

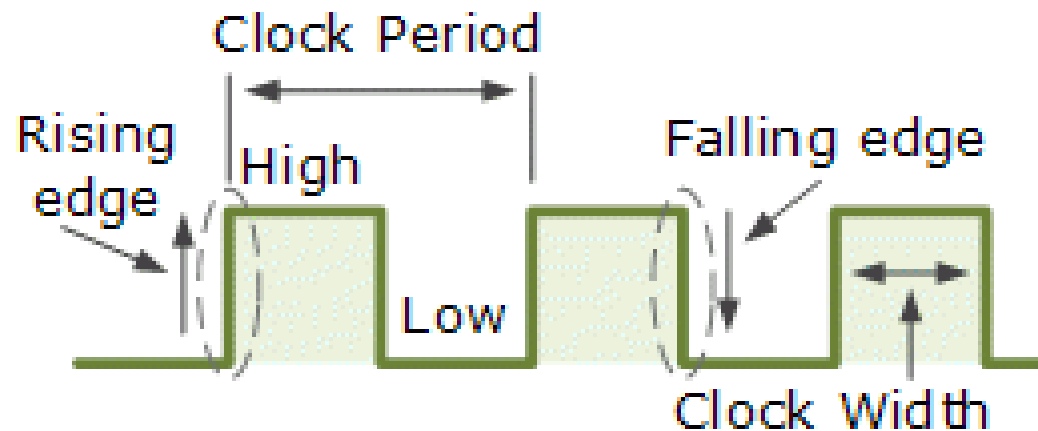
LIC: LECTURE

Signal Generators

- **Multivibrator: Need and Different Types**
 - **Astable Multivibrator**
 - **Monostable Multivibrator**
 - **Bistable Multivibrator**
- **Astable Multivibrator**
 - **Working Principal**
 - **Calculation of Time Period**
 - **Design Example**

Multivibrator

- The Multivibrator is the electronic circuit which is used to implement two state devices like oscillator, timer and flip-flops.
- Here, the two states refer to the two voltage levels of the Multivibrators.
- Depending upon the number of stages, the multivibrator can be divided into three types.



Multivibrator

Astable – A *free-running multivibrator* that has NO stable states but switches continuously between two states this action produces a train of square wave pulses at a fixed frequency. (Eg. Relaxation Oscillator)



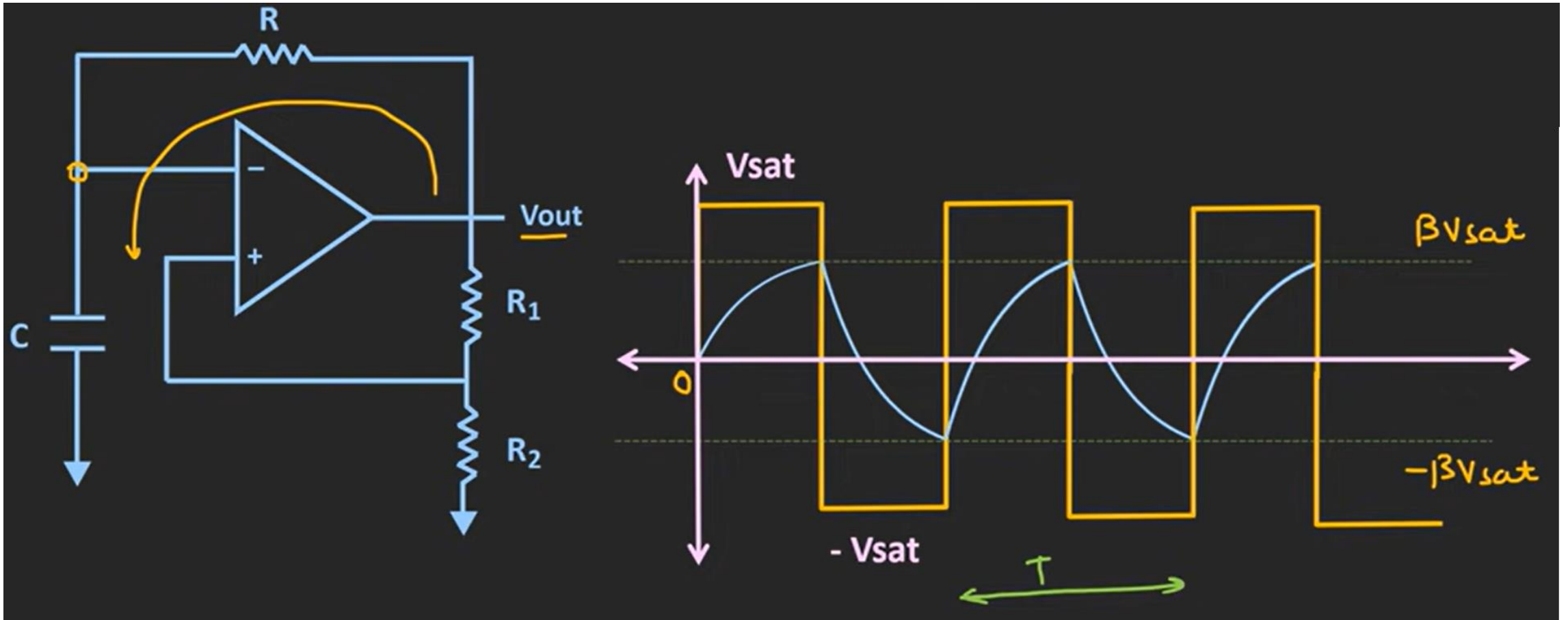
Monostable – A *one-shot multivibrator* that has only ONE stable state and is triggered externally with it returning back to its first stable state. (Eg. Timer applications)

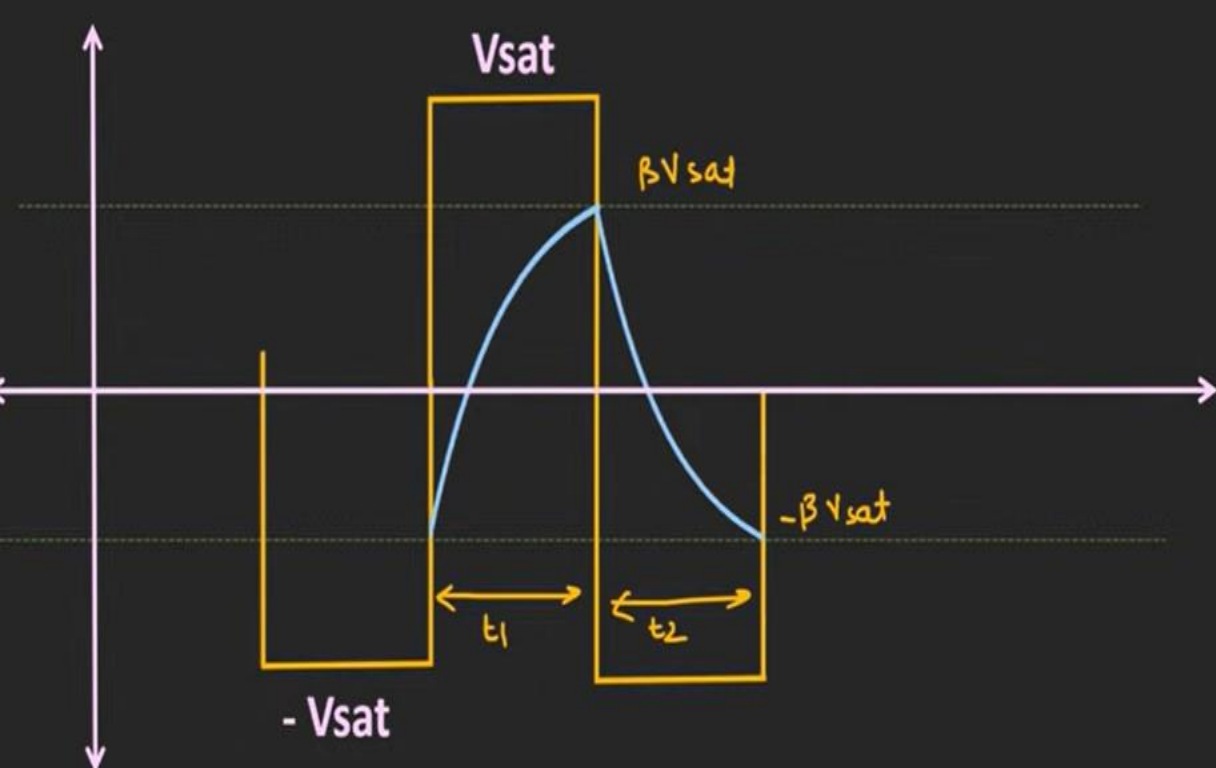


Bistable – A *flip-flop* that has TWO stable states that produces a single pulse either positive or negative in value. (Eg.-Sequential Circuits)



ASTABLE MULTIVIBRATOR (Free Running Multivibrator)





ASTABLE MULTIVIBRATOR

Derivation of Time Period
($T=t_1+t_2$)

Calculation of charging time- t_1

$$V_c(t) = V_{Final} + [V_{initial} - V_{Final}]e^{-t/RC}$$

$$V_{Final} = V_{sat}$$

$$V_{in} = -\beta V_{sat}$$

$$V_c(t_1) = V_{sat} + [-\beta V_{sat} - V_{sat}]e^{-t_1/RC}$$

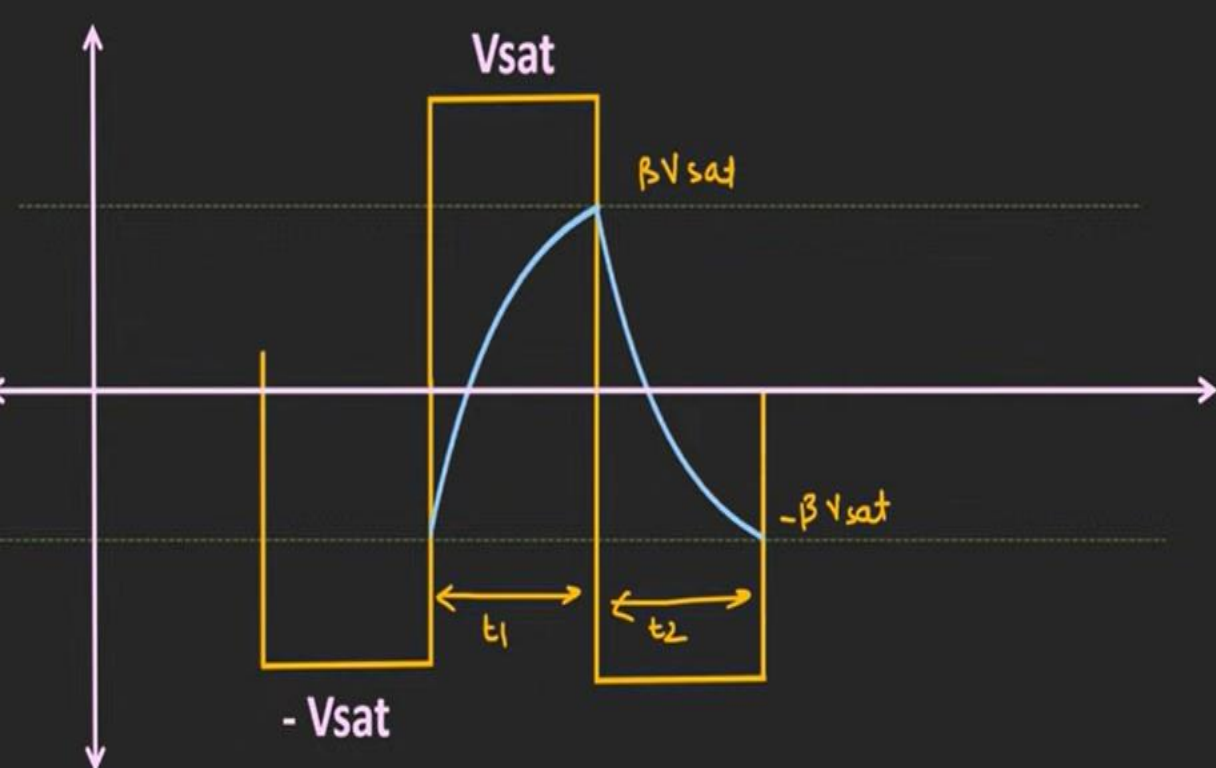
$$\beta V_{sat} = V_{sat} - [1 + \beta]V_{sat}e^{-t_1/RC}$$

$$\beta - 1 = -[1 + \beta]e^{-t_1/RC}$$

$$\left[\frac{1 - \beta}{1 + \beta} \right] = e^{-t_1/RC}$$

$$\Rightarrow t_1 = -RC \ln \left[\frac{1 - \beta}{1 + \beta} \right]$$

$$t_1 = RC \ln \left[\frac{1 + \beta}{1 - \beta} \right]$$



ASTABLE MULTIVIBRATOR

Derivation of Time Period
($T=t_1+t_2$)

Calculation of discharging time- t_2

$$V_c(t) = V_{Final} + [V_{initial} - V_{Final}]e^{-t/RC}$$

$$V_{initial} = \beta V_{sat} \rightarrow -\beta V_{sat}$$

$$V_{Final} = -V_{sat}$$

$$V_c(t_2) = -V_{sat} + [\beta V_{sat} - (-V_{sat})]e^{-t_2/RC}$$

$$-\beta V_{sat} = -V_{sat} + V_{sat} \times (1+\beta) \times e^{-t_2/RC}$$

$$\frac{1-\beta}{1+\beta} = e^{-t_2/RC}$$

$$\Rightarrow t_2 = RC \times \ln \left(\frac{1+\beta}{1-\beta} \right)$$

$$T = t_1 + t_2 = 2t_1 = 2RC \ln \left(\frac{1+\beta}{1-\beta} \right)$$

Design Problem-1

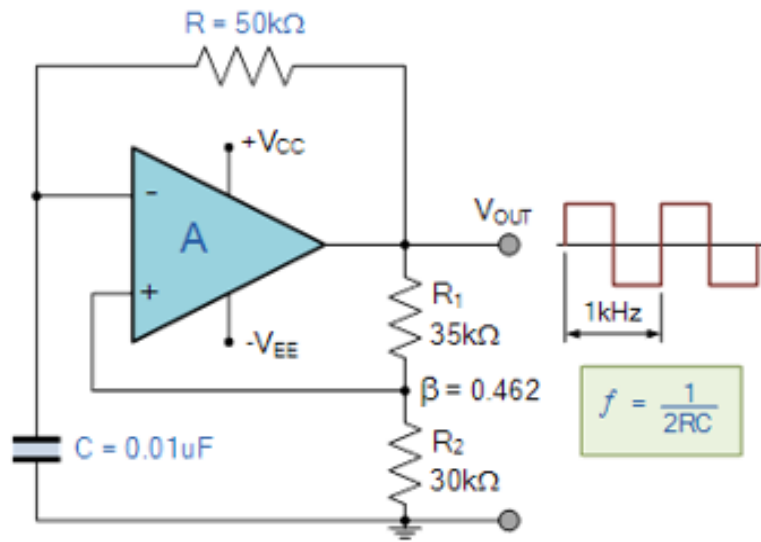
An op-amp multivibrator circuit is constructed using the following components.

$R_1 = 35 \text{ k}\Omega$, $R_2 = 30 \text{ k}\Omega$, $R = 50 \text{ k}\Omega$ and $C = 0.01 \text{ }\mu\text{F}$ and powered with $V_{CC} = 11\text{V}$, $V_{EE} = -11\text{V}$ DC supply.

Calculate the circuits frequency of oscillation.

Design Problem-1

An op-amp multivibrator circuit is constructed using the following components. $R_1 = 35\text{k}\Omega$, $R_2 = 30\text{k}\Omega$, $R = 50\text{k}\Omega$ and $C = 0.01\mu\text{F}$ and powered with $V_{CC}=11\text{V}$, $V_{EE}=-11\text{V}$ DC supply. Calculate the circuits frequency of oscillation.



$$\beta = \frac{R_2}{R_1 + R_2} = \frac{30\text{k}\Omega}{35\text{k}\Omega + 30\text{k}\Omega} = 0.462$$

$$T = 2RC \ln\left(\frac{1+\beta}{1-\beta}\right) = 2RC \ln\left(\frac{1+0.462}{1-0.462}\right)$$

$$T = 2 \times (50\text{k}\Omega \times 0.01\mu\text{F}) \times \ln(2.717)$$
$$\therefore T = 0.001 \times 1 = 0.001\text{Sec or } 1\text{ms}$$

$$\therefore f = \frac{1}{T} = \frac{1}{0.001} = 1,000\text{Hz or } 1\text{kHz}$$

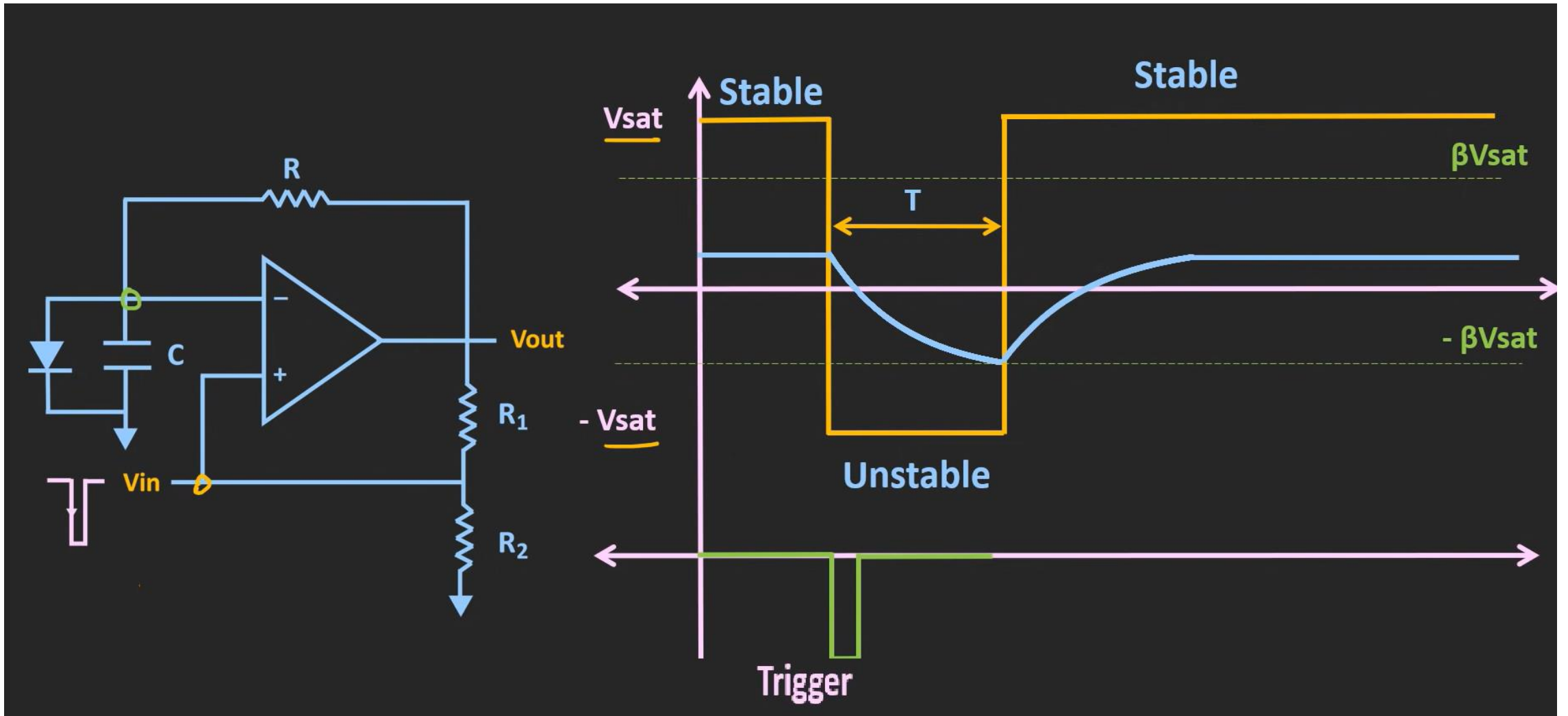
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Signal Generators

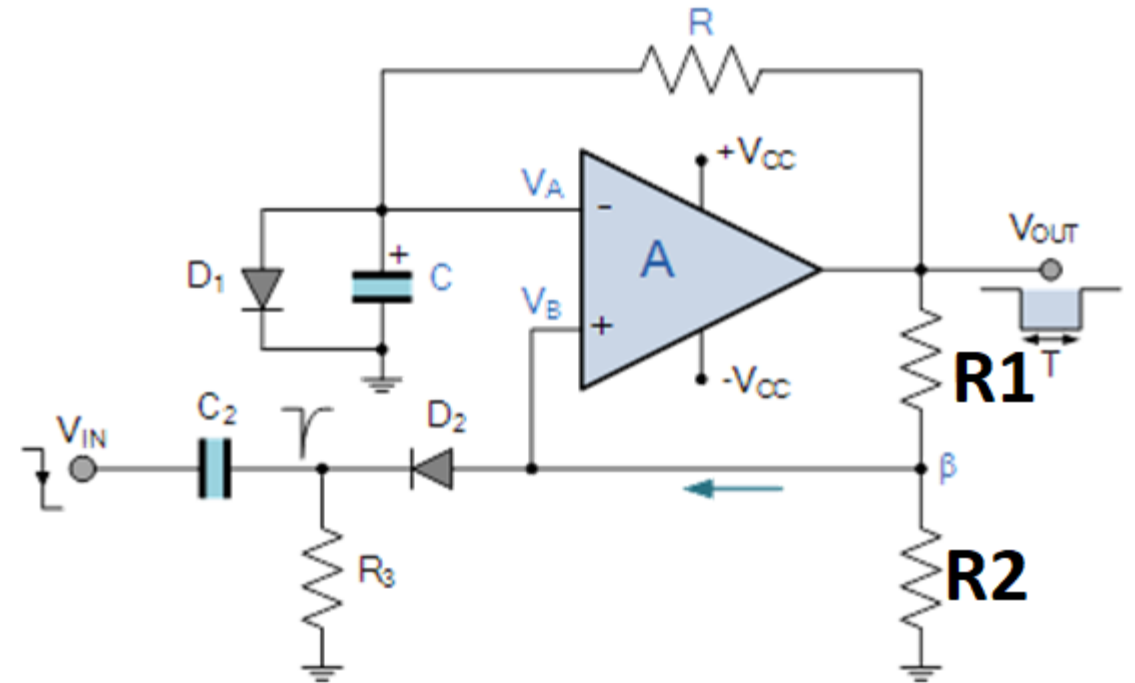
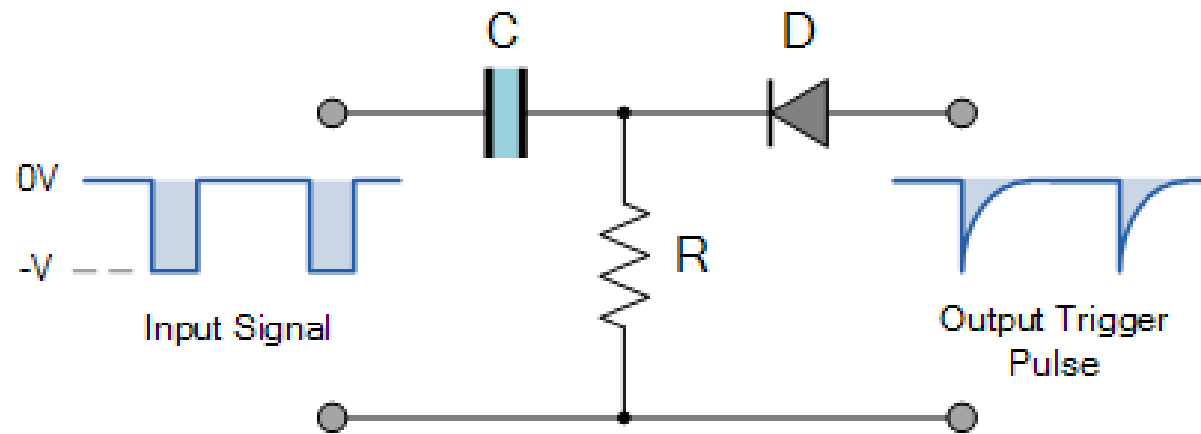
- ✓ **Astable Multivibrator**
 - ✓ **Working Principal**
 - ✓ **Calculation of Time Period**
 - ✓ **Design Example**
- **Monostable Multivibrator**
 - **Working Principal**
 - **Calculation of Time Period and Recovery Time**
 - **Design Example**

