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(54) **INVERTER, METHOD FOR TURNING OFF  
INVERTER, AND PHOTOVOLTAIC SYSTEM**

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**ABSTRACT**

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An inverter, a method for turning off an inverter, and a photovoltaic system are provided. Pulse blocking is performed on the inverter circuit in response to a short circuit of a negative electrode of a DC source to ground. Upon determining that a current of a first switching module is in a descending trend after the inverter circuit is subjected to the pulse blocking, the first switching module and a second switching module with a current of zero are turned off simultaneously in response to a first electrical parameter of the first switching module reaching a preset electrical parameter; or the first switching module and a second switching module with a current of zero are turned off simultaneously within a first duration starting from a time instant when an actual electrical parameter of the first switching module reaches the preset electrical parameter.

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Perform pulse blocking on an inverter circuit in response to a short circuit of a negative electrode of the direct-current source to the ground, where the pulse blocking includes blocking a driving pulse of each switching transistor in the inverter circuit

~ S401

Determine, upon determining that a current of a first switching module is in a descending trend after the inverter circuit is subjected to the pulse blocking, whether a first electrical parameter of the first switching module reaches a preset electrical parameter at a current time instant, where the preset electrical parameter corresponds to a safe current of the first switching module; and turn off, in response to the first electrical parameter of the first switching module reaching the preset electrical parameter, the first switching module and a second switching module with a current that is currently monitored as zero simultaneously; or turn off the first switching module and a second switching module with the current that is currently zero simultaneously within a first duration starting from a time instant when an actual electrical parameter of the first switching module reaches the preset electrical parameter

