1 Difference Equations

$$y(k) + a_1 y(k-1) + \dots + a_n y(k-n) =$$

 $b_0 u(k) + b_1 u(k-1) + \dots + b_m u(k-m)$ (1)

1.1 Solution to Difference Equations

$$y(k) = y_h(k) + y_p(k)$$

try $y_h(k) = \lambda^k \to \lambda^n + a_1 \lambda^{n-1} + \dots + a_n = 0$

2 Laplace Transforms

2.1 Basic Laplace Table

$$\mathcal{L}\{1(t)\} = \frac{1}{s}$$

$$\mathcal{L}\{t^{n}\} = \frac{n!}{s^{n+1}}$$

$$\mathcal{L}\{t^{k}\} = \frac{1}{(s-a)^{k+1}}$$

$$\mathcal{L}\{\sin(kt)\} = \frac{k}{s^{2}+k^{2}}$$

$$\mathcal{L}\{\sinh(kt)\} = \frac{s}{s^{2}-k^{2}}$$

$$\mathcal{L}\{\cosh(kt)\} = \frac{s}{s^{2}-k^{2}}$$

2.2 Basic Inverse Laplace Table

$$\begin{array}{c|c} \mathcal{L}^{-1}\left\{\frac{1}{s}\right\} = 1 & \mathcal{L}^{-1}\left\{1\right\} = \delta(t) \\ \mathcal{L}^{-1}\left\{\frac{1}{s-a}\right\} = e^{at} & \mathcal{L}^{-1}\left\{\frac{n!}{s^{n+1}}\right\} = t^n \\ \mathcal{L}^{-1}\left\{\frac{k}{s^2+k^2}\right\} = \sin(kt) & \mathcal{L}^{-1}\left\{\frac{s}{s^2+k^2}\right\} = \cos(kt) \\ \mathcal{L}^{-1}\left\{\frac{k}{s^2-k^2}\right\} = \sinh(kt) & \mathcal{L}^{-1}\left\{\frac{s}{s^2-k^2}\right\} = \cosh(kt) \end{array}$$

2.3 Forward Laplace Transform

$$\mathcal{L}{f(t)} = F(s) := \int_0^{+\infty} f(t)e^{-st}dt$$

2.4 Inverse Laplace Transform

$$f(t) = \frac{1}{2\pi i} \int_{\sigma - i\infty}^{\sigma + i\infty} F(s)e^{st} dt = \sum_{k=1}^{n} \operatorname{Res}(e^{st} F(s), s_k)$$

3 Z-Transforms

3.1 Forward Z-Transform

$$\mathscr{Z}{x(k)} = X(k) := \sum_{k=0}^{\infty} x(k)z^{-k}, \quad z \in \mathbb{C}$$

3.2 Inverse Z-Transform

$$x(k) = \mathcal{Z}^{-1}\{X(z)\} = \sum \operatorname{Res}(X(z)z^{k-1}, p_z)$$

3.2.1 Simple Pole

Res
$$(f(z), z_0) = \lim_{z \to z_0} (z - z_0) f(z)$$

3.2.2 Pole of Order N

Res
$$(f(z), z_0) = \frac{1}{(n-1)!} \lim_{z \to z_0} \frac{d^{n-1}}{dz^{n-1}} [(z-z_0)^n f(z)] \Big|_{z=0}$$

3.3 Linearity

For
$$d_1, d_2 \in \mathbb{R}$$

$$\mathcal{Z}\{d_1x_1(k) + d_2x_2(k)\} = d_1\mathcal{Z}\{x_1(k)\} + d_2\mathcal{Z}\{x_2(k)\}$$

