

## State Feedback controller

- Pole placement method.

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start initial si (0)0

bimorib ana paliat2

AS-A -> 2nd row napis pd

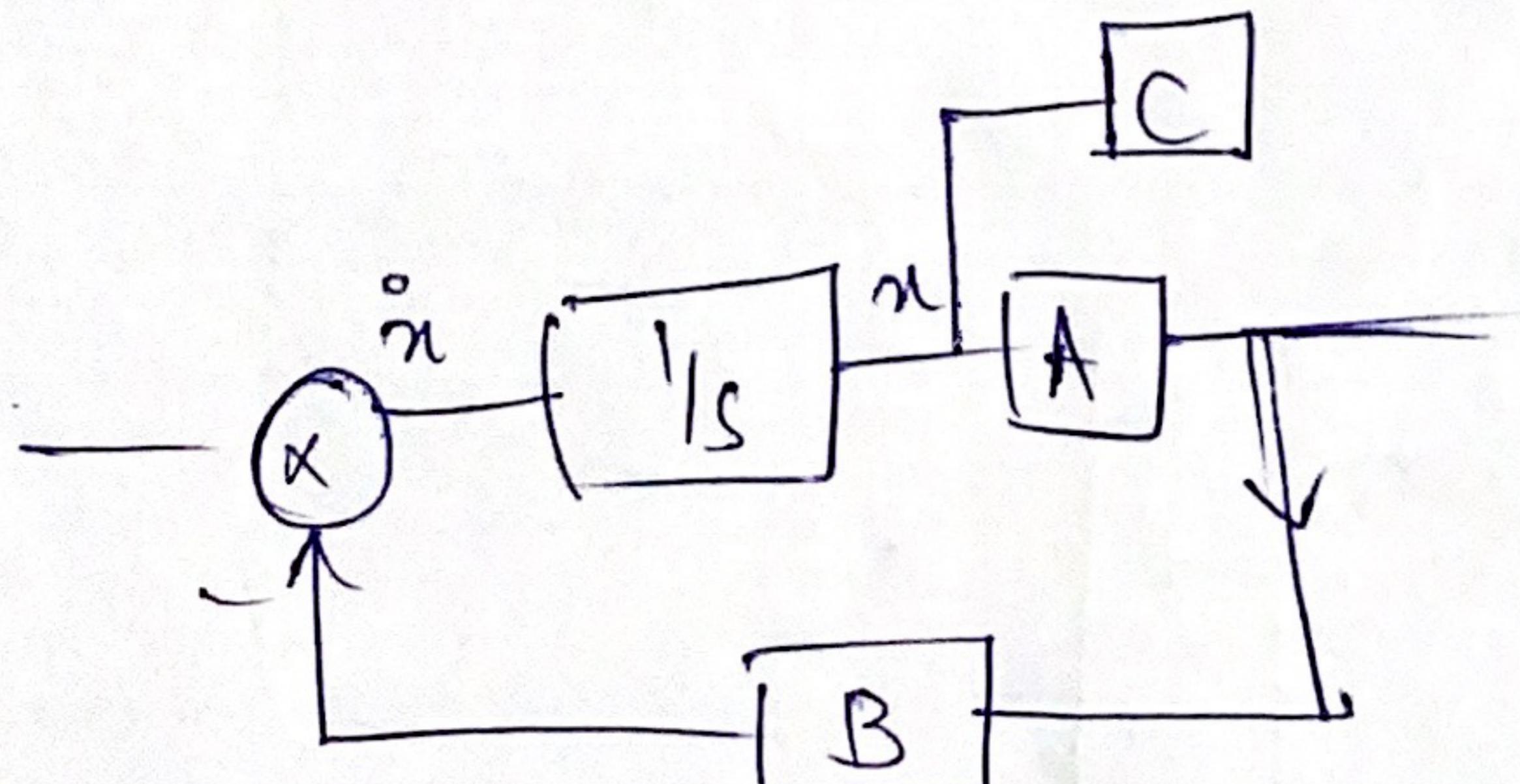
$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

we shall choose  $u = -Kx$ .

then  $\dot{x} = (A - BK)x \rightarrow ①$

$$y = (C - DK)x$$



The solution of ① is given by

$$x(t) = e^{(A-BK)t} \cdot x(0)$$

$x(0)$  is initial state.

Stability are determined  
by eigen values of  $A-BK$ .

Determination of matrix K using transformation matrix T.

Method ①

$$\dot{x} = Ax + Bu$$

$$u = -Kx$$

Step 1:

Check for controllable.

Step 2:

Finding the values of  $a_1, a_2, \dots, a_n$  from the

char. eq of matrix A.

$$|sI - A| = s^n + a_1 s^{n-1} + \dots + a_{n-1}s + a_n$$
$$\begin{bmatrix} 0 & 0 & \dots & 0 \\ 1 & 0 & \dots & 0 \\ 0 & 1 & \dots & 0 \\ \vdots & \vdots & \ddots & 1 \end{bmatrix}$$

Step 3:

Determine matrix  $T$ .

If controllable canonical form,  $T = I$

If not

$$\text{then } T = MW$$

$M = [B : AB : \dots : A^{n-1}B] \rightarrow$  controllability matrix,

$$W = \begin{bmatrix} a_{n-1} & a_{n-2} & \dots & a_1 & 1 \\ a_{n-2} & a_{n-3} & \dots & 1 & 0 \\ \vdots & \vdots & \ddots & 0 & 0 \\ a_1 & & & 0 & 0 \\ 1 & 0 & \dots & 0 & 0 \end{bmatrix}$$

Step 4:

Determine char eq with desired closed loop poles

$$(s - \alpha_1)(s - \alpha_2) \cdots (s - \alpha_n) = s^n + \alpha_1 s^{n-1} + \cdots + \alpha_{n-1} s + \alpha_n$$

Step 5:

$$K = [\alpha_n - \alpha_n : \alpha_{n-1} - \alpha_{n-1} : \dots : \alpha_2 - \alpha_2 : \alpha_1 - \alpha_1]^T$$

Ex:  $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -5 & -6 \end{bmatrix}_{3 \times 3}$        $B = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}_{3 \times 1}$

choose desired loop poles at  $s = -2 + j4$      $s = -2 - j4$      $s = -10$

Determine state feedback gain matrix K.

Step 1: Check controllability.  $A^2 = \begin{bmatrix} 0 & 0 & 1 \\ -1 & -5 & -6 \\ 6 & 29 & 31 \end{bmatrix}$

Sol.  $(sI - A)$

$$\begin{bmatrix} s & 0 & 0 \\ 0 & s & 0 \\ 0 & 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -5 & -6 \end{bmatrix} = \begin{bmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 1 & 5 & s+6 \end{bmatrix}$$

$$= s(s^2 + 6s + 5) + 1(1)$$

$$AB = \begin{bmatrix} 0 \\ 1 \\ -6 \end{bmatrix} \quad A^2 B = \begin{bmatrix} 1 \\ -6 \\ 31 \end{bmatrix} \quad = s^3 + 6s^2 + 5s + 1$$

$$\text{controllability matrix} = \begin{vmatrix} 0 & 0 & 1 \\ 0 & 1 & -6 \\ 1 & -6 & 3 \end{vmatrix} = -1$$

completely state controllable.

$$|sI - A| = s^3 + 6s^2 + 5s + 1$$

$$s^3 + a_1 s^2 + a_2 s + a_3 = 0$$

$$a_1 = 6 \quad a_2 = 5 \quad a_3 = 1$$

Here  $A$  = controllable canonical form.

desired char. polynomial.

$$\Rightarrow (s - (-2+j4))(s - (-2-j4))(s - (-10))$$

$$\Rightarrow (s+2-j4)(s+2+j4)(s+10)$$

$$(s^2 + 2s + s\cancel{j4} + 2s + 4 + \cancel{2j4} - s\cancel{j4} - 2\cancel{j4} - 16j^2)(s+10)$$

$$(s^2 + 4s + 20)(s+10)$$

$$s^3 + 4s^2 + 20s + 10s^2 + 40s + 200$$

$$s^3 + 14s^2 + 60s + 200 = 0$$

$$\alpha_1 = 14 \quad \alpha_2 = 60 \quad \alpha_3 = 200$$

then

$$K = \begin{bmatrix} 200-1 & : & 60-5 & : & 14-6 \end{bmatrix} \cdot T^{-1}$$

$$= [199 : 55 : 8]$$

$$\text{control signal, } u = -Kx - [199 \ 55 \ 8] \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

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Method ② Determination of matrix K using direct substitution

Method 1

System order  $\leq 3$

If  $n \geq 3$ , then

$$K = [k_1 \ k_2 \ k_3]$$

Sub K into desired characteristic polynomial  $(SI - A + BK)$   
and equate it to  $(s - \mu_1)(s - \mu_2)(s - \mu_3)$ .

$$(SI - A + BK) = (s - \mu_1)(s - \mu_2)(s - \mu_3)$$

equate the coeff. of like powers  
of s on both sides

Method ③

Determination of matrix K using Ackermann's formula

$$\text{Suppose } \dot{x} = Ax + Bu$$

$$\text{Control } u = -Kx.$$

Signal

desired poles are at  $s = \mu_1, s = \mu_2, \dots, s = \mu_n$ .

$$\text{then, } K = [0 \ 0 \ \dots \ 0 \ 1] [B : AB : A^2B : \dots : A^{n-1}B]^{-1}$$

where,

$$\phi(A) = A^n + \alpha_1 A^{n-1} + \alpha_2 A^{n-2} + \dots + \alpha_{n-1} A + \alpha_n I$$

$$|SI - A + BK| = \begin{bmatrix} s & 0 & 0 \\ 0 & s & 0 \\ 0 & 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -5 & 6 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \begin{bmatrix} k_1 & k_2 & k_3 \end{bmatrix}^T$$

$$\rightarrow \begin{bmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 1 & 5 & s+6 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ k_1 & k_2 & k_3 \end{bmatrix}$$

$$\rightarrow \begin{bmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 1+k_1 & 5+k_2 & s+6+k_3 \end{bmatrix}$$

$$= s(s(s+6+k_3) + (5+k_2)) + 1(1+k_1)$$

$$= s^3 + (6+k_3)s^2 + (5+k_2)s + 1+k_1$$

$$\Rightarrow s^3 + (4s^2 + 60s + 200) \quad \text{desired poles char. polynomial}$$

Compare

$$6+k_3 = 14 \rightarrow k_3 = 8$$

$$5+k_2 = 60 \rightarrow k_2 = 55$$

$$1+k_1 = 200 \rightarrow k_1 = 199.$$

General eq.

$$k_3 = \alpha_1 - \alpha_1$$

$$k_2 = \alpha_2 - \alpha_2$$

$$k_1 = \alpha_3 - \alpha_3$$

Ex. Method ③

$$K = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix} [B : AB : A^2B]^{-1} \phi(A)$$

$$\phi(A) = A^3 + \alpha_1 A^2 + \alpha_2 A + \alpha_3 I$$

$$= \begin{bmatrix} -1 & -5 & -6 \\ 6 & 29 & 31 \\ -31 & -149 & -157 \end{bmatrix} + 14 \begin{bmatrix} 0 & 0 & 1 \\ -1 & -5 & -6 \\ 6 & 29 & 31 \end{bmatrix} + 60 \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -5 & -6 \end{bmatrix} + 200 \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\phi(A) = \begin{bmatrix} 199 & 55 & 8 \\ -8 & 159 & 7 \\ -7 & -43 & 117 \end{bmatrix} + ((\alpha_1 + \alpha_2 + \alpha_3)I + (\alpha_1 A + \alpha_2 A^2 + \alpha_3 A^3))e$$

$$K = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 0 & 1 \\ 0 & 1 & -6 \\ 1 & -6 & 31 \end{bmatrix}^{-1} \begin{bmatrix} 199 & 55 & 8 \\ -8 & 159 & 7 \\ -7 & -43 & 117 \end{bmatrix}$$

$$K = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 5 & -6 & 1 \\ 6 & 1 & 0 \\ 1 & 0 & 0 \end{bmatrix}$$

$$K = \begin{bmatrix} 199 & 55 & 8 \end{bmatrix}$$

when there is an input.

$$\dot{x} = Ax + Bu$$

then  $u = -Kx + r$

then,  $\dot{x} = Ax + B(-Kx + r)$

$$\dot{x} = (A - BK)x + Br$$

State Observer.

mathematical  
model of  
Observer

observer gain.

$$\dot{\tilde{x}} = A\tilde{x} + Bu + k_e(y - C\tilde{x})$$

$$= (A - k_e C)\tilde{x} + Bu + k_e y$$

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## Non-linear

$$r_B + s(u_B \cdot A) = j$$

nonlinear terms

drop terms

higher order terms

to linear

now drop

$$(r_B + p_B) + u_B + k_A = f$$

$$r_B + u_B + k_A(2\delta_N - 1) =$$

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## Common Nonlinear System behaviour.

$$\dot{x} = -x + x^2$$

Linearised system I  ~~$\dot{x} = -x$~~   $\Rightarrow x(t) = x_0 e^{-t}$

non-linear system II  $\dot{x} = -x + x^2 \Rightarrow x(t) = \frac{x_0 e^{-t}}{1 - x_0 + x_0 e^{-t}}$

