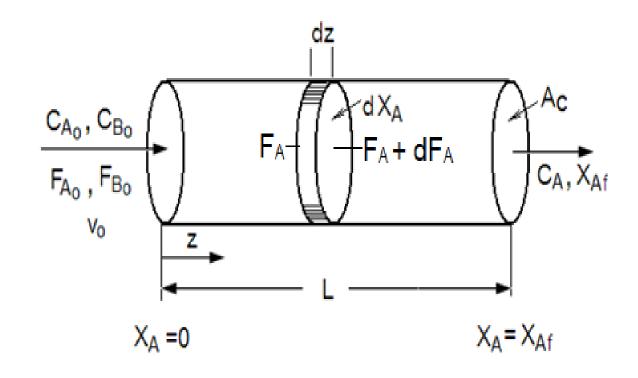
# Plug Flow Reactor

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## Plug Flow Reactor



Mole Balance:  $F_A = (F_A + dF_A) + (-r_A)dV$ 

$$-dF_A = (-r_A)dV$$
 or,  $-\frac{dF_A}{dV} = -r_A$ 

### Design of Plug Flow Reactor(PFR)

*Volume basis(Homogeneous reaction):* 

As, 
$$F_A = F_{A0}(1 - X_A)$$
 then  $F_{A0} \frac{dX_A}{dV} = -r_A$ 

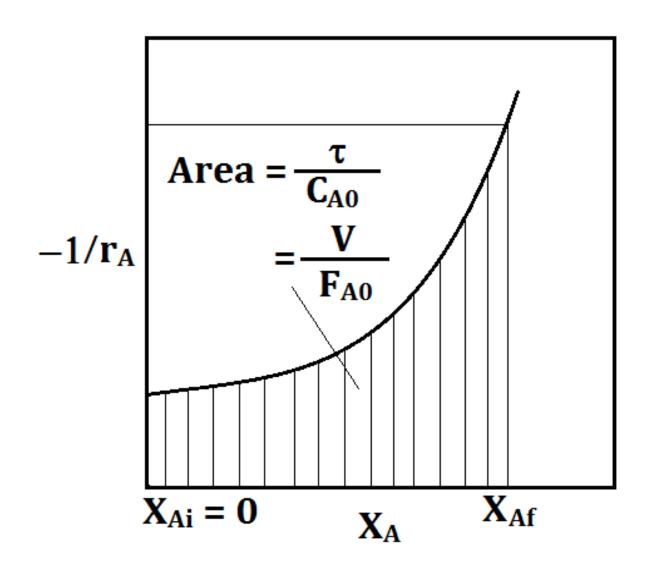
$$\frac{V}{F_{A0}} = \int_0^{X_{Af}} \frac{dX_A}{-r_A} or, \qquad \frac{\tau}{C_{A0}} = \int_0^{X_{Af}} \frac{dX_A}{-r_A}$$

Catalyst weight basis(Heteroneous reaction):

$$-\frac{dF_A}{dW}=-r_A'$$

$$\frac{W}{F_{A0}} = \int_0^{X_{Af}} \frac{dX_A}{-r_A'}$$

# Graphical Analysis for PFR design



# Plug Flow Reactor for Variable Density with First-Order Kinetics

$$Rate\ equation: -r_A = kC_A$$

$$\tau = C_{A0} \int_{X_{Ai}}^{X_{Af}} \frac{(1 + \varepsilon_A X_A) dX_A}{k C_{A0} (1 - X_A)}$$

$$k\tau = \int_0^{X_A} \frac{dX_A}{1 - X_A} + \varepsilon_A \int_0^{X_A} \frac{X_A dX_A}{1 - X_A}$$

$$k\tau = -(1 + \varepsilon_A) \ln(1 - X_A) - \varepsilon_A X_A = f(X_A)$$

For constant volume

$$\varepsilon_A = 0$$
:  $k\tau = -\ln(1 - X_A) = f(X_A)$ 

# Plug Flow Reactor for Variable Density with Second-Order Kinetics

Rate equation: 
$$-r_A = kC_A^2$$

Mole Balance:  $\tau = C_{A0} \int_0^{X_{Af}} \frac{dX_A}{-r_A}$ 
 $\tau = C_{A0} \int_0^{X_{Af}} \frac{X_A (1 + \varepsilon_A X_A)^2 dX_A}{kC_{A0}^2 (1 - X_A)^2}$ 
 $C_{A0}k\tau = 2\varepsilon_A (1 + \varepsilon_A) \ln (1 - X_A) \varepsilon_A^2 X_A + (1 + \varepsilon_A)^2 \frac{X_A}{1 - X_A}$ 
 $\tau = \frac{A_C L}{v_0}$ , where  $A_C$  is the cross sectional area

 $C_{A0}k au$  is called as Damköhler number(Flow reactor)

 $C_{A0}^{n-1}k\tau$  is the Damköhler number for nth order reaction(Flow Reactor)

 $X_A = kC_{A0}^{n-1}\tau(1-X_A)^n$  is the mole balance in CSTR

#### Damköhler number for batch reactor

- ullet For batch reactor  ${}'oldsymbol{ au}'$  will be replaced by 't'
- For batch reactor first-order reaction  $k\tau$  = kt
- For batch reactor n-th order reaction  $C_{A0}^{n-1}kt$
- All are dimensionless groups