3.4 Important Z-Transforms

$$\begin{split} \mathscr{Z}\{k\} &= \frac{z}{(z-1)^2} \\ \mathscr{Z}\{a^k\} &= \frac{z}{z-a} \\ \mathscr{Z}\{ka^k\} &= \frac{az}{(z-a)^2} \\ \mathscr{Z}\{ka^k\} &= \frac{az}{(z-a)^2} \\ \mathscr{Z}\{e^{ak}\} &= \frac{z}{z-e^a} \\ \mathscr{Z}\{\sin(ak)\} &= \frac{z\sin(a)}{z^2-2\cos(a)z+1} \\ \mathscr{Z}\{\sin(ak)b^k\} &= \frac{bz\sin(a)}{z^2-2\cos(a)bz+b^2} \\ \end{split}$$

$$\begin{split} \mathscr{Z}\{k^2\} &= \frac{z(z+1)}{(z-1)^3} \\ \mathscr{Z}\{ka^{k-1}\} &= \frac{z}{(z-a)^2} \\ \mathscr{Z}\{ka^{k-1}\} &= \frac{z}{(z-a)^2} \\ \mathscr{Z}\{ke^{ak}\} &= \frac{ze^a}{(z-e^a)^2} \\ \mathscr{Z}\{\cos(ak)\} &= \frac{z(z-\cos(a))}{z^2-2\cos(a)z+1} \\ \mathscr{Z}\{\cos(ak)b^k\} &= \frac{z(z-\cos(a))}{z^2-2\cos(a)bz+b^2} \end{split}$$

3.5 Convolution of Signals

For x(k), y(k) and $k \ge 0$,

$$x * y = \sum_{l=-\infty}^{\infty} x(l)y(k-l) = \sum_{l=0}^{k} x(l)y(k-l)$$

3.5.1 Sifting Property

$$f(t) * \delta(t - T_0) = f(t - T_0)$$

3.6 Multiplication by a^k

$$\mathscr{Z}\lbrace a^k x(k)\rbrace = \sum_{k=0}^{\infty} a^k x(k) z^{-k} = X\left(\frac{z}{a}\right)$$

3.7 Forward Shift

$$\mathscr{Z}\{x(k+m)\} = z^m X(z) - \sum_{l=0}^{m-1} x(l) z^m z^{-l}$$

$$\mathscr{Z}\{x(k+m)\} = z^m X(z) - [z^m x(0) + z^{m-1} x(1) + \ldots + zx(m-1)]$$
3.8 Backward Shift

9.1 Eigenvector Method for finding A^k

$$\mathscr{Z}\{x(k-m)\} = z^{-m}X(z) + \sum_{l=0}^{m-1} x(l-m)z^{-l}$$

$$\mathscr{Z}\{x(k-m)\} = z^{-m}X(z) + x(-m) + z^{-1}x(-m+1) + \dots + x(-1)z^{-1}$$

4 Final Value Theorem

If $\lim_{k\to\infty} x(k)$ exists, then

$$\lim_{k \to \infty} x(k) = \lim_{z \to 1} (z - 1) \cdot X(z)$$

4.1 FVT Existence Condition

 $\lim_{k\to\infty} x(k)$ exists (finite) iff X(z) has no poles in **10 Transient Response** $|z| \ge 1 \in \mathbb{C}$ and at most 1 pole at z = 1

5 Initial Value Theorem

$$\lim_{k \to 0} x(k) = \lim_{z \to \infty} X(z)$$

6 Discrete Time System Models

6.1 Difference Equations

$$v(k)+a_1v(k-1)+...+a_nv(k-n) = b_0u(k)+...+b_mu(k-m)$$

6.2 G4 Transfer Functions

$$E(z) = \frac{1}{1 + CG}R(z) + \frac{-G}{1 + CG}D(z)$$
$$U(z) = \frac{C}{1 + CG}R(z) + \frac{1}{1 + CG}D(z)$$

7 Model Conversion

7.1 CT SS to TF

$$Y(s) = [C(sI - A)^{-1}B + D]U(s)$$

7.2 CT TF to SS

$$V(s) = \frac{1}{s^n + \dots + a_0} U(s), Y(s) = (b_m s^m + \dots + b_0) V(s)$$

$$f(x,u) = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ -a_0 & -a_1 & -a_2 & \cdots & -a_{n-1} \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u$$

