



Automation and Robotics Engineering

Field and Service Robotics: Final project

Aerial Robots: Quadrotor Control with External Disturbances Estimations and Ground and Ceiling Effects Simulation

Students:

Riccardo Stucovitz, P38000181

Nicola Monetti, P38000238

Professor:

Fabio Ruggiero

Contents

1. Simulation Environment and Elements
 - 1.1. Simulation Tools and Environment
 - 1.2. X3D-BL Quadrotor
 - 1.3. Environment Scenario
 - 1.4. Trajectory planner
 - 1.5. Collision detector
2. Controllers
 - 2.1. Hierarchical controller
 - 2.2. Geometric controller
 - 2.3. Passivity-based controller
 - 2.4. Impact of "Filter and Derivative" Block on system performance
 - 2.5. Robustness comparison
3. Momentum-based Estimator
4. Simulations and considerations
 - 4.1. Hierarchical estimator-based control
 - 4.2. Geometric estimator-based control
 - 4.3. Passivity-and-estimator-based control
5. Conclusions



Aim of the project

Hypothesis:

- Perfect knowledge of current pose of the quadrotor in every time instant
- Well-known environment with several obstacles
- External disturbances and several physical effects

Goals:

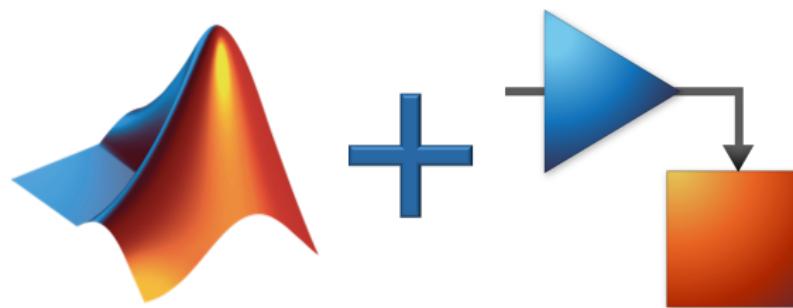
- Simulate the flight control of a quadrotor with different approaches
- Analyze the performance for each approach
- Analyze advantages and drawbacks for each approach

1. Simulation Environment and Elements





1.1. Simulation Tools and Environment



MATLAB R2024b & Simulink



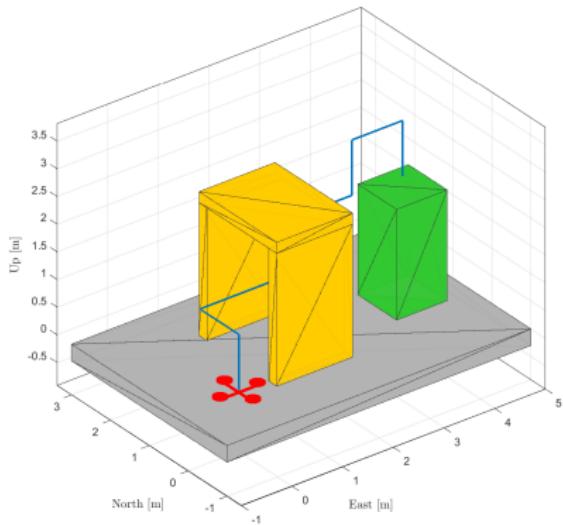
1.2. X3D-BL Quadrotor



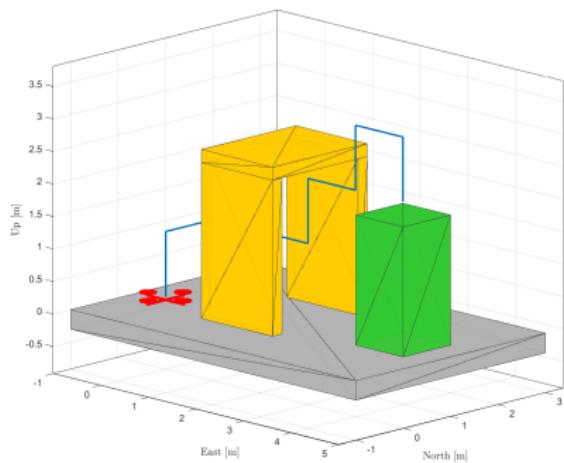
Symbols	Definitions	Values	Units
m	Mass	0.5	kg
I_{xx}, I_{yy}	Moment of inertia about the x and y axis	0.0023	$\text{kg} \cdot \text{m}^2$
I_{zz}	Moment of inertia about the z axis	0.00509	$\text{kg} \cdot \text{m}^2$
h	Height	100	mm
ρ	Radius of blade propeller	100	mm
l	Distance between the axis of rotation of the rotors and the center of the mass	170	mm
d	Distance between adjacent propeller axis	240	mm
w	Maximum width with propeller	570	mm



1.3. Environment Scenario



Diagonal - front view

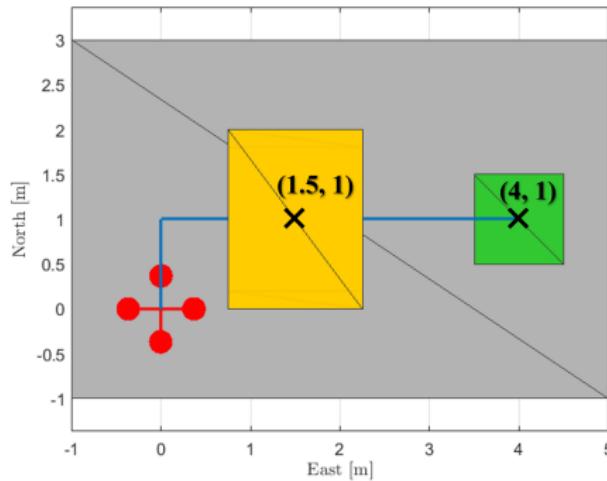


Diagonal - back view

[Click here to watch the video](#)



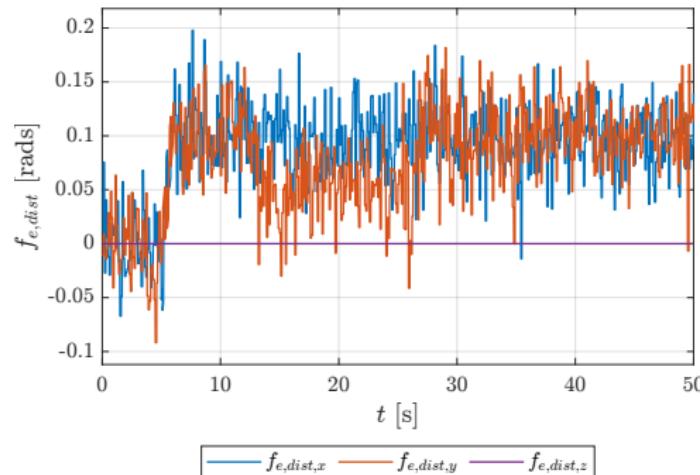
1.3. Environment Scenario



Top view



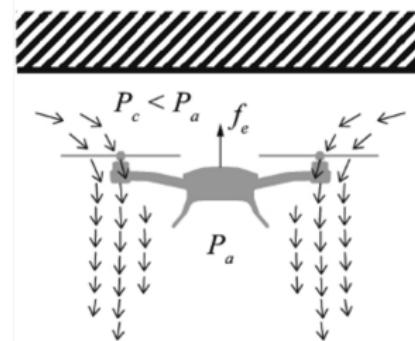
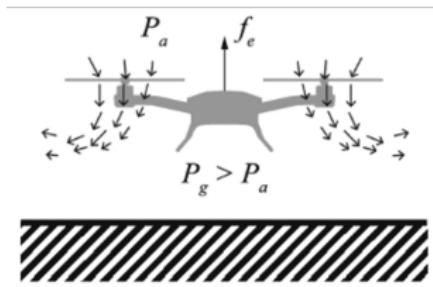
1.3. Environment Scenario: Wind external disturbance



After 5 s: **noisy wind effect** in the xy plane linearly increases to a mean value of $(f_{e,dist,x}, f_{e,dist,y}, f_{e,dist,z}) \approx (0.1, 0.1, 0)$ N, then remaining constant.



