

Problems on PFR

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Problem 1. In an isothermal batch reactor the conversion of a liquid reactant A is 70% in 13 min. Find the space time and space velocity necessary to effect this conversion in a plug flow reactor and mixed flow reactor. Consider the first order kinetics.

Solution:

Rate equation : $-r_A = kC_A$

$$-\ln(1 - X_A) = kt$$

$$X_A = 0.70, \quad \text{for, } t = 13 \text{ min}$$

$$k = 0.0926 \text{ min}^{-1}$$

For mixed reactor,

$$\tau = \frac{C_{A0}X_A}{-r_A} = \frac{C_{A0}X_A}{kC_{A0}(1-X_A)} = \frac{0.70}{0.0926 \times (1-0.7)} = 25.2 \text{ min}$$

For constant density system and plug-flow reactor

$$t_{batch} = \tau_{plug}$$

- $\frac{V}{F_{A0}} = \int_0^{X_{Af}} \frac{dX_A}{-r_A} \text{ *or*, } \frac{\tau}{C_{A0}} = \int_0^{X_{Af}} \frac{dX_A}{-r_A}$
- $\tau = C_{A0} \int_0^{X_{Af}} \frac{dX_A}{k C_{A0} (1 - X_A)} = \int_0^{X_{Af}} \frac{dX_A}{k (1 - X_A)}$
- $\tau = \frac{1}{k} [-\ln(1 - X_A)]_0^{0.7} = \frac{1}{0.0926} [-\ln(1 - 0.7)] = 13 \text{ min } \textit{Answer}$

- Problem 2 Assuming a stoichiometry $A \rightarrow R$ for a first order gas phase reaction, the size of a plug flow reactor for 99% conversion of pure A calculated to be 32 liters. In fact, however, the stoichiometry of the reaction $A \rightarrow 3R$. For this corrected stoichiometry, find the required volume of the reactor.
- Solution: Rate equation : $-r_A = kC_A$, $\varepsilon_A=0$,
- $\frac{V}{F_{A0}} = \int_0^{X_{Af}} \frac{dX_A}{-r_A}$
- $\frac{V}{v_0} = C_{A0} \int_0^{X_{Af}} \frac{dX_A}{-r_A} = C_{A0} \int_0^{X_{Af}} \frac{dX_A}{kC_{A0}(1-X_A)}$
- $\frac{V}{v_0} = \frac{1}{k} \ln \left(\frac{1}{1-X_A} \right)$ or, $\frac{32}{v_0} = \frac{1}{k} \ln \left(\frac{1}{1-0.99} \right)$
- $\frac{k}{v_0} = 0.144$
- For the corrected stoichiometry $A \rightarrow 3R$
- $\varepsilon_A = \frac{3-1}{1} = 2$

$$\tau = C_{A0} \int_{X_{Ai}}^{X_{Af}} \frac{(1 + \varepsilon_A X_A) dX_A}{k C_{A0} (1 - X_A)}$$

$$V \left(\frac{k}{v_0} \right) = \int_0^{X_A} \frac{dX_A}{1 - X_A} + \varepsilon_A \int_0^{X_A} \frac{X_A dX_A}{1 - X_A}$$

$$V \frac{k}{v_0} = -(1 + \varepsilon_A) \ln(1 - X_A) - \varepsilon_A X_A$$

$$V \times 0.144 = -(1 + 2) \ln(1 - 0.99) - 2 \times 0.99$$

$$V = 82.2 \text{ lit}$$

So, the reactor volume with the corrected stoichiometry = 82.2 lit

- Problem 3: The liquid phase decomposition of A is studied in a mixed flow reactor. The results of steady state runs are tabulated below. Find the holding time required (i) in a plug flow reactor as well as (ii) in a mixed flow reactor to obtain 75% conversion of reactant in a feed with $C_{A0} = 0.8$ mol/lit.

