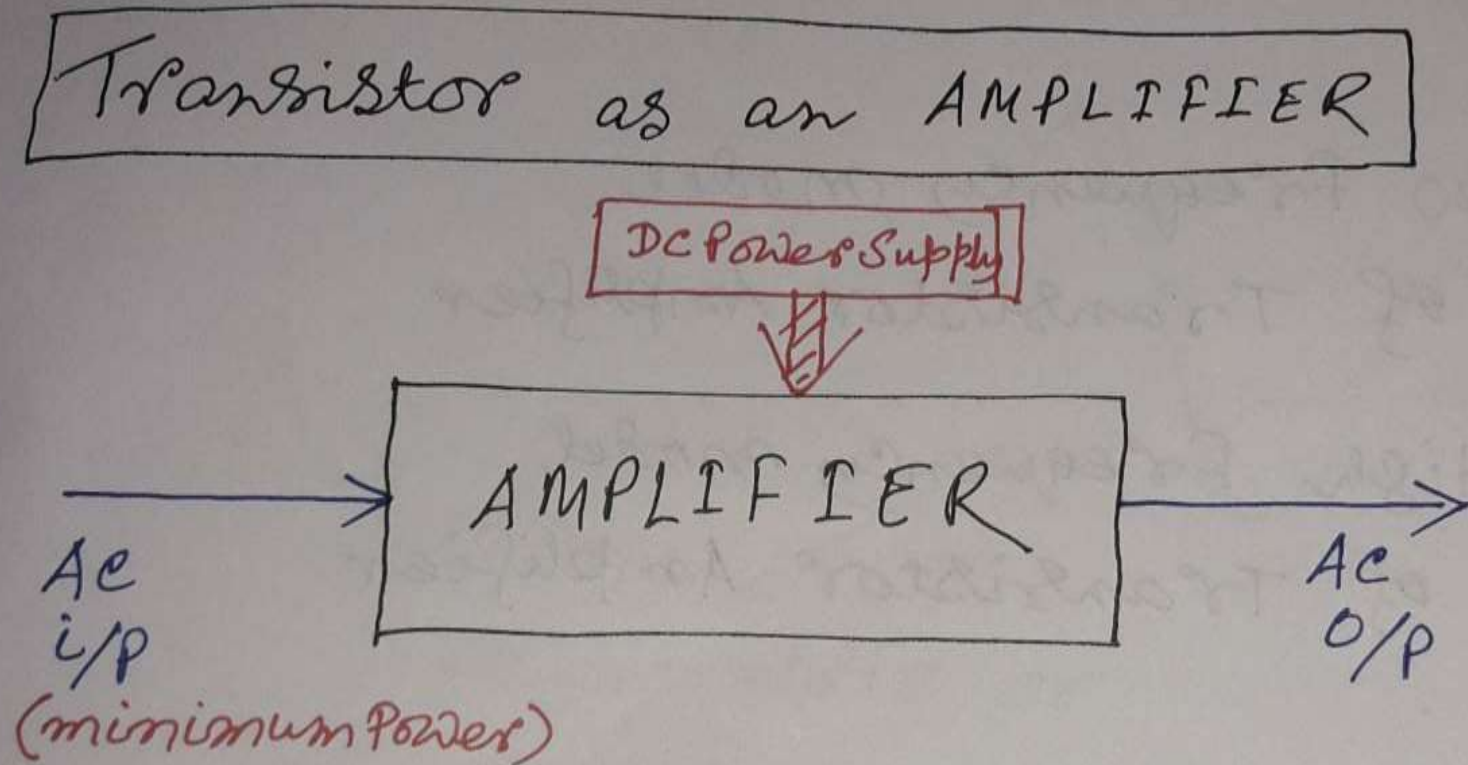
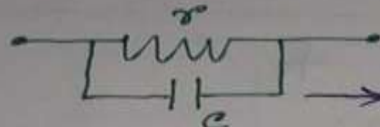
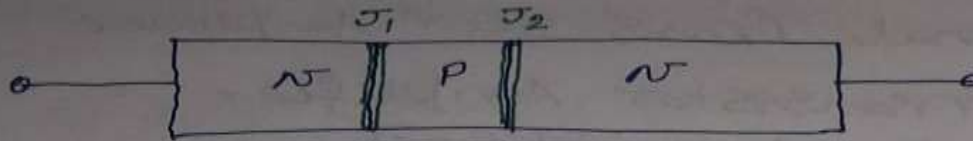


# Transistor Amplifier

# Transistor Amplifier



# Transistor Amplifier



Junction Capacitance

$$X_c = \frac{1}{2\pi f c}$$

At low frequency  
 $X_c \rightarrow \text{high}$   
(so may be neglected)

At high frequency  
 $X_c \rightarrow \text{low}$   
(cannot be neglected)

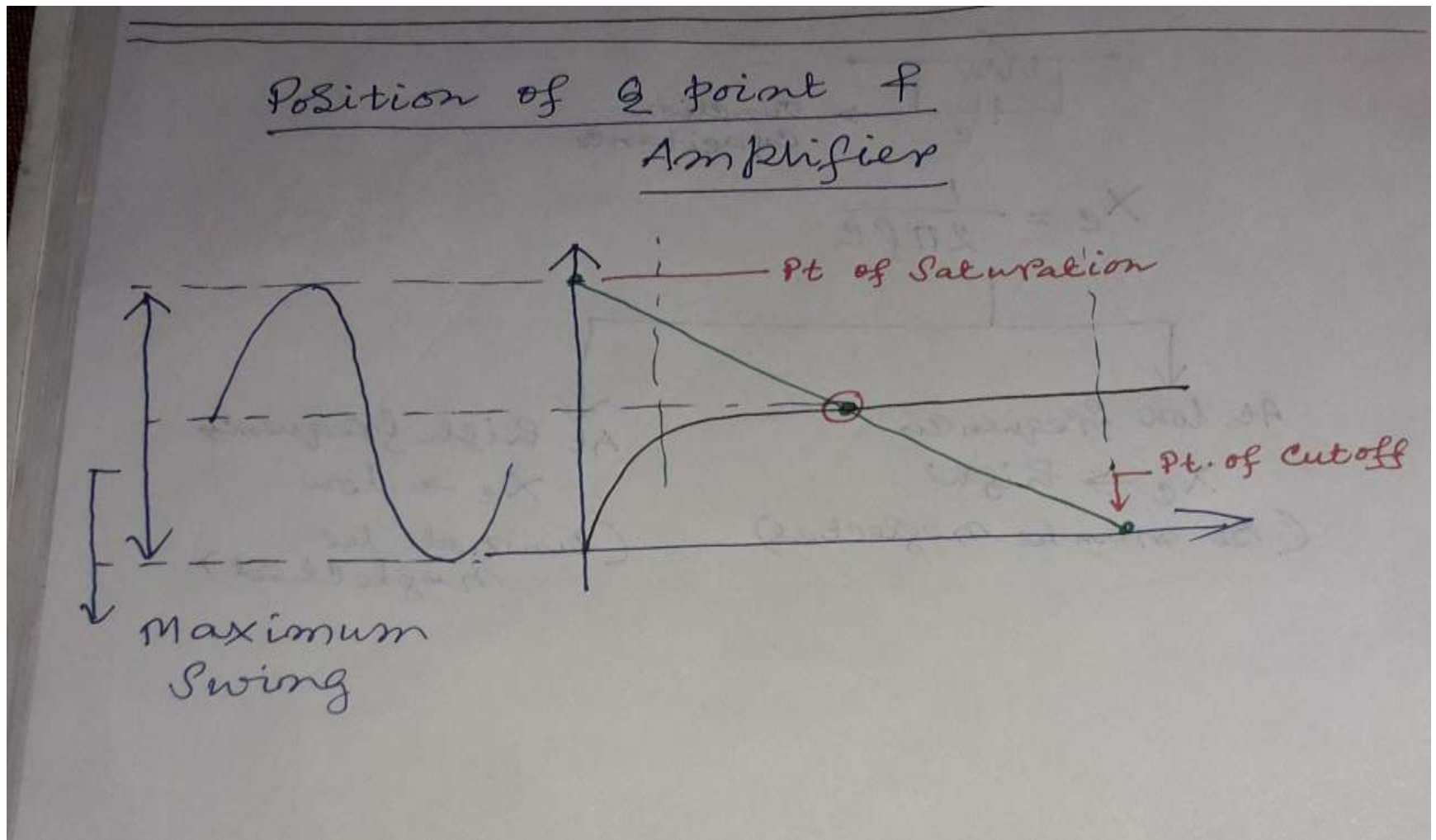
# Transistor Amplifier

- Low Frequency model of Transistor Amplifier
- High Frequency model of Transistor Amplifier

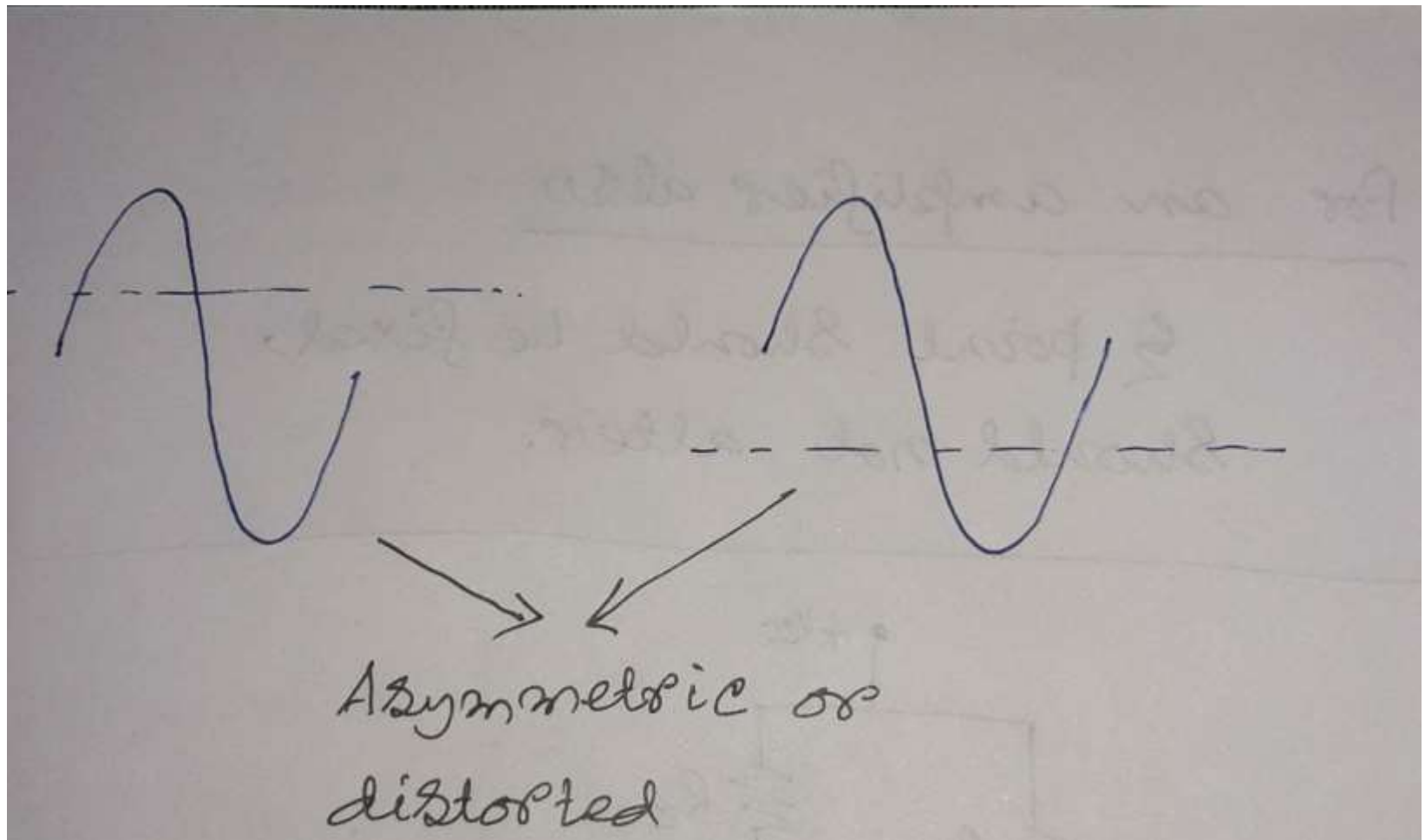
Another Consideration.

