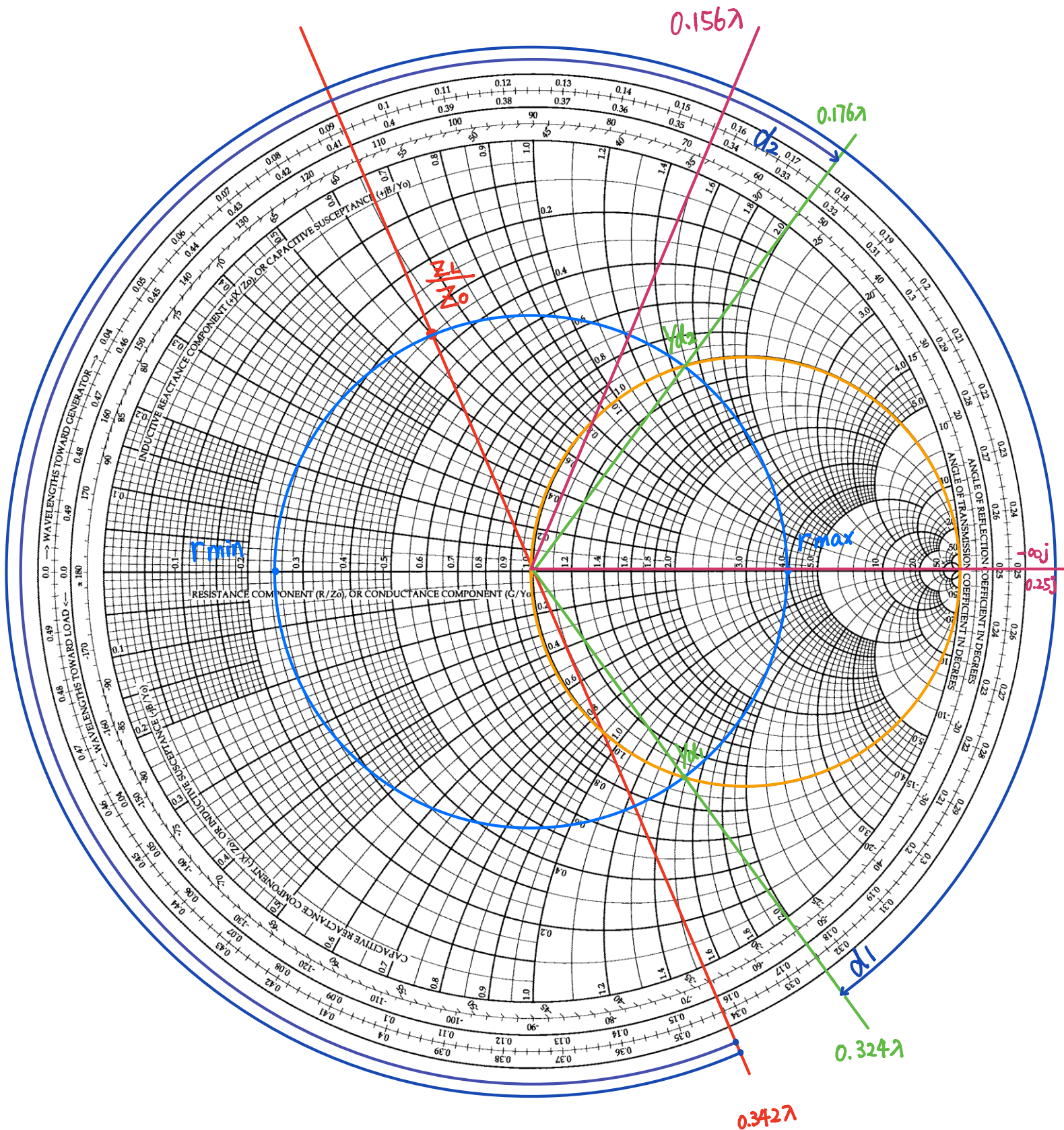


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Smith impedance chart



(a) The normalised impedance for load is :

$$\text{Normalised impedance} = \frac{Z_L}{Z_0} = \frac{17.5 + j30\Omega}{50\Omega} = 0.35 + j0.6$$

The  $0.35 + j0.6$  is plotted on the Smith Chart.

(b) The voltage standing wave ratio (VSWR) is equal to 4, draw this circle on the Smith chart. The normalised admittance  $y_L$  is obtained by rotating  $\frac{Z_L}{Z_0}$  by  $180^\circ$

Then plotting the matched condition circle ( $G=1$ ).

Rotating  $y_L$  with a distance  $d$  to intercept with  $G=1$  circle,

There will be two intercepts,  $y_{d1}$  and  $y_{d2}$

$$\begin{aligned}\text{For } d_1: \quad d_1 &= 0.5\lambda - 0.342\lambda + 0.324\lambda \\ &= 0.482\lambda\end{aligned}$$

$$\begin{aligned}\text{For } d_2: \quad d_2 &= 0.5\lambda - 0.342\lambda + 0.176\lambda \\ &= 0.334\lambda\end{aligned}$$

$$\text{Since } \lambda = \frac{c}{f} = \frac{3 \times 10^8 \text{ ms}^{-1}}{1.5 \times 10^9 \text{ Hz}} = 0.2 \text{ m} = 20 \text{ cm}$$

$$d_1 = 0.482 \times 20 \text{ cm} = 9.64 \text{ cm}$$

$$d_2 = 0.334 \times 20 \text{ cm} = 6.68 \text{ cm}$$

Since  $d_1 = 9.64 \text{ cm}$  which is greater than  $8 \text{ cm}$ , the  $d$  should be  $9.64 \text{ cm}$ .

Therefore, the  $y_d = 1 - j1.5$ , and  $d = 9.64 \text{ cm}$ .

(c) 
$$Y_{in} = Y_s + Y_d$$

Since  $Y_{in} = 1$ ,  $Y_d = 1 - j1.5$

$$Y_s = Y_{in} - Y_d$$

$$= 1 - (1 - j1.5)$$

$$= j1.5$$

The  $y_s$  is moving from the end of stub to  $j1.5$ .

$$\text{The required stub} = 0.156\lambda + 0.25\lambda = 0.406\lambda$$

$$\text{The length} = 0.406 \times 20 \text{ cm} = 8.12 \text{ cm}$$