

Theory of Electronic Nematic Criticality Constrained by Elastic Compatibility

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The defining property of electronic nematicity – the spontaneous breaking of rotational symmetry – implies an unavoidable coupling between the nematic order parameter and elastic strain fields, known as nemato-elasticity. While both quantities are rank-2 tensors, the strain tensor is constrained through the Saint Venant compatibility relations. These constraints, which take the form of three coupled second-order partial differential equations, arise from the lattice displacement vector's role as the potential field. The compatibility relations reflect the underlying gauge invariance of geometric deformations, which are violated only in the presence of crystalline defects. In this work, we develop a theory of nemato-elasticity that incorporates elastic compatibility explicitly through a co-rotating helical basis. Within our formalism, we show that elasticity bestows tensor compatibility upon the electronic nematic order parameter by suppressing incompatible electronic nematic fluctuations. As a result, nemato-elasticity is markedly different from bare nematicity. In ideal media devoid of defects, we show that the suppression of incompatible nematicity underlies direction-selective criticality, even in the absence of crystalline anisotropy. In realistic systems with defects, meanwhile, we show that elastic pinning fields emanate from distributions of quenched defects, generating random longitudinal and transverse conjugate fields experienced by the local nematic order parameter. The coexistence of direction-selective nematic criticality with pinning effects from random fields is naturally explained within our theory from the transformation to the helical basis, implying that local experimental probes of nematicity will be influenced by a linear – but nonlocal – combination of long-ranged and short-ranged helical nematic modes. Because the compatibility relations are gauge constraints endowed in the isotropic medium, our results constitute universal features of nemato-elastic criticality present in all crystalline systems.

I. INTRODUCTION

Initially proposed for cuprates and quantum Hall systems [1–4], the phenomenon of electronic nematicity has quickly expanded, since the discovery of iron-based superconductors [5–13], to an ever growing list of quantum materials with rather dissimilar properties [14–34]. On the one hand, this rich landscape of materials in which electronic degrees of freedom can drive the breaking of a rotational symmetry point to a broad range of possible microscopic mechanisms, from spin fluctuations [9, 10, 35, 36] to multi-component pairing excitations [37, 38]. On the other hand, they also raise questions about universal properties of electronic nematic phenomena, particularly close to critical points, either thermal or quantum [3, 39]. Moreover, besides their own interest as a new form of quantum many-body state, electronic nematicity is often intertwined with other degrees of freedom and quantum phases of interest, most notably unconventional superconductivity [40–42].

Despite their microscopic dissimilarities, electronic nematic phases all share a common feature which distinguishes them from classical nematic liquids: they are crystalline solids. Indeed, while the elastic properties of nematic liquids are contained in the nematic degrees of freedom, the electronic nematic order parameter inherits the elastic properties of the underlying lattice [43, 44]. This fact introduces two important effects for the phenomenological description of electronic nematicity. First, in isotropic liquid crystals, the nematic director can condense in any direction in space, meaning its order parameter is a rank-2 traceless symmetric quadrupolar tensor

with five degenerate components in three spatial dimensions [45]. In electronic nematics, meanwhile, the discrete rotational symmetry of the solid splits the fivefold degeneracy encoded in the tensor into different irreducible representations of the quadrupole within the corresponding point group of the lattice [46, 47]. The crystal anisotropy can reduce the five degenerate components down to a single “Ising” nematic order parameter, as is the case in the tetragonal-to-orthorhombic phase transitions of the iron-based superconductors [13], 2DEGs [46], cuprates [48] or collective Jahn-Teller systems [49, 50]. Two-dimensional hexagonal systems, meanwhile, realize the 3-state Potts nematic universality class, since the fivefold degeneracy of SO(3) is reduced to only twofold in the crystal [15, 17, 18, 22, 37, 51, 52]. Whereas these materials are effectively two-dimensional (or actually two-dimensional), there are also reports of electronic nematicity exhibiting a higher threefold degeneracy within cubic systems, returning electronic nematic phenomenology back to the fully three-dimensional regime [53, 54]. Regardless of the point group, however, each of these nematic irreducible representations are all subsets of the original five basis functions from SO(3).

The second major effect is *nemato-elasticity* – the bilinear coupling between electronic nematicity and symmetry-breaking elastic strains – and is the subject of this work and an accompanying Letter [55]. At first sight, such a bilinear coupling may seem trivial, since the structural degrees of freedom are not critical on their own, but only via their coupling to the electronic nematic degrees of freedom. However, elastic degrees of freedom are subjected to constraints that will be inevitably inherited by the critical nematicity. Indeed, it has been shown that nemato-elasticity has profound effects near the elec-

tronic nematic critical point that are not present in liquid crystals. Some of these effects include the development of a spontaneous symmetry-breaking ferroelastic strain [8, 9, 56, 57], complete softening of the appropriate elastic modulus by nematic fluctuations [44, 58], and direction-selective criticality [39, 51, 59, 60]. The first two effects reflect how electronic correlations can strongly alter the structural properties, while the latter effect arises from elastostatic fluctuations renormalizing the bare electronic nematic critical behavior. Originally associated with acoustic-phonon-driven ferroelastic instabilities [61–63], direction-selective criticality is an effect where thermal fluctuations of the order parameter soften anisotropically in a crystalline environment, i.e., the nematic susceptibility only diverges along specific momentum-space directions. This ultimately leads to only a sub-dimensional manifold of critical fluctuations with specific high-symmetry momenta, while suppressing most fluctuations at other momenta. In electronic nematics, this effect is believed to be responsible for the essentially mean-field critical behavior observed for Ising-nematics in low-dimensional systems [8, 39, 56, 59].

Despite the theoretical progress in nematic criticality gained from phonon-mediated direction-selective criticality, there remain important discrepancies between theoretical predictions and experimental observations, particularly at mesoscopic length scales. There has long been experimental evidence in samples that the electronic nematic order parameter condenses into domains [17, 50, 64–74] with random field disorder being a likely culprit for domain formation [17, 75–86]. If indeed pinning effects from random fields are responsible for the domains, then standard arguments from statistical mechanics would contend that the sharp nematic phase transition associated with long-range order should be heavily suppressed, if not lost altogether, in low-dimensional systems [75, 76, 78]. Moreover, while there are many sources of local random fields for the nematic order parameter, particularly in doped materials [46], one of the most obvious arises in the form of random strain fields [50, 85, 87]. These naturally arise as a consequence of nemato-elasticity in materials endowed with unavoidable structural disorder. Such random strains, particularly those emanating from crystalline defects, should be long-ranged and anisotropic [88–90], only amplifying the strength of random strain disorder [81, 82, 91].

From the perspective of elasticity, however, the same elastic fluctuations that give rise to the sharp mean-field phase transition also mediate the long-range random pinning fields from structural defects. This presents a seeming paradox which we seek to resolve with our proposed theory of nemato-elastic criticality. How can elastic fluctuations that mediate interactions favoring spontaneous symmetry breaking simultaneously also mediate random pinning fields which eliminate nematic criticality? Moreover, at the microscopic level, detailed experiments have observed a puzzling decoupling between the local strain and the electronic nematic order parameter, seemingly at odds with the expectation that these two fields are bilinearly coupled [72].

The focus of our theory is on a crucial feature of elasticity theory that, while important for structural disorder, has been overlooked in the electronic nematic literature: the Saint

Venant compatibility relations [90, 92–95]. These are a set of second-order partial differential equations that act as constraints between the various components of the spatially modulated strain tensor. The continuous deformation of a medium – one that displaces every unit cell from its equilibrium position at \mathbf{x} to its displaced position at $\mathbf{x} + \mathbf{u}(\mathbf{x})$ – requires that the information contained within the strain tensor must reflect the *vector* displacement field, $\mathbf{u}(\mathbf{x})$, rather than being a truly tensorial quantity like the electronic nematic order parameter, $\varphi_{ij}(\mathbf{x})$. Formally, these constraints arise because elasticity is a U(1) tensor gauge theory [45, 92, 95–98]. Using Kröner's incompatibility operator [89], one writes them as

$$\text{inc}(\boldsymbol{\varepsilon})_{ij} \equiv \epsilon_{ikl}\epsilon_{jmn}\partial_k\partial_m\varepsilon_{ln} = 0, \quad (1)$$

where ϵ_{ijk} is the Levi-Civita symbol. The expressions above are analogous to the curl-free constraints imposed on the electrostatic field, $(\nabla \times \mathbf{E})_i = \epsilon_{ijk}\partial_j E_k = 0$, which guarantees the existence of a scalar-valued electrostatic potential field that satisfies $\mathbf{E} = -\nabla\phi$. It is straightforward to show that the infinitesimal strain tensor of elastostatics,

$$\varepsilon_{ij}(\mathbf{x}) = \frac{1}{2} [\partial_j u_i(\mathbf{x}) + \partial_i u_j(\mathbf{x})], \quad (2)$$

satisfies Eq. (1). Thus, the displacement vector plays the part of a *vector-valued* potential field for the strain tensor. Any other tensor that satisfies Eq. (1) is called *compatible*, whereas any tensor that does not is called *incompatible* [89, 92]. These terms for tensors are analogous to the terms “conservative” or “irrotational”, and “nonconservative” or “rotational”, used for vector fields, respectively.

We emphasize that the compatibility relations are *geometrical* constraints – they must be obeyed if the deformation arises from a differentiable, *single-valued*, displacement vector field, $\mathbf{u}(\mathbf{x})$. When the compatibility relations are violated, then the deformation may be constructed from a multi-valued displacement vector field, attributed to structural defects which, in equilibrium, are responsible for plastic deformation [88–90, 92, 95, 99–104]. In contrast to the elastic regime, in which a solid returns to its equilibrium position after the applied external stress is removed, in the plastic regime the structural defects are impacted by the external stress, such that the solid cannot return to its equilibrium position.

From the perspective of electronic nematicity, a phenomenon which is most conveniently expressed in terms of the group theoretic language of condensed matter physics, the compatibility relations impose non-trivial relationships between the irreducible representations of the strain tensor. Importantly, as we will show, the compatibility relations couple strains with trivial character with those of nontrivial character at any momentum, even if infinitesimal but nonetheless nonzero. Given that the electronic nematic order parameter lowers a system's rotational symmetry, it can only couple directly to the strain components that transform as the same irreducible representation. One would expect from the symmetry analysis, therefore, that there is always at least one component of the strain tensor that will never be bilinearly coupled to electronic nematicity: the symmetry-preserving, volume-changing *dilatation* strain, $\text{Tr}(\boldsymbol{\varepsilon}) = \varepsilon_{xx} + \varepsilon_{yy} + \varepsilon_{zz} = \nabla \cdot \mathbf{u}(\mathbf{x})$, given its

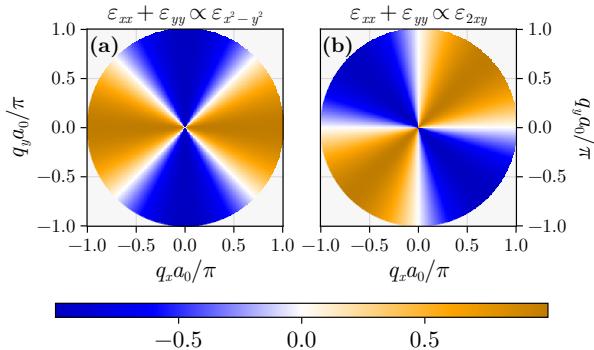


FIG. 1. Two-dimensional elastic compatibility relation enforced in momentum space. Each panel shows the dilatation, $\varepsilon_{xx} + \varepsilon_{yy} = \partial_x u_x + \partial_y u_y$ induced by a symmetry-breaking static strain wave with well-defined wavevector, \mathbf{q} . The direction-dependence of these constraints are present in systems of any crystal symmetry. The colorbar represents the form factors that relate the symmetry-breaking (a) deviatoric, $\varepsilon_{x^2-y^2} = \varepsilon_{xx} - \varepsilon_{yy}$, and the (b) shear, $\varepsilon_{2xy} = 2\varepsilon_{xy}$, strains to the symmetry-preserving dilatations, as enforced by the single compatibility condition in 2D.

invariance under rotations and reflections [105]. However, we will show that this expectation is not upheld for the vast majority of electronic nematic fluctuations because they inherit the constraints of the compatibility relations.

It is simplest to understand how electronic nematic fluctuations couple to symmetry-preserving dilatations by considering the two-dimensional limit first. Throughout the rest of the paper, we will work in the fully-three dimensional elastic medium. For planar deformations, the so-called “plane strain” problems of elasticity require that $u_z(\mathbf{x}) \equiv 0$ and $\partial_z u_i(\mathbf{x}) \equiv 0$ [90, 92, 106]. Thus, there are only three nonzero strain components, ε_{xx} , ε_{yy} , and ε_{xy} , while there are two components in the displacement vector: $\mathbf{u} = (u_x, u_y)$. There is only one compatibility relation needed as a constraint to match the number of independent components of these two quantities: $\text{inc}(\varepsilon)_{33} = 0$. Written out in its usual form, it is

$$\text{inc}(\varepsilon)_{33} = \partial_x^2 \varepsilon_{yy} + \partial_y^2 \varepsilon_{xx} - 2\partial_x \partial_y \varepsilon_{xy} = 0, \quad (3)$$

given that $\varepsilon_{xy} = \varepsilon_{yx}$. In symmetry-reduced form, meanwhile, the above becomes

$$\nabla^2(\varepsilon_{xx} + \varepsilon_{yy}) = (\partial_x^2 - \partial_y^2)(\varepsilon_{xx} - \varepsilon_{yy}) + (2\partial_x \partial_y)(2\varepsilon_{xy}). \quad (4)$$

The left-hand side is the symmetry-preserving dilatation strain, $\varepsilon_{x^2+y^2} \equiv \varepsilon_{xx} + \varepsilon_{yy}$, in two spatial dimensions. The right-hand side shows that symmetry-breaking deviatoric, $\varepsilon_{x^2-y^2} \equiv \varepsilon_{xx} - \varepsilon_{yy}$, and shear, $\varepsilon_{2xy} \equiv 2\varepsilon_{xy}$, strains with arbitrary spatial modulations will inevitably generate non-uniform dilatation strains [55, 57]. In momentum space, the equation above is written more succinctly as

$$\varepsilon_{x^2+y^2, \mathbf{q}} = \cos(2\phi) \varepsilon_{x^2-y^2, \mathbf{q}} + \sin(2\phi) \varepsilon_{2xy, \mathbf{q}}, \quad (5)$$

where the wavevector is parameterized in the plane as $\mathbf{q} \equiv (q \cos \phi, q \sin \phi)$ [55, 57].

These trigonometric form factors are plotted in momentum space in Fig. 1. The momenta in either panel where

the form factors are nonzero force non-uniform deviatoric and shear strains to induce non-uniform dilatations. Clearly this is the vast majority of momentum directions, and they convert either $\varepsilon_{x^2-y^2}$ or ε_{2xy} strains into symmetry-preserving, volume-changing strain. The relationship between these irreducible representations is universal and must occur in all crystals. Note that the compatibility condition in Eq. (4) is perfectly allowed from a symmetry perspective, since all terms transform trivially under any action from the orthogonal group $O(3)$, and thus under all point-group symmetry operations of any crystal. The key point is that the elastic compatibility relations are not symmetry-enforced constraints, but geometric constraints enforced by the gauge-field nature of elasticity theory.

In the special case of a φ_{2xy} -nematic order parameter, such as that in the iron-based superconductors [10–13, 57], the nematic fluctuations will naturally induce ε_{2xy} strain fluctuations through nematic-elasticity. However, Eq. (5) and Fig. 1(b) show that nematic fluctuations will also necessarily induce dilatations *unless* $\sin(2\phi) = 0$. These induced dilatations incur a higher energy cost associated with the bulk modulus of the material, which is often the largest elastic constant of the materials of interest. Similarly, for $\varphi_{x^2-y^2}$ -nematics, dilatations are generated *unless* $\cos(2\phi) = 0$. These are the critical momentum directions discussed before in the context of “direction-selective criticality” in Ising electronic nematics [39, 59]. Analogously, in 3-state Potts nematics of 2D hexagonal systems, where the order parameter is the $(\varphi_{x^2-y^2}, \varphi_{2xy})$ doublet, then Eq. (5) implies that dilatations are generated *unless* the nematic director is orthogonal to the momentum quadrupole, $(q_x^2 - q_y^2, 2q_x q_y)$, an effect predicted previously named “nematic-orbital coupling” [51]. In those works, direction-selective criticality was obtained by considering the coupling between the electronic nematic order parameter and the acoustic phonons – the Goldstone modes that emerge in elasticity theory – which usually have anisotropic velocities. We argue here that this effect is actually a direct consequence of the compatibility relations. Although they are indirectly encoded in the phonons, the latter are not the microscopic mechanism responsible for this effect.

The elastic compatibility’s role in direction-selective criticality is reflected by the fact that the use of the compatibility relations in Eq. (5) in deriving direction-selective criticality circumvents knowledge of the crystalline point group. We reiterate that these constraints exist even in the 2D isotropic continuum because they arise from the geometrical relationship between \mathbf{u} and ε_{ij} . Because of this, direction-selective criticality must also be a fundamental and universal consequence of compatibility, rather than being an effect of crystalline anisotropy. While these arguments completely account for direction-selective criticality for two-dimensional planar nematics, elastic deformation of real materials is fundamentally three-dimensional. Thus, there are two additional independent compatibility relations in Eq. (1) that determine the interdependence of the six components of the strain tensor. In turn, this means that in-plane nematic fluctuations can induce out-of-plane deformations, and *vice versa*.

In this paper we develop a fully three-dimensional theory

of nematic elasticity. The key ingredient of this framework is to write down the electronic nematic order parameter not in the usual d -orbital basis of irreducible representations, but in a basis we dub “helical”, which automatically accounts for the presence (or absence) of tensor compatibility. We focus on the isotropic limit, since it is clear from the 2D limit that direction-selectivity in crystals is precipitated down from geometrical constraints on deformation to strains within crystals. Within our theory we find that nematic-elastic criticality can always be thought of as a “planar” instability because the five degenerate nematic basis functions of $\text{SO}(3)$ split at each momentum into a critical doublet and a non-critical singlet and doublet. The critical components are identified with the compatible sector of the electronic nematic order parameter, and can be written as the symmetric gradient of a purely transverse displacement vector field. The non-critical components, meanwhile, are identified with incompatible electronic nematicity, and likewise couple to crystalline defects because of their mutual orthogonality to the compatible sector of nematicity. We discuss the several implications of our results for the general phenomenology of electronic nematics, resolving the aforementioned apparent contradictions.

The structure of the paper is as follows. In Section II, we establish the nematic-elastic bilinear in an isotropic medium, and elucidate how it renormalizes the bare electronic nematic free energy in the case of homogeneous deformation. In Section III, we contrast homogeneous with inhomogeneous deformations, and develop our theory of nematic elasticity while paying special attention to the Saint Venant compatibility relations. In this section we define our “helical basis” for nematic elasticity, and contrast it with the “ d -orbital” and Cartesian bases conventionally used in nematicity and elasticity problems, respectively. Starting in Section IV, we apply our helical basis to the problem of nematic elasticity, and find an anisotropic renormalization of the bare electronic mass in the isotropic elastic continuum. In Section IVB, we use the compatibility relations to prove that the anisotropic nematic mass suppresses incompatible electronic nematicity. From there, in Section V, we use this principle of incompatible nematic suppression to isolate the character of critical electronic nematic fluctuations in a 3D medium with only “polar” and “planar” momenta, and derive direction-selective criticality in the isotropic continuum explicitly. In Section VI, we incorporate elastic incompatibility, in the form of infinitesimal continuum plasticity, into our theory of nematic elasticity for applications in structurally disordered electronic nematics. We show that “nematic-plasticity” can only couple to the non-critical components of the helical nematic order parameter. The results indicate the protection of long-range nematic order despite short-range electronic nematic pinning by long-range structural disorder. We develop an analytically soluble model of disorder using an ensemble of uncorrelated straight edge dislocations and compute the disorder-averaged real-space correlation functions inevitably present for the local electronic nematic order parameters. We discuss our theory in the greater context of electronic nematic quantum materials in Section VII. Additionally, we provide various appendices (Appendices A–G) to supplement some calculations in the main text, including the solution for the

plasticity problem within the helical strain formalism for an elastic crystal of arbitrary symmetry (Appendix D) and the expansion of the elastic strain from a distribution of multipolar crystalline defects (Appendix F).

II. HOMOGENEOUS NEMATO-ELASTICITY

In this section, we begin the discussion by reviewing the simplest case of fluctuating *homogeneous* strains in an isotropic medium [39, 43, 51, 59, 107, 108]. The symmetry analysis serves as the foundation for the theory that incorporates spatially inhomogeneous strains throughout the rest of the paper. We show that fluctuating homogeneous strains renormalize the bare electronic nematic mass by introducing long-ranged, all-to-all, interactions with strength inversely proportional to the elastic shear modulus. We show that these interactions do not couple the nematic order parameters in the conventional d -orbital basis.

The electronic nematic order parameter in three spatial dimensions is defined as the local electronic quadrupolar density,

$$\varphi_{ij}(\mathbf{x}) = -\left\langle \hat{\psi}^\dagger(\mathbf{x}) \left(\partial_i \partial_j - \frac{1}{3} \nabla^2 \delta_{ij} \right) \hat{\psi}(\mathbf{x}) \right\rangle, \quad (6)$$

where $\hat{\psi}(\mathbf{x})$ is the many-body electronic wavefunction [3, 10, 46, 47]. Note that while the focus here is on the charge degrees of freedom, the expression above can be generalized in a straightforward way to include also spin, orbital, or superconducting degrees of freedom [9, 17, 35–38, 109–118]. In isotropic media, the components of φ_{ij} transform under rotations as the fivefold-degenerate $\ell = 2$ irreducible representation of $\text{SO}(3)$. The five nematic order parameters can be chosen to transform as the d -orbitals, $\{d_{z^2}, d_{x^2-y^2}, d_{2yz}, d_{2zx}, d_{2xy}\}$, and are likewise labeled with similar subscripts: $\varphi_{z^2}, \varphi_{x^2-y^2}$, etc., as is done in [47]. We construct these order parameters from the traceless φ_{ij} tensor according to the following convention:

$$\begin{aligned} \varphi_{z^2} &\equiv \frac{\varphi_{xx} + \varphi_{yy} - 2\varphi_{zz}}{\sqrt{3}}, & \varphi_{x^2-y^2} &\equiv \varphi_{xx} - \varphi_{yy}, \\ \varphi_{2yz} &\equiv 2\varphi_{yz}, & \varphi_{2zx} &\equiv 2\varphi_{zx}, & \varphi_{2xy} &\equiv 2\varphi_{xy}. \end{aligned} \quad (7)$$

These expressions define the *d-orbital basis* used in this paper and in Ref. [55]. In two spatial dimensions, the fivefold degeneracy of $\text{SO}(3)$ is split in $\text{SO}(2)$ into one $\ell = 0$ singlet, φ_{z^2} , an $\ell = 1$ doublet, $(\varphi_{2yz}, \varphi_{2zx})$, and an $\ell = 2$ doublet, $(\varphi_{x^2-y^2}, \varphi_{2xy})$. Given that in 2D, all derivatives with respect to z vanish, this implies that the $\ell = 1$ doublet vanishes identically: $\varphi_{2yz} = \varphi_{2zx} = 0$. The in-plane quadrupolar doublet, $(\varphi_{x^2-y^2}, \varphi_{2xy})$, accounts for the planar electronic nematic order parameters conventionally studied in quantum materials, despite most of them being 3D crystals.

The elastic strain tensor, ε_{ij} , being a rank-2 symmetric tensor itself, can be decomposed into symmetry-preserving and symmetry-breaking contributions that transform as $\ell = 0$ and $\ell = 2$ irreducible representations, respectively. Whereas the nematic order parameter is traceless by definition, the strain tensor has a nonzero trace, which quantifies the symmetry-preserving volume changes due to some distortion. In the elasticity literature, it is known as the *dilatation*

[88, 101, 102, 119]. Given that the dilatation does not break any symmetries, it cannot couple bilinearly to the electronic nematic order parameter. This contrasts with the symmetry-breaking *deviatoric* strains in the $\ell = 2$ irreducible representation. Strictly speaking, “deviatoric” refers to the traceless part of any tensor which encapsulates both the shear (off-diagonal) strains as well as the symmetry-breaking diagonal contributions [93, 119]. For brevity, we refer to both the diagonal and off-diagonal symmetry-breaking contributions as “deviatoric” strains. The strain tensor is then written as

$$\varepsilon_{ij} = \frac{1}{3}\varepsilon_0\delta_{ij} + \left(\varepsilon_{ij} - \frac{1}{3}\varepsilon_0\delta_{ij}\right), \quad (8)$$

where the first term contains the scalar dilatation strain, $\varepsilon_0 \equiv \text{Tr}(\varepsilon)$, and the second represents the symmetry-breaking deviatoric strain. The deviatoric strain, being a five-component $\ell = 2$ irreducible representation, can also be decomposed in the d -orbital basis as

$$\begin{aligned} \varepsilon_{z^2} &\equiv \frac{\varepsilon_{xx} + \varepsilon_{yy} - 2\varepsilon_{zz}}{\sqrt{3}}, & \varepsilon_{x^2-y^2} &\equiv \varepsilon_{xx} - \varepsilon_{yy}, \\ \varepsilon_{2yz} &\equiv 2\varepsilon_{yz}, & \varepsilon_{2yz} &\equiv 2\varepsilon_{zx}, & \varepsilon_{2xy} &\equiv 2\varepsilon_{xy}. \end{aligned} \quad (9)$$

The nematic-elastic contribution to the free energy, in an isotropic medium, takes the form

$$\Delta\mathcal{F}[\varphi_{ij}, \varepsilon_{ij}] \equiv -\lambda_0 \int_x \boldsymbol{\varphi}(x) \cdot \boldsymbol{\varepsilon}(x), \quad (10)$$

where λ_0 is the nematic-elastic coupling constant and $\int_x \equiv \int d^3x$. In the above, we vectorized the d -orbital basis as

$$\begin{aligned} \boldsymbol{\varphi} &\equiv \left(\varphi_{z^2}, \varphi_{x^2-y^2}, \varphi_{2yz}, \varphi_{2zx}, \varphi_{2xy}\right)^T, \\ \boldsymbol{\varepsilon} &\equiv \left(\varepsilon_{z^2}, \varepsilon_{x^2-y^2}, \varepsilon_{2yz}, \varepsilon_{2zx}, \varepsilon_{2xy}\right)^T, \end{aligned} \quad (11)$$

according to the Gell-Mann decomposition in Appendix A. The isotropic elastic free energy is given by

$$\mathcal{F}_{\text{elas}} = \frac{1}{2} \int_x \left\{ \lambda \varepsilon_0^2(x) + 2\mu \varepsilon_{ij}(x) \varepsilon_{ji}(x) \right\}, \quad (12)$$

where λ is the Lamé constant and μ is the shear modulus [45, 106]. Omitting the position dependence momentarily, the second term evaluates to $\varepsilon_{ij}\varepsilon_{ji} = \frac{1}{3}\varepsilon_0^2 + \frac{1}{2}(\boldsymbol{\varepsilon} \cdot \boldsymbol{\varepsilon})$ using Eq. (A6). Under homogeneous distortions, the total elastic part of the free energy, $\mathcal{F} = \mathcal{F}_{\text{elas}} + \Delta\mathcal{F}$, becomes

$$\mathcal{F} = V \left\{ \frac{1}{2} \left(\lambda + \frac{2\mu}{3} \right) \varepsilon_0^2 + \frac{1}{2} \mu (\boldsymbol{\varepsilon} \cdot \boldsymbol{\varepsilon}) - \lambda_0 (\bar{\varphi} \cdot \boldsymbol{\varepsilon}) \right\}, \quad (13)$$

where V is the volume and $\bar{\varphi}_a \equiv \frac{1}{V} \int_x \varphi_a(x)$. The spatial average, $\bar{\varphi}_a$, is proportional to the zero-momentum nematic order parameter, $\bar{\varphi}_a = \frac{1}{V} \varphi_{a,\mathbf{q}=0}$. Thermodynamic stability forces both the bulk modulus, $B \equiv \lambda + 2\mu/3$, and the shear modulus, μ , to be nonzero. Materials with positive Poisson ratios obey $B > \mu$, whereas so-called auxetic metamaterials can satisfy $B < \mu$ [45, 106]. In either case, a useful strict inequality is that

$$0 < \frac{4\mu}{3} < B + \frac{4\mu}{3} = \lambda + 2\mu. \quad (14)$$

Ferroelastic instabilities drive the renormalized shear modulus $\tilde{\mu}$ to zero, whether they be structurally driven [61–63] (proper ferroelastics) or electronically driven as in the case of electronic nematics [9, 11, 13] (pseudoproper ferroelastics). In the latter case, the soft electronic nematic fluctuations drive $\tilde{\mu} \rightarrow 0$, whereas the renormalized bulk modulus \tilde{B} remains nonzero. While that means the elastic medium is unstable to symmetry-breaking shear distortions, since $\tilde{B} > 0$, it remains stable against dilatation strain, indicating that these strains remain energetically expensive at the nematic-elastic transition.

Proceeding under the assumption that the ferroelastic transition is concomitant, then the bare elastic moduli are nonzero and the bare elastic free energy is stable at the harmonic level. One can then consider the correction to the nematic free energy due to fluctuating *homogeneous* strains. Minimizing with respect to the homogeneous strain yields an effective long-ranged nematic interaction of the form

$$\Delta\mathcal{F}_{\text{eff}}[\varphi] = -\frac{\lambda_0^2}{2\mu V} (\boldsymbol{\varphi}_{\mathbf{q}=\mathbf{0}} \cdot \boldsymbol{\varphi}_{\mathbf{q}=\mathbf{0}}) = -\frac{\lambda_0^2}{2\mu V} \int_{xx'} \boldsymbol{\varphi}(x) \cdot \boldsymbol{\varphi}(x'), \quad (15)$$

consistent with previous derivations within elastic crystals [39, 43, 51, 59, 60, 107]. In this derivation, however, the renormalization of the nematic mass is by fluctuating homogeneous strain in an *isotropic* medium. The only difference between this case and the crystalline cases is the number of components in the critical nematic irreducible representation. The bare shear modulus, μ , must also be adapted for the symmetry-breaking deviatoric strain in the same irreducible representation. The essential physics, regardless of the form of the correction, is clear even in the isotropic medium: homogeneous strains generate long-ranged, all-to-all, interactions for the electronic nematic order parameter which do not couple different nematic symmetry channels. While the last point regarding symmetry may seem obvious, it is not the case for fluctuating *inhomogeneous* strains. Indeed, as we show in this paper, the compatibility relations couple different nematic symmetry channels, *even in isotropic media*, with profound effects on nematic criticality.

