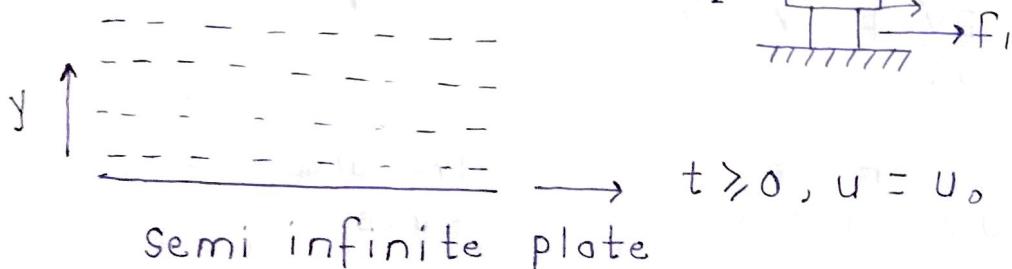


04/01/19

Manish Kaushal

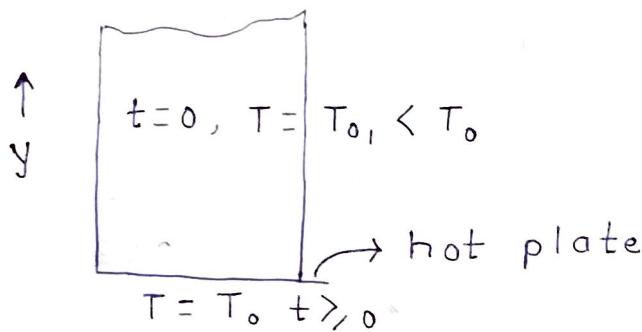
Unsteady / Transient transport of M^2 / Heat / Mass -

Momentum

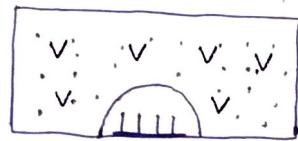


Here, momentum is taking some time to get transported from bottom layer to other layers above — hence “unsteady” state.

Heat



Mass



$\rightarrow A$ (sensor)
 $\rightarrow B$ (Blood)

A is getting consumed / reacting with B. First, V decreases at its surface, then a conc? gradient occurs in vertical direction, then it develops

- laterally. Therefore, unsteady state.
- Thermodynamics tells about equilibrium, steady state.
 - Heat Transfer deals with kinetics.

Cauchy Momentum Balance :

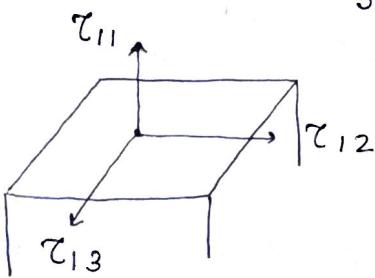
$$\rho \left(\frac{\partial \vec{v}}{\partial t} + \vec{v} \cdot \nabla \vec{v} \right) = - \nabla p + \nabla \cdot \vec{\tau} + \rho \vec{g}$$

$\underbrace{}$
A
 $\underbrace{}$
 $\underbrace{}$
Pressure forces
 $\underbrace{}$
Stress
 $\underbrace{}$
Body force

* N-S is applicable for Newtonian, incompressible fluids.

Tensor - has no physical meaning is just a matrix of 9 component

$$\begin{bmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \end{bmatrix}_{1 \times 3} \begin{bmatrix} \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & \tau_{33} \end{bmatrix}_{3 \times 3} = 1 \times 3$$



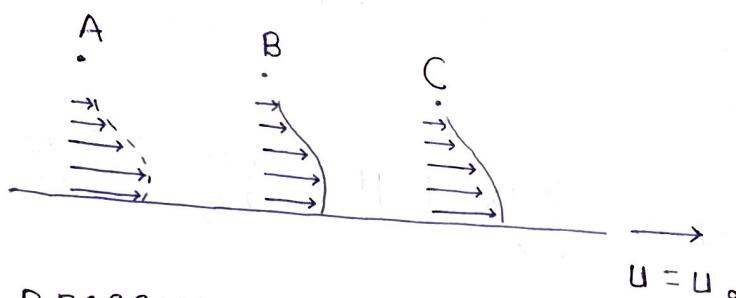
Operators, tensors are introduced to simplify mathematics.

$$\nabla = \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z}$$

In A, we have one having 3 component.
 $\nabla v \rightarrow$ tensor (3×3 combinations) = g
 " " " g "

- A combines all components in 1 eq?
- Momentum -

A, B and C are hydrodynamically equal. The conditions / environment surrounding them are same. So, why will the velocities be different?



No pressure gradient. Flow is due to movement of bottom plate

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = - \frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \Delta^2 u$$

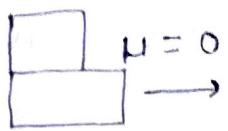
$$\rightarrow \frac{\partial u}{\partial x} = 0, v = 0, w = 0$$

$$\therefore \frac{\partial u}{\partial t} = \left(\frac{\mu}{\rho} \right) \frac{\partial^2 u}{\partial y^2}$$

ν : momentum diffusivity

More momentum gets transferred with greater (μ) .

No slip doesn't tell about static / dynamic but deals with relative velocity.



Slipping occurs

There will be no momentum transport if $\mu = 0$.

$$\text{I.C. : } u(y, t=0) = 0$$

$$\text{B.C. : } u(y=0, \forall t) = u_0$$

$$u(y \rightarrow \infty, \forall t) = 0$$

Scaling Analysis :

To see the relative importance of terms.

$$\rho \left(\frac{\partial \vec{U}}{\partial t} + \vec{U} \cdot \nabla \vec{V} \right) = - \underbrace{\nabla p + \nabla \cdot \vec{\tau}}_{\text{Viscous Stress}} + \rho \vec{g}$$

$$\tau_{ij} = -p \delta_{ij} + \lambda \frac{\partial u_k}{\partial x_k} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

$$\delta_{ij} = \begin{cases} 0 & i \neq j ; \text{ Identity} \\ 1 & i = j ; \text{ Matrix} \end{cases}$$

$$\frac{\partial u_k}{\partial x_k} = \frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} + \frac{\partial u_3}{\partial x_3}$$

p here is the thermodynamic pressure.

$$p_{\text{mech}} = \frac{(\tau_{11} + \tau_{22} + \tau_{33})}{3}$$

For NV eqⁿ to work,

$$p_{\text{ther}} = p_{\text{mech}}$$

Stokesian Fluid :-

If the relaxation time, i.e., time required by p_{ther} to become equal to p_{mech}

is very small, fluid is said to be Stokesian.

$$-P_{\text{mech}} = -P_{\text{therm}} + \left(\lambda + \frac{2}{3} \mu \right) \left(\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} + \frac{\partial u_3}{\partial x_3} \right)$$

For NS eqⁿ to work,

$$P_{\text{mech}} = P_{\text{therm}}$$

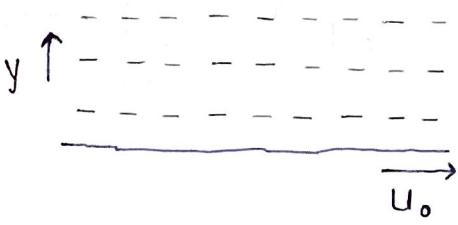
if $\left(\lambda + \frac{2}{3} \mu \right) = 0$, fluids follow Stokes hypothesis.

For incompressible fluid,

$$\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} + \frac{\partial u_3}{\partial x_3} = 0$$

Hence, NS eqⁿ will be applicable.

