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### Film forming apparatus, processing condition determination method, and film forming method

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#### Abstract

A film forming apparatus for forming a film by magnetron sputtering includes a substrate support supporting the substrate, a holder holding a target for emitting sputtered particles, a magnet unit having a magnet, first and second movement mechanisms configured to periodically move the substrate support and the magnet unit, respectively, and a controller. The controller is configured to control the first movement mechanism and the second movement mechanism so that a phase in a periodic movement of the substrate support remains the same at a start of film formation and at an end of film formation, a phase in a periodic movement of the magnet unit remains the same at a start of film formation and at an end of film formation, and the phase in the periodic movement of the substrate support and the phase in the periodic movement of the magnet unit do not match during film formation.

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**Inventors:** Imakita; Kenichi (Albany, NY), Chihaya; Hiroaki (Nirasaki, JP), Kitada; Toru (Nirasaki, JP), Gomi; Atsushi (Nirasaki, JP)

**Applicant:** Tokyo Electron Limited (Tokyo, JP)

**Family ID:** 1000008748282

**Assignee:** TOKYO ELECTRON LIMITED (Tokyo, JP)

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*Primary Examiner:* Berman; Jason

*Attorney, Agent or Firm:* Nath, Goldberg & Meyer

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## Background/Summary

### CROSS-REFERENCE TO RELATED APPLICATION

(1) This application is based upon and claims the benefit of priority from Japanese Patent Application No. 2021-105496, filed on Jun. 25, 2021, the entire contents of which are incorporated herein by reference.

### TECHNICAL FIELD

(2) The present disclosure relates to a film forming apparatus, a processing condition determination method, and a film forming method.

### BACKGROUND

(3) In the related art, there is known a sputtering apparatus that includes a sputtering cathode for supporting a target and a substrate support holder for supporting a substrate. In this sputtering apparatus, the sputtering cathode and the substrate support holder are provided so that, among the

perpendicular lines perpendicular to the plane including the film-formed surface of the substrate, the perpendicular line passing through the center point of the target and the perpendicular line passing through the center point of the substrate do not coincide with each other. The substrate support holder is rotatable about a rotation axis perpendicular to the film-formed surface of the substrate. Further, the sputtering apparatus includes a controller configured to control the rotation speed  $V$  (rps) of the substrate support holder so as to satisfy  $VT=N+\alpha$  by inputting the values of the total integer rotation speed  $N$ , the fractional rotation speed  $\alpha$ , and the deposition time  $T$  so that, when the total rotation speed of the substrate support holder at the deposition time  $T$  (seconds) of sputtered particles on the film-formed surface of the substrate is  $X$ ,  $X=N+\alpha$ , where  $N$  is the total integer rotation speed which is a positive integer, and  $\alpha$  is the fractional rotation speed which is a positive pure decimal number).

PRIOR ART DOCUMENT

Patent Document

(4) Patent Document 1: PCT International Publication No. 2009/157341

SUMMARY

(5) According to one embodiment of the present disclosure, there is provided a film forming apparatus for forming a film on a substrate by magnetron sputtering, including: a substrate support configured to support the substrate; a holder configured to hold a target for emitting sputtered particles so that the target faces the substrate support; a magnet unit provided on a side of the holder opposite to the substrate support and having a magnet; a first movement mechanism configured to periodically move the substrate support; a second movement mechanism configured to periodically move the magnet unit with respect to the target held by the holder; and a controller, wherein the controller is configured to control the first movement mechanism and the second movement mechanism so that a phase in a periodic movement of the substrate support remains the same at a start of film formation and at an end of film formation, a phase in a periodic movement of the magnet unit remains the same at a start of film formation and at an end of film formation, and the phase in the periodic movement of the substrate support and the phase in the periodic movement of the magnet unit do not match during film formation.

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## Description

### BRIEF DESCRIPTION OF DRAWINGS

- (1) The accompanying drawings, which are incorporated in and constitute a part of the specification, illustrate embodiments of the present disclosure, and together with the general description given above and the detailed description of the embodiments given below, serve to explain the principles of the present disclosure.
- (2) FIG. 1 is a vertical cross-sectional view showing an outline of a configuration of a film forming apparatus according to the present embodiment.
- (3) FIG. 2 is a diagram for explaining a configuration around a cathode.
- (4) FIG. 3 is a perspective view of a magnet unit.
- (5) FIG. 4 is a diagram showing a relationship between a position of the magnet unit with respect to a target and an area of a region of the target exposed to plasma.
- (6) FIG. 5 is a diagram showing the relationship between the position of the magnet unit with respect to the target and the area of the region of the target exposed to plasma.
- (7) FIG. 6 is a diagram for explaining a method of determining a total number of rotations of the stage and a total number of swings of the magnet unit during film formation.
- (8) FIG. 7 is a diagram for explaining a method of determining the total number of rotations of the stage and the total number of swings of the magnet unit during film formation.
- (9) FIG. 8 is a diagram showing a wafer in-plane film thickness distribution in a Comparative

Example.