III. INHOMOGENEOUS ELASTICITY AND TENSOR COMPATIBILITY

We show in this work that the simple, all-to-all symmetry-preserving, effective nematic interactions of the homogeneous deformation are replaced by more complex expressions when we consider inhomogeneous strains. In fact, we will obtain a more general form that contains the all-to-all interactions built in by taking the appropriate zero-momentum limit. The compatibility relations couple different nematic basis functions because they can couple the different strain components provided that the momentum transfer is not identically zero. Given that the degree of interdependence between the components is controlled by the momentum direction, in Subsection III A we use helicity to develop a basis for elasticity that is invariant with respect to changes in the momentum direction. We then apply the same “helical” basis for generic rank-2 symmetric tensors such as electronic nematicity in Subsection III B.

A. Helical Representation of the Strain Tensor

In an isotropic system, the wavevector \mathbf{q} provides an orthonormal basis $\{\hat{e}_1, \hat{e}_2, \hat{e}_3\}$ that can be obtained through a rotation $\mathcal{R}(\hat{q}) \equiv (\hat{e}_1 | \hat{e}_2 | \hat{e}_3)$ from any of the coordinate axes onto \hat{q} . For concreteness, we set $\hat{e}_1 = \hat{q}$, rendering the two other basis vectors as the azimuthal and spherical polar unit vectors, $\hat{e}_2 = \hat{e}_\phi$ and $\hat{e}_3 = -\hat{e}_\theta$, respectively. This leads to the rotation matrix

$$\mathcal{R}(\hat{q}) = \begin{pmatrix} \cos \phi \sin \theta & -\sin \phi & -\cos \phi \cos \theta \\ \sin \phi \sin \theta & \cos \phi & -\sin \phi \cos \theta \\ \cos \theta & 0 & \sin \theta \end{pmatrix}. \quad (16)$$

The helicity operator, $\mathfrak{h}(\hat{q})$, is defined in terms of the generators of rotations, $\{S_x, S_y, S_z\}$, as the scalar product [92, 95]:

$$\mathfrak{h}(\hat{q}) \equiv i\hat{q} \cdot \mathbf{S}. \quad (17)$$

When $\hat{q} = \hat{x}$, the helicity operator is simply iS_x , given as

$$\mathfrak{h}(\hat{q} = \hat{x}) = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & -i \\ 0 & i & 0 \end{pmatrix}, \quad (18)$$

which has the normalized eigenvectors

$$\hat{h}_0(\hat{q} = \hat{x}) = \hat{x}, \quad \hat{h}_\pm(\hat{q} = \hat{x}) = \frac{1}{\sqrt{2}} (\hat{y} \pm i\hat{z}), \quad (19)$$

with helical eigenvalues of $\{0, \pm 1\}$. These eigenvalues are the angular momenta with respect to the wavevector. Using the rotation matrix $\mathcal{R}(\hat{q})$, one can find the helical eigenvectors with respect to any other \hat{q} through

$$\hat{h}_0(\hat{q}) = \hat{e}_1, \quad \hat{h}_\pm(\hat{q}) = \frac{1}{\sqrt{2}} (\hat{e}_2 \pm i\hat{e}_3). \quad (20)$$

Inverting these expressions, the spherical basis vectors and helical basis vectors for arbitrary \hat{q} are related via

$$\begin{aligned} \hat{e}_1 &= \hat{q} = \hat{h}_0(\hat{q}), \\ \hat{e}_2 &= \frac{1}{\sqrt{2}} [\hat{h}_+(\hat{q}) + \hat{h}_-(\hat{q})], \\ \hat{e}_3 &= \frac{1}{i\sqrt{2}} [\hat{h}_+(\hat{q}) - \hat{h}_-(\hat{q})]. \end{aligned} \quad (21)$$

It is clear that the transverse unit vectors, $\hat{e}_{2,3}$, correspond to a linearly polarized helical basis, whereas \hat{h}_\pm are circularly polarized. However, in the isotropic medium, it is important to emphasize that any choice of two orthonormal vectors in the transverse plane to \hat{q} are degenerate with any other, reflecting a residual SO(2) symmetry about the \hat{q} axis, associated with different basis vectors in the transverse plane.

We now represent the (linear) strain tensor in this helical basis. In real-space, the strain tensor is given by Eq. (2). In Fourier space, the relationship between the strain and displacement vector amplitudes follows as

$$\varepsilon_{ij} \equiv \frac{i}{2} (q_j u_i + q_i u_j), \quad (22)$$

where we have omitted the explicit wavevector dependence of the displacement vector \mathbf{u} . In the linearly polarized helical

basis, we can expand the displacement vector into longitudinal and transverse components as

$$\varepsilon_1^h \equiv iq(\hat{e}_1 \cdot \mathbf{u}), \quad \varepsilon_2^h \equiv iq(\hat{e}_2 \cdot \mathbf{u}), \quad \varepsilon_3^h \equiv iq(\hat{e}_3 \cdot \mathbf{u}). \quad (23)$$

Using the transformation matrix in Eq. (16), and exploiting its orthogonality, it follows that

$$\boldsymbol{\varepsilon}_h = iq\mathcal{R}^T(\hat{q}) \cdot \mathbf{u}, \quad (24)$$

where $\boldsymbol{\varepsilon}_h = \{\varepsilon_1^h, \varepsilon_2^h, \varepsilon_3^h\}$ are the set of “helical strain” amplitudes. By inverting this expression, which holds at any $q > 0$, then the strain tensor can be written as

$$\varepsilon_{ij} = \frac{1}{2} (\hat{e}_{1,i} \hat{e}_{\beta,j} + \hat{e}_{1,j} \hat{e}_{\beta,i}) \varepsilon_\beta^h, \quad (25)$$

where we have used a Greek index to differentiate the helical indices 1, 2, 3 from the Cartesian components x, y, z .

Eq. (25) represents the helical representation of the strain tensor. It provides a map to the “Cartesian” representation of the strain amplitudes (left-hand side) from the one longitudinal and two transverse strains contained in $\boldsymbol{\varepsilon}_h$ – the linearly polarized “helical strains.” It is important to establish that the amplitudes at opposite momenta are related through

$$\begin{aligned} \hat{e}_\alpha(-\hat{q}) &= (-1)^{1+\delta_{\alpha,3}} \hat{e}_\alpha(\hat{q}), \\ \varepsilon_\alpha^h(-\hat{q}) &= (-1)^{\delta_{\alpha,3}} \varepsilon_\alpha^h(\hat{q})^*, \end{aligned} \quad (26)$$

where the asterisk denotes complex conjugation. The second equality follows from Eq. (23) and the fact that $u_i(-\mathbf{q}) = u_i(\mathbf{q})^*$, given the displacement vector is a real vector field in real-space. As a result, while $\varepsilon_{1,2}^h(\mathbf{x})$ are real in real-space, $\varepsilon_3^h(\mathbf{x})$ is purely imaginary. The strain tensor, meanwhile, must be real in real-space. Indeed, it follows from Eq. (25) and Eq. (26) that $\varepsilon_{ij}(-\hat{q}) = \varepsilon_{ij}(\hat{q})^*$.

From a symmetric perspective, Eq. (25) couples different irreducible representations for the strain at finite momentum. There is no contradiction with group theory, since the momentum-dependent pre-factors ensure that all symmetry transformation properties are preserved. Moreover, from Eq. (23), the longitudinal strain, ε_1^h , always transforms as a scalar whereas the two transverse strains, $\varepsilon_{2,3}^h$, transform together as a vectorial doublet under rotations in the transverse plane to \hat{q} . This contrasts with the Cartesian components of ε_{ij} which transform as various linear combinations of d -wave spherical harmonics. This coupling occurs because the wavevector breaks the SO(3) symmetry down to SO(2) through the formation of its little group, where the C_∞ axis of SO(2) is along \hat{q} . It is stressed that this happens at any nonzero q , and therefore only occurs for spatially modulated strains, regardless of how small $q \equiv |\mathbf{q}| > 0$ is. One contrasts this situation with the case of homogeneous strains where rotational isotropy is not broken by a wavevector.

B. Helical Gell-Mann Basis for Rank-2 Symmetric Tensors

The quadrupolar form factors in Eq. (25) couples the scalar dilatation strain, ε_1^h , with the transverse helical strains, $\varepsilon_{2,3}^h$,

when mapping them onto the usual Cartesian strain components, ε_{ij} . While these form factors completely cover all of linear elasticity, they do not form a complete basis of quadrupolar form factors in a five-dimensional vector space which describe arbitrary quadrupolar tensors, including electronic nematicity. In this subsection, we will define a complete basis for these form factors and use them in our discussion of nematicity in Section IV.

We define a symmetric quadrupolar tensor in the helical basis, $Q^{\alpha\beta}$, through its components as

$$Q_{ij}^{\alpha\beta}(\hat{q}) \equiv \frac{1}{2} (\hat{e}_{\alpha,j}\hat{e}_{\beta,i} + \hat{e}_{\alpha,i}\hat{e}_{\beta,j}). \quad (27)$$

The elastic form factors in Eq. (25) correspond to the case with $\alpha = 1$, allowing a concise way of writing the Cartesian components of the strain tensor as

$$\varepsilon_{ij} = Q_{ij}^{1\alpha}(\hat{q})\varepsilon_\alpha^h, \quad (28)$$

where summation over the repeated helical Greek indices is implied. Inverting the momentum direction, in accordance with Eq. (26), shows that this $Q^{\alpha\beta}$ tensor satisfies

$$Q_{ij}^{\alpha\beta}(-\hat{q}) = (-1)^{\delta_{\alpha,3} + \delta_{\beta,3}} Q_{ij}^{\alpha\beta}(\hat{q}). \quad (29)$$

For brevity, we will omit the explicit momentum dependence in the following, unless its role in the expressions is not clear. This tensor, $Q_{ij}^{\alpha\beta}$, is symmetric in both its Latin and Greek indices. The trace over the Latin indices follows as

$$\text{Tr}(Q^{\alpha\beta}) = \hat{e}_\alpha \cdot \hat{e}_\beta = \delta_{\alpha\beta}. \quad (30)$$

Likewise the trace over the product is

$$\text{Tr}(Q^{\alpha\beta}Q^{\gamma\delta}) = \frac{1}{2} (\delta_{\alpha\gamma}\delta_{\beta\delta} + \delta_{\alpha\delta}\delta_{\beta\gamma}). \quad (31)$$

From these expressions, we find that the three tensors relevant for elasticity, $\{Q^{11}, Q^{12}, Q^{13}\}$, are trace-orthogonal (see Eq. (B1)).

Given that Eq. (27) is symmetric in its Latin indices, it may be transformed into a vectorial representation with Eq. (A1):

$$\begin{aligned} Q_{ij}^{\alpha\beta} &= \frac{1}{3} Q_0^{\alpha\beta} \lambda_{ij}^0 + \frac{1}{2} \mathbf{Q}^{\alpha\beta} \cdot \boldsymbol{\lambda}_{ij}, \\ Q_0^{\alpha\beta} &= \text{Tr}(Q^{\alpha\beta}) = \delta_{\alpha\beta}, \\ \mathbf{Q}^{\alpha\beta} &= \text{Tr}(\boldsymbol{\lambda} Q^{\alpha\beta}) = \hat{e}_\alpha^T \cdot \boldsymbol{\lambda} \cdot \hat{e}_\beta, \end{aligned} \quad (32)$$

Likewise, from Eq. (A4) and Eq. (31), it follows that the Gell-Mann “quadrupolar vectors,” $\mathbf{Q}^{\alpha\beta}$, satisfy the following scalar product at every momentum, \hat{q} :

$$\mathbf{Q}^{\alpha\beta} \cdot \mathbf{Q}^{\gamma\delta} = \delta_{\alpha\gamma}\delta_{\beta\delta} + \delta_{\alpha\delta}\delta_{\beta\gamma} - \frac{2}{3}\delta_{\alpha\beta}\delta_{\gamma\delta}. \quad (33)$$

We recover a set of orthogonality conditions within the vectorial representation of these quadrupolar tensors. In particular,

\mathbf{Q}^{11} , \mathbf{Q}^{12} , and \mathbf{Q}^{13} are mutually orthogonal (see Eq. (B3)). From these vectors, one can write the strain as

$$\varepsilon_{ij} = \frac{1}{3}\varepsilon_1^h \lambda_{ij}^0 + \frac{1}{2} (\varepsilon_1^h \mathbf{Q}^{11} + \varepsilon_2^h \mathbf{Q}^{12} + \varepsilon_3^h \mathbf{Q}^{13}) \cdot \boldsymbol{\lambda}_{ij}. \quad (34)$$

We emphasize that there are six Cartesian components of the strain tensor, but they clearly only depend on three helical strains: one longitudinal and two transverse. This is reflected by the fact that, when written in the helical basis, the strain tensor automatically satisfies the Saint Venant compatibility relations. Indeed, an explicit calculation gives (see Appendix B):

$$\text{inc}(\mathbf{Q}^{\alpha\beta})_{ij} = -q^2 \varepsilon_{1\alpha\gamma} \varepsilon_{1\beta\gamma} Q_{ij}^{\gamma\delta}. \quad (35)$$

Therefore, using Eq. (28) and the anti-symmetric properties of the Levi-Civita symbol, it follows that $\text{inc}(\varepsilon)_{ij} = 0$. This result is of course the same as what one would obtain using the conventional basis for strain comprised of the displacement vector, Eq. (22). The utility of the helical basis is, however, that the helical strains are defined specifically in a coordinate system that co-rotates with the momentum. We can therefore always track the symmetry-preserving dilatation strain ε_1^h involved in nematicity through the momentum-dependence in Eq. (34). This is the main motivation to introduce the helical basis.

From Eq. (34), we see that, whereas the trace of the strain tensor only depends on the longitudinal strain, ε_1^h , the deviatoric part of the strain tensor, ε , depends on all three helical strain amplitudes, including the dilatation. The deviatoric strain, in the co-rotating vectorial representation, assumes the form

$$\varepsilon = \varepsilon_1^h \mathbf{Q}^{11} + \varepsilon_2^h \mathbf{Q}^{12} + \varepsilon_3^h \mathbf{Q}^{13}. \quad (36)$$

While these three quadrupolar vectors account for all of linear elasticity, they do not constitute a complete basis for electronic nematicity. Since the nematic vector in Eq. (11) is a five-component object, we define the nematic order parameter in the d -orbital basis in terms of projectors on the five orthonormal vectors, $\{\hat{\mathbf{Q}}_a\}$ that span the five-dimensional “nematic” vector space.

$$\boldsymbol{\varphi} = \sum_{a=1}^5 \Phi_a \hat{\mathbf{Q}}_a, \quad \Phi_a \equiv \hat{\mathbf{Q}}_a \cdot \boldsymbol{\varphi}, \quad (37)$$

These five orthonormal vectors are constructed in terms of the six components of $Q^{\alpha\beta}$ as shown in Appendix B and summarized in Eq. (B4). Because each of these five vectors co-rotate with the wavevector, their character and orthonormality is maintained for all $\mathbf{q} \neq \mathbf{0}$. Moreover, being orthonormal, their outer products satisfy the completeness relation:

$$\mathbf{I} = \sum_{a=1}^5 \hat{\mathbf{Q}}_a \hat{\mathbf{Q}}_a^T, \quad (38)$$

where \mathbf{I} is the 5×5 identity matrix.

The helical decomposition of the deviatoric strain tensor in this five-dimensional basis follows from Eq. (36) as

$$\boldsymbol{\varepsilon} \equiv \sum_{a=1}^5 \varepsilon_a \hat{\mathbf{Q}}_a = \left(\frac{2}{\sqrt{3}} \varepsilon_1^h \right) \hat{\mathbf{Q}}_1 + \varepsilon_2^h \hat{\mathbf{Q}}_2 + \varepsilon_3^h \hat{\mathbf{Q}}_3, \quad (39)$$

The difference between Eq. (36) and Eq. (39) is entirely within the contribution from the dilatation, given that $\hat{\mathbf{Q}}^{11}$ is not normalized, but $\hat{\mathbf{Q}}_1$ is. Thus, $\varepsilon_1 = \frac{2}{\sqrt{3}} \varepsilon_1^h$, $\varepsilon_{2,3} = \varepsilon_{2,3}^h$, and $\varepsilon_{4,5} = 0$. The five-component nematic order parameter, $\boldsymbol{\varphi}$, meanwhile, will be generally projected along all five $\hat{\mathbf{Q}}_a$ basis vectors. Even in an isotropic medium, this reduces the phase space of nematicity that benefits from nemato-elasticity. To see this, we write the nemato-elastic energy density from Eq. (10) in Fourier space. Given that both $\boldsymbol{\varphi}(\mathbf{x})$ and $\boldsymbol{\varepsilon}(\mathbf{x})$ are real fields, then for each d -orbital basis function, $\varphi_a(-\mathbf{q}) = \varphi_a(\mathbf{q})^*$ and $\varepsilon_a(-\mathbf{q}) = \varepsilon_a(\mathbf{q})^*$. Using the orthonormality of the helical $\hat{\mathbf{Q}}$ basis vectors, the nemato-elastic bilinear becomes

$$\begin{aligned} \lambda_0 \text{Re} \left(\boldsymbol{\varphi}^\dagger \cdot \boldsymbol{\varepsilon} \right) &= \lambda_0 \text{Re} \left(\sum_{a=1}^5 \Phi_a^* \varepsilon_a \right) \\ &= \lambda_0 \text{Re} \left(\frac{2}{\sqrt{3}} \Phi_1^* \varepsilon_1^h + \Phi_2^* \varepsilon_2^h + \Phi_3^* \varepsilon_3^h \right), \end{aligned} \quad (40)$$

for each nonzero wavevector, \mathbf{q} . Clearly, the full 3D rotational isotropy exhibited by the fivefold nematic degeneracy in the bare electronic theory is broken by coupling to the compatible strain tensor. This follows since the nonzero wavevector generates distinct effective ‘helical’ nemato-elastic couplings for the helical nematic order parameters. For $\Phi_{2,3}$, the coupling is unchanged between the d -orbital representation and the helical, whereas for Φ_1 , the effective coupling is $\frac{2}{\sqrt{3}} \lambda_0$, and it vanishes entirely for $\Phi_{4,5}$. In the case of $\Phi_{4,5}$, this means these nematic order parameters do not participate in nemato-elasticity at all, and they must reside in a nematic subspace that exists outside the domain of linear elasticity theory.

Before concluding this section, we point out that the co-rotating *vectorial* representation is easily transformed into a co-rotating *tensorial* representation using a basis of trace-orthonormal basis tensors, $\{\vartheta^a, a = 1, \dots, 5\}$. Indeed, it follows that Eq. (37) has an analogous tensorial decomposition. This tensorial representation will be much more convenient in discussing the role of nematic incompatibility, particularly in three spatial dimensions, as discussed in Section VI. The tensorial representation of Eq. (37) is given by

$$\begin{aligned} \varphi_{ij} &= \frac{1}{\sqrt{2}} \sum_{a=1}^5 \Phi_a \vartheta_{ij}^a, \quad \Phi_a = \sqrt{2} \text{Tr} (\vartheta^a \boldsymbol{\varphi}), \\ \text{Tr} (\vartheta^a) &= 0, \quad \text{Tr} (\vartheta^a \vartheta^b) = \delta_{ab}. \end{aligned} \quad (41)$$

This definition preserves the normalization of the nematic order parameter, $\boldsymbol{\varphi}^\dagger \cdot \boldsymbol{\varphi} = 2 \text{Tr} (\boldsymbol{\varphi}^\dagger \boldsymbol{\varphi})$ from Eq. (A4), using the same coefficients, $\{\Phi_a, a = 1, \dots, 5\}$, from the vectorial decomposition in Eq. (37). The basis tensors $\{\vartheta_a\}$ are related to the basis vectors $\{\hat{\mathbf{Q}}_a\}$ by substituting Eq. (37) into Eq. (A7) to obtain

$$\vartheta_{ij}^a = \frac{1}{\sqrt{2}} \left(\hat{\mathbf{Q}}_a \cdot \lambda_{ij} \right). \quad (42)$$

For completeness, we explicitly list these basis tensors in Appendix B in Eq. (B7). Importantly, these co-rotating tensors constitute a complete basis for rank-2 symmetric tensors at every momentum \mathbf{q} . Thus, if $A_{ij} = A_{ij}(\mathbf{q})$ is a rank-2 symmetric tensor at momentum, \mathbf{q} , then it can be written as

$$\begin{aligned} A_{ij} &= \frac{1}{3} (\text{Tr} A) \delta_{ij} + \frac{1}{\sqrt{2}} \sum_{a=1}^5 A_a \vartheta_{ij}^a, \\ A_a &= \sqrt{2} \text{Tr} (\vartheta^a A) = \hat{\mathbf{Q}}_a \cdot A. \end{aligned} \quad (43)$$

This decomposition can be viewed as a co-rotating generalization of Eq. (A1). Importantly, the characters of the coefficients, $\{\text{Tr} A, A_a\}$, remain invariant as the wavevector changes its direction in space.

IV. COMPATIBLE RESTRICTIONS ON ELECTRONIC NEMATIC FLUCTUATIONS

With the complete helical basis for electronic nematicity constructed, we apply it to the problem of nemato-elasticity in the isotropic continuum. Importantly, the character of the helical nematic order parameters, $\{\Phi_a\}$, will remain the same regardless of the momentum direction of the nematic fluctuations. Similarly, the helical nematic order parameters will only couple to helical strain amplitudes with the same character. This contrasts with the d -orbital basis, $\{\varphi_a\}$, where the compatibility relations couple the symmetry-breaking strains generated by electronic nematic fluctuations with symmetry-preserving dilatation strains from Eq. (36).

In Subsection IV A, we find the effective nematic free energy renormalized by thermally fluctuating elastostatic strain fields and show that even in the isotropic medium, one still recovers a set of constraints which splits the five-dimensional critical nematic manifold down to a two-dimensional one. In Subsection IV B, we show that these constraints are an expression of the geometry of elasticity theory through the suppression of *incompatible* electronic nematicity.

A. Renormalization of Electronic Nematic Mass in Isotropic Media

Before we begin, it is important to emphasize that an instability in a given nematic channel corresponds to the condensation of a subset of order parameters condensing in the d -orbital basis $\{\varphi_a\}$, whereas the nemato-elastic coupling is more clearly represented in the helical basis of nematic order parameters $\{\Phi_a\}$, as it accounts for the elastic compatibility relations in a consistent, $\hat{\mathbf{q}}$ -independent manner. Thus, our strategy is to integrate out the strain components in the helical basis first.

In an isotropic system, the nemato-elastic free energy in Eq. (12) diagonalizes within the helical basis, and assumes the

form

$$\mathcal{F}_{\text{elas}} = \frac{1}{2V} \sum_{\mathbf{q}} \left[(\lambda + 2\mu) |\varepsilon_1^h|^2 + \mu \sum_{\alpha=2,3} |\varepsilon_{\alpha}^h|^2 \right] - \frac{\lambda_0}{2V} \sum_{\mathbf{q}} \left(\frac{2}{\sqrt{3}} \Phi_1^* \varepsilon_1^h + \sum_{\alpha=2,3} \Phi_{\alpha}^* \varepsilon_{\alpha}^h + \text{c.c.} \right). \quad (44)$$

Minimizing the free energy with respect to the helical strain amplitudes yields the following equations of state

$$\varepsilon_1^h = \frac{2}{\sqrt{3}} \frac{\lambda_0}{\lambda+2\mu} \Phi_1, \quad \varepsilon_{2,3}^h = \frac{\lambda_0}{\mu} \Phi_{2,3}. \quad (45)$$

The minimization thus produces an effective correction to the electronic nematic free energy given by

$$\Delta \mathcal{F}_{\text{eff}} [\varphi] = -\frac{\lambda_0^2}{2V} \sum_{\mathbf{q}} \left\{ \frac{4|\Phi_1|^2}{3(\lambda+2\mu)} + \frac{1}{\mu} \sum_{\alpha=2,3} |\Phi_{\alpha}|^2 \right\}. \quad (46)$$

This term renormalizes the quadratic term of the bare isotropic nematic free energy in the d -orbital basis, yielding an effective nematic free energy of the form

$$\begin{aligned} \mathcal{F}_{\text{eff}} [\varphi] &= \mathcal{F}_{\text{nem}} [\varphi] + \Delta \mathcal{F}_{\text{eff}} [\varphi] \\ &= \frac{1}{2V} \sum_{\mathbf{q}} \varphi^{\dagger} \cdot \left\{ (r + q^2) \mathbf{I} - \mathcal{M}(\hat{q}) \right\} \cdot \varphi + \mathcal{O}(\varphi^3). \end{aligned} \quad (47)$$

In the bare free energy, $r > 0$ is the tuning parameter that triggers a continuous bare nematic transition at $r = 0$ (assuming that no higher order terms render the transition first-order). To obtain this expression, we simply used the definition in Eq. (37) to obtain the 5×5 direction-dependent nematic-mass-correction matrix

$$\mathcal{M}(\hat{q}) = \frac{\lambda_0^2}{\mu} \left(\hat{\mathbf{Q}}_2 \hat{\mathbf{Q}}_2^T + \hat{\mathbf{Q}}_3 \hat{\mathbf{Q}}_3^T + \varrho \hat{\mathbf{Q}}_1 \hat{\mathbf{Q}}_1^T \right). \quad (48)$$

The material-dependent nonuniversal ratio of the bare elastic constants, ϱ , is defined as

$$\varrho \equiv \frac{4\mu}{3(\lambda+2\mu)} \in (0, 1), \quad (49)$$

with the bounds obtained from the inequality in Eq. (14). We simplify this expression with Eq. (38), and obtain

$$\mathcal{M}(\hat{q}) = \frac{\lambda_0^2}{\mu} \left\{ \mathbf{I} - \left[(1-\varrho) \hat{\mathbf{Q}}_1 \hat{\mathbf{Q}}_1^T + \hat{\mathbf{Q}}_4 \hat{\mathbf{Q}}_4^T + \hat{\mathbf{Q}}_5 \hat{\mathbf{Q}}_5^T \right] \right\}. \quad (50)$$

This mass correction has two contributions: one isotropic in momentum and one anisotropic. Indeed, one observes that, upon substitution, the nematic free energy becomes

$$\begin{aligned} \mathcal{F}_{\text{eff}}^{(2)} [\varphi] &= \frac{1}{2V} \sum_{\mathbf{q}} \left(r - \frac{\lambda_0^2}{\mu} + q^2 \right) (\varphi^{\dagger} \cdot \varphi) \\ &\quad + \frac{1}{2V} \sum_{\mathbf{q}} \frac{\lambda_0^2}{\mu} \left\{ (1-\varrho) |\Phi_1|^2 + \sum_{\alpha=4,5} |\Phi_{\alpha}|^2 \right\}, \end{aligned} \quad (51)$$

truncated at second order. The isotropic part of the free energy, proportional to $\varphi^{\dagger} \cdot \varphi = \sum_{a=1}^5 |\Phi_a|^2$, enhances the bare nematic transition from $r = 0$ to $r_c \equiv \lambda_0^2/\mu$. This is consistent with the self-energy correction due to homogeneous distortions in Eq. (15). Being isotropic, this term does not couple the nematic basis functions in either the d -orbital or helical representations. The anisotropic part, however, *does* couple the nematic order parameter written in the d -orbital basis. Being the sum of non-negative numbers, the anisotropic term increases the energy of the nematic fluctuations. The *minimum* of the electronic nematic free energy thus *selects* the momentum directions that satisfy the following three constraints

$$\begin{aligned} \Phi_1 &= \hat{\mathbf{Q}}_1 \cdot \varphi = \sqrt{3} \text{Tr} \left(Q^{11} \varphi \right) = 0, \\ \Phi_4 &= \hat{\mathbf{Q}}_4 \cdot \varphi = 2 \text{Tr} \left(Q^{23} \varphi \right) = 0, \\ \Phi_5 &= \hat{\mathbf{Q}}_5 \cdot \varphi = \text{Tr} \left[\left(Q^{22} - Q^{33} \right) \varphi \right] = 0. \end{aligned} \quad (52)$$

These three constraints reduce the number of degenerate electronic nematic components from five to two, *even in an isotropic medium*. However, as long as these constraints are met, then the phase transition for the inhomogeneous strain case with $q > 0$ appears at the same value r_c as that computed for the homogeneous case with $q = 0$ (see Eq. (15)). Unlike the case of an order parameter that only couples to the fluctuating dilatation strain (see Appendix C), this mass renormalization is continuous at the origin, provided the three conditions in Eq. (52) are met. Thus, the homogeneous case is “built-in” to this more general form for inhomogeneous strain. The major physical difference between the inhomogeneous renormalization and the homogeneous renormalization, however, is the splitting of the fivefold nematic degeneracy clearly seen in the helical basis through the three conditions in Eq. (52).

Remarkably, the splitting of the helical order parameters in Eq. (52) is produced by the same symmetry-allowed nematic-elastic coupling as in the case of homogeneous deformations. Moreover, the splitting occurs for nematic-elasticity within an isotropic medium with full SO(3) rotational symmetry. The crucial difference between the homogeneous and inhomogeneous cases, however, is the presence of the wavevector in the latter, enforced by the compatible strain coupling to the nematic fluctuations. Without the displacement vector’s role as the vector-valued potential for the strain, and the subsequent compatibility relations it imposes on elasticity, one would expect the fivefold nematic degeneracy of an isotropic system to persist, as is the case for homogeneous deformations.