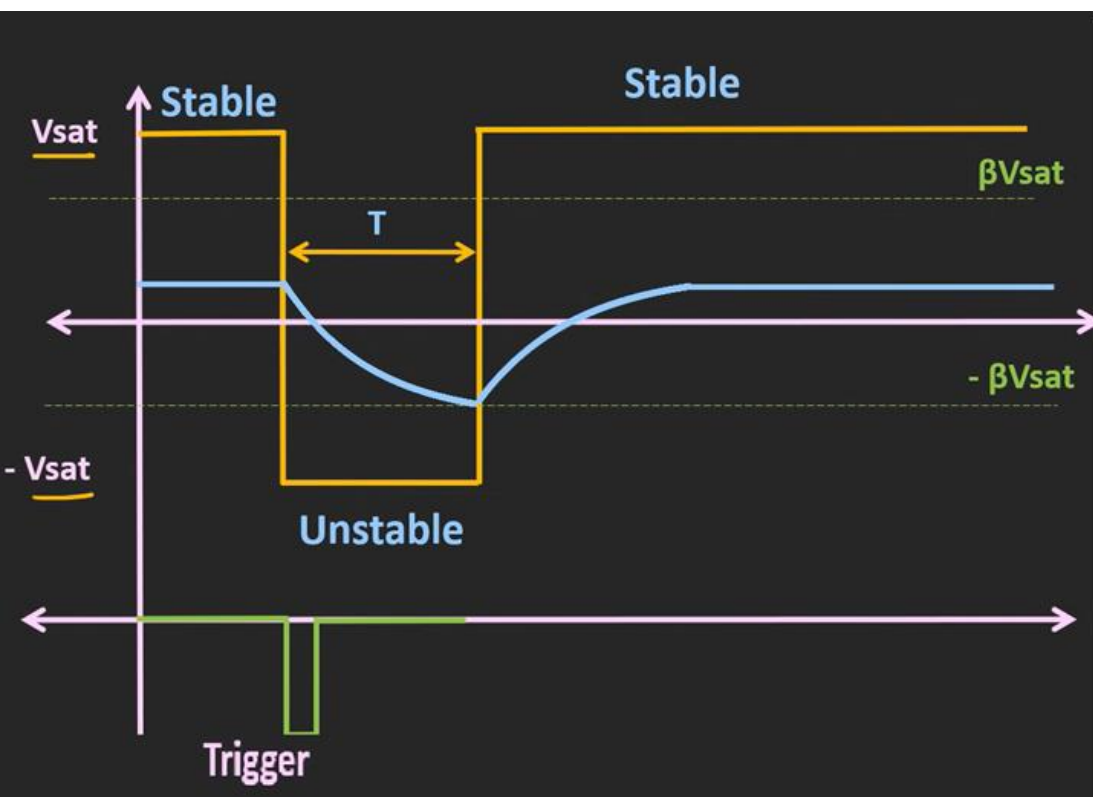
MONOSTABLE MULTIVIBRATOR

(1 STABLE & 1 QUASI-STABLE STATE-One Shot Multivibrator)



RC Differentiator Circuit





MONOSTABLE MULTIVIBRATOR

Derivation of Time Period (T) for
unstable state (Pulse Width)

$$V_C(t) = V_{FINAL} + (V_{INITIAL} - V_{FINAL})e^{-t/RC}$$

$$\left. \begin{aligned} V_{FINAL} &= -V_{SAT} \\ V_{INITIAL} &= V_D \\ V_C(t) &= -\beta V_{SAT} \end{aligned} \right\}$$

$$-\beta V_{SAT} = -V_{SAT} + (V_D - (-V_{SAT}))e^{-t/RC}$$

$$-\beta V_{SAT} = -V_{SAT} + (V_D + V_{SAT})e^{-t/RC}$$

$$V_{SAT} - \beta V_{SAT} = (V_D + V_{SAT})e^{-t/RC}$$

$$e^{-t/RC} = \frac{V_{SAT} [1 - \beta]}{V_{SAT} - \beta V_{SAT}}$$

$$e^{-t/RC} = \frac{V_{SAT} [1 - \beta]}{V_D + V_{SAT}} = \frac{V_{SAT}}{V_{SAT}} \left[\frac{1 - \beta}{1 + V_D/V_{SAT}} \right]$$

$$e^{-t/RC} = \frac{1 - \beta}{1 + \frac{V_D}{V_{SAT}}} \quad \text{taking natural log}$$

$$-\frac{t}{RC} = \ln \left[\frac{1 - \beta}{1 + V_D/V_{SAT}} \right]$$

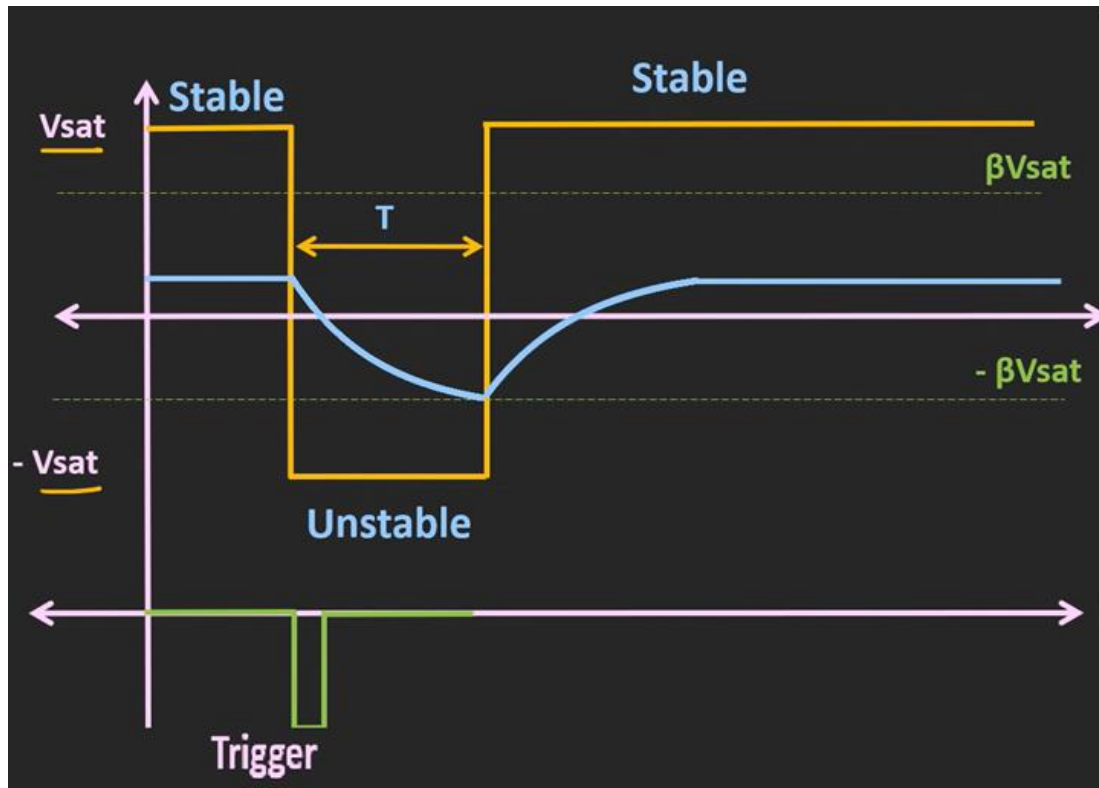
$$t = RC \ln \left[\frac{1 + V_D/V_{SAT}}{1 - \beta} \right] \quad *$$

$$t = RC \ln \left[\frac{1 + 0}{1 - R_2/R_1 + R_2} \right]$$

DISCHARGING time
 $V_D \ll | -V_{SAT} |$

If $V_D = 0$ & $\beta = R_2/R_1 + R_2$

$$t = RC \ln (1 + R_2/R_1) \quad *$$



MONOSTABLE MULTIVIBRATOR

Derivation of Charging
Time/Capacitor Recovery Time -
Stable State

$$V_C(t) = V_{final} + (V_{initial} - V_{final})e^{-t/RC}$$

$$V_{FINAL} = V_{SAT}$$

$$V_{initial} = -\beta V_{SAT}$$

$$V_C(t) = V_D$$

$$V_D = V_{SAT} + (-\beta V_{SAT} - V_{SAT})e^{-t/RC}$$

$$V_D - V_{SAT} = -V_{SAT}(1 + \beta)e^{-t/RC}$$

$$e^{-t/RC} = \frac{-(V_D - V_{SAT})}{V_{SAT}(1 + \beta)}$$

taking natural log

$$-\frac{t}{RC} = \ln \frac{V_{SAT} - V_D}{V_{SAT}(1 + \beta)}$$

$$t = -RC \ln \frac{1 - V_D/V_{SAT}}{1 + \beta}$$

$$t = RC \ln \frac{1 + \beta}{1 - (V_D/V_{SAT})}$$

An op-amp monostable circuit is constructed using the following components. $R_1 = 30\text{k}\Omega$, $R_2 = 30\text{k}\Omega$, $R = 150\text{k}\Omega$ and $C = 1.0\mu\text{F}$. If the op-amp monostable is supplied from a $\pm 12\text{V}$ supply and the timing period is initiated with a 10ms pulse.

Calculate the circuits timing period, capacitor recovery time, total time between trigger pulses and the differentiator network values. Draw the completed circuit.

Data given: $R_1 = R_2 = 30\text{k}\Omega$, $R = 150\text{k}\Omega$, $C = 1.0\mu\text{F}$ and pulse width equals ten milliseconds, (10ms).

$$\beta = \frac{R_1}{R_1 + R_2} = \frac{30\text{k}\Omega}{30\text{k}\Omega + 30\text{k}\Omega} = 0.5$$

$$T = RC \cdot \ln\left(1 + \frac{R_1}{R_2}\right)$$

$$= RC \times \ln\left(1 + \frac{30\text{k}\Omega}{30\text{k}\Omega}\right)$$

$$= 150\text{k}\Omega \times 1.0\mu\text{F} \times 0.693$$

$$T = 0.104\text{secs or } \underline{104\text{ms}}$$

$$T_{(\text{charging})} = RC \times \ln\left(\frac{1 + \beta}{1 - \frac{V_D}{V_{CC}}}\right)$$

$$T_{(\text{charging})} = RC \times \ln\left(\frac{1 + 0.5}{1 - \frac{0.7}{12}}\right)$$

$$\therefore T_{(\text{ch.})} = 150\text{k}\Omega \times 1.0\mu\text{F} \times 0.465 = \underline{70\text{ms}}$$

$$T_{(\text{total})} = T_{(\text{delay})} + T_{(\text{charging})}$$

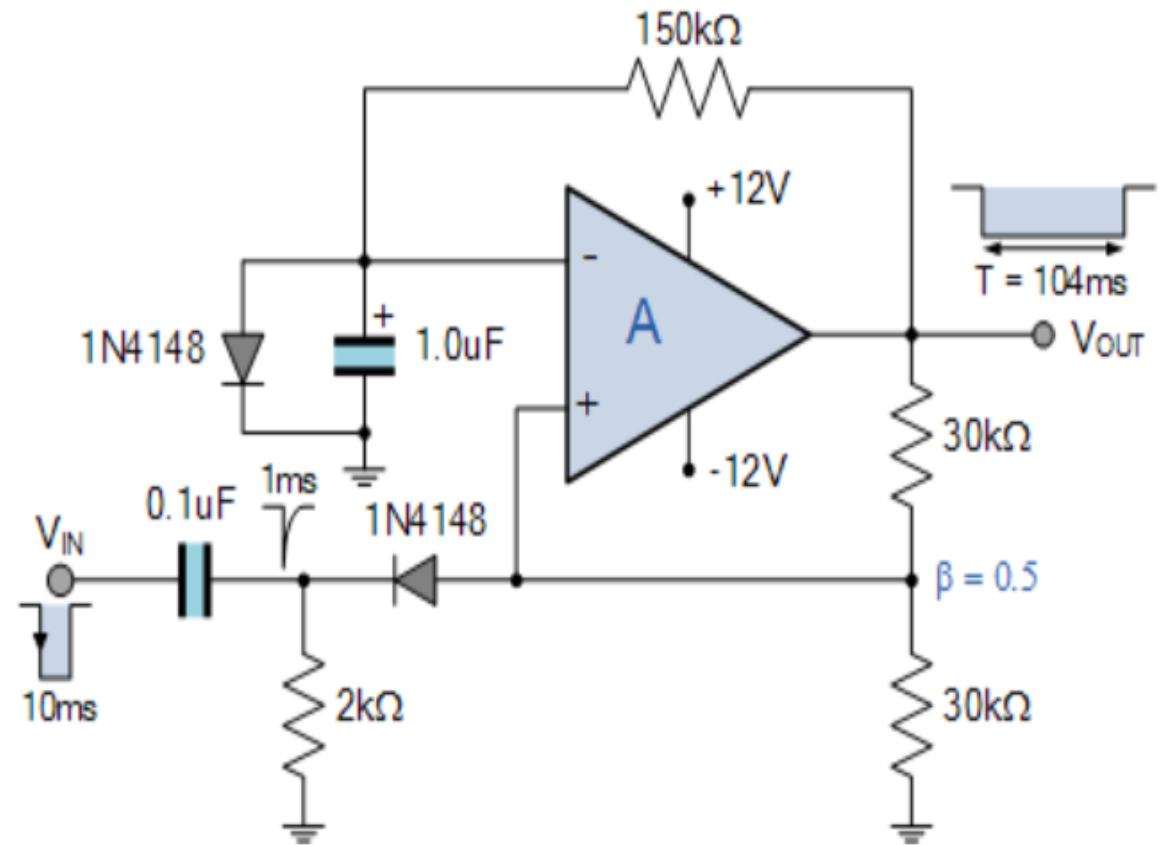
$$\therefore T_{(\text{total})} = 104\text{ms} + 70\text{ms} = 174\text{ms}$$

The input pulse is given as 10ms, therefore the negative spike duration will be 1ms (10%). If we assume a capacitance value of 0.1uF, then the differentiator RC values calculated as :

$$\text{Pulse width} = 1\text{ms} = 5RC$$

$$\text{If } C = 0.1\mu\text{F}$$

$$R = \frac{1\text{ms}}{5 \times 0.1\mu\text{F}} = 2000\Omega \text{ or } 2\text{k}\Omega$$

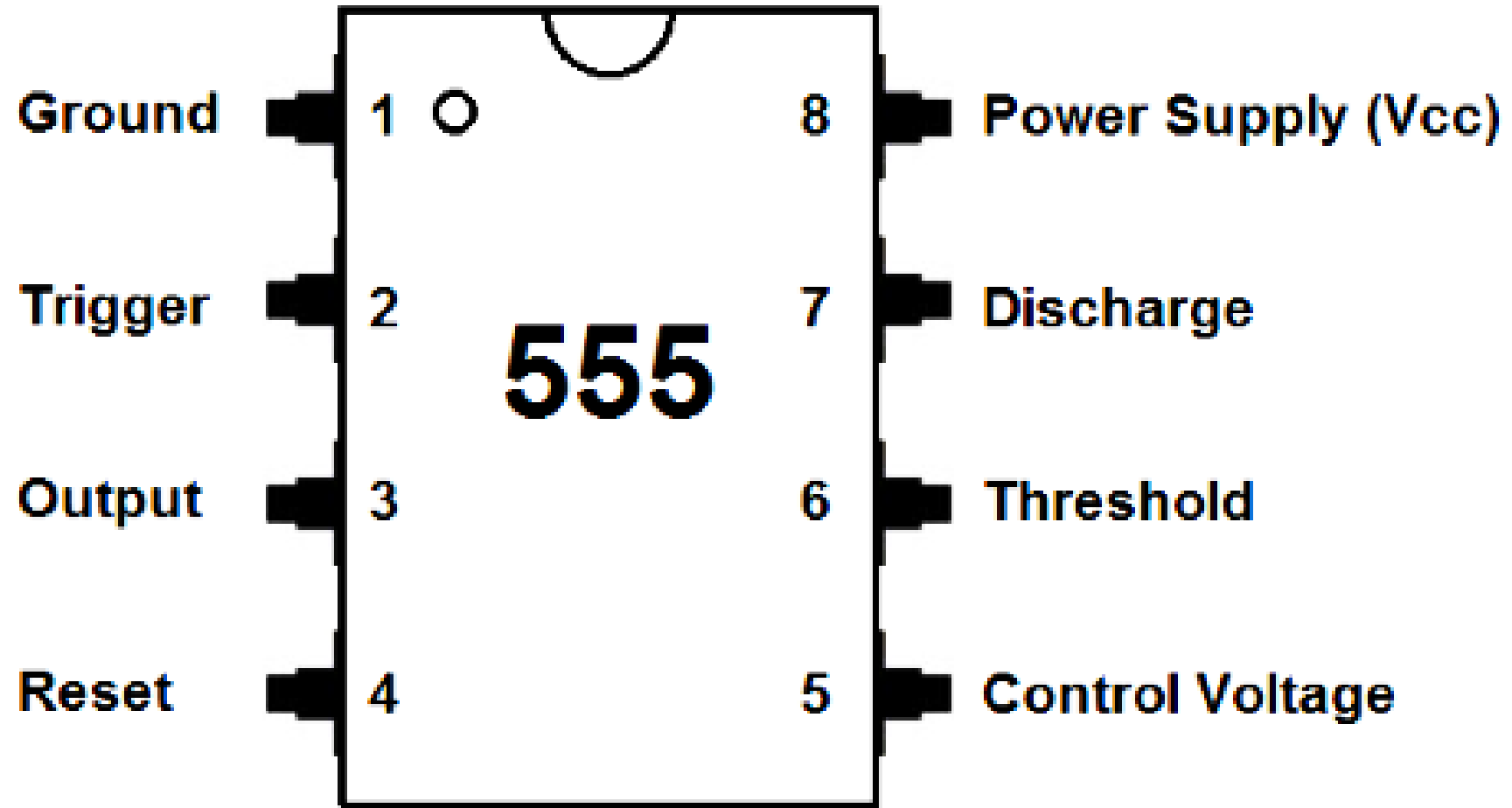


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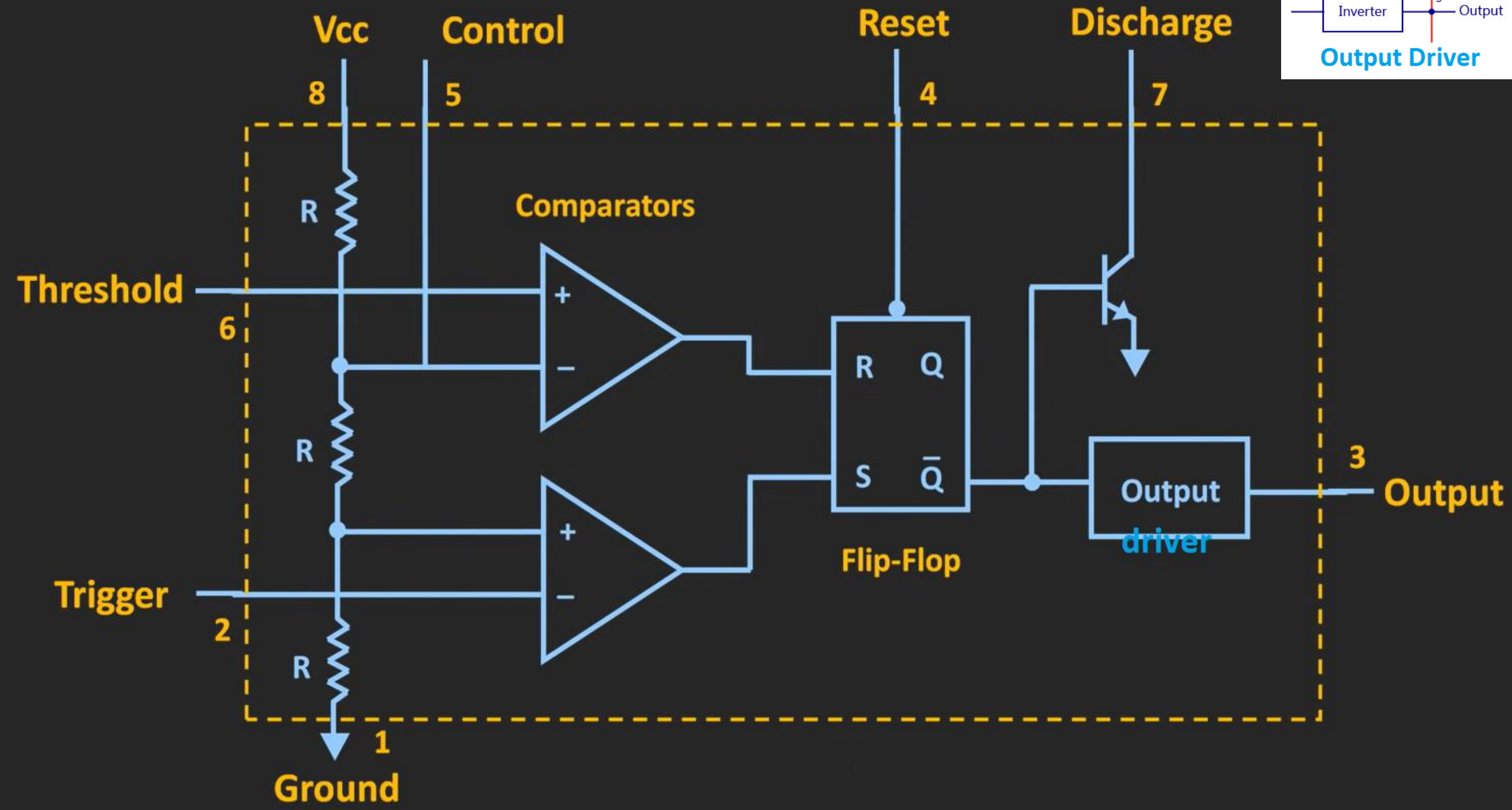
Signal Generators

- ✓ **Monostable Multivibrator using op-Amp**
 - ✓ Working Principal
 - ✓ Calculation of Time Period and Recovery Time
 - ✓ Design Example
- **555 Time IC**
 - Pin Configuration
 - Internal Block Diagram
- **Astable Multivibrator using Timer IC**