~ S402

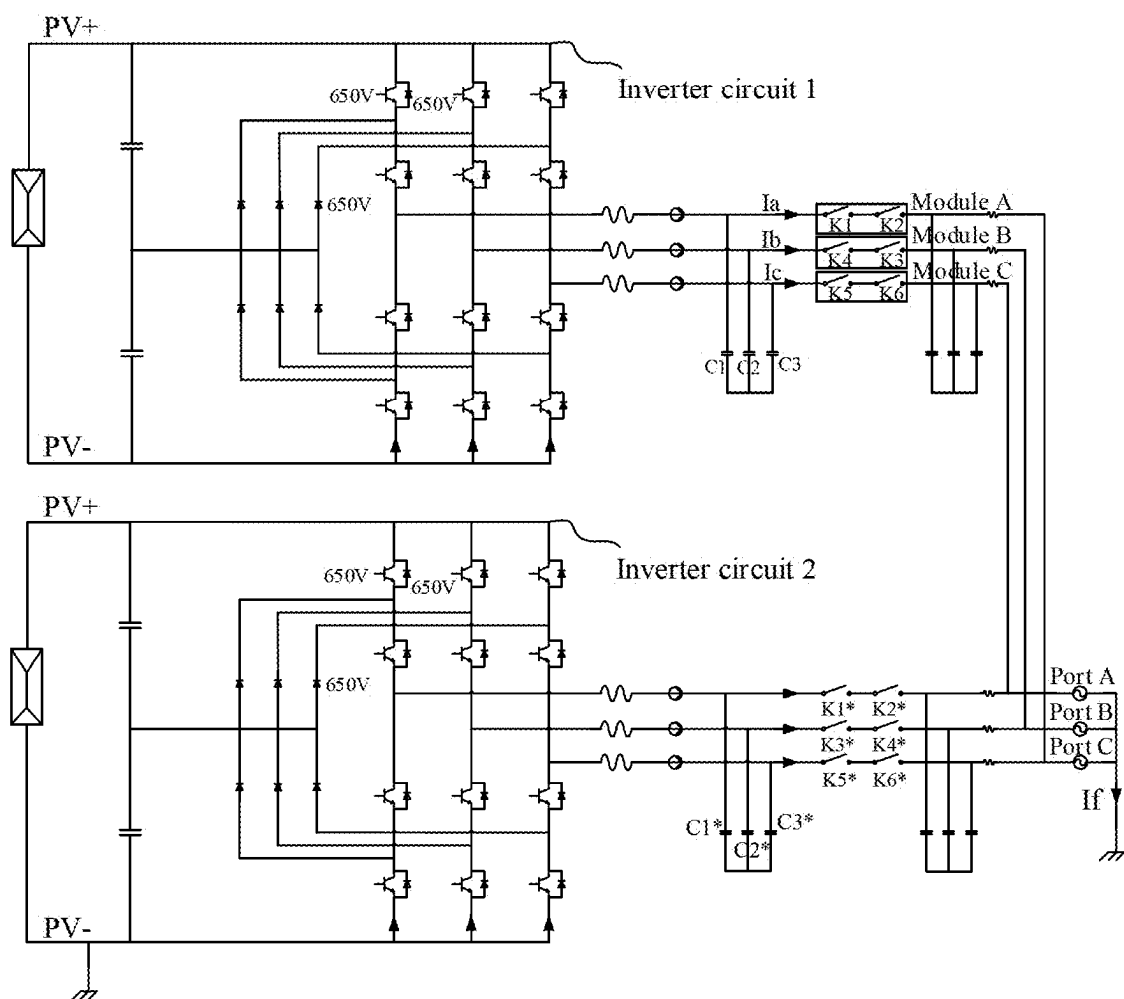


FIG. 1

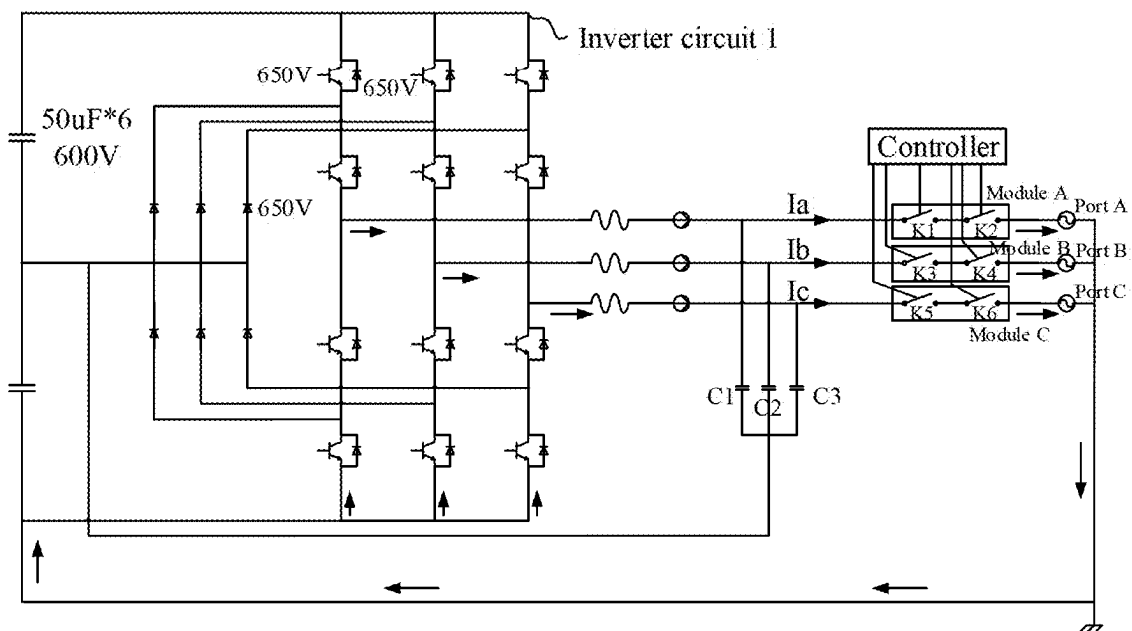


FIG. 2

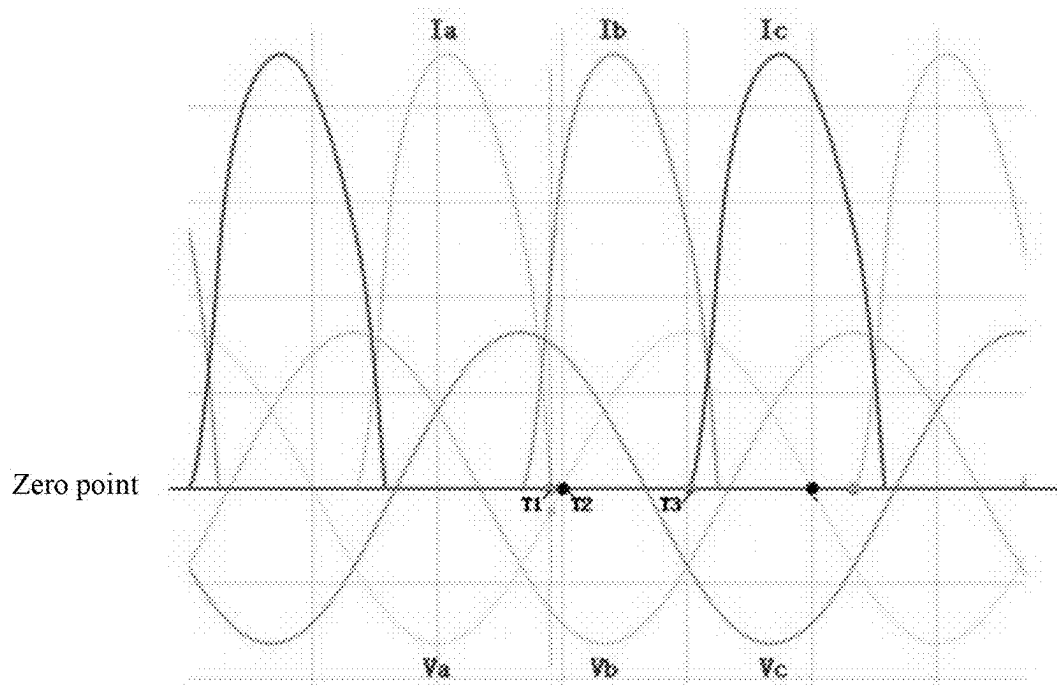


FIG. 3

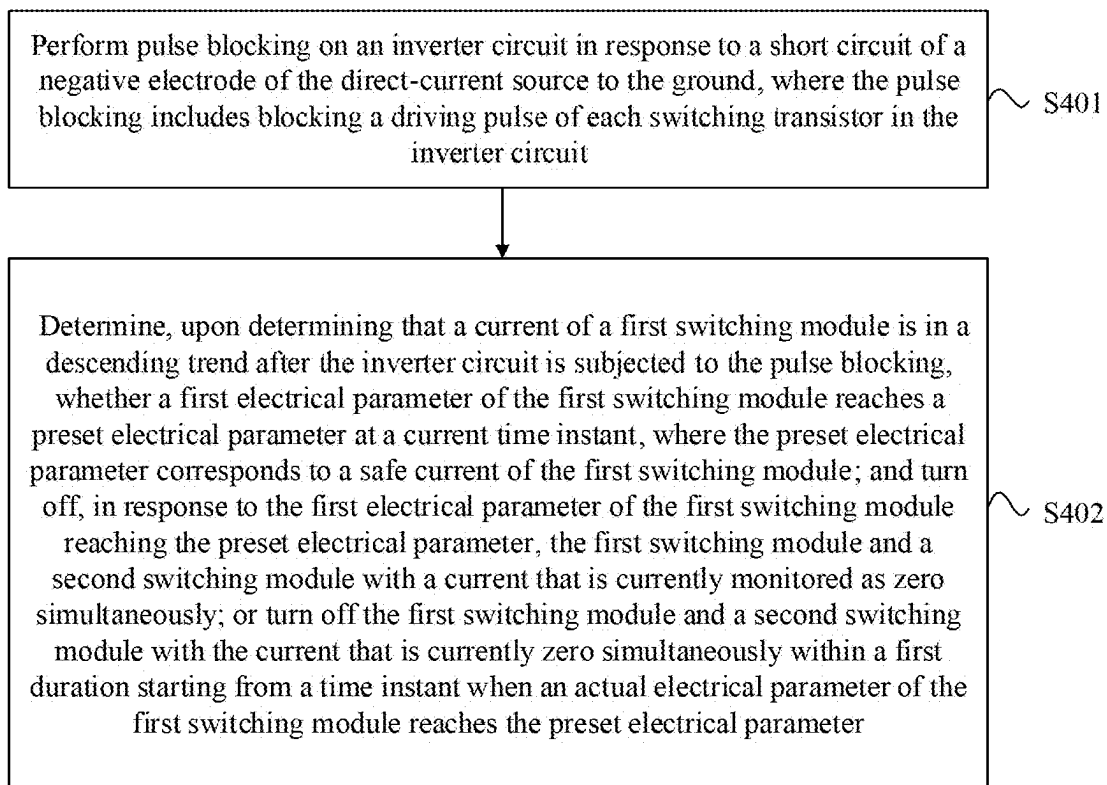


FIG. 4

## INVERTER, METHOD FOR TURNING OFF INVERTER, AND PHOTOVOLTAIC SYSTEM

[0001] The present application claims priority to Chinese Patent Application No. 202410178262.0, titled “INVERTER, METHOD FOR TURNING OFF INVERTER, AND PHOTOVOLTAIC SYSTEM”, filed on Feb. 8, 2024 with the China National Intellectual Property Administration, which is incorporated herein by reference in its entirety.

### FIELD

[0002] The present disclosure relates to the technical filed of inverters, in particular to an inverter, a method for turning off an inverter, and a photovoltaic system.

### BACKGROUND

[0003] During an operation of a photovoltaic inverter on site, output ends of multiple inverters are connected in parallel to transmit electric energy to a power grid, and a phase loss occurs due to an open relay of one phase or a blown alternating-current fuse, resulting in phase power unbalance in line voltages of the power grid. FIG. 1 is a schematic structural diagram illustrating that output ends of multiple inverters are connected in parallel to form a branch and the branch is connected to a power grid. In a case that grounding protection is performed on a negative electrode of a photovoltaic string connected to one of the inverters, after one phase relay is turned off, alternating-current equivalent parallel capacitances are different during operation of the other inverter, resulting in a large difference in three-phase capacitance, which may further lead to circulating current such as alternating-current resonance and increase the risk of failure.

### SUMMARY

[0004] In view of this, an inverter, a method for turning off an inverter, and a photovoltaic system are provided according to the present disclosure, to avoid the problem of phase power unbalance in voltage transmitted by other inverters to a power grid if grounding protection is performed on a negative electrode of a photovoltaic string connected to an inverter parallel with the other inverters.

[0005] In a first aspect, an inverter is provided according to the present disclosure. The inverter includes an inverter circuit, switching modules and a controller. An input end of the inverter circuit is configured to connect a direct-current (DC) source, an output end of each phase of the inverter circuit is connected to a corresponding switching module among the switching modules, and output ends of the switching modules are configured to connect a power grid. The controller is configured to: perform pulse blocking on the inverter circuit in response to a short circuit of a negative electrode of the DC source to ground, where the pulse blocking includes disabling a drive pulse for each switching transistor in the inverter circuit; and determine, upon determining that a current of a first switching module is in a descending trend after the inverter circuit is subjected to the pulse blocking, whether a first electrical parameter of the first switching module reaches a preset electrical parameter at a current time instant, where the preset electrical parameter corresponds to a safe current of the first switching module; and turn off, in response to the first electrical

parameter of the first switching module reaching the preset electrical parameter, the first switching module and a second switching module with a current that is currently monitored as zero simultaneously; or turn off the first switching module and a second switching module with a current that is currently zero simultaneously within a first duration starting from a time instant when an actual electrical parameter of the first switching module reaches the preset electrical parameter, where the first switching module and the second switching module each are one of the switching modules.