To understand how the wavevector changes the rotational symmetry of the isotropic medium, we consider its (rotational) little group – defined by the rotations that leave the wavevector invariant [120, 121]. This corresponds to SO(2) with the rotational axis being parallel to $\hat{q} = \hat{e}_1$. Within the little group, the fivefold degeneracy of the helical order parameters is split. This is evident from the distinct nematic-elastic couplings in the helical representation, written in Eq. (40). The (Φ_2, Φ_3) doublet retains the λ_0 coupling constant experienced by *all* five d -orbital order parameters, whereas the Φ_1 component couples to the dilatation strain with strength $\frac{2}{\sqrt{3}}\lambda_0$, and the (Φ_4, Φ_5)

doublet loses its coupling to the strains outright. This hierarchy arises from the little group's SO(2) symmetry, where the equivalence between the $\hat{e}_1, \hat{e}_2, \hat{e}_3$ directions is clearly broken given the \hat{e}_1 -vector's invariance. Because of this, the helical nematic order parameters are also inequivalent. For example, because the quantity Φ_1 only depends on \hat{e}_1 , it transforms as a "scalar", i.e., an angular-momentum-projection zero ($m = 0$ irreducible representation of SO(2)). In contrast, the transverse vectors \hat{e}_2 and \hat{e}_3 together constitute the $m = 1$ irreducible representation of SO(2) at each momentum. The doublet $\Phi_{2,3}$ thus transforms as a "vector" within the little group of the wavevector, given its dependence on the tensor product of \hat{e}_1 with either \hat{e}_2 or \hat{e}_3 . Finally, the remaining (Φ_4, Φ_5) doublet transforms as a "quadrupole" ($m = 2$ irreducible representation), since it depends on tensor products of \hat{e}_2 and \hat{e}_3 .

Given that the helical nematic order parameters are split into inequivalent irreducible representations, it is instructive to understand how this inequivalence affects the low-energy degrees of freedom at the nematic critical point. This is the subject of the remainder of this paper. Up to now, what we have been established is that the fivefold degeneracy of the nematic order parameters is lost. Of the original five nematic degrees of freedom, Eq. (52) establishes that fluctuations of the (Φ_2, Φ_3) "vectorial doublet" cause an instability. Meanwhile, the $\Phi_{1,4,5}$ order parameters remain gapped, because of their coupling with dilatation strain (Φ_1) or their oblivion to compatible strains ($\Phi_{4,5}$). However, from the definition of the helical order parameters in Eq. (37), the d -orbital content of the non-critical helical order parameters change as the momentum changes. This strongly suggests that whether a given d -orbital nematic order parameter, such as $\varphi_{2,xy}$, softens at the nematic critical point depends on the direction of its momentum. This restriction will occur even in the absence of crystalline anisotropy. This is the basis of the direction-selective criticality discussed in more details in the next section.

Before moving onto the next subsection, we comment on nemato-elastic criticality in the d -orbital basis. Specifically, we compute the static nematic susceptibilities for each order parameter in the d -orbital basis,

$$\begin{aligned} \chi_{aa}(\mathbf{q}) &\equiv \frac{1}{T} \langle \varphi_a(\mathbf{q}) \varphi_a(-\mathbf{q}) \rangle \\ &= \frac{1}{T} \sum_{b,c=1}^5 \hat{Q}_{b,a}(\hat{\mathbf{q}}) \hat{Q}_{c,a}(\hat{\mathbf{q}}) \langle \Phi_b(\mathbf{q}) \Phi_c(\mathbf{q})^* \rangle. \end{aligned} \quad (53)$$

where T is the temperature. Writing the effective nematic free energy of Eq. (51) first in the helical basis, we find

$$\begin{aligned} \mathcal{F}_{\text{eff}}^{(2)}[\varphi] &= \frac{1}{2V} \sum_{\mathbf{q}} \tilde{r}_c(\mathbf{q}) \sum_{a=2,3} |\Phi_a|^2 \\ &\quad + \frac{1}{2V} \sum_{\mathbf{q}} \left\{ \tilde{r}_1(\mathbf{q}) |\Phi_1|^2 + r(\mathbf{q}) \sum_{\alpha=4,5} |\Phi_\alpha|^2 \right\}, \end{aligned} \quad (54)$$

where $r(\mathbf{q}) \equiv r + q^2$, $\tilde{r}_1(\mathbf{q}) \equiv r(\mathbf{q}) - \lambda_0^2 \varrho / \mu$, and $\tilde{r}_c(\mathbf{q}) \equiv r(\mathbf{q}) - \lambda_0^2 / \mu$. We note that these inverse susceptibilities obey a strict hierarchy: $\tilde{r}_c(\mathbf{q}) < \tilde{r}_1(\mathbf{q}) < r(\mathbf{q})$ for all \mathbf{q} (since $\varrho < 1$

in Eq. (49)). In the helical representation, we observe that the effective nematic free energy is diagonal, and therefore

$$\langle \Phi_b(\mathbf{q}) \Phi_c(\mathbf{q})^* \rangle \propto \delta_{bc} \langle |\Phi_b(\mathbf{q})|^2 \rangle. \quad (55)$$

Substituting this result into Eq. (53), the static susceptibilities in the d -orbital basis follow as

$$\begin{aligned} \chi_{aa}(\mathbf{q}) &\equiv \frac{\hat{Q}_{2,a}^2(\hat{\mathbf{q}}) + \hat{Q}_{3,a}^2(\hat{\mathbf{q}})}{r(\mathbf{q}) - \lambda_0^2 / \mu} \\ &\quad + \frac{\hat{Q}_{1,a}^2(\hat{\mathbf{q}})}{r(\mathbf{q}) - \lambda_0^2 \varrho / \mu} + \frac{\hat{Q}_{4,a}^2(\hat{\mathbf{q}}) + \hat{Q}_{5,a}^2(\hat{\mathbf{q}})}{r(\mathbf{q})}. \end{aligned} \quad (56)$$

As the system is tuned from the isotropic phase across the nematic transition, the leading divergence will occur in the first term, arising from the compatible helical nematic fluctuations. This term is maximized for momentum directions where the form factors $\hat{Q}_{2,a}^2(\hat{\mathbf{q}})$ and $\hat{Q}_{3,a}^2(\hat{\mathbf{q}})$ are maximal. Thus, at the transition, the fluctuations in the d -orbital basis are dominated by the critical fluctuations of the helical amplitudes $\Phi_{2,3}$. However, it is also clear, meanwhile, that this equivalence only exists at the largest length scales: when $q \rightarrow 0$ along these selected momentum directions. Generally, however, d -orbital nematic fluctuations at any length scale will be a linear combination of all of the helical nematic fluctuations. This behavior distinguishes macroscopic long-wavelength electronic nematicity from mesoscopic short-wavelength electronic nematicity.

B. Suppression of Incompatible Electronic Nematicity

The nematic propagator will become critical first only along momentum directions where $\Phi_1 = \Phi_4 = \Phi_5 = 0$, from Eq. (52). It therefore stands to question exactly what each of these projections in the co-rotating helical basis represent physically. The first, Φ_1 , follows from Eq. (45) as a symmetry-preserving dilatation stress that, in the long-wavelength limit, corresponds to energetically expensive volume changes of the medium associated with the bulk modulus.

However, there are no equations of state to define the amplitudes $\Phi_{4,5}$, both of which remain un-condensed at nemato-elastic criticality. To gain insight, we use Eq. (41). By Fourier transforming the incompatibility operator from Eq. (1), we obtain

$$\text{inc}(A)_{ij} = -\epsilon_{ikl}\epsilon_{jmn}q_k q_m A_{ln}, \quad (57)$$

where A_{ij} is an arbitrary second-rank tensor.

When the incompatibility operator acts on ϑ_{ij}^a , it will act on the various components of Q_{ij}^{ab} , through Eq. (B7). Applying Eq. (35) to the helical basis tensors establishes that $\{Q^{1\alpha}, \alpha = 1, 2, 3\}$, Q^{23} , and $Q^{22} - Q^{33}$ are eigentensors of the incompatibility operator (see Eq. (B11)). The set $\{Q^{1\alpha}, \alpha = 1, 2, 3\}$ has vanishing incompatiblity, whereas the latter two tensors each have eigenvalue $q^2 > 0$. Additionally, we observe that the incompatibility of the identity tensor at $\hat{\mathbf{q}}$

is

$$\text{inc}(\mathbf{I})_{ij} = q^2 \left(Q_{ij}^{11} - \delta_{ij} \right). \quad (58)$$

Unlike the $Q^{\alpha\beta}$ tensors, the identity is not an eigentensor of the incompatibility operator.

Using these identities, the incompatibility of the $\{\theta^a\}$ tensors follows straightforwardly (see Eq. (B13)). Thus, the incompatibility of a generic rank-2 symmetric tensor, A , is

$$\text{inc } A = \frac{1}{3} \left(\text{Tr } A - \frac{\sqrt{3}}{2} A_1 \right) \text{inc}(\mathbf{I}) + \frac{q^2}{\sqrt{2}} \left(A_4 \vartheta^4 + A_5 \vartheta^5 \right). \quad (59)$$

Applying the incompatibility operator to the electronic nematic order parameter, we find that

$$\text{inc}(\varphi) = -\frac{1}{2\sqrt{3}} \Phi_1 \text{inc}(\mathbf{I}) + \frac{q^2}{\sqrt{2}} \left(\Phi_4 \vartheta^4 + \Phi_5 \vartheta^5 \right). \quad (60)$$

The conclusion is, therefore, that arbitrary electronic nematic fluctuations will have *incompatible* contributions – those that *cannot* be written as a symmetric derivative of some vector field. These are clearly the eigentensor components $\Phi_{4,5}$ which, along with the volume-changing dilatations Φ_1 , are suppressed when the system undergoes nematico-elastic criticality. The Φ_1 amplitude also reflects a degree of *incompatible* electronic nematicity. This is despite Q^{11} appearing in the strain tensor (Eq. (34)), which is, by definition, *compatible*. The reason for this behavior is because the nematic order parameter is strictly traceless, whereas the strain tensor has a trace: the dilatation. Indeed, using Eq. (59) for the strain tensor, we immediately see that $\text{inc}(\varepsilon) = 0$, since

$$\text{Tr } \varepsilon = \varepsilon_1^h = \frac{\sqrt{3}}{2} \varepsilon_1, \quad \varepsilon_4 = \varepsilon_5 = 0. \quad (61)$$

Thus, it is the dilatation that renders the strain compatible, whereas the Φ_1 contribution of nematicity reflects its intrinsic incompatibility as a traceless tensor.

Likewise, it is important to note that if a rank-2 symmetric tensor, B , is *completely incompatible*, then it must be true that $B_1 = 0$, just as $B_2 = B_3 = 0$. Therefore, the symmetric tensor

$$B_{ij} = \frac{1}{3} (\text{Tr } B) \delta_{ij} + \frac{1}{\sqrt{2}} \left(B_4 \vartheta_{ij}^4 + B_5 \vartheta_{ij}^5 \right), \quad (62)$$

is a tensor with zero compatibility. Note that, just as a completely compatible tensor has only three independent components, so too does a completely incompatible tensor.

To contextualize this tensor analysis within electronic nematics, the completely incompatible contributions to $\varphi_{ij}, \Phi_{4,5}$, are the most suppressed because they do not participate in nematico-elasticity. The helical “scalar” component, Φ_1 , is partially incompatible, and is therefore also suppressed because its compatible contribution induces costly dilatation strain, as is evident from the appearance of ϱ in Eq. (51). The critical nematico-elastic order parameters are only the completely compatible contributions to nematicity: $\Phi_{2,3}$. It is only the condensation of these fields that will drive the nematico-elastic instability in the long-wavelength limit. This can be understood in the following way. Because electronic nematic fluctuations induce compatible strains, they induce the vector-valued displacement field that serves as the vector-valued potential for the strain tensor. In turn, the critical tensor-valued electronic nematicity must itself be compatible. Hence, the critical nematic tensor itself must be proportional to the symmetric gradient of that same vector-valued potential field. Therefore, the planar constraints on critical nematicity in Eq. (52) arise to suppress *incompatible* electronic nematicity. We have thus established that electronic nematicity inherits the compatibility relations of elasticity theory even in the isotropic continuum. It thereby follows that these same restrictions are enforced within the crystalline point groups that comprise actual quantum materials.

V. DIRECTION-SELECTIVE NEMATIC CRITICALITY IN THE ISOTROPIC MEDIUM

Given the previous discussion of the suppression of incompatible nematicity, it is insightful to consider two limiting cases, defined by particular orientations of the momentum \mathbf{q} . The first is the “polar” limit where the critical wavevector is confined to a single direction. The second is the “planar” limit where the critical wavevector is free to rotate within a plane. This second limit corresponds to the case when the wavevector lies entirely within the xy -plane.

By considering these two cases, we will establish direction-selective electronic nematic criticality within an isotropic elastic medium. We will show that because the d -orbital content of the helical nematic order parameters explicitly depends on the momentum, and that the critical manifold is spanned only by (Φ_2, Φ_3) , then the orientation of the critical nematic director relative to its momentum will be constrained.

Generally speaking, we write the transformation between the helical and d -orbital nematic order parameters from Eq. (37) as $\boldsymbol{\varphi} \equiv \mathbb{D}(\hat{\mathbf{q}}) \cdot \boldsymbol{\Phi}$, where the columns of the 5×5 orthogonal matrix, $\mathbb{D}(\hat{\mathbf{q}})$, are the co-rotating $\{\hat{\mathbf{Q}}_a, a = 1, \dots, 5\}$ basis vectors. Written explicitly, where $\hat{\mathbf{q}} = (\cos \phi \sin \theta, \sin \phi \sin \theta, \cos \theta)$, the matrix is

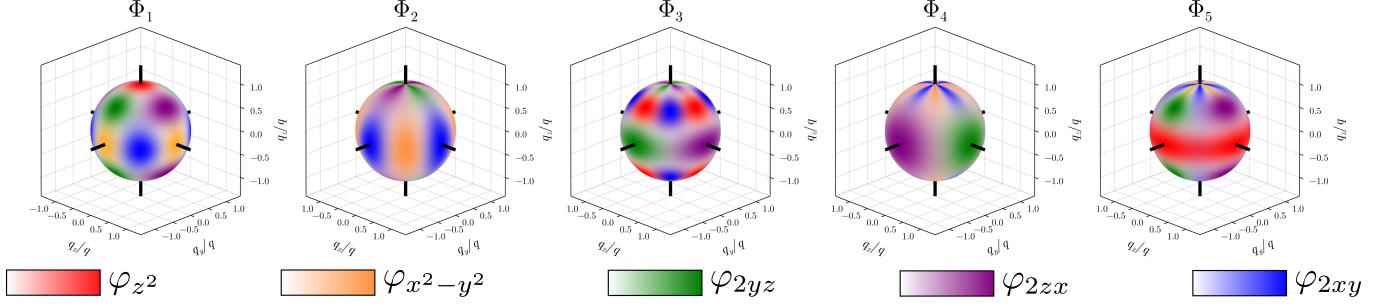


FIG. 2. Linear transformation from the d -orbital nematic basis, φ , into the helical basis, Φ , as functions of the wavevector, \mathbf{q} . The $\Phi_{1,2,4}$ panels are also shown in Ref. [55]. Each panel visualizes the square-amplitude $(\hat{Q}_{a,b})^2$ to determine the contribution to the Φ_a helical order parameter from the φ_b d -orbital order parameter. For Φ_3 , the φ_{z^2} and $\varphi_{x^2-y^2}$ (φ_{2xy}) amplitudes have coincident maximum magnitude along, for example, the [101] ([111]) directions.

$$\begin{aligned} \mathbb{D}(\hat{\mathbf{q}}) &= (\hat{\mathbf{Q}}_1 | \hat{\mathbf{Q}}_2 | \hat{\mathbf{Q}}_3 | \hat{\mathbf{Q}}_4 | \hat{\mathbf{Q}}_5) \\ &= \begin{bmatrix} -\frac{1+3\cos 2\theta}{4} & 0 & -\frac{\sqrt{3}}{2} \sin 2\theta & 0 & \frac{\sqrt{3}}{2} \sin^2 \theta \\ \frac{\sqrt{3}}{2} \cos 2\phi \sin^2 \theta & -\sin 2\phi \sin \theta & -\frac{1}{2} \cos 2\phi \sin 2\theta & \sin 2\phi \cos \theta & -\frac{1}{4} \cos 2\phi (3 + \cos 2\theta) \\ \frac{\sqrt{3}}{2} \sin \phi \sin 2\theta & \cos \phi \cos \theta & -\sin \phi \cos 2\theta & \cos \phi \sin \theta & \frac{1}{2} \sin \phi \sin 2\theta \\ \frac{\sqrt{3}}{2} \cos \phi \sin 2\theta & -\sin \phi \cos \theta & -\cos \phi \cos 2\theta & -\sin \phi \sin \theta & \frac{1}{2} \cos \phi \sin 2\theta \\ \frac{\sqrt{3}}{2} \sin 2\phi \sin^2 \theta & \cos 2\phi \sin \theta & -\frac{1}{2} \sin 2\phi \sin 2\theta & -\cos 2\phi \cos \theta & -\frac{1}{4} \sin 2\phi (3 + \cos 2\theta) \end{bmatrix}. \quad (63) \end{aligned}$$

The inverse mapping from the usual d -orbital basis into the co-rotating helical basis for nematicity is given concisely as $\Phi = \mathbb{D}^T(\hat{\mathbf{q}}) \cdot \varphi$. The individual elements of \mathbb{D} can therefore be interpreted as an ‘overlap amplitude’ identifying how strongly each d -orbital order parameter, φ_b , contributes to the helical order parameter, Φ_a , at each wavevector, $\hat{\mathbf{q}}$. In Fig. 2 we visualize this mapping by fixing the d -orbital nematic order parameter and then plotting the square amplitude for each of the helical basis functions. These square amplitudes are the same as the form factors that appear in the d -orbital nematic susceptibilities from Eq. (56), though in that case we used the elements of the $\mathbb{D}(\hat{\mathbf{q}})$ matrix, rather than $\mathbb{D}^T(\hat{\mathbf{q}})$ matrix. For instance, to show the contribution of φ_{z^2} to each of the helical order parameters $\Phi_{1,\dots,5}$, in Fig. 2, we fix $\varphi = (1, 0, 0, 0, 0)^T$, and then compute $\Phi = \mathbb{D}^T(\hat{\mathbf{q}}) \cdot \varphi = \hat{\mathbf{Q}}_1$. The resulting colormap shows $(\hat{Q}_{1,a})^2$ on the sphere for each Φ_a . The same procedure follows for the other four d -orbital nematic basis functions in the figure.

The phenomenon of direction-selective nematic criticality follows directly from Fig. 2. As explained above, the nematic instability is described by the condensation of a symmetry-

breaking order parameter φ_a in the d -orbital basis. Because of the nematico-elastic coupling, this instability is achieved along certain directions for which the overlap between φ_a and the three incompatible nematic order parameters in the helical basis $\Phi_{1,4,5}$ vanish. In other words, the instability is set by the momenta for which $(\hat{Q}_{1,a})^2 = (\hat{Q}_{3,a})^2 = (\hat{Q}_{5,a})^2 = 0$. Take, for instance, the case of Ising-nematicity φ_{2xy} on a tetragonal lattice. Clearly, from Fig. 2, these conditions are satisfied when the momentum direction $\hat{\mathbf{q}}$ lies along the [100] and [010] directions. Note also that, along these directions, there is a perfect overlap between φ_{2xy} and Φ_2 . Furthermore, because of the mutual orthogonality of the helical basis vectors, $\{\hat{\mathbf{Q}}_a\}$, if there is perfect overlap between φ_{2xy} and Φ_2 , that means that φ_{2xy} is orthogonal to *all other* helical order parameters: Φ_1, Φ_3, Φ_4 and Φ_5 .

To make broader statements about 3D nematico-elastic criticality, one must compute the volume-changing and incompatible contributions to the helical electronic nematic order parameter arising from the d -orbital order parameters. We obtain:

$$\Phi_1 = -\frac{1}{4}\varphi_{z^2}(1+3\cos 2\theta) + \frac{\sqrt{3}}{2}\sin \theta \left\{ \sin \theta \left(\varphi_{x^2-y^2} \cos 2\phi + \varphi_{2xy} \sin 2\phi \right) + 2\cos \theta \left(\varphi_{2yz} \sin \phi + \varphi_{2zx} \cos \phi \right) \right\}, \quad (64)$$

$$\Phi_4 = \sin \theta \left(\varphi_{2yz} \cos \phi - \varphi_{2zx} \sin \phi \right) + \cos \theta \left(\varphi_{x^2-y^2} \sin 2\phi - \varphi_{2xy} \cos 2\phi \right), \quad (65)$$

$$\Phi_5 = \sin \theta \left\{ \frac{\sqrt{3}}{2}\varphi_{z^2} \sin \theta + \cos \theta \left(\varphi_{2yz} \sin \phi + \varphi_{2zx} \cos \phi \right) \right\} - \frac{3+\cos 2\theta}{4} \left(\varphi_{x^2-y^2} \cos 2\phi + \varphi_{2xy} \sin 2\phi \right). \quad (66)$$

To proceed, it is convenient to treat separately two different limits, which we dub “polar” and “planar”. In the polar limit, we fix the wavevector to be nearly coincident with the z -axis. Then, using $\theta = \delta\theta \ll 1$ with $\phi \in [0, 2\pi)$, the expressions for the incompatible contributions to nematicity follow as

$$\begin{aligned}\Phi_1(\theta = \delta\theta) &= -\varphi_{z^2} + O(\delta\theta), \\ \Phi_4(\theta = \delta\theta) &= \varphi_{x^2-y^2} \sin 2\phi - \varphi_{2xy} \cos 2\phi + O(\delta\theta), \\ \Phi_5(\theta = \delta\theta) &= -\left(\varphi_{x^2-y^2} \cos 2\phi + \varphi_{2xy} \sin 2\phi\right) + O(\delta\theta).\end{aligned}\quad (67)$$

Since the nematico-elastic contribution to the free energy, Eq. (51), enforces that these three components vanish, we conclude that $\varphi_{z^2} = 0$, $\varphi_{x^2-y^2} = 0$, and $\varphi_{2xy} = 0$ in the polar limit. In other words, an electronic nematic instability with wavevector close to the q_z -axis can only take place in the channels φ_{2xz} and φ_{2yz} . Thus, writing the polar momentum as $\hat{q}_\perp \equiv \delta\theta(\hat{x} \cos \phi + \hat{y} \sin \phi) + \hat{z} + O(\delta\theta^2)$, the effective free energy in Eq. (51) reduces to

$$\mathcal{F}_{\text{eff}}^{(2)}[\varphi] \rightarrow \frac{1}{2V} \sum_{\mathbf{q}_\perp} \left(r - \frac{\lambda_0^2}{\mu} + q^2\right) \left(|\varphi_{2yz}|^2 + |\varphi_{2zx}|^2\right), \quad (68)$$

where the summation over wavevectors is constrained to the infinitesimal spherical cap centered on \hat{z} . The direction selectivity of the nematic instability is clear. When the momentum is constrained to the \hat{z} -axis, the fivefold degeneracy of the electronic nematic order parameter is broken down to twofold. In turn, the resulting critical nematic fluctuations, through Eq. (45) and Eq. (25), induce only the strain tensor components $\varepsilon_{yz} \propto \varphi_{2yz} \neq 0$ and $\varepsilon_{zx} \propto \varphi_{2zx} \neq 0$. Along these critical momentum directions, one can take the limit $q \rightarrow 0$ to obtain the macroscopic shear distortion of the lattice induced by nematicity and recover the same strained medium as in the homogeneous limit Eq. (15). Thus the limiting case of homogeneous deformation is contained within the more general inhomogeneous case.

These conditions show that if the critical momentum direction is along \hat{z} , then the critical nematic manifold in the d -orbital basis is spanned by the out-of-plane doublet $\varphi_\perp^\text{T} \equiv (\varphi_{2zx}, \varphi_{2yz})$. The unit director associated with these nematic components, \mathcal{N} , can be written in terms of the spherical polar angles α and β in the Cartesian coordinates as

$$\mathcal{N} \equiv (\cos \alpha \sin \beta, \sin \alpha \sin \beta, \cos \beta)^\text{T}. \quad (69)$$

Identifying the electronic nematic tensor in Cartesian coordinates as $\varphi_{ij} \equiv \varphi_\perp(\mathcal{N}_i \mathcal{N}_j - \frac{1}{3} \delta_{ij})$ [47] shows that the critical doublet can be written as

$$\varphi_\perp = \varphi_\perp \sin(2\beta) (\cos \alpha, \sin \alpha)^\text{T}. \quad (70)$$

Substituting this expression into Eq. (68) yields a free energy density given by

$$f_{\text{eff}}^{(2)}[\varphi_\perp] = \left(r - \frac{\lambda_0^2}{\mu} + q^2\right) \sin^2(2\beta) |\varphi_\perp|^2. \quad (71)$$

Above the transition, $r > \lambda_0^2/\mu$, $\langle \varphi_\perp \rangle = 0$. However, below the transition, $r < \lambda_0^2/\mu$, and the electronic nematic condenses with

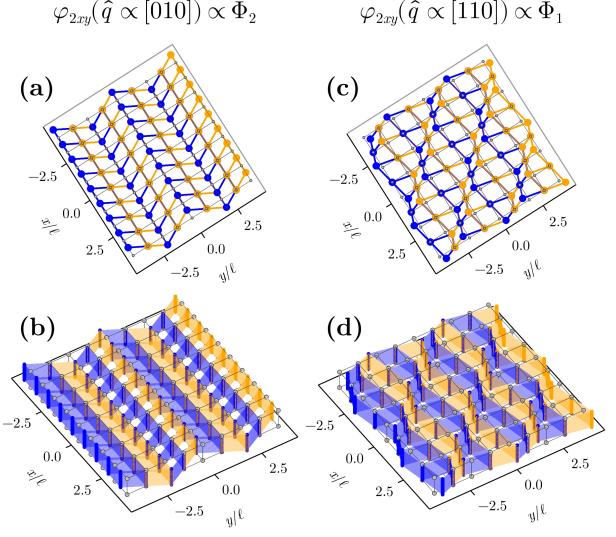


FIG. 3. Elastic deformations of a lattice in the presence of a compatible planar φ_{2xy} nematic order parameter with well-defined momentum, \mathbf{q} . In all figures, the modulation is sinusoidal, with identical amplitudes that are greatly exaggerated for visualization purposes. The equilibrium positions are indicated by the gray points, and the displaced locations are shown in blue and orange, obtained from solving the nematico-elastic equations of state, Eq. (45). The contrast of blue and orange is solely to emphasize displacements of volume elements of linear size ℓ . Top-down (a) and side (b) views of the strained three-dimensional isotropic medium undergoing a critical φ_{2xy} fluctuation mode, proportional to the helical Φ_2 nematic amplitude with $\hat{q} \propto [010]$. Top-down (c) and side (d) views of a non-critical φ_{2xy} fluctuation mode, proportional to the helical Φ_1 nematic amplitude with $\hat{q} \propto [110]$. The suppression of the φ_{2xy} wave in (c,d) is apparent from the accompanying dilatation strain, whereas the critical wave in (a,b) does not induce local-volume changes.

$\langle \varphi_\perp \rangle \neq 0$, allowing for a well-defined director angle. At the mean-field level, the director will lie along $\beta = \pi/4$ such that $\sin^2(2\beta)$ is maximized. This defines the nematic director to be at 45° relative to the momentum direction, $\hat{q} = \hat{z}$. This example illustrates the emergence of direction-selective criticality in an isotropic medium. We note that the lack of an α -dependence in the free energy reflects the residual $\text{SO}(2)$ symmetry in the isotropic medium associated with rotations about \hat{z} .

Expressing the two helical order parameters in terms of the d -orbital basis and the director, with Eq. (63), one obtains

$$\begin{aligned}\Phi_2 &= \varphi_{2yz} \cos \phi - \varphi_{2zx} \sin \phi = \varphi_\perp \sin(\alpha - \phi), \\ \Phi_3 &= -\varphi_{2yz} \sin \phi - \varphi_{2zx} \cos \phi = -\varphi_\perp \cos(\alpha - \phi),\end{aligned}\quad (72)$$

where we used the fact that $\beta = \pi/4$ and $\hat{q} = \hat{z}$. It follows then that certain momentum directions, encoded in ϕ , map the helical order parameters uniquely onto the individual d -orbital order parameters – even on the spherical cap in the polar limit that we are considering. For example, taking the momentum to lie along $[\delta\theta, 0, 1]$, i.e., $\phi = 0$ and infinitesimal $\delta\theta$, yields $\Phi_2 \propto \varphi_{2yz}$ and $\Phi_3 \propto \varphi_{2zx}$.