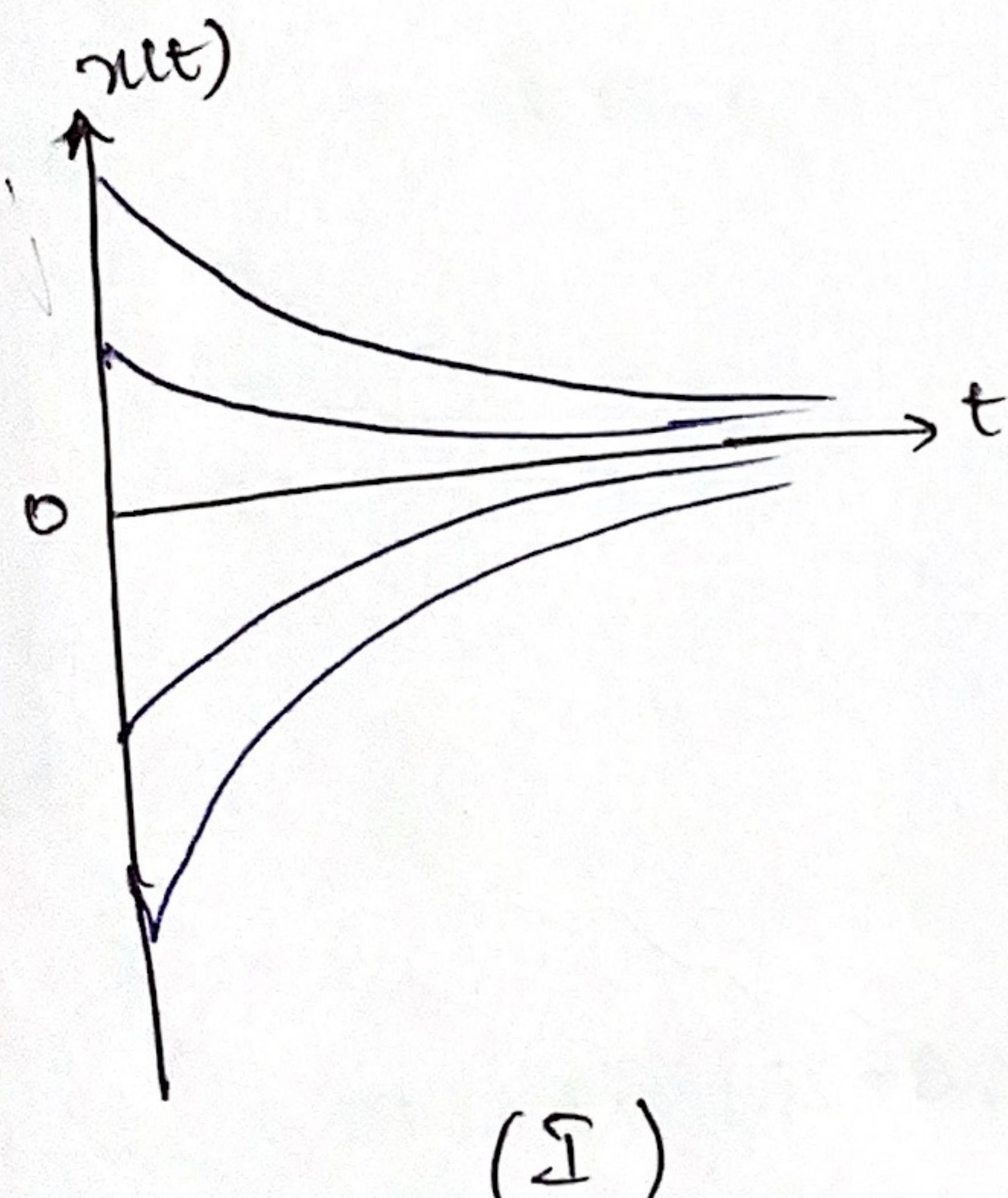
eq. points for I

$$\dot{x} = 0 \Rightarrow x = 0.$$

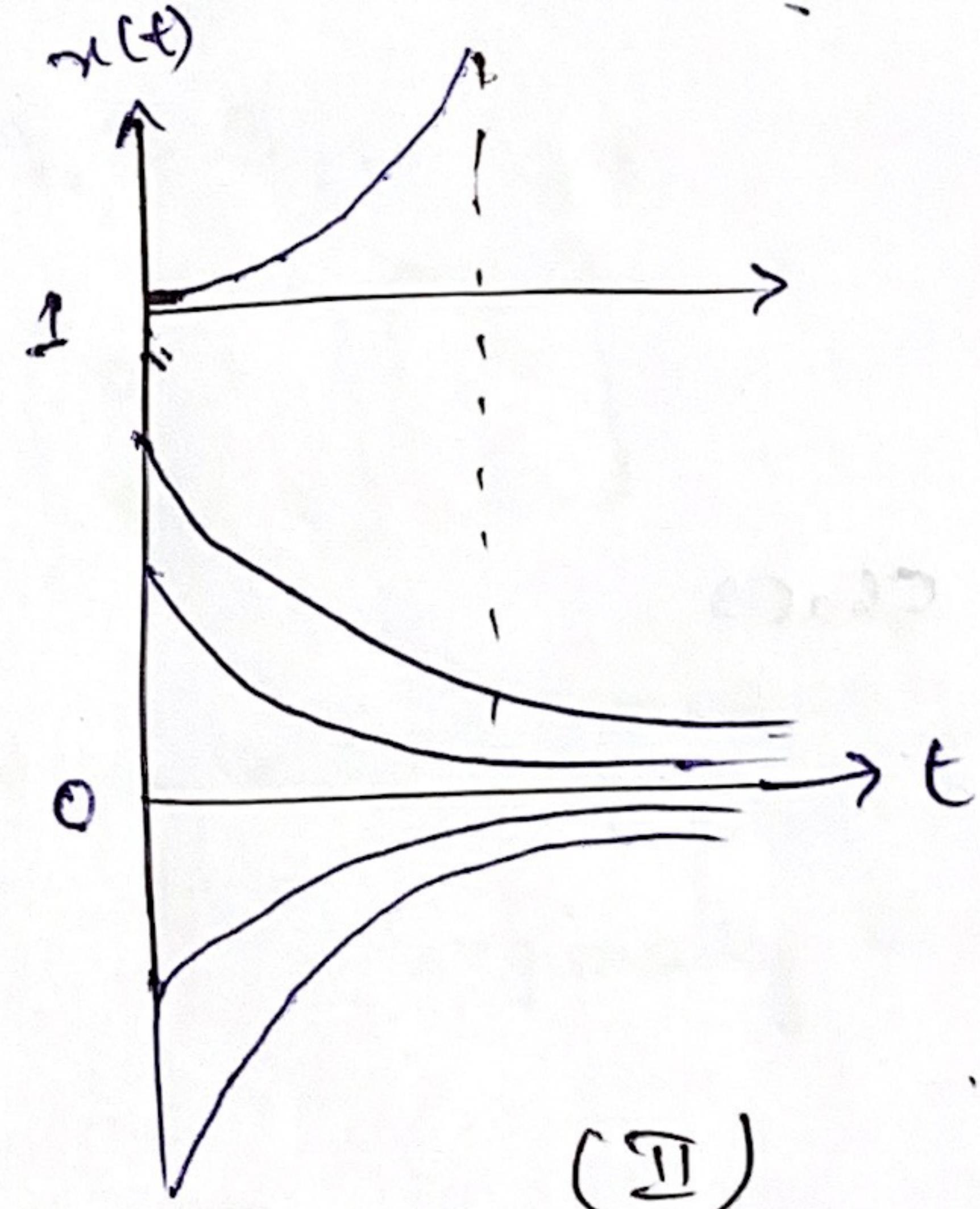
for II

~~$\dot{x} =$~~   $-x + x^2 = 0$

$$\Rightarrow x = 0, 1 \rightarrow \text{eq. points.}$$



(I)



(II)

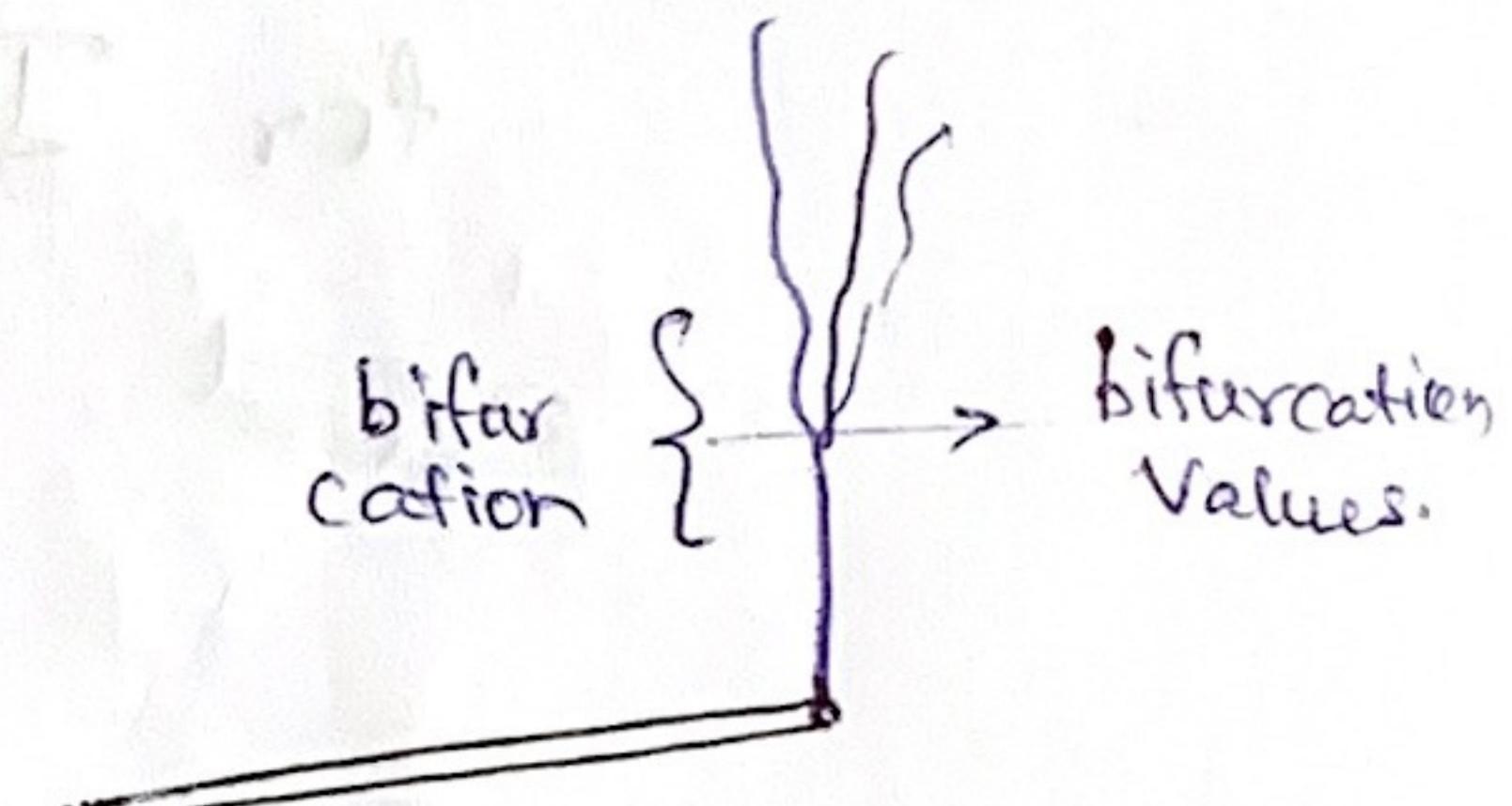
Second order nonlinear diff. eq'

$$m\ddot{x} + 2C(x^2 - 1)\dot{x} + kx = 0 \rightarrow \text{Vander Pol equation.}$$

limit cycles.

self excited oscillations.

Bifurcation.



Chaos

Jump response.



$$\ddot{\theta} + \frac{g}{l} \sin \theta = 0$$

$$x_1 = \theta$$

$$\dot{\theta} = \omega$$

eq. points

$$x_2 = \theta'$$

$$\ddot{\omega} = -\frac{g}{l} \sin \theta$$

$$(0, 0) (\pi, 0)$$

for  $l=1\text{m}$ .

$$\dot{\theta} = \omega$$

$$\ddot{\omega} = -9.81 \sin \theta$$

At eq., all derivatives are zero.

$$0 = \omega_d$$

$$\omega_d = 0$$

$$0 = -9.81 \sin \theta_d$$

$$\theta_d = \begin{cases} 0 \text{ rad} \\ \pi \text{ rad} \end{cases}$$

Consider a small deviation around eq.-point  $\theta_d = 0$

$$\theta = \theta_d + \epsilon_1 = \epsilon_1$$

$$\omega = \cancel{\omega_d} \cdot \omega_d + \epsilon_2 = \epsilon_2$$

for  $\theta_d = 0$ :

$$\epsilon_1 = \epsilon_2$$

using Maclaurin series:

$$\dot{\epsilon}_2 = -9.81 \sin \epsilon_1$$

$$\sin \epsilon_1 \approx \epsilon_1$$

$$\dot{\epsilon}_1 = \epsilon_2$$

$$\begin{bmatrix} \dot{\epsilon}_1 \\ \dot{\epsilon}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -9.81 & 0 \end{bmatrix} \begin{bmatrix} \epsilon_1 \\ \epsilon_2 \end{bmatrix}$$

for  $\theta_d = \pi$

$$\dot{\epsilon}_1 = \epsilon_2$$

$$\dot{\epsilon}_2 = -9.81 \sin(\pi + \epsilon_1)$$

$$\dot{\epsilon}_2 = 9.81 \epsilon_1$$

eigen values

$$0 + 3.13^\circ$$

$$0 - 3.13^\circ$$

marginally stable.

$$\begin{bmatrix} \dot{\epsilon}_1 \\ \dot{\epsilon}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 9.81 & 0 \end{bmatrix} \begin{bmatrix} \epsilon_1 \\ \epsilon_2 \end{bmatrix}$$

eigen values  $-3.13$

$$-3.13$$

Unstable.

$$Q. \quad 2xi + 18xi + 128000 - \frac{x^2}{x+2} = 0.03f \quad \text{find eq. points}$$

or 0.03 f = 80.

