

US Patent & Trademark Office

Patent Public Search | Text View

United States Patent Application Publication

20250260329

Kind Code

A1

Publication Date

August 14, 2025

Inventor(s)

WENG; Bingwen et al.

DC/DC CONVERSION CIRCUIT, INVERTER, AND METHOD FOR NEUTRAL POINT VOLTAGE BALANCING FOR INVERTER

Abstract

A direct-current conversion circuit, which is used for providing direct-current conversion between a first direct-current voltage and a second direct-current voltage is described. The direct-current conversion circuit comprises: a transformer, which comprises a primary-side winding and a secondary-side winding, wherein the primary-side winding comprises a center tap, and a first primary-side winding and a second primary-side winding, which are respectively connected to the center tap; a primary-side circuit, wherein a first side of the primary-side circuit is connected to the primary-side winding, a second side of the primary-side circuit comprises a first end, a second end, and a third end, and a first direct-current voltage is provided between the first end and the second end of the primary-side circuit; and a secondary-side circuit, wherein a first side of the secondary-side circuit is connected to the secondary side winding.

Inventors: WENG; Bingwen (Hangzhou, CN), LIAO; Yafeng (Hangzhou, CN), WU; Junxiong (Hangzhou, CN)

Applicant: HOYMILES POWER ELECTRONICS INC. (Hangzhou, CN)

Family ID: 1000008602826

Assignee: HOYMILES POWER ELECTRONICS INC. (Hangzhou, CN)

Appl. No.: 18/857113

Filed (or PCT Filed): May 12, 2023

PCT No.: PCT/CN2023/094002

Foreign Application Priority Data

CN 202210519822.5

May. 13, 2022

Publication Classification

Int. Cl.: H02M3/335 (20060101); H02M3/00 (20060101); H02M7/483 (20070101); H02M7/487 (20070101)

U.S. Cl.:

CPC H02M3/33584 (20130101); H02M3/01 (20210501); H02M7/4833 (20210501); H02M7/487 (20130101);

Background/Summary

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application claims priority to Chinese Patent Application No. CN202210519822.5, entitled “DC/DC CONVERSION CIRCUIT, INVERTER, AND METHOD FOR NEUTRAL POINT VOLTAGE BALANCING FOR INVERTER” filed on May 13, 2022, which is incorporated herein by reference in its entirety.

TECHNICAL FIELD

[0002] The present disclosure relates to the field of power electronics, and in particular, to a DC/DC conversion circuit, an inverter, and a method for neutral point voltage balancing for an inverter.

BACKGROUND

[0003] Over recent years, photovoltaic energy storage and the electric vehicle industry have developed rapidly, and more studies have been conducted on DC/DC conversion circuits. In some typical application scenarios, such as in an energy storage inverter, the DC/DC conversion circuit and a subsequent inverter circuit form a two-stage structure, where the DC/DC conversion circuit converts a low direct-current voltage of a battery into a high direct-current voltage, which is then converted into an alternating-current voltage by the inverter circuit and fed to a power grid. To reduce harmonic content and voltage stresses of switching devices, some inverter circuits use a three-level structure, such as a T-type three-level or neutral point clamped (NPC) three-level structure. Generally, the high direct-current voltage is divided by capacitors to generate a neutral point voltage.

[0004] However, in a practical circuit, inconsistent parameters of the capacitors or an external half-wave load may cause neutral point voltage shift. The neutral point voltage shift distorts output waveforms, reduces the capacitor lifespan, or even causes overvoltage in some components which damages a equipment.

[0005] Existing solutions for resolving the problem of neutral point voltage imbalance include a hardware solution and a software solution. The hardware solution is to add a neutral point voltage balancing bridge, which is equivalent to a Buck/Boost circuit, and transfers energy from a high-voltage side to a low-voltage side when the neutral point voltage shifts. However, this solution requires additional power components and inductors, which reduces efficiency of the equipment, and increases costs of the equipment. The software solution is to balance the neutral point voltage by using a special control method, which is complex and difficult to implement.

SUMMARY

[0006] To resolve the foregoing problems in the related art, this application proposes a DC/DC conversion circuit, an inverter, and a method for neutral point voltage balancing for an inverter. A transformer of a DC/DC conversion circuit in the inverter has a center tap, which is connected to a neutral point of the inverter, to provide a current loop to balance a neutral point voltage of the

inverter. This solution may achieve the balance of the neutral point voltage of the inverter without an additional balancing bridge or a complex control algorithm.

[0007] Based on an objective of the foregoing disclosure, this application provides a DC/DC conversion circuit, configured to provide direct-current conversion between a first direct-current voltage and a second direct-current voltage, including: [0008] a transformer, where the transformer includes a primary winding and a secondary winding, and the primary winding includes a center tap, and a first primary winding and a second primary winding respectively connected to the center tap; [0009] a primary circuit, where a first side of the primary circuit is connected to the primary winding, a second side of the primary circuit includes a first end, a second end, and a third end arranged between the first end and the second end, and the first direct-current voltage is provided between the first end and the second end of the primary circuit; and [0010] a secondary circuit, where a first side of the secondary circuit is connected to the secondary winding, and a second side of the secondary circuit provides the second direct-current voltage, where [0011] the third end of the primary circuit is connected to the center tap, to provide a current loop to balance a voltage between the first end and the third end of the primary circuit and a voltage between the second end and the third end of the primary circuit.