1.3. Environment Scenario: Ground and Ceiling Effects



Ground Effect: $\frac{u_{T,IGE}}{u_{T,OGE}} = k_{GE} = \frac{1}{1 - \left(\frac{\rho}{4z}\right)^2 - \frac{z\rho^2}{\sqrt{(d^2+4z^2)^3}} - \frac{z\rho^2}{2\sqrt{(2d^2+4z^2)^3}}}$

Ceiling Effect: $\frac{u_{T,ICE}}{u_{T,OCE}} = k_{CE} = \frac{1}{2} + \frac{1}{2} \sqrt{1 + \frac{1}{8\hat{z}^2}}, \quad \text{where } \hat{z} = z/\rho.$

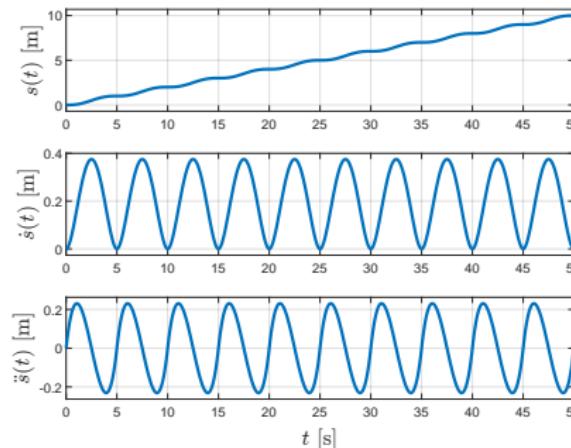
1.4. Trajectory planner: Time law

- Individual rectilinear trajectory:

$$s(t) = a_5 t^5 + a_4 t^4 + a_3 t^3 + a_2 t^2 + a_1 t + a_0, \quad \text{s.t.}$$

$$\begin{aligned} s(t_0) &= s(0) = 0, & \dot{s}(t_0) &= 0, & \ddot{s}(t_0) &= 0, \\ s(t_f) &= s(5) = 1, & \dot{s}(t_f) &= 0, & \ddot{s}(t_f) &= 0. \end{aligned}$$

- Overall time law and its time derivatives:





1.4. Trajectory planner: Geometric path

- Parametric representation of the individual rectilinear paths composing the overall trajectory, its velocity and acceleration:

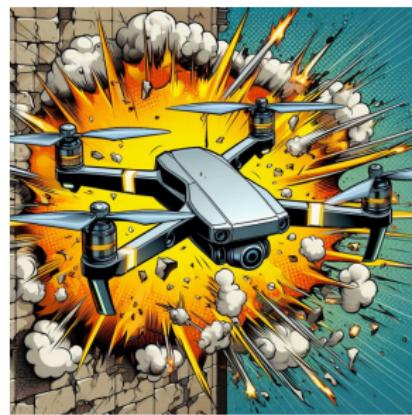
$$p(s) = p_i + \frac{s}{\|p_f - p_i\|}(p_f - p_i), \quad \dot{p}(s) = \frac{\dot{s}}{\|p_f - p_i\|}(p_f - p_i),$$

$$\ddot{p}(s) = \frac{\ddot{s}}{\|p_f - p_i\|}(p_f - p_i)$$

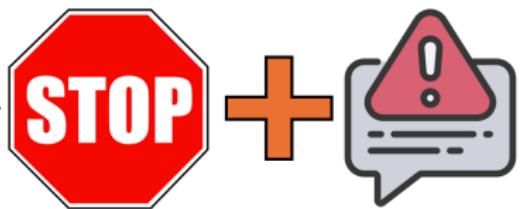
- Overall positional trajectory $p_d(t)$ starting from $p_0 = (0, 0, 0.2)$ m and ending at the top of the cylindrical column in $p_F = (4, 1, 2.2)$ m, remaining in hovering for further 5 s



1.5. Collision detector



DETECTION!



2. Controllers

- **Control approaches:**

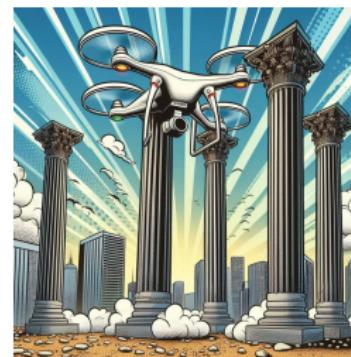
- Hierarchical

- Geometric

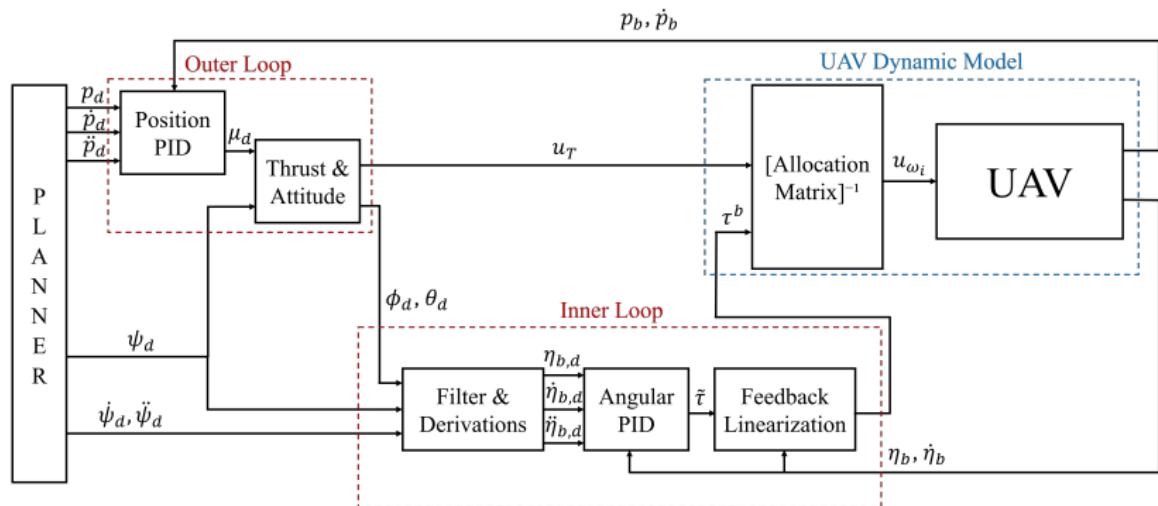
- Passivity-based

- **Common architecture:** Inner & Outer loops

- **Ideal conditions:** no external disturbances, physical effects



2.1. Hierarchical controller



Advantages & Drawbacks

Advantages:

- Two PID sub-controllers (inner and outer loops): tuning the gains variable one can deduct easily the effects on control action
- Stability proved just employing PD+ sub-controllers (even if in practice, an integral term is required)

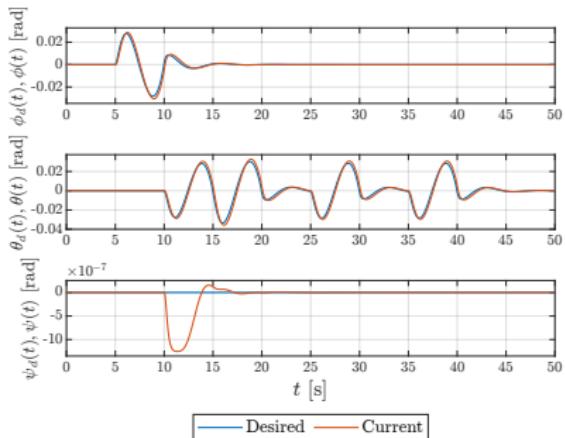
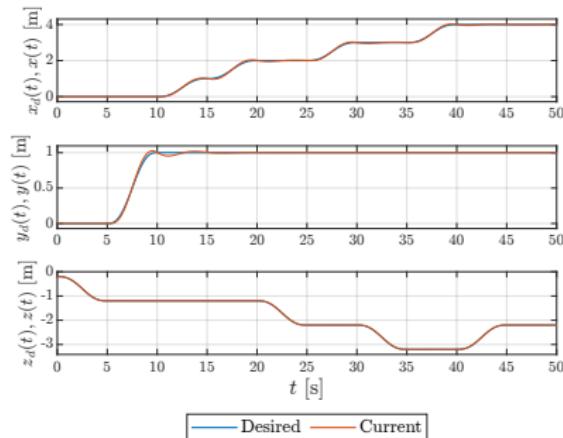
Drawbacks:

- Implementation of a "Filtering & derivation" operation of the angular references
- Partial Feedback linearization: the control system lacks robustness with respect to model uncertainties
- Sensitivity to representation singularities



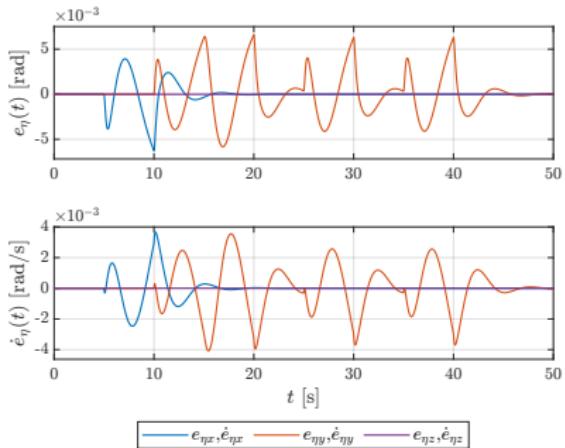
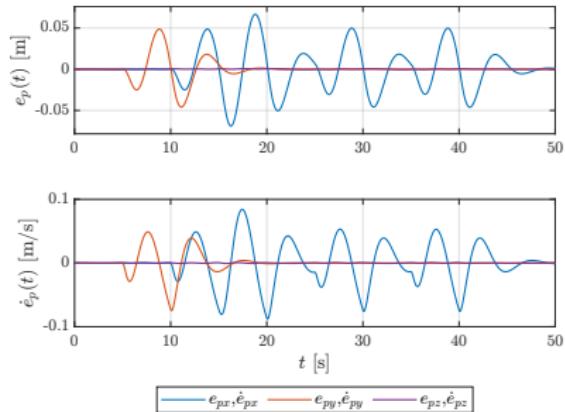
Desired & effective pose

$$K_p = K_e = [I_3 \quad I_3]:$$



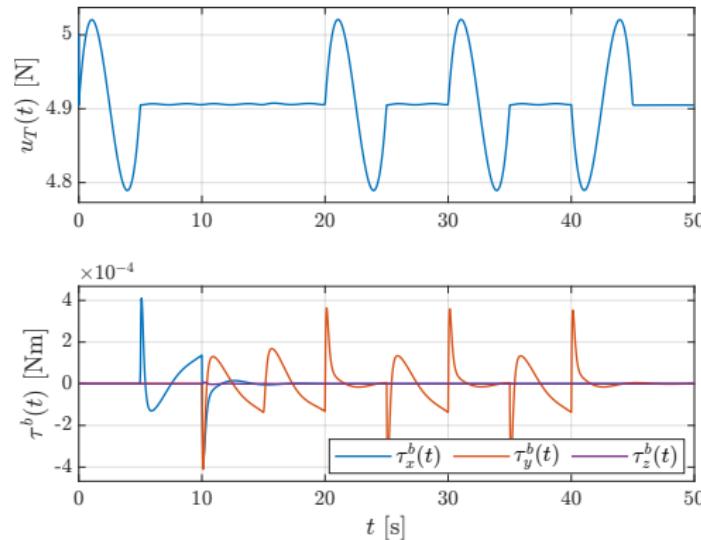


Linear & angular errors





Total thrust & torques

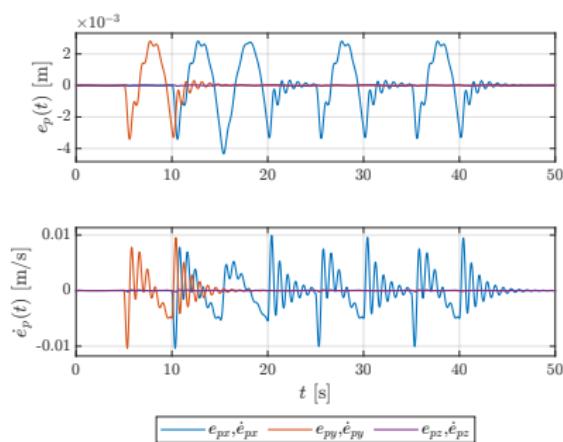


[Click here to watch the UAV animation](#)