PIN DIAGRAM

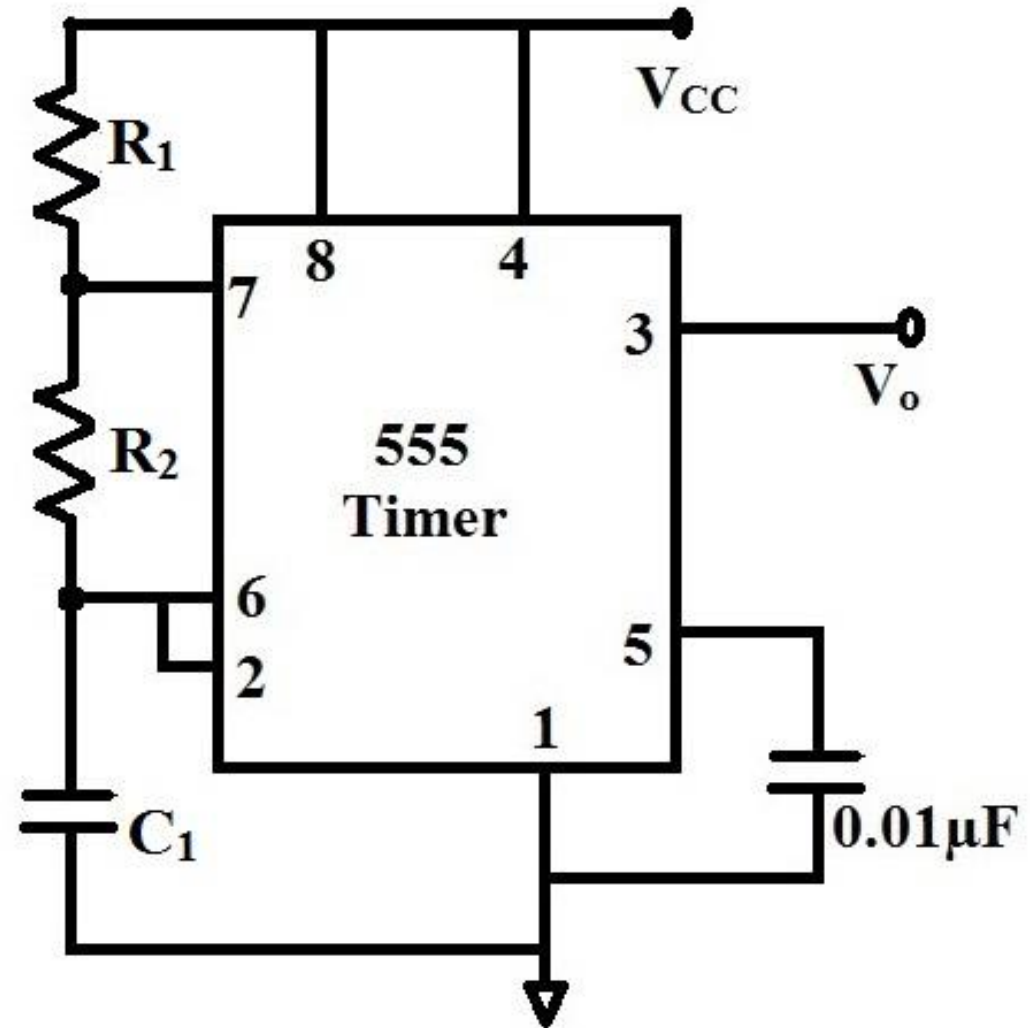


FUNCTIONAL BLOCK DIAGRAM OF 555 TIMER

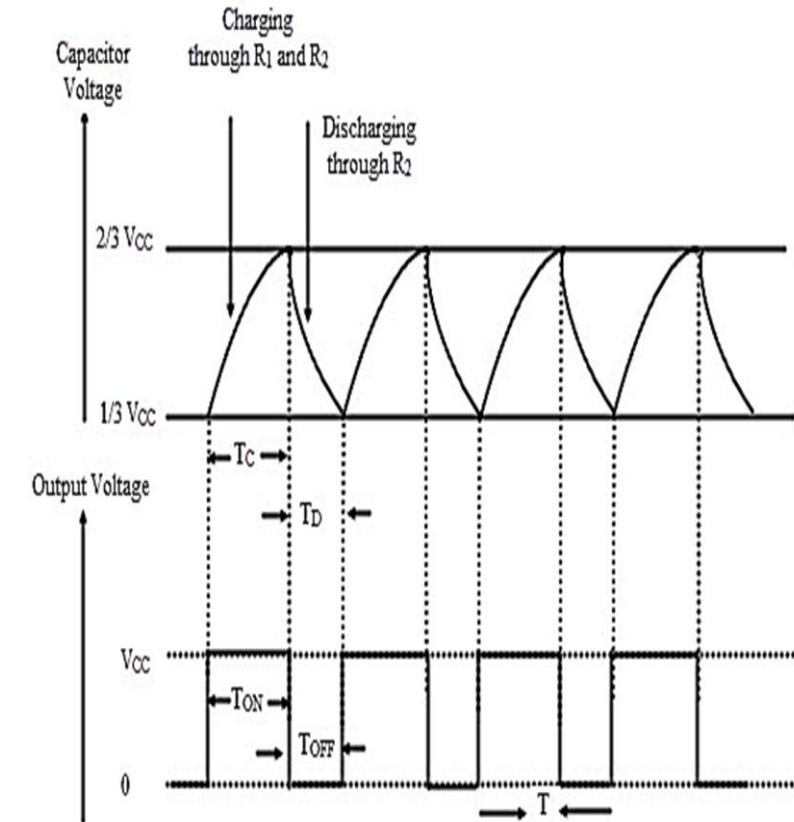
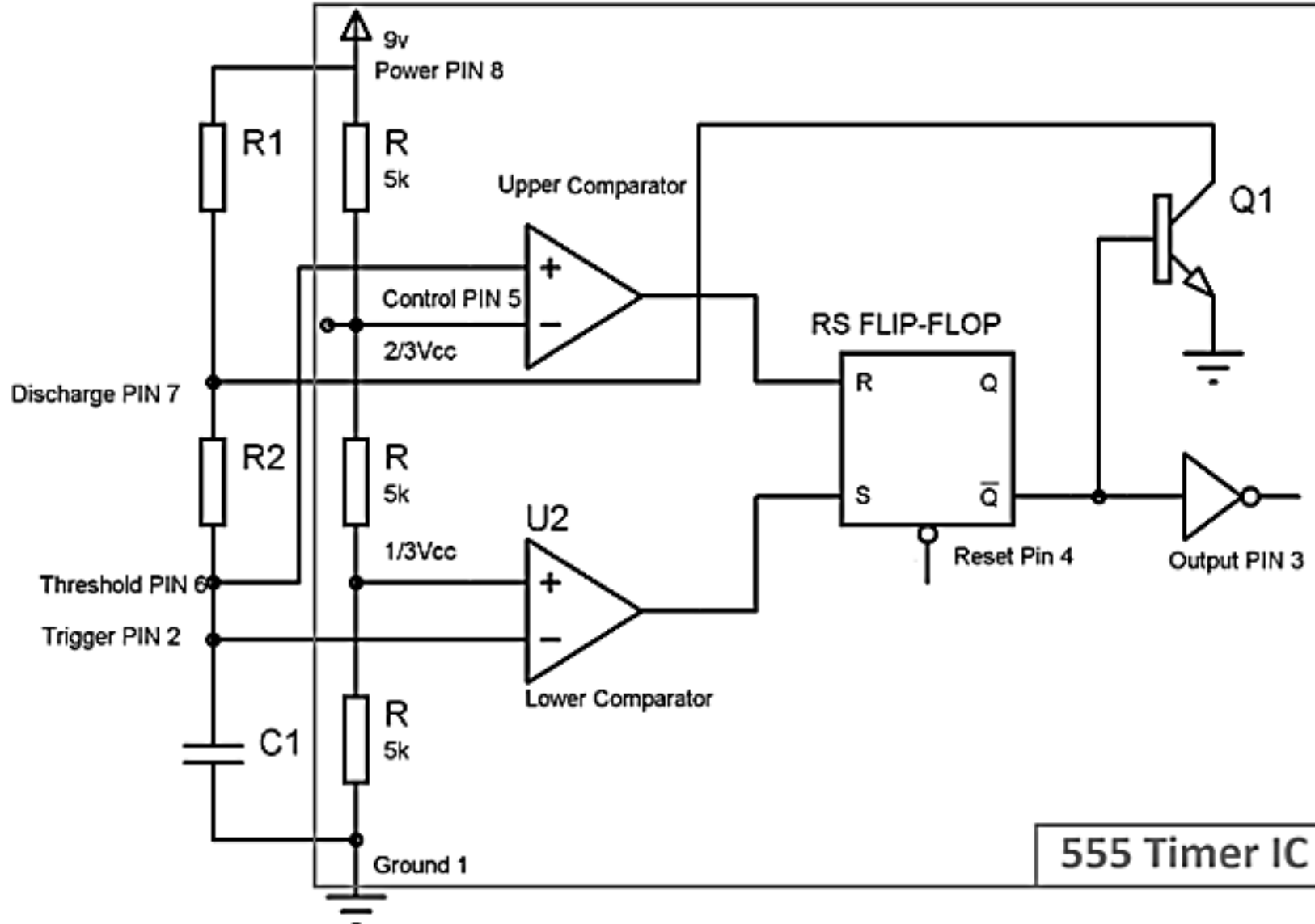


ASTABLE MULTIVIBRATOR USING 555 TIMER

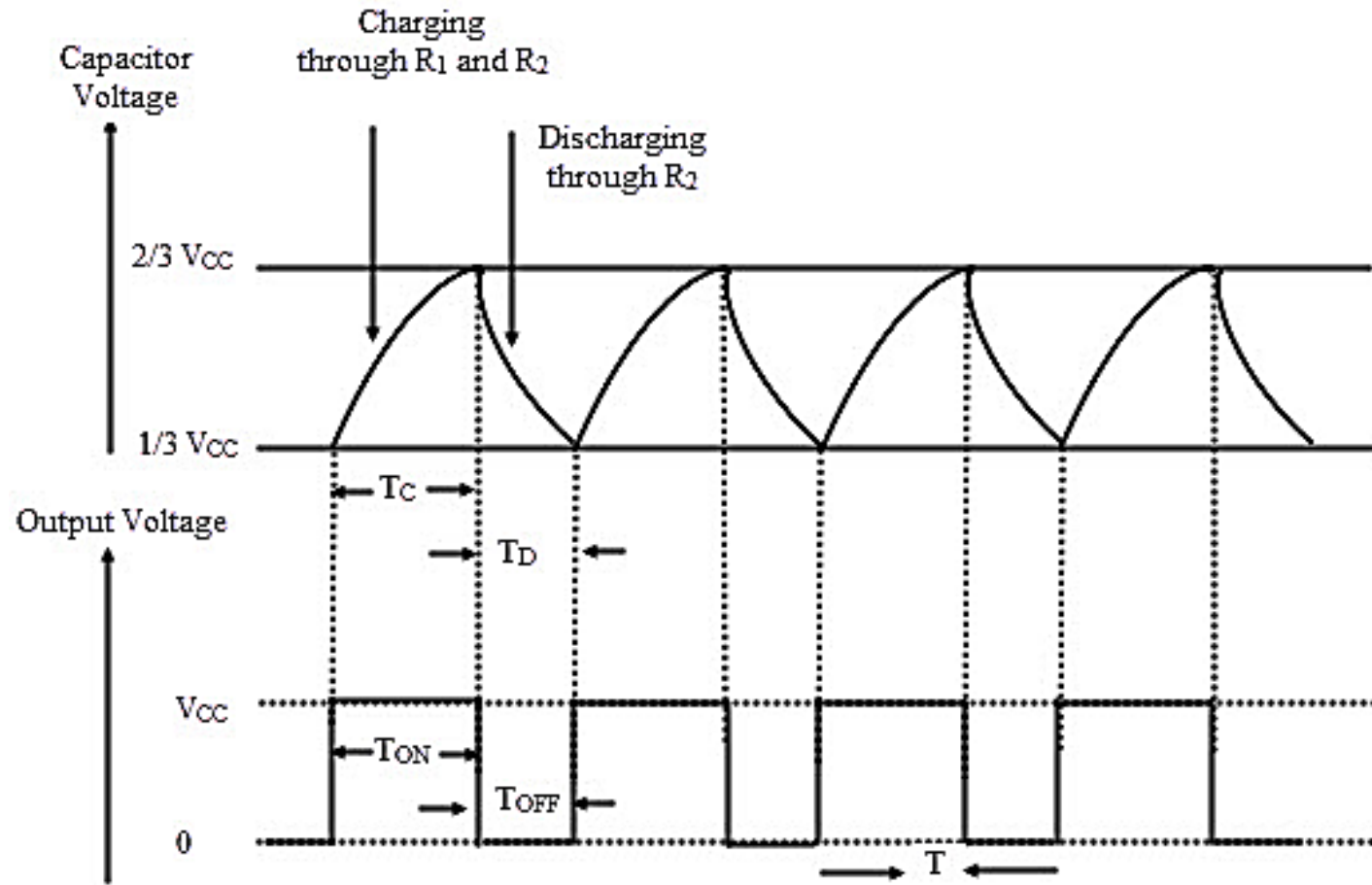
- 1 - Ground
- 2 - Trigger
- 3 - Output
- 4 - Reset
- 5 - Control
- 6 - Threshold
- 7 - Discharge
- 8 - Vcc



FUNCTIONAL BLOCK DIAGRAM OF ASTABLE MULTIVIBRATOR



TIMING PULSES



DERIVATION FOR THE EXPRESSION OF DUTY CYCLE

$$V_C = V_{CC} \left(1 - e^{-t/RC}\right)$$

- Time taken, t_1 by the circuit to charge from 0 - $\frac{2}{3}V_{CC}$,

$$\frac{2}{3}V_{CC} = V_{CC} \left(1 - e^{-t_1/RC}\right)$$



$$t_1 = 1.099RC$$

- Time taken, t_2 by the circuit to charge from $0 - \frac{1}{3}V_{CC}$,

$$\frac{1}{3}V_{CC} = V_{CC}(1 - e^{-t_2/RC})$$

$$t_2 = 0.405RC$$

- Time to charge from $\frac{1}{3}V_{CC}$ to $\frac{2}{3}V_{CC}$,

$$T_C = t_1 - t_2$$

$$T_C = 0.69(R_1 + R_2)C$$

- Capacitor discharges from $\frac{2}{3}V_{CC}$ to $\frac{1}{3}V_{CC}$.

$$\frac{1}{3}V_{CC} = \frac{2}{3}V_{CC}e^{-t/RC}$$

- Solving the equation we get ,

$$t = 0.69 T_D = 0.69 R_2 C$$

- Total time,

$$T = T_C + T_D$$

$$T = 0.69 (R_1 + 2R_2)C$$

$$f = \frac{1.45}{(R_1 + 2R_2)C}$$

- Duty cycle,

$$D\% = \frac{T_c}{T} \times 100\%$$

$$\Rightarrow D\% = \left(\frac{R_1 + R_2}{R_1 + 2 R_2} \right) \times 100\%$$

$$T = 0.69 (R_1 + 2R_2)C$$

$$f = \frac{1.45}{(R_1 + 2R_2)C}$$

EXAMPLE 10.3. In the circuit of Fig. 10.16 specify suitable components for $f_0 = 50$ kHz and $D(\%) = 75\%$.

Solution. Let $C = 1$ nF, so that $R_A + 2R_B = 1.44/(f_0 C) = 28.85$ k Ω . Imposing $(R_A + R_B)/(R_A + 2R_B) = 0.75$ gives $R_A = 2R_B$. Solving gives $R_A = 14.4$ k Ω (use 14.3 k Ω) and $R_B = 7.21$ k Ω (use 7.15 k Ω).

Q1) For an astable multivibrator using 555 timer, $R_1 = 6.8\text{k}\Omega$, $R_2 = 3.3\text{k}\Omega$ and $C = 0.1\mu\text{F}$. Calculate (a) t_{HIGH} , (b) t_{LOW} , (c) free running frequency and (d) duty cycle, D.

Ans :-

(a) $t_{\text{HIGH}} = 0.7\text{ms}$

(b) $t_{\text{LOW}} = 0.23\text{ms}$

(c) $f = 1.07\text{kHz}$

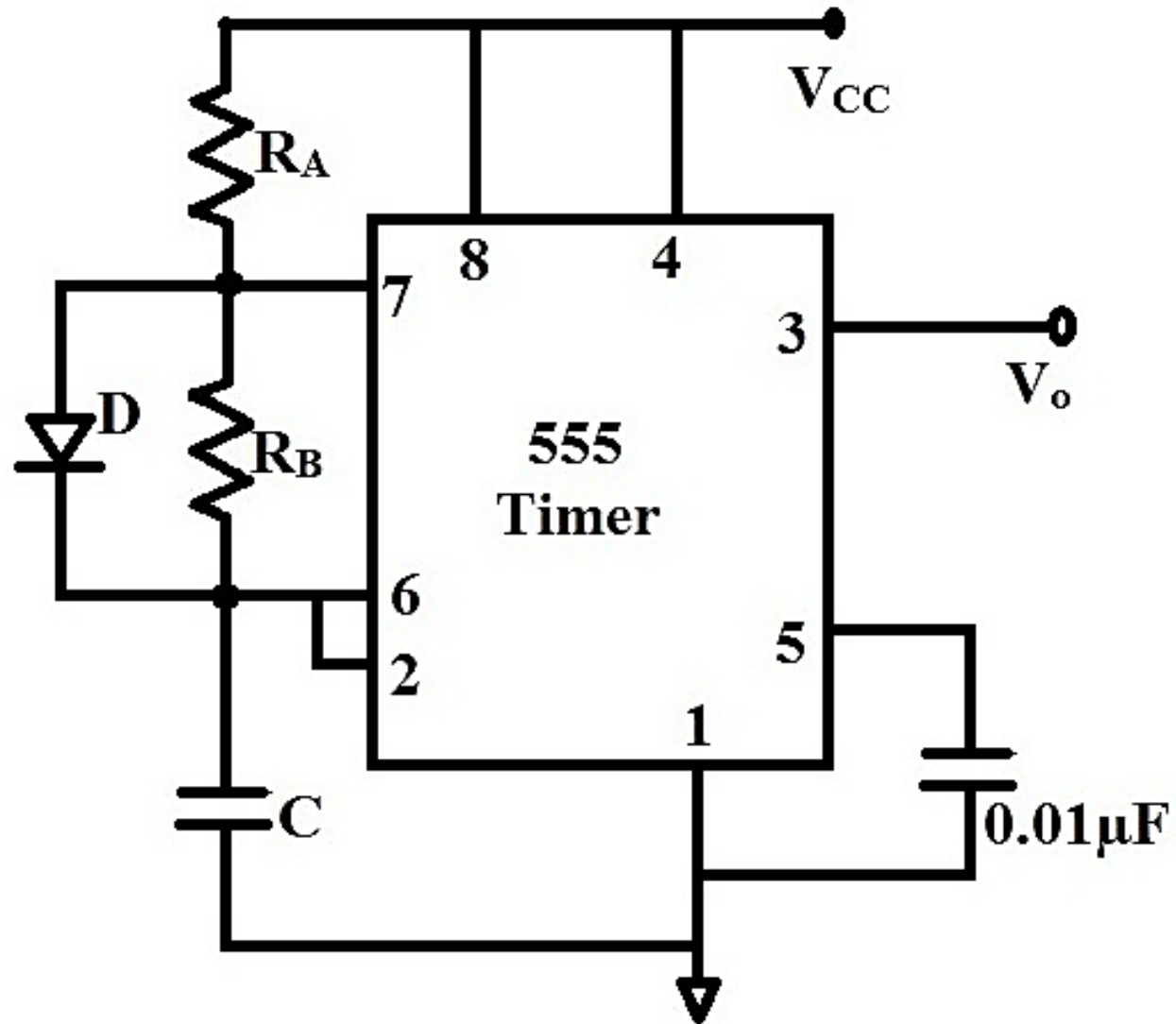
(d) $D = 0.75$ or 75%

LIC: LECTURE

Signal Generators

- ✓ **555 Time IC**
 - ✓ **Pin Configuration**
 - ✓ **Internal Block Diagram**
- ✓ **Astable Multivibrator using Timer IC**
 - **Design Example**
- **Bistable Multivibrator using Timer IC**
 - **Applications**