[0012] Further, the primary circuit includes a plurality of switching devices, a first current loop flowing through the first end and the third end of the primary circuit and the center tap, and a second current loop flowing through the center tap and the third end and the second end of the primary circuit are selectively provided by controlling switching of the switching devices, and a direction of the first current loop is opposite to a direction of the second current loop.

[0013] Further, the first primary winding and the second primary winding have a same number of turns.

[0014] Further, the primary circuit is a full-bridge structure or a half-bridge structure.

[0015] Further, the DC/DC conversion circuit further includes: a resonant tank, where the resonant tank includes a resonant capacitor, a first resonant inductor, and a second resonant inductor, where the resonant capacitor is connected between the secondary circuit and the secondary winding, and the first resonant inductor and the second resonant inductor are connected between the secondary circuit and the secondary winding or connected between the primary winding and the primary circuit.

[0016] Further, the secondary circuit is a full-bridge structure.

[0017] This application further provides an inverter, where the inverter includes a multi-level inverter circuit and the DC/DC conversion circuit as described above.

[0018] A direct-current side of the multi-level inverter circuit is electrically connected to a second side of a primary circuit of the DC/DC conversion circuit, and an alternating current side of the multi-level inverter circuit provides an alternating current output.

[0019] Further, the multi-level inverter circuit is a T-type multi-level inverter circuit or a diode-clamped multi-level inverter circuit.

[0020] Further, the inverter further includes a first voltage-dividing capacitor and a second voltage-dividing capacitor connected in series between the first end and the second end of the primary circuit, and a connection point between the first voltage-dividing capacitor and the second voltage-dividing capacitor is respectively connected to the center tap and a neutral point of the multi-level inverter circuit.

[0021] Further, the inverter is a three-phase inverter, including three multi-level inverter circuits.

[0022] This application further provides a method for neutral point voltage balancing for an inverter, where the inverter includes the DC/DC conversion circuit as described above, and the method includes: connecting the center tap of the transformer of the DC/DC conversion circuit in the inverter to the neutral point of the inverter, and providing a current loop to balance a neutral point voltage of the inverter.

[0023] Details of one or more embodiments of this application are provided in the subsequent

accompanying drawings and descriptions, so that other features, objectives, and advantages of this application are more concise and understandable.

Description

BRIEF DESCRIPTION OF THE DRAWINGS

[0024] To describe the technical solutions in embodiments of this application more clearly, the following briefly introduces the accompanying drawings required for describing the embodiments or the related art. Apparently, the accompanying drawings in the following description show only embodiments of this application, and a person of ordinary skill in the art may still derive other accompanying drawings from the disclosed accompanying drawings without creative efforts.

[0025] FIG. 1 is a schematic diagram of a DC/DC conversion circuit according to an embodiment of this application;

[0026] FIG. 2 is a schematic diagram of a control signal of a switching device of a primary circuit of a DC/DC conversion circuit according to an embodiment of this application;

[0027] FIG. 3 is a schematic diagram of a current loop when a primary circuit of a DC/DC conversion circuit is in a first working mode according to an embodiment of this application;

[0028] FIG. 4 is an equivalent circuit diagram when a primary circuit of a DC/DC conversion circuit is in a first working mode according to an embodiment of this application;

[0029] FIG. 5 is a schematic diagram of a current loop when a primary circuit of a DC/DC conversion circuit is in a second working mode according to an embodiment of this application;

[0030] FIG. 6 is an equivalent circuit diagram when a primary circuit of a DC/DC conversion circuit is in a second working mode according to an embodiment of this application;

[0031] FIG. 7 is a schematic diagram of an inverter according to an embodiment of this application;

[0032] FIG. 8 is a schematic diagram of an inverter according to another embodiment of this application;

[0033] FIG. 9 is a schematic diagram of an inverter according to still another embodiment of this application; and

[0034] FIG. 10 is a schematic diagram of an inverter according to yet still another embodiment of this application.

DETAILED DESCRIPTION

[0035] To enable a reader to better understand a design purpose of the present disclosure, the following specific embodiments are provided, so that the reader can vividly understand a structure, structural composition, a functional principle, and technical effects of the present disclosure.

However, it should be noted that, the following embodiments are not intended to limit a technical solution of the present disclosure. While analyzing and understanding the embodiments, a person skilled in the art may make a series of modifications and equivalent replacement to the technical solution provided in the present disclosure with reference to existing knowledge. A new technical solution derived from the modifications and equivalent replacement is also included in the present disclosure.

[0036] FIG. 1 is a schematic diagram of a DC/DC conversion circuit according to this application.

