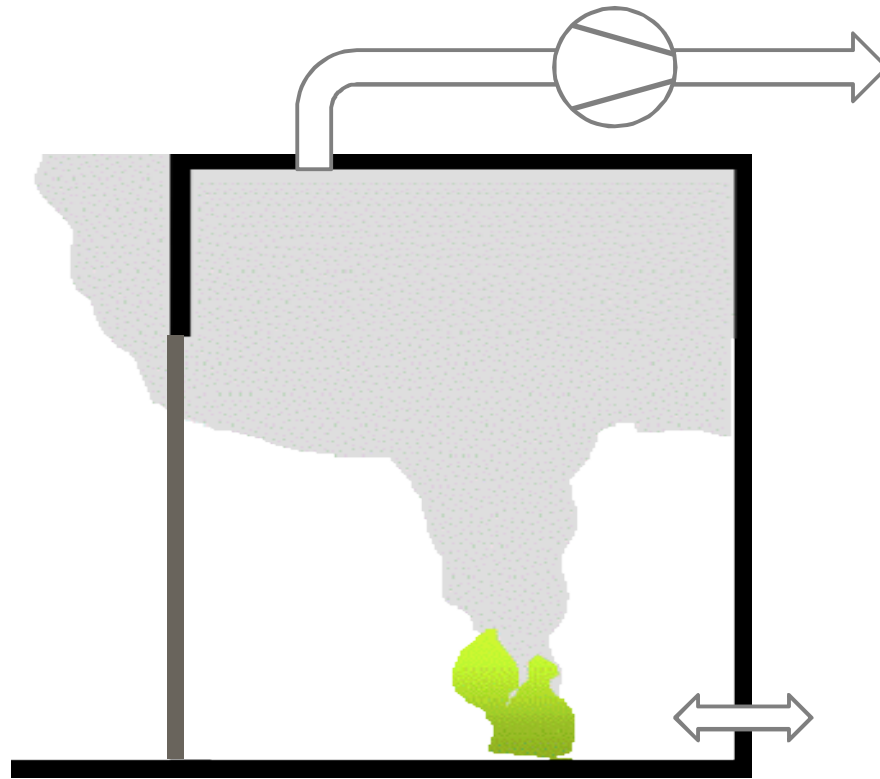


# Fire Modelling of Energy-Efficient Apartment Buildings – Consideration of air-tightness and mechanical ventilation

*Simo Hostikka  
Aalto University, Finland*

*Fire and Evacuation Modelling Technical Conference (FEMTC) 2016*

# Background



# The project

## Partners

- Aalto University
- Stravent Oy
- Southwest Finland Rescue Service
- Markku Kauriala Oy
- VTT Technical Research Centre of Finland Ltd.

## Thanks to

- Rahul Kallada Janardhan
- Umar Riaz
- Topi Sikanen (VTT)

## Sponsors

- Finnish Fire Protection Fund
- Hagab AB
- Criminal Sactions Agency
- Ministry of Environment



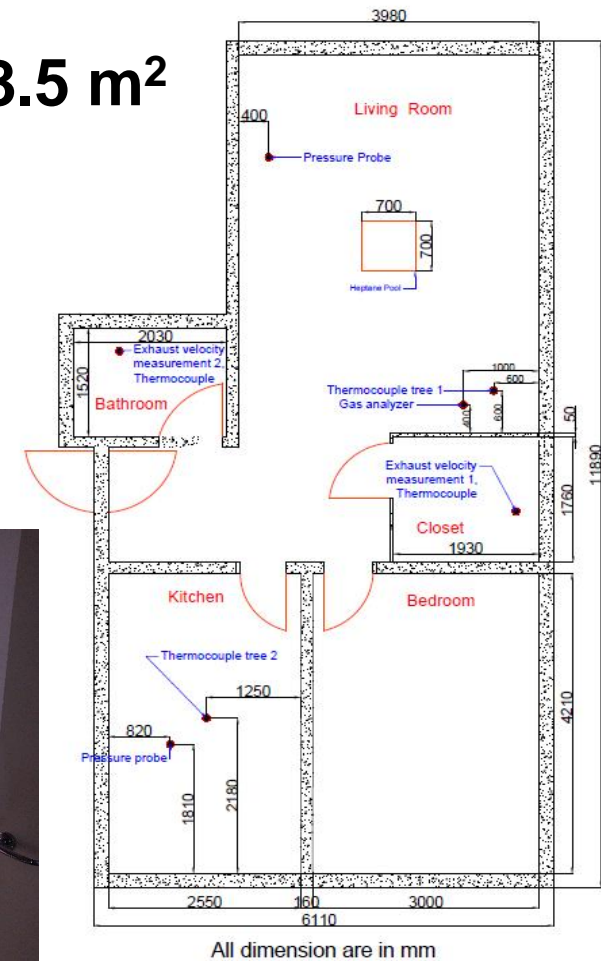
# Fire experiments

- 3-storey apartment building in Kurikka, western Finland
- Built in 1970's.
- Windows renewed few years ago.
- Tests in a 1st floor apartment

[https://www.youtube.com/watch?v=0Ss\\_ONolzLY](https://www.youtube.com/watch?v=0Ss_ONolzLY)



58.5 m<sup>2</sup>



# Air tightness measurements

SFS-EN 13829, Mikko Yli-Piipari / Vertia Oy



# Results of the air-tightness

Direction	$\Delta p$ [Pa]	$\dot{V}_{ \Delta p }$ [m <sup>3</sup> /s]	$q_{ \Delta p }$ [m <sup>3</sup> /hm <sup>2</sup> ]	$n_{ \Delta p }$ [1/h]	$A_{\text{leak}}$ [m <sup>2</sup> ]	$A_{\text{leak}}/A_{\text{env}}$
Underpressure	-30	0.047	1.0	1.1	0.011	$0.70 \times 10^{-4}$
Underpressure	-50	0.078	1.7	1.9	0.015	$0.89 \times 10^{-4}$
Underpressure	-70	0.10	2.2	2.4	0.016	$0.97 \times 10^{-4}$
Overpressure	30	0.091	2.0	2.2	0.022	$1.4 \times 10^{-4}$
Overpressure	50	0.12	2.7	2.9	0.023	$1.4 \times 10^{-4}$
Overpressure	70	0.15	3.3	3.6	0.024	$1.5 \times 10^{-4}$

## RakMK D3 (2012)

Requirement:  $q_{50} \leq 4 \text{ m}^3/\text{hm}^2$

Recommendation:  $q_{50} \leq 1 \text{ m}^3/\text{hm}^2$

## NFPA 92 (2012):

Very loose:  $A_{\text{leak}}/A_{\text{env}} = 12 \cdot 10^{-4}$

Loose:  $A_{\text{leak}}/A_{\text{env}} = 3.5 \cdot 10^{-4}$

Average:  $A_{\text{leak}}/A_{\text{env}} = 1.7 \cdot 10^{-4}$

Tight:  $A_{\text{leak}}/A_{\text{env}} = 0.50 \cdot 10^{-4}$

$$\dot{V}_{\text{leak}} = A_L C_d \text{sign}(\Delta p) \left( \frac{2 |\Delta p|}{\rho} \right)^{1/2}$$