(10) FIG. 9 is a diagram showing a wafer in-plane film thickness distribution in an Example.

#### DETAILED DESCRIPTION

(11) Reference will now be made in detail to various embodiments, examples of which are illustrated in the accompanying drawings. In the following detailed description, numerous specific details are set forth in order to provide a thorough understanding of the present disclosure.

However, it will be apparent to one of ordinary skill in the art that the present disclosure may be practiced without these specific details. In other instances, well-known methods, procedures, systems, and components have not been described in detail so as not to unnecessarily obscure aspects of the various embodiments.

(12) In a manufacturing process of a semiconductor device or the like, a film forming process for forming a desired film of a metal or the like is performed on a substrate such as a semiconductor wafer (hereinafter referred to as a “wafer”) or the like. For example, sputtering is used for the film forming process.

(13) The film forming apparatus for forming a film by sputtering includes, for example, a substrate support configured to support a substrate, and a cathode configured to hold a target on the front surface thereof so that the target for emitting sputtered particles faces the substrate support.

(14) When the target is held by the cathode so as to be non-parallel to the substrate, the substrate support may be configured to be rotatable, and the substrate supported by the substrate support may be rotated during film formation. This is to prevent the thickness of the film formed on the substrate by sputtering from varying on the surface of the substrate. In the related art, the total rotation of the substrate support holder is set to a predetermined value based on the deposition time of the sputtered particles and the rotation speed of the substrate support holder, thereby securing uniformity of the deposition amount, i.e., the film thickness.

(15) Further, when magnetron sputtering is adopted as sputtering, in order to effectively utilize the entire target, a magnet unit including a magnet and having a smaller size than the target may be provided, and the magnet unit may be configured to be swingable or rotatable with respect to the cathode. However, in the case of such magnetron sputtering, the uniformity of the film thickness may not be sufficiently secured only by adjusting the total rotation speed of the substrate support as in the related art.

(16) Therefore, the technique according to the present disclosure improves the in-plane film thickness uniformity when forming a film by magnetron sputtering.

(17) Hereinafter, the film forming apparatus, the processing condition determination method and the film forming method according to the present embodiment will be described with reference to the drawings. In the subject specification and the drawings, elements having substantially the same functional configuration are designated by the same reference numerals, and the duplicate description thereof will be omitted.

(18) <Film Forming Apparatus>

(19) FIG. 1 is a vertical cross-sectional view showing an outline of a configuration of the film forming apparatus 1 according to the present embodiment. FIG. 2 is a diagram for explaining a configuration around a cathode described later. FIG. 3 is a perspective view of a magnet unit described later.

(20) The film forming apparatus 1 shown in FIG. 1 is configured to form a film on a substrate by magnetron sputtering. Specifically, a film (e.g., Ta film) for a magnetic tunnel junction (MTJ) element is formed on a wafer W as a substrate by magnetron sputtering.

(21) The film forming apparatus 1 includes a processing container 10. The processing container 10 is configured to be depressurized and to accommodate the wafer W. The processing container 10 is formed of, for example, aluminum and is connected to a ground potential. An exhaust device 11 for reducing the pressure in the space K1 inside the processing container 10 is connected to the bottom of the processing container 10. The exhaust device 11 includes a vacuum pump (not shown) and the

like, and is connected to the processing container **10** via, for example, an APC valve **12**.

(22) Further, a wafer loading/unloading port **13** is formed on one side wall (the X-direction positive side wall in the figure) of the processing container **10**, and a gate valve **13a** for opening and closing the loading/unloading port **13** is provided at the loading/unloading port **13**.

(23) In the processing container **10**, a stage **14** as a substrate support for supporting the wafer W is provided. Specifically, the wafer W is horizontally mounted on the stage **14** so as to face the processing space K2 defined by the shield part **30** described later. The stage **14** supports the wafer W thus mounted. The stage **14** includes an electrostatic chuck **14a**, a heater **14b**, and a base portion **14c**.

(24) The electrostatic chuck **14a** includes, for example, a dielectric film and an electrode provided as an inner layer of the dielectric film. The electrostatic chuck **14a** is provided on the base portion **14c**. A DC power supply (not shown) is connected to the electrode of the electrostatic chuck **14a**. The wafer W mounted on the electrostatic chuck **14a** is attracted and held by the electrostatic chuck **14a** by the electrostatic attraction force generated by applying a DC voltage from the DC power supply to the electrode.

(25) The heater **14b** is configured to heat the wafer W supported by the stage **14**. The heater **14b** heats the wafer W supported by the stage (specifically, the electrostatic chuck **14a**) by heating the stage **14** (specifically, the electrostatic chuck **14a**). For example, a resistance heating type heater may be used as the heater **14b**. In addition, the heater **14b** is provided on, for example, the electrostatic chuck **14a**.

(26) The base portion **14c** is formed in a disk shape using, for example, aluminum. Depending on the type of the heater **14b** and the like, the heater **14b** may be provided on the base portion **14c**.

(27) The stage **14** may be provided with a cooling mechanism for cooling the wafer W mounted on the stage **14**.