The DC/DC conversion circuit includes: [0037] a transformer T.sub.1, where the transformer T.sub.1 includes a primary winding r_p and a secondary winding r_s , and the primary winding r_p includes a center tap, and a first primary winding r_{p1} and a second primary winding r_{p2} respectively connected to the center tap; [0038] a primary circuit 100, where a first side of the primary circuit 100 is connected to the primary winding r_p , a second side of the primary circuit 100 includes a first end, a second end, and a third end arranged between the first end and the second end, and the first direct-current voltage is provided between the first end and the second end of the

primary circuit **100**; and [0039] a secondary circuit **200**, where a first side of the secondary circuit **200** is connected to the secondary windings, and a second side of the secondary circuit **200** provides the second direct-current voltage $V_{sub.bat}$, where [0040] the third end of the primary circuit **100** is connected to the center tap, to provide a current loop to balance a voltage between the first end and the third end of the primary circuit **100** and a voltage between the second end and the third end of the primary circuit.

[0041] The primary circuit **100** includes a plurality of switching devices, a first current loop flowing through the first end and the third end of the primary circuit **100** and the center tap, and a second current loop flowing through the center tap and the third end and the second end of the primary circuit **100** are selectively provided by controlling switching of the switching devices, and a direction of the first current loop is opposite to a direction of the second current loop.

[0042] The first primary winding $rp1$ and the second primary winding $rp2$ have a same number of turns.

[0043] As an optional implementation, as shown in FIG. 1, the primary circuit includes a first full bridge. The first full bridge includes a first bridge arm and a second bridge arm connected in parallel between the first end and the second end of the primary circuit **100**.

[0044] The first bridge arm includes a first switching device $Q_{sub.1}$ and a third switching device $Q_{sub.3}$ connected in series. A connection point between the first switching device $Q_{sub.1}$ and the third switching device $Q_{sub.3}$ is used as a midpoint of the first bridge arm and is connected to one end of the first primary winding $rp1$.

[0045] The second bridge arm includes a second switching device $Q_{sub.2}$ and a fourth switching device $Q_{sub.4}$ connected in series. A connection point between the second switching device $Q_{sub.2}$ and the fourth switching device $Q_{sub.4}$ is used as a midpoint of the second bridge arm and is connected to one end of the second primary winding $rp2$. The other end of the first primary winding $rp1$ and the other end of the second primary winding $rp2$ are connected to the center tap.

[0046] The first switching device $Q_{sub.1}$ to the fourth switching device $Q_{sub.4}$ may be MOS transistors or IGBTs. Specifically, the MOS transistor is used as an example in this application. As shown in FIG. 1, a drain of the first switching device $Q_{sub.1}$ is connected to a drain of the second switching device $Q_{sub.2}$. A source of the first switching device $Q_{sub.1}$ is connected to a drain of the third switching device $Q_{sub.3}$, and a connection point is used as the midpoint of the first bridge arm. A source of the second switching device $Q_{sub.2}$ is connected to a drain of the fourth switching device $Q_{sub.4}$, and a connection point is used as the midpoint of the second bridge arm. A source of the third switching device $Q_{sub.3}$ is connected to a source of the fourth switching device $Q_{sub.4}$.

[0047] Further, in the embodiments of this application, the second side of the primary circuit **100** is electrically connected to a bus capacitor. The bus capacitor includes a first voltage-dividing capacitor $C_{sub.1}$ and a second voltage-dividing capacitor $C_{sub.2}$. The first voltage-dividing capacitor $C_{sub.1}$ and the second voltage-dividing capacitor $C_{sub.2}$ are connected in series between the first end and the second end of the primary circuit **100**. A connection point between the first voltage-dividing capacitor $C_{sub.1}$ and the second voltage-dividing capacitor $C_{sub.2}$ is a neutral point of a direct-current bus, and is connected to the center tap of the primary winding rp of the transformer $T_{sub.1}$. The first voltage-dividing capacitor $C_{sub.1}$ and the second voltage-dividing capacitor $C_{sub.2}$ have a same capacitance and a same parameter.

[0048] Further, by selectively controlling the first switching device $Q_{sub.1}$ or the fourth switching device $Q_{sub.4}$ to be turned on, a first current loop flowing through the first primary winding $rp1$, the first switching device $Q_{sub.1}$, and the first voltage-dividing capacitor $C_{sub.1}$, and a second current loop flowing through the second primary winding $rp2$, the fourth switching device $Q_{sub.4}$, and the second voltage-dividing capacitor $C_{sub.2}$ are provided.

[0049] As an optional implementation, by selectively controlling the second switching device $Q_{sub.2}$ or the third switching device $Q_{sub.3}$ to be turned on, a second current loop flowing

through the first primary winding $rp1$, the third switching device $Q.sub.3$, and the second voltage-dividing capacitor $C.sub.2$, and a first current loop flowing through the second primary winding $rp2$, the second switching device $Q.sub.2$, and the first voltage-dividing capacitor $C.sub.1$ are provided.

[0050] If a voltage on the third end shifts, that is, a voltage across the first voltage-dividing capacitor $C.sub.1$ and a voltage across the second voltage-dividing capacitor $C.sub.2$ are different. The difference between the voltage across the first voltage-dividing capacitor $C.sub.1$ and the voltage across the second voltage-dividing capacitor $C.sub.2$, resulting in a current value of the first current loop and a current value of the second current loop are different. A difference current between the two currents flows through the center tap of the transformer $T.sub.1$, and charges or discharges the first voltage-dividing capacitor $C.sub.1$ and the second voltage-dividing capacitor $C.sub.2$, so that the difference between the voltage across the first voltage-dividing capacitor $C.sub.1$ and the voltage across the second voltage-dividing capacitor $C.sub.2$ gradually decreases, until the voltage across the first voltage-dividing capacitor $C.sub.1$ and the voltage across the second voltage-dividing capacitor $C.sub.2$ are equal. Finally, the voltage between the first end and the second end of the primary circuit **100** and the voltage between the second end and the third end of the primary circuit **100** reach a balance.