(0, 0) (10, 0)

and  $P = \frac{1}{2} \pi r^2$

$\pi(10)^2 / 2 = 157$

$C_1 = 0$

$10^2/2 \cdot 18 \cdot P = C_1$

10000/200 = 500

$P = 500$

$10^2/2 \cdot 18 \cdot P = 500$

$10000/200 = 500$

0 <  $x < 10$  so domain positive since  $x$  is radius

$$P = 10^2/2 \cdot 18 = 900$$

$$P = 10^2/2 \cdot 18 = 900$$

three corner points

$$P = 10^2/2 \cdot 18 = 900$$

10000/200 = 500

$$P = 10^2/2 \cdot 18 = 900$$

$$\begin{pmatrix} 10 \\ 0 \end{pmatrix} \begin{pmatrix} 10 \\ 10 \end{pmatrix} \begin{pmatrix} 10 \\ 20 \end{pmatrix}$$

$$P = 10^2/2 \cdot 18 = 900$$

$$P = 10^2/2 \cdot 18 = 900$$

10000/200 = 500

$$P = 10^2/2 \cdot 18 = 900$$

state uniform

$$P = 10^2/2 \cdot 18 = 900$$

$$(10^2/2 \cdot 18) \cdot 10^2/2 \cdot 18 = 900$$

$$P = 10^2/2 \cdot 18 = 900$$

$$\begin{pmatrix} 10 \\ 10 \end{pmatrix} \begin{pmatrix} 10 \\ 20 \end{pmatrix} \begin{pmatrix} 20 \\ 20 \end{pmatrix}$$

10000/200 = 500

10000/200 = 500

state uniform

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# Phase plane analysis

$(x_1, x_2) \in \mathbb{R}^2$   $\dot{x}_1 = f_1(x_1, x_2)$  +  $\dot{x}_2 = f_2(x_1, x_2)$   $\approx$  LTI system

2nd order autonomous system

$$\ddot{x}_1 = f_1(x_1, x_2)$$

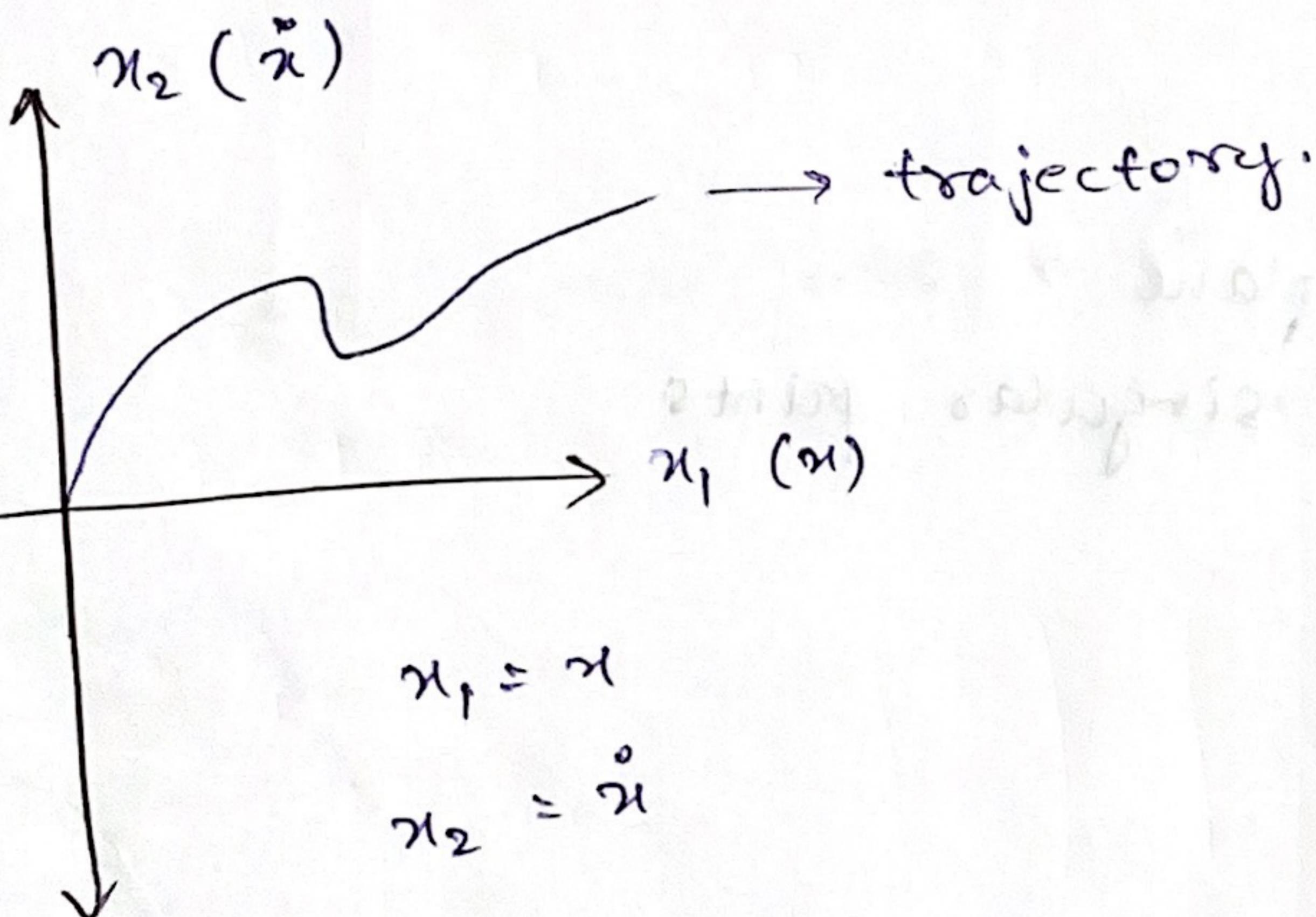
$$\ddot{x}_2 = f_2(x_1, x_2)$$

$x_1, x_2$  are states

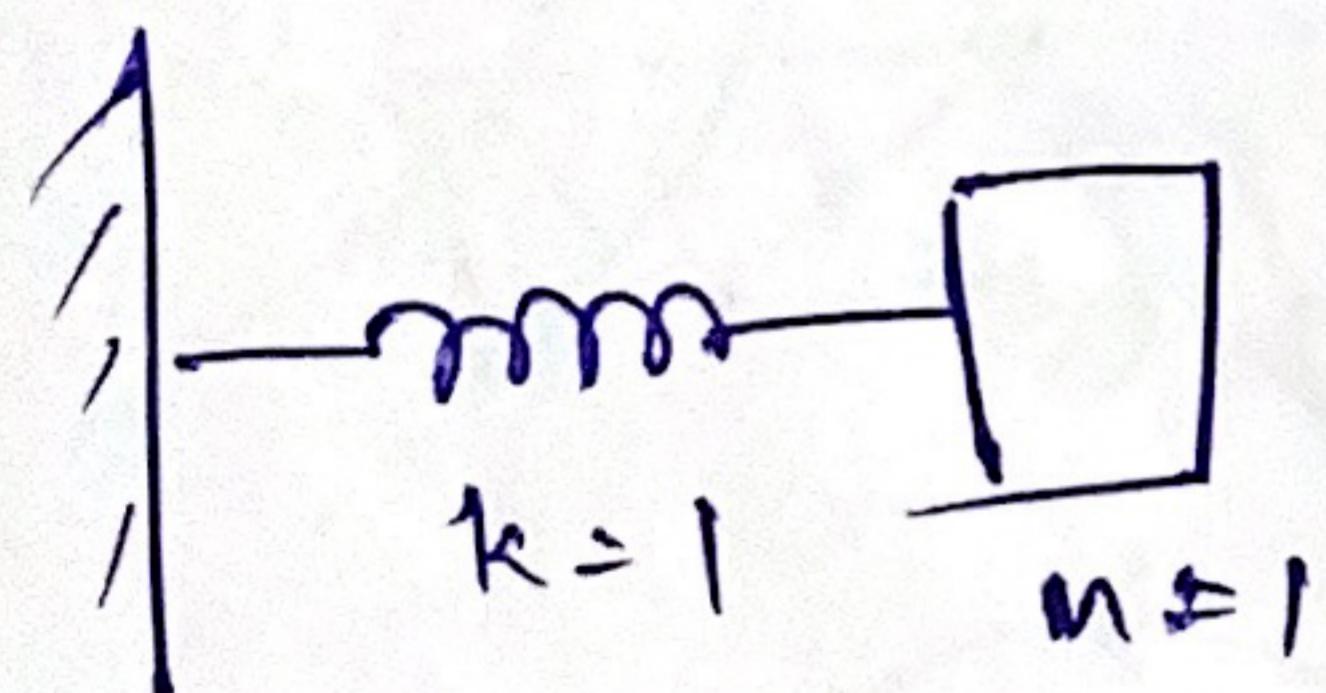
$f_1, f_2$  are non-linear functions

State space of this system is a plane having  $x_1, x_2$  as coordinates.

This is called as phase plane.



Mass spring system.



$$\ddot{x} + x = 0. \quad x(0) = x_0$$

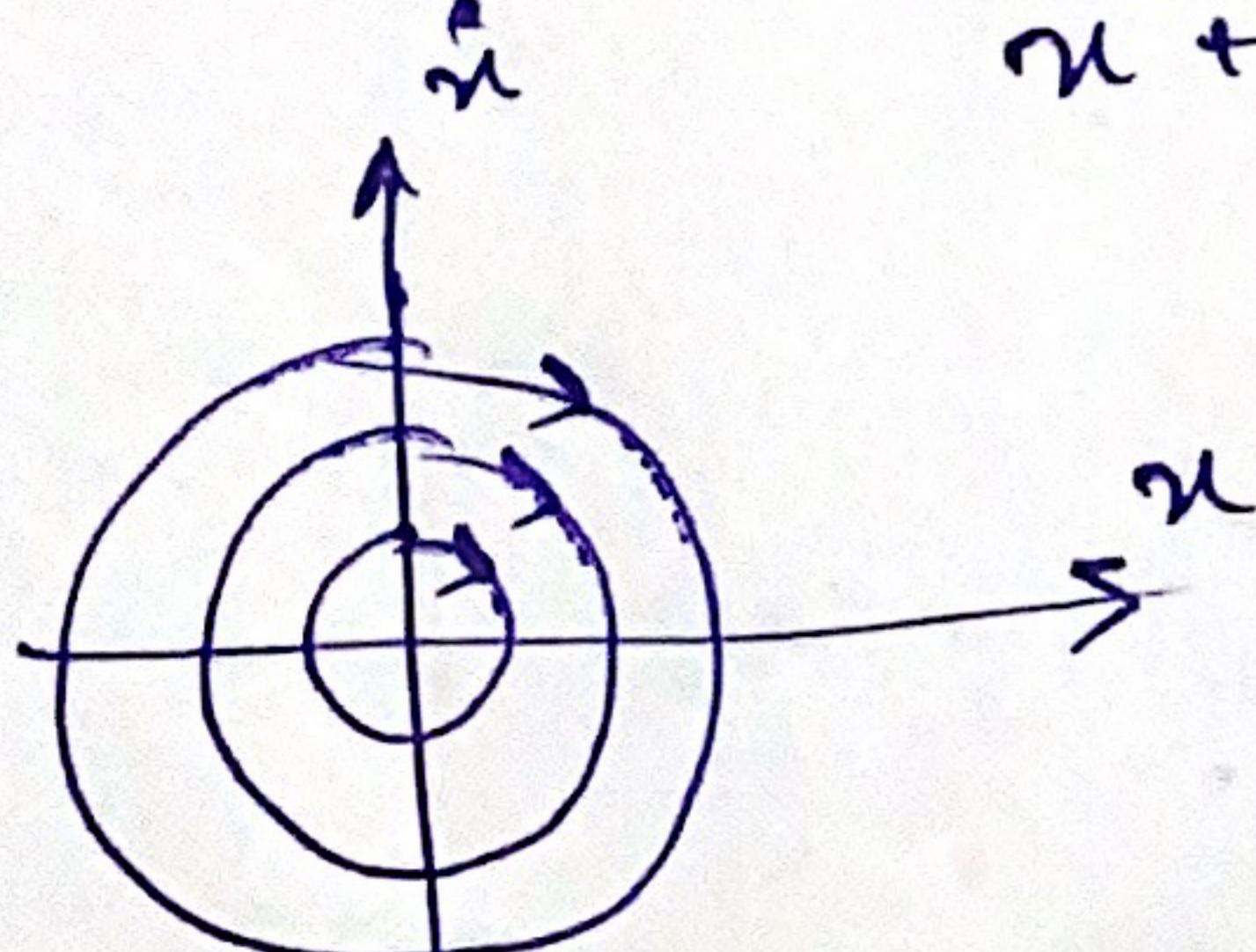
$$\dot{x}(0) = 0.$$

$$\text{Solution } x(t) = x_0 \cos t$$

$$\dot{x}(t) = -x_0 \sin t$$

$$x^2 + \dot{x}^2 = x_0^2$$

This is a circle.



