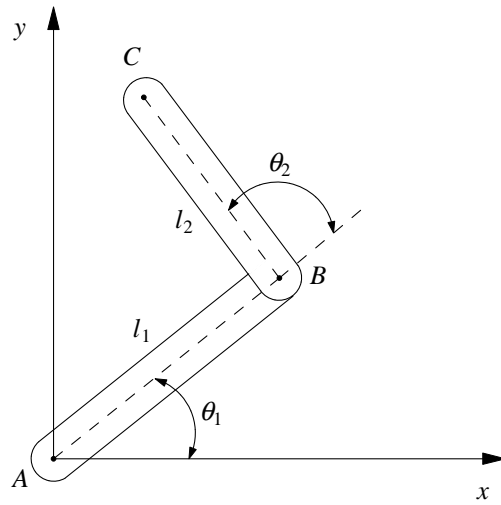


## 1. 2R Mechanism

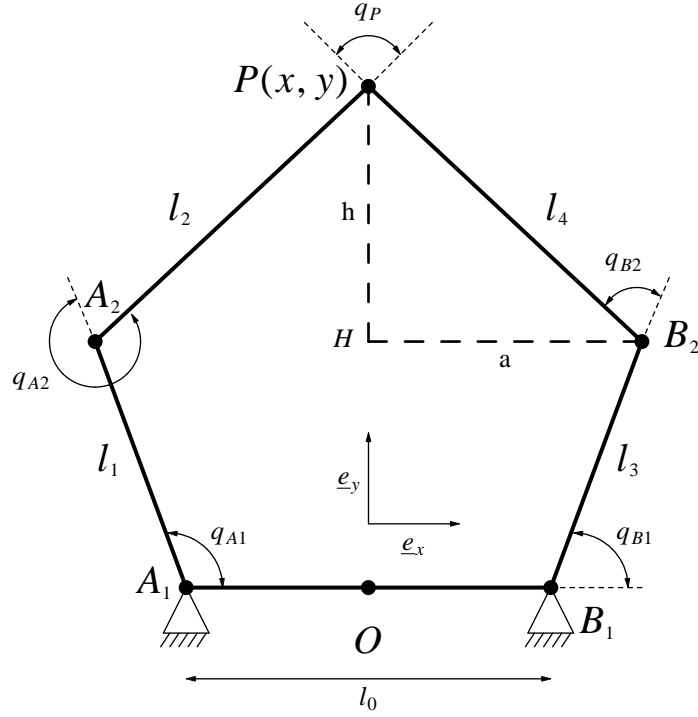


### 1.1. Direct Geometric Model

$$x = l_1 \cos \theta_1 + l_2 \cos(\theta_1 + \theta_2) \quad y = l_1 \sin \theta_1 + l_2 \sin(\theta_1 + \theta_2) \quad (1)$$

## 2. 5-bar Mechanism

### 2.1. Defining the problem



Consider the 5 bar mechanism shown above such that the viewer is seeing the top view of the mechanism. It consists of two active links of length  $l_1$  and  $l_3$ , two passive links  $l_2$  and  $l_4$ , as well as a fixed link  $l_0$ . These links are connected with revolute joints  $A_1, A_2, B_1, B_2$ , and  $P$ . The origin of the mechanism is at  $O$  and the end effector is assumed to be situated at  $P$ .

Also consider a point  $H$  positioned on the y-axis, and at the same height as  $A_1$  and  $A_2$ . This point is part of a right angle triangle  $\Delta PHB_2$  of height  $h$  and base  $a$ .

## 2.2. Direct Geometric Model

The position  $P(x, y)$  can be expressed in vector form as the sum of all the vectors from  $O$  to  $P$ .

$$\overline{OP} = \overline{OB_1} + \overline{B_2H} + \overline{HP} \quad (2)$$

First, in order to determine the co-ordinates of point  $H$ ,

$$\overline{OA_2} = l_1 \begin{bmatrix} \cos q_{A1} - \frac{d}{2} \\ \sin q_{A1} \end{bmatrix} \quad \overline{OB_2} = l_3 \begin{bmatrix} \cos q_{B1} + \frac{d}{2} \\ \sin q_{B1} \end{bmatrix} \quad (3)$$

