

US012388429B2

(12) United States Patent

Granger-Jones et al.

(54) GROUP DELAY DETERMINATION IN A COMMUNICATION CIRCUIT

(71) Applicant: Qorvo US, Inc., Greensboro, NC (US)

(72) Inventors: Marcus Granger-Jones, Scotts Valley, CA (US); Nadim Khlat, Cugnaux (FR)

(73) Assignee: Qorvo US, Inc., Greensboro, NC (US)

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35

U.S.C. 154(b) by 503 days.

(21) Appl. No.: 17/960,389

(22) Filed: Oct. 5, 2022

(65) Prior Publication Data

US 2023/0121439 A1 Apr. 20, 2023

Related U.S. Application Data

- (60) Provisional application No. 63/255,662, filed on Oct. 14, 2021.
- (51) Int. Cl. H03K 5/06 (2006.01) H03K 5/24 (2006.01) (Continued)

(Continued)

(10) Patent No.: US 12,388,429 B2

(45) **Date of Patent:** Aug. 12, 2025

(56) References Cited

U.S. PATENT DOCUMENTS

10,197,605 B2 * 2/2019 Quiquempoix G01R 23/165 2005/0036400 A1 * 2/2005 Chen G11C 7/1039 365/233.1

(Continued)

FOREIGN PATENT DOCUMENTS

EP 3070839 A1 9/2016 KR 101397548 B1 5/2014

OTHER PUBLICATIONS

Hussain, S., "Fast and Efficient Encoder with concurrent Bubble error correction for Flash ADC," International Journal of Modern Trends in Engineeringand Research, Jul. 2-4, 2015, Ijmter-2015, 9 pages.

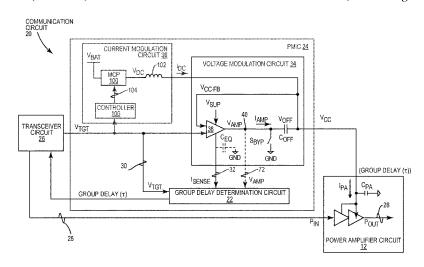
(Continued)

Primary Examiner — Ajibola A Akinyemi (74) Attorney, Agent, or Firm — Withrow & Terranova, P.L.L.C.

(57) ABSTRACT

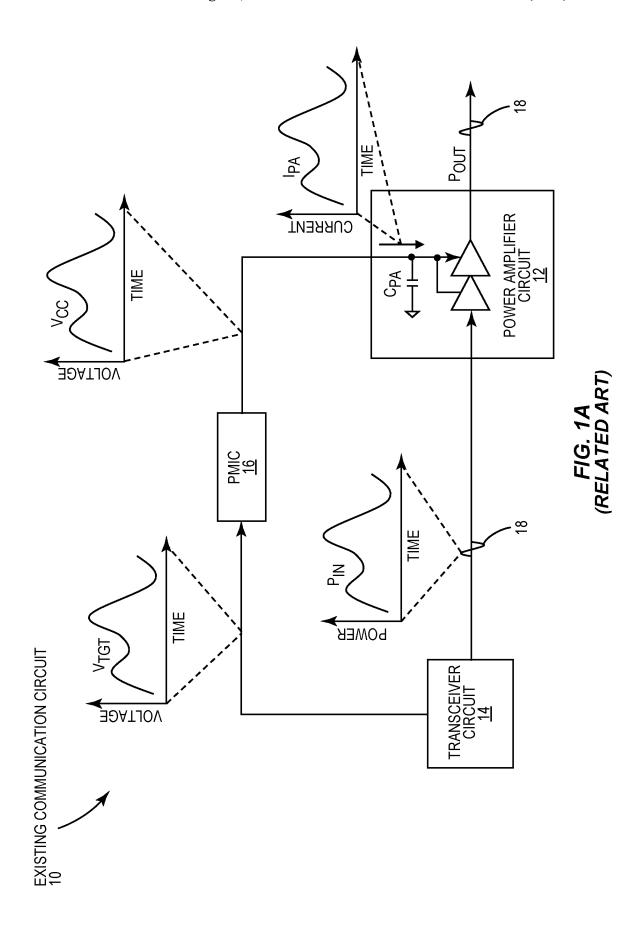
Group delay determination in a communication circuit is disclosed. The communication circuit includes a power amplifier circuit that amplifies a radio frequency (RF) signal based on a modulated voltage and a power management integrated circuit (PMIC) that generates the modulated voltage. Herein, the PMIC includes a group delay determination circuit to determine a relative group delay between the modulated voltage and a modulated current, which is internal to the power amplifier circuit and unknown to the PMIC, solely based on signals known to the PMIC. The determined relative group delay can help to time align the modulated voltage with the modulated current at the power amplifier circuit to improve error vector magnitude (EVM) and/or adjacent channel leakage ratio (ACLR). Further, by determining the relative group delay based on known signals to the PMIC, it is possible to achieve good time alignment between the modulated voltage and the modulated current.

