{D\psi}{Dt} \rho dV. \quad (46.225)$$

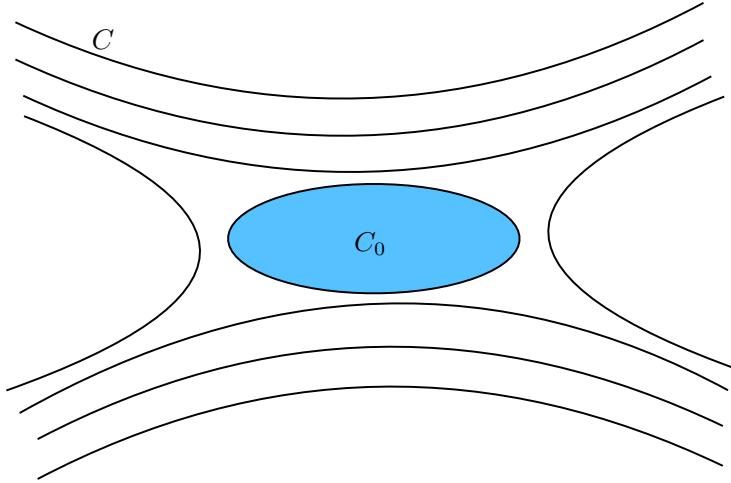


FIGURE 46.6: In a steady state flow, the tracer concentration within a constant  $C$  contour is constant. Diffusion has thus acted to remove all variations in tracer concentration within the region. In this figure, the concentration within the closed region has constant value  $C = C_0$ , whereas the region with open tracer contours remains non-homogeneous.

**EXERCISE 46.10: DIFFUSIVE HOMOGENIZATION OF SCALARS INSIDE CLOSED CONTOURS**  
The advection-diffusion equation for a tracer concentration is given by

$$\frac{\partial(\rho C)}{\partial t} + \nabla \cdot (\rho \mathbf{v} C) = -\nabla \cdot \mathbf{J} \quad (46.226)$$

where

$$\mathbf{J} = -\rho \mathbb{K} \cdot \nabla C \quad (46.227)$$

is a downgradient diffusive flux with  $\mathbb{K}$  a symmetric positive-definite diffusion tensor. In the steady state, the divergence of the advective tracer flux balances the convergence of the diffusive flux

$$\nabla \cdot (\rho \mathbf{v} C) = -\nabla \cdot \mathbf{J}. \quad (46.228)$$

Consider a two-dimensional steady state flow and consider a region enclosed by a constant tracer contour. Prove that the tracer concentration is homogeneous (i.e., a spatially constant) within the contour of constant  $C$ , as shown in Figure 46.6. Hence, in the steady state, diffusion removes all tracer variations within closed tracer contours; i.e., there are no tracer extrema within a closed tracer contour.

Hint: make use of a *reductio ad absurdum* argument and study the material in Section 50.10.

**EXERCISE 46.11: STEADY TWO DIMENSIONAL ADVECTION-DIFFUSION**

Consider the steady state advection-diffusion equation for a scalar field,  $Q$ , in a two dimensional non-divergent flow

$$\nabla \cdot (\mathbf{u} Q) = \nabla \cdot (\mathbb{K} \cdot \nabla Q) \quad \text{with} \quad \mathbf{u} = \hat{z} \times \nabla \psi, \quad (46.229)$$

and  $\mathbb{K}$  a diffusion tensor. Show that when evaluated along a contour of constant  $Q$  we can write

$$-(\hat{\mathbf{n}} \cdot \nabla Q)(\hat{\mathbf{t}} \cdot \nabla \psi) = \nabla \cdot (\mathbb{K} \cdot \nabla Q) \quad (46.230)$$

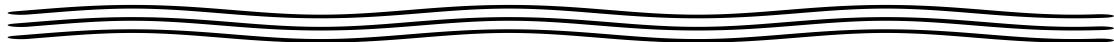
where  $\hat{\mathbf{t}}$  is the unit tangent along the contour and  $\hat{\mathbf{n}}$  is a unit vector pointing to the left of the tangent (e.g., see Figure 5.6). Assuming  $\hat{\mathbf{n}} \cdot \nabla Q \neq 0$ , this equation takes on the form

$$\hat{\mathbf{t}} \cdot \nabla \psi = -\frac{\nabla \cdot (\mathbb{K} \cdot \nabla Q)}{(\hat{\mathbf{n}} \cdot \nabla Q)}, \quad (46.231)$$

which provides a means to integrate the streamfunction,  $\psi$ , along contours of constant  $Q$ .

If  $Q$  is the quasi-geostrophic potential vorticity (Chapter 40), then contours of constant  $Q$  are known as *geostrophic contours*. Within this context, [Rhines and Holland \(1979\)](#) made use of the identity (46.231) in their study of ocean circulation in the presence of eddy diffusion of potential vorticity.

Hint: write the advection operator as a Jacobian and make use of Exercise 5.1.





## Eddy and mean tracer kinematics

Geophysical fluid flows exhibit multiple scales in both space and time. In the analysis of these flows, it is useful to seek a description that decomposes fluid properties into a mean component and a fluctuation relative to the mean. We perform an eddy-mean decomposition when interest concerns the mean field and impacts on the mean by the fluctuating instantaneous flow, with such impacts often termed *rectified* effects. The mean field can be defined in many fashions with subjective choices based on particulars of the flow and the analysis goals. The definition for the mean in turn affects what we refer to as the fluctuation. Quite generally, fluctuations take the form of transient linear waves, nonlinear and/or breaking waves, coherent structures, and/or a chaotic/turbulent soup of eddying features. In this chapter we develop a kinematic framework originally motivated by the analysis of scalar transport induced by small amplitude wave-like eddying features, but is also of use for turbulent processes and their parameterizations (e.g., Chapter 48).

We consider two kinematic methods to decompose the flow into a mean and eddy. The first is the *generalized Lagrangian mean (GLM)*, which is a hybrid Eulerian/Lagrangian method that introduces an Eulerian disturbance field to measure the position of a fluid particle relative to its mean position ([Andrews and McIntyre, 1978a,b](#); [Böhler, 2014a](#)). For our purposes it is sufficient to use only a small piece of the GLM framework to help unpack the kinematics of eddy tracer fluxes. The second kinematic method makes use of isopycnal vertical coordinates. We connect an isopycnal description to the GLM by applying the GLM just in the vertical direction. In this sense the isopycnal approach is quasi-Lagrangian since it fixes the horizontal position (Eulerian) yet allows the vertical to follow an adiabatic fluid parcel (Lagrangian). The isopycnal approach is frequently used to help understand how ocean mesoscale eddies affect stratification and tracer transport in stably stratified flows. Our presentation follows the methods developed by [McDougall and McIntosh \(2001\)](#) and summarized in Chapter 9 of [Griffies \(2004\)](#).

## CHAPTER GUIDE

Material in this chapter relies on an understanding of the tracer equation as derived in Section 15.1 and the maths and physics of the advection-diffusion equation explored in Chapter 46. We focus most discussion on incompressible flows discussed in Chapter 16 and applicable to the Boussinesq fluid commonly assumed for the ocean (Chapter 23). Generalizations to compressible fluids are straightforward, with examples provided by [Griffies and Greatbatch \(2012\)](#). The kinematics of isopycnal fluid layers in a perfect fluid (Sections 47.5 and 47.6) are posed using the isopycnal vertical coordinates detailed in Chapter 41 and further pursued in Chapter 43.

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47.1	Loose threads	1162
47.2	Reynolds decomposition	1163
47.3	Basic kinematics of the GLM	1163
47.3.1	Motivation	1164
47.3.2	Length scales and the small parameter	1165
47.3.3	Decomposing the particle trajectory	1165
47.3.4	GLM and the Stokes mean	1166
47.3.5	An example linear wave	1168
47.3.6	GLM with a materially constant scalar	1169
47.3.7	Further study	1170
47.4	Kinematics of eddy tracer fluxes	1170
47.4.1	Particle displacements and eddy tracer fluxes	1170
47.4.2	Symmetric and skew symmetric tracer fluxes	1171
47.4.3	Massaging the mean field tracer equation	1174
47.4.4	Connection to Stokes drift	1174
47.4.5	A linear rotating periodic wave example	1175
47.4.6	Further study	1176
47.5	Kinematics of volume transport in isopycnal layers	1177
47.5.1	Isopycnal mean	1177
47.5.2	Modified mean	1178
47.5.3	Transformed residual mean (TRM)	1179
47.5.4	Volume conservation and the thickness equation	1181
47.5.5	Ensemble mean kinematics in isopycnal coordinates	1182
47.5.6	Ensemble mean kinematics in geopotential coordinates	1183
47.5.7	Approximate ensemble mean kinematics in geopotential coordinates	1183
47.5.8	Further study	1185
47.6	Mean tracer equation	1185
47.6.1	Thickness weighted means	1185
47.6.2	Isopycnal mean thickness weighted tracer equation	1186
47.6.3	Subgrid scale tracer transport tensor	1186
47.6.4	Mean tracer transport beneath a density surface	1187
47.6.5	Summary of the tracer parameterization problem	1187
47.6.6	Comments	1188

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## 47.1 Loose threads

- Redo Figure 47.4.

## 47.2 Reynolds decomposition

At any point in space and time, we can decompose a field into a mean,  $\bar{\Phi}(\mathbf{x}, t)$ , and a departure from the mean,  $\Phi'(\mathbf{x}, t)$

$$\Phi(\mathbf{x}, t) = \bar{\Phi}(\mathbf{x}, t) + \Phi'(\mathbf{x}, t). \quad (47.1)$$

The departure from the mean is generally termed the “eddy” or the “fluctuation”. The following offers a non-exhaustive list of mean operators.

- **TIME MEAN:** If the mean operator is based on a long time mean, then the mean fields are assumed to be time independent:  $\bar{\Phi}(\mathbf{x}, t) = \bar{\Phi}(\mathbf{x})$ . This is a common operator when interest is focused on the long term mean fluid properties.
- **PHASE AVERAGE:** Rather than a time mean, we may choose to average over the phase (or period) of a wave. This choice is particularly relevant when the fluctuating field involves quasi-linear waves.
- **ZONAL MEAN:** If the mean operator is based on an average along a particular coordinate direction (e.g., zonal average), then the mean tracer concentration is independent of the “averaged out” direction.
- **COARSE GRAINING:** If the mean operator is based on an average over a spatial and temporal region, such as the mesoscale, then such coarse-graining averages out smaller scales.
- **ENSEMBLE MEAN:** Rather than a space or time mean operation, we may consider the mean computed over an ensemble of many flow realizations. For many purposes this is the most analytically convenient operator.

If a mean operator satisfies the following properties then it is said to provide a “Reynolds decomposition”

$$\overline{\Phi'} = 0 \quad (47.2a)$$

$$\overline{\bar{\Phi}} = \bar{\Phi} \quad (47.2b)$$

$$\overline{\gamma \bar{\Phi}} = \gamma \bar{\Phi} \quad \text{for } \gamma \text{ a constant.} \quad (47.2c)$$

Equation (47.2a) says that the mean of an eddy fluctuation vanishes. The equality (47.2b) says that the mean of a mean field returns the mean field. The final equality, (47.2c), says that a constant commutes with the mean operator. Notably, some or all of these properties are not satisfied by certain operators used for eddy-mean decompositions. However, in the following we assume they are satisfied.

## 47.3 Basic kinematics of the GLM

We here consider basic elements of generalized Lagrangian mean (GLM) theory. GLM is distinct from both the Eulerian mean and the Lagrangian mean. Rather, GLM is a hybrid between Lagrangian and Eulerian descriptions of fluid motions, so that it might be more appropriate to refer to it as the “hybrid Lagrangian-Eulerian mean theory”.

The GLM and the Eulerian mean for a fluid property are generally distinct, with their difference referred to as the *Stokes mean*

$$\text{Lagrangian mean} = \text{Eulerian mean} + \text{Stokes mean}. \quad (47.3)$$

This name is motivated from the *Stokes drift* introduced in Section 29.3, which we again encounter in Section 47.3.4. Note that the literature typically refers to the Stokes mean as the “Stokes correction”. We avoid that terminology in order to avoid the spurious notion that one type of mean operator is more correct than the other. We instead propose that a mean operator is subjectively chosen based on its suitability to a particular scientific question. Furthermore, no mean operator is suitable for all questions.

### 47.3.1 Motivation

Consider a materially constant scalar field

$$\frac{D\Phi}{Dt} = \frac{\partial\Phi}{\partial t} + \mathbf{v} \cdot \nabla\Phi = 0. \quad (47.4)$$

The scalar  $\Phi$  is constant following fluid particles whose trajectories are integral curves of the fluid velocity  $\mathbf{v}$ . The question arises how to develop a mean operator that averages over fluctuations in the trajectories while preserving the material constancy nature of the instantaneous equation  $D\Phi/Dt = 0$ . This aspiration is not trivial.

#### Eulerian mean

An Eulerian mean operator considered in Section 47.2 leads to the mean field equation

$$\frac{\partial\bar{\Phi}}{\partial t} + \bar{\mathbf{v}} \cdot \nabla\bar{\Phi} = -\overline{\mathbf{v}' \cdot \nabla\Phi'}. \quad (47.5)$$

Whereas  $\Phi$  is materially constant when following the instantaneous flow field  $\mathbf{v}$ , the Eulerian mean  $\bar{\Phi}$  is not materially constant when following  $\bar{\mathbf{v}}$  due to the source term  $-\overline{\mathbf{v}' \cdot \nabla\Phi'}$  provided by the eddy correlation. Furthermore, when given information only about the mean fields, then we must develop a closure for the unresolved correlation. Such closures are the topic of extensive research typical of eddy-mean decompositions. Nonetheless, we ask whether there are methods that offer insights into mean field behaviour even without making a closure assumption. GLM is one such method.

#### Lagrangian mean

An alternative approach is to remain in the Lagrangian frame, where material constancy of  $\Phi$  takes on the linear form

$$\frac{\partial\Phi(\mathbf{a}, t)}{\partial t} = 0. \quad (47.6)$$

Consider a mean operator computed as an average over a region of material space coordinate  $\mathbf{a}$ . For example, if  $\mathbf{a}$  is the initial fluid particle position, then an average coordinate,  $\bar{\mathbf{a}}$ , and corresponding averaged field,  $\bar{\Phi}$ , render a coarse-graining over the initial positions. Since each member of the Lagrangian average satisfies the linear equation (47.6), so too does the Lagrangian mean

$$\frac{\partial\bar{\Phi}(\bar{\mathbf{a}}, t)}{\partial t} = 0. \quad (47.7)$$

Although this equation retains the simplicity of the unaveraged version, it still requires information about trajectories. Trajectories are computed based on the flow map (i.e., the velocity field), with trajectories an impractical means for describing chaotic or turbulent fluids. GLM offers an alternative that aims to meld elements of the Eulerian (e.g., computability) to the Lagrangian (e.g., material constancy).

### Generalized Lagrangian mean

The GLM approach produces a GLM field that remains constant following the GLM velocity

$$\frac{\partial \bar{\Phi}^{(L)}}{\partial t} + \bar{v}^{(L)} \cdot \nabla \bar{\Phi}^{(L)} = 0. \quad (47.8)$$

Hence, GLM maintains the desirable properties of the Lagrangian mean. However, it does so using Eulerian methods which can prove to be more practical for many cases. Notably, even if the Eulerian velocity is non-divergent, as for a Boussinesq fluid, the GLM velocity is generally divergent. Although we will not prove the GLM result (47.8), we will motivate the GLM average from the analysis of small amplitude eddying motions.

### 47.3.2 Length scales and the small parameter

There are two length scales associated with an eddy or wave fluctuation. One characterizes the size of the eddy whose length scale we write as  $\lambda$ . If the eddy is a monochromatic wave, then  $\lambda$  is its wave length. The other length scale characterizes the size of particle displacements,  $|\xi|$ . In the following, we assume the particle displacements are small relative to  $\lambda$

$$|\xi| \ll \lambda \quad \text{small amplitude waves.} \quad (47.9)$$

We thus introduce the small non-dimensional ratio of length scales for the following analysis

$$\alpha = \frac{|\xi|}{\lambda} \ll 1. \quad (47.10)$$

### 47.3.3 Decomposing the particle trajectory

Recall the discussion of fluid particle trajectories given in Chapter 12. In this description, the trajectory of a particle is determined by integrating the relation between the particle trajectory and the particle velocity

$$\left[ \frac{\partial \mathbf{X}(\mathbf{a}, t)}{\partial t} \right]_{\mathbf{a}} = \mathbf{v}[\mathbf{X}(\mathbf{a}, t)] \implies \mathbf{X}(\mathbf{a}, t) = \mathbf{X}(\mathbf{a}, 0) + \int_0^t \mathbf{v}[\mathbf{X}(\mathbf{a}, t')] dt', \quad (47.11)$$

so that the trajectory measures the position of a particle relative to a chosen origin. The material coordinate,  $\mathbf{a}$ , distinguishes the continuum of fluid particles, thus making the trajectory a field in material space-time.

The GLM develops a hybrid Eulerian-Lagrangian method and it is motivated by linear or quasi-linear disturbances. Keeping this motivation in mind, we consider each point in space,  $\mathbf{x}$ , to be the mean position of a unique fluid particle. In turn, we introduce an Eulerian field,  $\xi(\mathbf{x}, t)$ , that measures the position of a fluid particle relative to its mean position. Correspondingly, the Eulerian mean of the disturbance field vanishes

$$\overline{\xi(\mathbf{x}, t)} = 0. \quad (47.12)$$

Note that the Eulerian mean operator can be any of the operators (or others) satisfying the Reynold's decomposition property discussed in Section 47.2

Specification of  $\xi(\mathbf{x}, t)$  for large amplitude disturbances (i.e., nonlinear waves) requires the full machinery of GLM, which is beyond our scope. Instead, to expose the rudiments we assume linear waves such as shown in Figure 47.1, for which the particle displacement amplitude is much

smaller than the wavelength of the disturbance

$$\alpha = \frac{|\xi|}{\lambda} \ll 1. \quad (47.13)$$

In this case the disturbance field is constructed by time integration of the eddy velocity field

$$\left[ \frac{\partial \xi(\mathbf{x}, t)}{\partial t} \right]_{\mathbf{x}} = \mathbf{v}'(\mathbf{x}, t) \implies \xi(\mathbf{x}, t) = \int^t \mathbf{v}'(\mathbf{x}, t') dt'. \quad (47.14)$$

With this specification for the disturbance field, we see that if the eddy velocity is non-divergent then so is the disturbance particle position field

$$\nabla \cdot \mathbf{v}' = 0 \implies \nabla \cdot \xi = 0. \quad (47.15)$$

The definition (47.14) for the disturbance field,  $\xi(\mathbf{x}, t)$ , is directly analogous to the particle trajectory position,  $\mathbf{X}(\mathbf{a}, t)$ , given by equation (47.11). However, there are important distinctions. Namely, the disturbance,  $\xi(\mathbf{x}, t)$ , is an Eulerian field that measures the position of a fluid particle relative to its mean position, with each Eulerian position  $\mathbf{x}$  corresponding to the mean position for a distinct fluid particle. In contrast, the particle position,  $\mathbf{X}(\mathbf{a}, t)$ , is a Lagrangian field that is attached to each fluid particle and measures the position of that particle relative to a unique origin.

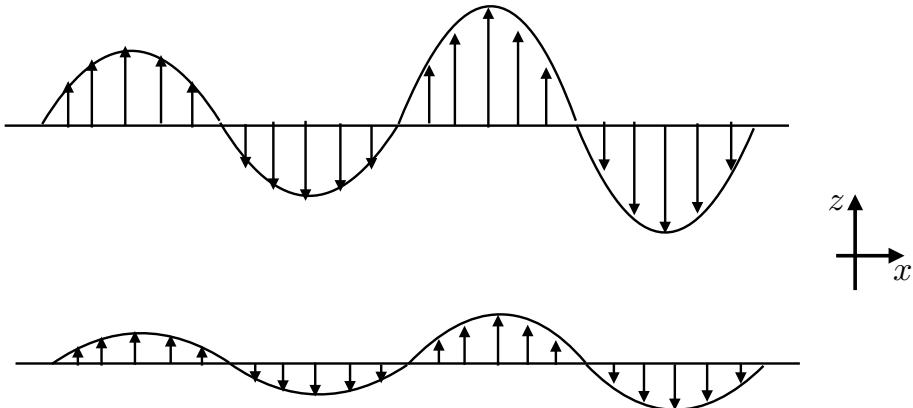


FIGURE 47.1: Illustrating the displacement of fluid particles at two selective vertical positions due to a linear transverse wave disturbance. The particle positions,  $\mathbf{x}^{(\xi)} = \mathbf{x} + \xi(\mathbf{x}, t)$ , have a disturbance field of the form  $\xi(\mathbf{x}, t) = \hat{z} \xi_0(x, z) \sin(kx - \omega t)$ , with  $\xi_0(x, z)$  a spatially dependent wave amplitude,  $\lambda = 2\pi/k$  the wavelength,  $\mathbf{k} = \hat{x} k$  the wavevector,  $\omega = ck$  the angular frequency, and  $c$  the wavespeed. Small amplitude waves satisfy  $|\xi_0| \ll \lambda$ . Note that this wave does not produce a Stokes drift since particle displacements are perpendicular to the wavevector:  $\xi \cdot \mathbf{k} = 0$  (see Section 47.3.5), whereas Stokes drift requires particle motion to have a nonzero component in the wave direction (see Figures 29.4 and 29.5). Even so, it does generally produce a Stokes mean for an arbitrary field  $\Phi$  (Section 47.3.4).

### 47.3.4 GLM and the Stokes mean

The mean of a fluid property,  $\Phi$ , is generally a function of how the property is sampled to compute the mean. For example, the mean of  $\Phi$  sampled on a fluctuating fluid particle differs from the mean sampled at the particle's mean position. Mathematically, this distinction means that

$$\underbrace{\Phi(\mathbf{x} + \xi(\mathbf{x}, t))}_{\text{GLM}} \neq \underbrace{\Phi(\mathbf{x}, t)}_{\text{Eulerian}}, \quad (47.16)$$

where it is common to make use of the shorthand<sup>1</sup>

$$\boldsymbol{x}^{(\xi)}(\boldsymbol{x}, t) \equiv \boldsymbol{x} + \boldsymbol{\xi}(\boldsymbol{x}, t) \quad (47.17)$$

for the instantaneous position of the fluid particle. The average

$$\overline{\Phi}^{(L)}(\boldsymbol{x}, t) \equiv \overline{\Phi(\boldsymbol{x} + \boldsymbol{\xi}(\boldsymbol{x}, t), t)} = \overline{\Phi(\boldsymbol{x}^{(\xi)})} \quad (47.18)$$

defines the generalized Lagrangian mean. As defined, the GLM is computed by evaluating the property  $\Phi$  at the position of a fluid particle,  $\boldsymbol{x}^{(\xi)}(\boldsymbol{x}, t) = \boldsymbol{x} + \boldsymbol{\xi}(\boldsymbol{x}, t)$ , where  $\boldsymbol{x}$  is both an arbitrary Eulerian field point and the mean position of a fluid particle,  $\overline{\boldsymbol{x}^{(\xi)}} = \boldsymbol{x}$ . In contrast, the Eulerian mean is determined by evaluating  $\Phi$  at the fixed Eulerian point in space

$$\overline{\Phi}^{(E)}(\boldsymbol{x}, t) \equiv \overline{\Phi(\boldsymbol{x}, t)}. \quad (47.19)$$

Following our discussion at the start of Section 47.3, we define the difference between the GLM and Eulerian mean as the Stokes mean

$$\overline{\Phi}^{(S)}(\boldsymbol{x}, t) = \overline{\Phi}^{(L)}(\boldsymbol{x}, t) - \overline{\Phi}^{(E)}(\boldsymbol{x}, t). \quad (47.20)$$

The Stokes mean arises from inhomogeneities in  $\Phi$ , which in turn lead to differences in its mean depending on how that field is sampled, whether sampled on a fluid particle,  $\boldsymbol{x}^{(\xi)}(\boldsymbol{x}, t)$ , or sampled at the mean position of the fluid particle,  $\boldsymbol{x}$ .

We mathematically expose the origin of the Stokes mean by performing a Taylor series expansion around the mean particle position

$$\Phi(\boldsymbol{x} + \boldsymbol{\xi}, t) = \Phi(\boldsymbol{x}, t) + \boldsymbol{\xi} \cdot \nabla \Phi(\boldsymbol{x}, t) + \frac{1}{2} \xi_m \xi_n \partial_m \partial_n \Phi(\boldsymbol{x}, t) + \mathcal{O}(\alpha^3). \quad (47.21)$$

The non-dimensional ratio  $\alpha = |\boldsymbol{\xi}|/\lambda \ll 1$  was introduced in equation (47.13), which measures the ratio of the amplitude for particle displacements to the wavelength,  $\lambda$ , of fluctuations in the field  $\Phi$ . Taking the mean of equation (47.21) then leads to an expression for the Stokes mean

$$\overline{\Phi}^{(S)}(\boldsymbol{x}, t) = \overline{\Phi}^{(L)}(\boldsymbol{x}, t) - \overline{\Phi}^{(E)}(\boldsymbol{x}, t) \quad (47.22a)$$

$$= \overline{\boldsymbol{\xi} \cdot \nabla \Phi} + \frac{1}{2} \overline{\xi_m \xi_n \partial_m \partial_n \Phi} + \mathcal{O}(\alpha^3). \quad (47.22b)$$

$$= \overline{\boldsymbol{\xi} \cdot \nabla \Phi'} + \frac{1}{2} \overline{\xi_m \xi_n} \partial_m \partial_n \overline{\Phi^{(E)}} + \mathcal{O}(\alpha^3), \quad (47.22c)$$

where we introduced the Eulerian fluctuation

$$\Phi'(\boldsymbol{x}, t) = \Phi(\boldsymbol{x}, t) - \overline{\Phi}^{(E)}(\boldsymbol{x}, t) \quad (47.23)$$

and all terms on the right hand side of equation (47.22c) are evaluated at  $(\boldsymbol{x}, t)$ . The Stokes drift (Section 29.3) associated with the GLM arises from setting  $\Phi$  equal to one of the velocity components

$$\bar{v}_p^{(S)} = \overline{\boldsymbol{\xi} \cdot \nabla v'_p} + \frac{1}{2} \overline{\xi_m \xi_n} \partial_m \partial_n \bar{v}_p^{(E)} + \mathcal{O}(\alpha^3). \quad (47.24)$$

---

<sup>1</sup>We place superscripts  $\xi, S, L, E$  inside parentheses to distinguish from tensor labels.

### 47.3.5 An example linear wave

We exemplify the previous discussion by considering the small amplitude linear wave

$$\boldsymbol{\xi} = -\frac{U(\mathbf{x})}{\omega} \sin(\mathbf{k} \cdot \mathbf{x} - \omega t) \quad (47.25a)$$

$$\mathbf{v}' = \partial_t \boldsymbol{\xi} = U(\mathbf{x}) \cos(\mathbf{k} \cdot \mathbf{x} - \omega t) \quad (47.25b)$$

$$\nabla v'_p = \nabla U_p \cos(\mathbf{k} \cdot \mathbf{x} - \omega t) - \mathbf{k} U_p \sin(\mathbf{k} \cdot \mathbf{x} - \omega t) \quad (47.25c)$$

$$\nabla \cdot \mathbf{v}' = (\nabla \cdot \mathbf{U}) \cos(\mathbf{k} \cdot \mathbf{x} - \omega t) - \mathbf{k} \cdot \mathbf{U} \sin(\mathbf{k} \cdot \mathbf{x} - \omega t) \quad (47.25d)$$

where  $\mathbf{U}$  is the velocity amplitude that is generally a function of space,  $\mathbf{k}$  is the wavevector, and

$$T = 2\pi/\omega \quad (47.26)$$

is the wave period. The wave renders an oscillatory motion to fluid particles, with the disturbance field specifying the instantaneous position of fluid particles whose mean position is  $\mathbf{x}$ . The disturbance field and velocity field both have a zero mean when time integrated over a wave period

$$\bar{\boldsymbol{\xi}}(\mathbf{x}) = \frac{1}{T} \int_0^T \boldsymbol{\xi}(\mathbf{x}, t') dt' = 0 \quad (47.27a)$$

$$\bar{\mathbf{v}'}(\mathbf{x}) = \frac{1}{T} \int_0^T \mathbf{v}'(\mathbf{x}, t') dt' = 0. \quad (47.27b)$$

To maintain a non-divergent eddy velocity at arbitrary times requires

$$\nabla \cdot \mathbf{v}' = 0 \implies \nabla \cdot \mathbf{U} = \mathbf{U} \cdot \mathbf{k} = 0. \quad (47.28)$$

The second condition means that the wave is transverse, so that particle displacements are orthogonal to the wavevector (e.g., Figure 47.1)

#### *Stokes drift*

Specializing to the velocity field (47.25b), substituting into the Stokes drift expression (47.24), and making use of an average over a wave period yields

$$\bar{\boldsymbol{\xi}} \cdot \nabla v'_p = \frac{U_p \mathbf{U} \cdot \mathbf{k}}{2\omega} \quad (47.29a)$$

$$\bar{v}_p^{(E)} = 0. \quad (47.29b)$$

The second equality holds since the velocity at a point arises just from the wave field, which has a zero Eulerian mean. Hence, to  $\mathcal{O}(\alpha^2)$ , the Stokes drift velocity associated with the GLM is given by

$$\bar{\mathbf{v}}^{(S)} = \frac{\mathbf{U}(\mathbf{U} \cdot \mathbf{k})}{2\omega} + \mathcal{O}(\alpha^2). \quad (47.30)$$

The Stokes drift vanishes at this order of accuracy for transverse waves in which  $\mathbf{U} \cdot \mathbf{k} = 0$ .

As a check on our formalism we consider a one-dimensional longitudinal wave, in which the Stokes drift is given by

$$\bar{v}^{(S)} = \frac{U^2}{2c} + \mathcal{O}(\alpha^2). \quad (47.31)$$

This result agrees with that derived using Lagrangian trajectories in Section 29.3 (see Exercise

29.1). Use of the GLM displacement field offers a somewhat more streamlined method for computing Stokes drift.

#### *Stokes mean for an arbitrary field*

The Stokes mean for an arbitrary field is given by

$$\bar{\Phi}^{(S)}(\mathbf{x}, t) = -\omega^{-1} \mathbf{U} \cdot \overline{\nabla \Phi' \sin(\mathbf{k} \cdot \mathbf{x} - \omega t)} + \mathcal{O}(\alpha^2) \quad (47.32a)$$

$$= -\omega^{-1} \overline{\nabla \cdot (\mathbf{U} \Phi')} \sin(\mathbf{k} \cdot \mathbf{x} - \omega t) + \mathcal{O}(\alpha^2), \quad (47.32b)$$

where the second equality made use of the non-divergent nature of the wave field (47.28). To second order in wave amplitude, the Stokes mean is determined by the projection of the gradient of the Eulerian fluctuation,  $\nabla \Phi'$ , onto the wave amplitude,  $\mathbf{U}$ . For example, consider a transverse wave such as that shown in Figure 47.1. Even though the Stokes drift vanishes to order  $\mathcal{O}(\alpha^2)$ , the Stokes mean,  $\bar{\Phi}^{(S)}(\mathbf{x}, t)$ , can be nonzero so long as there is a nonzero vertical gradient in the Eulerian fluctuation.

#### 47.3.6 GLM with a materially constant scalar

Consider a materially constant scalar field, such as a tracer concentration in the absence of mixing and sources

$$\frac{DC}{Dt} = 0. \quad (47.33)$$

#### *How the GLM for $C$ is related to the instantaneous $C$*

The GLM for  $C$  equals to the value of  $C$  on a fluid particle

$$\bar{C}^{(L)}(\mathbf{x}, t) = C(\mathbf{x} + \boldsymbol{\xi}, t). \quad (47.34)$$

This is a very important identity that packs in a lot of information. In words, it says that when evaluated at the mean fluid particle position,  $\mathbf{x}$ , the GLM field  $\bar{C}^{(L)}(\mathbf{x}, t)$  equals to the concentration,  $C$ , evaluated on a fluid particle at  $\mathbf{x} + \boldsymbol{\xi}$ . One means to understand this identity is to assume the GLM is an ensemble mean following fluid particles. Since  $C$  is constant on fluid particles, each ensemble member has the same value for  $C$ , in which case the GLM for  $C$  clearly equals the value of  $C$  for each ensemble member. We make particular use of the identity (47.34) when considering isopycnal kinematics in Sections 47.5 and 47.6.

#### *Relating the particle disturbance field to Eulerian properties of $C$*

There is a frequently used consequence of the identity (47.34) involving the disturbance field, the Eulerian fluctuation

$$C'(\mathbf{x}, t) = C(\mathbf{x}, t) - \bar{C}(\mathbf{x}, t) \quad (47.35)$$

and the Eulerian mean

$$C^{(E)}(\mathbf{x}, t) = \bar{C}(\mathbf{x}, t). \quad (47.36)$$

To derive it, recall the Taylor series expansion (47.21) truncated here to first order accuracy

$$C(\mathbf{x} + \boldsymbol{\xi}, t) = C(\mathbf{x}, t) + \boldsymbol{\xi} \cdot \nabla \bar{C}(\mathbf{x}, t) + \mathcal{O}(\alpha^2). \quad (47.37)$$

Taking the Eulerian mean of both sides renders

$$\overline{C(\mathbf{x} + \boldsymbol{\xi}, t)} = \overline{C}(\mathbf{x}, t) + \mathcal{O}(\alpha^2). \quad (47.38)$$

This identity means that the GLM equals to the Eulerian mean to order  $\mathcal{O}(\alpha^2)$ , which is a result consistent with the Stokes mean being an order  $\mathcal{O}(\alpha^2)$  quantity as seen by equation (47.22c). From equation (47.34) we know that  $C(\mathbf{x} + \boldsymbol{\xi}, t) = \overline{C(\mathbf{x} + \boldsymbol{\xi}, t)}$ , so that we can subtract equations (47.37) and (47.38) to find

$$C'(\mathbf{x}, t) = -\boldsymbol{\xi} \cdot \nabla \overline{C}(\mathbf{x}, t) + \mathcal{O}(\alpha^2). \quad (47.39)$$

Hence, to first order accuracy, the Eulerian fluctuation equals to minus the disturbance field projected onto the gradient of the mean field; i.e., the Eulerian fluctuation in the tracer is first order in the disturbance. We make use of this result when discussing the kinematics of eddy tracer fluxes in Section 47.4. Furthermore, for the isopycnal kinematics in Sections 47.5 and 47.6, we focus on vertical particle displacements,  $\boldsymbol{\xi} = \xi \hat{\mathbf{z}}$ , in which case the Eulerian fluctuation is given by

$$C'(z, t) = -\xi \partial_z \overline{C}(z, t) + \mathcal{O}(\alpha^2). \quad (47.40)$$

### 47.3.7 Further study

GLM was introduced in the seminal papers by [Andrews and McIntyre \(1978a,b\)](#). These papers offer a wealth of intellectual rewards after much study. GLM is also detailed in the monograph on waves and mean flows by [Bühler \(2014a\)](#).

## 47.4 Kinematics of eddy tracer fluxes

Consider the Eulerian eddy-mean decomposition for a materially constant tracer in an incompressible fluid. The advection equation for this tracer is given by

$$\frac{\partial C}{\partial t} + \nabla \cdot (\mathbf{v} C) = 0, \quad (47.41)$$

and its Eulerian mean is

$$\frac{\partial \overline{C}}{\partial t} + \nabla \cdot (\overline{\mathbf{v}} \overline{C}) = -\nabla \cdot \overline{\mathbf{v}' C'}. \quad (47.42)$$

The eddy advective flux,  $\mathbf{v}' C'$ , is the product of the eddy velocity and eddy tracer concentration. Its mean provides the correlation or mean eddy flux,  $\overline{\mathbf{v}' C'}$ . The convergence of this mean eddy flux provides a source to the advection equation for the Eulerian mean tracer concentration.

In this section we make use of the particle disturbance field of Section 47.3 to unpack the kinematics of eddy tracer fluxes induced by small amplitude waves. Although not offering new dynamical information, the particle disturbance field is a very useful means to frame the kinematics of tracer eddy fluxes.

### 47.4.1 Particle displacements and eddy tracer fluxes

Following Section 47.3, we here introduce a particle disturbance vector corresponding to small amplitude eddy fluctuations

$$\partial_t \boldsymbol{\xi}(\mathbf{x}, t) = \mathbf{v}'(\mathbf{x}, t) + \mathcal{O}(\alpha^2) \quad (47.43a)$$

$$\overline{\boldsymbol{\xi}} = 0. \quad (47.43b)$$

Correspondingly, each spatial point,  $\mathbf{x}$ , is the mean position of a fluid particle whose instantaneous position is  $\mathbf{x} + \boldsymbol{\xi}(\mathbf{x}, t)$ . Following the results from Section 47.3.6, to leading order we can write the Eulerian fluctuation in terms of the particle displacement (equation (47.39))

$$C'(\mathbf{x}, t) = -\boldsymbol{\xi} \cdot \nabla \bar{C}(\mathbf{x}, t) + \mathcal{O}(\alpha^2) \quad (47.44)$$

Notice that if the particle displacement is oriented along a mean tracer iso-surface, then  $\boldsymbol{\xi} \cdot \nabla \bar{C}(\mathbf{x}, t) = 0$  and there is no tracer fluctuation,  $C' = 0$ , to order  $\mathcal{O}(\alpha^2)$ . More general eddy motions lead to a nonzero tracer fluctuation with the eddy tracer flux taking on the form

$$\mathbf{v}' C' = -\partial_t \boldsymbol{\xi} (\boldsymbol{\xi} \cdot \nabla) \bar{C} + \mathcal{O}(\alpha^2). \quad (47.45)$$

We unpack this expression for the purpose of characterizing kinematic properties of the eddy tracer flux

#### 47.4.2 Symmetric and skew symmetric tracer fluxes

From equation (47.45), the  $m$ 'th component of the eddy tracer flux is given by

$$v'_m C' = -[(\partial_t \xi_m) \xi_n] \partial_n \bar{C}. \quad (47.46)$$

We here decompose this flux in order to characterize its kinematic properties.

##### *Decomposing the tracer flux*

Let us decompose the second order tensor  $(\partial_t \xi_m) \xi_n$  into its symmetric and anti-symmetric components<sup>2</sup>

$$2(\partial_t \xi_m) \xi_n = [(\partial_t \xi_m) \xi_n + (\partial_t \xi_n) \xi_m] + [(\partial_t \xi_m) \xi_n - (\partial_t \xi_n) \xi_m] \quad (47.47a)$$

$$= \partial_t (\xi_m \xi_n) + [(\partial_t \xi_m) \xi_n - (\partial_t \xi_n) \xi_m]. \quad (47.47b)$$

Introducing the symmetric and anti-symmetric correlation tensors

$$2\mathbb{K}_{mn} \equiv \overline{\partial_t (\xi_m \xi_n)} \quad (47.48a)$$

$$2\mathbb{A}_{mn} \equiv \overline{(\partial_t \xi_m) \xi_n} - \overline{(\partial_t \xi_n) \xi_m} \quad (47.48b)$$

allows us to write the mean eddy tracer flux

$$\overline{v'_m C'} = -(\mathbb{K}_{mn} + \mathbb{A}_{mn}) \partial_n \bar{C} \quad (47.49)$$

and the mean field tracer equation (47.42)

$$\frac{\partial \bar{C}}{\partial t} + \nabla \cdot (\bar{\mathbf{v}} \bar{C}) = \nabla \cdot [(\mathbb{K} + \mathbb{A}) \cdot \nabla \bar{C}]. \quad (47.50)$$

The right hand side of this equation equals to the convergence of the symmetric and skew-symmetric tracer fluxes<sup>3</sup>

$$\nabla \cdot [(\mathbb{K} + \mathbb{A}) \cdot \nabla \bar{C}] = -\nabla \cdot (\mathbf{F}^{(\text{sym})} + \mathbf{F}^{(\text{skew})}), \quad (47.51)$$

<sup>2</sup>See Section 13.3.5 for a similar decomposition of the velocity gradient tensor.

<sup>3</sup>We place parentheses around “skew” and “sym” to distinguish the name for these vectors from what may otherwise appear to be tensor labels.

where

$$\mathbf{F}^{(\text{sym})} = -\mathbb{K} \cdot \nabla \bar{C} \quad (47.52\text{a})$$

$$\mathbf{F}^{(\text{skew})} = -\mathbb{A} \cdot \nabla \bar{C} \quad (47.52\text{b})$$

$$\overline{\mathbf{v}' \bar{C}'} = \mathbf{F}^{(\text{sym})} + \mathbf{F}^{(\text{skew})}. \quad (47.52\text{c})$$

### The symmetric flux

In terms of particle displacements, the symmetric flux (47.52a) is given by

$$F_m^{(\text{sym})} = -\mathbb{K}_{mn} \partial_n \bar{C} = -\frac{1}{2} \overline{\partial_t(\xi_m \xi_n)} \partial_n \bar{C}. \quad (47.53)$$

The symmetric tensor  $\mathbb{K}$  vanishes when the average is over the period of a periodic wave, in which the particle displacements undergo reversible periodic excursions (see Section 47.4.5). For waves that decay in amplitude over the averaging period, particle displacements decrease in magnitude thus leading to an upgradient symmetric flux. In contrast, particle displacements increase in magnitude for waves that grow over the averaging period, in which case the flux is downgradient just as for diffusion. Furthermore, growing nonlinear waves generally break and then develop into turbulence, with turbulence leading to further particle separation and dispersive tracer mixing. Dispersive mixing is well parameterized by diffusion, and we have more to say about diffusive parameterizations of lateral dispersion in Section 48.4.

### The skew, advective, and rotational fluxes

Following our discussion in Section 46.7, we write the skew flux as

$$F_m^{(\text{skew})} = -\mathbb{A}_{mn} \partial_n \bar{C} = -\epsilon_{mnp} \Psi_p \partial_n \bar{C} = -(\nabla \bar{C} \times \Psi)_m, \quad (47.54)$$

where we introduced the vector streamfunction (dimensions squared length per time)<sup>4</sup>

$$\Psi = \frac{1}{2} \overline{\partial_t \xi \times \xi} = \frac{1}{2} \overline{\mathbf{v}' \times \xi}. \quad (47.55)$$

The vector streamfunction is half the angular momentum per mass of a fluid particle undergoing eddying motion, with the angular momentum computed relative to the mean particle position. The vector streamfunction is nonzero only if the eddy has a preferred sense of rotation, in which case the wave field is said to be *polarized*.

The skew flux can be written

$$\mathbf{F}^{(\text{skew})} = -\nabla \bar{C} \times \Psi \quad (47.56\text{a})$$

$$= (\nabla \times \Psi) \bar{C} - \nabla \times (\bar{C} \Psi) \quad (47.56\text{b})$$

$$= \mathcal{U}^{(\Psi)} \bar{C} - \nabla \times (\bar{C} \Psi) \quad (47.56\text{c})$$

$$= \mathbf{F}^{(\text{adv})} - \mathbf{F}^{(\text{rot})}, \quad (47.56\text{d})$$

so that the skew flux equals to an advective flux minus a rotational flux. We here introduced the non-divergent velocity

$$\mathcal{U}^{(\Psi)} = \nabla \times \Psi \quad (47.57)$$

<sup>4</sup> Middleton and Loder (1989) and Garrett (2006) introduce a skew-diffusivity,  $\mathbf{D}$ , which is opposite in sign to the vector streamfunction:  $\Psi = -\mathbf{D}$ .

and the non-divergent rotational flux

$$\mathbf{F}^{(\text{rot})} = \nabla \times (\bar{C} \Psi). \quad (47.58)$$

The divergence of the skew flux equals to the divergence of the advective flux

$$\nabla \cdot \mathbf{F}^{(\text{skew})} = \nabla \cdot (\mathbf{F}^{(\text{adv})} - \mathbf{F}^{(\text{rot})}) = \nabla \cdot \mathbf{F}^{(\text{adv})}, \quad (47.59)$$

so that the rotational flux has no impact on evolution of the mean tracer field.

#### *What does a point measurement estimate?*

From equation (47.52c), we see that a point measurement of the correlation  $\overline{\mathbf{v}' C'}$  provides an estimate of the diffusive and skew diffusive tracer fluxes

$$\overline{\mathbf{v}' C'} = \mathbf{F}^{(\text{sym})} + \mathbf{F}^{(\text{skew})} = -(\mathbb{K} + \mathbb{A}) \cdot \nabla \bar{C}. \quad (47.60)$$

Furthermore, for a periodic wave field, where the symmetric tensor vanishes, the correlation,  $\overline{\mathbf{v}' C'}$ , provides a direct estimate of the skew flux,  $-\nabla \bar{C} \times \Psi$ . One might instead presume that the point measurement offers a direct estimate of the advective flux,  $\bar{C} \mathcal{U}^{(\Psi)}$ , rather than the skew flux. But that presumption is wrong. Instead, since the skew flux equals to a rotational flux plus the advective flux, we have

$$\overline{\mathbf{v}' C'} = -\mathbb{K} \cdot \nabla \bar{C} - \nabla \bar{C} \times \Psi \quad (47.61a)$$

$$= -\mathbb{K} \cdot \nabla \bar{C} - \nabla \times (\bar{C} \Psi) + \bar{C} \nabla \times \Psi \quad (47.61b)$$

$$= -\mathbb{K} \cdot \nabla \bar{C} - \nabla \times (\bar{C} \Psi) + \bar{C} \mathcal{U}^{(\Psi)}. \quad (47.61c)$$

The rotational flux is generally nontrivial for polarized waves and so cannot be ignored. As detailed by [Fox-Kemper et al. \(2003\)](#), there is no general method for removing the rotational flux. We therefore find it more convenient to work directly with the skew flux than the advective flux.

#### *Area integrated tracer flux*

We now offer an interpretation for the rotational contribution by considering the mean of the tracer flux integrated over a static area  $\mathcal{S}$

$$\mathcal{T} = \overline{\int_{\mathcal{S}} \mathbf{v} C \cdot \hat{\mathbf{n}} dS} = \int_{\mathcal{S}} \overline{\mathbf{v} C} \cdot \hat{\mathbf{n}} dS = \int_{\mathcal{S}} [\overline{\mathbf{v} C} + \overline{\mathbf{v}' C'}] \cdot \hat{\mathbf{n}} dS. \quad (47.62)$$

In terms of particle displacements, the eddy correlation,  $\overline{\mathbf{v}' C'}$ , equals to the sum of the symmetric flux and the skew flux as in equation (47.60). Introducing the diffusive, advective, and rotational flux then renders

$$\mathcal{T} = \int_{\mathcal{S}} [\overline{\mathbf{v} C} + \mathcal{U}^{(\Psi)} \bar{C} - \nabla \times (\bar{C} \Psi) - \mathbb{K} \cdot \nabla \bar{C}] \cdot \hat{\mathbf{n}} dS. \quad (47.63)$$

Use of Stokes' Theorem transforms the rotational term to a line integral around the boundary of the area

$$\mathcal{T} = \int_{\mathcal{S}} [\overline{\mathbf{v} C} + \mathcal{U}^{(\Psi)} \bar{C} - \mathbb{K} \cdot \nabla \bar{C}] \cdot \hat{\mathbf{n}} dS - \oint_{\partial \mathcal{S}} \bar{C} \Psi \cdot d\mathbf{l}. \quad (47.64)$$

Following Section 2b of [Middleton and Loder \(1989\)](#), we interpret the boundary term as a Stokes contribution associated with the correlation of particle motion and perturbation velocity along

the boundary

$$\oint_{\partial S} \bar{C} \Psi \cdot d\mathbf{l} = (1/2) \oint_{\partial S} \bar{C} (\bar{\mathbf{v}}' \times \bar{\boldsymbol{\xi}}) \cdot d\mathbf{l}. \quad (47.65)$$

We further this interpretation when considering the transport beneath a fluctuating isopycnal surface in Section 47.6.4.

### 47.4.3 Massaging the mean field tracer equation

We here write the mean tracer equation (47.50) in various forms that can be found throughout the literature. For this purpose, write the right hand side of equation (47.50) in the form

$$\nabla \cdot [(\mathbb{K} + \mathbb{A}) \cdot \nabla \bar{C}] = \partial_m [(\mathbb{K}_{mn} + \mathbb{A}_{mn}) \partial_n \bar{C}] \quad (47.66a)$$

$$= \partial_m (\mathbb{K}_{mn} + \mathbb{A}_{mn}) \partial_n \bar{C} + (\mathbb{K}_{mn} + \mathbb{A}_{mn}) \partial_m \partial_n \bar{C} \quad (47.66b)$$

$$= \partial_m (\mathbb{K}_{mn} + \mathbb{A}_{mn}) \partial_n \bar{C} + \mathbb{K}_{mn} \partial_m \partial_n \bar{C}. \quad (47.66c)$$

The final equality follows from the identity

$$\mathbb{A}_{mn} \partial_m \partial_n \bar{C} = 0, \quad (47.67)$$

which results from the contraction of the anti-symmetric,  $\mathbb{A}_{mn}$ , to the symmetric operator  $\partial_m \partial_n$ . The second term,  $\mathbb{K}_{mn} \partial_m \partial_n \bar{C}$ , is a diffusion operator if symmetric tensor  $\mathbb{K}$  is also positive-definite. The first term in equation (47.66c) can be interpreted as an advection operator through the action of a non-divergent plus a divergent advection velocity

$$\partial_m (\mathbb{K}_{mn} + \mathbb{A}_{mn}) \partial_n \bar{C} = [\mathcal{U}^{(K)} + \mathcal{U}^{(\Psi)}] \cdot \nabla \bar{C}, \quad (47.68)$$

where<sup>5</sup>

$$\mathcal{U}_n^{(K)} \equiv -\partial_m \mathbb{K}_{mn} \implies \nabla \cdot \mathcal{U}^{(K)} = -\partial_n \partial_m \mathbb{K}_{mn} \neq 0 \quad (47.69a)$$

$$\mathcal{U}_n^{(\Psi)} \equiv -\partial_m \mathbb{A}_{mn} \implies \nabla \cdot \mathcal{U}^{(\Psi)} = \partial_n \partial_m \mathbb{A}_{mn} = 0. \quad (47.69b)$$

Bringing the above results together allows us to write the mean field tracer equation (47.50) in the following equivalent forms

$$\frac{\partial \bar{C}}{\partial t} + [\bar{\mathbf{v}} + \mathcal{U}^{(\Psi)} + \mathcal{U}^{(K)}] \cdot \nabla \bar{C} = \mathbb{K}_{mn} \partial_m \partial_n \bar{C} \quad \text{advective form} \quad (47.70a)$$

$$\frac{\partial \bar{C}}{\partial t} + \nabla \cdot (\bar{\mathbf{v}} + \mathcal{U}^{(\Psi)}) \bar{C} = \nabla \cdot (\mathbb{K} \cdot \nabla \bar{C}) \quad \text{flux form}, \quad (47.70b)$$

where we made use of the identities

$$\nabla \cdot \bar{\mathbf{v}} = 0 \quad \nabla \cdot \mathcal{U}^{(\Psi)} = 0 \quad \nabla \cdot \mathcal{U}^{(K)} \neq 0. \quad (47.71)$$

### 47.4.4 Connection to Stokes drift

From equation (47.24) we have the leading order expression for the Stokes drift

$$\bar{v}_p^{(S)} = \overline{\xi_n \partial_n \partial_t \xi_p} + \mathcal{O}(\alpha^2). \quad (47.72)$$

---

<sup>5</sup>Note that Middleton and Loder (1989) define  $\mathcal{U}_n^{(K)} \equiv +\partial_m \mathbb{K}_{mn}$ , which is the opposite sign to that used here in equation (47.69a), whereas they define  $\mathcal{U}_n^{(\Psi)} = -\partial_m \mathbb{A}_{mn}$  as in equation (47.69b).

As noted in equation (47.15), with  $\partial_t \boldsymbol{\xi} = \mathbf{v}'$  and with  $\nabla \cdot \mathbf{v}' = 0$ , the corresponding particle displacements are non-divergent,  $\nabla \cdot \mathbf{v}' = 0 \Rightarrow \nabla \cdot \boldsymbol{\xi} = 0$ . Consequently, to second order accuracy, the Stokes drift velocity can be written

$$\bar{v}_p^{(S)} = \overline{\xi_n \partial_n \partial_t \xi_p} \quad (47.73a)$$

$$= \partial_n [\overline{(\partial_t \xi_p) \xi_n}] \quad (47.73b)$$

$$= \partial_n (\mathbb{K}_{pn} + \mathbb{A}_{pn}) \quad (47.73c)$$

$$= \partial_n (\mathbb{K}_{np} - \mathbb{A}_{np}) \quad (47.73d)$$

$$= -\mathcal{U}_p^{(K)} + \mathcal{U}_p^{(\Psi)}. \quad (47.73e)$$

For the case of periodic waves, the Stokes drift velocity equals to the non-divergent skew velocity

$$\bar{\mathbf{v}}^{(S)} = \mathcal{U}^{(\Psi)} \Rightarrow \nabla \cdot \bar{\mathbf{v}}^{(S)} = 0 \quad \text{periodic waves.} \quad (47.74)$$

More generally, for non-periodic waves the divergent velocity is non-zero so that the Stokes velocity is also divergent

$$\bar{\mathbf{v}}^{(S)} = \mathcal{U}^{(\Psi)} - \mathcal{U}^{(K)} \Rightarrow \nabla \cdot \bar{\mathbf{v}}^{(S)} = -\nabla \cdot \mathcal{U}^{(K)} \neq 0 \quad \text{non-periodic waves.} \quad (47.75)$$

#### 47.4.5 A linear rotating periodic wave example

We illustrate some of the previous analysis by considering Consider a displacement vector comprised of a linear periodic wave in two-dimensions

$$\boldsymbol{\xi}(\mathbf{x}, t) = \Gamma [\hat{\mathbf{x}} \cos(kx - \omega t) + \hat{\mathbf{y}} \sin(kx - \omega t)] \quad (47.76a)$$

$$\partial_t \boldsymbol{\xi}(\mathbf{x}, t) = \omega \Gamma [\hat{\mathbf{x}} \sin(kx - \omega t) - \hat{\mathbf{y}} \cos(kx - \omega t)], \quad (47.76b)$$

where  $\Gamma$  the time-independent wave amplitude,  $T = 2\pi/\omega$  is the wave period, and  $\lambda = 2\pi/k$  is the wavelength. The fluid particles exhibit counter-clockwise circular motion in the horizontal plane with squared radius

$$\boldsymbol{\xi} \cdot \boldsymbol{\xi} = \Gamma^2. \quad (47.77)$$

We are motivated to let the mean operator be a phase average

$$\bar{\phi} = \frac{1}{T} \int_0^T \phi(t) dt, \quad (47.78)$$

which is the traditional operator used when examining the impacts of linear waves on mean fields. For spatially constant wave amplitude, we will see the the mean tracer concentration,  $\bar{C}$ , remains unchanged by these waves. The absence of a rectified change to  $\bar{C}$  reflects the linear periodic nature of the wave field.

#### Symmetric mixing tensor

The symmetric mixing tensor

$$\mathbb{K}_{mn} = \frac{\Gamma^2}{2T} \int_0^T dt \frac{\partial}{\partial t} \begin{bmatrix} \cos^2(kx - \omega t) & \cos(kx - \omega t) \sin(kx - \omega t) \\ \cos(kx - \omega t) \sin(kx - \omega t) & \sin^2(kx - \omega t) \end{bmatrix} \quad (47.79)$$

vanishes identically since the wave field is periodic so that the particle motion has an amplitude whose growing phase is exactly matched by its decaying phase.

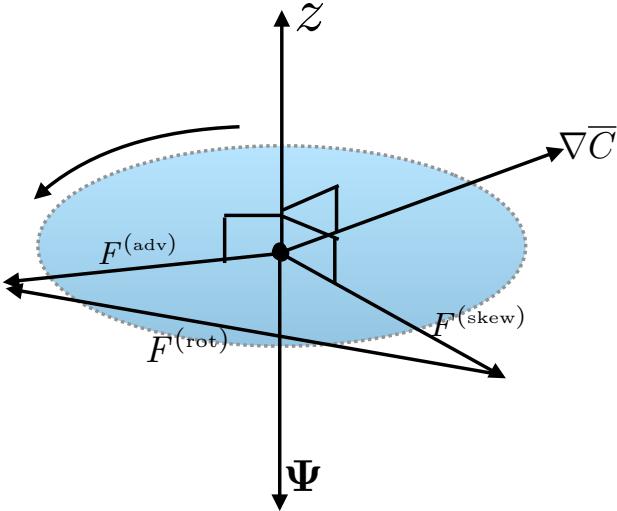


FIGURE 47.2: Sketch of the various tracer fluxes associated with the polarized displacement vector (47.76a). The particles are moving on the horizontal plane in a circle with time-independent radius  $\Gamma$ . The vector streamfunction (47.81) points in the negative  $\hat{z}$  direction. The mean concentration gradient,  $\nabla \bar{C}$ , generally points outside of the horizontal plane. However, it is only the horizontal components that contribute since the displacement vector is in the horizontal plane, thus resulting in horizontal skew, advective, and rotational fluxes.

#### Skew symmetric stirring tensor

In contrast, the skew-symmetric tensor has non-zero components

$$\mathbb{A}_{12} = -\mathbb{A}_{21} = \frac{\Gamma^2 \omega}{2} [\sin^2(kx - \omega t) + \cos^2(kx - \omega t)] = \frac{\Gamma^2 \omega}{2}, \quad (47.80)$$

which reflects the counter-clockwise polarization. The corresponding vector streamfunction is vertical

$$\Psi = \frac{\Gamma^2 \omega}{2} \hat{z}, \quad (47.81)$$

and the skew flux is horizontal

$$\mathbf{F}^{(\text{skew})} = \frac{\Gamma^2 \omega}{2} (\hat{z} \times \nabla \bar{C}). \quad (47.82)$$

Finally, the advective velocity is given by

$$\nabla \times \Psi = \omega \Gamma \nabla \Gamma \times \hat{z}, \quad (47.83)$$

with the advective velocity vanishing when the wave amplitude,  $\Gamma$ , is a constant. In this case, the advective tracer flux is zero, although the skew flux is non-zero. With a constant  $\Gamma$ , the skew flux has a zero divergence (it is a purely rotational flux when  $\Gamma$  is constant). Hence, for a constant wave amplitude, neither the skew flux nor the advective flux affect the evolution of  $\bar{C}$ . Figure 47.2 offers a schematic of the skew, advective, and rotational fluxes induced by a linear rotating particle wave in the horizontal plane.

#### 47.4.6 Further study

Much of this section follows [Plumb \(1979\)](#), [Middleton and Loder \(1989\)](#), and [Garrett \(2006\)](#), each of whom considered elements of tracer dispersion by waves and nonlinear eddies. Additional treatments can be found in the review article of [Moffatt \(1983\)](#), who considers rotating fluids and magnetic fluids.

## 47.5 Kinematics of volume transport in isopycnal layers

In this section we consider the reversible stirring of fluid parcels by turbulent flow in a perfect (i.e., no mixing or sources) stratified Boussinesq fluid. As the fluid parcels are stirred, they preserve their volume while changing their shape and stretching into finer scale filaments. Stirring by ocean mesoscale/baroclinic eddies offers the canonical example of such stirring. Eventually, small-scale processes, such as those summarized in Section 48.1.1 mix properties irreversibly. We are here focused just on the stirring part of this scenario.

Over space and time scales larger than the mesoscale, the stirring by ocean mesoscale eddies can be considered chaotic, which in turn motivates a stochastic perspective in which an ensemble of eddies is considered. The goal is to describe the ensemble mean properties of the perfect fluid, with a focus in this section on the kinematics of parcel rearrangement. Hence, eddy correlations in the present section appear between the thickness of a fluid layer and the velocity. We introduce trace matter in Section 47.6, at which point we also consider eddy correlations between velocity and tracer as in Section 47.4.

The material in this section is rather detailed. However, its mastery comes readily by keeping in mind the more general (and somewhat simpler) presentation of GLM offered in Section 47.3. We are motivated to provide full details in this section since the kinematics of isopycnal ensembles appears throughout the study of wave-mean flow interactions in adiabatic geophysical fluid mechanics, such as in the study of ocean mesoscale eddies.

### 47.5.1 Isopycnal mean

Each fluid parcel in a stably stratified perfect Boussinesq fluid preserves its potential density. We are interested in following the vertical motion of potential density layer interfaces as waves and turbulent processes transport layer thickness from one region to another. In contrast, we are not concerned with following the lateral position of a fluid parcel within a layer. Here we introduce the isopycnal mean, which is based on describing ensembles of perfect fluid parcels using isopycnal coordinates. In Section 47.5.3, we relate this isopycnal approach to the vertical/isopycnal GLM.

