

# Multibody System Dynamics: MBDyn Hydraulics Modeling



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### **Outline**

- Introduction
- Modeling Scales
- Multibody/Multiphysics Dynamics:
  - MBDyn Software
  - Modeling Approach
- Hydraulic Library Overview
- Examples

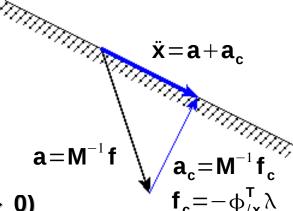
Multibody Dynamics: unconstrained mechanical systems...

$$M(x)\ddot{x} = f(x,\dot{x},t)$$

... plus kinematic constraints: constrained mechanical systems

$$\mathbf{M}(\mathbf{x})\ddot{\mathbf{x}} + \boldsymbol{\varphi}_{/\mathbf{x}}^{\mathsf{T}} \lambda = \mathbf{f}(\mathbf{x}, \dot{\mathbf{x}}, \mathbf{t})$$
$$\boldsymbol{\varphi}(\mathbf{x}, \mathbf{t}) = 0$$

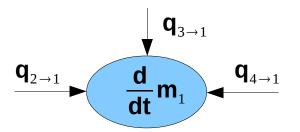
 System of differential-algebraic equations (DAE)



- Infinitely "fast" dynamics (time scale → 0)
- Requires unconditionally stable integration, algorithmic dissipation
   → implicit A/L-stable schemes

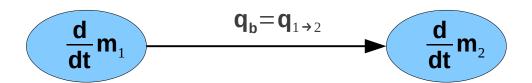
- Hydraulic system dynamics:
  - approximate or neglect local dynamics
  - spatial resolution: 0D & 1D
  - circuit theory: node pressures, branch flows
- Flow balance at nodes

$$\sum q_b = \frac{d}{dt}m_n$$

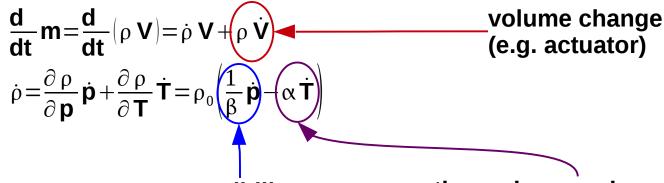


Constitutive properties of branches (e.g. pressure loss)

$$\Psi(\mathbf{q}_{b},\dot{\mathbf{q}}_{b},\mathbf{p}_{n1},\dot{\mathbf{p}}_{n1},\mathbf{p}_{n2},\dot{\mathbf{p}}_{n2},\mathbf{t})=0$$



Constitutive properties of fluid: linearization about reference condition



compressibility can be neglected if:

- m small
- bulk modulus large
- pressure rate small

thermal expansion can be neglected if:

- m small
- coefficient small
- temperature rate small

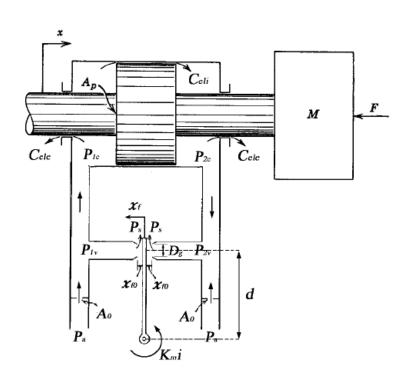
$$\frac{d}{dt}m = \frac{m}{\beta}\dot{p} - m\dot{T} + \rho\dot{V}$$

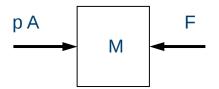
assume temperature rate small compared to time scale of hydro-mechanical processes



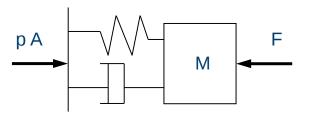
- Multiphysics problem: interaction between different domains (e.g. mechanical and hydraulic)
- Interaction described in terms of:
  - Frequency, bandwidth (how rapid phenomena are)
  - Power (how much work is transferred between domains)
- Determine how interaction can be simplified:
  - Truncation
  - Steady approximation
  - Quasi-steady approximation
  - Complete dynamics coupling

Example: actuator





truncated model: commanded force independed from dynamics



(quasi-)static model: commanded force depends on dynamics approx. as mass-spring-damper