- Small Signal Transistor Amplifier
- Power Transistor Amplifier  
[large signal amplifiers]

# Transistor Amplifier



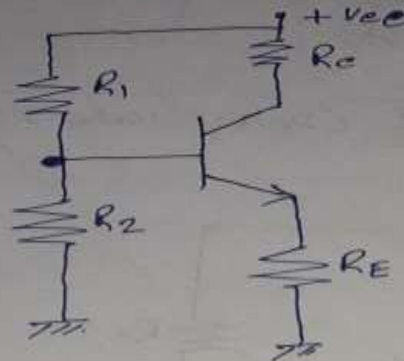
# Transistor Amplifier



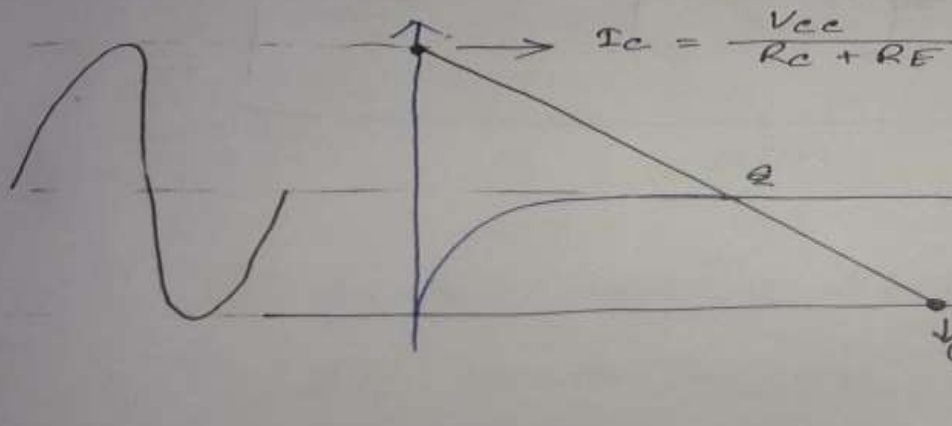
# Transistor Amplifier

To get an symmetrical.

The load line should pass through the middle.



Condn for maxm.  
symmetrical  
swing.



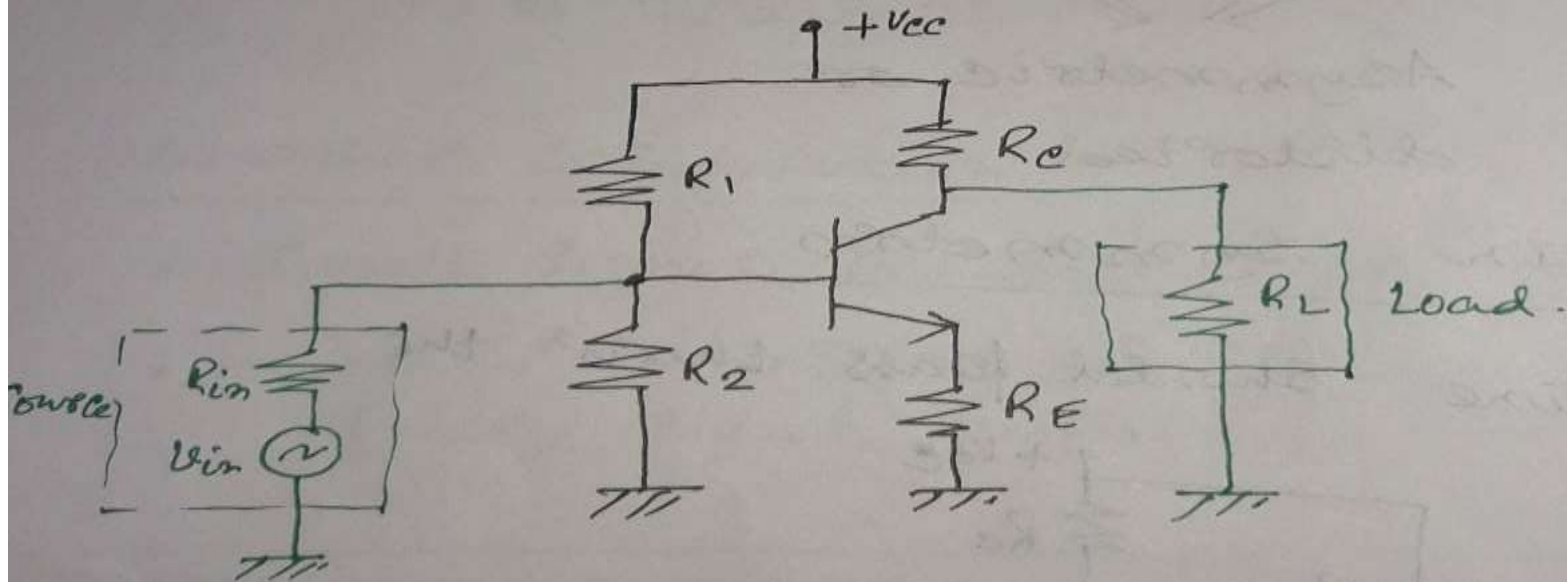
$$I_{CQ} = \frac{V_{CC}}{2(R_c + R_E)}$$
$$V_{CEQ} = \frac{V_{CC}}{2}$$



# Transistor Amplifier

For an amplifier also

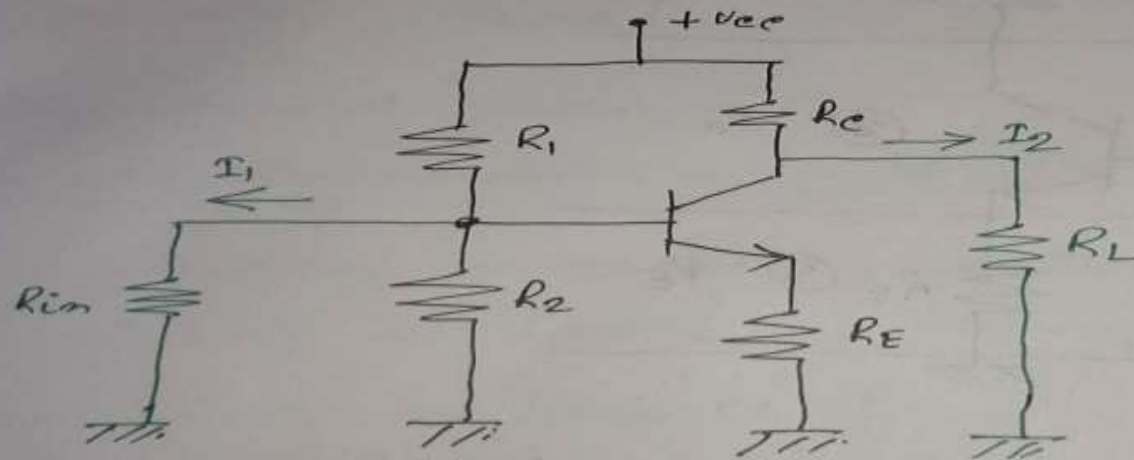
Q point should be fixed,  
should not alter.





# Transistor Amplifier

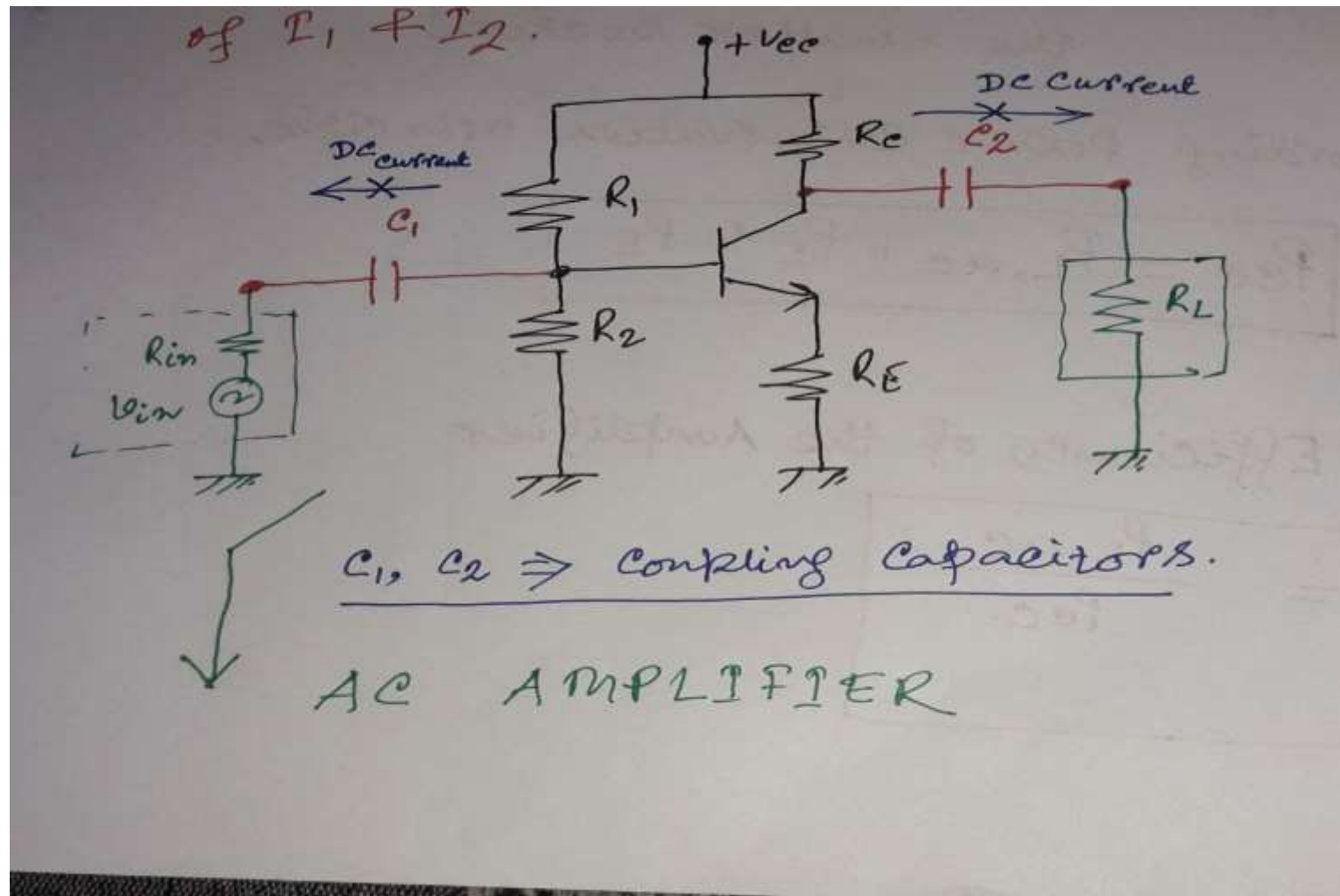
DC Equivalent circuit.