So the co-ordinates of  $H$  are:

$$\bar{H} = \frac{1}{2} \begin{bmatrix} l_1 \cos q_{A1} + l_3 \cos q_{B1} \\ l_1 \sin q_{A1} + l_3 \sin q_{B1} \end{bmatrix} \quad (4)$$

$\overline{B_2H}$  can be expressed as follows:

$$\overline{B_2H} = \begin{bmatrix} \frac{1}{2} (l_1 \cos q_{A1} + l_3 \cos q_{B1}) - l_3 \cos q_{B1} - \frac{l_0}{2} \\ \frac{1}{2} (l_1 \sin q_{A1} + l_3 \sin q_{B1}) - l_3 \sin q_{B1} \end{bmatrix} = \begin{bmatrix} \frac{1}{2} (l_1 \cos q_{A1} - l_3 \cos q_{B1}) - \frac{l_0}{2} \\ \frac{1}{2} (l_1 \sin q_{A1} - l_3 \sin q_{B1}) \end{bmatrix} \quad (5)$$

$\overline{HP}$  can be found as:

$$\overline{HP} = \tan^{-1}\left(\frac{h}{a}\right) \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \overline{B_2H} = \tan^{-1}\left(\frac{h}{a}\right) \begin{bmatrix} \frac{1}{2} (l_3 \sin q_{B1} - l_1 \sin q_{A1}) \\ \frac{1}{2} (l_1 \cos q_{A1} + l_3 \cos q_{B1}) - \frac{l_0}{2} \end{bmatrix} \quad (6)$$

$\overline{OB_1}$  and  $\overline{B_1B_2}$  can be trivially found as,

$$\overline{OB_1} = \begin{bmatrix} \frac{l_0}{2} \\ 0 \end{bmatrix} \quad \overline{B_1B_2} = \begin{bmatrix} l_3 \cos q_{B1} \\ l_3 \sin q_{B1} \end{bmatrix} \quad (7)$$

Adding all of these equations, we obtain  $\overline{OP}$ ,

$$\overline{OP} = \begin{bmatrix} \frac{l_0}{2} \\ 0 \end{bmatrix} + \begin{bmatrix} l_3 \cos q_{B1} \\ l_3 \sin q_{B1} \end{bmatrix} + \begin{bmatrix} \frac{1}{2} (l_1 \cos q_{A1} - l_3 \cos q_{B1}) - \frac{l_0}{2} \\ \frac{1}{2} (l_1 \sin q_{A1} - l_3 \sin q_{B1}) \end{bmatrix} + \tan^{-1}\left(\frac{h}{a}\right) \begin{bmatrix} \frac{1}{2} (l_3 \sin q_{B1} - l_1 \sin q_{A1}) \\ \frac{1}{2} (l_1 \cos q_{A1} + l_3 \cos q_{B1}) - \frac{l_0}{2} \end{bmatrix}$$

$$\therefore \overline{OP} = \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} \frac{1}{2} (l_1 \cos q_{A1} + l_3 \cos q_{B1}) + \tan^{-1}\left(\frac{h}{a}\right) \frac{1}{2} (l_3 \sin q_{B1} - l_1 \sin q_{A1}) \\ \frac{1}{2} (l_1 \sin q_{A1} + l_3 \sin q_{B1}) + \tan^{-1}\left(\frac{h}{a}\right) \left[ \frac{1}{2} (l_1 \cos q_{A1} + l_3 \cos q_{B1}) - \frac{l_0}{2} \right] \end{bmatrix} \quad (8)$$

### 2.3. Inverse Geometric Model

The Inverse Geometric Model can be found by considering each half of the 5 bar mechanism separately.