By rotating the momentum away from the polar limit, one further expects the critical nematic director to remain oriented

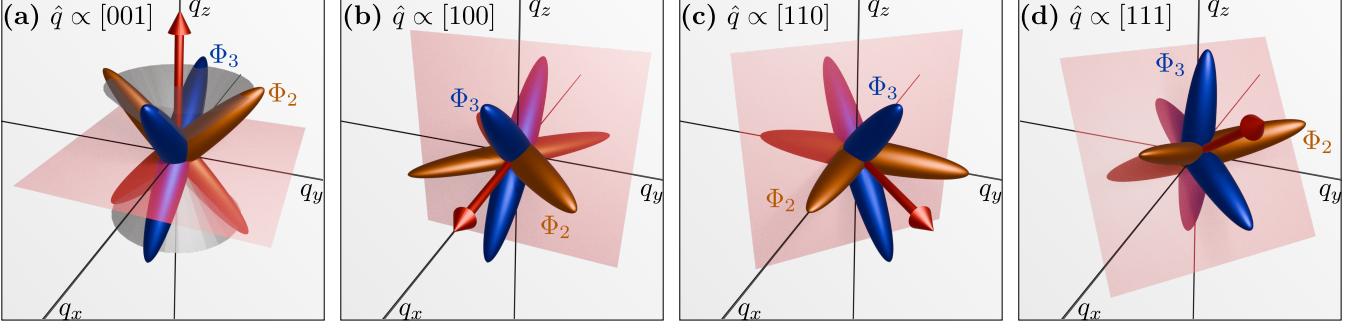


FIG. 4. Schematic of universal direction-selective nematic criticality induced by elastic compatibility. Each panel shows different nematic momenta directions, \hat{q} , as the red arrow. The orange and blue ellipsoids represent the possible critical (Φ_2, Φ_3) helical nematic order parameters for a given momentum direction. The semi-major axes of the ellipsoids are oriented parallel to the critical directors in the d -orbital basis selected by the specified momenta. Note that the critical director can point in any direction along the cone spanned by the blue and orange ellipsoids, shown explicitly in (a). Nematic directors that lie in the plane transverse to the momentum (red) are incompatible (Φ_4, Φ_5). (a) When the critical momentum is polar, $\hat{q} \propto [001]$, the $(\varphi_{2yz}, \varphi_{2zx})$ d -orbital order parameters span the critical nematic manifold, with directors aligned along the $[011]$ and $[101]$ axes, respectively. (b,c) When the critical momentum is in the plane, there is an in-plane director and an out-of-plane director. (b) For $\hat{q} \propto [100]$ (or $[010]$), the in-plane critical nematic order parameter is φ_{2xy} . (c) When $\hat{q} \propto [110]$ (or $[1\bar{1}0]$), the critical in-plane nematic order parameter is $\varphi_{x^2-y^2}$. (d) By rotating the critical momentum in the full 3D space, while the corresponding nematic orientations change in the d -orbital basis, it is always the (Φ_2, Φ_3) helical doublet which spans the critical manifold.

at 45° relative to the critical momentum directions. We show that this remains true in the more familiar planar limit, with critical momenta in the (q_x, q_y) plane, $\hat{q} = \hat{x} \cos \phi + \hat{y} \sin \phi$. Eq. (64), Eq. (65), and Eq. (66) now become

$$\begin{aligned}\Phi_1(\theta = \frac{\pi}{2}) &= \frac{1}{2}\varphi_{z^2} + \frac{\sqrt{3}}{2}\mathfrak{D}^T(\phi) \cdot \boldsymbol{\varphi}_{||}, \\ \Phi_4(\theta = \frac{\pi}{2}) &= (\hat{z} \times \hat{e}_1) \cdot \boldsymbol{\varphi}_{\perp}, \\ \Phi_5(\theta = \frac{\pi}{2}) &= \frac{\sqrt{3}}{2}\varphi_{z^2} - \frac{1}{2}\mathfrak{D}^T(\phi) \cdot \boldsymbol{\varphi}_{||},\end{aligned}\quad (73)$$

where $\mathfrak{D}^T(\phi) \equiv (\cos 2\phi, \sin 2\phi)$, $\boldsymbol{\varphi}_{||}^T \equiv (\varphi_{x^2-y^2}, \varphi_{2xy})$, and $\boldsymbol{\varphi}_{\perp}$ is the same out-of-plane doublet used in the polar limit. The effective nematic free energy in Eq. (51) takes the form

$$\begin{aligned}\mathcal{F}_{\text{eff}}^{(2)}[\boldsymbol{\varphi}] \rightarrow \frac{1}{2V} \sum_{\mathbf{q}_{||}} \Bigg\{ &\left(r - \frac{\lambda_0^2}{\mu} + q^2\right) (\boldsymbol{\varphi}^\dagger \cdot \boldsymbol{\varphi}) \\ &+ \frac{\lambda_0^2}{\mu} \left(1 - \frac{3\varrho}{4}\right) |\mathfrak{D}^T(\phi) \cdot \boldsymbol{\varphi}_{||}|^2 \\ &+ \frac{\lambda_0^2}{\mu} \left[(1 - \varrho) |\varphi_{z^2}|^2 + |\hat{e}_2 \cdot \boldsymbol{\varphi}_{\perp}|^2 \right] \\ &- \frac{\varrho\sqrt{3}}{4} \left[\varphi_{z^2}^* \mathfrak{D}^T(\phi) \cdot \boldsymbol{\varphi}_{||} + \text{c.c.} \right] \Bigg\}. \quad (74)\end{aligned}$$

In the third line above, we simplified the condition that $\Phi_4 = 0$ since $\hat{z} \times \hat{e}_1 = \hat{e}_2$ when $\hat{q} = \hat{e}_1$ is in the xy -plane. From these expressions, we see that nematic-elastic criticality will occur only when $\varphi_{z^2} = 0$, $\mathfrak{D}^T(\phi) \cdot \boldsymbol{\varphi}_{||} = 0$, and $\hat{e}_2 \cdot \boldsymbol{\varphi}_{\perp} = 0$. Clearly, the planar limit selects only nematic instabilities with $\varphi_{z^2} = 0$. Meanwhile, the second condition is known from two-dimensional hexagonal systems as ‘‘nematic-orbital’’ coupling that renormalizes the 3-state Potts nematic director [51]. It is identical to the 2D compatibility relation in Eq. (5) with the deviatoric and shear strain amplitudes replaced by the d -orbital

$\varphi_{x^2-y^2}$ and φ_{2xy} amplitudes, respectively. In a similar spirit to the polar limit, we recast the two-component in-plane nematic order parameter in terms of an amplitude and the director \mathcal{N} as

$$\boldsymbol{\varphi}_{||} \equiv \varphi_{||} \sin^2(\beta) (\cos 2\alpha, \sin 2\alpha)^T. \quad (75)$$

The second constraint becomes

$$\mathfrak{D}^T(\phi) \cdot \boldsymbol{\varphi}_{||} = \varphi_{||} \sin^2(\beta) \cos(2\phi - 2\alpha) = 0, \quad (76)$$

restricting the nematic director’s orientation in terms of the momentum direction, namely, $\alpha = \phi \pm \pi/4$. We demonstrate the deformation generated by a static planar nematic wave in a 3D isotropic medium in Fig. 3 by showing the simplified case of a tetragonal-to-orthorhombic φ_{2xy} -nematic, corresponding to $\alpha = \pi/4$. There is a clear difference between the nematic-elastic strain induced by planar modulations along critical directions ($\varphi_{2xy} \propto \Phi_2$) with that induced by modulation along non-critical directions ($\varphi_{2xy} \propto \Phi_1$). In the latter case, $\mathfrak{D}(\pi/4) \cdot \boldsymbol{\varphi}_{||} \neq 0$ because local dilatation strains accompany the shear strain, as is required by the compatibility relations and the helical equations of state in Eq. (45). The lattice displacement vector in the figure is obtained by directly integrating the sinusoidal strain wave, as was done for a purely 2D system in Ref. [57].

Returning to Eq. (74), the third condition, $\hat{e}_2 \cdot \boldsymbol{\varphi}_{\perp} = 0$, is a new type of nematic-orbital coupling for out-of-plane nematics, which is absent in the two-dimensional theory. Returning to the out-of-plane director, $\boldsymbol{\varphi}_{\perp}$, expressed in terms of the director \mathcal{N} , this third condition yields

$$\hat{e}_2 \cdot \boldsymbol{\varphi}_{\perp} = \boldsymbol{\varphi}_{\perp} \sin(2\beta) \sin(\alpha - \phi) \quad (77)$$

with the solution being that $\alpha = \phi$, showing that the out-of-plane director lies in the (\hat{e}_1, \hat{z}) -plane.

Enforcing $\varphi_{z^2} = 0$, these expressions can be reduced to an effective free energy for a 3D electronic nematic solely experiencing in-plane critical momenta:

$$\begin{aligned} \mathcal{F}_{\text{eff}}^{(2)} [\boldsymbol{\varphi}] \rightarrow & \frac{1}{2V} \sum_{\mathbf{q}_\parallel} \left\{ \left(r - \frac{\lambda_0^2}{\mu} + q^2 \right) (\boldsymbol{\varphi}_\parallel^\dagger \cdot \boldsymbol{\varphi}_\parallel) \right. \\ & + \frac{\lambda_0^2}{\mu} \left(1 - \frac{3\varrho}{4} \right) |\mathfrak{D}^T(\phi) \cdot \boldsymbol{\varphi}_\parallel|^2 \\ & + \left(r - \frac{\lambda_0^2}{\mu} + q^2 \right) (\boldsymbol{\varphi}_\perp^\dagger \cdot \boldsymbol{\varphi}_\perp) \\ & \left. + \frac{\lambda_0^2}{\mu} |\hat{\mathbf{e}}_2 \cdot \boldsymbol{\varphi}_\perp|^2 \right\}. \end{aligned} \quad (78)$$

Thus, the nematic order parameter, which is fivefold degenerate in the bare theory, splits into two twofold degenerate irreducible representations. The first one deals with the familiar planar nematic order parameters in $\boldsymbol{\varphi}_\parallel$, whereas the second one corresponds to the out-of-plane nematics $\boldsymbol{\varphi}_\perp$ with in-plane spatial modulations. Each of these irreducible representations is then further constrained by the derivative-dependent nematic-orbital couplings, $\mathfrak{D}^T(\phi) \cdot \boldsymbol{\varphi}_\parallel = 0$ and $\hat{\mathbf{e}}_2 \cdot \boldsymbol{\varphi}_\perp = 0$. This ultimately yields two separate critical compatible nematic directors, both lying in planes that contain \hat{q} . Indeed, treating these directors separately, the in-plane director maximizes the free energy below the transition for $\beta = \pi/2$, while the out-of-plane director does so for $\beta = \pi/4$. Thus, the directors can be expressed in terms of the in-plane momentum azimuthal angle ϕ as $\mathcal{N}_\parallel = (\cos(\phi \pm \pi/4), \sin(\phi \pm \pi/4), 0)$ and $\mathcal{N}_\perp = \frac{1}{\sqrt{2}}(\cos \phi, \sin \phi, 1)$. Calculating the angle between these directors and the in-plane momentum $\hat{q}_\parallel = (\cos \phi, \sin \phi, 0)$ gives:

$$\hat{q}_\parallel \cdot \mathcal{N}_\parallel = \hat{q}_\parallel \cdot \mathcal{N}_\perp = \frac{1}{\sqrt{2}}, \quad (79)$$

establishing that both directors are individually constrained at an angle of 45° relative to the momentum. Neither lie in the transverse plane to \hat{q} , as these directors would generate nematic incompatibility, which must be suppressed across the phase transition.

Fig. 4 combines the polar and planar limits discussed in this section to illustrate schematically how the critical nematic directors \mathcal{N} are fixed for a given momentum \hat{q} . The director orientations are shown as the semi-major axes of the ellipsoids. The orientation of the electronic nematic director \mathcal{N} is fixed to be on a cone that makes an angle of 45° relative to the momentum. In this regard, one can interpret this effect as a “precession” of the nematic director around the momentum \hat{q} induced by the elastic compatibility, resembling how a magnetic moment precesses around a magnetic field. Note that this critical cone rotates about the momentum \hat{q} . Regardless of the momentum, however, the critical modes are *always* spanned by the helical doublet (Φ_2, Φ_3) . Note that a director lying in the transverse plane to the momentum induces incompatible nematicity, encoded in the doublet (Φ_4, Φ_5) , which cost energy according to Eq. (51). Conversely, a director \mathcal{N} that is parallel to the momentum \hat{q} induces dilatation, encoded by

Φ_1 , which also incurs an energy cost. The fact that the critical nematic manifold is restricted by the wavevector, even in the isotropic continuum, is a consequence of the elastic compatibility relations, and will be inevitable in crystalline systems. In those systems, while the discrete rotational symmetry further splits the degeneracy between the *d*-orbital nematic order parameters, it will not change the meaning of the helical order parameters relative to the wavevector.

VI. ELASTIC INCOMPATIBILITY AND EMERGENT NEMATO-PLASTICITY

Our investigation of the role of tensor compatibility in nematic-elasticity showed that the electronic nematic order parameter inherits the constraints imposed by the compatibility relations. Moreover, we found that the requirement to suppress incompatible electronic nematic fluctuations led to the universal phenomenon of direction-selective criticality. In elasticity theory, it is well-known how to incorporate incompatible strains, which arise in the regime of plastic deformation by crystalline defects [88–90, 92, 95–104]. The goal of this section is to incorporate incompatible elastic strains into our theory of nematic-elasticity.

We first provide a brief review in Subsection VI A of the details of plasticity, viewed as a “defect gauge theory” [103, 122]. Our review will follow the notation given in both Mura’s and Kleinert’s textbooks, Refs. [90] and [92], respectively, and occasionally draw upon the approaches to continuum plasticity in [88, 89, 99–102, 123].

In subsection VI B, we demonstrate how to incorporate defect gauge theory into the helical strain formalism developed for nematic-elasticity. We show that the anisotropic contribution to the electronic nematic mass renormalization in Eq. (50) specifically projects out the incompatible part of the nematic tensor. Moreover, we show that the non-critical incompatible electronic nematic order parameters experience plastic strains as a conjugate field, whereas the compatible critical electronic nematic order parameters are insensitive to plastic defects. This further distinguishes mesoscopic electronic nematicity in the *d*-orbital representation from the macroscopic critical helical electronic nematic orders. Finally, we study an ensemble of straight edge dislocations as an analytically tractable example of a plastic strains in Subsection VI C, and use the helical formalism to compute their impact on the *d*-orbital electronic nematic order parameters as a random conjugate field.

A. Incompatible Elasticity and the Defect-Density Tensor

Even in the limit of infinitesimal deformations, not all strains in a crystal are compatible. In particular, in the presence of crystalline defects, the elastic strain tensor, now denoted by the script \mathcal{E}_{ij} , is incompatible [88, 90, 92, 99–102]. Incompatible strains emanate from defects such as disclinations, dislocations, vacancies, and interstitials [88–90, 124]. Whatever the defects are, they define a new equilibrium state for the medium that has been plastically deformed away from the ideal case. In

this new equilibrium state, these defects are “stress-free,” and any stresses within the material further deform the medium away from this new “defective equilibrium” [88, 90].

Quantitatively, one measures the deformation relative to this new defective equilibrium. Thus, the elastic strain is modified to

$$\mathcal{E}_{ij}(\mathbf{x}) \equiv \varepsilon_{ij}(\mathbf{x}) - \varepsilon_{ij}^P(\mathbf{x}) = \frac{1}{2} [\partial_j u_i(\mathbf{x}) + \partial_i u_j(\mathbf{x})] - \varepsilon_{ij}^P(\mathbf{x}), \quad (80)$$

where ε_{ij} denotes the compatible “total strain” tensor and ε_{ij}^P is the “plastic strain” tensor generated by the defects. Note that ε_{ij}^P is the strain measured with respect to the ideal, defect-free, limit. Hooke’s Law for stress is also expressed relative to the new defective equilibrium and takes the form

$$\sigma_{ij}(\mathbf{x}) = C_{ijkl} \mathcal{E}_{kl}(\mathbf{x}) = C_{ijkl} [\varepsilon_{kl}(\mathbf{x}) - \varepsilon_{kl}^P(\mathbf{x})], \quad (81)$$

where σ_{ij} is the stress tensor [88, 90, 92]. Since the total strain is compatible, it follows that the incompatibility of the elastic strain, η_{ij} , is given by

$$\eta_{ij}(\mathbf{x}) \equiv \text{inc}[\mathcal{E}(\mathbf{x})]_{ij} = -\text{inc}[\varepsilon^P(\mathbf{x})]_{ij}. \quad (82)$$

This tensor, η_{ij} , is known as the defect density tensor, and is related to the disclination density, Θ_{ij} , and the dislocation density, α_{ij} , as described in detail in references [90, 92, 95, 99–102].

The presence of incompatible strains generated by defects leads to an additional gauge redundancy in elasticity [92, 103, 123]. This becomes apparent by considering that the physical content encoded by the plastic strain tensor is contained in Eq. (82). In words, the incompatible contribution to the observable elastic strain, \mathcal{E} , defines the incompatible contribution to the plastic strain tensor. Therefore, one can add any compatible tensor to the plastic strain and obtain the same defect density. This is analogous to adding an arbitrary gradient to the vector potential of magnetostatics, $\mathbf{A}(\mathbf{x})$, and obtaining the exact same static magnetic field, $\mathbf{B}(\mathbf{x}) = \nabla \times \mathbf{A}(\mathbf{x})$, indicating that only the curl of the vector potential is physical. Since this gauge redundancy in plasticity occurs because of the inclusion of the plastic strain tensor, the resulting theory is called the “defect gauge theory” of plasticity [92, 95, 103, 122, 123, 125].

However, adding an arbitrary compatible tensor to $\varepsilon^P(\mathbf{x})$ in Eq. (80) will clearly change the observable elastic strain, unless the total strain is modified in a gauge-covariant manner. That is to say, the following local gauge transformations

$$\begin{aligned} \varepsilon_{ij}^P(\mathbf{x}) &\rightarrow [\varepsilon_{ij}^P(\mathbf{x})]' = \varepsilon_{ij}^P(\mathbf{x}) - \frac{1}{2} [\partial_j \Lambda_i(\mathbf{x}) + \partial_i \Lambda_j(\mathbf{x})], \\ \varepsilon_{ij}(\mathbf{x}) &\rightarrow [\varepsilon_{ij}(\mathbf{x})]' = \varepsilon_{ij}(\mathbf{x}) - \frac{1}{2} [\partial_j \Lambda_i(\mathbf{x}) + \partial_i \Lambda_j(\mathbf{x})], \\ \mathcal{E}_{ij}(\mathbf{x}) &\rightarrow [\mathcal{E}_{ij}(\mathbf{x})]' = \mathcal{E}_{ij}(\mathbf{x}), \end{aligned} \quad (83)$$

leave the stress state of the system invariant. In the above, we have used the position-dependent vector, $\Lambda(\mathbf{x})$, to denote the potential for the compatible tensor in the defect gauge transformation. Comparing with Eq. (80), one can write an equivalent gauge-covariant derivative for the displacement vector, \mathbf{u} , as

$$\partial_j u_i(\mathbf{x}) \rightarrow [\partial_j u_i(\mathbf{x})]' = \partial_j u_i(\mathbf{x}) - \partial_j \Lambda_i(\mathbf{x}), \quad (84)$$

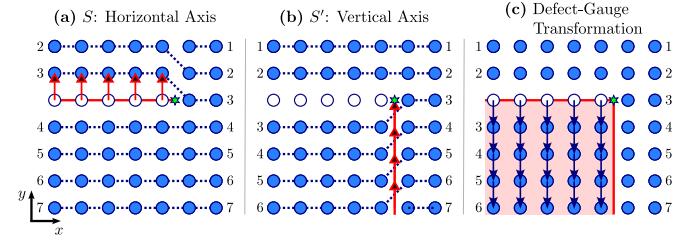


FIG. 5. Defect-gauge transformation acting on a straight edge dislocation. In each figure, the dislocation core is the green star. The Burgers vector is represented by the red vertical arrows and the crystal planes in the dislocated medium are numbered. (a) The Volterra surface is taken along the leftward horizontal axis, S , creating a discontinuous upward jump in the 3, 2, and 1, crystal planes, as read from right-to-left. (b) An equivalent Volterra surface is drawn vertically, S' , now leading to a downward jump of planes 3-7, read from right-to-left. Both S and S' are anchored to the dislocation core (green star) and have the same Burgers vector. (c) The appropriate defect-gauge transformation, as described in the text, amounts to a redefinition of the crystal planes around the defect core, effectively displacing all sites within the volume enclosed by S and S' . This physically equivalent redefinition of the displacement vector exemplifies defect gauge redundancy.

where the defect-gauge covariant derivative, \mathcal{D}_i , is defined by $\mathcal{D}_j u_i(\mathbf{x}) \equiv \partial_j u_i(\mathbf{x}) - \partial_j \Lambda_i(\mathbf{x})$ [92, 123]. The second term $\partial_j \Lambda_i$ that acts as the defect-gauge field is known as the “plastic distortion” tensor, β_{ij}^P , and its symmetric part is the plastic strain tensor, ε_{ij}^P .

These gauge transformations reflect the fact that, in order to describe an incompatible tensor in terms of a displacement vector, the latter needs to be multivalued. In other words, if we obtain a vector field, \mathbf{v} , such that $2\mathcal{E}_{ij}(\mathbf{x}) = \partial_j v_i(\mathbf{x}) + \partial_i v_j(\mathbf{x})$, then one can always shift it by a single-valued vector field $\Lambda(\mathbf{x})$ and obtain the same defect density. This problem is endemic in chemically pure media, whether isotropic or crystalline, since every constituent element, or unit cell, is indistinguishable from any other. In this regard, the multivaluedness reflects an ambiguity in uniquely assigning an equilibrium position of such constituents in a defective medium. The gauge field formalism simply avoids the need for multivalued functions [92].

From the perspective of the defects, this gauge ambiguity can be understood with the example of Volterra cutting surfaces in the elastic continuum that define dislocations and disclinations. In particular, if one keeps the defect lines (or cores) fixed, these cutting surfaces can be translated and rotated without affecting the defect density tensor [92, 99–103], as shown with the example case of a straight edge dislocation in Fig. 5. In this light, these defect surfaces are unphysical, but the defect lines are physically observable objects [45]. Within the context of geometry, the Volterra process of removing (or adding) material to a simply-connected domain renders it multiply-connected. An application of Weingarten’s Theorem to the Volterra surfaces in an elastic continuum establishes that, since the compatibility conditions are satisfied everywhere other than the Volterra surface, the displacement

vector can discontinuously change across that surface by no more than a translation and rigid rotation [92, 99, 102]. These define the Burgers vector, \mathbf{b} , and Frank vector, $\boldsymbol{\Omega}$, of the dislocation and disclination, respectively. This plastic jump in the displacement vector takes the form

$$\Delta u_i^P(\mathbf{x} \in S) = b_i + \epsilon_{ijk}\Omega_j x_k, \quad (85)$$

where S is the Volterra cutting surface. In the above, we have also assumed that the defect line intercepts the origin. By integrating this field (or its curl) over any closed circuit around the defect line, one obtains the Burgers (or Frank) vector, establishing these as the topological defects of elasticity [45, 92, 96, 97]. In Fig. 5(a), we show how a straight edge dislocation with a core aligned along the \hat{z} -axis is formed from a Volterra surface S , taken to be the xz plane. The third crystal plane of atoms – those that lie along the Volterra surface – is “removed” in order to plastically deform the defect-free medium into the dislocated medium. The Burgers vector is given by $\mathbf{b} = \hat{y}$, indicating that in the deformed medium, the third crystal plane is discontinuously translated vertically in the figure.

While the Volterra surface in Fig. 5(a) is sufficient, it is not unique. The same topological vectors, \mathbf{b} and $\boldsymbol{\Omega}$, can be obtained with a different Volterra surface, S' , provided that is also pinned to the same defect line. One can show that this change in surface amounts to a redefinition of the plastic displacement by a single-valued vector field [92]. We illustrate a special case of this transformation in Fig. 5 for the case of the straight edge dislocation. Comparing Figs. 5(a) and (b), the dislocation core is fixed, as indicated by the green star, but the Volterra surface is changed from the xz (S) plane to the yz plane (S'). As shown in the figure, while the result is a relabeling of which atoms in the dislocated medium correspond to the third through seventh crystal planes, the actual physical state of the dislocated medium is identical to that shown in Fig. 5(a). The only difference is a relabeling of the atomic positions. Given that this change in Volterra surface only changes the plastic displacement, u^P , by a single-valued vector field, it amounts to a *compatible* change in plastic strain. Thus, it is not a physical change of the system because it does not change the *incompatibility* of the elastic strain. The single-valued vector field constituting the unphysical, *compatible*, change to the plastic strain is shown in Fig. 5(c) everywhere within the red highlighted region.

This concludes our brief review of the gauge theory of defects in the limit of infinitesimal continuum elasticity. For completeness, we show how to use the helical formalism to obtain the elastic strain fields, $\mathcal{E}_{ij}(\mathbf{x})$, and total strain fields, $\varepsilon_{ij}(\mathbf{x})$, generated by the plastic strain tensor, $\varepsilon_{ij}^P(\mathbf{x})$, for a medium of arbitrary symmetry in Appendix D. The helical elastic strain Fourier amplitudes sourced by the plastic strain follows from Eq. (D5) as

$$\mathcal{E}_{ij} = \left[Q_{ij}^{1\alpha} \mathcal{S}_{\alpha\beta}(\hat{q}) Q_{lk}^{1\beta} C_{klmn} - \frac{1}{2} (\delta_{im}\delta_{jn} + \delta_{in}\delta_{jm}) \right] \varepsilon_{mn}^P, \quad (86)$$

in a medium with elastic constants C_{klmn} . As shown in Appendix D, the quantity $\mathcal{S}_{\alpha\beta}$ is the “helical compliance matrix,”

defined by

$$S_{\alpha\beta}(\hat{q}) \left(Q_{ji}^{1\beta} C_{ijkl} Q_{kl}^{1\gamma} \right) \equiv \delta_{\alpha\gamma}. \quad (87)$$

As proven in Appendix D, the elastic strain tensor \mathcal{E}_{ij} identically vanishes if the incompatibility of the plastic strain vanishes, $\text{inc}(\varepsilon^P)_{ij} = 0$, regardless of the elastic medium’s symmetry. Therefore, the defect gauge formalism isolates only the physical incompatibility contained within the plastic strain, ε_{ij}^P . In the special case of an isotropic medium, we find

$$\mathcal{E}_{ij} = \frac{1}{3} \varrho \Delta_p \delta_{ij} - \frac{1}{\sqrt{2}} \left[(1 - \varrho) \Delta_p \vartheta_{ij}^1 + \sum_{a=4,5} \varepsilon_a^P \vartheta_{ij}^a \right], \quad (88)$$

where ϱ is defined in Eq. (49) and $\Delta_p \equiv \frac{\sqrt{3}}{2} \varepsilon_1^P - \varepsilon_0^P$ quantifies the incompatible part of the plastic dilatation, $\varepsilon_0^P \equiv \text{Tr}(\varepsilon^P)$ (see Eq. (59)). As before, $\varepsilon_a^P \equiv \hat{Q}_a \cdot \varepsilon^P = \sqrt{2} \text{Tr}(\vartheta^a \varepsilon^P)$ are the components of the plastic strain in the helical basis.

B. Incompatible Electronic Nematicity and Defects

One of the central results of the previous section was that, in the presence of defects and plastic strains, only the combination $\mathcal{E}_{ij}(\mathbf{x}) \equiv \varepsilon_{ij}(\mathbf{x}) - \varepsilon_{ij}^P(\mathbf{x})$ is gauge invariant and therefore observable. Returning to nematic elasticity, given that electronic nematicity is observable, it can only couple to the components of the *elastic* strain tensor \mathcal{E}_{ij} . Hence, in materials with structural defects, one must generalize the bilinear $\varphi(\mathbf{x}) \cdot \varepsilon(\mathbf{x})$ to $\varphi(\mathbf{x}) \cdot \mathcal{E}(\mathbf{x})$. Using the Gell-Mann decomposition of a tensor, Eq. (A1), one finds that the nematico-elastic bilinear assumes the form: $\varphi(\mathbf{x}) \cdot \mathcal{E}(\mathbf{x}) = \varphi(\mathbf{x}) \cdot \varepsilon(\mathbf{x}) - \varphi(\mathbf{x}) \cdot \varepsilon^P(\mathbf{x})$. The elastic free energy density, in real-space, is then

$$f_{\text{elas}}(\varphi, \mathcal{E}) = \frac{1}{2} \left\{ \left(\lambda + \frac{2\mu}{3} \right) [\text{Tr} \mathcal{E}(\mathbf{x})]^2 + \mu \mathcal{E}(\mathbf{x}) \cdot \mathcal{E}(\mathbf{x}) \right\} - \lambda_0 \varphi(\mathbf{x}) \cdot \mathcal{E}(\mathbf{x}). \quad (89)$$

The difference between the defect-free case is the presence of two additional sources of total strain: plastic deviatoric *and* plastic dilatation strain.