[0006] In a second aspect, a method for turning off an inverter is further provided according to the present disclosure. The inverter includes: an inverter circuit and switching modules. An input end of the inverter circuit is configured to connect a direct-current (DC) source, an output end of each phase of the inverter circuit is connected to a corresponding switching module among the switching modules, and output ends of the switching modules are configured to connect a power grid. The method includes: performing pulse blocking on the inverter circuit in response to a short circuit of a negative electrode of the DC source to ground, where the pulse blocking includes disabling a drive pulse for each switching transistor in the inverter circuit; and determining, upon determining that a current of a first switching module is in a descending trend after the inverter circuit is subjected to the pulse blocking, whether a first electrical parameter of the first switching module reaches a preset electrical parameter at a current time instant, where the preset electrical parameter corresponds to a safe current of the first switching module; and turning off, in response to the first electrical parameter of the first switching module reaching the preset electrical parameter, the first switching module and a second switching module with a current that is currently monitored as zero simultaneously; or, turning off the first switching module and a second switching module with a current that is currently zero simultaneously within a first duration starting from a time instant when an actual electrical parameter of the first switching module reaches a preset electrical parameter, where the first switching module and the second switching module each are one of the switching modules.

[0007] In a third aspect, a photovoltaic system is provided according to the present disclosure. The photovoltaic system includes a photovoltaic string and an inverter, where the photovoltaic string is connected to an input end of the inverter, and is configured to supply direct-current (DC) power to the inverter; an output end of the inverter is configured to connect a power grid, convert DC power into alternating-current (AC) power, and transmit the AC power to the power grid; and the inverter is the inverter in the first aspect described above.

### BRIEF DESCRIPTION OF THE DRAWINGS

[0008] In order to illustrate technical solutions in embodiments of the present disclosure or the conventional technology more clearly, drawings to be used in the embodiments or the conventional technology are introduced simply hereinafter. It is apparent that the drawings described below show only some embodiments of the present disclosure. For those skilled in the art, other drawings may be obtained based on the provided drawings without any creative effort.

[0009] FIG. 1 is a schematic structural diagram illustrates that output ends of multiple inverters are connected in

parallel to form a branch, and the branch is connected to a power grid according to the background of the present disclosure;

**[0010]** FIG. 2 is a schematic structural diagram of an inverter according to an embodiment of the present disclosure;

**[0011]** FIG. 3 is a schematic diagram of a periodic current curve and a periodic voltage curve of each phase after an inverter is short-circuited to ground according to an embodiment of the present disclosure; and

**[0012]** FIG. 4 is a schematic flowchart of a method for turning off an inverter according to an embodiment of the present disclosure.

#### DETAILED DESCRIPTION

**[0013]** During an operation of a photovoltaic inverter on site, output ends of multiple inverters are connected in parallel to transmit electric energy to a power grid, and a phase loss occurs due to an open relay of one phase or a blown alternating-current fuse, resulting in phase power unbalance in line voltages of the power grid. As shown in FIG. 1, in a case that grounding protection is performed on a photovoltaic string connected to an inverter in an inverter circuit 1, and a switching module A of the inverter circuit 1 is turned off, the inverter circuit 1 is still connected to a capacitor C2 and a capacitor C3. As a result, alternating-current equivalent parallel capacitances are different during the operation of the inverter connected to an inverter circuit 2, resulting in a relatively large difference in three-phase capacitance of the inverter connected to the inverter circuit 2, which may further lead to circulating current such as alternating-current resonance, and increase the risk of failure.

**[0014]** In view of the above problems, an inverter, a method for turning off an inverter, and a photovoltaic system are provided according to the present disclosure. The inverter includes an inverter circuit, switching modules and a controller, where an input end of the inverter circuit is configured to connect a DC source, an output end of each phase of the inverter circuit is connected to a corresponding switching module among the switching modules, and output ends of the switching modules are configured to connect a power grid. The controller is configured to perform pulse blocking on the inverter circuit in response to a short circuit of a negative electrode of the DC source to ground, where the pulse blocking includes disabling a drive pulse for each switching transistor in the inverter circuit; and determine, upon determining that a current of a first switching module is in a descending trend after the inverter circuit is subjected to the pulse blocking, whether a first electrical parameter of the first switching module reaches a preset electrical parameter at a current time instant, where the preset electrical parameter corresponds to a safe current of the first switching module; and turn off, in response to the first electrical parameter of the first switching module reaching the preset electrical parameter, the first switching module and a second switching module with a current that is currently monitored as zero simultaneously; or, turn off the first switching module and a second switching module with a current that is currently zero simultaneously within a first duration starting from a time instant when an actual electrical parameter of the first switching module reaches the preset electrical parameter, where the first switching module and the second switching module each are one of the switching

modules; where the first switching module and the second switching module each are one of the switching modules. In the above description, the first switching module and the second switching module are turned off simultaneously, which may be referred to FIG. 1. As shown in FIG. 1, if the switching module A and the switching module B are turned off simultaneously, a capacitor C1 and a capacitor C2 are disconnected from the power grid, a capacitor C3 has one terminal connected to the switching module C and has the other terminal disconnected from the switching module. Consequently, the capacitor C3 is disconnected from the power grid, so that the capacitors in the inverter short-circuited to the ground do not affect other inverters connected in parallel with the short-circuited inverter to transmit electric energy to the power grid if the switching module A and the switching module B are turned off simultaneously, avoiding an occurrence of the circulating current such as alternating-current resonance, so that other inverters in normal operation can stably transmit electric energy to the power grid.

**[0015]** In order to understand the features and technical content of the embodiments of the present disclosure more thoroughly, implementations of the embodiments of the present disclosure are described in detail below with reference to the drawings. The drawings are only for the purpose of reference and illustration, and are not intended to limit the embodiments of the present disclosure. In the following description of the technology, to facilitate explanation, numerous details are set forth in order to provide a thorough understanding of the disclosed embodiments. However, one or more embodiments may still be implemented without these details. In other instances, well-known structures and devices may simplify presentation for simplicity of the drawings.

**[0016]** In the specification, the claims and the drawings of the embodiments of the present disclosure, terms such as “first” and “second” are merely for distinguishing similar objects rather than describing a specific order or sequence. The data used in such a way is interchangeable in proper circumstances, to facilitate describing the embodiments of the present disclosure. In an embodiment, the terms “comprise”, “include”, and any variations thereof are intended to cover non-exclusive inclusion.

**[0017]** Unless otherwise stated, the term “plurality” or “multiple” means two or more.

**[0018]** In the embodiments of the present disclosure, the character “/” indicates an “or” relationship between the objects before and after. For example, A/B represents: A or B.

**[0019]** The term “and/or” is an association relationship describing an object, indicating that there may be three relationships. For example, A and/or B represents three relationships: A, B, or A and B.

**[0020]** In order to make the purpose, technical solutions and advantages of the embodiments of the present disclosure more clear, technical solutions in the embodiments of the present disclosure are described clearly and completely hereinafter with reference to the drawings in the embodiments of the present disclosure. Apparently, the described embodiments are only some, rather than all of the embodiments of the present disclosure. Based on the embodiments of the present disclosure, all other embodiments obtained by those skilled in the art without any creative work fall into the protection scope of the present disclosure.

[0021] FIG. 2 is a schematic structural diagram of an inverter. FIG. 2 is a schematic structural diagram only illustrating that an inverter with an inverter circuit 1 is connected to a power grid (where the inverter is connected to the power grid through a port A, a port B, and a port C in FIG. 2, and is configured to transmit corresponding phase power to the power grid), and other inverters that are connected in parallel to the inverter and are connected to the power grid are not illustrated in the FIG. 2. It should be noted that, a short-circuited loop of the inverter to ground is indicated by the arrow in FIG. 2.

[0022] Referring to FIG. 2, an inverter includes an inverter circuit, switching modules and a controller. An input end of the inverter circuit is configured to connect a DC source, an output end of each phase of the inverter circuit is connected to a corresponding switching module among the switching modules, and output ends of the switching modules are configured to connect a power grid.