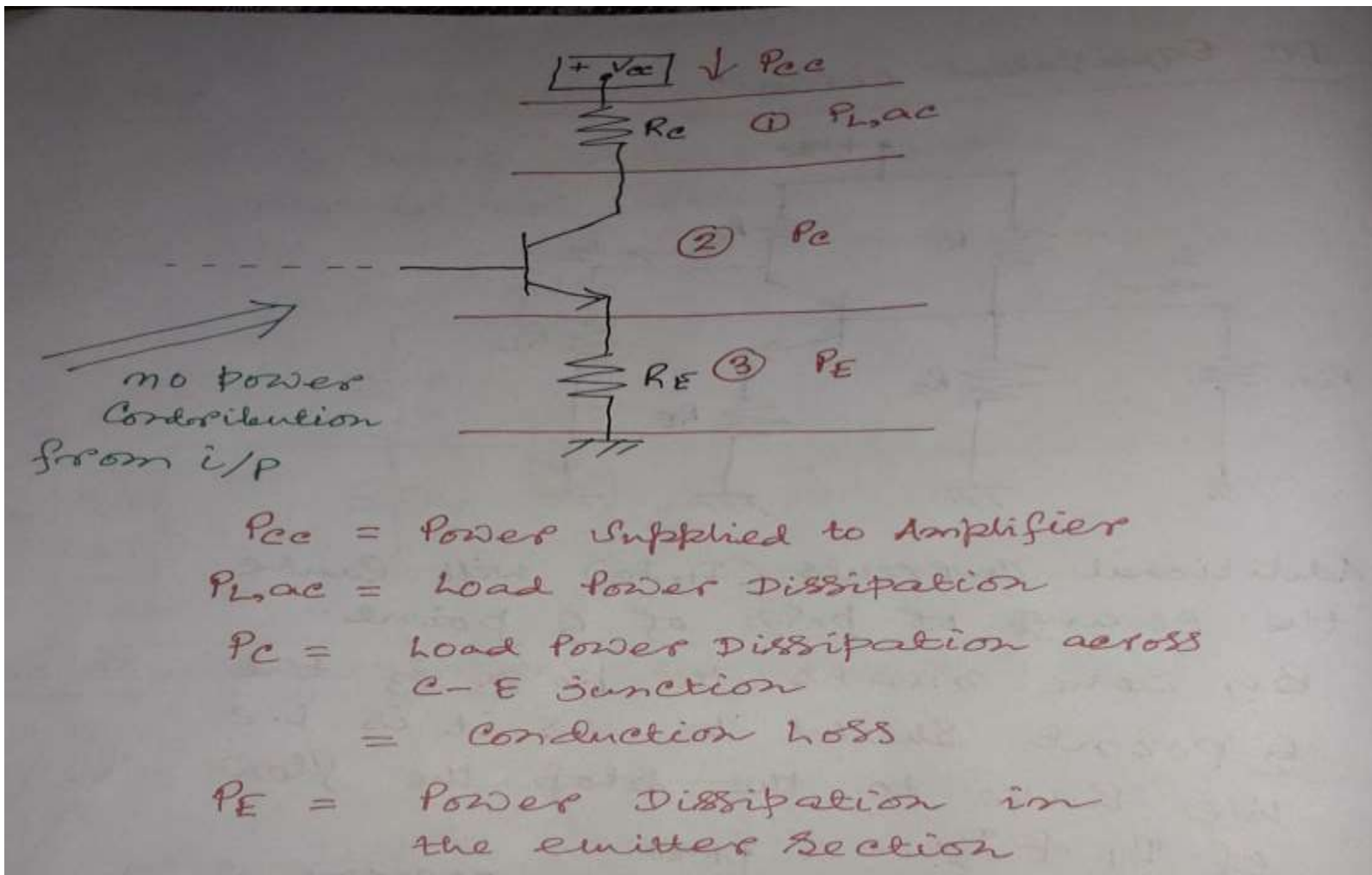
Additional currents ( $I_1, I_2$ ) will cause the change of posn. of Q point.

By some means the posn. of the Q point should be as it is i.e. we have to stop the flow of  $I_1$  &  $I_2$ .

# Transistor Amplifier



# Transistor Amplifier



# Transistor Amplifier

According to power conservation principle,

$$P_{cc} = P_{L,ac} + P_c + P_E$$

$\eta$  = Efficiency of the Amplifier

$$\eta = \frac{P_{L,ac}}{P_{cc}}$$

# Transistor Amplifier

As  $P_{CC}$  is fixed,  $[P_{CC} = V_{CC} \cdot I_{CQ}]$

So  $\eta \uparrow$   $P_{L,ac} \uparrow$

We cannot alter  $P_C$ .

So recommendation is to reduce  $P_E$ .

But, according to stability factor analysis,

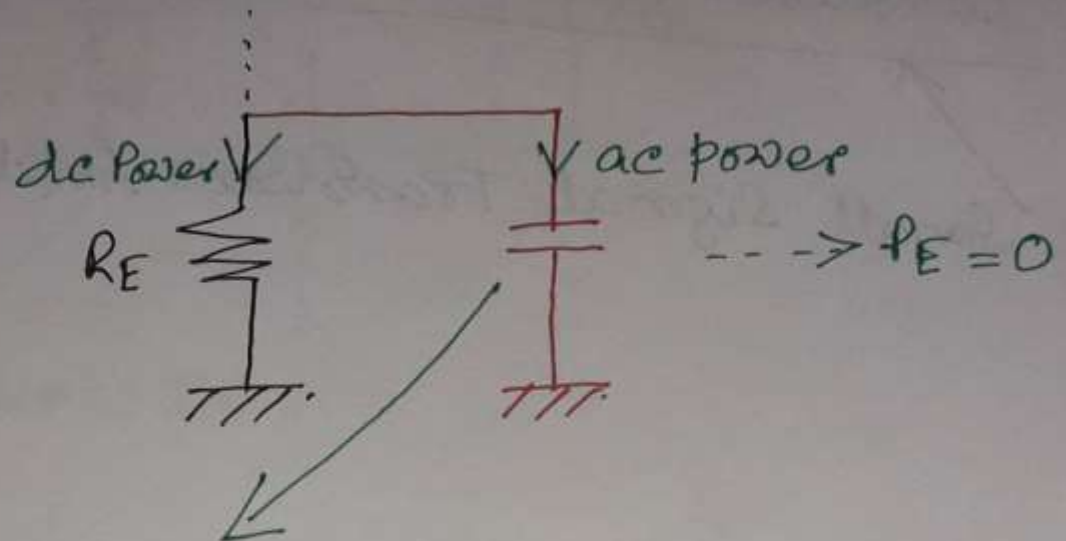
$R_E$  should be large  $[S_V = -\frac{1}{R_E}]$

then how to reduce  $P_E$

↓  
ac power dissipation  
in the emitter section.

# Transistor Amplifier

Solution.

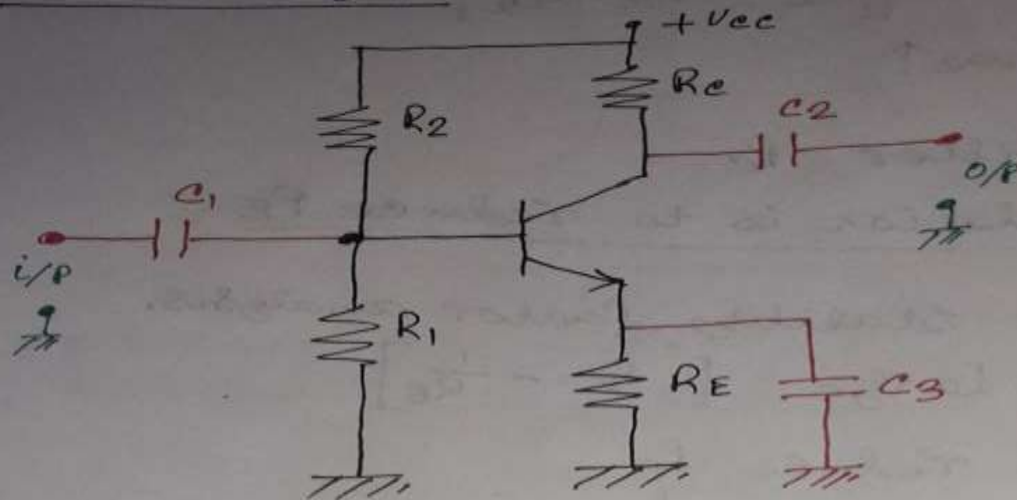


Bypass Capacitor



# Transistor Amplifier

Final Design



$C_1, C_2 \Rightarrow$  Coupling Capacitor

$C_3 \Rightarrow$  Bypass Capacitor

R-C Coupled Transistor Amplifier

Small Signal Transistor Amplifier



# Transistor Amplifier

## Low Frequency Model

Objective (1) To find out Gain

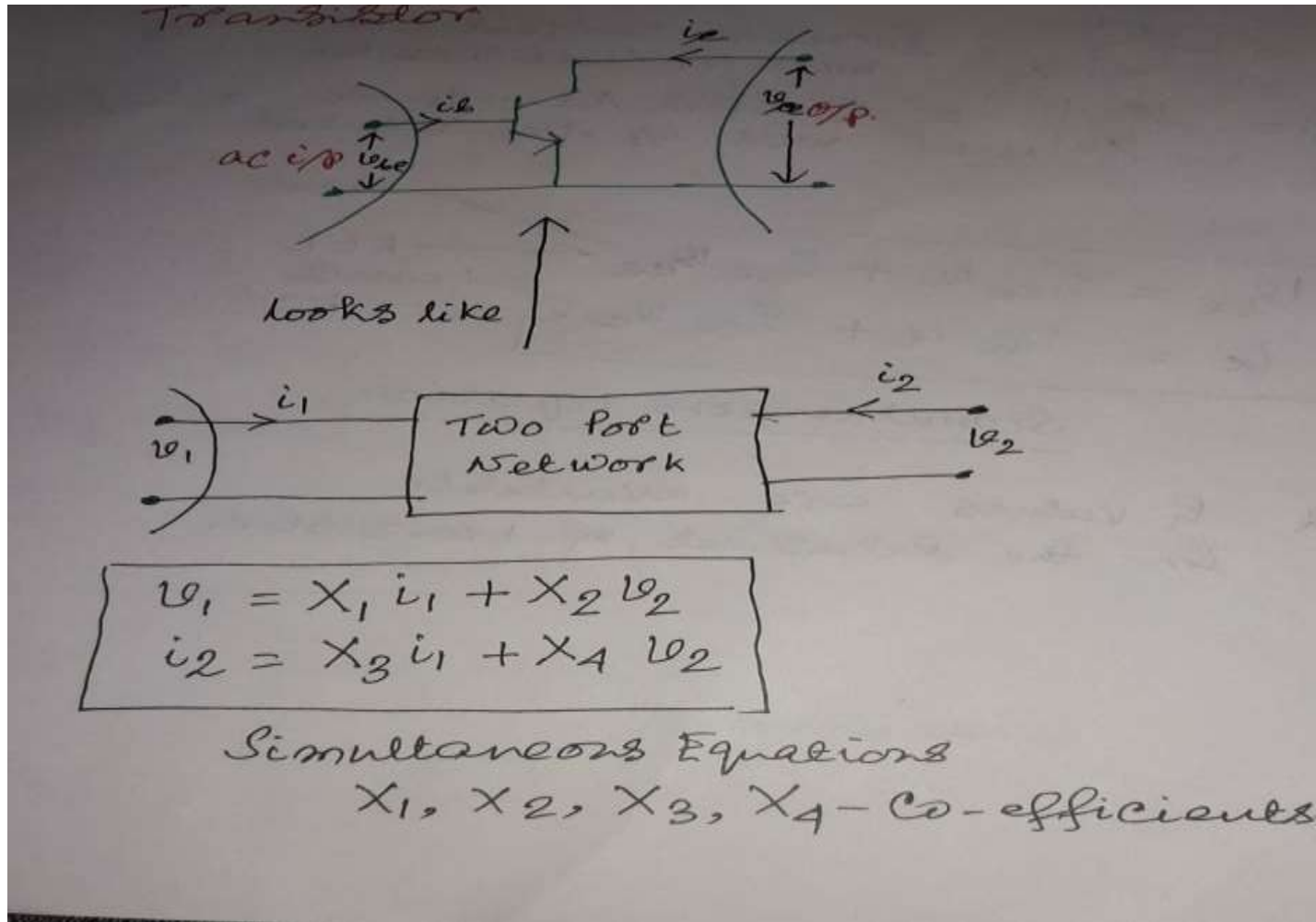
(2) To find out Gain vs. frequency i.e.  
frequency response

[helps to get Bandwidth]

- Effect of the internal capacitances are not considered.