# Ventilation configurations

**CLOSED**



**OPEN**



**NORMAL**



# Fire loads

## Group 1 (10 tests)

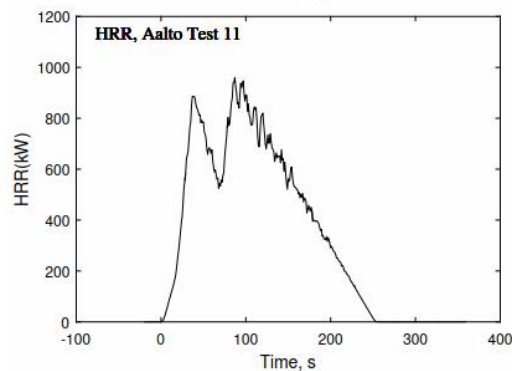
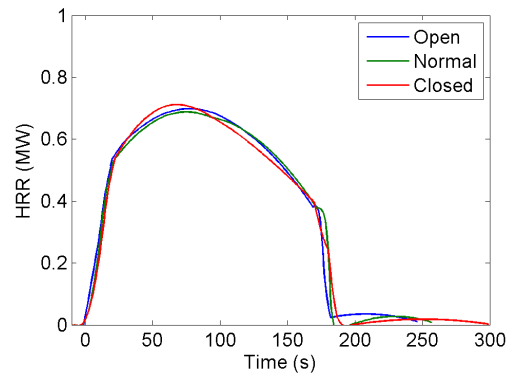
3 L n-heptane

0.7 m x 0.7 m pool

## Group 2 (3 tests)

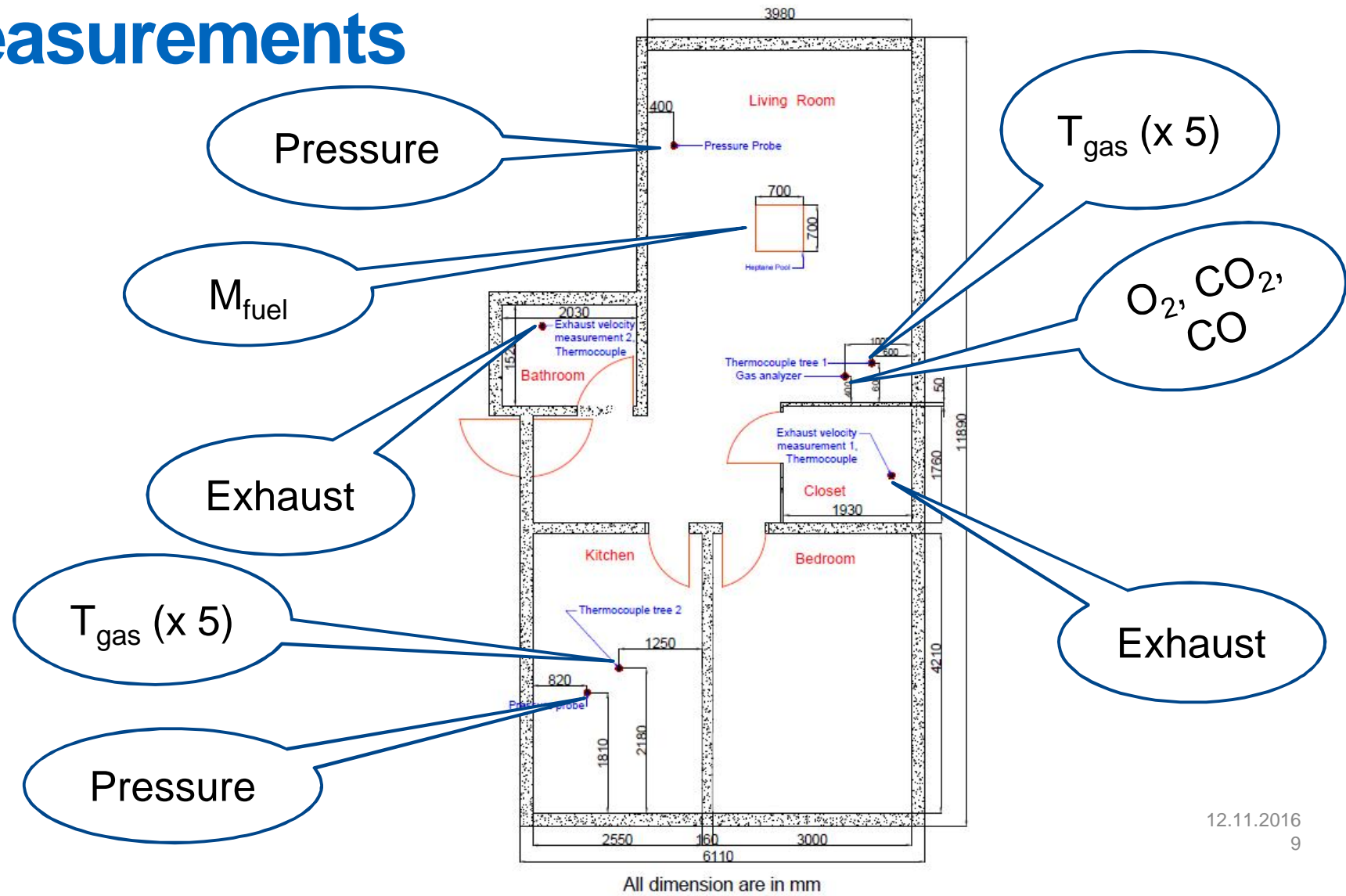
PUF mattress of about 3 kg

Both fires were ultrafast ( $t_g < 75$  s)