ADJUSTABLE DUTY CYCLE MULTIVIBRATOR



DUTY CYCLE DERIVATION

- During charging,

$$T_C = 0.69 R_A C$$

- During discharge,

$$T_D = 0.69 R_B C$$

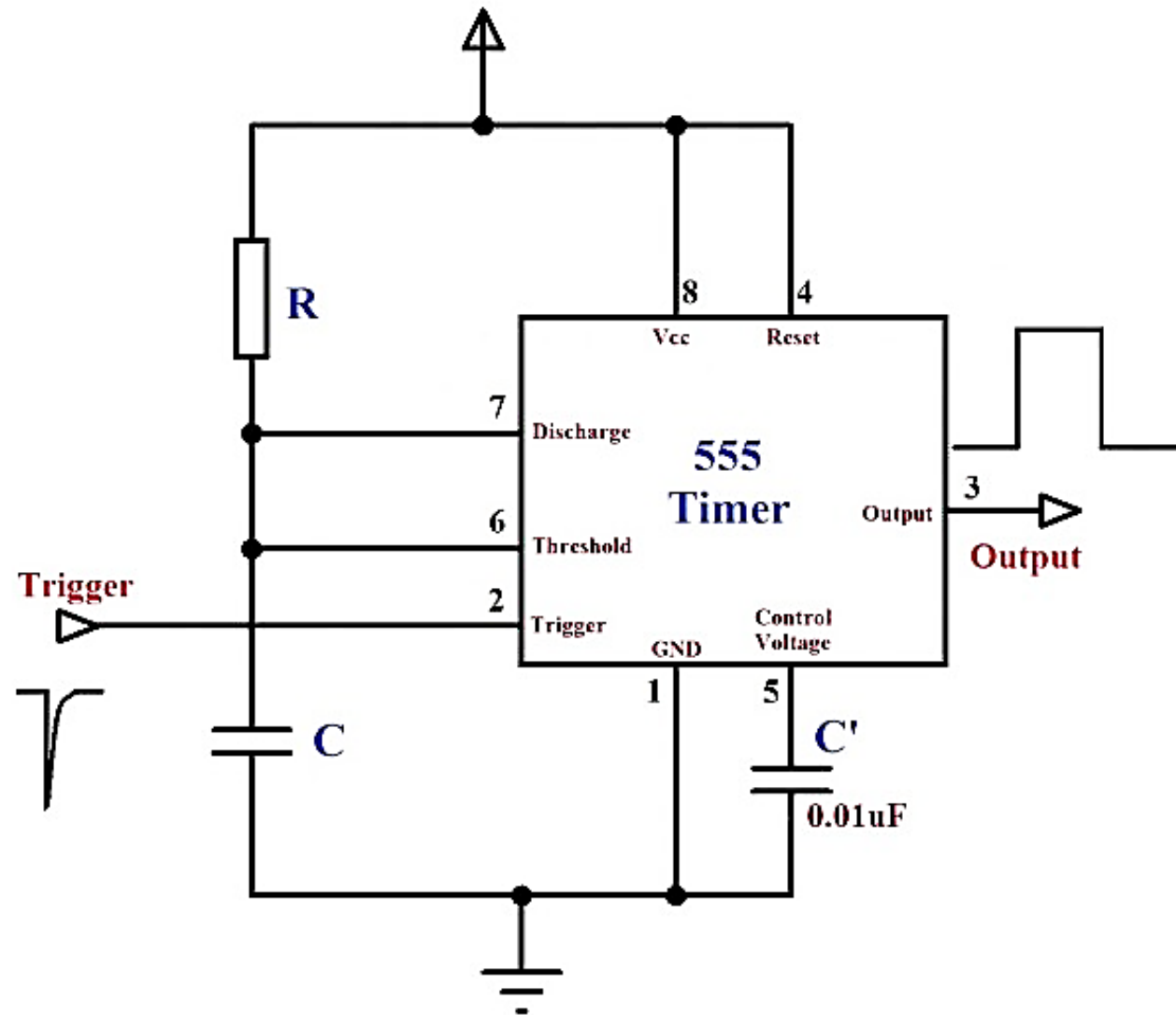
- Therefore, total time period T is,

$$T = 0.69 (R_A + R_B)C$$

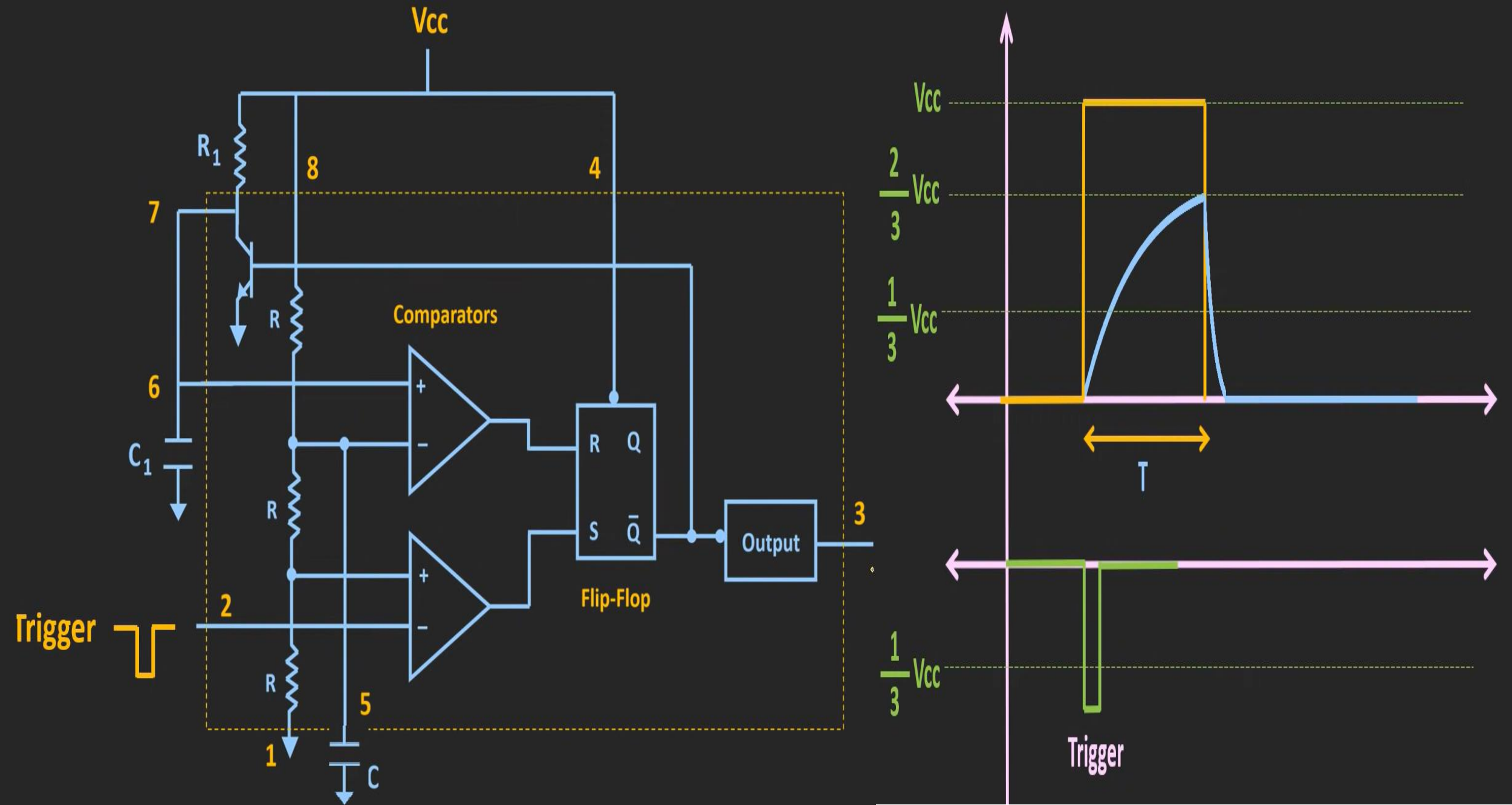
$$f = \frac{1.45}{(R_A + R_B)C}$$

$$D = \frac{R_A}{R_A + R_B}$$

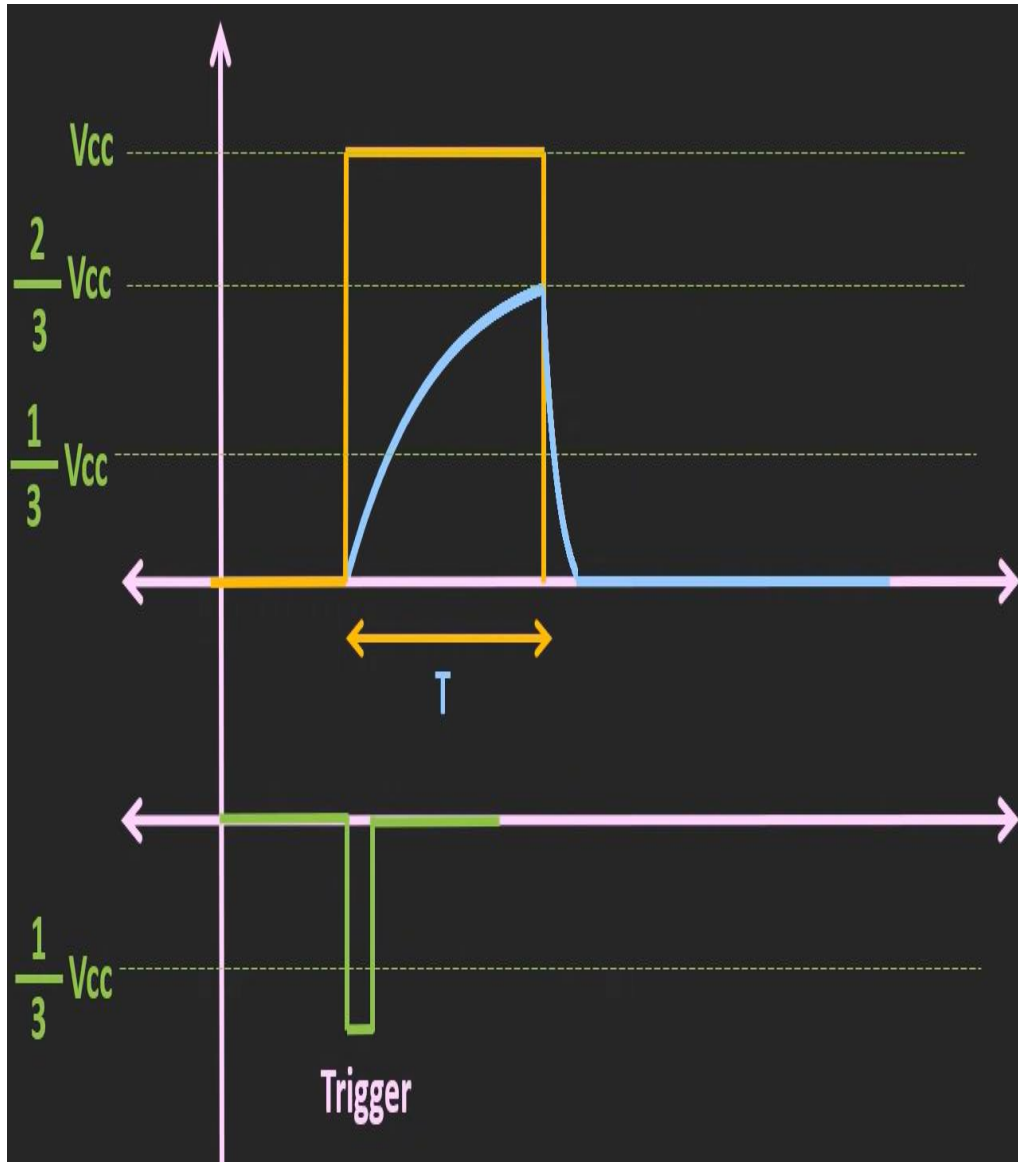
MONOSTABLE MULTIVIBRATOR USING 555 TIMER



FUNCTIONAL BLOCK DIAGRAM OF MONOSTABLE MULTIVIBRATOR



TIME PERIOD DERIVATION



$$V_c(t) = V_0 (1 - e^{-t/RC})$$

$$\begin{aligned} V_c(t) &= V_F + (V_I - V_F) e^{-t/RC} \\ &= V_{cc} + (0 - V_{cc}) e^{-t/RC} \end{aligned}$$

$$V_c(t) = V_{cc} \times (1 - e^{-t/RC})$$

$$\frac{1}{3} = e^{-t/RC}$$

$$\ln\left(\frac{1}{3}\right) = -\frac{t_1}{RC}$$

$$\Rightarrow t_1 = RC \times \ln(3)$$

$$t_1 \approx 1.1 RC$$

Q2) Design a monostable multivibrator using 555 timer to produce a pulse width of 100ms. Calculate the value of R by assuming the values of $C = 0.47\mu\text{F}$.

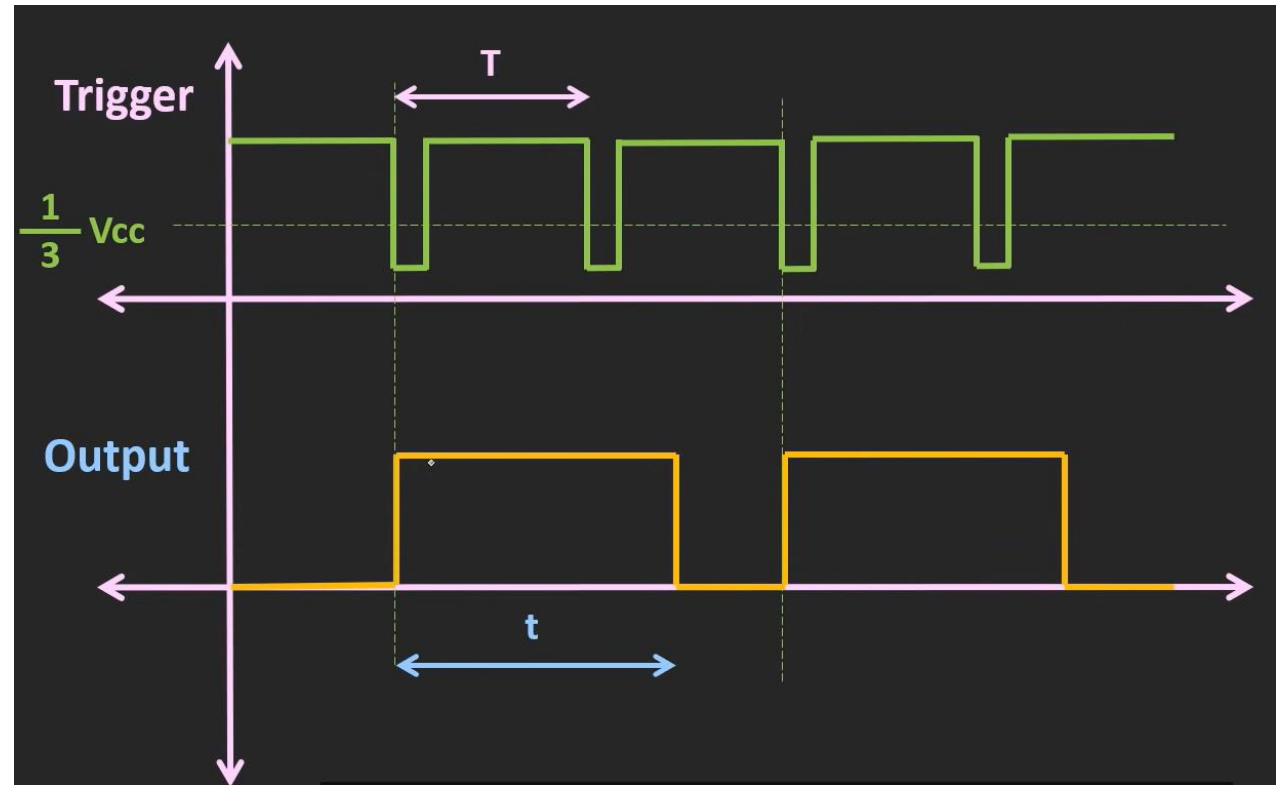
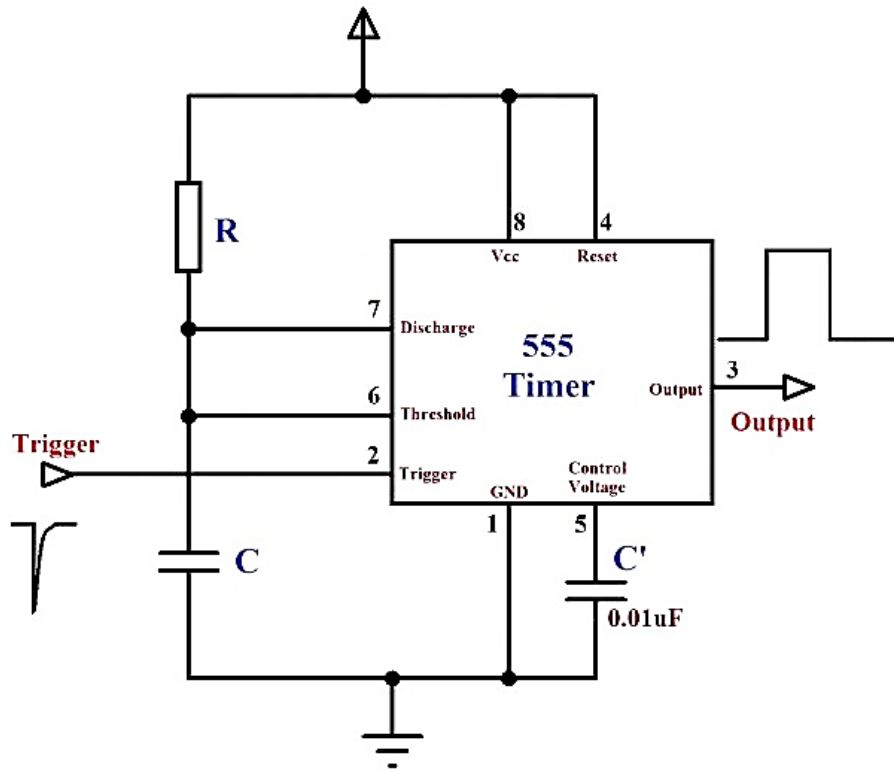
Ans: -

$$T = 1.1 RC$$

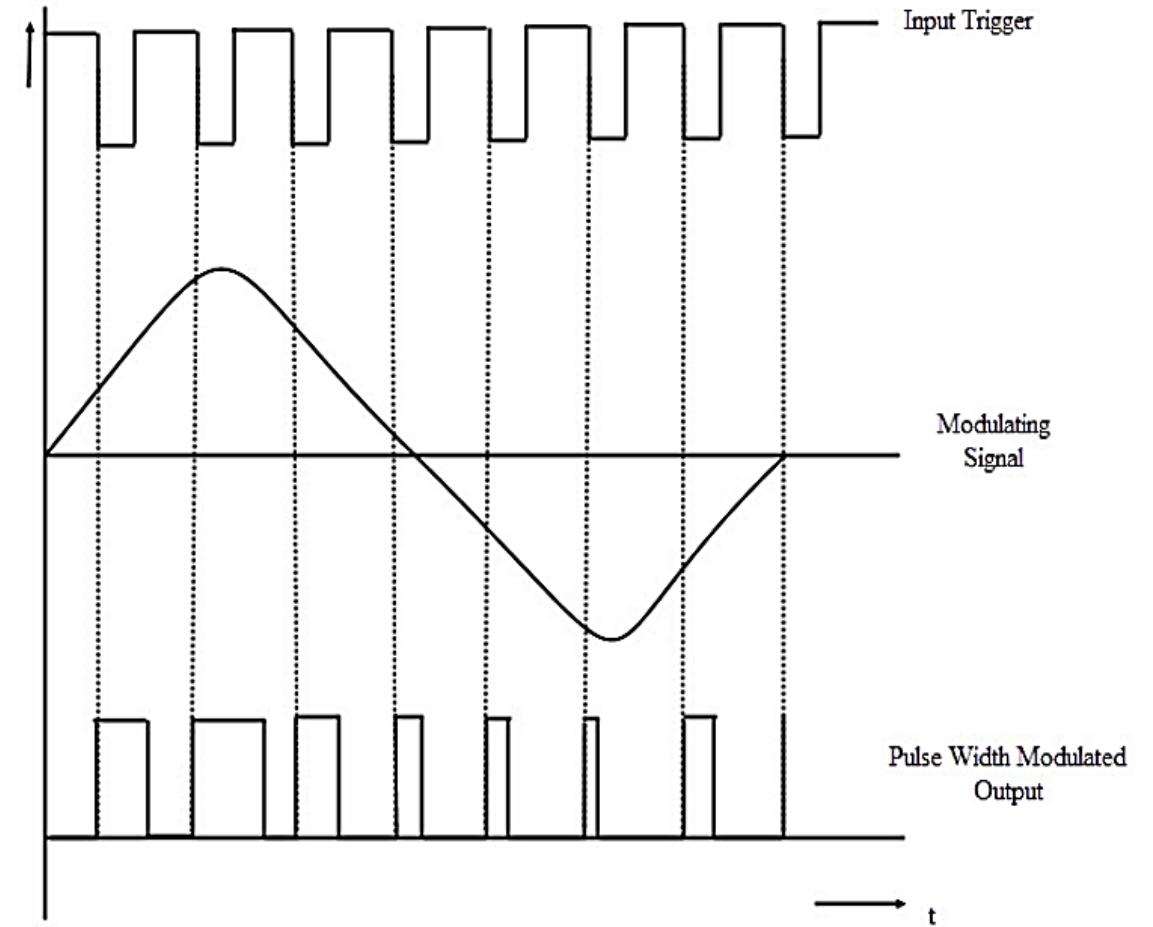
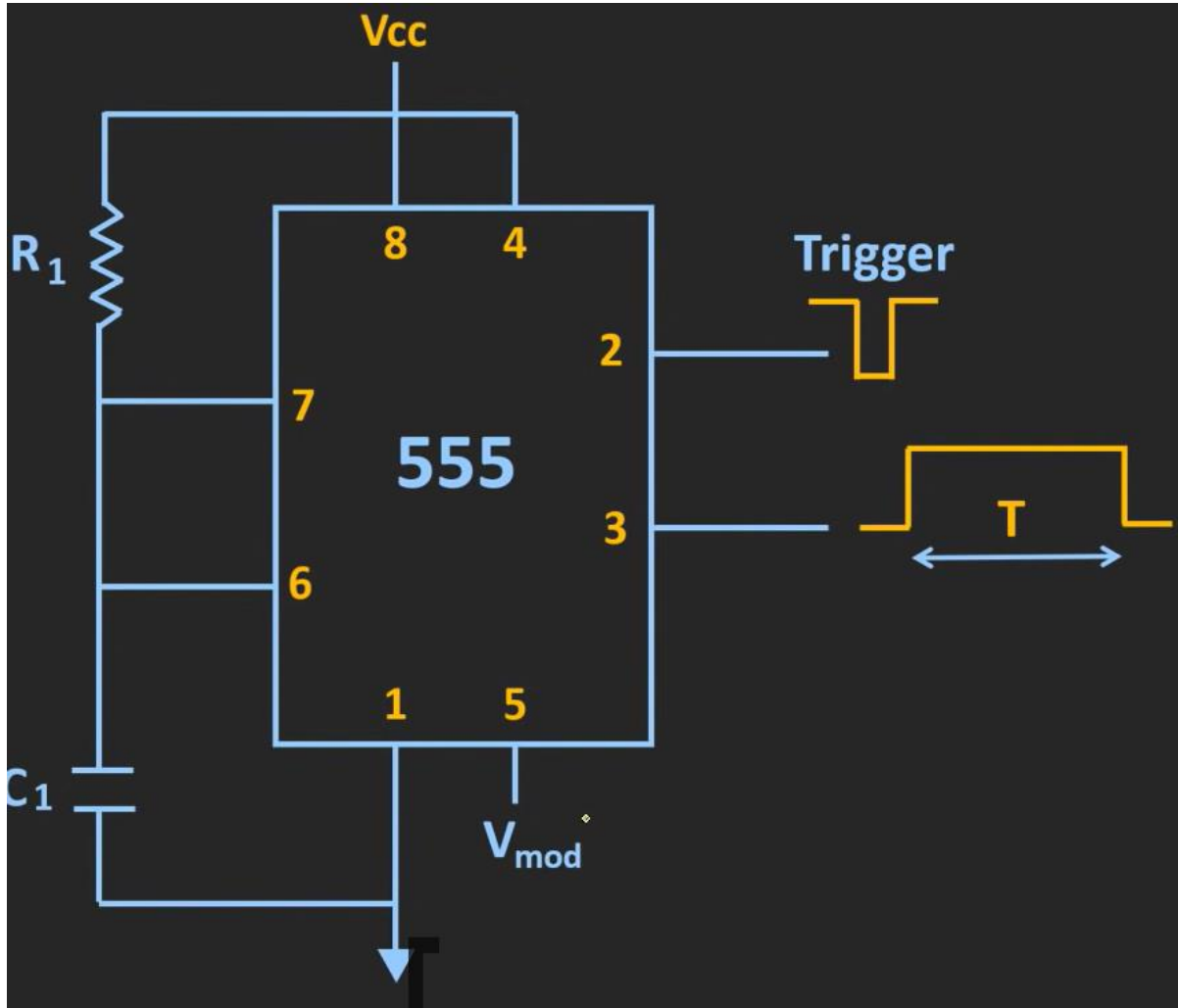
$$R = 193.423\text{k}\Omega$$