[0023] The DC source may be a photovoltaic string, a DC bus connected to multiple photovoltaic strings, or may be other energy storage modules capable of storing DC power.

[0024] The switching module may include at least one relay switch. The controller turns off one relay switch or multiple relay switches in the switching module, thus turning off the switching module. For example, in FIG. 2, the switching module A includes K1 and K2 connected in series.

[0025] The inverter circuit is a multi-phase inverter circuit. For example, referring to the inverter circuit shown in FIG. 2, the inverter circuit is a three-phase inverter circuit. Corresponding to the three-phase inverter circuit in FIG. 2, the switching module A, a switching module B, and a switching module C are arranged. Each phase of the inverter circuit is connected to the power grid through the switching module. For example, the switching module A includes K1 and K2 connected in series, the output end of the switching module A is connected to the port A to transmit power to the power grid. Similarly, the switching module B transmits phase power to the power grid through the port B, and the switching module C transmits phase power to the power grid through the port C.

[0026] The controller is configured to perform pulse blocking on the inverter circuit in response to a short circuit of a negative electrode of the DC source to the ground, where the pulse blocking includes disabling a drive pulse for each switching transistor in the inverter circuit.

[0027] In an embodiment, upon determining that a current of a first switching module is in a descending trend after the inverter circuit is subjected to the pulse blocking, it is determined whether a first electrical parameter of the first switching module reaches a preset electrical parameter at a current time instant, where the preset electrical parameter corresponds to a safe current of the first switching module. In response to the first electrical parameter of the first switching module reaching the preset electrical parameter, the first switching module and a second switching module with a current of zero at the current time instant are turned off simultaneously.

[0028] The safe current described above is determined based on a maximum impulse current that can be withstood by the switching module. For example, the safe current is zero if the switching module fails to withstand the impulse current.

[0029] The electrical parameter of the switching module may be acquired from an input terminal of the switching module, or may be acquired from an output terminal of the switching module.

[0030] In an embodiment, the first electrical parameter may be a current acquired from the first switching module. The preset electrical parameter is a first preset current, and the first preset current may be determined based on the safe current of the first switching module and a periodic current curve and a periodic voltage curve of each phase power after the inverter is short-circuited to the ground as shown in FIG. 3. For example, the first preset current may be the safe current, or may be a current corresponding to a time instant obtained by subtracting a first delay duration from a time instant corresponding to the safe current in a descending portion of the periodic current curve of phase power corresponding to the first switching module in FIG. 3. The first delay duration is a duration from a time instant when a turn-off signal is sent to the first switching module to a time instant when the first switching module is actually turned off.

[0031] In another embodiment, the first electrical parameter may be a voltage acquired from the first switching module. The preset electrical parameter is a first preset voltage, and the first preset current may be determined based on the safe current of the first switching module and the periodic current curve and the periodic voltage curve of each phase power after the inverter is short-circuited to the ground as shown in FIG. 3. For example, the first preset voltage may be a voltage corresponding to the safe current, or may be a voltage corresponding to the time instant obtained by subtracting the first delay duration from a time instant corresponding to the safe current in the descending portion of the periodic current curve of the phase power corresponding to the first switching module in FIG. 3.

[0032] In another embodiment, upon determining that the current of the first switching module is in a descending trend after the inverter circuit is subjected to the pulse blocking, the first switching module and the second switching module with a current of zero at a current time instant are turned off simultaneously within a first duration starting from a time instant when an actual electrical parameter of the first switching module reaches the preset electrical parameter. The first switching module and the second switching module each are one of the switching modules.

[0033] For example, referring to FIG. 3, the current  $I_a$  and the current  $I_c$  are both zero within a time interval from T1 to T3, and an A-phase switching module and a C-phase switching module are turned off simultaneously.

[0034] Based on the inverter, the first switching module and the second switching module are turned off simultaneously. For example, referring to FIG. 1, if the switching module A and the switching module C are turned off simultaneously, the capacitor C1 and the capacitor C3 in FIG. 1 are disconnected from the power grid. The capacitor C2 has only one terminal connected to the switching module B, and has the other terminal disconnected from the switching module. Consequently, the capacitor C2 is disconnected from the power grid, so that the capacitors in the inverter short-circuited to the ground do not affect other inverters connected in parallel with the short-circuited inverter to transmit electric energy to the power grid if the switching module A and the switching module C are turned off simultaneously, avoiding the circulating current such as

alternating-current resonance, so that other inverters in normal operation can stably transmit electric energy to the power grid.

**[0035]** In the embodiment described above, upon determining that the current of the first switching module is in the descending trend after the inverter circuit is subjected to pulse blocking, it is determined whether the first electrical parameter of the first switching module reaches the preset electrical parameter at a current time instant, where the preset electrical parameter corresponds to the safe current of the first switching module. In response to the first electrical parameter of the first switching module reaching the preset electrical parameter, the first switching module and the second switching module with a current of zero at the current time instant are turned off simultaneously.

**[0036]** In a case that the first electrical parameter is a current, it is determined that the first electrical parameter of the first switching module reaches the preset electrical parameter if the first electrical parameter of the first switching module is less than or equal to the first preset current, the current of the first switching module is continuously monitored if the current of the first switching module is greater than the first preset current until it is monitored that the current of the first switching module decreases to be less than or equal to the first preset current, and then it is determined that the first electrical parameter of the first switching module reaches the preset electrical parameter.

**[0037]** Taking the inverter in FIG. 2 and FIG. 3 as an example, the first electrical parameter is a current, and the preset electrical parameter is the first preset current. The first preset current may be the safe current of the first switching module, or may be the current corresponding to the time instant obtained by subtracting the first delay duration from the time instant corresponding to the safe current in the descending portion of the periodic current curve of the phase power corresponding to the first switching module in FIG. 3. The first delay duration is a duration from the time instant when the turn-off signal is sent to the first switching module to the time instant when the first switching module is actually turned off.

**[0038]** For example, referring to FIG. 3, the periodic current curve of the A-phase current  $I_a$  corresponding to the switching module A is taken as an example. In the descending portion of the periodic current curve, if the safe current of zero corresponding to a time instant T1, the current corresponding to the time instant obtained by subtracting the first delay duration of the switching module A from the time instant T1 is the first preset current of the switching module A.

**[0039]** For example, the first preset current of the first switching module is set to 0.6 amps (A), and it is determined that the current of the first switching module is in the descending trend. In an embodiment, the first electrical parameter (i.e., the current) of the first switching module is acquired as 0.5 A at a current time instant, and the first electrical parameter 0.5 A of the first switching module at the current time instant is less than the first preset current 0.6 A of the first switching module, and thus it is determined that the first electrical parameter of the first switching module reaches the preset electrical parameter. In another embodiment, if the first electrical parameter (i.e., the current) of the first switching module is acquired as 1 A at a current time instant, and the current of the 1 A is greater than the first preset current 0.6 A of the first switching module, and thus

the current of the first switching module is continuously monitored. For example, the current of the first switching module is continuously monitored as 0.9 A, 0.7 A and 0.5 A, until it is monitored that the current of the first switching module is less than or equal to the first preset current. That is, it is determined that the first electrical parameter of the first switching module reaches the preset electrical parameter if it is monitored that the current of the first switching module decreases to 0.5 A which is less than or equal to the first preset current 0.6 A.

**[0040]** Alternatively, in a case that the first electrical parameter is a voltage, it is determined that the first electrical parameter of the first switching module reaches the preset electrical parameter if the first electrical parameter of the first switching module is greater than or equal to the first preset voltage; and the voltage of the first switching module is continuously monitored if the voltage of the first switching module is less than the first preset voltage until it is monitored that the voltage of the first switching module increases to be greater than or equal to the first preset voltage, and then it is determined that the first electrical parameter of the first switching module reaches the preset electrical parameter.