#### *Defining the isopycnal ensemble*

An overbar with a potential density label,  $\overline{(\cdot)}^{(\varrho)}$ , denotes a mean over an ensemble of fluid parcels, each having the same potential density,  $\varrho$ , the same horizontal position,  $(x, y)$ , and the same time,  $t$ . Isopycnals undulate in space and time, which means that each ensemble member has a vertical position that is generally distinct from the ensemble mean depth,  $z$ . Furthermore, when the context is clear, it is useful to drop the dependence on  $(x, y, t)$  to highlight the dependence on potential density and/or the vertical position.

#### *Isopycnal ensemble mean*

The isopycnal ensemble mean makes use of potential density as a vertical coordinate (Chapters 41 and 43), with the mean field denoted by

$$\overline{\Phi}^{(\varrho)}(x, y, \varrho, t) \equiv \text{ensemble mean using isopycnal vertical coordinates.} \quad (47.84)$$

This average is straightforward to compute when using isopycnal coordinates, thus producing an isopycnal mean that is a function of the potential density,  $\varrho$ .

FIGURE 47.3: Schematic of the ensemble mean depth  $\bar{z}^\rho(x, y, \rho, t)$  of a particular potential density surface  $\rho$ . In general, different members of an isentropic ensemble live at different depths. Therefore, when considering ensemble members with the same potential density, the ensemble mean depth is the average over the different members. For the case of a two-member ensemble, as shown here,  $2\bar{z}^\rho(\rho) = z(1, \rho) + z(2, \rho)$ , where the depth  $z(1, \rho)$  is generally different from  $z(2, \rho)$ .

### 47.5.2 Modified mean

As a complement to the isopycnal approach in Section 47.5.1, we here introduce the vertical/isopycnal GLM, also known as the modified mean.

#### *Vertical/isopycnal GLM*

The discussion in Section 47.3 considered a three-vector particle displacement vector  $\xi(x, t)$ . In contrast, we are here interested just in the vertical displacement of an isopycnal layer interface

$$\xi(x, y, \varrho, t) = \hat{z}\xi(x, y, \varrho, t). \quad (47.85)$$

The displacement field  $\xi(x, y, \varrho, t)$  measures the vertical position of a potential density interface,  $\varrho$ , relative to its ensemble mean depth. For any particular ensemble member with potential density  $\varrho$ , we write its vertical position as (dropping  $x, y, t$  dependence for brevity)

$$z(\varrho) = \bar{z}^{(\varrho)} + \xi(\varrho), \quad (47.86)$$

where

$$\bar{z}^{(\varrho)} = \overline{z(\varrho)}^{(\varrho)} \quad (47.87)$$

is the isopycnal ensemble mean depth, and the displacement field has a zero ensemble mean

$$\overline{\xi(\varrho)}^{(\varrho)} = 0. \quad (47.88)$$

Given the above definitions for the vertical position, we define the *vertical/isopycnal GLM* for an arbitrary function

$$\tilde{\Phi}(x, y, \bar{z}^{(\varrho)}, t) \equiv \overline{\Phi(x, y, \bar{z}^{(\varrho)} + \xi(x, y, \varrho, t), t)}^{(\varrho)}. \quad (47.89)$$

As defined, the vertical/isopycnal GLM,  $\tilde{\Phi}$ , is a function of the ensemble mean vertical position,  $\bar{z}^{(\varrho)}$  (left hand side), and is determined by an ensemble mean of  $\Phi$  sampled at the depth of each ensemble member,  $\bar{z}^{(\varrho)} + \xi(\varrho)$ . [McDougall and McIntosh \(2001\)](#) refer to the vertical/isopycnal GLM (47.89) as the *modified mean*.

#### *Relating the modified mean to the isopycnal mean*

Following the general result (47.34), we know that the modified mean potential density,  $\tilde{\varrho}(x, y, \bar{z}^{(\varrho)}, t)$ , equals to the potential density of each ensemble member so that

$$\tilde{\varrho}(x, y, \bar{z}^{(\varrho)}, t) = \varrho(x, y, \bar{z}^{(\varrho)} + \xi(x, y, \varrho, t), t). \quad (47.90)$$

This relation means that the modified mean potential density is the functional inverse of the isopycnal ensemble mean vertical position. Consequently, the isopycnal ensemble mean of a function,  $\overline{\Phi}^{(\varrho)}$  (equation (47.84)), when evaluated at the modified mean potential density,  $\tilde{\varrho}$ ,

equals to the modified mean  $\tilde{\Phi}$  when evaluated at the vertical position of the mean density

$$\bar{\Phi}^{(\varrho)}(x, y, \tilde{\varrho}, t) = \tilde{\Phi}(x, y, \bar{z}^{(\varrho)}, t). \quad (47.91)$$

This is a very important identity that will be used in the following.

### 47.5.3 Transformed residual mean (TRM)

When working with isopycnal layers, it is very useful to use specific thickness weighting to account for the net amount of material within a layer, or to measure the net transport in the layer. For this purpose we make use of the *specific thickness* from Section 42.3 as given by<sup>6</sup>

$$h = \partial z / \partial \varrho = 1 / (\partial \varrho / \partial z) \quad (47.92)$$

and thus make use of thickness weighted fields,  $h \Phi$ , and the corresponding thickness weighted isopycnal ensemble mean

$$\hat{\Phi}(\varrho) = \frac{h \bar{\Phi}^{(\varrho)}}{\bar{h}^{(\varrho)}}. \quad (47.93)$$

The identity (47.90) then renders

$$\bar{\Phi}^{\#}(x, y, \bar{z}^{(\varrho)}, t) \equiv \hat{\Phi}(x, y, \tilde{\varrho}, t), \quad (47.94)$$

where  $\bar{\Phi}^{\#}$  is the *transformed residual mean* (TRM) evaluated at the isopycnal ensemble mean vertical position. This is yet another important identity that will be used in the following.

#### Depth integrated TRM transport

A particularly key TRM field is the TRM horizontal velocity

$$\hat{\mathbf{u}}(x, y, \tilde{\varrho}, t) = \bar{\mathbf{u}}^{\#}(x, y, \bar{z}^{(\varrho)}, t). \quad (47.95)$$

Following the discussion of the vertical gauge in Section 46.7.1 (see in particular equation (46.77)), we are led to define the depth integrated TRM transport

$$\bar{\mathbf{U}}^{\#}(\bar{z}^{(\varrho)}) = \int_{-H}^{\bar{z}^{(\varrho)}} \bar{\mathbf{u}}^{\#}(z) dz = \int_{\varrho(-H)}^{\tilde{\varrho}(\bar{z}^{(\varrho)})} \hat{\mathbf{u}}(\gamma) \bar{h}^{(\gamma)} d\gamma, \quad (47.96)$$

---

<sup>6</sup>As discussed in Section 41.9.1, specific thickness is the Jacobian of transformation between geopotential coordinates,  $(x, y, z, t)$ , and isopycnal coordinates,  $(x, y, \varrho, t)$ . For stably stratified ideal fluids,  $h$  is one-signed, hence making the coordinate transformation well defined. It is also related to the buoyancy frequency through (Section 24.5.5)  $N^2 = -(g/\rho_0) (\partial \varrho / \partial z) = -g/(\rho_0 h)$ .

with the second equality following from a change of coordinates from geopotential to isopycnal. We can go further with this expression by writing

$$\bar{U}^\#(\bar{z}^{(\varrho)}) = \int_{\varrho(-H)}^{\tilde{\varrho}(\bar{z}^{(\varrho)})} \hat{u}(\gamma) \bar{h}^{(\gamma)} d\gamma \quad \text{from equation (47.96)} \quad (47.97a)$$

$$= \int_{\varrho(-H)}^{\tilde{\varrho}(\bar{z}^{(\varrho)})} \bar{u} \bar{h}^{(\gamma)} d\gamma \quad \text{from equation (47.93)} \quad (47.97b)$$

$$= \int_{\varrho(-H)}^{\varrho(\bar{z}^{(\varrho)} + \xi)} \bar{u} \bar{h}^{(\gamma)} d\gamma \quad \text{from equation (47.90).} \quad (47.97c)$$

The final equality makes it clear that the TRM transport,  $\bar{U}^\#(\bar{z}^{(\varrho)})$ , is the ensemble mean volume transport for fluid denser than  $\varrho(\bar{z}^{(\varrho)} + \xi) = \tilde{\varrho}(\bar{z}^{(\varrho)})$ . This transport can also be written using geopotential coordinates

$$\bar{U}^\#(\bar{z}^{(\varrho)}) = \overline{\int_{-H}^{\bar{z}^{(\varrho)} + \xi} \mathbf{u} dz}. \quad (47.98)$$

The transport from each ensemble member is determined by integrating from the bottom to the depth,  $\bar{z}^{(\varrho)} + \xi$ , and then the TRM transport is determined by computing the ensemble mean for this transport.

### Quasi-Stokes transport

The TRM transport (47.98) can be decomposed into an Eulerian mean plus the correlation of a fluctuation

$$\bar{U}^\#(\bar{z}^{(\varrho)}) \equiv \bar{U}(\bar{z}^{(\varrho)}) + \bar{U}^{qs}(\bar{z}^{(\varrho)}). \quad (47.99)$$

The first term,

$$\bar{U}(\bar{z}^{(\varrho)}) = \int_{-H}^{\bar{z}^{(\varrho)}} \mathbf{u} dz \quad (47.100)$$

is the ensemble mean transport between the bottom and the ensemble mean depth,  $\bar{z}^{(\varrho)}$ . We interpret this transport as an Eulerian mean since the depth ranges are fixed. In contrast, the *quasi-Stokes* transport

$$\bar{U}^{qs}(\bar{z}^{(\varrho)}) \equiv \overline{\int_{\bar{z}^{(\varrho)}}^{\bar{z}^{(\varrho)} + \xi} \mathbf{u} dz} \quad (47.101)$$

measures the ensemble mean transport between the mean vertical position of an isopycnal,  $\bar{z}^{(\varrho)}$ , and that of each ensemble member,  $\bar{z}^{(\varrho)} + \xi(\varrho)$ . We refer to transport as “quasi-Stokes” given that is the difference between an isopycnal (i.e., quasi-Lagrangian) mean and an Eulerian mean (see Section 47.3)

$$\bar{U}^{qs} = \bar{U}^\# - \bar{U}. \quad (47.102)$$

As for the traditional Stokes drift discussed in Sections 29.3, and 47.3.5, which arises from a correlation between larger velocity when a wave crest is present, so too does the quasi-Stokes transport arise from a correlation between a larger velocity and a larger undulation in isopycnal thickness.

### Three-component TRM velocity

Following from the vertical gauge expression (46.76), we introduce the TRM vector streamfunction

$$\bar{\Psi}^\# = \bar{U}^\# \times \hat{z}, \quad (47.103)$$

and the corresponding three-dimensional non-divergent TRM velocity

$$\bar{v}^\# = \nabla \times \bar{\Psi}^\#. \quad (47.104)$$

The vertical component,

$$\bar{w}^\# = \hat{z} \cdot (\nabla \times \bar{\Psi}^\#), \quad (47.105)$$

has no corresponding component in an isopycnal description, which only requires the horizontal thickness weighted transport,  $\hat{u}$ . However, the TRM vector streamfunction only requires the horizontal TRM transport,  $\bar{U}^\#$ , so the two descriptions in effect make use of the same number of degrees of freedom.

#### 47.5.4 Volume conservation and the thickness equation

Consider two perspectives on volume conservation: one based on isopycnal coordinates and the other based on geopotential coordinates.

##### Isopycnal coordinates

In isopycnal vertical coordinates, the volume of a fluid element is written

$$\delta V = \delta x \delta y \delta z = \delta x \delta y \delta \varrho \hbar, \quad (47.106)$$

where we introduced the specific thickness,  $\hbar$ , from equation (47.92). Geometrically, the product  $|\hbar \delta \varrho|$  represents the vertical distance, or *thickness*, between the two infinitesimally close density classes  $\varrho$  and  $\varrho + \delta \varrho$  (see Figure 42.2). Material conservation of both volume and potential density implies conservation of the product of specific thickness and horizontal area  $\delta x \delta y \hbar$ , which leads to the thickness equation (Section 44.1.3)

$$\frac{\partial \hbar}{\partial t} + \nabla_\varrho \cdot (\hbar \mathbf{u}) = 0, \quad (47.107)$$

with  $\mathbf{u}$  the horizontal velocity field, the time derivative is computed with  $\varrho$  held fixed, and

$$\nabla_\varrho = \nabla_z + \mathbf{S} \frac{\partial}{\partial z} \quad (47.108)$$

is the horizontal derivative operator with  $\varrho$  held fixed and

$$\mathbf{S} = \nabla_\varrho z \quad (47.109)$$

is the horizontal slope of the potential density surface.

##### Geopotential coordinates

An Eulerian  $z$ -coordinate description of volume stirring within isopycnal layers is rendered via a combination of volume conservation,  $\nabla \cdot \mathbf{v} = 0$ , and material conservation of potential density,  $D\varrho/Dt = 0$ . When written as skewension rather than advection, the natural gauge is the vertical

gauge introduced in Section 46.7.1 (equation (46.74)), since this gauge only requires the same horizontal velocity field  $\mathbf{u}$  used with the isopycnal coordinate description. This gauge has an associated skew flux of potential density  $\mathbf{F}^{\text{skew}} = -\nabla\varrho \times \Psi$ , which leads to the evolution

$$\frac{\partial\varrho}{\partial t} = \nabla \cdot (\nabla\varrho \times \Psi), \quad (47.110)$$

where all derivatives are here taken with fixed Eulerian (geopotential) coordinates,  $(x, y, z)$ , and the divergence operator is three-dimensional.

### 47.5.5 Ensemble mean kinematics in isopycnal coordinates

Consider an ensemble of stably stratified (so that the layer specific thickness  $h$  is single-signed and nonvanishing) perfect Boussinesq fluid parcels with the same infinitesimal volume,  $\delta V = \delta x \delta y \delta z = \delta x \delta y h \delta\varrho$ , and same potential density,  $\varrho$ . Lacking any other marker, such as a tracer concentration, the ensemble members are distinguished from one another by values of their horizontal area,  $\delta A = \delta x \delta y$ , and their specific thickness,  $h$ , that is, their geometric attributes. The ensemble members are assumed to be stirred by different stochastic realizations of the fluid flow. Since each flow realization alters the geometric properties of the parcels, a mean field description focuses on the mean of these geometric properties.

In isopycnal coordinates,  $(x, y, \varrho, t)$ , the thickness equation (47.107) is satisfied by each ensemble member

$$\frac{\partial h}{\partial t} + \nabla_\varrho \cdot (h \mathbf{u}) = 0. \quad (47.111)$$

The ensemble mean computed over these fluid parcels with potential density  $\varrho$  satisfies

$$\partial_t \bar{h}^{(\varrho)} + \nabla_\varrho \cdot (\bar{h}^{(\varrho)} \bar{\mathbf{u}}^{(\varrho)} + \bar{h}' \bar{\mathbf{u}}'^{(\varrho)}) = 0, \quad (47.112)$$

where primed variables represent deviations from the isopycnal mean. The mean specific thickness  $\bar{h}^{(\varrho)}$  of parcels with potential density  $\varrho$  therefore satisfies the conservation equation

$$\partial_t \bar{h}^{(\varrho)} + \nabla_\varrho \cdot (\bar{h}^{(\varrho)} \hat{\mathbf{u}}) = 0. \quad (47.113)$$

In this equation we introduced the thickness weighted isopycnal ensemble mean horizontal velocity

$$\hat{\mathbf{u}} = \frac{\bar{h} \mathbf{u}^{(\varrho)}}{\bar{h}^{(\varrho)}} = \bar{\mathbf{u}}^{(\varrho)} + \frac{\bar{h}' \bar{\mathbf{u}}'^{(\varrho)}}{\bar{h}^{(\varrho)}} \equiv \bar{\mathbf{u}}^{(\varrho)} + \mathbf{u}^{\text{bolus}}, \quad (47.114)$$

along with the isopycnal ensemble mean horizontal velocity,  $\bar{\mathbf{u}}^{(\varrho)}$ , and the horizontal *bolus velocity*,  $\mathbf{u}^{\text{bolus}}$  originally introduced by Rhines (1982). The bolus velocity for an isopycnal layer corresponds to the transport

$$\bar{h}^{(\varrho)} \mathbf{u}^{\text{bolus}} = \bar{h}^{(\varrho)} (\hat{\mathbf{u}} - \bar{\mathbf{u}}^{(\varrho)}) = \bar{h}' \bar{\mathbf{u}}'^{(\varrho)} \quad (47.115)$$

arises from the along-isopycnal correlations between specific thickness and horizontal velocity.

Quite conveniently, the mean conservation equation (47.113) takes the *same* mathematical form as the conservation equation (47.111) satisfied by each ensemble member. The key difference is that the isopycnal ensemble mean thickness  $\bar{h}^{(\varrho)}$  is stirred by the thickness weighted isopycnal ensemble mean horizontal velocity  $\hat{\mathbf{u}}$ , whereas the thickness of each ensemble member is stirred by a randomly different realization of the horizontal velocity  $\mathbf{u}$ . The simplicity of the mean field description (47.113) is afforded by use of the Lagrangian vertical coordinate  $\varrho$ .

FIGURE 47.4: Schematic of the ensemble averaged potential density as measured by an observer at a fixed point  $(x, y, z, t)$  in space-time. In general, different members of the ensemble have potential density surfaces that live at different depths. That is, a fixed Eulerian space-time observer measures an ensemble mean potential density as the average over different potential density surfaces. For the case of a two-member ensemble as shown here,  $2\bar{\rho}^z(z) = \rho(1, z) + \rho(2, z)$ , where  $\rho(1, z)$  is generally different from  $\rho(2, z)$ .

### 47.5.6 Ensemble mean kinematics in geopotential coordinates

We now consider a geopotential coordinate description of the isopycnal ensemble. For this purpose, we interpret a vertical position,  $z$ , as the ensemble mean vertical position,  $\bar{z}^{(\varrho)}$ . Consequently, mean fields defined at the fixed vertical position correspond to either modified mean fields when not thickness weighted (equation (47.89)), or TRM fields when thickness weighted (equation (47.94)).

#### *Evolution of modified mean density*

Following the skewson formulation from Section 46.7, at the ensemble mean depth  $z = \bar{z}^\varrho$ , the streamfunction  $\bar{\Psi}^\#$  defines an effective skew flux of the modified mean potential density given by

$$\bar{\mathbf{F}}^\# = -\nabla \tilde{\varrho} \times \bar{\Psi}^\#. \quad (47.116)$$

Using the identity  $\bar{\Psi}^\# = \bar{\mathbf{U}}^\# \times \hat{\mathbf{z}}$ , we can write this expression in one of the forms

$$\bar{\mathbf{F}}^\# = -\bar{\mathbf{U}}^\# \partial_z \tilde{\varrho} + \hat{\mathbf{z}} \bar{\mathbf{U}}^\# \cdot \nabla_z \tilde{\varrho} \quad (47.117a)$$

$$= -(\bar{\mathbf{U}}^\# + \hat{\mathbf{z}} \mathbf{S} \cdot \bar{\mathbf{U}}^\#) \partial_z \tilde{\varrho}, \quad (47.117b)$$

where

$$\mathbf{S} = -\frac{\nabla_z \tilde{\varrho}}{\partial_z \tilde{\varrho}} \quad (47.118)$$

is the slope of the modified mean density field and  $\nabla_z = (\partial_x, \partial_y, 0)$  is the horizontal gradient operator taken with constant depth  $z = \bar{z}^{(\varrho)}$ . The convergence of the effective skew flux leads to a stirring of the modified mean density  $\tilde{\varrho}$  at the mean depth  $z = \bar{z}^{(\varrho)}$ ,

$$\frac{\partial \tilde{\varrho}}{\partial t} = \nabla \cdot (\nabla \tilde{\varrho} \times \bar{\Psi}^\#). \quad (47.119)$$

This equation represents an geopotential coordinate specification of the evolution of the modified mean density due to stirring by the mean eddies. It corresponds directly to the evolution equation (47.110) satisfied at depth  $z$  by a single member of the ensemble.

### 47.5.7 Approximate ensemble mean kinematics in geopotential coordinates

Equation (47.119) represents an exact  $z$ -coordinate description of the stirring of modified mean potential density. However, when working in geopotential coordinates, all that is available is Eulerian information. Hence, the Lagrangian information used to realize this exact description must be approximated.

*Estimating the quasi-Stokes transport*

The approximation requires us to estimate the quasi-Stokes transport  $\bar{U}^{\text{qs}}$  defined by equation (47.101). We addressed a similar estimation in Section 47.3.4 when discussing the Stokes mean. Here, we expand the TRM transport in a Taylor series about the geopotential  $z = \bar{z}^{(\varrho)}$

$$\bar{U}^\#(z) = \overline{\int_{-H}^{z+\xi} \mathbf{u}(s) ds} \quad (47.120\text{a})$$

$$= \bar{U}(z) + \overline{\mathbf{u}\xi}^{(z)} + \frac{1}{2} \overline{\partial_z \mathbf{u} \xi \xi}^{(z)} + \mathcal{O}(\alpha^3), \quad (47.120\text{b})$$

where neglected terms are third order in deviation quantities. Note that all ensemble means are taken at fixed vertical position, which accords with taking a Taylor series about the ensemble mean depth  $z = \bar{z}^{(\varrho)}$ .

The ensemble means in equation (47.120b) are interpreted as follows. The first term is the Eulerian mean horizontal transport passing beneath the ensemble mean depth,  $z = \bar{z}^{(\varrho)}$ . The second term,  $\overline{\mathbf{u}\xi}$  is the horizontal velocity evaluated at the ensemble mean depth and multiplied by the deviation,  $\xi$ , of the potential density surface from its mean depth, all averaged at fixed depth. An Eulerian split of the horizontal velocity  $\mathbf{u}$  into its Eulerian mean  $\bar{\mathbf{u}}^{(z)}$  and deviation  $\mathbf{u}'$  leads to the correlation

$$\overline{\mathbf{u}\xi}^{(z)} = \overline{\mathbf{u}'\xi}^{(z)}. \quad (47.121)$$

For the second order term, similar considerations lead to

$$\overline{\partial_z \mathbf{u} \xi \xi}^{(z)} \approx \partial_z \bar{\mathbf{u}}^z \overline{\xi \xi}^{(z)}, \quad (47.122)$$

where neglected terms are third order and higher. Combining these relations leads to the second order accurate expression

$$\bar{U}^\# \approx \bar{U} + \overline{\mathbf{u}'\xi}^{(z)} + \frac{1}{2} \overline{\xi \xi}^z \partial_z \bar{\mathbf{u}}^{(z)}. \quad (47.123)$$

*The disturbance field*

Following the discussion in Section 47.3.6, we here determine the disturbance field,  $\xi$ , in terms of fields at constant depth. For this purpose, use the identity (47.90) to give

$$\tilde{\varrho}(z) = \varrho(z + \xi) \quad (47.124\text{a})$$

$$= \varrho(z) + \partial_z \varrho(z) \xi + \frac{1}{2} \partial_{zz} \varrho(z) \xi^2 + \mathcal{O}(\alpha^3). \quad (47.124\text{b})$$

Subtracting the Eulerian mean of equation (47.124b) from the unaveraged equation (47.124b), and noting that  $\tilde{\varrho}$  is already a mean field, leads to the second order accurate expression for the deviation

$$\xi = -\varrho'(z)/\partial_z \bar{\varrho}^{(z)} + \mathcal{O}(\alpha^2), \quad (47.125)$$

where

$$\varrho(z) = \bar{\varrho}^{(z)} + \varrho'(z). \quad (47.126)$$

To within the same order, the deviation can be written

$$\xi = -\varrho'(z)/\partial_z \tilde{\varrho}(z) + \mathcal{O}(\alpha^2). \quad (47.127)$$

### Approximate quasi-Stokes transport

Substituting the deviation (47.127) into the approximate expression (47.120b) for the TRM transport yields an approximate expression for the Stokes transport

$$\mathbf{U}^{\text{qs}} = -\frac{\overline{\mathbf{u}' \varrho'}^{(z)}}{\partial_z \tilde{\varrho}} + \frac{\overline{\phi}^{(z)} \partial_z \overline{\mathbf{u}}^{(z)}}{(\partial_z \tilde{\varrho})^2} + \mathcal{O}(\alpha^3), \quad (47.128)$$

where

$$\overline{\phi}^{(z)} = \frac{1}{2} \overline{\varrho' \varrho'}^{(z)} \quad (47.129)$$

is the mean potential density variance. [McDougall and McIntosh \(2001\)](#) noted that the [Gent et al. \(1995\)](#) scheme offers a parameterization of the two correlations on the right hand side of equation (47.128). We have more to say regarding this parameterization in Section 48.1.

Substituting the deviation (47.127) into the approximate expression (47.124b) yields, to within terms of third order, the relation

$$\tilde{\varrho} = \overline{\varrho}^{(z)} - \partial_z \left[ \frac{\overline{\phi}^{(z)}}{\partial_z \overline{\varrho}^{(z)}} \right] + \mathcal{O}(\alpha^3). \quad (47.130)$$

As for the Stokes transport, the modified mean density and Eulerian mean density, when evaluated at the same depth, differ by terms that are second order in eddy amplitude.

### 47.5.8 Further study

This section is largely based on approaches used by [DeSzeke and Bennett \(1993\)](#), [McIntosh and McDougall \(1996\)](#), [Kushner and Held \(1999\)](#), and [McDougall and McIntosh \(2001\)](#) as summarized in Section 9.3 of [Griffies \(2004\)](#). Many other papers have applied this formalism to a variety of analyses, with examples including [Nurser and Lee \(2004a\)](#), [Nurser and Lee \(2004b\)](#), [Wolfe \(2014\)](#).

## 47.6 Mean tracer equation

We now include a tracer field to the ideal Boussinesq parcel and determine a mean field description for the tracer. The transport of tracer by eddies has both a reversible stirring component and an irreversible mixing component. The stirring arises from both the thickness correlation to velocity as well as the velocity correlated with tracer.

### 47.6.1 Thickness weighted means

Equation (47.114) introduced a specific thickness weighted mean operator, which will prove to be quite useful when considering the mean tracer equation. In general, for any field  $\Phi$  associated with a potential density layer  $\varrho$ , we define the decomposition into thickness weighted mean and deviation

$$\Phi(\varrho) = \widehat{\Phi}(\varrho) + \Phi''(\varrho) \quad (47.131a)$$

$$= \frac{\overline{h \Phi}^{(\varrho)}}{\overline{h}^{(\varrho)}} + \Phi''. \quad (47.131b)$$

It follows by definition that

$$\overline{h \Phi''}^{(\varrho)} = 0. \quad (47.132)$$

### 47.6.2 Isopycnal mean thickness weighted tracer equation

When attaching a tracer to fluid parcels, each member of the ensemble satisfies the isopycnal tracer equation

$$\frac{\partial C}{\partial t} + \mathbf{u} \cdot \nabla_{\varrho} C = 0. \quad (47.133)$$

Combining the tracer and thickness equations leads to the thickness weighted tracer equation

$$\frac{\partial(\hbar C)}{\partial t} + \nabla_{\varrho} \cdot (\hbar \mathbf{u} C) = 0. \quad (47.134)$$

Hence, in isopycnal coordinates and in the absence of irreversible processes, the evolution of thickness weighted tracer occurs via the isopycnally oriented convergence of the two-dimensional thickness weighted horizontal advective flux,  $\hbar \mathbf{u} C$ .

To address the problem of describing the ensemble mean tracer equation in isopycnal coordinates, decompose the tracer and velocity field into their thickness weighted average and deviation to give

$$\partial_t[\hbar(\hat{C} + C'')] + \nabla_{\varrho} \cdot [\hbar(\hat{\mathbf{u}} + \mathbf{u}'')](\hat{C} + C'') = 0. \quad (47.135)$$

Taking an ensemble average over fluid elements with the same potential density, and using equation (47.132), yield the mean thickness weighted tracer equation

$$\partial_t(\bar{h}^{(\varrho)} \hat{C}) + \nabla_{\varrho} \cdot (\bar{h}^{(\varrho)} \hat{C} \hat{\mathbf{u}}) = -\nabla_{\varrho} \cdot (\bar{h} \bar{C}'' \bar{\mathbf{u}}'')^{(\varrho)}. \quad (47.136)$$

Now introduce the correlation

$$\bar{h} \bar{C}'' \bar{\mathbf{u}}''^{(\varrho)} = \bar{h}^{(\varrho)} \widehat{C'' \mathbf{u}''} \quad (47.137)$$

(see equation (47.131b)), and recall that the mean thickness  $\bar{h}^{(\varrho)}$  satisfies the mean thickness equation (47.113). These two points lead to the evolution equation for the mean thickness weighted tracer concentration

$$(\partial_t + \hat{\mathbf{u}} \cdot \nabla_{\varrho}) \hat{C} = -\frac{1}{\bar{h}^{(\varrho)}} \nabla_{\varrho} \cdot (\bar{h}^{(\varrho)} \widehat{C'' \mathbf{u}''}). \quad (47.138)$$

### 47.6.3 Subgrid scale tracer transport tensor

The correlation between tracer and velocity found on the right-hand side of the mean thickness weighted tracer equation (47.138) is typically written in terms of a subgrid scale tracer transport tensor

$$\widehat{C'' \mathbf{u}''} = -\mathbb{J} \cdot \nabla_{\varrho} \hat{C}. \quad (47.139)$$

This definition leads to the evolution equation

$$(\partial_t + \hat{\mathbf{u}} \cdot \nabla_{\varrho}) \hat{C} = \frac{1}{\bar{h}^{(\varrho)}} \nabla_{\varrho} \cdot (\bar{h}^{(\varrho)} \mathbb{J} \cdot \nabla_{\varrho} \hat{C}). \quad (47.140)$$

The subgrid scale operator on the right hand side has the same general form as the diffusion operator written in isopycnal coordinates as derived in Section 41.15. However, in addition to symmetric diffusion processes, this operator includes skewed fluxes that lead to skew diffusion as discussed in Section 47.4.2. Whereas the diffusive aspect is commonly parameterized as dianeutral diffusion and neutral diffusion (Section 48.1), there is no parameterization for the skewed correlations for use in ocean models. We comment further on this situation in Section 48.3.8.

#### 47.6.4 Mean tracer transport beneath a density surface

It is useful to further elucidate the relevance of mean thickness weighted fields. For this purpose, consider the mean horizontal tracer transport occurring beneath a particular potential density surface  $\varrho = \tilde{\varrho}$ ,

$$\overline{C}^\#(\tilde{z}^{(\varrho)}) = \overline{\int_{-H}^{\tilde{z}^{(\varrho)} + \xi} C \mathbf{u} dz}. \quad (47.141)$$

Setting tracer concentration to unity recovers the expression (47.98) for the TRM transport. Changing coordinates and making use of the tracer correlation tensor renders

$$\overline{C}^\#(\tilde{z}^{(\varrho)}) = \int_{\varrho(-H)}^{\tilde{\varrho}(\tilde{z}^{(\varrho)})} \overline{C \mathbf{u} h^{(\varrho)}} d\varrho \quad (47.142a)$$

$$= \int_{\varrho(-H)}^{\tilde{\varrho}(\tilde{z}^{(\varrho)})} \overline{h^{(\varrho)}} d\varrho (\widehat{C} \widehat{\mathbf{u}} + \widehat{C'' \mathbf{u}''}) \quad (47.142b)$$

$$= \int_{\varrho(-H)}^{\tilde{\varrho}(\tilde{z}^{(\varrho)})} \overline{h^{(\varrho)}} d\varrho (\widehat{C} \widehat{\mathbf{u}} - \mathbb{J} \cdot \nabla_\varrho \widehat{C}) \quad (47.142c)$$

$$= \int_{-H}^{\tilde{z}^{(\varrho)}} dz (\widehat{C} \widehat{\mathbf{u}} - \mathbb{J} \cdot \nabla_\varrho \widehat{C}). \quad (47.142d)$$

Hence, the mean thickness weighted fields naturally appear when considering such physically interesting quantities as the mean horizontal transport of a tracer beneath the modified mean potential density surface.

#### 47.6.5 Summary of the tracer parameterization problem

Traditionally, the isopycnal parameterization problem for the evolution of the mean thickness weighted tracer requires a parameterization of the bolus velocity  $\mathbf{u}^{\text{bolus}}$ , which again is related to the thickness weighted horizontal velocity via

$$\widehat{\mathbf{u}}((\varrho)) = \frac{\overline{h \mathbf{u}}^{(\varrho)}}{\overline{h}^{(\varrho)}} = \overline{\mathbf{u}}^{(\varrho)} + \frac{\overline{h' \mathbf{u}'}^{(\varrho)}}{\overline{h}^{(\varrho)}} = \overline{\mathbf{u}}^{(\varrho)} + \mathbf{u}^{\text{bolus}}. \quad (47.143)$$

In addition to the bolus velocity, it is necessary to parameterize the subgrid scale tracer transport tensor

$$\widehat{C'' \mathbf{u}''} = -\mathbb{J} \cdot \nabla_\varrho \widehat{C}, \quad (47.144)$$

which generally has symmetric (diffusive) and antisymmetric (stirring) components (Section 47.4).

For a geopotential coordinate description, equation (47.94) is used to relate thickness weighted mean fields, defined as a function of  $\varrho$ , and TRM fields, defined as a function of the mean vertical position of  $\varrho$ , to write for the tracer field

$$\widehat{C}(x, y, \tilde{\varrho}, t) = \overline{C}^\#(x, y, \tilde{z}^{(\varrho)}, t). \quad (47.145)$$

Equation (47.145), and the developed formalism, leads to the mean field tracer equation in geopotential coordinates

$$\partial_t \overline{C}^\# = \nabla \cdot (\nabla \overline{C}^\# \times \overline{\Psi}^\#) + R(\overline{C}^\#), \quad (47.146)$$

where  $R(\overline{C}^\#)$  is the geopotential coordinate form of the mixing/stirring operator on the right-hand side of equation (47.140). Details for the transformation of the mixing/stirring operator from

isopycnal to geopotential coordinates are provided in Section 41.15.

### 47.6.6 Comments

Much in this section follows from [Smith \(1999\)](#), [McDougall and McIntosh \(2001\)](#), and [Young \(2012\)](#), each of which focused on the hydrostatic primitive equations assuming a vertically stable buoyancy stratification. The paper by [Young \(2012\)](#) is a milestone in the literature as he succeeded in formulating the ensemble mean primitive equations in a form where only the thickness weighted (residual mean) velocity appears. Prior attempts failed due to their insufficient mathematical framework. Hence, the formulation of [Young \(2012\)](#) eliminates the need to parameterize the bolus velocity or the quasi-Stokes transport since neither appear as separately identified terms.

Even so, realistic ocean general circulation models are not formulated as “residual mean” models. The key reason is that outside of the stably stratified interior, as in boundary layers, thickness weighted averaging is inappropriate. Instead, we need Eulerian averaged fields when formulating boundary layer closures (e.g., [Large et al., 1994](#)). [Young \(2012\)](#) thus provides a compelling method to decompose the flow into eddies and mean within the stably stratified interior. However, it is not sufficient to capture the full suite of flow regimes represented or parameterized by realistic ocean circulation models.



# Chapter 48

## Mathematics of parameterized tracer transport

In the presence of turbulent flow processes, tracer variance directly cascades to the small scales. This *downscale cascade* is facilitated by reversible stirring from balanced and unbalanced fluctuations (e.g., mesoscale eddies, submesoscale eddies, breaking gravity and lee waves, turbulent boundary layer processes). The cascade to progressively smaller scales eventually reaches the *Batchelor scale* (order millimetres; e.g., Section 11.5.1 of [Vallis \(2017\)](#)). At this scale, tracer gradients are sufficiently large in magnitude that molecular diffusion can readily act to dissipate tracer variance through irreversible diffusive mixing. Tracer transport at scales larger than the Batchelor scale is dominated by reversible stirring, whereas transport at and below the Batchelor scale is dominated by irreversible mixing from molecular diffusion. This phenomenology provides a constraint on the form of the tracer equation to be used for coarse grained numerical models, where the model grid scale,  $\Delta$ , is generally much larger than the Batchelor scale.

In this chapter, we study certain of the mathematical and physical properties of parameterized advective and diffusive tracer transport. In general, such parameterizations aim to encapsulate key aspects of physical processes too small to observe and/or simulate. This *subgrid scale parameterization problem* is far broader and deeper than available from a single chapter. We focus mostly on subgrid scale advection and diffusion operators arising from mesoscale eddy motions, yet even this limited focus involves far more than can be covered here. In particular, we do not discuss theories for how the eddy diffusivities are computed. Furthermore, we only consider parameterizations of the subgrid scale tracer flux, whose convergence provides a subgrid tendency for the coarse-grained tracer equation. Focusing on fluxes supports locality and conservation for the coarse-grained tracer equation, with these properties also shared by the uncoarsened tracer equation.

### CHAPTER GUIDE

Tracers evolve according to the advection-diffusion equation discussed in Chapter 46 and further unpacked in the tracer kinematics Chapter 47. We here build on material in these two chapters in summarizing the basics of advective-diffusive parameterizations of tracer transport. We also make use of neutral directions as detailed in Section 24.5. Mathematically we rely on Cartesian tensor analysis from Chapters 1 and 2.

48.1.1	A synopsis of ocean mixing processes . . . . .	1190
48.1.2	A rough comparison . . . . .	1191
48.1.3	Diffusive parameterization of fine scale mixing . . . . .	1192
48.1.4	Advectione-diffusive parameterization of eddy-induced transport . . . . .	1192
48.1.5	Mathematical elements of eddy-induced stirring . . . . .	1193
48.1.6	Dianeutral unit vector and the neutral slope . . . . .	1194
48.2	Various forms for small scale diffusion . . . . .	<b>1195</b>
48.2.1	Isotropic diffusion . . . . .	1195
48.2.2	Vertical diffusion . . . . .	1195
48.2.3	Dianeutral diffusion . . . . .	1195
48.3	Gent-McWilliams stirring . . . . .	<b>1196</b>
48.3.1	Details of the parameterization . . . . .	1197
48.3.2	Effects on buoyancy . . . . .	1197
48.3.3	Local adiabatic dissipation of available potential energy . . . . .	1199
48.3.4	Meridional overturning mass transport . . . . .	1200
48.3.5	Connection to form stress . . . . .	1201
48.3.6	Connection to isopycnal thickness diffusion . . . . .	1202
48.3.7	A parameterization based on a boundary value problem . . . . .	1204
48.3.8	Comments . . . . .	1205
48.4	Neutral diffusion . . . . .	<b>1205</b>
48.4.1	Motivation for neutral diffusion . . . . .	1205
48.4.2	Redi neutral diffusion . . . . .	1206
48.4.3	Small slope neutral diffusion . . . . .	1206
48.4.4	Neutral tangent plane neutral diffusion . . . . .	1207
48.4.5	Neutrality condition . . . . .	1208
48.4.6	Symmetry condition . . . . .	1208
48.4.7	GM skewson plus small slope neutral diffusion . . . . .	1209
48.4.8	Generalized vertical coordinates . . . . .	1209
48.5	Anisotropic neutral diffusion . . . . .	<b>1211</b>
48.5.1	Orthonormal triad of basis vectors . . . . .	1211
48.5.2	Anisotropic neutral diffusion tensor . . . . .	1212
48.5.3	Properties of the anisotropic neutral diffusive fluxes . . . . .	1213
48.5.4	Small slope anisotropic neutral diffusion . . . . .	1213
48.6	Anisotropic Gent-McWilliams stirring . . . . .	<b>1215</b>
48.6.1	Streamfunction and anti-symmetric tensor . . . . .	1215
48.6.2	Anisotropic Gent-McWilliams skew tracer flux . . . . .	1215
48.6.3	Anisotropic GM skewson plus small slope neutral diffusion . . . . .	1216
48.6.4	A parameterization based on a boundary value problem . . . . .	1216

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## 48.1 Summarizing tracer transport parameterizations

In this section we offer an outline of the tracer transport parameterizations, starting from the small scales and moving to the mesoscale.

### 48.1.1 A synopsis of ocean mixing processes

Irreversible mixing in the ocean takes place at the millimeter scale through the process of molecular or *Brownian motion* acting to dissipate property gradients. This mixing is generally represented by downgradient molecular diffusion ([Einstein, 1905](#)). The molecular diffusivity of matter (e.g., salt) in seawater is roughly  $10^{-9} \text{ m}^2 \text{ s}^{-1}$ , whereas the molecular thermal diffusivity is roughly 100 times larger (it is easier to diffuse enthalpy (heat) than matter, [Gill, 1982](#)). Reversible stirring by turbulent eddies greatly increases the magnitude of property gradients upon which *molecular diffusion* acts ([Eckart, 1948](#); [Nakamura, 2001](#); [Müller and Garrett, 2002](#)), thereby increasing the

total amount of irreversible mixing. Motivated by molecular diffusion, and following the pioneering work of [Taylor \(1921\)](#), it is common to parameterize mixing induced by eddy stirring as a diffusive closure with an eddy diffusivity that is far larger than molecular values. Furthermore, the eddy diffusivities are generally the same for all tracers since eddies generally act the same regardless the tracer. Double diffusive processes is the notable counter-example to this equivalence [Schmitt \(1994\)](#).

Mixing induced by eddies of length scale  $\mathcal{O}(\text{centimeters} - \text{metres})$  is associated with, among other *fine scale mixing* processes such as gravitational instability, shear instability and breaking internal gravity waves ([MacKinnon et al., 2013](#)), as well as a suite of boundary layer processes ([Large et al., 1994](#)). This mixing is commonly parameterized by a flow dependent isotropic eddy diffusivity. The magnitude of the eddy diffusivity is typically  $\mathcal{O}(10^{-3} - 10^{-2} \text{ m}^2 \text{ s}^{-1})$  in boundary layers, and  $\mathcal{O}(10^{-5} \text{ m}^2 \text{ s}^{-1})$  in the quiescent ocean interior ([Polzin et al., 1997; Whalen et al., 2012; Waterhouse et al., 2014](#)).

Mesoscale eddies, with size  $\mathcal{O}(10 - 100) \text{ km}$ , preferentially stir tracers along neutral directions ([McDougall, 1987a,b; McDougall et al., 2014](#)). The mesoscale eddy stirring in turn induces a mixing that is parametrized by downgradient diffusion along neutral directions (Section 48.4). When feeling the geometric constraints of the surface boundary, mesoscale stirring leads to horizontal oriented mixing across outcropped density surfaces ([Treguier et al., 1997; Ferrari et al., 2008; Danabasoglu et al., 2008](#)). This mixing is parameterized by downgradient horizontal diffusion. The neutral and horizontal eddy diffusivities associated with mesoscale processes are typically  $\mathcal{O}(10^2 - 10^3 \text{ m}^2 \text{ s}^{-1})$  in the ocean interior and can rise to  $\mathcal{O}(10^4 \text{ m}^2 \text{ s}^{-1})$  in the ocean surface layer ([Abernathay et al., 2013; Klocker and Abernathay, 2014; Cole et al., 2015](#)).

### 48.1.2 A rough comparison

What process is more important for setting tracer distributions: neutral diffusion induced by mesoscale eddies or small scale isotropic diffusion induced by breaking gravity waves? Since the neutral diffusivity arises from mesoscale eddy stirring, it is many orders of magnitude larger than the isotropic diffusivity arising from fine scale mixing. However, these two eddy diffusivities act on very different tracer gradients, in which case the net effects on tracer distributions could be more comparable.

To help answer the question, consider a scaling with a constant neutral diffusivity and a constant isotropic diffusivity. Furthermore, assume Cartesian orientation of the diffusion operators (i.e., zero neutral slope) and assume the isotropic diffusion is dominated by vertical diffusion (see Section 48.2). We are thus comparing the following two diffusion processes

$$\text{horizontal diffusion} = \kappa_{\text{horz}} \nabla_z^2 C \quad \text{and} \quad \text{vertical diffusion} = \kappa_{\text{vert}} \partial_{zz} C. \quad (48.1)$$

Now introduce a vertical scale  $H$  and horizontal scale  $L$  over which the tracer concentration changes by an amount  $\delta C$ . Doing so leads to the scaled diffusion operators

$$\text{horizontal diffusion} \sim (\kappa_{\text{horz}}/L^2) \delta C \quad \text{and} \quad \text{vertical diffusion} \sim (\kappa_{\text{vert}}/H^2) \delta C. \quad (48.2)$$

These operators have the same scale when

$$\kappa_{\text{vert}} = (H/L)^2 \kappa_{\text{horz}}. \quad (48.3)$$

Choosing  $L = 10^5 \text{ m}$  and  $H = 10^1 \text{ m}$  leads to

$$\kappa_{\text{vert}} = 10^{-8} \kappa_{\text{horz}}. \quad (48.4)$$

Furthermore, if  $\kappa_{\text{horz}} = 10^3 \text{ m}^2 \text{ s}^{-1}$ , then the two operators provide a similar contribution to tracer evolution if  $\kappa_{\text{vert}} = 10^{-5} \text{ m}^2 \text{ s}^{-1}$ . This is a rather small diffusivity that is generally thought to be on the order of that afforded by the background of breaking gravity waves in the ocean interior ([MacKinnon et al., 2013](#)). This scaling is crude since the length scales are dependent on details of the flow regime as are the eddy diffusivities. Even so, it suggests that the two diffusive processes can indeed contribute to tracer distributions by a similar amount.

### 48.1.3 Diffusive parameterization of fine scale mixing

Ignoring the cross-diffusion processes introduced in Section 21.7 (see also [IOC et al. \(2010\)](#), Section 2.5 of [Olbers et al. \(2012\)](#), and [Graham and McDougall \(2013\)](#)), the molecular diffusion of  $\Theta$  and  $S$  lead to the material evolution equations

$$\rho \frac{D\Theta}{Dt} = \nabla \cdot (\rho \kappa_\Theta \nabla \Theta) \quad (48.5a)$$

$$\rho \frac{DS}{Dt} = \nabla \cdot (\rho \kappa_S \nabla S), \quad (48.5b)$$

where  $\kappa_\Theta > 0$  and  $\kappa_S > 0$  are the molecular kinematic diffusivities for  $\Theta$  and  $S$ , respectively. For a measured scale,  $\Delta$ , larger than the scale where gravity waves break and dissipate kinetic energy (i.e., tens to hundreds of metres), diffusion is commonly used to parameterize the associated irreversible tracer mixing (e.g., [MacKinnon et al., 2013](#)). Diffusion is also used to parameterize mixing from other small scale processes, such as turbulent boundary layer processes, double-diffusion, breaking leewaves, and other processes. As discussed in Section 4 of [McDougall et al. \(2014\)](#), small scale mixing generally takes place in an isotropic manner. Its parameterization thus appears just as for isotropic molecular diffusion given by equation (48.5b), yet with a far larger eddy diffusivity  $\kappa_{\text{fine}} \gg \kappa_\Theta, \kappa_S$  that is a function of the flow

$$\rho \frac{D\Theta}{Dt} = \nabla \cdot (\rho \kappa_{\text{fine}} \nabla \Theta) \quad (48.6a)$$

$$\rho \frac{DS}{Dt} = \nabla \cdot (\rho \kappa_{\text{fine}} \nabla S). \quad (48.6b)$$

The same eddy diffusivity is used for both  $\Theta$  and  $S$ . This assumption follows the general approach for turbulent transport parameterizations (e.g, [Vallis, 2017](#)), whereby eddies are assumed to act in the same manner on any conserved scalar tracer.

### 48.1.4 Advection-diffusive parameterization of eddy-induced transport

Stirring from turbulent scales smaller than the grid scale is commonly parameterized by an eddy-induced stirring velocity,  $\mathbf{v}^*$ . For ocean mesoscale eddies, such parameterized stirring generally follows a variant of [Gent and McWilliams \(1990\)](#) and [Gent et al. \(1995\)](#), with this stirring quite important for setting large-scale ocean tracer distributions. In addition, mixing is promoted by the direct cascade from stirring. This mixing is parameterized by a diffusion operator distinct from that used for the small scale mixing discussed in Section 48.1.3.

Consider a second order subgrid scale transport tensor,  $\mathbb{M}$ , meant to parameterize both subgrid scale eddy stirring and eddy mixing. With this tensor, the evolution of salinity and Conservative

Temperature takes the form

$$\rho \frac{DS}{Dt} = \nabla \cdot (\rho \mathbb{M} \cdot \nabla S) \quad (48.7a)$$

$$\rho \frac{D\Theta}{Dt} = \nabla \cdot (\rho \mathbb{M} \cdot \nabla \Theta). \quad (48.7b)$$

As for the fine scale diffusion equations (48.6a) and (48.6b), we here use the same transport tensor for both  $S$  and  $\Theta$  as eddies are assumed to act in the same manner on any conserved scalar tracer. As presented in Chapter 46, we decompose the second order transport tensor into the sum of its symmetric and anti-symmetric components

$$\mathbb{M} = \mathbb{K} + \mathbb{A}. \quad (48.8)$$

When the symmetric tensor,  $\mathbb{K}$ , is positive-definite, it gives rise to downgradient diffusion. In contrast, the anti-symmetric tensor,  $\mathbb{A}$ , gives rise to skew-diffusion or eddy-induced advection.

### 48.1.5 Mathematical elements of eddy-induced stirring

As detailed in Sections 46.5, 46.6, and 47.4, the anti-symmetric tensor,  $\mathbb{A}$ , contributes to the parameterized transport according to

$$\nabla \cdot (\rho \mathbb{A} \cdot \nabla S) = \partial_m(\rho \mathbb{A}^{mn} \partial_n S) \quad (48.9a)$$

$$= \partial_m(\rho \mathbb{A}^{mn}) \partial_n S + \rho \mathbb{A}^{mn} \partial_m \partial_n S \quad (48.9b)$$

$$= -\rho v^{*n} \partial_n S, \quad (48.9c)$$

where we made use of the Einstein index notation with repeated indices summed over their range  $m, n = 1, 2, 3$ , and where  $\mathbb{A}^{mn}$  are the components to the anti-symmetric transport tensor  $\mathbb{A}$ . Additionally, we noted that

$$\rho \mathbb{A}^{mn} \partial_m \partial_n S = 0 \quad (48.10)$$

since  $\mathbb{A}^{mn}$  is anti-symmetric whereas  $\partial_m \partial_n S$  is symmetric (see Exercise 1.2). Finally, we introduced a density-weighted *eddy-induced velocity*

$$\rho v^{*n} = -\partial_m(\rho \mathbb{A}^{mn}). \quad (48.11)$$

Importantly,  $\rho \mathbf{v}^*$  has a zero divergence, again due to anti-symmetry of  $\mathbb{A}^{mn}$

$$\nabla \cdot (\rho \mathbf{v}^*) = \partial_n(\rho v^{*n}) = -\partial_n \partial_m(\rho \mathbb{A}^{mn}) = 0. \quad (48.12)$$

A zero-divergence for  $\rho \mathbf{v}^*$  means that it contributes no mass sources or sinks to the fluid.<sup>1</sup>

Transport from the anti-symmetric tensor thus provides a means to stir tracers due to unresolved eddy processes. The mathematical form of the stirring can be either through skew-diffusion or through advection (see Section 46.6). Choosing to make use of the advection form allows us to combine the contribution from the anti-symmetric transport tensor with the resolved advection

---

<sup>1</sup>For a Boussinesq fluid, the density factor is replaced by the constant reference density,  $\rho_0$ , so that  $\nabla \cdot \mathbf{v}^* = 0$  in the Boussinesq fluid. See section 7 of [Griffies and Greatbatch \(2012\)](#) for more details of the Boussinesq and non-Boussinesq forms for the parameterized eddy-induced transport.

operator, thus resulting in a *residual mean* material transport equation

$$\rho \frac{D^\dagger S}{Dt} = \nabla \cdot (\rho \mathbb{K} \cdot \nabla S) \quad (48.13a)$$

$$\rho \frac{D^\dagger \Theta}{Dt} = \nabla \cdot (\rho \mathbb{K} \cdot \nabla \Theta), \quad (48.13b)$$

where the residual mean material time derivative is given by

$$\frac{D^\dagger}{Dt} = \frac{\partial}{\partial t} + \mathbf{v}^\dagger \cdot \nabla \quad (48.14)$$

and the *residual mean velocity* is

$$\mathbf{v}^\dagger = \mathbf{v} + \mathbf{v}^*. \quad (48.15)$$

#### 48.1.6 Dianeutral unit vector and the neutral slope

When considering closures for subgrid mixing and stirring arising from mesoscale motions, we orient the parameterized processes according to buoyancy as that reflects the physics of mesoscale motions.<sup>2</sup> We thus follow the discussion in Section 24.5 by working with locally referenced Archimedean buoyancy to determine neutral directions. In particular, at each point in the fluid we orient stirring and mixing through use of the dianeutral unit vector (Section 24.5.3)

$$\hat{\gamma} = \frac{-\alpha \nabla \Theta + \beta \nabla S}{|-\alpha \nabla \Theta + \beta \nabla S|} \quad \text{and} \quad \hat{\gamma} = \hat{\mathbf{x}} \hat{\gamma}_x + \hat{\mathbf{y}} \hat{\gamma}_y + \hat{\mathbf{z}} \hat{\gamma}_z \quad \text{and} \quad \hat{\gamma} \cdot \hat{\gamma} = \hat{\gamma}_x^2 + \hat{\gamma}_y^2 + \hat{\gamma}_z^2 = 1, \quad (48.16)$$

with  $\hat{\gamma}$  pointing perpendicular to the neutral tangent plane in a direction towards larger density.<sup>3</sup> Furthermore, when the fluid is stably stratified in the vertical, which is common for the mesoscale and larger, then the squared buoyancy frequency is positive (Section 24.4)

$$N^2 = -g(-\alpha \partial_z \Theta + \beta \partial_z S) > 0. \quad (48.17)$$

We can thus introduce the slope of the neutral tangent plane relative to the  $(x, y)$  horizontal plane

$$\mathbf{S} = - \left[ \frac{-\alpha \nabla_z \Theta + \beta \nabla_z S}{-\alpha \partial_z \Theta + \beta \partial_z S} \right] = \frac{g(-\alpha \nabla_z \Theta + \beta \nabla_z S)}{N^2} = \hat{\mathbf{x}} S_x + \hat{\mathbf{y}} S_y. \quad (48.18)$$

For such stably stratified fluids, the dianeutral direction can be written in terms of the neutral slope

$$\hat{\gamma} = \frac{\mathbf{S} - \hat{\mathbf{z}}}{(1 + \mathbf{S}^2)^{1/2}}. \quad (48.19)$$

In this form we see that the dianeutral direction is vertically downward when the slopes vanish, which accords with this direction generally pointing toward increasing density.

<sup>2</sup>We offer further discussion of this point at the start of Section 48.4.

<sup>3</sup>Equation (4) in [McDougall et al. \(2014\)](#) makes use of the opposite convention so that their dianeutral direction points towards decreasing density. We instead follow the water mass transformation convention as in equation (50.38), so that  $\hat{\gamma}$  points in the direction of increasing density.

## 48.2 Various forms for small scale diffusion

We here follow Section 4 from [McDougall et al. \(2014\)](#) to highlight distinctions between isotropic diffusion, dianeutral diffusion,<sup>4</sup> and vertical diffusion. Although commonly considered interchangeable in the literature as parameterizations of small scale mixing, there are conceptual distinctions that we identify here. Note that the distinctions between these three diffusions are quantitatively small when neutral slopes are modest and when  $\kappa_{\text{ntr}} \gg \kappa_{\text{fine}}$ .

### 48.2.1 Isotropic diffusion

As discussed in Section 48.1.3, we generally parameterize fine scale mixing processes via an isotropic diffusion process using a diffusivity  $\kappa_{\text{fine}} > 0$ , diffusion tensor

$$\mathbb{K}_{\text{iso}} = \kappa_{\text{fine}} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}, \quad (48.20)$$

and corresponding diffusion flux

$$\mathbf{J}_{\text{iso}} = -\rho \mathbb{K}_{\text{iso}} \cdot \nabla C. \quad (48.21)$$

As illustrated in Figure 48.1, under the effects from isotropic diffusion, a region of tracer is diffused the same in all three directions so that, for example, a spherical tracer distribution remains spherical.

### 48.2.2 Vertical diffusion

Because vertical density gradients are generally much larger than lateral gradients, it is common to approximate the small scale isotropic diffusion tensor with a vertical diffusion tensor

$$\mathbb{K}_{\text{vert}} = \kappa_{\text{fine}} \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}, \quad (48.22)$$

with a corresponding vertical diffusive flux

$$\mathbf{J}_{\text{vert}} = -\rho \kappa_{\text{fine}} (\nabla C \cdot \hat{\mathbf{z}}) \hat{\mathbf{z}} = -\rho \mathbb{K}_{\text{iso}} \cdot \nabla C = -\rho \kappa_{\text{fine}} \partial_z C \hat{\mathbf{z}}. \quad (48.23)$$

In this manner, vertical mixing of a tracer patch occurs only in the vertical direction (see Figure 48.1).

### 48.2.3 Dianeutral diffusion

Dianeutral diffusion orients tracer fluxes according to the dianeutral direction (48.16)

$$\mathbf{J}_{\text{dia}} = -\rho \kappa_{\text{fine}} (\nabla C \cdot \hat{\gamma}) \hat{\gamma} = -\rho \mathbb{K}_{\text{dia}} \cdot \nabla C, \quad (48.24)$$

---

<sup>4</sup>Dianeutral diffusion is commonly also referred to as *diapycnal diffusion*, with diapycnal diffusion referring to diffusion across constant potential density surfaces. We distinguish dianeutral from diapycnal in this chapter since neutral directions are defined by locally referenced potential density, and as such neutral directions generally differ from isopycnals. Further discussion is provided in Section 24.5 as well as [McDougall \(1987a\)](#).

where the dianeutral diffusion tensor is given by

$$\mathbb{K}_{\text{dia}} = \kappa_{\text{fine}} \begin{bmatrix} \hat{\gamma}_x^2 & \hat{\gamma}_x \hat{\gamma}_y & \hat{\gamma}_x \hat{\gamma}_z \\ \hat{\gamma}_x \hat{\gamma}_y & \hat{\gamma}_y^2 & \hat{\gamma}_y \hat{\gamma}_z \\ \hat{\gamma}_x \hat{\gamma}_z & \hat{\gamma}_y \hat{\gamma}_z & \hat{\gamma}_z^2 \end{bmatrix}. \quad (48.25)$$

Assuming a vertically stable stratification, we can make use of the relation (48.19) to write  $\hat{\gamma}$  in terms of the slope,  $\mathbf{S}$ , thus rendering

$$(\nabla C \cdot \hat{\gamma}) \hat{\gamma} = \frac{(\mathbf{S} - \hat{\mathbf{z}}) \cdot \nabla C}{1 + \mathbf{S}^2} (\mathbf{S} - \hat{\mathbf{z}}) = \frac{1}{1 + \mathbf{S}^2} \begin{bmatrix} S_x^2 & S_x S_y & -S_x \\ S_x S_y & S_y^2 & -S_y \\ -S_x & -S_y & 1 \end{bmatrix} \begin{bmatrix} \partial_x C \\ \partial_y C \\ \partial_z C \end{bmatrix}, \quad (48.26)$$

so that the dianeutral diffusion tensor now takes on the form

$$\mathbb{K}_{\text{dia}} = \frac{\kappa_{\text{fine}}}{1 + \mathbf{S}^2} \begin{bmatrix} S_x^2 & S_x S_y & -S_x \\ S_x S_y & S_y^2 & -S_y \\ -S_x & -S_y & 1 \end{bmatrix}. \quad (48.27)$$

As illustrated in Figure 48.1, dianeutral diffusion elongates a tracer patch in the direction normal to the neutral tangent plane.

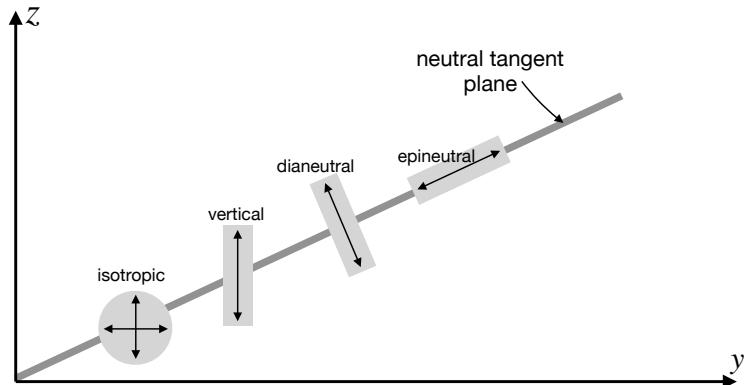


FIGURE 48.1: Illustrating the effects from various forms of diffusion on a tracer patch. When diffused with an isotropic diffusion tensor (equation (48.20)), a spherical patch remains spherical. When diffused with a vertical diffusion tensor (equation (48.22)), a tracer patch elongates in the vertical direction. When diffused with a dianeutral diffusion tensor (equation (48.27)), a tracer patch elongates in the direction normal to the slanted neutral tangent plane. Finally, when diffused with a neutral diffusion tensor, such as the Redi tensor (48.73) or the small slope tensor (48.74), a tracer patch elongates along the neutral tangent plane; i.e., in the *epineutral* direction. This figure is adapted from Figure 4 of [McDougall et al. \(2014\)](#).