7.3 DT SS to TF

$$Y(z) = [C(zI - A)^{-1}B + D]U(z)$$

7.4 DT TF to SS

$$V(z) = \frac{1}{z^n + \dots + a_0} U(z), Y(z) = (b_m z^m + \dots + b_1) V(z)$$

$$A = \begin{bmatrix} 1 & 0 & \dots & 0 \\ & \vdots & & \vdots \\ 0 & 0 & \dots & -a_{n-1} \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ \vdots \\ 0 \end{bmatrix}$$

$$C = \begin{bmatrix} 0 & \dots & 0 & b_1 & \dots & b_m \end{bmatrix}$$

8 Solution to State Space Models

$$x(k) = A^{k}x(0) + \sum_{i=0}^{k-1} A^{k-1-i}Bu(i)$$
$$y(k) = CA^{k}(0) + \sum_{i=0}^{k-1} CA^{k-1-i}Bu(i)$$

9 Solution to CT State Space Models

$$x(t) = e^{At}x(0) + \int_0^t e^{A(t-\tau)}Bu(\tau)dt$$

3.8 Backward Snift
$$\lambda \to \det(sI - A) = 0$$

$$\mathscr{Z}\{x(k-m)\} = z^{-m}X(z) + \sum_{l=0}^{m-1} x(l-m)z^{-l} \qquad AP = P\Lambda, \quad A^K = P\Lambda^K P^{-1}, \quad Av = \lambda v$$

$$\mathscr{Z}\{x(k-m)\} = z^{-m}X(z) + x(-m) + z^{-1}x(-m+1) + \ldots + x(-1)z^{-m+1}\Lambda = \begin{bmatrix} \lambda_1 & \ldots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \ddots & \lambda_n \end{bmatrix} \qquad P = \begin{bmatrix} v_1 & \ldots & v_n \end{bmatrix}$$

9.2 Z-Transform Method for finding A^k

Faster for $n \le 3$

$$A^k = \mathcal{Z}^{-1} \{ z(zI - A)^{-1} \}$$

10.1 Real Poles

$$\mathscr{Z}^{-1}\left[\frac{z}{z-p}\right] = p^k, k \ge 0$$

If |p| > 1, $v(k) \to \infty$. If p < 0, v(k) alternates between +ve,-ve values. If |p| < 1, $y(k) \rightarrow 0$

11 Sampled Data Systems

Sample, Hold operators are linear. $H \circ S$ is NOT time-invariant. $\hat{S} \circ H$ is time-invariant.

11.1 Sample Operator

$$y(t) \rightarrow y_d(k) = y(kT)$$

11.2 Hold Operator

$$u_d(k) = u(kT) \rightarrow u(t) = u(kT)$$
, $kT \le t < (k+1)T$

11.3 Discretized Plant LTI Model (HoS)

$$x((k+1)T = e^{AT}x(kT) + \int_0^T e^{As}ds \cdot Bu(kT)$$

$$A_d := e^{AT} \qquad B_d := \int_0^T e^{A\tau}d\tau \cdot B$$

$$G_d(z) = C_d(zI - A_d)^{-1}B_d + D_d$$

11.4 Eigenvector Method for Finding e^{AT}

$$AP = P\Lambda, \quad A = P\Lambda P^{-1}, \quad Av = \lambda v$$
$$e^{At} = Pe^{\Lambda t}P^{-1} = P\begin{bmatrix} e^{\lambda_1 t} & \cdots & \\ & e^{\lambda_n t} \end{bmatrix} P^{-1}$$

11.5 Inverse Laplace Transform for e^{AT}

$$e^{At} = \mathcal{L}^{-1}\{(sI - A)^{-1}\}$$

11.5.1 Matrix Exponential

$$e^{At} := I + At + \frac{A^2t^2}{2!} + \dots = \sum_{n=0}^{\infty} \frac{t^n A^n}{n!}$$

11.6 CT to DT Direct

$$G_d(z) = \frac{z-1}{z} \mathcal{Z} \left\{ S \left(\mathcal{L}^{-1} \left\{ \frac{G(s)}{s} \right\} \right) \right\}$$