#### 2.3.1. Left Half

First, let us find  $q_{A2}$  by considering the left part of the mechanism where,

$$\overline{OP} = \overline{OA_1} + \overline{A_1A_2} + \overline{A_2P} \quad (9)$$

$$\overline{OA_1} = \begin{bmatrix} -\frac{l_0}{2} \\ 0 \end{bmatrix} \quad \overline{A_1A_2} = \begin{bmatrix} l_1 \cos q_{A1} \\ l_1 \sin q_{A1} \end{bmatrix} \quad \overline{A_2P} = \begin{bmatrix} l_2 \cos(q_{A1} + q_{A2}) \\ l_2 \sin(q_{A1} + q_{A2}) \end{bmatrix} \quad (10)$$

$$\Rightarrow \overline{OP} = \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} \frac{l_0}{2} + l_1 \cos q_{A1} + l_2 \cos(q_{A1} + q_{A2}) \\ l_1 \sin q_{A1} + l_2 \sin(q_{A1} + q_{A2}) \end{bmatrix} \quad (11)$$

Consider the first row of the matrix in the above equation,

$$\cos(q_{A1} + q_{A2}) = \frac{x - \frac{l_0}{2} - l_1 \cos q_{A1}}{l_2} \quad (12)$$

Similarly, the second row can be written as,

$$\sin(q_{A1} + q_{A2}) = \frac{y - l_1 \sin q_{A1}}{l_2} \quad (13)$$

Dividing these, we get:

$$\tan(q_{A1} + q_{A2}) = \frac{2y - 2l_1 \sin q_{A1}}{2x + l_0 - 2l_1 \cos q_{A1}} \quad (14)$$

$$\therefore \boxed{q_{A1} = \tan^{-1} \left[ \frac{2y - 2l_1 \sin q_{A1}}{2x + l_0 - 2l_1 \cos q_{A1}} \right] - q_{A1}} \quad (15)$$

### 2.3.2. Right Half

Similarly, we can find  $q_{B2}$  by considering the right part of the mechanism where,

$$\overline{OP} = \overline{OB_1} + \overline{B_2H} + \overline{HP} \quad (16)$$

$$\overline{OB_1} = \begin{bmatrix} \frac{l_0}{2} \\ 0 \end{bmatrix} \quad \overline{B_1B_2} = \begin{bmatrix} l_3 \cos q_{B1} \\ l_3 \sin q_{B1} \end{bmatrix} \quad \overline{B_2P} = \begin{bmatrix} l_4 \cos(q_{B1} + q_{B2}) \\ l_4 \sin(q_{B1} + q_{B2}) \end{bmatrix} \quad (17)$$

$$\overline{OP} = \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} \frac{l_0}{2} + l_3 \cos q_{B1} + l_4 \cos(q_{B1} + q_{B2}) \\ l_3 \sin q_{B1} + l_4 \sin(q_{B1} + q_{B2}) \end{bmatrix} \quad (18)$$

Consider the first row of the matrix in the above equation,

$$\cos(q_{B1} + q_{B2}) = \frac{2x - l_0 - 2l_3 \cos q_{B1}}{l_4} \quad (19)$$

Similarly, the second row can be written as,

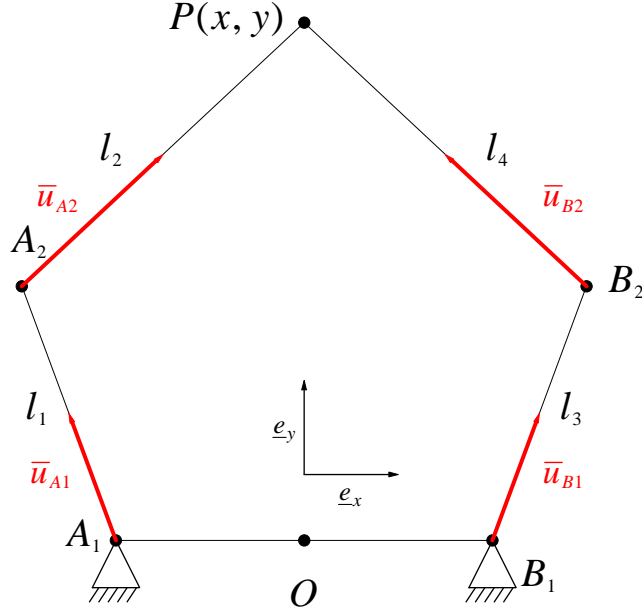
$$\sin(q_{B1} + q_{B2}) = \frac{y - l_3 \sin q_{B1}}{l_4} \quad (20)$$