APPLICATION OF MONOSTABLE MULTIVIBRATOR

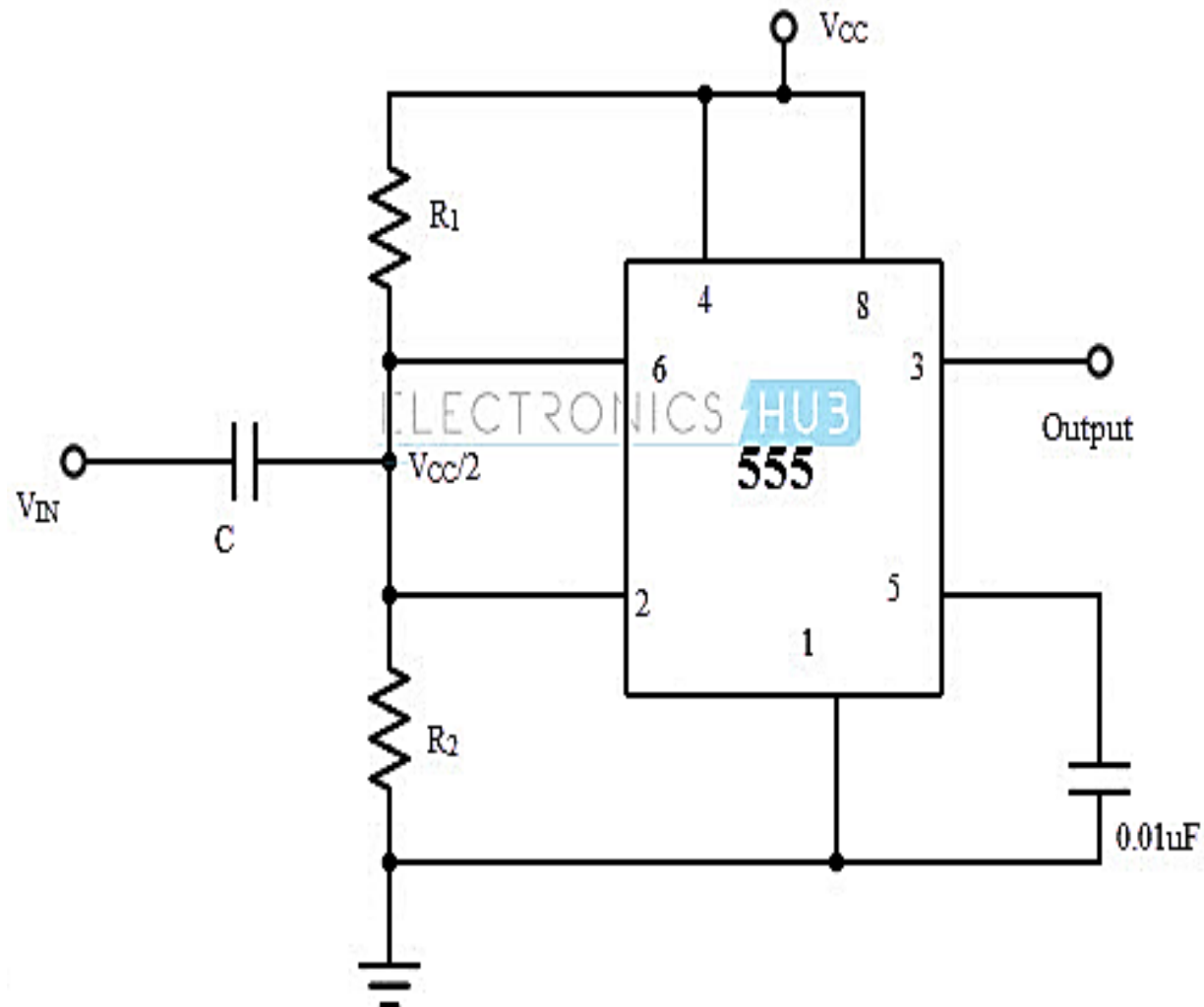
Frequency Divider



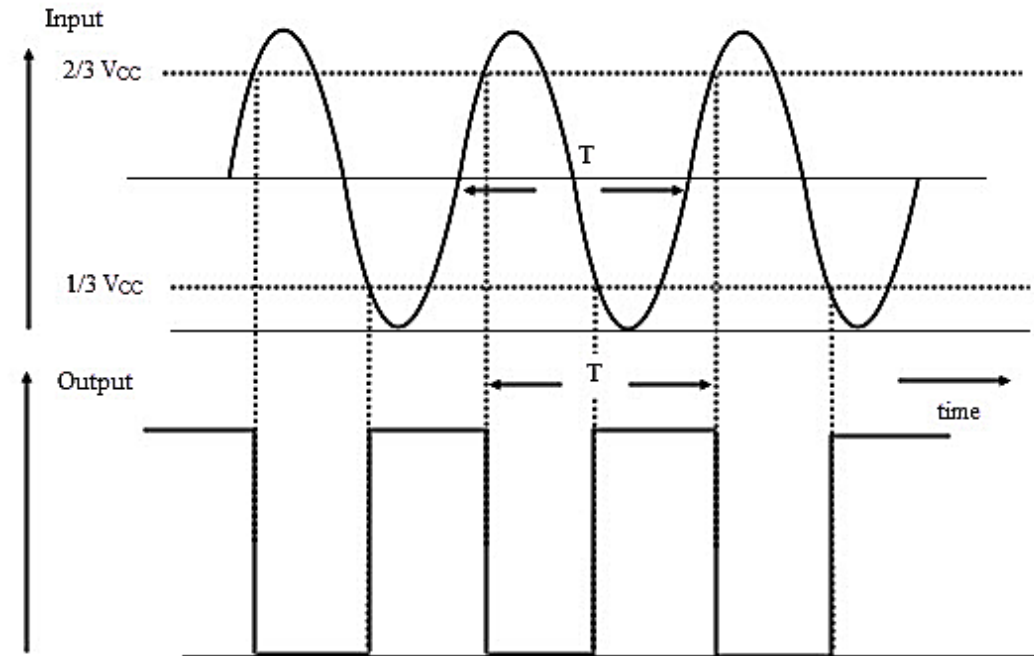
Pulse Width Modulation



SCHMITT TRIGGER



TIMING PULSES



LIC: LECTURE

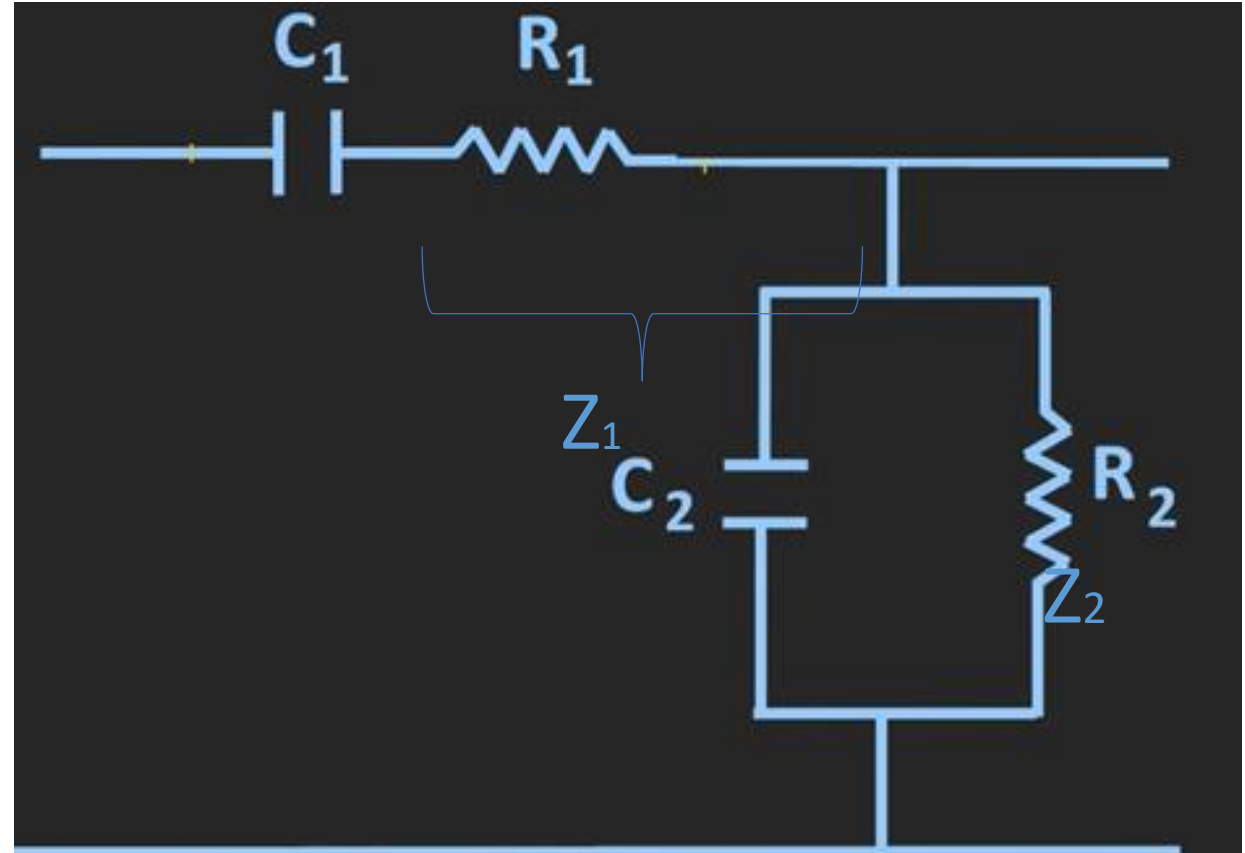
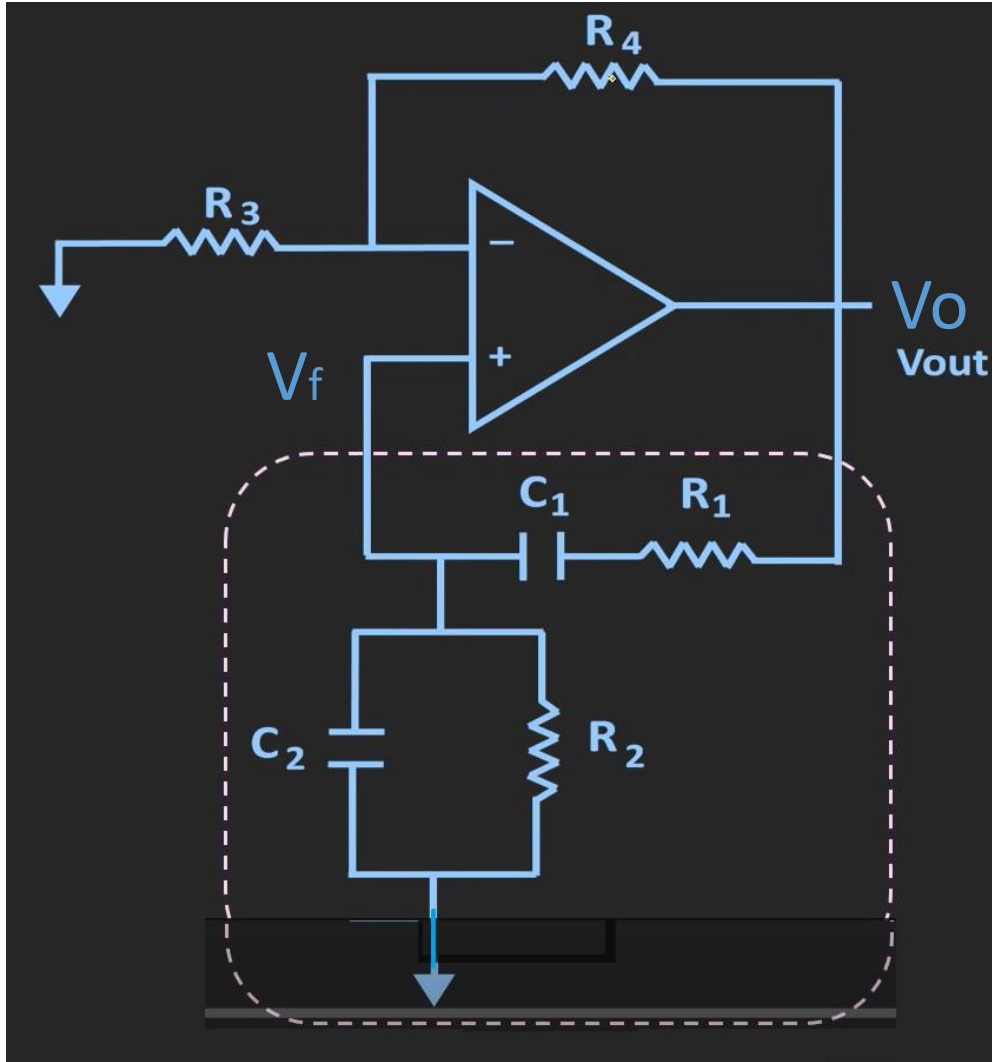
Signal Generators

- ✓ **Design of Multivibrators using Timer IC**
 - ✓ **Different Applications**
- **Sine Wave Generation Using Op-Amp**
 - **Circuit**
 - **Derivation of frequency of operation**
- **Triangular Wave Generation Using Op-Amp**
 - **Circuit**
 - **Derivation of frequency of operation**

Sine Wave Generation

- One of the simplest sine wave oscillators which uses a RC network in place of the conventional LC tuned tank circuit to produce a sinusoidal output waveform, is called a **Wien Bridge Oscillator**.
- The **Wien Bridge Oscillator** is so called because the circuit is based on a frequency-selective form of the Wheatstone bridge circuit.
- The Wien Bridge oscillator is a two-stage RC coupled amplifier circuit that has good stability at its resonant frequency, low distortion and is very easy to tune making it a popular circuit as an audio frequency oscillator but the phase shift of the output signal is considerably different from the previous phase shift **RC Oscillator**.

WEIN'S BRIDGE OSCILLATOR



$$\beta = V_f / V_o$$

The loop gain must be unity or greater. The feedback signal feeding back at the input must be phase-shifted by 360° (which is the same as zero degrees).

$$\frac{V_o}{V_{in}} = \frac{Z_2}{Z_1 + Z_2} \quad Z_2 = R_2 \parallel \left(\frac{1}{j\omega C_2} \right) = \frac{R_2}{1 + j\omega R_2 C_2}$$

$$\frac{V_o}{V_{in}} = \frac{R_2}{1 + j\omega R_2 C_2} \cdot \frac{1}{R_1 + \frac{1}{j\omega C_1} + \frac{R_2}{1 + j\omega R_2 C_2}}$$

$$\frac{V_o}{V_{in}} = \frac{R_2 C_1 j\omega C_1}{R_1 C_1 j\omega C_1 (1 + j\omega R_2 C_2) + 1 + j\omega R_2 C_2 + j\omega R_2 C_1}$$

$$\frac{V_o}{V_{in}} = \frac{j\omega R_2 C_1}{\underbrace{1 - \omega^2 R_1 R_2 C_1 C_2}_0 + j\omega [R_1 C_1 + R_2 C_2 + R_2 C_1]}$$

$$\omega^2 R_1 R_2 C_1 C_2 = 1$$

$$\Rightarrow \omega = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}}$$

$$\Rightarrow f = \frac{1}{2\pi \times \sqrt{R_1 R_2 C_1 C_2}} \Rightarrow f = \frac{1}{2\pi RC}$$

$$\frac{V_o}{V_{in}} = \frac{R_2 C_1}{R_1 C_1 + R_2 C_2 + R_2 C_1} = \beta \quad \beta = \frac{1}{3}$$

$$A\beta = 1$$

$$A = \frac{1}{\beta} = \frac{R_1 C_1 + R_2 C_2 + R_2 C_1}{R_2 C_1} = \frac{R_1}{R_2} + \frac{C_2}{C_1} + 1$$

$$A = \frac{1}{\beta} = \frac{R_1 C_1 + R_2 C_2 + R_2 C_1}{R_2 C_1} = \frac{R_1}{R_2} + \frac{C_2}{C_1} + 1$$

$$A = 1 + \frac{R_4}{R_3} = \frac{R_1}{R_2} + \frac{C_2}{C_1} + 1$$

$$\Rightarrow \frac{R_4}{R_3} = \frac{R_1}{R_2} + \frac{C_2}{C_1}$$

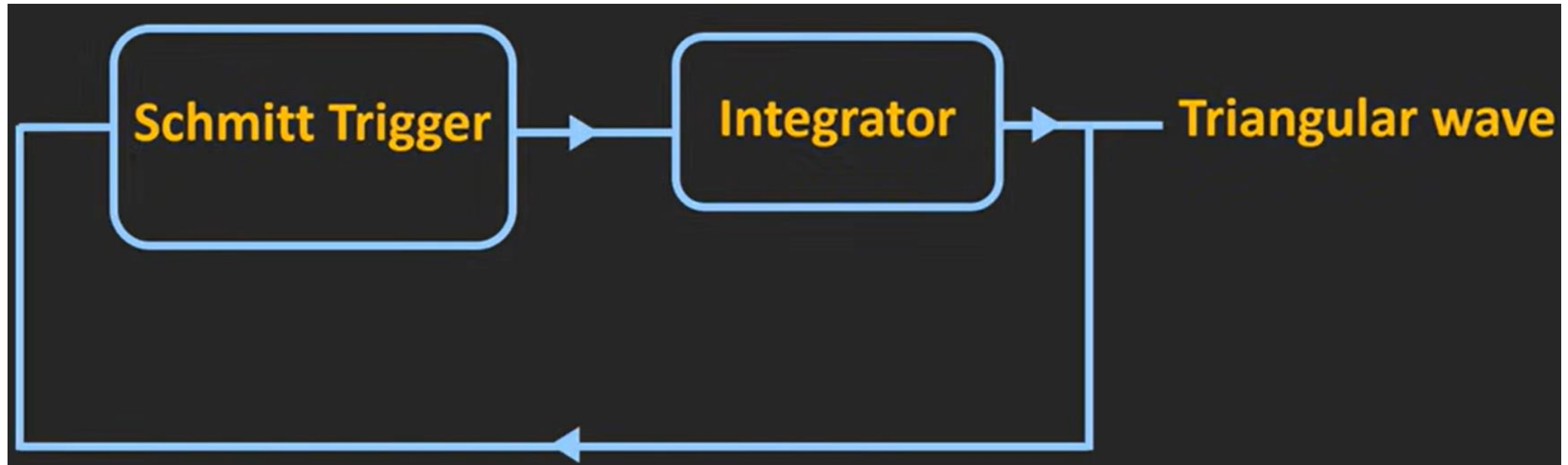
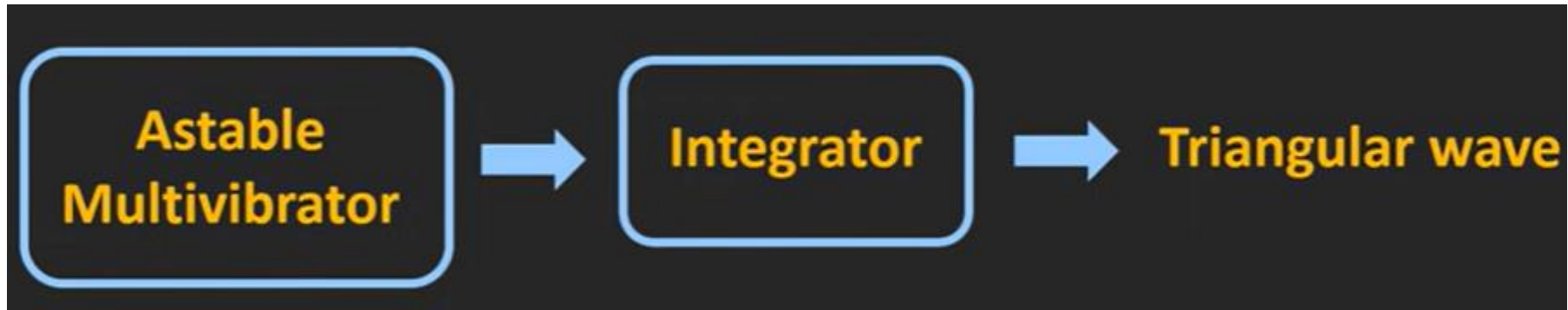
$$R_1 = R_2$$

$$C_1 = C_2$$

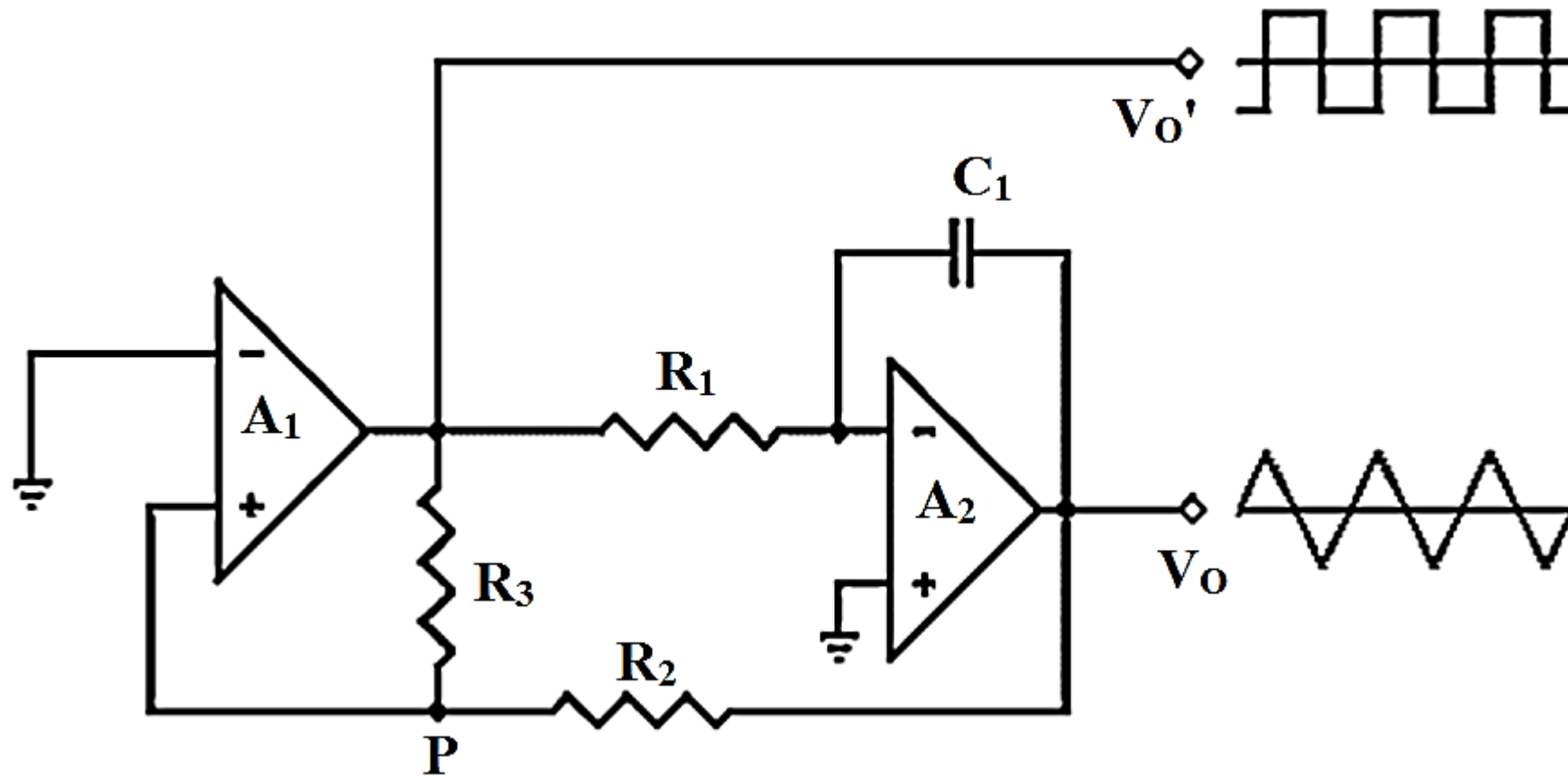
$$\Rightarrow \frac{R_4}{R_3} = 2$$

TRIANGULAR WAVE GENERATOR ????