# Measurements

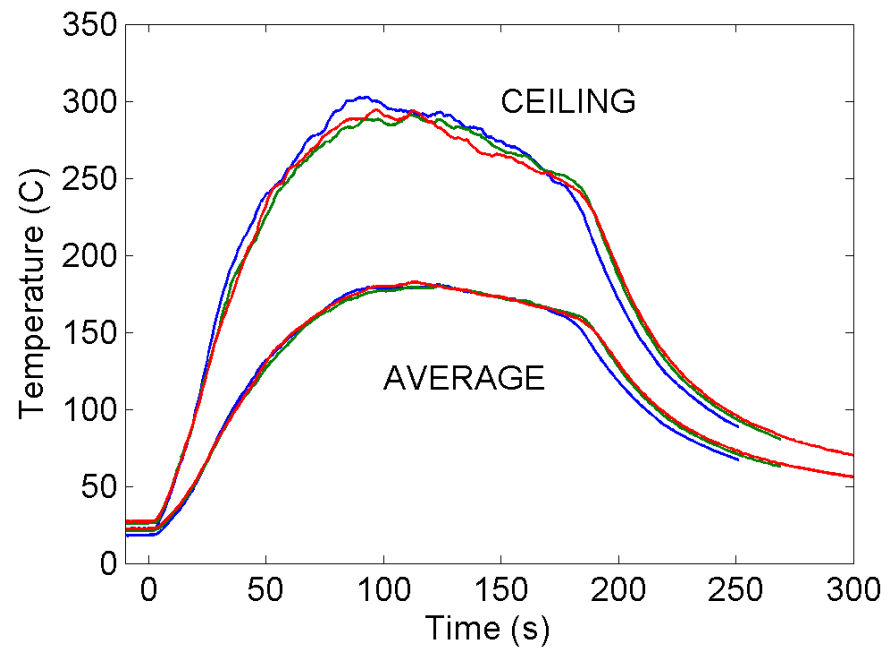




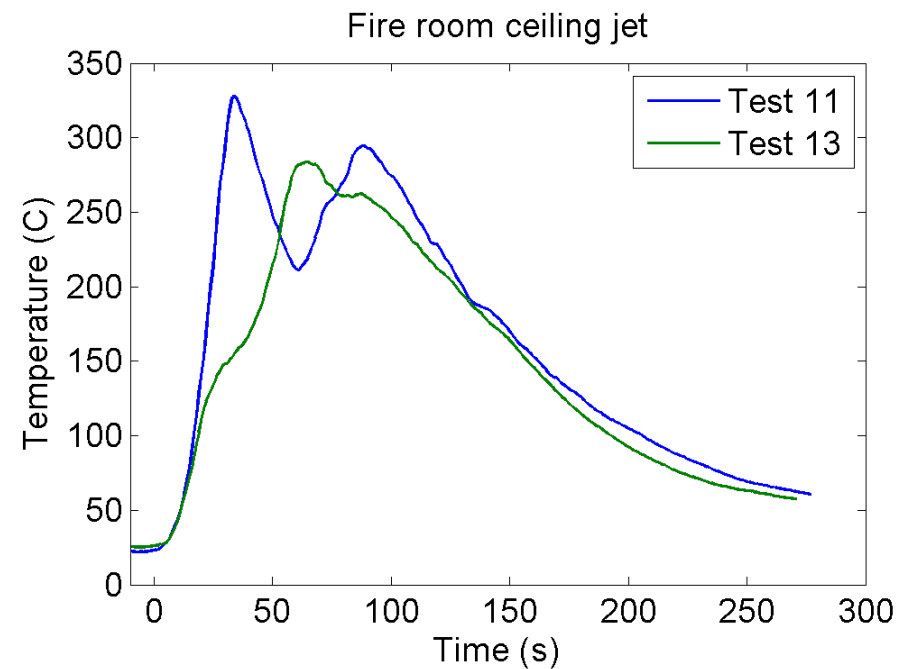
12.11.2016  
10

# Gas temperatures

## Heptane fires

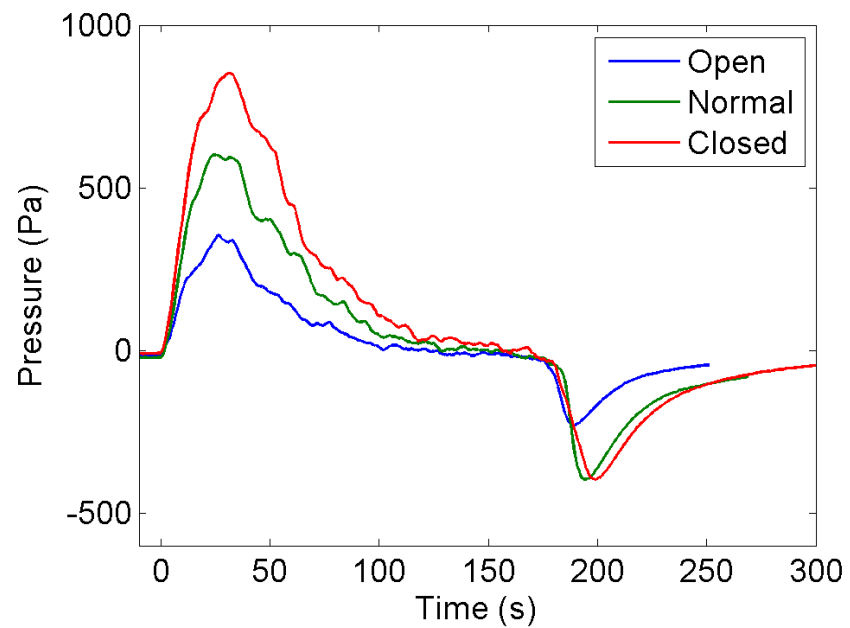


## PUF fires

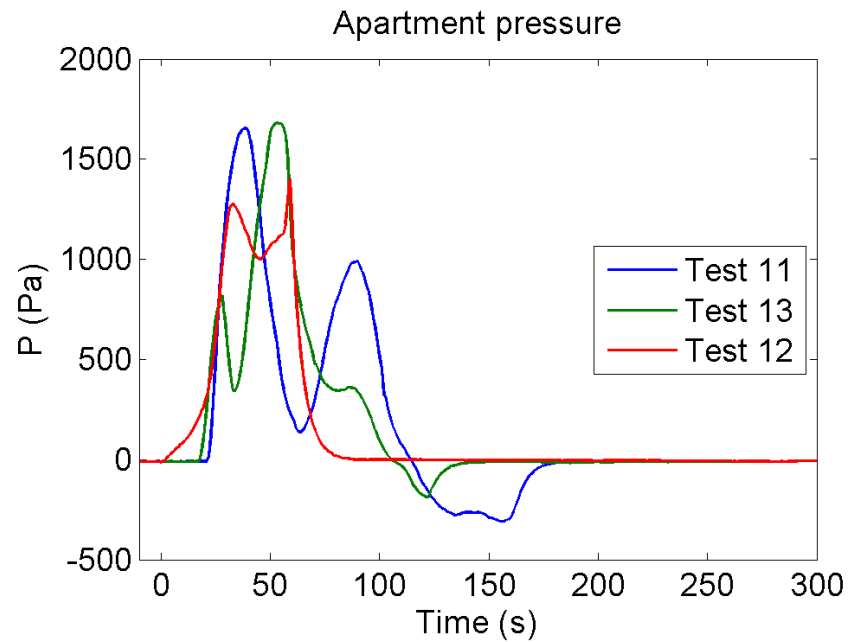


# Gas pressure

## Heptane fires



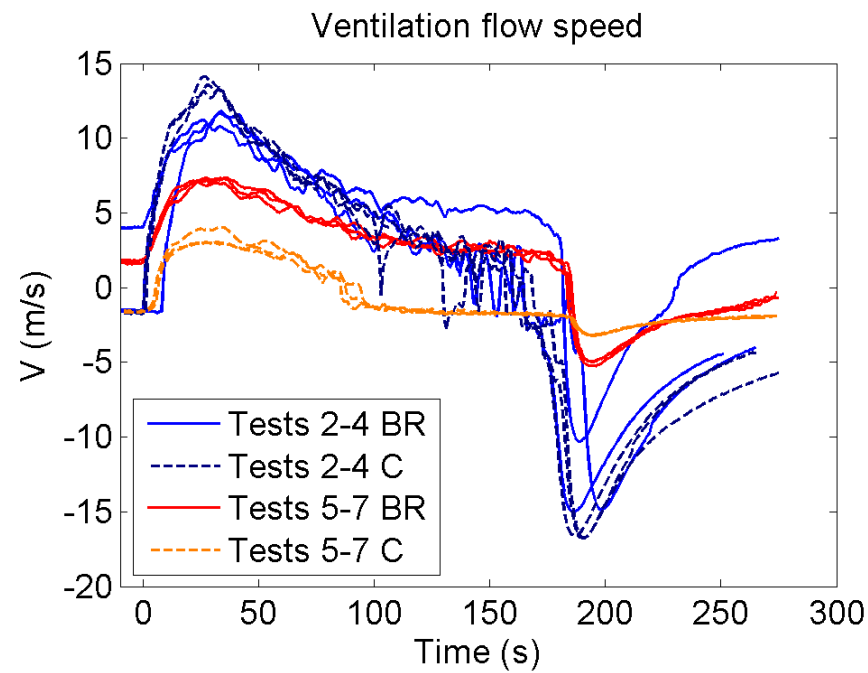