[0051] As an optional implementation, the second switching device $Q.sub.2$ and the third switching device $Q.sub.3$ or the first switching device $Q.sub.1$ and the fourth switching device $Q.sub.4$ may be replaced by diodes or the like.

[0052] As an optional implementation, the primary circuit **100** may be a half-bridge structure.

[0053] As an optional implementation, as shown in FIG. 1, the secondary circuit **200** includes a second full bridge and a voltage stabilizing capacitor $C.sub.S$. The second full bridge includes a third bridge arm and a fourth bridge arm connected in parallel. The third bridge arm includes a fifth switching device $S.sub.1$ and a seventh switching device $S.sub.3$, and the fourth bridge arm includes a sixth switching device $S.sub.2$ and an eighth switching device $S.sub.4$ connected in series. A connection point between the fifth switching device $S.sub.1$ and the seventh switching device $S.sub.3$ is used as a midpoint of the third bridge arm and is connected to one end of the secondary winding rs . A connection point between the sixth switching device $S.sub.2$ and the eighth switching device $S.sub.4$ is used as a midpoint of the fourth bridge arm and is connected to the other end of the secondary winding rs .

[0054] The fifth switching device $S.sub.1$ to the eighth switching device $S.sub.4$ are MOS transistors or IGBTs. The MOS transistor is used as an example in this application. A drain of the fifth switching device $S.sub.1$ is connected to a drain of the sixth switching device $S.sub.2$, and a source of the fifth switching device $S.sub.1$ is connected to a drain of the seventh switching device $S.sub.3$. A source of the sixth switching device $S.sub.2$ is connected to a drain of the eighth switching device $S.sub.4$, and a source of the seventh switching device $S.sub.3$ is connected to a source of the eighth switching device $S.sub.4$.

[0055] The voltage stabilizing capacitor $C.sub.S$ is connected in parallel with the third bridge arm, and is configured to stabilize the second direct-current voltage $V.sub.bat$ provided on the second side of the secondary circuit **200**.

[0056] In this embodiment, by controlling switching of switching devices in the primary circuit **100** and the secondary circuit **200**, the direct-current conversion is implemented while balancing the voltage between the first end and the third end of the primary circuit **100** and the voltage between the second end and the third end of the primary circuit **100**. This prevents a neutral point voltage shift caused by inconsistent parameters of the capacitors or an external half-wave load, which distorts the output waveforms, reduces the capacitor lifespan and causes overvoltage in some components which damages the equipment.

[0057] As an optional implementation, as shown in FIG. 1, the DC/DC conversion circuit further includes a resonant tank. The resonant tank includes a resonant capacitor $C.sub.r$ and a resonant

inductor, and the resonant inductor includes a first resonant inductor $L_{\text{sub.r1}}$ and a second resonant inductor $L_{\text{sub.r2}}$.

[0058] The resonant capacitor C_r is connected between the secondary circuit **200** and the secondary winding r_s , and the first resonant inductor $L_{\text{sub.r1}}$ and the second resonant inductor $L_{\text{sub.r2}}$ are connected between the primary winding r_p and the primary circuit **100**. Specifically, one end of the first resonant inductor $L_{\text{sub.r1}}$ is connected to the midpoint of the first bridge arm, and the other end of the first resonant inductor $L_{\text{sub.r1}}$ is connected to one end of the first primary winding r_{p1} . One end of the second resonant inductor $L_{\text{sub.r2}}$ is connected to the midpoint of the second bridge arm, and the other end of the second resonant inductor $L_{\text{sub.r2}}$ is connected to one end of the second primary winding r_{p2} .

[0059] As an optional implementation, the resonant inductors also can be arranged between the secondary circuit **200** and the secondary winding r_s .

[0060] An example in which the DC/DC conversion circuit is a bidirectional dual active bridge circuit is used below to describe a working principle of the present disclosure. Various existing control methods may be used to control the dual active bridge circuit, such as a dual phase-shifting control technology. This is not described herein again.

[0061] The bidirectional dual active bridge circuit may work in a boost mode in which power is transferred from a secondary side to a primary side and a buck mode in which power is transferred from the primary side to the secondary side. In this embodiment, an example in which the dual active bridge circuit works in the buck mode in which the power is transferred from the primary side to the secondary side is used. As an optional implementation, control signals of switching devices in the primary circuit **100** are shown in FIG. 2. The first switching device $Q_{\text{sub.1}}$ and the third switching device $Q_{\text{sub.3}}$ are complementarily turned on, and the second switching device $Q_{\text{sub.2}}$ and the fourth switching device $Q_{\text{sub.4}}$ are complementarily turned on. There is a phase shift angle $\Phi_{\text{sub.1}}$ between on signals of the first switching device $Q_{\text{sub.1}}$ and the fourth switching device $Q_{\text{sub.4}}$, as well as between on signals of the second switching device $Q_{\text{sub.2}}$ and the third switching device $Q_{\text{sub.3}}$.