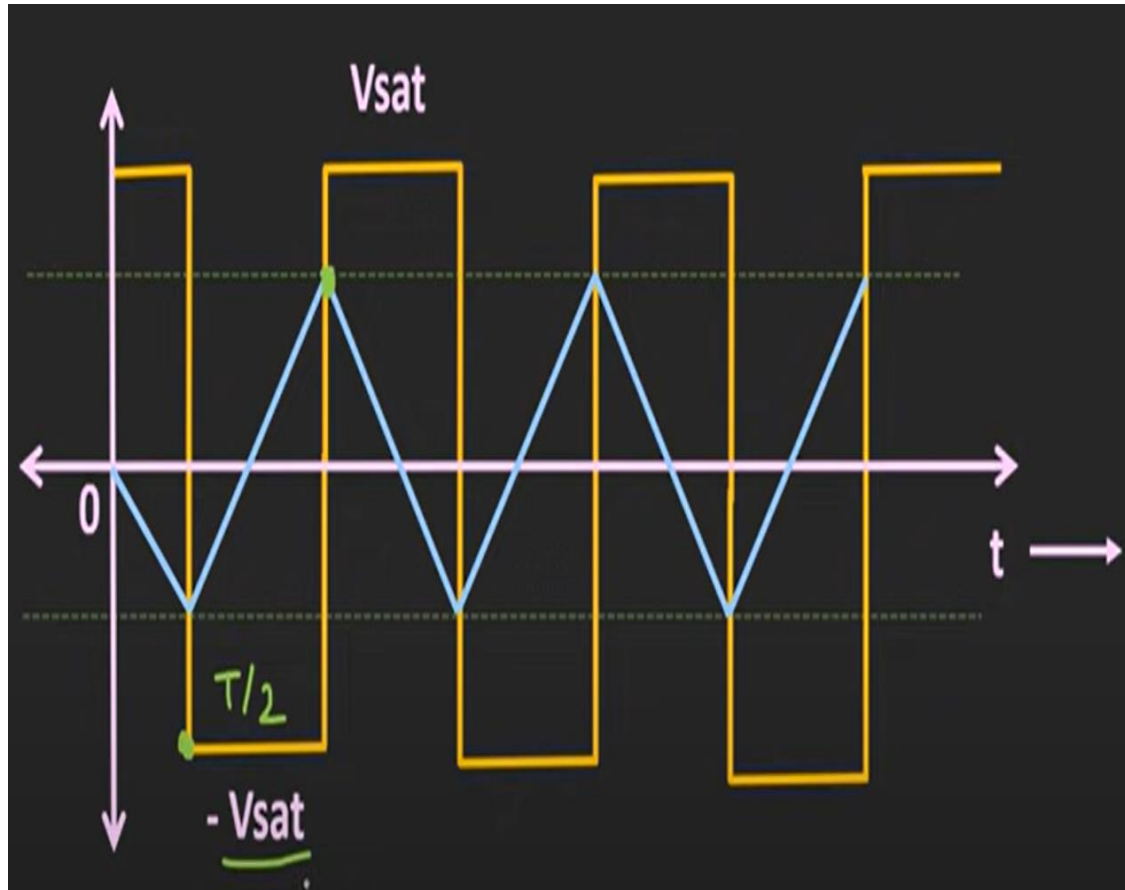
TRIANGULAR WAVE GENERATOR



TRIANGULAR WAVE GENERATOR using Schmitt Trigger



OUTPUT WAVEFORMS



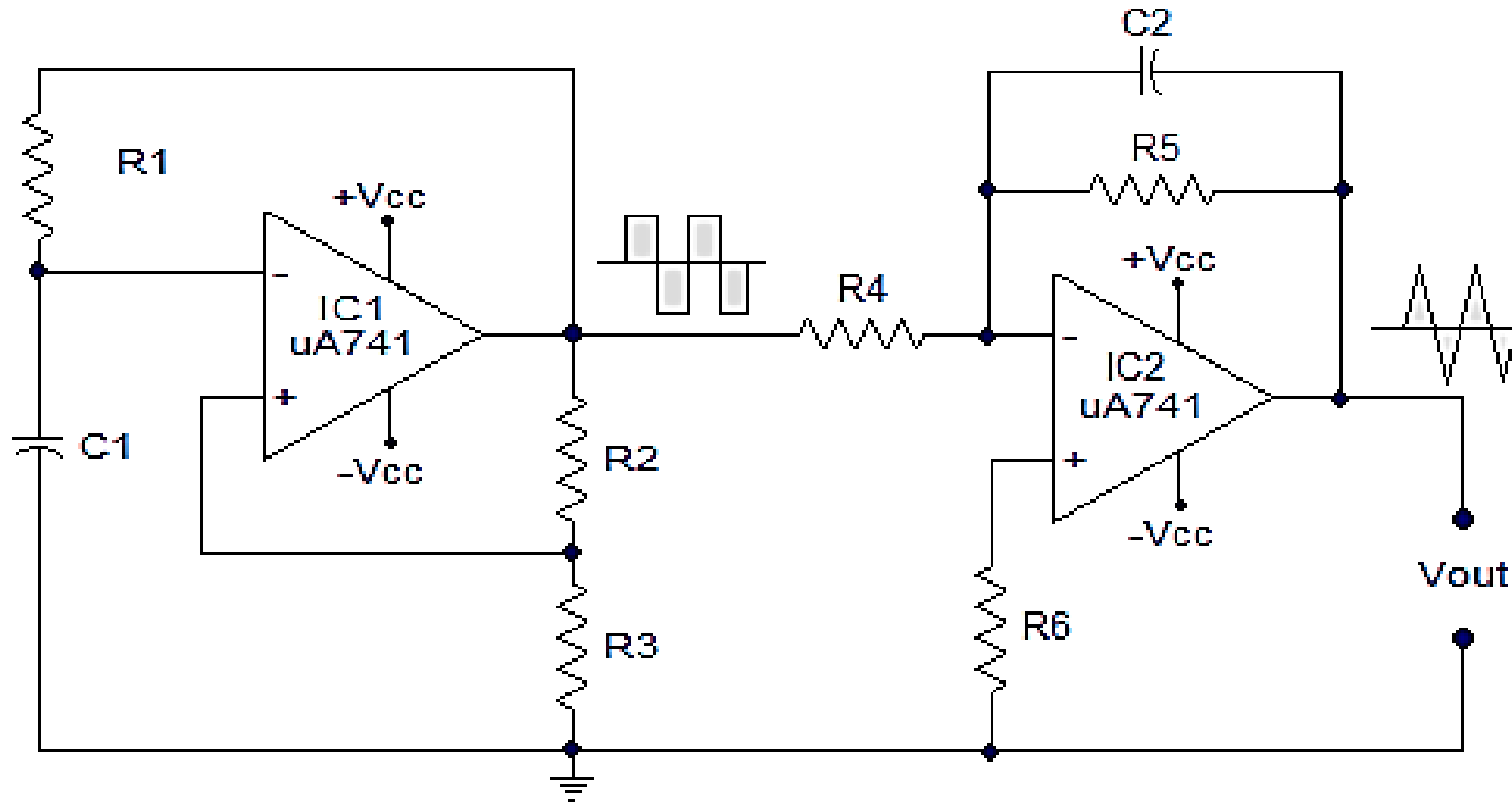
$$V_o = -\frac{1}{R_3 C_2} \int_0^t v_{in}(t) dt$$

$$V_{(P-P)} = -\frac{1}{R_3 C_2} \times (-V_{sat}) \times \frac{T}{2}$$

$$V_{P-P} = \frac{V_{sat} \times T}{2 R_3 C_2}$$

TRIANGULAR WAVE GENERATOR

using Astable Multivibrator



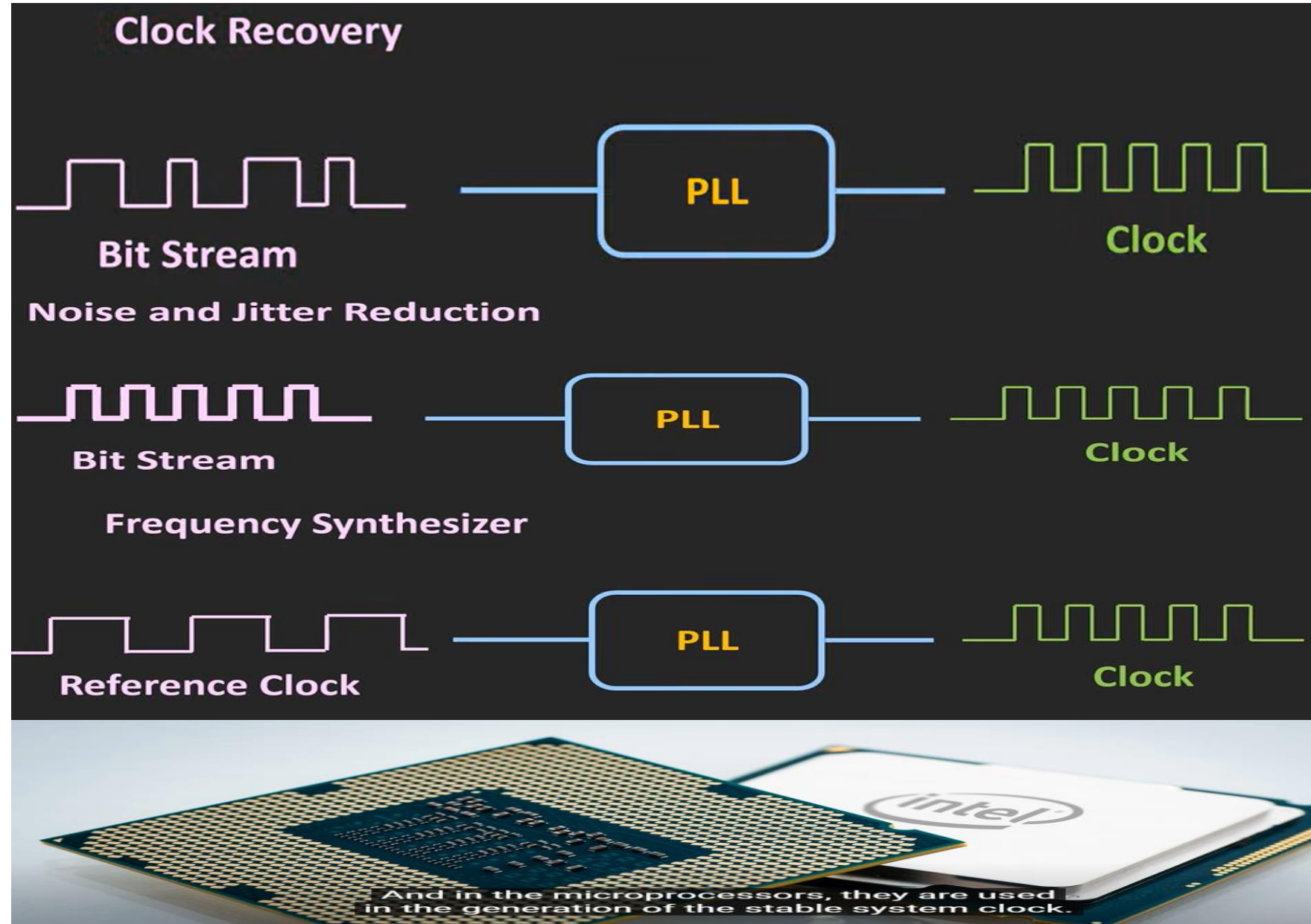
LIC: LECTURE

PHASE LOCKED LOOP (PLL)

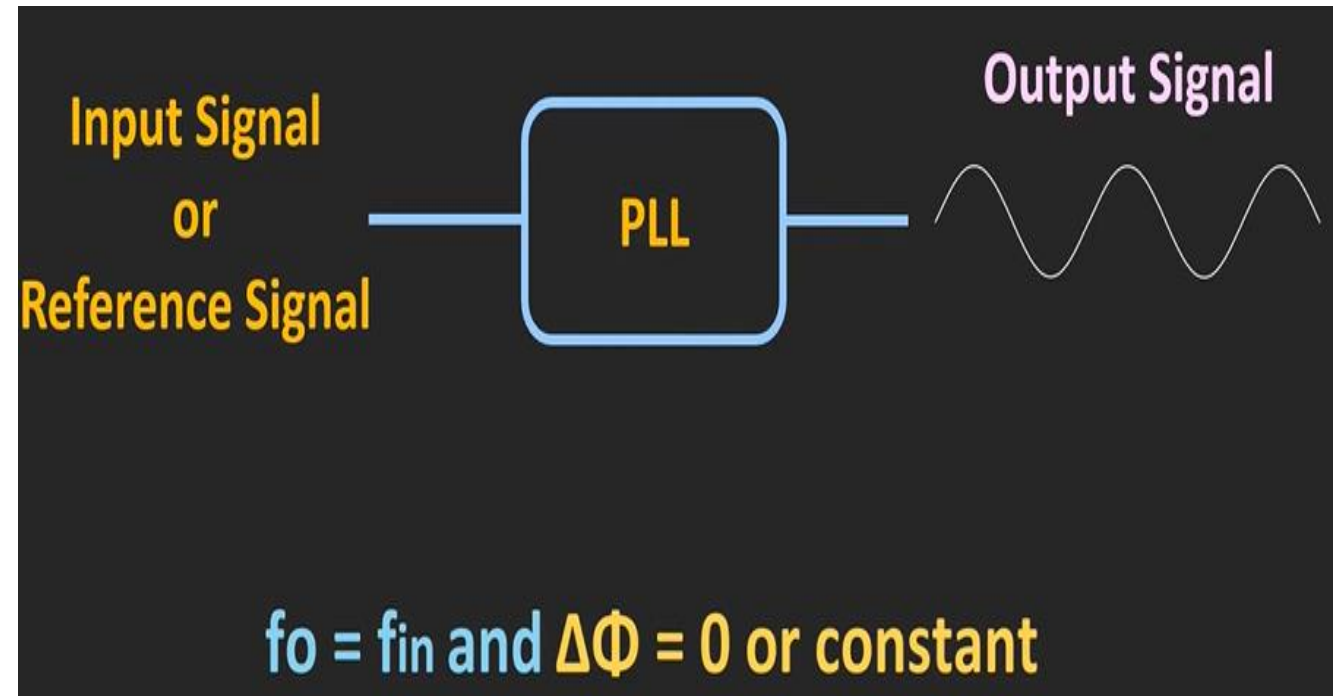
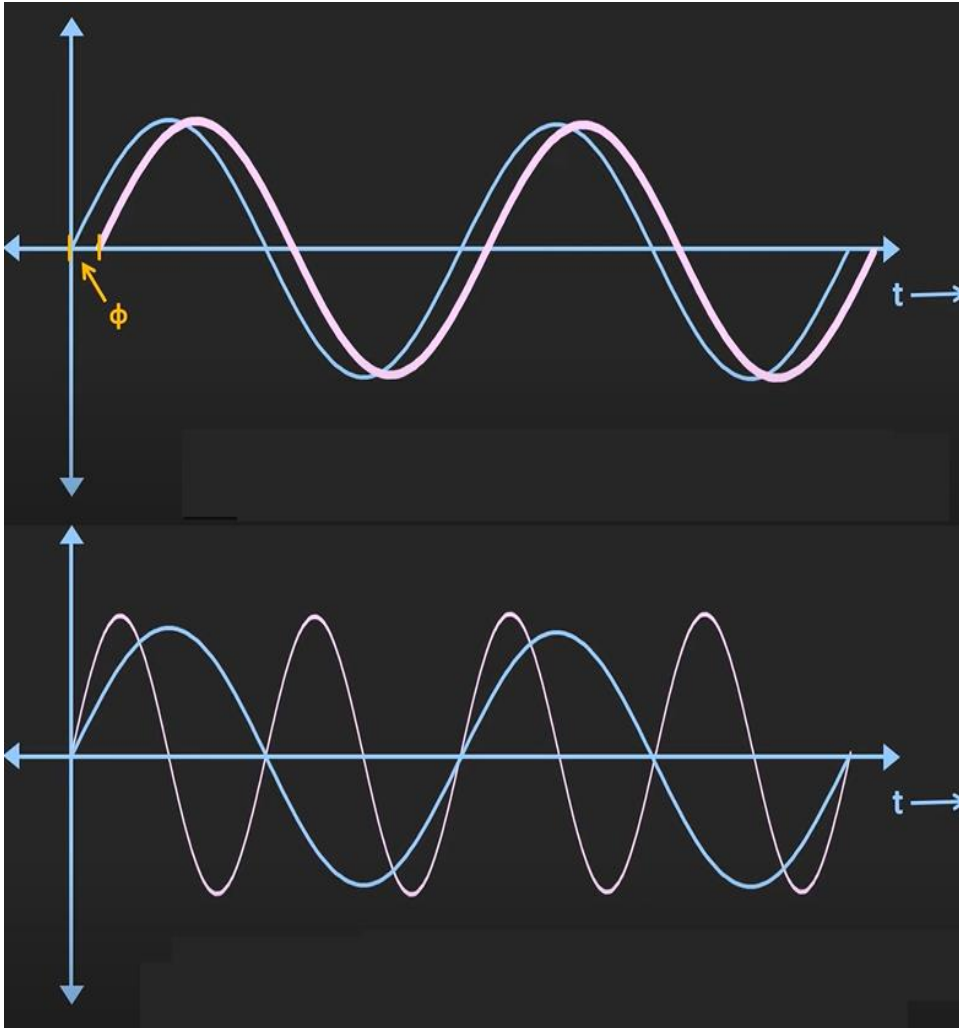
- **PLL Circuit**
 - **Need and Requirements**
 - **Circuit**
 - **Working Principal**
 - **Phase Detector Design**
 - **Voltage Controlled Oscillator**
 - **Application as Frequency Synthesizer ($f \cdot N$ or f/N)**

PHASE LOCKED LOOP (PLL)

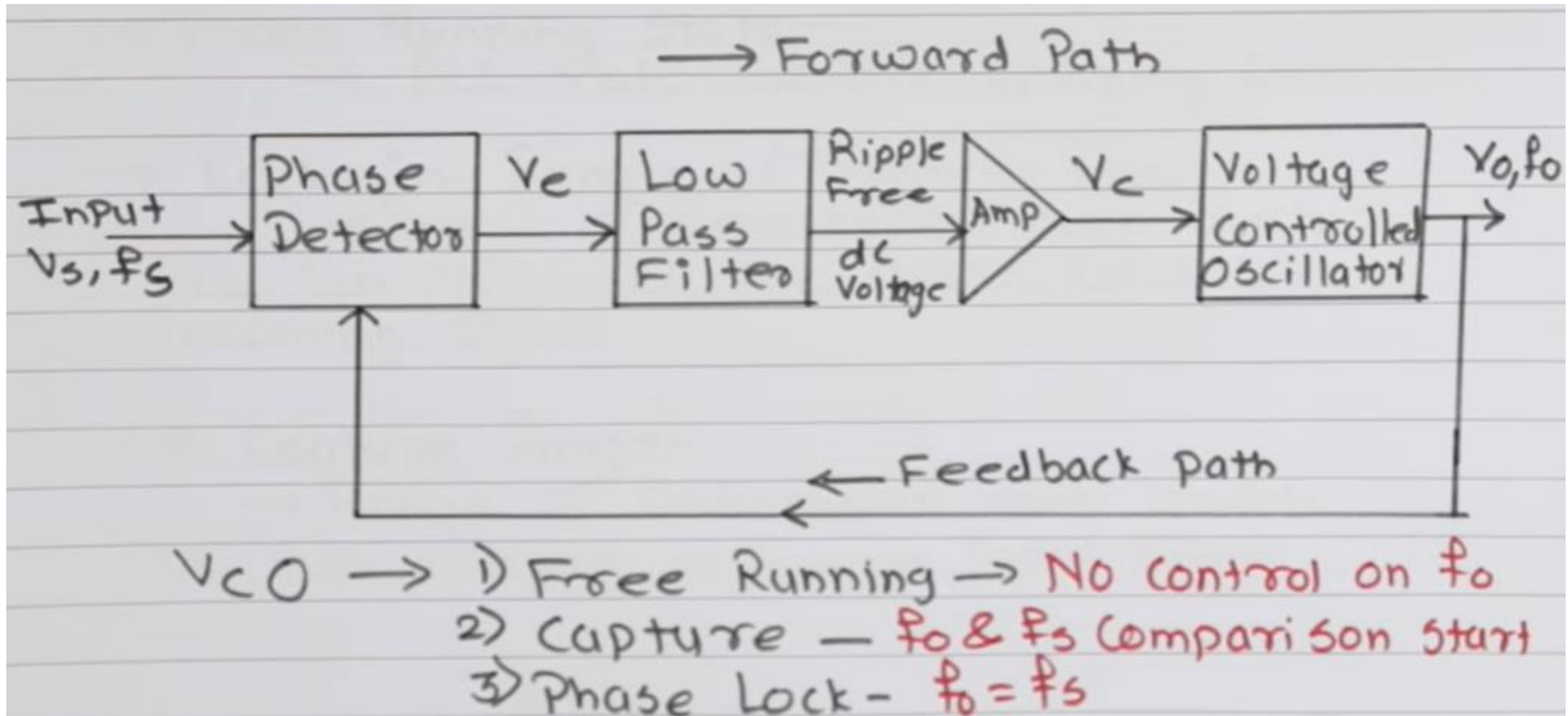
- Frequency Demodulation
- Clock Recovery
- Noise and Jitter Reduction
- Frequency Synthesizer
- Stable System Clock in Microprocessors



PHASE LOCKED LOOP (PLL)