## PUF fires



# Flow speed in exhaust duct

## Heptane pool fires

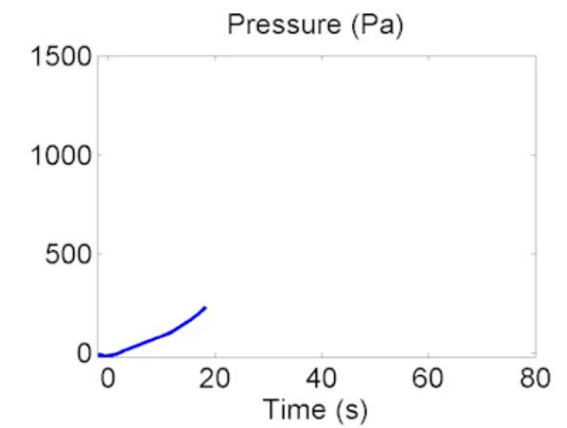
Test 2-4: OPEN  
Test 5-7: NORMAL  
BR = bathroom  
C = closet





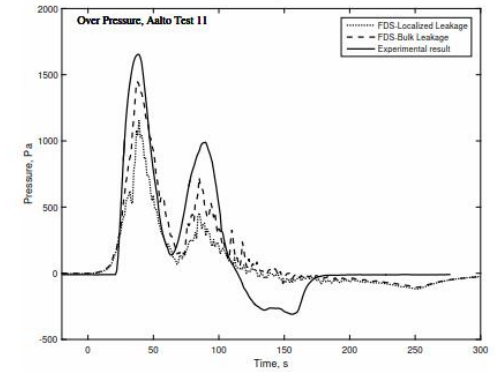
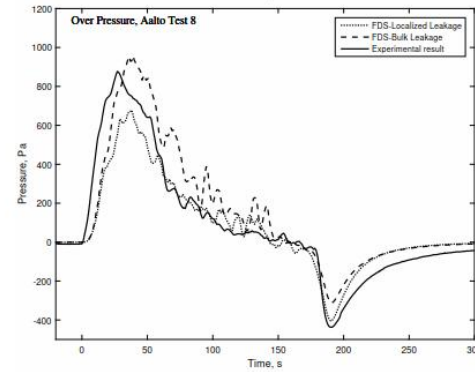
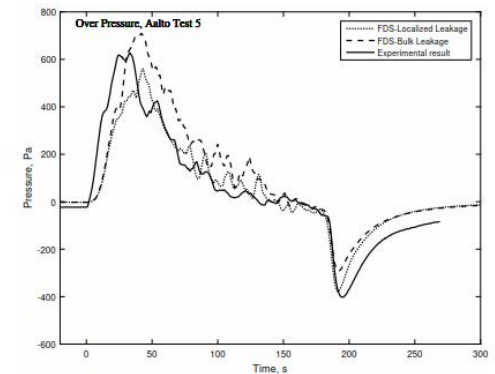
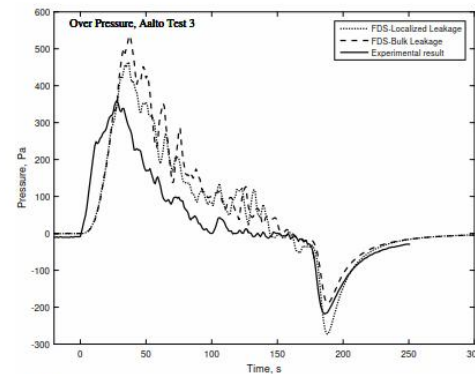
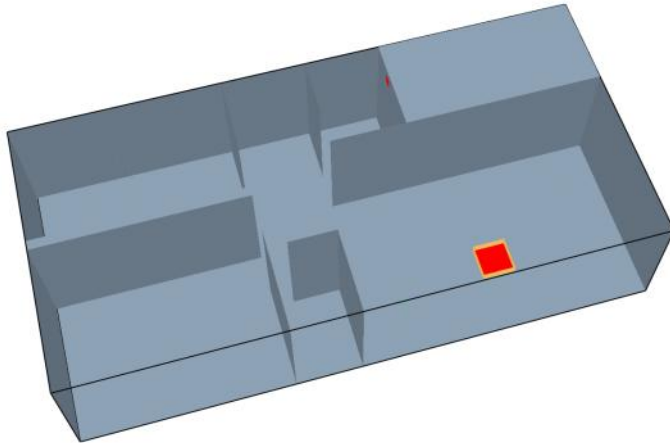