Coupled dynamic problem: state-space representation (e.g. linear)

$$\dot{x} = Ax + Bu$$
  
 $y = Cx + Du$ 

States partitioned based on frequency separation ("slow" vs. "fast"):

$$\begin{vmatrix} \dot{\mathbf{x}}_{s} \\ \dot{\mathbf{x}}_{f} \end{vmatrix} = \begin{bmatrix} \mathbf{A}_{ss} & \mathbf{A}_{sf} \\ \mathbf{A}_{fs} & \mathbf{A}_{ff} \end{bmatrix} \begin{bmatrix} \mathbf{x}_{s} \\ \mathbf{x}_{f} \end{bmatrix} + \begin{bmatrix} \mathbf{B}_{s} \\ \mathbf{B}_{f} \end{bmatrix} \mathbf{u}$$

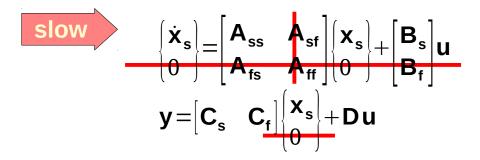
$$\mathbf{y} = \begin{bmatrix} \mathbf{C}_{s} & \mathbf{C}_{f} \end{bmatrix} \begin{bmatrix} \mathbf{X}_{s} \\ \mathbf{X}_{f} \end{bmatrix} + \mathbf{D}\mathbf{u}$$

 Approximations consist in reducing the system to the "slow" dynamics while preserving information about the "fast" dynamics

## **Approximations**

MBDyn

Truncation: only consider "slow" states



Reduced system:

$$\dot{x}_s = A_{ss} x_s + B_s u$$
  
 $y = C_s x_s + Du$ 



Steady approximation: statically approximate "fast" states

$$\frac{\begin{vmatrix} \dot{\mathbf{x}}_{s} \\ \mathbf{0} \end{vmatrix} = \begin{bmatrix} \mathbf{A}_{ss} & \mathbf{A}_{sf} \\ \mathbf{A}_{fs} & \mathbf{A}_{ff} \end{bmatrix} \begin{bmatrix} \mathbf{x}_{s} \\ \mathbf{x}_{f} \end{bmatrix} + \begin{bmatrix} \mathbf{B}_{s} \\ \mathbf{B}_{f} \end{bmatrix} \mathbf{u}}{\mathbf{y} = \begin{bmatrix} \mathbf{C}_{s} & \mathbf{C}_{f} \end{bmatrix} \begin{bmatrix} \mathbf{X}_{s} \\ \mathbf{X}_{f} \end{bmatrix} + \mathbf{D}\mathbf{u}}$$

Reduced system:

$$\begin{split} \dot{\mathbf{x}}_{s} &= \left(\mathbf{A}_{ss} - \mathbf{A}_{sf} \, \mathbf{A}_{ff}^{-1} \, \mathbf{A}_{fs}\right) \mathbf{x}_{s} + \left(\mathbf{B}_{s} - \mathbf{A}_{sf} \, \mathbf{A}_{ff}^{-1} \, \mathbf{B}_{f}\right) \mathbf{u} \\ \mathbf{x}_{f} &= -\mathbf{A}_{ff}^{-1} \, \mathbf{A}_{fs} \, \mathbf{x}_{s} - \mathbf{A}_{ff}^{-1} \, \mathbf{B}_{f} \, \mathbf{u} \\ \mathbf{y} &= \left(\mathbf{C}_{s} - \mathbf{C}_{f} \, \mathbf{A}_{ff}^{-1} \, \mathbf{A}_{fs}\right) \mathbf{x}_{s} + \left(\mathbf{D} - \mathbf{C}_{f} \, \mathbf{A}_{ff}^{-1} \, \mathbf{B}_{f}\right) \mathbf{u} \end{split}$$

Note: the original system becomes differential-algebraic (DAE)
 of index 1, thus reducible to ODE by direct substitution