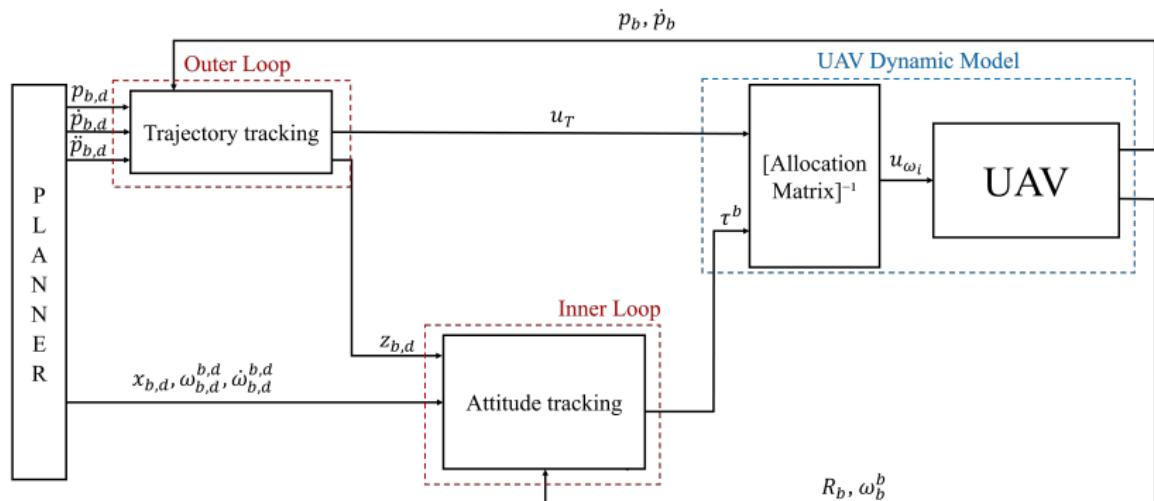
Linear & angular errors

$$K_p = 10 \begin{bmatrix} I_3 & I_3 \end{bmatrix}, \quad K_e = 100 \begin{bmatrix} I_3 & I_3 \end{bmatrix}:$$



[Click here to watch the UAV animation](#)

2.2. Geometric controller





Advantages & Drawbacks

Advantages:

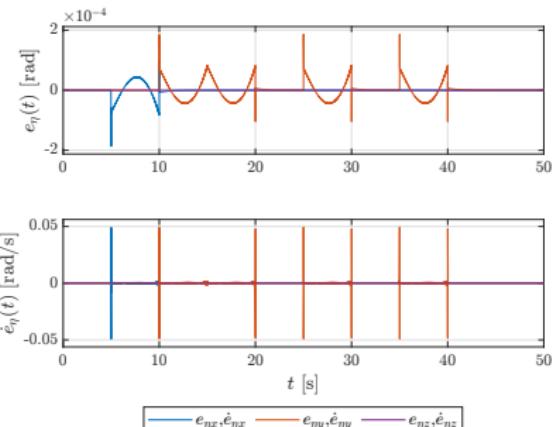
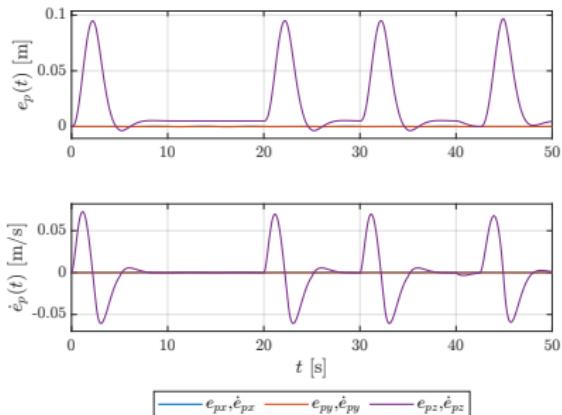
- Two linear sub-controllers advantages (already explained)
- No "Filtering & derivation" operation requested
- No representation singularities

Drawbacks:

- Lack of robustness due to Partial Feedback linearization (already explained)
- Exponential stability of the closed-loop system can be proven only if the initial attitude error is less than 90°

Linear & angular errors

$K_p = K_v = K_r = K_w = I_3$:

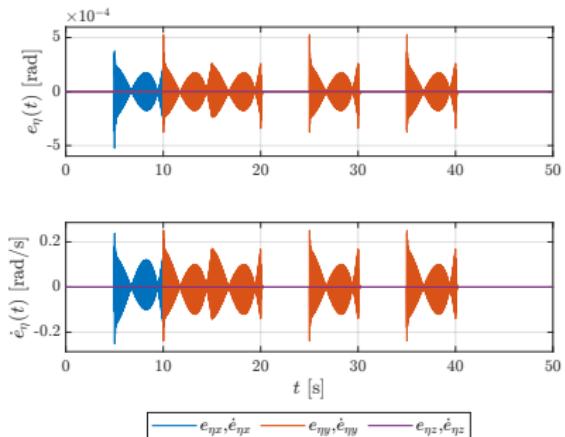
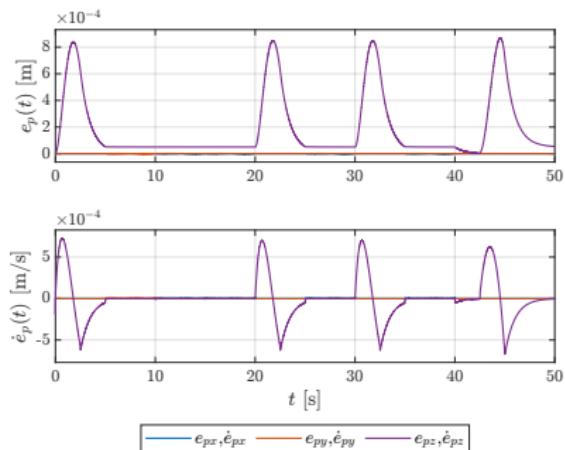


[Click here to watch the UAV animation](#)



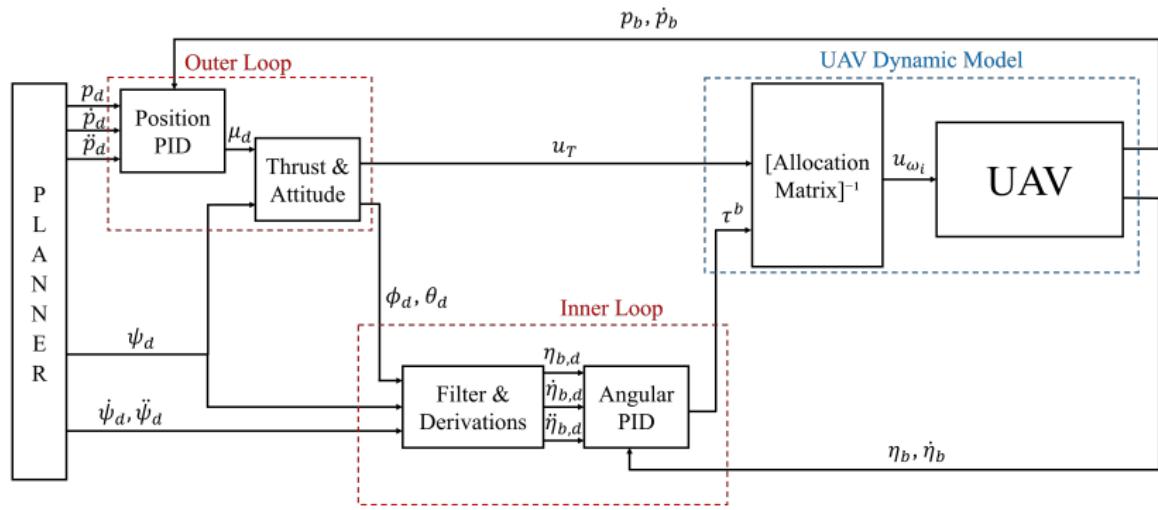
Linear & angular errors

$$K_p = K_v = 100I_3, \quad K_r = 10I_3, \quad K_w = I_3:$$



Click here to watch the UAV animation

2.3. Passivity-based controller



Advantages & Drawbacks

Advantages:

- Two linear controllers advantages (already explained)
- Robustness with respect to model uncertainties, since feedback linearization is not involved

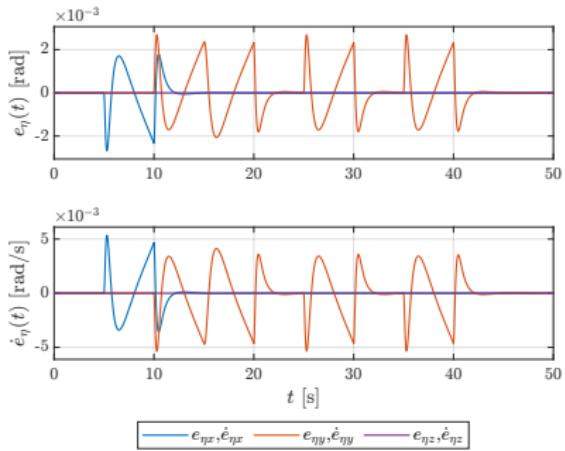
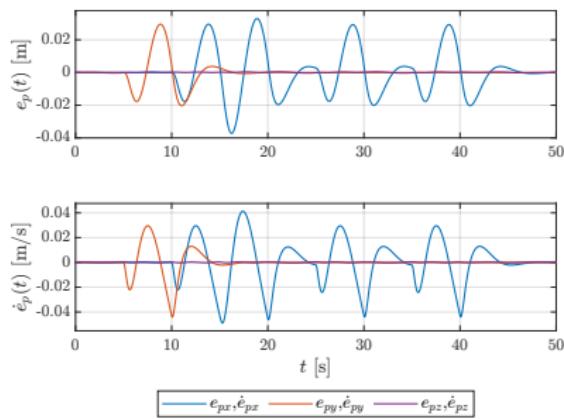
Drawbacks:

- Implementation of a "Filtering & derivation" operation of the angular references (already explained)
- Sensitivity to Representation singularities (already explained)



Linear & angular errors

$$K_p = [I_3 \quad I_3], \quad D_0 = I_3, \quad K_0 = \sigma D_0 = I_3:$$

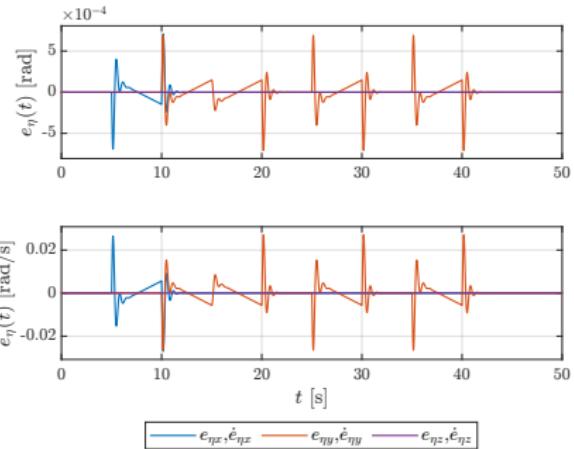
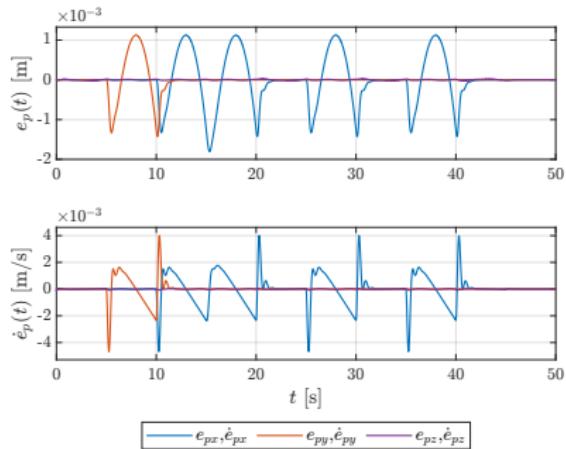


[Click here to watch the UAV animation](#)



Linear & angular errors

$$K_p = [20I_3 \quad 10I_3], \quad D_0 = I_3, \quad K_0 = \sigma D_0 = 20I_3:$$



Click here to watch the UAV animation

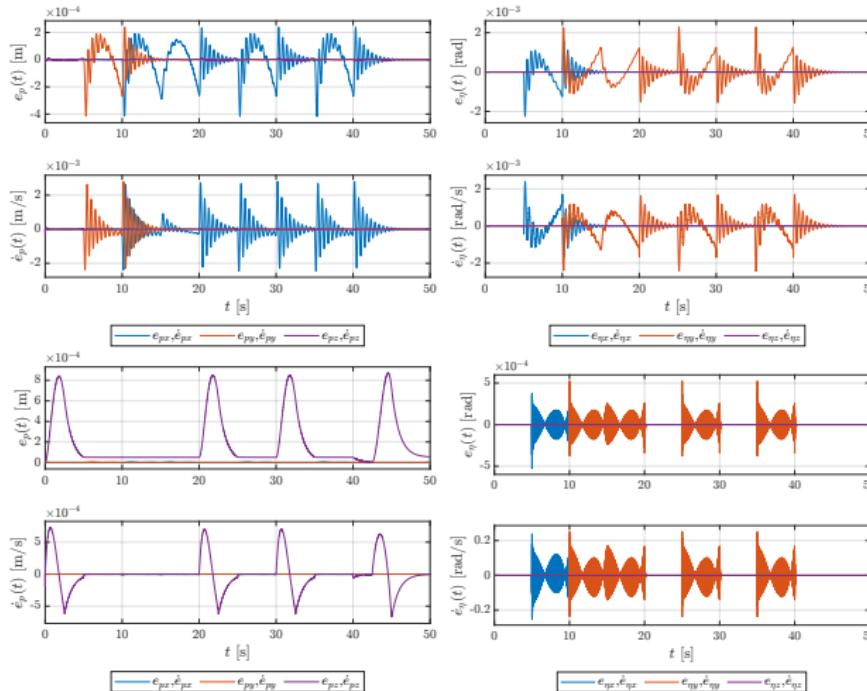


2.4. Impact of "Filter and Derivative" Block on system performance

- Hierarchical controller:
 - $w_c = 10 \text{ rad/s}$ → limit the control performance
 - $w_c = 30 \text{ rad/s}$ allows finding new optimal gains ($K_p = [100I_3 \quad 10I_3]$) and achieving performance comparable to the Geometric controller