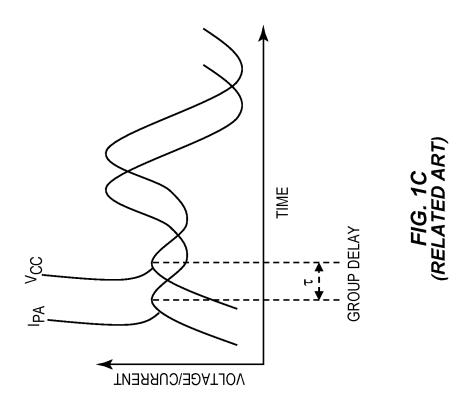
20 Claims, 9 Drawing Sheets

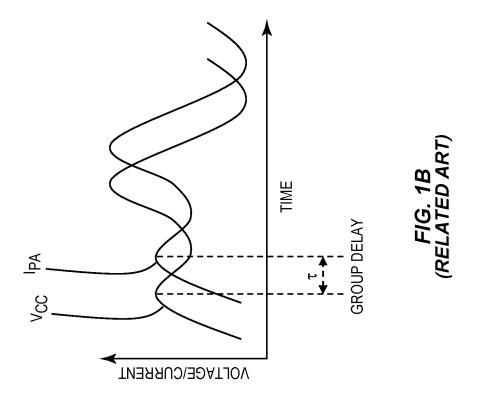


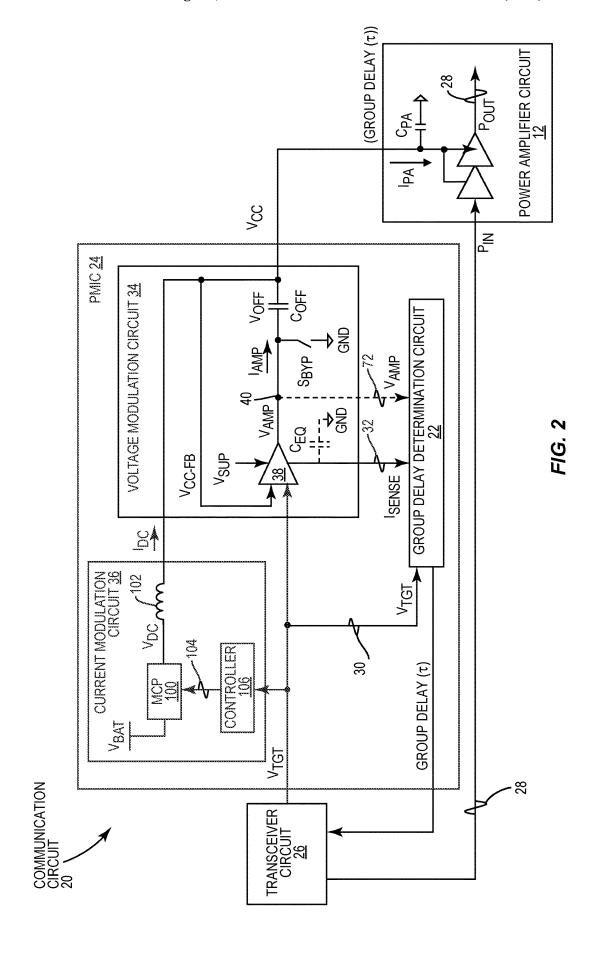
US 12,388,429 B2 Page 2

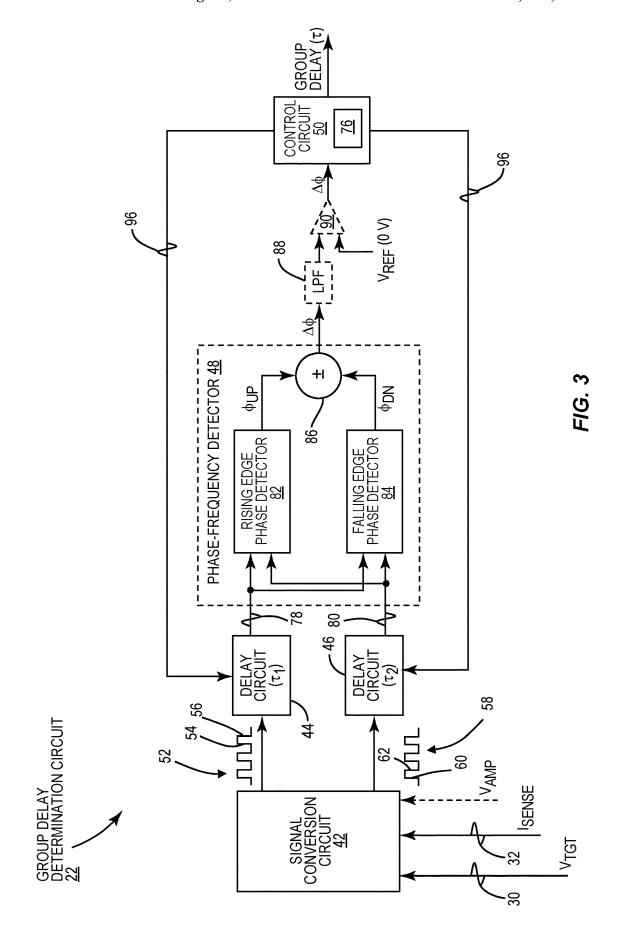
(51)	Int. Cl. H04B 1/40	(2015.01)	(56) References Cited		
	H03K 5/00	(2006.01)	U.S.	PATENT	DOCUMENTS
			2008/0242246 A1 2016/0365836 A1	10/2008 12/2016	Minnis et al. Khlat et al.
(58)	Field of Classification Search CPC		2020/0259685 A1 2023/0132888 A1	8/2020 5/2023	
			OTHER PUBLICATIONS Monticelli, D.M, "A quad CMOS single-supply op amp with rail-to-rail output swing," IEEE Journal of Solid-State Circuits, vol. 21, Issue 6, Dec. 1986, 9 pages. Pardhu, T. et al., "A low power flash ADC with Wallace tree encoder," 2014 Eleventh International Conference on Wireless and Optical Communications Networks (WOCN), Sep. 11-13, 2014, Vijayawada, India, IEEE, 4 pages. Extended European Search Report for European Patent Application No. 22201414.4, mailed Feb. 27, 2023, 10 pages. Extended European Search Report for European Patent Application No. 22205428.0, mailed Mar. 16, 2023, 11 pages.		
	See application f	* cited by examiner			