[0062] It may be learnt from the foregoing that, the primary circuit **100** includes four working modes, which are described with reference to FIG. 3 to FIG. 6.

[0063] FIG. 3 shows a first working mode of a primary circuit according to an embodiment of this application. In a first working mode, a first switching device $Q_{\text{sub.1}}$ and a second switching device $Q_{\text{sub.2}}$ are in an on state, and a third switching device $Q_{\text{sub.3}}$ and a fourth switching device $Q_{\text{sub.4}}$ are in an off state. In this case, the primary circuit **100** is freewheeling, and a first voltage-dividing capacitor $C_{\text{sub.1}}$ is discharged, a current loop in the primary circuit **100** is shown in FIG. 3, which includes a third current loop sequentially flowing through the first voltage-dividing capacitor $C_{\text{sub.1}}$, the first switching device $Q_{\text{sub.1}}$, a first resonant inductor $L_{\text{sub.r1}}$, and a first primary winding r_{p1} , and a fourth current loop sequentially flowing through the first voltage-dividing capacitor $C_{\text{sub.1}}$, the second switching device $Q_{\text{sub.2}}$, a second resonant inductor $L_{\text{sub.r2}}$, and a second primary winding r_{p2} . A direction of the third current loop is the same as a direction of the fourth current loop.

[0064] FIG. 4 shows an equivalent circuit diagram of a primary circuit in a first working mode. $I_{\text{sub.rp1}}$ is a current flowing through a first primary winding r_{p1} , $I_{\text{sub.rp2}}$ is a current flowing through a second primary winding r_{p2} , $I_{\text{sub.n1}}$ is a difference current between the current $I_{\text{sub.rp1}}$ and the current $I_{\text{sub.rp2}}$, and directions of arrows indicate reference directions of the currents. In the first working mode, the primary circuit **100** is equivalent to a case in which a first switching device $Q_{\text{sub.1}}$ is connected in series with a first resonant inductor $L_{\text{sub.r1}}$ and then connected in parallel with a first voltage-dividing capacitor $C_{\text{sub.1}}$, and a second switching device $Q_{\text{sub.2}}$ is connected in series with a second resonant inductor $L_{\text{sub.r2}}$ and then connected in parallel with the first voltage-dividing capacitor $C_{\text{sub.1}}$. A secondary winding r_s is converted to the primary side, and its equivalent inductors correspond to the third current loop and the fourth

current loop are L.sub.s1 and L.sub.s2 respectively. Specifically, one end of the first resonant inductor L.sub.r1 is connected to one end of the first voltage-dividing capacitor C.sub.1, and the other end of the first resonant inductor L.sub.r1 is connected to a dotted end of the first primary winding rp1 through the equivalent inductor L.sub.s1. A non-dotted end of the first primary winding rp1 is connected to the other end of the first voltage-dividing capacitor C.sub.1. One end of the second resonant inductor L.sub.r2 is connected to one end of the first voltage-dividing capacitor C.sub.1, and the other end of the second resonant inductor L.sub.r2 is connected to a non-dotted end of the second primary winding rp2 through the equivalent inductor L.sub.s2. A dotted end of the second primary winding rp2 is connected to the other end of the first voltage-dividing capacitor C.sub.1.

[0065] FIG. 5 shows a second working mode of a primary circuit according to an embodiment of this application. In the second working mode, a first switching device Q.sub.1 and a fourth switching device Q.sub.4 are in an on state, and a second switching device Q.sub.2 and a third switching device Q.sub.3 are in an off state. A current loop in the primary circuit **100** is shown in FIG. 5, which includes a first current loop sequentially flowing through a first primary winding rp1, a first resonant inductor L.sub.r1, the first switching device Q.sub.1, and a first voltage-dividing capacitor C.sub.1, and a second current loop flowing through a second primary winding rp2, a second voltage-dividing capacitor C.sub.2, the fourth switching device Q.sub.4, and a second resonant inductor L.sub.r2.

[0066] FIG. 6 shows an equivalent circuit diagram of a primary circuit in a second working mode. I.sub.rp1 is a current flowing through a first primary winding rp1, I.sub.rp2 is a current flowing through a second primary winding rp2, I.sub.n1 is a difference current between the current I.sub.rp1 and the current I.sub.rp2, and directions of arrows indicate reference directions of the currents. In the second working mode, one end of a first resonant inductor L.sub.r1 is connected to one end of a first voltage-dividing capacitor C.sub.1, and the other end of the first resonant inductor L.sub.r1 is connected to a dotted end of the first primary winding rp1 through an equivalent inductor L.sub.s1. A non-dotted end of the first primary winding rp1 is connected to the other end of the first voltage-dividing capacitor C.sub.1. One end of a second resonant inductor L.sub.r2 is connected to a non-dotted end of the second primary winding rp2, and the other end of the second resonant inductor L.sub.r2 is connected to one end of a second voltage-dividing capacitor C.sub.2 through an equivalent inductor L.sub.s2. The other end of the second voltage-dividing capacitor C.sub.2 is connected to a dotted end of the second primary winding rp2.