>> In the amplifier, frequency response of all components are known except Transistor.

# Transistor Amplifier



# Transistor Amplifier

From fig.

$$v_1 = v_{be}, i_1 = i_b$$

$$v_2 = v_{ce}, i_2 = i_c$$

$$\begin{cases} v_{be} = X_1 i_b + X_2 v_{ce} \\ i_c = X_3 i_b + X_4 v_{ce} \end{cases}$$

--- Hybrid parameter

$$X_1 = \left. \frac{v_{be}}{i_b} \right|_{v_{ce}=0} = \text{Input Impedance with o/p short circuited} = h_{ie}$$

$$X_2 = \left. \frac{v_{be}}{v_{ce}} \right|_{i_b=0} = \text{Reverse Voltage gain with i/p open circuited} = h_{re}$$

$$X_3 = \left. \frac{i_c}{i_b} \right|_{v_{ce}=0} = \text{Forward Current gain with o/p short circuited} = h_{fe}$$

$$X_4 = \left. \frac{i_c}{v_{ce}} \right|_{i_b=0} = \text{Output Admittance with i/p open circuited} = h_{oe}$$

$$\begin{cases} v_{be} = h_{ie} i_b + h_{re} v_{ce} \\ i_c = h_{fe} i_b + h_{oe} v_{ce} \end{cases}$$

eqn ①  
KVL  
eqn ②  
KCL

Simultaneous Equation.

\* If values are available in the datasheet of transistor.

# Transistor Amplifier

Handwritten equations for a transistor amplifier model, enclosed in a box. The equations are:

$$V_{be} = h_{ie} i_b + h_{re} V_{ce}$$
$$i_c = h_{fe} i_b + h_{oe} V_{ce}$$

Annotations on the right side of the box:

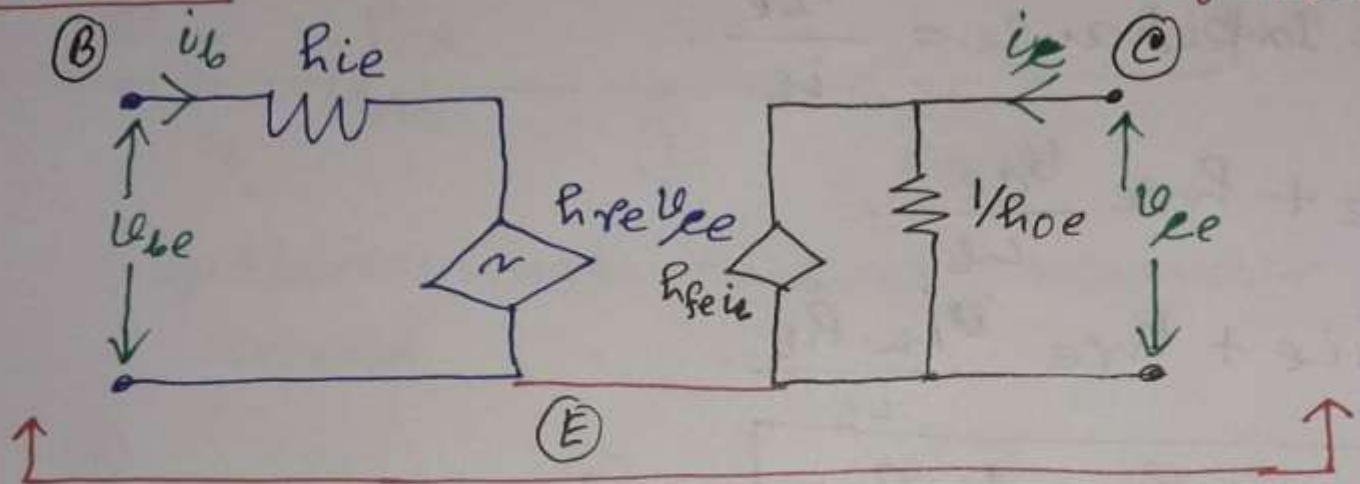
- eqn. ① points to the first equation.
- KVL points to the first equation.
- eqn. ② points to the second equation.
- KCL points to the second equation.

Simultaneous Equation.

\*  $h$  values are available in the datasheet of transistor.

# Transistor Amplifier

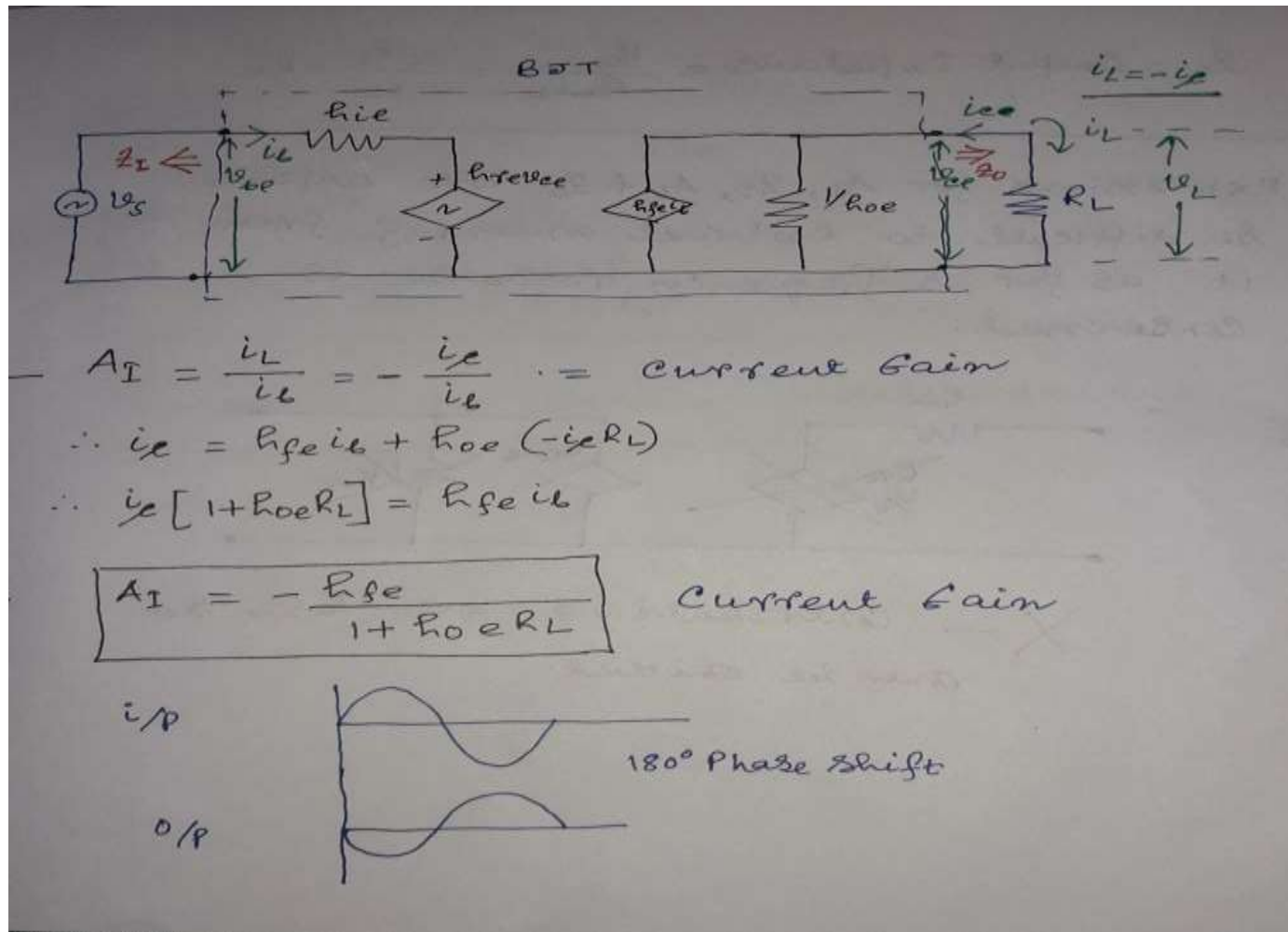
Equation 1



Equation 2

- BJT represented in low frequency hybrid parameter model.

# Transistor Amplifier





# Transistor Amplifier

$$Z_I = \text{Input Impedance} = \frac{V_{ce}}{i_b}.$$

$$= h_{ie} + h_{re} \frac{V_{ce}}{i_b}.$$

$$= h_{ie} + h_{re} \frac{i_L R_L}{i_b}.$$

$$\boxed{Z_I = h_{ie} + h_{re} A_I R_L}$$

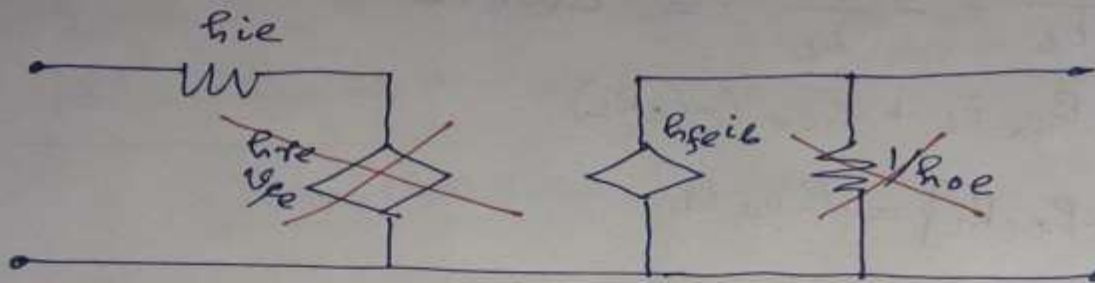
$$A_V = \text{Voltage Gain} = \frac{V_{ce}}{V_{be}} = \frac{i_L R_L}{i_b Z_I} = A_I \frac{R_L}{Z_I}.$$

$$Z_O = \text{Output Impedance} = \frac{V_{ce}}{i_L} = \frac{i_L R_L}{i_L} = R_L$$



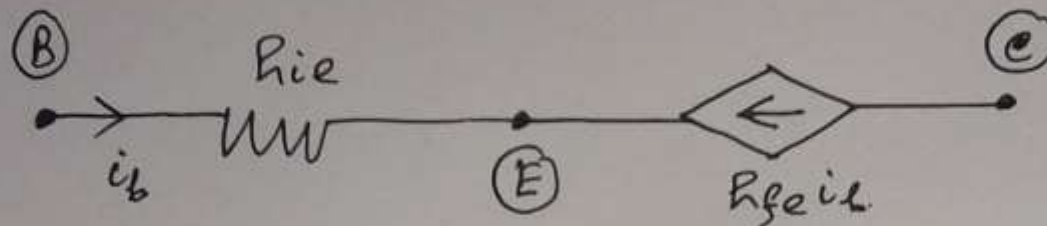
# Transistor Amplifier

Expressions for  $A_I$ ,  $Z_I$ ,  $A_V$  &  $Z_O$  are complex.  
So difficult to extract meaning from  
it as far as frequency response is  
concerned.