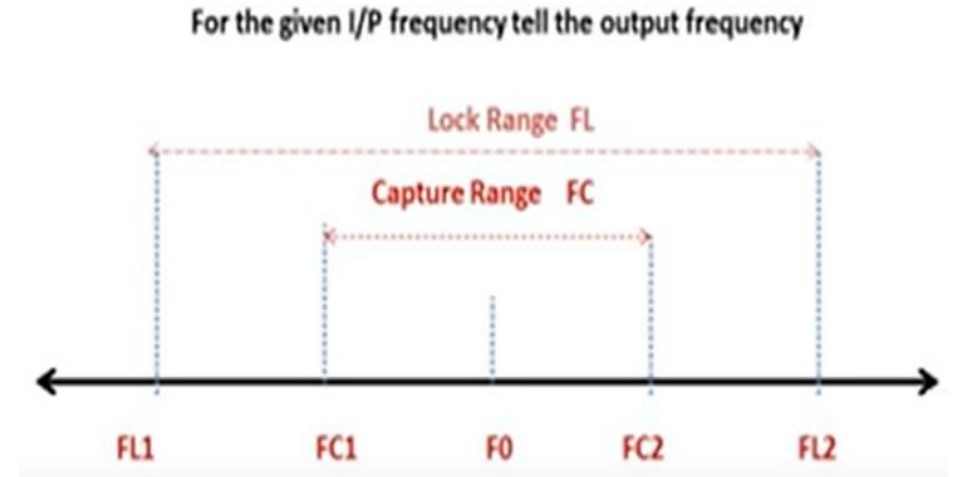


PLL Working Principal

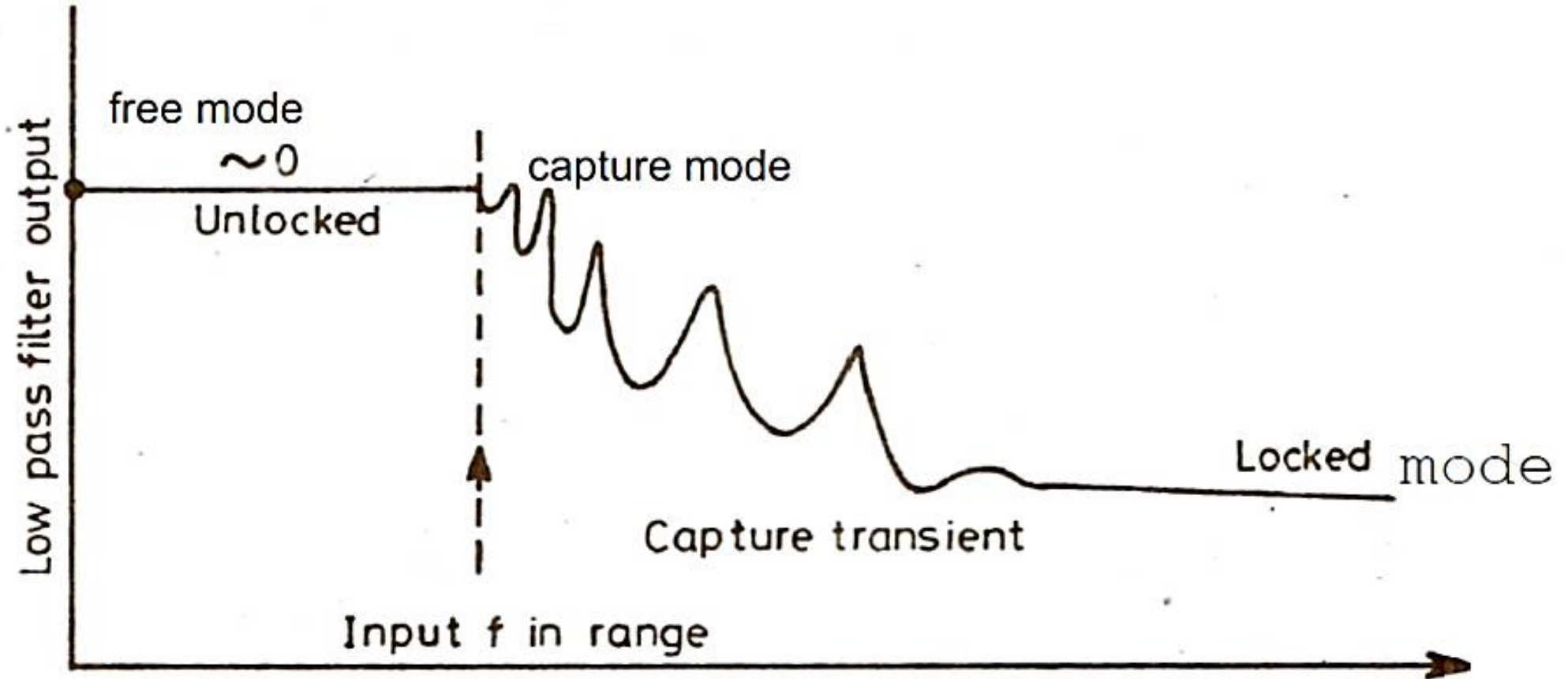


PLL Working Principal

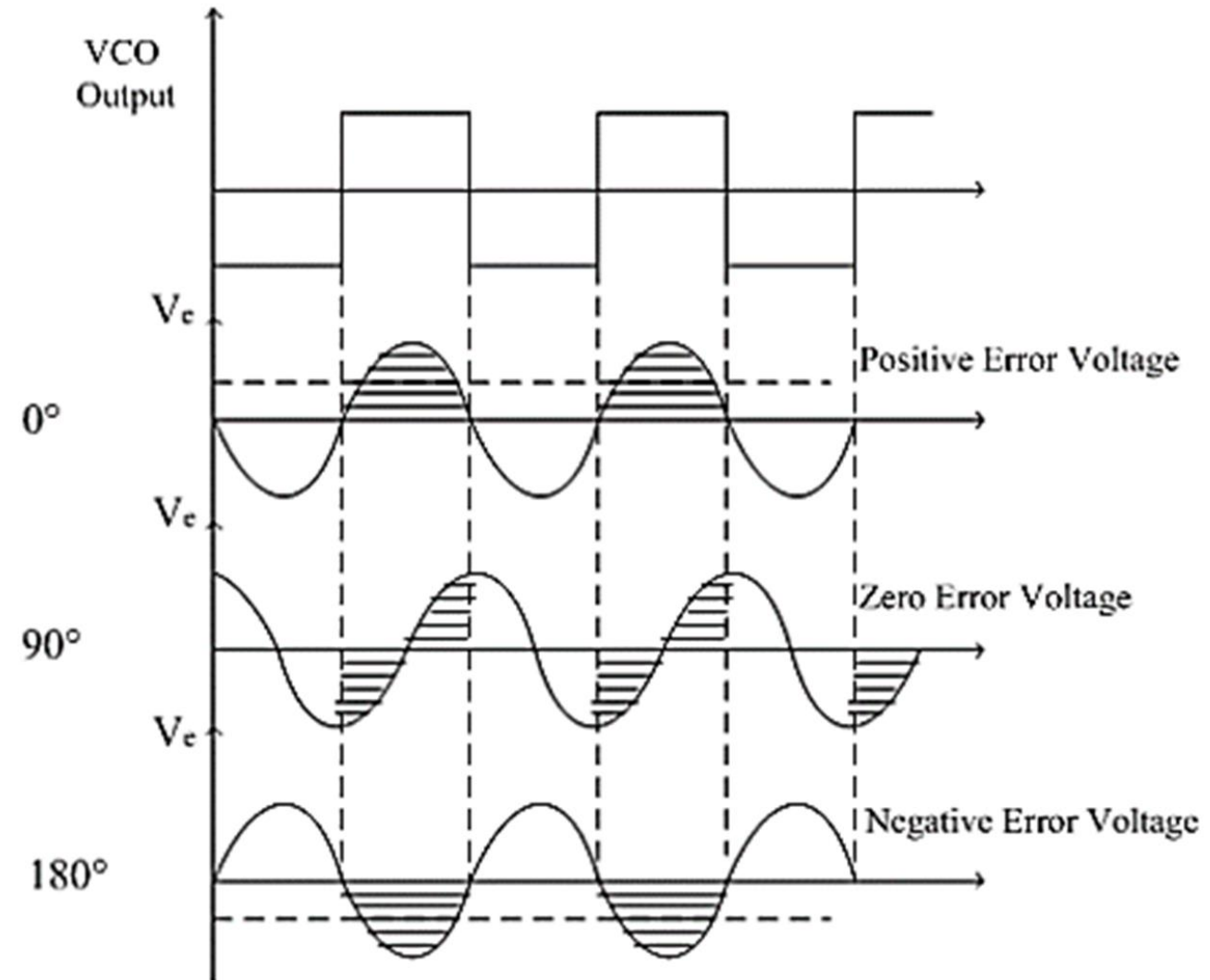
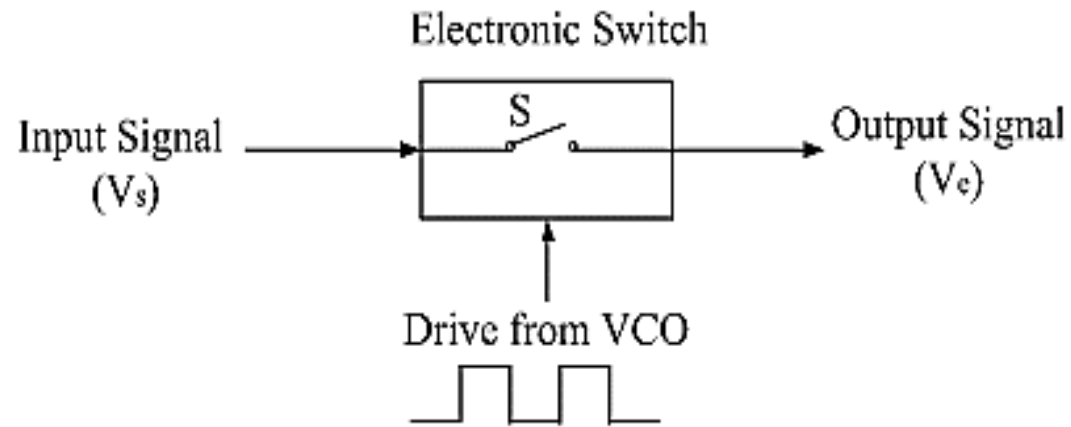
- **Lock range:** The range of frequencies over which the PLL maintains lock with the incoming signal is called the lock range of PLL.
- **Capture range:** The range of frequencies over which the PLL can acquire lock with an i/p signal is called the capture range.
- **PULL In Time:** The capture of an i/p signal does not take place as soon as the signal is applied, But it takes finite time. The total time taken by the PLL to establish lock is called pull-in time.



Capture transient



ANALOG PHASE DETECTOR



Analysis

❖ Phase detector is a multiplier which multiplies the input signal ($V_{in} = V_s \sin(2\pi f_{in}t)$) by the VCO signal ($V_{out} = V_o \sin(2\pi f_{out}t + \varphi)$)

❖ Therefore, Phase detector output,

$$V_e = kV_sV_o \sin(2\pi f_{in}t) \sin(2\pi f_{out}t + \varphi)$$

where $k \rightarrow$ phase comparator gain

$\varphi \rightarrow$ phase shift between the input signal and the VCO output.

$$\rightarrow V_e = \frac{kV_sV_o}{2} \left(\cos(2\pi f_{in}t - (2\pi f_{out}t + \varphi)) - \cos(2\pi f_{in}t + 2\pi f_{out}t + \varphi) \right)$$

❖ Above expression indicates that output contains a double frequency term and a DC component.

❖ Double frequency term is eliminated by the LPF and the DC signal is applied to the modulating input signal of the VCO.

❖ When at lock, $f_{in} = f_{out}$,

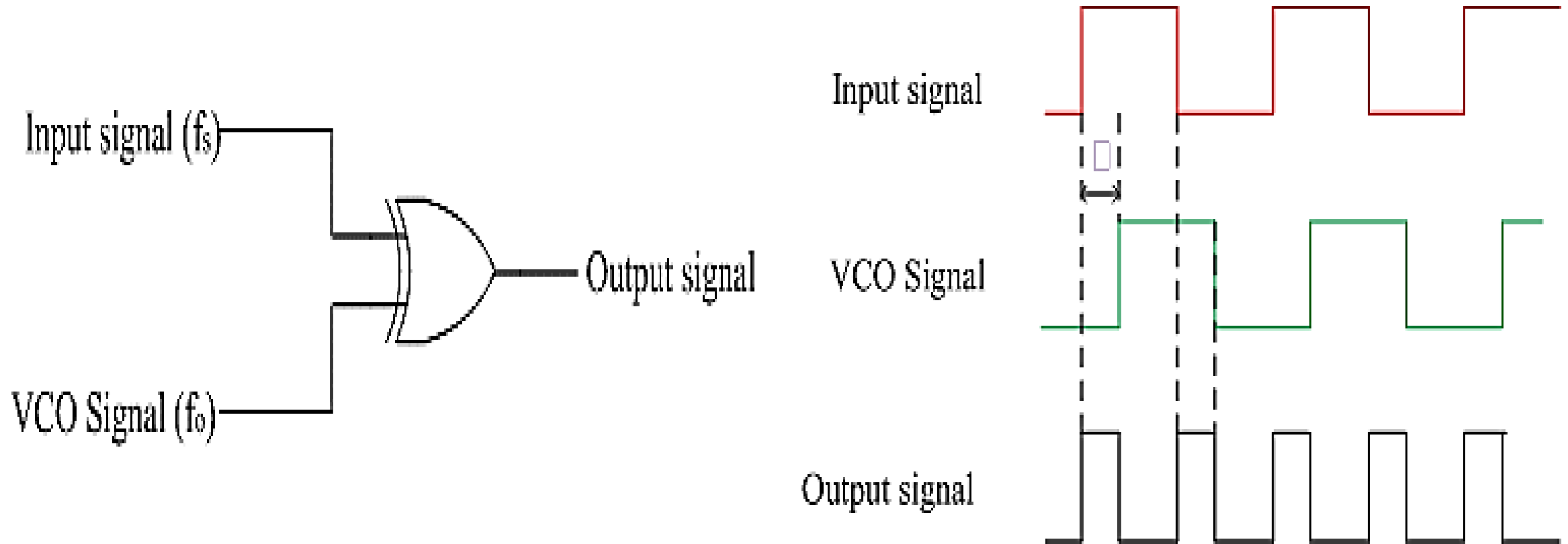
$$\rightarrow V_e = \frac{kV_sV_o}{2} (\cos(-\varphi) - \cos(2\pi * 2f_{out}t + \varphi))$$

❖ For a perfect locked state, the phase shift should be 90° , in order to get zero error signal, i.e. $V_e = 0$.

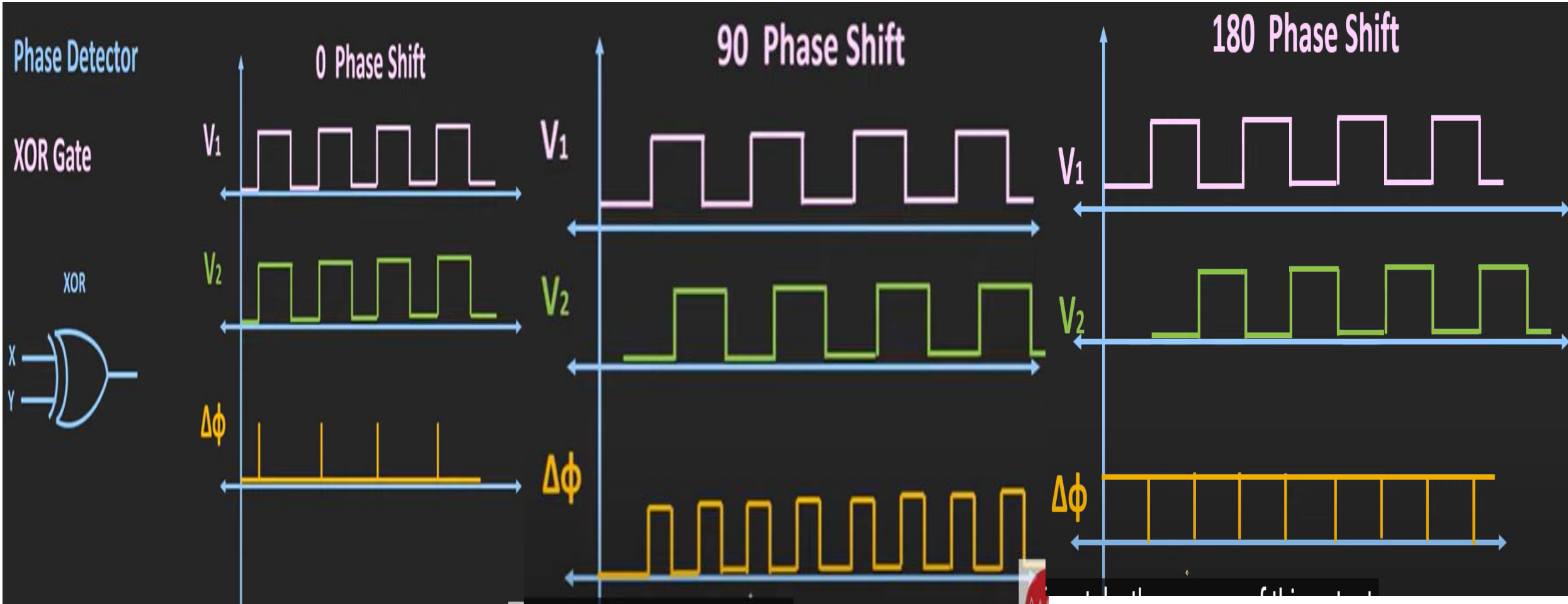
Drawbacks of Switch Type Phase Detector

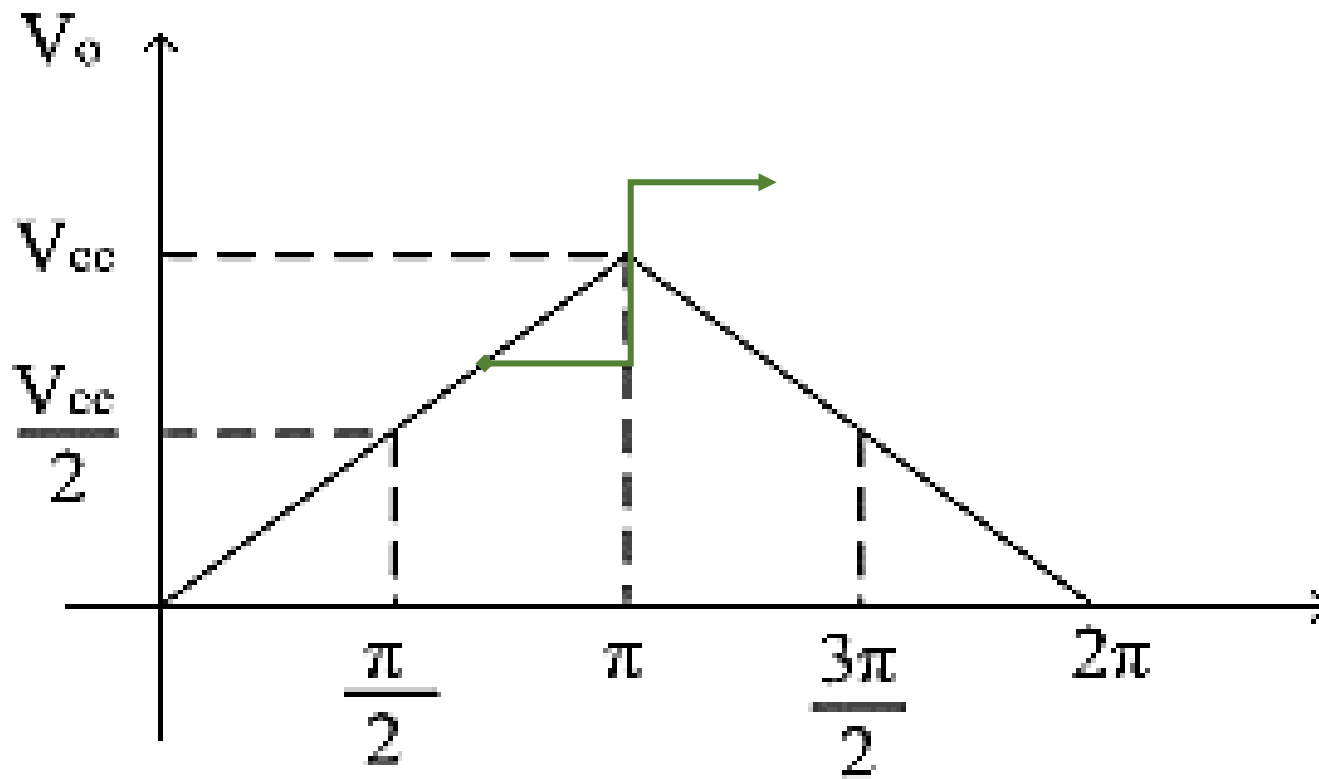
1. Output voltage V_e is proportional to the input signal amplitude making the phase detector gain and the loop gain dependent on the input signal amplitude.
 2. Output is proportional to $\cos \varphi$ and not φ making it non-linear.
- Both drawbacks can be eliminated by limiting the amplitude of the input signal i.e. converting the input to a constant amplitude square wave.

DIGITAL Phase Detector



DIGITAL Phase Detector





DC Output voltage V_o vs phase difference ϕ curve

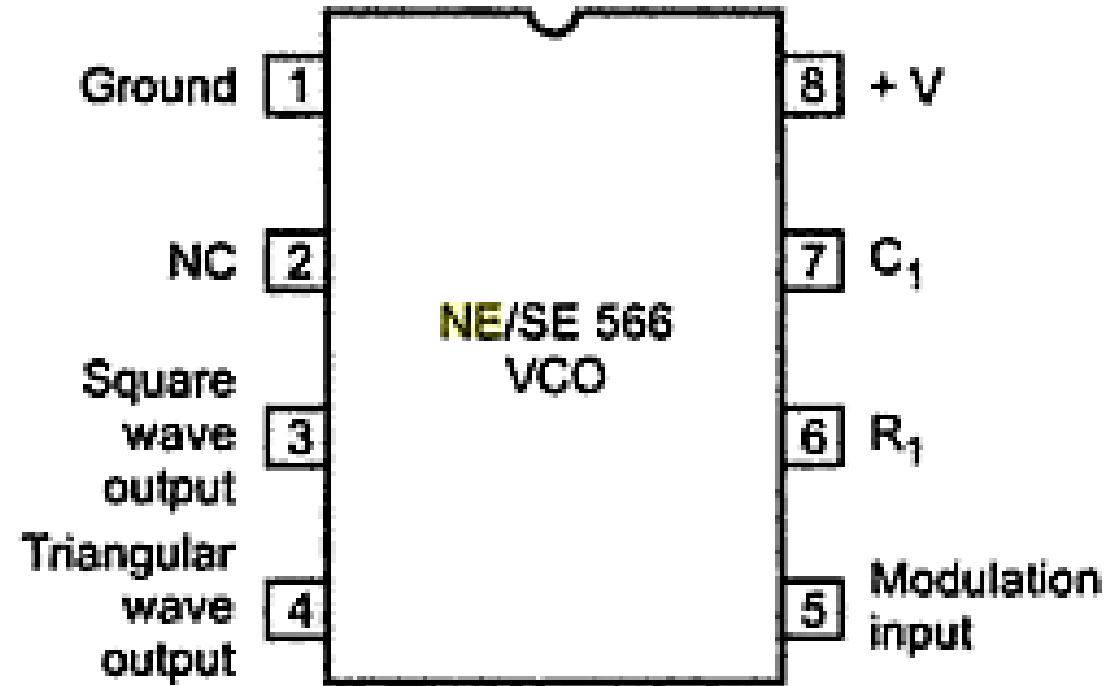
LIC: LECTURE

PHASE LOCKED LOOP (PLL)

✓ PLL Circuit

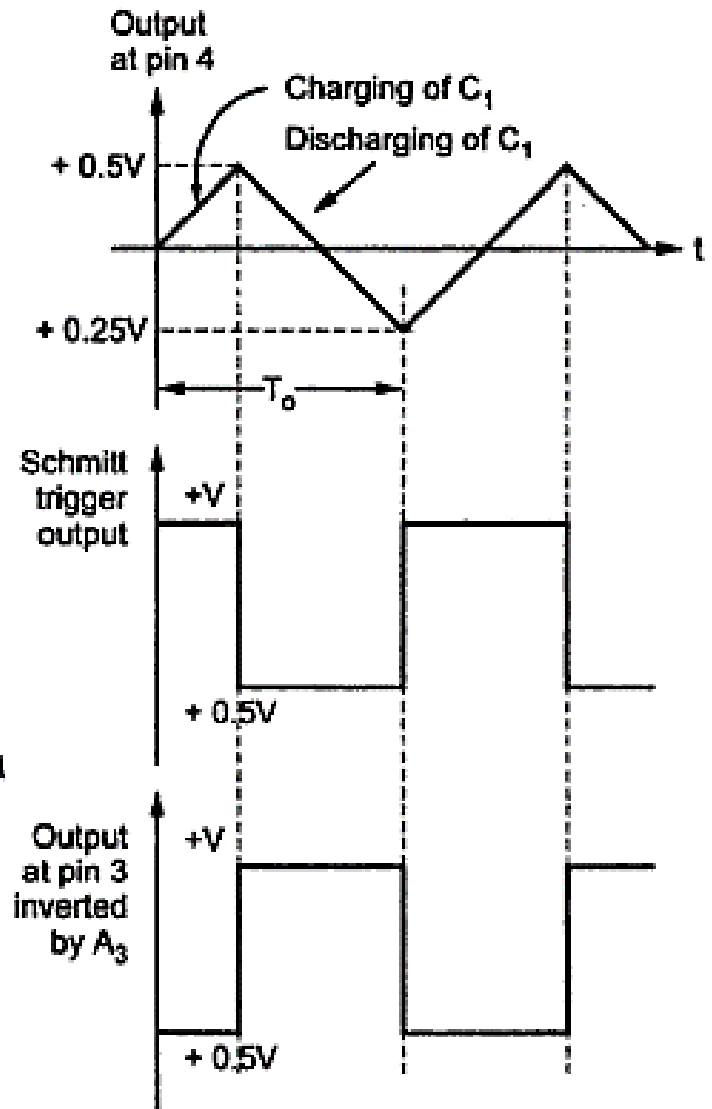
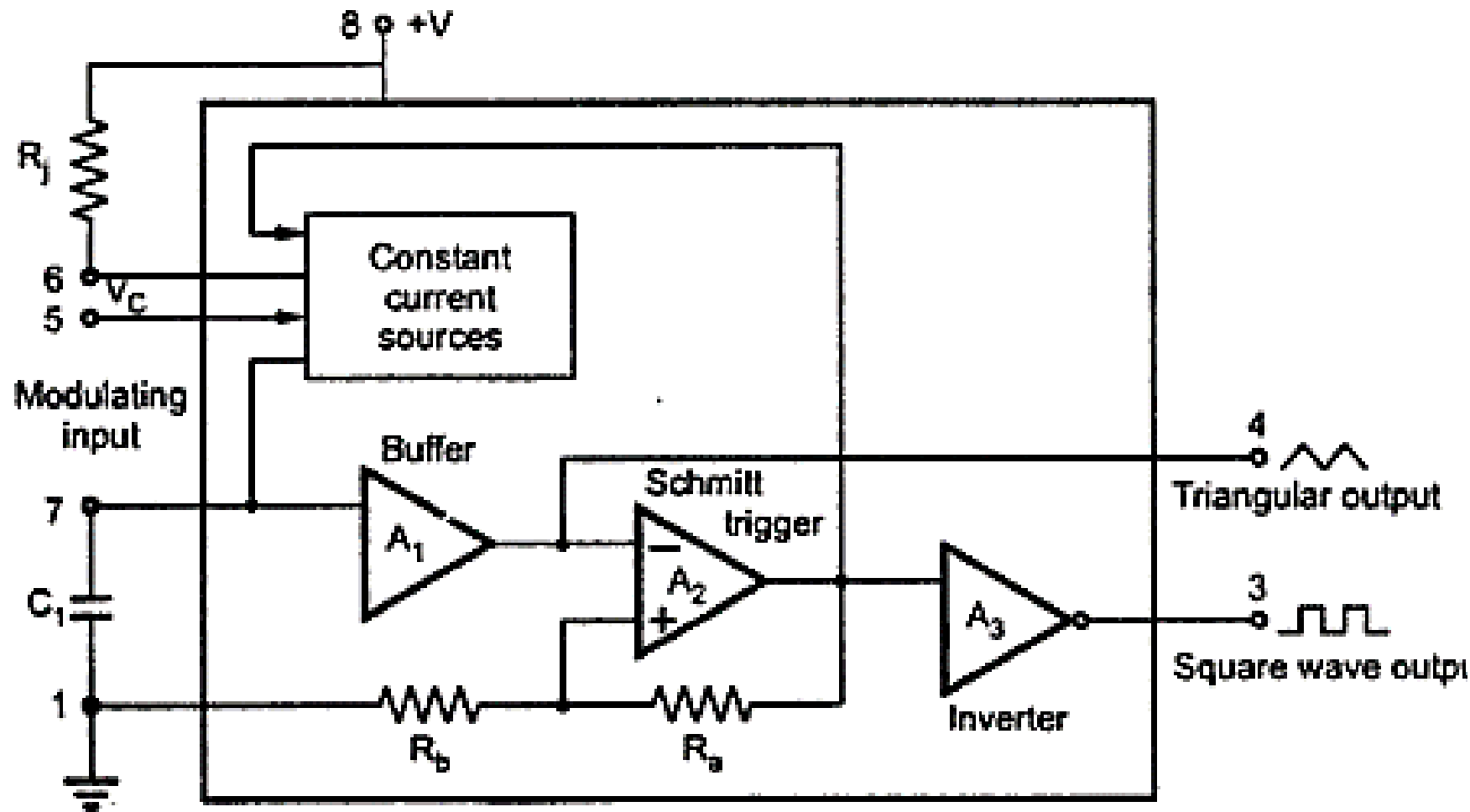
- ✓ Need and Requirements
- ✓ Circuit
- ✓ Working Principal
- ✓ Phase Detector Design
- Voltage Controlled Oscillator
- Application as Frequency Synthesizer ($f \cdot N$ or f/N)

