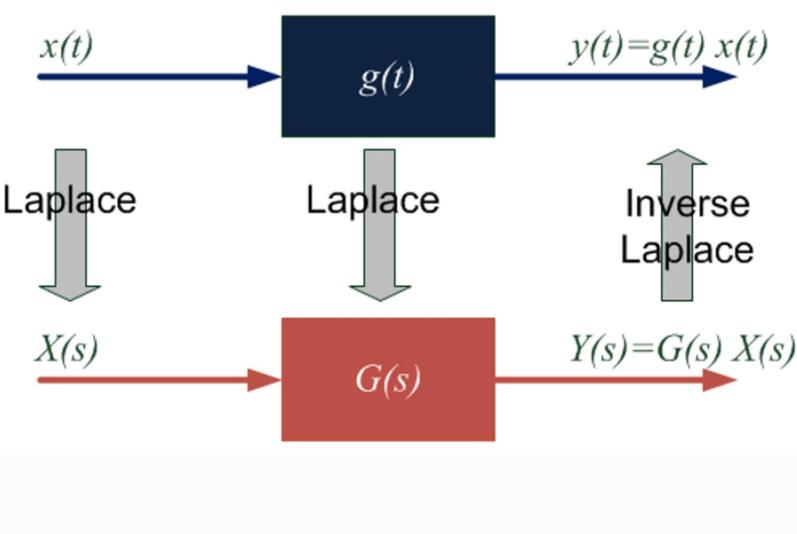


Number	$F(s)$	$f(t), t \geq 0$			
1	1	$\delta(t)$	12	$\frac{a}{s^2(s+a)}$	$\frac{1}{a}(at - 1 + e^{-at})$
2	$1/s$	$1(t)$	13	$\frac{b-a}{(s+a)(s+b)}$	$e^{-at} - e^{-bt}$
3	$1/s^2$	t	14	$\frac{s}{(s+a)^2}$	$(1-at)e^{-at}$
4	$2!/s^3$	t^2	15	$\frac{a^2}{s(s+a)^2}$	$1 - e^{-at}(1+at)$
5	$3!/s^4$	t^3	16	$\frac{(b-a)s}{(s+a)(s+b)}$	$be^{-bt} - ae^{-at}$
6	$m!/s^{m+1}$	t^m	17	$\frac{a}{s^2+a^2}$	$\sin at$
7	$\frac{1}{s+a}$	e^{-at}	18	$\frac{s}{s^2+a^2}$	$\cos at$
8	$\frac{1}{(s+a)^2}$	te^{-at}	19	$\frac{s+a}{(s+a)^2+b^2}$	$e^{-at} \cos bt$
9	$\frac{1}{(s+a)^3}$	$\frac{1}{2!}t^2e^{-at}$	20	$\frac{b}{(s+a)^2+b^2}$	$e^{-at} \sin bt$
10	$\frac{1}{(s+a)^m}$	$\frac{1}{(m-1)!}t^{m-1}e^{-at}$	21	$\frac{a^2+b^2}{s[(s+a)^2+b^2]}$	$1 - e^{-at} \left(\cos bt + \frac{a}{b} \sin bt \right)$
11	$\frac{a}{s(s+a)}$	$1 - e^{-at}$			

Number	Laplace Transform	Time Function	Comment
-	$F(s)$	$f(t)$	Transform pair
1	$\alpha F_1(s) + \beta F_2(s)$	$\alpha f_1(t) + \beta f_2(t)$	Superposition
2	$F(s)e^{-s\lambda}$	$f(t-\lambda)$	Time delay ($\lambda \geq 0$)
3	$\frac{1}{ a }F\left(\frac{s}{a}\right)$	$f(at)$	Time scaling
4	$F(s+a)$	$e^{-at}f(t)$	Shift in frequency
5	$s^m F(s) - s^{m-1}f(0)$ $-s^{m-2}\dot{f}(0) - \dots - f^{(m-1)}(0)$	$f^{(m)}(t)$	Differentiation
6	$\frac{1}{s}F(s)$	$\int_0^t f(\zeta) d\zeta$	Integration
7	$F_1(s)F_2(s)$	$f_1(t) * f_2(t)$	Convolution
8	$\lim_{s \rightarrow \infty} sF(s)$	$f(0^+)$	Initial Value Theorem
9	$\lim_{s \rightarrow 0} sF(s)$	$\lim_{t \rightarrow \infty} f(t)$	Final Value Theorem
10	$\frac{1}{2\pi j} \int_{\sigma_c-j\infty}^{\sigma_c+j\infty} F_1(\zeta)F_2(s-\zeta) d\zeta$	$f_1(t)f_2(t)$	Time product
11	$\frac{1}{2\pi} \int_{-j\infty}^{+j\infty} Y(-j\omega)U(j\omega) d\omega$	$\int_0^\infty y(t)u(t) dt$	Parseval's Theorem
12	$-\frac{d}{ds}F(s)$	$tf(t)$	Multiplication by time

Time Domain



$$f_1(t) + f_2(t) = 1(t) + t$$

$$\Rightarrow F_1(s) + F_2(s) = \frac{1}{s} + \frac{1}{s^2}$$

$$F_1(t) \cdot F_2(t) \neq F_1(s) \cdot F_2(s)$$

$$\ddot{y}(t)$$

$$\downarrow L$$

$$s^2 \cdot Y(s) - s \cdot y(0) - \dot{y}(0)$$

$$\dot{y}(t)$$

$$\downarrow L$$

$$s \cdot Y(s) - y(0)$$

$$\ddot{y}(t)$$

$$\downarrow L$$

$$s^3 Y(s) - s^2 y(0) - s \dot{y}(0) - \ddot{y}(0)$$

Step: $1(t) \rightarrow \frac{1}{s}$
 Impuls: $\delta(t) \rightarrow 1$
 Ramp: $t \rightarrow \frac{1}{s^2}$

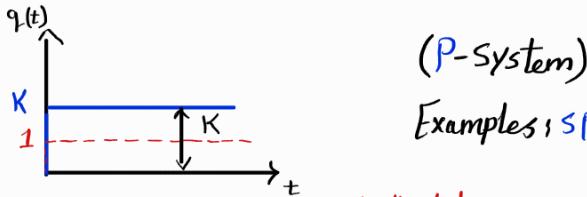
types of input signals.