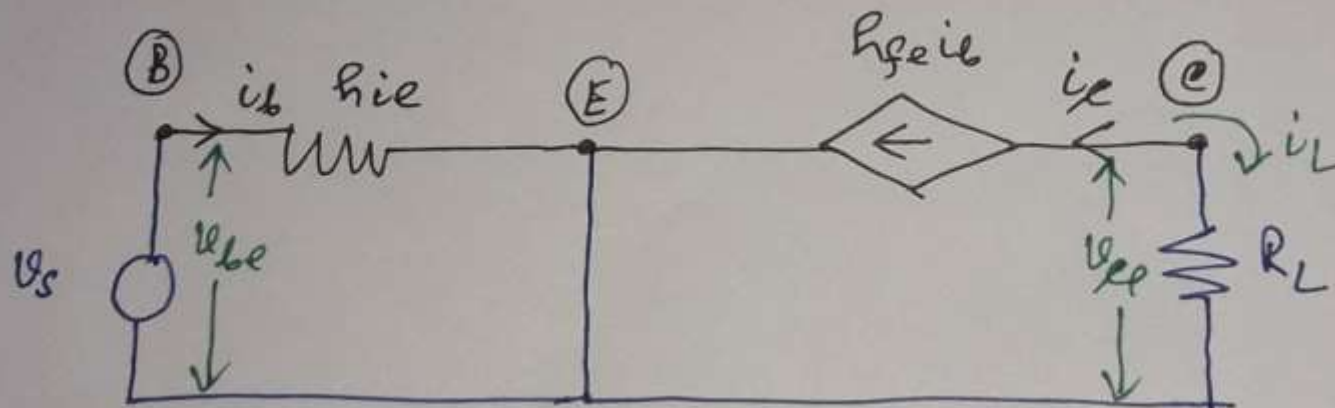


X — Contributions are less, so  
may be omitted.

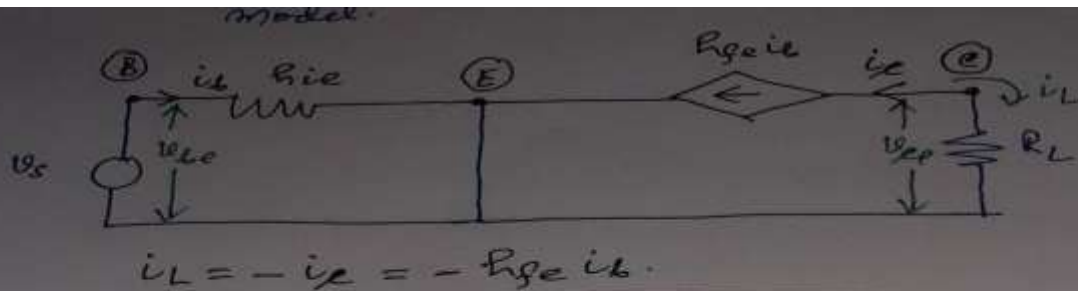
# Transistor Amplifier



⇒ Approximate hybrid parameter model.



# Transistor Amplifier



$$A_I = \text{Current Gain} = -h_{fe}$$

$$Z_I = \frac{v_{be}}{i_b} = \frac{h_{ie} i_b}{i_b} = h_{ie}$$

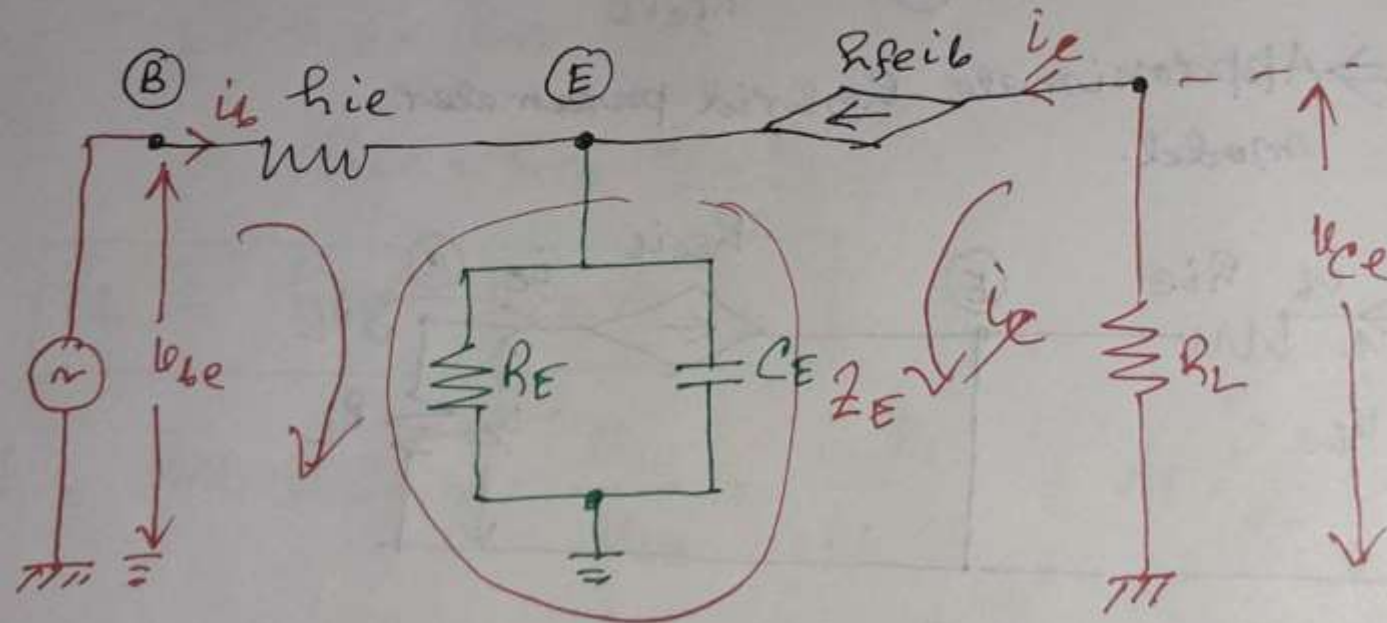
$$Z_O = \frac{v_{ce}}{i_c} = R_L$$

$$A_V = \frac{v_{ce}}{v_{be}} = \frac{i_c R_L}{i_b h_{ie}} = A_I \cdot \frac{R_L}{h_{ie}}$$

Available in the datasheet, mostly dependent of transistor parameters.

# Transistor Amplifier

Frequency Response of BJT Amplifier  
- Low frequency



# Transistor Amplifier

~~SWCE~~

$$i_c = h_{fe} i_b$$

$$v_{be} = h_{ie} i_b + i_b z_E + i_c z_E$$

$$= i_b [h_{ie} + z_E + h_{fe} z_E]$$

$$= i_b [h_{ie} + z_E (1 + h_{fe})]$$

$$v_{ce} = i_L R_L = -i_c R_L$$

$$= -h_{fe} i_b R_L$$

$$A_v = \frac{v_{ce}}{v_{be}} = - \frac{h_{fe} i_b R_L}{i_b [h_{ie} + z_E (1 + h_{fe})]} = \text{Voltage Gain}$$

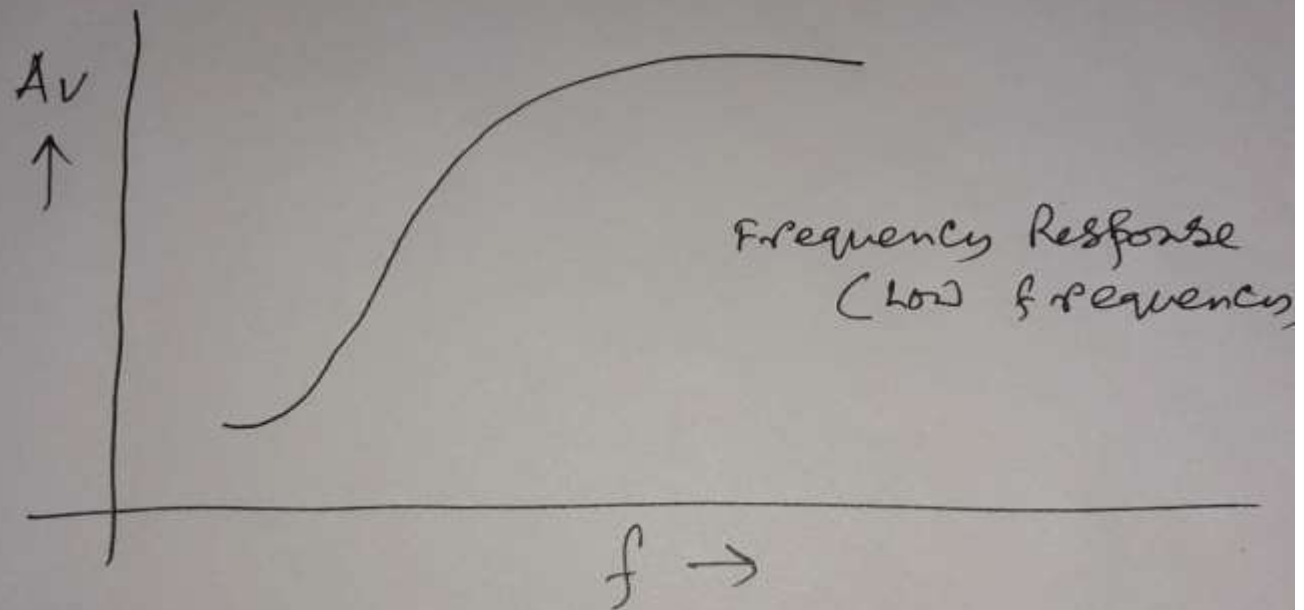
# Transistor Amplifier

$$Z_E = \frac{R_E \cdot \frac{1}{j\omega C_E}}{R_E + \frac{1}{j\omega C_E}}$$
$$= \frac{R_E / j\omega C_E}{\frac{j\omega C_E R_E + 1}{j\omega C_E}}$$