# PUF in closet, normal ventilation



# Validation of FDS modelling

**Prescribed HRR**  
**Simple HVAC**  
**Local / bulk leakage**

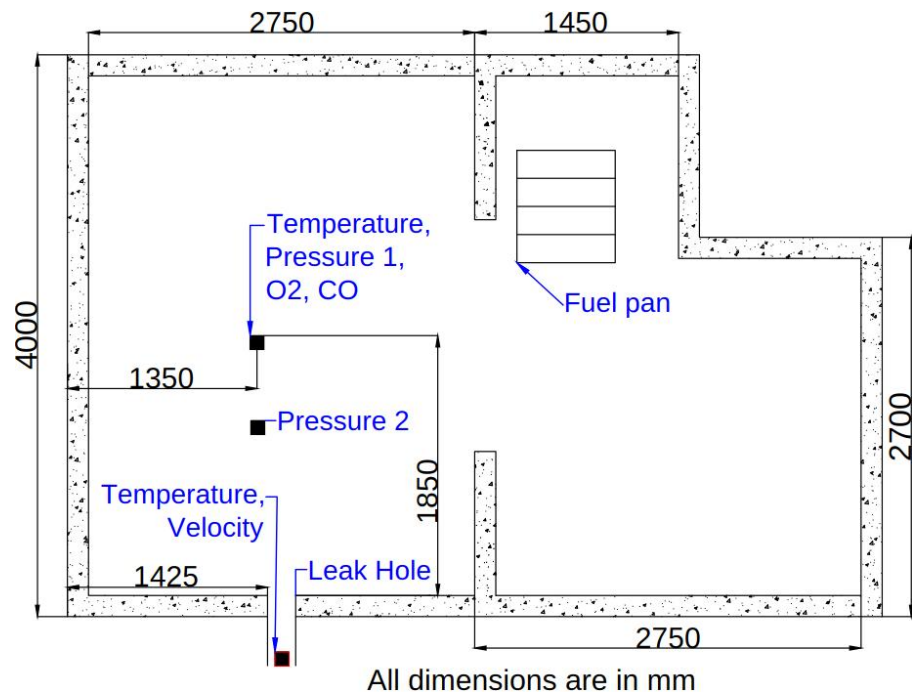


# Additional validation data

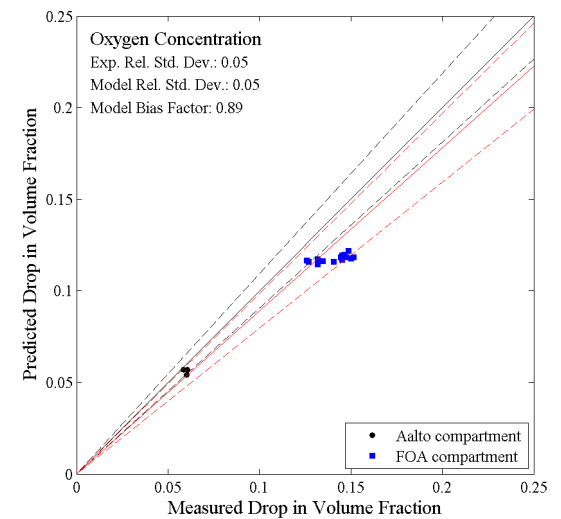
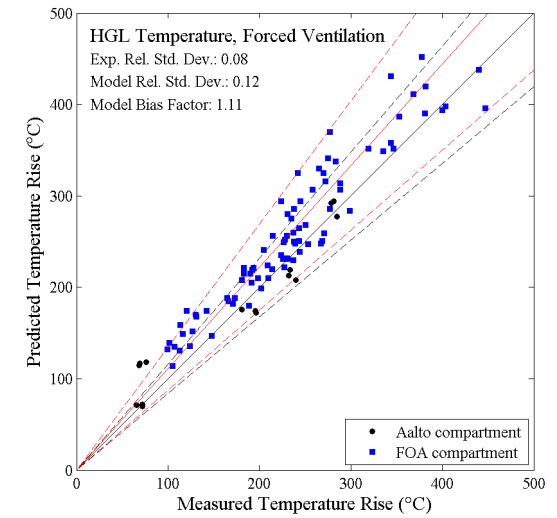
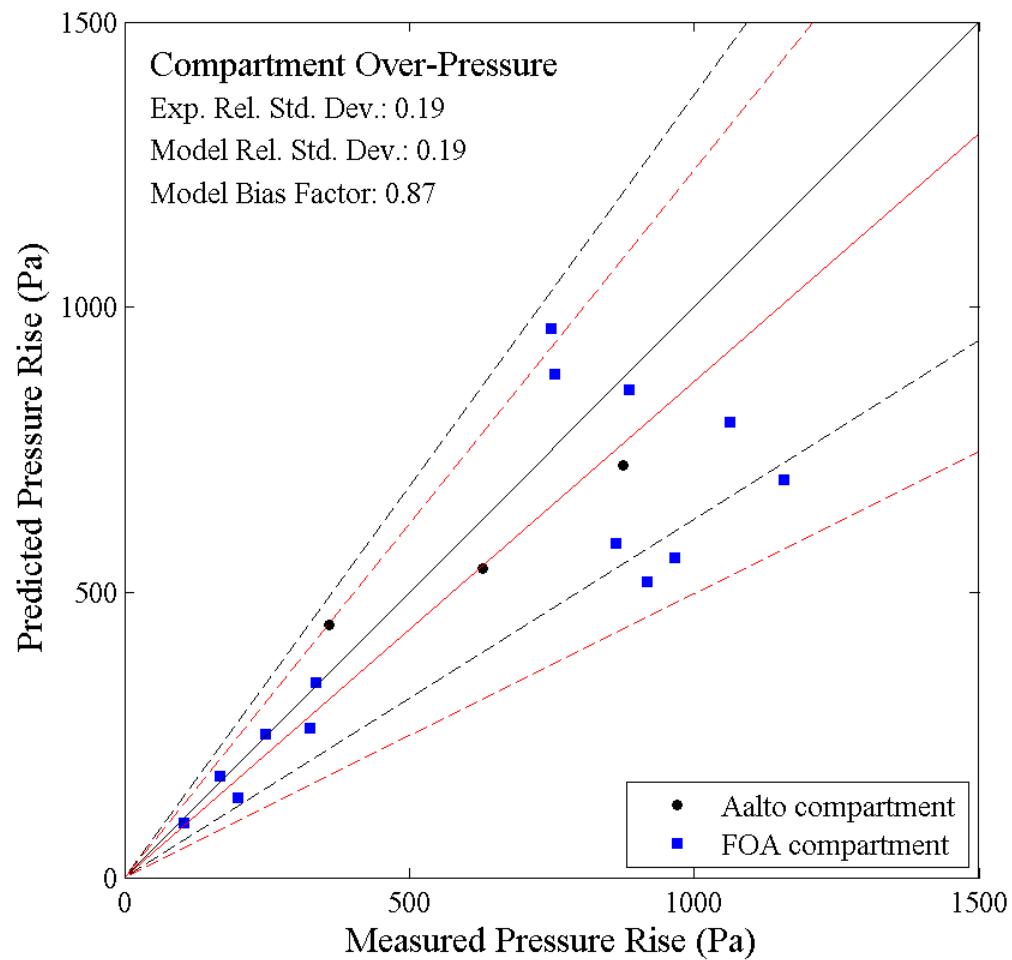
**FOA experiments by  
Hägglund et al. 1996 and 1998.**