**[0041]** The inverter in FIG. 2 and FIG. 3 are taken as an example. The first electrical parameter is the voltage, and the preset electrical parameter is the first preset voltage. The first preset voltage may be a voltage corresponding to the safe current of the first switching module, or may be a voltage corresponding to the time instant obtained by subtracting the first delay duration from the time instant corresponding to the safe current in the descending portion of the periodic current curve of the phase power corresponding to the first switching module in FIG. 3.

**[0042]** For example, referring to FIG. 3, the periodic current curve of the A-phase current  $I_a$  and the periodic voltage curve corresponding to the switching module A are taken as an example. In the descending portion of the periodic current curve and the corresponding periodic voltage curve, if the safe current is zero at the time instant T1, the voltage corresponding to the time instant obtained by subtracting the first delay duration of the switching module A from the time instant T1 is the first preset voltage of the switching module A.

**[0043]** For example, the first preset voltage of the first switching module is set to -0.5 volts (V), and it is determined that the current of the first switching module is in the descending trend (or the voltage is in a rising trend). In an embodiment, the first electrical parameter (i.e., the voltage) of the first switching module is acquired as -0.4V at a current time instant, and the first electrical parameter -0.4 of the first switching module at the current time instant is greater than the first preset voltage -0.5V of the first switching module, and thus it is determined that the first electrical parameter of the first switching module reaches the preset electrical parameter. In another embodiment, the first electrical parameter (i.e., the voltage) of the first switching module is acquired as -1V at a current time instant, and the voltage of the -1V is less than the first preset voltage -0.5V of the first switching module, and thus the voltage of the first switching module is continuously monitored. For example, the voltage of the first switching module is continuously monitored as -0.85V, -0.65V and -0.45V, until it is monitored that the voltage of the first switching module greater than or equal to the first preset voltage. That is, it is



determined that the first electrical parameter of the first switching module reaches the preset electrical parameter if it is monitored that the voltage of the first switching module increases to  $-0.45\text{V}$  which is greater than the first preset voltage  $-0.5\text{V}$ .

**[0044]** A time interval for acquiring the first electrical parameter of the first switching module may be constant, or may change. An electrical parameter acquisition module may be arranged for acquiring and recording the electrical parameter. For example, the time interval is determined based on a frequency or a period of phase power of the inverter circuit. For example, the frequency of the phase power is  $50\text{ Hz}$ , the period of the phase power is  $0.02\text{ S}$ , and the time interval may be one twentieth of the period, that is,  $0.001\text{ S}$ , so that the current change trend can be determined by multiple times of acquisitions.

**[0045]** After the first switching module and the second switching module are turned off simultaneously, a switching module that is on among the switching modules connected to the inverter circuit is turned off upon monitoring that a current of the switching module is in the descending trend and the first electrical parameter of the switching module reaches the preset electrical parameter.

**[0046]** In a case that the inverter is a three-phase inverter, for example, the three-phase inverter shown in FIG. 2, after the switching modules corresponding to two phases (i.e., a phase A and a phase C) are turned off, the switching module corresponding to the remaining phase (i.e., a phase B) may be turned off. Therefore, the B-phase switching module may be turned off in response to the current of the B-phase switching module in the descending trend, and the first electrical parameter of the B-phase switching module reaching the preset electrical parameter.

**[0047]** In the above embodiment, upon determining that the current of the first switching module is in the descending trend after the inverter circuit is subjected to the pulse blocking, the first switching module and the second switching module with the current of zero are turned off simultaneously within the first duration starting from the time instant when it is monitored that the actual electrical parameter of the first switching module reaches the preset electrical parameter. The first switching module and the second switching module each are one of the switching modules.

**[0048]** Within the first duration starting from the time instant when it is monitored that the actual electrical parameter of the first switching module reaches the preset electrical parameter, the first switching module and the second switching module with the current of zero are turned off simultaneously. The first duration is used to increase a time range for turn-off control by the controller, reduce a situation that the controller does not perform turn-off control until a next cycle, that is, reduce a situation that the switches withstand a large impulse current again during a process of waiting for the next cycle.

**[0049]** The monitoring may be implemented by continuously high-frequency sampling a current, to determine the current change trend and the current.

**[0050]** In another embodiment, the preset electrical parameter and the first duration are implemented in multiple manners, and details are described hereinafter.

**[0051]** In an embodiment, the actual electrical parameter reaching the preset electrical parameter lies in that an actual current is less than or equal to the preset electrical parameter.

**[0052]** The actual electrical parameter of the first switching module is a current actually acquired by the first switching module, that is, the actual current. The actual current is less than or equal to the preset electrical parameter in multiple manners, depending on the actual situations, and details are described as follows.

**[0053]** In a case that the first delay duration is ignored, the preset electrical parameter is zero. The first duration is a sum of a first time length and a quarter of a period of phase power corresponding to the first switching module. The first time length is a time length from a time instant when the current of the first switching module decreases to zero to a nearest time instant when the voltage of the first switching module is zero.

**[0054]** Referring to FIG. 3, the first duration is a time length from T1 to T3. The first time length is a time length from T1 to T2.

**[0055]** In a case that the first delay duration is considered, the preset electrical parameter is a current corresponding to a first time instant. The first time instant is a periodic time instant determined by subtracting the first delay duration from a time instant when the current in the periodic current curve corresponding to the first switching module decreases to zero. The first delay duration includes a duration from the time instant when the turn-off signal is sent to the first switching module to the time instant when the first switching module is actually turned off. The first duration is a sum of the first time length and the quarter of the period of phase power corresponding to the first switching module.

**[0056]** The first delay duration is mainly caused by a signal delay duration of a micro control unit (MCU) of the controller, a turn-off duration of the relay, a turn-off duration of the driving circuit, or the like. The signal delay duration of the MCU is determined based on human experience, the turn-off duration of the relay is determined based on the relay parameter, and the turn-off duration of the driving circuit is determined based on a driving voltage.

**[0057]** In a case that the first delay duration and a power-resistant duration are considered, the preset electrical parameter is a current corresponding to a second time instant. The second time instant is a periodic time instant determined by subtracting a second delay duration from the time instant when the current in the periodic current curve corresponding to the first switching module decreases to zero. The second delay duration includes a duration from the time instant when the turn-off signal is sent to the first switching module to the time instant when the first switching module is actually turned off, and the power-resistant duration from a time instant corresponding to a maximum impulse current withstood by the first switching module to the time instant when the current in the descending portion of the periodic current curve decreases to zero.

**[0058]** It should be noted that, the power-resistant duration of the first switching module is approximately equal to a power-resistant duration of the second switching module. The first power-resistant duration of the first switching module is the duration from the time instant corresponding to the maximum impulse current withstood by the first switching module to the time instant when the current in the descending portion of the periodic current curve corresponding to the first switching module decreases to zero. The power-resistant duration of the second switching module is a duration from a time instant when a current in a rising portion of the periodic current curve corresponding to the

second switching module is zero to a time instant corresponding to a maximum impulse current withstood by the second switching module. If the power-resistant duration of the first switching module is not equal to the power-resistant duration of the second switching module, a power-resistant duration with a short duration is selected from the two power-resistant durations as the final power-resistant duration.

[0059] In another embodiment, the actual electrical parameter reaching the preset electrical parameter lies in that an actual voltage is greater than or equal to the preset electrical parameter.

[0060] The actual electrical parameter of the first switching module is a voltage actually acquired by the first switching module, that is, the actual voltage. In addition, the actual voltage is greater than or equal to the preset electrical parameter in multiple manners, depending on the actual situations, and details are described as follows.

[0061] In a case that the first delay duration is ignored, the preset electrical parameter is a voltage corresponding to a time instant when a current of the first switching module decreases to zero. The first duration is a sum of a first time length and a quarter of a period of phase power corresponding to the first switching module. The first time length is a time length from the time instant when the current of the first switching module decreases to zero to a nearest time instant when the voltage of the first switching module is zero.