Dividing these, we get:

$$\tan(q_{B1} + q_{B2}) = \frac{2y - 2l_3 \sin q_{B1}}{2x - l_0 - 2l_3 \cos q_{B1}} \quad (21)$$

$$\therefore \boxed{q_{B2} = \tan^{-1} \left[ \frac{2y - 2l_3 \sin q_{B1}}{2x - l_0 - 2l_3 \cos q_{B1}} \right] - q_{B1}} \quad (22)$$

### 2.4. Jacobian Matrix



In order to write the Jacobian matrix, first let us rewrite the problem in terms of unit vectors  $\bar{u}_{A1}$ ,  $\bar{u}_{A2}$ ,  $\bar{u}_{B1}$ , and  $\bar{u}_{B2}$ . We can also rewrite  $\overline{OP}$  as  $\mathbf{p}$  and subsequently,

$$\overline{OP} = \overline{OA_1} + \overline{A_1A_2} + \overline{A_2P} \quad \overline{OP} = \overline{OB_1} + \overline{B_1B_2} + \overline{B_2P} \quad (23)$$

$$\mathbf{p} = -\frac{l_0}{2} \bar{e}_x + l_1 \bar{u}_{A1} + l_2 \bar{u}_{A2} \quad \mathbf{p} = \frac{l_0}{2} \bar{e}_x + l_3 \bar{u}_{B1} + l_4 \bar{u}_{B2} \quad (24)$$

Differentiating both of these equations with respect to time, we get

$$\dot{\mathbf{p}} = l_1 \dot{q}_{A1} E \bar{u}_{A1} + l_2 \dot{q}_{A2} E \bar{u}_{A2} \quad \dot{\mathbf{p}} = l_3 \dot{q}_{B1} E \bar{u}_{B1} + l_4 \dot{q}_{B2} E \bar{u}_{B2} \quad (25)$$

Where  $E = \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix}$  is the rotation matrix.

Since  $\bar{u}_{A2}$  and  $\bar{u}_{B2}$  are the two unit vectors associated with the passive links. Multiplying the above equations by the transpose of these vectors, we obtain:

$$\bar{u}_{A2}^T \dot{\mathbf{p}} = l_1 \dot{q}_{A1} \bar{u}_{A2}^T E \bar{u}_{A1} + l_2 \dot{q}_{A2} \bar{u}_{A2}^T E \bar{u}_{A2} \quad \bar{u}_{B2}^T \dot{\mathbf{p}} = l_3 \dot{q}_{B1} \bar{u}_{B2}^T E \bar{u}_{B1} + l_4 \dot{q}_{B2} \bar{u}_{B2}^T E \bar{u}_{B2} \quad (26)$$

The product of a vector and its transpose is equal to 0. Hence the second terms in both of the above equations can be eliminated. By combining the remaining terms, we can form the matrices:

$$\begin{bmatrix} \bar{u}_{A2}^T \\ \bar{u}_{B2}^T \end{bmatrix} \dot{\mathbf{p}} = \begin{bmatrix} l_1 \bar{u}_{A2}^T E \bar{u}_{A1} & 0 \\ 0 & l_3 \bar{u}_{B2}^T E \bar{u}_{B1} \end{bmatrix} \begin{bmatrix} \dot{q}_{A1} \\ \dot{q}_{B2} \end{bmatrix} \quad (27)$$

If we substitute  $A = \begin{bmatrix} \bar{u}_{A2}^T \\ \bar{u}_{B2}^T \end{bmatrix}$  and  $B = \begin{bmatrix} l_1 \bar{u}_{A2}^T E \bar{u}_{A1} & 0 \\ 0 & l_3 \bar{u}_{B2}^T E \bar{u}_{B1} \end{bmatrix}$  then we have,

$$A \dot{\mathbf{p}} = B \begin{bmatrix} \dot{q}_{A1} \\ \dot{q}_{B2} \end{bmatrix} \Rightarrow \dot{\mathbf{p}} = A^{-1} B \begin{bmatrix} \dot{q}_{A1} \\ \dot{q}_{B2} \end{bmatrix} \quad (28)$$