## 48.3 Gent-McWilliams stirring

As mentioned in Section 47.6.3, there are two processes that contribute to eddy-induced stirring. One involves the correlations between eddy fluctuations in the velocity and tracer fields. In Section 47.4, we considered the kinematics of correlations induced by small amplitude eddying motions, where we found that the eddy-induced motion of fluid particles leads to both a symmetric (mixing) and anti-symmetric (stirring) dispersion of tracer concentrations. There is currently no method proposed for parameterizing this form of eddy-induced stirring when it arises from subgrid scale processes, thus leaving unanswered its importance to large-scale tracer distributions.

The second process leading to eddy-induced stirring arises from correlations between fluctuations in isopycnal layer thickness and horizontal velocity. As detailed in Section 47.5, this second effect leads to a movement of volume between isopycnal layers, or equivalently we can conceive of it as the quasi-Stokes transport of volume arising from transient eddy motion. This eddy-induced volume stirring in turn affects an eddy-induced tracer stirring within isopycnal layers. Transient mesoscale eddies are the canonical dynamical process leading to this form of stirring. For simulations that do not resolve transient mesoscale eddies, we commonly parameterize the subgrid scale stirring through variants of the [Gent et al. \(1995\)](#) scheme. Various elements of this scheme are detailed in this section.

Most presentations of the [Gent et al. \(1995\)](#) scheme assume a Boussinesq fluid, though with Section 7 of [Griffies and Greatbatch \(2012\)](#) an exception. We here present the non-Boussinesq form, though in places make the Boussinesq approximation since doing so simplifies the presentation without losing anything fundamental.<sup>5</sup>

### 48.3.1 Details of the parameterization

[Gent et al. \(1995\)](#) parameterize the three-dimensional non-divergent eddy-induced mass flux (recall Section 46.6.2) according to

$$\rho \mathbf{v}^* = \nabla \times (\rho \Psi^*) \quad \text{with} \quad \Psi^* = \hat{\mathbf{z}} \times \kappa_{\text{gm}} \mathbf{S}, \quad (48.28)$$

where  $\mathbf{S}$  is the neutral slope given by equation (48.18), and  $\kappa_{\text{gm}} > 0$  is a kinematic diffusivity with dimensions of velocity times a length. Performing the curl on the streamfunction leads to the horizontal and vertical components to the eddy-induced mass flux

$$\rho \mathbf{u}^* = -\partial_z (\kappa_{\text{gm}} \rho \mathbf{S}) \quad \text{and} \quad \rho w^* = \nabla_z \cdot (\kappa_{\text{gm}} \rho \mathbf{S}), \quad (48.29)$$

along with the antisymmetric stirring tensor ([Griffies, 1998](#))

$$\mathbb{A}_{\text{gm}} = \kappa_{\text{gm}} \begin{bmatrix} 0 & 0 & -S_x \\ 0 & 0 & -S_y \\ S_x & S_y & 0 \end{bmatrix}. \quad (48.30)$$

Following the discussion in Section 46.6.3, we can identify the advective tracer flux, skew tracer flux, and rotational tracer flux corresponding to the Gent-McWilliams parameterization

$$\mathbf{J}^{\text{adv}} = \mathbf{J}^{\text{skew}} + \mathbf{J}^{\text{rot}} \quad (48.31)$$

where

$$\mathbf{J}^{\text{adv}} = C \rho \mathbf{v}^* = C \rho [-\partial_z (\kappa_{\text{gm}} \rho \mathbf{S}) + \hat{\mathbf{z}} \nabla_z \cdot (\kappa_{\text{gm}} \rho \mathbf{S})] \quad (48.32a)$$

$$\mathbf{J}^{\text{skew}} = -\nabla C \times \rho \Psi^* = \rho \kappa_{\text{gm}} [\mathbf{S} \partial_z C - \hat{\mathbf{z}} (\mathbf{S} \cdot \nabla C)] \quad (48.32b)$$

$$\mathbf{J}^{\text{rot}} = \nabla \times (\rho C \Psi^*). \quad (48.32c)$$

### 48.3.2 Effects on buoyancy

We now consider a Boussinesq fluid with a linear equation of state in order to focus on the impact of the Gent-McWilliams parameterization on buoyancy, which we measure with potential density,

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<sup>5</sup>In brief, for a Boussinesq fluid, the *in situ* density factor found throughout this section is set to the constant Boussinesq reference density,  $\rho_0$ .

$\varrho$ . In this case the parameterized skew flux of potential density due to the quasi-Stokes transport is given by

$$\rho_0^{-1} \mathbf{J}^{\text{skew}} = -\kappa_{\text{gm}} [\nabla_z \varrho - \hat{\mathbf{z}} \mathbf{S}^2 \partial_z \varrho] = -\kappa_{\text{gm}} [\nabla_z \varrho + \hat{\mathbf{z}} (\rho_0/g) (\mathbf{S} N)^2], \quad (48.33)$$

with the squared neutral slope and squared buoyancy frequency written

$$\mathbf{S}^2 = \mathbf{S} \cdot \mathbf{S} \quad \text{and} \quad N^2 = -\frac{g}{\rho_0} \frac{\partial \varrho}{\partial z}. \quad (48.34)$$

The parameterization yields a horizontal downgradient diffusive flux of potential density along with a vertical upgradient diffusive flux. As illustrated by Figure 48.2, so long as the stratification is stable ( $N^2 > 0$ ), which is assumed by the parameterization, the vertical component to the potential density skew flux is vertically downward, which corresponds to a vertically upward buoyancy skew flux. As we see in Section 48.3.3, this orientation ensures that the parameterization reduces available potential energy. Additionally, [Gent et al. \(1995\)](#) prescribe a diffusivity that vanishes on all boundaries, including the ocean surface. [McIntosh and McDougall \(1996\)](#) and [McDougall and McIntosh \(2001\)](#) present more discussion of vertical boundary conditions, which can be understood by considering the exact form of the quasi-Stokes transport defined by equation (47.101). Finally, we introduce a boundary value problem approach in Section 48.3.7 that also pays particular attention to the boundary conditions.

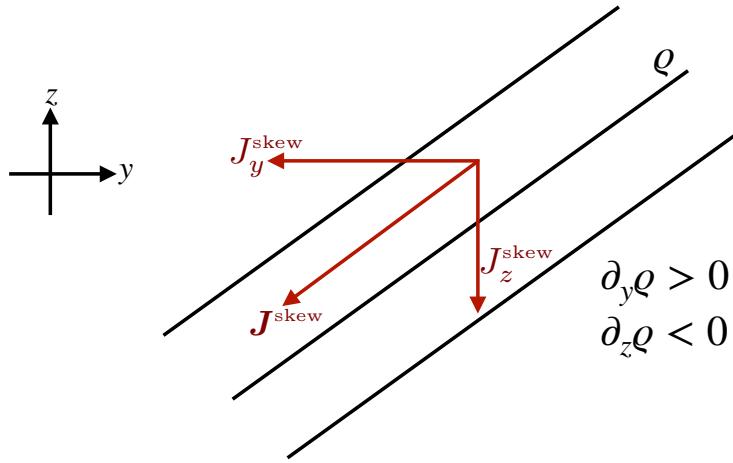


FIGURE 48.2: Orientation of the skew flux of potential density,  $\varrho$ , arising from the [Gent et al. \(1995\)](#) parameterization and as described by [Griffies \(1998\)](#). The sloped black lines are constant  $\varrho$  isosurfaces; i.e., isopycnals. The horizontal skew flux of potential density is downgradient (directed from high density to low density), whereas the vertical skew flux component is upgradient (directed from low density to high density). The net effect is a skew flux that is oriented parallel to isopycnals.

Figure 48.3 brings the elements of the parameterization together by illustrating the *Gent-McWilliams effect* for a meridional potential density front in the southern hemisphere. The mean geostrophic thermal wind flow is eastward, as in the Antarctic Circumpolar Current, whereas a parameterized *secondary circulation* acts to weaken the front. That is, the parameterization assumes that the mean effects from geostrophic eddies, whose kinetic energy is supported by the potential energy in the front, lead to a weakening of the potential density slope so that the front relaxes to the horizontal.

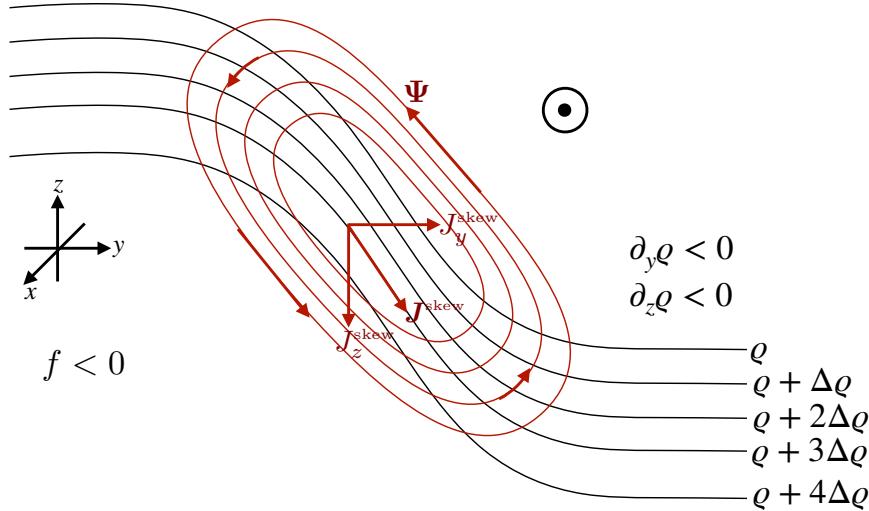


FIGURE 48.3: The Gent-McWilliams effect for a meridional potential density front in the Southern Hemisphere. Dense water rises to the south so that  $\partial_y \varrho < 0$ . The mean geostrophic thermal wind flow is eastward (out of the page), as in the Antarctic Circumpolar Current. With a stable stratification whereby  $\partial_z \varrho < 0$  the Gent-McWilliams streamfunction, equation (48.28), circulates counter-clockwise (red isolines), whereas the Gent-McWilliams skew flux for potential density, given by equation (48.33), has a northward (downgradient) meridional component and downward (upgradient) vertical component (red vectors). The result is a potential density tendency that relaxes the front towards the horizontal thus rendering a zero slope.

#### 48.3.3 Local adiabatic dissipation of available potential energy

We here consider the effects from the [Gent et al. \(1995\)](#) scheme on the available potential energy, continuing to assume a Boussinesq fluid with a linear equation of state. We express the behavior using both skew fluxes and advective fluxes. Since we are assuming the parameterization is adiabatic, the change in potential energy is identical to the change in available potential energy.

##### Skew flux approach

Let us approach the parameterization problem from the perspective of satisfying two general properties: (I) the subgrid scale operator adiabatically stirs while maintaining the same amount of fluid within isopycnal layers, (II) the subgrid operator locally dissipates potential energy through an adiabatic rearrangement of the potential density surfaces, with the dissipation vanishing when there is zero baroclinicity. That is, the scheme dissipates available potential energy. What is the form of the stirring operator implied by these two assumptions?

Adiabatic stirring of potential density can be realized via the convergence of a skew flux oriented parallel to potential density surfaces

$$\rho_0^{-1} \mathbf{J}^{\text{skew}} = -\nabla \varrho \times \Psi^*, \quad (48.35)$$

where at this point we have yet to specify  $\Psi^*$ . To see what the local dissipation of available potential energy imposes, consider the gravitational potential energy of the adiabatic Boussinesq system

$$P = g \int \varrho z \, dV, \quad (48.36)$$

where, again, we assume the *in situ* density equals to the potential density as per a linear equation of state (Section 24.3.5). Assuming all boundaries are material and static allows us to focus on

the time tendency of potential energy associated with the unknown flux

$$\frac{dP}{dt} = g \int z \frac{\partial \varrho}{\partial t} dV = -\frac{g}{\rho_0} \int (z \nabla \cdot \mathbf{J}^{\text{skew}}) dV = -\frac{g}{\rho_0} \int (z \partial_z J^z) dV = \frac{g}{\rho_0} \int J^z dV, \quad (48.37)$$

where  $J^z$  is the vertical flux component. We drop boundary effects by assuming the subgrid scale flux vanishes on all boundaries. To provide a *local* available potential energy sink requires

$$J^z \leq 0, \quad (48.38)$$

where zero occurs when the isopycnals are flat. It is sufficient to construct the vertical flux component using only the potential density field itself. For a stably stratified fluid in which  $\partial_z \varrho < 0$ , the following form provides a local available potential energy sink

$$\rho_0^{-1} J^z = \kappa_{\text{gm}} \mathbf{S}^2 \frac{\partial \varrho}{\partial z} = -(\kappa_{\text{gm}} \rho_0 / g) (\mathbf{S} \mathbf{N})^2 \leq 0. \quad (48.39)$$

The corresponding horizontal flux is given by a downgradient diffusive flux

$$\mathbf{J}^h = -\rho_0 \kappa_{\text{gm}} \nabla_z \varrho. \quad (48.40)$$

We have thus recovered the skew flux (48.33) as proposed by [Gent et al. \(1995\)](#). Note that [Aiki et al. \(2004\)](#) proceed in a similar manner yet do not assume locality of the available potential energy sink, thus deriving a more general subgrid scale operator.

#### Advection flux approach

The impacts on potential energy should be the same when representing the parameterization as an advective flux. To verify this result, return to equation (48.37) and make use of the vertical component of the advective flux rather than the skew flux

$$\frac{dP}{dt} = g \int \varrho w^* dV \quad (48.41a)$$

$$= g \int \varrho \nabla_z \cdot (\kappa_{\text{gm}} \mathbf{S}) dV \quad (48.41b)$$

$$= g \int \nabla_z \cdot (\varrho \kappa_{\text{gm}} \mathbf{S}) dV - g \int \nabla_z \varrho \cdot \kappa_{\text{gm}} \mathbf{S} dV \quad (48.41c)$$

$$= -\rho_0 \int \kappa_{\text{gm}} (\mathbf{S} \mathbf{N})^2 dV, \quad (48.41d)$$

which is the same result as for the skew flux.

#### 48.3.4 Meridional overturning mass transport

It is often of interest to compute the mass transport across a portion of the ocean. In particular, meridional-depth or meridional-potential density streamfunctions allow one to visualize and quantify the zonally integrated transport occurring in a closed basin or over the full globe. The quasi-Stokes transport provides a transport in addition to that from the resolved scale Eulerian mean transport, and the parameterization of [Gent et al. \(1995\)](#) leads to a straightforward computation of the quasi-Stokes contribution. For this purpose, write the net meridional mass transport of fluid across a basin and passing beneath a particular depth in the form (the minus sign is

conventional)

$$\mathcal{T}(y, z, t) = - \int dx \int_{-H}^z \rho(v + v^*) dz \quad (48.42a)$$

$$= - \int dx \int_{-H}^z \rho v dz + \int dx \int_{-H}^z \partial_z(\kappa_{\text{gm}} \rho S_y) dz \quad (48.42b)$$

$$= - \int dx \int_{-H}^z \rho v dz + \int \kappa_{\text{gm}} \rho S_y dx \quad (48.42c)$$

$$\equiv \mathcal{T}^{\text{eulerian}}(y, z, t) + \mathcal{T}^{\text{gm}}(y, z, t). \quad (48.42d)$$

For the penultimate step we set the parameterized quasi-Stokes transport to zero at the ocean bottom. We thus see that the parameterized quasi-Stokes transport adds a contribution that scales linearly with basin size, isopynal slope, and diffusivity,

$$\mathcal{T}^{\text{qs}} \sim \rho_0 L |\mathbf{S}| \kappa_{\text{gm}}. \quad (48.43)$$

As an example, let  $\rho = 1035 \text{ kg m}^{-3}$ ,  $\kappa_{\text{gm}} = 10^3 \text{ m}^2 \text{ s}^{-1}$ ,  $|\mathbf{S}| = 10^{-3}$ , and  $L = 10^7 \text{ m}$ , which yields  $\mathcal{T}^{\text{qs}} \approx 10 \times 10^9 \text{ kg s}^{-1}$ , which represents a nontrivial addition to that from the resolved scale velocity field.

### 48.3.5 Connection to form stress

We now connect the [Gent et al. \(1995\)](#) closure, normally implemented in the tracer equation, to vertical transfer of momentum through form stress. For this purpose we anticipate our general discussion of form stress in Section 19.1 and more detailed discussions in Sections 25.7 and 31.5. In those discussions, we identify form stress as the horizontal pressure force acting on a sloped surface, with our present concern with surfaces of constant isopycnals as discussed in Sections 25.7 and 31.5.

[Young \(2012\)](#) provides a general means for making the connection between [Gent et al. \(1995\)](#) and form stress for a continuously stratified fluid. For our more schematic purposes, we follow the treatment in [Greatbatch and Lamb \(1990\)](#), [Gent et al. \(1995\)](#) (their Section 4), [Ferreira and Marshall \(2006\)](#) (their Section 2), and [Zhao and Vallis \(2008\)](#) (their Section 2.2). For this purpose, assume the fluid is in Boussinesq planetary geostrophic balance (detailed in Section 25.5) whereby the horizontal momentum satisfies

$$\rho_0 f (\hat{z} \times \mathbf{u}) = -\nabla_z p + \partial_z \boldsymbol{\tau}. \quad (48.44)$$

The Coriolis acceleration balances the acceleration from horizontal pressure gradients plus a vertical transfer of horizontal stress. The horizontal stress term is generally quite small in the ocean interior, where the flow is in geostrophic balance, whereas it is large at the ocean surface where it arises from turbulent air-sea interactions; i.e., wind stress. Furthermore, it can be large at the bottom through turbulent bottom stresses.

To make the connection between [Gent et al. \(1995\)](#) and the vertical transfer of horizontal form stress, add  $\rho_0 f (\hat{z} \times \mathbf{u}^*)$  to both sides of equation (48.44) to obtain

$$\rho_0 f (\hat{z} \times \mathbf{u}^\dagger) = -\nabla_z p + \partial_z \boldsymbol{\tau} + \rho_0 f (\hat{z} \times \mathbf{u}^*), \quad (48.45)$$

where  $\mathbf{u}^\dagger = \mathbf{u} + \mathbf{u}^*$  is the horizontal residual mean velocity. This equation says that the Coriolis acceleration from the horizontal residual mean velocity balances pressure gradients, vertical frictional stresses, plus the Coriolis acceleration from the eddy-induced velocity. We further un-

pack the eddy Coriolis acceleration by noting that the planetary geostrophic velocity satisfies the thermal wind relation in the ocean interior (Section 25.5.6), whereby

$$f \partial_z \mathbf{u} = -(g/\rho_0) \hat{\mathbf{z}} \times \nabla \rho = -\hat{\mathbf{z}} \times N^2 \mathbf{S}. \quad (48.46)$$

We can thus write the Coriolis acceleration from the eddy-induced velocity in the form

$$f (\hat{\mathbf{z}} \times \mathbf{u}^*) = -f [\hat{\mathbf{z}} \times \partial_z (\kappa_{\text{gm}} \mathbf{S})] \quad (48.47a)$$

$$= -\partial_z [\hat{\mathbf{z}} \times (f \kappa_{\text{gm}} \mathbf{S})] \quad (48.47b)$$

$$= \frac{\partial}{\partial z} \left[ \frac{\kappa_{\text{gm}} f^2}{N^2} \frac{\partial \mathbf{u}}{\partial z} \right] \quad (48.47c)$$

$$= \frac{\partial}{\partial z} \left[ \nu_e \frac{\partial \mathbf{u}}{\partial z} \right], \quad (48.47d)$$

where the final equality introduced an eddy-induced vertical viscosity

$$\nu_e \equiv \kappa_{\text{gm}} (f^2/N^2). \quad (48.48)$$

Making use of this result in the planetary geostrophic equation (48.45) thus leads to

$$\rho_0 f (\hat{\mathbf{z}} \times \mathbf{u}^\dagger) = -\nabla_z p + \partial_z (\boldsymbol{\tau} + \boldsymbol{\tau}_e), \quad (48.49)$$

where

$$\rho_0^{-1} \boldsymbol{\tau}_e = \nu_e \partial_z \mathbf{u} \quad (48.50)$$

defines a horizontal mesoscale eddy stress arising from the thermal wind shears. Equation (48.49) says that the Coriolis acceleration from the horizontal residual mean velocity is in balance with the horizontal pressure gradient plus the vertical transfer of horizontal shears arising from both friction/wind/bottom drag *plus* a contribution from parameterized mesoscale eddies.

We conclude that the [Gent et al. \(1995\)](#) parameterization appears in the planetary geostrophic residual mean momentum equation as a vertical transport of horizontal stress determined by a viscosity  $\nu_e = \kappa_{\text{gm}} (f/N)^2$ . Notably, this vertical eddy transfer occurs in the absence of irreversible mixing. We thus interpret it as a parameterization of the vertical transfer of pressure form stress via mesoscale eddies that act between isopycnal layers. That is, the [Gent et al. \(1995\)](#) scheme offers a means to parameterize vertical transfer of horizontal form stress arising from undulating mesoscale eddies in the ocean interior. This interpretation is more thoroughly discussed in Section 25.7.

### 48.3.6 Connection to isopycnal thickness diffusion

Recall the ensemble mean thickness equation (47.113) for a Boussinesq fluid was derived in Section 47.5.5

$$\partial_t h + \nabla_\varrho \cdot (h \hat{\mathbf{u}}) = 0, \quad (48.51)$$

where

$$\hat{\mathbf{u}} = \mathbf{u} + \mathbf{u}^{\text{bolus}} \quad (48.52)$$

is the thickness weighted transport velocity affecting evolution of the ensemble mean thickness  $h$ . Note that for brevity we here drop the nomenclature  $(\ )^{(\varrho)}$  used in Section 47.5.5.

Isopycnal correlations of horizontal velocity and layer thickness define the bolus velocity via

$$h \mathbf{u}^{\text{bolus}} = \overline{h' \mathbf{u}'} \quad (48.53)$$

Now consider a downgradient diffusive closure for this correlation

$$\hbar \mathbf{u}^{\text{bolus}} = \overline{\hbar' \mathbf{u}'}^{(\varrho)} = -\mathbb{K}_{\text{thick}} \cdot \nabla_{\varrho} h, \quad (48.54)$$

with  $\mathbb{K}_{\text{thick}}$  a symmetric and positive-definite  $2 \times 2$  diffusion tensor. The mean thickness equation thus takes the form of an advection-diffusion equation in isopycnal coordinates

$$\partial_t h + \nabla_{\varrho} \cdot (\hbar \mathbf{u}) = \nabla_{\varrho} \cdot (\mathbb{K}_{\text{thick}} \cdot \nabla_{\varrho} h). \quad (48.55)$$

To make a connection between the thickness diffusion closure (48.54) and the [Gent et al. \(1995\)](#) closure discussed in Section 48.3.1, note that the specific thickness is the inverse of the vertical derivative of the potential density

$$h = 1/\partial_z \varrho. \quad (48.56)$$

Correspondingly, using the relation between derivative operators,  $\nabla_{\varrho} = \nabla_z + \mathbf{S} \partial_z$ , gives

$$\hbar^{-1} \nabla_{\varrho} h = -\hbar \nabla_{\varrho} (1/\hbar) \quad \text{product rule identity} \quad (48.57a)$$

$$= -(\partial_z \varrho)^{-1} (\nabla_z + \mathbf{S} \partial_z) \partial_z \varrho \quad \hbar = \partial z / \partial \varrho \text{ and } \nabla_{\varrho} = \nabla_z + \mathbf{S} \partial_z \quad (48.57b)$$

$$= -\frac{\partial_z (\nabla_z \varrho)}{\partial_z \varrho} + \frac{\partial_{zz} \varrho \nabla_z \varrho}{(\partial_z \varrho)^2} \quad \text{rearrangement} \quad (48.57c)$$

$$= -\partial_z [\nabla_z \varrho / (\partial_z \varrho)] \quad \text{product rule identity} \quad (48.57d)$$

$$= \partial_z \mathbf{S} \quad \text{isopycnal slope } \mathbf{S} = -\nabla_z \varrho / (\partial_z \varrho). \quad (48.57e)$$

Consequently, the bolus velocity takes the form

$$\mathbf{u}^{\text{bolus}} = -\hbar^{-1} \mathbb{K}_{\text{thick}} \cdot \nabla_{\varrho} h = -\mathbb{K}_{\text{thick}} \cdot \partial_z \mathbf{S}. \quad (48.58)$$

#### *The special case of depth independent diffusivity*

For the special case where  $\mathbb{K}_{\text{thick}}$  is independent of depth and proportional to the  $2 \times 2$  identity matrix, then

$$\mathbf{u}^{\text{bolus}} = -\partial_z (\kappa_{\text{gm}} \mathbf{S}) = \mathbf{u}^*, \quad (48.59)$$

where the horizontal component of the [Gent et al. \(1995\)](#) velocity,  $\mathbf{u}^*$ , was identified from equation (48.29). Again, this identity holds only for the special case of a vertically independent diffusivity tensor proportional to the identity.

#### *Further caveats*

The relevance of a depth-independent diffusivity has been questioned by many authors, such as [Killworth \(1997\)](#), [Treguier et al. \(1997\)](#), [Smith and Vallis \(2002\)](#), [Smith and Marshall \(2009\)](#), and [Abernathay et al. \(2013\)](#). We conclude from these studies that a depth independent diffusivity is not the best choice for the [Gent et al. \(1995\)](#) parameterization, in which case where one places the vertical derivative is crucial.

The relation between thickness diffusion with the [Gent et al. \(1995\)](#) parameterization further breaks down near boundaries. The reason is that the eddy diffusivity vanishes next to boundaries and thus has a depth-dependence. Additionally, as noted by [Holloway \(1997\)](#) and [Griffies et al. \(2000\)](#), thickness diffusion next to solid earth boundaries leads to an increase in potential energy, with isopycnals creeping up the topographic slope. Such unphysical behavior motivates isopycnal modelers instead to use *interfacial height* diffusion to dissipate noise in the thickness field.

### 48.3.7 A parameterization based on a boundary value problem

There have been variants of the [Gent et al. \(1995\)](#) scheme proposed in the literature, such as those of [Aiki et al. \(2004\)](#) and [Ferrari et al. \(2010\)](#). As for the [Gent et al. \(1995\)](#) scheme, these alternatives dissipate available potential energy without mixing between isopycnal classes. We here briefly discuss the scheme of [Ferrari et al. \(2010\)](#), which is used by a variety of ocean climate models largely since it contains a natural means to numerically regularize the eddy-induced streamfunction in regions of weak vertical stratification. These considerations are relevant especially in ocean climate models, where weak or zero vertical stratification is inevitable and so it is necessary to handle such regimes.

For the [Ferrari et al. \(2010\)](#) scheme we write the parameterized eddy streamfunction as

$$\Psi^* = \hat{z} \times \Upsilon \implies \mathbf{u}^* = -\partial_z \Upsilon \quad \text{and} \quad w^* = \nabla_z \cdot \Upsilon, \quad (48.60)$$

with  $\Upsilon$  determined by solving the following vertical boundary value problem at each horizontal position<sup>6</sup>

$$c^2 \frac{d^2 \Upsilon}{dz^2} - N^2 \Upsilon = -N^2 \Upsilon^{\text{gm}} \quad \text{and} \quad \Upsilon(\eta_b) = \Upsilon(\eta) = 0, \quad (48.61)$$

where (see equation (48.28))

$$\Upsilon^{\text{gm}} = \kappa_{\text{gm}} \mathbf{S} \quad \text{and} \quad N^2 \mathbf{S} = (g/\rho_0) \nabla_z \varrho. \quad (48.62)$$

We recover the [Gent et al. \(1995\)](#) scheme when setting the squared speed to zero,  $c^2 = 0$ , in which case  $\Upsilon = \Upsilon^{\text{gm}}$ . For  $c^2 > 0$ , the second order differential operator ensures that  $\Upsilon$  smoothly and continuously transitions through regions where the vertical stratification is weak ( $N^2$  is small), and hence where  $|\mathbf{S}|$  is large. In contrast, the standard regularization approaches, with  $c^2 = 0$ , are somewhat more *ad hoc* (e.g., see Chapter 15 of [Griffies \(2004\)](#)) or rather tedious (e.g., [Ferrari et al. \(2008\)](#)).

Following the discussion in Section 48.3.3, we deduce the impacts on potential energy (assuming a linear equation of state) via equation (48.37), where we make use of the vertical component of the potential density skew flux

$$\frac{1}{g} \frac{dP}{dt} = \frac{1}{\rho_0} \int J^z dV = - \int \hat{z} \cdot (\nabla \varrho \times \Psi^*) dV = - \int \nabla_z \varrho \cdot \Upsilon dV = -\frac{\rho_0}{g} \int N^2 \mathbf{S} \cdot \Upsilon dV. \quad (48.63)$$

The governing differential equation (48.61) leads to

$$\Upsilon \cdot \left[ c^2 \frac{d^2 \Upsilon}{dz^2} - N^2 \Upsilon \right] = -(g/\rho_0) \kappa_{\text{gm}} \Upsilon \cdot \nabla_z \varrho, \quad (48.64)$$

which rearranges to

$$(g/\rho_0) \kappa_{\text{gm}} \Upsilon \cdot \nabla_z \varrho = -c^2 \frac{d(\Upsilon \cdot \Upsilon')}{dz} + c^2 \Upsilon' \cdot \Upsilon' + N^2 \Upsilon \cdot \Upsilon, \quad (48.65)$$

where  $\Upsilon' = d\Upsilon/dz$ . Integrating over a vertical column and making use of the homogeneous Dirichlet boundary conditions from equation (48.61) leads to

$$\frac{g}{\rho_0} \int \kappa_{\text{gm}} \Upsilon \cdot \nabla_z \varrho dz = \int [c^2 \Upsilon' \cdot \Upsilon' + N^2 \Upsilon \cdot \Upsilon] dz \geq 0. \quad (48.66)$$

<sup>6</sup>Note that [Ferrari et al. \(2010\)](#) used the opposite sign convention on  $\Upsilon$  from that used here.

This inequality means that the potential energy of a vertical column is dissipated. However, locally at any point in the column the potential energy might increase due to the sign-indefinite term  $-c^2 d(\mathbf{Y} \cdot \mathbf{Y}')/dz$ . Notably, there is no *a priori* reason that mesoscale eddies dissipate potential energy at every point in space. Furthermore, numerical experiments documented in [Ferrari et al. \(2010\)](#) suggest that local potential energy dissipation is not necessary for a numerically stable operator. We conclude that this approach offers a suitable method for ocean climate simulations.

### 48.3.8 Comments

As noted in Section 47.6.3, there is presently no parameterization of subgrid scale stirring along neutral directions arising from the correlations between tracer and velocity fluctuations. Rather, the only parameterized subgrid scale stirring is associated with quasi-Stokes transport, with [Gent et al. \(1995\)](#) providing the canonical approach as summarized in this section. To parameterize the skew fluxes arising from tracer-velocity correlations requires one to study the polarization of the eddies giving rise to these skew fluxes, as per the discussion in Section 47.4.2 and [Middleton and Loder \(1989\)](#).

## 48.4 Neutral diffusion

*Neutral diffusion*, also referred to as *epineutral diffusion*, parameterizes the mixing induced by mesoscale eddy stirring. The parameterization assumes that the neutral diffusive flux of a tracer is oriented along a neutral direction or a *neutral tangent plane*. The neutral diffusive tracer flux for an arbitrary tracer,  $C$ , is perpendicular to the dianeutral unit vector

$$\mathbf{J} \cdot \hat{\gamma} = 0 \implies \mathbf{J} \cdot (-\alpha \nabla \Theta + \beta \nabla S) = 0, \quad (48.67)$$

where  $\hat{\gamma}$  is defined by equation (48.16).

### 48.4.1 Motivation for neutral diffusion

Pioneering models of the ocean circulation, such as that [Cox and Bryan \(1984\)](#), were formulated with the tracer mixing tensor oriented according to the horizontal and vertical directions. These simulations exhibited problems near strong density fronts, such as those found in western boundary currents, where temperature spuriously mixed across isopyncnals, thus degrading the strength of the front and leading to, among other problems, unphysically weak meridional heat transport ([Böning et al., 1995](#)). In earlier work based on tracer measurements, [Montgomery \(1938\)](#), [Veronis \(1975\)](#), and [Rooth \(1982\)](#) suggested that ocean properties were preferentially homogenized along local potential density surfaces rather than geopotential surfaces. Such measurements motivated [Solomon \(1971\)](#) and [Redi \(1982\)](#) to propose rotating the tracer mixing tensor according to neutral directions.

We offer further indirect evidence that mesoscale eddy induced diffusion is preferentially aligned along neutral directions. For that purpose, consider a diffusive flux is not aligned with neutral directions. In this case, diffusive mixing can cause tracer distributions to cross neutral directions, thus adding to that already parameterized from small scale mixing processes. As discussed in Section 14.1.5 of [Griffies \(2004\)](#) as well as Section 1 of [McDougall et al. \(2014\)](#), the extra mixing induced by this non-neutral orientation of the mesoscale induced diffusive fluxes is proportional to the squared slope between the proposed new direction and the neutral tangent plane. Estimates based on field measurements for interior ocean mixing constrain the magnitude of the tangent to be less than  $10^{-4}$ . This number is very small, indeed it is zero within error bars of field measurements. Although the measurements are sparse, they do support the use of a

neutral diffusion operator oriented so to respect the constraint (49.24). We thus make use of this constraint in designing the diffusion tensor in the remainder of this section.

#### 48.4.2 Redi neutral diffusion

One diffusive flux satisfying the property (48.67) is given by

$$\mathbf{J}_{\text{redi}} = -\rho \kappa_{\text{ntr}} [\nabla C - \hat{\gamma} (\hat{\gamma} \cdot \nabla C)], \quad (48.68)$$

where  $\kappa_{\text{ntr}} > 0$  is the neutral diffusivity (dimensions of squared length per time). We confirm that  $\mathbf{J}_{\text{redi}}$  is oriented down the tracer gradient by noting that

$$\mathbf{J}_{\text{redi}} \cdot \nabla C = -\rho \kappa_{\text{ntr}} [|\nabla C|^2 - (\hat{\gamma} \cdot \nabla C)^2] \leq 0. \quad (48.69)$$

We can write the neutral diffusive flux (48.68) in the downgradient flux-gradient relation

$$\mathbf{J}_{\text{redi}} = -\rho \mathbb{K}_{\text{redi}} \cdot \nabla C, \quad (48.70)$$

with the neutral diffusion tensor,  $\mathbb{K}_{\text{redi}}$ , given by

$$\mathbb{K}_{\text{redi}} = \kappa_{\text{ntr}} \begin{bmatrix} 1 - \hat{\gamma}_x^2 & -\hat{\gamma}_x \hat{\gamma}_y & -\hat{\gamma}_x \hat{\gamma}_z \\ -\hat{\gamma}_x \hat{\gamma}_y & 1 - \hat{\gamma}_y^2 & -\hat{\gamma}_y \hat{\gamma}_z \\ -\hat{\gamma}_x \hat{\gamma}_z & -\hat{\gamma}_y \hat{\gamma}_z & 1 - \hat{\gamma}_z^2 \end{bmatrix} \implies \mathbb{K}_{\text{redi}}^{mn} = \kappa_{\text{ntr}} (\delta^{mn} - \hat{\gamma}^m \hat{\gamma}^n). \quad (48.71)$$

The corresponding neutral diffusion operator is given by the three-dimensional flux convergence

$$\mathcal{R}_{\text{redi}} = -\nabla \cdot \mathbf{J}_{\text{redi}} = \partial_m (\rho \mathbb{K}_{\text{redi}}^{mn} \partial_n C). \quad (48.72)$$

When the neutral surfaces are stably stratified in the vertical, so that their slopes are bounded, then the diffusion tensor takes the following form originally suggested by *Redi* (1982), which is written in terms of the neutral slope

$$\mathbb{K}_{\text{redi}} = \frac{\kappa_{\text{ntr}}}{1 + S^2} \begin{bmatrix} 1 + S_y^2 & -S_x S_y & S_x \\ -S_x S_y & 1 + S_x^2 & S_y \\ S_x & S_y & S^2 \end{bmatrix}. \quad (48.73)$$

#### 48.4.3 Small slope neutral diffusion

Another form of the neutral diffusion flux is based on assuming a small magnitude for the slope of the neutral tangent plane relative to the horizontal, which is the case for most of the ocean interior even in frontal regions. With this approximation, the small slope neutral diffusion tensor takes the form

$$\mathbb{K}_{\text{small}} = \kappa_{\text{ntr}} \begin{bmatrix} 1 & 0 & S_x \\ 0 & 1 & S_y \\ S_x & S_y & S^2 \end{bmatrix}. \quad (48.74)$$

The corresponding small slope neutral diffusive flux is

$$\mathbf{J}_{\text{small}} = -\rho \kappa_{\text{ntr}} [\nabla_{\gamma} + \hat{\mathbf{z}} (\mathbf{S} \cdot \nabla_{\gamma})] C \quad (48.75)$$

where

$$\nabla_{\gamma} = \nabla_z + \mathbf{S} \partial_z \quad (48.76)$$

is the horizontal derivative operator computed on the neutral tangent plane (see equation (41.73)). To show that  $\mathbf{J}_{\text{small}} \cdot \hat{\gamma} = 0$ , we make use of the identity (48.19) so that

$$\mathbf{J}_{\text{small}} \cdot \hat{\gamma} = \frac{\mathbf{J}_{\text{small}} \cdot \mathbf{S} - \mathbf{J}_{\text{small}} \cdot \mathbf{S}}{(1 + \mathbf{S}^2)^{1/2}} = 0. \quad (48.77)$$

Furthermore, we confirm that  $\mathbf{J}_{\text{small}}$  is oriented down the tracer gradient by noting that

$$\mathbf{J}_{\text{small}} \cdot \nabla C = -\rho \kappa_{\text{ntr}} [\nabla_\gamma C \cdot \nabla_z C + (\mathbf{S} \cdot \nabla_\gamma C) \partial_z C] \quad (48.78\text{a})$$

$$= -\rho \kappa_{\text{ntr}} [|\nabla_z C|^2 + 2(\mathbf{S} \cdot \nabla_z C) \partial_z C + |\mathbf{S} \partial_z C|^2] \quad (48.78\text{b})$$

$$= -\rho \kappa_{\text{ntr}} |\nabla_z C + \mathbf{S} \partial_z C|^2 \quad (48.78\text{c})$$

$$= -\rho \kappa_{\text{ntr}} |\nabla_\gamma C|^2 \quad (48.78\text{d})$$

$$\leq 0. \quad (48.78\text{e})$$

The small slope approximation was proposed by [Cox \(1987\)](#). However, his form for the small slope neutral diffusion flux was incorrect as it did not satisfy  $\mathbf{J}_{\text{small}} \cdot \hat{\gamma} = 0$ . The corrected form given by equation (48.75) was first written by [Gent and McWilliams \(1990\)](#). The resulting small slope neutral diffusion operator is commonly used in ocean climate models ([Griffies et al., 1998](#); [Lemarié et al., 2012](#)), which results from computing the three-dimensional convergence

$$\mathcal{R}_{\text{small}} = -\nabla \cdot \mathbf{J}_{\text{small}} = \nabla_z \cdot (\rho \kappa_{\text{ntr}} \nabla_\gamma C) + \partial_z (\rho \kappa_{\text{ntr}} \mathbf{S} \cdot \nabla_\gamma C). \quad (48.79)$$

#### 48.4.4 Neutral tangent plane neutral diffusion

A third method to compute neutral diffusion is motivated by the form of isopycnal diffusion in isopycnal layered models. Rather than isopycnal layers, we work with layers determined locally by neutral tangent planes. The neutral tangent frame makes use of projected non-orthogonal generalized vertical coordinates detailed in Chapter 41.

Following the derivations given in Section 41.15, the neutral diffusive flux in the neutral tangent frame is given by the horizontal flux

$$\mathbf{J}_{\text{ntp}} = -\rho \kappa_{\text{ntr}} \nabla_\gamma C. \quad (48.80)$$

This flux is oriented down the tracer gradient as oriented along neutral directions

$$\mathbf{J}_{\text{ntp}} \cdot \nabla_\gamma C = -\rho \kappa_{\text{ntr}} |\nabla_\gamma C|^2, \quad (48.81)$$

which is the same as equation (48.78d) for the small slope fluxes. However, as a purely horizontal flux,  $\mathbf{J}_{\text{ntp}}$  is not oriented along neutral directions

$$\mathbf{J}_{\text{ntp}} \cdot \hat{\gamma} \neq 0. \quad (48.82)$$

Nevertheless, rather than computing the neutral diffusion operator as a horizontal convergence of this flux, the neutral tangent plane diffusion operator is computed by taking the convergence of  $\mathbf{J}_{\text{ntp}}$  along the neutral tangent plane as per equation (41.92)

$$\mathcal{R}_{\text{ntp}} = -\frac{1}{h^\gamma} [\nabla_\gamma \cdot (h^\gamma \mathbf{J}_{\text{ntp}})] = \frac{1}{h^\gamma} [\nabla_\gamma \cdot (h^\gamma \rho \kappa_{\text{ntr}} \nabla_\gamma C)], \quad (48.83)$$

where

$$h^\gamma = \frac{\partial z}{\partial \gamma} d\gamma = - \left[ \frac{g}{\rho_0 N^2} \right] d\gamma \quad (48.84)$$

measures the thickness of a layer defined by two neutral tangent planes (see equation (41.89)).

As detailed in Section 41.15,  $\mathcal{R}_{\text{ntp}}$  is identical to the small slope neutral diffusion operator (48.79)

$$\mathcal{R}_{\text{ntp}} = \mathcal{R}_{\text{small}}. \quad (48.85)$$

In principle, it is a matter of convenience which form of the operator one uses. However, there are certain issues to consider when implementing these operators in a numerical model. Notably, a discrete realization of  $\mathcal{R}_{\text{ntp}}$  allows for a diagonal downgradient implementation of neutral diffusion, just as isopycnal diffusion in an isopycnal ocean model. In contrast, a discrete realization of either  $\mathcal{R}_{\text{redi}}$  or  $\mathcal{R}_{\text{small}}$  cannot guarantee downgradient fluxes due to the off-diagonal nature of its neutral diffusive flux components ([Griffies et al. \(1998\)](#), [Beckers et al. \(1998\)](#), [Gnanadesikan \(1999\)](#), [Beckers et al. \(2000\)](#) [Lemarié et al. \(2012\)](#), [Shao et al. \(2020\)](#)). As a result, discrete realizations of  $\mathcal{R}_{\text{redi}}$  or  $\mathcal{R}_{\text{small}}$  can produce extrema, which are distinctly not properties of diffusion in the continuum (see Exercise 46.3). Hence, even though the continuum identity holds  $\mathcal{R}_{\text{ntp}} = \mathcal{R}_{\text{small}}$ , there are important differences that arise upon realizing these operators on a discrete lattice. [Shao et al. \(2020\)](#) provide further discussion of these points as part of their numerical realization of neutral diffusion.

#### 48.4.5 Neutrality condition

Given the expression (48.16) for the dianeutral unit vector,  $\hat{\gamma}$ , it is straightforward to show that the neutral diffusive flux for Conservative Temperature and salinity satisfy the constraints

$$\nabla \Theta \cdot [-\alpha \mathbf{J}(\Theta) + \beta \mathbf{J}(S)] = 0 \quad \text{and} \quad \nabla S \cdot [-\alpha \mathbf{J}(\Theta) + \beta \mathbf{J}(S)] = 0. \quad (48.86)$$

These constraints are generally satisfied if the diffusive fluxes satisfy the balance

$$\alpha \mathbf{J}(\Theta) = \beta \mathbf{J}(S) \implies \mathbb{K} \cdot \hat{\gamma} = 0. \quad (48.87)$$

We refer to this balance as the *neutrality condition*. It reflects the vanishing of the neutral diffusive flux of locally referenced potential density. It is maintained by the diffusive flux (48.68) of [Redi \(1982\)](#), the small slope flux (48.75) of [Gent and McWilliams \(1990\)](#), and the neutral tangent frame neutral diffusive flux (48.80). However, it is not maintained by the small slope fluxes from [Cox \(1987\)](#). Furthermore, [Griffies et al. \(1998\)](#) argued for the importance of maintaining this balance to avoid a nonlinear instability plaguing certain numerical realizations of neutral diffusion such as that from [Cox \(1987\)](#).

#### 48.4.6 Symmetry condition

Since the neutral diffusion tensor is symmetric (as are all diffusion tensors as discussed in Section 46.4), we have

$$\mathbf{J}(\Theta) \cdot \nabla S = -\kappa_{\text{ntr}} \rho \mathbb{K}^{mn} \partial_n \Theta \partial_m S \quad (48.88a)$$

$$= -\kappa_{\text{ntr}} \rho \mathbb{K}^{nm} \partial_n S \partial_m \Theta \quad (48.88b)$$

$$= -\kappa_{\text{ntr}} \rho \mathbb{K}^{nm} \partial_n S \partial_m \Theta \quad (48.88c)$$

$$= \mathbf{J}(S) \cdot \nabla \Theta. \quad (48.88d)$$

This symmetry condition holds for both the Redi neutral diffusion tensor and its small slope limit, and it is particularly useful in our discussion of cabbeling and thermobaricity in Section 49.3.

### 48.4.7 GM skewusion plus small slope neutral diffusion

A parameterization of mesoscale eddy stirring and mixing often appears in geopotential coordinate ocean models in the form of GM skewusion (Section 48.3.1) and small slope neutral diffusion (Section 48.4.3). The combined tracer flux takes the form

$$\rho^{-1} \mathbf{J} = -\kappa_{\text{ntr}} \nabla_z C + (\kappa_{\text{gm}} - \kappa_{\text{ntr}}) \mathbf{S} \partial_z C - \hat{\mathbf{z}} [(\kappa_{\text{ntr}} + \kappa_{\text{gm}}) \mathbf{S} \cdot \nabla_z C + \kappa_{\text{ntr}} \mathbf{S}^2 \partial_z C], \quad (48.89)$$

which can be written in terms of a subgrid scale transport tensor ([Griffies, 1998](#))

$$\rho^{-1} \begin{bmatrix} J^x \\ J^y \\ J^z \end{bmatrix} = \begin{bmatrix} \kappa_{\text{ntr}} & 0 & (\kappa_{\text{ntr}} - \kappa_{\text{gm}}) S_x \\ 0 & \kappa_{\text{ntr}} & (\kappa_{\text{ntr}} - \kappa_{\text{gm}}) S_y \\ (\kappa_{\text{ntr}} + \kappa_{\text{gm}}) S_x & (\kappa_{\text{ntr}} + \kappa_{\text{gm}}) S_y & \kappa_{\text{ntr}} \mathbf{S}^2 \end{bmatrix} \begin{bmatrix} \partial_x C \\ \partial_y C \\ \partial_z C \end{bmatrix}. \quad (48.90)$$

In the 1990s and throughout much of the 2000s, it was common to assume that  $\kappa_{\text{ntr}} = \kappa_{\text{gm}}$ , in which case the combined mixing tensor is

$$\mathbb{K}_{\text{small}} + \mathbb{A}_{\text{gm}} = \kappa_{\text{ntr}} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 2 S_x & 2 S_y & \mathbf{S}^2 \end{bmatrix} \quad \text{if } \kappa_{\text{ntr}} = \kappa_{\text{gm}}, \quad (48.91)$$

so that the subgrid scale flux simplifies to

$$\rho^{-1} \mathbf{J} = -\kappa_{\text{ntr}} \nabla_z C - \hat{\mathbf{z}} \kappa_{\text{ntr}} (2 \mathbf{S} \cdot \nabla_z C + \mathbf{S}^2 \partial_z C) \quad \text{if } \kappa_{\text{ntr}} = \kappa_{\text{gm}}. \quad (48.92)$$

Notably, the  $2 \times 2$  horizontal mixing tensor is diagonal. Hence, the horizontal tracer flux is the same as that which arises from downgradient horizontal tracer diffusion. The simplicity of the horizontal flux component was alluring to modelers. It was furthermore argued by [Dukowicz and Smith \(1997\)](#) to be a fundamental property of mesoscale turbulence. However, as emphasized through the works of [Treguier et al. \(1997\)](#), [Ferrari et al. \(2008\)](#), [Danabasoglu et al. \(2008\)](#), and [Ferrari et al. \(2010\)](#), the boundary conditions for neutral diffusion and GM skewusion are distinct, thus breaking their symmetry. Furthermore, studies such as [Smith and Marshall \(2009\)](#) and [Abernathay et al. \(2013\)](#) clearly point to the distinct vertical structure for the two diffusivities. Such distinctions are expected since the skew diffusivity and neutral diffusivity parameterize physically distinct processes: one parameterizes the quasi-Stokes transport and the other parameterizes downgradient diffusion along neutral directions.

### 48.4.8 Generalized vertical coordinates

Thus far we have considered neutral diffusion as realized in geopotential coordinates or using neutral tangent plane coordinates. Here, we detail the steps needed to realize neutral diffusion using the generalized vertical coordinates (GVCs) detailed in Chapters 41 and 42. This formulation is relevant for the now common use of generalized vertical coordinates for ocean modeling as reviewed by [Griffies et al. \(2020\)](#).

We start by recalling the expression (41.91) for a general diffusion operator written in terms of the generalized vertical coordinate,  $\sigma = \sigma(x, y, z, t)$

$$\mathcal{R} = -\frac{1}{h^\sigma} \left[ \nabla_\sigma \cdot (h^\sigma \mathbf{J}^h) + \delta_\sigma (z_\sigma \nabla \sigma \cdot \mathbf{J}) \right], \quad (48.93)$$

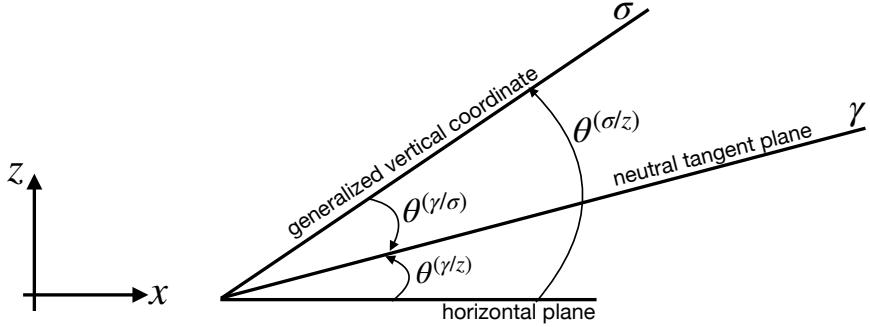


FIGURE 48.4: Slopes of a neutral tangent plane (denoted by  $\gamma$ ) relative to both the horizontal plane,  $\tan \theta^{(\gamma/z)}$ , and relative to a generalized vertical coordinate isoline,  $\tan \theta^{(\gamma/\sigma)}$ , where  $\sigma$  is a generalized vertical coordinate. We assume positive angles as measure counter-clockwise relative to the horizontal and relative to the  $\sigma$ -isoline, respectively. Hence, for this example,  $\theta^{(\gamma/z)} > 0$  yet  $\theta^{(\gamma/\sigma)} < 0$ . When extending to the two horizontal directions, the slopes generally satisfy  $\mathbf{S}^{(\sigma/z)} = \mathbf{S}^{(\gamma/z)} - \mathbf{S}^{(\gamma/\sigma)}$ , where  $|\mathbf{S}^{(\gamma/z)}| = |\tan \theta^{(\gamma/z)}|$  and  $|\mathbf{S}^{(\gamma/\sigma)}| = |\tan \theta^{(\gamma/\sigma)}|$ . Note that this relation between slope vectors also holds for arbitrary orientations of the  $\sigma$  isolines and neutral tangent planes.

where  $\delta_\sigma \equiv d\sigma / \partial_\sigma$  is the dimensionless derivative operator, and the thickness of a  $\sigma$ -layer is

$$h^\sigma = dz = z_\sigma d\sigma = \frac{\partial z}{\partial \sigma} d\sigma. \quad (48.94)$$

Now assume the flux,  $\mathbf{J}$ , is given by equation (48.75) for small slope neutral diffusion. Transforming to GVCs leads to the horizontal flux component

$$\mathbf{J}_{\text{small}}^h = -\rho \kappa_{\text{ntr}} \nabla_\gamma C \quad (48.95a)$$

$$= -\rho \kappa_{\text{ntr}} [\nabla_z + (\nabla_\gamma z) \partial_z] C \quad (48.95b)$$

$$= -\rho \kappa_{\text{ntr}} [\nabla_\sigma + (-\nabla_\sigma z + \nabla_\gamma z) \partial_z] C \quad (48.95c)$$

$$= -\rho \kappa_{\text{ntr}} [\nabla_\sigma + (-\mathbf{S}^{(\sigma/z)} + \mathbf{S}^{(\gamma/z)}) \partial_z] C \quad (48.95d)$$

$$= -\rho \kappa_{\text{ntr}} (\nabla_\sigma + \mathbf{S}^{(\gamma/\sigma)} \partial_z) C, \quad (48.95e)$$

where the neutral slopes as shown in Figure 48.4 satisfy the identity

$$\mathbf{S}^{(\sigma/z)} = \mathbf{S}^{(\gamma/z)} - \mathbf{S}^{(\gamma/\sigma)}. \quad (48.96)$$

Furthermore, we made use of the identity (41.73) relating the partial derivative operators

$$\nabla_\gamma = \nabla_z + (\nabla_\gamma z) \partial_z \quad \text{and} \quad \nabla_z = \nabla_\sigma - (\nabla_\sigma z) \partial_z. \quad (48.97)$$

The horizontal flux (48.95e) has the same form as when written using geopotential coordinates, only now with the derivative operator  $\nabla_\sigma$  and the slope  $\mathbf{S}^{(\gamma/\sigma)}$ . Correspondingly, the vertical flux component

$$J_{\text{small}}^z = \mathbf{J}_{\text{small}}^h \cdot \mathbf{S}^{(\gamma/z)} \quad (48.98)$$

takes the form

$$z_\sigma \nabla_\sigma \cdot \mathbf{J}_{\text{small}} = -\mathbf{S}^{(\sigma/z)} \cdot \mathbf{J}_{\text{small}}^h + J_{\text{small}}^z = \mathbf{J}_{\text{small}}^h \cdot \mathbf{S}^{(\gamma/\sigma)}, \quad (48.99)$$

which in turn yields the diffusion operator (48.93)

$$\mathcal{R} = -\frac{1}{h^\sigma} [\nabla_\sigma \cdot (h^\sigma \mathbf{J}_{\text{small}}^h) + \delta_\sigma (\mathbf{J}_{\text{small}}^h \cdot \mathbf{S}^{(\gamma/\sigma)})]. \quad (48.100)$$

In the special case when  $\sigma$  is parallel to the neutral direction so that  $\mathbf{S}^{(\gamma/\sigma)} = 0$ , the diffusion operator (48.100) reduces to the neutral tangent plane version given by equation (48.83).

## 48.5 Anisotropic neutral diffusion

The neutral diffusion discussed in Section 48.4 is based on isotropic diffusion in the neutral tangent plane. That assumption has been questioned by [Smith and Gent \(2004\)](#) and [Fox-Kemper et al. \(2013\)](#). We here develop some of the formalism appropriate for studying anisotropic neutral diffusion.

### 48.5.1 Orthonormal triad of basis vectors

We make use of the following orthonormal unit vectors<sup>7</sup> as depicted in Figure 48.5

$$\hat{\mathbf{e}}_{\bar{1}} = \frac{\hat{\mathbf{d}} \times \hat{\gamma}}{|\hat{\mathbf{d}} \times \hat{\gamma}|} \quad (48.101a)$$

$$\hat{\mathbf{e}}_{\bar{2}} = \frac{\hat{\gamma} \times (\hat{\mathbf{d}} \times \hat{\gamma})}{|\hat{\mathbf{d}} \times \hat{\gamma}|} = \frac{\hat{\mathbf{d}} - (\hat{\gamma} \cdot \hat{\mathbf{d}}) \hat{\gamma}}{|\hat{\mathbf{d}} \times \hat{\gamma}|} \quad (48.101b)$$

$$\hat{\mathbf{e}}_{\bar{3}} = \hat{\gamma} \quad (48.101c)$$

where

$$\hat{\mathbf{d}} = \hat{\mathbf{x}} \hat{d}_x + \hat{\mathbf{y}} \hat{d}_y + \hat{\mathbf{z}} \hat{d}_z \quad (48.102)$$

is an arbitrary unit vector that is not parallel to  $\hat{\gamma}$ . The three unit vectors  $(\hat{\mathbf{e}}_{\bar{1}}, \hat{\mathbf{e}}_{\bar{2}}, \hat{\mathbf{e}}_{\bar{3}})$  form an orthonormal triad at each point in the fluid so that

$$\hat{\mathbf{e}}_{\bar{1}} = \hat{\mathbf{e}}_{\bar{2}} \times \hat{\mathbf{e}}_{\bar{3}} \quad \text{and} \quad \hat{\mathbf{e}}_{\bar{2}} = \hat{\mathbf{e}}_{\bar{3}} \times \hat{\mathbf{e}}_{\bar{1}} \quad \text{and} \quad \hat{\mathbf{e}}_{\bar{3}} = \hat{\mathbf{e}}_{\bar{1}} \times \hat{\mathbf{e}}_{\bar{2}}. \quad (48.103)$$

These vectors are oriented by the arbitrary direction,  $\hat{\mathbf{d}}$ , and the dianeutral direction,  $\hat{\gamma}$ . We verify that  $\hat{\mathbf{e}}_{\bar{2}}$  has unit magnitude by noting that

$$|\hat{\mathbf{d}} \times \hat{\gamma}|^2 = |\hat{\gamma} \times (\hat{\mathbf{d}} \times \hat{\gamma})|^2 = 1 - (\hat{\mathbf{d}} \cdot \hat{\gamma})^2. \quad (48.104)$$

It is also useful to verify that  $\hat{\mathbf{e}}_{\bar{3}} = \hat{\mathbf{e}}_{\bar{1}} \times \hat{\mathbf{e}}_{\bar{2}}$  through the following vector identity (see equation (1.40b))

$$(\hat{\mathbf{d}} \times \hat{\gamma}) \times [\hat{\gamma} \times (\hat{\mathbf{d}} \times \hat{\gamma})] = \hat{\gamma} |\hat{\mathbf{d}} \times \hat{\gamma}|^2. \quad (48.105)$$

The unit vectors  $\hat{\mathbf{e}}_{\bar{1}}$  and  $\hat{\mathbf{e}}_{\bar{2}}$  are both within the neutral tangent plane since they are both orthogonal to  $\hat{\gamma}$ .

The unit vector  $\hat{\mathbf{e}}_{\bar{1}}$  is orthogonal to  $\hat{\mathbf{d}}$  whereas  $\hat{\mathbf{e}}_{\bar{2}}$  is parallel to  $\hat{\mathbf{d}}$  if  $\hat{\mathbf{d}} \cdot \hat{\gamma} = 0$ . For example, [Smith and Gent \(2004\)](#) proposed setting  $\hat{\mathbf{d}}$  to be a horizontal vector set according to the local horizontal flow direction, in which case

$$\hat{\mathbf{d}} = \frac{u \hat{\mathbf{x}} + v \hat{\mathbf{y}}}{(u^2 + v^2)^{1/2}}. \quad (48.106)$$

With  $\hat{\gamma}$  nearly vertical for much of the ocean interior, then  $\hat{\mathbf{e}}_{\bar{2}}$  becomes nearly aligned with  $\hat{\mathbf{d}}$ . For

<sup>7</sup>The basis vectors (48.101a)-(48.101c) are more suitable for present purposes than the analogous basis vectors defined by equations (14.4)-(14.6) in [Griffies \(2004\)](#). In particular, the basis (48.101a)-(48.101c) has a sensible limit when the neutral slopes are horizontal, in which  $\hat{\gamma} = -\hat{\mathbf{z}}$ .

these reasons we refer to  $\hat{e}_{\bar{1}}$  as the across- $\hat{d}$  direction and  $\hat{e}_{\bar{2}}$  as the along- $\hat{d}$  direction.

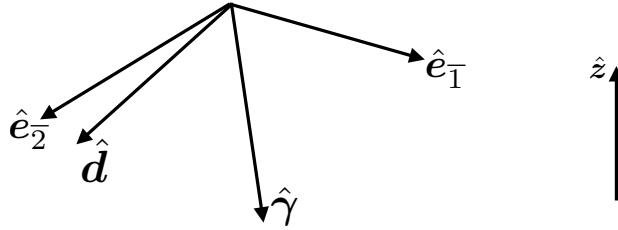


FIGURE 48.5: Depicting the orthonormal triad of basis vectors given by equations (48.101a)-(48.101c). Our convention is such that  $\hat{\gamma}$  typically points downward toward increasing density. The unit vector  $\hat{d}$  is arbitrary so long as it is not parallel to the dianeutral unit vector,  $\hat{\gamma}$ . It is horizontal when making use of the [Smith and Gent \(2004\)](#) proposal whereby  $\hat{d} = \mathbf{u}/|\mathbf{u}|$ , with  $\mathbf{u} = \hat{x} u + \hat{y} v$  the horizontal velocity vector. Since  $\hat{e}_{\bar{1}}$  is orthogonal to  $\hat{d}$ , we refer to  $\hat{e}_{\bar{1}}$  as the cross- $\hat{d}$  basis vector. Likewise, since  $\hat{e}_{\bar{2}}$  is nearly parallel to  $\hat{d}$ , especially when  $\hat{d}$  is close to horizontal and  $\hat{\gamma}$  is close to vertical (e.g., Section 48.5.4), then  $\hat{e}_{\bar{2}}$  is referred to as the along- $\hat{d}$  basis vector.