Conc of A in feed stream	Conc of A in exit stream	Holding time (seconds)
2.0	0.65	300
2.0	0.92	240
2.0	1.00	250
1.0	0.56	110
1.0	0.37	360
0.48	0.42	24
0.48	0.28	200
0.48	0.20	560

- Solution: Liquid phase reaction, $\varepsilon_A = 0$

- $\tau = \frac{C_{A0}X_A}{-r_A} = \frac{C_{A0}-C_A}{-r_A}$

- $\frac{1}{-r_A} = \frac{\tau}{C_{A0}-C_A}$

- Required conversion = 0.75 so, required

$$C_{Af} = C_{A0} (1 - X_A) = 0.8(1 - 0.75) = 0.2 \text{ mol/lit}$$

Form the given tabulated data $\frac{1}{-r_A}$ is to be calculated for each data point.

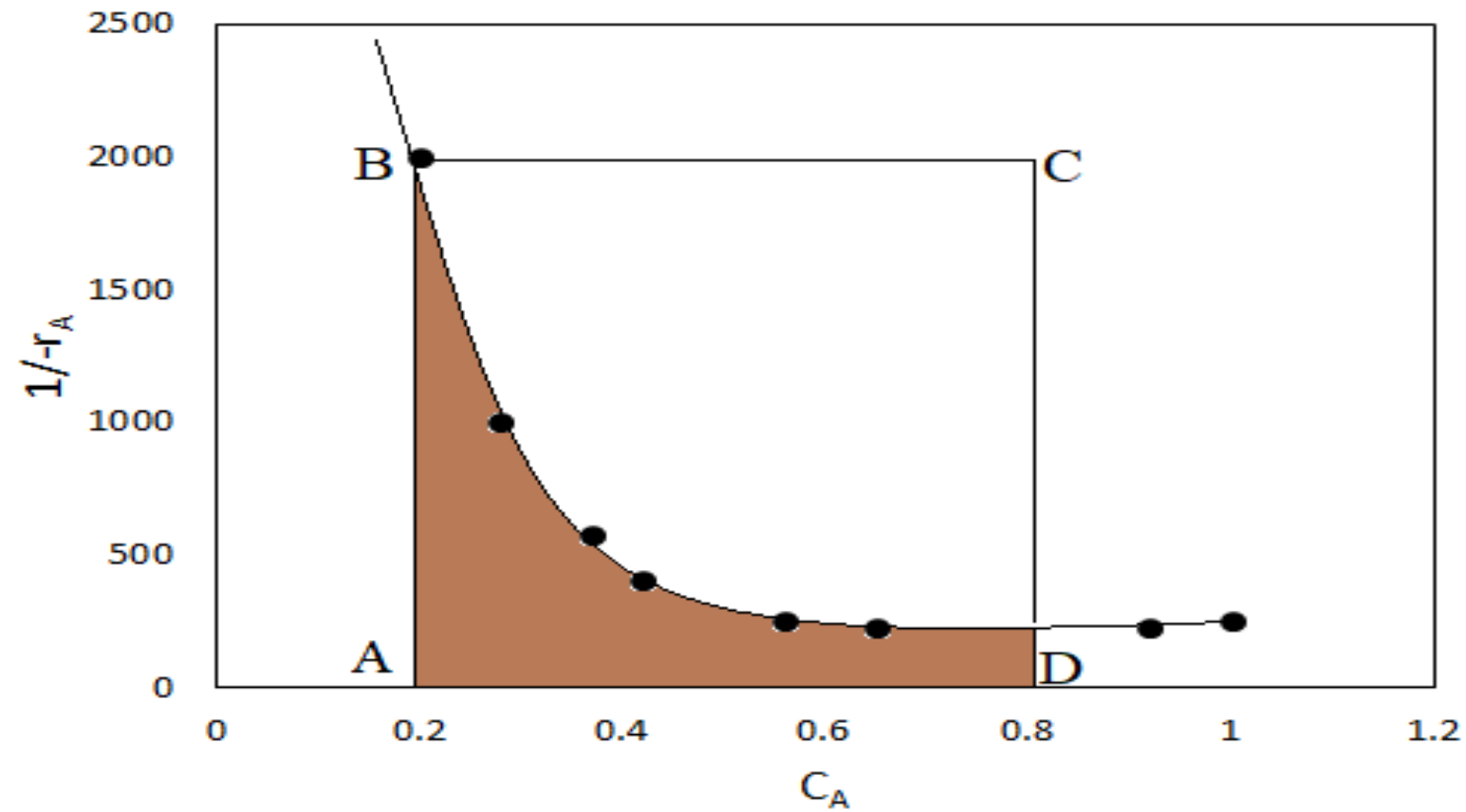
For example, for $C_{A0} = 2 \text{ mol/lit}$, $C_{af} = 0.65$, $\tau = 300 \text{ seconds}$

$$\frac{1}{-r_A} = \frac{300}{2 - 0.65} = 222.22 \frac{\text{mol}}{\text{lit. min}}$$