(28) Further, the stage **14** is connected to a rotation/movement mechanism **15** as a first movement mechanism. The rotation/movement mechanism **15** periodically moves the stage **14**. In the present embodiment, the rotation/movement mechanism **15** rotates and moves the stage **14**. Specifically, the rotation/movement mechanism **15** rotates the stage **14** about an axis AX passing through the center of the upper surface of the stage **14** perpendicularly to the upper surface of the stage **14**.

Further, the rotation/movement mechanism **15** can move the stage **14** up and down. The rotation/movement mechanism **15** includes, for example, a support shaft **15a** and a drive part **15b**.

(29) For example, the support shaft **15a** extends in the vertical direction so as to penetrate the bottom wall of the processing container **10**. A sealing member SL1 is provided between the support shaft **15a** and the bottom wall of the processing container **10**. The sealing member SL1 is a member that seals the space between the bottom wall of the processing container **10** and the support shaft **15a** such that the support shaft **15a** can rotate and move up and down. For example, the sealing member SL1 is a magnetic fluid seal. The upper end of the support shaft **15a** is connected to the center of the lower surface of the stage **14**, and the lower end thereof is connected to the drive part **15b**.

(30) The drive part **15b** includes a drive source such as a motor or the like and generates a drive force for rotating and moving the support shaft **15a** up and down. As the support shaft **15a** is rotated about the axis AX by the drive force generated by the drive part **15b**, the stage **14** is rotated about the axis AX. As the support shaft **15a** is moved up and down by the drive force generated by the drive part **15b**, the stage **14** is moved up and down.

(31) The number of rotations per unit time  $V_w$  of the stage **14** (hereinafter referred to as the rotation speed of the stage **14**) rotated by the rotation/movement mechanism **15** is, for example, 60 to 120 rotations per minute (i.e., 60 rpm to 120 rpm). If the rotation speed  $V_w$  of the stage **14** is less than 60 rpm, the total number of rotations of the wafer W required to make the film thickness distribution uniform cannot be obtained. Further, if the rotation speed  $V_w$  of the stage **14** is larger than 120 rpm, the load on the drive part **15b** or the like of the rotation/movement mechanism **15**

becomes large, and the lifespan of the rotation/movement mechanism **15** becomes short.

(32) The rotation/movement mechanism **15** (specifically, the drive part **15b**) is controlled by a controller U described later.

(33) Obliquely above the stage **14**, a holder **20a** made of a conductive material is provided to hold, for example, a target **20** made of Ta for emitting sputtered particles. The holder **20a** holds the target **20** so that the target **20** is located in the processing container **10**. The holder **20a** is attached to the ceiling of the processing container **10**. A through-hole is formed at the attachment position of the holder **20a** in the processing container **10**. Further, an insulating member **10a** is provided on the inner wall surface of the processing container **10** so as to surround the through-hole. The holder **20a** is attached to the processing container **10** via the insulating member **10a** so as to close the through-hole.

(34) The holder **20a** holds the target **20** on the front surface thereof so that the target **20** faces the stage **14**. Specifically, the holder **20a** holds the target **20** so that the target **20** faces the stage **14** and is tilted with respect to the upper surface of the stage **14**, i.e., the surface of the wafer W mounted on the upper surface of the stage **14**.

(35) The target **20** is formed, for example, in a rectangular shape in a plan view. When the target **20** is held in the holder **20a**, the long axis of the target **20** extends in the apparatus depth direction (Y direction in FIG. 1). The length of the target **20** in the apparatus depth direction (Y direction in FIG. 1) is larger than, for example, the diameter of the wafer W which is a film-forming target. When the diameter of the wafer W which is a film-forming target is 300 mm, the length of the target **20** in the apparatus depth direction (Y direction in FIG. 1) is, for example, 400 to 500 mm. The length of the target **20** in the direction (X' direction in FIG. 1) orthogonal to the apparatus depth direction (Y direction in FIG. 1) is, for example, 150 to 200 mm.

(36) Further, a power supply **21** is connected to the holder **20a**, and a negative DC voltage is applied from the power supply **21** to the holder **20a**. An AC voltage may be applied instead of the negative DC voltage. Further, as shown in FIG. 2, the holder **20a** is provided with a shield **22** for the purpose of preventing other portions from being contaminated by sputtered particles generated from the target **20** held by the holder **20a**. For example, the shield **22** is provided so as to cover the outer periphery of the target **20** held by the holder **20a**.

(37) Further, a magnet unit **23** is provided at a position on the side of the holder **20a** opposite to the stage **14**, i.e., on the back side of the holder **20a** and outside the processing container **10**. The magnet unit **23** is configured to form a magnetic field that leaks to the front side of the target **20** held by the holder **20a**. For example, as shown in FIG. 3, a rectangular parallelepiped central magnet **102** and an outer peripheral magnet **103** having a rectangular ring shape in a plan view are arranged on a flat plate-shaped yoke **101**. The central magnet **102** is provided along the longitudinal direction of the yoke **101**, and the outer peripheral magnet **103** is provided so as to surround the four sides of the central magnet **102** in a plan view. Further, the central magnet **102** and the outer peripheral magnet **103** are magnetized opposite to each other in the direction perpendicular to the central magnet side surface of the yoke **101**.