$$Z_E = \frac{R_E}{1 + j\omega C_E R_E}$$

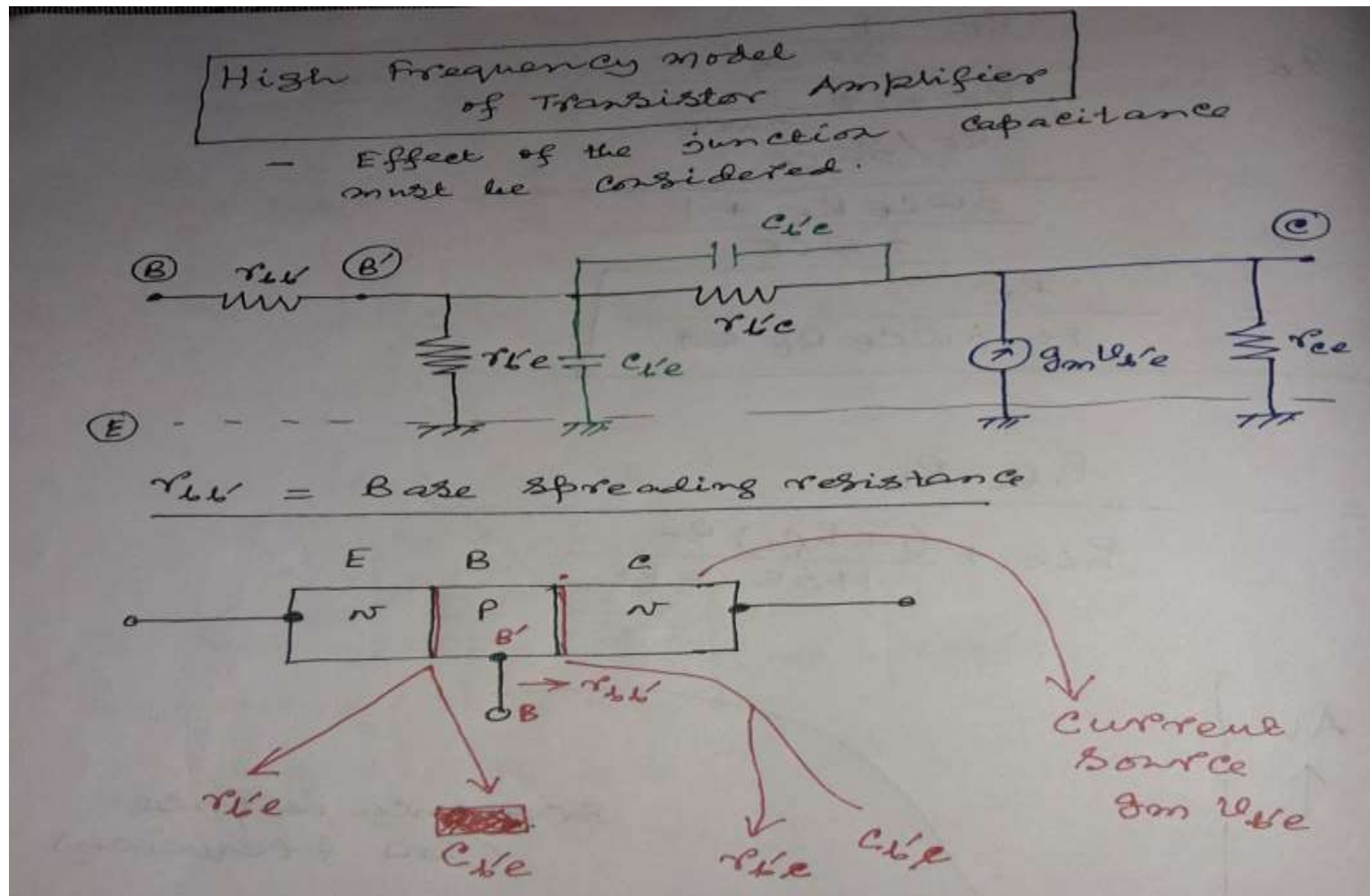
# Transistor Amplifier

$$A_v = - \frac{h_{fe} R_L}{h_{ie} + \frac{(1+h_{fe}) R_E}{1+j\omega C_E R_E}}$$





# High Frequency Model



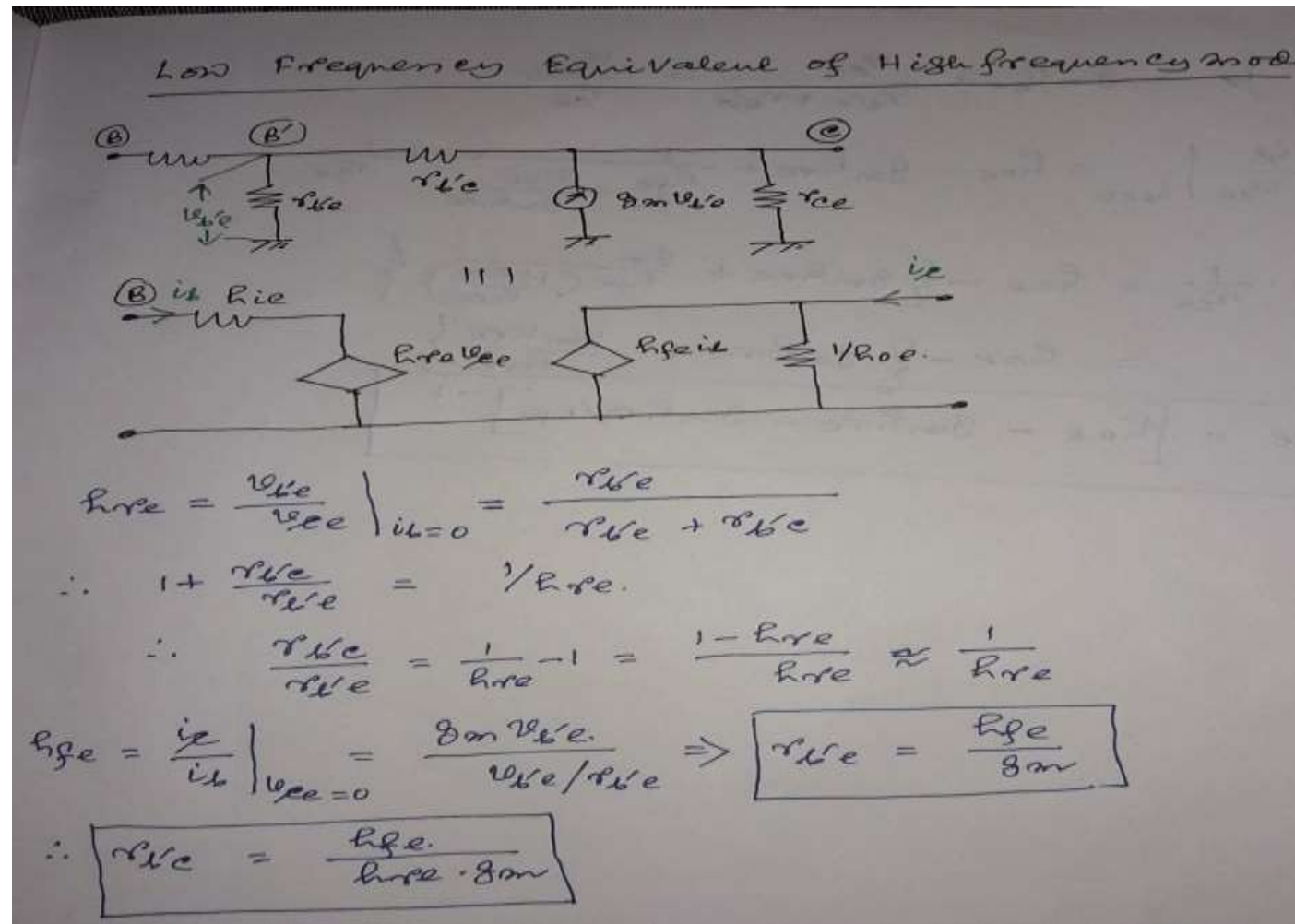
# High Frequency Model

$r$  values &  $g_m$  are not available in the datasheet.

$$g_m = \text{trans conductance} = \frac{i_e}{v_{be}} = \frac{di_e}{v_{be}} \\ = \frac{2}{v_{be}/i_e} = \frac{2}{r_e}$$

$$r_e = \frac{25\text{mV}}{I_E}$$

# High Frequency Model



# High Frequency Model

$$r_{bb'} + r_{b'e} = h_{ie}$$

$$\therefore r_{bb'} = h_{ie} - r_{b'e} \Rightarrow r_{bb'} = h_{ie} - \frac{h_{fe}}{g_m}$$

# High Frequency Model

$$i_e = g_m v_{be} + \frac{v_{ce}}{r_{be} + r_{be}} + \frac{v_{ce}}{r_{ce}}$$

$$\therefore \left. \frac{i_e}{v_{ce}} \right|_{i_b=0} = h_{oe} = g_m h_{re} + \frac{1}{\frac{h_{fe}}{g_m} + \frac{h_{fe}}{g_m h_{re}}} + \frac{1}{r_{ce}}$$

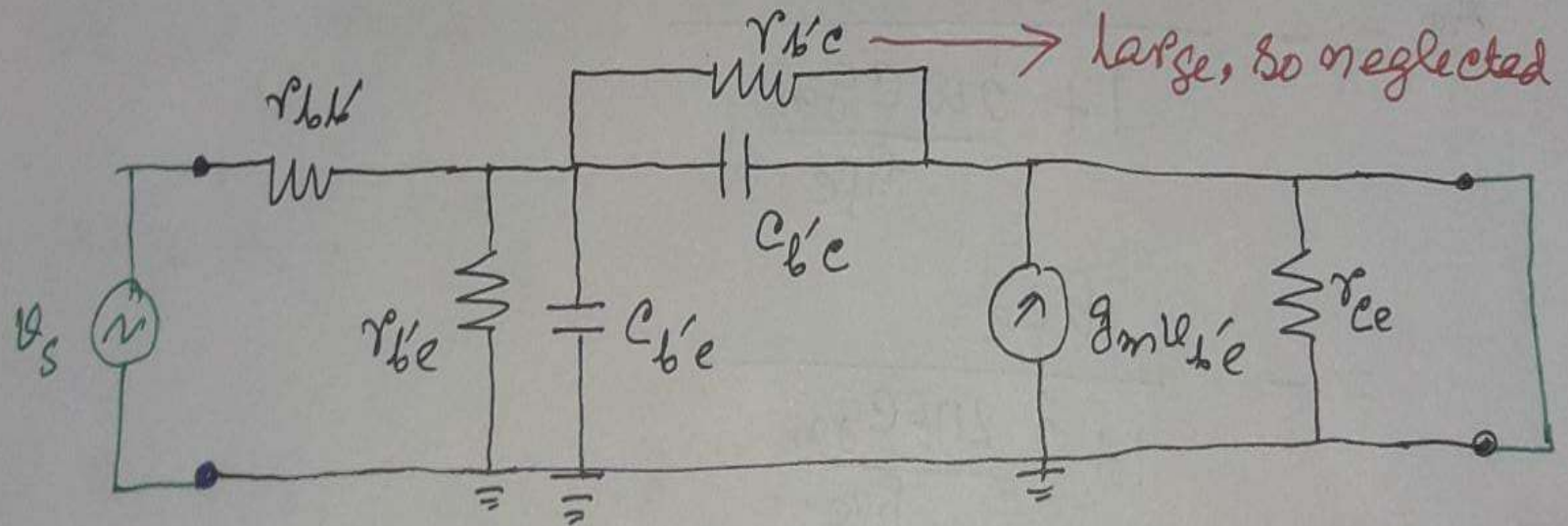
$$\therefore \frac{1}{r_{ce}} = h_{oe} - \left\{ g_m h_{re} + \frac{g_m}{h_{fe} \left( \frac{1+h_{re}}{h_{re}} \right)} \right\}$$