C_A	$1/(-r_A)$
0.65	222.22
0.92	222.22
1.0	250
0.56	250
0.37	571
0.42	400
0.28	1000
0.2	2000

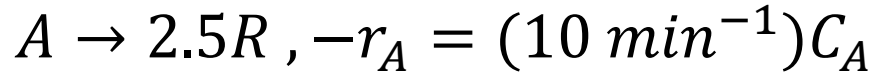
Plot $1/(-r_A)$ as a function of C_A .

τ for mixed flow reactor is the area of rectangle ABCD(area bounded by the rectangle starting from $C_{A0} = 0.8$ and ending at $C_{Af} = 0.2$. τ for PFR is the area under the curve and the x-axis between $C_{A0} = 0.8$ and $C_{Af} = 0.2$



For mixed flow reactor $\tau_m = \text{area of the rectangle ABCD} = 1200 \text{ s}$
 and for plug flow reactor = area under the curve (colored section) $\tau_p = 290 \text{ s}$

Problem 4: A gaseous feed of pure A with $C_{A0} = 2$ mol/lit and $F_{A0} = 100$ mol/min decomposes to give a variety of products in a plug flow reactor. The kinetics and stoichiometry of the reaction are given by



Find the conversion that can be obtained in a 22-liter reactor.

Solution: $A \rightarrow 2.5R$ is gaseous reaction so, $\varepsilon_A \neq 0$

$$\varepsilon_A = \frac{2.5 - 1}{1} = 1.5$$

$$\frac{V}{F_{A0}} = \int_{X_{Ai}}^{X_{Af}} \frac{(1 + \varepsilon_A X_A) dX_A}{k C_{A0} (1 - X_A)}$$

$$\frac{V}{F_{A0}} = \frac{1}{k C_{A0}} \left[\int_0^{X_A} \frac{dX_A}{1 - X_A} + \varepsilon_A \int_0^{X_A} \frac{X_A dX_A}{1 - X_A} \right]$$

$$\frac{V}{F_{A0}} = \frac{-(1 + \varepsilon_A) \ln(1 - X_A) - \varepsilon_A X_A}{k C_{A0}}$$