[0067] The primary circuit provided in the embodiments of this application further includes a third working mode. In the third working mode, a third switching device Q.sub.3 and a fourth switching device Q.sub.4 of the primary circuit are turned on, and a first switching device Q.sub.1 and a second switching device Q.sub.2 are turned off. The third working mode is symmetrical to the first working mode, details are not described herein again.

[0068] The primary circuit provided in the embodiments of this application further includes a fourth working mode. In the fourth working mode, the second switching device Q.sub.2 and the third switching device Q.sub.3 of the primary circuit are turned on, and the first switching device Q.sub.1 and the fourth switching device Q.sub.4 of the primary circuit are turned off. The fourth working mode is symmetrical to the second working mode, details are not described herein again.

[0069] According to above analysis, when the voltage on a third end of a primary circuit in a dual active bridge circuit provided in the embodiments of this application shifts, the voltage balancing can be achieved by the following method.

[0070] When the primary circuit **100** works in the second working mode or the fourth working mode, if the voltage across the first voltage-dividing capacitor C.sub.1 is not equal to the voltage across the second voltage-dividing capacitor C.sub.2, for example, the voltage across the first voltage-dividing capacitor C.sub.1 is greater than the voltage across the second voltage-dividing capacitor C.sub.2. the current of the first current loop is greater than the current of the second

current loop, and the difference current between the two current loops flows through the center tap of the primary winding r_p of the transformer T.sub.1, the first voltage-dividing capacitor C.sub.1 is discharged, and the second voltage-dividing capacitor C.sub.2 is charged, so that the difference between the voltages of the first voltage-dividing capacitor C.sub.1 and the second voltage-dividing capacitor C.sub.2 gradually decreases, until the voltages of the two capacitors tend to be equal, thereby achieving the neutral point voltage balancing. Similarly, when the voltage across the second voltage-dividing capacitor C.sub.2 is greater than the voltage across the first voltage-dividing capacitor C.sub.1, the second voltage-dividing capacitor C.sub.2 is discharged, and the first voltage-dividing capacitor C.sub.1 is charged, so that the difference between the voltages of the second voltage-dividing capacitor C.sub.2 and the first voltage-dividing capacitor C.sub.1 gradually decreases, until the voltages of the two capacitors tend to be equal.

[0071] In summary, this application proposes a DC/DC conversion circuit. The primary winding of the transformer of the DC/DC conversion circuit has a center tap. The center tap is connected to a neutral point of the direct-current bus. When the neutral point voltage of the direct-current bus on the direct-current side of the DC/DC conversion circuit shifts, the neutral point voltage can be adjusted to achieve balance. This solution does not require adding an additional component or a complex control method, and has a good practical value.

[0072] As an optional implementation, the embodiments of this application further provide an inverter, where the inverter includes the DC/DC conversion circuit as described above and a multi-level inverter circuit **300**.

[0073] A direct-current side of the multi-level inverter circuit **300** is electrically connected to a second side of a primary circuit of the DC/DC conversion circuit, for example, through a direct-current bus, and an alternating current side of the multi-level inverter circuit, for example, is connected to an alternating current power grid, provides an alternating current output.

[0074] Further, the inverter further includes a bus capacitor, which is connected between the direct-current bus, and a neutral point of the direct-current bus is connected to a neutral point of the multi-level inverter circuit.

[0075] FIG. 7 is a schematic diagram of an inverter according to an implementation of this application. A multi-level inverter circuit **300** is a T-type three-level inverter circuit, and includes four switching devices. A first switching device S.sub.A1 and a second switching device S.sub.A2 are connected in series and are connected between a first end and a second end of a primary circuit **100**. A connection point between the first switching device S.sub.A1 and the second switching device S.sub.A2 is used as a first output end of the multi-level inverter circuit **300**, and, for example, is connected to an alternating current power grid through an inverter inductor L.sub.XA. A third switching device S.sub.A3 and a fourth switching device S.sub.A4 are connected in anti-series. A first end of the third switching device S.sub.A3 is connected to a third end of the primary circuit **100** and is used as a second output end of the multi-level inverter circuit **300**, for example, is connected to a neutral wire of the alternating current power grid. A second end of the third switching device S.sub.A3 is connected to a second end of the fourth switching device S.sub.A4, and a first end of the fourth switching device S.sub.A4 is connected to the connection point between the first switching device S.sub.A1 and the second switching device S.sub.A2. An alternating current output is provided between the first output end and the second output end of the multi-level inverter circuit **300**.

[0076] Specifically, in the embodiments of this application, each switching device includes an IGBT and a freewheeling diode connected in anti-parallel with the IGBT. The first switching device S.sub.A1 is used as an example, which includes a first IGBT and a first freewheeling diode. A collector of the first IGBT is connected to a cathode of the first freewheeling diode, and an emitter of the first IGBT is connected to an anode of the first freewheeling diode.