[0062] In a case that the first delay duration is considered, the preset electrical parameter is a voltage corresponding to a time instant determined by subtracting the first delay duration from a time instant when a current of the first switching module decreases to zero. The first delay duration includes a duration from a time instant when the turn-off signal is sent to the first switching module to a time instant when the first switching module is actually turned off. The first duration is a sum of the first time length and a quarter of a period of phase power corresponding to the first switching module.

[0063] In a case that the first delay duration and the power-resistant duration are considered, the preset electrical parameter is a voltage corresponding to a time instant determined by subtracting a second delay duration from the time instant when the current of the first switching module decreases to zero. The second delay duration includes a duration from a time instant when the turn-off signal is sent to the first switching module to the time instant when the first switching module is actually turned off, and the power-resistant duration from a time instant corresponding to the maximum impulse current withstood by the first switching module to the time instant when the current in the descending portion of the periodic current curve decreases to zero. The first duration is a sum of the first time length, the quarter of the period of phase power corresponding to the first switching module and two times of the power-resistant duration.

[0064] The first time length (i.e., the time length from T1 to T2 in FIG. 3) is calculated by the following equation:

$$\Delta T = \frac{2\pi - \arcsin\left(\frac{V}{\sqrt{2}U}\right)}{2\pi} * \frac{1}{f}, \quad \frac{3\pi}{2} < \arcsin\left(\frac{V}{\sqrt{2}U}\right) < 2\pi$$

[0065] where, U represents a rated voltage of the phase power corresponding to the first switching module, V represents a voltage of the phase power corresponding to the first switching module, and f represents a frequency of the phase power corresponding to the first switching module.

[0066] Further, the first duration is calculated by the following equation:

$$T = \frac{\pi}{2\pi} * \frac{1}{f} + \Delta T$$

[0067] In another embodiment, after turning off the first switching module and the second switching module with the current of zero at the current time instant simultaneously, the controller is further configured to: turn off a switching module that is on among the switching modules connected to the inverter circuit upon monitoring that a current of the switching module is in the descending trend and the actual electrical parameter of the switching module reaches the preset electrical parameter.

[0068] In the two embodiments described above, it is determined that the current of the first switching module is in the descending trend by: continuously acquiring multiple currents of the first switching module, and determining that the current of the first switching module is in the descending trend in response to the multiple currents of the first switching module in the descending trend; or determining that the current of the first switching module is in the descending trend upon determining that the periodic voltage curve of phase power corresponding to the first switching module is in the rising trend.

[0069] A time interval for acquiring the electrical parameter may be constant, or may change. An electrical parameter acquisition module may be arranged for acquiring and recording the electrical parameter. For example, the time interval is determined based on a frequency or a period of phase power of the inverter circuit. For example, the frequency of the phase power is 50 Hz, the period of phase power is 0.02 S, and the time interval may be one twentieth of the period, that is, 0.001 S, so that the current change trend can be determined by multiple times of acquisitions.

[0070] In the embodiments described above, the switching module includes at least two relay switches, and a control terminal of each of the relay switches is connected to the controller.

[0071] The switching module is turned off by turning off one relay switch in the switching module, or turning off multiple relay switches in the switching module.

[0072] Multiple redundant switches are arranged on the switching module, so that the switches can alternately operate, prolonging the service life of each switch.

[0073] The inverter according to some embodiments of the present disclosure are described above. Based on this, a corresponding method is provided according to the present disclosure. The method according to an embodiment of the present disclosure is described hereinafter.

[0074] Reference is made to FIG. 4, which is a schematic flowchart of a method for turning off an inverter. The inverter includes an inverter circuit and switching modules. An input end of the inverter circuit is configured to connect a DC source, an output end of each phase of the inverter circuit is connected to a corresponding switching module

among the switching modules, and output ends of the switching modules are configured to connect a power grid. The method includes the following steps S401 and S402.

**[0075]** In step S401, pulse blocking is performed on the inverter circuit in response to a short circuit of a negative electrode of the DC source to ground, where the pulse blocking includes disabling a drive pulse for each switching transistor in the inverter circuit.

**[0076]** In step S402, upon determining that a current of a first switching module is in a descending trend after the inverter circuit is subjected to the pulse blocking, it is determined whether a first electrical parameter of the first switching module reaches a preset electrical parameter at a current time instant, where the preset electrical parameter corresponds to a safe current of the first switching module; and the first switching module and a second switching module with a current of zero at the current time instant are turned off simultaneously in response to the first electrical parameter of the first switching module reaching the preset electrical parameter.

**[0077]** Alternatively, upon determining that the current of the first switching module is in the descending trend after the inverter circuit is subjected to the pulse blocking, the first switching module and the second switching module with the current that is currently zero are turned off simultaneously within a first duration starting from a time instant when an actual electrical parameter of the first switching module reaches the preset electrical parameter.

**[0078]** Each of the first switching module and the second switching module is one of the switching modules connected to the inverter.

**[0079]** Based on the method for turning off the inverter described above, the first switching module and the second switching module are turned off simultaneously, disconnecting parallel capacitors in the short-circuited inverter to the ground from the power grid, avoiding the problem of circulating current such as alternating-current resonance due to a capacitance difference between various phases of other inverters in normal operation is large resulted from that the parallel capacitors in the short-circuited inverter to the ground are connected to the power grid, so that the other inverters in normal operation can stably transmit electric energy to the power grid.

**[0080]** In an embodiment, the first electrical parameter of the first switching module reaching the preset electrical parameter includes: determining that the first electrical parameter of the first switching module reaches the preset electrical parameter if the first electrical parameter is a current and the first electrical parameter of the first switching module is less than or equal to a first preset current; and determining that the first electrical parameter of the first switching module reaches the preset electrical parameter if the first electrical parameter is a voltage and the first electrical parameter of the first switching module is greater than or equal to a first preset voltage.

**[0081]** In another embodiment, after the determining whether the first electrical parameter of the first switching module reaches the preset electrical parameter at the current time instant, the method further includes: continuously monitoring the current of the first switching module if the first electrical parameter is the current and the current of the first switching module is greater than the first preset current, until it is monitored that the current of the first switching module decreases to be less than or equal to the first preset

current; and determining that the first electrical parameter of the first switching module reaches the preset electrical parameter; or continuously monitoring a voltage of the first switching module if the first electrical parameter is the voltage and the voltage of the first switching module is less than the first preset voltage, until it is monitored that the voltage of the first switching module increases to be greater than or equal to the first preset voltage; and determining that the first electrical parameter of the first switching module reaches the preset electrical parameter.

**[0082]** Further, after the turning off the first switching module and the second switching module simultaneously, the method further includes turning off a switching module that is on among the switching modules connected to the inverter circuit upon monitoring that a current of the switching module is in the descending trend and the first electrical parameter of the switching module reaches the preset electrical parameter.

**[0083]** In an embodiment, the actual electrical parameter reaching the preset electrical parameter lies in that an actual current is less than or equal to the preset electrical parameter.

**[0084]** In an embodiment, the preset electrical parameter is zero; the first duration is a sum of a first time length and a quarter of a period of phase power corresponding to the first switching module; and the first time length is a time length from a time instant when the current of the first switching module decreases to zero to a nearest time instant when the voltage of the first switching module is zero.

**[0085]** In another embodiment, the preset electrical parameter is a current corresponding to a first time instant, the first time instant is a periodic time instant determined by subtracting a first delay duration from a time instant when a current in a periodic current curve corresponding to the first switching module decreases to zero. The first delay duration includes a duration from a time instant when a turn-off signal is sent to the first switching module to a time instant when the first switching module is actually turned off. The first duration is a sum of the first time length and a quarter of a period of phase power corresponding to the first switching module.