- Quasi-steady approximation: use low-order dynamics
- In Laplace's domain:

$$y(s) = \left(C(sI - A)^{-1}B + D\right)u(s) = H(s)u(s)$$

$$y(s) \approx \left(H(0) + s\left(\frac{dH}{ds}\right)_{s=0} + \frac{s^2}{2}\left(\frac{d^2H}{ds^2}\right)_{s=0} + \dots + \frac{s^n}{n!}\left(\frac{d^nH}{ds^n}\right)_{s=0}\right)u(s)$$

$$H(0) = -CA^{-1}B + D$$

$$H'(0) = -CA^{-2}B$$

$$H''(0) = -2CA^{-3}B$$

$$\dots$$

$$H^{(n)}(0) = -(n!)CA^{-(n+1)}B$$

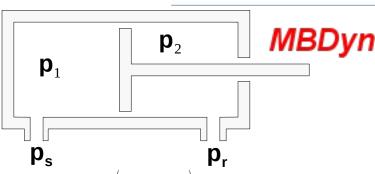
Back to time domain:

$$y(t) = H(0)u(t) + H'(0)\dot{u}(t) + \frac{1}{2}H''(0)\ddot{u}(t) + ...$$

 Note: time derivative of input! (Only makes sense when u is state of interacting system)

## **Approximations**

#### **12**



### **Example: actuator; equations:**

Flow balance in chamber 1

Flow balance in chamber 1 
$$p_s$$
  
 $V_1/\beta \dot{p}_1 = -A_p \dot{x} - C_{eli} A_{eli} (p_1 - p_2) - C_{ele} A_{ele} p_1 - C_{els} A_{els} (p_s - p_1)$ 

Flow balance in chamber 2

$$V_2/\beta \dot{p}_2 = +A_p \dot{x} - C_{eli} A_{eli} (p_2 - p_1) - C_{ele} A_{ele} p_2 - C_{elr} A_{elr} (p_2 - p_r)$$

Equilibrium of piston

$$\mathbf{m}\ddot{\mathbf{x}} = \mathbf{A}_{\mathbf{p}}(\mathbf{p}_1 - \mathbf{p}_2) - r\dot{\mathbf{x}} + \mathbf{F}$$

State-space realization

$$\begin{vmatrix} \dot{\boldsymbol{p}}_1 \\ \dot{\boldsymbol{p}}_2 \\ \dot{\boldsymbol{x}} \\ \dot{\boldsymbol{v}} \end{vmatrix} = \begin{bmatrix} -\boldsymbol{C}_{\boldsymbol{e}\boldsymbol{1}\boldsymbol{1}}\boldsymbol{\beta}/\boldsymbol{V}_1 & \boldsymbol{C}_{\boldsymbol{e}\boldsymbol{1}\boldsymbol{2}}\boldsymbol{\beta}/\boldsymbol{V}_1 & 0 & -\boldsymbol{A}_{\boldsymbol{p}}\boldsymbol{\beta}/\boldsymbol{V}_1 \\ \boldsymbol{C}_{\boldsymbol{e}\boldsymbol{1}\boldsymbol{2}}\boldsymbol{\beta}/\boldsymbol{V}_2 & -\boldsymbol{C}_{\boldsymbol{e}\boldsymbol{2}\boldsymbol{2}}\boldsymbol{\beta}/\boldsymbol{V}_2 & 0 & \boldsymbol{A}_{\boldsymbol{p}}\boldsymbol{\beta}/\boldsymbol{V}_2 \\ 0 & 0 & 0 & 1 \\ \boldsymbol{A}_{\boldsymbol{p}}/\boldsymbol{m} & -\boldsymbol{A}_{\boldsymbol{p}}/\boldsymbol{m} & 0 & -\boldsymbol{r}/\boldsymbol{m} \end{bmatrix} \begin{pmatrix} \boldsymbol{p}_1 \\ \boldsymbol{p}_2 \\ \boldsymbol{x} \\ \boldsymbol{v} \end{pmatrix} + \begin{pmatrix} \boldsymbol{C}_{\boldsymbol{e}\boldsymbol{1}\boldsymbol{0}}\boldsymbol{\beta}/\boldsymbol{V}_1 \boldsymbol{p}_s \\ \boldsymbol{C}_{\boldsymbol{e}\boldsymbol{2}\boldsymbol{0}}\boldsymbol{\beta}/\boldsymbol{V}_2 \boldsymbol{p}_r \\ 0 \\ \boldsymbol{F}/\boldsymbol{m} \end{pmatrix}$$

## **Approximations**

# MBDyn

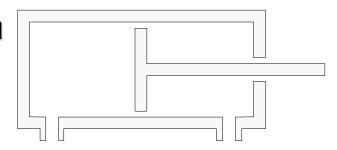
### Truncation approximation:

• Neglect hydraulics (velocities small, infinite power available)

$$m\ddot{x} = A_p(p_s - p_r) - r\dot{x} + F$$

Directly control the force exerted by the fluid

$$\begin{bmatrix} \dot{\mathbf{x}} \\ \dot{\mathbf{v}} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & -\mathbf{r}/\mathbf{m} \end{bmatrix} \begin{bmatrix} \mathbf{x} \\ \mathbf{v} \end{bmatrix} + \begin{bmatrix} 0 \\ \mathbf{A}_{\mathbf{p}}/\mathbf{m}(\mathbf{p}_{s} - \mathbf{p}_{r}) + \mathbf{F}/\mathbf{m} \end{bmatrix}$$



### **Static approximation:**

Neglect compressibility (volume is small, bulk modulus is high)

$$\begin{array}{ll} 0\!\simeq\!\!-\,\mathbf{A_p}\,\dot{\mathbf{x}}\!-\!\mathbf{C_{eli}}\,\mathbf{A_{eli}}\big(\mathbf{p}_1\!-\!\mathbf{p}_2\big)\!-\!\mathbf{C_{ele}}\,\mathbf{A_{ele}}\,\mathbf{p}_1\!-\!\mathbf{C_{els}}\,\mathbf{A_{els}}\big(\mathbf{p}_s\!-\!\mathbf{p}_1\big) \\ 0\!\simeq\!\!+\,\mathbf{A_p}\,\dot{\mathbf{x}}\!-\!\mathbf{C_{eli}}\,\mathbf{A_{eli}}\big(\mathbf{p}_2\!-\!\mathbf{p}_1\big)\!-\!\mathbf{C_{ele}}\,\mathbf{A_{ele}}\,\mathbf{p}_2\!-\!\mathbf{C_{elr}}\,\mathbf{A_{elr}}\big(\mathbf{p}_2\!-\!\mathbf{p}_r\big) \\ \mathbf{m}\,\ddot{\mathbf{x}}\!=\!\mathbf{A_p}\big(\mathbf{p}_1\!-\!\mathbf{p}_2\big)\!-\!r\,\dot{\mathbf{x}}\!+\!\mathbf{F} \end{array} \Rightarrow \!\mathbf{p}_1,\;\; \mathbf{p}_2\!\div\!\dot{\mathbf{x}}$$

Pressure depends on velocity: → equivalent damping

- AMESim:
  - Monolithic software (can be interfaced as dynamic module to other solvers)
  - Models hydraulic networks in detail
- ADAMS:
  - Module for basic solver
  - Introduces modeling capabilities of hydraulic components
- Modelica (Dymola, MathModelica, OpenModelica?)
  - Modeling language, based on open library of elements
  - Broad library for general-purpose components
  - Many fields, including hydraulics and multibody
  - Needs specific (closed) solver
- MBDyn



- MBDyn:
- Developed at Dipartimento di Ingegneria Aerospaziale, Politecnico di Milano
- Monolithic multibody/multiphysics general-purpose software
- It's free: released under GPL (GNU General Public License)
- Includes integrated hydraulic library

### **Software**

- Web site: <a href="http://www.mbdyn.org/">http://www.mbdyn.org/</a>
- Distributed as source code
- Developed for Linux
- Needs Un\*x-like build environment
  - Linux
  - Linux in virtual machine
  - MSYS/MinGW in windows
  - Cygwin in windows

- Command-line software
- Prepare an input file using your favourite text editor
- Execute:

```
# mbdyn -f input_file -o output_file_prefix
```

- Output in files with specific extensions
- Load output files in math environment (octave, scilab, matlab, ...)
   for plotting and further manipulation

### **Software**

**MBDyn** 

- Output can be reformatted for some post-processing tools
  - built-in: EasyAnim
  - ...
- Ongoing third-party project ("Blender & MBDyn") about using Blender <a href="http://www.blender.org/">http://www.blender.org/</a> for pre/post-processing:

http://www.baldwintechnology.com/



- The model and the analysis are defined in a textual input file
- Use your preferred editor to prepare the input file
- The structure and the syntax of the statements are described here http://www.mbdyn.org/ → Download (pick the manual for the version in use, or follow instructions)
- A set of tutorials and other documentation is presented here http://www.mbdyn.org/ → Documentation including example input files