Proportional: Relation between output & input is in general proportional.

a) Ideal : $q_1(t) = K u(t)$

$$G(s) = \frac{Y(s)}{U(s)} = K$$

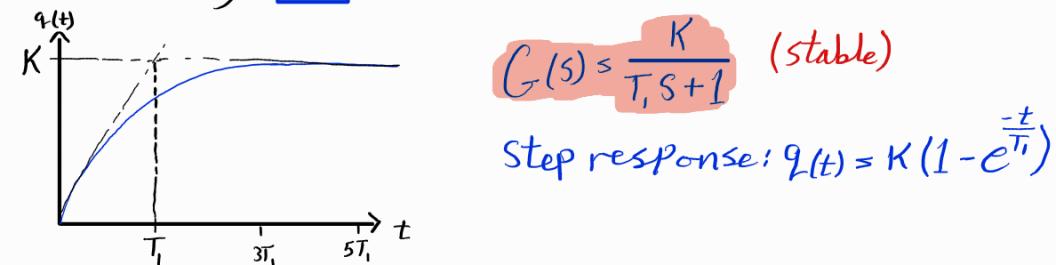
↓
input



(P-system)

Examples: spring, ohms resistance, Lever, gear, -----

b) With delay: $\boxed{PT_1} \xrightarrow{\text{more than the ideal}} T_1 \ddot{y}(t) + y(t) = K u(t)$



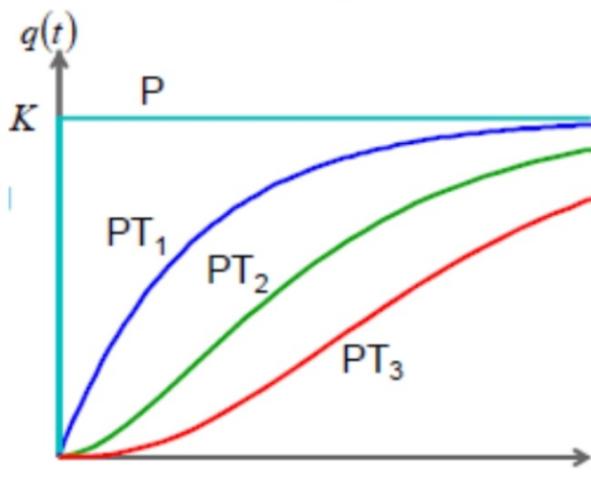
$$G(s) = \frac{K}{T_1 s + 1}$$

(stable)

Step response: $q(t) = K(1 - e^{-\frac{t}{T_1}})$

c) with delay: $\boxed{PT_2} \xrightarrow{\text{more than } PT_1} T_2^2 \ddot{y} + T_1 \dot{y} + y = K u \quad \text{or} \quad \ddot{y} + \frac{2D\omega_0}{T_2} \dot{y} + \frac{\omega_0^2}{T_2^2} y = \frac{K}{T_2} u$

Where $\omega_0 = \frac{1}{T_2}$, $D = \frac{T_1}{2T_2}$
↳ damping ratio



$$G(s) = \frac{K T_2^2}{s^2 + \left(\frac{T_1}{T_2^2}\right)s + \left(\frac{1}{T_2}\right)\omega_0^2}$$

$$f(s) = s^2 + 2DW_0 s + \omega_0^2$$

$$P_{1,2} = -DW_0 \pm \sqrt{D^2\omega_0^2 - \omega_0^2} = -DW_0 \pm \sqrt{\omega_0^2(D^2 - 1)}$$

$$P_{1,2} = -DW_0 \pm \omega_0 \sqrt{(D-1)(D+1)} = \omega_0 (-D \pm \sqrt{(D-1)(D+1)})$$

a) over damped $\rightarrow D > 1 \rightarrow$ under sqrt is positive & smaller than $D \rightarrow \begin{smallmatrix} \text{Re} \\ \ominus \end{smallmatrix} \quad \begin{smallmatrix} \text{Im} \\ \oplus \end{smallmatrix}$

b) critically damped $\rightarrow D = 1 \rightarrow \text{sqrt}=0 \rightarrow P_1 = P_2 \rightarrow \begin{smallmatrix} \text{Re} \\ \ominus \end{smallmatrix} \quad \begin{smallmatrix} \text{Im} \\ \oplus \end{smallmatrix}$