12 Spectral Mapping Theorem

Let $A \in \mathbb{R}^{n \times n}$ and let $f : \mathbb{C} \to \mathbb{C}$ be an analytic fn at the eigenvalues $\{\lambda_1, \dots, \lambda_n\}$ of A. Then f(A) is a matrix with eigenvalues $\{f(\lambda_1), \dots, f(\lambda_n)\}$.

$$\frac{N(s)}{(s-p_1)\dots(s-p_n)} \to \frac{N_d(z)}{(z-e^{p_1t})\dots(z-e^{p_nt})}$$

13 Fourier Transforms

$$y(j\omega) = \mathbb{F}\{y(t)\} = \int_{-\infty}^{\infty} y(\tau)e^{-j\omega\tau}d\tau$$
$$y_d(e^{j\omega t}) = \mathbb{F}\{y_d(k)\} = \sum_{k=0}^{\infty} y_d(k)e^{-j\omega Tk}$$

13.1 Convolutions of Fourier Transforms

$$\mathbb{F}\{x_1(t)\cdot x_2(t)\} = \frac{1}{2\pi}X_1(j\omega) * X_2(j\omega)$$

14 Periodic Extension

$$y_e(j\omega) = \sum_{k=-\infty}^{\infty} y(j\omega + jk\frac{2\pi}{T})$$

15 CT Frequency Response

$$G(s)|_{s=j\omega}=G(j\omega)$$
, $\omega\in[0,\infty)$

$$y(t) = G(j\omega)e^{j\omega t}$$

16 DT Frequency Response

$$G_d(z)|_{z=e^{j\omega T}} = G_d(e^{j\omega T})$$
$$y(k) = [G_d(e^{j\omega T})] \cdot e^{j\omega Tk}$$

16.1 DC Gain

$$G(s)|_{s=0} = G_d(z)|_{z=1}$$

16.2 DC Freq. Response and Artifact of Sampling

$$G_d(e^{j\theta}) = G_d(e^{j(\theta+2\pi)})$$

17 Sample Operator in Frequency

$$V(j\omega) = \mathbb{F}\left\{y(t) \cdot \sum_{k=-\infty}^{\infty} \delta(t - KT)\right\}$$
$$V(j\omega) = \frac{1}{2\pi}y(j\omega) * \mathcal{L}\left\{\sum_{k=-\infty}^{\infty} \delta(t - kT)\right\}$$
$$y_d(e^{j\omega T}) = \frac{1}{T}y_e(j\omega)$$

17.1 Fourier Transform of Impulse Train

$$\mathcal{L}\left\{\sum_{k=-\infty}^{\infty} \delta(t - kT)\right\} = \frac{2\pi}{T} \sum_{k=-\infty}^{\infty} \delta(\omega - \frac{2\pi}{T}k)$$

18 Hold Operator in Frequency

$$r(t) = \frac{1}{T} [1(t) - 1(t - T)] \to R(s) = \frac{1}{T} \left[\frac{1}{s} - \frac{e^{-Ts}}{s} \right]$$

$$U(j\omega) = TR(j\omega)U_d(e^{j\omega T})$$

19 Discrete Time and Frequency Domain

For a $H \circ G(s) \circ S$ system $(u_d(k) \to G_d(z) \to y_d(k))$

$$\begin{split} G_d(e^{j\omega T}) &= \frac{Y_d(e^{j\omega T})}{U_d(e^{j\omega T})} \qquad R(j\omega) = \frac{1 - e^{-j\omega T}}{j\omega T} \\ G_d(e^{j\omega T}) &= \sum_{m=0}^{\infty} G(j\omega + j\frac{2\pi}{T}k) \cdot R(j\omega + j\frac{2\pi}{T}k) \end{split}$$

20 Nyquist-Shannon Sampling Theorem

If $G_d(e^{j\omega t})$ known, and $|G(j\omega)|=0$ for $|\omega|\geq \frac{\pi}{T}$ (Nyquist Frequency), then $G(j\omega)$ is recoverable $(G_d(z)\to G(s))$.