→ No hydrodynamic B.L. Throughout
viscous forces important.



$$\frac{\partial u}{\partial t} = \nu \frac{\partial^2 u}{\partial y^2}$$

$$\text{I.C. : } t = 0 \quad u = 0 \quad \forall y$$

$$\text{B.C. : } y = 0 \quad u = u_\infty \quad \forall t$$

$$y \rightarrow \infty \quad u = 0 \quad \forall t$$

Scaling Analysis :-

$$\rho \left(\frac{\partial \bar{u}}{\partial t} + \bar{u} \cdot \nabla \bar{u} \right) = -\nabla \bar{p} + \mu \nabla^2 \bar{v} + \rho \vec{g}$$

$$u_0 = 10^{-3} \text{ m/s}$$

$$y = L = 10^{-4} \text{ m}$$

$$\rho = 10^3 \text{ kg/m}^3$$

$$\mu = 10^{-3} \text{ Pa.s}$$

Order of magnitude analysis:-

$$\sim \frac{U_0}{t_{ref}} \sim \frac{U_0^2}{L} \sim \frac{\rho U_0^2}{L} + \sim \frac{\mu U_0}{L^2}$$

If $\frac{\partial \bar{U}}{\partial t}$ and $\bar{U} \cdot \nabla \bar{U}$ has to survive,
order of the two terms should be
equal.

$$\frac{U_0}{t_{ref}} = \frac{U_0^2}{L} \Rightarrow t_{ref} = \frac{L}{U_0}$$

$$U^* = \frac{U}{U_0}$$

$$\rho \left(\frac{U_0^2}{L} \frac{\partial \bar{U}^*}{\partial t^*} + \frac{U_0^2}{L} \bar{U}^* \cdot \nabla \bar{U}^* \right) = - \frac{\rho U_0^2}{L} \nabla p^* + \mu \frac{U_0}{L^2} \nabla^2 \bar{U}^*$$

$$\Rightarrow \left(\frac{\partial \bar{U}^*}{\partial t^*} + \bar{U}^* \cdot \nabla \bar{U}^* \right) = - \nabla p^* + \frac{1}{Re} \nabla^2 \bar{U}^*$$

$$\text{where, } Re = \frac{\rho U_0 L}{\mu}$$

$$Re = \frac{\rho U_0^2}{\mu \frac{U_0}{L}} = \frac{\text{Inertial forces}}{\text{Viscous forces}}$$

For higher velocity, inertial forces dominate viscous forces, second term on R.H.S is zero, therefore potential flow regime. For lower velocity, L.H.S. = 0, therefore creeping flow regime.

For potential flow, bernoulli's eqⁿ
applicable.

$$Re = \frac{10^3 \times 10^{-3} \times 10^{-4}}{10^{-3}} = 0.1$$

$$\frac{\partial u}{\partial t} = \nu \frac{\partial^2 u}{\partial y^2}$$

$$\sim \frac{u_0}{t_{ref}} \sim \nu \frac{u_0}{\delta^2}; \quad \delta \text{ varies with time}$$

$$\delta = \delta(t)$$

$$t_{ref} = t \quad \{ t : \text{running time} \}$$

$$\frac{u_0}{t} = \nu \frac{u_0}{\delta^2} \Rightarrow \delta \sim \sqrt{2\nu t}$$

δ is momentum diffusion length scale.

Hydrodynamic B.L. : viscous forces important

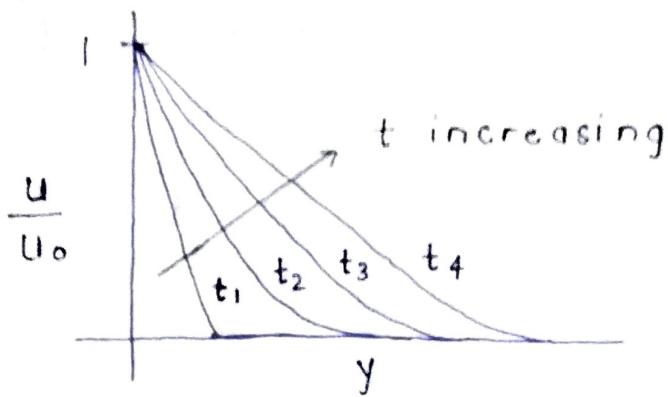
$$\delta = \sqrt{2\nu t} = \sqrt{4\nu t}$$

Error function :-

$$\operatorname{erf}(x) = \frac{2}{\sqrt{\pi}} \int_0^x e^{-z^2} dz$$

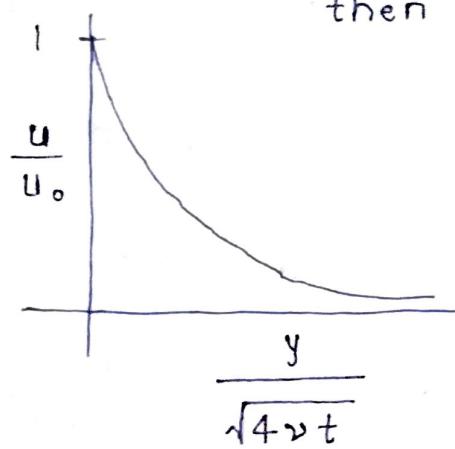
Gamma function :-

$$\Gamma(z) = \int_0^\infty x^{z-1} e^{-x} dx$$



Self-Similarity :

if the distance from the plate is non-dimensionalised, we get a single curve
then self-similar



$$\frac{\partial u}{\partial t} = \nu \frac{\partial^2 u}{\partial y^2}$$

$$\bar{u} = \frac{u}{u_0} \quad \eta = \frac{y}{\delta}$$

$$\frac{\partial \bar{u}}{\partial t} = \nu \frac{\partial^2 \bar{u}}{\partial \eta^2}$$

B.C. :
 $y = 0 \quad \bar{u} = 1$
 $y = \infty \quad \bar{u} = 0$

$$I.C. : \quad t = 0 \quad \bar{u} = 0 \quad \forall y$$

$$\eta = \frac{y}{\sqrt{4\nu t}}$$

Similarity transformation variable

$$\bar{u} = u/u_0 = f(\eta)$$

$$\frac{\partial \bar{u}}{\partial t} = \frac{\partial \bar{u}}{\partial \eta} \cdot \frac{\partial \eta}{\partial t} = -\frac{1}{2} \left(\frac{\partial f}{\partial \eta} \right) \frac{y}{\sqrt{4\alpha t} \cdot t}$$

$$= -\frac{\eta}{2t} \frac{\partial f}{\partial \eta}$$

$$\frac{\partial \bar{u}}{\partial y} = \frac{\partial \bar{u}}{\partial \eta} \cdot \frac{\partial \eta}{\partial y} = \frac{\partial f}{\partial \eta} \cdot \frac{1}{\sqrt{4\alpha t}}$$

$$\frac{\partial^2 \bar{u}}{\partial y^2} = \frac{\partial}{\partial y} \left(\frac{\partial \bar{u}}{\partial \eta} \right) = \frac{\partial}{\partial \eta} \left(\frac{\partial f}{\partial \eta} \frac{1}{\sqrt{4\alpha t}} \right) \frac{\partial \eta}{\partial y}$$

$$= \frac{1}{\sqrt{4\alpha t}} \cdot \left(\frac{\partial^2 f}{\partial \eta^2} \right) \frac{1}{\sqrt{4\alpha t}} = \frac{1}{4\alpha t} \frac{\partial^2 f}{\partial \eta^2}$$

$$-\frac{\eta}{2t} \frac{\partial f}{\partial \eta} = \frac{\partial^2 f}{\partial \eta^2}$$

$$\frac{\partial^2 f}{\partial \eta^2} + 2\eta \frac{\partial f}{\partial \eta} = 0$$

$$\eta = 0 \rightarrow f = 1$$

$$(y = 0, t \rightarrow \infty)$$

$$\eta = \infty \rightarrow f = 0$$

$$\text{Let } \frac{\partial f}{\partial \eta} = \Psi$$

$$\Rightarrow \frac{\partial \Psi}{\partial \eta} + 2\eta \Psi = 0$$

$$\frac{\partial \Psi}{\Psi} = -2\eta d\eta$$

$$\ln \Psi = -\eta^2 + C$$

$$\Rightarrow \Psi = C e^{-\eta^2}$$

$$\frac{\partial f}{\partial \eta} = c e^{-\eta^2}$$

$$f_{\eta=0} - f_{\eta=\infty} = \int_0^\infty c e^{-\eta^2} d\eta$$

$$f = 1 + c \int_0^\infty e^{-\eta^2} d\eta$$

$$\eta \rightarrow \infty \quad f = 0$$

$$0 = 1 + c \int_0^\infty e^{-\eta^2} d\eta$$

$$\eta^2 = z \Rightarrow \eta = \sqrt{z} \Rightarrow d\eta = \frac{1}{2\sqrt{z}} dz$$