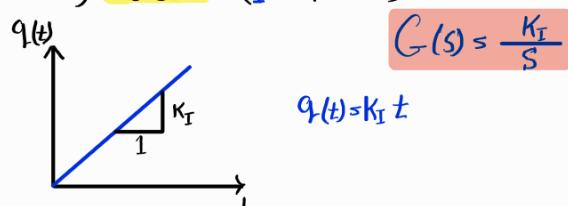
c) Damped $\rightarrow 0 < D < 1 \rightarrow \begin{smallmatrix} \text{Re} \\ \ominus \end{smallmatrix} \quad \begin{smallmatrix} \text{Im} \\ \circ \end{smallmatrix}$

$$D = \sqrt{\frac{\ln(\text{overshoot})^2}{\pi^2 + \ln(\text{overshoot})^2}}$$

d) Undamper $\rightarrow D = 0 \rightarrow \begin{smallmatrix} \text{Re} \\ \oplus \end{smallmatrix} \quad \begin{smallmatrix} \text{Im} \\ \mp \end{smallmatrix}$ (Boundary stable)

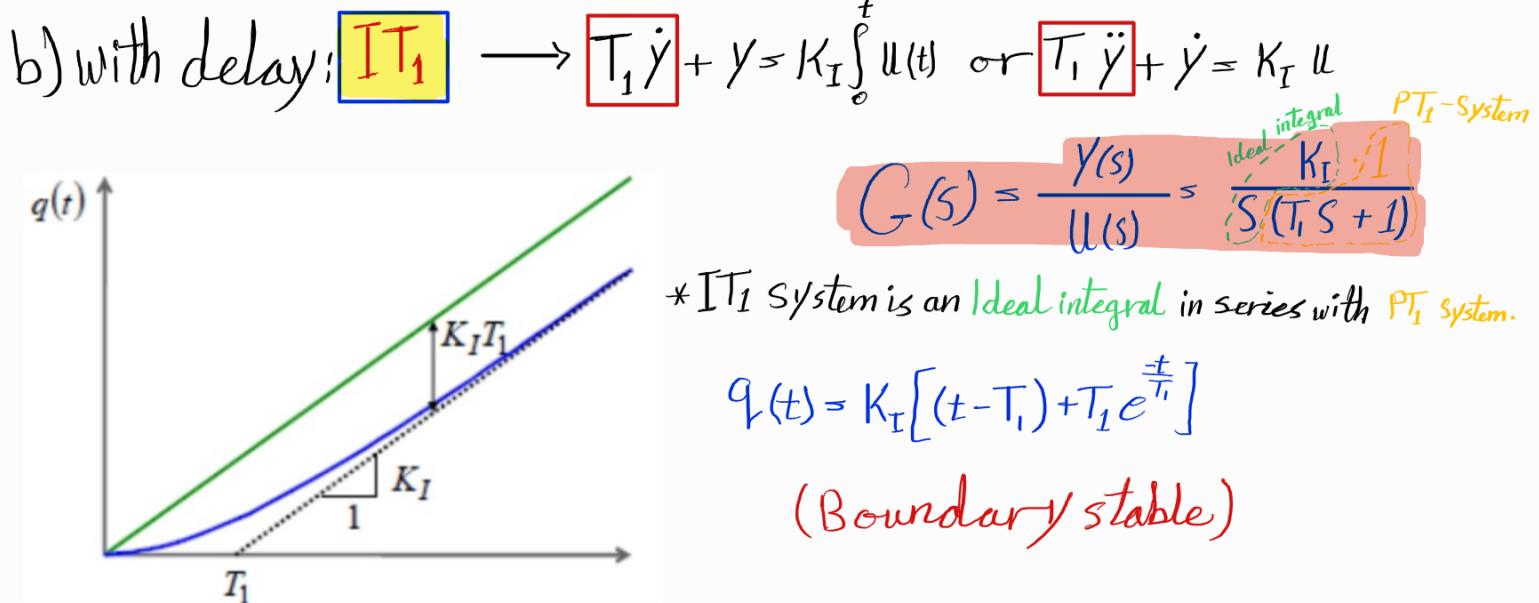
Integral: Although input is constant, the output is increasing over time.

a) Ideal: (I-System) $\rightarrow y = K_I \int_0^t u(t) dt$ or $\dot{y} = K_I u(t)$



$$G(s) = \frac{K_I}{s}$$

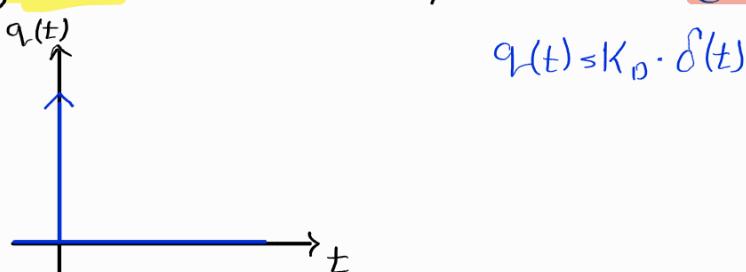
(Boundary stable)



Derivative : output is a derivative of the input.