Where Jacobian Matrix  $J = A^{-1}B$

#### 2.4.1. Calculating the Inverse Jacobian Matrix

$$A = \begin{bmatrix} \cos(q_{A1} + q_{A2}) & \sin(q_{A1} + q_{A2}) \\ \cos(q_{B1} + q_{B2}) & \sin(q_{B1} + q_{B2}) \end{bmatrix} \quad (29)$$

$$\begin{aligned} \Rightarrow \det(A) &= \sin(q_{B1} + q_{B2}) \cos(q_{A1} + q_{A2}) - \cos(q_{B1} + q_{B2}) \sin(q_{A1} + q_{A2}) \\ &= \sin(q_{B1} + q_{B2} - q_{A1} - q_{A2}) \end{aligned} \quad (30)$$

$$\text{adj}(A) = \begin{bmatrix} \sin(q_{B1} + q_{B2}) & -\sin(q_{A1} + q_{A2}) \\ -\cos(q_{B1} + q_{B2}) & \cos(q_{A1} + q_{A2}) \end{bmatrix} \quad (31)$$

$$A^{-1} = \frac{1}{\det(A)} \text{adj}(A)$$

$$\Rightarrow A^{-1} = \frac{1}{\sin(q_{B1} + q_{B2} - q_{A1} - q_{A2})} \begin{bmatrix} \sin(q_{B1} + q_{B2}) & -\sin(q_{A1} + q_{A2}) \\ -\cos(q_{B1} + q_{B2}) & \cos(q_{A1} + q_{A2}) \end{bmatrix} \quad (32)$$

#### 2.4.2. Calculating the Forward Jacobian Matrix

Now, we find the values of  $l_1 \bar{u}_{A2}^T E \bar{u}_{A1}$  and  $l_3 \bar{u}_{B2}^T E \bar{u}_{B1}$ .

$$l_1 \bar{u}_{A2}^T E \bar{u}_{A1} = l_1 [\cos(q_{A1} + q_{A2}) \quad \sin(q_{A1} + q_{A2})] \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} \cos q_{A1} \\ \sin q_{A1} \end{bmatrix} \quad (33)$$

$$= l_1 \sin(q_{A1} + q_{A2} - q_{A1}) = l_1 \sin q_{A2}$$

$$l_3 \bar{u}_{B2}^T E \bar{u}_{B1} = l_3 [\cos(q_{B1} + q_{B2}) \quad \sin(q_{B1} + q_{B2})] \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} \cos q_{B1} \\ \sin q_{B1} \end{bmatrix} \quad (34)$$

$$= l_3 \sin(q_{B1} + q_{B2} - q_{B1}) = l_3 \sin q_{B2}$$

$$\Rightarrow B = \begin{bmatrix} l_1 \sin q_{A2} & 0 \\ 0 & l_3 \sin q_{B2} \end{bmatrix} \quad (35)$$

#### 2.4.3. Calculating the Jacobian Matrix

We know that  $J = A^{-1}B$

$$J = \frac{1}{\sin(q_{B1} + q_{B2} - q_{A1} - q_{A2})} \begin{bmatrix} l_1 \sin q_{A2} \sin(q_{B1} + q_{B2}) & -l_3 \sin(q_{A1} + q_{A2}) \sin q_{B2} \\ -l_1 \sin q_{A2} \cos(q_{B1} + q_{B2}) & l_3 \cos(q_{A1} + q_{A2}) \sin q_{B2} \end{bmatrix} \quad (36)$$

## 2.5. Stiffness Matrix

The Stiffness Matrix is usually written as  $K_x = J^{-T} K_\theta J^{-1}$ . However, since Joint Stiffness  $K_\theta$  is being ignored, the Cartesian Stiffness Matrix can be written as  $K_x = J^{-T} J^{-1}$ . Where,

$$J = \frac{1}{\sin(q_{B1} + q_{B2} - q_{A1} - q_{A2})} \begin{bmatrix} l_1 \sin q_{A2} \sin(q_{B1} + q_{B2}) & -l_3 \sin(q_{A1} + q_{A2}) \sin q_{B2} \\ -l_1 \sin q_{A2} \cos(q_{B1} + q_{B2}) & l_3 \cos(q_{A1} + q_{A2}) \sin q_{B2} \end{bmatrix} \quad (37)$$