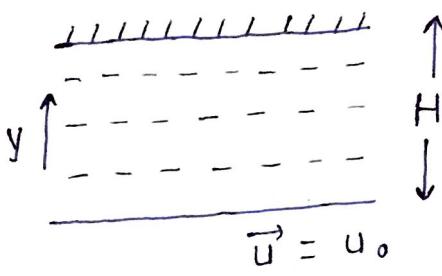
$$0 = 1 + \frac{c}{2} \int_0^\infty e^{-z} z^{\frac{1}{2}-1} dz$$

$$0 = 1 + \frac{c}{2} \Gamma(1/2) = 1 + \frac{c}{2} \sqrt{\pi}$$

$$\Rightarrow c = -\frac{2}{\sqrt{\pi}}$$

$$f = 1 - \frac{2}{\sqrt{\pi}} \int_0^\infty e^{-\eta^2} d\eta = 1 - \text{erf}(\eta)$$

$$\frac{u}{u_0} = 1 - \text{erf} \left(\frac{y}{\sqrt{4vt}} \right).$$



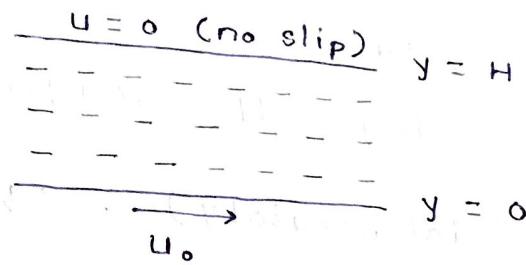
$$u = f(y, t)$$

$$y = 0, u = u_0 \quad \} \text{ B.C.}$$

$$y = H, u = 0$$

$$t = 0, u = 0 \quad \forall y \quad \} \text{ I.C.}$$

6-02-2019



Unsteady
state
confined
flows

$$\frac{\partial u}{\partial t} = \nu \frac{\partial^2 u}{\partial y^2} \quad u = u(y)$$

$$\frac{\partial \bar{u}}{\partial t} \frac{u_0}{t_c} = \nu \frac{u_0}{H^2} \frac{\partial^2 \bar{u}}{\partial \bar{y}^2}$$

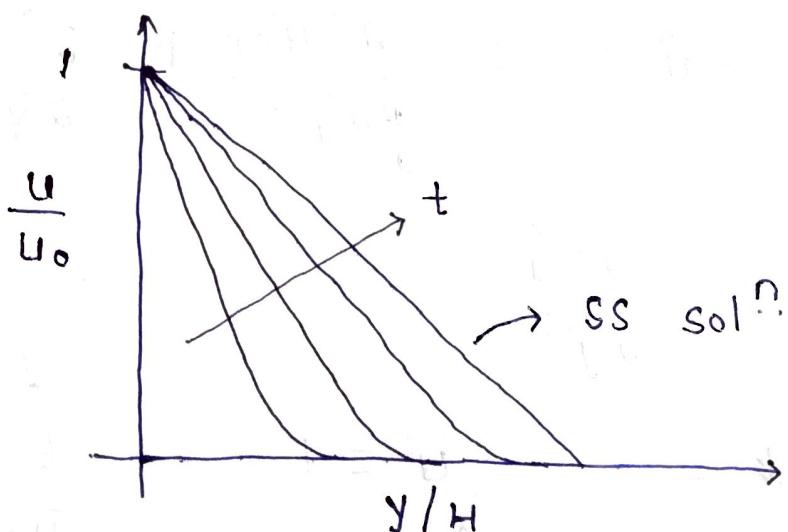
$$\frac{\partial \bar{u}}{\partial t} = \frac{t_c \nu}{H^2} \left(\frac{\partial^2 \bar{u}}{\partial \bar{y}^2} \right) \Rightarrow \text{All terms have order of mag. equal to 1.}$$

$$\frac{t_c \nu}{H^2} \sim O(1) \Rightarrow t_c = \frac{H^2}{\nu}$$

where t_c is M^2 diffusion time scale

$t \ll t_c$, it reduces to infinite domain problem and error function solⁿ will work.

$t \gg t_c$, steady state $u = ay + b$



This profile is not self-similar like the one in previous problem.

$$t_c = \frac{(100 \times 10^{-6})^2}{10^{-3} / 10^3} = 0.01 \text{ s}$$

(for water where $H = 100 \mu\text{m}$)

$$\frac{t_c v}{H^2} = 1 \quad (\text{deliberately}), \text{ eqn becomes}$$

$$\frac{\partial \bar{u}}{\partial t} = \frac{\partial^2 \bar{u}}{\partial \bar{y}^2}$$

$$\text{B.C. : } \bar{y} = 0 \quad \bar{u} = 1$$

$$\bar{y} = 1 \quad \bar{u} = 0$$

$$\text{I.C. : } \bar{t} = 0 \quad \bar{u} = 0$$

$$\bar{u} = 0$$

$$\bar{u} = \bar{u}_{ss} + \hat{u} \rightarrow \text{unsteady part}$$

$\hookrightarrow \text{ss soln.}$

ss solution -

$$0 = \frac{\partial^2 \bar{u}_{ss}}{\partial \bar{y}^2}$$

$$\Rightarrow \bar{u}_{ss} = a\bar{y} + b \quad \bar{y} = 0 \quad \bar{u}_{ss} = 1$$

$$\bar{y} = 1 \quad \bar{u}_{ss} = 0$$

$$\Rightarrow \bar{u}_{ss} = 1 - \bar{y}$$

Unsteady part -

$$\frac{\partial}{\partial \bar{t}} (\bar{u}_{ss} + \hat{u}) = \cancel{\frac{\partial^2 \bar{u}_{ss}}{\partial \bar{y}^2}} + \frac{\partial^2 \hat{u}}{\partial \bar{y}^2}$$

$$\Rightarrow \frac{\partial \hat{u}}{\partial \bar{t}} = \frac{\partial^2 \hat{u}}{\partial \bar{y}^2}$$

I.C. :-

$$\text{B.C. } \bar{y} = 0 \quad \bar{u} = 1$$

$$\bar{E} = 0 \quad \bar{u} = 0$$

$$\bar{u}_{ss} + \hat{u} = 1$$

$$\bar{u}_{ss} + \hat{u} = 0$$

$$\Rightarrow \hat{u} = 0$$

$$\hat{u} = -\bar{u}_{ss}$$

$$\hat{u} = \bar{y} - 1$$

$$\bar{y} = 1 \quad \hat{u} = 0$$

Homogeneous B.C. So separation of variables work.

separation of variables -

$$\hat{u} = f(\bar{y}) g(\bar{t}) = fg$$

$$fg' = gf''$$

$$\frac{g'}{g} = \frac{f''}{f} = a$$

$$\frac{g'}{g} = a \Rightarrow \frac{dg}{g} = a d\bar{t} \Rightarrow g = c e^{a \bar{t}}$$

a should be negative. Let $a = -\lambda^2$

$$g = c e^{-\lambda^2 \bar{t}}$$

$$\frac{f''}{f} = -\lambda^2 \Rightarrow f'' + \lambda^2 f = 0$$

$$f = a \cos \lambda \bar{y} + b \sin \lambda \bar{y}$$

$$\Rightarrow \forall \bar{t} \quad \hat{u} = 0 \Rightarrow fg = 0 \Rightarrow f = 0 \\ (\bar{y} = 0)$$

$$\text{when } \bar{y} = 1, \hat{u} = 0 \Rightarrow fg = 0 \Rightarrow f = 0$$

From 1st condition $a = 0$

From 2nd condition

$$f = b \sin \lambda \bar{y} \Rightarrow 0 = b \sin \lambda$$

$$b \neq 0, \therefore \sin \lambda = 0 \Rightarrow \lambda_n = n\pi$$

$$\Rightarrow \hat{u} = \sum b_n \sin(\lambda_n \bar{y}) e^{-\lambda_n^2 t}$$

$$\bar{u} = (1 - \bar{y}) + \sum b_n (\sin(\lambda_n \bar{y})) e^{-\lambda_n^2 t}$$

↳ general sol?

$$\bar{u} = (1 - \bar{y}) + \sum A_n \sin(\lambda_n \bar{y}) e^{-\lambda_n^2 t}$$

$$\text{where } \{A_n = c b_n\}$$

$$\text{At } t = 0, \bar{u} = 0 \neq \bar{y}$$

$$\therefore \bar{y} - 1 = \sum A_n \sin \lambda_n \bar{y} \quad - (*)$$

$$\text{Let } q_n = \sin \lambda_n \bar{y}$$

$$\text{We have, } f'' + \lambda^2 f = 0$$

$$\Rightarrow \frac{d^2 f_n}{d \bar{y}^2} + \lambda_n^2 f_n = 0 \quad \{f_n = A_n \sin \lambda_n \bar{y}\}$$

for some m ,

$$\int_0^1 f_m \frac{d^2 f_n}{d \bar{y}^2} d \bar{y} + \int_0^1 \lambda_n^2 f_n f_m d \bar{y} = 0$$

$$f_m \left. \frac{d f_n}{d \bar{y}} \right|_0^1 - \int_0^1 \frac{d f_m}{d \bar{y}} \frac{d f_n}{d \bar{y}} d \bar{y} + \lambda_n^2 \int_0^1 f_m f_n d \bar{y} = 0 \quad - (b)$$