Example: System with derivative behavior \rightarrow shock absorber

a) Ideal: (D -system) $\rightarrow y = K_D \dot{u}$ $G(s) = K_D \cdot s$

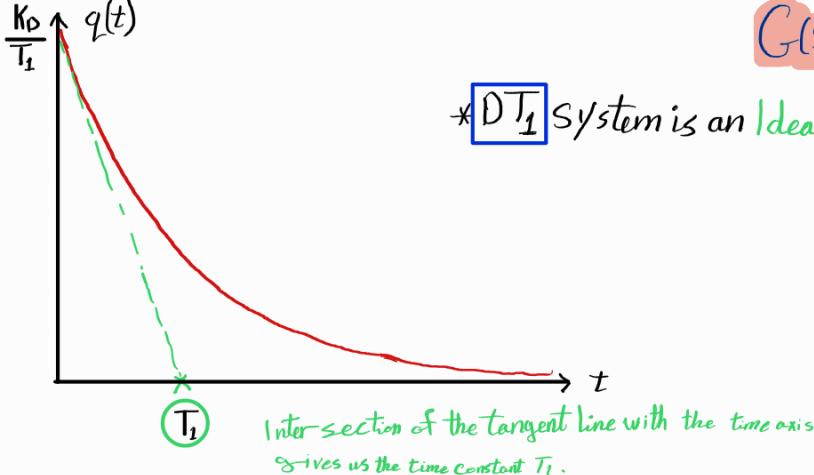


b) with delay: DT_1 $\rightarrow T_1 \dot{y} + y = K_D \dot{u}$

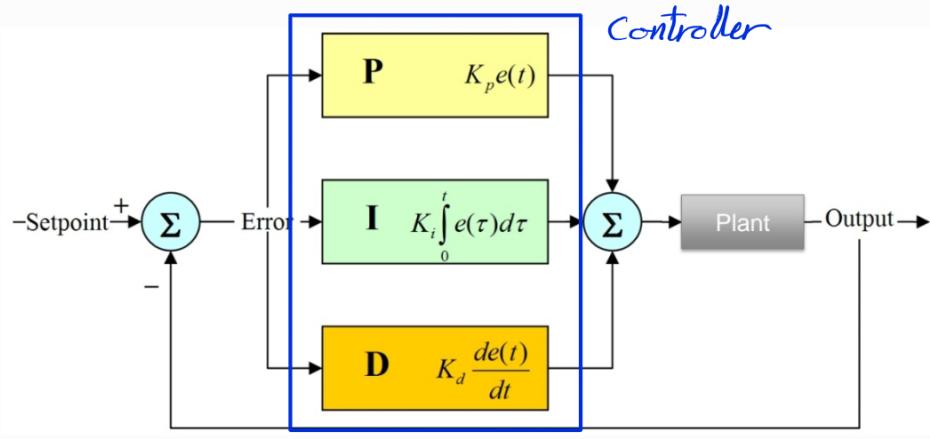
$$G(s) = \frac{\text{ideal } D \cdot (K_D s \cdot 1)}{T_1 s + 1}$$

* DT_1 system is an Ideal derivative system in series with PT_1 system.

Stable system



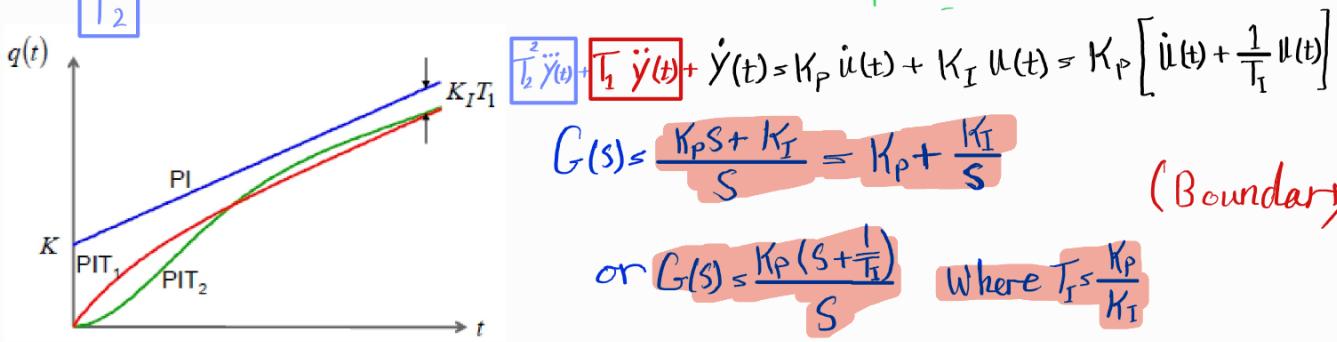
Combined System types:



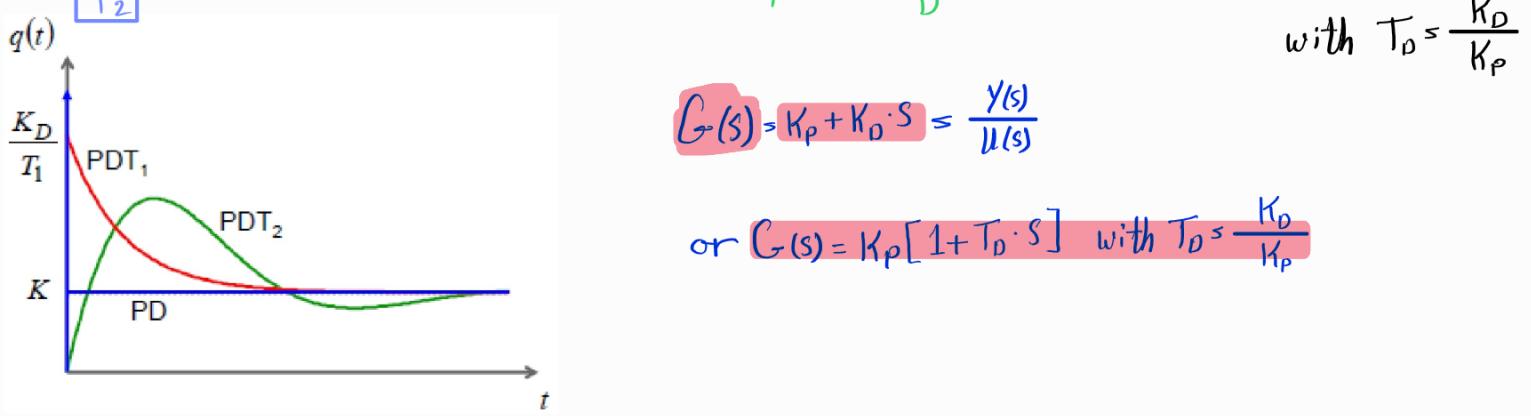
Important combined system types:

- * PI-system (with delay)
- * PD-system (with delay)
- * PID-system (with delay)

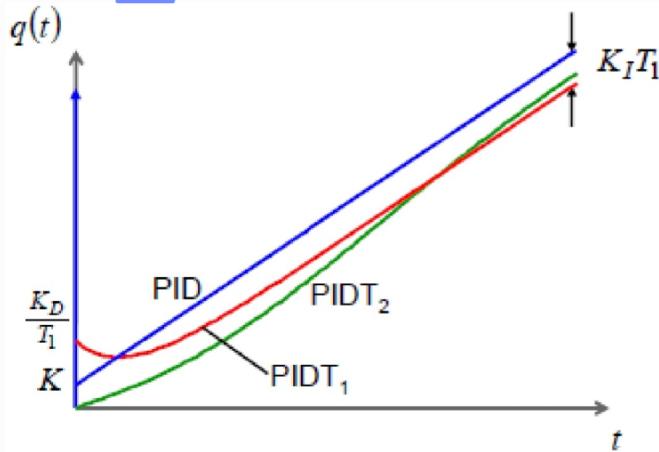
* PI $\boxed{T_1}$ -System $\boxed{\frac{d^2}{dt^2}y(t)} + \boxed{T_1 \dot{y}(t)} + y(t) = \underbrace{K_p u(t)}_{P} + \underbrace{K_I \int_0^t u(\tau) d\tau}_{I} = K_p \left[u(t) + \frac{1}{T_I} \int_0^t u(\tau) d\tau \right]$ where $T_I = \frac{K_p}{K_I}$



* PD $\boxed{T_1}$ -System $\boxed{\frac{d^2}{dt^2}y(t)} + \boxed{T_1 \dot{y}(t)} + y(t) = \underbrace{K_p u(t)}_{P} + \underbrace{K_D \ddot{u}(t)}_{D} = K_p \left[u(t) + T_D \ddot{u}(t) \right]$



PID $\begin{matrix} T_1 \\ T_2 \end{matrix}$ - System $T_2^2 \ddot{Y}(t) + T_1 \dot{Y}(t) + \dot{Y}(t) = K_I u(t) + K_P \dot{u}(t) + K_D \ddot{u}(t)$



$$G(s) = \frac{K_D s^2 + K_P s + K_I}{s}$$

(Boundary stable)

Example:

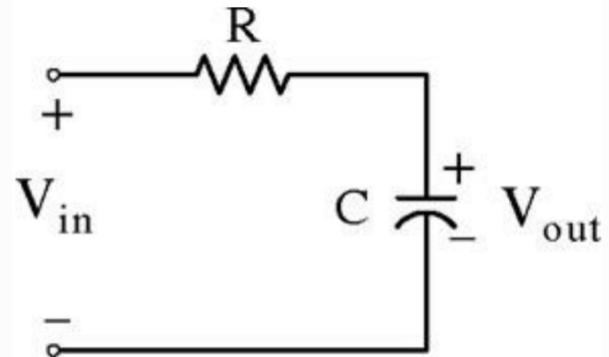
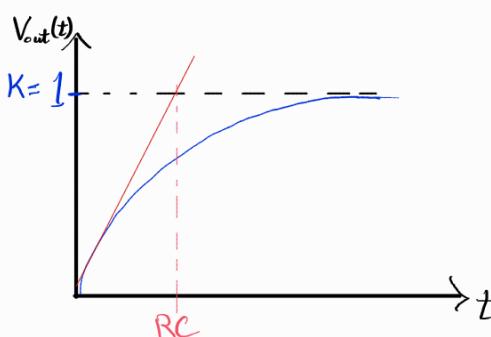
$$\underbrace{V_{out}(t)}_{\text{with } T_1 \text{ delay}} + \underbrace{RC}_{\text{ideal P-system}} \dot{V}_{out}(t) = V_{in}(t)$$

a) TF? $TF = G(s) = \frac{V_{out}(s)}{V_{in}(s)} = \frac{1}{RCs + 1}$

b) Standard system type? PT_1

c) What are the parameters? $K=1$, $T_1=RC$

d) Draw step response:



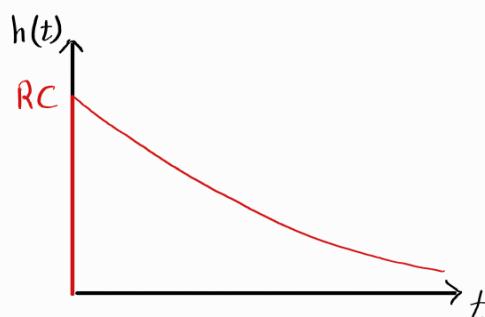
e) Impulse response?