(38) As shown in FIG. 1, the magnet unit **23** is connected to a movement mechanism **24** as a second movement mechanism. The movement mechanism **24** is configured to periodically move the magnet unit **23**. In the present embodiment, the movement mechanism **24** swings or reciprocates the magnet unit **23** along the back surface of the holder **20a** in the apparatus depth direction (Y direction in FIGS. 1 and 3). In other words, the movement mechanism **24** moves the magnet unit **23** along the back surface of the holder **20a** in the positive apparatus depth direction (positive Y direction in FIGS. 1 and 3) and in the negative apparatus depth direction (negative Y direction in FIGS. 1 and 3).

(39) The movement mechanism **24** includes, for example, a rail **24a** extending along the apparatus depth direction (Y direction in FIGS. 1 and 3), and a drive part **24b** including a drive source such as a motor or the like. By the drive force generated by the drive part **24b**, the magnet unit **23** is moved

along the rail **24a** in the apparatus depth direction (Y direction in FIGS. **1** and **3**). More specifically, by the drive force generated by the drive part **24b**, the magnet unit **23** is moved to reciprocate between one end of the target **20** (the negative side end in the Y direction in FIGS. **1** and **3**) and the other end of the target **20** (the positive side end in the Y direction in FIGS. **1** and **3**). This prevents the target **20** from being locally consumed and makes it possible to utilize almost the entire target **20**.

(40) In counting the “number of swings” of the magnet unit **23** in the subject specification, for example, the movement of the target **20** from the negative end in the apparatus depth direction to the positive end in the apparatus depth direction is counted as one swing, and the movement of the target **20** from the positive end in the apparatus depth direction to the negative end in the apparatus depth direction is counted as one swing. Accordingly, when the magnet unit **23** reciprocates once, the “number of swings” of the magnet unit **23** is two.

(41) The number of swings per unit time of the magnet unit **23** swung by the movement mechanism **24** (hereinafter referred to as the swing speed of the magnet unit **23**) is, for example, 30 to 120 times/minute. If the swing speed  $V_m$  of the magnet unit **23** is less than 30 times/minute, it is not possible to sufficiently prevent the target **20** from being locally consumed. Further, if the swing speed  $V_m$  of the magnet unit **23** is larger than 120 times/minute, the load on the drive part **24b** or the like of the movement mechanism **24** becomes large and the lifespan of the movement mechanism **24** becomes short.

(42) The movement mechanism **24** (specifically, the drive part **24b**) is controlled by the controller **U** described later.

(43) Further, the film forming apparatus **1** includes a shield part **30** that forms a processing space **K2** in the processing container **10**. The shield part **30** is provided in the processing container **10**.

(44) The shield part **30** includes a first shield member **31** and a second shield member **32**. The first shield member **31** and the second shield member **32** are formed of, for example, aluminum.

(45) The first shield member **31** is a pot-shaped member having an open upper portion. The first shield member **31** has a hole **31a** formed on the bottom surface thereof to expose the processing space **K2** to the wafer **W** mounted on the stage **14**. The first shield member **31** is supported in the processing container **10** via, for example, a support member (not shown).

(46) The second shield member **32** is a lid member that closes the upper opening of the first shield member **31** and is formed so that the central portion in a plan view protrudes upward. The second shield member **32** has an opening **32a**. Sputtered particles from the target **20** held by the holder **20a** are supplied to the processing space **K2** through the opening **32a**.

(47) Further, one end of a rotary shaft **33** is connected to the central portion of the second shield member **32**. The central axis of the rotary shaft **33** substantially coincides with the axis **AX**. The rotary shaft **33** extends to the outside of the processing container **10**, and the other end of the rotary shaft **33** is connected to the rotation mechanism **34**. The rotation mechanism **34** rotates the rotary shaft **33** about the axis **AX**. The rotation mechanism **34** includes a drive part (not shown) including a drive source such as a motor or the like that generates a drive force for rotating the rotary shaft **33**.

(48) By rotating the second shield member **32**, the opening **32a** of the second shield member **32** can be caused to face the target **20** held by the holder **20a**, or the portion of the second shield member **32** where the opening **32a** is not formed can be caused to face the target **20**.

(49) Further, the film forming apparatus **1** includes a gas supply (not shown) for supplying a gas into the processing container **10**. The gas supply includes, for example, a gas source, a flow rate controller such as a mass flow controller or the like, and a gas introduction part. The gas source stores a gas (e.g., Ar gas) excited in the processing container **10**. The gas source is connected to the gas introduction part via the flow controller. The gas introduction part is a member that introduces the gas from the gas source into the processing container **10**.