### 48.5.2 Anisotropic neutral diffusion tensor

We consider anisotropy according to the unit vectors  $\hat{e}_{\bar{1}}$  and  $\hat{e}_{\bar{2}}$ . Hence, the diffusion tensor as represented using the locally orthogonal triad  $(\hat{e}_{\bar{1}}, \hat{e}_{\bar{2}}, \hat{e}_{\bar{3}})$  is given by

$$\bar{\mathbb{K}}_{\text{aniso}} = \begin{bmatrix} \kappa_{\text{cross}} & 0 & 0 \\ 0 & \kappa_{\text{along}} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad (48.107)$$

where  $\kappa_{\text{cross}} > 0$  and  $\kappa_{\text{along}} > 0$  are the generally distinct neutral diffusivities. This tensor takes on the component form

$$\bar{\mathbb{K}}_{\text{aniso}}^{\bar{m}\bar{n}} = \kappa_{\text{cross}} \hat{e}_{\bar{1}}^{\bar{m}} \hat{e}_{\bar{1}}^{\bar{n}} + \kappa_{\text{along}} \hat{e}_{\bar{2}}^{\bar{m}} \hat{e}_{\bar{2}}^{\bar{n}} \quad (48.108a)$$

$$= \kappa_{\text{cross}} (\delta^{\bar{m}\bar{n}} - \hat{e}_{\bar{2}}^{\bar{m}} \hat{e}_{\bar{2}}^{\bar{n}} - \hat{e}_{\bar{3}}^{\bar{m}} \hat{e}_{\bar{3}}^{\bar{n}}) + \kappa_{\text{along}} (\delta^{\bar{m}\bar{n}} - \hat{e}_{\bar{1}}^{\bar{m}} \hat{e}_{\bar{1}}^{\bar{n}} - \hat{e}_{\bar{3}}^{\bar{m}} \hat{e}_{\bar{3}}^{\bar{n}}), \quad (48.108b)$$

where the second expression made use of the following decomposition of the unit tensor in terms of the orthonormal basis vectors

$$\delta^{\bar{m}\bar{n}} = \hat{e}_{\bar{1}}^{\bar{m}} \hat{e}_{\bar{1}}^{\bar{n}} + \hat{e}_{\bar{2}}^{\bar{m}} \hat{e}_{\bar{2}}^{\bar{n}} + \hat{e}_{\bar{3}}^{\bar{m}} \hat{e}_{\bar{3}}^{\bar{n}}. \quad (48.109)$$

Note that  $\bar{\mathbb{K}}_{\text{aniso}}^{\bar{m}\bar{n}}$  is invariant under  $\hat{d} \rightarrow -\hat{d}$ . Likewise, it is invariant under a change in the sign of  $\hat{\gamma}$ . Furthermore, note that we recover the isotropic Redi diffusion tensor (48.71) by setting  $\kappa_{\text{cross}} = \kappa_{\text{along}} = \kappa_{\text{ntr}}$  and in which case

$$\bar{\mathbb{K}}_{\text{aniso}}^{\bar{m}\bar{n}} = 2\kappa_{\text{ntr}} (\delta^{\bar{m}\bar{n}} - \hat{e}_{\bar{3}}^{\bar{m}} \hat{e}_{\bar{3}}^{\bar{n}}) - \kappa_{\text{ntr}} (\hat{e}_{\bar{1}}^{\bar{m}} \hat{e}_{\bar{1}}^{\bar{n}} + \hat{e}_{\bar{2}}^{\bar{m}} \hat{e}_{\bar{2}}^{\bar{n}}) \quad (48.110a)$$

$$= \kappa_{\text{ntr}} (\delta^{\bar{m}\bar{n}} - \hat{e}_{\bar{3}}^{\bar{m}} \hat{e}_{\bar{3}}^{\bar{n}}) \quad (48.110b)$$

$$= \bar{\mathbb{K}}_{\text{redi}}^{\bar{m}\bar{n}}. \quad (48.110c)$$

To render a geopotential-Cartesian representation of the anisotropic diffusion tensor, we can make use of the transformation methods for Cartesian tensors developed in Section 1.7. We do so by transforming from the locally orthogonal neutral plane coordinate system, defined by the orthonormal triad (48.101a)-(48.101c), to the geopotential-Cartesian coordinate system, defined by the Cartesian triad

$$\hat{e}_1 = \hat{x} \quad \text{and} \quad \hat{e}_2 = \hat{y} \quad \text{and} \quad \hat{e}_3 = \hat{z}. \quad (48.111)$$

Since we are working with Cartesian tensors, this transformation is a local rotation matrix,  $\mathcal{R}$ , so that<sup>8</sup>

$$\mathbb{K}_{\text{aniso}}^{mn} = \mathcal{R}_{\bar{m}}^m \mathcal{R}_{\bar{n}}^n \mathbb{K}_{\text{aniso}}^{\bar{m}\bar{n}} \implies \mathbb{K}_{\text{aniso}} = \mathcal{R} \bar{\mathbb{K}}_{\text{aniso}} \mathcal{R}^T, \quad (48.112)$$

where the second equality made use of matrix notation with  $\mathcal{R}^T$  the transpose, and where the elements to the rotation matrix are given by the direction cosines following equation (1.53)

$$\mathcal{R} = \begin{bmatrix} \hat{e}^1 \cdot \hat{e}_{\bar{1}} & \hat{e}^1 \cdot \hat{e}_{\bar{2}} & \hat{e}^1 \cdot \hat{e}_{\bar{3}} \\ \hat{e}^2 \cdot \hat{e}_{\bar{1}} & \hat{e}^2 \cdot \hat{e}_{\bar{2}} & \hat{e}^2 \cdot \hat{e}_{\bar{3}} \\ \hat{e}^3 \cdot \hat{e}_{\bar{1}} & \hat{e}^3 \cdot \hat{e}_{\bar{2}} & \hat{e}^3 \cdot \hat{e}_{\bar{3}} \end{bmatrix} = \begin{bmatrix} \hat{x} \cdot \hat{e}_{\bar{1}} & \hat{x} \cdot \hat{e}_{\bar{2}} & \hat{x} \cdot \hat{e}_{\bar{3}} \\ \hat{y} \cdot \hat{e}_{\bar{1}} & \hat{y} \cdot \hat{e}_{\bar{2}} & \hat{y} \cdot \hat{e}_{\bar{3}} \\ \hat{z} \cdot \hat{e}_{\bar{1}} & \hat{z} \cdot \hat{e}_{\bar{2}} & \hat{z} \cdot \hat{e}_{\bar{3}} \end{bmatrix}. \quad (48.113)$$

The machinery outlined here for the transformation is straightforward but tedious (i.e., two matrix multiplies). A more streamlined approach, also used for determining the Cartesian components to the Redi tensor (48.73), is to simply express  $(\hat{e}_{\bar{1}}, \hat{e}_{\bar{2}}, \hat{e}_{\bar{3}})$  using geopotential-Cartesian coordinates and then plug directly into equation (48.108b).

### 48.5.3 Properties of the anisotropic neutral diffusive fluxes

We here verify some standard properties for the anisotropic neutral diffusive flux for tracers

$$\mathbf{J}_{\text{aniso}} = -\rho \mathbb{K}_{\text{aniso}} \cdot \nabla C. \quad (48.114)$$

*Downgradient orientation within the neutral tangent plane*

By construction, the flux is downgradient along the two orthogonal directions,  $\hat{e}_{\bar{1}}$  and  $\hat{e}_{\bar{2}}$ ,

$$\mathbf{J}_{\text{aniso}} = -\rho \kappa_{\text{cross}} \hat{e}_{\bar{1}} (\hat{e}_{\bar{1}} \cdot \nabla C) - \rho \kappa_{\text{along}} \hat{e}_{\bar{2}} (\hat{e}_{\bar{2}} \cdot \nabla C). \quad (48.115)$$

Furthermore, the flux is within the neutral tangent plane

$$\mathbf{J}_{\text{aniso}} \cdot \hat{\gamma} = 0 \quad (48.116)$$

due to orthogonality between the basis vectors

$$\hat{e}_{\bar{1}} \cdot \hat{\gamma} = \hat{e}_{\bar{2}} \cdot \hat{\gamma} = 0. \quad (48.117)$$

*Neutrality condition*

The neutrality condition (48.87) follows since

$$(-\alpha \nabla \Theta + \beta \nabla S) \cdot \hat{e}_{\bar{1}} = (-\alpha \nabla \Theta + \beta \nabla S) \cdot \hat{e}_{\bar{2}} = 0, \quad (48.118)$$

so that

$$\alpha \mathbf{J}_{\text{aniso}}(\Theta) = \beta \mathbf{J}_{\text{aniso}}(S). \quad (48.119)$$

### 48.5.4 Small slope anisotropic neutral diffusion

We now consider the special case in which the orientation direction,  $\hat{d}$ , is strictly horizontal and normalized so that

$$\hat{d} \cdot \hat{d} = \hat{d}_x^2 + \hat{d}_y^2 = 1. \quad (48.120)$$

<sup>8</sup>Since we are dealing with Cartesian tensors there is no distinction between raised or lowered tensor indices in equation (48.112). We choose to follow the convention of general tensors in Chapters 6 and 7 simply to help organize elements of the tensor.

Additionally, we assume the neutral slope is small so that the neutral directions are nearly horizontal. In this case the basis vectors (48.101a)-(48.101c) take on the following form valid to  $\mathcal{O}(|\mathbf{S}|)$

$$\hat{\mathbf{e}}_{\bar{1}\text{small}} = \hat{\mathbf{d}} \times (\mathbf{S} - \hat{\mathbf{z}}) \quad (48.121\text{a})$$

$$\hat{\mathbf{e}}_{\bar{2}\text{small}} = \hat{\mathbf{d}} + \hat{\mathbf{z}} (\hat{\mathbf{d}} \cdot \mathbf{S}) \quad (48.121\text{b})$$

$$\hat{\mathbf{e}}_{\bar{3}\text{small}} = \mathbf{S} - \hat{\mathbf{z}}. \quad (48.121\text{c})$$

Note that  $\hat{\mathbf{e}}_{\bar{3}\text{small}}$  is orthogonal to  $\hat{\mathbf{e}}_{\bar{1}\text{small}}$  and  $\hat{\mathbf{e}}_{\bar{2}\text{small}}$ , however  $\hat{\mathbf{e}}_{\bar{1}\text{small}} \cdot \hat{\mathbf{e}}_{\bar{2}\text{small}}$  is  $\mathcal{O}(\mathbf{S} \cdot \mathbf{S})$ . Likewise, each of these vectors is normalized only to  $\mathcal{O}(\mathbf{S} \cdot \mathbf{S})$ .

Making use of the small slope basis vectors in the anisotropic diffusion tensor (48.108a), and expressing them in geopotential-Cartesian coordinates leads to the small slope anisotropic neutral diffusion tensor<sup>9</sup>

$$\mathbb{K}_{\text{small aniso}} = \kappa_{\text{cross}} \begin{bmatrix} 1 & 0 & S_x \\ 0 & 1 & S_y \\ S_x & S_y & \mathbf{S} \cdot \mathbf{S} \end{bmatrix} + \Delta\kappa_{\text{ntr}} \begin{bmatrix} \hat{d}_x^2 & \hat{d}_x \hat{d}_y & (\hat{\mathbf{d}} \cdot \mathbf{S}) \hat{d}_x \\ \hat{d}_x \hat{d}_y & \hat{d}_y^2 & (\hat{\mathbf{d}} \cdot \mathbf{S}) \hat{d}_y \\ (\hat{\mathbf{d}} \cdot \mathbf{S}) \hat{d}_x & (\hat{\mathbf{d}} \cdot \mathbf{S}) \hat{d}_y & (\hat{\mathbf{d}} \cdot \mathbf{S})^2 \end{bmatrix}, \quad (48.122)$$

where

$$\Delta\kappa_{\text{ntr}} = \kappa_{\text{along}} - \kappa_{\text{cross}}. \quad (48.123)$$

As for the unapproximated anisotropic neutral diffusion tensor (48.108a), its small slope version,  $\bar{\mathbb{K}}_{\text{small aniso}}$ , is invariant if we swap the direction  $\hat{\mathbf{d}} \rightarrow -\hat{\mathbf{d}}$ . Furthermore, in the form (48.122) we trivially see that  $\bar{\mathbb{K}}_{\text{small aniso}} = \bar{\mathbb{K}}_{\text{small}}$  (equation (48.74)) in the isotropic limit where  $\kappa_{\text{cross}} = \kappa_{\text{along}} = \kappa_{\text{ntr}}$ .

The anisotropic small slope neutral diffusive flux is given by

$$\mathbf{J}_{\text{small aniso}} = -\rho \mathbb{K}_{\text{small aniso}} \cdot \nabla C, \quad (48.124)$$

with horizontal and vertical components

$$\mathbf{J}_{\text{small aniso}}^h = -\rho \kappa_{\text{cross}} \nabla_\gamma C - \rho \Delta\kappa_{\text{ntr}} \hat{\mathbf{d}} (\hat{\mathbf{d}} \cdot \nabla_\gamma) C \quad (48.125\text{a})$$

$$J_{\text{small aniso}}^z = \mathbf{S} \cdot \mathbf{J}_{\text{small aniso}}^h, \quad (48.125\text{b})$$

where  $\nabla_\gamma = \nabla_z + \mathbf{S} \partial_z$  is the horizontal operator as per equation (48.76). By making use of the expression (48.19),  $\hat{\gamma} = (\mathbf{S} - \hat{\mathbf{z}})(1 + \mathbf{S}^2)^{-1/2}$ , we readily find that

$$\mathbf{J}_{\text{small aniso}} \cdot \hat{\gamma} = 0. \quad (48.126)$$

Similarly, we can verify that the neutrality condition (Section 48.4.5) is maintained

$$\mathbb{K}_{\text{small aniso}} \cdot \hat{\gamma} = 0 \implies \alpha \mathbf{J}_{\text{small aniso}}(\Theta) = \beta \mathbf{J}_{\text{small aniso}}(S). \quad (48.127)$$

Finally, as per the discussion in Section 48.4.4, we can evaluate the small slope anisotropic neutral diffusion operator by following the non-orthogonal neutral tangent approach rather than the three-dimensional Cartesian approach. It is the non-orthogonal neutral tangent approach that is appropriate for vertical Lagrangian ocean models such as detailed in [Griffies et al. \(2020\)](#) and [Shao et al. \(2020\)](#).

---

<sup>9</sup>Equation (48.122) agrees with equations (10) and (14) from [Smith and Gent \(2004\)](#).

## 48.6 Anisotropic Gent-McWilliams stirring

In addition to proposing the use of a small slope anisotropic neutral diffusion tensor (equation (48.122)), *Smith and Gent* (2004) proposed a complementary anisotropic version of the Gent-McWilliams stirring. We here detail the parameterization, again assuming the orientation direction,  $\hat{\mathbf{d}}$ , is horizontal

$$\hat{\mathbf{d}} = \hat{\mathbf{x}} \hat{d}_x + \hat{\mathbf{y}} \hat{d}_y, \quad (48.128)$$

just as assumed when discussing the anisotropic small slope neutral diffusion operator in Section 48.5.4.

### 48.6.1 Streamfunction and anti-symmetric tensor

The parameterized eddy-induced streamfunction is generalized from that in equation (48.28) to read

$$\Psi^* = \hat{\mathbf{z}} \times \kappa_{\text{gm-cross}} \mathbf{S} + \hat{\mathbf{z}} \times (\kappa_{\text{gm-cross}} - \kappa_{\text{gm-along}}) (\hat{\mathbf{d}} \cdot \mathbf{S}) \hat{\mathbf{d}}, \quad (48.129)$$

and the corresponding anti-symmetric stirring tensor is

$$\mathbb{A}_{\text{gm-aniso}} = \kappa_{\text{gm-cross}} \begin{bmatrix} 0 & 0 & -S_x \\ 0 & 0 & -S_y \\ S_x & S_y & 0 \end{bmatrix} + \Delta \kappa_{\text{gm}} (\hat{\mathbf{d}} \cdot \mathbf{S}) \begin{bmatrix} 0 & 0 & -\hat{d}_x \\ 0 & 0 & -\hat{d}_y \\ \hat{d}_x & \hat{d}_y & 0 \end{bmatrix}, \quad (48.130)$$

where

$$\Delta \kappa_{\text{gm}} = \kappa_{\text{gm-along}} - \kappa_{\text{gm-cross}}. \quad (48.131)$$

As for the small slope anisotropic neutral diffusion tensor (48.122), we write the skew tensor  $\mathbb{A}_{\text{gm-aniso}}$  in equation (48.130) in a form that manifestly reduces to the isotropic Gent-McWilliams stirring tensor  $\mathbb{A}_{\text{gm}}$  when  $\kappa_{\text{gm-along}} = \kappa_{\text{gm-cross}} = \kappa_{\text{gm}}$ .

### 48.6.2 Anisotropic Gent-McWilliams skew tracer flux

The anisotropic Gent-McWilliams skew tracer flux is

$$\mathbf{J}_{\text{gm-aniso}} = -\rho \mathbb{A}_{\text{gm-aniso}} \cdot \nabla C \quad (48.132a)$$

$$= \rho \kappa_{\text{gm-cross}} [\mathbf{S} \partial_z C - \hat{\mathbf{z}} (\mathbf{S} \cdot \nabla_z C)] + \rho \Delta \kappa_{\text{gm}} (\hat{\mathbf{d}} \cdot \mathbf{S}) [\hat{\mathbf{d}} \partial_z C - \hat{\mathbf{z}} (\hat{\mathbf{d}} \cdot \nabla_z C)]. \quad (48.132b)$$

When acting on locally referenced potential density,  $C = \gamma$ , the flux reduces to

$$\mathbf{J}_{\text{gm-aniso}} = \rho \kappa_{\text{gm-cross}} [-\nabla_z \gamma + \hat{\mathbf{z}} \mathbf{S}^2 \partial_z \gamma] + \rho \Delta \kappa_{\text{gm}} (\hat{\mathbf{d}} \cdot \mathbf{S}) [\hat{\mathbf{d}} + \hat{\mathbf{z}} (\hat{\mathbf{d}} \cdot \mathbf{S})] \partial_z \gamma. \quad (48.133)$$

As discussed in Section 48.3.3, a negative vertical component to the potential density skew flux ensures that the available potential energy is dissipated,

$$\hat{\mathbf{z}} \cdot \mathbf{J}_{\text{gm-aniso}} = \rho [\kappa_{\text{gm-cross}} \mathbf{S}^2 + \Delta \kappa_{\text{gm}} (\hat{\mathbf{d}} \cdot \mathbf{S})^2] \partial_z \gamma < 0 \implies \text{APE dissipated}. \quad (48.134)$$

Stably stratified water means that  $\partial_z \gamma < 0$ , in which case  $\hat{\mathbf{z}} \cdot \mathbf{J}_{\text{gm-aniso}} < 0$  since

$$\kappa_{\text{gm-cross}} \mathbf{S}^2 + \Delta \kappa_{\text{gm}} (\hat{\mathbf{d}} \cdot \mathbf{S})^2 = \kappa_{\text{gm-cross}} [\mathbf{S}^2 - (\hat{\mathbf{d}} \cdot \mathbf{S})^2] + \kappa_{\text{gm-along}} (\hat{\mathbf{d}} \cdot \mathbf{S})^2 > 0. \quad (48.135)$$

### 48.6.3 Anisotropic GM skewion plus small slope neutral diffusion

As noted in Section 48.4.7, there are strong reasons to keep the Gent-McWilliams skew flux parameterization distinct from the neutral diffusion parameterization. The central practical reason for the distinction concerns their different treatment of boundary conditions and generally distinct diffusivities. Even so, we here briefly comment on the special case where we ignore these distinctions and set the skew flux and neutral diffusivities the same

$$\kappa_{\text{gm-cross}} = \kappa_{\text{cross}} \quad \text{and} \quad \kappa_{\text{gm-along}} = \kappa_{\text{along}}. \quad (48.136)$$

This is the approach assumed by [Smith and Gent \(2004\)](#). With the small slope approximation to neutral diffusion, we find the combined anisotropic mixing tensor becomes

$$\begin{aligned} \mathbb{K}_{\text{small aniso}} + \mathbb{A}_{\text{gm-aniso}} = \\ \kappa_{\text{cross}} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 2S_x & 2S_y & S \cdot S \end{bmatrix} + \Delta\kappa \begin{bmatrix} \hat{d}_x^2 & \hat{d}_x \hat{d}_y & 0 \\ \hat{d}_x \hat{d}_y & \hat{d}_y^2 & 0 \\ 2(\hat{d} \cdot S) \hat{d}_x & 2(\hat{d} \cdot S) \hat{d}_y & (\hat{d} \cdot S)^2 \end{bmatrix}. \end{aligned} \quad (48.137)$$

The vanishing right hand column terms simplifies the horizontal tracer fluxes computed from this tensor. However, again, this formulation lacks support from theory that supports the distinct treatments of the skew flux and neutral flux.

### 48.6.4 A parameterization based on a boundary value problem

We now follow the approach from Section 48.3.7 to develop a boundary value problem version of the anisotropic Gent-McWilliams stirring. For this purpose we consider the vertical boundary value problem

$$c^2 \frac{d^2 \boldsymbol{\Upsilon}}{dz^2} - N^2 \boldsymbol{\Upsilon} = -N^2 \boldsymbol{\Upsilon}^{\text{gm-aniso}} \quad \text{and} \quad \boldsymbol{\Upsilon}(\eta_b) = \boldsymbol{\Upsilon}(\eta) = 0, \quad (48.138)$$

where (see equation (48.129))

$$\boldsymbol{\Upsilon}^{\text{gm-aniso}} = \kappa_{\text{gm-cross}} \mathbf{S} + \hat{z} \times \Delta\kappa_{\text{gm}} (\hat{d} \cdot \mathbf{S}) \hat{d}. \quad (48.139)$$

As in Section 48.3.7, we deduce the impacts on potential energy (assuming a linear equation of state) via the vertical component of the potential density skew flux,

$$\frac{1}{g} \frac{dP}{dt} = \frac{1}{\rho_0} \int J^z dV = - \int \nabla_z \varrho \cdot \boldsymbol{\Upsilon} dV. \quad (48.140)$$

The governing differential equation (48.138) leads to

$$\boldsymbol{\Upsilon} \cdot \left[ c^2 \frac{d^2 \boldsymbol{\Upsilon}}{dz^2} - N^2 \boldsymbol{\Upsilon} \right] = -N^2 \boldsymbol{\Upsilon} \cdot \boldsymbol{\Upsilon}^{\text{gm-aniso}} \quad (48.141)$$

which rearranges to

$$N^2 \boldsymbol{\Upsilon} \cdot \boldsymbol{\Upsilon}^{\text{gm-aniso}} = -c^2 \frac{d(\boldsymbol{\Upsilon} \cdot \boldsymbol{\Upsilon}')}{dz} + c^2 \boldsymbol{\Upsilon}' \cdot \boldsymbol{\Upsilon}' + N^2 \boldsymbol{\Upsilon} \cdot \boldsymbol{\Upsilon}. \quad (48.142)$$

Integrating over a vertical column and making use of the homogeneous Dirichlet boundary conditions in equation (48.138) leads to

$$\frac{g}{\rho_0} \int \boldsymbol{\Upsilon} \cdot \nabla_z \varrho dz = - \int N^2 \Delta \kappa_{gm} (\hat{\mathbf{d}} \cdot \mathbf{S}) (\hat{\mathbf{d}} \cdot \boldsymbol{\Upsilon}) dz + \int [c^2 \boldsymbol{\Upsilon}' \cdot \boldsymbol{\Upsilon}' + N^2 \boldsymbol{\Upsilon} \cdot \boldsymbol{\Upsilon}] dz, \quad (48.143)$$

which can be rearranged into the equivalent form

$$\begin{aligned} & \frac{g}{\rho_0} \int \boldsymbol{\Upsilon} \cdot \nabla_z \varrho dz \\ &= \underbrace{\int [c^2 \boldsymbol{\Upsilon}' \cdot \boldsymbol{\Upsilon}' + N^2 (\boldsymbol{\Upsilon} \cdot \boldsymbol{\Upsilon} - (\hat{\mathbf{d}} \cdot \boldsymbol{\Upsilon})^2)] dz}_{\text{positive semi-definite}} + \underbrace{\int N^2 (\hat{\mathbf{d}} \cdot \boldsymbol{\Upsilon}) \hat{\mathbf{d}} \cdot (\boldsymbol{\Upsilon} - \mathbf{S} \Delta \kappa_{gm}) dz}_{\text{sign indefinite}}. \end{aligned} \quad (48.144)$$

The first term on the right hand side is positive semi-indefinite whereas the second term is sign indefinite. If the second term is positive, or smaller in magnitude than the first term, then the parameterization provides a column integrated sink of potential energy. Otherwise, potential energy for the column can increase. There are no existing numerical implementations of this scheme to determine its suitability for realistic ocean climate simulations.





# Chapter 49

## Ocean density and sea level

Conservative temperature,  $\Theta$ , is the preferred means to measure the transport of enthalpy in the ocean, and salinity,  $S$ , measures the concentration of dissolved salt matter. These two scalar fields are referred to as *active* tracers as they both impact density and in turn affect pressure and ocean currents. In this chapter we study how the evolution of  $\Theta$  and  $S$  affects density.  $\Theta$  and  $S$  are conservative tracers so that the net changes in potential enthalpy and salt over the global ocean domain arise from net imbalances in their boundary fluxes. Likewise, ocean mass is a conserved field, with global mass changes arising from imbalances in boundary mass fluxes such as those occurring from increases in land ice melt. However, ocean volume, and hence ocean density and buoyancy, are not conserved fields. These points have direct impact on how global mean sea level is affected by ocean processes such as mixing, with rudiments presented in this chapter.

### CHAPTER GUIDE

Basic notions of thermodynamics, such as Section 21.8, motivate the use of Conservative Temperature as a measure of ocean enthalpy transfer, rather than *in situ* temperature. The material in this chapter considers how we measure air-sea buoyancy fluxes and analyze changes to global mean sea level. Both of these topics are increasingly important for studies of anthropogenic climate change.

49.1	Loose threads . . . . .	1220
49.2	Material evolution of <i>in situ</i> density . . . . .	1220
49.2.1	Material changes to pressure . . . . .	1221
49.2.2	Material changes to $\Theta$ and $S$ . . . . .	1221
49.2.3	General expression for density changes . . . . .	1221
49.2.4	Unpacking the subgrid contributions . . . . .	1222
49.2.5	Synthesis of the density equation . . . . .	1224
49.3	Cabbeling and thermobaricity . . . . .	1225
49.3.1	Basic manipulations . . . . .	1225
49.3.2	A tidy form . . . . .	1226
49.3.3	Cabbeling . . . . .	1227
49.3.4	Thermobaricity . . . . .	1227
49.3.5	Comments . . . . .	1228
49.4	Salt and freshwater budgets . . . . .	1228
49.4.1	Salt and freshwater . . . . .	1228
49.4.2	Mass budgets . . . . .	1229
49.5	Surface boundary conditions for $S$ and $\Theta$ . . . . .	1230

---

49.5.1	Salt and freshwater . . . . .	1230
49.5.2	The non-advective salt flux boundary condition . . . . .	1231
49.5.3	Conservative Temperature boundary condition . . . . .	1233
49.5.4	Comments and further reading . . . . .	1233
49.6	Surface boundary fluxes of buoyancy . . . . .	<b>1233</b>
49.6.1	Outlining the boundary fluxes of enthalpy and salt . . . . .	1234
49.6.2	Evolution from surface boundary fluxes . . . . .	1234
49.6.3	Buoyancy tendency from surface boundary fluxes . . . . .	1235
49.6.4	Comments . . . . .	1236
49.7	Global mean sea level . . . . .	<b>1236</b>
49.7.1	Definitions and assumptions . . . . .	1236
49.7.2	Budget for global mean sea level . . . . .	1237
49.7.3	Changes due to mass input . . . . .	1238
49.7.4	Steric changes due to changes in density . . . . .	1238
49.7.5	Enthalpy flux imbalances giving rise to thermosteric sea level . . . . .	1239
49.7.6	Global sea level in a Boussinesq fluid . . . . .	1239
49.7.7	Global halosteric sea level changes are negligible . . . . .	1240
49.7.8	Further study . . . . .	1240

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## 49.1 Loose threads

- Schematics for cabbeling and thermobaricity.

## 49.2 Material evolution of *in situ* density

Changes to the *in situ* density of seawater affects pressure forces in the ocean as well as the volume occupied by the ocean fluid (i.e., sea level). As discussed in Section 24.3.2, it is common to write the seawater equation of state for density as a function of potential temperature, salinity, and pressure. A somewhat more accurate approach makes use of the Conservative Temperature rather than the potential temperature, where the Conservative Temperature,  $\Theta$ , is the potential enthalpy divided by a constant heat capacity ([McDougall, 2003](#); [IOC et al., 2010](#)). We thus make use of the empirical relation for the seawater density in the functional form

$$\rho = \rho(\Theta, S, p), \quad (49.1)$$

where  $S$  is the salinity rather than the salt concentration ( $S = 1000 \text{ S}$ ).

We formulate the material evolution of density as weighted by the specific volume<sup>1</sup>

$$\nu = \rho^{-1}, \quad (49.2)$$

so that we study

$$\frac{D \ln \rho}{Dt} = \frac{\partial \ln \rho}{\partial \Theta} \frac{D\Theta}{Dt} + \frac{\partial \ln \rho}{\partial S} \frac{DS}{Dt} + \frac{\partial \ln \rho}{\partial p} \frac{Dp}{Dt} \quad (49.3a)$$

$$= -\alpha \frac{D\Theta}{Dt} + \beta \frac{DS}{Dt} + \frac{\dot{p}}{\rho c_s^2}. \quad (49.3b)$$

---

<sup>1</sup>In other chapters we write the specific volume as  $\nu_s = 1/\rho$  to distinguish it from  $\nu$  that is used for kinematic viscosity. However, in this chapter we write  $\nu = 1/\rho$  to enable a shorthand for partial derivatives as defined by equation (49.8). We have no use kinematic viscosity in this chapter.

In this equation we introduced the thermal expansion coefficient, the haline contraction coefficient, the squared speed of sound, and the vertical pseudo-velocity in pressure

$$\alpha = - \left[ \frac{\partial \ln \rho}{\partial \Theta} \right]_{p,S} \quad \beta = \left[ \frac{\partial \ln \rho}{\partial S} \right]_{p,\Theta} \quad c_s^2 = \left[ \frac{\partial p}{\partial \rho} \right]_{S,\Theta} \quad \dot{p} = \frac{Dp}{Dt}. \quad (49.4)$$

For the remainder of this section we unpack the processes contributing to the density material time evolution (49.3).

### 49.2.1 Material changes to pressure

To garner some exposure to the physics of  $\dot{p}$  as it appears in equation (49.3), we consider the special case of a hydrostatic fluid, where the volume per time per horizontal area of fluid crossing a surface of constant hydrostatic pressure is given by (see Section 42.4.6)

$$w^{(p)} = \frac{\partial z}{\partial p} \frac{Dp}{Dt} = -(\rho g)^{-1} \dot{p}. \quad (49.5)$$

The transport measured by  $w^{(p)}$  is the pressure-coordinate analog of the vertical velocity component  $w = Dz/Dt$  in a geopotential coordinate representation of the vertical. That is, fluid moving into regions of increasing hydrostatic pressure ( $\dot{p} > 0$ ) represents downward movement of fluid, with  $w^{(p)} < 0$  in this case. Conversely, motion into decreasing hydrostatic pressure represents upward motion, with  $w^{(p)} > 0$ . This vertical movement generally occurs in the presence of waves, currents, and mixing; i.e., both reversible and irreversible processes give rise to vertical motion.

### 49.2.2 Material changes to $\Theta$ and $S$

We now focus on the salinity and temperature contributions to the evolution of *in situ* density. To do so, assume that the material evolution of  $\Theta$  and  $S$  are given by the convergence of a subgrid scale flux

$$\rho \frac{D\Theta}{Dt} = -\nabla \cdot \mathbf{J}^{(\Theta)} \quad (49.6a)$$

$$\rho \frac{DS}{Dt} = -\nabla \cdot \mathbf{J}^{(S)}. \quad (49.6b)$$

The Conservative Temperature equation (49.6a) was derived in Section 21.8, whereas the Absolute Salinity equation (49.6b) follows from our derivation of the tracer equation in Section 15.1.<sup>2</sup>

### 49.2.3 General expression for density changes

The expressions (49.6a) and (49.6b) for material changes in  $\Theta$  and  $S$  then lead to

$$-\alpha \frac{D\Theta}{Dt} + \beta \frac{DS}{Dt} = \nu_\Theta \nabla \cdot \mathbf{J}^{(\Theta)} + \nu_S \nabla \cdot \mathbf{J}^{(S)} \quad (49.7a)$$

$$= \nabla \cdot [\nu_\Theta \mathbf{J}^{(\Theta)} + \nu_S \mathbf{J}^{(S)}] - [\mathbf{J}^{(\Theta)} \cdot \nabla \nu_\Theta + \mathbf{J}^{(S)} \cdot \nabla \nu_S] \quad (49.7b)$$

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<sup>2</sup>We here ignore remineralization processes that can contribute to a source term in the salinity equation (49.6b). Such source terms are discussed in [IOC et al. \(2010\)](#).

where again  $\nu = \rho^{-1}$  is the specific volume and its partial derivatives are

$$\nu_\Theta = \frac{\partial \nu}{\partial \Theta} = \frac{\alpha}{\rho} \quad \text{and} \quad \nu_S = \frac{\partial \nu}{\partial S} = -\frac{\beta}{\rho}. \quad (49.8)$$

Bringing the above results together leads to the density equation

$$\frac{D \ln \rho}{Dt} - \frac{\dot{p}}{\rho c_s^2} = \nabla \cdot [\nu_\Theta \mathbf{J}^{(\Theta)} + \nu_S \mathbf{J}^{(S)}] - [\mathbf{J}^{(\Theta)} \cdot \nabla \nu_\Theta + \mathbf{J}^{(S)} \cdot \nabla \nu_S], \quad (49.9)$$

which has the equivalent form

$$\frac{D \rho}{Dt} - \frac{\dot{p}}{c_s^2} = \nabla \cdot [\alpha \mathbf{J}^{(\Theta)} - \beta \mathbf{J}^{(S)}] - [\mathbf{J}^{(\Theta)} \cdot \nabla \alpha - \mathbf{J}^{(S)} \cdot \nabla \beta]. \quad (49.10)$$

We brought the source term from motion across pressure surfaces (Section 49.2.1) onto the left hand side, as this term appears in the absence of subgrid processes. The first term on the right hand side represents the divergence of a buoyancy flux due to subgrid scale fluxes of Conservative Temperature and salinity. In turn, density increases in regions where the buoyancy flux diverges (e.g.,  $\Theta$  reducing and  $S$  increasing). These fluxes arise from a variety of mixing processes, some of which are surveyed in Section 48.1.1. The second term on the right hand side of equations (49.9) and (49.10) relates to properties of the locally referenced potential density surface. We study this source term arising from neutral diffusion in Section 49.3, where we encounter cabbeling and thermobaricity. Further effects arise from unresolved eddy-induced stirring, with that process contributing to the material time derivative operator to render a residual mean velocity (Section 48.1.4).

#### 49.2.4 Unpacking the subgrid contributions

Recall from Section 48.1 that the subgrid scale fluxes are generally written in terms of a second order mixing tensor,  $\mathbb{M}$ ,

$$\mathbf{J}^{(\Theta)} = -\rho \mathbb{M} \cdot \nabla \Theta \quad \text{and} \quad \mathbf{J}^{(S)} = -\rho \mathbb{M} \cdot \nabla S. \quad (49.11)$$

Furthermore,  $\mathbb{M}$  is typically decomposed as in equation (48.8) into its symmetric diffusion tensor,  $\mathbb{K}$ , and anti-symmetric stirring tensor,  $\mathbb{A}$ ,

$$\mathbb{M} = \mathbb{K} + \mathbb{A}. \quad (49.12)$$

We decompose the contributions to density according to these subgrid stirring and diffusion processes via the following manipulations

$$\frac{D \rho}{Dt} - \frac{\dot{p}}{c_s^2} = \alpha \nabla \cdot \mathbf{J}^{(\Theta)} - \beta \nabla \cdot \mathbf{J}^{(S)} \quad (49.13a)$$

$$= -\alpha \nabla \cdot (\rho \mathbb{M} \cdot \nabla \Theta) + \beta \nabla \cdot (\rho \mathbb{M} \cdot \nabla S). \quad (49.13b)$$

Expanding the  $\Theta$  term leads to

$$\alpha \nabla \cdot \mathbf{J}^{(\Theta)} = -\alpha \nabla \cdot (\rho \mathbb{M} \cdot \nabla \Theta) \quad (49.14a)$$

$$= -\alpha \nabla \cdot (\rho \mathbb{A} \cdot \nabla \Theta) - \alpha \nabla \cdot (\rho \mathbb{K} \cdot \nabla \Theta) \quad (49.14b)$$

$$= -\alpha \nabla \cdot (\rho \mathbb{A}) \cdot \nabla \Theta - \alpha \nabla \cdot (\rho \mathbb{K} \cdot \nabla \Theta), \quad (49.14c)$$

$$= -\alpha \mathbf{v}^* \cdot \nabla \Theta - \alpha \nabla \cdot (\rho \mathbb{K} \cdot \nabla \Theta). \quad (49.14d)$$

To reach this result we made use of the identities

$$\nabla \cdot (\rho \mathbb{A} \cdot \nabla \Theta) = \partial_m(\rho \mathbb{A}^{mn} \partial_n \Theta) \quad \text{expose tensor indices} \quad (49.15a)$$

$$= \partial_m(\rho \mathbb{A}^{mn}) \partial_n \Theta + \rho \mathbb{A}^{mn} \partial_m \partial_n \Theta \quad \text{product rule} \quad (49.15b)$$

$$= \partial_m(\rho \mathbb{A}^{mn}) \partial_n \Theta \quad \mathbb{A}^{mn} \partial_m \partial_n \Theta = 0 \quad (49.15c)$$

$$= -\rho \mathbf{v}^* \cdot \nabla \Theta \quad \partial_m(\rho \mathbb{A}^{mn}) = -\rho \mathbf{v}^{*n}. \quad (49.15d)$$

In the final equality we introduced the density weighted eddy-induced velocity,  $\rho \mathbf{v}^*$ , defined by equation (48.11). The same manipulations for the salinity term lead to

$$\frac{D\rho}{Dt} - \frac{\dot{p}}{c_s^2} + \rho \mathbf{v}^* \cdot (-\alpha \nabla \Theta + \beta \nabla S) = -\alpha \nabla \cdot (\rho \mathbb{K} \cdot \nabla \Theta) + \beta \nabla \cdot (\rho \mathbb{K} \cdot \nabla S). \quad (49.16)$$

We can write this expression in terms of the residual mean material time operator

$$\frac{D^\dagger}{Dt} = \frac{D}{Dt} + \mathbf{v}^* \cdot \nabla, \quad (49.17)$$

through adding and subtracting  $c_s^{-2} \mathbf{v}^* \cdot \nabla p$

$$\rho \mathbf{v}^* \cdot (-\alpha \nabla \Theta + \beta \nabla S) = \mathbf{v}^* \cdot (-\rho \alpha \nabla \Theta + \rho \beta \nabla S + c_s^{-2} \nabla p) - c_s^{-2} \mathbf{v}^* \cdot \nabla p = \mathbf{v}^* \cdot (\nabla \rho - c_s^{-2} \nabla p), \quad (49.18)$$

which then leads to

$$\frac{D\rho}{Dt} - \frac{\dot{p}}{c_s^2} + \rho \mathbf{v}^* \cdot (-\alpha \nabla \Theta + \beta \nabla S) = \frac{D^\dagger \rho}{Dt} - \frac{1}{c_s^2} \frac{D^\dagger p}{Dt}, \quad (49.19)$$

so that

$$\frac{D^\dagger \rho}{Dt} - \frac{1}{c_s^2} \frac{D^\dagger p}{Dt} = -\alpha \nabla \cdot (\rho \mathbb{K} \cdot \nabla \Theta) + \beta \nabla \cdot (\rho \mathbb{K} \cdot \nabla S). \quad (49.20)$$

Transport from the symmetric tensor,  $\mathbb{K}$ , corresponds to diffusion so long as the tensor is positive semi-definite. The diffusion operator in the residual mean evolution equation (49.20) can be written

$$-\alpha \nabla \cdot (\rho \mathbb{K} \cdot \nabla \Theta) + \beta \nabla \cdot (\rho \mathbb{K} \cdot \nabla S) = \nabla \cdot [\rho \mathbb{K} \cdot (-\alpha \nabla \Theta + \beta \nabla S)] + \rho \nabla \alpha \cdot \mathbb{K} \cdot \nabla \Theta - \rho \nabla \beta \cdot \mathbb{K} \cdot \nabla S, \quad (49.21)$$

so that the *in situ* density evolves according to

$$\frac{D^\dagger \rho}{Dt} - \frac{1}{c_s^2} \frac{D^\dagger p}{Dt} = -\underbrace{\nabla \cdot [\rho \mathbb{K} \cdot (\alpha \nabla \Theta - \beta \nabla S)]}_{\text{conservative processes}} + \underbrace{\rho \nabla \alpha \cdot \mathbb{K} \cdot \nabla \Theta - \rho \nabla \beta \cdot \mathbb{K} \cdot \nabla S}_{\text{sources from nonlinear EOS processes}}. \quad (49.22)$$

We now discuss the physical processes associated with the right hand side terms.

- LINEAR EQUATION OF STATE: A linear equation of state has  $\nabla \alpha = \nabla \beta = 0$  and is independent of pressure, so that the evolution equation (49.22) takes the form

$$\frac{D^\dagger \rho}{Dt} = -\nabla \cdot [\rho \mathbb{K} \cdot (\alpha \nabla \Theta - \beta \nabla S)]. \quad (49.23)$$

Under the residual mean transport with a linear equation of state, density remains materially constant in the absence of any diffusion.

- NONLINEAR EQUATION OF STATE: A nonlinear equation of state is characterized by spatially

dependent thermal expansion and haline contraction coefficients. Mixing of  $\Theta$  and  $S$  in the presence of a nonlinear equation of state generally gives rise to material evolution of *in situ* density through cabbeling and thermobaricity ([McDougall, 1987b](#)). We offer a summary of these processes in Section 49.3.

- NEUTRAL DIFFUSION:

Neutral diffusion from Section 48.4 maintains a density-compensated diffusive flux of  $\Theta$  and  $S$  so that

$$\mathbb{K}_{\text{neutral}} \cdot (\alpha \nabla \Theta - \beta \nabla S) = 0. \quad (49.24)$$

Hence, neutral diffusion leaves *in situ* density changed only via the nonlinear equation of state processes.

- ISOTROPIC SMALL SCALE DIFFUSION:

As discussed in Section 48.1.3, it is common to parameterize fine scale mixing processes using an isotropic diffusivity so that the diffusion tensor is given by

$$\mathbb{K}_{\text{isotropic}} = \kappa \mathbb{I}, \quad (49.25)$$

where  $\mathbb{I}$  is the unit tensor and  $\kappa > 0$  is the isotropic eddy diffusivity.

### 49.2.5 Synthesis of the density equation

In summary, the material time evolution equation for *in situ* density in the presence of subgrid scale processes takes the form

$$\frac{D\rho}{Dt} = \underbrace{\frac{1}{c_s^2} \frac{Dp}{Dt}}_{\text{compressibility}} - \underbrace{\mathbf{v}^* \cdot (-\alpha \nabla \Theta + \beta \nabla S)}_{\text{eddy-induced stirring}} - \underbrace{\nabla \cdot [\rho \kappa (-\alpha \nabla \Theta + \beta \nabla S)]}_{\text{small scale diffusive mixing}} + \underbrace{\rho \nabla \alpha \cdot \mathbb{K} \cdot \nabla \Theta - \rho \nabla \beta \cdot \mathbb{K} \cdot \nabla S}_{\text{nonlinear EOS processes from eddy mixing}}. \quad (49.26)$$

We thus have the following physical processes contributing to the evolution of *in situ* density.

- ADIABATIC COMPRESSION: Material changes to pressure in the presence of a finite sound speed lead to changes in the fluid density.
- SMALL SCALE MIXING: Small scale mixing is parameterized by an isotropic diffusivity,  $\kappa$ . This diffusivity is the same for all tracers, with the exception of double-diffusive processes whereby material tracers (e.g., salinity, nutrients) have a diffusivity distinct from temperature ([Schmitt, 1994](#)). Given the dominance of vertical stratification over the horizontal, it is common to approximate the isotropic diffusion operator with a vertical diffusion operator (but see Section 4 of [McDougall et al. \(2014\)](#) for caveats).
- EDDY-INDUCED STIRRING: For subgrid scale stirring, such as from mesoscale (and submesoscale) eddies, we introduce a parameterized eddy-induced advection operator. When combined with the resolved advection, we are led to a residual mean material time derivative,  $D^\dagger/Dt$ .
- EDDY-INDUCED DIFFUSION: Subgrid scale eddy-induced stirring leads to a direct cascade of  $\Theta$  and  $S$  variance to the small scales. Mixing arising from this cascade is parameterized by neutral diffusion, whereby the diffusive fluxes of  $\Theta$  and  $S$  are density compensated according to the constraint (49.24).

- NONLINEAR EOS PROCESSES: Mixing of  $\Theta$  and  $S$  in the presence of a nonlinear equation of state means that *in situ* density evolves due to cabbeling and thermobaricity (Section 49.3). The dominant contributions to these processes arise from eddy-stirring induced mixing (i.e., neutral diffusion) (McDougall, 1987b), though small scale mixing also has a contribution.

## 49.3 Cabbeling and thermobaricity

We now return to the density equation (49.10)

$$\frac{D \ln \rho}{Dt} - \frac{\dot{p}}{\rho c_s^2} = \nabla \cdot [\nu_\Theta \mathbf{J}^{(\Theta)} + \nu_S \mathbf{J}^{(S)}] - (\mathbf{J}^{(\Theta)} \cdot \nabla \nu_\Theta + \mathbf{J}^{(S)} \cdot \nabla \nu_S), \quad (49.27)$$

and here focus on temperature and salinity fluxes just from the neutral diffusion process described in Section 48.4. The neutrality condition (48.87) is a fundamental property of neutral diffusion, and it takes the following form in terms of specific volume

$$\nu_\Theta \mathbf{J}^{(\Theta)} + \nu_S \mathbf{J}^{(S)} = 0. \quad (49.28)$$

Consequently, neutral diffusion affects density evolution only through the source term

$$\left[ \frac{D \ln \rho}{Dt} \right]_{\text{ntral diff}} = -\mathbf{J}^{(\Theta)} \cdot \nabla \nu_\Theta - \mathbf{J}^{(S)} \cdot \nabla \nu_S. \quad (49.29)$$

In the remainder of this section we manipulate this expression in order to more clearly identify the variety of physical processes associated with neutral diffusion in the presence of a nonlinear equation of state.

### 49.3.1 Basic manipulations

As a first step, eliminate the salt flux by using the neutrality condition (49.28)

$$\mathbf{J}^{(\Theta)} \cdot \nabla \nu_\Theta + \mathbf{J}^{(S)} \cdot \nabla \nu_S = \mathbf{J}^{(\Theta)} \cdot [\nu_S \nabla \nu_\Theta - \nu_\Theta \nabla \nu_S]/\nu_S. \quad (49.30)$$

Next, expand the gradients of the specific volume to write

$$\nabla \nu_\Theta = \nu_{\Theta\Theta} \nabla \Theta + \nu_{\Theta S} \nabla S + \nu_{\Theta p} \nabla p \quad \text{and} \quad \nabla \nu_S = \nu_{SS} \nabla S + \nu_{\Theta S} \nabla \Theta + \nu_{Sp} \nabla p, \quad (49.31)$$

so that

$$\begin{aligned} \nu_S \nabla \nu_\Theta - \nu_\Theta \nabla \nu_S &= \nabla \Theta (\nu_S \nu_{\Theta\Theta} - \nu_\Theta \nu_{\Theta S}) \\ &\quad + \nabla S (\nu_S \nu_{\Theta S} - \nu_\Theta \nu_{SS}) + \nabla p (\nu_S \nu_{Sp} - \nu_\Theta \nu_{Sp}). \end{aligned} \quad (49.32)$$

We again make use of the neutrality condition (49.28), as well as the symmetry condition (48.88d) to write

$$\mathbf{J}^{(\Theta)} \cdot \nabla S (\nu_S \nu_{\Theta S} - \nu_\Theta \nu_{SS}) = -\mathbf{J}^{(\Theta)} \cdot \nabla \Theta \left[ \nu_\Theta \nu_{\Theta S} - \nu_{SS} \frac{(\nu_\Theta)^2}{\nu_S} \right]. \quad (49.33)$$

Bringing these results together leads to

$$\begin{aligned} \mathbf{J}^{(\Theta)} \cdot \nabla \nu_{\Theta} + \mathbf{J}^{(S)} \cdot \nabla \nu_S &= \mathbf{J}^{(\Theta)} \cdot \nabla p \left[ \nu_{\Theta p} - \nu_{pS} \frac{\nu_{\Theta}}{\nu_S} \right] \\ &\quad + \mathbf{J}^{(\Theta)} \cdot \nabla \Theta \left[ \nu_{\Theta \Theta} - 2 \nu_{\Theta S} \frac{\nu_{\Theta}}{\nu_S} + \nu_{SS} \left( \frac{\nu_{\Theta}}{\nu_S} \right)^2 \right], \end{aligned} \quad (49.34)$$

which can be written in terms of density partial derivatives as

$$\begin{aligned} \mathbf{J}^{(\Theta)} \cdot \nabla \nu_{\Theta} + \mathbf{J}^{(S)} \cdot \nabla \nu_S &= -\rho^{-2} \mathbf{J}^{(\Theta)} \cdot \nabla p \left[ \rho_{\Theta p} - \rho_{pS} \frac{\rho_{\Theta}}{\rho_S} \right] \\ &\quad - \rho^{-2} \mathbf{J}^{(\Theta)} \cdot \nabla \Theta \left[ \rho_{\Theta \Theta} - 2 \rho_{\Theta S} \frac{\rho_{\Theta}}{\rho_S} + \rho_{SS} \left( \frac{\rho_{\Theta}}{\rho_S} \right)^2 \right]. \end{aligned} \quad (49.35)$$

### 49.3.2 A tidy form

We next write the bracket terms in forms consistent with those introduced by [McDougall \(1987b\)](#) in his classic paper discussing cabbeling and thermobaricity. For that purpose, introduce the *thermobaricity* parameter (dimensions of inverse temperature times inverse pressure) whose form is given by

$$\mathcal{T} = \beta \partial_p \left[ \frac{\alpha}{\beta} \right] \quad (49.36a)$$

$$= \frac{\partial \alpha}{\partial p} - \frac{\alpha}{\beta} \frac{\partial \beta}{\partial p} \quad (49.36b)$$

$$= \rho \nu_S \partial_p \left[ \frac{\nu_{\Theta}}{\nu_S} \right] \quad (49.36c)$$

$$= -\rho^{-1} \rho_S \partial_p \left[ \frac{\rho_{\Theta}}{\rho_S} \right] \quad (49.36d)$$

$$= -\rho^{-1} \left[ \rho_{\Theta p} - \rho_{pS} \left[ \frac{\rho_{\Theta}}{\rho_S} \right] \right], \quad (49.36e)$$

and the *cabbeling* parameter (dimensions of squared inverse temperature)

$$\mathcal{C} = \frac{\partial \alpha}{\partial \Theta} + 2 \frac{\alpha}{\beta} \frac{\partial \alpha}{\partial S} - \left( \frac{\alpha}{\beta} \right)^2 \frac{\partial \beta}{\partial S} \quad (49.37a)$$

$$= -\rho^{-1} \left[ \rho_{\Theta \Theta} - 2 \rho_{\Theta S} \left[ \frac{\rho_{\Theta}}{\rho_S} \right] + \rho_{SS} \left[ \frac{\rho_{\Theta}}{\rho_S} \right]^2 \right] \quad (49.37b)$$

$$= \rho \left[ \nu_{\Theta \Theta} - 2 \nu_{\Theta S} \left[ \frac{\nu_{\Theta}}{\nu_S} \right] + \nu_{SS} \left[ \frac{\nu_{\Theta}}{\nu_S} \right]^2 \right] \quad (49.37c)$$

to render the very compact result

$$\mathbf{J}^{(\Theta)} \cdot \nabla \nu_{\Theta} + \mathbf{J}^{(S)} \cdot \nabla \nu_S = \rho^{-1} \mathbf{J}^{(\Theta)} \cdot (\mathcal{T} \nabla p + \mathcal{C} \nabla \Theta) \quad (49.38)$$

which in turn yields the material evolution of *in situ* density due to neutral diffusion

$$\left[ \frac{D\rho}{Dt} \right]_{\text{ntral diff}} = -\mathbf{J}^{(\Theta)} \cdot (\mathcal{T} \nabla p + \mathcal{C} \nabla \Theta). \quad (49.39)$$

### 49.3.3 Cabbeling

Consider the mixing of two seawater elements. Let the fluid elements separately have distinct Conservative Temperature and/or salinity, but equal locally referenced potential density. For a linear equation of state, whereby density is a linear function of  $\Theta$  and  $S$ , then the resulting mixed fluid element has the same density as the unmixed separate elements. However, for a nonlinear equation of state, the mixed element generally has a different density. Furthermore, a property of seawater is that the density of the mixed element is actually greater than the unmixed elements. This densification upon mixing is a physical process known as *cabbeling* ([McDougall, 1987b](#)).

The sign definite nature of cabbeling (i.e., cabbeling always results in denser fluid elements after mixing) is a direct result of the geometry of the locally referenced potential density surface when viewed in Conservative Temperature and salinity space. This property in turn manifests with the following inequality for the cabbeling parameter

$$\mathcal{C} = \frac{\partial \alpha}{\partial \Theta} + 2 \frac{\alpha}{\beta} \frac{\partial \alpha}{\partial S} - \left[ \frac{\alpha}{\beta} \right]^2 \frac{\partial \beta}{\partial S} \geq 0. \quad (49.40)$$

Given the downgradient nature of the neutral diffusive fluxes, we have

$$\text{Cabbeling} \equiv -\mathcal{C} \mathbf{J}^{(\Theta)} \cdot \nabla \Theta \geq 0, \quad (49.41)$$

thus providing a mathematical expression for the cabbeling source (with dimensions of density per time). That is, cabbeling results in a positive material evolution of density; i.e., density increases due to cabbeling. An increase in the density within a column of fluid results in the reduction of the sea level due to compression of the column.

### 49.3.4 Thermobaricity

The thermobaricity parameter

$$\mathcal{T} = \beta \frac{\partial}{\partial p} \left[ \frac{\alpha}{\beta} \right] \quad (49.42)$$

is nonzero due to pressure dependence of the ratio of the thermal expansion coefficient to the haline contraction coefficient. As both thermal and haline effects are present, the parameter  $\mathcal{T}$  is more precisely split into two terms

$$\begin{aligned} \mathcal{T} &= \frac{\partial \alpha}{\partial p} - \frac{\alpha}{\beta} \frac{\partial \beta}{\partial p} \\ &= -\frac{\rho_{\Theta p}}{\rho} + \frac{\rho_\Theta}{\rho_S} \frac{\rho_{pS}}{\rho} \end{aligned} \quad (49.43)$$

Thermobaricity is the common name for the sum, since pressure variations in the thermal expansion coefficient dominate those of the haline contraction coefficient. The thermal expansion coefficient generally increases as pressure increases, thus making the thermobaric parameter positive.

Since neutral gradient of temperature need not be oriented in a special manner relative to the neutral gradient of pressure, there is no sign-definite nature to the thermobaricity source term

(with units of density per time)

$$\text{Thermobaricity} \equiv -\mathcal{T} \mathbf{J}^{(\Theta)} \cdot \nabla p \quad (49.44)$$

appearing in equation (49.38). Thus, thermobaricity can either increase or decrease density, depending on details of the density and fluxes. However, as noted by [McDougall and You \(1990\)](#), thermobaricity typically increases density in much of the World Ocean.

### 49.3.5 Comments

[Griffies and Greatbatch \(2012\)](#) discuss the impacts on global mean sea level from thermobaricity and cabbeling as diagnosed from an ocean model. Given that cabbeling always densifies and thermobaricity is also dominated by densification, these processes lead to a general reduction in global mean sea level. [Klocker and McDougall \(2010\)](#), [Groeskamp et al. \(2016\)](#), and [Groeskamp et al. \(2019\)](#) diagnose cabbeling and thermobaricity from observational based measurements, with [Groeskamp et al. \(2019\)](#) also offering a more robust numerical method for performing that diagnostic calculation.

Although cabbeling and thermobaricity lead to watermass transformation and associated transport of water across neutral directions, they are distinct from other mixing processes such as breaking gravity waves (Section 48.1). Namely, cabbeling and thermobaricity arise from the stirring by mesoscale eddies along neutral directions, which in turn leads to neutral diffusion acting on Conservative Temperature and salinity. Transient mesoscale eddies impart a downscale cascade of tracer variance that is ultimately halted by irreversible molecular mixing, or microscale processes active before reaching the molecular level. This mixing is the ultimate cause for cabbeling and thermobaricity, with the overall strength of the cabbeling and thermobaricity determined by the strength of the mesoscale stirring.

## 49.4 Salt and freshwater budgets

We here specialize the kinematics of material tracers given in Section 15.5 to the case of seawater, which we treat as a two component fluid comprised of salt and freshwater concentrations. We extend this discussion in Section 49.6 by studying the role of surface boundary salt, enthalpy, and water transports on changes in ocean buoyancy.<sup>3</sup>

### 49.4.1 Salt and freshwater

Seawater is comprised of two material tracers: freshwater along with a suite of dissolved trace “salts”. The ratio of salts is roughly constant over the World Ocean. We are thus able to make use of a single effective mass concentration known as the *salt concentration*<sup>4</sup>

$$S = \frac{\text{mass of salt}}{\text{mass of seawater}} = \frac{\text{mass of salt}}{\text{mass of freshwater} + \text{mass of salt}} \quad (49.45)$$

<sup>3</sup>We provide a theoretical discussion of Conservative Temperature in Section 21.8. For present purposes, we merely need to know it is the ocean tracer best suited to measuring enthalpy (heat) transport ([McDougall, 2003](#); [IOC et al., 2010](#)).

<sup>4</sup>We use the salt concentration,  $S$ , in this section to avoid 1/1000 factors needed if working with salinity,  $S = 1000 \text{S}$ .

to specify the amount of salt within an element of seawater. In practice oceanographers choose to work with the *salinity*,<sup>5</sup>

$$S = 1000 \text{ S}, \quad (49.46)$$

which converts from typical salt concentrations of  $S = 0.035$  to a salinity of  $S = 35$ . The complement to salt concentration is the freshwater concentration or mass fraction for an element of seawater

$$F = \frac{\text{mass of freshwater}}{\text{mass of seawater}} = \frac{\text{mass of freshwater}}{\text{mass of freshwater} + \text{mass of salt}} = 1 - S. \quad (49.47)$$

Other trace matter occurs at very low concentrations so as to make seawater, in effect, a two-component fluid consisting of freshwater plus dissolved salt.<sup>6</sup> We here derive the mass budget for salt and freshwater as well as the associated kinematic boundary conditions.

#### 49.4.2 Mass budgets

Following our discussion of the tracer equation in Section 15.1, the mass budget equations for an element of seawater take the form

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0 \quad \text{seawater} \quad (49.48)$$

$$\frac{\partial(\rho S)}{\partial t} + \nabla \cdot (\rho \mathbf{v} S + \mathbf{J}^{(S)}) = 0 \quad \text{salt} \quad (49.49)$$

$$\frac{\partial(\rho F)}{\partial t} + \nabla \cdot (\rho \mathbf{v} F + \mathbf{J}^{(F)}) = 0 \quad \text{freshwater}. \quad (49.50)$$

Equation (49.48) is the mass budget for seawater and equation (49.49) is the mass budget for salt. The freshwater budget (49.50) is derived by subtracting the salt budget (49.49) from the seawater mass budget (49.48). Hence, only two of the three mass budget equations (49.48)-(49.50) are independent.