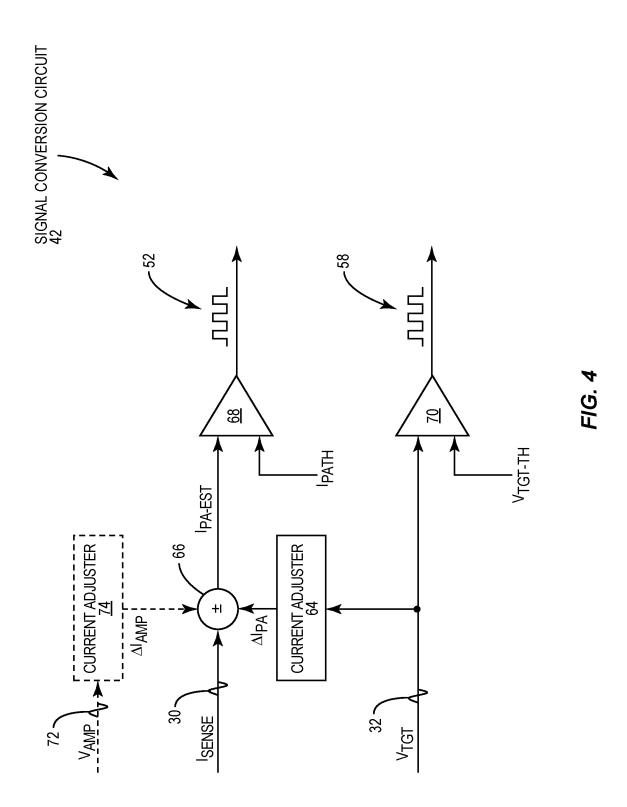


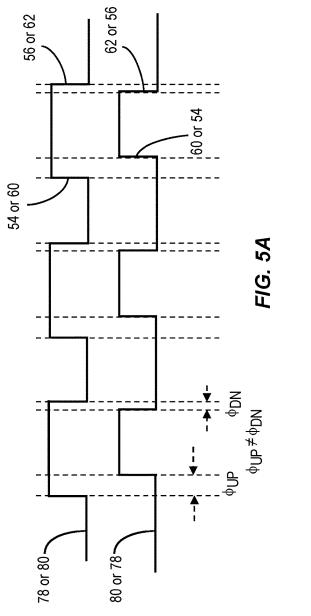


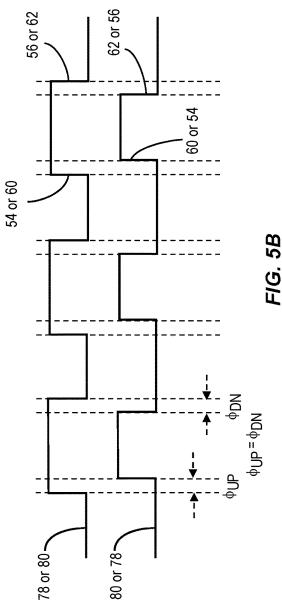


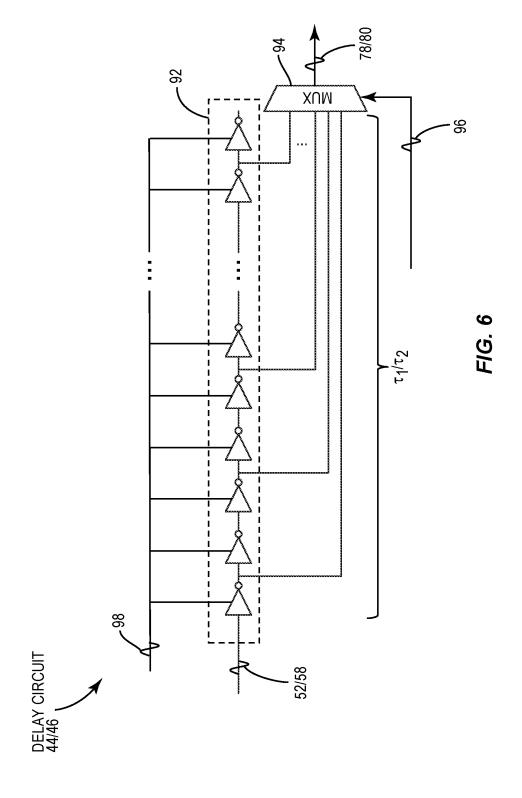




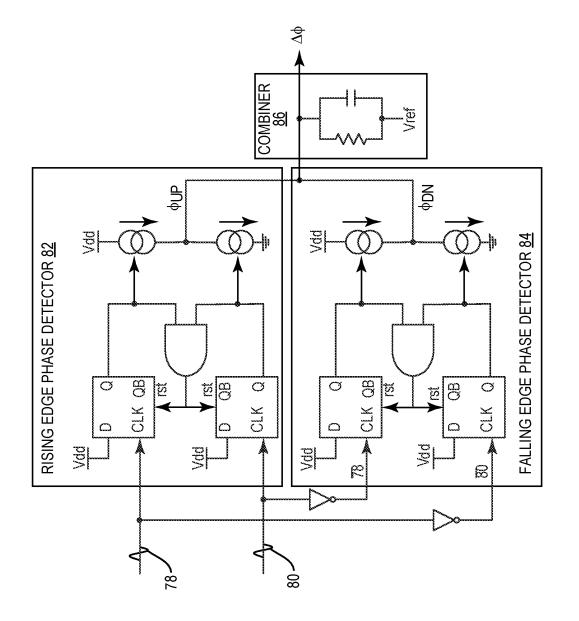






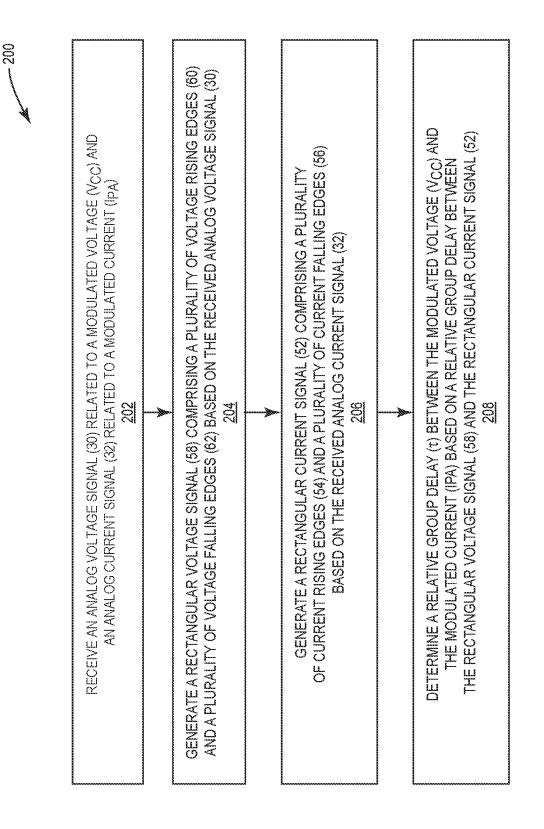


Aug. 12, 2025









F/G. 8

GROUP DELAY DETERMINATION IN A COMMUNICATION CIRCUIT

RELATED APPLICATIONS

This application claims the benefit of U.S. provisional patent application Ser. No. 63/255,662, filed on Oct. 14, 2021, the disclosure of which is hereby incorporated herein by reference in its entirety.

FIELD OF THE DISCLOSURE

The technology of the disclosure relates generally to determining a group delay in a communication circuit, such as a wireless transmission circuit.

BACKGROUND

Mobile communication devices have become increasingly common in current society for providing wireless communication services. The prevalence of these mobile communication devices is driven in part by the many functions that are now enabled on such devices. Increased processing capabilities in such devices means that mobile communication devices have evolved from being pure communication sophisticated mobile multimedia centers that enable enhanced user experiences.

A fifth-generation new radio (5G-NR) wireless communication system is widely regarded as a technological advancement that can achieve significantly higher data 30 throughput, improved coverage range, enhanced signaling efficiency, and reduced latency compared to the existing third generation (3G) and fourth generation (4G) communication systems. A 5G-NR mobile communication device usually transmits and receives a radio frequency (RF) 35 signal(s) in a millimeter wave (mmWave) RF spectrum that is typically above 6 GHz. Notably, the RF signal(s) transmitted in the mmWave RF spectrum may be more susceptible to propagation attenuation and interference that can result in substantial reduction in data throughput. To help 40 mitigate propagation attenuation and maintain desirable data throughput, the 5G-NR mobile communication device employs a power amplifier(s) to amplify the RF signal(s) before transmitting in the mmWave RF spectrum.

Envelope tracking (ET) and average power tracking 45 (APT) are power management techniques designed to improve operating efficiency of the power amplifier(s). Specifically, the power amplifier(s) is configured to amplify the RF signal(s) based on a modulated voltage (ET voltage or APT voltage) that closely tracks a time-variant power 50 envelope of the RF signal(s). The time-variant voltage is typically generated by a power management integrated circuit (PMIC) in the wireless communication device. Notably, the modulated voltage and the RF signal(s) may have experienced different group delays when arriving at the 55 power amplifier(s). Herein, a group delay refers generally to a sum of time delay experienced by a signal propagating through one or more active/passive circuits of different processing capabilities and/or operating frequencies. As a result, the modulated voltage may become misaligned with 60 the time-variant power envelope of the RF signal(s) at the power amplifier(s) to therefore cause a degraded error vector magnitude (EVM) and/or adjacent channel leakage ratio (ACLR) in the RF signal(s). In this regard, it is desirable to ensure that the PMIC can maintain good alignment between 65 the modulated voltage and the time-variant power envelope of the RF signal(s).

2 SUMMARY

Aspects disclosed in the detailed description include group delay determination in a communication circuit. The communication circuit includes a power amplifier circuit that amplifies a radio frequency (RF) signal based on a modulated voltage and a power management integrated circuit (PMIC) that generates the modulated voltage. Herein, the PMIC includes a group delay determination circuit that 10 is configured to determine a relative group delay between the modulated voltage and a modulated current, which is internal to the power amplifier circuit and unknown to the PMIC, solely based on signals (e.g., voltage, current, etc.) that are known to the PMIC. In an embodiment, the determined relative group delay can be used to time align the modulated voltage with the modulated current at the power amplifier circuit to thereby improve error vector magnitude (EVM) and/or adjacent channel leakage ratio (ACLR) of the RF signal. Further, by determining the relative group delay based on known signals to the PMIC, it is possible to achieve good time alignment between the modulated voltage and the modulated current.

In one aspect, a group delay determination circuit is provided. The group delay determination circuit includes a signal conversion circuit. The signal conversion circuit is configured to receive an analog voltage signal related to a modulated voltage and an analog current signal related to a modulated current. The signal conversion circuit is also configured to generate a rectangular voltage signal including multiple voltage rising edges and multiple voltage falling edges based on the received analog voltage signal. The signal conversion circuit is also configured to generate a rectangular current signal including multiple current rising edges and multiple current falling edges based on the received analog current signal and the received analog voltage signal. The group delay determination circuit also includes a control circuit. The control circuit is configured to determine a relative group delay between the modulated voltage and the modulated current based on a relative delay between the rectangular voltage signal and the rectangular current signal.

In another aspect, a communication circuit is provided. The communication circuit includes a power amplifier circuit. The power amplifier circuit is configured to amplify an RF signal associated with a time-variant input power based on a modulated voltage and induces a modulated current that tracks the time-variant input power of the RF signal. The communication circuit also includes a power amplifier integrated circuit (PMIC). The PMIC includes a voltage modulation circuit. The voltage modulation circuit is configured to generate the modulated voltage based on a modulated target voltage. The PMIC also includes a group delay determination circuit. The group delay determination circuit includes a signal conversion circuit. The signal conversion circuit is configured to receive an analog voltage signal related to the modulated voltage and an analog current signal related to the modulated current. The signal conversion circuit is also configured to generate a rectangular voltage signal including multiple voltage rising edges and multiple voltage falling edges based on the received analog voltage signal. The signal conversion circuit is also configured to generate a rectangular current signal including multiple current rising edges and multiple current falling edges based on the received analog current signal and the received analog voltage signal. The group delay determination circuit also includes a control circuit. The control circuit is configured to determine a relative group delay between the modulated

voltage and the modulated current based on a relative delay between the rectangular voltage signal and the rectangular current signal.

In another aspect, a method for determining a group delay in a communication circuit is provided. The method includes receiving an analog voltage signal related to a modulated voltage and an analog current signal related to a modulated current. The method also includes generating a rectangular voltage signal including multiple voltage rising edges and multiple voltage falling edges based on the received analog voltage signal. The method also includes generating a rectangular current signal including multiple current rising edges and multiple current falling edges based on the received analog current signal and the received analog voltage signal. The method also includes determining a relative group delay between the modulated voltage and the modulated current based on a relative delay between the rectangular voltage signal and the rectangular current signal.