Enhanced Hierarchical control VS Geometric control

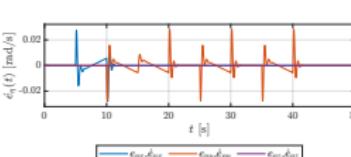
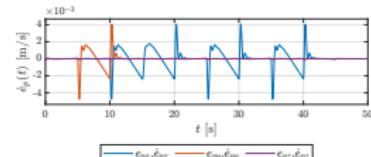
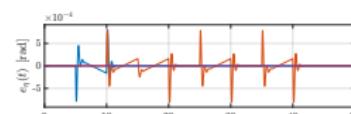
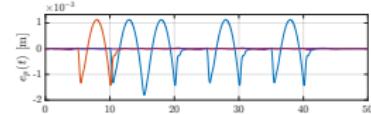
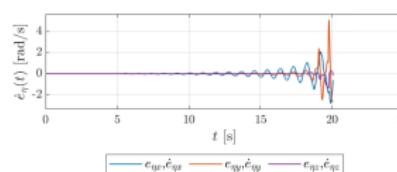
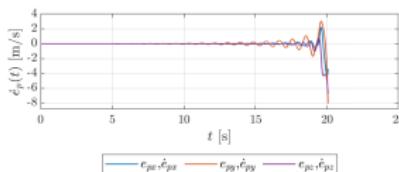
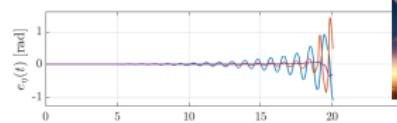
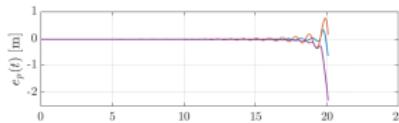


Click here to watch the Enhanced Hierarchical control



2.5. Robustness comparison

- Test: $I_b \times 5 \rightarrow$ animations: Hierarchical, Passivity-based controls
- Test: $I_b \times 50 \rightarrow$ animations: Passivity-based control





3. Momentum-based Estimator

Linear relationship between the external wrench and its estimation in the Laplace domain:

$$\mathcal{L} \begin{bmatrix} \hat{f}_e \\ \hat{\tau}_e \end{bmatrix} = G(s) \mathcal{L} \begin{bmatrix} f_e \\ \tau_e \end{bmatrix} = \text{diag}(G_1, G_2, \dots, G_6) \mathcal{L} \begin{bmatrix} f_e \\ \tau_e \end{bmatrix}$$

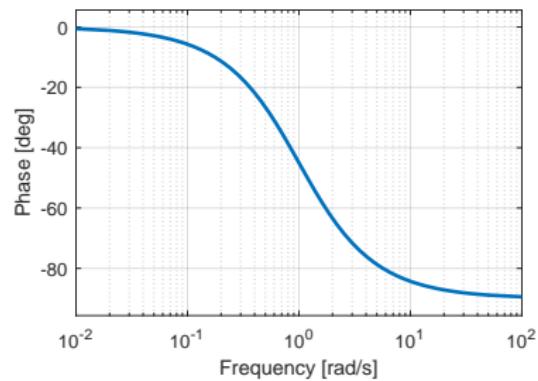
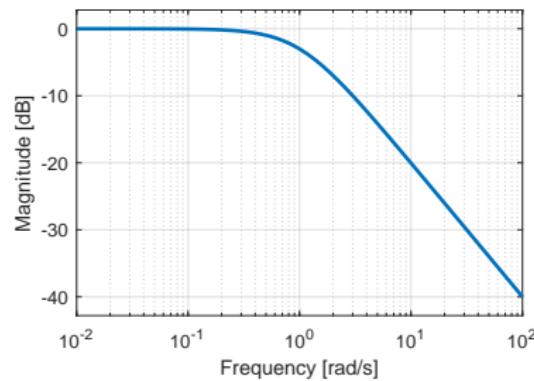
with $G(s) \in \mathbb{C}^{6 \times 6}$ diagonal matrix of transfer functions $G_i(s)$, first-order low-pass filters:

$$G_i(s) = \frac{w_c}{s + w_c}, \quad i = 1, \dots, 6$$

where $w_c = 1$ is the chosen cut-off frequency.



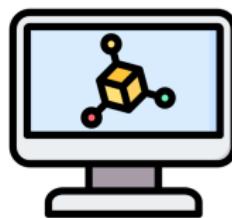
- Bode diagrams of $G_i(s)$:





4. Simulations and considerations

All the elements introduced previously are taken into account for the purpose of the simulations.



Simulation
Environment &
Elements

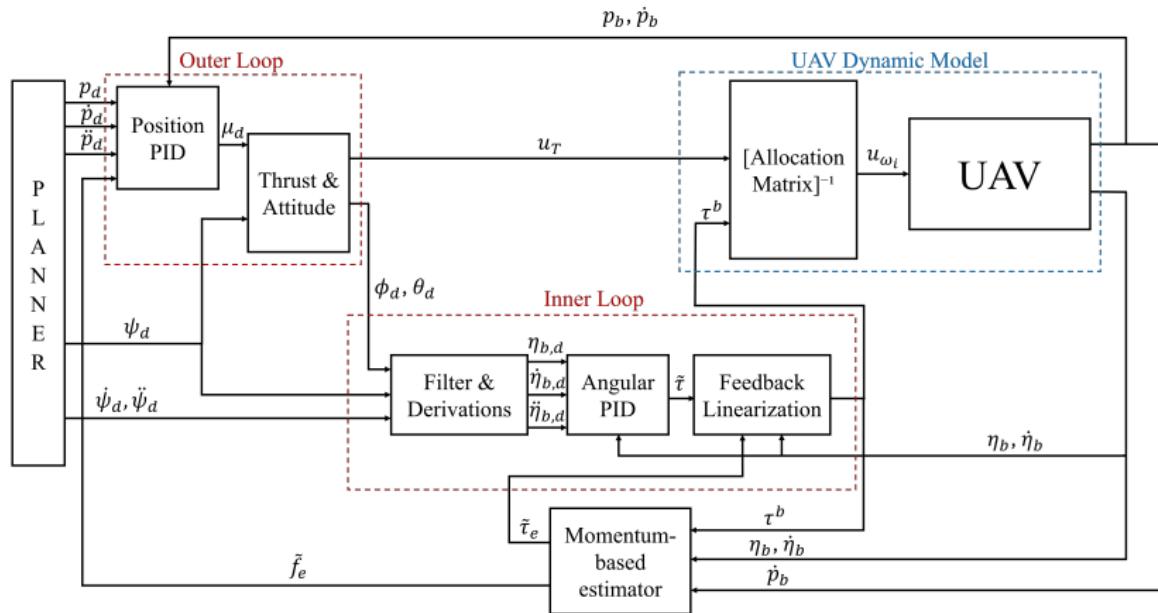


Controllers



Moment-based
Estimator

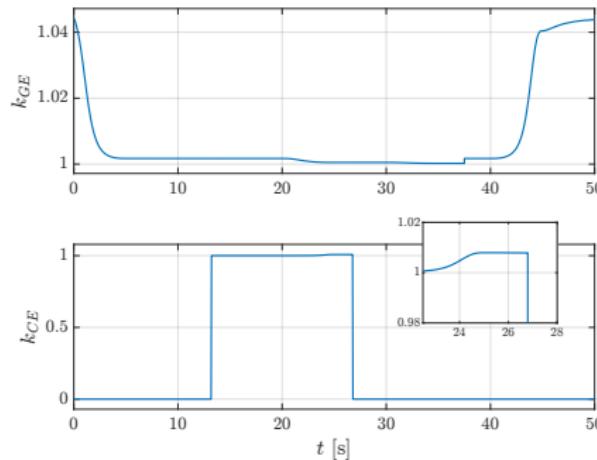
4.1. Hierarchical estimator-based control