We make use of the barycentric velocity in the above conservation laws, where the barycentric velocity for the ocean is given by

$$\mathbf{v} = S \mathbf{v}^{(S)} + F \mathbf{v}^{(F)}. \quad (49.51)$$

The velocities  $\mathbf{v}^{(S)}$  and  $\mathbf{v}^{(F)}$  are, respectively, the molecular center of mass velocities for salt and freshwater within a fluid element, in which case

$$\frac{\partial S}{\partial t} + \mathbf{v}^{(S)} \cdot \nabla S = 0 \quad \text{and} \quad \frac{\partial F}{\partial t} + \mathbf{v}^{(F)} \cdot \nabla F = 0. \quad (49.52)$$

Furthermore, the fluxes  $\mathbf{J}^{(S)}$  and  $\mathbf{J}^{(F)}$  arise from the difference between the salt and freshwater velocities from the barycentric velocity

$$\mathbf{J}^{(S)} = \rho S (\mathbf{v}^{(S)} - \mathbf{v}) \quad \text{and} \quad \mathbf{J}^{(F)} = \rho F (\mathbf{v}^{(F)} - \mathbf{v}). \quad (49.53)$$

These fluxes are often parameterized by downgradient diffusive fluxes

$$\mathbf{J}^{(S)} = -\rho K \cdot \nabla S \quad \text{and} \quad \mathbf{J}^{(F)} = -\rho K \cdot \nabla F, \quad (49.54)$$

---

<sup>5</sup>More precisely, the salinity,  $S$ , as defined by equation (49.46) is the *Absolute Salinity*. Absolute Salinity is distinct from the *practical salinity* determined by conductivity measurements. [IOC et al. \(2010\)](#) provides a full accounting of the theory and practice of ocean salinity.

<sup>6</sup>See [IOC et al. \(2010\)](#) for more discussion of the variations of salt concentration ratios over the ocean, as well as the impacts from biogeochemical tracers.

where  $\mathbb{K}$  is the kinematic diffusivity tensor for salt in seawater, which is a positive semi-definite symmetric tensor. We use the same diffusivity tensor for salt and freshwater since the diffusion of one is balanced by the other. When concerned with molecular processes, the diffusivity tensor is isotropic with diffusivities set by the molecular value of  $10^{-9} \text{ m}^2 \text{ s}^{-1}$ . However, as discussed in Section 48.1, the eddy diffusivity is far larger than the molecular diffusivity in the presence of turbulent eddy processes, which also introduces anisotropies to the diffusion tensor.

The advective flux of seawater is comprised of a salt flux plus a freshwater flux

$$\rho \mathbf{v} = \rho S \mathbf{v}^{(S)} + \rho F \mathbf{v}^{(F)}. \quad (49.55)$$

Conversely, the salt flux and freshwater flux can be represented as a *non-advection flux* plus an advective flux where advection is defined by the barycentric velocity

$$\rho S \mathbf{v}^{(S)} = \rho S (\mathbf{v}^{(S)} - \mathbf{v}) + \rho S \mathbf{v} = \mathbf{J}^{(S)} + \rho S \mathbf{v} \quad (49.56a)$$

$$\rho F \mathbf{v}^{(F)} = \rho F (\mathbf{v}^{(F)} - \mathbf{v}) + \rho F \mathbf{v} = \mathbf{J}^{(F)} + \rho F \mathbf{v}. \quad (49.56b)$$

The non-advection fluxes,  $\mathbf{J}^{(S)}$  and  $\mathbf{J}^{(F)}$ , lead to an exchange of mass with zero net movement of mass. In contrast, the advective flux moves mass as determined by the barycentric velocity. Furthermore, note that the center of mass velocities,  $\mathbf{v}^{(S)}$  and  $\mathbf{v}^{(F)}$ , offer a conceptual framework of use to formulate the kinematic boundary conditions. Even so, they offer no new information beyond that contained in the fluxes  $\mathbf{J}^{(S)}$  and  $\mathbf{J}^{(F)}$ .

## 49.5 Surface boundary conditions for $S$ and $\Theta$

In this section we summarize the surface boundary conditions holding for the salinity and Conservative Temperature equations. This treatment complements that given in Section 15.5.3.

### 49.5.1 Salt and freshwater

In deriving the boundary condition (15.78) in Section 14.4.3, we made use of the barycentric velocity  $\mathbf{v}$  for an element of seawater. We can garner further kinematic insights into the two-component ocean system by decomposing the total mass flux into contributions from salt and freshwater

$$\mathcal{Q}_m = \mathcal{Q}_S + \mathcal{Q}_F, \quad (49.57)$$

and by introducing the center of mass velocities for salt and freshwater according to

$$-\mathcal{Q}_m = \rho (\mathbf{v} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} \quad (49.58a)$$

$$= \rho [S \mathbf{v}^{(S)} + F \mathbf{v}^{(F)} - \mathbf{v}^{(\eta)}] \cdot \hat{\mathbf{n}} \quad (49.58b)$$

$$= \rho [S (\mathbf{v}^{(S)} - \mathbf{v}^{(\eta)}) + \mathbf{v}^{(\eta)} + F \mathbf{v}^{(F)} - \mathbf{v}^{(\eta)}] \cdot \hat{\mathbf{n}} \quad (49.58c)$$

$$= S \rho (\mathbf{v}^{(S)} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} + (1 - S) \rho (\mathbf{v}^{(F)} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} \quad (49.58d)$$

$$= S \rho (\mathbf{v}^{(S)} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} + F \rho (\mathbf{v}^{(F)} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} \quad (49.58e)$$

$$\equiv -(\mathcal{Q}_S + \mathcal{Q}_F), \quad (49.58f)$$

where we wrote

$$S \rho (\mathbf{v}^{(S)} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} = -\mathcal{Q}_S \quad (49.59a)$$

$$F \rho (\mathbf{v}^{(F)} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} = -\mathcal{Q}_F. \quad (49.59b)$$

In these equations, we introduced the velocity,  $\mathbf{v}^{(\eta)}$ , of a point fixed to the free surface. We only need the projection of this velocity in the outward normal direction, which is written by equation (49.57)

$$\mathbf{v}^{(\eta)} \cdot \hat{\mathbf{n}} = \frac{\partial \eta / \partial t}{|\nabla(z - \eta)|} = \frac{\partial \eta / \partial t}{\sqrt{1 + |\nabla \eta|^2}} \implies \mathbf{v}^{(\eta)} \cdot \hat{\mathbf{n}} dS = \partial_t \eta dA, \quad (49.60)$$

where  $dS$  is the area element on the free surface and  $dA$  is its horizontal projection. Note that in many regions, the ocean surface is impermeable to salt, in which case the ocean surface acts as a material surface in terms of the salt velocity

$$\rho (\mathbf{v}^{(S)} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} = 0 \quad \text{zero surface salt flux.} \quad (49.61)$$

The key exception to this boundary condition concerns sea ice, whereby salt is exchanged between liquid seawater and sea ice upon the melting or freezing of ice.

For most applications, it is preferable to make use of equation (49.56a) to eliminate the salt velocity  $\mathbf{v}^{(S)}$  in favor of the non-advection flux  $\mathbf{J}^{(S)} = \rho S (\mathbf{v}^{(S)} - \mathbf{v})$ , in which case the kinematic boundary condition (49.59a) takes the form

$$-\mathcal{Q}_S = S \rho (\mathbf{v}^{(S)} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} = S \rho (\mathbf{v}^{(S)} - \mathbf{v} + \mathbf{v} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} = \mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} - S \mathcal{Q}_m. \quad (49.62)$$

Turning this equation around leads to the non-advection flux

$$\mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} = S \mathcal{Q}_m - \mathcal{Q}_S = S \mathcal{Q}_F - F \mathcal{Q}_S, \quad (49.63)$$

which relates the mass transport crossing the ocean surface at  $z = \eta$  (right hand side) to the non-advection salt transport on the ocean side of the surface boundary (left hand side). A form of this equation was also given by equation (15.80). To support intuition and to check signs, consider the case with  $\mathcal{Q}_S = 0$  so that  $\mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} = S \mathcal{Q}_F$ . This expression means there is an upward non-advection flux of salt ( $\mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} > 0$ ) on the ocean side of the  $z = \eta$  boundary in the presence of an input of freshwater through the ocean surface ( $S \mathcal{Q}_F > 0$ ). For the converse, let  $\mathcal{Q}_F = 0$  so that  $\mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} = -F \mathcal{Q}_S$ . Now, there is a downward non-advection flux of salt ( $\mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} < 0$ ) on the ocean side of the  $z = \eta$  boundary in the presence of salt input through the ocean surface ( $F \mathcal{Q}_S > 0$ ).

### 49.5.2 The non-advection salt flux boundary condition

The above properties of boundary mass transfer result from the kinematic property of a fluid element whose mass is constant, and so the transfer of freshwater across the boundary of a fluid element is compensated by an opposite transfer of salt. The ocean boundary interface acts as a boundary for the fluid elements adjacent to the surface. Hence, to move mass across the  $z = \eta$  interface requires mass to be replenished to the surface fluid elements.

#### *Diffusive closure for the non-advection flux*

Consider an ocean without any mixing, such as for a perfect fluid. In this case, mass arriving to the ocean surface from  $\mathcal{Q}_m > 0$  will not be incorporated into the ambient ocean fluid, but instead will form a separate unmixed surface lens. When mass is exchanged across the ocean surface, mixing is required to incorporate the mass into the ambient ocean fluid. To determine the level of mixing, assume that  $\mathbf{J}^{(S)}$  takes the form of a diffusive flux (49.54) so that the boundary condition (49.63) becomes

$$\mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} = -\rho [\mathbb{K} \cdot \nabla S] \cdot \hat{\mathbf{n}} = S \mathcal{Q}_m - \mathcal{Q}_S = S \mathcal{Q}_F - F \mathcal{Q}_S. \quad (49.64)$$

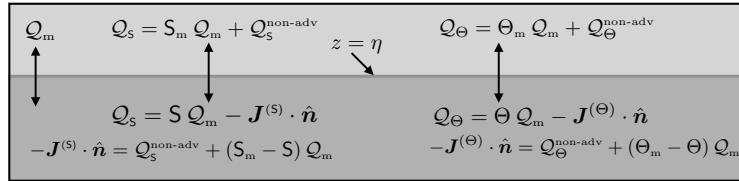


FIGURE 49.1: A schematic of an infinitesimal region of the ocean surface boundary at  $z = \eta(x, y, t)$ , with  $z < \eta$  the ocean.  $Q_m d\delta = Q_m dA$  is the mass transport (mass per time) that crosses the interface and carries a tracer concentration. We depict the case for salt concentration,  $S$ , and Conservative Temperature,  $\Theta$ , and the expressions for their net boundary fluxes.

This equation sets the level of diffusion on the ocean side of the surface boundary that is needed to generate the non-advectional transport. The diffusive mixing of salt and freshwater mediate the transfer of mass across the ocean surface so to incorporate that mass into the ambient ocean fluid. For example, freshwater added to the ocean ( $Q_f > 0$ ) diffuses downward as salt diffuses upward toward the surface.

#### *Salt dissolved within the mass transport*

In the case when salt is transported across the ocean boundary, as occurs with sea ice melting and formation, it does so largely dissolved in the water that is transported. There can also be a non-advectional transport, such as via parameterized turbulent fluxes, so that the net salt flux is given by

$$Q_S = S_m Q_m + Q_S^{\text{non-adv}}. \quad (49.65)$$

If there are more sources of this transfer then a relation such as this holds for each process. We are thus led to the net salt flux

$$Q_S = -[\rho S(\mathbf{v} - \mathbf{v}^{(\eta)}) + \mathbf{J}^{(S)}] \cdot \hat{\mathbf{n}} = S Q_m - \mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} = S_m Q_m + Q_S^{\text{non-adv}}. \quad (49.66)$$

which leads to the non-advectional salt flux on the ocean side of the boundary

$$-\mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} = Q_S^{\text{non-adv}} + (S_m - S) Q_m. \quad (49.67)$$

Figure 49.1 provides a schematic summary of the salt flux boundary condition. Furthermore, note that this boundary condition is consistent with that derived in Section 15.5.3 for a general tracer, in particular with equation (15.77).

#### *Treatment in observational analyses and numerical models*

In ocean climate modeling applications, the salt mass flux,  $Q_S$ , typically does not affect the kinematic boundary conditions. This approximation is reasonable given that the dominant contributor to the mass flux,  $Q_m$ , is the freshwater. Even so, there remains a net salt transported across the ocean surface in the presence of sea ice melt and formation. The above boundary conditions, in particular equations (49.66) and (49.67), remain unchanged. Furthermore, it is necessary to specify the boundary tracer concentration,  $S(z = \eta)$ . For salt, this value is typically set equal to that within the ocean model surface grid cell. This choice is also common for observation-based studies.

### 49.5.3 Conservative Temperature boundary condition

Conservative Temperature, potential temperature, potential vorticity, and passive tracers each satisfy the tracer equation (49.49), with distinct tracer flux vectors  $\mathbf{J}$ . However, they are not material tracers and so the kinematic constraints holding for salt do not hold for these other tracers. We describe the thermodynamic properties of Conservative Temperature in Section 21.8 and the processes affecting its boundary fluxes in Section 49.6. Here we begin our treatment of this tracer by outlining its surface boundary condition.

As per the general discussion in Section 15.5.3, the net surface boundary flux of Conservative Temperature is written

$$\mathcal{Q}_\Theta = \Theta_m \mathcal{Q}_m + \mathcal{Q}_\Theta^{\text{non-adv}} = [-\rho \Theta (\mathbf{v} - \mathbf{v}^{(\eta)}) + \mathbf{J}^{(\Theta)}] \cdot \hat{\mathbf{n}} = \Theta \mathcal{Q}_m - \mathbf{J}^{(\Theta)} \cdot \hat{\mathbf{n}}. \quad (49.68)$$

In this equation,  $\mathcal{Q}_\Theta^{\text{non-adv}}$  arises from the non-advection enthalpy fluxes outside the ocean domain that impact on the upper ocean interface, such as from radiant and turbulent fluxes, whereas  $\Theta_m$  is the Conservative Temperature of the boundary mass flux. Rearrangement leads to the net expression for the non-advection flux on the ocean side of the upper ocean boundary

$$-\mathbf{J}^{(\Theta)} \cdot \hat{\mathbf{n}} = \mathcal{Q}_\Theta^{\text{non-adv}} + (\Theta_m - \Theta) \mathcal{Q}_m, \quad (49.69)$$

where  $\Theta = \Theta(z = \eta)$  is the Conservative Temperature at the surface interface. A common assumption made for models and observational studies is to set  $\Theta_m - \Theta(z = \eta) = 0$ , in which case

$$-\mathbf{J}^{(\Theta)} \cdot \hat{\mathbf{n}} = \mathcal{Q}_\Theta^{\text{non-adv}} \text{ if } \Theta_m - \Theta(z = \eta) = 0. \quad (49.70)$$

Figure 49.1 provides a schematic summary of the  $\Theta$  flux boundary condition.

### 49.5.4 Comments and further reading

*Nurser and Griffies* (2019) offer further discussion of the kinematic boundary condition for salt and freshwater. We make use of many results from this section when discussing surface ocean buoyancy fluxes in Section 49.6 and water mass transformation in Section 50.6.

## 49.6 Surface boundary fluxes of buoyancy

As introduced in Chapter 24, buoyancy measures the gravitational acceleration of a fluid element relative to that of the fluid environment surrounding the element. A reduction in density for the fluid element is associated with an increase in buoyancy; that is, the fluid element becomes more *buoyant*. Changes in buoyancy arise through changes in density associated with temperature and salinity changes, with buoyancy changes computed relative to a fixed pressure level. In this way, buoyancy changes are directly related to processes that impact locally referenced potential density through changes in the temperature and salinity of a fluid element.

In this section we derive the equation describing the changes in ocean buoyancy due to enthalpy (commonly referred to as “heat”), salt, and water fluxes crossing the ocean boundaries. For this purpose, we expose certain of the issues associated with coupling numerical models of the ocean, atmosphere, and land. A detailed treatment of boundary layer physics is well outside of our scope. We thus take a phenomenological perspective, developing budget equations but not diving into details of the turbulent exchange of matter and enthalpy across the ocean surface boundary. Furthermore, we are only concerned with the upper ocean boundary, so that we ignore geothermal fluxes crossing the ocean bottom boundary.

### 49.6.1 Outlining the boundary fluxes of enthalpy and salt

Broadly, the boundary fluxes are associated with the following physical processes.

- Turbulent processes transfer enthalpy through latent and sensible heating.
- Longwave radiation cools the upper ocean, with this radiation affected by the upper ocean skin temperature.
- Penetrative shortwave radiation is absorbed in seawater and so increases buoyancy in regions where the thermal expansion coefficient is positive.<sup>7</sup>
- All of the above processes are referred to as *non-advection* transports. They are not associated with a net mass transport across the ocean surface. In contrast, advective processes transfer enthalpy and salt across the ocean surface through the transfer of mass across the interface.
- Salt is transferred between the liquid ocean and sea ice when sea ice melts and forms. This transfer is proportional to the water mass flux and the difference in salinity between the liquid ocean and sea ice. There may be additional turbulent salt fluxes as well, but there is a negligible transfer of salt associated with precipitation, evaporation, or river runoff.

### 49.6.2 Evolution from surface boundary fluxes

We now develop finite volume budget equations for potential enthalpy (via Conservative Temperature,  $\Theta$ ), salt, and seawater mass for a grid cell region next to the ocean surface, with a focus on contributions due to surface boundary fluxes. For that purpose, introduce the following quantities for a grid cell,

$$M = \int_{\text{cell}} \rho dV = \langle \rho \rangle V \quad V = \int_{\text{cell}} dV = A \bar{h} \quad A = \int_{\text{cell}} dA \quad (49.71\text{a})$$

$$\bar{h} A = \int_{\text{cell}} \left[ \int_{\text{cell}} dz \right] dA \quad \langle C \rangle M = \int_{\text{cell}} C \rho dV, \quad (49.71\text{b})$$

so that  $\langle \rho \rangle$  is the cell averaged density,  $\langle C \rangle$  is the cell mass weighted averaged tracer concentration,  $\bar{h}$  is the cell area averaged thickness,  $V$  is the cell volume, and  $A$  is the cell horizontal area. These definitions allow us to write

$$\frac{d}{dt} \left[ \int_{\text{cell}} \rho C dV \right] = \frac{d}{dt} [\langle C \rangle M] = A \frac{d}{dt} [\bar{h} \langle C \rangle \langle \rho \rangle], \quad (49.72)$$

where the horizontal area of a cell is assumed to be constant in time. The surface boundary fluxes have similar grid cell area averages.

Focusing just on contributions from surface boundary transport leads to the budget equations

$$\frac{\partial(\rho h \Theta)}{\partial t} = Q_m \Theta_m + Q_\Theta^{\text{non-adv}} \quad (49.73\text{a})$$

$$\frac{\partial(\rho h S)}{\partial t} = Q_m S_m + Q_S^{\text{non-adv}} \quad (49.73\text{b})$$

$$\frac{\partial(\rho h)}{\partial t} = Q_m, \quad (49.73\text{c})$$

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<sup>7</sup>The Baltic Sea is an outlier in the World Ocean, whose fresh and cold waters often realize a negative thermal expansion so that heating can increase rather than reduce density.

where we used a partial time derivative since we are holding the horizontal position fixed. Furthermore, we reduced notational clutter by dropping the angle brackets for volume average and the horizontal overline for area average. For a three-dimensional budget, the right hand side to these equations is combined with fluxes crossing interior cell boundaries. Finally, we wrote the fluxes as

$$Q_m A = \mathcal{Q}_m \mathcal{S} \quad \text{and} \quad Q_\Theta^{\text{non-adv}} A = \mathcal{Q}_\Theta^{\text{non-adv}} \mathcal{S} \quad \text{and} \quad Q_S^{\text{non-adv}} A = \mathcal{Q}_S^{\text{non-adv}} \mathcal{S}, \quad (49.74)$$

where  $\mathcal{S}$  is the area on the free surface and  $A$  is the corresponding horizontal area of the grid cell.

### 49.6.3 Buoyancy tendency from surface boundary fluxes

For many purposes, it is of interest to quantify the impacts on ocean buoyancy arising from surface boundary fluxes. For that purpose, we here develop the budget for buoyancy in a surface model grid cell region, focusing on surface flux contributions.

Buoyancy has a time tendency given by

$$-\frac{\rho_0}{g} \frac{\partial b}{\partial t} = \rho_\Theta \frac{\partial \Theta}{\partial t} + \rho_S \frac{\partial S}{\partial t}, \quad (49.75)$$

where we introduced the shorthand

$$\rho_\Theta = \left[ \frac{\partial \rho}{\partial \Theta} \right]_{S,p} \quad \text{and} \quad \rho_S = \left[ \frac{\partial \rho}{\partial S} \right]_{\Theta,p} \quad (49.76)$$

for the partial derivatives of density with respect to Conservative Temperature and salinity, respectively, each with pressure held constant. We wish to form an evolution equation for buoyancy at the ocean surface grid cell just due to the effects of surface forcing. For this purpose, multiply the temperature equation (49.73a) by  $\rho_\Theta$  and add to the salinity equation (49.73b) multiplied by  $\rho_S$

$$\rho_\Theta \left[ \frac{\partial(\rho h \Theta)}{\partial t} \right] + \rho_S \left[ \frac{\partial(\rho h S)}{\partial t} \right] = Q_m (\rho_\Theta \Theta_m + \rho_S S_m) + \rho_\Theta Q_\Theta^{\text{non-adv}} + \rho_S Q_S^{\text{non-adv}}. \quad (49.77)$$

Now use the mass budget (49.73c) and introduce the buoyancy tendency according to equation (49.75) to render an expression for the time tendency of the surface ocean buoyancy

$$-(\rho_0/g) \rho h \left[ \frac{\partial b}{\partial t} \right]^{\text{surface}} = Q_m [\rho_\Theta (\Theta_m - \Theta) + \rho_S (S_m - S)] + \rho_\Theta Q_\Theta^{\text{non-adv}} + \rho_S Q_S^{\text{non-adv}}. \quad (49.78)$$

Introducing the thermal expansion and saline contraction coefficients

$$\alpha = -\frac{1}{\rho} \left[ \frac{\partial \rho}{\partial \Theta} \right]_{S,p} \quad \text{and} \quad \beta = \frac{1}{\rho} \left[ \frac{\partial \rho}{\partial S} \right]_{\Theta,p} \quad (49.79)$$

yields

$$\left[ \frac{\partial b}{\partial t} \right]^{\text{surface}} = \frac{g}{\rho_0 h} \left( Q_m [\alpha (\Theta_m - \Theta) - \beta (S_m - S)] + \alpha Q_\Theta^{\text{non-adv}} - \beta Q_S^{\text{non-adv}} \right) \quad (49.80a)$$

$$= \frac{g}{\rho_0 h} \left( \alpha [Q_m (\Theta_m - \Theta) + Q_\Theta^{\text{non-adv}}] - \beta [Q_m (S_m - S) + Q_S^{\text{non-adv}}] \right). \quad (49.80b)$$

In regions where the thermal expansion coefficient is positive ( $\alpha_\Theta$ ), adding a boundary mass

$(Q_m > 0)$  that has  $\Theta_m > \Theta$  increases the buoyancy of the surface ocean; i.e., adding relatively warm water increases surface ocean buoyancy. Likewise, where the haline contraction coefficient is positive ( $\beta > 0$ ), adding boundary mass with  $S_m < S$  increases buoyancy of the surface ocean; i.e., adding relatively freshwater increases surface ocean buoyancy. The same behavior holds for the turbulent fluxes, where  $Q_\Theta^{\text{non-adv}} > 0$  (adding turbulent thermal energy to the ocean) increases surface ocean buoyancy whereas  $Q_S^{\text{non-adv}} > 0$  (adding salt to the ocean) decreases buoyancy. Finally, note that in some contexts it is useful to take the limit as the thickness,  $h$ , becomes vanishingly small and to introduce a Dirac delta (see Section 4.2) and thus write<sup>8</sup>

$$\left[ \frac{\partial b}{\partial t} \right]^{\text{surface}} = \frac{g \delta(z - \eta)}{\rho_0} \left( Q_m [\alpha (\Theta_m - \Theta) - \beta (S_m - S)] + \alpha Q_\Theta^{\text{non-adv}} - \beta Q_S^{\text{non-adv}} \right) \quad (49.81\text{a})$$

$$= \frac{g \delta(z - \eta)}{\rho_0} \left( \alpha [Q_m (\Theta_m - \Theta) + Q_\Theta^{\text{non-adv}}] - \beta [Q_m (S_m - S) + Q_S^{\text{non-adv}}] \right). \quad (49.81\text{b})$$

This form is of use when organizing processes according to interior processes and surface boundary processes, such as when considering water mass transformation analysis in Section 50.8.

#### 49.6.4 Comments

The buoyancy flux expression (49.80b) is of use for boundary layer parameterizations, such as the KPP scheme of [Large et al. \(1994\)](#) and [Van Roekel et al. \(2018\)](#). It is furthermore used when studying water mass transformations as reviewed by [Groeskamp et al. \(2019\)](#) and summarized in Chapter 50.

### 49.7 Global mean sea level

In this section we consider some basic features of global mean sea level by making use of the mass budget of liquid seawater. This analysis highlights the distinction between the mass budget and the volume (sea level) budget.

#### 49.7.1 Definitions and assumptions

Seawater mass is a conserved quantity so that the total liquid seawater mass,  $m$ , changes only via boundary mass fluxes

$$\frac{dm}{dt} = \mathcal{A} \overline{Q_m}, \quad (49.82)$$

where  $\mathcal{A}$  is the ocean surface area,  $\overline{Q_m}$  is the area averaged surface mass flux, and we assume there is no mass entering through the ocean bottom. The global volume of liquid seawater

$$V = m / \langle \rho \rangle \quad (49.83)$$

changes due to mass changes *and* changes to the global mean density,  $\langle \rho \rangle$ . Throughout this section we assume the surface area is constant in time, thus neglecting the relatively small changes associated with volume changes along sloping beaches. We also assume a temporally constant area averaged ocean bottom depth,  $\bar{H}$ . These two assumptions mean that changes in ocean volume arise just from changes in global mean sea level,  $\bar{\eta}$ . Since around the year 2000, measurements

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<sup>8</sup>From Section 4.2, we know that the Dirac delta,  $\delta(z - \eta)$ , has dimensions of inverse length, so that equation (49.81b) is dimensionally consistent.

estimate that global area mean sea level has increased at a rate of

$$\left[ \frac{d\bar{\eta}}{dt} \right]_{\text{observed}} \approx 3 \text{ mm yr}^{-1}, \quad (49.84)$$

and that this rate is increasing (positive sea level acceleration). As part of the analysis in this section we make use of the following phenomenological numbers and make a few assumptions to facilitate calculations.

- global seawater volume  $\mathcal{V} \approx 1.3 \times 10^{18} \text{ m}^3$
- global ocean surface area  $\mathcal{A} \approx 3.6 \times 10^{14} \text{ m}^2$
- global ocean mean density  $\langle \rho \rangle \approx 1035 \text{ kg m}^{-3}$
- specific heat capacity for seawater  $c_p \approx 3992 \text{ J kg}^{-1}\text{K}^{-1}$
- Ignore mass fluxes transported through the sea floor, which are small relative to surface mass fluxes.
- Ignore salinity and pressure effects on density, so that changes in global mean density arise just from changes in global mean Conservative Temperature.
- Assume a constant thermal expansion coefficient

$$\alpha = -\frac{1}{\rho} \left[ \frac{\partial \rho}{\partial \Theta} \right]_{S,p} \approx 2 \times 10^{-4} \text{ K}^{-1}. \quad (49.85)$$

This is not a great approximation, since the thermal expansion coefficient ranges over the ocean by a factor of 10. Nonetheless, for this section it is sufficient for deducing rough numbers that are consistent with errors in measurements for global boundary enthalpy and mass fluxes.

### 49.7.2 Budget for global mean sea level

Expression (49.83) for ocean volume leads to its time derivative

$$\frac{d\mathcal{V}}{dt} = \frac{1}{\langle \rho \rangle} \frac{dm}{dt} - \frac{m}{\langle \rho \rangle^2} \frac{d\langle \rho \rangle}{dt} \quad (49.86a)$$

$$= \frac{\mathcal{A} \overline{Q_m}}{\langle \rho \rangle} - \frac{\mathcal{V}}{\langle \rho \rangle} \frac{d\langle \rho \rangle}{dt}, \quad (49.86b)$$

where we used equation (49.82) to express mass changes in terms of the surface mass flux. Additionally, the ocean volume is given by

$$\mathcal{V} = \int dA \int_{-H}^{\eta} dz = \mathcal{A} (\overline{H} + \bar{\eta}), \quad (49.87)$$

so that its time changes arise from changes in the global mean sea level

$$\frac{d\mathcal{V}}{dt} = \mathcal{A} \frac{d\bar{\eta}}{dt}. \quad (49.88)$$

Combining the two volume equations (49.86b) and (49.88) yields the budget equation for global mean sea level

$$\frac{d\bar{\eta}}{dt} = \frac{\overline{Q_m}}{\langle \rho \rangle} - \frac{\mathcal{V}}{\mathcal{A} \langle \rho \rangle} \frac{d\langle \rho \rangle}{dt}. \quad (49.89)$$

The first term arises from changes in ocean mass whereas the second term arises from changes in global mean seawater density.

### 49.7.3 Changes due to mass input

To ground these formulae in phenomenology, assume that a surface mass flux gives one-half of the observed sea level rise

$$\frac{1}{2} \left[ \frac{d\bar{\eta}}{dt} \right]_{\text{observed}} = \frac{\overline{Q_m}}{\langle \rho \rangle}. \quad (49.90)$$

This distribution of measured sea level is roughly correct. With  $\langle \rho \rangle = 1035 \text{ kg m}^{-3}$  and  $d\bar{\eta}/dt \approx 3 \text{ mm yr}^{-1}$ , we need an area averaged mass flux across the ocean surface

$$\overline{Q_m} \approx 5 \times 10^{-8} \text{ kg m}^{-2} \text{ s}^{-1}. \quad (49.91)$$

Integrated over the global ocean area, this flux leads to a mass transport of

$$\mathcal{T} = \mathcal{A} \overline{Q_m} \approx 1.8 \times 10^7 \text{ kg s}^{-1} \approx 0.015 \times \mathcal{T}^{\text{river}}. \quad (49.92)$$

That is, global mean sea level rises at a rate of  $1.5 \text{ mm yr}^{-1}$  if there is a net additional mass added to the ocean equal to roughly 1.5% of the net river water entering the ocean,  $\mathcal{T}^{\text{river}}$ . This additional net mass is largely coming from the melting of land-ice.

### 49.7.4 Steric changes due to changes in density

Steric effects generally refer to properties of a substance associated with the space occupied by atoms. In the sea level context, steric effects refer to changes in sea level associated with density changes, with changes in density associated with changes in the volume occupied by seawater molecules. Changes in global mean sea level arising from changes in the global mean density are called global steric sea level changes. From the sea level budget equation (49.89) we know that steric changes are written mathematically as

$$\left[ \frac{d\bar{\eta}}{dt} \right]_{\text{steric}} \equiv - \frac{\mathcal{V}}{\mathcal{A} \langle \rho \rangle} \frac{d\langle \rho \rangle}{dt}. \quad (49.93)$$

Global mean density will change primarily from changes in global mean Conservative Temperature. If we assume the ocean thermal expansion is constant, then

$$\frac{1}{\langle \rho \rangle} \frac{d\langle \rho \rangle}{dt} = -\alpha \frac{d\langle \Theta \rangle}{dt}, \quad (49.94)$$

so that steric sea level changes are primarily driven by *thermosteric* effects

$$\left[ \frac{d\bar{\eta}}{dt} \right]_{\text{thermosteric}} \equiv \frac{\alpha \mathcal{V}}{\mathcal{A}} \frac{d\langle \Theta \rangle}{dt}. \quad (49.95)$$

With  $\alpha \approx 2 \times 10^{-4} \text{ K}^{-1}$  and  $d\bar{\eta}/dt \approx 1.5 \text{ mm yr}^{-1}$ , we have

$$\frac{d\langle\Theta\rangle}{dt} \approx 0.2 \text{ K century}^{-1}. \quad (49.96)$$

That is, a global thermosteric sea level rise of  $1.5 \text{ mm yr}^{-1}$  corresponds to a rate of increase in the global volume mean ocean temperature of roughly  $0.2 \text{ K century}^{-1}$ .

### 49.7.5 Enthalpy flux imbalances giving rise to thermosteric sea level

A global mean ocean temperature change can arise from an area averaged surface ocean enthalpy flux

$$\overline{Q_H} \approx \langle \rho \rangle c_p \overline{H} \frac{d\langle\Theta\rangle}{dt}. \quad (49.97)$$

Plugging in numbers leads to the enthalpy flux

$$\overline{Q_H} \approx 1 \text{ W m}^{-2}. \quad (49.98)$$

That is, a surface ocean enthalpy flux of roughly  $1 \text{ W m}^{-2}$  (ocean area normalized) gives rise to a global mean thermosteric sea level rise of roughly  $1.5 \text{ mm yr}^{-1}$ .

An enthalpy flux of  $1 \text{ W m}^{-2}$  is small compared to, say, that crossing the surface of a typical light bulb. However,  $1 \text{ W m}^{-2}$  is comparable to that accumulating within the earth system due to increases in greenhouse gases (Otto et al., 2013). That is,  $1 \text{ W m}^{-2}$  averaged over the global ocean, or  $0.7 \text{ W m}^{-2}$  averaged over the surface area of the planet,<sup>9</sup> is roughly the net heating associated with anthropogenic climate change. Such seemingly small increases in surface heating represent a nontrivial increase in the earth's energy budget that are leading to the observed sizable climate changes and sea level rise.

A specific means to gauge the magnitude of  $1 \text{ W m}^{-2}$  distributed over the ocean surface area,  $\mathcal{A}$ , is to compare to the enthalpy flux due to blasting one atomic bomb per second ( $\Delta t = 1 \text{ s}$ ) and uniformly distributing its released energy over the ocean surface area every second.  $\mathcal{E}_{\text{bomb}} \approx 6.3 \times 10^{13} \text{ J}$  distributed over the ocean area each second corresponds to a surface ocean enthalpy flux of

$$Q_{\text{bomb}} = \frac{\mathcal{E}_{\text{bomb}}}{\mathcal{A} \Delta t} \approx 0.17 \text{ W m}^{-2}. \quad (49.99)$$

Hence, an enthalpy flux of  $1 \text{ W m}^{-2}$  due to anthropogenic climate warming corresponds to  $1/0.17 \approx 6$  bombs per second. This way of framing the net heating of the ocean due to anthropogenic climate change dramatically illustrates the huge magnitude of the heating created by the burning of carbon based energy sources.

### 49.7.6 Global sea level in a Boussinesq fluid

The sea level for a Boussinesq ocean evolves according to the kinematic free surface equation (16.8)

$$\partial_t \eta^{\text{bouss}} = -\nabla \cdot \mathbf{U} + Q_m/\rho_0, \quad (49.100)$$

where

$$\mathbf{U} = \int_{-H}^{\eta} \mathbf{u} dz \quad (49.101)$$

is the depth integrated horizontal velocity and  $\rho_0$  is the Boussinesq reference density. This equation results from ignoring all changes to density, except for those related to the buoyancy force

<sup>9</sup>The ocean covers roughly 70% of the earth surface.

appearing in the momentum equations. Integrating the sea surface height equation (49.100) over the surface area of the global ocean reveals that the global mean Boussinesq sea level evolves according to

$$\frac{d\bar{\eta}^{\text{bouss}}}{dt} = \frac{\overline{Q_m}}{\rho_0}. \quad (49.102)$$

Hence,  $\bar{\eta}^{\text{bouss}}$  changes only so long as there are boundary mass fluxes. In contrast to the real ocean, the sea level computed from a Boussinesq ocean is unaffected by a surface enthalpy flux,  $\overline{Q_H} \neq 0$ . This result in turn means that we cannot use the prognostic sea surface height,  $\eta^{\text{bouss}}$ , level from a Boussinesq ocean model to compute changes the global mean sea level. Instead, corrections are required, as first identified by [Greatbatch \(1994\)](#) and further detailed in Appendix D of [Griffies and Greatbatch \(2012\)](#).

#### 49.7.7 Global halosteric sea level changes are negligible

When freshwater enters the ocean, such as from melting continental ice sheets, it adds to the ocean mass and in turn increases global mean sea level. This change is referred to as *barystatic sea level change* according to the sea level terminology paper from [Gregory et al. \(2019\)](#). Although ocean salinity changes upon changing the freshwater content, the net effect on global mean sea level is almost entirely barystatic since the global halosteric effect is negligible. We can understand why the global halosteric effect is so tiny by recognizing that freshwater entering the ocean sees its salinity increase whilst the ambient seawater is itself freshened. These compensating salinity changes (which are often mistakenly ignored) have corresponding compensating sea level changes, thus bringing the global halosteric effect to near zero. Appendix B of [Gregory et al. \(2019\)](#) works through a two-bucket thought experiment where one bucket holds freshwater and the other holds seawater, with the Conservative Temperature and pressures identical for the two buckets. They compute how the total water volume changes upon homogenizing the water in the two buckets, while conserving the masses of freshwater and salt. Their result shows that the total volume of homogenized water equals to the sum of the volume initially in the two separate buckets to within 0.1%. Hence, the change in volume is almost entirely barystatic, with the global halosteric effect entirely negligible when considering global sea level changes.

#### 49.7.8 Further study

The discussion of steric and thermosteric sea level changes are further explored in [Griffies and Greatbatch \(2012\)](#) and [Griffies et al. \(2014\)](#). The global halosteric discussion is based on Appendix B of the sea level terminology paper from [Gregory et al. \(2019\)](#). The [Gregory et al. \(2019\)](#) paper is also notable for providing a conceptual rationalization of the often confusing terminology used in sea level studies.



# Chapter 50

## Water mass transformation analysis

A *water mass* refers to a region of seawater characterized by a suite of quasi-homogeneous properties used to distinguish this water from other water masses. Water masses are typically formed through surface boundary processes. As these waters enter the ocean interior they are advected over basin scales while they are also eroded or *transformed* by irreversible mixing processes. Water masses offer a conceptual means to partition or bin the ocean into distinct classes whose origin, movement, and transformation can be measured, modeled, and studied. Scalar properties generally used to classify water masses are simpler to measure than vector properties such as velocity. Hence, a water mass perspective offers the means to infer ocean circulation within water mass space without directly measuring the velocity.

In this chapter we develop the mathematical and physical basis for *water mass analysis* and its extension to *tracer mass analysis*. This formalism considers the budgets for seawater mass and tracer mass within layers or classes defined by properties such as buoyancy, Conservative Temperature, salinity, or biogeochemical tracers. It offers a framework for understanding certain facets of geophysical fluid mechanics that is distinct from the more familiar Eulerian and Lagrangian methods used in fluid mechanics. It has thus found use throughout oceanography and atmospheric sciences.

Readers of this chapter may appreciate the following paraphrase from A. Sommerfeld's quote given in the thermodynamics Chapter 20.

Water mass analysis appears somewhat mysterious and puzzling on first encounter. On second encounter things start to fall into place, except perhaps for a few pesky math niceties. On third encounter, when deciding to do calculations, one returns to that unsettled feeling of the first encounter. However, by now, familiarity with the words and maths means that the mystery presents no practical bother. One simply turns the crank without thinking too much about the underlying foundations.

In hopes of partially dispelling the mystery, and maintaining an appreciation for the foundations, we here couple the many mathematical equations with schematics and conceptual descriptions. Even so, there should be no presumption that this subject can be mastered without a healthy degree of head-scratching.

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## CHAPTER GUIDE

The development in this chapter requires the vector calculus encountered in Chapter 2; elements of the generalized vertical coordinates from Chapters 41 and 42; kinematics from Chapter 14; tracer budgets from Chapter 15; advection and diffusion maths in Chapter 46, and features of parameterized tracer transport and mixing discussed in Chapter 48. This is a rather long chapter that works through a number of related budget analyses with the aim to ground the theory with examples motivated from the growing literature.

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50.1	Conceptual framework . . . . .	1243
50.1.1	Water mass configuration space . . . . .	1243
50.1.2	A novel kinematic lens . . . . .	1244
50.1.3	Transformation and formation . . . . .	1245
50.2	Buoyancy transformation and formation . . . . .	1245
50.2.1	A three-layer thought experiment . . . . .	1246
50.2.2	How processes lead to transformations . . . . .	1247
50.3	Mathematical framework . . . . .	1248
50.3.1	Seawater mass in an infinitesimal cylinder . . . . .	1249
50.3.2	Seawater mass within a finite region . . . . .	1250
50.3.3	Seawater mass distribution/density function . . . . .	1250
50.3.4	Example regions . . . . .	1250
50.3.5	Integrals of arbitrary functions . . . . .	1253
50.3.6	Moments of $\lambda$ . . . . .	1253
50.3.7	Internal and external $\lambda$ -moments . . . . .	1254
50.3.8	Further study . . . . .	1255
50.4	Water mass transformation across a $\lambda$ -surface . . . . .	1255
50.4.1	Dia-surface flux and interior transformation . . . . .	1255
50.4.2	Transformation as the derivative of an integral . . . . .	1256
50.4.3	Processes and kinematics . . . . .	1257
50.4.4	Some details concerning interior transformation . . . . .	1259
50.5	Budget for seawater mass in a $\Delta\lambda$ -layer . . . . .	1261
50.5.1	Transport crossing interior open boundaries . . . . .	1261
50.5.2	Mass transport crossing the ocean surface . . . . .	1261
50.5.3	Mass budget . . . . .	1262
50.6	Budget for $\lambda$ mass in a $\lambda_\infty$ -region . . . . .	1262
50.6.1	Processes affecting the mass of $\lambda$ -stuff . . . . .	1263
50.6.2	Summary of the $\lambda$ budget . . . . .	1265
50.6.3	Processes leading to water mass transformation . . . . .	1265
50.7	Surface water mass transformation . . . . .	1267
50.7.1	Circulation driven by surface transformation . . . . .	1267
50.7.2	Further study . . . . .	1268
50.8	Buoyancy water mass transformation . . . . .	1268
50.8.1	Material time changes to $S$ and $\Theta$ . . . . .	1268
50.8.2	Interior buoyancy water mass transformation . . . . .	1269
50.8.3	Surface non-advectional flux for $S$ and $\Theta$ . . . . .	1270
50.8.4	Surface buoyancy water mass transformation . . . . .	1270
50.9	Tracer mass analysis . . . . .	1271
50.9.1	General form of the mass budget . . . . .	1272
50.9.2	Tracer processes . . . . .	1273
50.9.3	Transport across an interior layer interface . . . . .	1274
50.9.4	Transport across interior and surface boundaries . . . . .	1274
50.9.5	The layer tracer budget . . . . .	1275
50.9.6	Further study . . . . .	1275

---

50.10 Regions bounded by a tracer contour/surface . . . . .	1275
50.10.1 Closed region bounded by a tracer surface/contour . . . . .	1276
50.10.2 Region with $C \geq \tilde{C}$ . . . . .	1277
50.10.3 Comments and further study . . . . .	1279

## 50.1 Conceptual framework

Water mass analysis is a mathematical formalism supporting the study of budgets for seawater mass and tracer mass within layers or classes defined by properties such as Archimedean buoyancy (Chapter 24; shortened to “buoyancy” here), Conservative Temperature, salinity, or biogeochemical tracers. Water mass analysis is concerned with processes affecting the evolution of fluid within layers and in the characterization of circulation inferred from this evolution. This analysis is quite useful for oceanography since it is common to describe ocean geography in terms of characteristic water properties, with such properties often originating through extremely large buoyancy fluxes at the high latitudes that form waters such as the Antarctic Bottom Water (AABW) and North Atlantic Deep Water (NADW). Our goals here are fundamental, so that we do not delve into the phenomenology of ocean water masses. Rather, we dive into the maths and physics underlying the method.

We speak of a *water mass configuration space*, in which some or all of the coordinates of this space are determined by properties other than geographic/depth coordinates.<sup>1</sup> For example, Figure 50.1 provides an example configuration space described by  $(S, \Theta, p)$ , whereby a fluid element has its position in water mass configuration space<sup>2</sup> determined by its Conservative Temperature,  $\Theta$ , salinity,  $S$ , and pressure,  $p$ . We may also consider the water mass configuration space defined by binning the ocean according to potential density classes, or some other measure of buoyancy. We can also retain some degree of geographical information through binning according to latitude and buoyancy. Note that there is no implied constraint that the buoyancy surfaces remain stably stratified in the vertical, nor indeed that any of the water mass coordinates retain a 1-to-1 relation with geographic/depth space. We have more to say on this point in the following.

### 50.1.1 Water mass configuration space

We specify the position of a fluid element within water mass configuration space by specifying a list of properties and/or spatial information. That is, we can choose any number of properties or geographical coordinates to specify water mass configuration space. Consequently, water mass configuration space has an arbitrary number of dimensions. We furthermore observe that water mass configuration space generally has no metric<sup>3</sup>, particularly when none of the chosen coordinates are geographical (latitude or longitude) or depth. Hence, there is generally no notion of distance or angles between points in water mass configuration space. Indeed, what does it mean to be orthogonal and temperature-salinity space or when studying the density-binned distribution of seawater?

The absence of a metric is something we have already seen when studying thermodynamic configuration space in Chapter 20, with mention of this point given in Section 20.1.5. Mathematically, we say that both thermodynamic configuration space and water mass configuration space

<sup>1</sup>We prefer the term “configuration space” over the alternative “phase space”, since phase space in Hamiltonian dynamics specifically refers to position and momentum coordinates. In contrast, configuration space, as used in our discussion of water masses, can be determined by most any property or geographic position.

<sup>2</sup>This water mass configuration space also serves as a thermodynamic configuration space when using the Gibbs potential discussed in Section 20.7.6.

<sup>3</sup>See Section 7.1 for a discussion of metric tensors, which are needed to measure distance on a manifold.

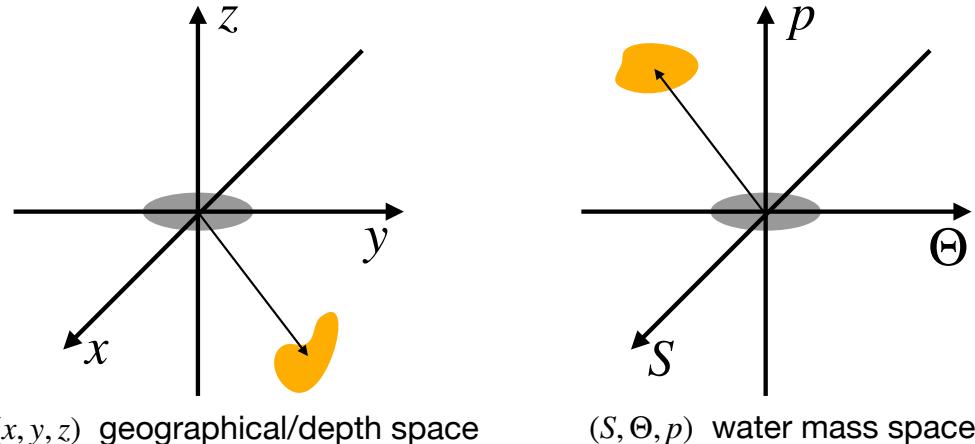


FIGURE 50.1: Left panel: a fluid element is positioned in geographical/depth space ( $x, y, z$ ) according to its horizontal ( $x, y$ ) (longitude, latitude) position and its vertical geopotential,  $z$ . Right panel: the same fluid element is positioned in a particular water mass configuration space, here defined by  $(S, \Theta, p)$  with salinity,  $S$ , Conservative Temperature,  $\Theta$ , and pressure,  $p$ . Mapping between the two spaces is generally not 1-to-1. Namely, a point in configuration space can be occupied by more than one point in geographical space since more than a single point in geographical space can have the same values for  $(S, \Theta, p)$ . Although the coordinate axes are depicted as mutually orthogonal in the right panel, there is no objective means to determine angles in water mass configuration space since it contains no metric. That is, water mass configuration space, just as thermodynamic state space (Section 20.1.5), is a *differentiable manifold*.

are *differentiable manifolds*. Even so, one commonly sees a point in thermodynamic space depicted on a diagram with orthogonal axes (e.g., pressure-volume diagrams), or a position in water mass configuration space similarly depicted with orthogonal axes as in Figure 50.1. However, this depiction is arbitrary since there is no geometric structure afforded to such spaces since there is no metric tensor, which in turn means we cannot determine angles or orthogonality. Depictions with orthogonal axes merely satisfy a subjective desire for geometric structure when in fact there is none afforded to the manifold. Differential forms provide a suitable formalism for conducting calculus on a differential manifold sans a metric as detailed by [Nurser et al. \(2022\)](#).

### 50.1.2 A novel kinematic lens

A water mass configuration space views the ocean circulation through the lens afforded by layers or classes. This perspective contrasts to the fixed points or regions of an Eulerian perspective, or the moving fluid particles or corresponding fluid regions of a Lagrangian perspective. Hence, the kinematic perspective of water mass analysis complements that from the Eulerian and Lagrangian kinematics encountered in other parts of this book (see Chapter 12 for a reminder of Eulerian and Lagrangian kinematics).

A point in water mass configuration space can be comprised of many points in geographic/depth space. Hence, there is no presumption of a 1-to-1 mapping between geographic/depth space and water mass configuration space. This situation is familiar to descriptive oceanographers who well know that there can be more than one fluid element in the ocean that has a particular  $(S, \Theta, p)$  value. Or more precisely, when classifying seawater according to binned values,  $(\Theta \pm \Delta\Theta/2, S \pm \Delta S/2, p \pm \Delta p/2)$ , fluid elements from any part of the ocean can fit into a particular bin so that a distribution of seawater in water mass configuration space is non-local in geographical/depth space. Even when classifying seawater according to latitude, longitude, and potential density, the possible case of a non-monotonic vertical potential density profile means that there is generally no 1-to-1 mapping between potential density and depth.

The lack of 1-to-1 mapping between water mass configuration space and geographic/depth

space is a fundamental kinematic distinction from the 1-to-1 relation that holds between the Eulerian and Lagrangian descriptions of fluid motion (see Chapter 12). This property can be frustrating since circulation viewed in water mass configuration space generally has incomplete geographic/depth information, and yet oceanographers wish to know where on the planet something is happening.<sup>4</sup> Conversely, abandoning the 1-to-1 relation is liberating since water mass configuration space provides a framework to infer ocean circulation, within the water mass space, even without measuring velocity of the fluid in geographical space. Correspondingly, viewing ocean circulation through a water mass lens can offer understanding that complements traditional Eulerian or Lagrangian views.

### 50.1.3 Transformation and formation

Water moves through water mass configuration space as it is modified or *transformed* by irreversible boundary and interior ocean processes.<sup>5</sup> Such processes lead to material changes in fluid elements through mixing, solar radiation, and chemical reactions. The convergence (i.e., the local imbalance) of such transformation processes leads to the *formation* and destruction of water mass classes. As water moves through water mass configuration space we are afforded a distinct view of ocean circulation that has both direct and indirect connections to circulation in geographical/depth space. Notably, and quite trivially, we measure zero motion along a coordinate axis in water mass configuration space when the property defining that axis remains unchanged. For example, adiabatic and isohaline processes such as linear waves can render nontrivial motion in geographical/depth space whereas they lead to no motion in  $(S, \Theta)$  space.

If one is interested in reversible processes then water mass configuration space generally offers an inappropriate kinematic perspective. Furthermore, given the possible non-local  $(x, y, z)$  aspects of water mass configuration space, it provides an unnatural venue to study forces and stresses acting between spatially adjacent fluid elements. Hence, momentum dynamics is better handled via Eulerian or Lagrangian kinematics. Where water mass configuration space shines is by revealing the dynamics associated with irreversible processes that affect properties defining the water mass classes. For example, a water mass perspective has found use in framing key questions of primary interest in the Anthropocene, such as ocean buoyancy and its transformation through interior and boundary mixing, ocean heat uptake and transport, the hydrological cycle, steric sea level rise, and irreversible changes to biogeochemical properties (see [Groeskamp et al. \(2019\)](#) for a review with many references).

## 50.2 Buoyancy transformation and formation

Archimedean buoyancy is a common property used to distribute seawater, this buoyancy commonly approximated by potential density (Chapter 24). In this section we introduce the notions of *transformation* and *formation* when partitioning the ocean according to density ( $\gamma$ ) classes that locally measure buoyancy.<sup>6</sup> The ideas presented here extend to any scalar property used to bin the ocean fluid.

Water mass *transformation* measures the mass per time of water that moves across an iso-surface in space, or moves from one bin to another within a distribution. By convention, the transformation is positive if water moves to larger density (more generally to a larger value for

<sup>4</sup>Auxiliary methods such as the water tagging method of [Groeskamp et al. \(2014\)](#) can be used to recover some geographical information.

<sup>5</sup>In many parts of this book the word “transformation” refers to coordinate transformations. Here, “transformation” refers to a process acting to irreversibly change seawater properties.

<sup>6</sup>Many researchers make use of the *neutral density* coordinate defined by [Jackett and McDougall \(1997\)](#).

the property defining the layer or class) and negative if it enters a lighter density layer (smaller value for the property). Water mass *formation* refers to the difference in transformation across the surfaces bounding a layer, so that formation measures the change in mass of the layer. That is, *formation is the layer integrated convergence of transformation in water mass configuration space.*

Both transformation and formation have dimensions of mass per time (or volume per time when considering Boussinesq fluids) and are typically measured in Sverdrup units:

$$1 \text{ Sv} = 10^6 \text{ m}^3 \text{ s}^{-1} \quad \text{volume-Sverdrup} \quad (50.1a)$$

$$1 \text{ Sv} = 10^9 \text{ kg s}^{-1} \quad \text{mass-Sverdrup.} \quad (50.1b)$$

The volume-Sverdrup is commonly used in Boussinesq fluids with kinematics based on volume conservation (Chapter 23), whereas the mass-Sverdrup is commonly used in non-Boussinesq fluids whose kinematics is based on mass conservation. Even so, the mass-Sverdrup can be used for Boussinesq fluids merely by multiplying the volume-Sverdrup by the constant Boussinesq reference density,  $\rho_0$ .

### 50.2.1 A three-layer thought experiment

To illustrate the concepts of transformation and formation, bin the World Ocean into density classes, thus ignoring all geographic and depth information. Furthermore, assume only three density classes bounded by four density interfaces:

$$\text{light density layer} = [\gamma - \delta\gamma/2, \gamma + \delta\gamma/2] \quad (50.2a)$$

$$\text{middle density layer} = [\gamma + \delta\gamma/2, \gamma + 3\delta\gamma/2] \quad (50.2b)$$

$$\text{heavy density layer} = [\gamma + 3\delta\gamma/2, \gamma + 5\delta\gamma/2], \quad (50.2c)$$

where  $\delta\gamma > 0$  is the size for the density bins. Figure 50.2 depicts a sample mass distribution; i.e., the mass census for seawater binned into these three density layers.<sup>7</sup> Now introduce a process that results in water leaving the middle density layer and entering both the light layer and the heavy layer. Let  $G(\sigma)$  measure the mass per time that water crosses the density interface  $\gamma = \sigma$ ; i.e.,  $G(\sigma)$  is the transformation. This particular thought experiment has the following transformations across the various layer interfaces

$$G(\sigma) = \begin{cases} 0 & \sigma = \gamma - \delta\gamma/2 \quad \text{closed boundary} \\ < 0 & \sigma = \gamma + \delta\gamma/2 \quad \text{mass moves to light density from middle density} \\ > 0 & \sigma = \gamma + 3\delta\gamma/2 \quad \text{mass moves from middle density to heavy density} \\ 0 & \sigma = \gamma + 5\delta\gamma/2 \quad \text{closed boundary.} \end{cases} \quad (50.3)$$

The difference in the transformation across the interface boundaries of a particular layer determines the formation/destruction of water into that layer. Here, the convergence of water into the light and heavy layers means that there is a positive formation of water in these two density layers. In contrast, the divergence of water from the middle density layer means there is a negative formation or a destruction of some of its water. We write these layer formations mathematically

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<sup>7</sup>A realistic ocean experiences boundary forcing that makes the maximum and minimum density a function of time. It is thus common to fix the lower density limit to be well below the lightest water in the ocean and the upper density limit well above the maximum density, thus ensuring that all seawater is contained by the chosen binning. We introduce such “infinity” bounds in Section 50.3.3.

as follows

$$\text{light-formation} = -[G(\gamma + \delta\gamma/2) - G(\gamma - \delta\gamma/2)] > 0 \quad (50.4a)$$

$$\text{middle-formation} = -[G(\gamma + 3\delta\gamma/2) - G(\gamma + \delta\gamma/2)] < 0 \quad (50.4b)$$

$$\text{heavy-formation} = -[G(\gamma + 5\delta\gamma/2) - G(\gamma + 3\delta\gamma/2)] > 0. \quad (50.4c)$$

The minus sign out front emphasizes that the formation is the layer integrated *convergence* of the transformation.

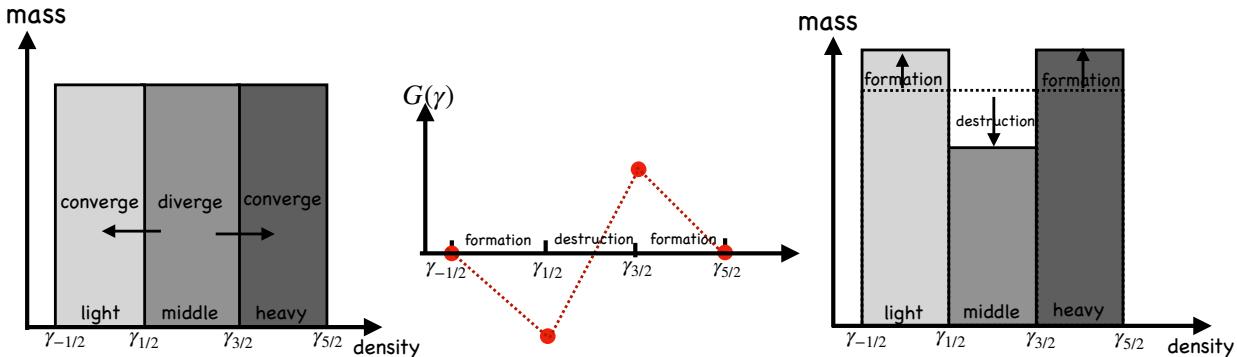


FIGURE 50.2: A sample mass distribution of the ocean binned into density layers (light, middle, heavy) bounded by the four density interfaces:  $\gamma_{n/2} = \gamma + n\delta\gamma/2$  for  $n = -1, 1, 3, 5$ . The left panel depicts an ocean state with equal mass in each layer. Some process is then imagined to cause water to diverge from the middle layer and converge to the light and heavy layers. The right panel shows the mass distribution after the water has moved, so that the middle layer has experienced a negative *formation* (i.e., net loss of mass) whereas the light and heavy layers have experienced a positive *formation* (i.e., net mass gain). The middle panel depicts the *transformation*,  $G$ , which measures the mass per time moving across the layer boundaries. By convention,  $G > 0$  for water moving into a heavier density layer and  $G < 0$  for water entering a lighter density layer. The addition of more layers refines the picture (e.g., by smoothing the plot of  $G$ ) but it does not modify the basic ideas illustrated in this thought experiment.

### 50.2.2 How processes lead to transformations

The central focus of water mass analysis is the movement of water between layers or classes, with this movement modifying the water mass distribution. Here we outline a few of the processes that affect this movement within water mass space, again focusing on buoyancy yet with an easy generalization to any other property that defines the water mass. Notably, we are not concerned with whether the fluid element moves, the boundary moves, or both, since it is only the relative motion that changes the water mass distribution. Indeed, we cannot determine motion of the fluid element without direct information about the velocity field. We return to this point when providing a mathematical expression for these ideas in Section 50.4.1.

#### *Interior transformation from mixing*

Mixing moves water across layer boundaries, with properties materially modified in the presence of mixing (so long as there are spatial gradients in the property). For example, recall our discussion in Chapter 15 where we saw that mixing causes tracers to move between fluid elements even as mixing does not alter the net mass of fluid elements (see the discussion of barycentric velocity in Section 15.1.2). Hence, in the presence of mixing, seawater fluid elements retain a fixed mass and yet the mass is redistributed among layers defined by property isosurfaces since the isosurfaces move in the presence of mixing.

### Surface mass fluxes

Rain and evaporation alter the mass of the ocean. In turn, the layers where rain and evaporation occur; i.e., layers that outcrop, will have their mass altered. Additionally, if the buoyancy of the mass flux differs from that of the ocean layer that it enters/leaves, then the buoyancy of the ocean layer is modified.

### Surface and bottom boundary transformation

Buoyancy surfaces that outcrop at the ocean surface or incrop at the ocean bottom are exposed to strong boundary fluxes that generally modify the buoyancy of the fluid within a layer. This modification in turn causes the layer boundaries to move so that the mass distributed within the layers is modified. A particularly striking example occurs in the upper ocean boundary layer where surface forcing leads to the seasonal migration of density outcrops. The associated lateral movement of density layers causes water to entrain and detrain from a layer since the layer boundaries can move faster than fluid elements. In so doing, the seasonal cycle of surface buoyancy forcing can inflate or deflate a buoyancy layer by moving the layer boundaries so that the layer entrains or detrains mass.