(The derivative of the step response, where the step response is the integral of impulse.)

$$q(t) = K(1 - e^{-\frac{t}{RC}}) = 1 - e^{-\frac{t}{RC}}$$

$$\dot{q}(t) = h(t) = \frac{1}{RC} \cdot e^{-\frac{t}{RC}}$$

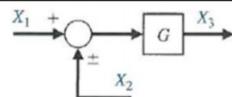
f) Draw impulse response



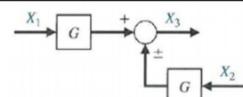
5.1 Block Diagram Transformations

Transformation	Original Diagram	Equivalent Diagram
1. Combining blocks in cascade / series		
2. Combining blocks in parallel		
3. Moving a summation point behind a block		
4. Moving a pickoff point ahead of a block		
5. Moving a pickoff point behind a block		
6. Moving a summation point ahead of a block		
7. Eliminating a feedback loop		

3. Moving a summation point behind a block



$$X_3 = G(s)(X_1 \pm X_2)$$



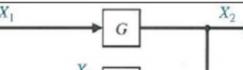
$$X_3 = X_1 G(s) \pm X_2 G(s)$$

5. Moving a pickoff point behind a block

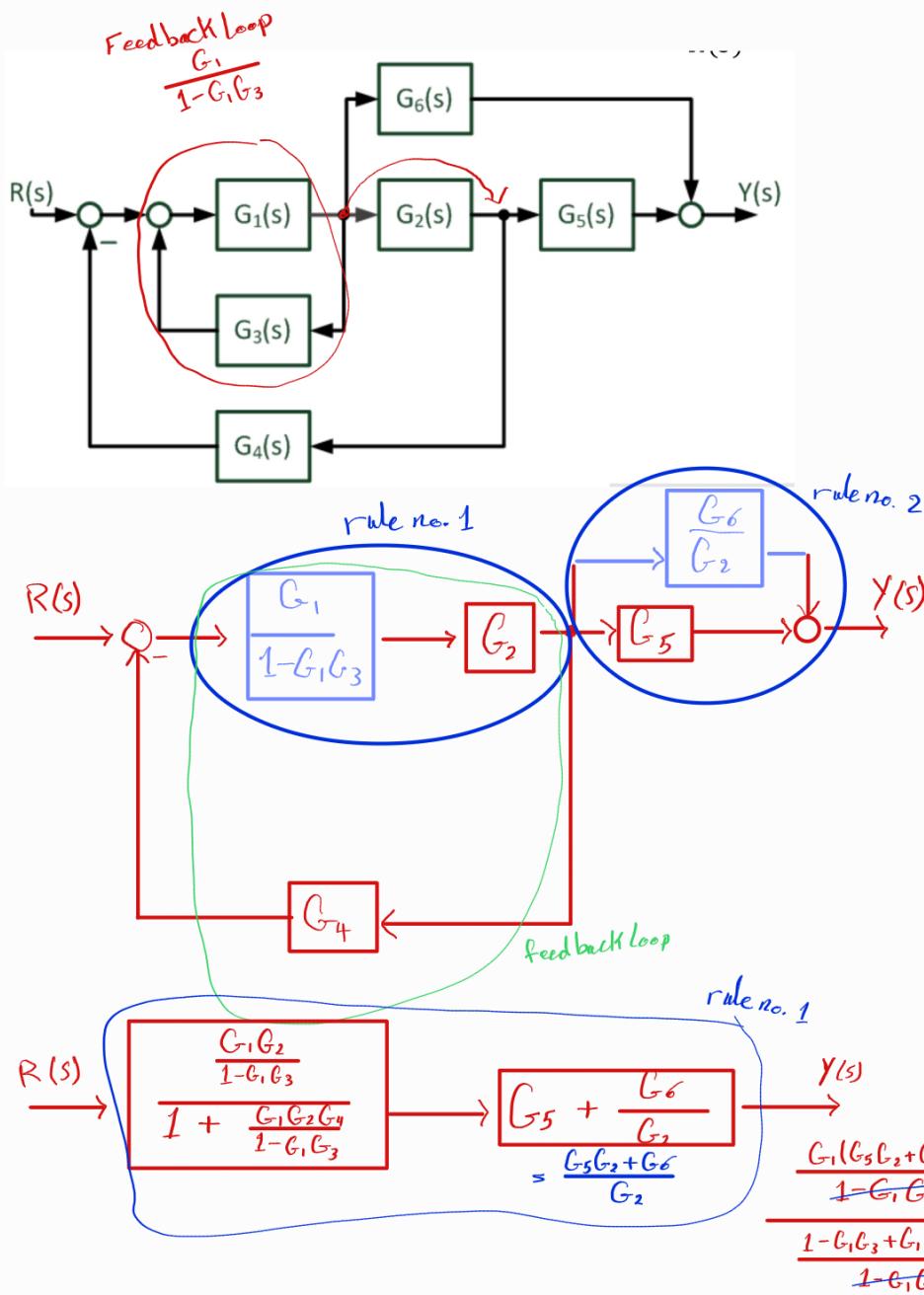


$$X_2 = X_1 G(s)$$

$$X_1 = X_1$$



$$X_1 = X_2 \cdot \frac{1}{G(s)} = X_1 G(s) \cdot \frac{1}{G(s)} = X_1$$



$$R(s) \rightarrow \boxed{\frac{G_1(G_5G_2+G_6)}{1-G_1G_3+G_1G_2G_4}} \rightarrow Y(s)$$

$$\therefore TF = \frac{Y(s)}{R(s)} = \frac{G_1(G_5G_2+G_6)}{1-G_1G_3+G_1G_2G_4}$$