Swapping m and n

$$- \int_0^1 \frac{d f_n}{d \bar{y}} \frac{d f_m}{d \bar{y}} d \bar{y} + \lambda_m^2 \int_0^1 f_m f_n d \bar{y} = 0 \quad - (c)$$

$$(\lambda_m^2 - \lambda_n^2) \int_0^1 f_m f_n d\bar{y} = 0$$

$$\Rightarrow m \neq n \quad \int_0^1 f_m f_n d\bar{y} = 0$$

From $\textcircled{*}$

$$(\bar{y} - 1) = \sum A_n (\sin \lambda_n \bar{y}) = \sum A_n q_n$$

Multiplying by q_m

$$\Rightarrow \int_0^1 (\bar{y} - 1) q_m d\bar{y} = \int_0^1 \sum A_n q_n q_m d\bar{y}$$

$$\text{R.H.S.} = 0 \quad \text{for } n \neq m.$$

For $n = m$

$$\int_0^1 (\bar{y} - 1) q_m d\bar{y} = \int_0^1 A_n q_n^2 d\bar{y}$$

$$\int_0^1 (\bar{y} - 1) \sin \lambda_n \bar{y} d\bar{y} = \int_0^1 A_n \sin^2 \lambda_n \bar{y} d\bar{y}$$

$$\int_0^1 \bar{y} \sin \lambda_n \bar{y} d\bar{y} - \int_0^1 \sin \lambda_n \bar{y} d\bar{y} = \text{R.H.S}$$

$$\left[-\bar{y} \frac{\cos \lambda_n \bar{y}}{\lambda_n} - \left\{ -\frac{\sin \lambda_n \bar{y}}{\lambda_n^2} \right\} \right]_0^1$$

$$+ \frac{\cos \lambda_n \bar{y}}{\lambda_n^2} \Big|_0^1 = \text{R.H.S}$$

$$- \frac{1 \cdot (-1)^n}{\lambda_n} - 0 - \{ 0 - 0 \} + \frac{(-1)^n}{\lambda_n}$$

$$- \frac{1}{\lambda_n} = \text{R.H.S}$$

$$R.H.S. = \frac{A_n}{2}$$

$$\Rightarrow -\frac{1}{\lambda_n} = \frac{A_n}{2}$$

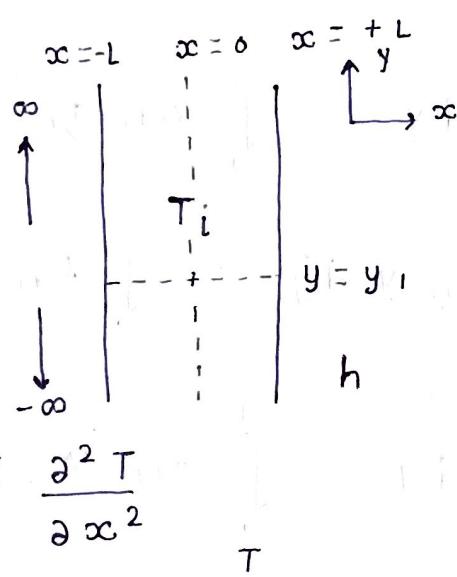
$$\Rightarrow A_n = -\frac{2}{\lambda_n} = -\frac{2}{n\pi}$$

$$\bar{u} = (1-\bar{y}) + \sum (A_n \sin \lambda_n \bar{y}) e^{-\lambda_n^2 t}$$

$$\bar{u} = (1-\bar{y}) - \frac{2}{\pi} \sum \frac{\sin \lambda_n \bar{y}}{n} e^{-\lambda_n^2 t}$$

Unsteady Heat Transfer :-

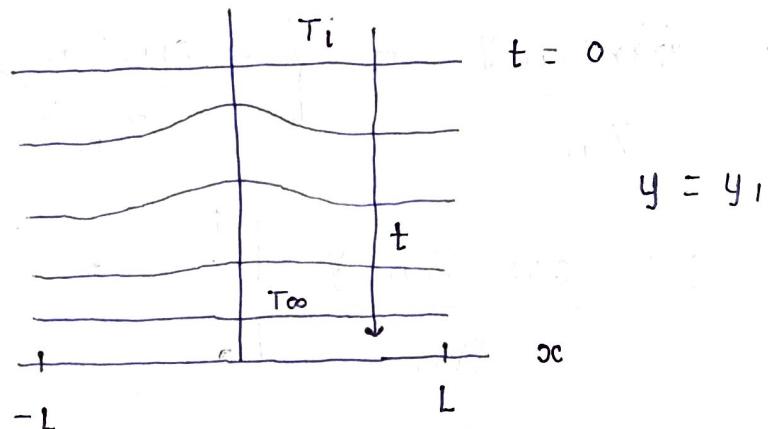
1-D heat conduction



$$T_i > T_\infty$$

$$\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial x^2}$$

$$\alpha = \frac{k}{\rho C_p}$$



γ = thermal diffusion time scale

$$\gamma = \frac{L^2}{\alpha}$$

$$x = 0 \quad \frac{\partial T}{\partial x} = 0$$

$$x = \pm L \quad -k \frac{\partial T}{\partial x} \Big|_{x=L} = h (T_{x=L} - T_{\infty})$$

I.C. $t = 0, T = T_i \forall x$

Non-dimensionalising the eqn

$$\theta = \frac{T - T_{\infty}}{T_i - T_{\infty}} \quad \bar{x} = \frac{x}{L} \quad \bar{t} = \frac{t}{t_c}$$

$$\frac{(T_i - T_{\infty})}{t_c} \frac{\partial \theta}{\partial \bar{t}} = \frac{\alpha (T_i - T_{\infty})}{L^2} \frac{\partial^2 \theta}{\partial \bar{x}^2}$$

$$\frac{1}{t_c} \frac{\partial \theta}{\partial \bar{t}} = \frac{\alpha}{L^2} \frac{\partial^2 \theta}{\partial \bar{x}^2}$$

$$\left(\frac{\partial \theta}{\partial \bar{t}} \right) = \left(\frac{\alpha t_c}{L^2} \right) \left(\frac{\partial^2 \theta}{\partial \bar{x}^2} \right)$$

$$\frac{\alpha t_c}{L^2} \sim 1 \quad \Rightarrow t_c = \frac{L^2}{\alpha}$$

$$\frac{\partial \theta}{\partial \bar{t}} = \frac{\partial^2 \theta}{\partial \bar{x}^2}$$

$$\frac{\partial \theta}{\partial F_0} = \frac{\partial^2 \theta}{\partial \bar{x}^2}$$

$$F_0 = \frac{t \alpha}{L^2}$$

$$= \frac{t}{t_c}$$

B.C. :-

$$\bar{x} = 0 \quad \frac{\partial \theta}{\partial \bar{x}} = 0$$

$$\bar{x} = 1, -k \frac{(T_i - T_{\infty})}{L} \frac{\partial \theta}{\partial \bar{x}} \Big|_{\bar{x}=1} = h (T_i - T_{\infty}) \theta \Big|_{\bar{x}=1}$$

$$\Rightarrow \frac{\partial \theta}{\partial x} \Big|_{x=1} = - \frac{hL}{k} \theta \Big|_{x=1}$$

I.C. :-

$$\Rightarrow \theta'(1) = - Bi \theta(1)$$

$F_0 = 0, \theta_0 = 1$

$$T = f(\bar{x}) g(F_0) = 0$$

$$fg' = g f''$$

$$\frac{g'}{g} = \frac{f''}{f} = -\lambda^2$$

$$-\lambda^2 F_0$$

$$\frac{g'}{g} = -\lambda^2 \Rightarrow g = c_1 e^{-\lambda^2 F_0}$$

$$f'' + \lambda^2 f = 0 \Rightarrow f = a \cos(\lambda \bar{x}) + b \sin(\lambda \bar{x})$$

$$\left. \begin{array}{l} \frac{\partial f}{\partial x} \Big|_{x=0} = 0 \\ f'(1) = - Bi(f(1)) \end{array} \right] \Rightarrow \begin{array}{l} f' = -a\lambda \sin(\lambda \bar{x}) \\ f' \Big|_{x=0} = b\lambda = 0 \\ \Rightarrow b = 0 \end{array}$$

$$f'(1) = -a\lambda \sin \lambda = -Bi a \cos \lambda$$

$$\Rightarrow \lambda \tan \lambda = Bi \rightarrow \text{not a finite no. for every value of } \lambda.$$