(50) When the gas is supplied from the gas supply and the electric power is supplied to the target

**20** by the power supply **21**, the gas supplied in the processing container **10** is excited. Further, the magnet unit **23** generates a magnetic field in the vicinity of the front surface of the target **20**, and plasma is concentrated in the vicinity of the front surface of the target **20**. Then, when the positive ions in the plasma collide with the target **20**, the substance constituting the target **20** is emitted from the target **20** as sputtered particles. As a result, a desired film is formed on the wafer W.

(51) As shown in FIG. 1, the film forming apparatus **1** further includes the controller U. The controller U is composed of, for example, a computer equipped with a CPU, a memory, and the like, and includes a program storage part (not shown). The program storage part stores programs for controlling the drive part **15b**, the power supply **21**, the drive part **24b**, and the like to realize the below-described film forming process in the film forming apparatus **1**. Further, the program storage part stores a program for determining processing conditions for film formation. The above programs may be recorded on a computer-readable storage medium and may be installed on the controller U from the storage medium. The storage medium may be transitory or non-transitory. In addition, a part or all of the programs may be implemented by dedicated hardware (circuit board).

(52) <Total Number of Rotations  $N_w$  of Stage **14** and Total Number of Swings  $N_m$  of Magnet Unit **23** During Film Formation>

(53) When the target **20** is tilted with respect to the upper surface of the stage **14**, i.e., the surface of the wafer W mounted on the upper surface of the stage **14** as described above, the film thickness when a film is formed on the wafer W may be non-uniform in the plane of the wafer W. This is because the distance to the target **20** is different for each region on the surface of the wafer W. In order to eliminate the in-plane non-uniformity of the film thickness, the stage **14** on which the wafer W is mounted is rotated during film formation. However, when the magnet unit **23** is used, even if the stage **14** is rotated, the in-plane uniformity of the film thickness may be insufficient for the following reasons.

(54) That is, in order to effectively utilize the target **20**, the magnet unit **23** is configured to swing with respect to the target **20** so that the magnetic field formed by the magnet unit **23** covers the entire width of the target **20**. Further, the size of the region of the target **20** exposed to plasma P differs depending on whether the magnet unit **23** is located at a portion facing the center of the target **20** in the swing direction as shown in FIG. 4, or at a portion facing the end of the target **20** in the swing direction as shown in FIG. 5. Therefore, the number of sputtered particles emitted from the target **20** also varies, and the deposition amount of thin film deposited on the wafer W per unit time (i.e., the deposition rate of the thin film on the wafer W) also varies. Then, for example, if the magnet unit **23** is located at the center of the target **20** a plurality of times during film formation, depending on the relationship between the rotation speed  $V_w$  of the stage **14** and the swing speed  $V_m$  of the target **20**, the orientation (position in the rotation direction) of the wafer W on the stage **14** when the magnet unit **23** is located at the center of the target **20** may be the same each time. In this case, even if the stage **14** is rotated during the film formation, the distribution of the film thickness in the plane of the wafer W may be biased.

(55) In view of this point and the like, in the present embodiment, the controller U controls the drive part **15b** and the drive part **24b** so as to satisfy the following conditions (1) to (3) at the time of film formation. (1) The phase in the rotational movement of the stage **14** (specifically, the position in the rotational direction of the stage **14**, i.e., the orientation of the stage **14**) remains the same at the start of film formation and at the end of film formation. (2) The phase of the swing of the magnet unit **23** remains the same at the start of film formation and at the end of film formation. (3) The phase in the rotational movement of the stage **14** and the phase in the swing of the magnet unit **23** do not match during film formation.

(56) Satisfying the above condition (1) means that the total number of rotations  $N_w$  of the stage **14** during film formation becomes a natural number. As a result, the time length at which each region of the surface of the wafer W on the stage **14** is closest to the target **20** can be made equal for the respective regions. Thus, the thickness of the formed film can be made uniform in the wafer plane.



(57) Satisfying the above condition (2) means that the total number of swings  $N_m$  of the magnet unit **23** during film formation becomes a natural number. As a result, the consumption of the target **20** can be made uniform in the plane of the target **20**.

(58) Satisfying the above conditions (1) to (3) means that the total number of swings  $N_m$  is not an integer multiple of the total number of rotations  $N_w$ , and the total number of rotations  $N_w$  is not an integer multiple of the total number of swings  $N_m$ . As a result, when the magnet unit **23** is located at the center of the target **20** a plurality of times during film formation, the orientation of the wafer **W** on the stage **14** at the time when the magnet unit **23** is located at the center of the target **20** can be changed each time. In other words, the position **A** where the thin film is mainly deposited when the magnet unit **23** is located at the center of the target **20** is not one position in the plane of the wafer **W** as shown in FIG. 6, but may be multiple positions (e.g., every  $30^\circ$ ) in the plane of the wafer **W** as shown in FIG. 7. Therefore, it is possible to suppress the occurrence of local film thickness unevenness, and it is possible to improve the uniformity of the film thickness in the plane of the wafer **W**.

(59) <Processing Condition Determination Method>

(60) Next, an example of a method for determining the processing conditions for film formation by magnetron sputtering using the film forming apparatus **1**, specifically, an example of a method for determining the processing conditions for the rotation of the stage **14** and the swing of the magnet unit **23** during film formation, will be described.