5.2 Closed-Loop Behavior

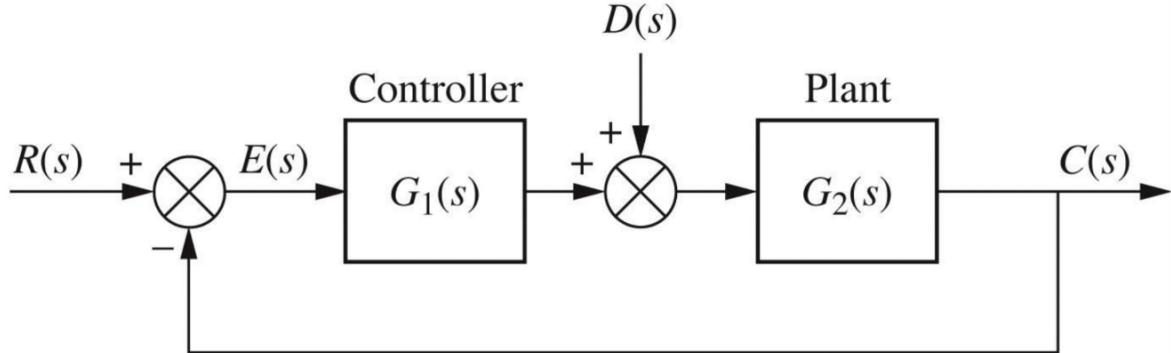


Figure 7.11
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To investigate the reference TF, we set the disturbance function = 0

Reference transfer function → Disturbance $D(s) = 0$

$$G_R(s) = \frac{C(s)}{R(s)} = \frac{G_1(s) G_2(s)}{1 + G_1(s) G_2(s)} = \frac{G_C(s) G_P(s)}{1 + G_C(s) G_P(s)}$$

ideally
 ≈ 1

5.2 Closed-Loop Behavior

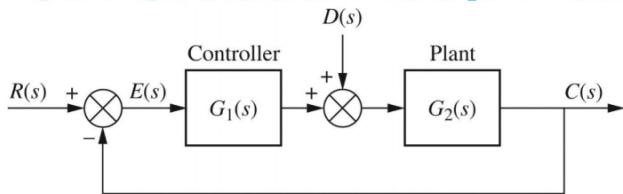
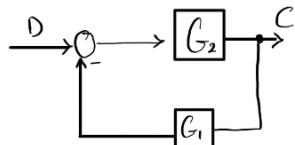


Figure 7.11
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To investigate the disturbance TF, we set the reference function = 0

Disturbance transfer function → Reference $R(s) = 0$

$$G_D(s) = \frac{C(s)}{D(s)} = \frac{G_2(s)}{1 + G_1(s) G_2(s)} = \frac{G_P(s)}{1 + G_C(s) G_P(s)}$$

ideally
 ≈ 0

Let's control a plant with **PT1** characteristic by using a **P-controller**:

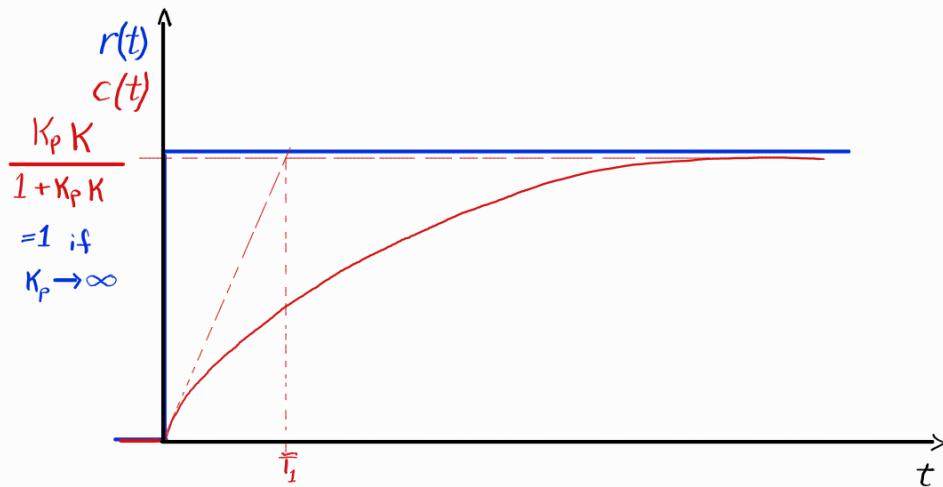
$$G_P(s) = \frac{K}{T_1 s + 1} ; G_C(s) = K_P$$

Reference TF:

$$G_R(s) = \frac{\frac{K_p K}{T_1 s + 1}}{1 + \frac{K_p K}{T_1 s + 1}} = \frac{K_p K}{T_1 s + 1 + K_p K} = \frac{\frac{K_p K}{K_p K + 1}}{\frac{T_1}{1 + K_p K} \cdot s + 1}$$