Penetrative shortwave radiation provides another means to modify water masses, with penetrative radiation a function of the optical properties of the fluid. This radiation provides a source of heating that can penetrate into the upper few tens of meters in the ocean, and can impact on the temperature and density structure of the ocean layers affected by radiation.

Finally, we note that layers that intersect the ocean bottom are exposed to geothermal heating as well as enhanced mixing from bottom boundary layer mixing. Each of these processes affects a transformation of the buoyancy, thus modifying the buoyancy layer interfaces and mass distribution within the layers.

### Interior sources and sinks

When studying water masses defined by biogeochemical tracers (e.g., carbon, oxygen, nutrients), there are a variety of chemical reactions and biological processes that act to modify these properties. These processes generally cannot be represented mathematically as the convergence of a flux. They are thus sometimes referred to as “non-conservative” processes (see Section 21.10).

## 50.3 Mathematical framework

In this section we develop a suite of mathematical tools of use to quantify the conceptual ideas presented in Sections 50.1 and 50.2. In particular, we develop a formalism for integrating properties within a region bounded by isosurfaces of a scalar field,  $\lambda = \lambda(\mathbf{x}, t)$ . The formulation is given from both a geometric perspective afforded by geographic/depth space, and a complementary distributional perspective afforded by binning seawater mass according to  $\lambda$ -classes. As in our study of Eulerian and Lagrangian kinematics elsewhere in this book, it is here useful to be adept at both the geographic/depth space perspective and the distributional perspective.

In Section 50.2 we assumed  $\lambda$  is the buoyancy field,  $\lambda = \gamma$ , whereas here we assume it is a generic scalar field,  $\lambda(\mathbf{x}, t)$ . In contrast to the case of a generalized vertical coordinate (Chapters 41 and 42), we make no assumption regarding the stratification of  $\lambda$ . Rather,  $\lambda$ -isosurfaces are free to overturn or even to be situated in spatially disconnected regions. This freedom is motivated by the behavior of most oceanographic scalar properties, which commonly exhibit vertically unstratified or negatively stratified profiles, particularly within boundary layers.

### 50.3.1 Seawater mass in an infinitesimal cylinder

Consider the calculation of seawater mass within an infinitesimal  $\lambda$ -layer bounded by two isosurfaces,  $[\lambda - \delta\lambda/2, \lambda + \delta\lambda/2]$ , as in Figure 50.3. The mass within a tiny cylinder extending from one interface to the other is given by the seawater density,  $\rho$ , multiplied by the volume of the cylinder,<sup>8</sup>

$$\delta M = \rho \delta V = \rho \delta h \delta \mathcal{S}, \quad (50.5)$$

where  $\delta \mathcal{S}$  is the cross-sectional area element and  $\delta h$  is the layer thickness. The geometric thickness,  $\delta h$ , is related to the differential  $\lambda$ -increment separating the two interfaces according to

$$\delta \lambda = \nabla \lambda \cdot \delta \mathbf{x} = |\nabla \lambda| \hat{\mathbf{n}} \cdot \delta \mathbf{x} = |\nabla \lambda| \delta h \quad \text{with} \quad \hat{\mathbf{n}} = \nabla \lambda |\nabla \lambda|^{-1}, \quad (50.6)$$

where  $\delta \mathbf{x}$  is a position vector connecting points on the two interfaces. We thus see that the layer thickness is given by

$$\delta h = \frac{\delta \lambda}{|\nabla \lambda|}, \quad (50.7)$$

which connects a geometric property of the layer,  $\delta h$ , to the  $\lambda$ -increment,  $\delta \lambda > 0$ . For a given  $\lambda$ -increment, the layer thickness is smaller with more tightly packed  $\lambda$ -isosurfaces as reflected by a larger  $|\nabla \lambda|$ . Furthermore, the geometric thickness is oriented according to the normal direction,  $\hat{\mathbf{n}}$ , so that  $\delta h$  measures the distance between the  $\lambda$ -interfaces in the direction of the normal direction. It follows that the seawater mass within the cylinder is given by

$$\delta M = \rho \delta V = \rho \delta h \delta \mathcal{S} = \frac{\rho \delta \lambda \delta \mathcal{S}}{|\nabla \lambda|}. \quad (50.8)$$

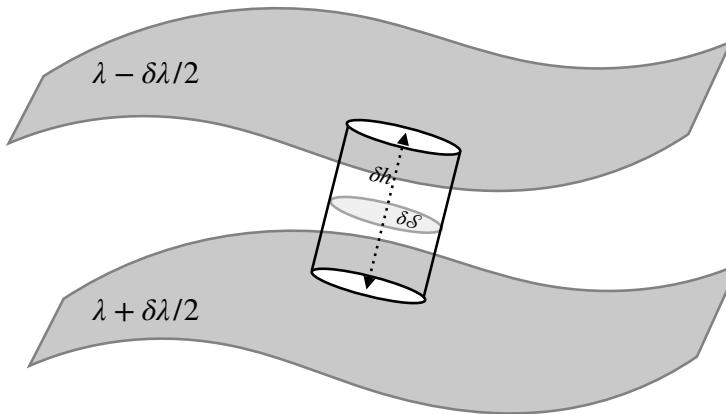


FIGURE 50.3: This schematic shows an infinitesimally thin  $\lambda$ -layer bounded by two interfaces  $[\lambda - \delta\lambda/2, \lambda + \delta\lambda/2]$ , with the  $\lambda$ -increment  $\delta\lambda > 0$ . The cylinder region extends between the two iso-surfaces and it has thickness  $\delta h = \delta\lambda/|\nabla\lambda|$  and cross-sectional area  $\delta \mathcal{S}$ . The cylinder is oriented according to the normal direction  $\hat{\mathbf{n}} = |\nabla\lambda|^{-1} \nabla\lambda$ . We assume  $|\nabla\lambda| \neq 0$ , as required to define a normal direction. Indeed, if  $\nabla\lambda = 0$  then we could not perform a binning according to  $\lambda$  classes, so the  $|\nabla\lambda| \neq 0$  assumption is basic to the use of the scalar field,  $\lambda$ , for water mass analysis.

<sup>8</sup>Recall our notational convention is as follows:  $\delta$  refers to an infinitesimal increment of a property measured within the fluid whereas  $d$  is a differential increment used for computing integrals. We made use of the same geometric analysis in Section 36.1.2 when studying potential vorticity.

### 50.3.2 Seawater mass within a finite region

Making use of the infinitesimal cylinder mass (50.8) allows us to write the mass of seawater within the  $\lambda$ -region  $\lambda_1 \leq \lambda \leq \lambda_2$

$$M(\lambda_1, \lambda_2) \equiv \int_{\Omega(\lambda_1 \leq \lambda \leq \lambda_2)} dM = \int_{\lambda_1}^{\lambda_2} \left[ \int_{\partial\Omega(\lambda)} \frac{\rho d\mathcal{S}}{|\nabla\lambda|} \right] d\lambda. \quad (50.9)$$

In this equation,  $\Omega(\lambda_1 \leq \lambda \leq \lambda_2)$  is the region in space bounded by the  $\lambda_1$ -interface and  $\lambda_2$ -interface, and  $\partial\Omega(\lambda)$  is the surface defined by a  $\lambda$ -isosurface. The  $\partial\Omega(\lambda)$  integral is taken over the area of the  $\lambda$ -isosurface, which is then integrated over the range,  $\lambda_1 \leq \lambda \leq \lambda_2$ , to thus accumulate the layer mass.

### 50.3.3 Seawater mass distribution/density function

The region bounded by the layer interfaces can have any shape in space and can even be spatially disconnected. This complexity motivates us to introduce the *mass distribution* or *mass density* function by integrating the mass over the surface,  $\partial\Omega(\lambda)$

$$m(\lambda) \equiv \frac{dM}{d\lambda} = \int_{\partial\Omega(\lambda)} \frac{\rho d\mathcal{S}}{|\nabla\lambda|}. \quad (50.10)$$

A mass distribution function is quite useful when the distribution is highly non-local in geographic/depth space. It is also effective when using multiple water mass coordinates such as  $\Theta$  and  $S$  as discussed in [Nurser et al. \(2022\)](#). These points motivate leaving geographic/depth perspective to simply define the mass distribution function so that

$$dM = m(\lambda) d\lambda = \text{mass within the infinitesimal } \lambda\text{-layer } [\lambda - d\lambda/2, \lambda + d\lambda/2], \quad (50.11)$$

with an illustration given by Figure 50.4. The mass distribution function is the mass density within  $\lambda$  space; i.e., the mass per  $\lambda$ . Knowledge of the mass distribution function allows us to compute the seawater mass within a finite region, as in equation (50.9), according to

$$M(\lambda_1, \lambda_2) \equiv \int_{\Omega(\lambda_1 \leq \lambda \leq \lambda_2)} dM = \int_{\lambda_1}^{\lambda_2} m(\lambda) d\lambda. \quad (50.12)$$

### 50.3.4 Example regions

To help ground the previous expressions for mass, we here consider some example regions that are commonly considered in water mass analysis.

*$\Delta\lambda$ -layer defined by  $[\lambda_1, \lambda_2] = [\lambda - \Delta\lambda/2, \lambda + \Delta\lambda/2]$*

A  $\Delta\lambda$ -layer is defined with the bounding interface values

$$\lambda_1 = \lambda - \Delta\lambda/2 \text{ and } \lambda_2 = \lambda + \Delta\lambda/2, \quad (50.13)$$

for some finite difference increment  $\Delta\lambda > 0$ . In this case the layer mass is

$$M(\lambda - \Delta\lambda/2, \lambda + \Delta\lambda/2) = \int_{\lambda - \Delta\lambda/2}^{\lambda + \Delta\lambda/2} \left[ \int_{\partial\Omega(\lambda')} \frac{\rho d\mathcal{S}}{|\nabla\lambda'|} \right] d\lambda' = \int_{\lambda - \Delta\lambda/2}^{\lambda + \Delta\lambda/2} m(\lambda') d\lambda'. \quad (50.14)$$

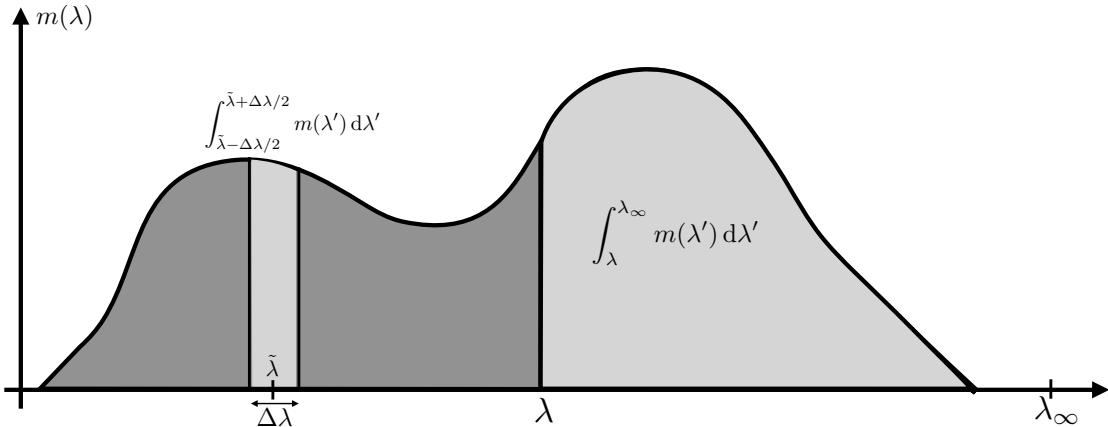


FIGURE 50.4: An example mass distribution function,  $m(\lambda) = dM/d\lambda$ , which measures the mass of seawater per  $\lambda$ -increment. Integration over a finite  $\lambda$ -region measures the seawater mass within that region. For example, the mass within a  $\Delta\lambda$ -layer is given by  $M(\tilde{\lambda} - \Delta\lambda/2, \tilde{\lambda} + \Delta\lambda/2) = \int_{\tilde{\lambda} - \Delta\lambda/2}^{\tilde{\lambda} + \Delta\lambda/2} m(\lambda') d\lambda'$  whereas the mass within the  $\lambda_\infty$ -region is  $M(\lambda, \lambda_\infty) = \int_\lambda^{\lambda_\infty} m(\lambda') d\lambda'$ , where we assume that  $\lambda_\infty$  is an arbitrary fixed value that is larger than any  $\lambda$  realized within the ocean.

Characterizing ocean properties according to their value of  $\lambda$  is generally performed by decomposing the ocean into  $\Delta\lambda$ -bins and forming histograms to estimate the continuous distribution.

$\lambda_\infty$ -region defined by  $[\lambda_1, \lambda_2] = [\lambda, \lambda_\infty]$

A  $\lambda_\infty$ -region is defined with

$$\lambda_1 = \lambda \text{ and } \lambda_2 = \lambda_\infty, \quad (50.15)$$

where  $\lambda_\infty$  is an arbitrary fixed constant that is larger than any value of  $\lambda$  realized in the ocean. The region mass is thus given by

$$M(\lambda, \lambda_\infty) = \int_{\Omega(\lambda \leq \lambda_\infty)} dM = \int_\lambda^{\lambda_\infty} \left[ \int_{\partial\Omega(\lambda')} \frac{\rho d\mathcal{S}}{|\nabla \lambda'|} \right] d\lambda' = \int_\lambda^{\lambda_\infty} m(\lambda') d\lambda'. \quad (50.16)$$

An example  $\lambda_\infty$ -region is shown in Figure 50.5. The  $\lambda_\infty$ -region as so defined provides an expression for the differential mass increment

$$M(\lambda, \lambda_\infty) = \int_\lambda^{\lambda_\infty} m(\lambda') d\lambda' \implies dM(\lambda, \lambda_\infty) = -m(\lambda) d\lambda, \quad (50.17)$$

which follows since  $\lambda_\infty$  is a constant.

The value of the fixed constant,  $\lambda_\infty$ , is arbitrarily large, indeed it could be infinite. We can set it to an arbitrarily large constant value since there is no contribution to the integral from regions with  $\lambda'$  outside the range realized within the ocean, merely since there is no ocean mass in that region. As an example, let  $\lambda = \Theta$ , the Conservative Temperature, in which the region  $\Theta \leq \Theta_\infty$  encompasses the ocean region where the Conservative Temperature is larger (warmer) than  $\Theta$ .

$\lambda_{-\infty}$ -region defined by  $[\lambda_1, \lambda_2] = [\lambda_{-\infty}, \lambda]$

A  $\lambda_{-\infty}$ -region is defined with

$$\lambda_1 = \lambda_{-\infty} \text{ and } \lambda_2 = \lambda, \quad (50.18)$$

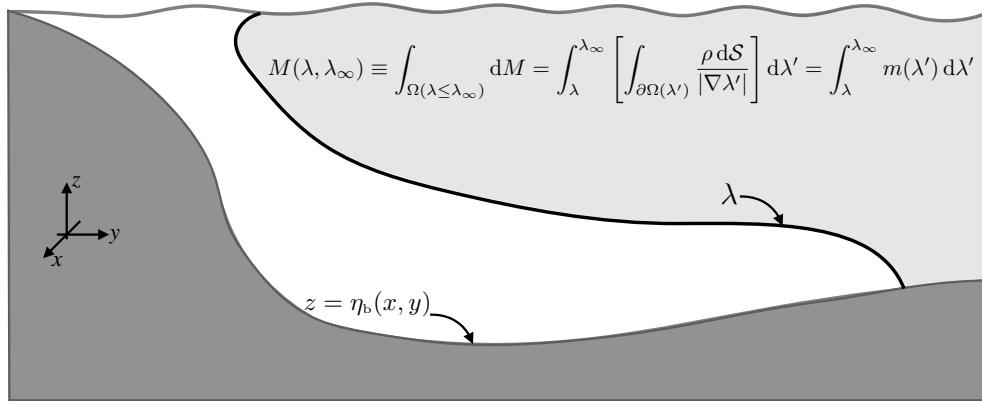


FIGURE 50.5: Depicting the mass of fluid within a  $\lambda_\infty$ -region, where  $\lambda \leq \lambda_\infty$  with  $\lambda_\infty$  is an arbitrary constant that is larger than any value of  $\lambda$  in the ocean domain. This figure is oriented for the southern hemisphere with Antarctica on the left. An example of such a region is for  $\lambda = \Theta$ , whereby warmer waters are typically shallower and towards the equator.

where  $\lambda_{-\infty}$  is an arbitrary constant that is smaller than any value of  $\lambda$  realized in the ocean. The region mass is thus given by

$$M(\lambda_{-\infty}, \lambda) \equiv \int_{\Omega(\lambda_{-\infty} \leq \lambda)} dM = \int_{\lambda_{-\infty}}^{\lambda} \left[ \int_{\partial\Omega(\lambda')} \frac{\rho dS}{|\nabla\lambda'|} \right] d\lambda' = \int_{\lambda_{-\infty}}^{\lambda} m(\lambda') d\lambda'. \quad (50.19)$$

This mass is the complement of that contained in the  $\lambda_\infty$ -region. The  $\lambda_{-\infty}$ -region mass implies a corresponding differential mass increment via

$$M(\lambda_{-\infty}, \lambda) = \int_{\lambda_{-\infty}}^{\lambda} m(\lambda') d\lambda' \implies dM(\lambda_{-\infty}, \lambda) = m(\lambda) d\lambda. \quad (50.20)$$

$\lambda_{\pm\infty}$ -region defined by  $[\lambda_1, \lambda_2] = [\lambda_{-\infty}, \lambda_\infty]$

The full ocean is contained in the  $\lambda_{\pm\infty}$ -region

$$\lambda_1 = \lambda_{-\infty} \text{ and } \lambda_2 = \lambda_\infty, \quad (50.21)$$

so that the full ocean mass is written

$$M(\lambda_{-\infty}, \lambda_\infty) = \int_{\Omega(\lambda_{-\infty} \leq \lambda \leq \lambda_\infty)} dM = \int_{\lambda_{-\infty}}^{\lambda_\infty} \left[ \int_{\partial\Omega(\lambda)} \frac{\rho dS}{|\nabla\lambda|} \right] d\lambda = \int_{\lambda_{-\infty}}^{\lambda_\infty} m(\lambda') d\lambda'. \quad (50.22)$$

*Difference of mass between two  $\lambda_\infty$ -regions*

The difference in mass between two  $\lambda_\infty$ -regions is given by

$$M(\lambda_1, \lambda_\infty) - M(\lambda_2, \lambda_\infty) = \int_{\lambda_1}^{\lambda_\infty} \left[ \int_{\partial\Omega(\lambda)} \frac{\rho dS}{|\nabla\lambda|} \right] d\lambda - \int_{\lambda_2}^{\lambda_\infty} \left[ \int_{\partial\Omega(\lambda)} \frac{\rho dS}{|\nabla\lambda|} \right] d\lambda. \quad (50.23)$$

The arbitrary constant,  $\lambda_\infty$ , drops out when taking the difference so that we are left with the mass within the intersection of the two regions

$$M(\lambda_1, \lambda_2) = M(\lambda_1, \lambda_\infty) - M(\lambda_2, \lambda_\infty) = \int_{\lambda_1}^{\lambda_2} \left[ \int_{\partial\Omega(\lambda)} \frac{\rho dS}{|\nabla \lambda|} \right] d\lambda = \int_{\lambda_1}^{\lambda_2} m(\lambda') d\lambda'. \quad (50.24)$$

### 50.3.5 Integrals of arbitrary functions

We can extend the above formalism to integrals of an arbitrary function,  $\mathcal{F}(x, t)$ , over a region defined by  $\lambda_{1,2}$ -interfaces

$$\mathcal{I}_{\mathcal{F}}(\lambda_1, \lambda_2) \equiv \int_{\Omega(\lambda_1 \leq \lambda \leq \lambda_2)} \mathcal{F} dM = \int_{\lambda_1}^{\lambda_2} \left[ \int_{\partial\Omega(\lambda)} \frac{\mathcal{F} \rho dS}{|\nabla \lambda|} \right] d\lambda. \quad (50.25)$$

Performing the area integral amounts to binning the function according to  $\lambda$ -increments, in which case we define the distribution function

$$m_{\mathcal{F}}(\lambda) = \int_{\partial\Omega(\lambda)} \frac{\mathcal{F} \rho dS}{|\nabla \lambda|}, \quad (50.26)$$

so that an integral over the distribution is given by

$$\mathcal{I}_{\mathcal{F}}(\lambda_1, \lambda_2) = \int_{\lambda_1}^{\lambda_2} m_{\mathcal{F}}(\lambda) d\lambda. \quad (50.27)$$

In particular, consider the integral over a  $\lambda_\infty$ -region

$$\mathcal{I}_{\mathcal{F}}(\lambda, \lambda_\infty) = \int_{\lambda}^{\lambda_\infty} \left[ \int_{\partial\Omega(\lambda')} \frac{\mathcal{F} \rho dS}{|\nabla \lambda'|} \right] d\lambda' = \int_{\lambda}^{\lambda_\infty} m_{\mathcal{F}}(\lambda') d\lambda', \quad (50.28)$$

which has the derivative

$$\frac{\partial \mathcal{I}_{\mathcal{F}}(\lambda, \lambda_\infty)}{\partial \lambda} = - \int_{\partial\Omega(\lambda)} \frac{\mathcal{F} \rho dS}{|\nabla \lambda|} = -m_{\mathcal{F}}(\lambda), \quad (50.29)$$

as follows from the fundamental theorem of calculus. Note how the derivative removes the reference value,  $\lambda_\infty$ . Analogously, the integral over a  $\lambda_{-\infty}$ -region has the derivative

$$\frac{\partial \mathcal{I}_{\mathcal{F}}(\lambda_{-\infty}, \lambda)}{\partial \lambda} = \int_{\partial\Omega(\lambda)} \frac{\mathcal{F} \rho dS}{|\nabla \lambda|} = m_{\mathcal{F}}(\lambda). \quad (50.30)$$

### 50.3.6 Moments of $\lambda$

Setting  $\mathcal{F} = \lambda$  in the integral (50.25) renders

$$\Lambda(\lambda_1, \lambda_2) \equiv \int_{\Omega(\lambda_1 \leq \lambda \leq \lambda_2)} \lambda dM = \int_{\Omega(\lambda_1 \leq \lambda \leq \lambda_2)} \lambda \rho dV = \int_{\lambda_1}^{\lambda_2} \left[ \int_{\partial\Omega(\lambda)} \frac{\lambda \rho dS}{|\nabla \lambda|} \right] d\lambda. \quad (50.31)$$

If  $\lambda$  is a tracer concentration (tracer mass per seawater mass), then  $\Lambda(\lambda_1, \lambda_2)$  is the mass of tracer within the layer. Observe that  $\lambda$  can be pulled outside of the surface integral in equation (50.31)

since  $\lambda$  is constant along  $\partial\Omega(\lambda)$ , thus rendering

$$\Lambda(\lambda_1, \lambda_2) = \int_{\lambda_1}^{\lambda_2} \left[ \int_{\partial\Omega(\lambda)} \frac{\rho d\mathcal{S}}{|\nabla\lambda|} \right] \lambda d\lambda = \int_{\lambda_1}^{\lambda_2} m(\lambda) \lambda d\lambda. \quad (50.32)$$

We can likewise define any higher powers as

$$\Lambda^{(n)}(\lambda_1, \lambda_2) \equiv \int_{\lambda_1}^{\lambda_2} \left[ \int_{\partial\Omega(\lambda)} \frac{\rho d\mathcal{S}}{|\nabla\lambda|} \right] \lambda^n d\lambda = \int_{\lambda_1}^{\lambda_2} m(\lambda) \lambda^n d\lambda = M(\lambda_1, \lambda_2) \langle \lambda^n \rangle. \quad (50.33)$$

The final equality introduced the mean value for the power

$$\langle \lambda^n \rangle = \frac{\int_{\lambda_1}^{\lambda_2} m(\lambda) \lambda^n d\lambda}{\int_{\lambda_1}^{\lambda_2} m(\lambda) d\lambda} \quad (50.34)$$

as defined over the  $[\lambda_1, \lambda_2]$  region. We refer to  $\langle \lambda^n \rangle$  as the  $n$ -moment of  $\lambda$ , with  $n = 1$  yielding the mean.

### 50.3.7 Internal and external $\lambda$ -moments

Now specify the region  $[\lambda_1, \lambda_2] = [\tilde{\lambda}, \lambda_\infty]$  for the moment equation (50.33). Making use of the differential mass increment,  $dM(\lambda, \lambda_\infty) = -m(\lambda) d\lambda$  as in equation (50.17) allows us to integrate the moment equation by parts

$$\Lambda^{(n)}(\tilde{\lambda}, \lambda_\infty) = \int_{\tilde{\lambda}}^{\lambda_\infty} \lambda^n m(\lambda) d\lambda \quad (50.35a)$$

$$= - \int_{\tilde{\lambda}}^{\lambda_\infty} \lambda^n dM \quad (50.35b)$$

$$= \int_{\tilde{\lambda}}^{\lambda_\infty} [-d(\lambda^n M) + n M \lambda^{n-1} d\lambda] \quad (50.35c)$$

$$= -\lambda_\infty^n M(\lambda_\infty, \lambda_\infty) + \lambda_\infty^n M(\tilde{\lambda}, \lambda_\infty) + n \int_{\tilde{\lambda}}^{\lambda_\infty} M(\lambda, \lambda_\infty) \lambda^{n-1} d\lambda \quad (50.35d)$$

$$= \lambda_\infty^n M(\tilde{\lambda}, \lambda_\infty) + n \int_{\tilde{\lambda}}^{\lambda_\infty} M(\lambda, \lambda_\infty) \lambda^{n-1} d\lambda, \quad (50.35e)$$

where the final equality follows since  $M(\lambda_\infty, \lambda_\infty) = 0$ . Making use of equation (50.33) thus leads to

$$M(\tilde{\lambda}, \lambda_\infty) \langle \lambda^n \rangle = \underbrace{M(\tilde{\lambda}, \lambda_\infty) \tilde{\lambda}^n}_{\text{external moment}} + \underbrace{n \int_{\tilde{\lambda}}^{\lambda_\infty} M(\lambda, \lambda_\infty) \lambda^{n-1} d\lambda}_{\text{internal moment}}. \quad (50.36)$$

We refer to the rightmost term as the *internal moment* since it is an integral over the region, whereas  $M(\tilde{\lambda}, \lambda_\infty) \tilde{\lambda}^n$  is the *external moment*, which is the region mass times the boundary value,  $\tilde{\lambda}^n$ . We choose the moniker “external” since the external moment increases in direct proportion to the mass crossing the ocean layer boundaries, including the external boundaries. In Section 50.6 we develop a budget for the  $n = 1$  moment, in which the internal moment from equation (50.36) takes the form

$$M(\tilde{\lambda}, \lambda_\infty) [\langle \lambda \rangle - \tilde{\lambda}] = \int_{\tilde{\lambda}}^{\lambda_\infty} M(\lambda, \lambda_\infty) d\lambda. \quad (50.37)$$

We return to the notion of internal and external moments in Section 50.10.2.

### 50.3.8 Further study

The formulation given here in terms of mass distribution functions follows that of [Waln \(1977\)](#) and [Waln \(1982\)](#). In these two papers, Waln pioneered the formalism of water mass analysis, which is sometimes referred to as *Waln analysis* in his honor. The concept of internal and external tracer moments follows the internal and external heat introduced by [Holmes et al. \(2019\)](#).

## 50.4 Water mass transformation across a $\lambda$ -surface

We here develop the formalism to quantify transport of seawater crossing an interior  $\lambda$ -interface. This transport is referred to as the *water mass transformation* and is written as  $G(\lambda)$ . Figure 50.6 illustrates how this transformation appears in a mass budget for a  $\Delta\lambda$ -layer.

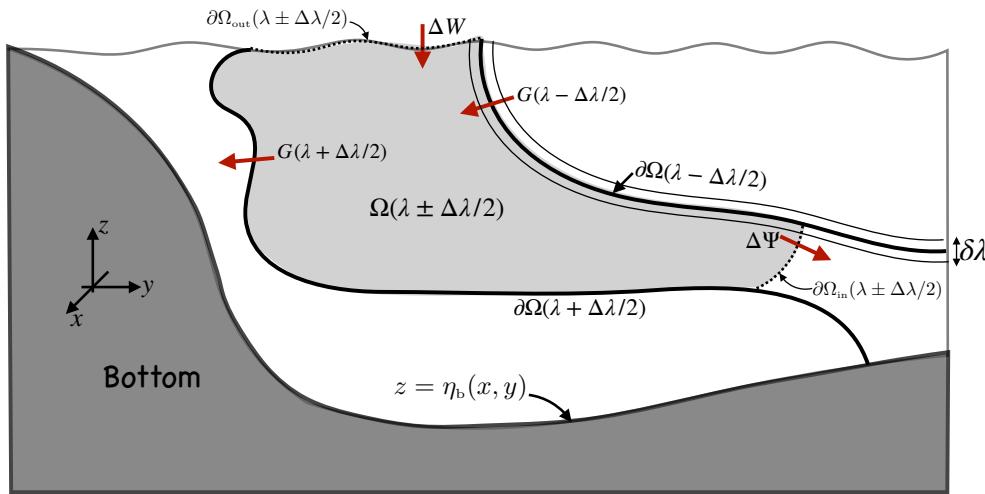


FIGURE 50.6: A layer of seawater with scalar property  $\lambda$  within the range  $[\lambda - \Delta\lambda/2, \lambda + \Delta\lambda/2]$  and defined over a geographical domain  $\Omega(\lambda \pm \Delta\lambda/2)$ . In this example,  $\lambda$  increases to the south, towards Antarctica, with  $\lambda = \gamma$  (Section 50.2) an example. The net seawater mass transport crossing the layer interfaces  $\partial\Omega(\lambda \pm \Delta\lambda/2)$  is  $G(\lambda \pm \Delta\lambda/2)$ , with  $G > 0$  for water moving to regions of larger  $\lambda$ . The seawater mass crossing the layer through the geographical bounds  $\partial\Omega_{in}(\lambda \pm \Delta\lambda/2)$  is written  $\Delta\Psi(\lambda \pm \Delta\lambda/2)$ , with  $\Delta\Psi(\lambda \pm \Delta\lambda/2) > 0$  for water leaving  $\Omega(\lambda \pm \Delta\lambda/2)$ . The boundary  $\partial\Omega_{in}(\lambda \pm \Delta\lambda/2)$  is absent when the domain extends across a basin or the global ocean (e.g., see Figure 50.8). The mass crossing the sea surface,  $\partial\Omega_{out}(\lambda \pm \Delta\lambda/2)$ , through rain, evaporation, melt, or rivers is written  $\Delta W(\lambda \pm \Delta\lambda/2)$ , with  $\Delta W(\lambda \pm \Delta\lambda/2) > 0$  for mass entering  $\Omega(\lambda \pm \Delta\lambda/2)$ . A layer interface can have an arbitrary stratification, such as the vertically non-monotonic profile depicted here for the  $\lambda + \Delta\lambda/2$  interface. Additionally, the domain  $\Omega(\lambda \pm \Delta\lambda/2)$  can generally be disconnected. The net domain boundaries are written  $\partial\Omega_{in}(\lambda \pm \Delta\lambda/2) + \partial\Omega_{out}(\lambda \pm \Delta\lambda/2) + \partial\Omega(\lambda + \Delta\lambda/2) + \partial\Omega(\lambda - \Delta\lambda/2)$ . The  $\delta\lambda$  layer surrounding the  $\partial\Omega(\lambda - \Delta\lambda/2)$  arises as part of the method detailed in Section 50.4.2 for computing  $G$  according to the  $\lambda$ -derivative of an integral over the  $\delta\lambda$  layer.

### 50.4.1 Dia-surface flux and interior transformation

The object that measures the local water mass transformation is the dia-surface flux detailed in Section 42.4.7. This flux is given by

$$w^{\text{dia}} = \hat{\mathbf{n}} \cdot (\mathbf{v} - \mathbf{v}^{(\lambda)}) = \frac{\dot{\lambda}}{|\nabla\lambda|} \quad \text{with} \quad \hat{\mathbf{n}} = \frac{\nabla\lambda}{|\nabla\lambda|} \quad \text{and} \quad \dot{\lambda} = \frac{D\lambda}{Dt}, \quad (50.38)$$

with  $w^{\text{dia}} > 0$  for water moving to regions of larger  $\lambda$ . It is computed as the projection of the relative velocity,  $(\mathbf{v} - \mathbf{v}^{(\lambda)})$ , onto the direction normal to the surface, with the relative velocity being the difference between the fluid particle velocity,  $\mathbf{v}$ , and the velocity of a point on the  $\lambda$ -interface,  $\mathbf{v}^{(\lambda)}$ . The velocity of a point on the surface,  $\mathbf{v}^{(\lambda)}$ , satisfies the following kinematic constraint<sup>9</sup>

$$(\partial_t + \mathbf{v}^{(\lambda)} \cdot \nabla) \lambda = 0. \quad (50.39)$$

This constraint is based on assuming  $\mathbf{v}^{(\lambda)}$  measures the velocity of a point fixed to the  $\lambda$ -surface. So in brief, the dia-surface flux,  $w^{\text{dia}}$ , locally measures the flux of seawater (volume per area per time) that penetrates a  $\lambda$ -interface in the direction of increasing  $\lambda$ .

The interior water mass transformation,  $G(\lambda)$ , is the area integral of  $\rho w^{\text{dia}}$  over the full extent of the  $\lambda$ -surface

$$G(\lambda) \equiv \int_{\partial\Omega(\lambda)} \rho w^{\text{dia}} dS = \int_{\partial\Omega(\lambda)} \rho \hat{\mathbf{n}} \cdot (\mathbf{v} - \mathbf{v}^{(\lambda)}) dS = \int_{\partial\Omega(\lambda)} \frac{\rho \dot{\lambda}}{|\nabla \lambda|} dS, \quad (50.40)$$

where  $\partial\Omega(\lambda)$  is the surface occupied by the  $\lambda$ -interface (see Figure 50.6). Furthermore, the dimensions of  $G(\lambda)$  are mass per time

$$G(\lambda) \quad [=] \quad \text{M T}^{-1}, \quad (50.41)$$

thus measuring the mass per time crossing the  $\lambda$ -interface.

Based on the definition (50.40), we see that interior water mass transformation across a  $\lambda$ -interface occurs when there is a material change,  $\dot{\lambda} \neq 0$ , in the property defining the interface. Interior material changes arise from mixing, which generally causes irreversible changes to  $\lambda$ , thus driving seawater across the moving  $\lambda$ -interfaces. Material changes can also arise from sources and sinks, as when considering buoyancy surfaces in the presence of a nonlinear equation of state (Chapter 49). Sources and sinks are also commonly encountered by biogeochemical tracers.

### 50.4.2 Transformation as the derivative of an integral

Following the discussion from Section 50.3.5, we set  $\mathcal{F} = \dot{\lambda}$  and consider the mass integral

$$\mathcal{I}_{\dot{\lambda}}(\lambda, \lambda_{\infty}) = \int_{\Omega(\lambda \leq \lambda_{\infty})} \dot{\lambda}' dM = \int_{\lambda}^{\lambda_{\infty}} \left[ \int_{\partial\Omega(\lambda')} \frac{\rho \dot{\lambda}'}{|\nabla \lambda'|} dS \right] d\lambda' = \int_{\lambda}^{\lambda_{\infty}} G(\lambda') d\lambda'. \quad (50.42)$$

The fundamental theorem of calculus leads to the expression of the water mass transformation as the derivative

$$G(\lambda) = -\frac{\partial \mathcal{I}_{\dot{\lambda}}(\lambda, \lambda_{\infty})}{\partial \lambda} \quad (50.43a)$$

$$= -\lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \left[ \int_{\lambda+\delta\lambda/2}^{\lambda_{\infty}} G(\lambda') d\lambda' - \int_{\lambda-\delta\lambda/2}^{\lambda_{\infty}} G(\lambda') d\lambda' \right] \quad (50.43b)$$

$$= \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\lambda-\delta\lambda/2}^{\lambda+\delta\lambda/2} G(\lambda') d\lambda' \quad (50.43c)$$

$$= \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\Omega(\lambda \pm \delta\lambda/2)} \rho \dot{\lambda}' dV. \quad (50.43d)$$

---

<sup>9</sup>We encountered the relation (50.39) in Section 14.4.2 when deriving the kinematic boundary condition for a moving surface.

We conclude that calculation of interior water mass transformation requires the various contributions to the material time change,  $\dot{\lambda}$ , a weighting of the time changes according to the mass of the fluid element,  $dM = \rho dV$ , and a binning of  $\rho \dot{\lambda} dV$  according to  $\lambda$ -classes. Note that in the final equality, equation (50.43d), the limit  $\delta\lambda \rightarrow 0$  might appear to lead to a singularity. However, as seen by the form in equation (50.43c), the integration region volume also gets smaller as  $\delta\lambda \rightarrow 0$  so that the limit is well defined.

### 50.4.3 Processes and kinematics

There are two equivalent and complementary methods to view interior water mass transformation: the process method and the kinematic method.

#### *Process method*

The *process method* focuses on physical processes leading to movement of fluid across the  $\lambda$ -interface, thus providing information concerning *why* interior transformation occurs. It does so by binning processes contributing to the right hand side of the equation

$$\rho \dot{\lambda} = -\nabla \cdot \mathbf{J} + \rho \dot{\Upsilon}, \quad (50.44)$$

where  $\mathbf{J}$  is a flux arising from non-advection processes such as diffusion, and  $\dot{\Upsilon}$  is a source/sink term (dimensions of  $\lambda$  per time) that cannot be written as the convergence of a flux. The tracer equation (50.44) inserted into the transformation equation (50.43d) leads to

$$G(\lambda) = \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\Omega(\lambda \pm \delta\lambda/2)} [-\nabla \cdot \mathbf{J} + \rho \dot{\Upsilon}] dV \quad (50.45a)$$

$$= \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \oint_{\partial\Omega(\lambda \pm \delta\lambda/2)} [-\mathbf{J} \cdot \hat{\mathbf{n}}] dS + \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\Omega(\lambda \pm \delta\lambda/2)} \rho \dot{\Upsilon} dV, \quad (50.45b)$$

The second equality made use of the divergence theorem to convert the volume integral into a surface integral. For the tracer sources, we assume they do not modify the seawater mass at a point so that there is no source in the seawater mass equation.

For many purposes it is useful to decompose the non-advection flux divergence into contributions from interior processes, such as ocean mixing, and boundary fluxes

$$\nabla \cdot \mathbf{J} = \nabla \cdot [\mathbf{J}_{\text{int}} + \mathbf{J}_{\text{out}} + \mathbf{J}_{\text{bot}}]. \quad (50.46)$$

By definition,

$$\mathbf{J}_{\text{int}} \cdot \hat{\mathbf{n}} = 0 \quad \text{on } \partial\Omega_{\text{out}}(\lambda \pm \delta\lambda/2) \text{ and } \partial\Omega_{\text{bot}}(\lambda \pm \delta\lambda/2), \quad (50.47)$$

whereas  $\mathbf{J}_{\text{int}} \cdot \hat{\mathbf{n}}$  is generally nonzero on interior layer boundaries. In contrast, the boundary fluxes,  $\mathbf{J}_{\text{out}} \cdot \hat{\mathbf{n}}$  and  $\mathbf{J}_{\text{bot}} \cdot \hat{\mathbf{n}}$ , are identically zero everywhere except on their respective boundaries. Correspondingly, it is convenient to bin the volume weighted divergence,  $\nabla \cdot \mathbf{J}_{\text{int}} dV$ , according to  $\lambda$ -classes, and to likewise bin the area weighted boundary fluxes,  $\mathbf{J}_{\text{out}} \cdot \hat{\mathbf{n}} dS$  and  $\mathbf{J}_{\text{bot}} \cdot \hat{\mathbf{n}} dS$ . In

this way we write the non-advection contribution to water mass transformation in the form

$$\begin{aligned} G(\lambda)_{\text{non-adv}} = & \underbrace{- \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\Omega(\lambda \pm \delta\lambda/2)} \nabla \cdot \mathbf{J}_{\text{int}} dV}_{\text{interior transformation} = \text{volume integral of convergence}} \\ & - \underbrace{\lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\partial\Omega_{\text{out}}(\lambda \pm \delta\lambda/2)} \mathbf{J}_{\text{out}} \cdot \hat{\mathbf{n}} d\mathcal{S}}_{\text{surface transformation} = \text{area integral of surface boundary fluxes}} \\ & - \underbrace{\lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\partial\Omega_{\text{bot}}(\lambda \pm \delta\lambda/2)} \mathbf{J}_{\text{bot}} \cdot \hat{\mathbf{n}} d\mathcal{S}}_{\text{bottom transformation} = \text{area integral of bottom boundary fluxes}}. \end{aligned} \quad (50.48)$$

Again, this expression decomposes the contribution from interior processes, here represented as the volume integral of the interior flux convergence, from the surface and bottom contributions, here represented as the area integral of the boundary fluxes. This decomposition is further examined in Section 50.7 where we focus on the surface contribution to water mass transformation.

Since the boundary fluxes are, by definition, zero except on the boundaries, their divergence can be written in terms of a Dirac delta distribution<sup>10</sup>

$$\nabla \cdot [\mathbf{J}_{\text{out}} + \mathbf{J}_{\text{bot}}] = \mathbf{J}_{\text{out}} \cdot \hat{\mathbf{n}} \delta(z - \eta) + \mathbf{J}_{\text{bot}} \cdot \hat{\mathbf{n}} \delta(z - \eta_b). \quad (50.49)$$

Although this equation is more physically formal than mathematically rigorous, its use in the transformation equation (50.45a) correctly leads to the expression (50.48). Consequently, equation (50.49) proves to be a useful shorthand.

### Kinematic method

The *kinematic method* focuses on the kinematic means for realizing dia-surface transport, thus providing information concerning *how* interior transformation occurs. It does so by binning processes contributing to the right hand side of

$$\rho \dot{\lambda} = \partial_t(\rho \lambda) + \nabla \cdot (\rho \lambda \mathbf{v}), \quad (50.50)$$

which arises from the local time tendency plus advection, so that

$$G(\lambda) = \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\Omega(\lambda \pm \delta\lambda/2)} [\partial_t(\rho \lambda) + \nabla \cdot (\rho \lambda \mathbf{v})] dV. \quad (50.51)$$

### Comments

As we saw, equality of the process method and kinematic method follows simply because the two provide equivalent expressions for the material time derivative. However, in the analysis of numerical model output, it can be nontrivial to realize this equivalence due to the extreme care required to diagnose the terms appearing in the scalar budget equation.

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<sup>10</sup>We detail properties of the Dirac delta distribution in Section 4.2. It has dimensions of inverse the dimensions of its argument, so that when the argument has dimensions of length then the Dirac delta has dimensions of inverse length. We thus see that equation (50.49) is dimensionally consistent.

### 50.4.4 Some details concerning interior transformation

We here consider some details of the water mass transformation arising just from interior processes such as diffusion.

#### *A global integrated constraint on $G(\lambda)_{\text{int}}$*

Consider the integrated water mass transformation given by equation (50.42), only now integrate over the full ocean domain

$$\mathcal{I}_{\dot{\lambda}}(\lambda_{-\infty}, \lambda_{\infty}) = \int_{\lambda_{-\infty}}^{\lambda_{\infty}} G(\lambda') d\lambda' = \int_{\Omega(\lambda_{-\infty}, \lambda_{\infty})} \rho \dot{\lambda}' dV. \quad (50.52)$$

This integral vanishes for water mass transformations arising just from interior processes

$$[\mathcal{I}_{\dot{\lambda}}(\lambda_{-\infty}, \lambda_{\infty})]_{\text{int}} = \int_{\lambda_{-\infty}}^{\lambda_{\infty}} G(\lambda')_{\text{int}} d\lambda' \quad (50.53a)$$

$$= - \int_{\Omega(\lambda_{-\infty}, \lambda_{\infty})} \nabla \cdot \mathbf{J}_{\text{int}} dV \quad (50.53b)$$

$$= - \oint_{\partial\Omega(\lambda_{-\infty}, \lambda_{\infty})} \mathbf{J}_{\text{int}} \cdot \hat{\mathbf{n}} dS \quad (50.53c)$$

$$= 0, \quad (50.53d)$$

which follows since  $\mathbf{J}_{\text{int}} \cdot \hat{\mathbf{n}} = 0$  on the ocean boundaries. Hence, there can be no net water mass transformation across a  $\lambda$  surface arising from interior processes

$$\int_{\lambda_{-\infty}}^{\lambda_{\infty}} G(\lambda')_{\text{int}} d\lambda' = 0. \quad (50.54)$$

Instead, interior processes only lead to rearrangement of water within the  $\lambda$ -bins. This result follows since the interior processes conserve the total content of  $\lambda$  within the global domain. It provides a constraint on numerical realizations of water mass transformation diagnostics.

#### *Interior transformation across constant $\lambda$ surfaces*

We now focus on the transformation occurring along surfaces of constant  $\lambda$  (Figure 50.7) so that

$$G(\lambda)_{\text{int}} = - \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\Omega(\lambda \pm \delta\lambda/2)} \nabla \cdot \mathbf{J}_{\text{int}} dV \quad (50.55a)$$

$$= - \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \left[ \int_{\Omega(\lambda + \delta\lambda/2)} \hat{\mathbf{n}} \cdot \mathbf{J}_{\text{int}} dS - \int_{\Omega(\lambda - \delta\lambda/2)} \hat{\mathbf{n}} \cdot \mathbf{J}_{\text{int}} dS \right]. \quad (50.55b)$$

Transformation occurs if there is an imbalance between the diffusive transport across the two bounding surfaces,  $\Omega(\lambda + \delta\lambda/2)$  and  $\Omega(\lambda - \delta\lambda/2)$ . As a special case, assume the ocean surface is a constant  $\lambda$  surface with  $\lambda = \lambda_{\text{top}}$ . Along this surface we have  $\hat{\mathbf{n}} \cdot \mathbf{J}_{\text{int}} = 0$ , so that the transformation at  $\lambda_{\text{top}} - \delta\lambda/2$  has a contribution just from the flux crossing the  $\Omega(\lambda_{\text{top}} - \delta\lambda)$  surface

$$\lim_{\delta\lambda \rightarrow 0} G(\lambda_{\text{top}} - \delta\lambda/2)_{\text{int}} = \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\Omega(\lambda_{\text{top}} - \delta\lambda)} \hat{\mathbf{n}} \cdot \mathbf{J}_{\text{int}} dS. \quad (50.56)$$

Likewise, along the top surface we have

$$G(\lambda_{\text{top}})_{\text{int}} = \lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\Omega(\lambda_{\text{top}} - \delta\lambda/2)} \hat{\mathbf{n}} \cdot \mathbf{J}_{\text{int}} \, d\mathcal{S}, \quad (50.57)$$

where we set  $\hat{\mathbf{n}} \cdot \mathbf{J}_{\text{int}} = 0$  for the surface  $\Omega(\lambda_{\text{top}} + \delta\lambda/2)$ , since this surface exists outside of the ocean.

The results (50.56) and (50.57) make it appear that  $G(\lambda_{\text{top}} - \delta\lambda/2)_{\text{int}}$  and  $G(\lambda_{\text{top}})_{\text{int}}$  are unbounded as  $\delta\lambda \rightarrow 0$ , so long as there is a nonzero diffusive transport through  $\Omega(\lambda_{\text{top}} - \delta\lambda)$  or  $\Omega(\lambda_{\text{top}} - \delta\lambda/2)$ . However, this unbounded water mass transformation is not realized since the diffusive flux gets smaller in magnitude when approaching the ocean surface, and it does so in order to satisfy the no-flux surface boundary condition (50.47) satisfied by interior processes<sup>11</sup>

$$\hat{\mathbf{n}} \cdot \mathbf{J}_{\text{int}} = 0 \quad \text{at } z = \eta. \quad (50.58)$$

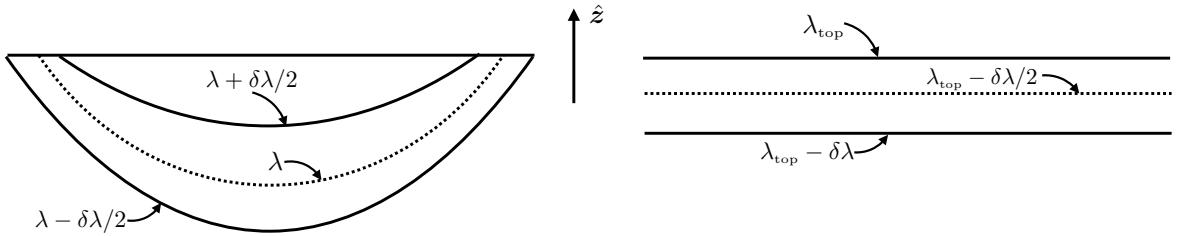


FIGURE 50.7: Example  $\lambda$  surfaces for studying interior transformation due to diffusion. The left panel shows  $\lambda$  surfaces that outcrop to the ocean surface, with the dotted surface the chosen  $\lambda$  surface across which we compute the water mass transformation. The right panel assumes the  $\lambda$  surfaces are flat and with  $\lambda = \lambda_{\text{top}}$  the value along the ocean surface.

To further our understanding of the transformation in the region near the ocean surface, let the  $\lambda$  surfaces be flat near the ocean surface so that  $\hat{\mathbf{n}} = -\hat{\mathbf{z}}$  along  $\Omega(\lambda_{\text{top}} - \delta\lambda)$ . Setting the diffusive flux to

$$\mathbf{J} = -\rho_0 \kappa \nabla \lambda \quad (50.59)$$

as per a Boussinesq fluid with reference density  $\rho_0$  and diffusivity  $\kappa > 0$ , leads to the transformation

$$G(\lambda_{\text{top}} - \delta\lambda/2)_{\text{int}} = \frac{1}{\delta\lambda} \int_{\Omega(\lambda_{\text{top}} - \delta\lambda)} (\rho_0 \kappa \partial_z \lambda) \, d\mathcal{S}. \quad (50.60)$$

With  $\kappa \partial_z \lambda > 0$ , the transformation is positive,  $G(\lambda_{\text{top}} - \delta\lambda/2)_{\text{int}} > 0$ , so that water is entrained into the layer bounded by  $\lambda_{\text{top}} - \delta\lambda$  and  $\lambda_{\text{top}}$ . Note that in the absence of boundary fluxes, the value of  $\lambda_{\text{top}}$  is reduced due to diffusive mixing with interior waters since these waters have lower values of  $\lambda$ . Furthermore, as the surface is approached,  $\partial_z \lambda$  reduces in magnitude to satisfy the no-flux condition,  $\kappa \partial_z \lambda = 0$ , at the ocean surface. In this manner, the transformation remains bounded even as  $\delta\lambda \rightarrow 0$ .

<sup>11</sup>As discussed in Sections 15.5.3, 49.5, and 50.8.3, when water is transported across the ocean surface the diffusive flux picks up a nonzero boundary contribution. That contribution is assumed to be part of the surface transformation in equation (50.48) so that the interior diffusive flux still satisfies the no-flux boundary condition (50.58).

## 50.5 Budget for seawater mass in a $\Delta\lambda$ -layer

In this section we construct the seawater mass budget for a  $\Delta\lambda$ -layer, making reference to Figure 50.6 for the notation. As a shorthand, we write the layer mass as

$$\Delta M(\lambda \pm \Delta\lambda/2) \equiv M(\lambda - \Delta\lambda/2, \lambda + \Delta\lambda/2), \quad (50.61)$$

along with a similar notation for other contributions to the layer mass budget.

### 50.5.1 Transport crossing interior open boundaries

As depicted in Figure 50.6, the layer region has an open boundary that is within the interior of the ocean. The mass transport leaving the layer through this interior open boundary is written

$$\Delta\Psi(\lambda \pm \Delta\lambda/2) = \int_{\partial\Omega_{in}(\lambda \pm \Delta\lambda/2)} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} dS, \quad (50.62)$$

where  $\mathbf{v}^{(b)}$  is the velocity for a point on the boundary and  $\hat{\mathbf{n}}$  is the outward normal along the boundary. Introducing the mass distribution for this transport renders the equivalent expression

$$\Delta\Psi(\lambda \pm \Delta\lambda/2) = \int_{\lambda - \Delta\lambda/2}^{\lambda + \Delta\lambda/2} \dot{m}_\Psi(\lambda') d\lambda', \quad (50.63)$$

where

$$\dot{m}_\Psi(\lambda) d\lambda = \text{mass per time crossing } \partial\Omega_{in} \text{ within the increment } [\lambda - d\lambda/2, \lambda + d\lambda/2]. \quad (50.64)$$

We make particular use of  $\dot{m}_\Psi$  in Section 50.6 when studying the  $\lambda$ -budget in a  $\Delta\lambda$ -layer. One common example for an open interior boundary is when choosing a particular latitude, in which case  $\mathbf{v}^{(b)} = 0$  and  $\hat{\mathbf{n}} = \hat{\mathbf{y}}$  so that

$$\Delta\Psi(\lambda \pm \Delta\lambda/2) = \int_{\partial\Omega_{in}(\lambda \pm \Delta\lambda/2)} \rho v dx dz. \quad (50.65)$$

In this case,  $\partial\Omega_{in}(\lambda \pm \Delta\lambda/2)$  specifies the depth and longitude range for the layer at its intersection along the constant latitude boundary.

### 50.5.2 Mass transport crossing the ocean surface

The mass transport crossing the ocean free surface is written

$$\Delta W(\lambda \pm \Delta\lambda/2) = - \int_{\partial\Omega_{out}(\lambda \pm \Delta\lambda/2)} \rho (\mathbf{v} - \mathbf{v}^{(\eta)}) \cdot \hat{\mathbf{n}} dS = \int_{\partial\Omega_{out}(\lambda \pm \Delta\lambda/2)} \mathcal{Q}_m dS, \quad (50.66)$$

where we made use of the surface kinematic boundary condition (14.63) to write

$$\rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} \equiv -\mathcal{Q}_m, \quad (50.67)$$

where  $\mathcal{Q}_m dS$  is the mass transport of water crossing the free surface ( $\mathcal{Q}_m > 0$  for water entering the ocean). Introducing the mass distribution leads to the equivalent expression

$$\Delta W(\lambda \pm \Delta\lambda/2) = \int_{\lambda - \Delta\lambda/2}^{\lambda + \Delta\lambda/2} \dot{m}_w(\lambda') d\lambda', \quad (50.68)$$

where

$$\dot{m}_W(\lambda) d\lambda = \text{mass per time crossing } \partial\Omega_{\text{out}} \text{ within the increment } [\lambda - d\lambda/2, \lambda + d\lambda/2]. \quad (50.69)$$

We make particular use of  $\dot{m}_W$  in Section 50.6 when studying the  $\lambda$ -budget in a  $\Delta\lambda$ -layer.

### 50.5.3 Mass budget

Bringing the above pieces together leads to the layer mass budget

$$\frac{d\Delta M}{dt} = -\Delta\Psi + \Delta W - [G(\lambda + \Delta\lambda/2) - G(\lambda - \Delta\lambda/2)], \quad (50.70)$$

where for brevity we dropped  $\lambda \pm \Delta\lambda/2$  arguments for  $\Delta M$ ,  $\Delta\Psi$ , and  $\Delta W$ . It is common to define the layer mass *formation* as the mass accumulation within the layer

$$\underbrace{\frac{d\Delta M}{dt} + \Delta\Psi}_{\text{storage + outflow}} = \underbrace{\Delta W - [G(\lambda + \Delta\lambda/2) - G(\lambda - \Delta\lambda/2)]}_{\text{formation into layer } \Omega_{(\lambda \pm \Delta\lambda/2)}}. \quad (50.71)$$

This equality defines water mass formation as the time change for the mass within the layer (sometimes referred to as the *storage term*), plus the net mass leaving the interior open boundary. Formation into a layer occurs if there is mass converging through transformation across interior layer interfaces, plus mass entering through the surface boundary outcrop region.

We arrive at a differential equation for the mass budget (50.71) by dividing through by the layer increment,  $\Delta\lambda$ , and taking the limit as this increment tends to zero

$$\frac{\partial}{\partial\lambda} \left[ \frac{dM}{dt} + \Psi - W + G \right] = 0. \quad (50.72)$$

Integrating from a reference value  $\lambda_{-\infty}$  to  $\lambda$  leads to

$$\int_{\lambda_{-\infty}}^{\lambda} \frac{\partial\Psi}{\partial\lambda} d\lambda = \int_{\lambda_{-\infty}}^{\lambda} \frac{\partial}{\partial\lambda} \left[ -\frac{dM}{dt} + W - G \right] d\lambda \implies \Psi = -\frac{dM}{dt} + W - G. \quad (50.73)$$

We dropped the contribution from the constant reference value,  $\lambda_{-\infty}$ , since it sits outside of the ocean domain. The differential water mass equation (50.73) is a continuous version of the discrete equation (50.71). We wrote this equation as an expression for  $\Psi$  given that an accumulation from the bottom up leads to a transport streamfunction in the steady limit.

## 50.6 Budget for $\lambda$ mass in a $\lambda_\infty$ -region

We build from our understanding of the seawater mass budget in Section 50.5 to develop a budget for the mass of  $\lambda$  within the  $\lambda_\infty$ -region of Section 50.3.4 and as illustrated in Figure 50.8. Part of our aim is to further develop the formalism while also offering added insights into the causes for water mass transformation,  $G(\lambda)$ .

We here choose to be specific by considering  $\lambda$  to be an intensive property such as a material tracer concentration, in which case  $\lambda \rho dV$  has dimensions of tracer mass.<sup>12</sup> For non-material scalar fields, such as Conservative Temperature or buoyancy, the dimensions are modified accordingly.

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<sup>12</sup>See Section 15.3.1 for more on intensive and extensive fluid properties.

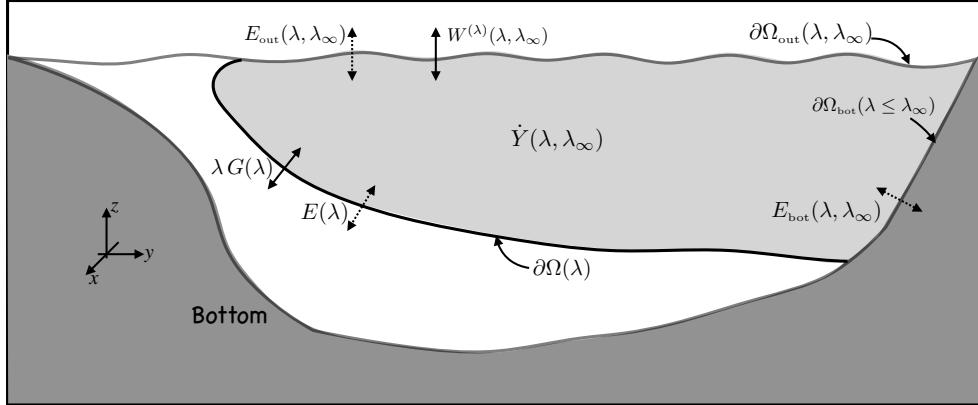


FIGURE 50.8: A  $\lambda_\infty$ -region for studying the  $\lambda$  budget, with the region bounded by the solid-earth bottom,  $\partial\Omega_{\text{bot}}(\lambda \leq \lambda_\infty)$ , the ocean surface boundary,  $\partial\Omega_{\text{out}}(\lambda, \lambda_\infty)$ , and the  $\lambda$ -interface,  $\partial\Omega(\lambda)$ . Hence, in contrast to the  $\Delta\lambda$ -region shown in Figure 50.6, the  $\lambda_\infty$ -region has no interior open boundary. Along the surface boundary, the  $\lambda$  budget is affected by the non-advectional transport,  $E_{\text{out}}(\lambda, \lambda_\infty)$ , arising from processes such as diffusion, plus advective transport,  $W^{(\lambda)}(\lambda, \lambda_\infty)$ , arising from mass transported across the surface that can carry a non-zero amount of  $\lambda$ . Along the bottom boundary, the  $\lambda$  budget is affected by non-advectional transport,  $E_{\text{bot}}(\lambda, \lambda_\infty)$ , arising from processes such as geothermal heating. There is no corresponding advective transport along the bottom since we assume there is no mass crossing the ocean bottom. Along the interior boundary,  $\partial\Omega(\lambda)$ , the budget is affected by non-advectional transport,  $E(\lambda)$ , arising from diffusion, as well as advective transport through  $\lambda G(\lambda)$ , with  $G(\lambda)$  the interior water mass transformation from Section 50.4. Finally, there is the possibility for an interior volume source,  $\dot{Y}(\lambda \leq \lambda_\infty)$ , particularly for buoyancy in the presence of a nonlinear equation of state, and for biogeochemical tracers.

