#### A Model With Clean and Dirty Capital Stocks and and R&D in Green Innovation-

Assume there are two capital sectors, each with AK production technology  $(Y_i = A_i K_i, i = d, g)$  and each with its own capital stock that evolves with quadratic adjustments costs and Brownian shocks as follows:

$$dK_d/K_d = \left[\alpha_d + i_d - \frac{\phi_d}{2}i_d^2\right]dt + \sigma_d dW$$
$$dK_g/K_g = \left[\alpha_g + i_g - \frac{\phi_g}{2}i_g^2\right]dt + \sigma_g dW$$

We also assume there is R&D investment that leads to an increased arrival rate of a one time jump in Sector 2 productivity. The arrival rate is denoted as t and evolves as follows

$$d\lambda_t/\lambda_t = (\varphi i_\lambda - \alpha_\lambda) dt + \sigma_\lambda dW$$

The key dierence between the sectors is that production from Sector 1 generates emissions. As a result, the evolution of atmospheric temperature is give by the Matthews Approximation, so that temperature  $Y_t$  and cumulative carbon emissions are given by

$$dY_t = E_t(\beta_f dt + \varsigma dW)$$

where  $\beta_f$  is the Matthews parameter and  $\eta$  is the scaling factor converting Sector d output  $A_dK_d$  into emissions such that

$$E_t = \eta A_d K_d$$

Output can be used in for consumption, investment in either capital stock, or for R&D into improving the productivity of Sector g :

$$C = A_d K_d - i_d K_d + A_a K_a - i_a K_a - i_\lambda \lambda$$

We assume exponential-quadratic damages to preferences so that our utility is augmented when accounting for climate damages. Flow utility is a log function over consumption, assuming perfect substitutability over output from the two sectors so that

$$U(C) = \delta \log(A_d K_d - i_d K_d + A_g K_g - i_g K_g - i_\lambda \lambda) - \delta \log N_t$$

where the  $\log N_t$  follows from BBH2 as

$$\log N_t = \Gamma(Y)$$

$$\Gamma(y) = \gamma_1 y + \frac{\gamma_2}{2} y^2 + \frac{\gamma_3}{2} \mathbf{1}_{y \ge \bar{y}} (y - \bar{y})^2$$

Taking these pieces together we get the HJB equation

$$\begin{split} \delta V(K_d,K_g,\lambda,Y,\log N) &= \max_{i_g,i_d,i_\lambda} \delta \log(A_dK_d - i_dK_d + A_gK_g - i_gK_g - i_\lambda\lambda) - \delta \log N \\ &+ \{\alpha_d + i_d - \frac{\phi_d}{2}i_d^2\}V_dK_d + \{\alpha_g + i_g - \frac{\phi_g}{2}i_g^2\}V_gK_g + \frac{\sigma_d^2K_d^2}{2}V_{dd} + \frac{\sigma_g^2K_g^2}{2}V_{gg} \\ &+ \beta_f E_dV_Y + \frac{1}{2}\varsigma^2E_d^2V_{YY} + [\{\gamma_1 + \gamma_2Y_t\}\beta_fE_d + \frac{\gamma_2}{2}\varsigma^2E_d^2]V_{\log N} + \frac{\varsigma^2E_d^2}{2}V_{\log N\log N} \\ &+ (\varphi i_\lambda - \alpha_\lambda)\lambda V_\lambda + \frac{(\sigma_\lambda\lambda)^2}{2}V_{\lambda\lambda} + \lambda\left(V(K_d,K_g,\lambda,Y,\log N;A_g') - V(K_d,K_g,\lambda,Y,\log N;A_g)\right) \end{split}$$

The FOC for investment and R&D are given by

$$0 = -\delta (A_d K_d - i_d K_d + A_g K_g - i_g K_g - i_\lambda \lambda)^{-1} + (1 - \phi_d i_d) V_d$$
  

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$$0 = -\delta (A_d K_d - i_d K_d + A_g K_g - i_g K_g - i_\lambda \lambda)^{-1} + \varphi V_\lambda$$