After expanding the plastic strain tensor in the helical representation from Eq. (D7) and Eq. (D8), the nematico-elastic bilinear becomes

$$\begin{aligned} \varphi^\dagger \cdot \mathcal{E} &= \sum_{a=1}^5 \Phi_a^* \mathcal{E}_a \\ &= \frac{2}{\sqrt{3}} \Phi_1^* \left(\varepsilon_1^h - \varepsilon_0^P - \Delta_p \right) \\ &\quad + \sum_{\alpha=2,3} \Phi_\alpha^* \left(\varepsilon_\alpha^h - \varepsilon_\alpha^P \right) - \sum_{\alpha=4,5} \Phi_\alpha^* \varepsilon_\alpha^P. \end{aligned} \quad (90)$$

In the above, the differences $\varepsilon_1^h - \varepsilon_0^P$ and $\varepsilon_\alpha^h - \varepsilon_\alpha^P$ for $\alpha = 2, 3$, reflect the gauge redundancy in the plastic strain tensor associated with the addition of an arbitrary compatible tensor. By

coupling the helical nematic order parameter to these differences, nematic-elasticity remains defect-gauge invariant. The elastic free energy density in the presence of defects is

$$\begin{aligned} f_{\text{elas}}(\varphi, \varepsilon, \varepsilon^P) = & \frac{1}{2} \left\{ (\lambda + 2\mu) |\varepsilon_1^h - \varepsilon_0^p|^2 + \mu \sum_{a=2,3} |\varepsilon_a^h - \varepsilon_a^p|^2 \right\} \\ & - \frac{\lambda_0}{2} \left\{ \frac{2}{\sqrt{3}} \left(\Phi_1^* + \frac{2}{\sqrt{3}} \frac{\mu}{\lambda_0} \Delta_p^* \right) (\varepsilon_1^h - \varepsilon_0^p) \right. \\ & \quad \left. + \sum_{a=2,3} \Phi_a^* (\varepsilon_a^h - \varepsilon_0^p) + \text{c.c.} \right\} \\ & + \frac{1}{2} \mu \left(\frac{4}{3} |\Delta_p|^2 + \sum_{a=4,5} |\varepsilon_a^p|^2 \right) \\ & + \frac{\lambda_0}{2} \left(\frac{2}{\sqrt{3}} \Phi_1^* \Delta_p + \sum_{a=4,5} \Phi_a^* \varepsilon_a^p + \text{c.c.} \right). \end{aligned} \quad (91)$$

Minimizing with respect to the compatible helical strain yields the following equations of state:

$$\begin{aligned} \varepsilon_1^h &= \varepsilon_0^p + \frac{2\lambda_0}{\sqrt{3}(\lambda+2\mu)} \left(\Phi_1 + \frac{2\mu}{\sqrt{3}\lambda_0} \Delta_p \right), \\ \varepsilon_{2,3}^h &= \varepsilon_{2,3}^p + \frac{\lambda_0}{\mu} \Phi_{2,3}. \end{aligned} \quad (92)$$

Comparing these equations of state with the defect-free case in Eq. (45) allows one to quickly compute the effective correction to the nematic free energy

$$\begin{aligned} \Delta f_{\text{eff}}(\Phi, \varepsilon^P) = & -\frac{\lambda_0^2}{2\mu} \left\{ \sum_{a=2,3} |\Phi_a|^2 + \varrho \left| \Phi_1 + \frac{2\mu}{\sqrt{3}\lambda_0} \Delta_p \right|^2 \right\} \\ & + \frac{1}{2} \mu \left(\frac{4}{3} |\Delta_p|^2 + \sum_{a=4,5} |\varepsilon_a^p|^2 \right) \\ & + \frac{\lambda_0}{2} \left(\frac{2}{\sqrt{3}} \Phi_1^* \Delta_p + \sum_{a=4,5} \Phi_a^* \varepsilon_a^p + \text{c.c.} \right). \end{aligned} \quad (93)$$

where ϱ is defined in Eq. (49). The first line has the same form as in the defect-free case, albeit now there is a renormalized coupling between Φ_1 and the incompatible component of the plastic dilatation, Δ_p , since both fields couple to the elastic dilatation, $\varepsilon_1^h - \varepsilon_0^p$. The total effective free energy can be separated into three parts

$$\begin{aligned} \mathcal{F}_{\text{eff}}^{(2)}[\varphi, \varepsilon^P] = & \mathcal{F}_{\text{eff}}^{(2)}[\varphi, 0] \\ & + \frac{\lambda_0}{2V} \sum_{\mathbf{q}} \left\{ \frac{2(1-\varrho)}{\sqrt{3}} \Phi_1^* \Delta_p + \sum_{a=4,5} \Phi_a^* \varepsilon_a^p + \text{c.c.} \right\} \\ & + \frac{\mu}{2V} \sum_{\mathbf{q}} \left\{ \frac{4}{3}(1-\varrho) |\Delta_p|^2 + \sum_{a=4,5} |\varepsilon_a^p|^2 \right\}. \end{aligned} \quad (94)$$

The first line corresponds to the usual renormalization of the electronic nematic free energy in an ideal, defect-free crystal, coinciding with Eq. (51). The last line is the elastostatic self-energy of the defects, consistent with Eq. (D22) in the limit of

$\varphi \rightarrow 0$, and it clearly only depends on the physical, incompatible, contributions to the plastic strain tensor, ε_{ij}^p . The second line is new, and represents nonlocal, momentum-dependent, bilinear interactions between the electronic nematic order parameter and the plastic strain. We therefore call it the *nemato-plastic* free energy, and we write it as

$$\mathcal{F}_{\text{np}}[\varphi, \varepsilon^P] \equiv \frac{\lambda_0}{2V} \sum_{\mathbf{q}} \left\{ \frac{2}{\sqrt{3}} (1-\varrho) \Phi_1^* \Delta_p + \sum_{a=4,5} \Phi_a^* \varepsilon_a^p + \text{c.c.} \right\}. \quad (95)$$

Thus, the incompatible part of the plastic strain only couples to the electronic nematic order parameters that are already suppressed by direction-selective criticality. From Eq. (94), the quantities $\Phi_{2,3}$ do not experience structural disorder through a bilinear coupling. Indeed, their transition is enhanced by λ_0^2/μ , like the case of homogeneous and inhomogeneous deformations in defect-free media (Sections II and IV, respectively). On the other hand, the other three components $\Phi_{1,4,5}$, which are suppressed in defect-free media, experience the structural disorder. Thus, the compatibility relations of elasticity protect the critical order parameters $\Phi_{2,3}$ from experiencing local defect strains through a nemato-plastic bilinear coupling.

In real-space, however, these distinct effects of defects on the nematic order parameter are less obvious, particularly when one uses the conventional, d -orbital basis for electronic nematicity. Eq. (95) establishes a plastic conjugate field for the d -orbital electronic nematic order parameter, \mathbf{h} , defined in momentum space via

$$\mathbf{h}_{\mathbf{q}} \equiv - \left\{ \Gamma_0(\hat{q}) \varepsilon_{0,\mathbf{q}}^p + \Gamma(\hat{q}) \cdot \boldsymbol{\varepsilon}_{\mathbf{q}}^p \right\}, \quad (96)$$

$$\Gamma_0(\hat{q}) \equiv -\frac{2}{\sqrt{3}} (1-\varrho) \hat{Q}_1, \quad (97)$$

$$\Gamma(\hat{q}) \equiv (1-\varrho) \hat{Q}_1 \hat{Q}_1^T + \hat{Q}_4 \hat{Q}_4^T + \hat{Q}_5 \hat{Q}_5^T. \quad (98)$$

In the expression above, we made the wavevector dependence explicit for clarity (though it is implied by definition in $\{\hat{Q}_a\}$). The form factors in the expression above are both even under inversion, $\Gamma_0(-\hat{q}) = \Gamma_0(\hat{q})$ and $\Gamma(-\hat{q}) = \Gamma(\hat{q})$, from Eq. (B5). Importantly, we note that this conjugate field is exactly the elastic strain generated by plasticity – given in Eq. (D14) and Eq. (D15) – *in the absence of electronic nematicity*. Thus, $\mathbf{h}_{\mathbf{q}} = \mathcal{E}_{\mathbf{q}}|_{\varphi=0}$, implying that one can obtain the defect-generated conjugate field for the nematic order parameter by solving for the physical elastic strain separately from the nematic problem, despite both the nematic and plastic fields being coupled to the same fluctuating total strain. Meanwhile, it is insightful to note that $\Gamma(\hat{q})$ is exactly the anisotropic contribution to the renormalized 5×5 electronic nematic mass matrix in Eq. (50), which can be written as

$$\mathcal{M}(\hat{q}) = \frac{\lambda_0^2}{\mu} \{ \mathbf{I} - \Gamma(\hat{q}) \}, \quad (99)$$

exemplifying that direction-selective criticality occurs in the isotropic medium precisely to project out incompatible electronic nematic fluctuations.

In real-space, the nematicplastic free energy as

$$\mathcal{F}_{\text{np}} [\boldsymbol{\varphi}(\mathbf{x}), \mathbf{h} [\boldsymbol{\varepsilon}_{ij}^P(\mathbf{x})]] = -\lambda_0 \int_x \mathbf{h}(\mathbf{x}) \cdot \boldsymbol{\varphi}(\mathbf{x}), \quad (100)$$

$$\begin{aligned} \mathbf{h}(\mathbf{x}) = & - \int_{x'} \left\{ \Gamma_0(\mathbf{x} - \mathbf{x}') \boldsymbol{\varepsilon}_0^P(\mathbf{x}') \right. \\ & \left. + \Gamma(\mathbf{x} - \mathbf{x}') \cdot \boldsymbol{\varepsilon}^P(\mathbf{x}') \right\}. \end{aligned} \quad (101)$$

At this level, the defects can generate long-range conjugate fields for all five nematic d -orbital order parameters. Furthermore, we note that the character of the defect source can change as the strain is propagated through the medium by both the 5×1 quadrupolar vector $\Gamma_0(\mathbf{x})$ and 5×5 matrix $\Gamma(\mathbf{x})$.

Elastic fluctuations mediate long-range and anisotropic interactions in real-space between the physical plastic strain and the electronic nematic order parameter. However, as is already apparent in Eq. (94), these interactions are between those components of the electronic nematic order parameter that remain massive at the nematico-elastic critical point. Treating the defects as quenched, then the implication is that the electronic nematic order parameter, in the d -orbital basis, suffers from long-range, anisotropic, and correlated random field disorder. Despite this random pinning effect on the d -orbital basis, the nematico-elastic criticality survives since the critical nematico-elastic order parameters, $\Phi_{2,3}$, do not experience the structural disorder. Higher order or dynamical effects may become important if the nematico-elastic criticality deviates from the Gaussian fixed point, but such a discussion lies outside the scope of this work.

Yet, as is the case with any bilinear, there is an inverse, or reciprocal, effect as well. In this theory, the reciprocal effect would be plasticity generated by electronic nematicity. If it is the case that $\lambda_0^2/\mu \ll 1$, then one expects that the internal fivefold degeneracy of the bare electronic nematic order parameter, $\boldsymbol{\varphi}$, is approximately held. The effect on the structure can be quite devastating then, since the elastically suppressed components, $\Phi_{1,4,5}$, are almost as soft as the compatible nematic order parameters, $\Phi_{2,3}$. If this happens, then one expects that the observable plastic amplitudes, Δ_p and $\boldsymbol{\varepsilon}_{4,5}^P$, will be softened considerably by the nematic fluctuations. Such effects may lead to a proliferation of plastic defects within an electronic nematic, although more quantitative statements can only be made by considering higher-order effects of plasticity which lie outside the scope of the present work.

C. Random Nematic Fields Generated by an Ensemble of Straight Edge Dislocations

In this section, we provide a concrete, analytically tractable example of random conjugate elastic strain fields for the electronic nematic order parameter generated by a distribution of quenched random plastic defects. We focus on straight edge dislocations with Burgers vectors oriented in the xy -plane. Once the elastic strains are obtained, we calculate the spatial correlations for these fields, treating the sources – the defects – as random uncorrelated variables. This contrasts with

more conventional random field approaches where the strain fields themselves are treated as random uncorrelated variables [75, 76, 81, 82, 85]. As explained above, however, a random distribution of strains does not satisfy the elastic compatibility relations. We show that the conjugate elastic strains have long-range autocorrelations, which are reminiscent of correlated random fields [77, 81, 91]. However, an important difference is that these autocorrelations are anisotropic and the random fields for the different orbital basis functions are highly correlated. Since the different orbital basis functions generally split due to the discrete rotational symmetry in crystals, random fields in orthogonal symmetry channels act as random *transverse* fields rather than random *longitudinal* ones [49, 50]. The statistical-dependence of these random longitudinal and transverse fields that act on orthogonal symmetry channels may pull the electronic nematic criticality back into the quantum regime, even at nonzero temperature where thermal fluctuations dominate the critical behavior in the defect-free case. This suggests that structurally disordered electronic nematics may motivate a new class of random field problem hitherto unexplored in statistical physics. The role of dynamics in structurally disordered electronic nematics is however outside the scope of the current work where we only consider classical critical behavior.

We employ the nematico-plastic theory to compute the elastic strain fields conjugate to the nematic order parameter in the d -orbital basis, $\boldsymbol{\varphi}$, created by a single straight edge dislocation. The plastic distortion tensor for the dislocation anchored to the z -axis and with Burgers vector $\mathbf{b} = (b_x, b_y)$ in the convenient “slip gauge” is given by

$$\beta_{ij}^P(\mathbf{x}) = b_x \delta_{i,x} \delta_{j,y} \delta(y) \Theta(-x) - b_y \delta_{i,y} \delta_{j,x} \delta(x) \Theta(-y), \quad (102)$$

as worked out in Appendix E. The plastic strain tensor is its symmetric part. Since $\lambda_{ij}^1 = \delta_{i1}\delta_{j2} + \delta_{i2}\delta_{j1}$ from Eq. (A2), then the plastic strain is

$$\boldsymbol{\varepsilon}_{ij}^P(\mathbf{x}) = \frac{1}{2} \{ b_x \delta(y) \Theta(-x) - b_y \delta(x) \Theta(-y) \} \lambda_{ij}^1, \quad (103)$$

from which we readily obtain its decomposition in the d -orbital basis

$$\boldsymbol{\varepsilon}^P(\mathbf{x}) = (0, 0, 0, 0, b_x \delta(y) \Theta(-x) - b_y \delta(x) \Theta(-y))^T, \quad (104)$$

and $\boldsymbol{\varepsilon}_0^P(\mathbf{x}) = 0$. Clearly, only $\boldsymbol{\varepsilon}_{2xy}^P$ is nonzero for this defect-gauge choice. We obtain the conjugate strain, $\mathbf{h}(\mathbf{x})$, via Fourier transform, using Eq. (96). The Fourier transform of $\boldsymbol{\varepsilon}_{2xy}^P(\mathbf{x})$ gives

$$\boldsymbol{\varepsilon}_{2xy}^P = \int_x e^{-i\mathbf{q} \cdot \mathbf{x}} \{ b_x \delta(y) \Theta(-x) - b_y \delta(x) \Theta(-y) \} \quad (105)$$

$$= 2\pi \delta(q_z) \lim_{\eta \rightarrow 0^+} \left(\frac{ib_x}{q_x + i\eta} - \frac{ib_y}{q_y + i\eta} \right), \quad (106)$$

where we have taken the infinite-volume limit. Simplifying and taking the principal part, we have

$$\boldsymbol{\varepsilon}_{2xy}^P(\mathbf{q}) = 4\pi i \delta(q_z) \left(\frac{b_x \sin \phi - b_y \cos \phi}{q \sin 2\phi} \right), \quad (107)$$

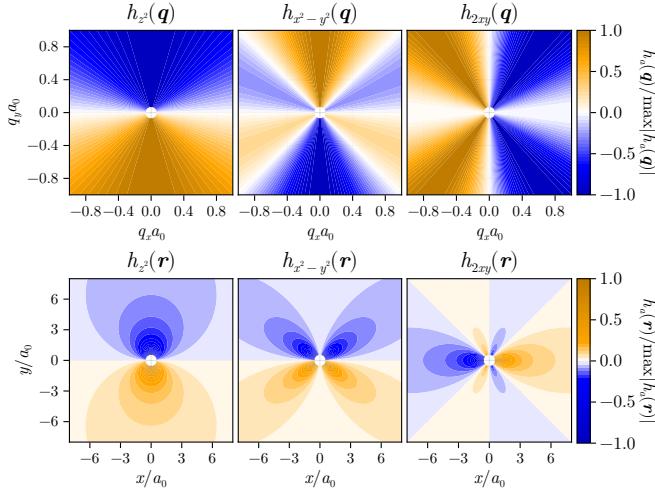


FIG. 6. Fourier- and real-space elastic strain fields emanating from a single straight edge dislocation in an isotropic elastic medium. Each column is one of the three nonzero elastic strain fields in the d -orbital basis, and are each normalized by their maximum magnitude. The positive (negative) values correspond to tensile (compressive) strain. The Burgers vector is chosen as $\mathbf{b} = a_0 \hat{x}$, where a_0 is the lattice constant. Top row: The Fourier space fields are shown, from Eq. (108), as a function of momentum \mathbf{q} . Bottom row: Real-space elastic strain fields for each nonzero elastic strain in the d -orbital basis from Eq. (109). The minimum radius is taken to be $a_0/2$.

where ϕ is the polar angle of the momentum \mathbf{q} . The conjugate field, \mathbf{h} , then follows as $\mathbf{h} = -\Gamma(\hat{\mathbf{q}}) \cdot \boldsymbol{\varepsilon}^P$, where $\Gamma(\hat{\mathbf{q}})$ is given by Eq. (98). The detailed steps are performed in Appendix E. Expanding and simplifying Eq. (E11), we obtain

$$\mathbf{h} = \delta(q_z) \frac{2\pi i}{1-\nu_3} \frac{b_x \sin \phi - b_y \cos \phi}{q} \left(\frac{1-2\nu_3}{\sqrt{3}}, -\cos 2\phi, 0, 0, -\sin 2\phi \right)^T. \quad (108)$$

As can be seen from these expressions, and from the top row of Fig. 6, all field amplitudes vanish for momenta parallel to the Burgers vector. Moreover, the two in-plane $h_{x^2-y^2}$ and h_{2xy} fields have additional zeroes due to the incompatible projector $\Gamma(\hat{\mathbf{q}})$. Indeed, these extra directions show that the elastic strain fields specifically lack momenta along the critical, and therefore compatible, directions for the electronic nematic orders. This is verified by comparing directly with Eq. (5), Fig. 1, and Fig. 2, which show that $\varphi_{x^2-y^2}$ (φ_{2xy}) is critical when $\cos(2\phi) = 0$ ($\sin(2\phi) = 0$). Performing an inverse Fourier transformation, the elastic strain field can be written in real-space as

$$\begin{aligned} h_{z^2}(r_{\parallel}) &= \frac{1-2\nu_3}{2\pi(1-\nu_3)\sqrt{3}} \frac{(-\hat{z}) \cdot (\mathbf{b} \times \hat{r}_{\parallel})}{r_{\parallel}}, \\ h_{x^2-y^2}(r_{\parallel}) &= -\frac{\mathbf{b} \cdot \hat{r}_{\parallel}}{2\pi(1-\nu_3)} \frac{\sin 2\phi_r}{r_{\parallel}}, \\ h_{2xy}(r_{\parallel}) &= \frac{\mathbf{b} \cdot \hat{r}_{\parallel}}{2\pi(1-\nu_3)} \frac{\cos 2\phi_r}{r_{\parallel}}, \end{aligned} \quad (109)$$

with $\mathbf{r}_{\parallel} \equiv (x, y, 0) = r_{\parallel}(\cos \phi_r, \sin \phi_r, 0)$.

We have recovered the well-known expressions for the elastic strain fields around a single straight edge dislocation

[50, 102, 106, 126], written in the more convenient d -orbital basis of electronic nematicity. These fields are plotted on a continuous mesh for $r_{\parallel} > a_0/2$ in Fig. 6, where a_0 is taken to be the lattice constant. One clearly observes long-range behavior emanating from a single defect, as well as an anisotropy developing with respect to the coordinate axes. We emphasize that the defect source, ε_{ij}^P , is only of $2xy$ character, whereas the field that couples to the electronic nematic order parameter has additional z^2 and $x^2 - y^2$ character due to the nonlocality of the helical transformation in real-space.

We now consider an ensemble of N uncorrelated, noninteracting, quenched dislocations as a model for random elastic strain disorder for the electronic nematic order parameter within a structurally disordered isotropic medium. We denote the elastic strain from the α^{th} edge dislocation with Burgers vector \mathbf{b}^{α} and core location \mathbf{x}^{α} by $\mathbf{h}(\mathbf{x} - \mathbf{x}^{\alpha}; \mathbf{b}^{\alpha})$. The elastic strain from an ensemble of N dislocations follows in real and momentum space as

$$\mathbf{h}(\mathbf{x}) = \sum_{\alpha=1}^N \mathbf{h}(\mathbf{x} - \mathbf{x}^{\alpha}; \mathbf{b}^{\alpha}), \quad (110)$$

$$\mathbf{h}_{\mathbf{q}} = - \sum_{\alpha=1}^N e^{i\mathbf{q} \cdot \mathbf{x}^{\alpha}} \Gamma(\hat{\mathbf{q}}) \cdot \boldsymbol{\varepsilon}^P(\mathbf{q}; \mathbf{b}^{\alpha}). \quad (111)$$

Example realizations for various dislocation concentrations in an isotropic elastic medium are shown in Fig. 7, where the strain fields are plotted on a continuous square mesh within a system of linear size $L = 128a_0$, with a_0 being the lattice constant. The minimum distance from any dislocation core was taken to be $a_0/2$ to avoid the singularities. These realizations uniformly sample random dislocation cores by choosing any point $(x, y) \in (-L, L)^2$, but they enforce that the total Burgers vector vanish. From Fig. 7, one observes that even at high dislocation concentrations, the total strain field in the orbital basis retains spatial structure, having large regions of space that favor either compressive or tensile strain. The strain fields that decay as $1/r$ in Eq. (109) indicate that the entire dislocated medium experiences local symmetry breaking strains, which would tend to locally pin the electronic nematic order parameters in the d -orbital basis. This statement remains true even at the lowest concentrations because the strains are long-ranged, ultimately arising from the displacement vector's role in elasticity as the vector-valued potential for the strain tensor. This feature, in turn, is an expression of elasticity theory's global Euclidean symmetry that leaves the energy invariant under rigid translations and rotations.

To better quantify the spatial structure contained within this defect ensemble, we compute the correlation functions from each realization, and then perform a disorder average over all realizations. The 5×5 correlation matrix for the ensemble, $C_{ab}(\mathbf{q})$, is given by

$$C(\mathbf{q}) \equiv \mathbf{h}_{\mathbf{q}} \mathbf{h}_{-\mathbf{q}}^T = \sum_{\alpha, \beta=1}^N e^{i\mathbf{q} \cdot (\mathbf{x}^{\alpha} - \mathbf{x}^{\beta})} \mathcal{K}^{\alpha\beta}(\mathbf{q}), \quad (112)$$

$$\mathcal{K}^{\alpha\beta}(\mathbf{q}) \equiv \Gamma(\hat{\mathbf{q}}) \cdot \boldsymbol{\varepsilon}^P(\mathbf{q}; \mathbf{b}^{\alpha}) \boldsymbol{\varepsilon}^P(-\mathbf{q}; \mathbf{b}^{\beta})^T \cdot \Gamma^T(-\hat{\mathbf{q}}).$$

For simplicity, we assume that the dislocations are uncorre-

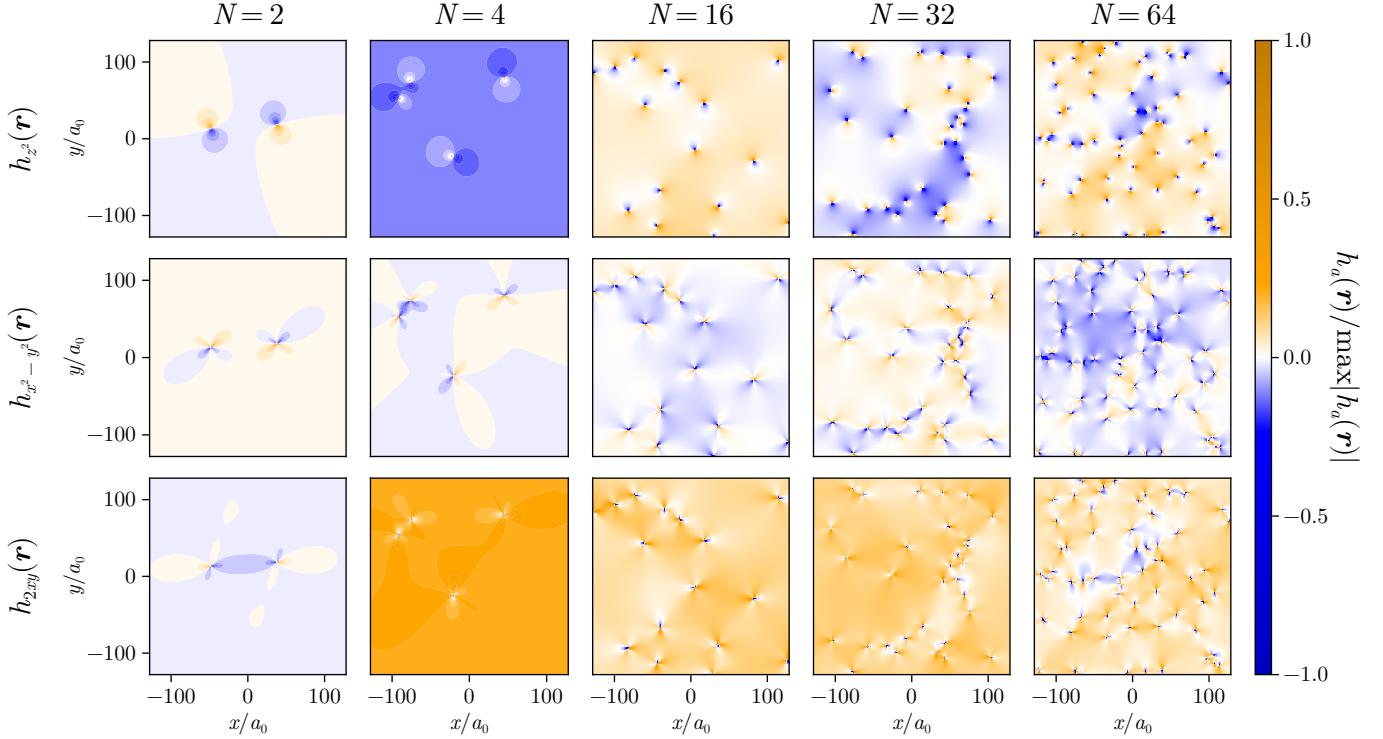


FIG. 7. Elastic strain field realizations of N uncorrelated random straight edge dislocations. The rows show the superimposed strain fields for each dislocation, calculated from Eq. (109). Each field is normalized by its maximum value, and the minimum radial distance from each dislocation core is taken to be $a_0/2$. The columns sweep various concentrations of dislocations by increasing N from left to right. The strains within each column are computed from the same set of random dislocations. The $N = 2, 4$ columns are contour plots to highlight the different regions of compressive and tensile strain, whereas $N = 16, 32, 64$ all show a continuous color gradient. In each realization, the dislocation cores are randomly chosen uniformly. The length of each Burgers vectors is a_0 , and half of their orientations are sampled uniformly within the xy -plane. The other half are opposite the first to enforce a vanishing total Burgers vector in each realization.

lated between themselves, that they can appear with uniform probability throughout the medium, and that their Burgers vectors are distributed isotropically. From these assumptions, it

is possible to derive six nonzero, disorder-averaged, spatial correlation functions for the various components of the elastic strain field, \mathbf{h} , as shown in Appendix E. These are given by

$$\begin{aligned} \llbracket C_{z^2,z^2}(\mathbf{q}) \rrbracket &= 2\pi^2 N \xi^2 \frac{(1-2\nu_3)^2}{3} \frac{\delta(q_z)}{q^2}, & \llbracket C_{z^2,x^2-y^2}(\mathbf{q}) \rrbracket &= -2\pi^2 N \xi^2 \frac{1-2\nu_3}{\sqrt{3}} \frac{\delta(q_z) \cos(2\phi)}{q^2}, \\ \llbracket C_{x^2-y^2,x^2-y^2}(\mathbf{q}) \rrbracket &= 2\pi^2 N \xi^2 \frac{\delta(q_z) [1+\cos(4\phi)]}{2q^2}, & \llbracket C_{z^2,2xy}(\mathbf{q}) \rrbracket &= -2\pi^2 N \xi^2 \frac{1-2\nu_3}{\sqrt{3}} \frac{\delta(q_z) \sin(2\phi)}{q^2}, \\ \llbracket C_{2xy,2xy}(\mathbf{q}) \rrbracket &= 2\pi^2 N \xi^2 \frac{\delta(q_z) [1-\cos(4\phi)]}{2q^2}, & \llbracket C_{x^2-y^2,2xy}(\mathbf{q}) \rrbracket &= 2\pi^2 N \xi^2 \frac{\delta(q_z) \sin(4\phi)}{2q^2}, \end{aligned} \quad (113)$$

where we have defined the parameter $\xi^2 \equiv \llbracket b^2 \rrbracket / (1 - \nu_3)^2$. With the exception of $\llbracket C_{z^2,z^2}(\mathbf{q}) \rrbracket$, all of these correlations are anisotropic. The cross-correlations exhibit anti-correlations between the different basis functions as well.

Finally, we compute these correlation functions in real-

space, as shown in Appendix E. There is a logarithmic divergence that naturally appears in the limit that $r_{\parallel} \rightarrow 0$ due to the breakdown of continuum elasticity near the dislocation core. After regularizing this integral by the macroscopic but finite size of the system, L , then the real-space correlations follow as

$$\begin{aligned} \llbracket C_{z^2,z^2}(\mathbf{r}_\parallel) \rrbracket &= N\xi^2 \frac{(1-2\nu_3)^2}{3} \log\left(\frac{L}{2r_\parallel}\right), & \llbracket C_{z^2,x^2-y^2}(\mathbf{r}_\parallel) \rrbracket &= \frac{1}{2}N\xi^2 \frac{1-2\nu_3}{\sqrt{3}} \cos(2\phi_r), \\ \llbracket C_{x^2-y^2,x^2-y^2}(\mathbf{r}_\parallel) \rrbracket &= \frac{1}{4}N\xi^2 \left\{ \log\left(\frac{L}{2r_\parallel}\right) + \frac{1}{4} \cos(4\phi_r) \right\}, & \llbracket C_{z^2,2xy}(\mathbf{r}_\parallel) \rrbracket &= \frac{1}{2}N\xi^2 \frac{1-2\nu_3}{\sqrt{3}} \sin(2\phi_r), \\ \llbracket C_{2xy,2xy}(\mathbf{r}_\parallel) \rrbracket &= \frac{1}{4}N\xi^2 \left\{ \log\left(\frac{L}{2r_\parallel}\right) - \frac{1}{4} \cos(4\phi_r) \right\}, & \llbracket C_{x^2-y^2,2xy}(\mathbf{r}_\parallel) \rrbracket &= \frac{1}{8}N\xi^2 \sin(4\phi_r), \end{aligned} \quad (114)$$

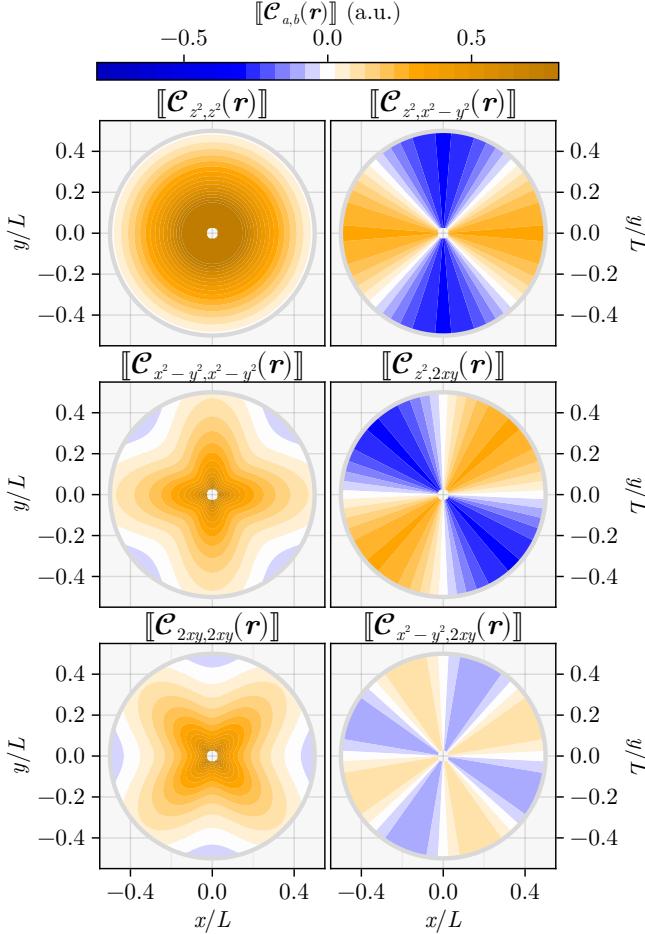


FIG. 8. Disorder-averaged real-space elastic strain correlations from an ensemble of uncorrelated straight edge dislocations in a system of size L . The expressions for these functions are given in Eqs. (114) and are all normalized by their maximum magnitudes. The subscripts label the d -orbital basis functions in $\mathbf{h}(\mathbf{r})$. While the spatial auto-correlation functions (left-column) display a radial dependence, the cross-correlation functions between d -orbital basis functions do not. The planar correlation functions $\llbracket C_{x^2-y^2,x^2-y^2} \rrbracket$, $\llbracket C_{2xy,2xy} \rrbracket$, and $\llbracket C_{x^2-y^2,2xy} \rrbracket = \llbracket C_{2xy,x^2-y^2} \rrbracket$ appear in Ref. [55] as well.

as shown in the appendix. The spatial dependence of these functions are shown in Fig. 8.