[0077] According to the foregoing analysis, it may be learnt that, when parameters of the capacitor are inconsistent, or there is an external half-wave load, causing a neutral point voltage shift of the

inverter, a current loop between the neutral point of the direct-current bus of the inverter and the center tap of the transformer T1 can balance the neutral point voltage of the direct-current bus, to prevent output waveforms from being distorted, the capacitor lifespan from being reduced, and overvoltage in some components which damages the equipment.

[0078] Further, the inverter in the embodiments of this disclosure multiplexes a DC/DC conversion circuit, which can implement direct-current conversion and balance the neutral point voltage when direct-current conversion is performed without an additional balancing bridge or a complex control algorithm. This reduces costs and control difficulty.

[0079] FIG. 8 is a schematic diagram of an inverter according to another implementation of this application. A multi-level inverter circuit 300 is a three-phase inverter circuit, which includes three T-type three-level inverter circuits. The T-type three-level inverter circuit in this implementation is similar to that in a previous implementation and is not described herein again.

[0080] FIG. 9 is a schematic diagram of an inverter according to still another implementation of this application. A multi-level inverter circuit 300 is a diode-clamped three-level inverter circuit, which includes two clamping diodes and a first switching device S.sub.A1 to a fourth switching device S.sub.A4 connected in series between the first end and the second end of the primary circuit 100. The first switching device S.sub.A1 and the third switching device S.sub.A3 are connected in series to form a positive half-bridge arm, and the second switching device S.sub.A2 and the fourth switching device S.sub.A4 are connected in series to form a negative half-bridge arm. A connection point between the positive half-bridge arm and the negative half-bridge arm is used as a first output end of the multi-level inverter circuit 300. The two clamping diodes are connected in series and then are connected between switching devices in the positive half-bridge arm and switching devices in the negative half-bridge arm for clamping. A connection point between the two clamping diodes is connected to the third end of the primary circuit 100 and is used as a second output end of the multi-level inverter circuit 300. An alternating current output is provided between the first output end and the second output end of the multi-level inverter circuit 300.

[0081] FIG. 10 is a schematic diagram of an inverter according to yet still another implementation of this application. A multi-level inverter circuit 300 is a five-level inverter circuit, which includes eight switching devices and one clamping capacitor C.sub.f.

[0082] A first switching device S.sub.A1 to a fourth switching device S.sub.A4 are connected in series and are connected between a first end and a second end of a primary circuit 100, and a fifth switching device S.sub.A5 and a sixth switching device S.sub.A6 are connected in anti-series. A first end of the fifth switching device SAS is connected to a third end of the primary circuit 100, and as a first output end of the multi-level inverter circuit 300, a second end of the fifth switching device S.sub.A5 is connected to a second end of the sixth switching device S.sub.A6. A first end of the sixth switching device S.sub.A6 is connected to a connection point between the second switching device S.sub.A2 and the third switching device S.sub.A3.

[0083] A first end of the clamping capacitor C.sub.f is connected to a connection point between the first switching device S.sub.A1 and the second switching device S.sub.A2, and a second end of the clamping capacitor C.sub.f is connected to a connection point between the third switching device S.sub.A3 and the fourth switching device S.sub.A4. A seventh switching device S.sub.A7 and an eighth switching device S.sub.A8 are connected in series and then connected in parallel with the clamping capacitor C.sub.f. A connection point between the seventh switching device S.sub.A7 and the eighth switching device S.sub.A8 is used as a second output end of the multi-level inverter circuit 300. An alternating current output is provided between the first output end and the second output end of the multi-level inverter circuit 300.

[0084] In summary, the embodiments of this application provide an inverter, including a DC/DC conversion circuit and a multi-level inverter circuit. A primary winding of a transformer of the DC/DC conversion circuit has a center tap, and the center tap is connected to a neutral point of a direct-current bus. The inverter in the present disclosure multiplexes the DC/DC conversion circuit,

which implements direct-current conversion and balances the neutral point voltage the same time without an additional balancing bridge or a complex control algorithm. This reduces costs and control difficulty, and also has the advantages of reducing harmonic content that multi-level inverter circuits have.

[0085] As an optional implementation, the embodiments of this application further provide a method for neutral point voltage balancing for an inverter, where the inverter includes the DC/DC conversion circuit as described above, and the method includes: connecting the center tap of the transformer of the DC/DC conversion circuit in the inverter to the neutral point of the inverter, and providing a current loop to balance a neutral point voltage of the inverter. The neutral point voltage balancing can be achieved without an additional balancing bridge or a complex control algorithm. This reduces costs and control difficulty.

It should be understood that, a person of ordinary skill in the art may make improvements or variations according to the foregoing descriptions, and such improvements and variations shall all fall within the protection scope of the appended claims of the present disclosure. Accompanying drawings corresponding to specific implementations are provided to assist understanding, making it easier for a reader to fully understand abstract generic terms of technical concepts involved in the present disclosure by understanding concrete terms. When comprehensively understanding the present disclosure and comparing it with technical solutions other than those provided by the present disclosure, appearance of the accompanying drawings should not be used as the only reference basis. After the concept of the present disclosure is understood, a series of modifications, equivalent replacement, blending of features, deletion and reorganization of non-essential technical features, proper addition and reorganization of non-essential technical features common in the related art, and the like made in accordance with the accompanying drawings or not in accordance with the accompanying drawings should be understood as being included within the spirit of the present disclosure.