- Nodes instantiate degrees of freedom and the corresponding balance equations
- Static structural nodes only instantiate equilibrium equations

$$0 = \sum_{\mathbf{m}} \mathbf{f}$$
$$0 = \sum_{\mathbf{m}} \mathbf{m}$$

Dynamic structural nodes also instantiate momentum and momenta moment definitions

$$\mathbf{M} \dot{\mathbf{x}} = \beta$$

$$\mathbf{J} \boldsymbol{\omega} = \gamma$$

$$\dot{\boldsymbol{\beta}} = \sum_{\mathbf{f}} \mathbf{f}$$

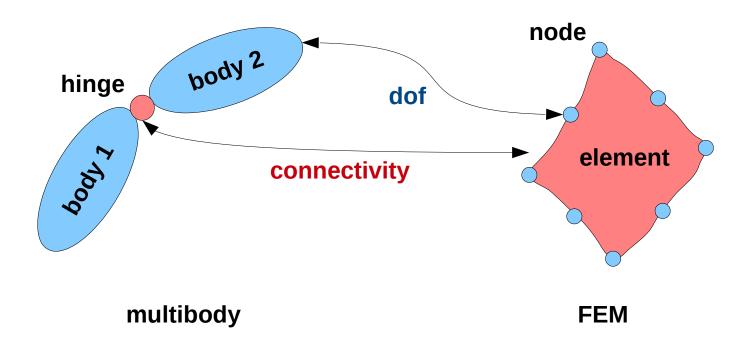
$$\dot{\boldsymbol{\gamma}} = \sum_{\mathbf{m}} \mathbf{m}$$

Hydraulic nodes (pressure) instantiate flow balance equations

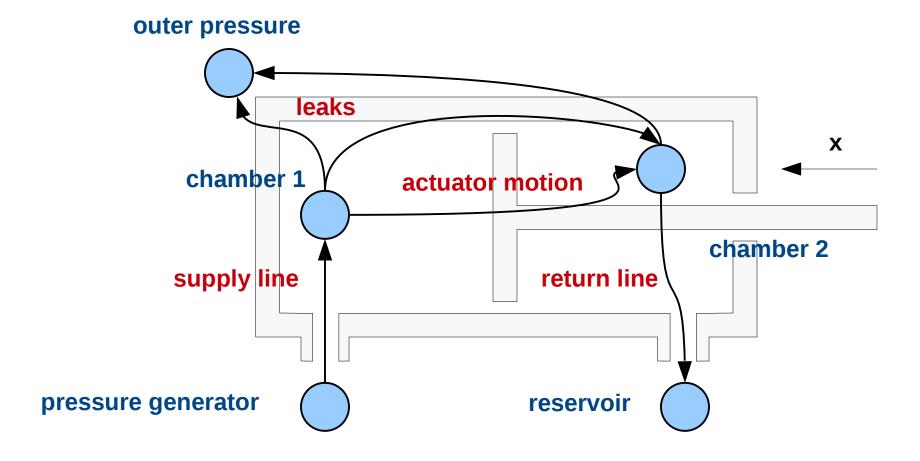


- Elements write contributions to equations instantiated by nodes
- Elements represent "connectivity" and "constitutive properties"
- Elements can add further, "private" equations and variables (e.g. algebraic constraints and Lagrange multipliers)
- Mechanical elements typically add forces and moments to equilibrium equations
- Mechanical constraints ("joints") may add algebraic relationships between kinematic degrees of freedom
- Hydraulic elements typically add flow contributions to flow balance equations in nodes

 Multibody vs. FEM: nodes at bodies vs. nodes at frontier (node → body; element → hinge)



Hydraulic modeling: network



# Hydraulic Element Library: Pressure Generator

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- Not specifically implemented; use a "clamp" genel instead
- This element adds a scalar algebraic equation that enforces a specific value (possibly time-dependent) on a scalar node

$$\mathbf{p} = \mathbf{p}_0(\mathbf{t})$$

 This algebraic equation implies a Lagrange multiplier on the flow balance equation related to the pressure node

$$\sum \mathbf{q} + \lambda = 0$$

 The Lagrange multiplier represents the flow required to grant the imposed pressure value

# Hydraulic Element Library: Imposed Flow



- Not specifically implemented, use an "abstract" force instead
- This element adds a contribution, possibly time-dependent, to an arbitrary scalar equation

$$q=q(t)$$

 Note: in MBDyn, a negative flow enters the circuit at the given node, a positive flow leaves the circuit at the given node