This concludes the discussion of straight edge dislocations. To summarize, these correlation functions demonstrate long-range, non-analytic, and statistical interdependence of the random elastic strain fields emanated by an ensemble of independent and identically distributed dislocations. One identifies auto-correlations as well as correlations between different d

orbital basis functions, implying that the presence of generic defects will produce conjugate symmetry-breaking fields for all five electronic nematic order parameters in the d -orbital basis. These fields, albeit random, can never be assumed independent of one another. Furthermore, the anisotropy embedded within these long-range correlations, to our knowledge, has not been considered before when one discusses long-range correlated random field disorder. Because the anisotropy persists at all length scales, it will likely induce new statistical physics for disordered critical nematico-elasticity.

While here we focused on the case of straight edge dislocations, we remark that these conclusions are generally valid for any distribution of plastic defects. Since the defect density tensor, η_{ij} , is related to the physical incompatibility contained within the plastic strain, Eq. (82), one can readily obtain the conjugate elastic strain $\mathbf{h} = \mathcal{E}|_{\varphi=0}$ in terms of the defect density η_{ij} , rather than in terms of the plastic strain ε_{ij}^P . We show how this is done within our helical formalism in Appendix F. Quite generally, η_{ij} can be expanded in multipoles, which correspond to different types of defects – for instance, the dipole term corresponds to dislocations whereas the quadrupole term corresponds to vacancies [87]. If one considers the defect density as a distribution of quenched multipoles, one still finds a similar anisotropic family of quenched elastic strains which will host long-ranged, anisotropic, correlations. Simply put, when the defects are treated as random, rather than the strains themselves, it is clear that different symmetry channels will strongly depend on one another and cannot be treated as independent disorder fields.

VII. DISCUSSION

Electronic nematicity, a rotational symmetry-breaking phase of matter, appears within a wide range of interesting quantum materials and can be induced by a wide range of microscopic mechanisms. Given the appearance of universal electronic nematic signatures across many distinct families of quantum materials, a phenomenological description applicable to all is warranted, and indeed necessary, to better understand electronic nematicity as a quantum phase of matter.

One of the most important effects that electronic nematicity has in crystalline quantum materials is the bilinear coupling between the electronic nematic order parameter and the symmetry-breaking components of the elastic strain tensor. This nematico-elastic coupling is absent in classical nematic liquids, given their lack of shear rigidity. Meanwhile, because it does exist in quantum materials, nematico-elasticity has shed light on many aspects of electronic nematicity that differentiate it further from nematicity in liquid crystals. For

example, the reduced rotational symmetry in crystalline environments allows for electronic nematicity to manifest different universality classes [10, 37, 47, 51]. Moreover, elastic fluctuations tend to suppress the phase space for thermal nematic fluctuations, effectively favoring the mean-field nematic criticality [39, 51, 59] frequently observed in experiments [6, 8, 44, 56, 127]. Additionally, coupling the nematic order locally to intrinsic defect strains introduces random field disorder for the nematic order parameter [50, 85]. Such disorder may explain the apparent mesoscopic nematic inhomogeneities that have been frequently observed via local probes in actual samples [17, 50, 64, 65, 67–74].

While the qualitative understanding of electronic nematicity gained from understanding these two individual aspects of nemato-elasticity is strong, they together seem contradictory. How is it that the same nemato-elastic interactions favor mean-field criticality while simultaneously propagating random pinning fields from omnipresent crystalline defects? This question is not purely academic – even in systems where the disorder is specifically tuned, and therefore rotational symmetry is already broken at small distances, one can still observe sharp criticality indicative of a diverging electronic nematic correlation length [50, 66, 128].

We have shown in this paper, and in the accompanying shorter paper, Ref. [55], that nemato-elasticity quantitatively transforms the behavior of the bare electronic nematic order parameter, and addresses this apparent contradiction. The transformation is initiated by the Saint-Venant compatibility relations, well-known to elasticity theory as a geometrical constraint of continuous deformations. In short, the electronic nematic order parameter inherits the compatibility relations from elasticity theory. By satisfying them, one establishes a nonlocal transformation between the usual “ d -orbital basis” of electronic nematicity and the two critical “helical” nematic order parameters. These helical order parameters, being the components of a manifestly compatible tensor, are blind to random incompatible strain fields generated by structural disorder, and thus can remain critical even in a plastically deformed medium. In this sense, our theory provides a framework to understand how the presence of a sharp electronic nematic phase transition is protected in structurally disordered media.

Within the context of electronic nematics overall, our theory of critical nemato-elasticity primarily establishes that electronic nematic fluctuations, which are degenerate in the bare theory, are not in an elastic medium. This is because electronic nematicity is represented by a tensor quantity that can have both compatible and incompatible contributions, whereas the elastic strain tensor in ideal media exclusively contains compatible contributions. In the context of crystalline nematics, the degeneracy of different orbital nematic fluctuations even in the *same* critical irreducible representation may split depending on their momenta – indeed, this is the phenomenon of direction-selective criticality. While being responsible for the unexpected mean-field behavior of electronic nematic phase transitions in low dimensions, the suppression of incompatible nematicity may also be responsible for an apparent planar universality exhibited across the many electronic nematics families, even the fully three-dimensional ones. By “planar uni-

versality,” we mean that the critical momenta near electronic nematic phase transitions lies in the basal plane, despite many of these materials having different electronic and structural properties [13]. Within the context of our theory, this planar universality may be accounted for since the electronic nematic directors must be coplanar with their critical momenta. Given that most actual nematics condense the $\varphi_{x^2-y^2}$ or φ_{2xy} basis functions due to their uniaxial symmetry, this means that the only critical momenta can lie in the xy plane so as to suppress nematic incompatibility. While there may be other reasons for this behavior, it would be somewhat coincidental that 3D tetragonal-to-orthorhombic nematics with different electronic properties all exhibit effectively two-dimensional physics governed by in-plane transfer momenta close to criticality.

From a mesoscopic perspective, meanwhile, the fact that the d -orbital and helical bases are related by a local transformation in momentum-space requires that they are related by a nonlocal transformation in real-space. Thus, one cannot associate local probes of electronic anisotropies with the local critical nematic order parameter. In terms of a given d -orbital nematic order parameter, such as φ_{2xy} , the critical macroscopic order parameter is only realized by first softening along the directions where φ_{2xy} maps uniquely onto the critical helical doublet, (Φ_2, Φ_3) , and then taking the infinite wavelength limit. This distinction is not just academic: given the growing experimental capabilities in measuring mesoscopic nematicity [57, 72, 73, 129], one must contend with the nonlocality that is endemic to elastic deformation in electronic nematics. For example, there is evidence that nematic domain boundaries may generate mesoscopic strain modulations within the bulk domains, with wavevectors exactly aligned along the critical directions that force the nematic tensor to be compatible [57].

Additionally, Ref. [72] reported a striking disparity between microscopic nematicity and the associated shear structural deformations. This is a puzzling observation, since one would naively expect from the bilinear nemato-elastic coupling that the microscopic φ_{2xy} nematic order parameter triggers a microscopic shear deformation ε_{xy} . Our results, however, show that this discrepancy is a consequence of the nonlocal transformation between the helical and d -orbital representations of the strain tensor. Given the presumptive role of structural disorder in the experiments performed in that work, we would associate the local nematicity in the d -orbital basis directly with pinning effects from crystalline defects, which are orthogonal to the critical (helical) nematic order parameters. Because of the nonlocal transformation between the d -orbital and helical representations, one expects the local $\varphi_{2xy}(x)$ nematic modulations to be composed of non-critical helical modulations $\Phi_{1,4,5}$. Thus, local probes will be influenced by non-critical anisotropies – those that always remain massive and short-ranged.

Our theory establishes a framework to discuss plasticity and nematicity; hence, the term, “nemato-plasticity.” Given the reciprocity that exists in nemato-elasticity, it is reasonable to ask whether electronic nematicity, as collective electronic modes, can induce plastic deformation in their host crystal. While this lies outside the scope of the current work, we emphasize that our helical theory of nemato-elasticity provides

the first defect-gauge invariant formalism within which one can discuss plasticity generated by electronic nematic fluctuations. Given the strong influence that plasticity and plastic deformation can have on electronic properties, as recently demonstrated experimentally in the quantum paraelectric SrTiO₃ [126], the possibility that *intrinsic* electronic nematicity can be a tuning parameter for plastic deformation is an exciting prospect that has not been considered before.

We have established the crucial and unifying role of the Saint Venant compatibility relations in nemo-elasticity. By developing a formalism that is particularly sensitive to them, the compatibility relations provide a resolution for the apparent paradox within nemo-elasticity. Because of the tensor gauge field constraints they impose on the strain tensor, elastic fluctuations indeed enhance the critical electronic correlations that spontaneously drive the system into the nematic phase. However, they do not enhance any nematic fluctuations, rather only those that reside within a critical *compatible* manifold. Because this compatible sector is orthogonal to the non-critical, *incompatible* nemo-plastic phase space, the compatibility relations protect electronic nematic criticality in the presence of structural disorder. Given the crucial role of electronic nematicity in stabilizing other correlated electronic phases – such as unconventional superconductivity [40–42] – our results will have far reaching impacts within many quantum materials.

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Appendix A: Gell-Mann Decomposition of Rank-2 Tensors

Electronic nematicity is frequently discussed in terms of crystalline point groups, and therefore is usually represented as multi-component *vectorial* irreducible representations within those groups [47]. This situation contrasts with elasticity, which is most conveniently expressed in its *tensorial* form – that is, with respect to its Cartesian coordinates [106]. This is true not just in more obvious engineering applications, but also in gauge-theoretic formulations [92, 95, 103, 123]. The Gell-Mann matrices of SU(3) provide a convenient machinery to transform rank-2 tensors between their tensorial and vectorial representations. In this appendix, we tabulate the Gell-Mann matrix conventions used and derive some identities used throughout this work.

Let A be a rank-2 symmetric tensor in three spatial dimensions. It can always be decomposed in the following form

$$A = \frac{1}{3}(\text{Tr } A)\lambda^0 + \frac{1}{2}\mathbf{A} \cdot \boldsymbol{\lambda}, \quad \mathbf{A} = \text{Tr}(\boldsymbol{\lambda} A), \quad (\text{A1})$$

where λ^0 is the identity and where we have defined the 5-component Gell-Mann vector to be $\boldsymbol{\lambda} \equiv (\lambda^8, \lambda^3, \lambda^6, \lambda^4, \lambda^1)^T$.

Here use the following definitions of the traceless symmetric Gell-Mann matrices:

$$\begin{aligned} \lambda^1 &= \begin{pmatrix} 0 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}, & \lambda^3 &= \begin{pmatrix} 1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 0 \end{pmatrix}, & \lambda^4 &= \begin{pmatrix} 0 & 0 & 1 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix}, \\ \lambda^6 &= \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & 1 & 0 \end{pmatrix}, & \lambda^8 &= \frac{1}{\sqrt{3}} \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & -2 \end{pmatrix}. \end{aligned} \quad (\text{A2})$$

The other three Gell-Mann matrices, $\lambda^{2,5,7}$, are all anti-symmetric, and are not important for this work. The ordering of the Gell-Mann vector, $\boldsymbol{\lambda}$, is chosen to mirror the orbital ordering of the basis functions of the electronic nematic order parameter in Eq. (11). One can show Eq. (A1) holds even in the case where A has a nonzero anti-symmetric part, using the two trace properties of the Gell-Mann matrices [130]:

$$\text{Tr}(\boldsymbol{\lambda}^a) = 3\delta_{0a}, \quad \text{Tr}(\boldsymbol{\lambda}^a \boldsymbol{\lambda}^b) = 2\delta_{ab}. \quad (\text{A3})$$

Using these properties, it follows that A is in one-to-one correspondence with the deviatoric, traceless, part of the tensor. This vector, \mathbf{A} , uniquely maps the deviatoric part of the symmetric tensor A in the d -orbital basis onto the A_{ij} components in the Cartesian basis.

Let B be another rank-2 tensor (with or without an antisymmetric part). From Eq. (A3), it follows that

$$\text{Tr}(AB) = \frac{1}{3}(\text{Tr } A)(\text{Tr } B) + \frac{1}{2}(\mathbf{A} \cdot \mathbf{B}). \quad (\text{A4})$$

The above expression is a consequence of the Fierz identity for Gell-Mann matrices,

$$\lambda_{ij}^a \lambda_{kl}^a = 2 \left(\delta_{il} \delta_{jk} - \frac{1}{3} \delta_{ij} \delta_{kl} \right). \quad (\text{A5})$$

From Eq. (A4), it follows that

$$\text{Tr}(AA) = \frac{1}{3}(\text{Tr } A)^2 + \frac{1}{2}(\mathbf{A} \cdot \mathbf{A}). \quad (\text{A6})$$

Moving back to nemo-elasticity, both the nematic order parameter from Eq. (6) and strain tensor in Eq. (8) can be written in vectorial form as

$$\varphi_{ij} = \frac{1}{2}\boldsymbol{\varphi} \cdot \boldsymbol{\lambda}_{ij}, \quad \boldsymbol{\varepsilon}_{ij} = \frac{1}{3}(\text{Tr } \boldsymbol{\varepsilon})\lambda_{ij}^0 + \frac{1}{2}\boldsymbol{\varepsilon} \cdot \boldsymbol{\lambda}_{ij}, \quad (\text{A7})$$

with $\text{Tr } \boldsymbol{\varphi} \equiv 0$. The vector $\boldsymbol{\varepsilon}$ is in one-to-one correspondence with the deviatoric part of the strain tensor.

Appendix B: Quadrupolar Form Factor Identities

In this appendix, we provide some explicit identities necessary for constructing the co-rotating helical basis of deviatoric tensors.

We start by calculating the traces and trace-norms of the $\{Q^{11}, Q^{12}, Q^{13}\}$ tensors of compatible elasticity. From Eq.

(30) and Eq. (31), it follows that

$$\begin{aligned}\text{Tr}(\mathbf{Q}^{11}) &= 1, & \text{Tr}(\mathbf{Q}^{11}\mathbf{Q}^{11}) &= 1, & \text{Tr}(\mathbf{Q}^{11}\mathbf{Q}^{12}) &= 0, \\ \text{Tr}(\mathbf{Q}^{12}) &= 0, & \text{Tr}(\mathbf{Q}^{12}\mathbf{Q}^{12}) &= \frac{1}{2}, & \text{Tr}(\mathbf{Q}^{11}\mathbf{Q}^{13}) &= 0, \\ \text{Tr}(\mathbf{Q}^{13}) &= 0, & \text{Tr}(\mathbf{Q}^{13}\mathbf{Q}^{13}) &= \frac{1}{2}, & \text{Tr}(\mathbf{Q}^{12}\mathbf{Q}^{13}) &= 0,\end{aligned}\quad (\text{B1})$$

establishing them as a set of three trace-orthogonal tensors at each momentum, \hat{q} .

Using the Gell-Mann decomposition in Eq. (32), we find that

$$\begin{aligned}\mathbf{Q}^{11} &= \frac{1}{3}\lambda^0 + \frac{1}{2}\mathbf{Q}^{11}\cdot\lambda = \frac{1}{3}\lambda^0 + \frac{1}{2}(\hat{\mathbf{e}}_1^\top \cdot \lambda \cdot \hat{\mathbf{e}}_1)\cdot\lambda, \\ \mathbf{Q}^{12} &= \frac{1}{2}\mathbf{Q}^{12}\cdot\lambda = \frac{1}{2}(\hat{\mathbf{e}}_1^\top \cdot \lambda \cdot \hat{\mathbf{e}}_2)\cdot\lambda, \\ \mathbf{Q}^{13} &= \frac{1}{2}\mathbf{Q}^{13}\cdot\lambda = \frac{1}{2}(\hat{\mathbf{e}}_1^\top \cdot \lambda \cdot \hat{\mathbf{e}}_3)\cdot\lambda.\end{aligned}\quad (\text{B2})$$

The Gell-Mann vectors satisfy:

$$\begin{aligned}\mathbf{Q}^{11}\cdot\mathbf{Q}^{11} &= \frac{4}{3}, & \mathbf{Q}^{11}\cdot\mathbf{Q}^{12} &= 0, \\ \mathbf{Q}^{12}\cdot\mathbf{Q}^{12} &= 1, & \mathbf{Q}^{11}\cdot\mathbf{Q}^{13} &= 0, \\ \mathbf{Q}^{12}\cdot\mathbf{Q}^{12} &= 1, & \mathbf{Q}^{12}\cdot\mathbf{Q}^{13} &= 0.\end{aligned}\quad (\text{B3})$$

To normalize these vectors, and to find two other orthonormal vectors necessary to complete the basis, we appeal to Eq. (33), repeated here for convenience as

$$\mathbf{Q}^{\alpha\beta}\cdot\mathbf{Q}^{\gamma\delta} = \delta_{\alpha\gamma}\delta_{\beta\delta} + \delta_{\alpha\delta}\delta_{\beta\gamma} - \frac{2}{3}\delta_{\alpha\beta}\delta_{\gamma\delta}. \quad (\text{B3})$$

The remaining two orthogonal vectors can be obtained from the expression above by setting $\alpha = 1$, representing the known vectors from elasticity in Eq. (B3). Then \mathbf{Q}^{23} can be obtained immediately since each term in the inner product vanishes. This is the fourth basis vector. The fifth follows a similar logic, but since all values of the Greek indices $\{1, 2, 3\}$ have been used by the first four basis vectors, we must appeal to repeated indices, as is the case for \mathbf{Q}^{11} . Since this will incur a nonzero overlap with \mathbf{Q}^{11} from the last term in Eq. (33), by taking the difference between \mathbf{Q}^{22} and \mathbf{Q}^{33} , we eliminate this overlap, and arrive at the last basis vector needed for a complete set. The definitions of the orthonormalized Gell-Mann vectors in the co-rotating helical basis are therefore

$$\begin{aligned}\hat{\mathbf{Q}}_1 &\equiv \frac{\sqrt{3}}{2}\mathbf{Q}^{11}, & \hat{\mathbf{Q}}_2 &\equiv \mathbf{Q}^{12}, \\ \hat{\mathbf{Q}}_3 &\equiv \mathbf{Q}^{13}, & \hat{\mathbf{Q}}_4 &\equiv \mathbf{Q}^{23}, & \hat{\mathbf{Q}}_5 &\equiv \frac{1}{2}(\mathbf{Q}^{22} - \mathbf{Q}^{33}).\end{aligned}\quad (\text{B4})$$

Their orthonormality can be established using Eq. (33) in a similar tabulation as Eq. (B3). These quadrupolar unit vectors at \hat{q} are directly proportional to those at $-\hat{q}$. From Eq. (26), it follows that

$$\hat{\mathbf{Q}}_a(-\hat{q}) = (-1)^{\delta_{a,3} + \delta_{a,4}} \hat{\mathbf{Q}}_a(\hat{q}). \quad (\text{B5})$$

With these basis vectors established, in a similar spirit to Eq. (A1), we can write any rank-2 symmetric tensor $A_{ij} = A_{ji}$ in a helical Gell-Mann decomposition as

$$A_{ij} = \frac{1}{3}(\text{Tr } A)\delta_{ij} + \frac{1}{2}\left(\sum_{a=1}^5 A_a \hat{\mathbf{Q}}_a\right)\cdot\lambda_{ij}, \quad A_a \equiv \hat{\mathbf{Q}}_a \cdot \mathbf{A}. \quad (\text{B6})$$

We now show how the $\{\vartheta^a\}$ basis tensors in Eq. (42) are related to the basis vectors in Eq. (B4) and ultimately the $Q_{ij}^{\alpha\beta}$ form factors defined in Eq. (27). In particular, these tensors are related by

$$\begin{aligned}\vartheta_{ij}^1 &= \frac{1}{\sqrt{2}}(\hat{\mathbf{Q}}_1 \cdot \lambda_{ij}) = \sqrt{\frac{3}{2}}(Q_{ij}^{11} - \frac{1}{3}\delta_{ij}), \\ \vartheta_{ij}^2 &= \frac{1}{\sqrt{2}}(\hat{\mathbf{Q}}_2 \cdot \lambda_{ij}) = \sqrt{2}Q_{ij}^{12}, \\ \vartheta_{ij}^3 &= \frac{1}{\sqrt{2}}(\hat{\mathbf{Q}}_3 \cdot \lambda_{ij}) = \sqrt{2}Q_{ij}^{13}, \\ \vartheta_{ij}^4 &= \frac{1}{\sqrt{2}}(\hat{\mathbf{Q}}_4 \cdot \lambda_{ij}) = \sqrt{2}Q_{ij}^{23}, \\ \vartheta_{ij}^5 &= \frac{1}{\sqrt{2}}(\hat{\mathbf{Q}}_5 \cdot \lambda_{ij}) = \frac{1}{\sqrt{2}}(Q_{ij}^{22} - Q_{ij}^{33}).\end{aligned}\quad (\text{B7})$$

From direct substitution, it follows from Eq. (B5) that by reversing the momentum, the ϑ basis tensors obey

$$\vartheta_{ij}^a(-\hat{q}) = (-1)^{\delta_{a,3} + \delta_{a,4}} \vartheta_{ij}^a(\hat{q}). \quad (\text{B8})$$

From these basis tensors, any rank-2 symmetric tensor, $A_{ij} = A_{ji}$, can be decomposed in momentum space as Eq. (43) in the main text. We repeat it here for completeness as

$$\begin{aligned}A_{ij} &= \frac{1}{3}(\text{Tr } A)\delta_{ij} + \frac{1}{\sqrt{2}}\sum_{a=1}^5 A_a \vartheta_{ij}^a, \\ A_a &= \sqrt{2}\text{Tr}(\vartheta^a A) = \hat{\mathbf{Q}}_a \cdot \mathbf{A}.\end{aligned}\quad (\text{B3})$$

This *tensorial* decomposition is completely equivalent to the *vectorial* one in Eq. (B6), with the exact same coefficients. However, the tensorial one proves more convenient for calculations involving tensor incompatibility.

To find the incompatibility of a given tensor, it follows from Eq. (43) and Eq. (B7) that one must compute $\text{inc}(I)$ and $\text{inc}(Q^{\alpha\beta})$. Starting with the latter, and applying Eq. (57), we have

$$\begin{aligned}\text{inc}(\mathbf{Q}^{\alpha\beta})_{il} &= -\frac{q^2}{2}\epsilon_{ijk}\epsilon_{lmn}\hat{\mathbf{e}}_{1,j}\hat{\mathbf{e}}_{1,m}(\hat{\mathbf{e}}_{\alpha,k}\hat{\mathbf{e}}_{\beta,n} + \hat{\mathbf{e}}_{\alpha,n}\hat{\mathbf{e}}_{\beta,k}) \\ &= -\frac{q^2}{2}\left\{(\hat{\mathbf{e}}_1 \times \hat{\mathbf{e}}_\alpha)_i(\hat{\mathbf{e}}_1 \times \hat{\mathbf{e}}_\beta)_l + (\hat{\mathbf{e}}_1 \times \hat{\mathbf{e}}_\beta)_i(\hat{\mathbf{e}}_1 \times \hat{\mathbf{e}}_\alpha)_l\right\}.\end{aligned}\quad (\text{B9})$$

Given that the $\hat{\mathbf{e}}_\alpha$ unit vectors are a right-handed orthonormal set at each \hat{q} , it follows that $(\hat{\mathbf{e}}_\alpha \times \hat{\mathbf{e}}_\beta)_i = \epsilon_{\alpha\beta\gamma}\hat{\mathbf{e}}_{\gamma,i}$. Thus, we find that

$$\text{inc}(\mathbf{Q}^{\alpha\beta})_{ij} = -q^2\epsilon_{1\alpha\gamma}\epsilon_{1\beta\gamma}Q_{ij}^{\gamma\delta}. \quad (\text{B10})$$

Applying this formula to the five orthogonal $\mathbf{Q}^{\alpha\beta}$ tensors yields

$$\begin{aligned}\text{inc}(\mathbf{Q}^{11}) &= 0, & \text{inc}(\mathbf{Q}^{12}) &= 0, \\ \text{inc}(\mathbf{Q}^{13}) &= 0, & \text{inc}(\mathbf{Q}^{23}) &= q^2Q^{23}, \\ \text{inc}(\mathbf{Q}^{22} - \mathbf{Q}^{33}) &= q^2(Q^{22} - Q^{33}),\end{aligned}\quad (\text{B11})$$

which shows that each of these tensors is an eigentensor of the incompatibility operator. The incompatibility of the identity tensor, meanwhile, follows from

$$\begin{aligned} \text{inc}(\mathbf{I})_{il} &= -q^2 \epsilon_{ijk} \epsilon_{lmn} \hat{\epsilon}_{1,j} \hat{\epsilon}_{1,m} \delta_{kn} \\ &= -q^2 (\delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}) \hat{\epsilon}_{1,j} \hat{\epsilon}_{1,m}. \end{aligned} \quad (\text{B12})$$

Simplifying the last expression then yields Eq. (58). From these identities, it follows that

$$\begin{aligned} \text{inc} \vartheta^1 &= \sqrt{\frac{3}{2}} \text{inc} \left(Q^{11} - \frac{1}{3} \mathbf{I} \right) = -\frac{q^2}{\sqrt{6}} \left(Q^{11} - \mathbf{I} \right), \\ \text{inc} \vartheta^2 &= \sqrt{2} \text{inc} Q^{12} = 0, \\ \text{inc} \vartheta^3 &= \sqrt{2} \text{inc} Q^{12} = 0, \\ \text{inc} \vartheta^4 &= \sqrt{2} \text{inc} Q^{23} = q^2 \vartheta^4 \\ \text{inc} \vartheta^5 &= \frac{1}{\sqrt{2}} \text{inc} \left(Q^{22} - Q^{33} \right) = q^2 \vartheta^5. \end{aligned} \quad (\text{B13})$$

From these expressions, the incompatibility of any rank-2 symmetric tensor follows as Eq. (59) in the main text and repeated here for convenience:

$$\text{inc} A = \frac{1}{3} \left(\text{Tr} A - \frac{\sqrt{3}}{2} A_1 \right) \text{inc}(\mathbf{I}) + \frac{q^2}{\sqrt{2}} \left(A_4 \vartheta^4 + A_5 \vartheta^5 \right). \quad (\text{59})$$

Appendix C: Bilinear Order Parameter Coupling to Dilatation

In this appendix, we show that a bilinear coupling to dilatation leads to a discontinuous mass renormalization for an scalar order parameter, \mathcal{A} , which is invariant under spatial rotations and inversion [131–136]. Unlike the bilinear coupling to deviatoric strain, such as nematic-elasticity, coupling to dilatation does not lead to direction-selective criticality since the renormalization is discontinuous at $\mathbf{q} = \mathbf{0}$.

