$V_{in} = V_{in} = V$ Apparent Power dissaparted over the load, 5%: $S_{L} = \frac{\overline{J_{L}^{2}}}{\overline{Z_{L}}} = \frac{\overline{J_{L}^{2}}}{\overline{J_{L}^{2}}} = \frac{\overline{J_{L}^{2}}}{\overline{J_{L}^{2}}} = \frac{\overline{J_{L}^{2}}}{\overline{J_{L}^{2}}} = \frac{\overline{J_{L}^{2}}}{\overline{J_{L}^{2}}}$ $= V_{m} \frac{R_{L} + jX_{L}}{\left(R_{S} + jX_{S} + R_{L} + jX_{L}\right)^{2}}$ We're only concerned with Real power dissapation so we can ignore the imaginary term Pr = Vm Rs+RL+j(XS+X)]Z Wow we can take the denominator as a magnitude and ignore the phase. 1P21 = Vm Rs+R22+ (xs+x)21]2 => |P_L| = Vin (Rs+R) 2+ (Xx+XL) 2

Now we take the derivative with respect to X_2 $\frac{d1P_L1}{dx_L} = -\frac{2(x_s + x_L)}{(1 + (x_s + x_L)^2)^2}$

which is made zero only when $X_z = -X_5$ Plugging this relation back into equation O

1P21 = Vin 2 R2 (Rs + RL)2

which is the some relation we get brom the proof of DC MPT from page 63 of Bowick, which concluded with the following condition for MPT:

R_L=R_S

So, for maxpower transfer in an Al impulitive circuit,

X2 = -Xs and A2 = Rs

· · ZL = Zs