For some λ_n ,

$$\lambda_n \tan \lambda_n = Bi$$

$$\theta = \sum A_n \cos(\lambda_n \bar{x}) e^{-\lambda_n^2 t}$$

Applying the initial condition,

$$1 = \sum A_n \cos \lambda_n \bar{x}$$

$$\int_0^1 (\cos \lambda_m \bar{x}) d\bar{x} = \sum A_n \int_0^1 (\cos \lambda_n \bar{x}) (\cos \lambda_m \bar{x}) d\bar{x}$$

$$\frac{\sin \lambda_m}{\lambda_m} \left| \begin{array}{l} \\ 1 \\ \end{array} \right|_0 = \frac{\sum A_n}{2} \int_0^1 \cos(\lambda_m + \lambda_n) \bar{x} d\bar{x}$$

$$+ \frac{\sum A_n}{2} \int_0^1 \cos(\lambda_m - \lambda_n) \bar{x} d\bar{x}$$

$$\frac{\sin \lambda_m}{\lambda_m} = \frac{\sum A_n}{2} \left\{ \frac{\sin(\lambda_m + \lambda_n)}{\lambda_m + \lambda_n} \bar{x} + \frac{\sin(\lambda_m - \lambda_n)}{\lambda_m - \lambda_n} \bar{x} \right\}_0^1$$

$$\frac{\sin \lambda_m}{\lambda_m} = \frac{\sum A_n}{2} \left\{ \frac{\sin(\lambda_m + \lambda_n)}{(\lambda_m + \lambda_n)} + \frac{\sin(\lambda_m - \lambda_n)}{(\lambda_m - \lambda_n)} \right\}$$

$$\frac{\sin \lambda_m}{\lambda_m} = \frac{\sum A_n}{2} \cdot \frac{1}{\lambda_m^2 - \lambda_n^2}$$

$$\left\{ (\lambda_m - \lambda_n) \sin(\lambda_m + \lambda_n) + (\lambda_m + \lambda_n) \sin(\lambda_m - \lambda_n) \right\}$$

$$\frac{\sin \lambda_m}{\lambda_m} = \frac{\sum A_n}{2} \cdot \frac{1}{\lambda_m^2 - \lambda_n^2}$$

$$\left\{ \begin{array}{l} \lambda_m \left\{ \sin(\lambda_m + \lambda_n) + \sin(\lambda_m - \lambda_n) \right\} \\ -\lambda_n \left\{ \sin(\lambda_m + \lambda_n) - \sin(\lambda_m - \lambda_n) \right\} \end{array} \right.$$

$$\frac{\sin \lambda_m}{\lambda_m} = \sum A_n \left(\frac{\lambda_m \sin \lambda_m \cos \lambda_n - \lambda_n \cos \lambda_m \sin \lambda_n}{\lambda_m^2 - \lambda_n^2} \right)$$

$$\lambda_n \tan \lambda_n = \lambda_m \tan \lambda_m = Bi$$

$$\Rightarrow \lambda_n \sin \lambda_n \cos \lambda_m = \lambda_m \sin \lambda_m \cos \lambda_n$$

R.H.S. of $\textcircled{*}$ is zero for $m \neq n$

for $m = n$

$$\int_0^1 (\cos \lambda_m \bar{x}) d\bar{x} = A_m \int_0^1 \cos^2 \lambda_m \bar{x} d\bar{x}$$

$$\frac{\sin \lambda_m}{\lambda_m} = \frac{A_m}{2} \int_0^1 (\cos 2\lambda_m \bar{x} + 1) d\bar{x}$$

$$\frac{\sin \lambda_m}{\lambda_m} = \frac{A_m}{2} \left[\frac{\sin 2\lambda_m \bar{x}}{2\lambda_m} + \bar{x} \right]_0^1$$

$$\frac{\sin \lambda_m}{\lambda_m} = \frac{A_m}{2} \left[\frac{\sin 2\lambda_m}{2\lambda_m} + 1 \right]$$

$$\Rightarrow A_m = \frac{2 \sin \lambda_m}{\lambda_m} \left(\frac{2\lambda_m}{2\lambda_m + \sin 2\lambda_m} \right)$$

$$\Rightarrow A_m = \frac{4 \sin \lambda_m}{2\lambda_m + \sin 2\lambda_m}$$

$$\theta = \sum A_m \cos (\lambda_m \bar{x}) e^{-\lambda_m^2 F_0}$$

$$\text{where } A_m = \frac{4 \sin \lambda_m}{2\lambda_m + \sin 2\lambda_m}$$

Heisler Chart :

$$\theta_0 = \theta_0 (F_0) \quad \{ \theta_0 = \text{Mid line temp.} \}$$

For some $F_0 = a$,

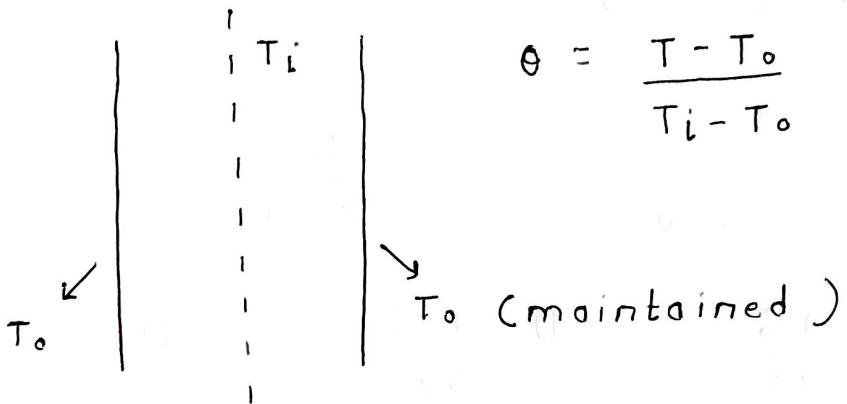
$$\theta_0 = \sum A_n e^{-\lambda n^2 a} \quad - \textcircled{1}$$

$$\theta_{F_0=a} (\bar{x}) = \sum A_n (\cos \lambda n \bar{x}) e^{-\lambda n^2 a} \quad - \textcircled{2}$$

$$\text{eq, } \textcircled{2} / \textcircled{1}$$

$$\frac{\theta_{(F_0=a)} (\bar{x})}{\theta_0 (F_0=a)} = \frac{\sum A_n (\cos \lambda n \bar{x}) e^{-\lambda n^2 a}}{\sum A_n e^{-\lambda n^2 a}}$$

Q.



$$\theta = \frac{T - T_0}{T_i - T_0}$$

$$1.C. : t = 0 \quad T = T_i \quad \forall x$$

$$B.C. : x = 0 \quad \frac{\partial T}{\partial x} = 0 \quad \forall t$$

$$x = L \quad T = T_0 \quad \forall t$$

Significance of scaling analysis?

Based on scaling analysis, we can design our equipments.

{ Book: Gupta and Gupta }

5/03/2019

Diffusion from instantaneous point source

$$r = 0, t = 0$$

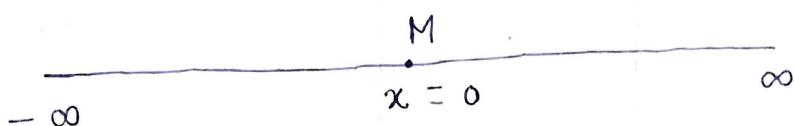
m_A

$$\rho_A = \frac{m_A}{(4\pi D_{AB} t)^{3/2}} \exp\left(-\frac{r^2}{4 D_{AB} t}\right)$$

(1) Check the validity of Fick's Law

$$(2) \int \rho_A dV = m_A \quad (\text{for any } t)$$

$$(3) t \rightarrow 0$$



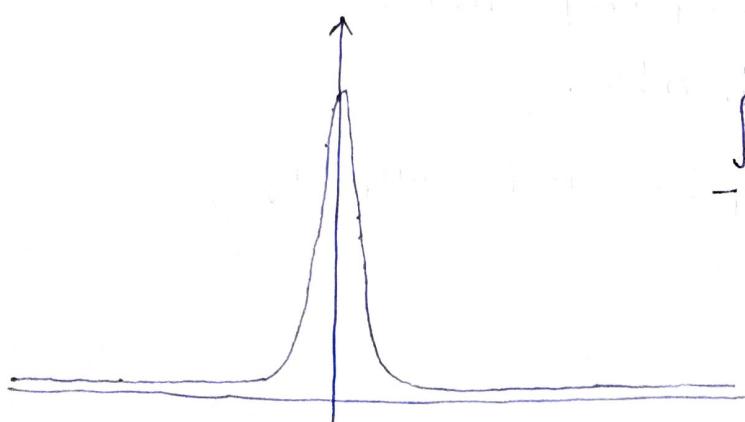
$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2} - \textcircled{1}$$