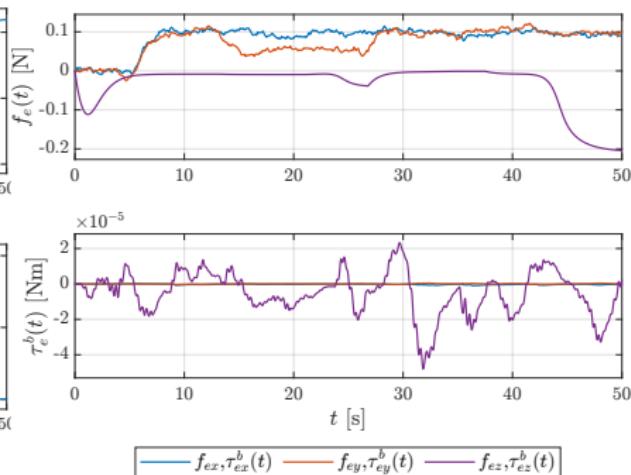


Ground and Ceiling effects Ratios & External Forces Estimation

$$K_p = 10 \begin{bmatrix} I_3 & I_3 \end{bmatrix}, \quad K_e = 100 \begin{bmatrix} I_3 & I_3 \end{bmatrix}:$$

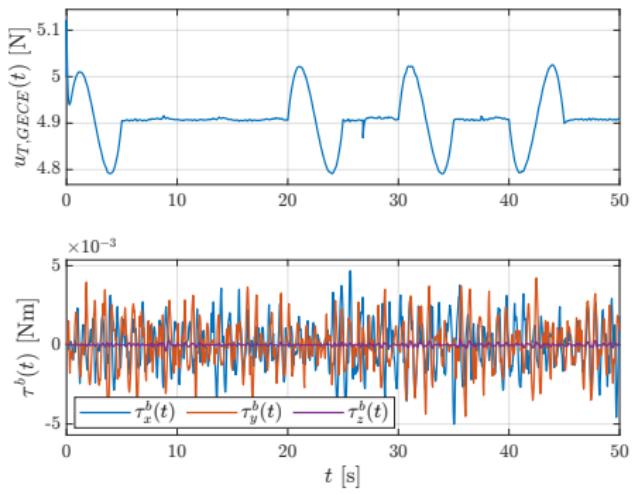


(a) Ground and ceiling effects ratios

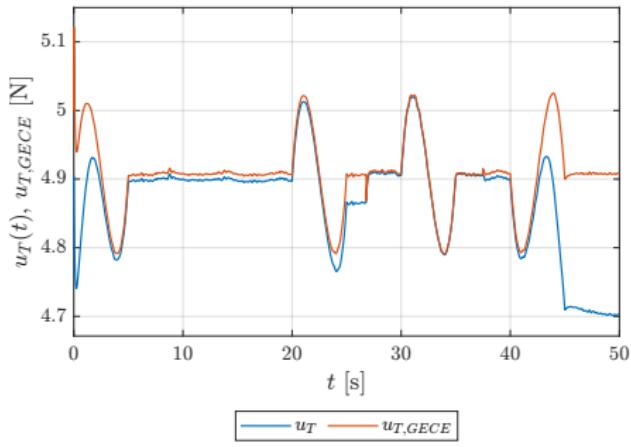


(b) External generalized forces estimate

Total thrust & torques



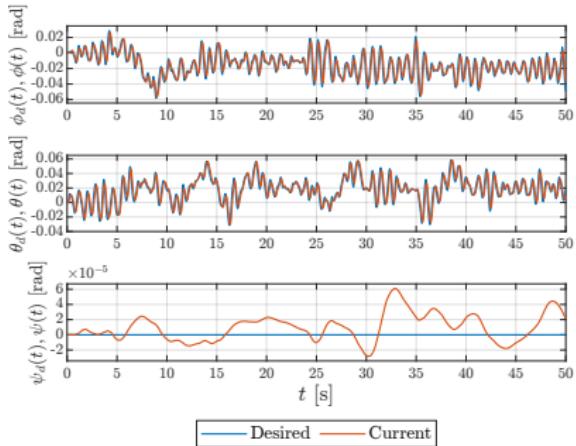
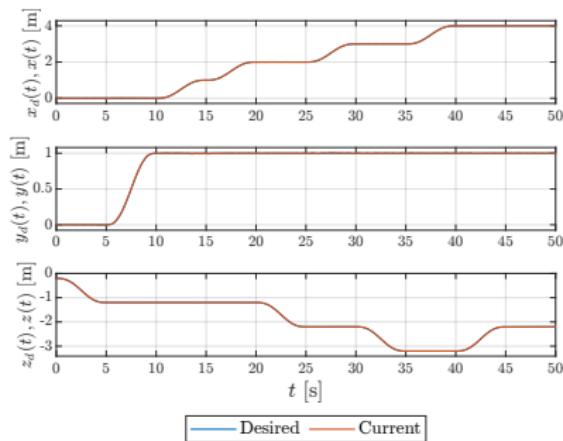
(a) Total thrust and torques.