2nd order system:

$$\ddot{x} + f(x, \dot{x}) = 0 \quad x = f_1(x_1, x_2)$$
$$\dot{x}_1 = x_2 = f_1(x_1, x_2) \quad \dot{x}_2 = f_2(x_1, x_2)$$
$$\dot{x}_2 = -f_0(x_1, x_2) = f_2(x_1, x_2)$$

for eq. point /

$$f_1(x_1, x_2) = 0$$

$$f_2(x_1, x_2) = 0$$

eq. points on phase plane  
are called singular points

ex:  $\ddot{x}_1 + 0.6x_1 + 3x_1 + x_1^2 = 0$

$$x_1 = \dot{x}$$

$$x_2 = \ddot{x}$$

$$\ddot{x}_1 = x_2$$

$$\ddot{x}_2 = \ddot{\dot{x}} = -x_1^2 - 3x_1 - 0.6\dot{x}$$

$$\ddot{x}_2 = -x_1^2 - 3x_1 - 0.6x_2$$

for eq. points

$$\dot{x}_1 = 0 \Rightarrow x_2 = 0$$

$$\dot{x}_2 = 0 \Rightarrow -x_1^2 - 3x_1 - 0.6x_2 = 0$$

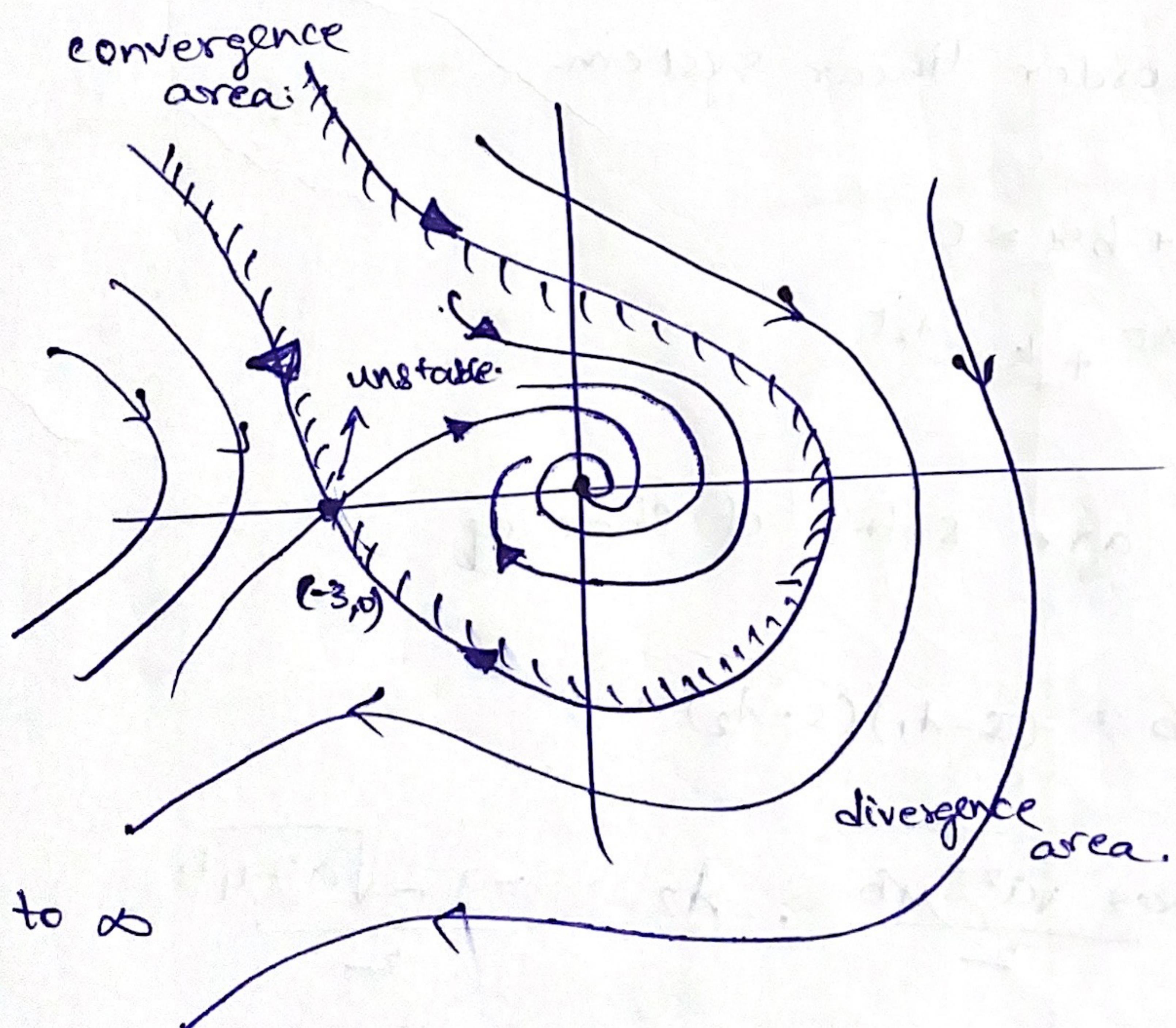
$$x_1^2 + 3x_1 = 0$$

$$x_1(x_1 + 3) = 0$$

$$\Rightarrow x_1 = 0, -3$$

eq. points are  $(0, 0)$

&  $(-3, 0)$

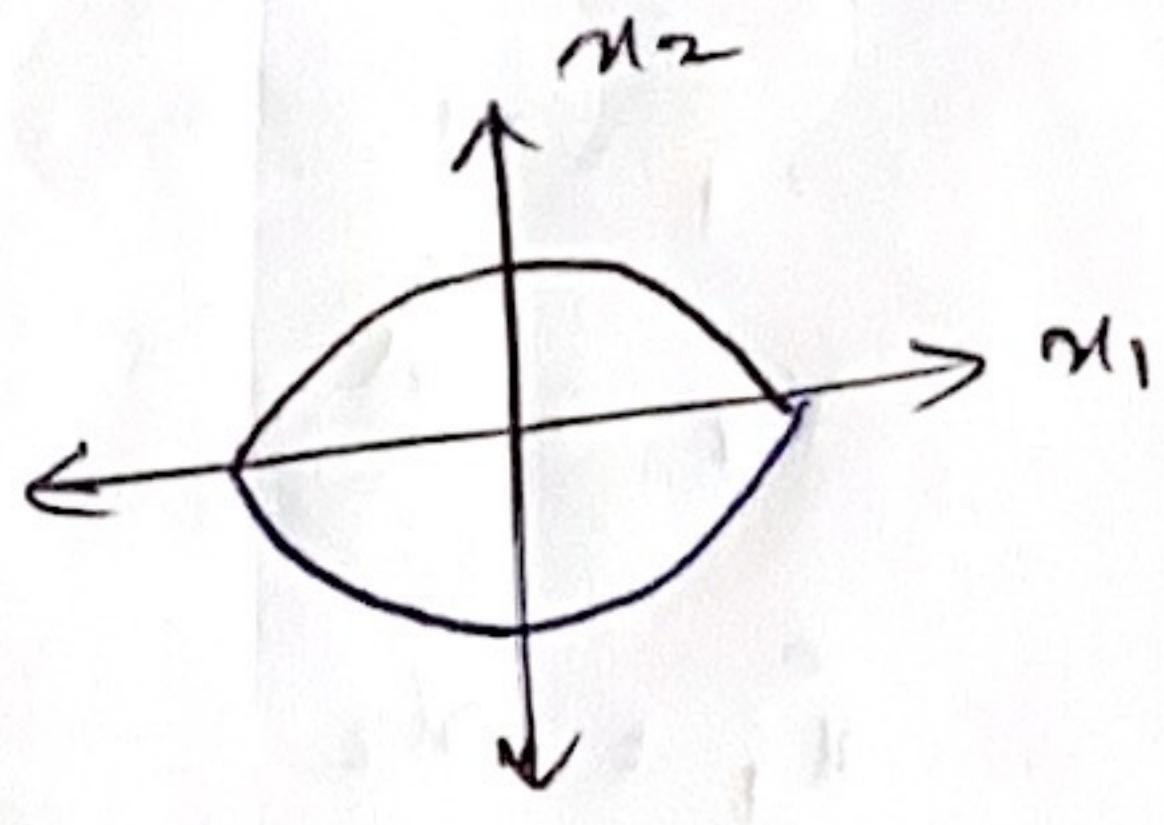


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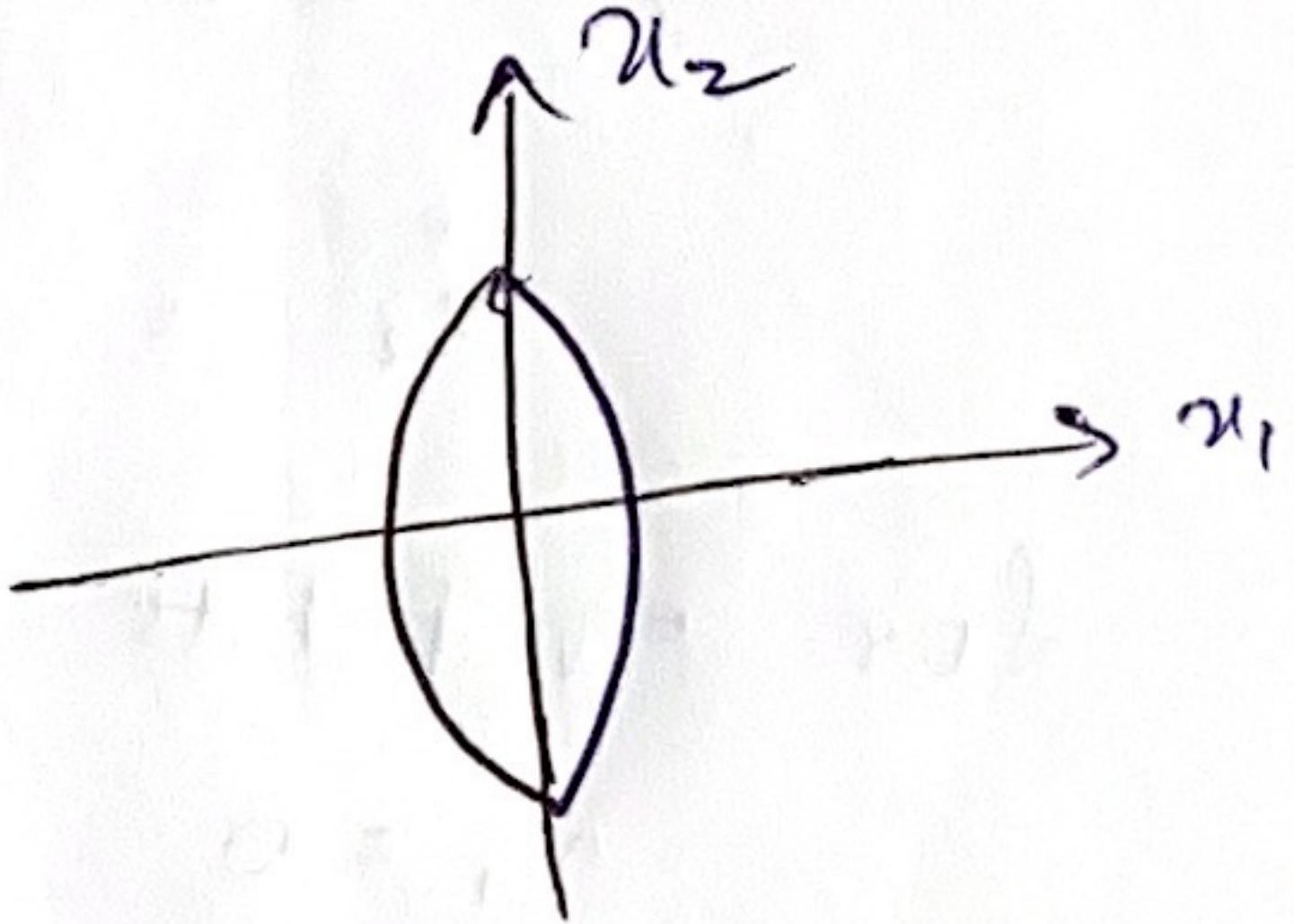
## Symmetry in phase plane portraits

Symmetry about the  $x_1$  axis

$$f(x_1, x_2) = f(x_1, -x_2)$$

Symmetry about the  $x_2$  axis

$$f(x_1, x_2) = f(-x_1, x_2)$$

about  $x_1$  &  $x_2$  axes.

$$f(x_1, x_2) = f(x_1, -x_2) = -f(-x_1, x_2)$$

only one quarter of it has to be explicitly considered

about origin

$$f(x_1, x_2) = -f(-x_1, -x_2)$$

Consider 2nd order linear system.