# Hydraulic Element Library: Dynamic Pipeline



- Dynamic pipes are formulated using a finite-volume approach
- Degenerate into static when pressure time derivatives neglected
- Differential mass balance:

$$\frac{\mathbf{D}}{\mathbf{D}\mathbf{t}}\mathbf{dm} = 0 \rightarrow \mathbf{q}_{/\mathbf{x}} + \mathbf{A} \, \rho_{/\mathbf{t}} = 0$$

Differential momentum balance:

$$\frac{\mathbf{D}}{\mathbf{D}\mathbf{t}}\mathbf{d}\mathbf{q} = \mathbf{d}\mathbf{f} \rightarrow \mathbf{q}_{/\mathbf{t}} + \left(\frac{\mathbf{q}^2}{\rho \mathbf{A}} + \mathbf{A} \mathbf{p}\right)_{/\mathbf{x}} = \mathbf{f}_{\mathbf{v}}$$

Discretization:

$$\mathbf{q}(\mathbf{x},\mathbf{t}) = \begin{bmatrix} \frac{1-\xi}{2} & \frac{1+\xi}{2} \end{bmatrix} \begin{bmatrix} \mathbf{q}_1(\mathbf{t}) \\ \mathbf{q}_2(\mathbf{t}) \end{bmatrix}$$

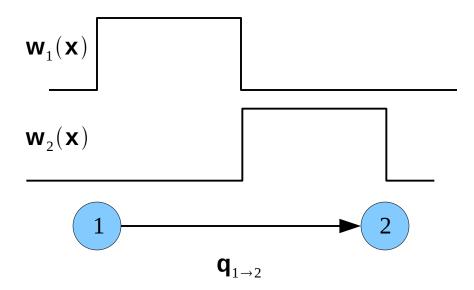
$$\mathbf{p}(\mathbf{x},\mathbf{t}) = \begin{bmatrix} \frac{1-\xi}{2} & \frac{1+\xi}{2} \end{bmatrix} \begin{bmatrix} \mathbf{p}_1(\mathbf{t}) \\ \mathbf{p}_2(\mathbf{t}) \end{bmatrix}$$

$$\mathbf{x} = \mathbf{x}(\xi)$$

# Hydraulic Element Library: Dynamic Pipeline



- Piecewise-constant weight functions:
- Weight the mass and momentum balance equations
- Four constitutive equations in pressure and flow at nodes



## **Example: Pressure Wave in Pipeline**

MBDyn

 From: R. Piché, A. Ellman, "A Fluid Transmission Line Model for Use with ODE Simulators", 8<sup>th</sup> Bath International Fluid Power Workshop, Sep. 20-22 1995, University of Bath, UK

Length: 19.74 m

• Radius: 6.17e-3 m

Density: 870 kg/m<sup>3</sup>

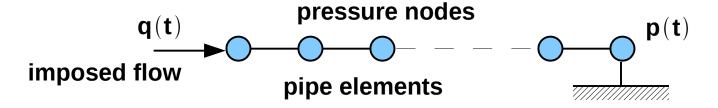
Viscosity: 8.e-5 m^2/s

Sound celerity: 1.4e3 m/s

Impulsive flow: 0.001 m^3/s

Duration: 0.1e-3 s

Impulsive dynamics

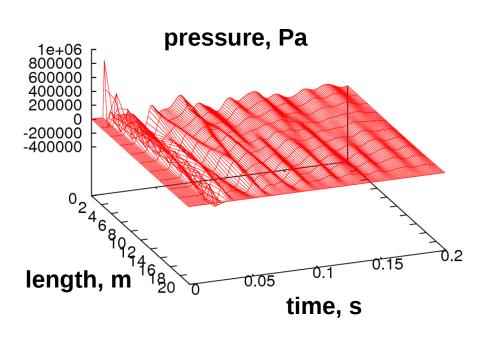


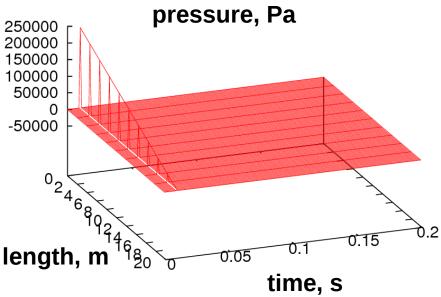
imposed pressure

## **Example: Pressure Wave in Pipeline**

MBDyn

Dynamic pipe (10 "dynamic pipe" elements)
 compared to static pipe, "impulsive" flow input:

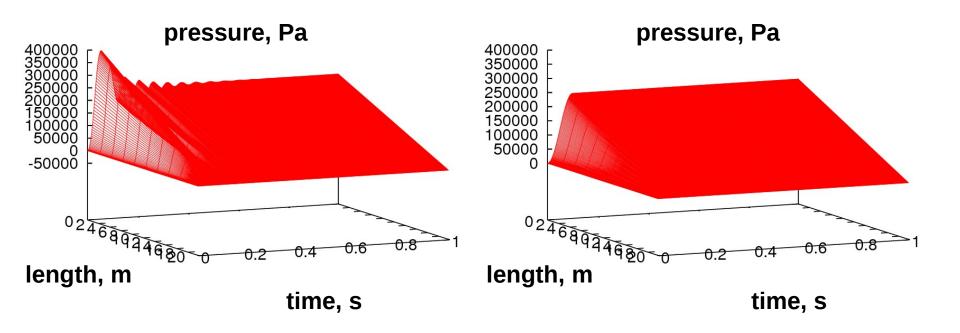




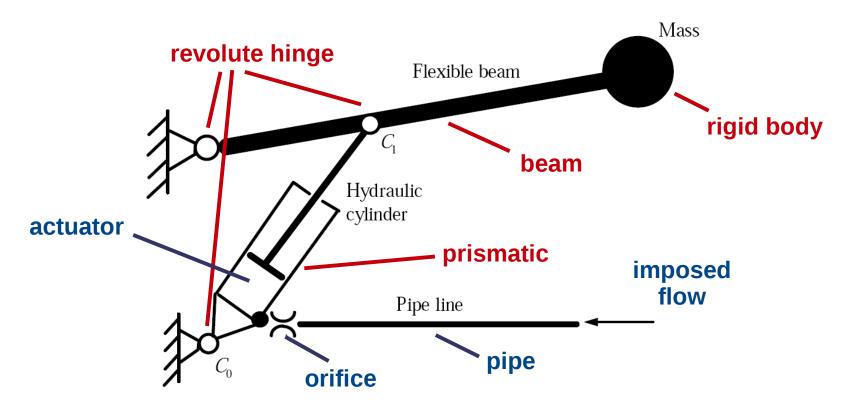
## **Example: Pressure Wave in Pipeline**

**MBDyn** 

Dynamic pipe (10 "dynamic pipe" elements)
 compared to static pipe, "smooth" flow input:



 From: J. Mäkinen, A. Ellman, R. Piché, "Dynamic Simulations of Flexible Hydraulic-Driven Multibody Systems using Finite Strain Beam Theory", 5<sup>th</sup> Scandinavian International Conference on Fluid Power, Linköping, 1997, Sweden

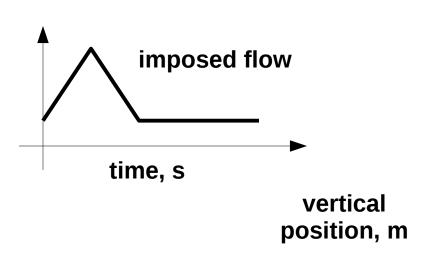


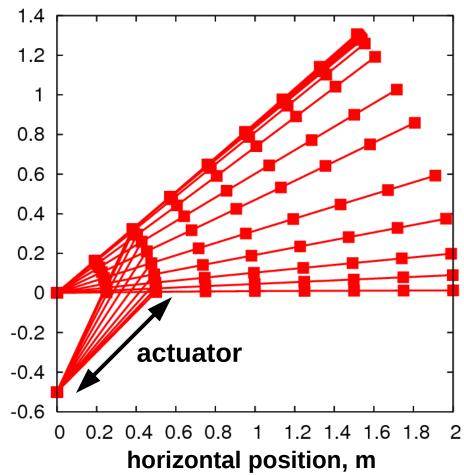
Input file: https://www.mbdyn.org/userfiles/documents/examples/actuator