Those skilled in the art will appreciate the scope of the disclosure and realize additional aspects thereof after readaccompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

The accompanying drawings incorporated in and forming 25 a part of this specification illustrate several aspects of the disclosure and, together with the description, serve to explain the principles of the disclosure.

FIG. 1A is a schematic diagram of an exemplary existing communication circuit wherein a modulated voltage and a modulated current can become time misaligned at a power amplifier circuit;

FIG. 1B is a graphic diagram providing an exemplary illustration of the modulated voltage leading the modulated

FIG. 1C is a graphic diagram providing an exemplary 35 illustration of the modulated voltage lagging behind the modulated current;

FIG. 2 is a schematic diagram of an exemplary communication circuit wherein a group delay determination circuit can be configured according to embodiments of the present 40 disclosure to determine a relative group delay between a modulated voltage and a modulated current, which is unknown to the group delay determination circuit, solely based on signals known to the group delay determination

FIG. 3 is a schematic diagram providing an exemplary illustration of the group delay determination circuit in FIG. 2 that is configured according to an embodiment of the present disclosure;

FIG. 4 is a schematic diagram illustrating a signal conversion circuit in the group delay determination circuit of 50 FIG. 3:

FIGS. 5A and 5B are graphic diagrams illustrating operations of the group delay determination circuit of FIG. 3;

FIG. 6 is a schematic diagram illustrating a delay circuit in the group delay determination circuit of FIG. 3;

FIG. 7 is a schematic diagram illustrating a phase-frequency detector in the group delay determination circuit of FIG. 3; and

FIG. 8 is a flowchart of an exemplary process that can be employed by the communication circuit of FIG. 2 for 60 determining the relative group delay between the modulated voltage and the modulated current.

DETAILED DESCRIPTION

The embodiments set forth below represent the necessary information to enable those skilled in the art to practice the

embodiments and illustrate the best mode of practicing the embodiments. Upon reading the following description in light of the accompanying drawing figures, those skilled in the art will understand the concepts of the disclosure and will recognize applications of these concepts not particularly addressed herein. It should be understood that these concepts and applications fall within the scope of the disclosure and the accompanying claims.

It will be understood that, although the terms first, second, etc. may be used herein to describe various elements, these elements should not be limited by these terms. These terms are only used to distinguish one element from another. For example, a first element could be termed a second element, and, similarly, a second element could be termed a first element, without departing from the scope of the present disclosure. As used herein, the term "and/or" includes any and all combinations of one or more of the associated listed items.

It will be understood that when an element such as a layer, ing the following detailed description in association with the 20 region, or substrate is referred to as being "on" or extending "onto" another element, it can be directly on or extend directly onto the other element or intervening elements may also be present. In contrast, when an element is referred to as being "directly on" or extending "directly onto" another element, there are no intervening elements present. Likewise, it will be understood that when an element such as a layer, region, or substrate is referred to as being "over" or extending "over" another element, it can be directly over or extend directly over the other element or intervening elements may also be present. In contrast, when an element is referred to as being "directly over" or extending "directly over" another element, there are no intervening elements present. It will also be understood that when an element is referred to as being "connected" or "coupled" to another element, it can be directly connected or coupled to the other element or intervening elements may be present. In contrast, when an element is referred to as being "directly connected" or "directly coupled" to another element, there are no intervening elements present.

> Relative terms such as "below" or "above" or "upper" or "lower" or "horizontal" or "vertical" may be used herein to describe a relationship of one element, layer, or region to another element, layer, or region as illustrated in the Figures. It will be understood that these terms and those discussed above are intended to encompass different orientations of the device in addition to the orientation depicted in the Figures.

The terminology used herein is for the purpose of describing particular embodiments only and is not intended to be limiting of the disclosure. As used herein, the singular forms "a," "an," and "the" are intended to include the plural forms as well, unless the context clearly indicates otherwise. It will be further understood that the terms "comprises," "comprising," "includes," and/or "including" when used herein specify the presence of stated features, integers, steps, 55 operations, elements, and/or components, but do not preclude the presence or addition of one or more other features, integers, steps, operations, elements, components, and/or groups thereof.

Unless otherwise defined, all terms (including technical and scientific terms) used herein have the same meaning as commonly understood by one of ordinary skill in the art to which this disclosure belongs. It will be further understood that terms used herein should be interpreted as having a meaning that is consistent with their meaning in the context of this specification and the relevant art and will not be interpreted in an idealized or overly formal sense unless expressly so defined herein.

Aspects disclosed in the detailed description include group delay determination in a communication circuit. The communication circuit includes a power amplifier circuit that amplifies a radio frequency (RF) signal based on a modulated voltage and a power management integrated circuit (PMIC) that generates the modulated voltage. Herein, the PMIC includes a group delay determination circuit that is configured to determine a relative group delay between the modulated voltage and a modulated current, which is internal to the power amplifier circuit and unknown to the PMIC, solely based on signals (e.g., voltage, current, etc.) that are known to the PMIC. In an embodiment, the determined relative group delay can be used to time align the modulated voltage with the modulated current at the power amplifier circuit to thereby improve error vector magnitude (EVM) and/or adjacent channel leakage ratio (ACLR) of the RF signal. Further, by determining the relative group delay based on known signals to the PMIC, it is possible to achieve good time alignment between the modulated voltage and the modulated current.

Before discussing group delay determination of the present disclosure, starting at FIG. 2, a brief overview of an existing communication circuit that may experience a group delay between a modulated voltage and a modulated current is first provided with reference to FIGS. 1A-1C.

FIG. 1A is a schematic diagram of an exemplary existing communication circuit 10 wherein a modulated voltage V_{CC} and a modulated current I_{P4} can become time misaligned at a power amplifier circuit 12. The existing communication circuit 10 also includes a transceiver circuit 14 and a PMIC 30 16

The transceiver circuit **14** is configured to generate an RF signal 18 having a time-variant input power P_{IN} and provide the RF signal 18 to the power amplifier circuit 12. The transceiver circuit 14 also generates a modulated target 35 voltage V_{TGT} that tracks the time-variant input power P_{IN} and provides the modulated target voltage \mathbf{V}_{TGT} to the PMIC 16. The PMIC 16 is configured to generate a modulated voltage \mathbf{V}_{CC} that tracks the modulated target voltage \mathbf{V}_{TGT} and provides the modulated voltage $V_{\it CC}$ to the power 40 amplifier circuit 12. Herein, the modulated target voltage \mathbf{V}_{TGT} and the modulated voltage \mathbf{V}_{CC} are time-variant voltages that are so generated (a.k.a. modulated) in accordance with the time-variant input power P_{IN}. Understandably, the transceiver circuit 14 may control (a.k.a. adjust) relative 45 timing between the modulated target voltage \mathbf{V}_{TGT} and the RF signal 18 by delaying/advancing one or more of the modulated target voltage V_{TGT} and the RF signal 18.

The power amplifier circuit 12 is configured to amplify the RF signal 18 from the time-variant input power P_{IN} to a 50 time-variant output power Pour based on the modulated voltage V_{CC} . Notably, the power amplifier circuit 12 often includes a load capacitor C_{Pd} to help improve impedance matching between the power amplifier circuit 12 and the PMIC 16. The load capacitor C_{Pd} , however, can cause a 55 modulated current I_{Pd} that closely resembles the time-variant input power P_{IN} of the RF signal 18. Herein, the modulated current I_{Pd} is a time-variant current that varies according to the time-variant input power P_{IN} of the RF signal 18.

The modulated voltage V_{CC} and the modulated current I_{PA} are typically monotonically related. However, since the modulated voltage V_{CC} is provided by the PMIC ${\bf 16}$ and the modulated current I_{PA} is induced internally in the power amplifier circuit ${\bf 12}$, the modulated voltage V_{CC} and the modulated current I_{PA} can experience different group delays at the power amplifier circuit ${\bf 12}$. As a result, the modulated

6

voltage $V_{\it CC}$ and the modulated current $I_{\it Pd}$ can become misaligned at the power amplifier circuit 12.