**Heptane pool fires in  
concrete enclosure.**

**No HRR measurement.**

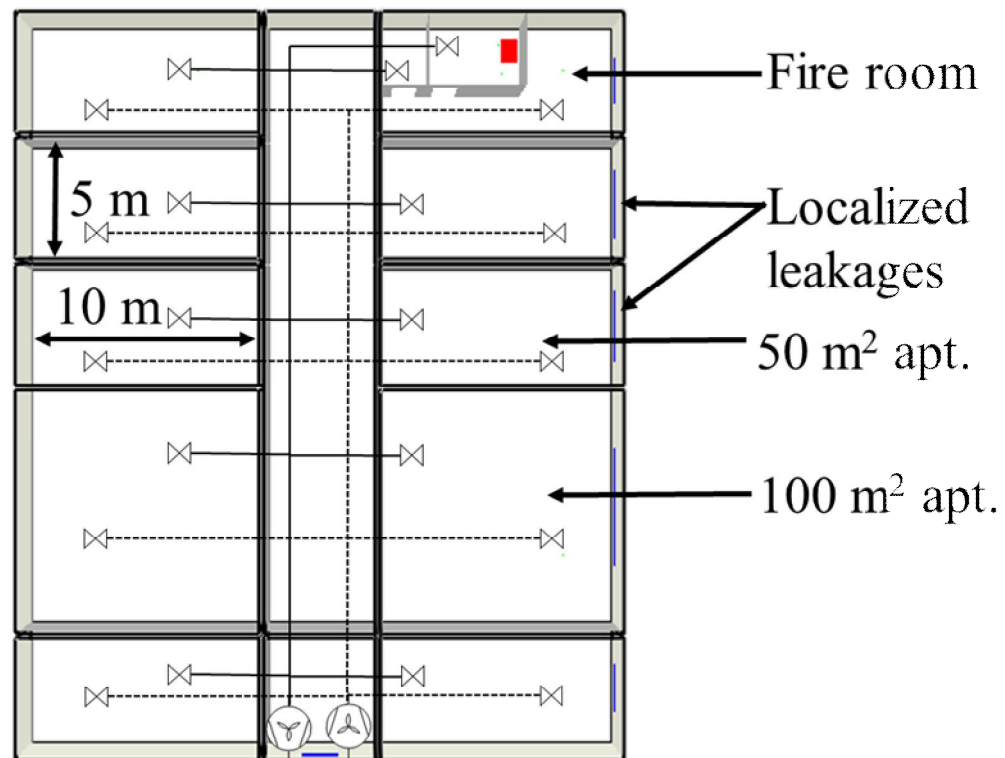


# Summary





# Apartment case study



## Three air-tightness levels

1. Traditional:  $q_{50} = 3.0 \text{ m}^3/\text{m}^2\text{h}$
2. Normal:  $q_{50} = 1.5 \text{ m}^3/\text{m}^2\text{h}$
3. Near-zero:  $q_{50} = 0.75 \text{ m}^3/\text{m}^2\text{h}$

## HRR: $t^2$ -fires medium – ultra-fast

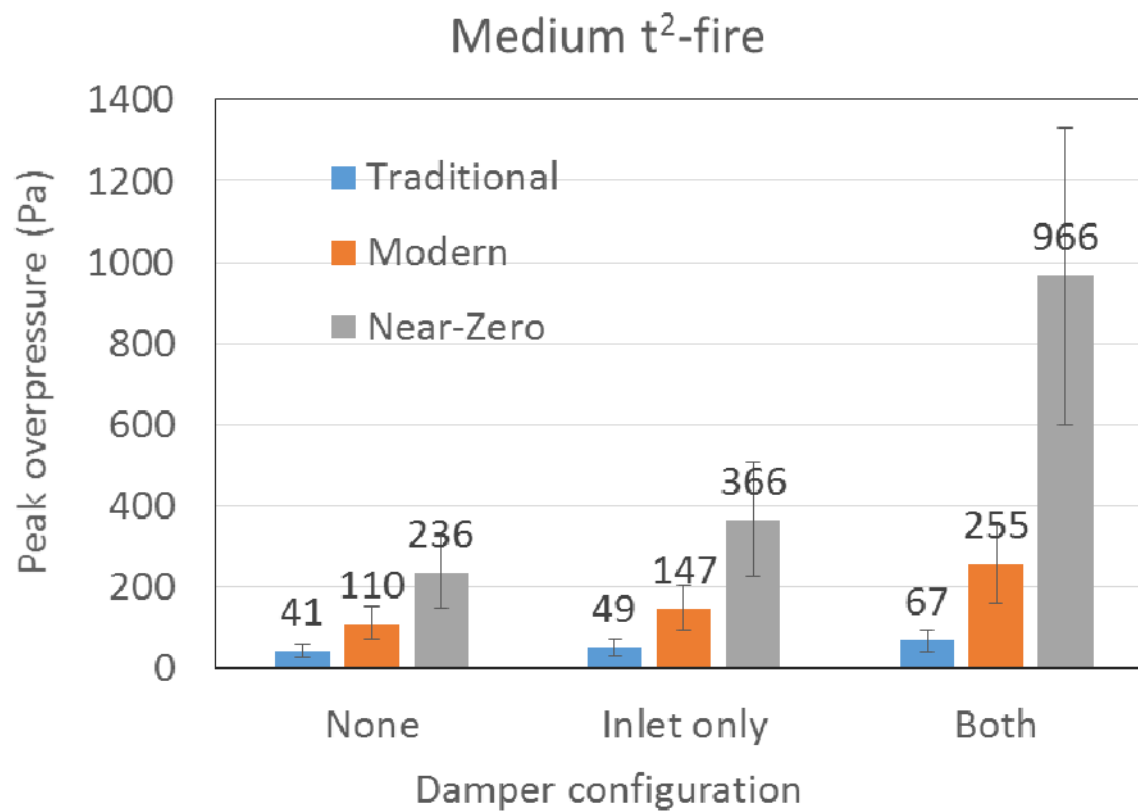
### Damper configurations:

1. No dampers
2. Only inlet branch closed
3. Both inlet and outlet closed

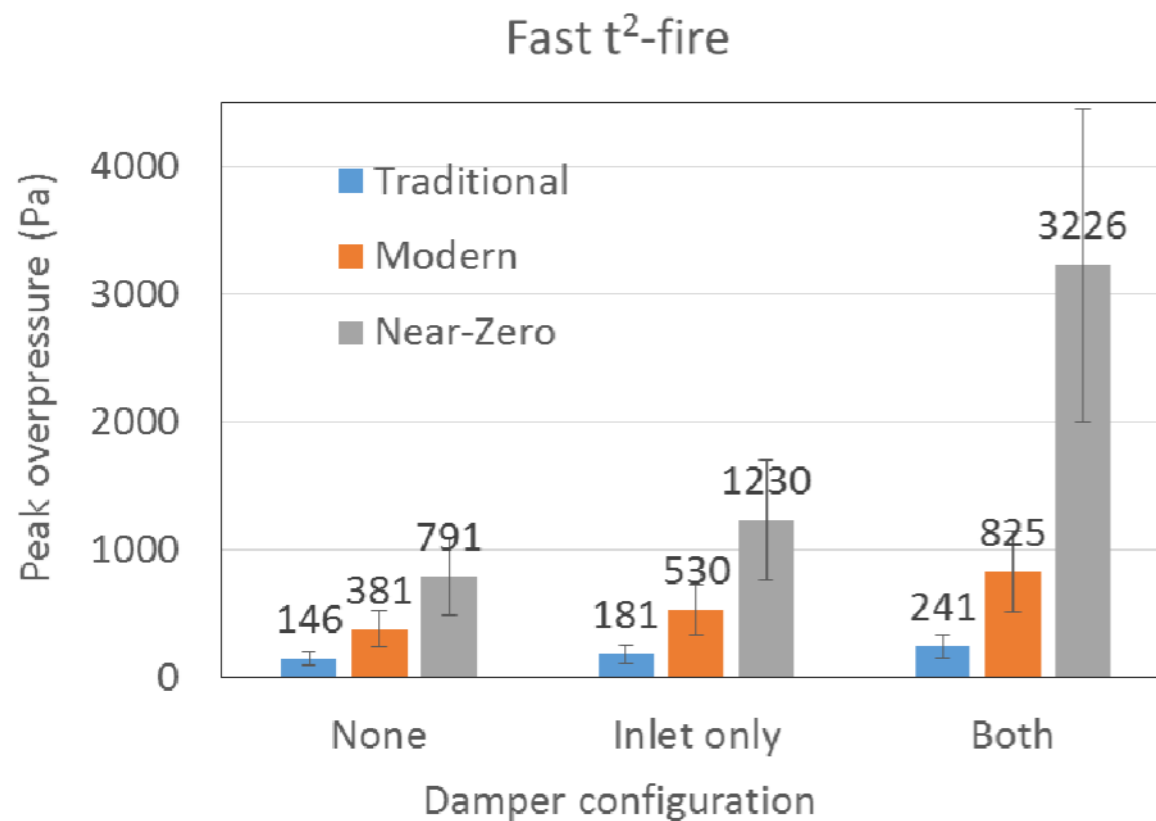
### Fan configurations

1. On
2. Off and open
3. Off and outside damper closed

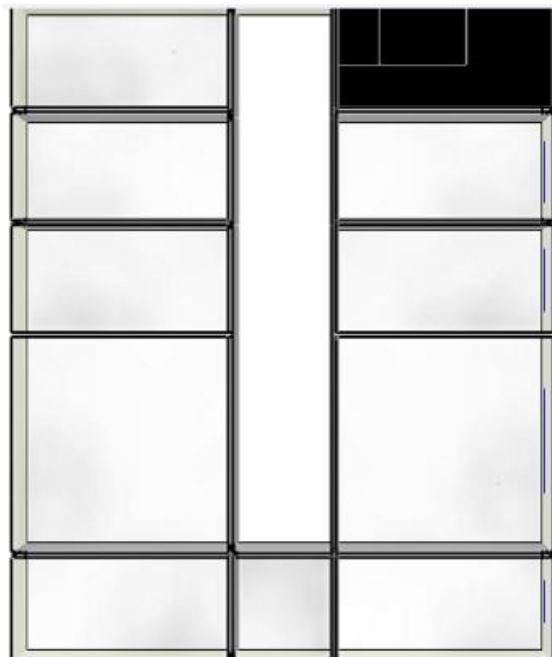
# Peak pressures with medium fire



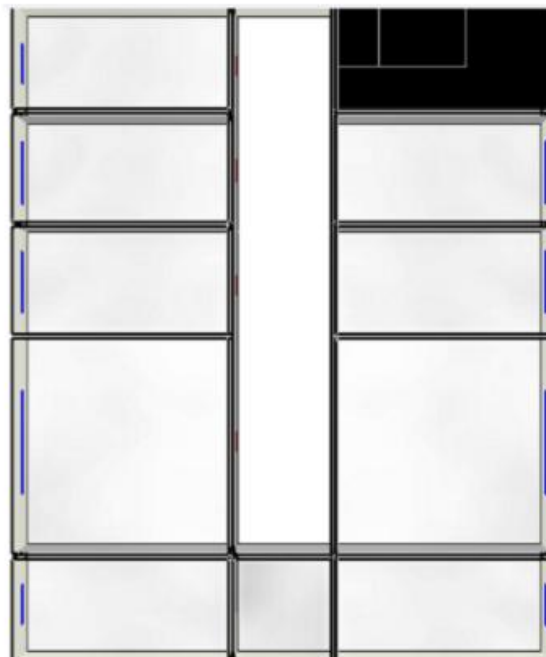
# Peak pressures with fast fires



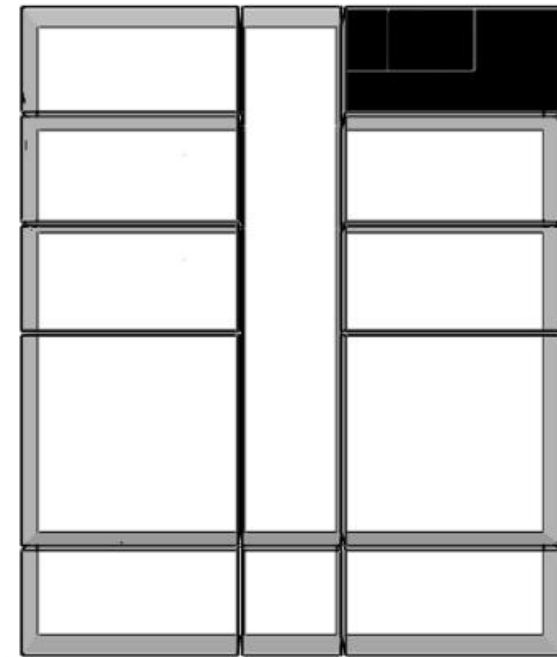
# Smoke spreading to neighbours



(a) Fan = Off, Dampers = Off

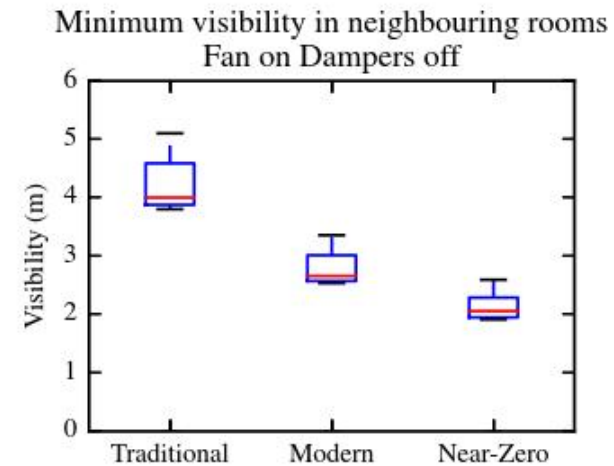
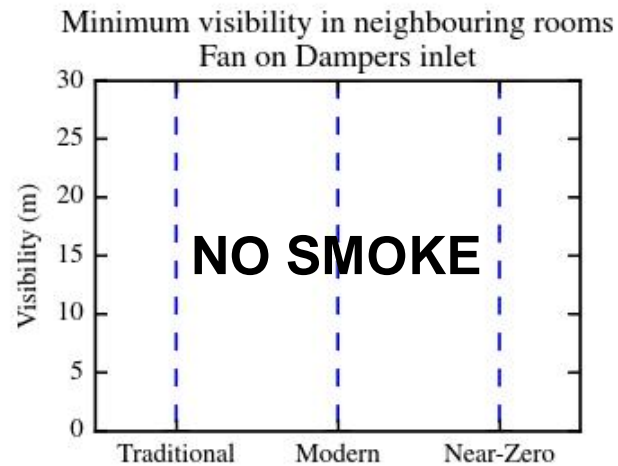
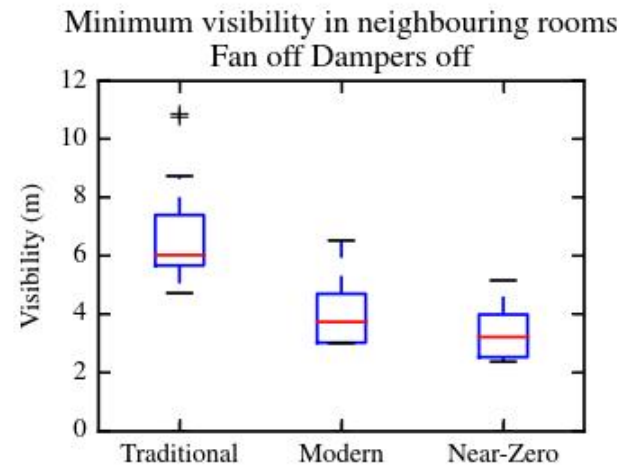
