

Control Systems

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CONTENTS

Abstract—The objective of this manual is to introduce control system design at an elementary level.

Download python codes using

svn co <https://github.com/gadepall/school/trunk/control/ketan/codes>

1 COMPENSATORS

1.1 Phase Lead

1.1. Given the unity feedback system of Fig. ?? , with

$$G(s) = \frac{K}{s(s+5)(s+20)} \quad (1.1.1)$$

The uncompensated system has about 55% peak overshoot and a peak time of 0.5 seconds when $K_v = 10$. Use frequency response technique to design a lead compensator to reduce the percent overshoot to 10% , while keeping the peak time and steady state error about the same or less. Consider second order approximations.

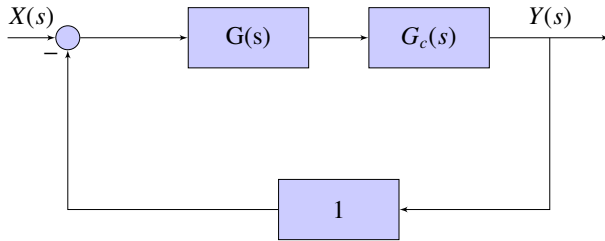


Fig. 1.1

1.2. Solution:

$$K_v = \lim_{s \rightarrow 0} sG(s) = 10 \quad (1.2.1)$$

$$\Rightarrow K = 1000 \quad (1.2.2)$$

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The bode plot for $G(s)$ is as follows :

$$G(s) = \frac{1000}{s(s+5)(s+20)} \quad (1.2.3)$$

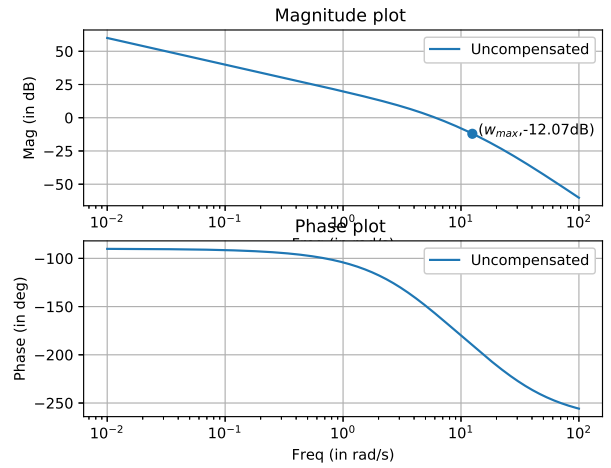


Fig. 1.2: $G(s)$ Bode Plot

$$\zeta = \frac{-\ln\left(\frac{OS\%}{100}\right)}{\sqrt{\pi^2 + \left(\ln\left(\frac{OS\%}{100}\right)\right)^2}} \quad (1.2.4)$$

$$PhaseMargin = \phi_M = \tan^{-1} \left(\frac{2\zeta}{\sqrt{-2\zeta^2 + \sqrt{4\zeta^4 + 1}}} \right) \quad (1.2.5)$$

The following code computes the above quantities.

codes/ee18btech11026/ee18btech11026_1.py

The required additional phase contribution by the compensator will be:

$$\phi_{max} = 58.9 - 21.16 + correctionfactor \quad (1.2.6)$$

$$CorrectionFactor = 25^\circ \quad (1.2.7)$$

Specifications	Actual	Expected
OS%	55%	10%
ζ	0.186	0.591
ϕ_m	21.16°	58.59°
T_p	0.5	≤ 0.5
K_v	10	≤ 10

TABLE 1.2: Table of Specifications

$$\phi_{max} = 62^\circ \quad (1.2.8)$$

Note : Since we know that the lead network will also increase the phase-margin frequency, we add a correction factor to compensate for the lower uncompensated systems phase angle. Choosing the correction factor is a trial and error procedure so as to reach our expected specifications.

The gain compensator's T.F will be of the form:

$$G_c(s) = \frac{1}{\beta} \left(\frac{s + \frac{1}{T}}{s + \frac{1}{T\beta}} \right) \quad (1.2.9)$$

This form of T.F does not influence the steady state error.