FIGS. 1B and 1C illustrate two scenarios where the modulated voltage V_{CC} and the modulated current I_{PA} are misaligned at the power amplifier circuit 12. Specifically, FIG. 1B shows that the modulated voltage V_{CC} is ahead of (a.k.a. leading) the modulated current I_{PA} by a relative group delay τ and FIG. 1C shows that the modulated voltage V_{CC} is behind of (a.k.a. trailing) the modulated current I_{PA} by the relative group delay τ .

With reference back to FIG. 1A, the relative group delay τ can cause distortion (e.g., amplitude clipping) in the RF signal 18, which can further lead to a degraded EVM and/or ACLR in the RF signal 18. In this regard, it is desirable to eliminate the relative group delay τ between the modulated voltage V_{CC} and the modulated current I_{E4} . Moreover, to be able to eliminate the relative group delay τ , it is necessary to first measure the relative group delay τ between the modulated voltage V_{CC} and the modulated current I_{E4} .

Conventionally, the relative group delay τ is measured at the power amplifier circuit 12 with a calibration/test equipment of some sort. This proves to be a challenging task given the fact that the existing communication circuit 10 often employs multiple power amplifier circuits made by different vendors. In this regard, it is further desirable to determine the relative group delay τ without complexity associated with the conventional approach.

FIG. 2 is a schematic diagram of an exemplary communication circuit 20, wherein a group delay determination circuit 22 in a PMIC 24 is configured according to embodiments of the present disclosure to determine a relative group delay τ between a modulated voltage V_{CC} and a modulated current I_{E4} solely based on signals available in the PMIC 24. By determining the relative group delay τ inside the PMIC 24 based solely on the signals available in the PMIC 24, it is possible to eliminate the complexity associated with the conventional approach of determining the relative group delay τ in the existing communication circuit 10 of FIG. 1A. As a result, it is possible to drop the PMIC 24 into the communication circuit 20 to work with any power amplifier circuit of any vendor, such as the power amplifier circuit 12 in FIG. 1A.

In a non-limiting example, the communication circuit 20 includes a transceiver circuit 26 and the power amplifier circuit 12 in FIG. 1A. Notably, the power amplifier circuit 12 is provided herein to simply illustrate the fact that the PMIC 24 can operate with any power amplifier circuit of any vendor, including but not limited to the power amplifier circuit 12 in the existing communication circuit of FIG. 1A.

The transceiver circuit **26** is configured to generate an RF signal **28** associated with a time-variant input power P_{IN} and the power amplifier circuit **12** is configured to amplify the RF signal **28** from the time-variant input power to a time-variant output power Pour based on the modulated voltage V_{CC} . As previously explained in FIG. **1A**, the power amplifier circuit **12** can induce the modulated current I_{EA} that can be misaligned from the modulated voltage V_{CC} by the relative group delay τ . Moreover, as illustrated in FIGS. **1B** and **1C**, the modulated voltage V_{CC} can either lead or trail behind the modulated current I_{EA} by the relative group delay τ .

Given that the modulated current I_{PA} is induced inside the power amplifier circuit 12, the PMIC 24 would therefore have no direct knowledge about the modulated current I_{PA} . In addition, the PMIC 24 may also have no knowledge about the modulated voltage V_{CC} as received by the power amplifier circuit 12. As such, the group delay determination circuit

22 needs to estimate the relative group delay τ solely based on signals that are available in the PMIC 24.

In an embodiment, the group delay determination circuit 22 is configured to estimate the relative group delay τ based on at least an analog voltage signal 30 that is related to the 5 modulated voltage $V_{\it CC}$ and an analog current signal 32 that is related to the modulated current I_{PA} . The analog voltage signal 30 and the analog current signal 32 are either generated inside the PMIC 24 or provided to the PMIC 24 from outside the PMIC 24. In this regard, the group delay deter- 10 mination circuit 22 is able to determine the relative group delay τ independent of the power amplifier circuit 12.

In an embodiment, the PMIC 24 includes a voltage modulation circuit 34 and a current modulation circuit 36. The voltage modulation circuit 34 includes a voltage ampli- 15 fier 38, an offset capacitor C_{OFF} , and a bypass switch S_{BYP} . The voltage amplifier 38 is configured to generate a modulated initial voltage $V_{A\!M\!P}$ based on a modulated target voltage $V_{\textit{TGT}}$, which is generated by the transceiver circuit **26** to track the time-variant input power P_{IN} of the RF signal 20 **28**, and a supply voltage V_{SUP} .

The offset capacitor C_{OFF} and the bypass switch S_{BYP} are both coupled to an output 40 of the voltage amplifier 38. The offset capacitor C_{OFF} is configured to raise the modulated initial voltage $V_{A\!M\!P}$ by an offset voltage $V_{O\!F\!F}$ to thereby generate the modulated voltage $V_{\it CC}$ ($V_{\it CC}$ = $V_{\it AMP}$ + $V_{\it OFF}$). In an embodiment, the offset voltage $V_{\it OFF}$ can be modulated by charging or discharging the offset capacitor $\mathbf{C}_{O\!F\!F}.$ For a specific example as to how the offset voltage $\mathbf{V}_{O\!F\!F}$ can be modulated to raise the modulated initial voltage $V_{A\!M\!P}$ to the 30 modulated voltage V_{CC} , please refer to U.S. patent application Ser. No. 17/946,224, entitled "MULTI-VOLTAGE GENERATION CIRCUIT" (hereinafter "Application224").

Notably, while the offset capacitor C_{OFF} is being charged slow depending on the size of the offset capacitor C_{OFF} , the voltage modulation circuit 34 must maintain the modulated voltage V_{CC} at a desired level. In this regard, the voltage amplifier 38 may source or sink a high-frequency current I_{AMP} (e.g., an alternating current) to allow the load capacitor 40 C_{PA} , which is much smaller than the offset capacitor C_{OFF} , to be quickly charged or discharged to maintain the modulated voltage $V_{\it CC}$. In this regard, the high-frequency current I_{AMP} is similar to the modulated current I_{PA} and can thus be utilized to represent the modulated current I_{Pd} in the power 45 load capacitor C_{Pd} in the power amplifier circuit 12 in FIG. amplifier circuit 12.

In an embodiment, the voltage amplifier 38 may generate a sensed current I_{SENSE} to proportionally represent the highfrequency current I_{AMP} . In a non-limiting example, the sensed current I_{SENSE} is inversely related to the high-fre- 50 quency current I_{AMP} by a scaling factor k (k>100). As such, the sensed current I_{SENSE} is smaller than the high-frequency current I_{AMP} .

On another hand, since the voltage modulation circuit 34 is configured to generate the modulated voltage $V_{\it CC}$ based $\,$ 55 $\,$ on the modulated target voltage $\mathbf{V}_{\mathit{TGT}}\!,$ the modulated voltage $V_{\it CC}$ will be substantially similar to the modulated voltage V_{TGT} . Accordingly, the modulated target voltage V_{TGT} can be utilized to represent the modulated voltage V_{CC} as received at the power amplifier circuit 12.

In this regard, according to an embodiment of the present disclosure, the group delay determination circuit 22 is configured to receive the modulated target voltage V_{TGT} as the analog voltage signal 30 and the sensed current $I_{\mbox{\scriptsize SENSE}}$ as the analog current signal 32. Accordingly, as described below in FIG. 3, the group delay determination circuit 22 is able to determine the relative group delay τ between the modulated

8

voltage V_{CC} and the modulated current I_{PA} by determining the relative group delay τ between the modulated target voltage V_{TGT} and the sensed current I_{SENSE} .

FIG. 3 is a schematic diagram providing an exemplary illustration of the group delay determination circuit 22 in FIG. 2 according to an embodiment of the present disclosure. Common elements between FIGS. 2 and 3 are shown therein with common element numbers and will not be re-described herein.