Using the fact that  $\varphi V_{\lambda} = \delta (A_d K_d - i_d K_d + A_g K_g - i_g K_g - i_{\lambda} \lambda)^{-1}$ , we can simplify to

$$\begin{split} i_d &= \frac{1}{\phi_d} - \frac{\varphi}{\phi_d} \frac{V_\lambda}{V_d} \\ i_g &= \frac{1}{\phi_g} - \frac{\varphi}{\phi_g} \frac{V_\lambda}{V_g} \\ i_\lambda &= \frac{1}{\lambda} \left( (A_d - (\frac{1}{\phi_d} - \frac{\varphi}{\phi_d} \frac{V_\lambda}{V_d})) K_d + (A_g - (\frac{1}{\phi_g} - \frac{\varphi}{\phi_g} \frac{V_\lambda}{V_g})) K_g - \frac{\delta}{\varphi V_\lambda} \right) \end{split}$$

We can analytically simplify out  $\log Nt$  to get a simplied HJB

$$\begin{split} \delta v(K_d,K_g,\lambda,Y) &= \max_{i_g,i_d,i_\lambda} \delta \log (A_dK_d - i_dK_d + A_gK_g - i_gK_g - i_\lambda\lambda) \\ &+ \{\alpha_d + i_d - \frac{\phi_d}{2}i_d^2\}v_dK_d + \{\alpha_g + i_g - \frac{\phi_g}{2}i_g^2\}v_gK_g + \frac{\sigma_d^2K_d^2}{2}v_{dd} + \frac{\sigma_g^2K_g^2}{2}v_{gg} \\ &+ \beta_f E_d v_Y + \frac{1}{2}\varsigma^2 E_d^2 v_{YY} - [\{\gamma_1 + \gamma_2 Y_t\}\beta_f E_d + \frac{\gamma_2}{2}\varsigma^2 E_d^2] \\ &+ (-\alpha_\lambda + \varphi i_\lambda)\lambda v_\lambda + \frac{(\sigma_\lambda\lambda)^2}{2}v_{\lambda\lambda} + \lambda \left(v(K_d,K_g,\lambda,Y;A_g') - v(K_d,K_g,\lambda,Y;A_g)\right) \end{split}$$

FOC

$$\begin{split} i_d &= \frac{1}{\phi_d} - \frac{\varphi}{\phi_d} \frac{v_\lambda}{v_d} \\ i_g &= \frac{1}{\phi_g} - \frac{\varphi}{\phi_g} \frac{v_\lambda}{v_g} \\ i_\lambda &= \frac{1}{\lambda} \left( (A_d - (\frac{1}{\phi_d} - \frac{\varphi}{\phi_d} \frac{v_\lambda}{v_d})) K_d + (A_g - (\frac{1}{\phi_g} - \frac{\varphi}{\phi_g} \frac{v_\lambda}{v_g})) K_g - \frac{\delta}{\varphi v_\lambda} \right) \end{split}$$

From this we can layer on different forms of uncertainty.

## 1 Post jump

Replace  $E_d$  with  $\eta A_d K_d$ . We solve post jump HJB:

$$\begin{split} \delta v(K_d, K_g, Y; A_g') &= \max_{i_g, i_d} \delta \log(A_d K_d - i_d K_d + A_g' K_g - i_g K_g) \\ &+ \{\alpha_d + i_d - \frac{\phi_d}{2} i_d^2\} v_d K_d + \{\alpha_g + i_g - \frac{\phi_g}{2} i_g^2\} v_g K_g + \frac{\sigma_d^2 K_d^2}{2} v_{dd} + \frac{\sigma_g^2 K_g^2}{2} v_{gg} \\ &+ \beta_f (\eta A_d K_d) v_Y + \frac{1}{2} \varsigma^2 (\eta A_d K_d)^2 v_{YY} - [\{\gamma_1 + \gamma_2 Y_t\} \beta_f (\eta A_d K_d) + \frac{\gamma_2}{2} \varsigma^2 (\eta A_d K_d)^2] \end{split}$$

denote

$$mc = \delta (A_d K_d - i_d K_d + A'_q K_g - i_g K_g)^{-1}$$

FOC

$$i_d = \frac{1}{\phi_d} - \frac{mc}{\phi_d v_d}$$
$$i_g = \frac{1}{\phi_g} - \frac{mc}{\phi_g v_g}$$

$$X = [\log K, L, Y]', \quad \log K = \log(K_d + K_g), \quad L = \log K_g - \log K_d$$