Important Relations to find T and β :

$$\phi_{max} = \tan^{-1} \frac{1 - \beta}{2\sqrt{\beta}} \quad (1.2.10)$$

The Compensator's magnitude at the phase margin frequency ω_{max}

$$|G_c(j\omega_{max})| = \frac{1}{\sqrt{\beta}} \quad (1.2.11)$$

$$T = \frac{1}{\omega_{max} \sqrt{\beta}} \quad (1.2.12)$$

Using the above formulae :

$$\beta = 0.062 \quad (1.2.13)$$

$$|G_c(j\omega_{max})| = 12.07 \text{ dB} \quad (1.2.14)$$

If we select ω_{max} to be the new phase-margin frequency, the uncompensated systems magnitude at this frequency must be -12.07 dB to yield a 0 dB crossover at ω_{max} for the compensated system.

From the bode plot of the un-compensated

system, find ω_{max} where the magnitude is -12.07 dB. This becomes our new phase-margin frequency.

$$\omega_{max} = 12.5 \text{ rad/sec} \quad (1.2.15)$$

$$T = 0.321 \quad (1.2.16)$$

The Compensator's T.F is as follows :

$$G_c(s) = 16.13 \left(\frac{s + 3.115}{s + 50.25} \right) \quad (1.2.17)$$

The open loop T.F for the compensated system is :

$$G(s).G_c(s) = 16130 \left(\frac{(s + 3.115)}{s(s + 50.25)(s + 5)(s + 20)} \right) \quad (1.2.18)$$

1.3. Verification : We could observe the affect of the lead-phase compensator from the phase plots.

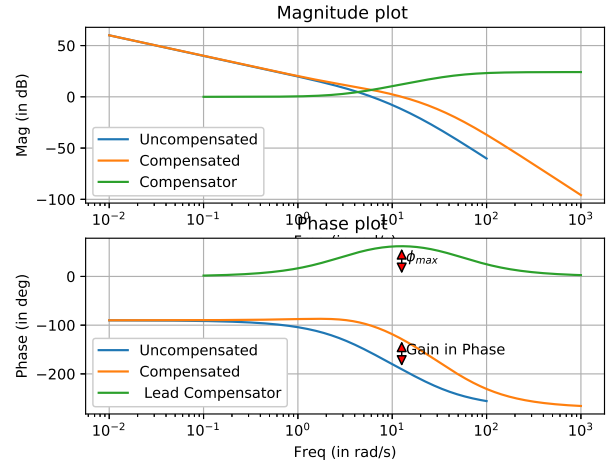


Fig. 1.3: Combined Bode Plots

The time responses for a unit step input in a unity feedback system with and without a compensator are as follows :

These plots are generated using the below code:

```
codes/ee18btech11026/ee18btech11026_2.py
```

1.4. Result : The below is the summary for the designed lead-compensator

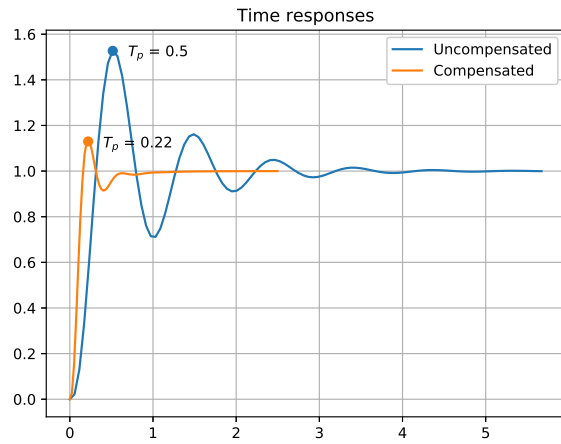


Fig. 1.3: Time response for a unit step input

Specifications	Expected	Proposed
OS%	10%	11%
T_p	≤ 0.5	0.22
K_v	≤ 10	10

TABLE 1.4: Comparing the desired and obtained results