**[0086]** In another embodiment, the preset electrical parameter is a current corresponding to a second time instant, the second time instant is a periodic time instant determined by subtracting a second delay duration from a time instant when a current in the periodic current curve corresponding to the first switching module decreases to zero. The second delay duration includes a duration from a time instant when the turn-off signal is sent to the first switching module to a time instant when the first switching module is actually turned off, and a power-resistant duration from a time instant corresponding to a maximum impulse current withstood by the first switching module to the time instant when the current in a descending portion of the periodic current curve decreases to zero. The first duration is a sum of the first time length, a quarter of a period of phase power corresponding to the first switching module and two times of the power-resistant duration.

**[0087]** In another embodiment, the actual electrical parameter reaching the preset electrical parameter lies in that an actual voltage is greater than or equal to the preset electrical parameter.

**[0088]** In an embodiment, the preset electrical parameter is a voltage corresponding to a time instant when a current of the first switching module decreases to zero. The first

duration is a sum of the first time length and a quarter of a period of phase power corresponding to the first switching module. The first time length is a time length from a time instant when the current of the first switching module decreases to zero to a nearest time instant when the voltage of the first switching module is zero.

**[0089]** In another embodiment, the preset electrical parameter is a voltage corresponding to a time instant determined by subtracting a first delay duration from a time instant when a current of the first switching module decreases to zero. The first delay duration includes a duration from a time instant when the turn-off signal is sent to the first switching module to a time instant when the first switching module is actually turned off. The first duration is a sum of the first time length and a quarter of a period of phase power corresponding to the first switching module.

**[0090]** In another embodiment, the preset electrical parameter is a voltage corresponding to a time instant determined by subtracting a second delay duration from the time instant when the current of the first switching module decreases to zero. The second delay duration includes a duration from a time instant when the turn-off signal is sent to the first switching module to the time instant when the first switching module is actually turned off, and a power-resistant duration from a time instant corresponding to the maximum impulse current withstood by the first switching module to the time instant when the current in the descending portion of the periodic current curve decreases to zero. The first duration is a sum of the first time length, a quarter of a period of phase power corresponding to the first switching module and two times of the power-resistant duration.

**[0091]** Further, the first time length is calculated by the following equation:

$$\Delta T = \frac{2\pi - \arcsin\left(\frac{V}{\sqrt{2}U}\right)}{2\pi} * \frac{1}{f}, \frac{3\pi}{2} < \arcsin\left(\frac{V}{\sqrt{2}U}\right) < 2\pi$$

**[0092]** where, U represents a rated voltage of the phase power corresponding to the first switching module, V represents a voltage of the phase power corresponding to the first switching module, and f represents a frequency of the phase power corresponding to the first switching module.

**[0093]** Further, after turning off the first switching module and the second switching module with the current that is currently zero simultaneously, the method further includes: turning off a switching module that is on among the switching modules connected to the inverter circuit upon monitoring that a current of the switching module is in the descending trend and the actual electrical parameter of the switching module reaches the preset electrical parameter.

**[0094]** In an embodiment, it is determined that the current of the first switching module is in the descending trend by: continuously acquiring multiple currents of the first switching module, and determining that the current of the first switching module is in the descending trend in response to the multiple currents of the first switching module in the descending trend; or determining that the current of the first switching module is in the descending trend upon determining that the periodic voltage curve of phase power corresponding to the first switching module is in the rising trend.

**[0095]** In an embodiment, a photovoltaic system is further provided according to the present disclosure. The photovoltaic system includes a photovoltaic string and an inverter. The photovoltaic string is connected to an input end of the inverter, and is configured to supply DC power to the inverter. An output end of the inverter is configured to connect a power grid, and convert DC power into alternating-current (AC) power and transmit the AC power to the power grid, where the inverter is at least one of the inverter according to any one of the embodiments described above or the inverter to which the method for turning off an inverter is applied described above.

**[0096]** A corresponding device and a computer storage medium are further provided according to embodiments of the present disclosure, for implementing the solutions according to the embodiments of the present disclosure.

**[0097]** The device includes a memory and a processor, the memory is configured to store an instruction or code, and the processor is configured to execute the instruction or code, so that the device performs the method for turning off the inverter according to any embodiment of the present disclosure.

**[0098]** The computer storage medium stores codes. The codes cause, when being executed by a device, the device to perform the method for turning off the inverter according to any embodiment of the present disclosure.

**[0099]** The expressions “first”, “second” (if any) and similar variant described in the embodiments of the present disclosure are used only for distinguish different names, rather than indicating the first or the second in a sequence.

**[0100]** From the descriptions of the above embodiments, those skilled in the art can clearly appreciate that all or a part of steps in the method according to the above embodiments may be implemented by means of software and a general hardware platform. Based on such understanding, technical solutions of the present disclosure may be embodied as a software product. The computer software product may be stored in a storage medium, such as a read-only memory (ROM)/RAM, a magnetic disc, or an optical disc, and the computer software product includes multiple instructions for enabling a computer device (which may be a personal computer, a server, or a network communication device such as a router) to perform the methods described in various embodiments or some parts of the embodiments of the present disclosure.

**[0101]** The embodiments are described in this specification in a progressive manner. Various embodiments may refer to each other for the same or similar parts, and each embodiment places emphasis on a difference from other embodiments. Especially, for the apparatus embodiments, since they are similar with the method embodiments, the description of the apparatuses is simple, and reference may be made to the relevant part of the method embodiments. Some or all of the modules may be selected as needed to achieve the purpose of the solution of the embodiments. Those skilled in the art can understand and implement the solution without any creative effort.

**[0102]** The foregoing descriptions are only exemplary embodiments of the present disclosure, and are not intended to limit the protection scope of the present disclosure.

1. An inverter, comprising:  
 an inverter circuit;  
 switching modules; and  
 a controller, wherein  
 an input end of the inverter circuit is configured to connect  
 a direct-current (DC) source, an output end of each  
 phase of the inverter circuit is connected to a corre-  
 sponding switching module among the switching mod-  
 ules, and output ends of the switching modules are  
 configured to connect a power grid; and  
 the controller is configured to:  
 perform pulse blocking on the inverter circuit in response  
 to a short circuit of a negative electrode of the DC  
 source to ground, wherein the pulse blocking comprises  
 disabling a drive pulse for each switching transistor in  
 the inverter circuit;  
 determine, upon determining that a current of a first  
 switching module is in a descending trend after the  
 inverter circuit is subjected to the pulse blocking,  
 whether a first electrical parameter of the first switching  
 module reaches a preset electrical parameter at a cur-  
 rent time instant, wherein the preset electrical param-  
 eter corresponds to a safe current of the first switching  
 module; and  
 turn off, in response to the first electrical parameter of the  
 first switching module reaching the preset electrical  
 parameter, the first switching module and a second  
 switching module with a current that is currently moni-  
 tored as zero simultaneously; or  
 turn off the first switching module and a second switching  
 module with a current that is currently zero simultane-  
 ously within a first duration starting from a time instant  
 when an actual electrical parameter of the first switch-  
 ing module reaches the preset electrical parameter,  
 wherein the first switching module and the second  
 switching module each are one of the switching mod-  
 ules.

2. The inverter according to claim 1, wherein for the  
 determining whether a first electrical parameter of the first  
 switching module reaches a preset electrical parameter, the  
 controller is configured to:  
 determine that the first electrical parameter of the first  
 switching module reaches the preset electrical param-  
 eter if the first electrical parameter is a current and the  
 first electrical parameter of the first switching module  
 is less than or equal to a first preset current; and  
 determine that the first electrical parameter of the first  
 switching module reaches the preset electrical param-  
 eter if the first electrical parameter is a voltage and the  
 first electrical parameter of the first switching module  
 is greater than or equal to a first preset voltage.