(b) Total thrusts: generated solely by the control input and acting on the drone

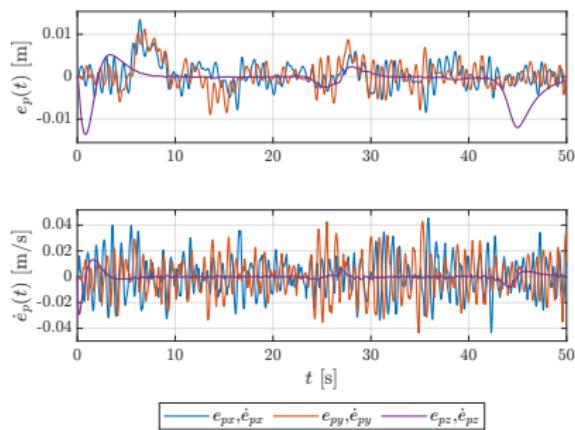


Desired & effective pose



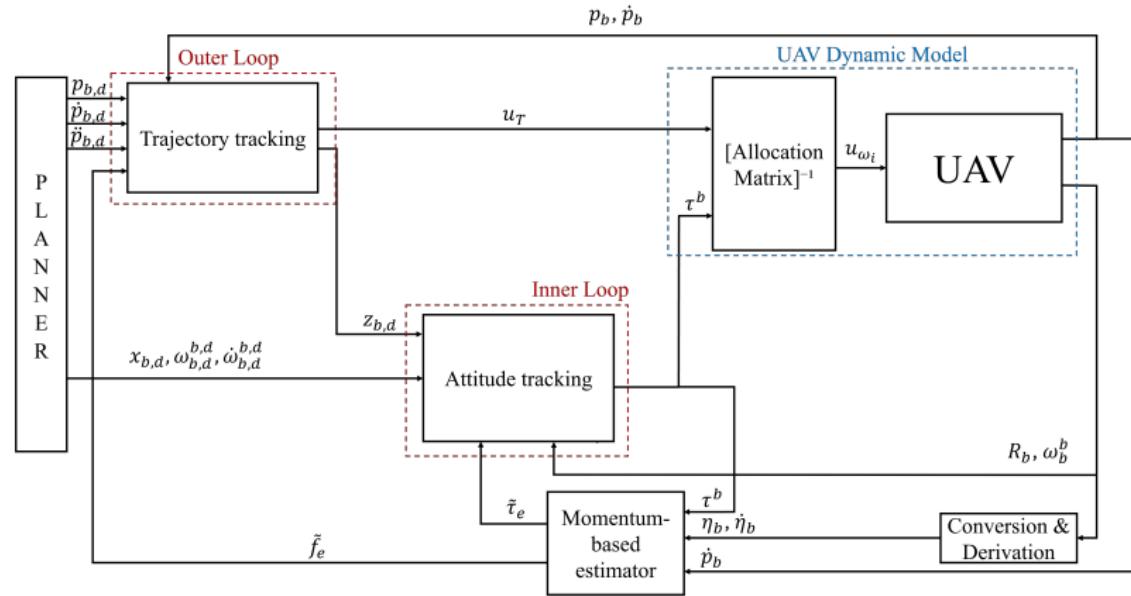


Linear & angular errors



[Click here to watch the UAV animation](#)

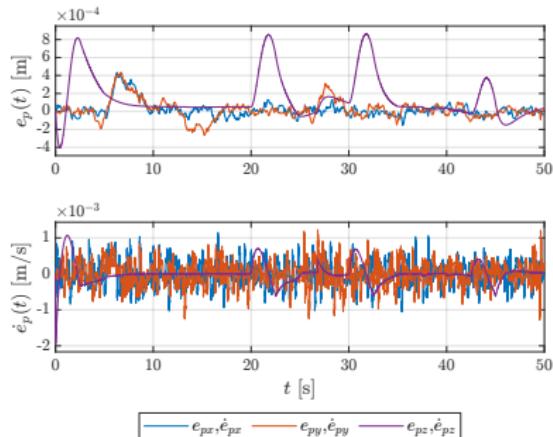
4.2. Geometric estimator-based control





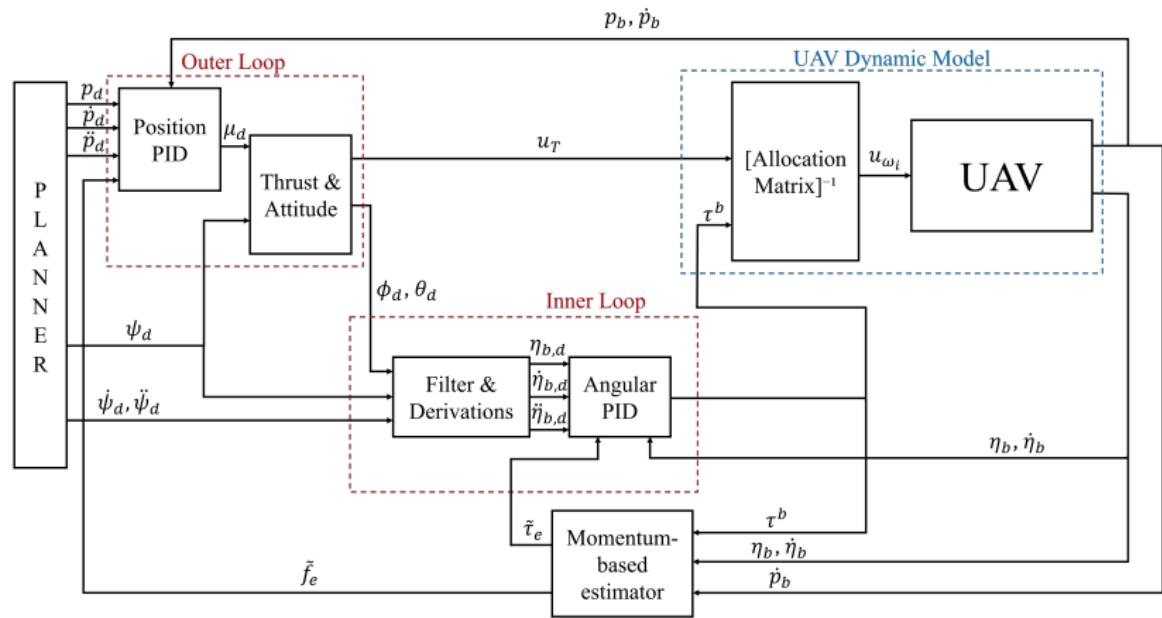
Linear & angular errors

$$K_p = K_v = 100I_3, \quad K_r = 10I_3, \quad K_w = I_3:$$



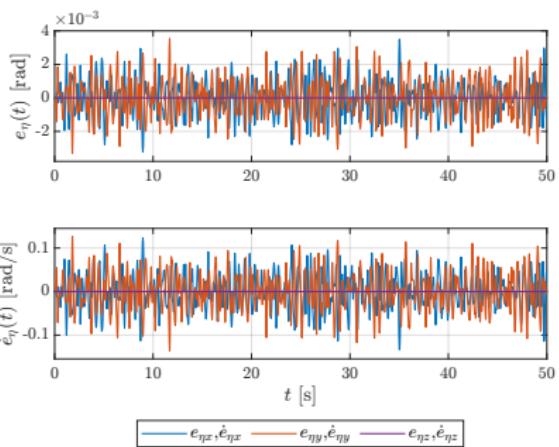
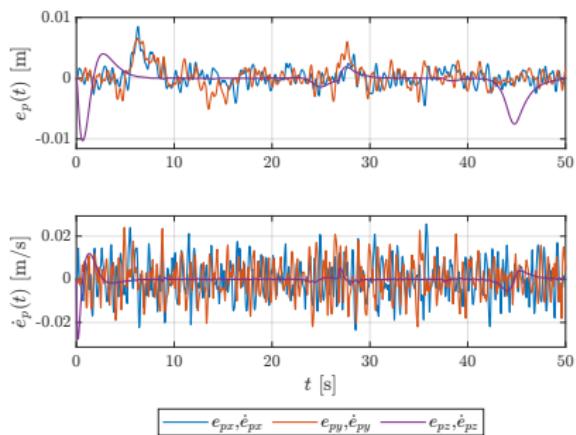
[Click here to watch the UAV animation](#)

4.3. Passivity-and-estimator-based control



Linear & angular errors

$$K_p = [20I_3 \quad 10I_3], \quad D_0 = I_3, \quad K_0 = \sigma D_0 = 20I_3:$$



[Click here to watch the UAV animation](#)



5. Conclusions

Which controller delivers the best performance?

- In an ideal scenario → **Geometric controller**
- In a realistic scenario:
 - **Geometric controller** for positional control
 - **Passivity-based controller** for angular control

What if model uncertainty is considered?

Both theory and the analysis under ideal conditions clearly indicate that the **Passivity-based controller** consistently achieves superior performance.



**THANK YOU
FOR YOUR
ATTENTION**