$$\ddot{x} + a\dot{x} + bx = 0$$

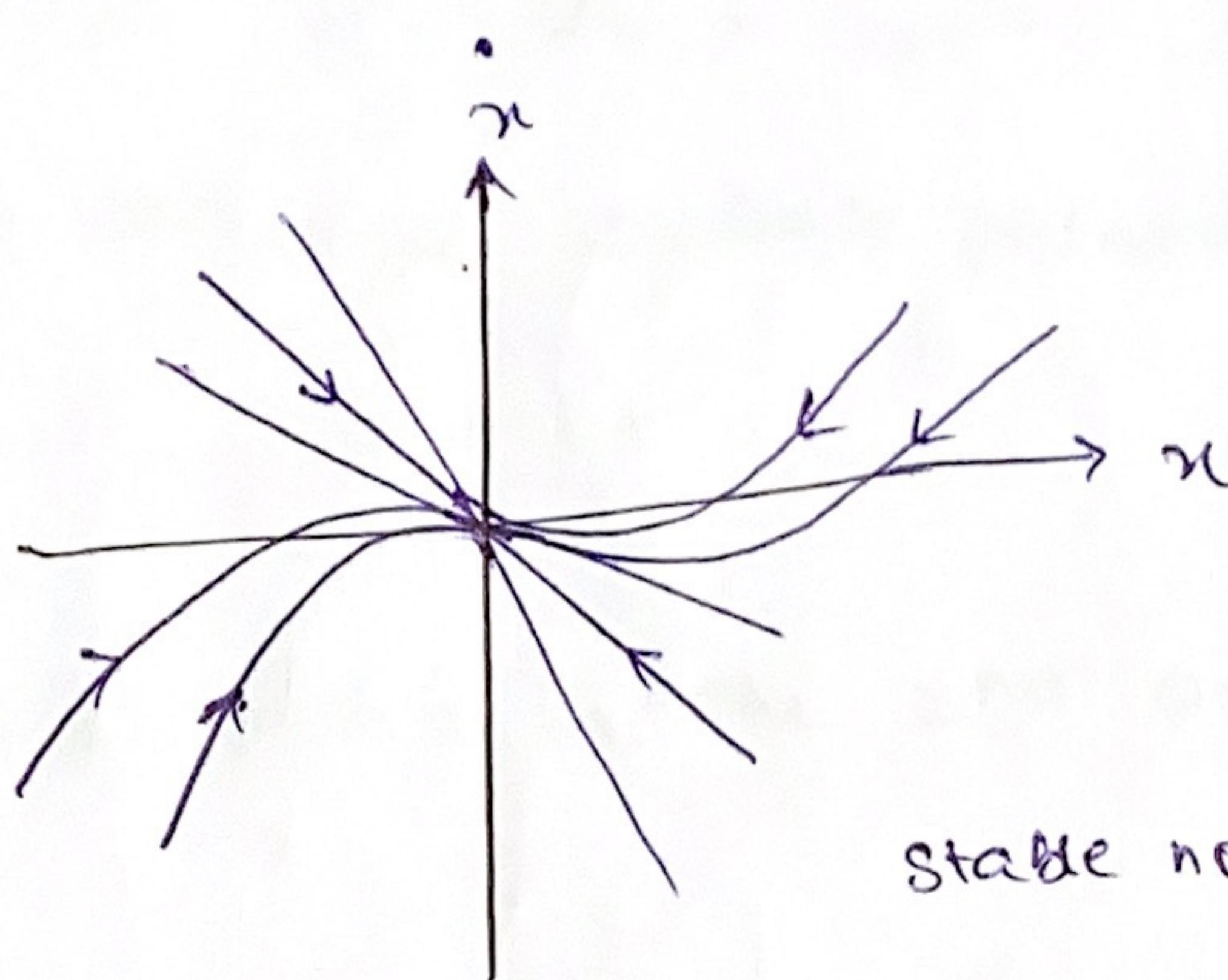
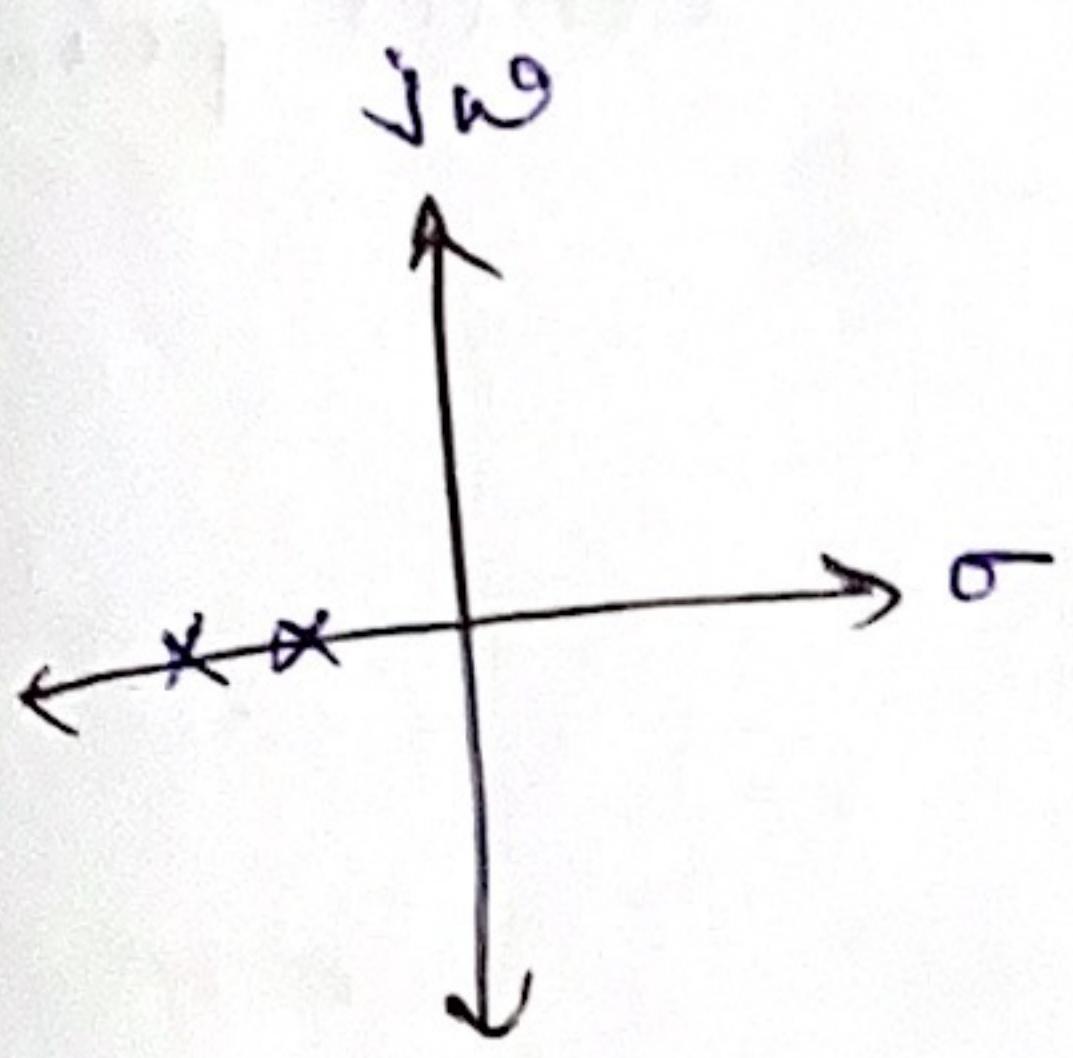
$$x(t) = k_1 e^{\lambda_1 t} + k_2 e^{\lambda_2 t}$$

 $\lambda_1, \lambda_2$  are soln's of char eq.

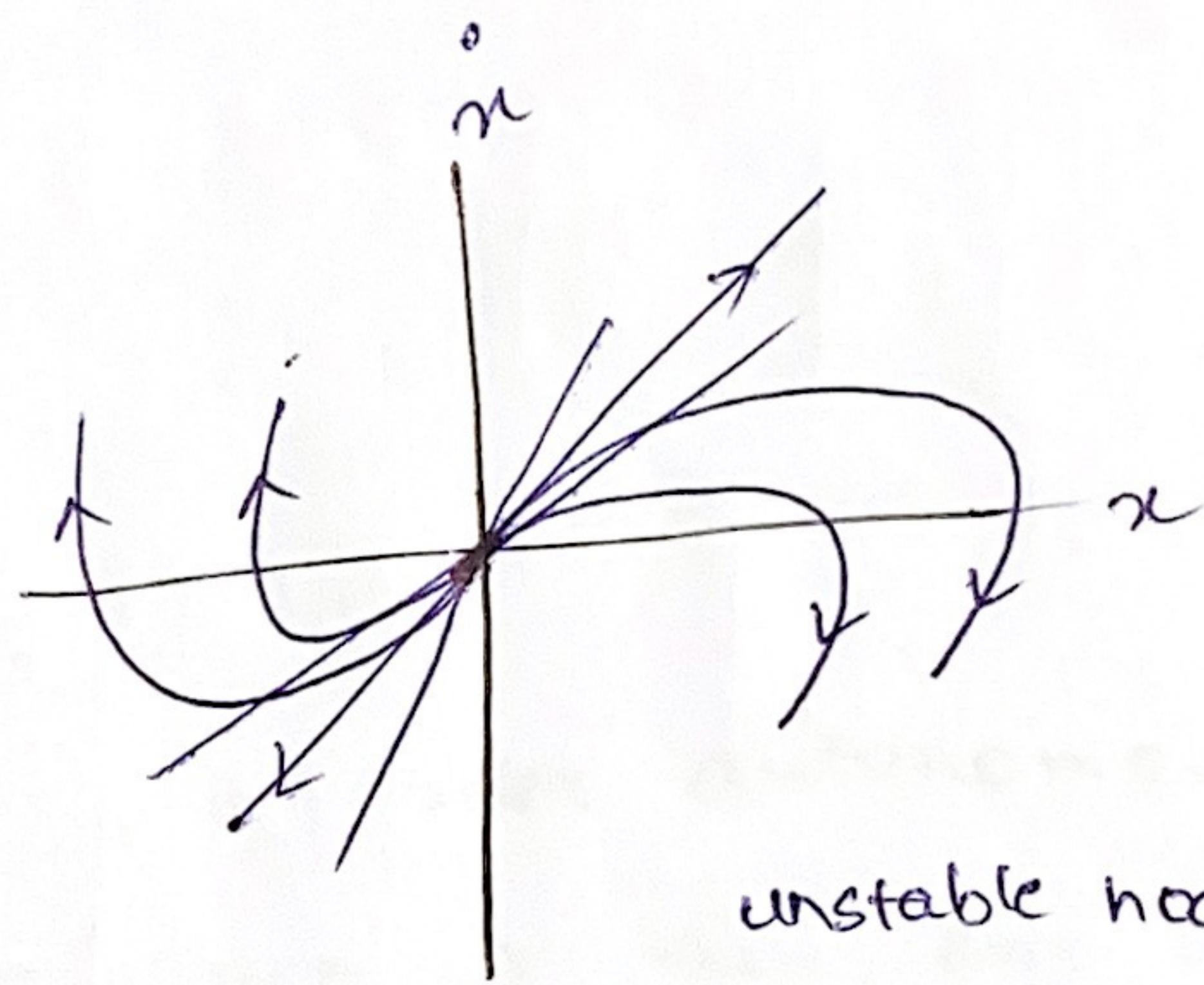
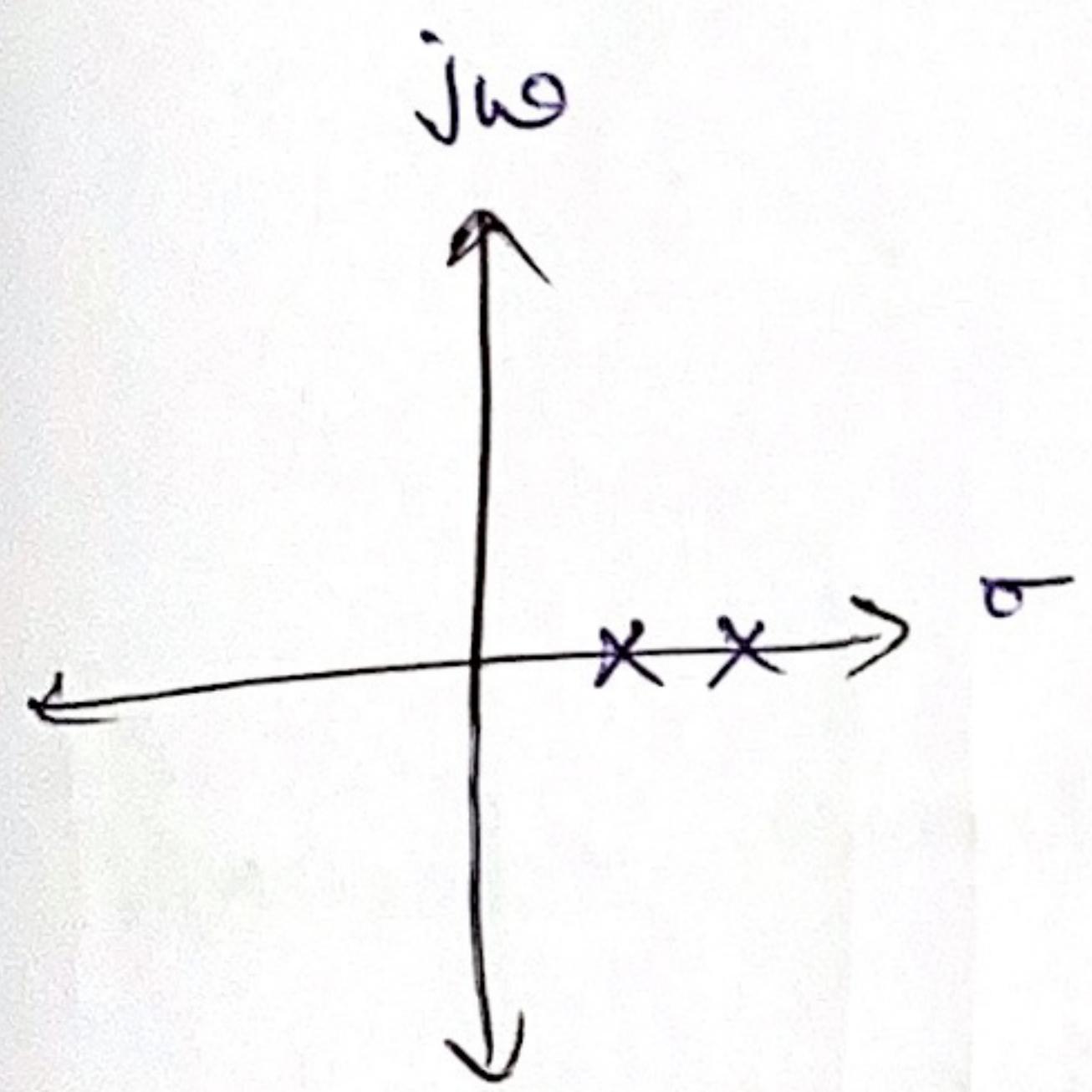
$$s^2 + as + b = (s - \lambda_1)(s - \lambda_2) = 0$$

$$\Rightarrow \lambda_1 = \frac{-a + \sqrt{a^2 - 4b}}{2}, \quad \lambda_2 = \frac{-a - \sqrt{a^2 - 4b}}{2}$$