$$G_d(e^{j\omega T}) \approx G(j\omega) \qquad |\omega| << \frac{\pi}{T}$$

21 Stability

An DT system x(k+1) = Ax(k) is asy. stable if

$$x(k) = A^k x(0) \to 0, \quad \forall x(0)$$

 $A^k \to \text{as } k \to \infty$

A DT system is stable if

$$\forall x(0), x(k) \leq M \quad \forall k \geq 0$$

21.1 Asymptotic Stability

A system is AS iff $|\lambda| < 1 \ \forall \ \lambda \in \sigma(A)$

21.2 Internal Stability

A system is stable iff $|\lambda| \le 1 \, \forall \, \lambda \in \sigma(A)$. Additionally, for any $\lambda \in \sigma(A)$ with $|\lambda| = 1$ and λ has multiplicity $k \ge 1$, there must be k linearly independent eigenvectors $(A_i$ is diagonalizable).

22 Controlability

22.1 Controlability Matrix

 $Q_c = [B \quad AB \quad \dots \quad A^{n-1}B] \quad Q_c \in \mathbb{R}^{n \times n \cdot m}$ A pair (A, B) is controllable if $\operatorname{rank}(Q_c) = n$

22.2 PBH Test

(A,B) is **controllable** iff for eigenvalues $\lambda \in \sigma(A)$

$$rank[A - \lambda I \quad B] = n$$

(A, B) is **stabilizable** if $\exists F$ s.t. $\sigma(A + BF) \in \{|z| < 1\}$

$$(rank)[A - \lambda I \quad B] = n$$

for each eigenvalue $\lambda \in \sigma(A)$ with $|\lambda| \ge 1$

22.3 Controlable Canonical Form (CCF)

$$x(k+1) = \begin{bmatrix} 0 & 1 & & \\ & & \ddots & \\ a_1 & a_2 & \dots & a_n \end{bmatrix} x(k) + \begin{bmatrix} 0 \\ \vdots \\ 1 \end{bmatrix} u(k)$$

22.4 Cayleigh-Hamilton Theorem

Every square matrix A satisfies its own characteristic polynomial

$$\Delta(A) = 0 \implies A^n = -a_1 A^{n-1} - \dots - a_n I$$

23 Pole Placement Theorem

Given $p_1, ..., p_n$ desired CLS poles, and using state feedback $u(k) = [F_1 \quad ... \quad F_n]x(k)$

1.
$$r(z) = (z - p_1)(z - p_2)...(z - p_n)$$

- 2. Convert (A, B) to CCF $(\overline{A}, \overline{B})$
- 3. Compute $\Delta(z) = \det(zI (\overline{A} + \overline{BF}))$
- 4. Match coefficients $\Delta(z) = \Delta_d(z) = r(z)$
- 5. $F = \overline{F}P^{-1}$

23.1 P, P^{-1} and Related Matrices

$$Q_c = W = \begin{bmatrix} B & AB & \dots & A^{n-1}B \end{bmatrix}$$

$$\overline{Q_c} = \begin{bmatrix} \overline{B} & \overline{AB} & \dots & \overline{A}^{n-1}\overline{B} \end{bmatrix}$$

$$P = Q_c \overline{Q_c}^{-1}$$

23.2 Deadbeat Control

If (A, B) controllable, assign all

$$\sigma(A + BK) = \{0, \dots, 0\} \implies \Delta s = s^n$$

24 Ackermann's Formula

Let $\{\lambda_{1d}, ..., \lambda_{nd}\}$ be the desired poles of A + BK $\Delta_d(z) = (z - \lambda_{1d})...(z - \lambda_{nd}) = z^n + r_1 z^{n-1} + ... + r_n$

$$K = -[0 \dots 0 \quad 1] Q_c^{-1} \Delta_d(A)$$

$$\Delta_d(A) = A^n + r_1 A^{n-1} + \dots + r_n I$$

24.1 Stabilizability

A system is stabilizable if

$$\exists K \in \mathbb{R}^{n \times m} \text{ s.t. } \sigma(A_d + B_d K) \subset \{z \in \mathbb{C}, |z| < 1\}$$

25 Observability

25.1 Observability Matrix

$$Q_o = \begin{bmatrix} C \\ CA \\ CA^{n-1} \end{bmatrix} \quad Q_o \in \mathbb{R}^{n \cdot (p \times n)}$$

A pair (C, A) is observable if $rank(Q_0) = n$ (full col rank).