## **Example: Hydraulically Actuated Beam**

**MBDyn** 

#### 4 3-node beam elements

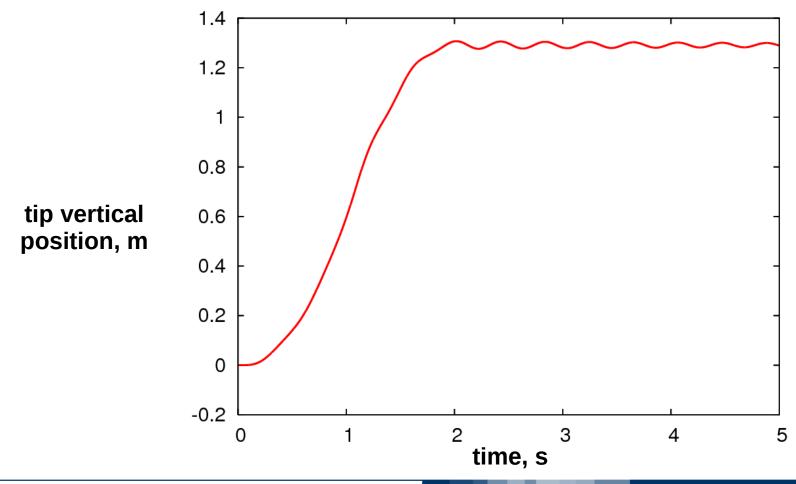




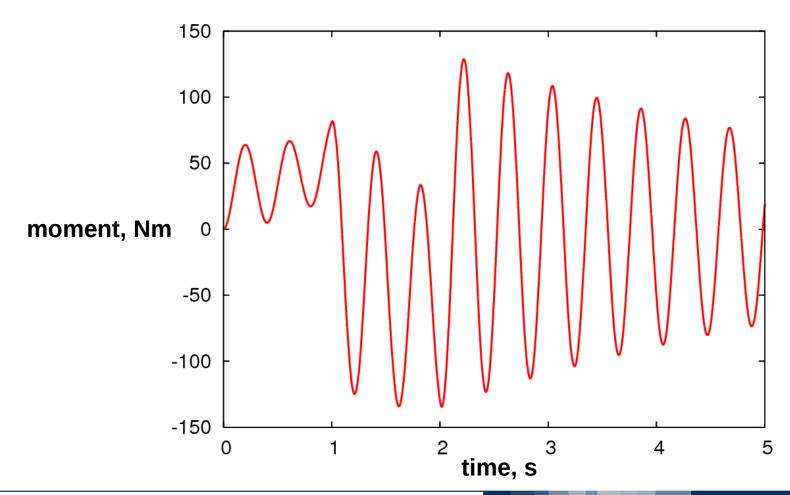
## **Example: Hydraulically Actuated Beam**

**MBDyn** 

### Tip vertical displacement



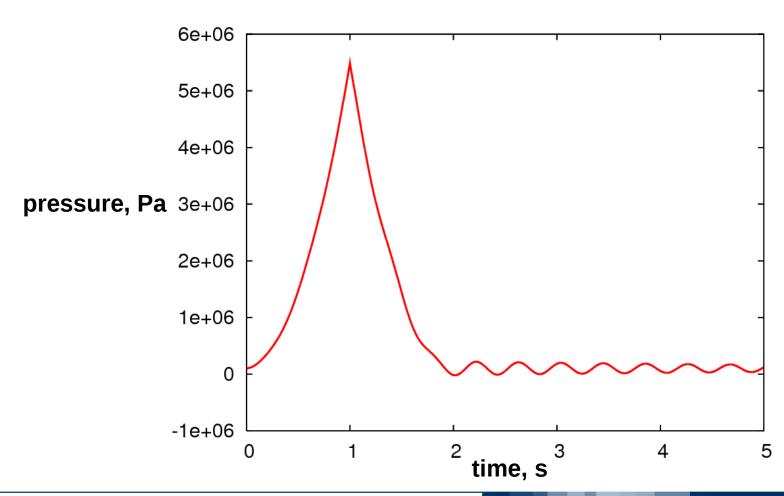
Internal bending moment close to actuator connection



## **Example: Hydraulically Actuated Beam**

**MBDyn** 

### Pressure at imposed flow node



#### **Consclusions**

**MBDyn** 

- Multibody: natural environment for integration of multiphysics
- Need for further development: complete library, build test suite, validate components
- The software is free: try it, and feed back!

http://www.mbdyn.org/

mbdyn-users@mbdyn.org