We assume that the bilinear coupling is of the form

$$\Delta \mathcal{F} = -\gamma \int_x \mathcal{A}(\mathbf{x}) \varepsilon_0(\mathbf{x}), \quad (\text{C1})$$

with γ being the coupling constant for the theory. Writing the dilatation in terms of the homogeneous and inhomogeneous contributions yields

$$\varepsilon_0(\mathbf{x}) = \bar{\varepsilon}_0 + \frac{1}{V} \sum_{\mathbf{q}>0} e^{i\mathbf{q}\cdot\mathbf{x}} \varepsilon_{0,\mathbf{q}}, \quad (\text{C2})$$

with a bilinear coupling given by

$$\Delta \mathcal{F} = -\frac{\gamma V}{2} \bar{\mathcal{A}} \bar{\varepsilon}_0 - \frac{\gamma}{2V} \sum_{\mathbf{q}>0} \left(\mathcal{A}^* \varepsilon_{0,\mathbf{q}}^h + \text{c.c.} \right), \quad (\text{C3})$$

in the helical representation with $\varepsilon_{0,\mathbf{q}} = \varepsilon_{1,\mathbf{q}}^h$. Here $\bar{\mathcal{A}} \equiv \frac{1}{V} \int_x \mathcal{A}(\mathbf{x})$ and $\bar{\varepsilon}_0 \equiv \frac{1}{V} \int_x \varepsilon_0(\mathbf{x})$. Notice how the $\varepsilon_{2,3}^h$ helical strains are not involved at all in this problem. The total

elastic free energy is then

$$\begin{aligned} \mathcal{F} &= V \left\{ \frac{1}{2} B \bar{\varepsilon}_0^2 - \gamma \bar{\mathcal{A}} \bar{\varepsilon}_0 \right\} \\ &\quad + \frac{1}{2V} \sum_{\mathbf{q}>0} \left\{ (\lambda + 2\mu) |\varepsilon_1^h|^2 + \mu \sum_{a=2,3} |\varepsilon_a^h|^2 - \gamma (\mathcal{A} \varepsilon_1^h + \text{c.c.}) \right\}, \end{aligned} \quad (\text{C4})$$

where the bulk modulus is $B = \lambda + \frac{2\mu}{3}$. We have already taken the homogeneous deviatoric strains to be zero in the above given the lack of homogeneous deviatoric stress. The equations of state are obtained as

$$\begin{aligned} \bar{\varepsilon}_0 &= \frac{\gamma}{B} \bar{\mathcal{A}}, \\ \varepsilon_1^h &= \frac{\gamma}{\lambda + 2\mu} \bar{\mathcal{A}}, \\ \varepsilon_{2,3}^h &= 0. \end{aligned} \quad (\text{C5})$$

The effective correction to the free energy for $\mathcal{A}(\mathbf{x})$ then assumes the form

$$\mathcal{F}_{\text{eff}} = -\frac{\gamma^2}{2V} \left\{ \frac{1}{B} \mathcal{A}_{\mathbf{q}=0}^2 + \frac{1}{B + \frac{4\mu}{3}} \sum_{\mathbf{q}>0} |\mathcal{A}|^2 \right\}, \quad (\text{C6})$$

where $\mathcal{A}_{\mathbf{q}=0} = \int_x \mathcal{A}(\mathbf{x}) = V \bar{\mathcal{A}}$. Note that

$$\frac{1}{B} - \frac{1}{B + \frac{4\mu}{3}} = \frac{\varrho}{B} > 0, \quad (\text{C7})$$

since both $B > 0$ and $\mu > 0$ are required by thermodynamic stability. The quantity ϱ in the expression above is defined in Eq. (49). Thus, the mass renormalization is *discontinuous* as $q \rightarrow 0$ for *all* momentum directions. Furthermore, the largest enhancement comes from the homogeneous component, rather than the inhomogeneous component. As a result, the $\mathcal{A}_{\mathbf{q}=0}$ order parameter is critical before any of the inhomogeneous ones with nonzero momentum. This contrasts with the case of direction-selective nematic criticality in Eq. (51), where if the three direction-dependent constraints in Eq. (52) are met, then the inhomogeneous renormalization is identical to the homogeneous renormalization in Eq. (15). We also note the lack of directionality present in these effective interactions. This is because the order parameter couples directly to the dilatation without any direction-dependent form factors. Again, this is distinct from nematic-elastic criticality. We note that nematic-elasticity is also distinct from the so-called “Larkin-Pikin” mechanism that drives second-order transitions to weakly first-order transitions. In this case, because in this case the square of the order parameter couples to the dilatation, fluctuations of the latter renormalize the order parameter’s quartic coefficient rather than its mass [43, 137–139].

Appendix D: Helical Elastostatics in Systems with Quenched Plastic Strain

In this section, we provide a solution to elastostatics problems involving known quenched plastic strain fields. We solve

these problems within the helical strain formalism. The solution is obtained by finding a closed-form expression for the elastic strain, \mathcal{E}_{ij} , given a plastic strain, ε_{ij}^P . With this solution, one can obtain the elastic strain from any distribution of defects by relating ε_{ij}^P to the defect density tensor, η_{ij} , as shown in Appendix F. We first construct the solution formally in a system with arbitrary symmetry and then specialize to the case of an isotropic medium.

The equilibrium condition for an isolated medium is that its stress tensor, $\sigma_{ij}(\mathbf{x})$, is divergenceless: $\partial_i \sigma_{ij}(\mathbf{x}) = 0$ [90, 106]. In momentum space, this expression can be written as

$$\hat{\epsilon}_{\alpha,j} q_i \sigma_{ij} = q \hat{\epsilon}_{\alpha,j} \hat{\epsilon}_{1,i} \sigma_{ij} = q Q_{ij}^{1\alpha} \sigma_{ij} = 0, \quad (\text{D1})$$

where we projected the dangling Cartesian index, j , into the helical basis. In moving between the second and third equality, we exploited the symmetry of the stress tensor. Through Hooke's Law, one relates the elastic strain to the stress, at which point it follows immediately that equilibrium is maintained in real-space as long as

$$C_{ijkl} \partial_i \varepsilon_{kl}(\mathbf{x}) = C_{ijkl} \partial_i \varepsilon_{kl}^P(\mathbf{x}). \quad (\text{D2})$$

In momentum space, this yields

$$Q_{ji}^{1\alpha} C_{ijkl} Q_{kl}^{1\beta} \varepsilon_{\beta}^h = Q_{ji}^{1\alpha} C_{ijkl} \varepsilon_{kl}^P. \quad (\text{D3})$$

It is useful to now define the symmetric “helical elastic constant” matrix, $\mathcal{C}_{\alpha\beta}(\hat{q})$, as

$$\mathcal{C}_{\alpha\beta}(\hat{q}) \equiv Q_{ji}^{1\alpha}(\hat{q}) C_{ijkl} Q_{kl}^{1\beta}(\hat{q}). \quad (\text{D4})$$

Being real and symmetric, it is diagonalizable, and therefore invertible (provided it is positive-definite). We define its inverse as the “helical compliance” matrix, $\mathcal{S}_{\alpha\beta}(\hat{q}) \equiv [\mathcal{C}(\hat{q})]^{-1}_{\alpha\beta}$. To solve the elastostatics problem given a fixed plastic strain, ε_{ij}^P , one must obtain the helical strain amplitudes, ε_{α}^h , the total strain amplitudes, ε_{ij} , and the elastic strain amplitudes, \mathcal{E}_{ij} . In the helical representation, it is straightforward to invert Eq. (D3) and find ε_{α}^h , from which we can also readily obtain ε_{ij} :

$$\begin{aligned} \varepsilon_{\alpha}^h &= \mathcal{S}_{\alpha\beta}(\hat{q}) Q_{ji}^{1\beta} C_{ijkl} \varepsilon_{kl}^P, \\ \varepsilon_{ij} &= Q_{ij}^{1\alpha} \varepsilon_{\alpha}^h = Q_{ij}^{1\alpha} \mathcal{S}_{\alpha\beta}(\hat{q}) Q_{lk}^{1\beta} C_{klmn} \varepsilon_{mn}^P. \end{aligned} \quad (\text{D5})$$

The elastic strain amplitudes follow directly from $\mathcal{E}_{ij} = \varepsilon_{ij} - \varepsilon_{ij}^P$, and are given in the main text as Eq. (86). For convenience, we repeat it here:

$$\mathcal{E}_{ij} = \left[Q_{ij}^{1\alpha} \mathcal{S}_{\alpha\beta}(\hat{q}) Q_{lk}^{1\beta} C_{klmn} - \frac{1}{2} (\delta_{im} \delta_{jn} + \delta_{in} \delta_{jm}) \right] \varepsilon_{mn}^P. \quad (\text{86})$$

The real-space solution follows from the above equation via Fourier transformation over the infinite domain. This constitutes the full solution to the plasticity problem at the level of linear (infinitesimal) strain. While not immediately obvious, if the plastic strain tensor is purely compatible, meaning it has no gauge-invariant physical part, such that $\text{inc}(\varepsilon^P)_{ij} = 0$, then $\mathcal{E}_{ij} = 0$ in Eq. (86). This is true in any medium of any degree of crystalline anisotropy. To prove this, assume that the

incompatible part of the plastic strain vanishes, such that the plastic strain can be written in the helical basis as $\varepsilon_{ij}^P = Q_{ij}^{1\alpha} \varepsilon_{\alpha}^P$ for $\alpha = 1, 2, 3$, as we did for the completely compatible strain tensor in Eq. (28). Upon substitution into Eq. (86), we will have

$$\begin{aligned} Q_{ij}^{1\alpha} \mathcal{S}_{\alpha\beta}(\hat{q}) Q_{lk}^{1\beta} C_{klmn} Q_{mn}^{1\gamma} \varepsilon_{\gamma}^P &= Q_{ij}^{1\alpha} \mathcal{S}_{\alpha\beta}(\hat{q}) \mathcal{C}_{\beta\gamma}(\hat{q}) \varepsilon_{\gamma}^P \\ &= Q_{ij}^{1\alpha} \varepsilon_{\alpha}^P. \end{aligned} \quad (\text{D6})$$

This establishes the total strain as $\varepsilon_{ij} \equiv \varepsilon_{ij}^P$, rendering the physical elastic strain $\mathcal{E}_{ij} = 0$. In this sense, Eq. (86) can be thought of as projecting out only the physical incompatibility contained in the plastic strain ε_{ij}^P . This physical part is generated by a nonzero defect density tensor, shown in Appendix F.

To connect these results with nematicity, it is helpful to unpack the plastic strain, and afterwards, apply it to obtain the elastic strain Eq. (86) in an isotropic medium. We thus seek an expression for $C_{ijkl} \varepsilon_{kl}^P$. Unlike the *compatible* total strain, the *incompatible* plastic strain must be expanded according to Eq. (43) (also Appendix B) as

$$\varepsilon_{ij}^P = \frac{1}{3} (\text{Tr } \varepsilon^P) \delta_{ij} + \frac{1}{\sqrt{2}} \sum_{a=1}^5 \varepsilon_a^P \vartheta_{ij}^a. \quad (\text{D7})$$

All six coefficients are required since the plastic strain is not compatible. However, given that the total compatible strain also has a trace and $\vartheta_{ij}^{1,2,3}$ projections, it follows that neither $\text{Tr } \varepsilon^P$, nor $\varepsilon_{1,2,3}^P$, are gauge-invariant quantities. This contrasts with the $\varepsilon_{4,5}^P$ components, which clearly are gauge-invariant, since they are the projections along the eigentensors of the incompatibility operator with nonzero eigenvalue. Likewise, from Eq. (61), it follows that one can define the ε_1^P coefficient as

$$\varepsilon_1^P \equiv \frac{2}{\sqrt{3}} (\varepsilon_0^P + \Delta_P), \quad (\text{D8})$$

where $\varepsilon_0^P \equiv \text{Tr } \varepsilon^P$. Then, Δ_P can be interpreted as the incompatible plastic dilatation. Upon substitution, we find

$$C_{ijkl} \varepsilon_{kl}^P = \frac{1}{3} \varepsilon_0^P C_{ijkk} + \frac{1}{\sqrt{2}} \sum_{a=1}^5 \varepsilon_a^P (C_{ijkl} \vartheta_{kl}^a). \quad (\text{D9})$$

In an isotropic medium, $C_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu (\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk})$ [106], from which one obtains $C_{ijkk} = 3(\lambda + 2\mu/3) \delta_{ij}$ and $C_{ijkl} \vartheta_{kl}^a = 2\mu \vartheta_{ij}^a$ from Eq. (41) and Eq. (42). Then,

$$C_{ijkl} \varepsilon_{kl}^P = \left(\lambda + \frac{2\mu}{3} \right) \varepsilon_0^P \delta_{ij} + \sqrt{2}\mu \sum_{a=1}^5 \varepsilon_a^P \vartheta_{ij}^a, \quad (\text{D10})$$

from which we obtain

$$Q_{ji}^{1\beta} C_{ijkl} \varepsilon_{kl}^P = \left[(\lambda + 2\mu) \varepsilon_0^P + \frac{4\mu}{3} \Delta_P \right] \delta_{1\beta} + \mu \left(\varepsilon_2^P \delta_{2\beta} + \varepsilon_3^P \delta_{3\beta} \right), \quad (\text{D11})$$

using the trace of $Q^{\alpha\beta}$, Eq. (B7), and Eq. (D8). The helical elastic constants, $\mathcal{C}_{\alpha\beta}$, and the helical compliance, $\mathcal{S}_{\alpha\beta}$, are

$$\begin{aligned}\mathcal{C}_{\alpha\beta}(\hat{q}) &= (\lambda + 2\mu)\delta_{1\alpha}\delta_{1\beta} + \mu \sum_{c=2,3} \delta_{c\alpha}\delta_{c\beta}, \\ \mathcal{S}_{\alpha\beta}(\hat{q}) &= \frac{1}{\lambda + 2\mu}\delta_{1\alpha}\delta_{1\beta} + \frac{1}{\mu} \sum_{c=2,3} \delta_{c\alpha}\delta_{c\beta}.\end{aligned}\quad (\text{D12})$$

The solution in the isotropic medium follows from Eq. (D5) as

$$\begin{aligned}\varepsilon_{\alpha}^h &= \left(\varepsilon_0^p + \varrho\Delta_p\right)\delta_{1\alpha} + \sum_{b=2,3} \varepsilon_b^p\delta_{b\alpha}, \\ \varepsilon_{ij} &= \frac{1}{3}\left(\varepsilon_0^p + \varrho\Delta_p\right)\delta_{ij} \\ &\quad + \frac{1}{\sqrt{2}}\left[\frac{2}{\sqrt{3}}\left(\varepsilon_0^p + \varrho\Delta_p\right)\vartheta_{ij}^1 + \sum_{a=2,3} \varepsilon_a^p\vartheta_{ij}^a\right]\end{aligned}\quad (\text{D13})$$

with the elastic strain amplitudes given in the main text as Eq. (88), repeated here for completeness as

$$\varepsilon_{ij} = \frac{1}{3}\varrho\Delta_p\delta_{ij} - \frac{1}{\sqrt{2}}\left[(1-\varrho)\Delta_p\vartheta_{ij}^1 + \sum_{a=4,5} \varepsilon_a^p\vartheta_{ij}^a\right]. \quad (88)$$

The quantity ϱ is defined in Eq. (49). Note that only the gauge-invariant contributions to the plasticity tensor, $\{\Delta_p, \varepsilon_{4,5}^p\}$, contribute to the physical elastic strain ε_{ij} , as proven in full generality earlier from Eq. (86). The deviatoric part of the elastic strain can be obtained from ε_{ij} using Eq. (A1) and Eq. (42) as

$$\begin{aligned}\mathcal{E} &= -(1-\varrho)\Delta_p\hat{\mathbf{Q}}_1 - \sum_{a=4,5} \varepsilon_a^p\hat{\mathbf{Q}}_a \\ &= \frac{2(1-\varrho)}{\sqrt{3}}\hat{\mathbf{Q}}_1\varepsilon_0^p - \left[(1-\varrho)\hat{\mathbf{Q}}_1\hat{\mathbf{Q}}_1^T + \sum_{a=4,5} \hat{\mathbf{Q}}_a\hat{\mathbf{Q}}_a^T\right]\cdot\boldsymbol{\varepsilon}^p.\end{aligned}\quad (\text{D14})$$

In the last expression, we have rewritten the plastic strain in terms of its trace and orbital components. One readily identifies these form factors from Eq. (97) and Eq. (98) in the main text. The elastic strain in the d -orbital basis can then be simplified using them as

$$\mathcal{E} = -\{\Gamma_0(\hat{q})\varepsilon_0^p + \Gamma(\hat{q})\cdot\boldsymbol{\varepsilon}^p\}. \quad (\text{D15})$$

In the Subsection VIB we show that this deviatoric elastic strain field, generated by plasticity, couples bilinearly to the electronic nematic order parameter.

Before concluding this appendix, we calculate the free energy minimum for an isotropic system with quenched plastic defect strain. Generalizing the variational free energy in Eq. (12) in the defect gauge theory amounts to

$$\mathcal{F}_{\text{elas}}[\mathcal{E}] = \frac{1}{2V} \sum_{\mathbf{q}} \left\{ \left(\lambda + \frac{2\mu}{3}\right) |\text{Tr } \mathcal{E}|^2 + \mu \mathcal{E}^\dagger \cdot \mathcal{E} \right\}. \quad (\text{D16})$$

Using Eq. (D7), we write the elastic strain as

$$\begin{aligned}\varepsilon_{ij} &= \frac{1}{3}\left(\varepsilon_1^h - \varepsilon_0^p\right)\delta_{ij} + \frac{1}{\sqrt{2}}\left(\frac{2}{\sqrt{3}}\varepsilon_1^h - \varepsilon_1^p\right)\vartheta_{ij}^1 \\ &\quad + \frac{1}{\sqrt{2}}\left[\sum_{a=2,3} \left(\varepsilon_a^h - \varepsilon_a^p\right)\vartheta_{ij}^a - \sum_{a=4,5} \varepsilon_a^p\vartheta_{ij}^a\right].\end{aligned}\quad (\text{D17})$$

With Eq. (D8), it is clear that ε_0^p and ε_1^p are not independent. Instead, the physical, incompatible dilatation Δ_p is. Substituting in Eq. (D8) for ε_1^p yields an elastic strain tensor of

$$\begin{aligned}\varepsilon_{ij} &= \frac{1}{3}\left(\varepsilon_1^h - \varepsilon_0^p\right)\delta_{ij} + \frac{1}{\sqrt{2}}\left[\frac{2}{\sqrt{3}}\left(\varepsilon_1^h - \varepsilon_0^p - \Delta_p\right)\right]\vartheta_{ij}^1 \\ &\quad + \frac{1}{\sqrt{2}}\left[\sum_{a=2,3} \left(\varepsilon_a^h - \varepsilon_a^p\right)\vartheta_{ij}^a - \sum_{a=4,5} \varepsilon_a^p\vartheta_{ij}^a\right].\end{aligned}\quad (\text{D18})$$

Thus, the elastic dilatation is the gauge invariant combination $\varepsilon_1^h - \varepsilon_0^p$, while the elastic Gell-Mann vector is

$$\mathcal{E} = \left[\frac{2}{\sqrt{3}}\left(\varepsilon_1^h - \varepsilon_0^p - \Delta_p\right), \varepsilon_2^h - \varepsilon_2^p, \varepsilon_3^h - \varepsilon_3^p, -\varepsilon_4^p, -\varepsilon_5^p \right]^T. \quad (\text{D19})$$

The free energy density follows as

$$\begin{aligned}f_{\text{elas}}(\mathcal{E}) &= \frac{1}{2} \left\{ \left(\lambda + \frac{2\mu}{3}\right) |\varepsilon_1^h - \varepsilon_0^p|^2 + \frac{4}{3}\mu |\varepsilon_1^h - \varepsilon_0^p - \Delta_p|^2 \right. \\ &\quad + \mu \sum_{a=2,3} |\varepsilon_a^h - \varepsilon_a^p|^2 + \mu \sum_{a=4,5} |\varepsilon_a^p|^2 \Big\} \\ &= \frac{1}{2} \left\{ (\lambda + 2\mu) |\varepsilon_1^h - \varepsilon_0^p|^2 + \mu \sum_{a=2,3} |\varepsilon_a^h - \varepsilon_a^p|^2 \right. \\ &\quad - \frac{4}{3}\mu \left[\Delta_p^* \left(\varepsilon_1^h - \varepsilon_0^p \right) + \text{c.c.} \right] \\ &\quad \left. + \frac{4}{3}\mu |\Delta_p|^2 + \mu \sum_{a=4,5} |\varepsilon_a^p|^2 \right\}.\end{aligned}\quad (\text{D20})$$

In moving from the first to the second equality, we factored out the incompatible dilatation, and reorganized the terms. We now can minimize with respect to the single-valued helical strain fields. Doing so yields

$$\varepsilon_{\alpha}^h = \left(\varepsilon_0^p + \varrho\Delta_p\right)\delta_{1\alpha} + \sum_{b=2,3} \varepsilon_b^p\delta_{b\alpha}, \quad (\text{D21})$$

consistent with Eq. (D13). This establishes the minimization of the free energy as equivalent to the divergenceless stress condition used in deriving Eq. (D13), and it is employed in this work for nematic-elasticity. Substituting this result back into the variational free energy yields

$$\mathcal{F}_{\text{elas}}\left(\varepsilon_{ij}^p\right) = \frac{\mu}{2V} \sum_{\mathbf{q}} \left\{ \frac{4}{3}(1-\varrho)|\Delta_p|^2 + \sum_{a=4,5} |\varepsilon_a^p|^2 \right\}, \quad (\text{D22})$$

given that $(\lambda + 2\mu)\varrho^2 = \frac{4}{3}\mu\varrho$ from Eq. (49). We note that the minimum free energy explicitly depends only on the physical incompatible part of the plastic strain tensor generated by defects.

Appendix E: Elastic Strains from Straight Edge Dislocations

In this appendix, we discuss the “slip gauge” of dislocations to demonstrate the defect-gauge redundancy in plasticity. We then provide the details of how to compute the elastic strain fields from straight edge dislocations within the slip gauge. We also include some relevant intermediate steps in computing their spatial correlation functions. Our derivation of the plastic strain for this type of defect, and the notation used in the derivation, primarily follows Kleinert’s book [92] with influence from de Wit’s works [99–102].

We begin with a straight edge dislocation described by a Burgers vector \mathbf{b} in the xy -plane and a dislocation line (or core) oriented along the z -axis, as shown in Fig. 5. Assuming that the defect is a pure dislocation, then the plastic jump in the displacement vector is given by

$$\Delta_j u_i^P(\mathbf{x}; S) = b_i \delta_j(\mathbf{x}; S) \equiv b_i \int_S dS_j(\mathbf{x}') \delta(\mathbf{x} - \mathbf{x}'), \quad (\text{E1})$$

where we have adapted the notation for the vector-valued delta-function on the surface S from Refs. [92, 99–102] to make the \mathbf{x} -dependence explicit. The subscript j on the Δ represents the tensorial nature of the plastic jump. The discontinuity in the displacement vector is measured with respect to the Volterra surface, and therefore the abrupt change can occur in any component $u_{x,y,z}$ across the surface oriented in any direction x, y, z . At this point, a defect gauge must be chosen – that is, one must define the Volterra surface, S . We choose the negative- x half of the xz -plane, and anchor the dislocation line at the origin, as shown in Fig. 5(a). It follows then that $dS = (0, dx dz, 0)$ and therefore

$$\begin{aligned} \Delta_j u_i^P(\mathbf{x}) &= b_i \delta_{j,y} \int_{-\infty}^0 dx' \int_{-\infty}^{\infty} dz' \delta(x - x') \delta(y) \delta(z - z') \\ &= b_i \delta_{j,y} \delta(y) \Theta(-x), \end{aligned} \quad (\text{E2})$$

where $\Theta(x)$ is the usual Heaviside function. This is one gauge choice for the plastic distortion tensor, $\beta_{ij}^P(\mathbf{x})$, for a straight edge dislocation. It is consistent with the topology associated with the Burgers vector [45, 90, 106].

This gauge choice turns out to only be convenient when the dislocation is a slip – meaning that $\mathbf{b} \cdot d\mathbf{S}(\mathbf{x}) = 0, \forall \mathbf{x}$, as shown in Fig. 5(b). We now demonstrate that a defect gauge transformation can transform any straight edge dislocation with Burgers vector $\mathbf{b} = (b_x, b_y)$ into two slip dislocations along either coordinate axis. For b_x , the Volterra surface, S , suffices. For b_y , we rotate the Volterra surface by 90° so that it is now the negative- y half of the yz -plane. Then this new S' surface has area element $dS' = (-dy dz, 0, 0)$ and a plastic displacement vector given by

$$\Delta_j u_i^P(\mathbf{x}; S') = b_y \delta_{i,y} \delta_j(\mathbf{x}; S') = -b_y \delta_{i,y} \delta_{j,x} \delta(x) \Theta(-y), \quad (\text{E3})$$

as illustrated in Fig. 5(b). This choice of Volterra surface is also consistent with the topology of the dislocation, and therefore there is an ambiguity that arises between surfaces S and S' , as both describe the same topological defect. The

difference between the plastic displacements for b_y follows as

$$\begin{aligned} \Delta_j u_i^P(\mathbf{x}; S') - \Delta_j u_i^P(\mathbf{x}; S) &= -b_y \delta_{i,y} \left\{ \delta_{j,x} \delta(x) \Theta(-y) \right. \\ &\quad \left. + \delta_{j,y} \delta(y) \Theta(-x) \right\} \\ &= -b_y \delta_{i,y} \{-\delta_j(\mathbf{x}; S') + \delta_j(\mathbf{x}; S)\} \\ &= -b_y \delta_{i,y} \delta_j(\mathbf{x}; \partial\mathcal{V}), \end{aligned} \quad (\text{E4})$$

where the boundary of the volume enclosed by the surfaces S and S' is defined as $\partial\mathcal{V} \equiv S - S'$. This nontrivial, position-dependent difference would express itself in the displacement vector, and therefore the total strain tensor, despite the fact that both Volterra surfaces parameterize the same defect. Thus, the edge dislocation exemplifies the defect-gauge redundancy of plasticity.

We proceed with what we dub the “slip gauge” for the straight edge dislocation, namely that we can find a new Volterra surface S' that satisfies $\mathbf{b} \cdot d\mathbf{S}'(\mathbf{x}) = 0$, for all $\mathbf{x} \in S'$. To show that it is gauge-equivalent to the dislocation defined by S , we demonstrate that the change in Volterra surface amounts only to a compatible change in the plastic strain tensor – that is, it amounts to a redefinition of the displacement vector. For this case, as shown in Fig. 5(c), the Volterra surfaces S and S' encapsulate the rectangular prism, $\mathcal{V} = \{\mathbf{x} \in \mathbb{R}^3 : x < 0 \text{ and } y < 0\}$. We have defined its surface normals such that they are outer-facing (hence the negative sign on S'). We now define a delta-function acting on the volume \mathcal{V} through its sifting property as $\int_{\mathcal{V}} f(\mathbf{x}) \delta(\mathbf{x}; \mathcal{V}) \equiv \int_{\mathcal{V}} d^3x f(\mathbf{x})$. Using the test function $f(\mathbf{x}) = \partial_i g(\mathbf{x})$ and the divergence theorem, it can be shown that $\partial_i \delta(\mathbf{x}; \mathcal{V}) = -\delta_i(\mathbf{x}; \partial\mathcal{V})$ [100]. Thus, the difference between the plastic fields for the b_y component of the Burgers vector are

$$\Delta_j u_i^P(\mathbf{x}; S') - \Delta_j u_i^P(\mathbf{x}; S) = b_y \delta_{i,y} \partial_j \delta(\mathbf{x}; \mathcal{V}). \quad (\text{E5})$$

The defect-gauge transformation from $S \rightarrow S'$ is therefore summarized in the displacement vector as

$$\mathbf{u}(\mathbf{x}; S) \rightarrow \mathbf{u}(\mathbf{x}; S') = \mathbf{u}(\mathbf{x}; S) + b_y \hat{\mathbf{y}} \delta(\mathbf{x}; \mathcal{V}), \quad (\text{E6})$$

and since this amounts to a redefinition of $\mathbf{u}(\mathbf{x})$ by a single-valued vector field, $\Lambda(\mathbf{x}) = -b_y \hat{\mathbf{y}} \delta(\mathbf{x}; \mathcal{V})$, as shown in Fig. 5 (see Eq. (84) as well). Thus, transforming between S and S' constitutes only a compatible change to the plastic strain tensor, $\varepsilon_{ij}^P(\mathbf{x})$. It does not alter the physical content of the dislocation, since its incompatibility is unchanged.