$$R = \frac{K_g}{K_d + K_g} = \frac{\exp(L)}{1 + \exp(L)}$$

$$\begin{split} \mathrm{d}(K_d + K_g) &= \left( [\alpha_d + i_d - \frac{\phi_d}{2} i_d^2] K_d + [\alpha_g + i_g - \frac{\phi_g}{2} i_g^2] K_g \right) \mathrm{d}t + (\sigma_d K_d + \sigma_g K_g) \, \mathrm{d}W \\ \mathrm{d}K/K &= \left( [\alpha_d + i_d - \frac{\phi_d}{2} i_d^2] (1 - R) + [\alpha_g + i_g - \frac{\phi_g}{2} i_g^2] R \right) \mathrm{d}t + (\sigma_d (1 - R) + \sigma_g R) \, \mathrm{d}W \\ \mathrm{d}\log K &= \left( [\alpha_d + i_d - \frac{\phi_d}{2} i_d^2] (1 - R) + [\alpha_g + i_g - \frac{\phi_g}{2} i_g^2] R - \frac{|\sigma_d (1 - R) + \sigma_g R|^2}{2} \right) \mathrm{d}t \\ &+ (\sigma_d (1 - R) + \sigma_g R) \, \mathrm{d}W \end{split}$$

$$dL = d(\log K_g - \log K_d) = \left( (\alpha_g + i_d - \frac{\phi_g}{2} i_g^2) - (\alpha + i_d - \frac{\phi_d}{2} i_d^2) \right) dt + (\sigma_g - \sigma_d) dW$$
$$dY = \eta A_d (1 - R) K(\beta_f dt + \varsigma dW)$$

$$\begin{split} \delta v(\log K, L, Y; A_g') &= \max_{i_g, i_d} \delta \log((A_d - i_d)(1 - R) + (A_g' - i_g)R) + \delta \log K \\ &+ \left( \{\alpha_d + i_d - \frac{\phi_d}{2}i_d^2\}(1 - R) + \{\alpha_g + i_g - \frac{\phi_g}{2}i_g^2\}R - \frac{|\sigma_d(1 - R) + \sigma_g R|^2}{2} \right) v_k \\ &+ \frac{|\sigma_d(1 - R) + \sigma_g R|^2}{2} v_{kk} \\ &+ \left( (\alpha_g + i_g - \frac{\phi_g}{2}i_g^2) - (\alpha + i_d - \frac{\phi_d}{2}i_d^2) \right) v_l \\ &+ \beta_f (\eta A_d(1 - R)K) v_Y + \frac{1}{2} \varsigma^2 (\eta A_d(1 - R)K)^2 v_{YY} \\ &- [\{\gamma_1 + \gamma_2 Y_t\} \beta_f (\eta A_d(1 - R)K) + \frac{\gamma_2}{2} \varsigma^2 (\eta A_d(1 - R)K)^2] \end{split}$$

$$\begin{split} \delta v(\log K, R, Y; A_g') &= \max_{i_g, i_d} \delta \log((A_d - i_d)(1 - R) + (A_g' - i_g)R) + \delta \log K \\ &+ \left( \{\alpha_d + i_d - \frac{\phi_d}{2} i_d^2\}(1 - R) + \{\alpha_g + i_g - \frac{\phi_g}{2} i_g^2\}R - \frac{\mid \sigma_d(1 - R) + \sigma_g R\mid^2}{2} \right) v_k \\ &+ \frac{\mid \sigma_d(1 - R) + \sigma_g R\mid^2}{2} v_{kk} \\ &+ \left( (\alpha_g + i_g - \frac{\phi_g}{2} i_g^2) - (\alpha + i_d - \frac{\phi_d}{2} i_d^2) \right) [R(1 - R)] \, v_r \\ &+ \beta_f (\eta A_d(1 - R)K) v_Y + \frac{1}{2} \varsigma^2 (\eta A_d(1 - R)K)^2 v_{YY} \\ &- [\{\gamma_1 + \gamma_2 Y_t\} \beta_f (\eta A_d(1 - R)K) + \frac{\gamma_2}{2} \varsigma^2 (\eta A_d(1 - R)K)^2] \end{split}$$