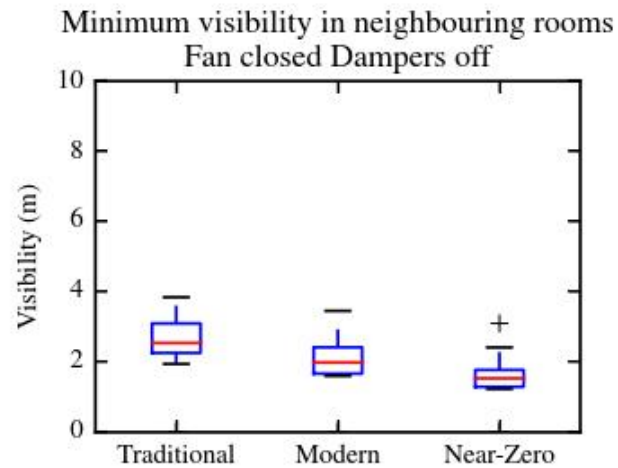


(b) Fan = On, Dampers = Off



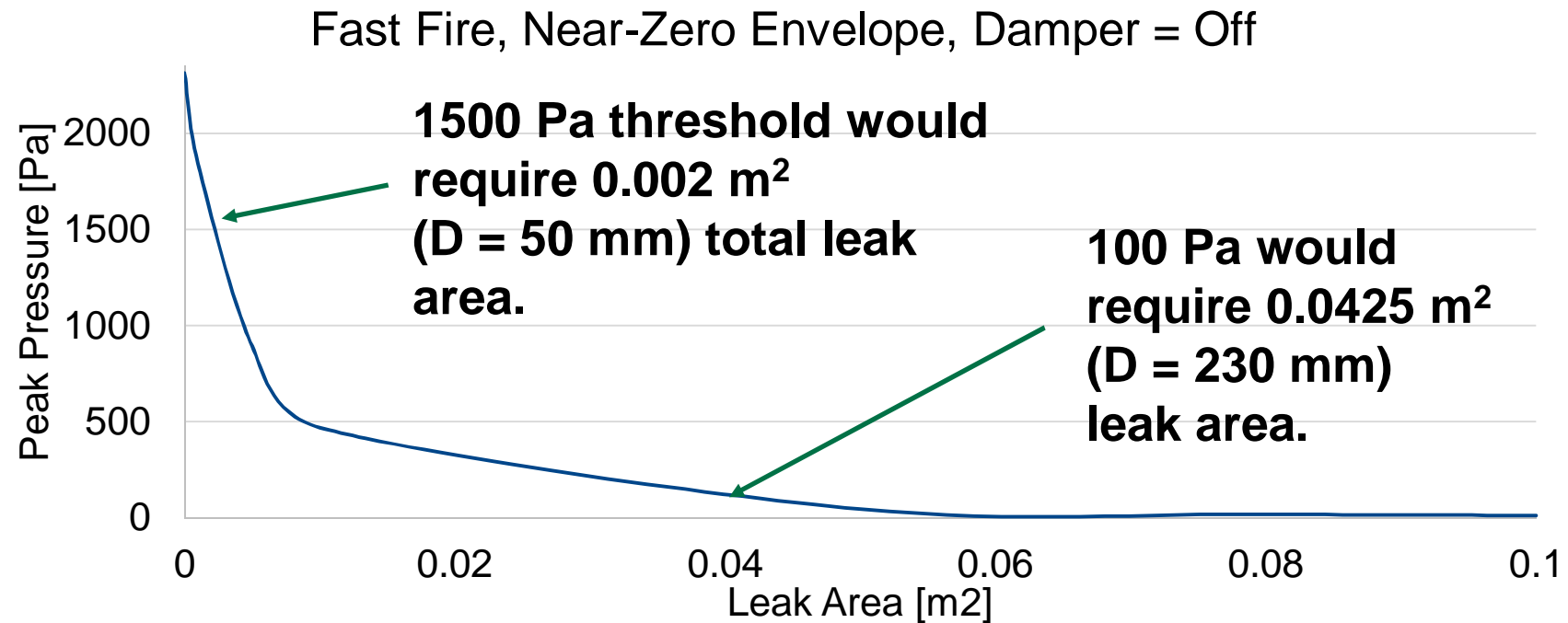
(c) Fan = On, Dampers = Inlet

# Smoke spreading: visibility

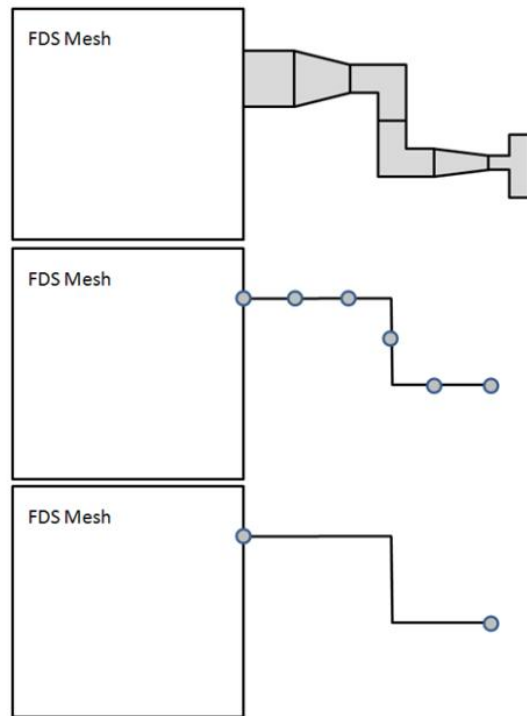




# Pressure management



# Issues with the HVAC system modelling



1. Real systems are too complex for "engineering" the model.
2. Fan units are much more than just a fan. Pressure losses of the fan unit can dominate.
3. Real systems are always tuned and balanced for normal mode of operation. We can do the same for the FDS model, but a better tool would help.