25.2 PBH Test

(C,A) is **observable** iff for eigenvalues $\lambda \in \sigma(A)$

$$\operatorname{rank} \begin{bmatrix} A - \lambda I \\ C \end{bmatrix} = n$$

(C,A) is **detectable** if $\exists L \text{ s.t. } \sigma(A-LC) \in \{|z|<1\}$ $\operatorname{rank} \begin{bmatrix} A & C \\ C \end{bmatrix} = n$

for each eigenvalue $\lambda \in \sigma(A)$ with $|\lambda| \ge 1$

25.3 Observers and Dynamic Compensation

Assuming (A, B) controllable, (C, A) observable. $\hat{x}(k+1) = A\hat{x}(k) + Bu(k) + L(y(k) - \hat{y}(k))$

$$\hat{y}(k) = C\hat{x}(k)$$

25.4 Estimation Error

$$\tilde{x}(k) = x(k) - \hat{x}(k)$$
 $\tilde{x}(k+1) = (A - LC)\tilde{x}(k)$

25.5 Observer Based Control

$$u(k) = K\hat{x}(k)$$

$$\begin{bmatrix} x(k+1) \\ \hat{x}(k+1) \end{bmatrix} = \begin{bmatrix} (A+BK) & -BK \\ 0 & (A-LC) \end{bmatrix} \cdot \begin{bmatrix} x(k) \\ \hat{x}(k) \end{bmatrix}$$

25.6 Separation Principle

$$\sigma(A_{cl}) = \sigma(A + BK) \cup \sigma(A - LC)$$

26 Minimal Order Observers

$$\begin{bmatrix} x_1' \\ x_2' \end{bmatrix} = \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} \cdot \begin{bmatrix} x_1 \\ x_2' \end{bmatrix} + \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} u \quad y = \begin{bmatrix} I & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2' \end{bmatrix}$$

$$\hat{x}(k) = \begin{bmatrix} y(k) \\ \nu(k) + Ly(k) \end{bmatrix} \quad \nu(k) = \hat{x}_2(k) - Lx_1(k)$$

$$\nu(k+1) = (A_{22} - LA_{12})\nu(k) + (B_2 - LB_1)u(k)$$

$$+ (A_{21} - LA_{11})x_1(k) - (A_{22} - LA_{12})Lx_1(k)$$

27 Duality Theory

(C,A) observable \iff (A^T,C^T) controllable (C,A) detectable \iff (A^T,C^T) stabilizable controllable \implies stabilizable observable \implies detectable

28 Pathological Sampling

A freq
$$\omega_S = \frac{2\pi}{T}$$
 is pathological if
$$e^{\lambda_1 T} = e^{\lambda_2 T} \quad , \lambda_1, \lambda_2 \in \sigma(A)$$
$$\lambda_i = \lambda_j + j \cdot \frac{2\pi}{T} l \quad i, j \in \{i, \dots, n\}, \ l \in \mathbb{Z}$$

29 Exosystem

$$\dot{\omega} = S\omega \quad \omega(k+1) = S\omega(k) \quad r = C_2\omega$$

29.1 Common Exosystems

| r(t)/r(k) | S | | ω |
|-------------------------|---|--|--|
| sin(at) | $\begin{bmatrix} 0 \\ -a \end{bmatrix}$ | a | $\begin{bmatrix} r \\ \dot{r} \end{bmatrix}$ |
| 1(kT) | 1 | 01 | r(k) |
| $kT \cdot 1(kT)$ | $\begin{bmatrix} 0 \\ -1 \end{bmatrix}$ | $\begin{bmatrix} 1 \\ 2 \end{bmatrix}$ | $\begin{bmatrix} r(k) \\ r(k+1) \end{bmatrix}$ |
| $\sin(akT) \cdot 1(kT)$ | $\begin{bmatrix} \cos(aT) \\ -\sin(aT) \end{bmatrix}$ | $ \frac{\sin(aT)}{\cos(aT)} $ | $\begin{bmatrix} r(k) \\ r(k+1) \end{bmatrix}$ |