With the “slip-gauge” for straight edge dislocations established, we turn to computing the elastic strain fields within the helical formalism. We start from Eq. (107), which we repeat here as

$$\varepsilon_{2xy}^P(\mathbf{q}) = 4\pi i \delta(q_z) \left(\frac{b_x \sin \phi - b_y \cos \phi}{q \sin 2\phi} \right), \quad (\text{107})$$

for convenience. The entire plastic strain tensor itself follows in the Cartesian basis simply as

$$\varepsilon_{ij}^P = \frac{1}{2} \varepsilon_{2xy}^P \lambda_{ij}^1, \quad (\text{E7})$$

meaning that it is traceless in this slip gauge, $\varepsilon_0^P = 0$, and that its Gell-Mann vectorial representation from Eq. (A1) is $\boldsymbol{\varepsilon}^P = (0, 0, 0, 0, \varepsilon_{2xy}^P)^T$. The conjugate field for the d -orbital nematic order parameter is then $\mathbf{h} = -\Gamma(\hat{q}) \cdot \boldsymbol{\varepsilon}^P$, since $\varepsilon_0^P = 0$. For convenience, $\Gamma(\hat{q})$ is repeated here

$$\Gamma = (1 - \varrho) \hat{\mathbf{Q}}_1 \hat{\mathbf{Q}}_1^T + \hat{\mathbf{Q}}_4 \hat{\mathbf{Q}}_4^T + \hat{\mathbf{Q}}_5 \hat{\mathbf{Q}}_5^T. \quad (\text{E9})$$

Due to the $\delta(q_z)$, the momentum is confined to the xy -plane in momentum space, where

$$\begin{aligned} \hat{\mathbf{Q}}_1^T &= \left(\frac{1}{2}, \frac{\sqrt{3}}{2} \cos 2\phi, 0, 0, \frac{\sqrt{3}}{2} \sin 2\phi \right), \\ \hat{\mathbf{Q}}_4^T &= (0, 0, \cos \phi, -\sin \phi, 0), \\ \hat{\mathbf{Q}}_5^T &= \left(\frac{\sqrt{3}}{2}, -\frac{1}{2} \cos 2\phi, 0, 0, -\frac{1}{2} \sin 2\phi \right). \end{aligned} \quad (\text{E8})$$

In this case, $\hat{\mathbf{Q}}_4 \cdot \boldsymbol{\varepsilon}^P = 0$. Likewise, it follows that $\hat{\mathbf{Q}}_5 = \frac{1}{\sqrt{3}} (2\mathbf{1}_{z^2} - \hat{\mathbf{Q}}_1)$ where the vector $\mathbf{1}_{z^2} \equiv (1, 0, 0, 0, 0)^T$. Defining a similar vector, $\mathbf{1}_{2xy} \equiv (0, 0, 0, 0, 1)^T$, we have that

$$\begin{aligned} \Gamma(\hat{q}; q_z = 0) \cdot \mathbf{1}_{2xy} &= \left\{ (1 - \varrho) \hat{\mathbf{Q}}_1 \hat{\mathbf{Q}}_1^T + \hat{\mathbf{Q}}_5 \hat{\mathbf{Q}}_5^T \right\} \cdot \mathbf{1}_{2xy} \\ &= \left\{ (1 - \varrho) \hat{\mathbf{Q}}_1 - \frac{1}{3} (2\mathbf{1}_{z^2} - \hat{\mathbf{Q}}_1) \right\} (\hat{\mathbf{Q}}_1^T \cdot \mathbf{1}_{2xy}) \\ &= -\frac{4}{3} \left\{ \frac{1}{2} \mathbf{1}_{2xy} - \left(1 - \frac{3}{4} \varrho \right) \hat{\mathbf{Q}}_1 \right\} (\hat{\mathbf{Q}}_1^T \cdot \mathbf{1}_{2xy}) \\ &= -\frac{2}{\sqrt{3}} \sin 2\phi \left\{ \frac{1}{2} \mathbf{1}_{2xy} - \left(1 - \frac{3}{4} \varrho \right) \hat{\mathbf{Q}}_1 \right\}. \end{aligned} \quad (\text{E9})$$

Recalling that the 3D Poisson ratio is given by $\nu_3 = \lambda/2(\lambda + \mu)$ [90, 92, 106], one can show that $1 - 3\varrho/4 = 1/2(1 - \nu_3)$ using Eq. (49). From this, it follows that

$$\Gamma(\hat{q}; q_z = 0) \cdot \mathbf{1}_{2xy} = -\frac{\sin 2\phi}{(1 - \nu_3)\sqrt{3}} \left\{ (1 - \nu_3) \mathbf{1}_{2xy} - \hat{\mathbf{Q}}_1 \right\}. \quad (\text{E10})$$

Thus, the elastic strain follows as

$$\begin{aligned} \mathbf{h} &= -[\Gamma(\hat{q}; q_z = 0) \cdot \mathbf{1}_{2xy}] \varepsilon_{2xy}^P \\ &= \frac{\varepsilon_{2xy}^P \sin 2\phi}{(1 - \nu_3)\sqrt{3}} \left\{ (1 - \nu_3) \mathbf{1}_{z^2} - \hat{\mathbf{Q}}_1 \right\}. \end{aligned} \quad (\text{E11})$$

Expanding out the expression above yields Eq. (108), repeated here for convenience as

$$\mathbf{h} = \delta(q_z) \frac{2\pi i}{1 - \nu_3} \frac{b_x \sin \phi - b_y \cos \phi}{q} \left(\frac{1 - 2\nu_3}{\sqrt{3}}, -\cos 2\phi, 0, 0, -\sin 2\phi \right)^T. \quad (\text{E10})$$

In real-space, the elastic strain fields follow from the inverse Fourier transform. Starting with Eq. (108), the elastic strain can be written formally as

$$\begin{aligned} \mathbf{h}(\mathbf{x}) &= \frac{2\pi}{1 - \nu_3} (b_x \partial_y - b_y \partial_x) \\ &\times \left[-\frac{1 - 2\nu_3}{\sqrt{3}} \left(\partial_x^2 + \partial_y^2 \right), \left(\partial_x^2 - \partial_y^2 \right), 0, 0, (2\partial_x \partial_y) \right]^T g_4(\mathbf{x}), \end{aligned} \quad (\text{E12})$$

where we have used the $n = 4$ function in the family of $(n/2)$ -harmonic Green's functions, $g_n(\mathbf{r})$:

$$g_n(\mathbf{r}) \equiv \int \frac{d^3 q}{(2\pi)^3} \frac{\delta(q_z) e^{i\mathbf{q} \cdot \mathbf{r}}}{q^n}. \quad (\text{E13})$$

The first three functions are computed iteratively in the infinite medium in Appendix G and $g_4(\mathbf{r})$ is obtained within it as Eq. (G6). Upon differentiation, we find

$$\begin{aligned} h_{z^2}(x, y) &= \frac{1 - 2\nu_3}{2\pi(1 - \nu_3)\sqrt{3}} \frac{b_y x - b_x y}{x^2 + y^2}, \\ h_{x^2 - y^2}(x, y) &= -\frac{1}{2\pi(1 - \nu_3)} \frac{2xy(b_x x + b_y y)}{(x^2 + y^2)^2}, \\ h_{2xy}(x, y) &= \frac{1}{2\pi(1 - \nu_3)} \frac{(x^2 - y^2)(b_x x + b_y y)}{(x^2 + y^2)^2}, \end{aligned} \quad (\text{E14})$$

Writing $\mathbf{r}_\parallel \equiv (x, y, 0) \equiv r_\parallel(\cos \phi_r, \sin \phi_r, 0)$, then the expressions above simplify into those given in Eq. (109).

We now proceed to calculate the spatial correlation functions for an ensemble of uncorrelated, uniformly distributed, and isotropically oriented straight edge dislocations. Starting from the definition of the correlation function for a single realization of dislocations, Eq. (112), since each defect core can be positioned uniformly within the plane then averaging over the complex exponential term enforces that all spatial correlations must be between any given defect *with itself*. That is, assuming $\langle\langle e^{i\mathbf{q} \cdot (x^\alpha - x^\beta)} \rangle\rangle = \delta_{\alpha\beta}$, where the double brackets represent the disorder average, then

$$\begin{aligned} \langle\langle C(\mathbf{q}) \rangle\rangle &= \sum_{\alpha=1}^N \langle\langle \mathcal{K}^{\alpha\alpha}(\mathbf{q}) \rangle\rangle \\ \langle\langle \mathcal{K}^{\alpha\alpha}(\mathbf{q}) \rangle\rangle &= \Gamma(\hat{q}) \cdot [\mathbf{e}^P(\mathbf{q}; \mathbf{b}^\alpha) \mathbf{e}^P(-\mathbf{q}; \mathbf{b}^\alpha)^T] \cdot \Gamma^T(-\hat{q}) \end{aligned} \quad (\text{E15})$$

To proceed, we use Eq. (107) and the fact that $\mathbf{e}^P = \varepsilon_{2xy}^P \mathbf{1}_{2xy}$ to compute

$$\langle\langle \varepsilon_{2xy}^P(\mathbf{q}; \mathbf{b}^\alpha) \varepsilon_{2xy}^P(-\mathbf{q}; \mathbf{b}^\alpha)^T \rangle\rangle = \frac{8\pi^2 \delta(q_z)}{q^2 \sin^2 2\phi} \langle\langle (b^\alpha)^2 \rangle\rangle. \quad (\text{E16})$$

To obtain the disorder average above, the Burgers vector was first written as $\mathbf{b}^\alpha \equiv b^\alpha(\cos \beta, \sin \beta)$. If we assume the Burgers vectors are isotropically distributed, then it follows that $\langle\langle \cos[2(\beta - \phi)] \rangle\rangle = 0$. Next, we define $\langle\langle (b^\alpha)^2 \rangle\rangle \equiv \langle\langle b^2 \rangle\rangle$ for all dislocations to obtain a disorder-averaged spatial correlation function given by

$$\langle\langle C(\mathbf{q}) \rangle\rangle = N \frac{8\pi^2 \langle\langle b^2 \rangle\rangle \delta(q_z)}{q^2 \sin^2 2\phi} \left\{ \Gamma(\hat{q}) \cdot \mathbf{1}_{2xy} \mathbf{1}_{2xy}^T \cdot \Gamma^T(-\hat{q}) \right\}, \quad (\text{E17})$$

where $\mathbf{1}_{2xy}^T \equiv (0, 0, 0, 0, 1)$ and we have used the fact that $\Gamma(-\hat{q}) = \Gamma(\hat{q})$. The factor of N is a consequence of the Central-Limit Theorem since the dislocations are uncorrelated and identically distributed. Despite the defects being spatially uncorrelated, the elastic strains clearly are correlated, with the incompatible projector $\Gamma(\hat{q})$ being responsible for the spatial correlations. To simplify the above, we use Eq. (E10). Defining it as the vector, Ψ , yields

$$\Psi = -\frac{\sin 2\phi}{2(1 - \nu_3)} \left(\frac{1 - 2\nu_3}{\sqrt{3}}, -\cos 2\phi, 0, 0, -\sin 2\phi \right)^T. \quad (\text{E18})$$

Then, the disordered averaged correlation function is

$$\langle\langle C(\mathbf{q}) \rangle\rangle = N \frac{8\pi^2 \langle\langle b^2 \rangle\rangle \delta(q_z)}{q^2 \sin^2 2\phi} \Psi \Psi^T. \quad (\text{E19})$$

The correlation function therefore will have six nonzero components (of a possible fifteen). There are three autocorrelations – that is, correlations generated within the same orbital basis function – and three cross-correlations. These six correlations functions are listed in Eq. (113).

The real-space functions are obtained through inverting the Fourier transform. Recalling the following trigonometric identities,

$$\begin{aligned} q^4 \cos(4\phi) &= q_x^4 + q_y^4 - 6q_x^2 q_y^2, \\ q^4 \sin(4\phi) &= 4q_x q_y (q_x^2 - q_y^2), \end{aligned} \quad (\text{E20})$$

it follows from Eq. (113) that

$$\begin{aligned} \langle\langle C_{z^2,z^2}(\mathbf{r}_\parallel) \rangle\rangle &= 2\pi^2 N \xi^2 \frac{(1-2\nu_3)^2}{3} \tilde{g}_2\left(\frac{r_\parallel}{L}\right), \\ \langle\langle C_{x^2-y^2,x^2-y^2}(\mathbf{r}_\parallel) \rangle\rangle &= \pi^2 N \xi^2 \left\{ \tilde{g}_2\left(\frac{r_\parallel}{L}\right) \right. \\ &\quad \left. + \left(\partial_x^4 + \partial_y^4 - 6\partial_x^2 \partial_y^2 \right) g_6(\mathbf{r}_\parallel) \right\}, \\ \langle\langle C_{2xy,2xy}(\mathbf{r}_\parallel) \rangle\rangle &= \pi^2 N \xi^2 \left\{ \tilde{g}_2\left(\frac{r_\parallel}{L}\right) \right. \\ &\quad \left. - \left(\partial_x^4 + \partial_y^4 - 6\partial_x^2 \partial_y^2 \right) g_6(\mathbf{r}_\parallel) \right\}, \\ \langle\langle C_{z^2,x^2-y^2}(\mathbf{r}_\parallel) \rangle\rangle &= 2\pi^2 N \xi^2 \cdot \frac{1-2\nu_3}{\sqrt{3}} \left[\left(\partial_x^2 - \partial_y^2 \right) g_4(\mathbf{r}_\parallel) \right], \\ \langle\langle C_{z^2,2xy}(\mathbf{r}_\parallel) \rangle\rangle &= 2\pi^2 N \xi^2 \cdot \frac{1-2\nu_3}{\sqrt{3}} \left[(2\partial_x \partial_y) g_4(\mathbf{r}_\parallel) \right], \\ \langle\langle C_{x^2-y^2,2xy}(\mathbf{r}_\parallel) \rangle\rangle &= \pi^2 N \xi^2 \left[4\partial_x \partial_y \left(\partial_x^2 - \partial_y^2 \right) g_6(\mathbf{r}_\parallel) \right], \end{aligned} \quad (\text{E21})$$

$$\langle\langle C_{x^2-y^2,2xy}(\mathbf{r}_\parallel) \rangle\rangle = \pi^2 N \xi^2 \left[4\partial_x \partial_y \left(\partial_x^2 - \partial_y^2 \right) g_6(\mathbf{r}_\parallel) \right], \quad (\text{E22})$$

with $\tilde{g}_2(r_\parallel/L)$ being a formally divergent integral that needs regularization, and where $g_6(\mathbf{r})$ is given in Eq. (G7). We proceed to compute the former and save the detailed calculations of the latter for Appendix G.

To regularize the divergent integral, we start by adding a mass, m , to the explicit expression for $g_2(\mathbf{r})$ to find

$$g_2(\mathbf{r}; m) \equiv \int \frac{d^3 q}{(2\pi)^3} \frac{\delta(q_z) e^{i\mathbf{q} \cdot \mathbf{r}}}{q^2 + m^2} = \frac{1}{2\pi} \int_0^\infty \frac{dq}{4\pi^2} \frac{q J_0(q r_\parallel)}{q^2 + m^2}, \quad (\text{E23})$$

where the second equality was obtained by exploiting the rotational symmetry and the Jacobi-Anger expansion. When $m \rightarrow 0$, this integral is logarithmically divergent in the lower-bound, and is associated with the linear size of a finite system, L . Using the Laplace transform of the cosine and Bessel functions, one obtains a regularized integral given by

$$g_2(r_\parallel; m) = \frac{1}{4\pi^2} K_0(m r_\parallel), \quad (\text{E24})$$

where $K_\nu(x)$ is the modified Bessel function of the second kind [140]. The behavior of $K_0(x)$ for small x is well-known to be

logarithmic: $K_0(x) \rightarrow -\log(x)$ [140]. In a periodic system of size L , the maximum separation between points is $L/2$. We therefore identify the regularizing mass, m , as $m^{-1} \equiv L/2$. Then, taking the limit of the Bessel function yields

$$\tilde{g}_2\left(\frac{r_\parallel}{L}\right) \equiv \lim_{L \rightarrow \infty} g_2\left(r_\parallel; \frac{2}{L}\right) \rightarrow \frac{1}{4\pi^2} \log\left(\frac{L}{2r_\parallel}\right). \quad (\text{E25})$$

In the limiting form, we have inverted the arguments of the logarithm by absorbing the overall negative sign. Importantly, notice that the limiting behavior of the regularized $\tilde{g}_2(r)$ yields the same fundamental Green's function in Eq. (G3). Combining these results and differentiating $g_6(\mathbf{r}_\parallel)$ from Eq. (G7) yields Eq. (114).

Appendix F: Multipolar Expansion of Plastic Strain

As discussed in Section VI and Appendix D, only the incompatible part of the plastic strain tensor is physical. This defines the defect density tensor in elasticity theory in terms of the elastic strain tensor. In the main text it is given as Eq. (82), and repeated here as

$$\eta_{ij}(\mathbf{x}) \equiv \text{inc}[\mathcal{E}(\mathbf{x})]_{ij} = -\text{inc}[\varepsilon^P(\mathbf{x})]_{ij}. \quad (\text{E22})$$

The defect density tensor is related to the disclination and dislocation density tensors, both of which are defect-gauge invariant quantities [89, 92]. Because of the manifest defect-gauge invariance of the defect density, in this appendix we compute the plastic strain tensor ε_{ij}^P in terms of η_{ij} . Using Eq. (86), we will then be able to formally compute the gauge-invariant elastic strain fields emanating from an arbitrary distribution of defects, which we will express as a multipolar expansion.

Because the plastic strain is a symmetric tensor, so is its incompatibility. Thus, η_{ij} is a rank-2 symmetric tensor which can be written in our helical decomposition from Eq. (43) (also Appendix B) as

$$\eta_{ij} \equiv \frac{1}{3} \eta_0 \delta_{ij} + \frac{1}{\sqrt{2}} \sum_{a=1}^5 \eta_a \vartheta_{ij}^a. \quad (\text{F1})$$

A similar decomposition follows for the plastic strain in Eq. (D7). From Eq. (59), applying the incompatibility operator to Eq. (D7) yields

$$\text{inc}(\varepsilon^P) = \frac{1}{3} \left(\varepsilon_0^P - \frac{\sqrt{3}}{2} \varepsilon_1^P \right) \text{inc}(I) + \frac{q^2}{\sqrt{2}} \sum_{a=4,5} \varepsilon_a^P \vartheta^a. \quad (\text{F2})$$

Recalling from Eq. (58) that $\text{inc}(I) = q^2 (Q^{11} - I)$, and using Eq. (B7), we write

$$\text{inc}(I) = \frac{2}{3} q^2 \left(\sqrt{\frac{3}{2}} \vartheta^1 - I \right). \quad (\text{F3})$$

Substituting this into the above, and making use of the incom-

patible dilatation, Δ_p , from Eq. (D8), we have that

$$\begin{aligned} \text{inc}(\varepsilon^p)_{ij} &= \frac{1}{3}(-\Delta_p) \cdot \frac{2}{3}q^2 \left(\sqrt{\frac{3}{2}}\vartheta_{ij}^1 - \delta_{ij} \right) + \frac{q^2}{\sqrt{2}} \sum_{a=4,5} \varepsilon_a^p \vartheta_{ij}^a \\ &= \frac{1}{3} \left(\frac{2}{3}q^2 \Delta_p \right) \delta_{ij} + \frac{1}{\sqrt{2}} \left(-\frac{2}{3\sqrt{3}}q^2 \Delta_p \right) \vartheta_{ij}^1 \\ &\quad + \frac{1}{\sqrt{2}} \sum_{a=4,5} \left(q^2 \varepsilon_a^p \right) \vartheta_{ij}^a. \end{aligned} \quad (\text{F4})$$

Comparing this decomposition to Eq. (F1), we can express the defect density coefficients in terms of the three physical contributions to the plastic strain as

$$\begin{aligned} \eta_0 &= -\frac{2}{3}q^2 \Delta_p, \quad \eta_1 = +\frac{2}{3\sqrt{3}}q^2 \Delta_p, \\ \eta_2 = \eta_3 &= 0, \quad \eta_4 = -q^2 \varepsilon_4^p, \quad \eta_5 = -q^2 \varepsilon_5^p. \end{aligned} \quad (\text{F5})$$

Importantly, we find that, despite the defect density tensor nominally having six elements as a rank-2 symmetric tensor, because there are only *three* incompatible components of the plastic strain, there are only *three* independent coefficients in η_{ij} . We choose the trace, η_0 , to be the independent degree of freedom, and write $\eta_1 = -\frac{1}{\sqrt{3}}\eta_0$.

With these relations, we can write the plastic strain tensor as

$$\begin{aligned} \varepsilon_{ij}^p &= \frac{1}{3}\varepsilon_0^p \delta_{ij} + \frac{1}{\sqrt{2}} \left\{ \left(\frac{2}{\sqrt{3}}\varepsilon_0^p \right) + \sum_{a=2,3} \varepsilon_a^p \vartheta_{ij}^a \right\} \\ &\quad - \frac{1}{q^2\sqrt{2}} \left\{ \left(\sqrt{3}\eta_0 \right) \vartheta_{ij}^1 + \sum_{a=4,5} \eta_a \vartheta_{ij}^a \right\}. \end{aligned} \quad (\text{F6})$$

Recognizing the first line in the second equality as a *compatible* tensor from Eq. (61), we can write it in terms of an unphysical defect-gauge vector field Λ . The plastic strain then simplifies to

$$\varepsilon_{ij}^p = \frac{i}{2} (q_j \Lambda_i + q_i \Lambda_j) - \frac{1}{q^2\sqrt{2}} \left\{ \left(\sqrt{3}\eta_0 \right) \vartheta_{ij}^1 + \sum_{a=4,5} \eta_a \vartheta_{ij}^a \right\}. \quad (\text{F7})$$

Focusing on incompatible part, and using Eq. (43), we can write it as

$$\frac{1}{q^2} \left\{ \sqrt{\frac{3}{2}}\vartheta_{ij}^1 \delta_{kl} + \sum_{a=4,5} \vartheta_{ij}^a \vartheta_{kl}^a \right\} \eta_{kl} \equiv \mathcal{G}_{ijkl}(\mathbf{q}) \eta_{kl}. \quad (\text{F8})$$

The Green's tensor above provides the formal solution to the plastic strain induced by any distribution of defects in Fourier and momentum space as

$$\begin{aligned} \varepsilon_{ij}^p &= \frac{i}{2} (q_j \Lambda_i + q_i \Lambda_j) - \mathcal{G}_{ijkl}(\mathbf{q}) \eta_{kl}, \\ \varepsilon_{ij}^p(\mathbf{x}) &= \frac{1}{2} [\partial_j \Lambda_i(\mathbf{x}) + \partial_i \Lambda_j(\mathbf{x})] - \int_{x'} \mathcal{G}_{ijkl}(\mathbf{x} - \mathbf{x}') \eta_{kl}(\mathbf{x}'). \end{aligned} \quad (\text{F9})$$

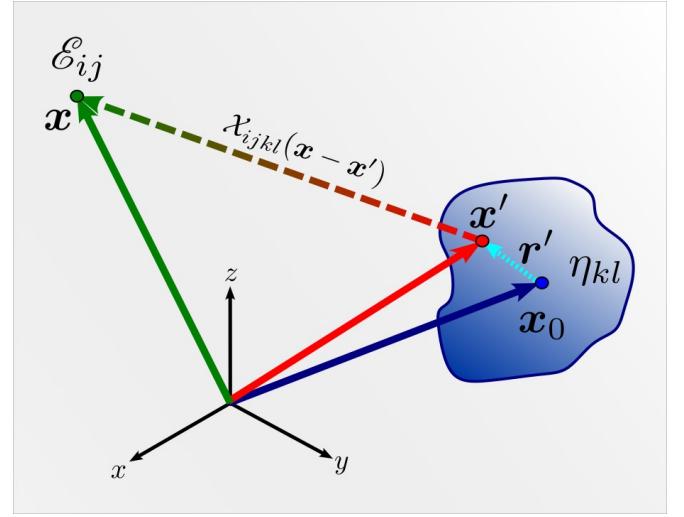


FIG. 9. Geometry of the multipolar defect expansion. This expansion approximates the elastic strain field $\mathcal{E}_{ij}(\mathbf{x})$ from a distribution of defects $\eta_{kl}(\mathbf{x}')$ (blue shaded region), centered on the point \mathbf{x}_0 . The propagation occurs through the Green's tensor, $X_{ijkl}(\mathbf{x} - \mathbf{x}')$, defined in Fourier space as Eq. (F12). The convolution in real-space, Eq. (F13), runs over the defect distribution with the integration variable, \mathbf{x}' , shifted relative to the center of the distribution through $\mathbf{r}' = \mathbf{x}' - \mathbf{x}_0$. In the far field limit, $\max(|\mathbf{r}'|) \ll |\mathbf{x} - \mathbf{x}_0|$.

The expression is universal for any defect density tensor in any medium as it is agnostic about the material-dependent elastic constants. Given that we have an expression for the unobservable *plastic* strain, one can formally obtain the observable, gauge-invariant, *elastic* strain with the use of Eq. (86). The compatible part that depends on Λ will not affect the elastic strain, as proven in Appendix D. In the case of an isotropic medium, we can substitute Eq. (F5) directly into Eq. (88) and obtain the gauge-invariant elastic strain as

$$\mathcal{E}_{ij} = \frac{1}{q^2} \left\{ \left[-\frac{1}{2}\varrho \delta_{ij} + \frac{3}{2\sqrt{2}}(1-\varrho) \vartheta_{ij}^1 \right] \delta_{kl} + \sum_{a=4,5} \vartheta_{ij}^a \vartheta_{kl}^a \right\} \eta_{kl}. \quad (\text{F10})$$

This last line defines another Green's tensor, $X_{ijkl}(\mathbf{q})$ which explicitly depends on the elastic constants, making it non-universal. This material-dependent tensor is defined by

$$\mathcal{E}_{ij} \equiv X_{ijkl}(\mathbf{q}) \eta_{kl}. \quad (\text{F11})$$

By comparing this expression with the general solution for the elastic strain, Eq. (86), and substituting in Eq. (F9), we find

$$X_{ijkl}(\mathbf{q}) = - \left[Q_{ij}^{1\alpha} \mathcal{S}_{\alpha\beta}(\hat{\mathbf{q}}) Q_{lk}^{1\beta} C_{klmn} - \delta_{im} \delta_{jn} \right] \mathcal{G}_{mnrs}(\mathbf{q}). \quad (\text{F12})$$

In real-space, the elastic strain for a medium of arbitrary symmetry is then formally written as

$$\mathcal{E}_{ij}(\mathbf{x}) = \int_{x'} X_{ijkl}(\mathbf{x} - \mathbf{x}') \eta_{kl}(\mathbf{x}'). \quad (\text{F13})$$

With the elastic strain known in terms of the Green's tensor, $X_{ijkl}(\mathbf{x})$, we can expand it formally in terms of multipolar defects. Assuming the defects are localized around some region centered on \mathbf{x}_0 , then we first change the integration variable to $\mathbf{r}' = \mathbf{x}' - \mathbf{x}_0$. Assuming one measures the elastic strain in the “far field” regime, such that $\max(|\mathbf{r}'|) \ll |\mathbf{x} - \mathbf{x}_0|$, then the integrand can be expanded as

$$X_{ijkl}(\mathbf{x} - \mathbf{x}_0 - \mathbf{r}') = X_{ijkl}(\mathbf{x} - \mathbf{x}_0) - r'_m \partial'_m X_{ijkl}(\mathbf{x} - \mathbf{x}_0) + \frac{1}{2} r'_m r'_n \partial'_m \partial'_n X_{ijkl}(\mathbf{x} - \mathbf{x}_0) + \dots \quad (\text{F14})$$

Using the identity $\partial'_m X_{ijkl}(\mathbf{x} - \mathbf{x}_0 - \mathbf{r}') = -\partial_m X_{ijkl}(\mathbf{x} - \mathbf{x}_0 - \mathbf{r}')$, then the elastic strain follows as

$$\mathcal{E}_{ij}(\mathbf{x}) = X_{ijkl}(\mathbf{x} - \mathbf{x}_0) \overline{\eta_{kl}} + \partial_m X_{ijkl}(\mathbf{x} - \mathbf{x}_0) \overline{\eta_{kl}^m} + \frac{1}{2} \partial_m \partial_n X_{ijkl}(\mathbf{x} - \mathbf{x}_0) \overline{\eta_{kl}^{mn}} + \dots \quad (\text{F15})$$

with the defect monopole, dipole, and quadrupole being defined by

$$\begin{aligned} \overline{\eta_{kl}} &\equiv \int_x \eta_{kl}(\mathbf{x}), \\ \overline{\eta_{kl}^m} &\equiv \int_x (x_m - x_0) \eta_{kl}(\mathbf{x}), \\ \overline{\eta_{kl}^{mn}} &\equiv \int_x (x_m - x_0)(x_n - x_0) \eta_{kl}(\mathbf{x}). \end{aligned} \quad (\text{F16})$$

Higher-order multipoles are generated in an analogous fashion. We remark that the monopolar and dipolar contributions are related to the Frank and Burgers vector of the disclination and dislocation, respectively [92, 101, 102]. In two spatial dimensions, only η_{33} is nonzero, and the resulting monopolar “charge” is the scalar-valued disclination [96–98]. Otherwise, in three dimensions, the monopole is vector-valued, given the three independent degrees of freedom in η_{ij} (see Eq. (F5)).

This multipole expansion establishes that one should expect long-ranged and potentially anisotropic elastic strain fields emanating from plastic defects. These will generically create pinning fields for the electronic nematic order parameter in the d -orbital basis, since the nematic-plastic conjugate field is the zero-nematic limit of the elastic strain: $\mathbf{h} = \mathcal{E}|_{\varphi=0}$. Meanwhile, because of defect-gauge invariance – present for a medium of any symmetry – the critical helical nematic order parameters, (Φ_2, Φ_3) , are orthogonal to the elastic strain, and do not participate in nematic-plasticity at the bilinear level.

Appendix G: Family of Fundamental Harmonic Green's Functions

In this appendix, we obtain the fundamental Green's function for the two-dimensional biharmonic and triharmonic equations, defined in Eq. (E13). We first note that from the definition of $g_n(\mathbf{r})$, that

$$\begin{aligned} \left(\partial_x^2 + \partial_y^2 \right) g_2(\mathbf{r}) &= -\frac{1}{2\pi} \delta(\mathbf{r}_\parallel), \\ \left(\partial_x^2 + \partial_y^2 \right)^2 g_4(\mathbf{r}) &= +\frac{1}{2\pi} \delta(\mathbf{r}_\parallel), \\ \left(\partial_x^2 + \partial_y^2 \right)^3 g_6(\mathbf{r}) &= -\frac{1}{2\pi} \delta(\mathbf{r}_\parallel), \end{aligned} \quad (\text{G1})$$

where $\mathbf{r}_\parallel \equiv (x, y, 0) \equiv r_\parallel (\cos \phi_r, \sin \phi_r, 0)$. Because of the $\delta(q_z)$ in Eq. (E13), there is no z -dependence in these partial differential equations. The fundamental Green's functions – the solutions to the above differential equations taken on the infinite domain – also satisfy a recursive relationship

$$\begin{aligned} \left(\partial_x^2 + \partial_y^2 \right) g_{2m}(\mathbf{r}) &= -g_{2(m-1)}(\mathbf{r}), \quad m \in \mathbb{Z}^+, \\ g_0(\mathbf{r}) &= -\frac{1}{2\pi} \delta(\mathbf{r}_\parallel). \end{aligned} \quad (\text{G2})$$

which can be integrated to obtain $n = 2, 4, 6$. Starting with $n = 2$, one obtains the function $g_2(\mathbf{r}_\parallel)$ using the same methods of electrostatics to obtain the electrostatic potential around a uniformly charged wire. Thus, we find $g_2(\mathbf{r}_\parallel)$ as

$$g_2(\mathbf{r}) = -\frac{1}{4\pi^2} \log(r_\parallel), \quad (\text{G3})$$

which happens to source the biharmonic Green's function as

$$\left(\partial_x^2 + \partial_y^2 \right) g_4(\mathbf{r}) = -g_2(\mathbf{r}). \quad (\text{G4})$$

Again, assuming infinite boundaries, one can readily obtain $g_4(r_\parallel)$, recalling that the two-dimensional cylindrically-symmetric Laplacian is

$$\left(\partial_x^2 + \partial_y^2 \right) g_4(r_\parallel) = \frac{1}{r_\parallel} \partial_{r_\parallel} [r_\parallel \partial_{r_\parallel} g_4(r_\parallel)]. \quad (\text{G5})$$

Integration yields

$$g_4(\mathbf{r}) = \frac{1}{16\pi^2} r_\parallel^2 [\log(r_\parallel) - 1]. \quad (\text{G6})$$

Iterating one final time yields $g_6(\mathbf{r})$ as

$$g_6(\mathbf{r}) = \frac{1}{512\pi^2} r_\parallel^4 [3 - 2\log(r_\parallel)]. \quad (\text{G7})$$

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