Herein, the group delay determination circuit 22 includes a signal conversion circuit 42, a first delay circuit 44, a second delay circuit 46, a phase-frequency detector 48, and a control circuit 50. The signal conversion circuit 42 receives the analog voltage signal 30 (e.g., the modulated target voltage V_{TGT}) and the analog current signal 32 (e.g., the sensed current I_{SENSE}). As is further described in FIG. 4 below, the signal conversion circuit 42 is configured to generate a rectangular current signal 52 (a.k.a. pulse signal), which includes multiple current rising edges 54 and multiple current falling edges 56, based on the analog voltage signal 30. The signal conversion circuit 42 is also configured to generate a rectangular voltage signal 58 (a.k.a. pulse signal), which includes multiple voltage rising edges 60 and multiple voltage falling edges 62, based on the received analog current signal 32 and the received analog voltage signal 30.

FIG. 4 is a schematic diagram illustrating the signal conversion circuit 42 in the group delay determination circuit 22 of FIG. 3 according to an embodiment of the present disclosure. Common elements between FIGS. 3 and 4 are shown therein with common element numbers and will not be re-described herein.

Herein, the signal conversion circuit 42 includes a current adjuster 64, a current combiner 66, a first comparator 68, and a second comparator 70. The current adjuster 64 is configor discharged toward the offset voltage V_{OFF} , which may be 35 ured to estimate a differential ΔI_{PA} between the modulated current I_{PA} and the analog current signal 32, which is equivalent to the sensed current I_{SENSE} , based on the analog voltage signal 30 that is equivalent to the modulated target voltage V_{TGT} . In a non-limiting example, the current adjuster 64 can estimate the differential ΔI_{PA} based on equation (Eq. 1) below.

$$\Delta I_{PA} = C_{PA}/(k*dV_{TGT}/dt) \tag{Eq. 1}$$

In the equation (Eq. 1), C_{PA} represents a capacitance of the 2 and k (k>1) represents the scaling factor between the sensed current I_{SENSE} and the high-frequency current I_{AMP} . Understandably, the differential ΔI_{PA} can be either positive or negative. The current combiner 66 is configured to combine the analog current signal 32 with the estimated differential ΔI_{PA} to generate an estimation I_{PA-EST} that can more accurately represent the modulated current I_{PA} .

The first comparator 68 is configured to generate the rectangular current signal 52 based on the estimation I_{PA-EST} and a predefined current threshold I_{PA-TH} . The second comparator 70 is configured to generate the rectangular voltage signal 58 based on the analog voltage signal 30 and a predefined voltage threshold $V_{TGT\text{-}TH}$. In an embodiment, the predefined current threshold $I_{PA\text{-}TH}$ and the predefined voltage threshold $V_{\mathit{TGT-TH}}$ may be determined to provide a highest possible sensitivity to accurately detect the current rising edges 54, the current falling edges 56, the voltage rising edges 60, and the voltage falling edges 62.

With reference back to FIG. 2, the voltage amplifier 38 may include such components (e.g., switches) that can cause a parasitic capacitance $\mathbf{C}_{\!\mathit{EQ}}$ that can interact with the modulated initial voltage V_{AMP} to potentially impact the high-

frequency current I_{AMP} and, therefore, the sensed current I_{SENSE} . In this regard, to ensure that the high-frequency current LAMP, and accordingly the sensed current I_{SENSE} , can accurately represent the modulated current I_{PA} , it is desirable to further take into consideration the parasitic 5 capacitance C_{EQ} in the determination of the relative group delay τ .

In this regard, the group delay determination circuit 22 may be further configured to receive a second analog voltage signal 72. In an embodiment, the second analog voltage signal 72 is the modulated initial voltage V_{AMP} generated by the voltage amplifier 38.

With reference to FIG. 4, the signal conversion circuit 42 may further include a second current adjuster 74 to estimate an adjustment term ΔI_{AMP} to the analog current signal 32 based on the second analog voltage signal 72. In a non-limiting example, the second current adjuster 74 can estimate the adjustment term ΔI_{AMP} based on equation (Eq. 2) below.

$$\Delta I_{AMP} = C_{EQ}/(k*dV_{AMP}/dt) \tag{Eq. 2}$$

In the equation (Eq. 2), C_{EQ} represents the parasitic capacitance of the voltage amplifier $\bf 38$ in the power amplifier circuit $\bf 12$ in FIG. 2 and k (k>1) represents the scaling factor between the sensed current I_{SENSE} and the high-frequency current I_{AMP} . Accordingly, the current combiner $\bf 66$ is configured to combine the analog current signal $\bf 32$ with the estimated differential ΔI_{PA} and the estimated adjustment term ΔI_{AMP} to generate the estimation I_{PA-EST} . Understandably, by further taking into consideration of the parasitic capacitance C_{EQ} , the estimation I_{PA-EST} can represent the modulated current I_{PA} with further improved accuracy.

With reference back to FIG. 3, notably when the modulated voltage V_{CC} and the modulated current $I_{E\!A}$ are misaligned by the relative group delay τ , the rectangular current 35 signal 52 and the rectangular voltage signal 58 will be out of phase as well. As such, it is necessary to first make sure that the modulated target voltage V_{TGT} and the sensed current I_{SENSE} are in phase before determining the relative group delay τ .

In an embodiment, the control circuit 50 is configured to dynamically delay the rectangular current signal 52 and/or the rectangular voltage signal 58 to thereby cause the rectangular current signal 52 to be in-phase with the rectangular voltage signal 58. Once the rectangular current 45 signal 52 and the rectangular voltage signal 58 become in phase, the control circuit 50 can then determine the relative group delay τ between the rectangular current signal 52 and the rectangular voltage signal 58.

In a non-limiting example, the control circuit **50** can 50 include a processor **76** (e.g., a digital signal processor) to dynamically control the first delay circuit **44** to delay the rectangular current signal **52** and/or control the second delay circuit **46** to delay the rectangular voltage signal **58**. More specifically, the control circuit **50** can control the first delay 55 circuit **44** to delay the rectangular current signal **52** by a first adjustable delay τ_1 to generate a delayed rectangular current signal **78** and/or control the second delay circuit **46** to delay the rectangular voltage signal **58** by a second adjustable delay **12** to generate a delayed rectangular voltage signal **80**. 60

Understandably, the delayed rectangular current signal 78 is essentially the same as the rectangular current signal 52, except for a difference in a relative phase. As such, the delayed rectangular current signal 78 will also include the current rising edges 54 and the current falling edges 56. 65 Likewise, the delayed rectangular voltage signal 80 is essentially the same as the rectangular voltage signal 58, except

10

for a difference in a relative phase. As such, the delayed rectangular voltage signal 80 will also include the voltage rising edges 60 and the voltage falling edges 62.

The phase-frequency detector 48 is configured to determine a phase differential $\Delta \varphi$ between the delayed rectangular current signal 78 and the delayed rectangular voltage signal 80. According to an embodiment of the present disclosure, the control circuit 50 can determine that the delayed rectangular current signal 78 and the delayed rectangular voltage signal 80 are in phase when the phase differential $\Delta \varphi$ between the delayed rectangular current signal 78 and the delayed rectangular voltage signal 80 is equal to zero ($\Delta \approx 0$).

In an embodiment, the phase-frequency detector **48** can include a rising edge phase detector **82**, a falling edge phase detector **84**, and a combiner **86**. The rising edge phase detector **82** is configured to detect a rising edge phase offset ϕ_{UP} between each of the current rising edges **54** and a respective one of the voltage rising edges **60**. The falling edge phase detector **84** is configured to detect a falling edge phase offset ϕ_{DN} between each of the current falling edges **56** and a respective one of the voltage falling edges **62**. The combiner **86** is configured to subtract the falling edge phase offset ϕ_{DN} from the rising edge phase offset ϕ_{UP} to generate the phase differential $\Delta \phi$, as shown in equation (Eq. 3) below

$$\Delta \phi = \phi_{UP} - \phi_{DN} \tag{Eq. 3}$$

FIGS. 5A and 5B are graphic diagrams providing exemplary illustrations as to how the group delay determination circuit 22 of FIG. 3 can phase align the delayed rectangular current signal 78 and the delayed rectangular voltage signal 80. Common elements between FIGS. 3 and 5A-5B are shown therein with common element numbers and will not be re-described herein.