### 50.6.1 Processes affecting the mass of $\lambda$ -stuff

Our starting point is the Leibniz-Reynolds budget for a scalar field derived in Section 15.3.4, here including the possibility of scalar sources

$$\frac{d}{dt} \left[ \int_{\Omega(\lambda \leq \lambda_\infty)} \rho \lambda dV \right] = \int_{\Omega(\lambda \leq \lambda_\infty)} \rho \dot{Y} dV - \int_{\partial\Omega(\lambda \leq \lambda_\infty)} \left[ \rho \lambda (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J} \right] \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (50.74)$$

The right hand side of this budget equation can be decomposed into the following processes illustrated in Figure 50.8.

#### *Non-conservative sources and sinks*

As noted in Section 50.4.3, the source term  $\rho \dot{Y}$  accounts for processes that cannot be represented as the convergence of a flux. We write its region integrated contribution using the shorthand

$$\dot{Y}(\lambda \leq \lambda_\infty) \equiv \int_{\Omega(\lambda \leq \lambda_\infty)} \rho \dot{Y} dV \equiv \int_\lambda^{\lambda_\infty} \dot{m}_{\dot{Y}}(\lambda') d\lambda'. \quad (50.75)$$

The final equality introduced the distribution function for the source, in which

$$\dot{m}_{\dot{Y}}(\lambda) d\lambda = \text{mass per time of } \lambda \text{ created within the region } [\lambda - d\lambda/2, \lambda + d\lambda/2]. \quad (50.76)$$

*Transport from non-advection processes*

The contribution from boundary area integrated non-advection fluxes appears in the term

$$-\int_{\partial\Omega(\lambda \leq \lambda_\infty)} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} = -\int_{\partial\Omega_{\text{out}}(\lambda \leq \lambda_\infty)} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\partial\Omega_{\text{bot}}(\lambda \leq \lambda_\infty)} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\partial\Omega(\lambda)} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (50.77)$$

Recall the minus signs arise since a non-advection flux increases the  $\lambda$  content of the region if the flux is oriented into the region, whereas  $\hat{\mathbf{n}}$  is the region outward normal. The surface  $\partial\Omega_{\text{out}}(\lambda \leq \lambda_\infty)$  extends along the upper ocean boundary and supports non-advection surface boundary fluxes. Likewise, the boundary  $\partial\Omega_{\text{bot}}(\lambda \leq \lambda_\infty)$  intersects the ocean bottom and generally experiences bottom boundary fluxes such as geothermal heating. Finally, the surface  $\partial\Omega(\lambda)$  has non-advection fluxes that cross the  $\lambda$ -interface, with diffusive fluxes the canonical example. The boundary area integrated non-advection fluxes give rise to non-advection transports, with dimensions of mass of  $\lambda$  per time, that are written using the shorthand

$$-\int_{\partial\Omega(\lambda \leq \lambda_\infty)} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} = E_{\text{out}}(\lambda, \lambda_\infty) + E_{\text{bot}}(\lambda, \lambda_\infty) + E(\lambda), \quad (50.78)$$

with a term having a positive value if it increases the  $\lambda$  mass of the region. We furthermore find it useful to introduce the distribution functions according to

$$E_{\text{out}}(\lambda, \lambda_\infty) + E_{\text{bot}}(\lambda, \lambda_\infty) = \int_\lambda^{\lambda_\infty} [\dot{m}_{\text{out}}^{\text{E}}(\lambda') + \dot{m}_{\text{bot}}^{\text{E}}(\lambda')] d\lambda', \quad (50.79)$$

where

$$\dot{m}_{\text{out}}^{\text{E}}(\lambda) d\lambda = \text{mass of } \lambda \text{ per time from } \partial\Omega_{\text{out}} \text{ transport in range } [\lambda - d\lambda/2, \lambda + d\lambda/2] \quad (50.80\text{a})$$

$$\dot{m}_{\text{bot}}^{\text{E}}(\lambda) d\lambda = \text{mass of } \lambda \text{ per time from } \partial\Omega_{\text{bot}} \text{ transport in range } [\lambda - d\lambda/2, \lambda + d\lambda/2]. \quad (50.80\text{b})$$

 *$\lambda$  transported with interior boundary mass fluxes*

We next consider the contribution to the budget equation (50.74) arising from the transport of  $\lambda$  with mass that crosses the interior boundary,  $\partial\Omega(\lambda)$ , whereby

$$-\int_{\partial\Omega(\lambda)} \rho \lambda (\mathbf{v} - \mathbf{v}^{(\lambda)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = -\lambda \int_{\partial\Omega(\lambda)} \rho (\mathbf{v} - \mathbf{v}^{(\lambda)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = \lambda G(\lambda), \quad (50.81)$$

To reach this result we noted that  $\lambda$  can be pulled outside of the  $\partial\Omega(\lambda)$  integral since it is constant along this surface, thus allowing for the introduction of the water mass transformation,  $G(\lambda)$ , given by equation (50.40).

*Surface boundary mass fluxes*

The final term contributing to the right hand side of the  $\lambda$  budget equation (50.74) arises from the surface mass transport along the boundary  $\partial\Omega_{\text{out}}(\lambda \leq \lambda_\infty)$

$$-\int_{\partial\Omega(\lambda \leq \lambda_\infty)} \rho \lambda (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\partial\Omega_{\text{out}}(\lambda \leq \lambda_\infty)} \lambda \mathcal{Q}_m d\mathcal{S} \equiv W^{(\lambda)}(\lambda, \lambda_\infty). \quad (50.82)$$

To reach the first equality we followed the steps in Section 50.5.2 by using the kinematic boundary condition (14.63) to introduce the surface mass transport,  $\mathcal{Q}_m d\mathcal{S}$ . The final equality introduced a shorthand that corresponds to the  $W(\lambda, \lambda_\infty)$  from Section 50.5.2. In the following, we find it

useful to introduce the mass distribution function  $\dot{m}_w(\lambda)$  from equation (50.69), thus rendering

$$W(\lambda, \lambda_\infty) = \int_\lambda^{\lambda_\infty} \dot{m}_w(\lambda') d\lambda' \quad \text{and} \quad W^{(\lambda)}(\lambda, \lambda_\infty) = \int_\lambda^{\lambda_\infty} \lambda \dot{m}_w(\lambda') d\lambda'. \quad (50.83)$$

Following the discussion in Sections 49.5.2, we have not assumed a relation between  $\lambda$  along the interface,  $\partial\Omega_{\text{out}}(\lambda \leq \lambda_\infty)$ , and the concentration,  $\lambda_m$ , contained in the entering mass. We prefer to keep the discussion general for now, providing a relation only when necessary.

### 50.6.2 Summary of the $\lambda$ budget

Bringing terms together leads to the  $\lambda$  mass budget equation (50.74) in the form

$$\begin{aligned} \frac{d}{dt} \left[ \int_{\Omega(\lambda \leq \lambda_\infty)} \rho \lambda dV \right] \\ = \dot{Y}(\lambda \leq \lambda_\infty) + E_{\text{out}}(\lambda, \lambda_\infty) + E_{\text{bot}}(\lambda, \lambda_\infty) + E(\lambda) + W^{(\lambda)}(\lambda, \lambda_\infty) + \lambda G(\lambda). \end{aligned} \quad (50.84)$$

This budget takes the equivalent form in terms of the distribution functions

$$\frac{d}{dt} \int_\lambda^{\lambda_\infty} \lambda' m(\lambda') d\lambda' = \int_\lambda^{\lambda_\infty} [\dot{m}_{\dot{Y}}(\lambda') + \dot{m}_{\text{out}}^E(\lambda') + \dot{m}_{\text{bot}}^E(\lambda') + \lambda \dot{m}_w(\lambda')] d\lambda' + E(\lambda) + \lambda G(\lambda). \quad (50.85)$$

Setting  $\lambda$  to a global constant and assuming there are no seawater mass sources leads to the seawater mass budget for the  $\lambda_\infty$ -region

$$\frac{d}{dt} \left[ \int_{\Omega(\lambda \leq \lambda_\infty)} \rho dV \right] = W(\lambda, \lambda_\infty) + G(\lambda), \quad (50.86)$$

which takes on the following form in terms of distributions

$$\frac{d}{dt} \int_\lambda^{\lambda_\infty} m(\lambda') d\lambda' = \int_\lambda^{\lambda_\infty} \dot{m}_w(\lambda') d\lambda' + G(\lambda). \quad (50.87)$$

### 50.6.3 Processes leading to water mass transformation

We now focus on the left hand side of equation (50.86) for the purpose of identifying terms leading to water mass transformation by making use of the moment equation (50.37) to write

$$\int_{\Omega(\lambda \leq \lambda_\infty)} \rho \lambda dV = M(\lambda, \lambda_\infty) \langle \lambda \rangle = M(\lambda, \lambda_\infty) \lambda + \int_\lambda^{\lambda_\infty} M(\lambda', \lambda_\infty) d\lambda', \quad (50.88)$$

which then leads to

$$\frac{d[M(\lambda, \lambda_\infty) \langle \lambda \rangle]}{dt} = \lambda \frac{dM(\lambda, \lambda_\infty)}{dt} + \int_\lambda^{\lambda_\infty} \frac{dM(\lambda', \lambda_\infty)}{dt} d\lambda'. \quad (50.89)$$

*Integrated water mass transformation over the  $\lambda_\infty$ -region*

Use of the  $\lambda$  budget equation (50.86) for the left hand side of equation (50.89), and the mass budget equation (50.86) for the right hand side renders

$$\begin{aligned}\dot{Y}(\lambda \leq \lambda_\infty) + E_{\text{out}}(\lambda, \lambda_\infty) + E_{\text{bot}}(\lambda, \lambda_\infty) + E(\lambda) + W^{(\lambda)}(\lambda, \lambda_\infty) + \lambda G(\lambda) \\ = \lambda [W(\lambda, \lambda_\infty) + G(\lambda)] + \int_\lambda^{\lambda_\infty} [W(\lambda', \lambda_\infty) + G(\lambda')] d\lambda'.\end{aligned}\quad (50.90)$$

Contributions from the surface boundary mass fluxes cancel as per the following identity

$$W^{(\lambda)}(\lambda, \lambda_\infty) - \lambda W(\lambda, \lambda_\infty) = \int_\lambda^{\lambda_\infty} (\lambda' - \lambda) \dot{m}_w(\lambda') d\lambda' \quad (50.91a)$$

$$= \int_\lambda^{\lambda_\infty} \left[ \int_{\lambda'}^{\lambda_\infty} \dot{m}_w(\lambda'') d\lambda'' \right] d\lambda' \quad (50.91b)$$

$$= \int_\lambda^{\lambda_\infty} W(\lambda', \lambda_\infty) d\lambda', \quad (50.91c)$$

where the second equality follows from the double integral formula (3.97). To understand the physical reason we see no water mass transformation from surface mass fluxes, recall the discussion in Section 49.5.2. Namely, mixing and internal sources provide the only means for irreversible changes to water masses and thus to water mass transformation. In contrast, boundary mass transport contributes to transformation only if the mass participates in mixing. That is, the mass associated with boundary mass transport is incorporated into the ocean (or leaves the ocean) only in the presence of mixing. It is thus reassuring that the formalism leads to this same conclusion. Furthermore, this result is consistent with the expression (50.45b), whereby the water mass transformation is, again, determined solely in terms of the non-advectional fluxes at the region boundaries plus the interior source term.

Cancelling the mass transport terms thus leads to the integrated water mass transformation

$$\int_\lambda^{\lambda_\infty} G(\lambda') d\lambda' = \dot{Y}(\lambda \leq \lambda_\infty) + E_{\text{out}}(\lambda, \lambda_\infty) + E_{\text{bot}}(\lambda, \lambda_\infty) + E(\lambda), \quad (50.92)$$

which is, again, just another way to write equation (50.45b). We thus see that the accumulated effects from sources within the interior plus non-advectional fluxes along the surface and interior boundaries lead to an integrated interior water mass transformation. Note that each term in this equation has dimensions of  $\lambda$ -mass per time.

*Water mass transformation across the  $\lambda$ -interface*

We can develop an expression for the water mass transformation across the  $\lambda$ -interface by taking  $\partial/\partial\lambda$  of equation (50.92) to reveal

$$G(\lambda) = -\frac{\partial}{\partial\lambda} \left[ \dot{Y}(\lambda \leq \lambda_\infty) + E_{\text{out}}(\lambda, \lambda_\infty) + E_{\text{bot}}(\lambda, \lambda_\infty) + E(\lambda) \right], \quad (50.93)$$

thus revealing that the water mass transformation across a  $\lambda$ -surface is the  $\lambda$ -convergence of the mixing processes plus the interior sources. Finally, this equation takes on the following distributional form

$$G(\lambda) = \dot{m}_{\dot{Y}}(\lambda) + \dot{m}_{\text{bot}}^E(\lambda) + \dot{m}_{\text{out}}^E(\lambda) - \frac{\partial E(\lambda)}{\partial\lambda}. \quad (50.94)$$

## 50.7 Surface water mass transformation

We have articulated all the terms needed to form the  $\Delta\lambda$ -layer mass budget according to Figure 50.6 as well as the  $\lambda_\infty$ -region mass budget according to Figure 50.8. In this section we focus on contributions to transformation from surface processes in the transformation equation (50.94)

$$G_{\text{out}}(\lambda) \equiv -\frac{\partial E_{\text{out}}(\lambda, \lambda_\infty)}{\partial \lambda} = \dot{m}_{\text{out}}^E(\lambda) = -\lim_{\delta\lambda \rightarrow 0} \frac{1}{\delta\lambda} \int_{\partial\Omega_{\text{out}}(\lambda \pm \delta\lambda/2)} \mathbf{J} \cdot \hat{\mathbf{n}} \, d\mathcal{S}, \quad (50.95)$$

where the final equality made use of equation (50.45b). Such *surface transformation* forms the focus of many studies of water mass transformation because it only requires surface boundary information, which is generally more accessible than information from interior ocean mixing processes or bottom geothermal processes. Furthermore, much of the transformation of water occurs in surface regions since this region is home to large contributions from surface boundary fluxes and associated ocean mixing. The basic equation we use is the non-advection flux equation (15.80), rewritten here for our scalar field  $\lambda$

$$-\mathbf{J} \cdot \hat{\mathbf{n}} = \mathcal{Q}_\lambda - \lambda \mathcal{Q}_m = \mathcal{Q}_\lambda^{\text{non-adv}} + (\lambda_m - \lambda) \mathcal{Q}_m. \quad (50.96)$$

### 50.7.1 Circulation driven by surface transformation

The layer mass budget (50.71) and its continuous expression (50.73) provide the basis for inferences about circulation and transformation. As an illustration, consider the continuous expression (50.73) and integrate from the reference value up to  $\lambda$

$$\int_{\lambda_\infty}^\lambda \Psi \, d\lambda' = \int_{\lambda_\infty}^\lambda \left[ -\frac{\partial M}{\partial t} + W - G \right] \, d\lambda'. \quad (50.97)$$

The left hand side is an expression for the circulation in  $\lambda$ -space at the specified interior open boundary. The right hand side means that a nonzero circulation is driven by mass through the ocean surface, convergence of mass transformed across the  $\lambda$ -interfaces, and/or time changes to the mass within the domain. Correspondingly, in the absence of surface boundary mass fluxes, a steady circulation is driven just by water mass transformation

$$\int_{\lambda_\infty}^\lambda \Psi \, d\lambda' = - \int_{\lambda_\infty}^\lambda G \, d\lambda'. \quad (50.98)$$

We depict an example in Figure 50.9 where the surface outcrop of the layer is exposed to air-sea interactions that lead to a meridional movement of the  $\lambda - \Delta\lambda/2$ -interface. This movement laterally entrains mass into the layer. If there is a net convergence of mass into the layer, then the layer mass increases. A steady state mass budget for the layer is reached if the amount of mass entrained through surface transformation is reflected in the same mass leaving through the circulation at the open boundary  $\partial\Omega_{\text{in}}(\lambda \pm \Delta\lambda/2)$ . We depict another case in Figure 50.10, here focusing on how a meridional gradient in the surface buoyancy loss causes entrainment into buoyancy layers. These and other statements related to the water mass budget are rather routine mathematically. Yet since the mass budget is formulated over layers, the mass budget offers the means to make very general statements about the circulation even without a direct measurement of the flow. This is a key power of water mass analysis.

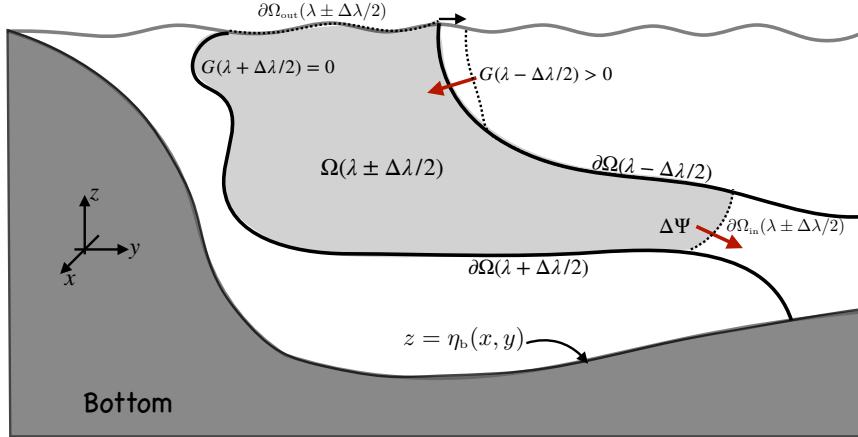


FIGURE 50.9: An example of a surface transformation driven circulation oriented according to the Southern Ocean with Antarctica to the left. Here we depict a layer that is exposed to some form of air-sea interaction that causes the  $\lambda - \Delta\lambda/2$ -interface to move meridionally. For example, if  $\lambda = \gamma$ , then an air-sea buoyancy flux generally causes  $\gamma$  outcrops to move laterally. Movement of the near-surface portion of the  $\partial\Omega(\lambda - \Delta\lambda/2)$  interface causes seawater to entrain into the layer and thus contribute to the surface water mass transformation  $G(\lambda - \Delta\lambda/2) > 0$  (red arrow near the surface directed to the south). In turn, the boundary  $\partial\Omega_{in}(\lambda \pm \Delta\lambda/2)$  expands as the near-surface portion of the interface  $\partial\Omega(\lambda - \Delta\lambda/2)$  moves to the south as a result of the entrained new water (black arrow moving to the north). If there is a net convergence of water mass into the layer (e.g., by having less mass move across the other layer interface at  $\partial\Omega(\lambda + \Delta\lambda/2)$ ), then mass accumulates within the layer  $[\lambda - \Delta\lambda/2, \lambda + \Delta\lambda/2]$ . There is a steady state (i.e., layer mass is constant) only if the same amount of mass that converges into the layer via surface or interior water mass transformation leaves the layer through circulation at the boundary  $\partial\Omega_{in}(\lambda \pm \Delta\lambda/2)$ .

### 50.7.2 Further study

Much of the formalism in this section follows that reviewed by [Groeskamp et al. \(2019\)](#). This paper offers specific examples of water mass transformation analysis as well as citations to numerous research papers.

## 50.8 Buoyancy water mass transformation

In Section 50.2 we considered the transformation of water masses as defined by buoyancy classes, with  $\lambda = \gamma$  where  $\gamma$  is a field whose isosurfaces approximate constant buoyancy directions; i.e., the neutral directions from Section 24.5. We here fill in further details for such buoyancy water mass analysis.

### 50.8.1 Material time changes to $S$ and $\Theta$

The material time derivative of  $\gamma$  can be written as the sum of contributions from salinity and Conservative Temperature

$$\rho \dot{\gamma} = \frac{\partial \gamma}{\partial S} \rho \dot{S} + \frac{\partial \gamma}{\partial \Theta} \rho \dot{\Theta}. \quad (50.99)$$

Following the decomposition of the water mass transformation in Section 50.4.3, for a general tracer, we here write the material time derivatives in the form

$$\rho \dot{S} = -\nabla \cdot \mathbf{J}_{int}^{(S)} - \mathbf{J}_{out}^{(S)} \cdot \hat{\mathbf{n}} \delta(z - \eta) - \mathbf{J}_{bot}^{(S)} \cdot \hat{\mathbf{n}} \delta(z - \eta_b) \quad (50.100a)$$

$$\rho \dot{\Theta} = -\nabla \cdot \mathbf{J}_{int}^{(\Theta)} - \mathbf{J}_{out}^{(\Theta)} \cdot \hat{\mathbf{n}} \delta(z - \eta) - \mathbf{J}_{bot}^{(\Theta)} \cdot \hat{\mathbf{n}} \delta(z - \eta_b), \quad (50.100b)$$

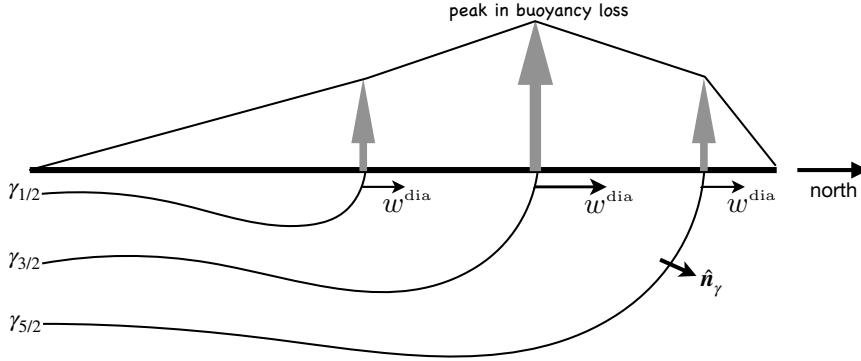


FIGURE 50.10: An example of surface water mass transformation, here illustrating the effects of transformation due to a meridional gradient in the surface buoyancy loss (we here assume that  $\lambda$  is buoyancy as measured by the neutral density  $\gamma$ ). The example is oriented for the northern hemisphere with increasing latitudes to the north/right. Buoyancy loss is denoted by the blue vertical arrows indicating the removal of buoyancy from the ocean, thus causing surface water to loose buoyancy. The surface buoyancy loss causes  $\gamma$  interfaces to migrate to the south, which in turn causes dianeutral mass flux to move from lighter layers to denser layers (black vectors pointed to the north,  $w^{\text{dia}}$ ). With a peak in the buoyancy loss at a particular latitude, more entrainment is driven into the layer to the north of the peak (water converges to the layer  $\gamma_{3/2} \leq \gamma \leq \gamma_{5/2}$ ) and less entrainment into the layer to the south (water diverges from the layer  $\gamma_{1/2} \leq \gamma \leq \gamma_{3/2}$ ).

where we assumed there are no interior sources of  $S$  or  $\Theta$ . The surface and bottom boundary contributions are weighted by Dirac delta distributions and projected into the normal direction along the two respective boundary surfaces. Following from the decomposition of water mass transformation given by equation (50.48), we are thus led to the following form for buoyancy

$$\begin{aligned}
G(\gamma) = & - \underbrace{\lim_{\delta\gamma \rightarrow 0} \frac{1}{\delta\gamma} \int_{\Omega(\gamma \pm \delta\gamma/2)} \left( \frac{\partial\gamma}{\partial S} \nabla \cdot \mathbf{J}_{\text{int}}^{(S)} + \frac{\partial\gamma}{\partial \Theta} \nabla \cdot \mathbf{J}_{\text{int}}^{(\Theta)} \right) dV}_{\text{interior buoyancy transformation} = \text{volume integral of convergence}} \\
& - \underbrace{\lim_{\delta\gamma \rightarrow 0} \frac{1}{\delta\gamma} \int_{\partial\Omega_{\text{out}}(\gamma \pm \delta\gamma/2)} \left( \frac{\partial\gamma}{\partial S} \mathbf{J}_{\text{out}}^{(S)} + \frac{\partial\gamma}{\partial \Theta} \mathbf{J}_{\text{out}}^{(\Theta)} \right) \cdot \hat{\mathbf{n}} d\mathcal{S}}_{\text{surface buoyancy transformation} = \text{area integral of surface boundary fluxes}} \\
& - \underbrace{\lim_{\delta\gamma \rightarrow 0} \frac{1}{\delta\gamma} \int_{\partial\Omega_{\text{bot}}(\gamma \pm \delta\gamma/2)} \left( \frac{\partial\gamma}{\partial S} \mathbf{J}_{\text{bot}}^{(S)} + \frac{\partial\gamma}{\partial \Theta} \mathbf{J}_{\text{bot}}^{(\Theta)} \right) \cdot \hat{\mathbf{n}} d\mathcal{S}}_{\text{bottom buoyancy transformation} = \text{area integral of bottom boundary fluxes}}. \tag{50.101}
\end{aligned}$$

This expression is explored in the remainder of this section.

### 50.8.2 Interior buoyancy water mass transformation

Contributions from cabling, thermobaricity, and halobaricity (Section 49.3) arise from the interior transformation appearing in equation (50.101). Furthermore, in the special case of a linear equation of state, whereby  $\partial\gamma/\partial\Theta$  and  $\partial\gamma/\partial S$  are constants, then equation (50.54) means that the global integral of the interior transformation vanishes

$$\int_{\gamma_{-\infty}}^{\gamma_{\infty}} G_{\text{int}}(\gamma) d\gamma = \int_{\mathcal{R}} \left( \frac{\partial\gamma}{\partial S} \nabla \cdot \mathbf{J}_{\text{int}}^{(S)} + \frac{\partial\gamma}{\partial \Theta} \nabla \cdot \mathbf{J}_{\text{int}}^{(\Theta)} \right) dV = 0 \quad \text{if } \nabla(\partial\gamma/\partial\Theta) = 0, \nabla(\partial\gamma/\partial S) = 0, \tag{50.102}$$

where  $\mathcal{R}$  is the global ocean domain. By inference, we conclude that any nonzero result for this integral is a global measure of the effects from the nonlinear equation of state

$$\text{contribution from nonlinear equation of state} = \int_{\gamma_{-\infty}}^{\gamma_{\infty}} G_{\text{int}}(\gamma) d\gamma. \quad (50.103)$$

### 50.8.3 Surface non-advection flux for $S$ and $\Theta$

We review a few of the distinct characteristics of surface non-advection fluxes of  $S$  and  $\Theta$  as detailed in Section 49.5.2, here working with salinity,  $S$ , rather than salt concentration,  $S = S/1000$ .

#### *Non-advection salt flux*

The non-advection surface boundary flux for salt is given by equation (49.67), here written as

$$-\mathbf{J}^{(S)} \cdot \hat{\mathbf{n}} = \mathcal{Q}_S^{\text{non-adv}} + (S_m - S) \mathcal{Q}_m, \quad (50.104)$$

where  $\mathcal{Q}_S^{\text{non-adv}}$  is a non-advection salt flux, such as might arise from parameterized turbulent transfer. For the salt concentration of water crossing the ocean surface, we generally take  $S_m = 0$  for precipitation, evaporation, and river runoff, whereas  $S_m \neq 0$  for ice melt and formation. Furthermore, the boundary term,  $S = S(z = \eta)$ , is commonly approximated by the bulk salt concentration in the upper ocean.

#### *Non-advection flux for Conservative Temperature*

For Conservative Temperature we follow the discussion in Section 49.5.3, whereby the non-advection flux is given by equation

$$-\mathbf{J}^{(\Theta)} \cdot \hat{\mathbf{n}} = \mathcal{Q}_{\Theta}^{\text{non-adv}} + (\Theta_m - \Theta) \mathcal{Q}_m. \quad (50.105)$$

It is common to approximate the difference  $\Theta_m - \Theta(z = \eta) = 0$ , in which case the non-advection flux is just due to turbulent and radiative heat fluxes

$$-\mathbf{J}^{(\Theta)} \cdot \hat{\mathbf{n}} = \mathcal{Q}_{\Theta}^{\text{non-adv}} \text{ if } \Theta_m - \Theta(z = \eta) = 0. \quad (50.106)$$

### 50.8.4 Surface buoyancy water mass transformation

To touch base with the commonly employed surface buoyancy transformation, insert the surface fluxes into equation (50.101) as per Section 50.8.3 to write

$$\begin{aligned} G(\gamma)^{\text{surface}} &= \\ &\lim_{\delta\gamma \rightarrow 0} \frac{1}{\delta\gamma} \int_{\partial\Omega_{\text{out}}(\gamma \pm \delta\gamma/2)} (\gamma \beta_S [\mathcal{Q}_S^{\text{non-adv}} + (S_m - S) \mathcal{Q}_m] - \gamma \alpha_{\Theta} [\mathcal{Q}_{\Theta}^{\text{non-adv}} + (\Theta_m - \Theta) \mathcal{Q}_m]) d\mathcal{S}, \end{aligned} \quad (50.107)$$

where we introduced the thermal expansion and saline contraction coefficients, here defined according to<sup>13</sup>

$$\alpha_{\Theta} = -\frac{1}{\gamma} \frac{\partial \gamma}{\partial \Theta} \quad \text{and} \quad \beta_S = \frac{1}{\gamma} \frac{\partial \gamma}{\partial S}. \quad (50.108)$$

<sup>13</sup>In practice, it is common to replace the factor of  $\gamma^{-1}$  with  $\rho_0^{-1}$  on the right hand side of equation (50.108), with  $\rho_0$  the constant Boussinesq reference density from Chapter 23.

Recall that  $G(\gamma) > 0$  occurs when water is transformed into regions with larger  $\gamma$ . For example, net surface cooling in the presence of a positive thermal expansion coefficient ( $\alpha_\Theta > 0$ ) leads to  $\mathcal{Q}_\Theta^{\text{non-adv}} + (\Theta_m - \Theta) \mathcal{Q}_m < 0$ . Such cooling then leads to a positive contribution to  $G(\gamma)_{\text{surface}}$  as water is transformed from light to heavy  $\gamma$ -classes. Likewise, a positive net salt transport into the upper ocean,  $\mathcal{Q}_S^{\text{non-adv}} + (S_m - S) \mathcal{Q}_m > 0$ , leads to a positive contribution to  $G(\gamma)_{\text{surface}}$ .

The integrand to equation (50.107) corresponds to minus the surface buoyancy flux derived in Section 49.6.3. The only difference is that we here make use of the surface element,  $d\mathcal{S}$ , and the corresponding fluxes  $\mathcal{Q}_\Theta^{\text{non-adv}}$ ,  $\mathcal{Q}_S^{\text{non-adv}}$ , and  $\mathcal{Q}_m$ . However, if the ocean surface has no overturns, we can write its vertical position as  $z = \eta(x, y, t)$  and can also define the horizontal projection of the area element as (see equation (5.30))

$$d\mathcal{S} = \sqrt{1 + |\nabla \eta|^2} dA. \quad (50.109)$$

In this case we can introduce the fluxes  $Q_\Theta^{\text{non-adv}}$ ,  $Q_S^{\text{non-adv}}$ , and  $Q_m$  used in Section 49.6.3 via

$$\mathcal{Q}_\Theta^{\text{non-adv}} d\mathcal{S} = Q_\Theta^{\text{non-adv}} dA \quad \text{and} \quad \mathcal{Q}_S^{\text{non-adv}} d\mathcal{S} = Q_S^{\text{non-adv}} dA \quad \text{and} \quad \mathcal{Q}_m d\mathcal{S} = Q_m dA, \quad (50.110)$$

to render

$$\begin{aligned} G(\gamma)^{\text{surface}} = \\ \lim_{\delta\gamma \rightarrow 0} \frac{1}{\delta\gamma} \int_{\partial\Omega_{\text{out}}(\gamma \pm \delta\gamma/2)} (\gamma \beta_s [Q_S^{\text{non-adv}} + (S_m - S) Q_m] - \gamma \alpha_\Theta [Q_\Theta^{\text{non-adv}} + (\Theta_m - \Theta) Q_m]) dA. \end{aligned} \quad (50.111)$$

Integrating the surface transformation (50.111) over all  $\gamma$ -classes leads to the identity<sup>14</sup>

$$\begin{aligned} \int_{\gamma=-\infty}^{\gamma=\infty} G(\gamma)^{\text{surface}} d\gamma = \\ \int_{z=\eta} (\gamma \beta_s [Q_S^{\text{non-adv}} + (S_m - S) Q_m] - \gamma \alpha_\Theta [Q_\Theta^{\text{non-adv}} + (\Theta_m - \Theta) Q_m]) dA. \end{aligned} \quad (50.112)$$

This equality means that the diagnosed surface transformation,  $G(\gamma)^{\text{surface}}$ , which is obtained by binning surface fluxes into  $\gamma$ -classes, must properly add up to the area integrated surface fluxes as weighted by the surface value of  $\gamma$ . This equality can be a useful check on the integrity of numerical binning code used to diagnose surface water mass transformation.

## 50.9 Tracer mass analysis

In Sections 50.5 and 50.6 we developed the budgets for  $\lambda$  within layers defined  $\lambda$ . Here we extend that analysis to develop budgets for a tracer concentration,  $C$ , localized in a region within a layer of buoyancy,  $\gamma$ , as depicted in Figure 50.11. The upper panels to this figure illustrate a tracer patch in geographic/depth space along with isolines of buoyancy, whereas the lower panels show the tracer distribution (histogram) binned within the buoyancy classes. If the tracer is mixed within a layer, such as via the neutral diffusion process of Section 48.4, then the tracer patch is spread laterally within the buoyancy layer and yet the distribution (lower panel) is unchanged. In contrast, if the tracer is mixed across layer interfaces then the tracer distribution is spread within buoyancy space.

<sup>14</sup>The density bound  $\gamma_{-\infty}$  is a constant that is lower than any  $\gamma$  realized in the global domain, whereas  $\gamma_\infty$  is a constant that is larger than any realized  $\gamma$ .

Another means to alter the tracer distribution is to modify the buoyancy field. This situation is especially common for tracer near the surface, where boundary buoyancy forcing can act to move the layers thus causing tracer to move between layers even if the tracer patch is stationary in geographical space. That is, if the tracer moves at a velocity distinct from the buoyancy field, then its distribution within buoyancy classes will change.

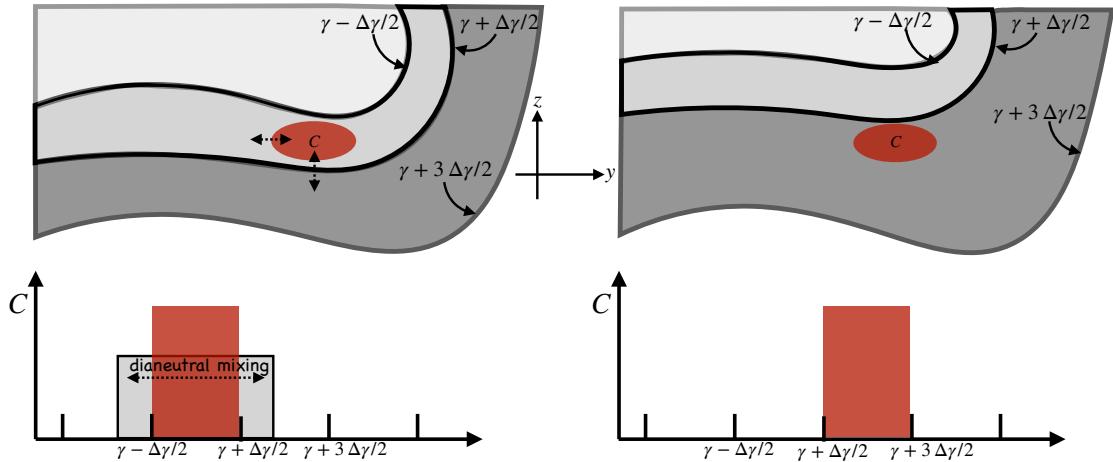


FIGURE 50.11: Depicting a tracer patch within the buoyancy layer bounded by the interface values  $[\gamma - \Delta\gamma/2, \gamma + \Delta\gamma/2]$  (left panel) and  $[\gamma + \Delta\gamma/2, \gamma + 3\Delta\gamma/2]$  (right panel). The upper panels show the tracer and buoyancy in geographic/depth space whereas the bottom panels show the tracer distribution (histogram) binned according to buoyancy. There are two general means to modify the distribution of tracer within the buoyancy classes. The first occurs via dianeutral mixing that spreads the tracer distribution to other buoyancy layers as depicted by the vertical arrow in the upper left panel and the horizontal arrows in the lower left panel. The lateral arrow in the upper left panel depicts neutral diffusion, which laterally spreads the tracer within a layer but does not alter the distribution across layers (see Section 48.4). The second means to alter the distribution occurs when the buoyancy surfaces move relative to the tracer. This scenario is depicted in the lower right panel whereby the tracer patch originally in buoyancy layer  $[\gamma - \Delta\gamma/2, \gamma + \Delta\gamma/2]$  now finds itself in the layer  $[\gamma + \Delta\gamma/2, \gamma + 3\Delta\gamma/2]$ . This depiction is not realistic, since motion of interior buoyancy surfaces generally occurs along with mixing of tracer patches. Nonetheless, this example emphasizes that motion of the buoyancy surfaces need not coincide with motion of the tracer patch.

### 50.9.1 General form of the mass budget

As depicted in Figure 50.11 for buoyancy layers, and Figure 50.12 for generic layers, there are two general processes whereby a tracer distribution within layers can be modified: (i) the tracer can mix between layers and (ii) the layers can move relative to the tracer. These ideas transcend buoyancy and thus can be applied to any scalar field,  $\lambda$ , used to classify water masses. We quantify these two processes by writing the time change of tracer content within a  $\lambda$ -layer, which is arrived at by applying the Leibniz-Reynolds transport theorem from Section 15.3.4 to a  $\lambda$ -layer

$$\frac{d}{dt} \Delta M_C(\lambda \pm \Delta\lambda/2) = \int_{\Omega(\lambda \pm \Delta\lambda/2)} \rho \dot{C} dV - \oint_{\partial\Omega(\lambda \pm \Delta\lambda/2)} \rho C (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} dS, \quad (50.113)$$

where

$$\Delta M_C(\lambda \pm \Delta\lambda/2) = \int_{\Omega(\lambda \pm \Delta\lambda/2)} \rho C dV \quad (50.114)$$

is the mass of tracer within the layer. The volume integral on the right hand side of equation (50.113) arises from material time changes to the tracer within the layer, whereas the surface integral arises from dia-surface transport across the layer boundary.

### 50.9.2 Tracer processes

We determine the material time changes for a “conservative” tracer according to the convergence of a flux

$$\rho \dot{C} = \rho \frac{DC}{Dt} = -\nabla \cdot \mathbf{J}. \quad (50.115)$$

Many biogeochemical tracers have additional “non-conservative” source terms beyond the flux convergence considered here. These effects can be readily incorporated into the following by adding a source term that acts throughout a layer and not just at the layer boundaries.

Gauss’ divergence theorem converts the convergence,  $-\nabla \cdot \mathbf{J}$ , into the area integral of fluxes over the layer boundaries, including interior layer interfaces as well as intersections with the surface and bottom boundaries. For the interior interfaces it is typically simpler diagnostically to bin the volume integrated material time changes within the  $\lambda$ -classes. In contrast, the surface and bottom boundary contributions are fed into the budget via Neumann boundary conditions applied to the flux  $\mathbf{J}$

$$\mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} = \text{boundary tracer transport}. \quad (50.116)$$

Note that when there is an advective/skew diffusive component to the subgrid scale flux (Chapters 47 and 48), then it adds to the resolved advective component to render a residual mean material time operator

$$\rho \frac{D^\dagger C}{Dt} = -\nabla \cdot \mathbf{J}_{\text{non-advect}}, \quad (50.117)$$

where

$$\frac{D^\dagger}{Dt} = \frac{\partial}{\partial t} + (\mathbf{v} + \mathbf{v}^*) \cdot \nabla, \quad (50.118)$$

with  $\mathbf{v}^*$  an eddy-induced velocity (see Section 48.1). For the purposes of water mass transformation analysis, we write

$$\dot{C} = \frac{D^\dagger C}{Dt}, \quad (50.119)$$

thus incorporating the eddy-induced stirring into the kinematic expression for the material time derivative.

There are many interior and boundary processes that contribute to  $\dot{C}$  within a layer. As a general expression for these contributions to the layer budget we write

$$\Delta E_C(\lambda \pm \Delta\lambda/2) = \int_{\Omega(\lambda \pm \Delta\lambda/2)} \rho \dot{C} dV = - \int_{\Omega(\lambda \pm \Delta\lambda/2)} \nabla \cdot \mathbf{J} dV \quad (50.120)$$

which is sometimes usefully decomposed into interior and surface boundary processes

$$\Delta E_C^{\text{int}}(\lambda \pm \Delta\lambda/2) = \int_{\Omega(\lambda \pm \Delta\lambda/2)} \rho \dot{C}^{\text{int}} dV \quad (50.121a)$$

$$\Delta E_C^{\text{out bdy}}(\lambda \pm \Delta\lambda/2) = - \int_{\partial\Omega_{\text{out}}(\lambda \pm \Delta\lambda/2)} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (50.121b)$$

If the region boundary intersects the ocean bottom along  $\partial\Omega_{\text{bot}}(\lambda \pm \Delta\lambda/2)$ , then there is an additional bottom boundary contribution in the form

$$\Delta E_C^{\text{bot bdy}}(\lambda \pm \Delta\lambda/2) = - \int_{\partial\Omega_{\text{bot}}(\lambda \pm \Delta\lambda/2)} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (50.122)$$

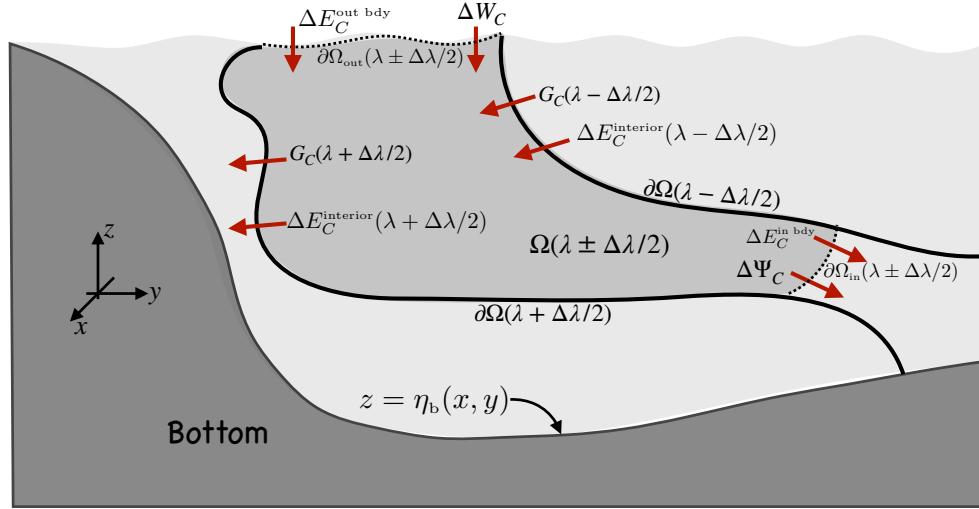


FIGURE 50.12: As for the schematic of a layer seawater mass budget depicted in Figure 50.6, we here illustrate the tracer budget within a layer of seawater with scalar property  $\lambda$  within the range  $[\lambda - \Delta\lambda/2, \lambda + \Delta\lambda/2]$  and defined over a geographical/depth domain  $\partial\Omega_{\text{in}}(\lambda \pm \Delta\lambda/2) + \partial\Omega_{\text{out}}(\lambda \pm \Delta\lambda/2) + \partial\Omega(\lambda + \Delta\lambda/2) + \partial\Omega(\lambda - \Delta\lambda/2)$ . The budget for a tracer,  $C$ , over this layer is affected by the transport of tracer substance across the variety of layer boundaries. Transport processes include those determined by mixing and/or radiation across interior and surface boundaries,  $\Delta E_C$  (equation (50.121b)). This term has no associated transfer of seawater mass and thus is absent from the water mass budget in Figure 50.6. Tracer budgets are also affected by processes that move seawater mass across layer boundaries: water mass transformation processes giving rise to  $G_C(\lambda \pm \Delta\lambda/2)$  (equation (50.123)); transport across the surface domain boundary,  $\Delta W_C$ , arising from precipitation, evaporation, runoff, and melt (equation (50.124)); and transport within the circulation crossing an interior domain boundary,  $\Delta\Psi_C$  (equation (50.125)).

### 50.9.3 Transport across an interior layer interface

The surface integral in the budget (50.113) involves transport across the layer interfaces, with this transport requiring motion of the interface relative to a fluid particle. The same formalism introduced earlier can be used to compute this transport. That is, we can generalize the transformation equation (50.43d) to write

$$G_C(\lambda) = \int_{\partial\Omega(\lambda)} \rho C (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} \, dS = \frac{\partial}{\partial \lambda} \int_{\Omega(\lambda_0 \leq \lambda)} \rho \dot{C} \, dV. \quad (50.123)$$

As a check, note that for the special case where the tracer concentration is a constant along the layer interface, then  $G_C(\lambda) = C G(\lambda)$ . We consider this special case in Section 50.10 when studying budgets over regions bounded by a tracer isosurface.

### 50.9.4 Transport across interior and surface boundaries

We now consider the impact on layer tracer mass budgets due to boundary transport. The budget contribution from mass fluxes crossing the ocean surface boundary is determined by making use of the surface kinematic boundary condition (15.79)

$$\Delta W_C = \int_{\partial\Omega_{\text{out}}(\lambda \pm \Delta\lambda/2)} \rho C (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} \, dS = \int_{\partial\Omega_{\text{out}}(\lambda \pm \Delta\lambda/2)} Q_m C_m \, dA, \quad (50.124)$$

where  $C_m$  is the tracer concentration within the mass transported across the boundary.<sup>15</sup> As a check, note that in the special case of a constant tracer concentration in the mass transported across the boundary, then  $\Delta W_C = C_m \Delta W$ , where  $\Delta W$  is the water mass transported across the ocean free surface as given by equation (50.66).

For the interior open boundary the contribution is written in the generic manner

$$\Delta\Psi_C = \int_{\partial\Omega_{in}(\lambda \pm \Delta\lambda/2)} C \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (50.125)$$

Again, in the special case where the tracer concentration is a constant along the interior boundary,  $C_b$ , then  $\Delta\Psi_C = C_b \Delta\Psi$ , where  $\Delta\Psi$  is the seawater mass transport given by equation (50.62).

### 50.9.5 The layer tracer budget

Bringing all terms together leads to the layer tracer mass budget

$$\frac{d\Delta M_C}{dt} + \Delta\Psi_C = \Delta E_C + \Delta W_C - [G_C(\lambda + \Delta\lambda/2) - G_C(\lambda - \Delta\lambda/2)], \quad (50.126)$$

which is directly analogous to the seawater layer mass budget (50.70), with the added term  $\Delta E_C$  arising from material tracer changes. As for the seawater mass budget discussed in Section 50.5.3, the layer tracer budget (50.126) provides the framework for rather general inferences about tracer transport within  $\lambda$ -classes.

### 50.9.6 Further study

Much in this section follows the treatment given by [Groeskamp et al. \(2019\)](#). This paper offers specific examples of tracer mass analysis, which is an area seeing many new applications within the ocean and atmospheric communities.

## 50.10 Regions bounded by a tracer contour/surface

In Section 50.9 we developed equations for a layer tracer budget where the scalar field,  $\lambda$ , that defines the layer is generally distinct from the tracer,  $C$ , whose budget we are studying. In this section we specialize to the case where we set  $\lambda = C$  so that the region boundaries are determined by the tracer whose budget is under study. These budgets were introduced in Sections 50.5 and 50.6, and here we derive some rather useful simplifications that arise as a result of setting  $\lambda = C$ .

As in Section 50.9, our starting point is the Leibniz-Reynolds budgets from Section 15.3.4 for seawater mass and tracer mass computed over an arbitrary region,  $\mathcal{R}$

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho C dV \right] = - \int_{\partial\mathcal{R}} [\rho C (\mathbf{v} - \mathbf{v}^{(b)}) + \mathbf{J}] \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (50.127a)$$

$$\frac{d}{dt} \left[ \int_{\mathcal{R}} \rho dV \right] = - \int_{\partial\mathcal{R}} [\rho (\mathbf{v} - \mathbf{v}^{(b)})] \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (50.127b)$$

The region  $\mathcal{R}$  is rather arbitrary, and can in general be disconnected. Throughout this section we

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<sup>15</sup>Note that equation (26) in [Groeskamp et al. \(2019\)](#) incorrectly writes the integrand in equation (50.124) as  $Q_m (C_m - C)$ .

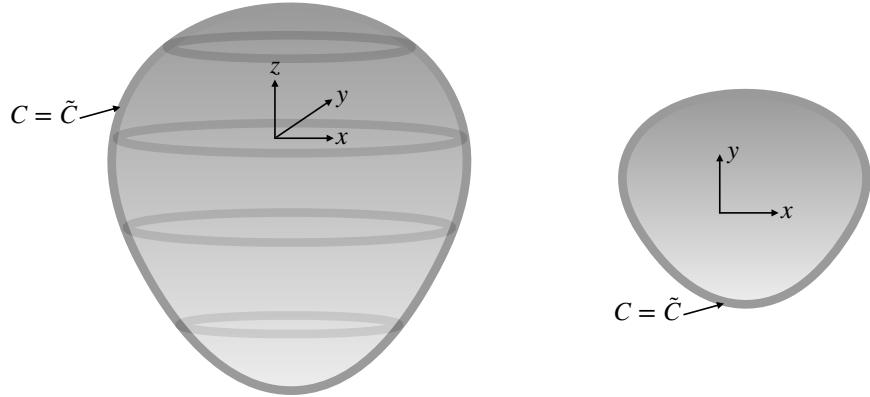


FIGURE 50.13: Left panel: a closed three-dimensional region,  $\tilde{\mathcal{R}}$ , with its boundary,  $\partial\tilde{\mathcal{R}}$ , defined by a surface of constant tracer concentration,  $C = \tilde{C}$ . Right panel: the analog closed two-dimensional region with its boundary defined by a contour of constant tracer concentration,  $C = \tilde{C}$ .

make use of the following shorthand notation for region-integrated quantities

$$M = \int_{\mathcal{R}} \rho dV \quad \text{region seawater mass} \quad (50.128a)$$

$$M_C = \int_{\mathcal{R}} C \rho dV \quad \text{region tracer mass} \quad (50.128b)$$

$$\langle C \rangle = \frac{1}{M} \int_{\mathcal{R}} C \rho dV = \frac{M_C}{M} \quad \text{region averaged tracer concentration.} \quad (50.128c)$$

### 50.10.1 Closed region bounded by a tracer surface/contour

Consider a closed region,  $\tilde{\mathcal{R}}$ , bounded by a surface of constant tracer concentration,  $C = \tilde{C}$ , such as depicted in Figure 50.13. The tracer budget (50.127a) for this region is given by

$$\frac{d(M \langle C \rangle)}{dt} = -\tilde{C} \int_{\partial\tilde{\mathcal{R}}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{\partial\tilde{\mathcal{R}}} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} \quad (50.129)$$

where we pulled the tracer concentration outside of the surface integral since, by construction, it is constant on the boundary,  $\partial\tilde{\mathcal{R}}$ . Use of the mass budget (50.127b) then leads to the rather tidy result

$$\frac{d[M(\langle C \rangle - \tilde{C})]}{dt} = - \int_{\partial\tilde{\mathcal{R}}} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (50.130)$$

The left hand side is the time change of the mass-weighted difference between the region averaged tracer concentration,  $\langle C \rangle$ , and the value of the tracer concentration defining the region boundary,  $\tilde{C}$ . These time changes are driven by a nonzero diffusive tracer transport bringing tracer mass across the region boundary. A nonzero diffusive flux on the region boundary arises only when there is a gradient of tracer concentration across that boundary. In the special case of a zero net diffusive tracer transport across the region boundary, the budget equation (50.130) reaches a steady state whereby

$$\frac{d}{dt} [M(\langle C \rangle - \tilde{C})] = 0 \iff \int_{\partial\tilde{\mathcal{R}}} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} = 0. \quad (50.131)$$

A 3D region bounded by a constant tracer concentration is not commonly encountered in large-scale ocean and atmospheric fluids. In contrast, we often encounter quasi-2D regions as depicted in Figure 50.14, in which one may find 2D regions bounded by a closed contour of

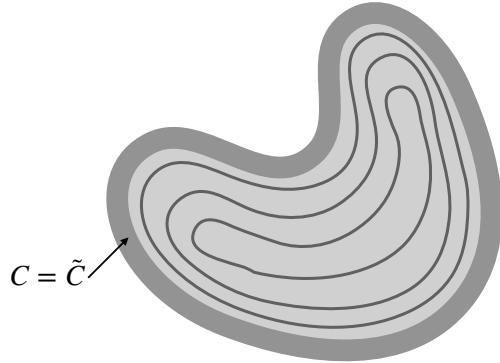


FIGURE 50.14: A two-dimensional region bounded by a finite-thick shell with constant tracer concentration,  $C = \tilde{C}$ . Inside the shell region the tracer concentration is not uniform.

constant tracer concentration. For example, in many parts of the ocean and atmosphere transport occurs predominantly along 2D surfaces defined by a constant buoyancy. We may thus find closed contours of tracer concentrations along constant buoyancy surfaces.

To help illustrate a necessary condition to reach a steady state, consider the particular example depicted in Figure 50.14. In this figure, the tracer contour defining the region boundary is a thick shell defined by a uniform concentration  $C = \tilde{C}$ . The diffusive flux vanishes at each point within the boundary shell since the tracer concentration is uniform. Hence, the steady budget (50.131) leads to

$$(\langle C \rangle - \tilde{C}) \frac{dM}{dt} + M \frac{d\langle C \rangle}{dt} = 0. \quad (50.132)$$

If the total seawater mass within the region is constant, then the averaged tracer concentration is also constant, so that both terms in this steady budget vanish individually. Even so, this configuration does not reach a steady state at each point throughout the domain interior. The reason is that diffusion in the interior causes tracer to move from regions of high concentration to low concentration. Consequently, at any particular point within the domain there is an evolving tracer concentration. The only way for each point to reach a steady state within a region bounded by a tracer contour is for the tracer concentration to be a uniform constant throughout the region interior

$$C = \tilde{C} \quad \text{steady state tracer throughout a closed tracer region.} \quad (50.133)$$

Diffusion thus expells tracer gradients from steady state regions bounded by closed tracer contours, thus leaving a homogenous interior.

## 50.10.2 Region with $C \geq \tilde{C}$

As a second example of the formalism, consider the tracer budget for a region where the tracer concentration is greater than or equal to a particular tracer value as depicted in Figure 50.15. In contrast to the domain in Figure 50.12, here there is no inner boundary. We introduce the

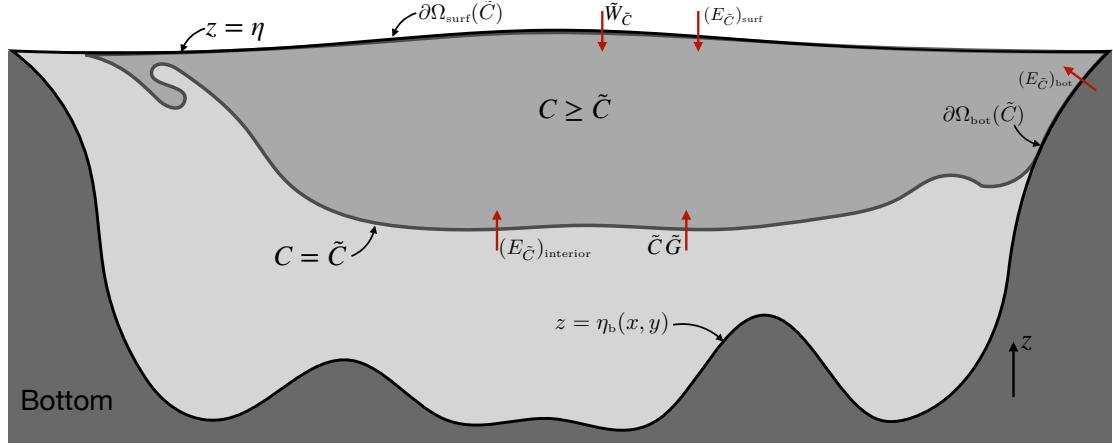


FIGURE 50.15: An ocean region where the tracer concentration is greater than a nominal value,  $C \geq \tilde{C}$ . A specific example is with  $C = \Theta$ , the Conservative Temperature, in which we are concerned with the ocean with temperature greater than  $\tilde{\Theta}$ . Here we depict a case where the tracer concentration generally increases upward (as with  $C = \Theta$ ), and yet with vertical stratification not everywhere monotonic, such as for  $C = \Theta$  in the high latitudes where salinity effects on density stratification become dominant. Transport processes affecting the budget of  $C$  within this region arise from mixing at the interior boundary and surface boundary,  $(E_{\tilde{C}})_{int}$  and  $(E_{\tilde{C}})_{surf}$ , advection at the surface,  $\tilde{W}_{\tilde{C}}$ , and the tracer weighted water mass transformation across the interior layer boundary,  $\tilde{C}\tilde{G}$ .

following terms in developing both the seawater mass budget and the tracer substance budget

$$\tilde{M} = \int_{C \geq \tilde{C}} \rho dV \quad \text{seawater mass in the region } C \geq \tilde{C} \quad (50.134a)$$

$$\tilde{M}_{\tilde{C}} = \int_{C \geq \tilde{C}} C \rho dV = \tilde{M} \langle C \rangle \quad \text{tracer mass in the region } C \geq \tilde{C} \quad (50.134b)$$

$$\tilde{G} = - \int_{C = \tilde{C}} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = - \int_{C = \tilde{C}} \rho w^{\text{dia}} d\mathcal{S} \quad \text{transformation across } \tilde{C} \quad (50.134c)$$

$$\tilde{G}_{\tilde{C}} = - \int_{C = \tilde{C}} C \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = - \int_{C = \tilde{C}} C \rho w^{\text{dia}} d\mathcal{S} \quad \text{tracer advected across } \tilde{C} \quad (50.134d)$$

$$\tilde{W} = - \int_{\partial\Omega_{surf}(\tilde{C})} \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\partial\Omega_{surf}(\tilde{C})} Q_m dA \quad \text{surface mass transport} \quad (50.134e)$$

$$\tilde{W}_{\tilde{C}} = - \int_{\partial\Omega_{surf}(\tilde{C})} C \rho (\mathbf{v} - \mathbf{v}^{(b)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = \int_{\partial\Omega_{surf}(\tilde{C})} C Q_m dA \quad \text{surface mass } C\text{-transport} \quad (50.134f)$$

$$(E_{\tilde{C}})_{int} = - \int_{C = \tilde{C}} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} \quad \text{subgrid } C\text{-transport across } \tilde{C} \quad (50.134g)$$

$$(E_{\tilde{C}})_{surf} = - \int_{\partial\Omega_{surf}(\tilde{C})} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} \quad \text{subgrid } C\text{-transport across surface} \quad (50.134h)$$

$$(E_{\tilde{C}})_{bot} = - \int_{\partial\Omega_{bot}(\tilde{C})} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} \quad \text{subgrid } C\text{-transport across bottom} \quad (50.134i)$$

Recall that  $\hat{\mathbf{n}}$  is the *outward* normal on a boundary so that positive values for the above transports increase the tracer mass within the region. For equations (50.134c) and (50.134d), we introduced the dia-surface transport velocity according to equation (50.38) for flow across the  $C = \tilde{C}$  layer interface. Likewise, for equations (50.134e) and (50.134f) we made use of the surface kinematic boundary condition (14.73c)

$$\rho(\mathbf{v} - \mathbf{v}^{(s)}) \cdot \hat{\mathbf{n}} d\mathcal{S} = -Q_m dA, \quad (50.135)$$

where  $Q_m$  is the mass transport across the free surface, with  $Q_m > 0$  adding mass to the ocean, and  $dA$  is the horizontal projection of the surface area element. By inspection of Figure 50.15, the seawater mass and tracer mass budgets for this region are given by

$$\frac{d\widetilde{M}}{dt} = \widetilde{G} + \widetilde{W} \quad (50.136a)$$

$$\frac{d[\widetilde{M} \langle C \rangle]}{dt} = \widetilde{C} \widetilde{G} + \widetilde{W}_{\widetilde{C}} + (E_{\widetilde{C}})_{\text{surf}} + (E_{\widetilde{C}})_{\text{bot}} + (E_{\widetilde{C}})_{\text{int}}, \quad (50.136b)$$

where we assumed that no mass crosses through the solid earth. Furthermore, along the  $\tilde{C}$ -boundary we pulled the tracer concentration outside of the surface integral to write  $\widetilde{G}_{\widetilde{C}} = \widetilde{C} \widetilde{G}$ .