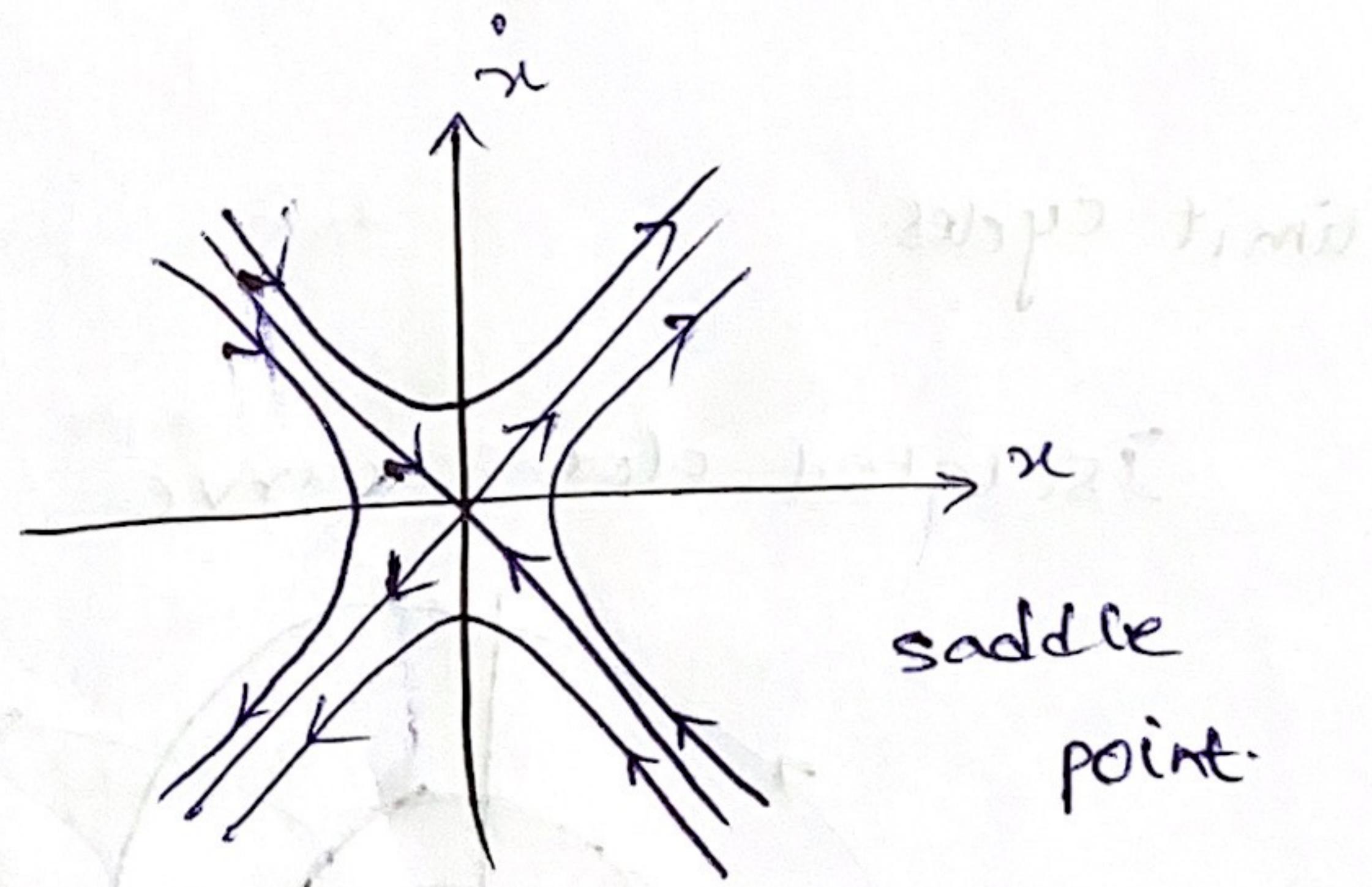
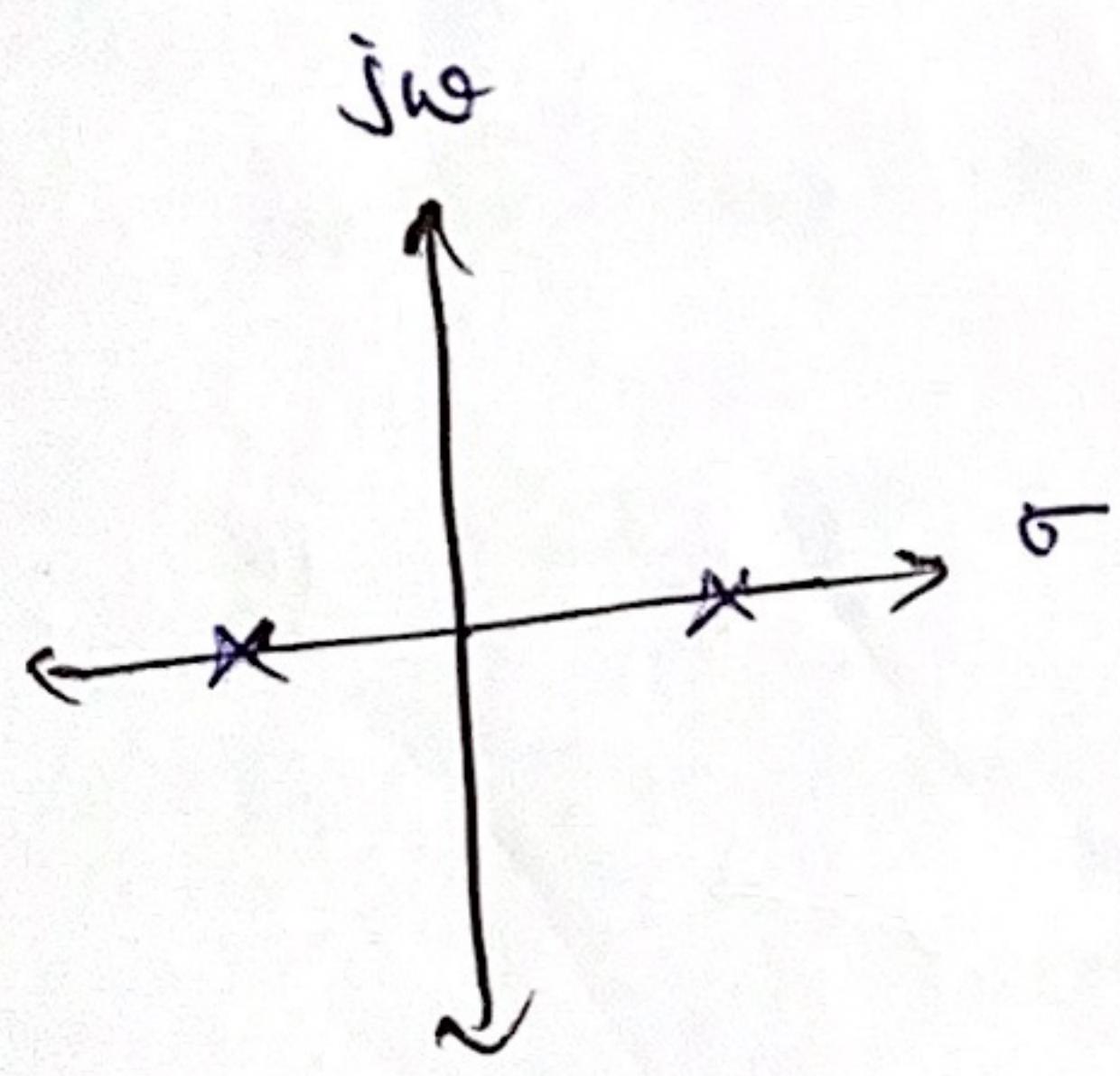
## Phase portraits of linear systems



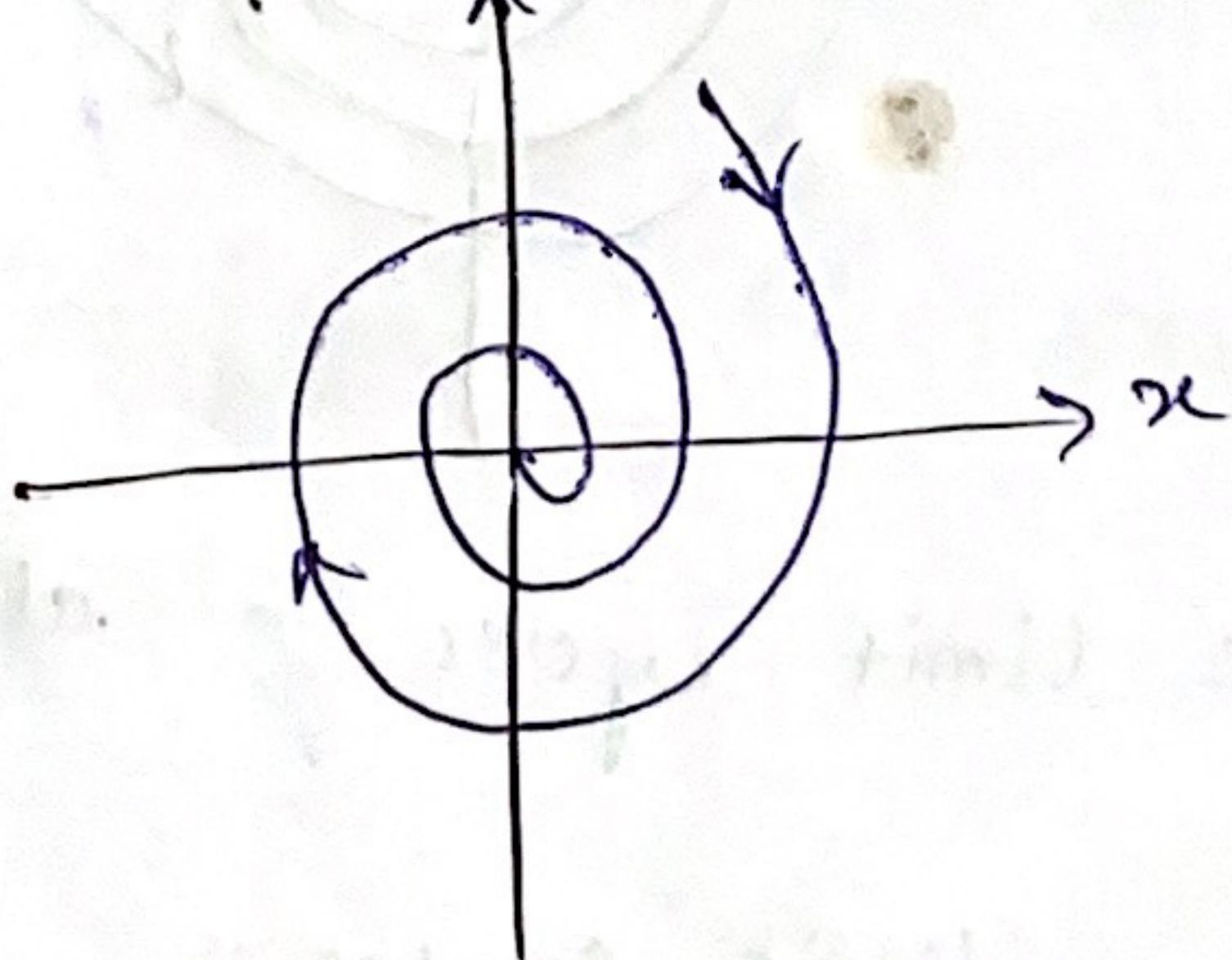
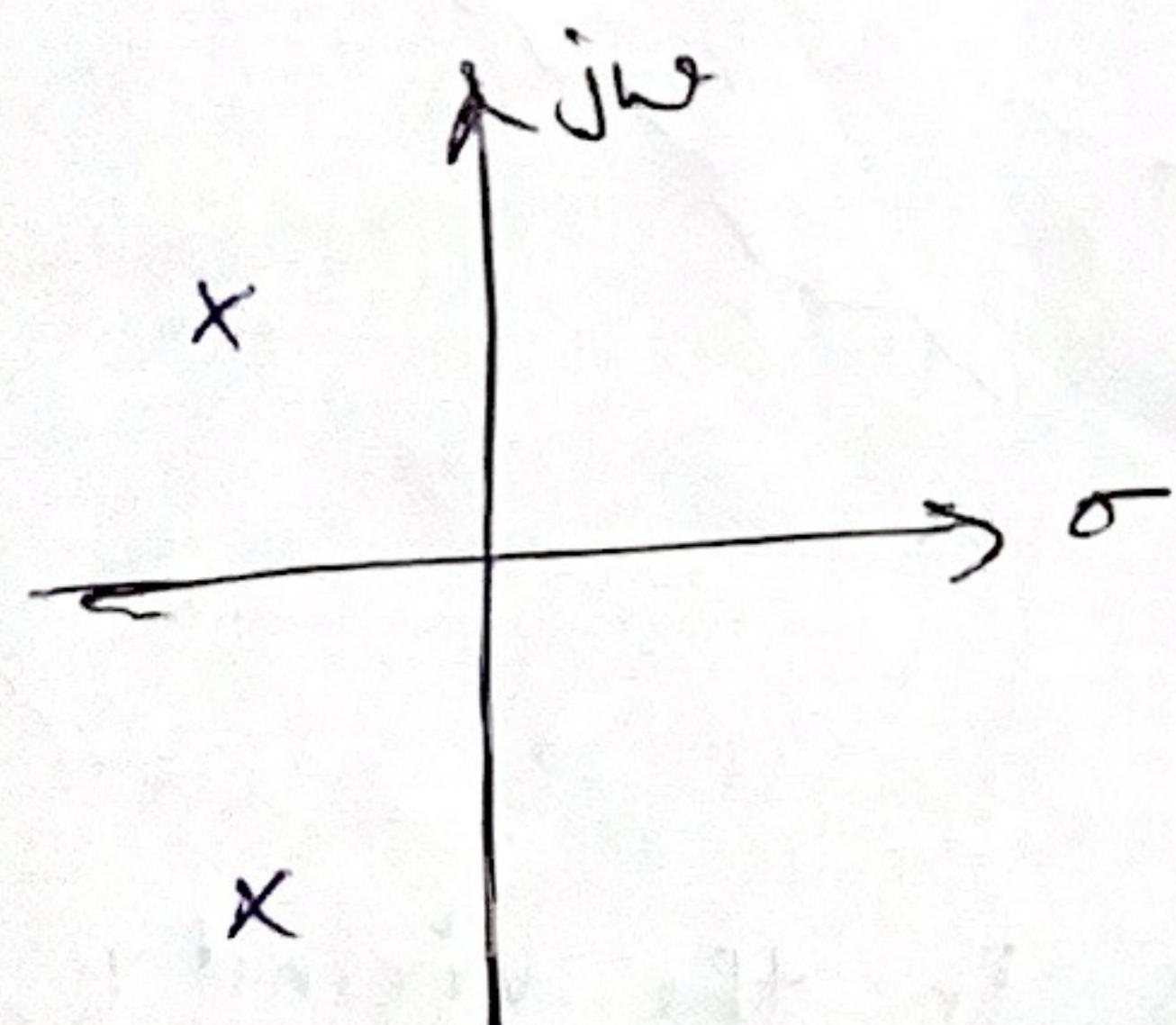
stable node.