(61) In this determination method, for example, the controller **U** determines the processing conditions for the rotation of the stage **14** and the swing of the magnet unit **23** during film formation so that the above conditions (1) to (3) are satisfied. Specifically, the processing conditions may be determined as follows.

(62) (Step S1: Determination of Film Formation Time)

(63) For example, first, when a target film thickness value is inputted to the controller **U** by an operator or the like via an input device such as a keyboard or the like, the controller **U** determines the film formation time  $T$ , i.e., the deposition time  $T$ , from the target film thickness value and the film formation rate by the film forming apparatus **1**, i.e., the deposition rate of a thin film acquired in advance.

(64) (Step S2: Determination of Total Number of Rotations  $N_w$  and Rotation Speed  $V_w$  of Stage **14**)

(65) Next, the controller **U** determines the total number of rotations  $N_w$  of the stage **14** and the rotation speed  $V_w$  of the stage **14** during film formation. Specifically, the controller **U** determines the rotation speed  $V_w$  of the stage **14** from a range of 60 rpm to 120 rpm based on the film formation time  $T$  determined in step S1, so that the total number of rotations  $N_w$  of the stage **14** during film formation becomes a natural number.

(66) (Step S3: Determination of Total Number of Swings  $N_m$  and Swing Speed  $V_m$  of Magnet Unit **23**)

(67) Then, the controller **U** determines the total number of swings  $N_m$  of the magnet unit **23** and the swing speed  $V_m$  of the magnet unit **23** during film formation. Specifically, the swing speed  $V_m$  of the magnet unit **23** is determined from a range of 30 times/minute to 120 times/minute based on the film formation time  $T$  determined in step S1, so that the total number of swings  $N_m$  of the magnet unit **23** during film formation becomes a natural number satisfying the above (3). In other words, the controller **U** determines the swing speed  $V_m$  of the magnet unit **23** from the range of 30 times/minute to 120 times/minute so that  $N_m = N_w \pm n$  (where  $n$  is an arbitrary natural number) is satisfied and  $N_m/N_w$  and  $N_w/N_m$  are not integers.

(68) If, in step S2 and step S3, there are multiple rotation speeds  $V_w$  of the stage **14**, which satisfy that: (1)  $N_m = N_w \pm n$  (where  $N_m$  and  $N_w$  are natural numbers, and  $n$  is an arbitrary natural number); (2)  $N_m/N_w$  and  $N_w/N_m$  are not integers; (3) the rotation speed  $V_w$  of the stage **14** is in the range of 60 rpm to 120 rpm; and (4) the swing speed  $V_m$  of the magnet unit **23** is in the range of 30

times/minute to 120 times/minute, the highest rotation speed  $V_w$  is selected. This is to suppress variations in film formation. Further, if there are multiple swing speeds  $V_m$  of the magnet unit **23** with respect to the determined/selected rotation speed  $V_w$  of the stage **14**, the largest swing speed  $V_m$  is similarly selected.

(69) <Film Forming Process>

(70) Next, an example of the film forming process using the film forming apparatus **1** will be described. The following process is performed under the control of the controller **U**.

(71) (S11: Loading)

(72) First, the wafer **W** is loaded into the processing container **10**. Specifically, the gate valve **13a** is opened, and the transfer mechanism (not shown) holding the wafer **W** is inserted into the processing container **10** from the vacuum atmosphere transfer chamber (not shown) adjacent to the processing container **10** adjusted to a desired pressure by the exhaust device **11** via the loading/unloading port **13**. The pressure in the processing container **10** and in the transfer chamber at this time is, for example, 10.sup.-7 Torr to 10.sup.-9 Torr. Next, the wafer **W** is delivered from the transfer mechanism onto the raised support pins (not shown). Thereafter, the transfer mechanism is withdrawn from the processing container **10**, and the gate valve **13a** is closed. At the same time, the support pins are lowered. The wafer **W** is placed on the stage **14** and is attracted and held by the electrostatic attraction force of the electrostatic chuck **14a**. Further, the stage **14** is raised, and the wafer **W** is moved to a position directly under the hole **31a** of the shield part **30**.

(73) (S12: Rotation of Stage **14**)

(74) Subsequently, the rotation/movement mechanism **15** is controlled so that the stage **14** is rotated at the rotation speed  $V_w$  determined in step S2 or the like described above.

(75) (Step S13: Swing of Magnet Unit **23**)

(76) Further, the movement mechanism **24** is controlled so that the magnet unit **23** swings at the swing speed  $V_m$  determined in step S3 or the like described above.