FOC

$$mc = \delta((A_d - i_d)(1 - R) + (A'_q - i_g)R)^{-1}$$

$$mc = (1 - \phi_d i_d) \left( (v_k - R v_r) \right)$$

$$\Rightarrow i_d = \frac{1}{\phi_d} \left[ 1 - \frac{mc}{v_k - R v_r} \right]$$

$$mc = (1 - \phi_g i_g) \left( v_k + (1 - R) v_l \right)$$

$$\Rightarrow i_g = \frac{1}{\phi_g} \left[ 1 - \frac{mc}{v_k + (1 - R) v_r} \right]$$

#### 1.1 tests

## 1.1.1 Preliminary results: try $i_d = i_g = 0$ , no optimization

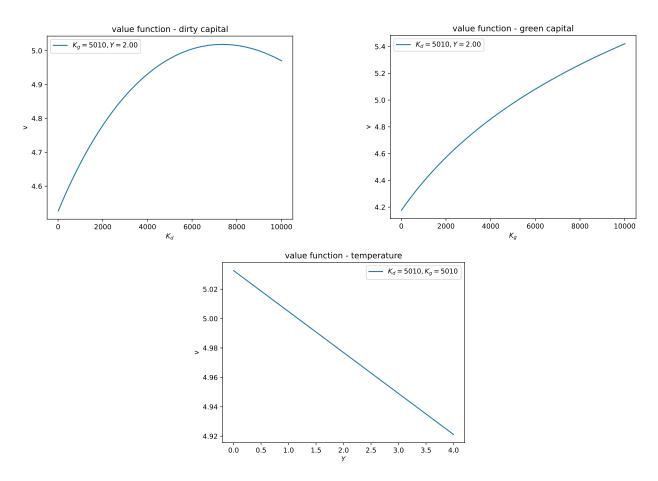


Figure 1: Results for value function,  $i_d=0, i_g=0$ 

#### 1.1.2 steady state

try set

$$\alpha_d + i_d - \frac{\phi_d}{2}i_d^2 = 0 \Rightarrow i_d^* = 0.022$$

$$\alpha_g + i_g - \frac{\phi_g}{2}i_g^2 = 0 \Rightarrow i_g^* = 0.022$$

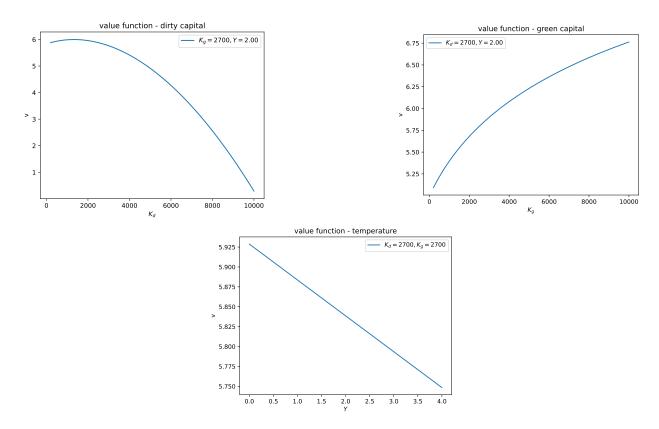


Figure 2: Results for value function,  $i_d^{\ast}=0.022, i_g^{\ast}=0.022$ 

# 2 Pre jump

## A State variables

Capital:

$$K_d \in [0, 10, 000]$$
  
 $K_g \in [0, 10, 000]$   
 $\lambda \in [0, 0.1]$   
 $Y \in [0, 4]$ 

### **B** Parameters

Economy

Parameters	values
δ	0.01
$(\alpha_d, \phi_d, \sigma_d)$	(-0.02, 8, 0.016)
$(\alpha_g, \phi_g, \sigma_g)$	(-0.02, 8, 0.016)
$(\alpha_{\lambda}, \varphi, \sigma_{\lambda})$	(0, 0.1, 0.016)
$A_d$	0.12
$(A_g, A_g')$	(0.10, 0.15)

Temperature and damage

Parameters	values
$\beta_f$	1.86 / 1000
ς	1.2*1.86 / 1000
$\gamma_1$	0.00017675
$\gamma_2$	2 * 0.0022
$\gamma_3$	0
$ar{y}$	2

 $\eta$  are determined as follows:

• Initial capital:  $K_0 = 85/0.115 \approx 739$ 

•  $K_{d,0} = K_0 \times \frac{2}{3} \approx 493$ 

• Choose  $\eta$  such that  $10 = \eta \times 0.12 \times 493 \Rightarrow \eta \approx 0.17$