3. The inverter according to claim 2, wherein after the  
 determining whether a first electrical parameter of the first  
 switching module reaches a preset electrical parameter at a  
 current time instant, the controller is further configured to:  
 continuously monitor the current of the first switching  
 module if the first electrical parameter is the current  
 and the current of the first switching module is greater  
 than the first preset current, until it is monitored that the  
 current of the first switching module decreases to be  
 less than or equal to the first preset current; and  
 determine that the first electrical parameter of the first  
 switching module reaches the preset electrical param-  
 eter; or

continuously monitor a voltage of the first switching  
 module if the first electrical parameter is the voltage  
 and the voltage of the first switching module is less than  
 the first preset voltage, until it is monitored that the  
 voltage of the first switching module increases to be  
 greater than or equal to the first preset voltage; and  
 determine that the first electrical parameter of the first  
 switching module reaches the preset electrical param-  
 eter.

4. The inverter according to claim 3, wherein after the  
 turning off the first switching module and the second switch-  
 ing module simultaneously, the controller is further config-  
 ured to:

turn off a switching module that is on among the switch-  
 ing modules connected to the inverter circuit upon  
 monitoring that a current of the switching module is in  
 the descending trend and the first electrical parameter  
 of the switching module reaches the preset electrical  
 parameter.

5. The inverter according to claim 1, wherein the actual  
 electrical parameter reaching the preset electrical parameter  
 lies in that:

an actual current is less than or equal to the preset  
 electrical parameter.

6. The inverter according to claim 3, wherein a first time  
 length is a time length from a time instant when the current  
 of the first switching module decreases to zero to a nearest  
 time instant when the voltage of the first switching module  
 is zero, wherein

the preset electrical parameter is zero; the first duration is  
 a sum of the first time length and a quarter of a period  
 of phase power corresponding to the first switching  
 module;

the preset electrical parameter is a current corresponding  
 to a first time instant, the first time instant is a periodic  
 time instant determined by subtracting a first delay  
 duration from a time instant when a current in a  
 periodic current curve corresponding to the first switch-  
 ing module decreases to zero, the first delay duration  
 comprises a duration from a time instant when a  
 turn-off signal is sent to the first switching module to a  
 time instant when the first switching module is actually  
 turned off, and the first duration is a sum of the first  
 time length and a quarter of a period of phase power  
 corresponding to the first switching module; or

the preset electrical parameter is a current corresponding  
 to a second time instant, the second time instant is a  
 periodic time instant determined by subtracting a sec-  
 ond delay duration from a time instant when a current  
 in a periodic current curve corresponding to the first  
 switching module decreases to zero; the second delay  
 duration comprises a duration from a time instant when  
 a turn-off signal is sent to the first switching module to  
 a time instant when the first switching module is  
 actually turned off, and a power-resistant duration from  
 a time instant corresponding to a maximum impulse  
 current withstood by the first switching module to the  
 time instant when the current in a descending portion of  
 the periodic current curve decreases to zero; and the  
 first duration is a sum of the first time length, a quarter  
 of a period of phase power corresponding to the first  
 switching module and two times of the power-resistant  
 duration.

7. The inverter according to claim 1, wherein the actual electrical parameter reaching the preset electrical parameter lies in that:

an actual voltage is greater than or equal to the preset electrical parameter.

8. The inverter according to claim 7, wherein a first time length is a time length from a time instant when the current of the first switching module decreases to zero to a nearest time instant when a voltage of the first switching module is zero, wherein

the preset electrical parameter is a voltage corresponding to a time instant when the current of the first switching module decreases to zero; and the first duration is a sum of the first time length and a quarter of a period of phase power corresponding to the first switching module;

the preset electrical parameter is a voltage corresponding to a time instant determined by subtracting a first delay duration from a time instant when the current of the first switching module decreases to zero, the first delay duration comprises a duration from a time instant when a turn-off signal is sent to the first switching module to a time instant when the first switching module is actually turned off; and the first duration is a sum of the first time length and a quarter of a period of phase power corresponding to the first switching module; or

the preset electrical parameter is a voltage corresponding to a time instant determined by subtracting a second delay duration from a time instant when the current of the first switching module decreases to zero; the second delay duration comprises a duration from a time instant when a turn-off signal is sent to the first switching module to a time instant when the first switching module is actually turned off, and a power-resistant duration from a time instant corresponding to a maximum impulse current withstood by the first switching module to a time instant when the current in a descending portion of the periodic current curve decreases to zero; and the first duration is a sum of the first time length, a quarter of a period of phase power corresponding to the first switching module and two times of the power-resistant duration.

9. The inverter according to claim 6, wherein

the first time length is calculated by the following equation:

$$\Delta T = \frac{2\pi - \arcsin\left(\frac{V}{\sqrt{2}U}\right)}{2\pi} * \frac{1}{f}, \frac{3\pi}{2} < \arcsin\left(\frac{V}{\sqrt{2}U}\right) < 2\pi$$

wherein, U represents a rated voltage of the phase power corresponding to the first switching module, V represents a voltage of the phase power corresponding to the first switching module, and f represents a frequency of the phase power corresponding to the first switching module.

10. The inverter according to claim 8, wherein the first time length is calculated by the following equation:

$$\Delta T = \frac{2\pi - \arcsin\left(\frac{V}{\sqrt{2}U}\right)}{2\pi} * \frac{1}{f}, \frac{3\pi}{2} < \arcsin\left(\frac{V}{\sqrt{2}U}\right) < 2\pi$$

wherein, U represents a rated voltage of the phase power corresponding to the first switching module, V represents a voltage of the phase power corresponding to the first switching module, and f represents a frequency of the phase power corresponding to the first switching module.

11. The inverter according to claim 9, wherein after the turning off the first switching module and a second switching module with a current that is currently zero simultaneously, the controller is further configured to:

turn off a switching module that is on among the switching modules connected to the inverter circuit upon monitoring that a current of the switching module is in the descending trend and the actual electrical parameter of the switching module reaches the preset electrical parameter.

12. The inverter according to claim 10, wherein after the turning off the first switching module and a second switching module with a current that is currently zero simultaneously, the controller is further configured to:

turn off a switching module that is on among the switching modules connected to the inverter circuit upon monitoring that a current of the switching module is in the descending trend and the actual electrical parameter of the switching module reaches the preset electrical parameter.

13. The inverter according to claim 1, wherein for determining that a current of a first switching module is in a descending trend, the controller is further configured to:

continuously acquire a plurality of currents of the first switching module; and determine that the current of the first switching module is in the descending trend in response to the plurality of currents of the first switching module in the descending trend; or

determine that the current of the first switching module is in the descending trend upon determining that a periodic voltage curve of phase power corresponding to the first switching module is in a rising trend.

14. A method for turning off an inverter, wherein the inverter comprises: an inverter circuit and switching modules; an input end of the inverter circuit is configured to connect a direct-current (DC) source, an output end of each phase of the inverter circuit is connected to a corresponding switching module among the switching modules, and output ends of the switching modules are configured to connect a power grid, and the method comprises:

performing pulse blocking on the inverter circuit in response to a short circuit of a negative electrode of the DC source to ground, wherein the pulse blocking comprises disabling a drive pulse for each switching transistor in the inverter circuit; and

determining, upon determining that a current of a first switching module is in a descending trend after the inverter circuit is subjected to the pulse blocking, whether a first electrical parameter of the first switching

module reaches a preset electrical parameter at a current time instant, wherein the preset electrical parameter corresponds to a safe current of the first switching module; and  
turning off, in response to the first electrical parameter of the first switching module reaching the preset electrical parameter, the first switching module and a second switching module with a current that is currently monitored as zero simultaneously; or  
turning off the first switching module and a second switching module with a current that is currently zero simultaneously within a first duration starting from a time instant when an actual electrical parameter of the first switching module reaches the preset electrical parameter, wherein the first switching module and the second switching module each are one of the switching modules.

**15.** A photovoltaic system, comprising:

a photovoltaic string; and

an inverter, wherein

the photovoltaic string is connected to an input end of the inverter, and is configured to supply direct-current (DC) power to the inverter;

an output end of the inverter is configured to connect a power grid, convert DC power into alternating-current (AC) power, and transmit the AC power to the power grid; and

the inverter is at least one of the inverter according to claim 1.

\* \* \* \* \*