(77) (Step S14: Film Formation)

(78) Subsequently, by magnetron sputtering, a desired film is formed on the wafer **W** for the film formation time  $T$  determined in step S1 described above. Specifically, for example, an Ar gas is supplied from the gas supply (not shown) into the processing container **10**. Further, electric power is supplied from the power supply **21** to the target **20**. The Ar gas in the processing container **10** is ionized by the electric power supplied from the power supply **21**, and the electrons generated by the ionization are drift-moved by the magnetic field (i.e., the leaked magnetic field) formed in front of the target **20** by the magnet unit **23**, thereby generating high-density plasma. The surface of the target **20** is sputtered by the Ar ions generated in the plasma, and the sputtered particles are deposited on the wafer **W** to form a thin film. If the film formation time  $T$  determined in step S1 described above elapses after the power supply from the power supply **21** is started, the power supply is stopped, the gas supply from the gas supply (not shown) is also stopped, and the rotation of the stage **14** and the swing of the magnet unit **23** are also stopped.

(79) (Step S15: Unloading)

(80) Thereafter, the wafer **W** is unloaded from the processing container **10**. Specifically, the wafer **W** is unloaded from the processing container **10** in an operation opposite to the loading operation of step S11. Then, the process returns to the above-mentioned loading step, and a next wafer **W** on which a film is to be formed is processed in the same manner

(81) <Main Effects of the Present Embodiment>

(82) As described above, according to the present embodiment, it is possible to suppress the occurrence of local film thickness unevenness when forming a film by magnetron sputtering, and it is possible to improve uniformity of the film thickness in the plane of the wafer **W**.

EXAMPLE

(83) FIGS. **8** and **9** are diagrams showing in-plane film thickness distributions in a Comparative Example and an Example, respectively. In the Comparative Example and the Example, a target **20**

made of Ta was used, and film formation was performed by magnetron sputtering with a target film thickness of 1 nm under the condition of a film formation rate of 0.125 nm/s. That is, the film formation time T was set to 8 seconds.

(84) Further, in the Comparative Example and the Example, the total number of rotations  $N_w$  of the stage **14** was set to 8 times, and the rotation speed of the stage **14** was set to 60 rpm of  $(N_w/T) \times 60$  (where  $N_w$  is 8 times, and T is 8 seconds).

(85) Then, in the Example, the total number of swings  $N_m$  of the magnet unit **23** was set to 9 times of  $N_m = N_w + 1$  (where  $N_w$  is 8 times) so as to satisfy the condition that both  $N_m/N_w$  and  $N_w/N_m$  are not integers. During the film formation, the phase in the rotational movement of the stage **14** and the phase in the swing of the magnet unit **23** were prevented from matching. On the other hand, in the Comparative Example, the total number of swings  $N_m$  of the magnet unit **23** was set to 8 times of  $N_m = N_w$  (where  $N_w$  is 8 times) so as not to satisfy the condition that both  $N_m/N_w$  and  $N_w/N_m$  are not integers. During the film formation, the phase in the rotational movement of the stage **14** and the phase in the swing of the magnet unit **23** were allowed to match.

(86) In the Comparative Example, the phase in the rotational movement of the stage **14** and the phase in the swing of the magnet unit **23** are allowed to match during the film formation. As a result, as shown in FIG. 8, there is a portion where the Ta film is extremely thick. The thickness of the Ta film is non-uniform in the plane of the wafer W. Further, in the Comparative Example, the coefficient of variation (CV) of the film thickness, which is obtained by dividing the standard deviation of the film thickness by the average value of the film thickness, is 2.0%.

(87) On the other hand, in the Example, as shown in FIG. 9, unlike the Comparative Example, there is no portion where the Ta film is extremely thick. Moreover, in the Example, the coefficient of variation of the film thickness is 0.6%.

(88) From the above results, it can be noted that, by using the method of the present disclosure, a thin film having a film thickness distribution with a coefficient of variation of 1% or less can be formed on a wafer W even when the magnetron sputtering is performed while swinging the magnet unit **23**.

(89) <Modification>

(90) In the above example, the total number of rotations  $N_w$  and the rotation speed  $V_w$  of the stage **14** are determined first, and the total number of swings  $N_m$  and the swing speed  $V_m$  of the magnet unit **23** are determined later. However, the total number of swings  $N_m$  and the swing speed  $V_m$  of the magnet unit **23** may be determined first, and the total number of rotations  $N_w$  and the rotation speed  $V_w$  of the stage **14** may be determined later. Specifically, the controller U may first determine the swing speed  $V_m$  of the magnet unit **23** from a predetermined range based on the film formation time T so that the total number of swings  $N_m$  of the magnet unit **23** becomes a natural number. Then, the controller U may determine the rotation speed  $V_w$  of the stage **14** from a predetermined range based on the film formation time T so that the total number of rotations  $N_w$  of the stage **14** during film formation becomes a natural number satisfying the above (3).

(91) Further, in the above example, the stage **14** is rotated. However, the mode of periodic movement of the stage **14** is not limited thereto. For example, like the magnet unit **23**, the stage **14** may be swung in a predetermined direction such as a horizontal direction or the like. In this case as well, the technique according to the present disclosure may be applied.