where,

$$C = \frac{M}{L} \quad (\text{linear density})$$

$$\text{B.C. : } x = \pm \infty, C \rightarrow 0$$

$$\text{I.C. : } t = 0, C = \frac{M}{L} \delta(x)$$



$$\int_{-\infty}^{\infty} \delta(x) dx = 1$$

$$\hat{c}(\alpha, t) = \int_{-\infty}^{\infty} c(x, t) e^{-i\alpha x} dx \quad (\text{Fourier Transform})$$

$$c_t = \frac{\partial c}{\partial t}$$

$$\int c_t e^{-i\alpha x} dx = \frac{\partial \hat{c}}{\partial t}(\alpha, t)$$

$$\int cx e^{-i\alpha x} dx = i\alpha \hat{c}(\alpha, t)$$

$$\int c_{xx} e^{-i\alpha x} dx = -\alpha^2 \hat{c}(\alpha, t)$$

Applying F.T. on eqⁿ ①

$$\frac{d\hat{c}}{dt} + D\alpha^2 \hat{c} = 0$$

$$\hat{c}(\alpha, t) = F(\alpha) \exp(-D\alpha^2 t)$$

Put $t = 0$,

$$F(\alpha) = \hat{c}(\alpha, 0) = \int \frac{M}{L} s(x) e^{-i\alpha x} dx$$

$$= \frac{M}{L}$$

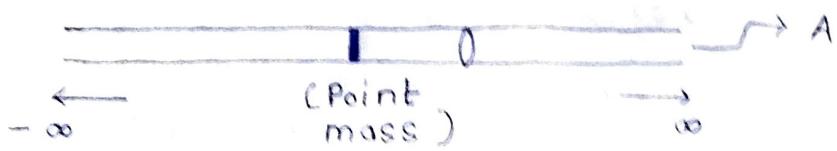
$$\hat{c}(\alpha, t) = \frac{M}{L} \exp(-D\alpha^2 t)$$

$$F(x, t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{c}(\alpha, t) e^{i\alpha x} d\alpha$$

$$c(x, t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{M}{L} \exp(-D\alpha^2 t) e^{i\alpha x} d\alpha$$

Profile is symmetric.

$$c(x, t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{M}{L} (\exp(-D\alpha^2 t)) \cos \alpha x$$



$$\Delta V = \lim_{\Delta x \rightarrow 0} A \Delta x$$

$$\Rightarrow \Delta V \rightarrow 0$$

$$c(t=0, x=0) = \lim_{\Delta V \rightarrow 0} \frac{M}{(A \Delta x)}$$

$$c(t=0) = \frac{M}{A} \delta(x) \leftarrow \text{I.C.}$$

$$\text{B.C. : } c(t, x=\pm\infty) = 0$$

$$\frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial x^2}$$

$$\frac{\partial \hat{c}}{\partial t} + D\alpha^2 \hat{c} = 0$$

$$\hat{c}(\alpha, t) = F(\alpha) \exp(-D\alpha^2 t)$$

$$\hat{c}(\alpha, 0) = F(\alpha)$$

$$\hat{c}(\alpha, 0) = \int_{-\infty}^{\infty} \frac{M}{A} \delta(x) e^{-i\alpha x} dx$$

$$= \frac{M}{A} = F(\alpha)$$

$$\hat{c}(\alpha, t) = \frac{M}{A} \exp(-D\alpha^2 t)$$

$$c(x, t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{M}{A} \exp(-D\alpha^2 t) e^{i\alpha x} d\alpha$$

$$\alpha = \frac{y}{\sqrt{Dt}} \Rightarrow d\alpha = \frac{dy}{\sqrt{Dt}}$$

$$c(x, t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{M}{A} \frac{\exp(-y^2)}{\sqrt{Dt}} \left(\cos\left(\frac{yx}{\sqrt{Dt}}\right) \right) dy$$

$$= \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{M}{A \sqrt{Dt}} \exp(-y^2) \cos(\eta y) dy$$

where $\eta = x / \sqrt{Dt}$

$$I(\eta) = \int_0^{\infty} e^{-y^2} \cos(\eta y) dy \quad - (*)$$

$$\frac{dI}{d\eta} = -\frac{1}{2} \int_0^{\infty} 2y e^{-y^2} \sin(\eta y) dy$$

$$\frac{dI}{d\eta} = \frac{1}{2} \int_0^{\infty} \sin(\eta y) d(e^{-y^2})$$

$$= e^{-y^2} \sin(\eta y) \Big|_0^{\infty} - \frac{1}{2} \int_0^{\infty} \eta e^{-y^2} \cos(\eta y) dy$$

$$= -\frac{\eta}{2} \int_0^{\infty} e^{-y^2} \cos \eta y dy$$

$$= -\frac{\eta}{2} I$$

$$\frac{dI}{d\eta} + \frac{\eta}{2} I = 0$$

$$\Rightarrow I(\eta) = I_0 \exp\left(-\frac{\eta^2}{4}\right)$$

Put $\eta = 0$ in $(*)$

$$I_0 = \frac{\sqrt{\pi}}{2}$$

$$\Rightarrow I = \frac{\sqrt{\pi}}{2} \exp\left(-\frac{\eta^2}{4}\right)$$

$$C(x, t) = \frac{M}{2A\sqrt{\pi D t}} \exp\left(-\frac{x^2}{4Dt}\right)$$

$$C(x, 0) = \frac{M}{A} \delta(x)$$

$$M = \int_A C(x, t) dA$$

$$= \int_{-\infty}^{\infty} \frac{M}{A} \delta(x) A dx$$

$$= M$$

$$\pi_1 = \frac{C}{M/(A\sqrt{Dt})}$$

$$\pi_2 = \frac{x}{\sqrt{Dt}}$$

$$\pi_1 = f(\pi_2) \Rightarrow C = \frac{M}{A\sqrt{Dt}} f\left(\frac{x}{\sqrt{Dt}}\right)$$

$$\eta = \frac{x}{\sqrt{Dt}} \Rightarrow \frac{d\eta}{dt} = -\frac{1}{2} \frac{x}{\sqrt{D} \sqrt{t}} = -\frac{\eta}{2t}$$

$$\frac{d\eta}{dx} = \frac{1}{\sqrt{Dt}}$$

3 fundamental variables : M, L, T

C is a dependent variable.

$$\left. \begin{array}{l} C \\ (\frac{M}{A}) \\ D \\ x \\ t \end{array} \right\} \text{Independent Variables}$$

Choose any fundamental quantity. Lets say T.

$$T = (C)^x \left(\frac{M}{A}\right)^y (D)^z$$

$$T = M^x L^{-3x} M^y L^{-2y} L^{2z} T^{-z}$$

$$z = -1 \quad x + y = 0 \quad 3x + 2y = 2z = -2$$

$$x = -2 \quad y = 2$$

$$\pi_1 = \frac{t}{(C^{-2}) \left(\frac{M}{A}\right)^2 D^{-1}} = \frac{c^2}{\left(\frac{M}{A}\right)^2 \frac{1}{Dt}}$$

$$\pi_1 = \frac{c}{M / A \sqrt{Dt}} = f(\pi_2)$$

$$\pi_2 = \frac{x}{\sqrt{Dt}}$$

$$\Rightarrow c = \frac{M}{A \sqrt{Dt}} f \left(\frac{x}{\sqrt{Dt}} \right)$$

$$\frac{x}{\sqrt{Dt}} = \eta$$

$$\frac{\partial \eta}{\partial t} = -\frac{\eta}{2t}, \quad \frac{\partial \eta}{\partial x} = \frac{1}{\sqrt{Dt}}$$

$$\frac{\partial C}{\partial t} = \frac{\partial}{\partial t} \left(\frac{M}{A\sqrt{Dt}} f(\eta) \right)$$

$$= \frac{M}{A\sqrt{Dt}} \frac{\partial f}{\partial t} - \frac{1}{2t} f \cdot \left(\frac{M}{A} \right) \frac{1}{\sqrt{Dt}}$$

$$= \frac{M}{A\sqrt{Dt}} \left(\frac{\partial f}{\partial \eta} \right) \left(-\frac{\eta}{2t} \right) + \frac{M}{A\sqrt{Dt}} \left(-\frac{f}{2t} \right)$$

$$\frac{\partial C}{\partial t} = \frac{-M}{2A + \sqrt{Dt}} \left(\eta \frac{\partial f}{\partial \eta} + f \right)$$

$$\frac{\partial C}{\partial x} = \frac{M}{A\sqrt{Dt}} \cdot \frac{\partial f}{\partial \eta} \cdot \frac{1}{\sqrt{Dt}}$$