Just as we did in Section 50.10.1, the tracer budget (50.136b) can be simplified by making use of the seawater mass budget (50.136a) to eliminate the water mass transformation contribution  $\widetilde{G}$ , thus rendering

$$\frac{d\widetilde{M}_{I\widetilde{C}}}{dt} = [\widetilde{W}_{\widetilde{C}} - \widetilde{W} \widetilde{C}] + (E_{\widetilde{C}})_{\text{surf}} + (E_{\widetilde{C}})_{\text{bot}} + (E_{\widetilde{C}})_{\text{int}}. \quad (50.137)$$

In this equation we introduced the *internal tracer mass* according to

$$\widetilde{M}_{I\widetilde{C}} \equiv \widetilde{M} (\langle C \rangle - \widetilde{C}) = \int_{C \geq \widetilde{C}} (C - \widetilde{C}) \rho dV. \quad (50.138)$$

For completeness we express the internal tracer mass budget (50.137) in its integral form

$$\frac{d\widetilde{M}_{I\widetilde{C}}}{dt} = \int_{\partial\Omega_{\text{out}}} \left[ Q_m (C - \widetilde{C}) dA - \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} \right] - \int_{\partial\Omega_{\text{bot}}} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S} - \int_{C=\widetilde{C}} \mathbf{J} \cdot \hat{\mathbf{n}} d\mathcal{S}. \quad (50.139)$$

### 50.10.3 Comments and further study

Elimination of the watermass transformation,  $\widetilde{G}$ , from the internal tracer mass budget equations (50.137) and (50.139) offers a practical advantage since  $\widetilde{G}$  can be rather noisy in applications. Furthermore, for some applications (e.g., see [Holmes et al. \(2019\)](#)) it is sufficient to consider the simpler budget (50.137) for internal tracer mass, rather than the budget (50.136b) for the total tracer mass.

The two-dimensional version of the result (50.133) was studied by [Rhines and Young \(1982\)](#) when studying the mechanics of isopycnal quasi-geostrophic potential vorticity in ocean gyres. We further consider their result in Exercise 46.10. It is satisfying to see their result follow from the present formalism based on Leibniz-Reynolds.





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# Index

- $\beta$ -plane approximation, 529
- $f$ -plane approximation, 529
- AABW, 1241
- absolute circulation, 886
- absolute momentum, 209
- absolute reference frame, 172
- Absolute Salinity, 1228
- absolute salinity, 456, 585
- absolute temperature, 234
- absolute vorticity, 828
  - impermeability, 933
- absolute vorticity invariance, 814
- acceleration, 171
  - centrifugal, 188, 192
  - centripetal, 188
  - Coriolis, 188, 192
  - inertial, 184, 189
  - planetary Cartesian, 188
  - spherical, 190
    - spherical metric, 192
- acoustic wave, 51
- acoustic waves, 370, 511
- action/reaction law, 373
- active tracer, 46, 1138
- adiabatic, 436
- adiabatic flow, 1139
- adiabatic lapse rate, 465
- adjoint diffusion equation, 94
- adjoint operator, 95, 97
- advection, 1123, 1127
  - reversible, 492
- advection equation, 46, 716
- advection of velocity vector identity, 30
- advection operator, 251
- advection-diffusion equation, 331, 1140
- advective boundary transport, 1234
- advective flux, 1230
- advective time scale, 953
- advective tracer flux, 317, 1124, 1197
- affine tensor algebra, 5
- ageostrophic components, 1000
- ageostrophic flow, 654, 961
- ageostrophic velocity, 654
- air-water interface, 403
- anelastic approximation, 336, 546
- angular momentum, 172, 206, 214, 380, 792, 830, 835, 877
  - axial, 221
- barotropic model, 821
- conservation, 214
- free vortex, 785
- shalllow water, 759
- angular velocity, 173, 176
- anisotropic Gent-McWilliams, 1215
- anisotropic neutral diffusion, 1211
- anisotropic tensor, 19
- anti-cyclonic, 210
- anti-cyclonic motion, 612
- anticipated potential vorticity, 823
- arc length, 31, 114, 119
- arc-length, 339
- Archimedean buoyancy, 540, 581, 583
- Archimedes' Principle, 583
- area
  - surface, 117
- area evolution
  - incompressible, 346
- arrested Ekman layer, 673
- aspect ratio, 523, 547, 548, 952, 954
- association versus causation, 552
- associative relations, v
- asymptotic methods, 959

- atmospheric form stress, 410, 413  
atmospheric pressure torque, 852, 894, 899  
available potential energy, 567, 1199  
    approximate, 573  
    exact, 572  
    QG fluid, 1012  
Avogadro's number, 234  
axial angular momentum, 187, 366  
    atmosphere, 368  
    depth integrated, 424  
    ocean, 423  
    ring of air, 367  
    steady state, 426  
    zonal acceleration, 218  
axial vector, 10
- back-reaction, 581  
backward diffusion equation, 94  
balanced model, 997  
balances, v  
baroclinic, 527, 619, 877  
baroclinic velocity, 420, 750  
baroclinicity, 613, 873, 877, 896, 914  
    Boussinesq, 892  
    generalized vertical coordinates, 1075  
    ideal gas, 905  
    seawater, 916  
baroclinicity  
    solenoid, 878  
barometric law, 475  
barotropic, 527, 877  
barotropic flow, 621, 873  
barotropic model, 799  
barotropic velocity, 420, 750  
barotropization, 617  
barycenter, 316  
barycentric velocity, 241, 243, 315, 318, 326,  
    375, 1229  
barystatic sea level changes, 1240  
basic one-form, 181  
basis one-forms, 136  
basis vector, 181  
basis vectors, 127, 135  
    changes, 180  
Batchelor scale, 1189  
Beltrami flow, 42  
Bernoulli function, 934  
Bernoulli potential, 497, 1082  
    Boussinesq and hydrostatic, 924
- Bernoulli theorem  
    traditional derivation, 498  
Bernoulli's Principle, 498  
Bernoulli's theorem, 498  
    pipe flow, 499  
beta effect, 804, 814, 832, 849, 852, 887, 899,  
    984  
    two-dimensional example, 889  
beta plane, 803  
beta-effect  
    topographic, 839, 963  
beta-plane approximation, 531  
bi-orthogonality relation, 136  
Bjerknes circulation theorem, 887  
body force  
    homogeneous layer, 848  
body forces, x, 358, 373  
boldface notation, 128  
Boltzmann constant, 472  
bolus velocity, 1093, 1099  
bottom drag, 558  
bottom following coordinates, 1026  
bottom geostrophic velocity, 899  
bottom kinematic boundary condition, 713  
bottom pressure torque, 852, 853, 879, 894,  
    896, 899, 985  
bottom transformation, 1257  
bottom vertical velocity, 985, 986  
boundary conditions, 1141  
boundary Green's function, 86, 88  
boundary layer, 653, 661  
boundary layers, 402, 654  
boundary propagator, 88, 103, 1150  
    normalization, 105  
boundary stress, 558  
boundary velocity, 325  
boundary water mass transformation, 1262  
Boussinesq  
    energetics, 558  
    mass continuity, 541  
    momentum equation, 540  
Boussinesq approximation, 335, 336, 538  
    generalized, 575  
    ocean equations, 542  
    reference density, 542  
    traditional, 545  
Boussinesq continuity  
    density evolution, 544  
Boussinesq dynamic enthalpy, 561, 562

- Boussinesq equations  
non-dimensional, 972, 979
- Boussinesq fluid, 608  
energetics, 576
- Boussinesq reference density, 337
- Brownian motion, 1190
- Buckingham-II theorem, 950
- budget analysis, 320
- bulk viscosity, 391
- buoyancy, 525, 581, 1219  
effective, 598, 600  
globally referenced, 589  
homogeneous fluid, 545
- buoyancy and height  
relation, 570
- buoyancy boundary condition, 1233
- buoyancy budget  
surface ocean, 1235
- buoyancy coordinates, 125, 1026
- buoyancy force, 584
- buoyancy frequency, 592  
ideal gas, 594
- buoyancy sorting, 573
- buoyancy stratification, 589
- buoyancy work, 559
- Burger number, 955, 1013
- cabbeling, 543, 1225, 1227
- cabbeling parameter, 1226
- capillary pressure, 405, 406
- capillary tube, 403
- capillary waves, 407
- capillary-gravity waves, 398
- Cartesian coordinates, 125, 153  
summary, 154
- Cartesian tensor algebra, 5
- Cauchy problem  
hyperbolic, 58  
parabolic, 55
- Cauchy's equation of motion, 360
- Cauchy's fundamental lemma, 375
- Cauchy's solution, 272, 273
- Cauchy's stress principle, 375
- Cauchy's theorem, 377
- Cauchy-Green strain tensor, 273
- Cauchy-Stokes decomposition, 278
- causal free space Green's function, 93
- Causal Green's function, 93
- causal Green's function, 105
- causal relations, v
- causality condition, 93
- causation versus association, 552
- center of mass motion, 308
- center of mass velocity, 316, 1230
- centrifugal acceleration, 199, 531, 638–640, 810  
particle motion, 210  
planetary orbital, 683  
planetary rotation, 683  
spherical, 193
- centripetal acceleration, 199, 638–640
- channel, 751
- channel flow, 629
- Chapman-Kolmogorov relation, 97, 98
- characteristic curves, 48  
advection equation, 49  
wave equation, 58
- chemical energy flux, 494
- chemical potential, 448, 456, 461
- chemical reactions, 313
- chemical work, 450
- Christoffel symbols, 147  
metric connection, 148  
related to metric, 149
- circuit, 32, 112
- circulation, 32, 39, 783  
absolute, 886  
around a streamline, 848  
free vortex, 785  
friction effects, 846  
Rayleigh drag, 848  
rotating fluids, 885  
shallow water, 846  
solid-body rotation, 787  
tornado, 871  
wind stress, 848
- circulation induction, 888
- circulation theorem, 847
- co-tangent space, 136
- coarse graining, 1163
- coherent structure, 269
- cold core eddy, 734
- column vorticity, 854
- compatibility  
total mass + tracer mass, 318
- composition  
diffusion equation, 97, 1147
- composition property, 97, 1147

- compression, 285  
conservation equation  
    Eulerian flux-form, 321  
    material form, 321  
conservation laws, 171, 207, 212, 228, 510  
conservation of indices, 127  
conservative force, 174  
conservative property, 511  
Conservative Temperature, 468, 505, 507, 585, 1219  
conservative tracers, 1110  
conservative vector field, 42  
constituent mass flux, 316  
constitutive relation, 389, 390  
contact force  
    pressure, 377  
contact forces, x, 358, 373  
contact pressure force, 743  
contact pressure forces, 740  
continuity, 336  
continuity equation, 292  
continuum approximation, 229, 230  
continuum hypothesis, 229  
contour, 112  
contraction, 9  
contravariant tensor index, 124, 181  
convective time derivative, 251  
converging flow  
    PV constraints, 840  
coordinate invariance, 122  
coordinate representation  
    Cartesian, 6  
Coriolis acceleration, 188, 215  
    large-scale motion, 194  
    shallow atmosphere, 194  
    spherical, 193  
Coriolis parameter, 194  
Couette flow, 389, 400  
Coulomb gauge, 1127  
couplet, 385  
covariant curl, 151  
covariant derivative  
    metric tensor, 149  
    one-form, 148  
    scalar, 147  
    vector, 147  
covariant differentiation, 123  
covariant divergence  
    vector, 149  
covariant Laplacian  
    scalar, 150  
covariant tensor index, 124, 181  
Crocco's theorem, 513  
cross-diffusion, 1192  
curl integrated over a closed surface, 36  
curl of a curl, 30  
curl of cross product, 30  
curl of vector, 26  
curl-free vector, 27  
curvature, 405  
    curve, 115  
    Gaussian, 119  
    surface, 118  
curvature circle, 115  
curves on a surface, 119  
cyclonic, 210  
cyclonic eddy, 734  
cyclonic motion, 612  
cyclostrophic balance, 648  
cylindrical coordinates, 125  
cylindrical-polar coordinates, 160  
D'Alembert wave solution, 59  
d'Alembert's paradox, 390  
d'Alembert's theorem, 390  
deformation gradient tensor, 272  
deformation radius, 846, 977, 999, 1013  
    shallow water, 766, 845, 955, 966  
deformation rate, 275  
deformation rates, 285  
deformation tensor, 247  
deformational flow, 285  
delta sheets of potential vorticity, 567  
density, 586  
density evolution, 1192  
density time changes, 1220  
depth of no motion, 619  
determinant  
    exponential, 150  
developing flow, 251  
deviator, 392  
deviatoric friction tensor, 392  
deviatoric rate of strain tensor, 392, 488  
deviatoric stress, 359, 390  
dia-surface flow, 1138  
dia-surface transfer  
    shallow water, 725  
dia-surface transport, 331, 1043, 1047

- incompressible, 1052  
dia-surface velocity  
    compared to vertical, 1054  
dia-surface velocity component, 1050  
diabatic, 436  
diabatic processes, 1139  
diagnostic equation, v, 255  
dianeutral direction, 591, 1194  
diapycnal transport velocity, 305  
diapycnal velocity component, 1080  
differentiable manifold, 438, 1243  
diffusion, 1229  
diffusion dissipation functional, 1120  
diffusion equation, 54, 92  
diffusion tensor, 1175, 1192, 1230  
diffusion tensor transformation, 1212  
diffusive fluxes, 318, 326  
diffusive tracer flux, 317  
diffusivity, 1230  
    eddy, 557  
dilation, 278  
dimensionless numbers, 950  
Dirac delta, 69  
    Cartesian, 71  
    sifting property, 70  
    spherical, 71  
Dirac delta distribution, 1257, 1268  
Dirac delta sheet, 90, 103  
direct stress, 390  
direction cosines, 17  
Dirichlet boundary condition, 52, 54, 81, 1142  
Dirichlet boundary conditions, 77, 1142  
dispersion relation  
    inertia-gravity waves, 765  
    inertial waves, 625  
    shallow water gravity wave, 764  
displacement tensor, 272  
dissipation, 359, 489  
distance, 8  
distance to polar axis, 187  
divergence, 394  
divergence of cross product, 29  
divergence of curl, 29  
divergence operator  
    Cartesian, 25  
divergence theorem, 34, 291  
    scalar fields, 35  
diverging flow, 284  
domain of influence, 59  
Doppler shift, 817  
dot product, 8  
double integral formulate, 1266  
double integral identity, 64  
downscale cascade, 1189  
drag coefficient, 558  
dual form stress, 421, 428, 743, 748  
dual pressure form stress, 1102  
duality  
    Eulerian and Lagrangian, 271  
duality between one-form and vector, 135  
duality vectors & one-forms, 136  
Dufour effect, 503  
Duhamel's integral  
    heat equation, 56  
    wave equation, 60  
dynamic enthalpy, 561  
dynamic pressure, 642, 722  
dynamic pressure gradient, 363  
dynamic topography, 527  
dynamic viscosity, 391  
dynamical constraints, 206, 207, 212, 228  
dynamical pressure, 525, 827  
Eötvös correction, 194  
earth radius, 678  
earth's angular rotation, 176  
earth's mass, 195  
earth's radius, 176, 195  
earth's solid body speed, 176  
eddy diffusivity, 557  
eddy tracer fluxes, 1170  
eddy viscosity, 557, 654  
    Ekman layer, 661  
eddy-induced mass flux, 1124  
eddy-induced mass streamfunction, 1124  
eddy-induced velocity, 557, 579, 1124, 1193  
effective beta, 839, 964  
effective buoyancy, 581, 589, 598, 600  
effective free surface height, 709  
effective gravity, 530  
Einstein index convention, 6  
Einstein summation convention, 128  
Ekman  
    balance, 654  
Ekman balance  
    mass transport, 662  
    natural coordinates, 656

- Rayleigh drag, 657  
spiral motion, 659
- Ekman boundary layers, 402, 653, 654
- Ekman downwelling, 666
- Ekman layer  
arrested, 673  
bottom, 668  
horizontal transport, 662  
ocean surface, 662  
velocity profile, 668
- Ekman layer thickness, 661
- Ekman mechanics, 653
- Ekman number, 660, 661
- Ekman pumping, 666
- Ekman suction, 666
- Ekman transport, 664
- Ekman upwelling, 666
- Ekman velocity, 985
- Eliasson-Palm fluxes, 750
- Eliasson-Palm flux, 748, 1093, 1103
- Eliasson-Palm flux tensor, 742, 1103
- elliptic PDE  
classification, 50  
properties, 50
- energy  
total, 495
- ensemble average, 1097
- ensemble mean, 1163
- enthalpy, 459, 505  
budget, 493
- enthalpy budget, 495, 503
- enthalpy capacity, 463
- entropy, 439, 442, 444, 458  
perfect fluid, 492
- entropy budget, 500
- entropy flux, 501
- entropy maximum, 445
- entropy source, 501, 503
- epineutral diffusion, 1205
- epsilon product identity, 30
- epsilon tensor product identity, 15
- equation of motion, 360  
Cartesian, 198  
particle, 197  
rotating, 361  
spherical, 198, 362
- equation of state, 457–461, 471, 585  
linear, 543  
oceanic Boussinesq, 544
- equatorial radius, 199
- equilibrium tide, 679
- equivalent barotropic depth, 807
- equivalent barotropic flow, 807
- Ertel potential vorticity, 911, 913
- Euclidean metric, 8
- Euclidean space, 121
- Euler equation, 361, 369, 393  
reversible, 371
- Euler form, 449
- Euler's theorem, 447, 448
- Eulerian and Lagrangian duality, 271
- Eulerian coordinates  
Cartesian, 125  
cylindrical, 125  
spherical, 125
- Eulerian flux-form, 510
- Eulerian mean, 1164
- Eulerian reference frame, 228, 244
- Eulerian region, 322
- Eulerian time derivative, 124, 251
- evolving flow, 251
- exact differential, 38, 174, 442, 450  
hiker analogy, 39
- exact differentials, 340
- exact geostrophic balance, 643
- exact hydrostatic balance, 364
- Exner function, 478
- extensive property, 320, 437
- exterior moment of  $\lambda$ , 1253
- external forces, 373
- external moment, 1254
- external pressure, 524
- external tracer mass, 1277
- external velocity, 420, 750
- f-plane approximation, 209, 530
- fetch, 757
- Fick's law of diffusion, 503
- field point, 69, 75
- fine scale mixing, 1191, 1192
- first kinematic viscosity, 391
- first law of thermodynamics, 439, 440, 455, 495  
moving fluid, 492  
potential temperature, 494
- flat space, 121
- flow lines, 261
- fluid dynamics, x

- fluid element, 243, 314, 318, 581  
 fluid kinematics, x  
 fluid material region, 243  
 fluid parcel, 242  
     constituents, 315  
 fluid particle, 241  
 fluid particle trajectories, 245  
 fluid particle trajectory, 262  
 fluid region, 243  
 flux, 43  
 flux-form conservation law, 290, 920  
 flux-form conservation laws, 510  
 force couplet, 385  
 force potential, 174  
 forces  
     body, 358  
     contact, 358  
 form stress, 377, 421, 428, 740, 743, 745, 746, 1201  
     dual, 743, 748  
     geostrophic eddies, 629  
     isopycnal layer, 631  
     isopycnal surface, 630  
     mathematical expression, 411  
 formation, 1262  
 Fourier's heat law, 331  
 Fourier's law, 493  
 Fourier's law of conduction, 503  
 free particle, 212  
 free space Green's function, 75  
 free vortex, 784, 796  
 freely falling particle, 224  
 freshwater boundary condition, 1230, 1231  
 freshwater budget, 1228  
 freshwater velocity, 1230  
 friction  
     vertical shear, 395  
 friction driven velocity, 654  
 friction tensor, 389  
 frictional dissipation, 488, 496  
 frictional force, 393  
 frictional torque, 989  
 Froude number, 254, 548, 727, 951, 953, 955  
 functional degrees of freedom, 336  
 functional variations, 1120  
 functions versus scalars, 137  
 fundamental solution  
     Laplace operator, 75  
 fundamental theorem of calculus, 33  
     fundamental thermodynamic relation, 442  
     Galilean boost, 172  
     Galilean invariance, 171, 178, 256, 391, 823  
         kinetic energy, 220  
     Galilean transformation, 172, 256, 321, 769  
         material time operator, 257  
     gauge freedom, 921, 944  
     gauge function, 496, 838  
     gauge invariance, 1127  
     gauge symmetry, 340, 342, 496  
         pressure, 359  
     gauge transformation, 40  
     Gauss's divergence theorem, 34, 151, 1071  
     Gaussian curvature, 119  
     general covariance, 122  
     general orthogonal coordinates, 165  
     general vertical coordinates, 326  
         basis one-forms, 1028  
         basis vectors, 1027  
         circulation, 1041  
         common confusion, 1025  
         contravariant velocity, 1033  
         covariant velocity, 1033  
         diffusion operator, 1038  
         divergence, 1038  
         divergence theorem, 1038  
         Jacobian, 1034  
         layer integrated diffusion, 1039  
         Levi-Civita tensor, 1035  
         material time derivative, 1038  
         metric tensor, 1034  
         partial derivatives, 1036  
         position vector, 1030  
         related to Cartesian, 1024  
         specific thickness, 1034  
         triple product identity, 1029  
         vector, 1032  
         vector cross product, 1035  
         velocity, 1033  
         volume element, 1035  
         vorticity, 1040  
     generalized Lagrangian mean, 1161  
     generalized vertical coordinates, 246, 1020  
         examples, 1044  
     Gent-McWilliams  
         anisotropic, 1215  
         available potential energy, 1199  
         boundary value problems, 1204

- form stress, 1201  
secondary circulation, 1198  
thickness diffusion, 1202
- Gent-McWilliams effect, 1198  
Gent-McWilliams parameterization, 1196  
geopotential, 197, 544  
height, 475  
reference, 484  
thickness, 475
- geopotential coordinates, 199  
geopotential height  
ideal gas, 529  
geostrophic adjustment, 841  
potential vorticity, 844  
geostrophic advection, 1007  
geostrophic balance, v, 607, 611  
exact, 643
- geostrophic contours, 840, 1158  
geostrophic eddies, 629  
geostrophic eddy, 734  
geostrophic momentum, 861  
geostrophic number, 975  
geostrophic streamfunction, 961, 963  
geostrophic Sverdrup balance, 618, 990  
geostrophic transport, 732  
geostrophy  
isopycnal models, 1082  
pressure coordinates, 614  
shallow water, 730
- geothermal heating, 331  
Gibbs potential, 451, 454, 461, 491  
Gibbs relation, 442  
Gibbs-Duhem, 450  
GLM, 1161, 1166  
isopycnal, 1178  
GLM and tracers, 1169  
GLM kinematics, 1163  
global conservation law, 920  
global conservation laws, 511  
global mean sea level, 1236  
Godfrey's island rule, 857  
gradient operator, 22  
Cartesian and GVC, 1036  
general vertical coordinate, 1036
- gradient wind  
regular high, 651
- gradient wind balance, 649  
barotropic flow, 809
- gravest vertical mode, 617
- gravitational acceleration, 195, 680  
approximate, 196  
effective, 197
- gravitational force, 175  
gravitational potential, 678  
earth-moon, 683  
general case, 678
- gravitational potential energy, 196, 483  
mixing, 486  
regional, 484  
stratification, 485
- gravitational stability, 592  
gravitational work, 454, 499  
gravity wave speed, 764  
gravity waves, 782  
non-rotating, 844
- Green's function  
advection-diffusion equation, 1143  
composition, 97, 1147  
diffusion, 93  
diffusion adjoint, 94  
diffusion equation, 92  
diffusion free space, 93  
free space for Laplace, 75  
non-closed reciprocity, 1146  
one-dimensional Poisson, 77  
reciprocity, 84, 95, 1143
- Green's function method, 68
- Green's functions  
passive tracers, 1140
- Green's identities, 36
- group velocity  
Rossby waves, 819
- GVCs, 1020  
gyre circulation, 850  
gyres and channels, 758
- Hadley circulation, 368  
haline, 586  
haline contraction, 464  
haline contraction coefficient, 586, 587  
halosteric sea level, 1240  
Hamilton's operator, 22  
harmonic function, 26, 28, 341, 782  
mean-value property, 51  
harmonic functions, 51  
Haynes-McIntyre PV flux, 930  
heat capacity, 463  
heat equation, 54, 92

- heat flow direction, 445  
heat function, 459  
heating, 440  
Heaviside step function, 73, 93, 843  
height and buoyancy  
    relation, 570  
helicity, 908  
Helmholtz decomposition, 40, 341  
Helmholtz decomposition of Coriolis, 44  
Helmholtz equation, 60  
Helmholtz free energy, 460  
Helmholtz's first theorem, 871  
Helmholtz's second theorem, 871  
Helmholtz's third theorem, 871  
heuristics, 68  
homogeneous, 437  
homogeneous function, 447, 448  
homogeneous solution, 50  
homogeneous tensor, 19  
Hooke's Law, 391  
Hughes gyre model, 854  
hydrostatic approximation, 364, 544, 598, 717  
    background state, 524  
    ocean models, 543  
    scaling, 523, 546  
    vertical motion, 518, 529  
hydrostatic balance, 364, 383  
    approximate, 518, 520  
    exact versus approximate, 365  
    forces, 383  
    torques, 385  
hydrostatic fluid, 219  
hydrostatic number, 975  
hydrostatic pressure, 584, 708  
    evolution, 521, 550  
    expressions, 520  
hydrostatic primitive equations, 518  
hyperbolic PDE  
    classification, 50  
    domain of influence, 59  
hyperbolic PDEs, 57  
hypsometric equation, 475  
  
ice skater, 830  
ideal gas, 471  
    adiabatic lapse rate, 474  
    buoyancy frequency, 594  
    compressibility, 474  
    enthalpy, 473  
    equation of state, 471  
    geopotential thickness, 475  
    heat capacity, 472  
    internal energy, 472  
    lapse rate, 594  
    potential temperature, 476  
    sound speed, 474  
    thermal expansion coefficient, 473  
ideal gas law, 234  
impermeability vs. material invariance, 934  
Impermeability, 1011  
impermeability  
    absolute vorticity components, 933  
    kinematics, 931  
impermeability theorem, 929, 941  
    confusions, 933  
    planetary geostrophy, 982  
    seawater, 934  
impulse, 74  
impulse response function, 74, 79, 105, 1151  
in situ density, 587  
in situ temperature, 467, 505  
    evolution, 506  
incompressible, 335  
incompressible flow, 336  
incrop, 567  
incropping buoyancy, 567  
index convention, 6  
index gymnastics, 15, 127  
index raising and lowering, 136  
induction vector, 1010  
inertia-gravity waves, 629, 765, 766  
    topographic forcing, 768  
inertial acceleration, 184  
inertial frequency, 610  
inertial motion, 645  
inertial oscillation, 646  
inertial oscillations, 209, 623, 977  
    ocean, 211  
    period, 211  
inertial reference frame, 171, 172, 228  
inertial velocity, 183  
    spherical, 190  
inertial waves, 607, 623  
    dispersion relation, 625  
    group velocity, 626  
    near, 627  
inexact differential, 38, 440, 442, 450

- integrating factor, 39  
influence function, 79  
information entropy, 1154  
initial value problem, 843  
initial value problems, 105  
injection work, 497  
inner product, 8  
integral curve, 241, 262  
integral surface, 48  
integrating factor, 442, 450  
integration in  $\lambda$ -space, 1248  
intensive property, 320, 437  
interfacial form stress, 410, 416, 743, 745, 1101  
interior moment of  $\lambda$ , 1253  
interior transformation, 1257  
intermolecular forces, 404  
internal energy, 433, 438, 458, 495, 566  
internal energy budget, 495  
internal energy capacity, 463  
internal forces, 358, 373  
internal moment, 1254  
internal pressure, 524  
internal tracer mass, 1277  
internal velocity, 420, 750  
inverse barometer response, 709  
inverse energy cascade, 808  
inversion, 842  
irreversible process, 444  
irreversible thermodynamics, 481  
irrotational, 781  
irrotational flow, 342, 782, 789  
irrotational vector, 27  
island rule, 857  
isopycnal coordinates, 125, 1026  
isopycnal ensemble, 1177  
isopycnal GLM, 1178  
isopycnal layer transport, 1177  
isopycnal mean, 1177  
isopycnal primitive equations, 1078  
isopycnals, 305  
isotropic tensor, 19
- Jacobian  
ratio of volumes, 249  
Jacobian evolution, 283  
Jacobian of transformation, 134, 141  
Jacobian on a curve, 120, 1158  
Jacobian operator, 120, 805, 1007, 1158
- JEBAR, 994  
jets, 816  
Joule heating, 496  
Joule unit of energy, 235  
Kelvin waves, 629, 775  
Kelvin's circulation theorem, 872, 879, 912, 914  
Kelvin-Helmholtz instability, 976  
kinematic b.c.  
buoyancy surface, 305  
geometric derivation, 301  
incompressible flow, 337  
material interface, 300  
moving material, 299  
ocean free surface, 305  
permeable surface, 302  
static material, 298  
kinematic boundary condition, 298  
kinematic boundary conditions, 713  
tracers, 1230  
kinematic free surface equation, 306  
kinematic viscosity, 391  
kinematic water mass transformation, 1256  
kinematics of two-dimensional flow, 284  
kinetic energy, 174, 220, 487  
axial angular momentum, 221  
Boussinesq, 559  
cartesian coordinates, 221  
geopotential coordinates, 222  
hydrostatic Boussinesq, 576  
spherical coordinates, 221  
kinetic energy dissipation, 488, 489  
kinetic stress, 387, 419, 739, 1101  
kinetic stress tensor, 803  
kinetic theory, 234  
Knudsen number, 231, 479  
Kronecker tensor, 8, 133, 181  
laboratory reference frame, 172, 244  
Lagrangian coordinates, 126  
Lagrangian mean, 1164  
Lagrangian reference frame, 228, 244  
Lagrangian region, 318  
Lagrangian time derivative, 124, 251  
laminar subregion, 402  
Laplace's equation, 50, 51, 782  
properties, 51  
Laplacian friction, 659  
Laplacian operator, 26

- law of atmospheres, 475  
law of cosines, 683  
layer mass continuity, 1060  
  compressible, 1061  
  pressure coordinates, 1062  
Legendre transformation, 457, 459–461  
Leibniz’s rule, 322, 894  
Leibniz-Reynolds  
  brute force, 328  
Leibniz-Reynolds transport theorem, 322,  
  940  
length scale  
  gradient, 233  
  macroscopic, 230  
  mean free path, 230, 235  
  measurement, 233  
  molecular, 230  
  simulation, 233  
level of no motion, 527, 718  
Levi-Civita tensor  
  general coordinates, 143  
  volume element, 144  
Levi-Civita tensor, 9, 142, 810  
lid pressure, 799, 808  
linear equation of state, 588  
linear momentum, 171, 791  
  conservation, 171  
  finite volume, 388  
  Lagrangian volume, 388  
local conservation laws, 511  
local Rossby number, 642  
local thermodynamic equilibrium, 481, 490  
locally referenced potential density, 593  
longitudinal waves, 370, 763  
longwave radiation, 1234  
Lorenz convention, 567
- Mach number, 370, 537  
macroscopically small, 229  
macrostates, 435  
Magnus acceleration, 364, 642, 827  
Margules’ relation, 731, 734  
Marshall potential vorticity flux, 934  
mass  
   $\lambda$ -layer, 1248  
mass budget  
   $\lambda$ -layer, 1262  
  fluid column, 307, 308  
  weak formulation, 315  
mass budgets, 326  
mass conservation, 228, 294  
  arbitrary Eulerian region, 291  
  Eulerian flux-form, 290  
  finite Eulerian cube, 290  
  Jacobian derivation, 293  
  Lagrangian, 292  
  Lagrangian derivation, 295  
  multi-components, 315  
mass continuity  
  generalized vertical coordinates, 1059  
  layer integrated, 1060  
mass density, 585  
mass density function, 1250  
mass distribution function, 1250  
mass equation  
  general vertical coordinates, 1068  
mass flux, 290  
mass flux through a surface, 302  
mass-Sverdrup, 1245  
material area evolution, 279  
material constant, 321  
material coordinates, 126, 245, 246  
  choices, 246  
material curve, 272  
  evolution, 273  
material fluid parcel, 242, 436  
material invariance, 254, 255  
material invariant, 321  
material line elements, 881  
material surface, 254  
material time derivative, 124, 251  
  general vertical coordinates, 1054  
  invariance, 258, 259  
  isopycnal models, 1080  
  space-time, 261  
material volume evolution, 283  
materially closed, 436  
materially closed system, 440  
materially invariant volume, 336  
materially open, 436  
mathematically rigorous, 68, 69  
matrices, 19  
matter concentration, 456  
matter conservation, 510  
matter flow direction, 453  
Maxwell relations, 451, 464  
mean tracer equation, 1185  
mechanical energy, 174, 487, 489

- Boussinesq, 558, 560–562, 577  
conservation, 222  
particle, 220
- mechanical energy dissipation, 398, 488  
mechanical flux, 489  
mechanical pressure, 389, 392  
mechanical stress, 387  
mechanical work, 174, 220, 441  
geopotential, 454
- meridional overturning circulation, 347  
meridional overturning transport, 1200  
meridional transport, 984  
mesoscale eddies, 1189, 1192  
mesoscale eddy mixing, 1191  
method of characteristics, 48  
metric acceleration, 192  
metric acceleration terms, 363  
metric tensor, 132, 273  
Cartesian coordinates, 132  
coordinate representation, 133  
coordinate transformation, 134  
determinant, 141  
general, 133  
inverse, 136, 137  
relating vectors & one-forms, 136
- metricity condition, 149  
microscopically large, 229  
microstates, 435  
mixed boundary condition, 1141  
mixing, 1192  
surface boundary, 1231
- mixing tensor, 1192  
modified mean, 1178  
molar mass, 449  
mole, 234  
molecular composition  
air, 234  
water, 234
- molecular diffusion, 1190, 1192  
molecular diffusivity, 577  
molecular viscosity, 397, 577  
moment arm, 188, 214  
moment of inertia, 173, 174, 830  
moment-arm, 366  
moments of  $\lambda$ , 1253  
momentum  
angular, 172  
approximate axial angular, 219  
axial angular, 187, 213, 366, 534
- axial angular and Coriolis, 215  
linear, 212  
potential, 208, 212
- momentum equation, 738  
flux form, 387, 1069  
general vertical coordinates, 1068  
horizontal, 1069  
natural coordinates, 641  
spherical, 362  
vector-invariant, 363, 1069  
vertical, 1069
- momentum flux, 290  
Monge gauge, 111  
Montgomery potential, 632, 1079  
motional forces, 598  
motional vertical acceleration, 600  
Munk gyre model, 854
- NADW, 1241  
natural boundary condition, 1120  
natural coordinates, 637, 638  
isobars, 655  
vorticity, 787
- Navier-Stokes equation, 361, 393, 394, 396  
non-dimensional, 396
- near inertial waves, 627  
nearly horizontal motion, 219  
net stress tensor, 396
- Neumann boundary condition, 53, 54, 332, 1120, 1142
- Neumann boundary conditions, 77, 89, 1142
- neutral density, 1245  
neutral diffusion, 1205  
anisotropic, 1211
- neutral directions, 588, 590, 1205  
neutral helicity, 596
- neutral slope, 1194  
neutral tangent plane, 1205
- neutral tangent plane coordinates, 1212
- neutrality condition, 591, 1208, 1213  
neutrally buoyant, 581, 584
- Newton's equation of motion, 360  
Newton's gravitational constant, 195  
Newton's gravitational law, 195  
Newton's second law, 171  
Newton's third law, 373, 375, 399, 746  
pressure, 376
- Newtonian fluid, 390, 391  
Newtonian gravity, 69

- Newtonian gravity field, 683  
Newtonian time, 121, 124  
no normal flow b.c., 298  
no-flux boundary condition, 331, 673  
no-slip boundary condition, 394, 400  
Noether's Theorem, 207, 228  
non-advection flux, 1230  
non-advection transport, 1234  
non-conservative forces, 175  
non-conservative process, 511  
non-dimensionalization, 956  
Ekman balance, 660  
hydrostatic approximation, 547  
non-dispersive waves, 764  
non-divergent barotropic, 800  
non-divergent barotropic model, 799  
non-divergent velocity field, 336  
non-hydrostatic pressure, 710  
non-hydrostatic primitive equations, 520  
non-inertial reference frame, 172  
non-Newtonian constitutive relations, 396  
non-orthogonal coordinates, 126  
normal derivative, 24  
normal direction, 24, 112  
normal stress, 390  
normal vector, 339
- obduction, 1058  
oblate spheroid, 199  
oblique coordinates, 138  
observation point, 75  
ocean buoyancy, 1219  
ocean free surface, 1045  
ocean gyres, 849  
topographic form stress, 852  
ocean mesoscale eddy, 734  
ocean mixed layer base, 1045  
ocean mixing processes, 1190  
ocean-atmosphere equations, 508  
oceanic Boussinesq, 537, 538  
mass, 545  
weight, 545  
oceanic form stress, 410  
one-forms, 135  
basis, 136  
coordinate representation, 135  
one-way wave equation, 57  
orbital motion, 683  
orthogonal curvilinear coordinates, 165
- oscillator equation, 210  
outcrop, 567  
outcropping buoyancy, 567  
outer product, 18, 123, 387, 739  
outward normal  
solid-earth bottom, 299  
overturning streamfunction, 347
- parabolic PDE  
classification, 50  
parabolic PDEs, 54  
smoothing property, 55  
parameterizations, 233, 1189  
partial derivatives  
transformation, 146  
partial entropy, 451  
partial internal energy, 451  
partial volumes, 451  
particle displacement, 1170  
particle mechanics, 171  
particle trajectory  
fall to equatorial plane, 225  
free fall to center, 224  
spherical motion, 224  
particular solution, 50  
passive tracer, 46  
passive tracer source, 1142  
passive tracers, 320, 1140  
path, 112  
orientable, 112  
simple, 112  
path dependent integrals, 440  
path integral  
arc length, 31  
scalar function, 31  
vector function, 32  
pathlines, 262  
analog to car flow, 262  
perfect fluid, iii, 242, 436  
periodic channel, 751  
permutation symbol, 9, 142, 810  
product identity, 15  
phase averaging, 1163  
phase speed  
Rossby waves, 818  
physically formal, 68, 69  
physics as geometry, 122  
Pitot tube, 363  
planar curves, 113

- planetary beta effect, 618  
planetary Cartesian coordinates, 184, 185  
planetary centrifugal acceleration, 188, 199  
planetary centripetal acceleration, 188  
planetary geostrophic potential vorticity, 840  
planetary geostrophy, 614, 901, 957  
    continuously stratified, 971  
    equations, 980  
    potential vorticity, 981  
    vorticity equation, 615  
planetary induction, 888  
planetary spherical coordinates, 184  
planetary vorticity, x, 618  
Poincaré waves, 765  
point mass, 69  
point transformation, 246  
points, 6  
Poisson equation, 195, 806, 809  
    Green's function, 81, 89  
    pressure, 601  
Poisson's equation, 50, 53, 75  
    Dirichlet boundaries, 86  
    max-min principle, 53  
    Neumann boundaries, 90  
polar coordinates, 160  
polar radius, 199  
polarized gravity waves, 768  
position coordinates, 246  
position vector  
    Cartesian representation, 184  
    spherical representation, 184  
postulate of total energy conservation, 503  
potential density, 587  
    locally referenced, 593  
potential energy, 174  
    Boussinesq, 560  
    shallow water layer, 1102  
potential enthalpy, 468, 507  
potential flow, 782  
potential momentum, 198, 212  
potential properties, 585  
potential property, 468  
potential scalar properties, 512  
potential temperature, 466, 467, 505, 585  
    evolution, 506  
    specific entropy, 469  
potential vorcity  
    Eulerian flux-form budget, 920  
potential vorticity, 1041  
substance, 920  
baroclinic fluid, 914  
barotropic fluid, 912  
Bernoulli potential, 924  
Boussinesq, 1076  
cylinder, 830  
delta sheet, 567  
derivation, 921  
dynamical tracer, 915  
Ertel, 911, 913, 1005  
flux, 924, 934  
flux vector, 920, 922  
flux-form equation, 838  
fluxes, 930  
gauge choice, 924  
generalized vertical coordinates, 1074  
hydrostatic Boussinesq, 921  
impermeability, 929, 982  
induction vector, 1010  
inversion, 842  
isopycnal coordinates, 1084  
Kelvin circulation theorem, 834  
kinematic derivation, 923  
Marshall flux, 934  
name, 834, 915  
non-conservative processes, 837, 918  
ocean layer, 939  
perfect fluid, 912  
planetary geostrophy, 840, 966, 981  
potential density, 917  
preferred form of flux?, 944  
quasi-geostrophic, 1005  
quasi-geostrophy, 962, 963, 966  
Rossby, 833  
seawater, 934  
seawater equation of state, 916  
shallow water, 832  
substance, 930  
symmetric instability, 943  
TWA, 1105  
two-dimensional non-divergent, 804  
potential vorticity “stuff”, 838  
potential vorticity budget  
    layer, 939  
potential vorticity concentration, 936  
potential vorticity flux, 838  
    air-sea boundary, 942  
    land-sea boundary, 941  
    steady state constraints, 936

- potential vorticity impermeability  
kinematics, 931
- potential vorticity substance  
integrated, 936
- power, 220
- practical salinity, 1228
- Prandtl ratio, 977
- pressure  
contact force, 1072  
contact stress, 1071  
dynamic, 722  
dynamical pressure, 539  
gradient force, 1071  
interfacial form stress, 1073  
mechanical, 389, 392  
Pascal unit, 235  
poisson equation, 809  
Poisson equation, 551  
sources, 552  
stagnation, 498  
standard atmosphere, 234  
stress, 375  
thermodynamic, 389  
total, 498
- pressure coordinates, 1026
- pressure driven velocity, 654
- pressure force, 743  
two-dimensional flow, 810
- pressure forces, 740
- pressure form stress, 377, 740, 743  
dual, 1102  
shallow water, 745
- pressure gradient  
bottom, 526  
external, 524, 526  
hydrostatic, 525, 526, 549  
ideal gas, 529  
internal, 524, 526, 549
- pressure gradients  
hydrostatic, 613
- pressure source  
Coriolis, 812  
friction, 813  
irrotational flow, 812  
rotation, 810  
self-advection, 810  
solid-body flow, 810  
strain, 810
- pressure time derivative, 1221
- pressure torque, 985  
atmosphere, 989  
bottom, 989
- pressure torques, 749, 899
- pressure transport, 511
- pressure work, 441, 499
- primitive equations, 216
- primitive equations, 518, 608  
nomenclature, 520
- process water mass transformation, 1256
- prognostic equation,  $v$ , 62, 255
- pseudo angular momentum, 209
- pseudo vector, 10
- pseudo-vector, 780
- pycnocline, 734
- Pythagoras' Theorem, 8
- quasi-equilibrium thermodynamics, 481
- quasi-geostrophic potential vorticity, 962, 963
- quasi-geostrophy, 958
- quasi-Lagrangian coordinates, 126
- quasi-static process, 229, 236, 437, 481
- quasi-Stokes transport, 1180, 1184
- quotient rule, 380
- radius of curvature, 115, 118, 639, 646, 787
- rarefied gas, 232
- rate of strain  
vorticity source, 881
- rate of strain tensor, 275, 276, 284, 285, 488, 552, 781, 794, 810
- Rayleigh drag, 175, 391, 657, 848, 897
- re-entrant channel, 751, 817
- real fluid, iii
- reciprocity  
diffusion equation, 95  
Poisson equation, 79, 84
- reciprocity relation, 1143
- rectification, 1094
- rectified, 1161
- reduce gravity model, 734
- reduced gravity, 719, 731
- reduced gravity model, 527, 718
- reference density, 337
- reference frames  
absolute, 178  
inertial, 178  
non-inertial, 178  
rotating, 178
- reference geopotential, 484

- reference pressure, 587  
region following the flow, 294  
relative chemical potential, 456  
rescaled geopotential coordinate, 1064  
residual mean transport, 1193  
residual mean velocity, 1193  
response function, 74, 105, 462  
reversibility, 207  
reversible process, 444  
Reynolds average, 1097  
Reynolds decomposition, 1163  
Reynolds number, 232, 397, 660, 675  
    atmosphere, 397  
    Gulf Stream rings, 397  
    turbulence, 397  
Reynolds stress, 387, 1100, 1101  
Reynolds transport theorem, 293, 296  
    linear momentum, 388  
    multi-component fluid, 326  
Richardson number, 548, 976  
Riemannian differential geometry, 122, 131  
right hand rule, 9  
rigid body rotation, 278  
rigid lid, 725, 808  
rigid lid approximation, 618, 994  
Robin boundary condition, 1141  
Rossby deformation radius, 977  
Rossby number, 609, 675, 953–955, 975  
    Gulf Stream ring, 610  
    kitchen sink, 610  
    local, 642  
Rossby potential vorticity, 837  
Rossby waves, 531, 629, 817  
    dispersion relation, 817  
    group velocity, 819  
    phase speed, 818  
    stationary, 818  
rotating tank, 531, 759, 811  
    parabolic free surface, 533  
    solid body motion, 533  
rotation matrix, 17, 1212  
rotation tensor, 275, 277, 285, 552, 781, 794, 810, 881  
rotational flow, 285  
rotational fluxes, 1172  
rotational tracer flux, 1124, 1197  
  
salinity, 585, 1219  
salt boundary condition, 1230, 1231  
  
salt budget, 1228  
salt concentration, 1228  
salt velocity, 1230  
scalar field, 6  
scalar mechanics, 1110  
scalar potential, 28  
scalar product, 8  
    general tensors, 138  
    invariance, 18  
scalar streamfunctions, 344  
scale analysis, 546, 950  
scale height, 475  
scaling  
    homogeneous function, 447  
sea breeze, 905  
sea level, 1236  
    Boussinesq fluid, 1239  
    steric, 1238  
    thermosteric, 1238, 1239  
sea level budget, 1237  
seawater Boussinesq, 537  
seawater chemical potential, 456, 461  
seawater equation of state, 916  
seawater mass distribution, 1250  
second kinematic viscosity, 391, 393  
second law of thermodynamics, 439, 442, 444  
self-adjoint, 84, 1119, 1144  
self-adjoint operator, 95  
self-advection, 810  
self-attraction and loading, 687  
sgn function, 73  
shallow fluid approximation, 216, 219, 518  
shallow water  
    gravity wave dispersion, 766  
    gravity wave speed, 764  
    hydrostatic approximation, 717  
    inertia-gravity waves, 765  
    Kelvin waves, 775  
    linear potential vorticity, 765  
    linear relative vorticity, 762  
    linearized equations, 761  
    momentum equation, 738  
    non-dimensional, 956  
    non-rotating gravity waves, 762  
    planetary geostrophy, 957  
    quasi-geostrophy, 958  
shallow water columns, 717  
shallow water equations  
    N-layers, 743

- shallow water model  
formulation, 708  
stacked, 721
- shallow water momentum, 711
- shallow water potential vorticity, 832
- shallow water pressure, 708
- shallow water PV invariance, 833
- shallow water Sverdrup balance, 849
- shallow water thickness, 711
- shallow water vertical velocity, 715
- shear flow, 575
- shear stresses, 390
- shearing strain, 285
- shortwave radiation, 1234
- sign-function, 843
- simple ideal gas, 471, 472
- simply connected surface, 596
- singular limit, 661
- skew diffusion, 1125, 1193
- skew diffusion tensor, 1125
- skew symmetric stirring tensor, 1176
- skew symmetric tracer fluxes, 1171
- skew tracer flux, 1124, 1197
- skewson, 1127
- slippery Ekman layer, 673
- slope Burger number, 976
- slope of a surface, 304
- smooth velocity field, 262
- solenoid, 878
- solenoidal velocity, 335
- solid body rotation, 178
- solid body velocity  
spherical, 187
- solid-body rotation, 41, 786, 795, 796
- Sorret effect, 503
- sorting buoyancy, 573
- sound speed, 370, 464, 565, 586  
ideal gas, 474
- source point, 69, 75
- Southern Ocean channel, 751
- space increments  
Eulerian, 270  
Lagrangian, 271
- specific entropy, 469
- specific gas constant  
air, 471  
atmosphere, 475
- specific thickness, 1046, 1179, 1181
- specific volume, 491
- spherical coordinates, 125, 155, 182
- basis one-forms, 157
- basis vectors, 157
- differential operators, 159
- Levi-Civita tensor, 158
- metric, 158
- position, 157
- summary, 160
- transformation from Cartesian, 155
- vector components, 159
- vector cross product, 159
- velocity, 157
- volume element, 158
- spin, 552
- splat, 552
- stacked shallow water model, 721
- stagnation pressure, 363
- standard atmosphere, 234
- standard pressure, 230
- standard temperature, 230, 234
- state function, 440
- static equilibrium sea level, 678, 679
- static forces, 581, 598
- stationary Rossby waves, 818
- steady flow, 251, 252
- steady state, 251, 255, 321, 435, 491, 758
- steady state solution, 50
- steepest descent, 23
- step response function, 106
- steric sea level, 527
- steric sea level changes, 1238
- stirring, 1192  
reversible, 492
- Stoke's theorem, 151
- Stokes drift, 1093, 1168, 1174
- Stokes mean, 1163, 1166
- Stokes' theorem, 33, 783
- Stokesian fluid, 390
- Stommel gyre model, 854
- storage, 1262
- strain, 285
- stratification, 589
- streaklines, 264
- streamfunction, 340, 800  
meridional-depth overturning, 347
- quasi-geostrophy, 963
- streamlines, 338
- transport, 339, 343, 344
- two-dimensional flow, 338

- vector, 342  
vertical gauge, 343  
streamlines, 262, 298, 338  
streamlines versus pathlines, 263  
streamtubes, 262  
stress  
    boundary, 558  
    contact, 358  
    deviatoric, 359, 390  
    direct, 390  
    friction, 359  
    normal, 390  
    pressure, 359  
    shallow water, 726  
    shear, 390  
stress boundary condition  
    Lagrangian interface, 401  
    permeable interface, 401  
    solid boundary, 400  
stress on an interface, 398  
stress tensor, 358, 373, 377  
    net, 396  
    symmetry, 380  
stress-strain relation, 389  
stresses  
    local equilibrium, 375, 399  
stretching, 882  
    material lines, 276  
strong formulation, 240, 328, 383, 385  
sub-inertial frequency, 629  
subduction, 1058  
subgrid scales, 1189  
subgrid-scale parameterizations, 615  
subharmonic function, 53  
substantial time derivative, 251  
super-inertial frequency, 629  
super-inertial waves, 766  
superposition property, 69  
surface  
    orientable, 112  
surface area, 117  
    horizontal projection, 303, 304, 330  
surface derivative operator, 280  
surface gravity waves, 710  
surface tension, 373, 375, 398, 402, 442  
    gas bubbles, 407  
surface transformation, 1257  
    buoyancy, 1268  
surface velocity, 299  
surface water mass transformation, 1266, 1267  
    circulation, 1267  
Sverdrup, 1245  
Sverdrup balance, v, 618, 849, 902, 989, 990  
    geostrophic, 990  
symmetric mixing tensor, 1175  
symmetric tracer fluxes, 1171  
symmetries, 205, 207, 228  
    spatial, 212  
symmetry, 171  
symmetry condition, 1208  
tangent direction, 23, 112  
tangent plane approximation, 529  
tangent plane Cartesian coordinates, 185  
tangent space, 136  
tangent vector, 31, 339  
Taylor columns, 617, 717  
Taylor curtains, 622  
Taylor series, 22  
Taylor-Bretherton identity, 805, 1093, 1105  
Taylor-Proudman effect, 607, 616, 622, 628  
temperature, 467, 585  
tensile force, 404  
tension strain, 285  
tensor analysis  
    algebra summarized, 181  
    contraction of indices, 123  
    covariant differentiation, 123  
    permissible operations, 123  
    quotient rule, 123  
    tensor fields, 6  
    tensors, 6  
    tensors and matrices, 19  
    uses for GFM, 2  
tensor operations, 123  
tensor product, 123  
tensor quotient rule, 123  
terrain following coordinates, 1026  
test charges, 241  
test fluid element, 243, 581, 588  
test paddle wheel, 780  
test particles, 241  
tetrahedron fluid region, 377  
theorem of stress means, 371  
thermal energy, 438  
thermal equation of state, 471, 585  
thermal expansion, 338, 463

- thermal expansion coefficient, 586, 587  
thermal wind, 734  
    atmosphere, 620  
    shallow water, 731  
thermal wind balance, 607, 613, 1001  
    Antarctic Circumpolar Current, 619  
    diagnostics, 619  
    ocean, 619  
thermo-hydrodynamical equations, 508  
thermobaricity, 543, 1225, 1227  
thermobaricity parameter, 1226  
thermodynamic configuration space, 438, 562  
thermodynamic equilibrium, 435, 439, 445, 452, 467  
    fluid elements, 447  
    macroscopic motion, 446  
thermodynamic postulates, 439  
thermodynamic potential, 440  
thermodynamic potentials, 457  
thermodynamic pressure, 389  
    non-divergent flow, 389  
thermodynamic relation  
    specific, 456  
thermodynamic relations  
    steady state, 491  
thermodynamic state, 435  
thermodynamic systems  
    exchanges, 436  
thermodynamic temperature, 439  
thermodynamics  
    moving fluid, 490  
thermohaline circulation, 538, 545  
thickness, 1181  
    specific, 1046, 1068  
    specific thickness, 1080  
thickness diffusion  
    Gent-McWilliams, 632  
thickness equation, 1064  
    isopycnal models, 1080  
thickness weighted averaging, 1098  
thickness weighted mean, 1185  
thickness weighting, 1179  
third law of thermodynamics, 439  
tidal acceleration, 680  
tides  
    earth-moon system, 681  
    realistic effects, 687  
    semi-diurnal, 681  
tilting, 882  
material lines, 276  
time  
    coordinate, 124  
    parameter, 124  
time averages, 62  
time derivative notation, 297  
time derivatives  
    summary, 328  
time mean, 1163  
time reversal symmetry, 207  
time scale  
    molecular collisions, 236  
time tendency, 62, 251  
topographic beta, 839, 963, 964  
topographic form stress, 410, 413  
    components, 415  
    gyres, 852  
    zonal ridge, 413  
topography  
    two-dimensional non-divergent, 805  
tornado, 871  
tornadoes, 649  
torque, 172  
torque density, 382  
torques, 877, 983  
total energy, 438, 495  
total pressure, 363  
total time derivative, 251  
tracer boundary condition  
    no-normal derivative, 331  
tracer boundary conditions, 330  
    air-sea boundary, 332  
    bottom, 331  
tracer budgets, 326, 330  
tracer concentration, 316, 456  
tracer equation, 314, 316  
    derived, 316  
    Eulerian and Lagrangian forms, 317  
    general vertical coordinates, 1068  
    layer integrated, 1065  
    mean, 1185  
    shallow water, 716  
tracer fluxes  
    rotational, 1172  
    skew symmetric, 1171  
    symmetric, 1171  
tracer mass  
    external, 1277  
    internal, 1277

- tracer mass analysis, 1241, 1271  
  external, 1277  
  internal, 1277  
  special cases, 1275
- tracer mechanics, xi, 228
- tracer parameterizations, 1189
- tracer transport tensor, 1186
- tracers  
  passive, 320
- traditional approximation, 519
- trajectories, 245
- trajectory, 124, 171, 262  
  generalized vertical coordinates, 1057
- transformation  
  Cartesian, 18  
  Cartesian coordinates, 16  
  geometric, 17  
  inverse, 16  
  jacobian, 247  
  material and position, 246  
  orthogonal, 16  
  rotation, 16  
  tensor, 18
- transformation matrix, 134, 272  
  coordinates, 134  
  determinant, 142, 145  
  discrete algorithm, 248  
  general vertical coordinates, 1024  
  inverse, 146  
  Jacobian, 134, 141  
  space-time components, 144
- transformation of vectors, 182
- transformed residual mean, 1179
- transforming Cartesian to spherical, 187, 191
- transition to turbulence, 397
- translation, 278
- translation motion, 786
- transport, 43
- transport streamfunction, 339, 422
- transport theorem  
  scalar field, 326
- transverse waves, 370, 625
- TRM, 1179
- TRM velocity, 1181
- turbulence, 394, 397  
  turbulence closure, 233  
  turbulent cascade and vortex stretching, 885  
  turbulent cascade and vorticity, 782  
  turbulent energy cascade, 398
- turbulent transport, 1192, 1234
- two-dimensional flow, 799  
  kinematics, 284
- two-dimensional incompressible, 889
- two-dimensional turbulence, 808
- two-layer shallow water, 721
- ultraviolet catastrophe, 398
- uniqueness  
  diffusion equation, 102  
  Dirichlet problem, 81, 82  
  Neumann problem, 89
- unit vector, 8
- unit vectors  
  rotation, 24
- universal gas constant, 234, 471
- vanishing layers, 1083
- vector field, 6
- vector invariant, 642
- vector invariant velocity equation, 363, 826
- vector product, 9  
  general coordinate, 144  
  geometric, 11
- vector rotation, 178
- vector streamfunction, 342
- vector-invariant velocity equation, 874
- vectors, 6
- velocity, 171  
  basis vectors, 183  
  coordinate, 183  
  particle motion, 183  
  spherical, 190  
  surface, 299
- velocity circulation, 783
- velocity equation, 363  
  vector-invariant, 363, 1069, 1082
- velocity gradient tensor, 275, 794
- velocity potential, 341, 345
- velocity scale  
  molecular rms speed, 236
- velocity self-advection, 810, 874
- velocity vector, 126  
  generalized vertical coordinates, 1057  
  planetary Cartesian representation, 185  
  spherical representation, 186
- vertical Ekman transport, 664
- vertical gauge, 343, 1128
- vertical shear, 276
- vertical stiffness, 622, 623

- vertical stiffening, 616  
vertical stratification, 592  
    energetics, 485  
vertical velocity, 1054, 1100  
    decomposed, 1055  
    shallow water, 715  
    two-dimensional non-divergent, 802  
viscosity, 389  
    air, 233  
    dynamic, 233  
    eddy, 557  
    kinematic, 233  
    water, 233  
viscous dissipation, 489  
viscous flux, 489  
viscous tensor, 389  
volume  
    *n*-space, 14  
    between isosurfaces, 912  
    defined by vectors, 13  
    element for integration, 14  
volume budget  
    column of water, 306  
    material region, 294  
volume element  
    general coordinates, 144  
    invariant, 141  
volume equation, 293  
volume evolution, 325  
    incompressible, 346  
volume-Sverdrup, 1245  
vortex force, 364  
vortex line, 869  
vortex lines, 276, 882  
vortex stretching, 832, 984  
vortex tilting, 832  
vortex tube, 869  
vortex tubes, 882  
vortical flow, 341  
vortical motion, 948  
vorticity, 39, 277, 284, 285, 394, 498, 780,  
    794, 803  
    absolute, 786, 828  
    baroclinicity, 873  
    barotropic flow, 873  
    beta effect, 984  
    bottom boundary, 895  
    Boussinesq, 890  
    curvature, 789, 814  
    depth averaged velocity, 992  
    depth integrated, 894  
    depth integrated velocity, 991  
    dynamics, 874  
    free vortex, 784  
    frozen-in, 882  
    general vertical coordinate, 1069  
    generalized vertical coordinates, 1074  
    hydrostatic, 890  
    isopycnal coordinates, 1084  
    isopycnal models, 1082  
    line element rotation, 781  
    meridional transport, 988  
    natural coordinates, 787  
    non-divergent, 782  
    of a column, 854  
    orbital, 789, 814  
    planetary, 786  
    planetary geostrophic, 615  
    quasi-geostrophy, 962  
    relative, 786, 1069  
    rotating fluids, 885  
    rotating reference frame, 781  
    shallow water, 828  
    shear, 789, 814  
    stretching, 882, 984  
    surface boundary, 897  
    tilting, 882  
    torques, 877  
    TWA, 1105  
    two-dimensional non-divergent, 804  
    vertical component, 893  
vorticity and turbulent cascade, 782  
vorticity budget  
    depth integrated, 983  
vorticity dynamics, 828  
vorticity equation, 875  
    hydrostatic, 891  
    planetary geostrophy, 893  
vorticity filaments, 881  
vorticity flux vector, 894  
warm core eddy, 734  
water mass, 467, 1241  
water mass analysis  
    mathematics, 1248  
    tracers, 1271  
water mass configuration space, 1243  
water mass formation, 1245, 1262

- buoyancy, 1245  
water mass transformation, 1241, 1245, 1255  
    boundary, 1262  
    buoyancy, 1245, 1268  
    dia-surface flux, 1255  
    interior, 1255  
    kinematic, 1256  
    kinematic method, 1258  
    process, 1256  
    process method, 1257  
    processes, 1247, 1265  
    surface, 1266, 1267  
wave equation, 770  
    domain of influence, 59  
waves  
    inertia-gravity, 629  
    inertial, 623  
    Kelvin, 629  
    Rossby, 629  
weak formulation, 240, 315, 328, 383, 386  
western boundary intensification, 849  
western boundary layer, 815  
western intensification, 850  
wind driven circulation, 666  
wind stress  
    homogeneous layer, 848  
    shallow water, 726  
wing flow, 498  
work, 220  
work by gravity, 175  
work-energy theorem, 174, 499  
working, 440  
Young-Laplace formula, 405  
    derivation, 405  
zero buoyancy layer thickness, 567  
zeroth law of thermodynamics, 439  
zonal channel, 817  
zonal flow  
    absolute vorticity constraints, 814  
zonal mean, 1163  
zonal ridge  
    topographic form stress, 413  
zonally re-entrant, 751