(92) Further, in the above example, the magnet unit **23** is caused to swing. However, the mode of periodic movement of the magnet unit **23** is not limited thereto. For example, when the target **20** is circular in a plan view, the magnet unit **23** may be rotated about the central axis of the target **20** along the back surface of the holder **20a**. Further, the magnet unit **23** may be moved so as to draw a rectangular locus along the back surface of the holder **20a** about the central axis of the target **20**. In these cases as well, the technique according to the present disclosure may be applied.

(93) The embodiments disclosed herein should be considered to be exemplary and not limitative in all respects. The above-described embodiments may be omitted, replaced, or modified in various

forms without departing from the scope of the appended claims and their gist.

(94) According to the present disclosure in some embodiments, it is possible to improve the in-plane film thickness uniformity when forming a film by magnetron sputtering.

(95) While certain embodiments have been described, these embodiments have been presented by way of example only and are not intended to limit the scope of the disclosures. Indeed, the embodiments described herein may be embodied in a variety of other forms. Furthermore, various omissions, substitutions and changes in the form of the embodiments described herein may be made without departing from the spirit of the disclosures. The accompanying claims and their equivalents are intended to cover such forms or modifications as would fall within the scope and spirit of the disclosures.

## Claims

1. A film forming apparatus for forming a film on a substrate by magnetron sputtering, comprising: a substrate support configured to support the substrate; a holder configured to hold a target for emitting sputtered particles so that the target faces the substrate support; a magnet unit provided on a side of the holder opposite to the substrate support and having a magnet; a first movement mechanism configured to periodically move the substrate support; a second movement mechanism configured to periodically move the magnet unit with respect to the target held by the holder; and a controller, wherein the controller is configured to control the first movement mechanism and the second movement mechanism so that a phase in a periodic movement of the substrate support remains the same at a start of film formation and at an end of film formation, a phase in a periodic movement of the magnet unit remains the same at a start of film formation and at an end of film formation, and the phase in the periodic movement of the substrate support and the phase in the periodic movement of the magnet unit do not match during film formation.
2. The apparatus of claim 1, wherein the controller is configured to control the first movement mechanism and the second movement mechanism so as to satisfy a condition that a total number of movements  $N_w$  of the substrate support during film formation and a total number of movements  $N_m$  of the magnet unit during film formation are natural numbers different from each other, the total number of movements  $N_m$  is not an integer multiple of the total number of movements  $N_w$ , and the total number of movements  $N_w$  is not an integer multiple of the total number of movements  $N_m$ .
3. The apparatus of claim 2, wherein the controller is configured to control the first movement mechanism so that the substrate support is moved at the number of movements per unit time of the substrate support which is determined from a predetermined range based on a time required for film formation so that the total number of movements  $N_w$  of the substrate support during film formation becomes a natural number.
4. The apparatus of claim 3, wherein the predetermined range is 60 to 120 times per minute.
5. The apparatus of claim 4, wherein the controller is configured to control the second movement mechanism so that the magnet unit is moved at the number of movements per unit time of the magnet unit which is determined from another predetermined range based on the time required for film formation so that the total number of movements  $N_w$  of the magnet unit during film formation becomes a natural number satisfying the condition.
6. The apparatus of claim 5, wherein said another predetermined range is 30 to 120 times per minute.
7. The apparatus of claim 3, wherein the controller is configured to control the second movement mechanism so that the magnet unit is moved at the number of movements per unit time of the magnet unit which is determined from another predetermined range based on the time required for film formation so that the total number of movements  $N_w$  of the magnet unit during film formation becomes a natural number satisfying the condition.

8. A processing condition determination method for determining a processing condition at which a film is formed on a substrate by magnetron sputtering using a film forming apparatus, wherein the film forming apparatus includes a substrate support configured to support the substrate, a holder configured to hold a target for emitting sputtered particles so that the target faces the substrate support, and a magnet unit provided on a side of the holder opposite to the substrate support and having a magnet, the processing condition determining method comprising: moving the substrate support periodically during film formation while the magnet unit is periodically moved with respect to the target held by the holder, and determining the processing condition related to movements of the substrate support and the magnet unit during film formation so that a phase in a periodic movement of the substrate support remains the same at a start of film formation and at an end of film formation, a phase in a periodic movement of the magnet unit remains the same at a start of film formation and at an end of film formation, and the phase in the periodic movement of the substrate support and the phase in the periodic movement of the magnet unit do not match during film formation.

9. A film forming method for forming a film on a substrate by magnetron sputtering using a film forming apparatus, wherein the film forming apparatus includes a substrate support configured to support the substrate, a holder configured to hold a target for emitting sputtered particles so that the target faces the substrate support, and a magnet unit provided on a side of the holder opposite to the substrate support and having a magnet, the method comprises forming a film on the substrate by magnetron sputtering by periodically moving the substrate support while periodically moving the magnet unit with respect to the target held by the holder, and in the forming the film, the substrate support and the magnet unit are moved so that a phase in a periodic movement of the substrate support remains the same at a start of film formation and at an end of film formation, a phase in a periodic movement of the magnet unit remains the same at a start of film formation and at an end of film formation, and the phase in the periodic movement of the substrate support and the phase in the periodic movement of the magnet unit do not match during film formation.

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