VOLTAGE Controlled Oscillator (VCO)



Pin Configuration

BLOCK DIAGRAM



Output Frequency Calculation

- Total voltage on the capacitor changes from $0.25 V_{CC}$ to $0.5 V_{CC}$.

$$\therefore \Delta V = 0.25 V_{CC}$$

- Capacitor charges with a constant current source.

$$\frac{\Delta V}{\Delta t} = \frac{i}{C_1}$$
$$\Delta t = \frac{0.25 V_{CC} C_1}{i}$$

- Time period of triangular waveform = $2\Delta t$

- Frequency, f_o is

$$f_o = \frac{1}{T}$$

- But,

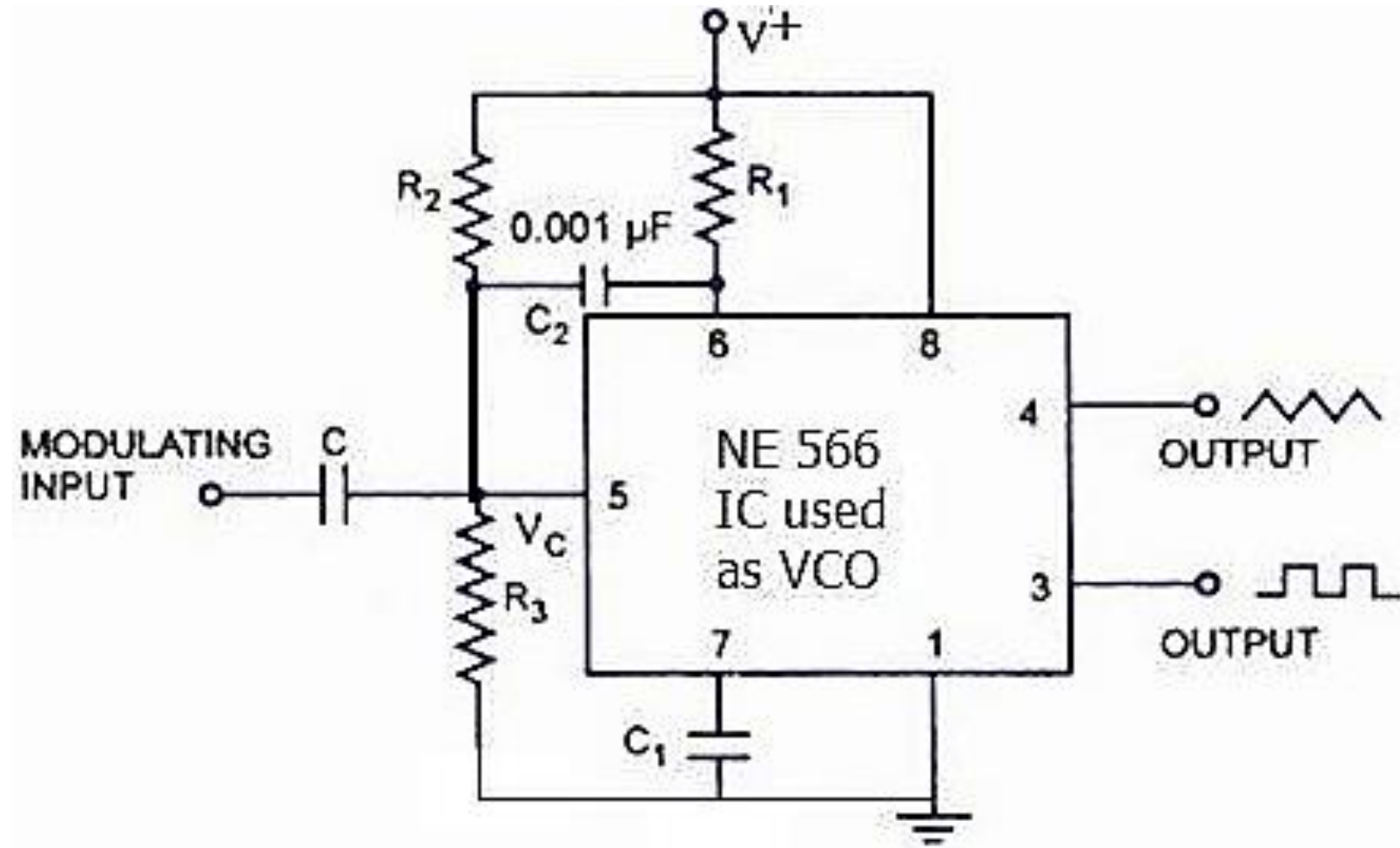
$$i = \frac{V_{CC} - V_C}{R_1}$$

- where V_C = voltage at pin 5.

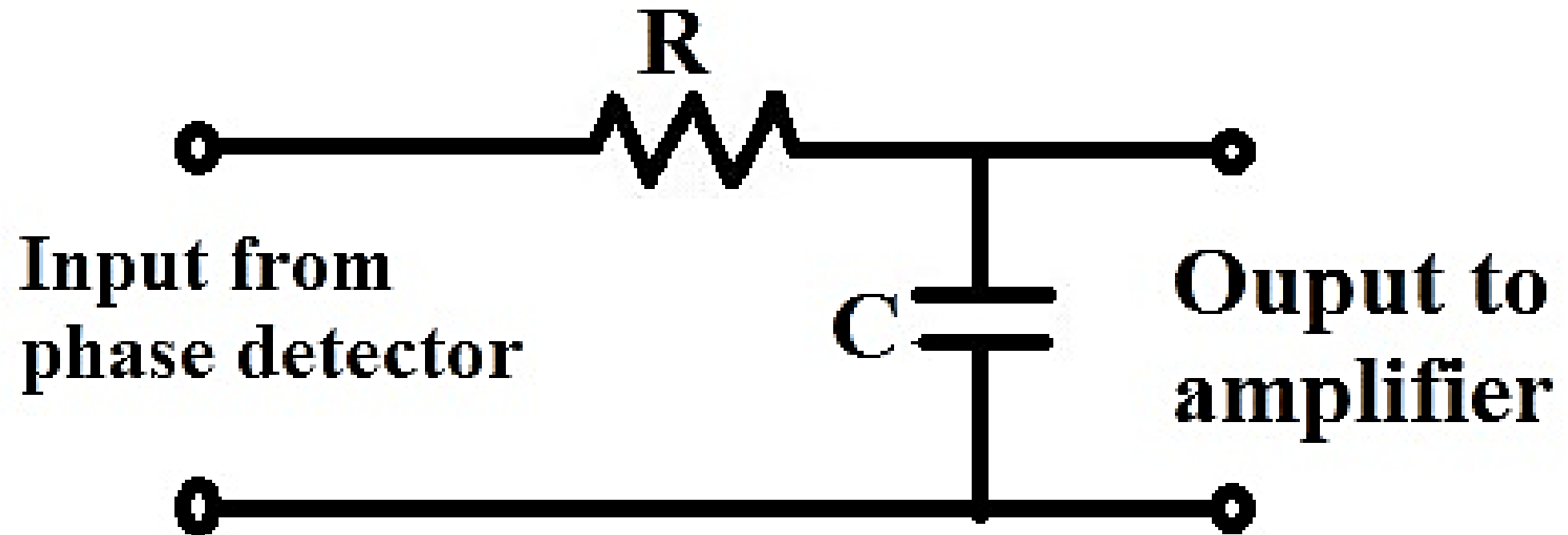
$$f_o = \frac{2(V_{CC} - V_C)}{C_1 R_1 V_{CC}}$$

Outcomes

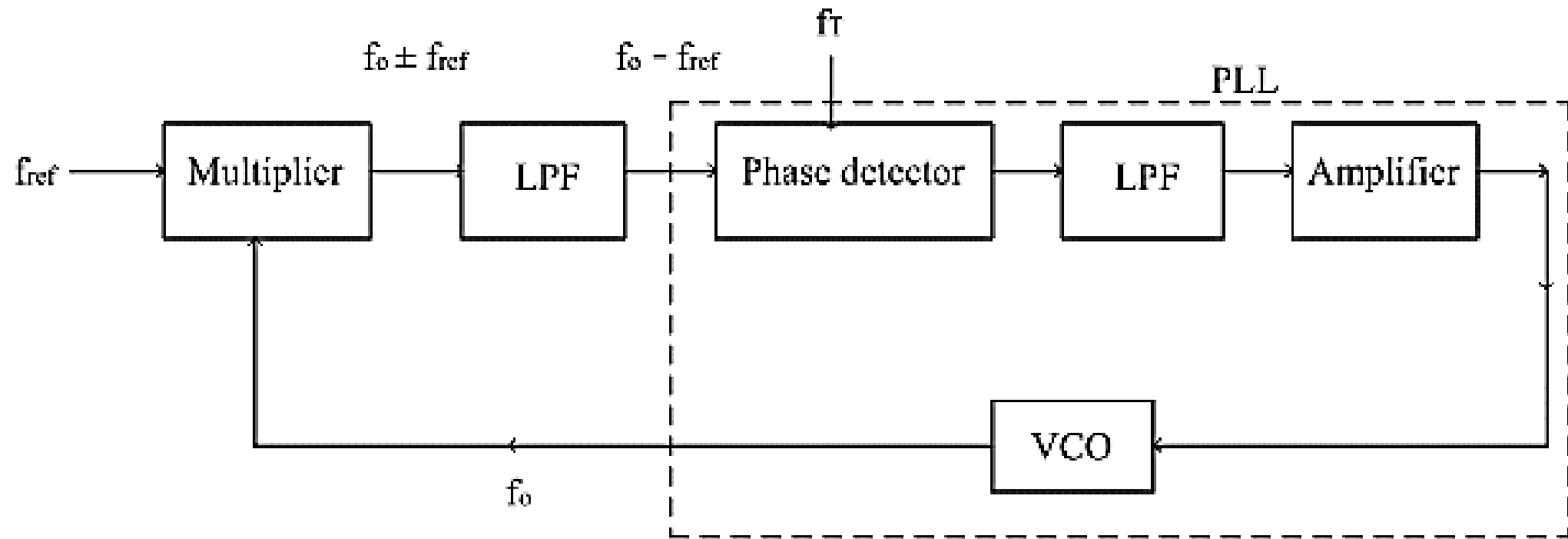
- Output freq. of VCO can be changed by –
 - a) R_1
 - b) C_1
 - c) Modulating input V_C
- V_C can be varied by connecting a $R_2 - R_3$ circuit as shown in the circuit.



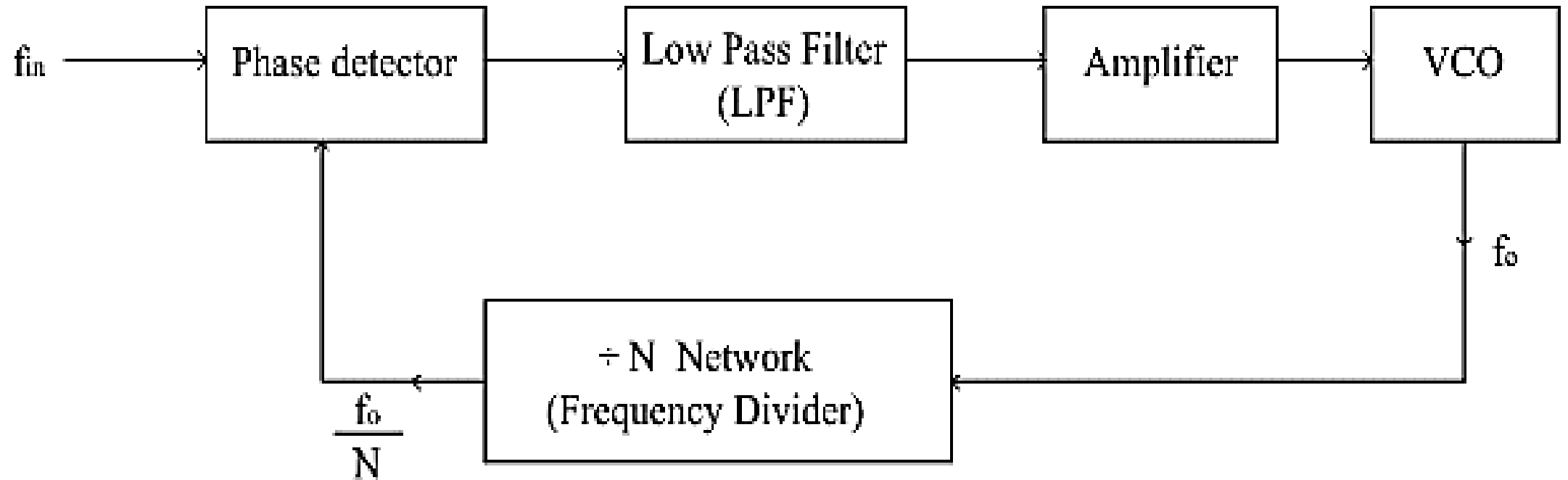
Low Pass Filter



Frequency Translation

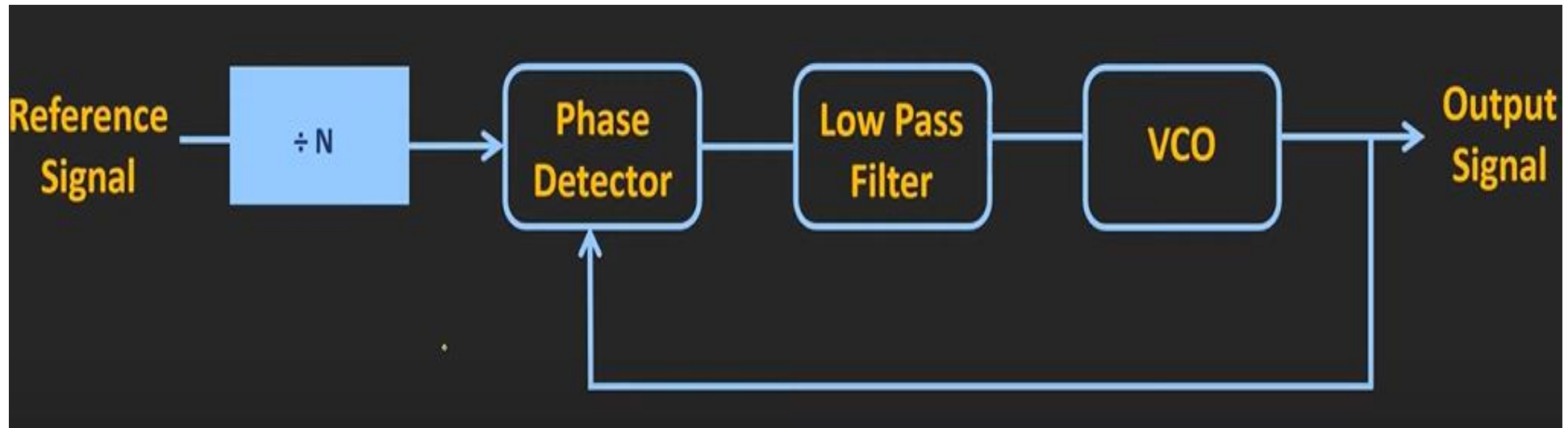
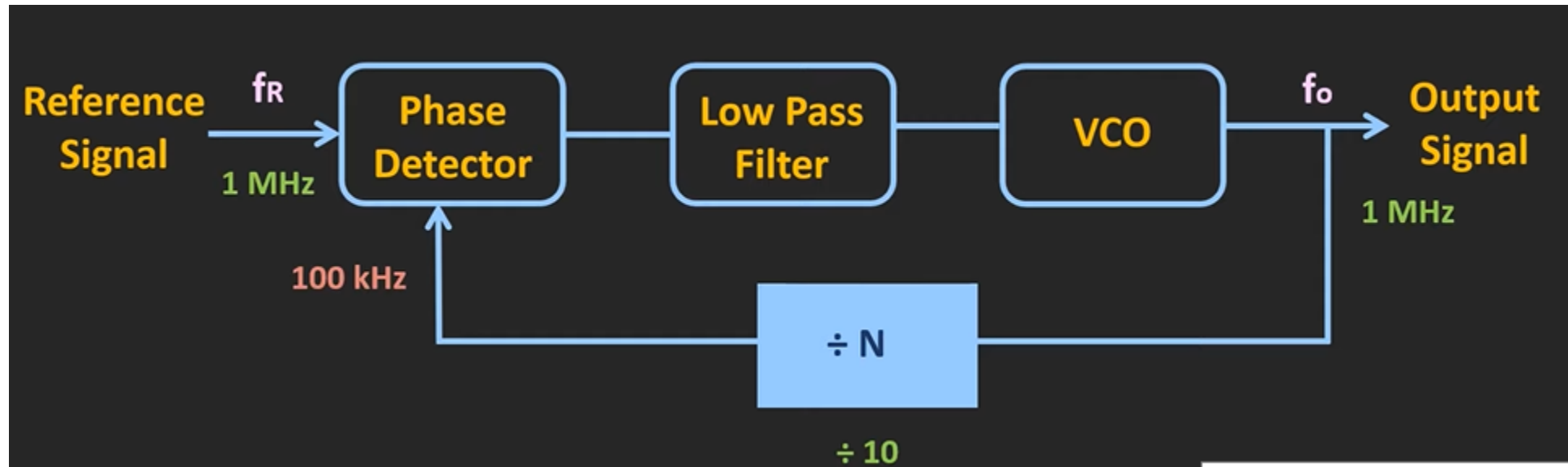


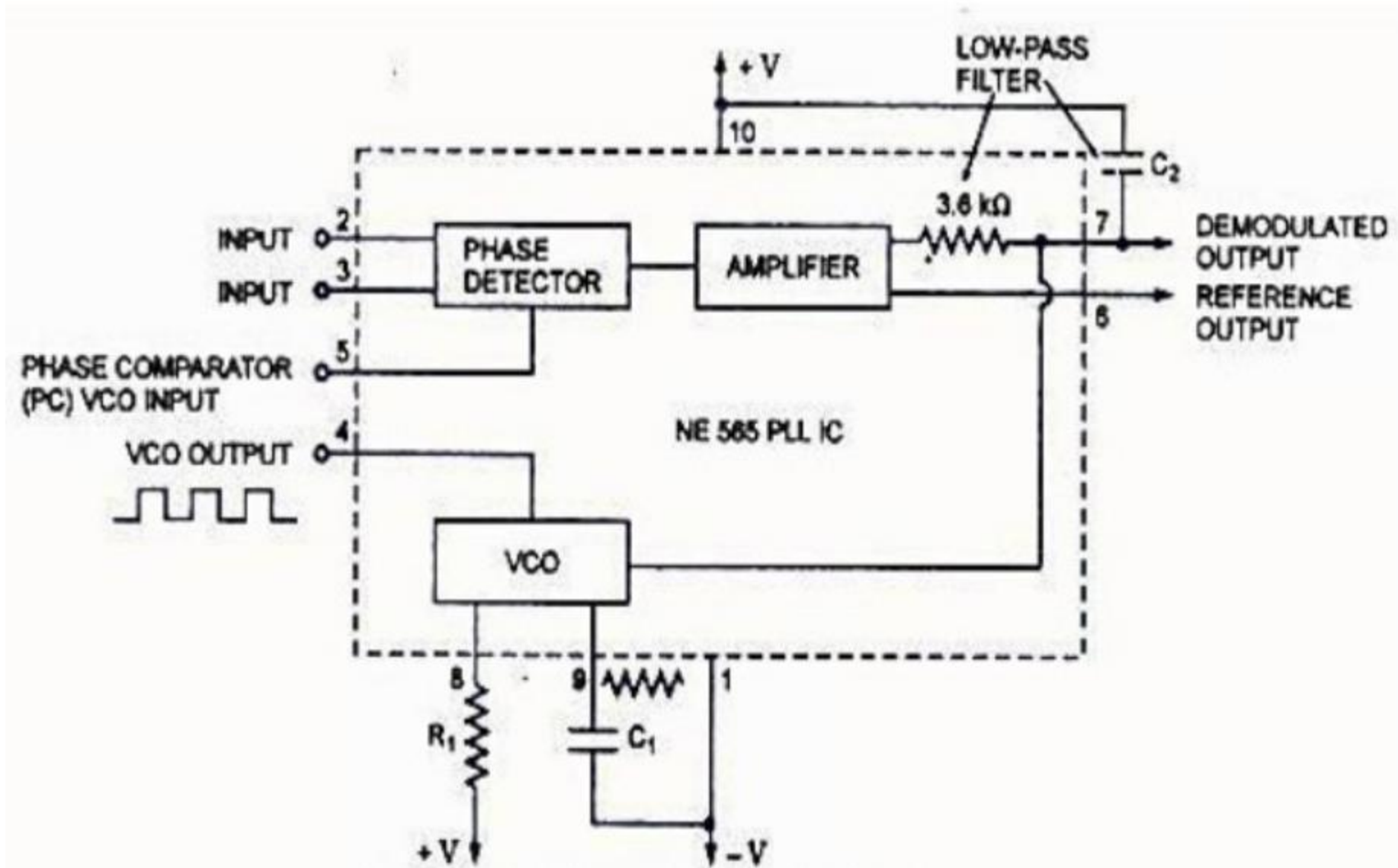
Frequency multiplier/ divider



FREQUENCY MULTIPLIER

Frequency Synthesizer





Monolithic Phase Locked loop (NE/SE 565)