FIG. **5**A provides a visual illustration of the delayed rectangular current signal **78** and the delayed rectangular voltage signal **80** that are out of phase. Regardless of whether the delayed rectangular current signal **78** is ahead of the delayed rectangular voltage signal **80** or behind the delayed rectangular voltage signal **80**, the rising edge phase offset ϕ_{UP} is different from the falling edge phase offset ϕ_{DN} . As a result, according to equation (Eq. 3), the phase differential $\Delta \phi$ will not be equal to zero.

FIG. **5**B provides a visual illustration of the delayed rectangular current signal **78** and the delayed rectangular voltage signal **80** that are in phase. Herein, regardless of whether the delayed rectangular current signal **78** is ahead of the delayed rectangular voltage signal **80** or behind the delayed rectangular voltage signal **80**, the rising edge phase offset ϕ_{UP} is equal to the falling edge phase offset ϕ_{DN} . As a result, according to equation (Eq. 3), the phase differential $\Delta \phi$ will be equal to zero.

With reference back to FIG. 3, the group delay determination circuit 22 may further include a lowpass filter (LPF) 88 and a comparator 90. The comparator 90 may operate based on a reference voltage V_{REF} (e.g., 0 V) to help ensure that the phase differential $\Delta \phi$ is equal to zero when the phase differential $\Delta \phi$ is substantially close to zero (e.g., <0.01).

When the phase differential $\Delta \varphi$ is equal to zero, the control circuit **50** may determine the relative group delay τ between the rectangular current signal **52** and the rectangular voltage signal **58** based on equation (Eq. 4) below.

$$\tau = \tau_1 - \tau_2 + \tau_{ADJ} \tag{Eq. 4}$$

In the equation (Eq. 4), τ_1 represents the first adjustable delay introduced by the first delay circuit **44**, τ_2 represents the second adjustable delay introduced by the second delay

circuit 46, and τ_{ADJ} represents a predefined temporal offset that compensates for any estimation error. In an embodiment, the control circuit 50 may provide the determined relative group delay τ to the transceiver circuit 26 in FIG. 2 such that the transceiver circuit 26 can delay or advance the RF signal 28 based on the determined relative group delay τ to thereby ensure that the modulated current I_{PA} is aligned with the modulated voltage V_{CC} at the power amplifier circuit 12.

FIG. 6 is a schematic diagram illustrating an exemplary 10 implementation of the first delay circuit 44 and the second delay circuit 46 in the group delay determination circuit 22 of FIG. 3. Common elements between FIGS. 3 and 6 are shown therein with common element numbers and will not be re-described herein.

In an embodiment, each of the first delay circuit 44 and the second delay circuit 46 can include a respective delay line 92 and a respective multiplexer 94. The multiplexer 94 may be controlled by the control circuit 50 in FIG. 5 via a control signal **96** to selectively delay the rectangular current 20 signal 52 by the first adjustable delay ti or the rectangular voltage signal 58 by the second adjustable delay 12. In an embodiment, the delay line 92 may be calibrated by a calibration signal 98.

FIG. 7 is a schematic diagram illustrating an exemplary 25 implementation of the phase-frequency detector 48 in the group delay determination circuit 22 of FIG. 3. Common elements between FIGS. 3 and 7 are shown therein with common element numbers and will not be re-described

With reference back to FIG. 2, the current modulation circuit 36 includes a multi-level charge pump (MCP) 100 and a power inductor 102. The MCP 100, which can be a buck-boost direct-current (DC) to DC (DC-DC) converter, is configured to generate a low-frequency voltage V_{DC} (e.g., a 35 wherein the control circuit is further configured to: DC voltage) as a function of a battery voltage V_{BAT} . Specifically, the MCP 100 may operate in a buck mode to generate the low-frequency voltage V_{DC} at $0 \times V_{BAT}$ (0 V) or $1 \times V_{BAT}$, or in a boost mode to generate the low-frequency voltage V_{DC} at $2\times V_{BAT}$. In addition, the MCP 100 may 40 toggle between $0 \times V_{BAT}(0 \text{ V})$, $1 \times V_{BAT}$, and/or $2 \times V_{BAT}$ based on a duty cycle 104 to thereby generate the low-frequency voltage V_{DC} at a desired voltage level. In a non-limiting example, the current modulation circuit 36 can include a controller 106 (e.g., a microcontroller or a microprocessor) that determines the duty cycle 104 based on the modulated target voltage V_{TGT}

The power inductor 102 is configured to induce a lowfrequency current IDC based on the low-frequency voltage ${
m V}_{DC}$. In an embodiment and as further described in Appli- 50 cation 244, the low-frequency current I_{DC} is configured to modulate the offset voltage $\mathbf{V}_{O\!F\!F}$ across the offset capacitor

C_{OFF}.

The communication circuit **20** of FIG. **2** can be configured to support group delay determination as described above 55 based on a process. In this regard, FIG. 8 is a flowchart of an exemplary process 200 determining the group delay τ in the communication circuit 20 of FIG. 2.

Herein, the group delay determination circuit 22 receives the analog voltage signal 30 that is related to the modulated 60 voltage \mathbf{V}_{CC} and the analog current signal 32 that is related to the modulated current I_{PA} (step 202). Next, the group delay determination circuit 22 generates the rectangular voltage signal 58 having the voltage rising edges 60 and the voltage falling edges 62 based on the received analog voltage signal 30 (step 204). The group delay determination circuit 22 also generates the rectangular current signal 52

12

having the current rising edges 54 and the current falling edges 56 based on the received analog current signal 32 (step 206). Accordingly, the group delay determination circuit 22 determines the relative group delay τ between the modulated voltage \mathbf{V}_{CC} and the modulated current $\mathbf{I}_{P\!A}$ based on the relative group delay τ between the rectangular voltage signal 58 and the rectangular current signal 52 (step 208).

Those skilled in the art will recognize improvements and modifications to the embodiments of the present disclosure. All such improvements and modifications are considered within the scope of the concepts disclosed herein and the claims that follow.

What is claimed is:

- 1. A group delay determination circuit comprising:
- a signal conversion circuit configured to:
 - receive an analog voltage signal related to a modulated voltage and an analog current signal related to a modulated current;
 - generate a rectangular voltage signal comprising a plurality of voltage rising edges and a plurality of voltage falling edges based on the received analog voltage signal; and
 - generate a rectangular current signal comprising a plurality of current rising edges and a plurality of current falling edges based on the received analog current signal and the received analog voltage signal; and
- a control circuit configured to determine a relative group delay between the modulated voltage and the modulated current based on a relative delay between the rectangular voltage signal and the rectangular current signal.
- 2. The group delay determination circuit of claim 1,
 - dynamically delay at least one of the rectangular voltage signal and the rectangular current signal to thereby cause the rectangular voltage signal to be in-phase with the rectangular current signal; and
 - determine the relative group delay between the rectangular voltage signal and the rectangular current signal when the rectangular voltage signal is in-phase with the rectangular current signal.
- 3. The group delay determination circuit of claim 2, 45 further comprising:
 - a first delay circuit configured to delay the rectangular current signal by a first adjustable delay to generate a delayed rectangular current signal comprising the plurality of current rising edges and the plurality of current falling edges;
 - a second delay circuit configured to delay the rectangular voltage signal by a second adjustable delay to generate a delayed rectangular voltage signal comprising the plurality of voltage rising edges and the plurality of voltage falling edges; and
 - a phase-frequency detector configured to determine a phase differential between the delayed rectangular current signal and the delayed rectangular voltage signal; wherein the control circuit is further configured to:
 - control at least one of the first delay circuit and the second delay circuit until the phase differential is equal to zero; and
 - determine the relative group delay between the rectangular voltage signal and the rectangular current signal when the phase differential is equal to zero.
 - 4. The group delay determination circuit of claim 3, wherein the relative group delay comprises a difference

between the first adjustable delay and the second adjustable delay and a predefined temporal offset.