$$= h_{oe} - \left\{ g_m h_{re} + \frac{g_m h_{re}}{h_{fe}} \right\}$$

$$r_{ce} = \left[ h_{oe} - g_m h_{re} - g_m h_{re} / h_{fe} \right]^{-1}$$

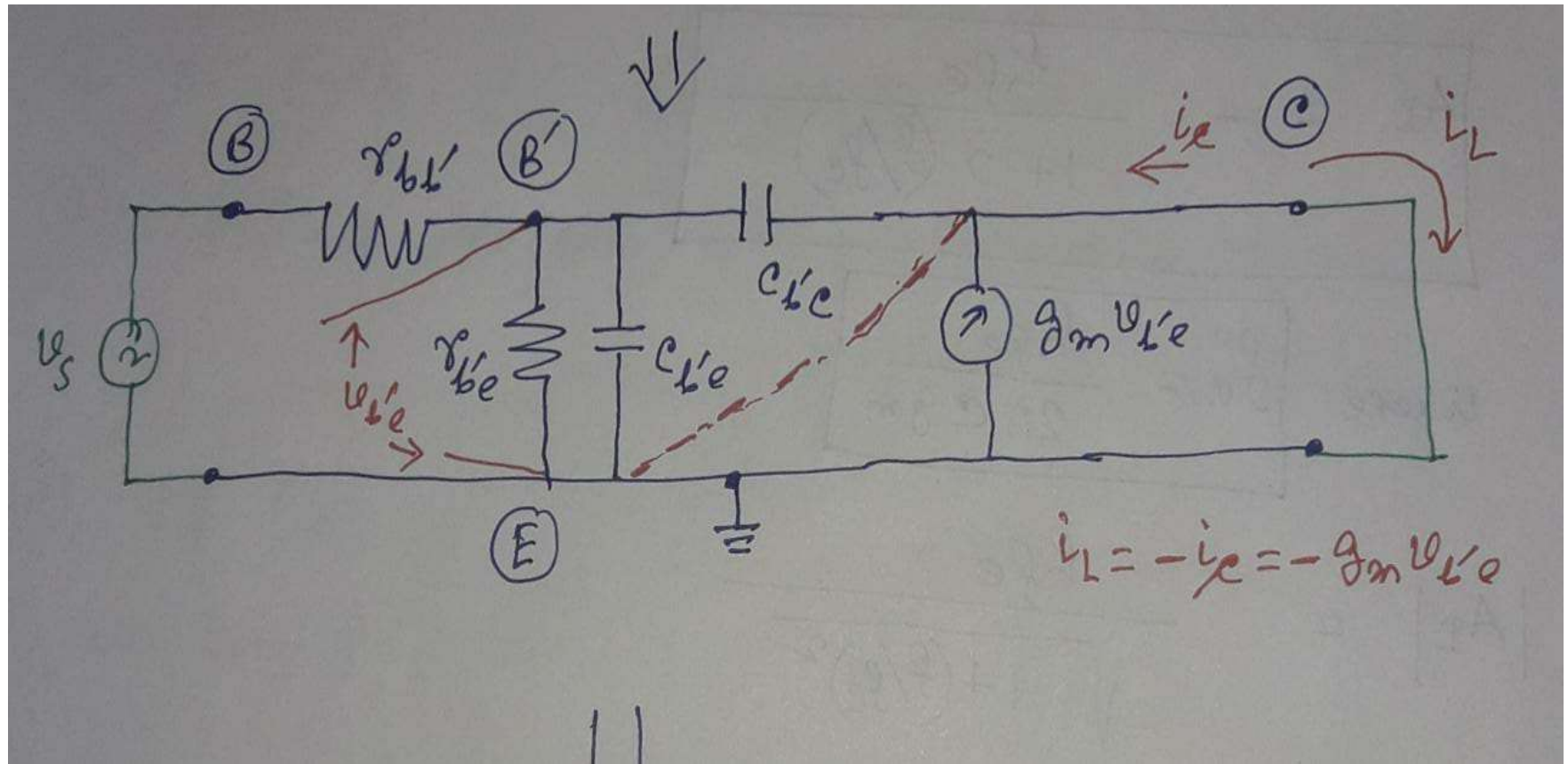
# High Frequency Model

Frequency Response When o/p Short Circuited



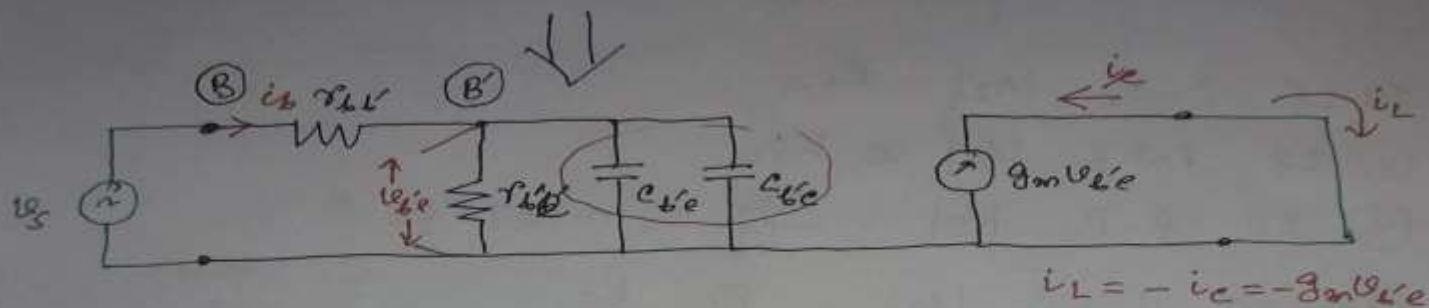


# High Frequency Model





# High Frequency Model



$$C = C_{be} + C_{bc}$$

$$i_b = v_{be} \left[ \frac{1}{r_{be}} + j\omega C \right]$$

$$= v_{be} \left[ \frac{g_m}{\beta_{fe}} + j\omega C \right]$$

$$\therefore A_T = \frac{i_L}{i_b} = - \frac{g_m v_{be}}{v_{be} \left[ \frac{g_m}{\beta_{fe}} + j\omega C \right]}$$

# High Frequency Model

$$A_I = - \frac{h_{fe}}{1 + j\omega C \frac{h_{fe}}{g_m}}$$

$$= - \frac{h_{fe}}{1 + j \frac{2\pi f C h_{fe}}{g_m}}$$

$$A_I = - \frac{h_{fe}}{1 + j(f/f_c)}$$

where  $f_c = \frac{g_m}{2\pi C h_{fe}}$

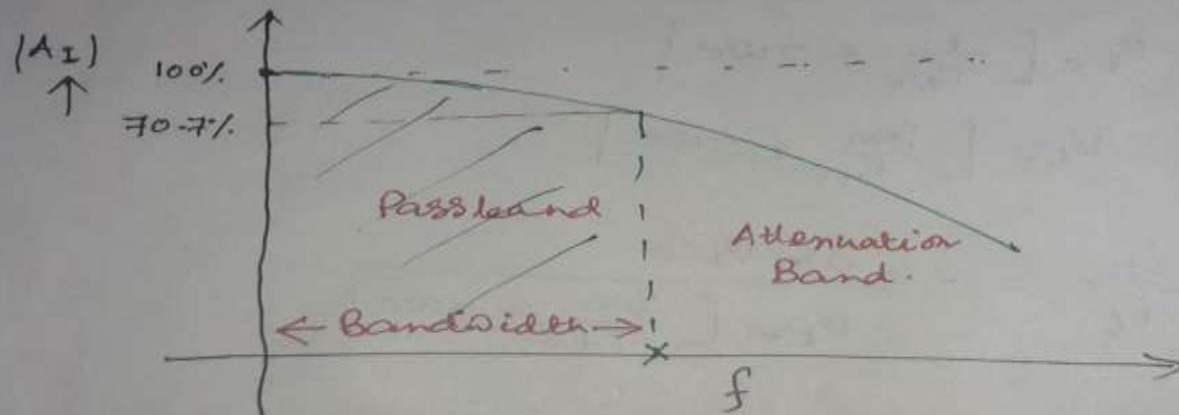
$$f_c = \frac{g_m}{2\pi C h_{fe}}$$

$$|A_I| = \frac{h_{fe}}{\sqrt{1 + (f/f_c)^2}}$$

# High Frequency Model

$$|A_T| = \frac{R_{fe}}{\sqrt{1 + (f/f_c)^2}}$$

- ① If  $f = 0$ ,  $|A_T| = R_{fe}$
- ② If  $f \ll f_c$ ,  $|A_T| \approx R_{fe}$
- ③ If  $f = f_c$ ,  $|A_T| = \frac{R_{fe}}{\sqrt{2}} = 0.707 R_{fe}$
- ④ If  $f \gg f_c$ ,  $|A_T| = R_{fe} \cdot \frac{f_c}{f}$



# High Frequency Model

As  $|A_I|$  is a large quantity, normally it is expressed in terms of dB.

$$|A_I|_{\text{in dB}} = 20 \log_{10} |A_I|$$

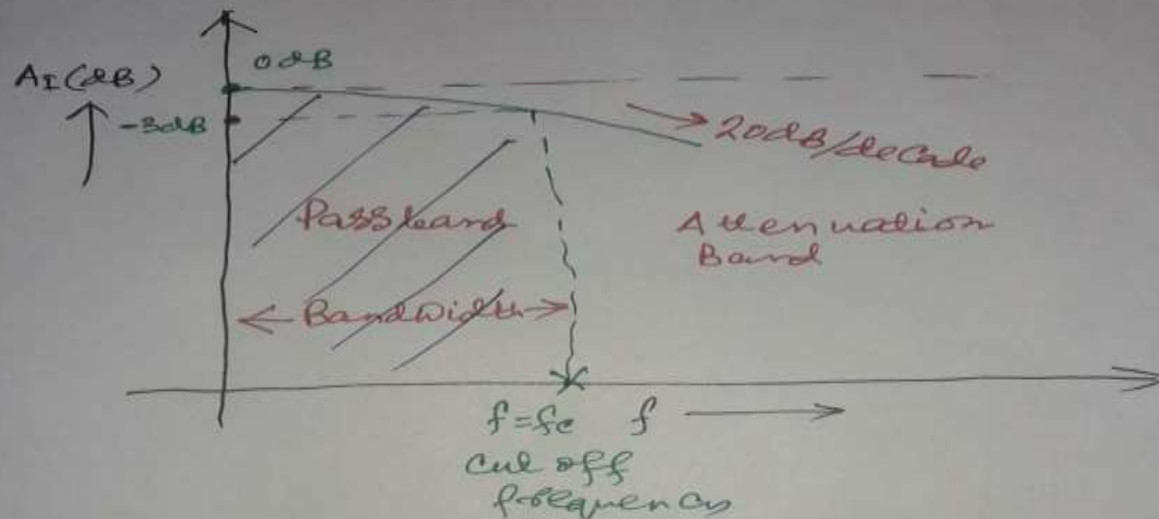
- ① If  $f=0$ ,  $|A_I|_{\text{in dB}} = 20 \log_{10} h_{fe} \dots (\text{max.}) \dots 10 \text{ dB}$
- ② If  $f \ll f_c$ ,  $|A_I|_{\text{in dB}} \approx 20 \log_{10} h_{fe} \dots \nearrow$
- ③ If  $f=f_c$   $|A_I|_{\text{dB}} = 20 \log_{10} h_{fe} - 20 \log_{10} \sqrt{2}$   
 $= 0 \text{ dB} - 3 \text{ dB} = -3 \text{ dB}$