Claims

1. A DC/DC conversion circuit, configured to provide direct-current conversion between a first direct-current voltage and a second direct-current voltage, comprising: a transformer, wherein the transformer comprises a primary winding and a secondary winding, and the primary winding comprises a center tap, and a first primary winding and a second primary winding respectively connected to the center tap; a primary circuit, wherein a first side of the primary circuit is connected to the primary winding, a second side of the primary circuit comprises a first end, a second end, and a third end arranged between the first end and the second end, and the first direct-current voltage is provided between the first end and the second end of the primary circuit; and a secondary circuit, wherein a first side of the secondary circuit is connected to the secondary winding, and a second side of the secondary circuit provides the second direct-current voltage, wherein the third end of the primary circuit is connected to the center tap, to provide a current loop to balance a voltage between the first end and the third end of the primary circuit and a voltage between the second end and the third end of the primary circuit.
2. The DC/DC conversion circuit according to claim 1, wherein the primary circuit comprises a plurality of switching devices, a first current loop flowing through the first end and the third end of the primary circuit and the center tap, and a second current loop flowing through the center tap and the third end and the second end of the primary circuit are selectively provided by controlling switching of the switching devices, and a direction of the first current loop is opposite to a direction of the second current loop.
3. The DC/DC conversion circuit according to claim 1, wherein the first primary winding and the second primary winding have a same number of turns.
4. The DC/DC conversion circuit according to claim 1, wherein the primary circuit is a full-bridge

structure or a half-bridge structure, the secondary circuit is a full-bridge structure.

5. The DC/DC conversion circuit according to claim 1, further comprising: a resonant tank, wherein the resonant tank comprises a resonant capacitor, a first resonant inductor, and a second resonant inductor, wherein the resonant capacitor is connected between the secondary circuit and the secondary winding, and the first resonant inductor and the second resonant inductor are connected between the secondary circuit and the secondary winding or connected between the primary winding and the primary circuit.

6. The DC/DC conversion circuit according to claim 1, wherein the secondary circuit is a full-bridge structure.

7. An inverter, wherein the inverter comprises a multi-level inverter circuit and a DC/DC conversion circuit, a direct-current side of the multi-level inverter circuit is electrically connected to a second side of a primary circuit of the DC/DC conversion circuit, and an alternating current side of the multi-level inverter circuit provides an alternating current output; and the DC/DC conversion circuit is configured to provide direct-current conversion between a first direct-current voltage and a second direct-current voltage, and the DC/DC conversion circuit comprises: a transformer, wherein the transformer comprises the primary winding and a secondary winding, and the primary winding comprises a center tap, and a first primary winding and a second primary winding respectively connected to the center tap; a primary circuit, wherein a first side of the primary circuit is connected to the primary winding, a second side of the primary circuit comprises a first end, a second end, and a third end arranged between the first end and the second end, and the first direct-current voltage is provided between the first end and the second end of the primary circuit; and winding, and a second side of the secondary circuit provides the second direct-current voltage, wherein the third end of the primary circuit is connected to the center tap, to provide a current loop to balance a voltage between the first end and the third end of the primary circuit and a voltage between the second end and the third end of the primary circuit.

8. The inverter according to claim 7, wherein the multi-level inverter circuit is a T-type multi-level inverter circuit or a diode-clamped multi-level inverter circuit.

9. The inverter according to claim 7, wherein the inverter further comprises a first voltage-dividing capacitor and a second voltage-dividing capacitor connected in series between the first end and the second end of the primary circuit, and a connection point between the first voltage-dividing capacitor and the second voltage-dividing capacitor is connected to the center tap and a neutral point of the multi-level inverter circuit.

10. The inverter according to claim 7, wherein the inverter is a three-phase inverter, comprising three multi-level inverter circuits.

11. The inverter according to claim 7, wherein the primary circuit comprises a plurality of switching devices, a first current loop flowing through the first end and the third end of the primary circuit and the center tap, and a second current loop flowing through the center tap and the third end and the second end of the primary circuit are selectively provided by controlling switching of the switching devices, and a direction of the first current loop is opposite to a direction of the second current loop.

12. The inverter according to claim 7, wherein the first primary winding and the second primary winding have a same number of turns.

13. The inverter according to claim 7, wherein the primary circuit is a full-bridge structure or a half-bridge structure.

14. The inverter according to claim 7, wherein the DC/DC conversion circuit further comprises: a resonant tank, wherein the resonant tank comprises a resonant capacitor, a first resonant inductor, and a second resonant inductor, wherein the resonant capacitor is connected between the secondary circuit and the secondary winding, and the first resonant inductor and the second resonant inductor are connected between the secondary circuit and the secondary winding or connected between the primary winding and the primary circuit.

- 15.** The inverter according to claim 7, wherein the secondary circuit is a full-bridge structure.
- 16.** A method for neutral point voltage balancing for an inverter, wherein the inverter comprises the DC/DC conversion circuit according to claim 1, and the method comprises: connecting the center tap of the transformer of the DC/DC conversion circuit in the inverter to the neutral point of the inverter, and providing a current loop to balance a neutral point voltage of the inverter.
-