- 5. The group delay determination circuit of claim 3, wherein the phase-frequency detector comprises:
 - a rising edge phase detector configured to detect a rising 5 edge phase offset between each of the plurality of voltage rising edges and a respective one of the plurality of current rising edges;
 - a falling edge phase detector configured to detect a falling edge phase offset between each of the plurality of voltage falling edges and a respective one of the plurality of current falling edges; and
 - a combiner configured to subtract the falling edge phase offset from the rising edge phase offset to generate the 15 phase differential.
- 6. The group delay determination circuit of claim 1, wherein the signal conversion circuit comprises:
 - a current estimator configured to estimate a differential between the modulated current and the analog current 20 signal based on the analog voltage signal;
 - a current combiner configured to combine the analog current signal with the estimated differential to generate an estimation of the modulated current;
 - a first comparator configured to generate the rectangular 25 current signal based on the estimation of the modulated current and a predefined current threshold; and
 - a second comparator configured to generate the rectangular voltage signal based on the analog voltage signal and a predefined voltage threshold.
- 7. The group delay determination circuit of claim 1, wherein the signal conversion circuit comprises:
 - a current estimator configured to estimate a differential between the modulated current and the analog current signal based on the analog voltage signal;
 - a second current estimator configured to estimate an adjustment term to the analog current signal based on a second analog voltage signal;
 - a current combiner configured to combine the analog current signal with the estimated differential and the 40 estimated adjustment term to generate an estimation of the modulated current;
 - a first comparator configured to generate the rectangular current signal based on the estimation of the modulated current and a predefined current threshold; and
 - a second comparator configured to generate the rectangular voltage signal based on the analog voltage signal and a predefined voltage threshold.
 - **8**. A communication circuit comprising:
 - a power amplifier circuit configured to amplify a radio 50 frequency (RF) signal associated with a time-variant input power based on a modulated voltage and induce a modulated current that tracks the time-variant input power of the RF signal; and
 - a power amplifier integrated circuit (PMIC) comprising: 55 a voltage modulation circuit configured to generate the modulated voltage based on a modulated target voltage; and
 - a group delay determination circuit comprising:
 - a signal conversion circuit configured to:
 - receive an analog voltage signal related to the modulated voltage and an analog current signal related to the modulated current;
 - generate a rectangular voltage signal comprising a plurality of voltage rising edges and a plurality of voltage falling edges based on the received analog voltage signal; and

14

- generate a rectangular current signal comprising a plurality of current rising edges and a plurality of current falling edges based on the received analog current signal and the received analog voltage signal; and
- a control circuit configured to determine a relative group delay between the modulated voltage and the modulated current based on a relative delay between the rectangular voltage signal and the rectangular current signal.
- 9. The communication circuit of claim 8, further comprising a transceiver circuit configured to:
 - generate the RF signal associated with the time-variant input power;
 - generate the modulated target voltage that tracks the time-variant input power of the RF signal;
 - receive the determined relative group delay between the modulated voltage and the modulated current; and
 - delay the RF signal by the determined relative group delay to thereby time align the modulated voltage and the modulated current at the power amplifier circuit.
- 10. The communication circuit of claim 8, wherein the voltage modulation circuit comprises:
 - a voltage amplifier configured to:
 - generate a modulated initial voltage based on the modulated target voltage;
 - cause a high-frequency current between the voltage amplifier and the power amplifier circuit; and
 - generate a sensed current proportionally related to the high-frequency current; and
 - an offset capacitor configured to raise the modulated initial voltage by an offset voltage modulated by a low-frequency current to thereby generate the modulated voltage.
- 11. The communication circuit of claim 10, wherein the PMIC further comprises a current modulation circuit configured to generate the low-frequency current based on the modulated target voltage and as a function of a battery voltage.
- 12. The communication circuit of claim 10, wherein the group delay determination circuit is further configured to: receive the modulated target voltage as the analog voltage signal; and
 - receive the sensed current as the analog current signal.
- 13. The communication circuit of claim 11, wherein the signal conversion circuit comprises:
 - a current estimator configured to estimate a differential between the modulated current and the analog current signal based on the analog voltage signal;
 - a current combiner configured to combine the analog current signal with the estimated differential to generate an estimation of the modulated current;
 - a first comparator configured to generate the rectangular current signal based on the estimation of the modulated current and a predefined current threshold; and
 - a second comparator configured to generate the rectangular voltage signal based on the analog voltage signal and a predefined voltage threshold.
- 14. The communication circuit of claim 10, wherein the group delay determination circuit is further configured to: receive the modulated target voltage as the analog voltage signal;
 - receive the modulated initial voltage as a second analog voltage signal; and
 - receive the sensed current as the analog current signal.

- 15. The communication circuit of claim 14, wherein the signal conversion circuit comprises:
 - a current estimator configured to estimate a differential between the modulated current and the analog current signal based on the analog voltage signal;
 - a second current estimator configured to estimate an adjustment term to the analog current signal based on the second analog voltage signal;
 - a current combiner configured to combine the analog current signal with the estimated differential and the estimated adjustment term to generate an estimation of the modulated current;
 - a first comparator configured to generate the rectangular current signal based on the estimation of the modulated current and a predefined current threshold; and
 - a second comparator configured to generate the rectangular voltage signal based on the analog voltage signal and a predefined voltage threshold.
- **16.** A method for determining a group delay in a com- ₂₀ munication circuit comprising:
 - receiving an analog voltage signal related to a modulated voltage and an analog current signal related to a modulated current;
 - generating a rectangular voltage signal comprising a ²⁵ plurality of voltage rising edges and a plurality of voltage falling edges based on the received analog voltage signal;
 - generating a rectangular current signal comprising a plurality of current rising edges and a plurality of current falling edges based on the received analog current signal and the received analog voltage signal; and
 - determining a relative group delay between the modulated voltage and the modulated current based on a relative delay between the rectangular voltage signal and the rectangular current signal.
 - 17. The method of claim 16, further comprising:
 - dynamically delaying at least one of the rectangular voltage signal and the rectangular current signal to thereby cause the rectangular voltage signal to be in-phase with the rectangular current signal; and
 - determining the relative group delay between the rectangular voltage signal and the rectangular current signal when the rectangular voltage signal is in-phase with the rectangular current signal.

16

- 18. The method of claim 17, further comprising:
- delaying the rectangular current signal by a first adjustable delay to generate a delayed rectangular current signal comprising the plurality of current rising edges and the plurality of current falling edges;
- delaying the rectangular voltage signal by a second adjustable delay to generate a delayed rectangular voltage signal comprising the plurality of voltage rising edges and the plurality of voltage falling edges;
- determining a phase differential between the delayed rectangular current signal and the delayed rectangular voltage signal; and
- determining the relative group delay between the rectangular voltage signal and the rectangular current signal when the phase differential is equal to zero, wherein the relative group delay comprises a difference between the first adjustable delay and the second adjustable delay and a predefined temporal offset.
- 19. The method of claim 16, further comprising:
- estimating a differential between the modulated current and the analog current signal based on the analog voltage signal;
- combining the analog current signal with the estimated differential to generate an estimation of the modulated current:
- generating the rectangular current signal based on the estimation of the modulated current and a predefined current threshold; and
- generating the rectangular voltage signal based on the analog voltage signal and a predefined voltage threshold.
- 20. The method of claim 16, further comprising:
- estimating a differential between the modulated current and the analog current signal based on the analog voltage signal;
- estimating an adjustment term to the analog current signal based on a second analog voltage signal;
- combining the analog current signal with the estimated differential and the estimated adjustment term to generate an estimation of the modulated current;
- generating the rectangular current signal based on the estimation of the modulated current and a predefined current threshold; and
- generating the rectangular voltage signal based on the analog voltage signal and a predefined voltage threshold

* * * * *