# High Frequency Model

① If  $f \gg f_c$

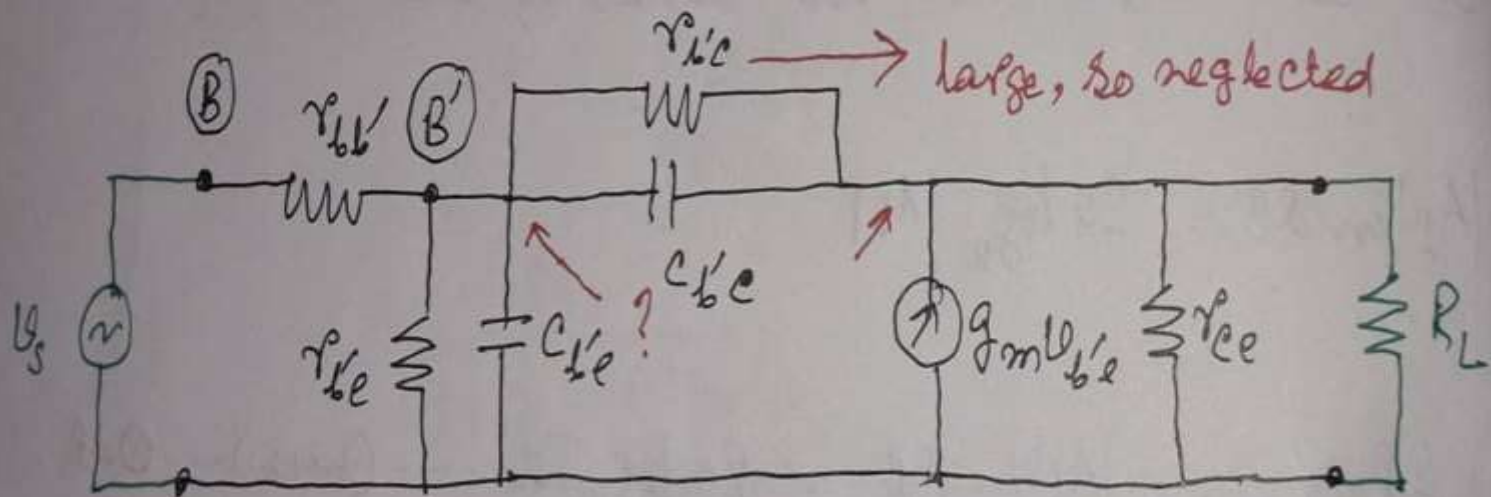
lets say  $f = 10 f_c$ .

$$A_i(\text{in dB}) = 20 \log_{10} f_{fc} - 20 \log_{10} 10 \\ = -20 \text{ dB.}$$



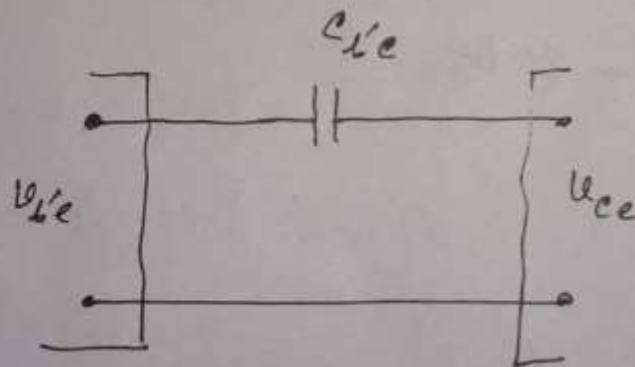
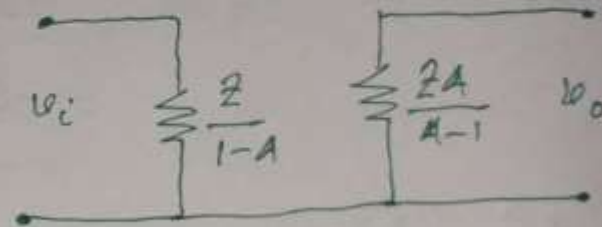
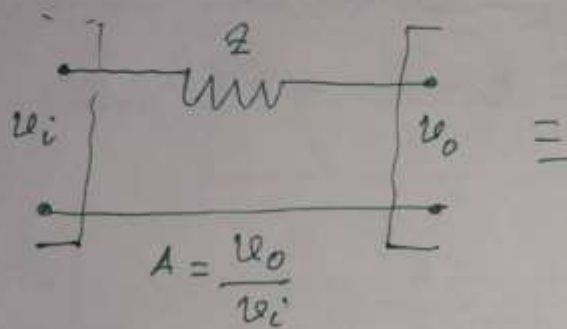
# High Frequency Model

Frequency Response when  $R_L$  is Connected at the load



# High Frequency Model

Use Miller's Theorem



$$A = \frac{v_{ce}}{v_{b'e}} = - \frac{g_m v_{b'e} R_L}{v_{b'e}}$$

$$\boxed{A = -g_m R_L}$$



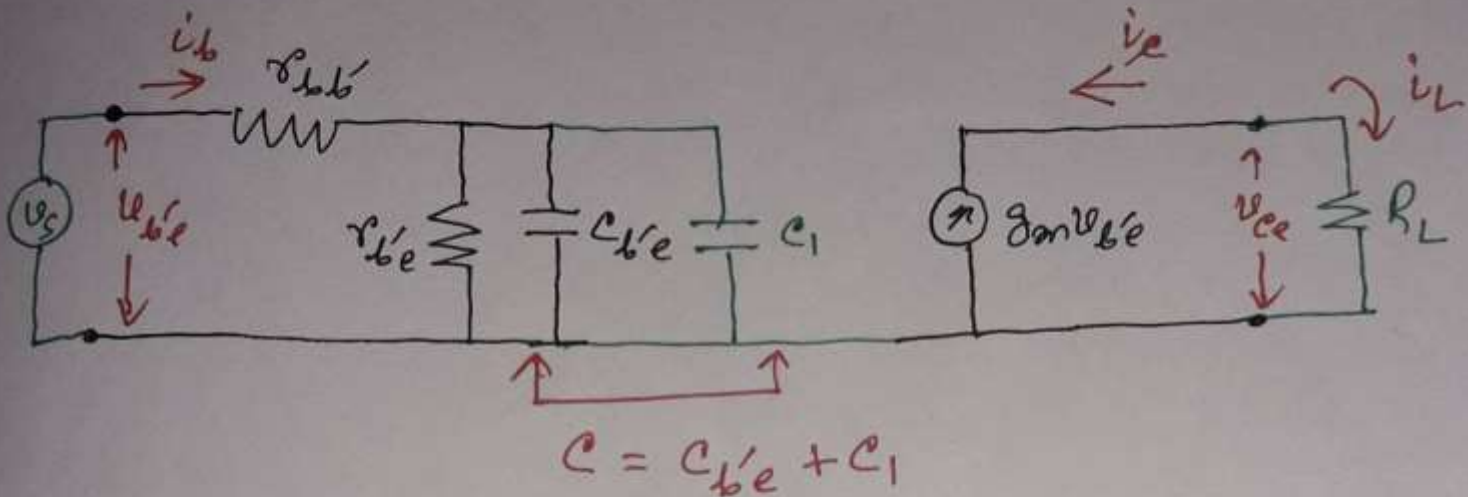
# High Frequency Model

$$\frac{Z}{1-A} = \frac{\frac{1}{j\omega C_L'c}}{1+g_m R_L} = \frac{1}{j\omega C_L'c (1+g_m R_L)}$$
$$= \frac{1}{j\omega C_1}$$

where  $C_1 = C_L'c (1+g_m R_L)$

$$\frac{Z_A}{A-1} = \frac{(-g_m R_L) \frac{1}{j\omega C_L'c}}{-g_m R_L - 1} \approx \frac{1}{j\omega C_L'c}$$

# High Frequency Model



$$\begin{aligned}
 i_b &= v_{be'} \left[ \frac{1}{r_{be'}} + j\omega C \right] \\
 &= v_{be'} \left[ \frac{g_m}{h_{fe}} + j\omega C \right]
 \end{aligned}$$

# High Frequency Model

$$A_I = \frac{i_L}{i_b} = \frac{-g_m v_{b'e}}{v_{b'e} \left[ \frac{g_m}{h_{fe}} + j\omega C \right]}$$
$$= - \frac{h_{fe}}{1 + \frac{j\omega C h_{fe}}{g_m}}$$

$$A_I = - \frac{h_{fe}}{1 + j \left( \frac{f}{f_c} \right)}$$

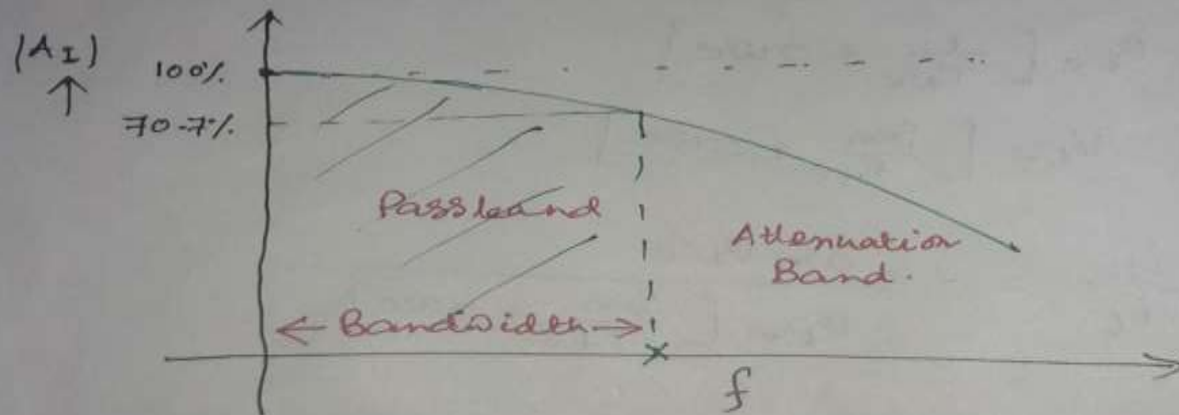
where  $f_c = \frac{g_m}{2\pi C h_{fe}}$

$$C = C_{b'e} + C_{b'c} (1 + g_m R_L)$$

# High Frequency Model

$$|A_T| = \frac{R_{fe}}{\sqrt{1 + (f/f_c)^2}}$$

- ① If  $f = 0$ ,  $|A_T| = R_{fe}$
- ② If  $f \ll f_c$ ,  $|A_T| \approx R_{fe}$
- ③ If  $f = f_c$ ,  $|A_T| = \frac{R_{fe}}{\sqrt{2}} = 0.707 R_{fe}$
- ④ If  $f \gg f_c$ ,  $|A_T| = R_{fe} \cdot \frac{f_c}{f}$

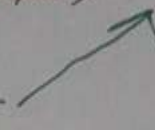


# High Frequency Model

As  $|A_I|$  is a large quantity, normally it is expressed in terms of dB.

$$|A_I|_{\text{in dB}} = 20 \log_{10} |A_I|$$

① If  $f=0$ ,  $|A_I|_{\text{in dB}} = 20 \log_{10} h_{fe} \dots \text{(max.)} \dots 10 \text{ dB}$

② If  $f \ll f_c$ ,  $|A_I|_{\text{in dB}} \approx 20 \log_{10} h_{fe} \dots$  

③ If  $f=f_c$   $|A_I|_{\text{(dB)}} = 20 \log_{10} h_{fe} - 20 \log_{10} \sqrt{2}$   
 $= 0 \text{ dB} - 3 \text{ dB} = -3 \text{ dB}$

# High Frequency Model

① If  $f \gg f_c$

lets say  $f = 10 f_c$ .

$$\begin{aligned} A_i(\text{in dB}) &= 20 \log_{10} f_{fc} - 20 \log_{10} 10 \\ &= -20 \text{ dB.} \end{aligned}$$