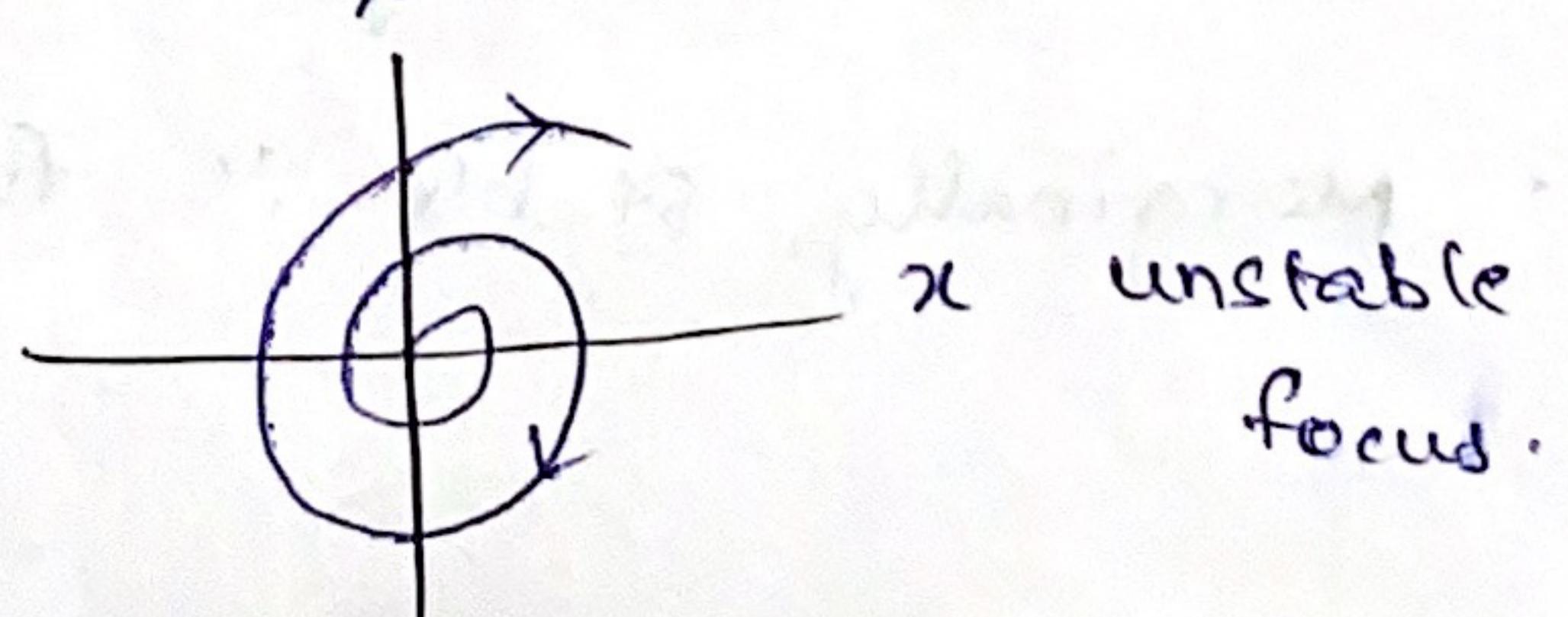
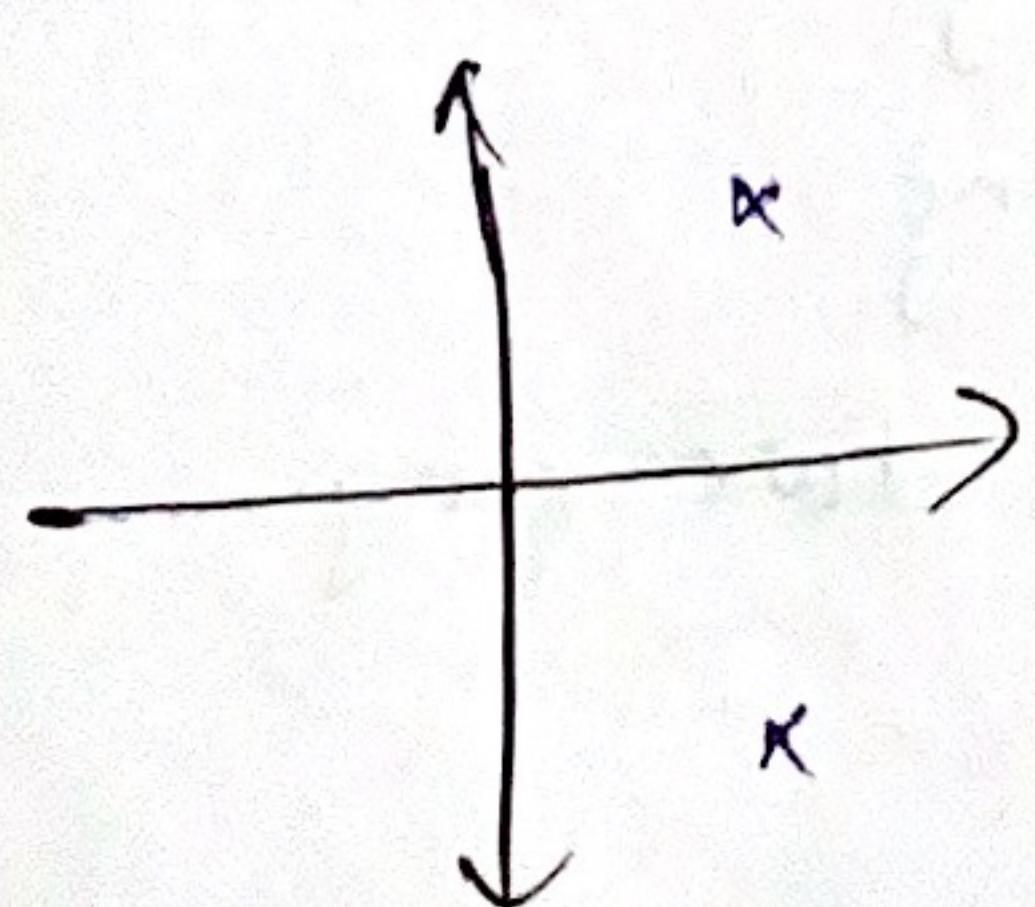
unstable node.



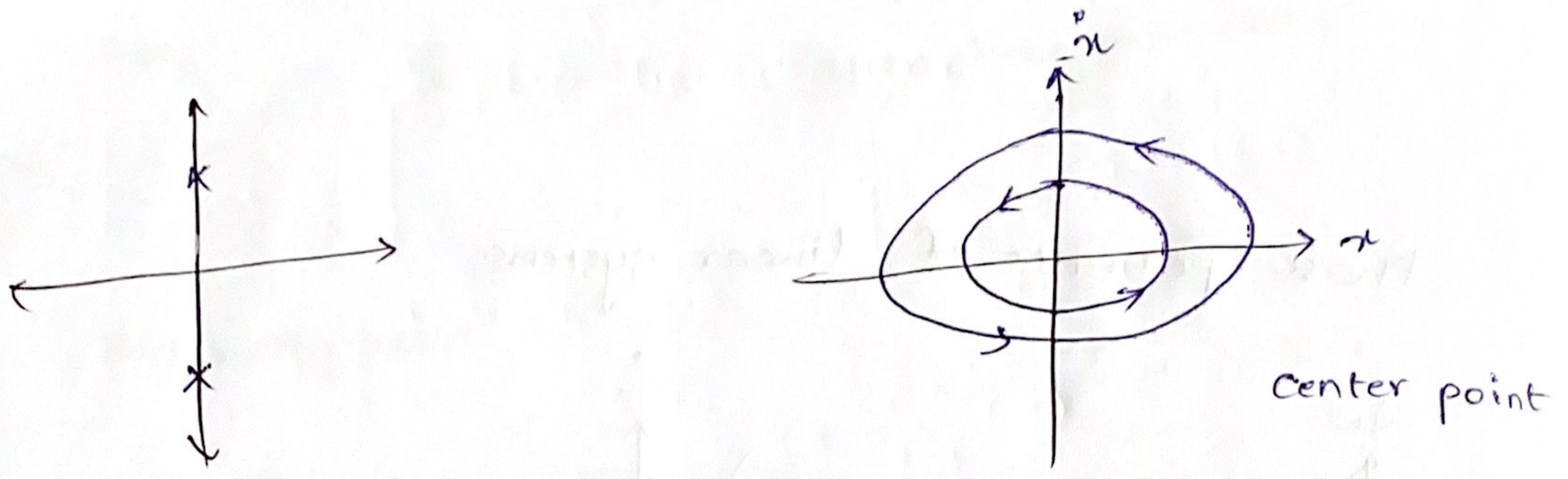
saddle point.



stable focus.

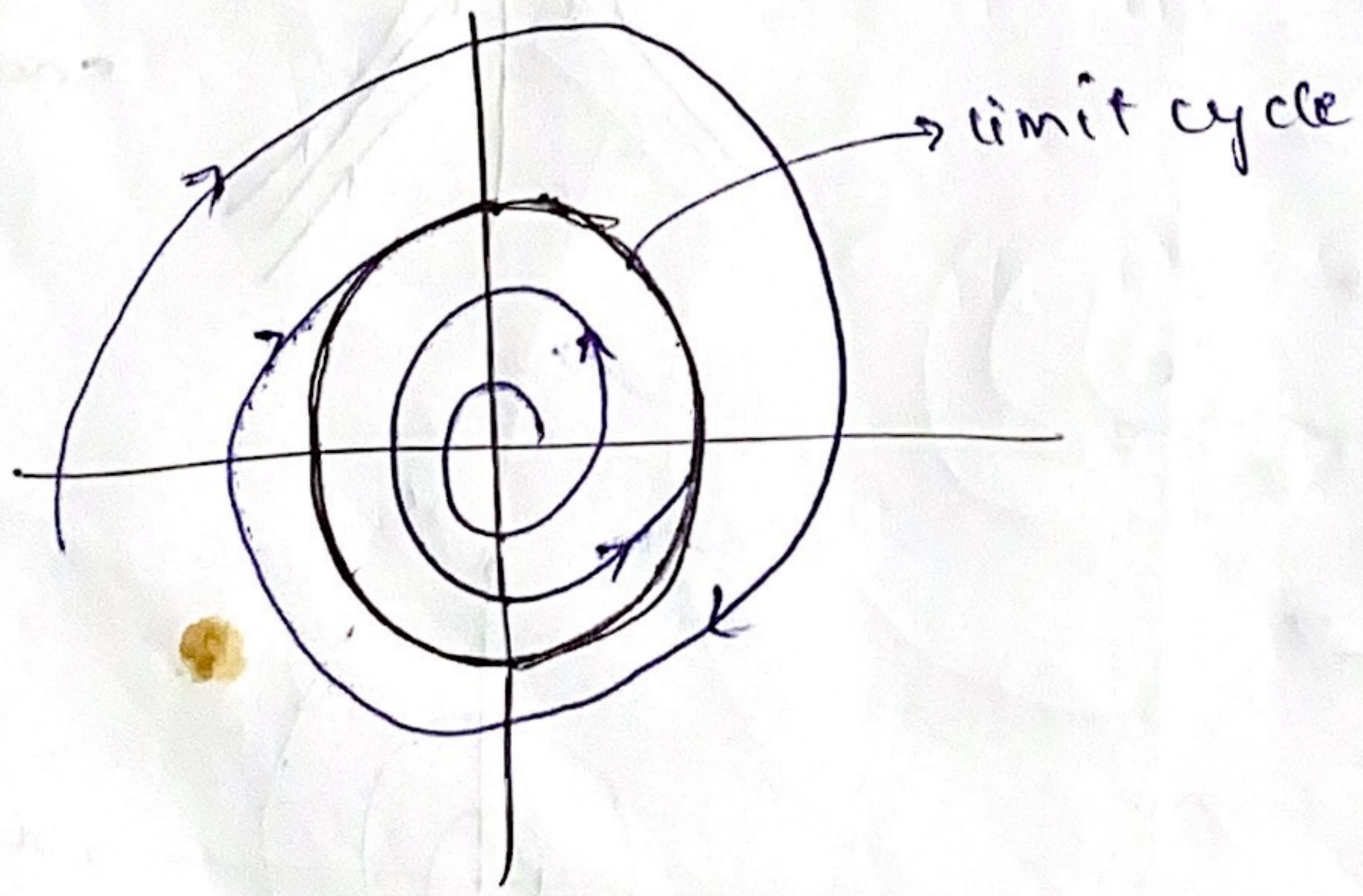


unstable focus.



limit cycles.