$$\frac{\partial^2 C}{\partial x^2} = \frac{M}{A\sqrt{Dt}} \cdot \frac{1}{Dt} \frac{d^2 f}{d\eta^2}$$

$$\Rightarrow \frac{d^2 f}{d\eta^2} + \frac{1}{2} \left(f + \eta \frac{df}{d\eta} \right) = 0$$

$$\frac{d^2 f}{d\eta^2} + \frac{1}{2} \frac{d}{d\eta} (f\eta) = 0$$

$$\frac{d}{d\eta} \left(\frac{df}{d\eta} + \frac{f\eta}{2} \right) = 0$$

$$\frac{df}{d\eta} + f \frac{\eta}{2} = c_0$$

$$M = \int_{-\infty}^{\infty} C A dx$$

$$M = \int_{-\infty}^{\infty} \frac{M}{A \sqrt{Dt}} f\left(\frac{x}{\sqrt{Dt}}\right) A' dx$$

$$1 = \int_{-\infty}^{\infty} f(\eta) d\eta = 1$$

We have,

$$C(-\infty, t) = 0 \Rightarrow f(-\infty) = 0$$

$$C(x, 0) = \frac{M}{A} S(x)$$

$$f\left(\frac{x}{\sqrt{Dt}}\right) = S(x) \sqrt{Dt}$$

$$\text{Let } C_0 = 0$$

$$\frac{df}{d\eta} = -\frac{f\eta}{2}$$

$$\Rightarrow \ln f = -\frac{\eta^2}{4} + C_1$$

$$\Rightarrow f = C_1 \exp\left(-\frac{\eta^2}{4}\right)$$

$$\int_{-\infty}^{\infty} f d\eta = \int_{-\infty}^{\infty} C_1 \exp\left(-\frac{\eta^2}{4}\right) d\eta$$

$$1 = 2 \int_0^{\infty} C_1 \exp\left(-\frac{\eta^2}{4}\right) d\eta$$

$$\text{Let } \Rightarrow \frac{\eta}{2} = \xi$$

$$4 \int_0^{\infty} C_1 \exp\left(-\xi^2\right) d\xi = 1$$

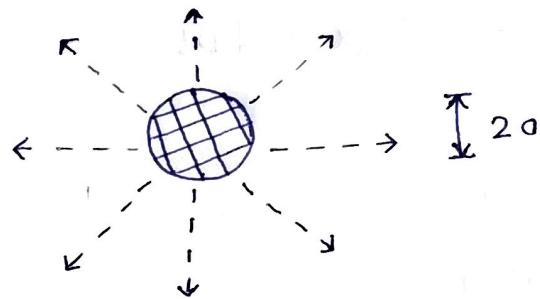
$$4 C_1 \frac{\sqrt{\pi}}{2} = 1$$

$$C_1 = \frac{1}{2\sqrt{\pi}}$$

$$C(x, t) = \frac{M}{A \sqrt{Dt}} \frac{1}{2\sqrt{\pi}} \exp\left(-\frac{x^2}{4Dt}\right)$$

$$C(x, t) = \frac{M}{A \sqrt{4\pi Dt}} \exp\left(-\frac{x^2}{4Dt}\right)$$

* Book : Conduction of heat in solids by Carslaw and Jaeger



$$t = 0, \quad C_0 = \frac{M}{\frac{4}{3}\pi a^3}$$

$$\frac{\partial C}{\partial t} = \frac{D}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial C}{\partial r} \right)$$

$$C = \frac{C_0}{2r (\pi Dt)^{1/2}} \int_0^\infty r' \left\{ \exp\left(-\frac{(r-r')^2}{4Dt}\right) - \exp\left(-\frac{(r+r')^2}{4Dt}\right) \right\} dr'$$

for $a \rightarrow 0$

$$C = \frac{M}{\frac{4}{3} \pi a^3} \cdot \frac{1}{8} \cdot \frac{e^{-r^2/4Dt}}{(\pi Dt)^{1/2}}$$

Scaling Analysis :

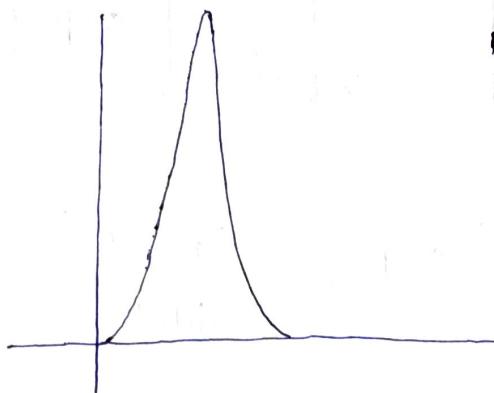
$$C = C_0 \cdot \frac{e^{-r^2/4Dt}}{8(\pi Dt)^{1/2}}$$

* 3 D diffusion, no θ and ϕ .

$r \rightarrow 0$ to a . beyond this $C = 0$

$$C = C_0 = \frac{M}{\frac{4}{3} \pi a^3}, \quad 0 < r \leq a$$

$$C = 0, \quad r > a$$



$r \rightarrow$ space
no connection
with time

$$\text{Substitute } C = \frac{u}{r}$$

Solve R.H.S :-

$$\frac{\partial}{\partial t} \left(\frac{u}{r} \right) = \frac{D}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \left(\frac{u}{r} \right)}{\partial r} \right)$$

$$\Rightarrow \frac{\partial}{\partial t} \left(\frac{u}{r} \right) = \frac{D}{r^2} \cdot 2r \frac{\partial \left(\frac{u}{r} \right)}{\partial r} + \frac{D}{r^2} \cdot \cancel{x^2}$$

$$\frac{\partial^2 \left(\frac{u}{r} \right)}{\partial r^2}$$

$$\frac{1}{\rho} \frac{\partial u}{\partial t} = \frac{D}{\rho} \frac{\partial^2 u}{\partial r^2}$$

$$\Rightarrow \frac{\partial u}{\partial t} = D \frac{\partial^2 u}{\partial r^2} \Rightarrow u = f(r, t)$$

r' can be any value

$$u = t^{-1/2} \exp \left(-\frac{(r-r')^2}{4Dt} \right) \text{ particular solution}$$

$$T = f = \sum a_n \cos \lambda_n \bar{x} \exp (-t^2 \lambda_n)$$

$$f = a \cos \lambda \bar{x}$$

$$* \frac{\partial u}{\partial t} = \left[\exp \left(-\frac{(r-r')^2}{4Dt} \right) \right] \left[\frac{(r-r')^2}{4D} \right. \\ \left. - \frac{1}{t^{3/2}} \right] - \frac{1}{2t^{3/2}} \left[\exp \left(-\frac{(r-r')^2}{4Dt} \right) \right]$$

$$\frac{\partial u}{\partial r} = t^{-1/2} \left\{ \exp \left(-\frac{(r-r')^2}{4Dt} \right) \right\} \left(\frac{-1}{4Dt} \right. \\ \left. (2(r-r')) \right)$$

$$\frac{\partial u}{\partial r} = - \frac{(r-r')^2}{2Dt^{3/2}} \exp \left[-\frac{(r-r')^2}{4Dt} \right]$$

$$\frac{\partial^2 u}{\partial r^2} = \frac{-1}{2Dt^{3/2}} \left\{ -\frac{(r-r')^2}{2Dt} \exp \left[-\frac{(r-r')^2}{4Dt} \right] \right. \\ \left. + \exp \left(-\frac{(r-r')^2}{4Dt} \right) \right\}$$

$$= \frac{(r-r')^2}{4D^2 t^{5/2}} \exp \left[-\frac{(r-r')^2}{4Dt} \right] -$$

$$\frac{1}{2Dt^{3/2}} \exp \left[-\frac{(r-r')^2}{4Dt} \right]$$

$$* f = \sum_{n=0}^{\infty} a_n \cos \lambda_n \bar{x}$$

$$\lambda_n = \left(n \pm \frac{1}{2} \right) \pi$$

a_n is dependent on λ_n .

For all $\lambda_n \rightarrow$ we get solution

$$u = \frac{1}{2\sqrt{\pi Dt}} \int_{-\infty}^{\infty} f(r') \exp \left(-\frac{(r-r')^2}{4Dt} \right) dr'$$

$\rightarrow r'$ is the variable. choice dependent.