30 Regulator Problem

$$x(k+1) = Ax(k) + Bu(k) + E\omega(k)$$

$$\omega(k+1) = S\omega(k) \quad e(k) = Cx(k) + D\omega(k)$$

30.1 Regulator Equations

$$\pi S = A\pi + B\Gamma + E$$
 $0 = c\pi + D$

30.2 Regulator Model

$$z(k) = x(k) - \pi\omega(k)$$

$$z(k+1) = Az(k) + B(u(k) - \Gamma\omega(k)) \quad e(k) = Cz(k)$$

30.3 State Feedback (Full State Measurement)

$$u(k) = K(x(k) - \pi\omega(k)) + \Gamma\omega(k)$$

30.4 State Feedback + Observers

Assuming (A, B) controllable, (C, A) observable. Assuming (C, D), $A \in S$ observable

30.4.1 Estimation Error

$$\tilde{x}(k) = x(k) - \hat{x}(k)$$
 $\tilde{\omega}(k) = \omega(k) - \hat{\omega}(k)$

30.4.2 Observer Based Control

$$u(k) = \Gamma \hat{\omega}(k) + K(\hat{x}(k) - \pi \hat{\omega}(k))$$

$$\hat{x}(k+1) = A\hat{x}(k) + Bu(k) + E\hat{\omega}(k) + L_1(e(k) - \hat{e}(k))$$

$$\hat{\omega}(k+1) = S\hat{\omega}(k) + L_2(e(k) - \hat{e}(k))$$

$$\hat{e}(k) = C\hat{x}(k) + D\hat{\omega}(k)$$

$$\overline{A} = \begin{bmatrix} A_d & E \\ 0 & S \end{bmatrix}, \overline{B} = \begin{bmatrix} B_d \\ 0 \end{bmatrix}, \overline{C} = \begin{bmatrix} C_d & D_d \end{bmatrix}$$

$$\begin{bmatrix} \hat{x}' \\ \hat{\omega}' \end{bmatrix} = \overline{A} \cdot \begin{bmatrix} \hat{x} \\ \hat{\omega} \end{bmatrix} + \overline{B}u(k) + \overline{L}(e(k) - \overline{C} \begin{bmatrix} \hat{x} \\ \hat{\omega} \end{bmatrix})$$

30.5 Regulator Design

- 1. Design *K* using pole placement
- 2. Solve regulator problem equations for (π, Γ)
- 3. Write state feedback solution (Sec. 30.3)
- 4. Design Observers (Sec. 30.4.2)
- 5. Write observer-based controller s.t. $\sigma(\overline{A} \overline{L} \cdot \overline{C}) \in \mathbb{C}^2$ (Sec. 30.4.2)

31 Discretization of CT Controllers

31.1 c2d (Step Invariance) Method

$$C_d(z) = \operatorname{c2d}(C(s)) = \frac{z-1}{z} \mathscr{Z} \left\{ S \left(\mathscr{L}^{-1} \left\{ \frac{C(s)}{s} \right\} \right) \right\}$$

31.2 Bilinear Transformation

$$s = \frac{2}{T} \frac{z-1}{z+1}$$
 $C_d(z) = C\left(\frac{2}{T} \frac{z-1}{z+1}\right)$

31.3 Pole-Zero Matching

For C(s) with d = # poles - # zeros ≥ 1 , there are d infinite zeros.

$$C(s) = K \frac{(s+b_1)(s+b_2)\dots(s+b_m)}{(s+a_1)(s+a_2)\dots(s+a_n)} \quad n \ge m$$

$$C_d(z) = k_d \frac{(z+1)^d(z-e^{-b_1T})\dots(z-e^{-b_mT})}{(z-e^{-a_1T})\dots(z-e^{-a_nT})}$$

Only add factor $(z + 1)^d$ to num of $C_d(z)$ if d = n - m > 0. Choose K_d s.t. $C_d(1) = C(0)$