\xrightarrow{R}

PT₁-System

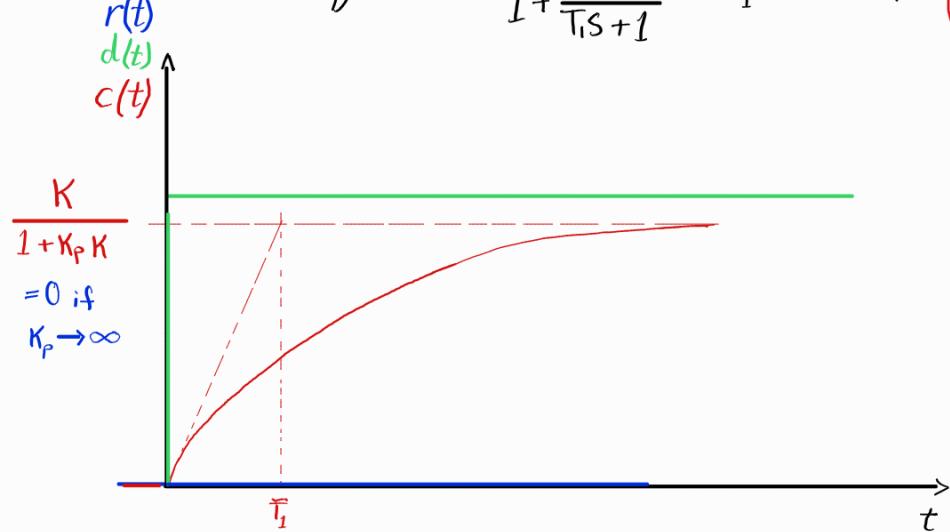


Disturbance TF:

$$G_D(s) = \frac{\frac{K}{T_1 s + 1}}{1 + \frac{K_p K}{T_1 s + 1}} = \frac{K}{T_1 s + 1 + K_p K} = \frac{\frac{K}{K_p K + 1}}{\frac{T_1}{1 + K_p K} \cdot s + 1}$$

\xrightarrow{R}

PT₁-System



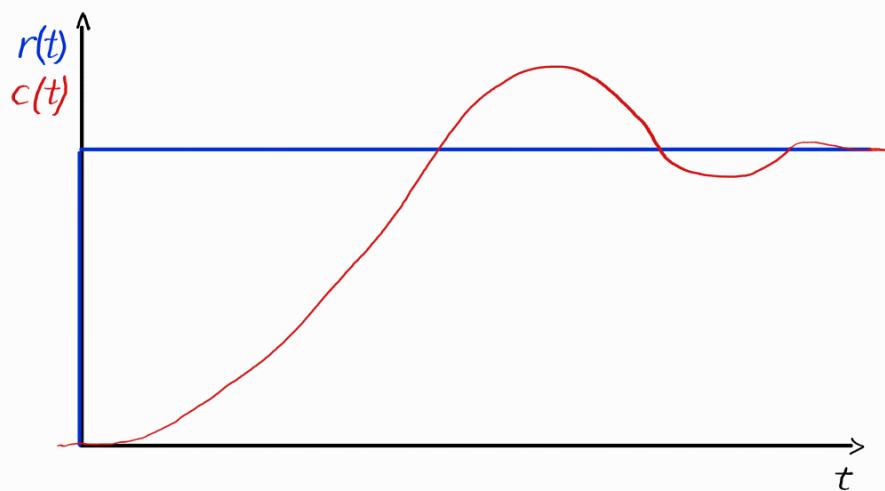
Let's control our plant with PT1 characteristic by using an I-controller:

$$G_P(s) = \frac{K}{T_1 s + 1} ; G_C(s) = \frac{K_I}{s}$$

Reference TF:

$$G_R(s) = \frac{\frac{K_I K}{s(T_1 s + 1)}}{1 + \frac{K_I K}{s(T_1 s + 1)}} = \frac{K_I K}{T_1 s^2 + s + K_I K} = \frac{K_I K / T_1}{s^2 + \frac{1}{T_1} s + \frac{K_I K}{T_1}} \text{ w. } \omega_o = \sqrt{\frac{K_I K}{T_1}}$$

PT₂ - System



if we set $s=0$
the gain $G_R(s)=1$
(which is good)

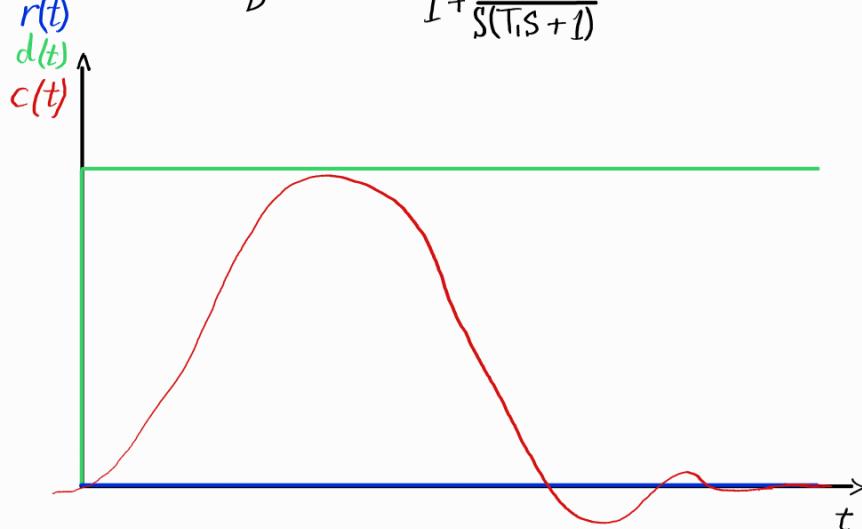
$$2\sqrt{\frac{K_I K}{T_1}} = \frac{1}{T_1} \Rightarrow D = \frac{1}{2\sqrt{T_1 K_I K}}$$

$K_I \uparrow \Rightarrow D \downarrow$

Disturbance TF:

$$G_D(s) = \frac{\frac{K}{T_1 s + 1}}{1 + \frac{K_I K}{s(T_1 s + 1)}} = \frac{K \cdot s}{T_1 s^2 + s + K_I K} \text{ w. } \omega_o = \sqrt{\frac{K_I K}{T_1}}$$

DT₂ - System



good that
disturbance TF is
going to zero.