Isolated closed curve



Stable limit cycles : all trajectories in the vicinity  
are converging

Unstable limit cycles : all are diverging

M marginally stable : few converging & diverging.

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## Existence of limit cycles

$N$  - no. of nodes, centers, foci enclosed in a limit cycle.

$S$  - no. of enclosed saddle points.

Poincaré: If limit cycle exists in the 2nd order,

$$\text{then } N = S + 1$$

### Poincaré-Bendixson

If a trajectory of 2nd order autonomous system remains in a finite region  $\Omega$ , then one of the following is true

- a) It goes to an eq. point.
- b) It tends to an asymptotically stable limit cycle.
- c) The trajectory is itself a limit cycle.

### Bendixson

For a nonlinear system, no limit cycle can exist in a region  $\Omega$  in which  $\frac{\partial f_1}{\partial x_1} + \frac{\partial f_2}{\partial x_2}$  doesn't vanish and doesn't change sign.

## Jacobian linearization:

Consider an autonomous system  $\dot{x} = f(x)$  where  $f(x)$  is continuously differentiable and  $f(0) = 0$ . Then,

$$\dot{x} = \left( \frac{\partial f}{\partial x} \right)_{x=0} x + f_{h.o.t}(x)$$

$f_{h.o.t}$  = higher order terms.

$$\text{let } A = \left( \frac{\partial f}{\partial x} \right)_{x=0}$$

Now, the system is  $\dot{x} = Ax$

$$\begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} \end{bmatrix} \Big|_{x=0} = \frac{\partial f}{\partial x} \Big|_{x=0}$$

↑  
Jacobian matrix

for a non-autonomous nonlinear system with control input  $u$ .  $\dot{x} = f(x, u)$

such that  $f(0, 0) = 0$

$$\dot{x} = \frac{\partial f}{\partial x} x + \frac{\partial f}{\partial u} \cdot u + f_{h.o.t}(x, u)$$

$$\text{let } A = \left( \frac{\partial f}{\partial x} \right)_{(x=0, u=0)} \quad B = \left( \frac{\partial f}{\partial u} \right)_{(u=0, x=0)}$$

then,  $\dot{x} = Ax + Bu$

## Tutorial - 6

1. For the nonlinear system given below, find the eq. points and determine the type of each isolated eq. point.

$$\dot{x}_1 = -x_1 + 2x_1^3 + x_2$$

$$\dot{x}_2 = -x_1 - x_2$$

$$-x_1 - x_2 = 0$$

$$\Rightarrow x_2 = -x_1$$

$$-x_1 + 2x_1^3 + x_2 = 0$$

$$\Rightarrow -x_1 + 2x_1^3 - x_1 = 0$$

$$\Rightarrow x_1^3 - x_1 = 0$$

$$\Rightarrow x_1 = 1, -1, 0$$

Sol. for finding eq. points

$$x_1 = 0$$

$$x_2 = 0$$

~~$$-x_1 + 2x_1^3 + x_2 \neq -x_1 - x_2$$~~

~~$$x_2 = -x_1$$~~

~~$$2x_1^3 + 2x_2 = 0$$~~

~~$$x_1^3 + x_2 = 0$$~~

~~$$x_1^3 - x_1 = 0$$~~

$$x_1 = 1, -1, 0$$

$$x_2 = 1, -1, 0$$

~~$$x_1 = 2x_1^3 + x_2$$~~

~~$$x_2 = -x_1 = -2x_1^3 - x_2$$~~

~~$$2x_2 =$$~~

eq. points are  $(0, 0)$   $(1, -1)$   $(-1, 1)$

Linearize around the eq. points.

$$\dot{x} = Ax$$

where  $A = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} \end{bmatrix}$

$$= \frac{\partial}{\partial x_1} (-x_1 + 2x_1^3 + x_2)$$

$$-1 + 6x_1^2 \quad 1$$

$$(0,0) \quad (1,-1) \quad (-1,1)$$

$$\begin{bmatrix} -1 & 1 \\ -1 & -1 \end{bmatrix} \quad \begin{bmatrix} 5 & 1 \\ -1 & -1 \end{bmatrix} \quad \begin{bmatrix} 5 & 1 \\ -1 & -1 \end{bmatrix}$$

$$-1 \quad -1$$

$$(0,0)$$

(0,0)

$$\begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix} - \begin{bmatrix} -1 & 1 \\ -1 & -1 \end{bmatrix}$$

$$\begin{vmatrix} \lambda+1 & -1 \\ 1 & \lambda+1 \end{vmatrix} = (\lambda+1)^2 + 1$$

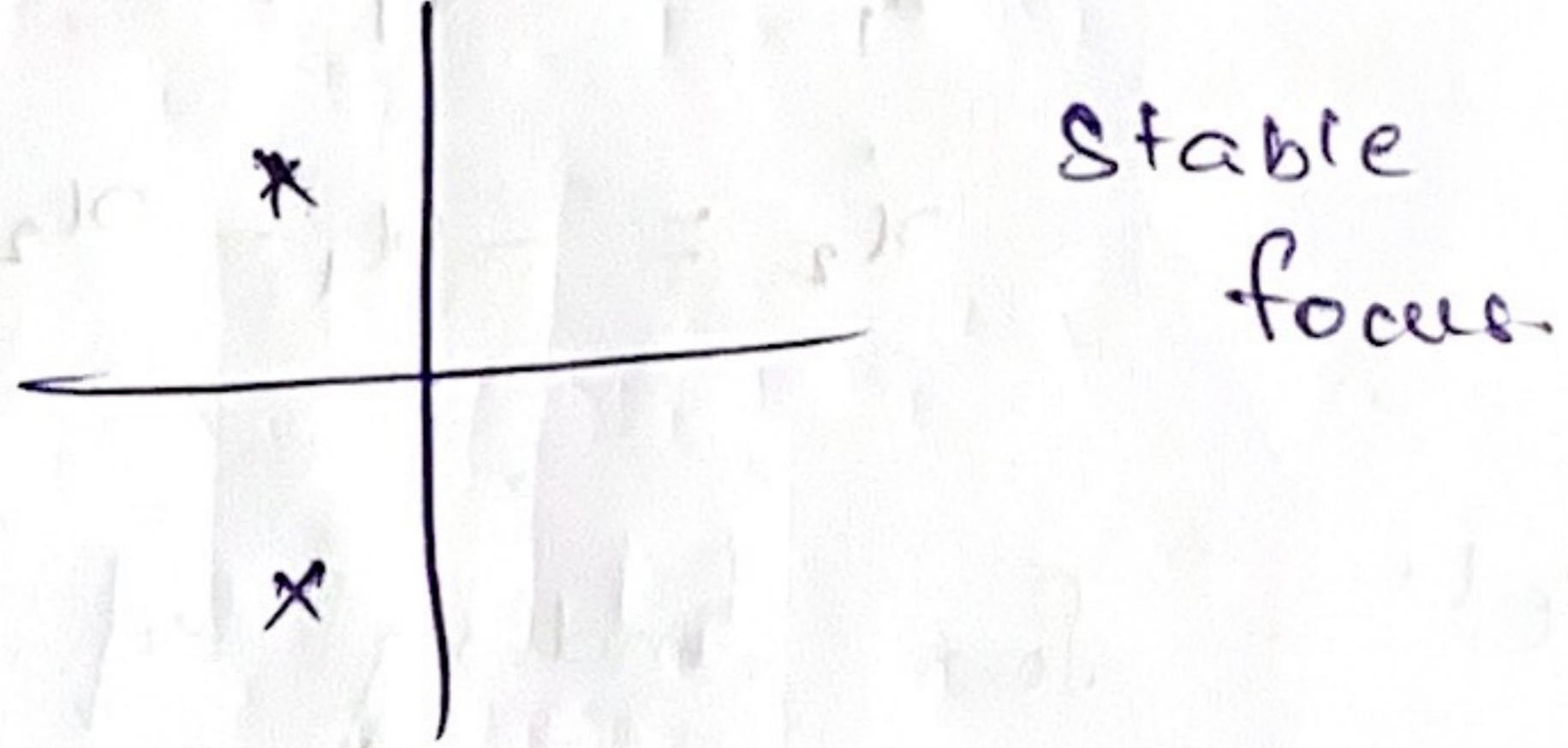
$$\lambda^2 + 1 + 2\lambda + 1$$

$$\lambda^2 + 2\lambda + 2$$

$$\lambda = -1 + j$$

$$-1 - j$$

(1, -1)



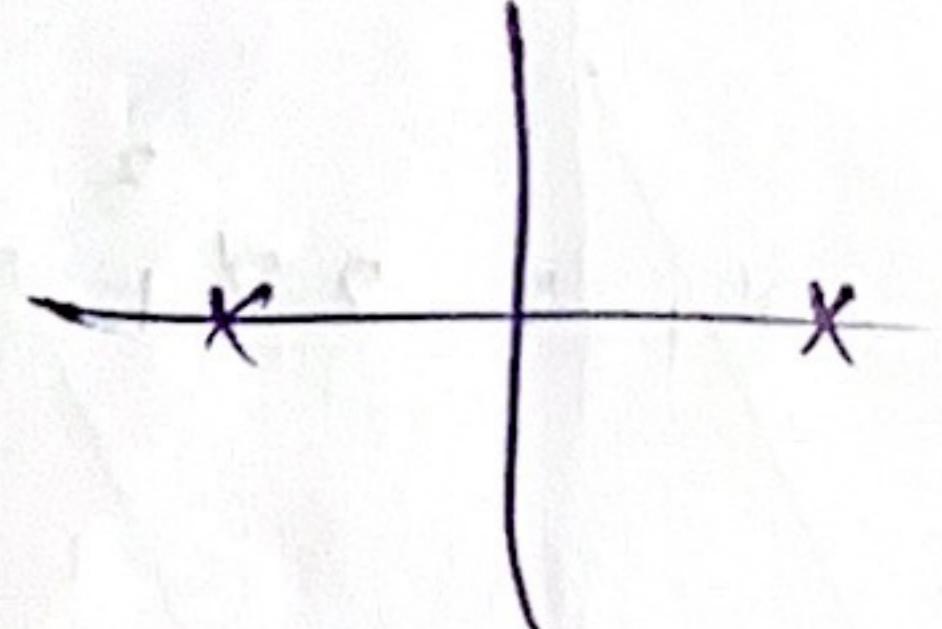
$$\begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix} - \begin{bmatrix} 5 & 1 \\ -1 & -1 \end{bmatrix}$$

$$\begin{vmatrix} \lambda-5 & -1 \\ 1 & \lambda+1 \end{vmatrix} = (\lambda-5)(\lambda+1) + 1$$

$$\lambda^2 - 5\lambda + \lambda - 5 + 1$$

$$\lambda^2 - 4\lambda - 4 = 0$$

$$\Rightarrow \lambda = 2+2\sqrt{2}, 2-2\sqrt{2}$$



(1, 1) It is a saddle point.

$$\textcircled{1}. \quad \dot{x}_1 = x_1 + x_1 x_2$$

$$\dot{x}_2 = -x_2 + x_2^2 + x_1 x_2 - x_1^3$$

SOL.

$$\dot{x}_1 = 0$$

$$\dot{x}_2 = 0$$

$$\cancel{x_1(1+x_2)} = 0 \quad \cancel{x_1} = \cancel{-x_1 x_2}$$

$$x_2 = -1$$

$$-x_2 + x_2^2 + x_1 x_2 - x_1^3 = 0$$

$$-x_2 + x_2^2 + x_1 x_2 - x_1^3 = 0$$

eq. points, are

(0,0) (0,1) (1,-1)

$$1+1-x_1-x_1^3=0$$

$$x_1^3+x_1-2=0$$