$$\frac{22}{100} = \frac{-(1 + 1.5) \ln(1 - X_A) - 1.5X_A}{10 \times 2}$$

$$4.4 = -2.5 \ln(1 - X_A) - 1.5X_A$$

By trial and error,

for $X_A = 0.7$, $RHS = 4.05$

$X_A = 0.750$, $RHS = 4.591$

$X_A = 0.740$, $RHS = 4.478$

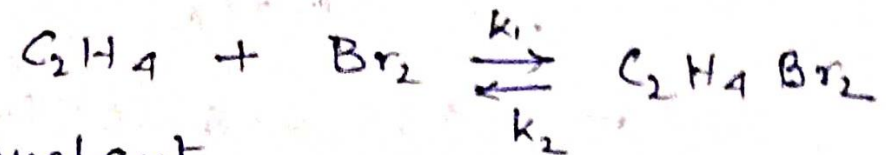
$X_A = 0.735$, $RHS = 4.4225$

$X_A = 0.734$, $RHS = 4.412$

$X_A = 0.733$, $RHS = 4.4005$

Therefore, $X_A = 0.733$, is the correct conversion, i.e 73.3 %

Problem -5: At 600 K the gas-phase reaction



has rate constant

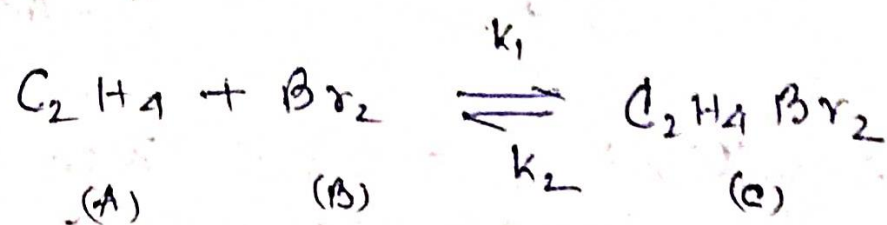
$$k_1 = 500 \text{ liter/mol}\cdot\text{hr} \quad k_2 = 0.032 \text{ hr}^{-1}$$

If a plug flow reactor is to be fed 600 m³/hr of gas containing 60% Br₂ and 30% C₂H₄ and 10% inert by volume at 600 K and 1.5 atm compute

(a) the maximum possible fractional conversion of C₂H₄ into C₂H₄Br₂

(b) the volume of reaction vessel required to obtain 60% of this maximum conversion.

Solution:



$$-r_{C_2H_4} = k_1 [C_2H_4] [Br_2] - k_2 [C_2H_4Br_2]$$

$$K_c = \frac{k_1}{k_2} = \frac{C_c}{C_A C_B} = \frac{(C_{c0} + C_{A0} x_{Ac}) (1 + \epsilon_A x_A)}{C_{A0} (1 - x_{Ac}) (C_{B0} - C_{A0} x_{Ac})}$$

$$P_{H_2} = 1.5 \text{ atm}$$

$$C_{A0} = \frac{1.5 \times 0.3}{0.082 \times 600} = 0.009135 \frac{\text{gmol}}{\text{lit}}$$

$$P_{A0} = 1.5 \times 0.3$$



$$\epsilon = \frac{0.7 - 1}{1} = -0.3$$

$$\begin{aligned} \text{or } \epsilon &= y_{A0} \delta \\ &= 0.3(-1) \\ &= -0.3 \end{aligned}$$

$$C_A = \frac{C_{A0} (1 - x_A)}{1 - 0.3 x_A}$$

$$C_B = \frac{C_{B0} - C_{A0} x_A}{1 - 0.3 x_A}$$

$$C_c = \frac{C_{A0} x_A}{1 - 0.3 x_A}$$

$$\epsilon = -$$

$$-r_A = 500 \times 0.00914 \frac{(1-x_A)}{1-0.3x_A} \times \frac{(0.0183 - 0.00914x_A)}{1-0.3x_A}$$

$$\text{As } C_{B0} = 0.0183$$

$$C_{A0} = 0.00914$$

$$= 0.032 \times \frac{0.00914 x_A}{1-0.3x_A}$$

$$= \frac{0.04177 \times (1-x_A)(2-x_A)}{(1-0.3x_A)^2} - \frac{292.48 \times 10^{-6} x_A}{1-0.3x_A}$$

$$\tau = \frac{V}{v_0} = C_{A0} \int_0^{x_A} \frac{dx_A}{-r_A}$$

$$= C_{A0} \int_0^{x_A} \frac{dx_A}{\frac{0.04177 (1-x_A)(2-x_A)}{(1-0.3x_A)^2} - \frac{292.48 \cdot 10^{-6} x_A}{(1-0.3x_A)}}$$

At equilibrium $x_A = x_{Ae}$

$$0.04177 \frac{(1-x_{Ae})(2-x_{Ae})}{(1-0.3x_{Ae})^2} = 292.48 \times 10^{-6} \frac{x_{Ae}}{(1-0.3x_{Ae})}$$

$$0.04177 \times (1-x_{Ae})(2-x_{Ae}) = 292.48 \times 10^{-6} \times x_{Ae} (1-0.3x_{Ae})$$

or $x_{Ae} \approx 1.0 \quad \therefore x_A \approx 0.6$

x_A	$f(x)$
0.1	0.0758
0.2	0.068
0.3	0.06
0.4	0.0516
0.5	0.043
0.6	0.0345

on Integration. $\tau = 0.00914 \times 10.7$
 $= 0.0978$

Volume of reaction $= 600 \times 0.0978$
 $= 58.678 \text{ m}^3$ *Ans*