$t \rightarrow 0$, $u = f(r)$ (known) \rightarrow

so f appears in integral.

$$u = cr$$

$$at t=0, c = c_0$$

$$\Rightarrow u = c_0 r$$

$$r' = r + 2\sqrt{Dt} \quad \text{Eq}$$

$$dr' = 2\sqrt{Dt} dr \quad \text{Eq}$$

[at some particular instant, t]

27.03.19.

$$\Rightarrow u = \frac{1}{\sqrt{\pi}} \int_{-\infty}^{\infty} f(r + 2\sqrt{Dt} \xi) e^{-\xi^2} d\xi$$

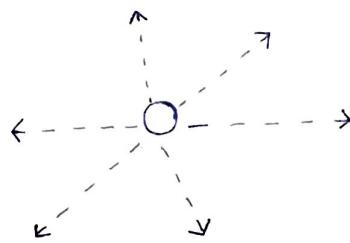
$$t \rightarrow 0$$

$$\begin{aligned}\Rightarrow u &= \frac{1}{\sqrt{\pi}} \int_{-\infty}^{\infty} f(r) e^{-\xi^2} d\xi \\&= f(r) * \frac{1}{\sqrt{\pi}} \int_{-\infty}^{\infty} e^{-\xi^2} d\xi \\&= f(r) \cdot \frac{2}{\sqrt{\pi}} \int_0^{\infty} e^{-\xi^2} d\xi \\&= f(r) \frac{2}{\sqrt{\pi}} \cdot \frac{\sqrt{\pi}}{2}\end{aligned}$$

$$u = f(r) \cdot 1$$

$$\Rightarrow u = f(r)$$

27.03.19



$$u = cr$$

$$\frac{\partial u}{\partial t} = D \frac{\partial^2 u}{\partial r^2}$$

$$t = 0, \quad u = C_0 r, \quad 0 < r < a \quad C_0 = \frac{M}{\frac{4}{3} \pi a^3}$$

$$= 0 \quad a < r$$

$$u = \frac{1}{2 \sqrt{\pi D t}} \int_{-\infty}^{\infty} f(r') \left(\exp \left(-\frac{(r-r')^2}{4 D t} \right) \right) dr'$$

where I.C. $t = 0 \quad u = f(r)$

$$\text{or, } u = \frac{1}{2 \sqrt{\pi D t}} \int_0^{\infty} f(r') \left\{ \exp \left(-\frac{(r-r')^2}{4 D t} \right) - \exp \left(-\frac{(r+r')^2}{4 D t} \right) \right\} dr'$$

$$u = \frac{1}{2 \sqrt{\pi D t}} \left(\exp \left(\frac{-r^2}{4 D t} \right) \right)$$

$$\int_0^a r' \exp \left(\frac{-r'^2}{4 D t} \right) \left\{ \exp \left(\frac{rr'}{2 D t} \right) - \exp \left(\frac{-rr'}{2 D t} \right) \right\} dr'$$

$$C = \frac{C_0}{2(\sqrt{\pi Dt})^3} \left(\exp\left(-\frac{r^2}{4Dt}\right) \right) \left\{ 1 + \left(\frac{r^2}{Dt} - 6 \right) \frac{\sigma^2}{40Dt} \right\} \times \frac{1}{3}$$

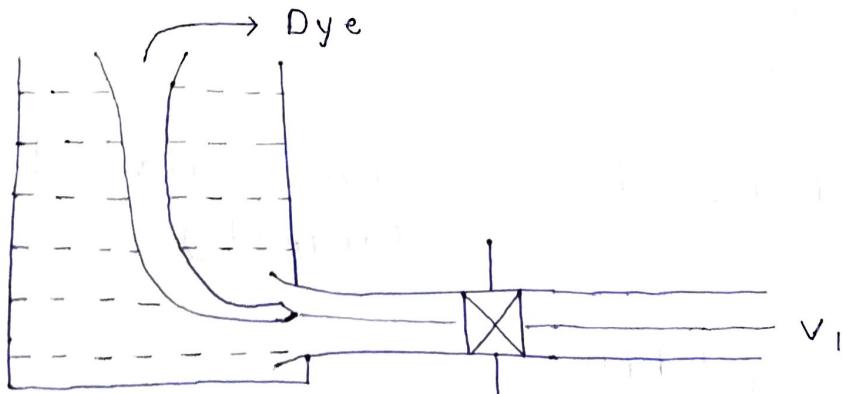
for $a \rightarrow 0$

$$C = \frac{C_0}{2(\sqrt{\pi Dt})^3} \exp\left(-\frac{r^2}{4Dt}\right) \times \frac{1}{3}$$

$$\Rightarrow C = \frac{M}{8(\pi Dt)^{3/2}} \exp\left(-\frac{r^2}{4Dt}\right)$$

Turbulence :

Reynold's Experiment :



At low velocity, regular and orderly flow.

Turbulent : erratic

fluctuations in
velocity. Irregular
flow

$$v_2 > v_1$$

$$v_3$$

$$v_4$$

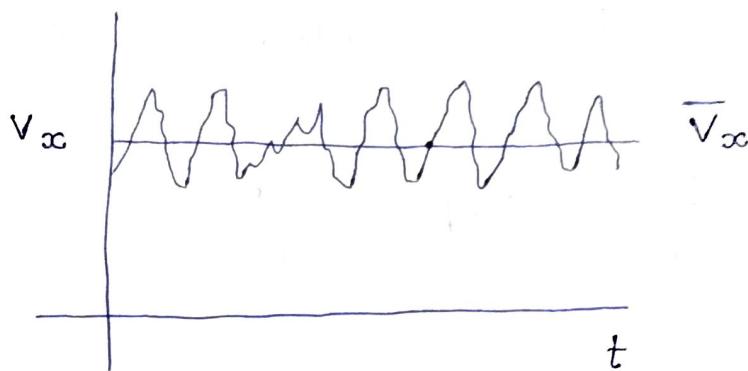
$$v_x(s, t) = \bar{v}_x(s) + v_x'(s, t)$$

↓

time independent

Such processes are known as stationary processes.

$\bar{v}_x(s)$: averaged over time



$$\lim_{T \rightarrow \infty} \frac{1}{2T} \int_{t-T}^{t+T} v_x' dt' = \bar{v}_x' = 0$$

provided, $T \gg$ time scale of fluctuations (largest)



Eddies

↳ lumps of fluid rotating

statistical averaging → to get something deterministic / predictable

Reynold's Decomposition:

$$v_x = \bar{v}_x + v_x'(x, y, z, t)$$

$$\begin{aligned}
 v_x &= \bar{v}_\infty + v'_\infty \\
 \int_{t-T}^{t+T} v_x dt' &\stackrel{?}{=} \frac{\int_{t-T}^{t+T} \bar{v}_\infty dt'}{2T} + \frac{\int_{t-T}^{t+T} v'_\infty dt'}{2T} \\
 \bar{v}_x &= \bar{v}_\infty + \bar{v}'_\infty \\
 \Rightarrow \bar{v}'_\infty &= 0 \\
 \frac{\bar{v}_x}{\bar{v}_x} \frac{\partial v_y'}{\partial x} &= \left(\int_{t-T}^{t+T} \bar{v}_\infty \frac{\partial v_y'}{\partial x} dt' \right) / 2T \\
 &= \bar{v}_\infty \frac{\int_{t-T}^{t+T} \frac{\partial v_y'}{\partial x} dt'}{2T} \\
 &= \bar{v}_\infty \frac{\partial}{\partial x} \frac{\int_{t-T}^{t+T} v_y' dt'}{2T} \\
 &= \bar{v}_\infty \cdot 0 = 0
 \end{aligned}$$

$$\begin{aligned}
 Re &= \frac{\text{Inertial force}}{\text{Viscous force}} = \frac{(\rho l^3) \frac{\bar{U}^2}{L}}{\mu \frac{\bar{U}}{L} \cdot l^2} \\
 &= \frac{\rho \bar{U} l}{\mu}
 \end{aligned}$$

Maximum length scale of an eddy ~
Radius of the pipe

For each eddy, we can have a local
Re.

$$l_e = f(Re, l_c)$$

Tl

↳ length scale of eddy

rate of extraction of energy from

$$\text{bigger eddy} \sim \frac{\bar{U}^2}{t}; \quad t = \frac{L}{\bar{U}}$$

{ l is or the order of length scale of system. Hence $\bar{U}_{\text{eddy}} \sim \bar{U}$ }

$$\dot{\epsilon} = \frac{\bar{U}^3}{L}$$

rate of dissipation by smallest eddy

$$\sim \dot{\epsilon} = (\mu \frac{\partial v_x}{\partial y}) \left(\frac{\partial v_x}{\partial y} \right) \rho^{-1}$$

$$v_x \sim u_e \quad (\text{order of velocity of } y \sim l_e \quad \text{smallest eddy})$$

$$\Rightarrow \dot{\epsilon} \sim \nu \frac{u_e^2}{l_e^2}$$

For smallest eddy $Re \sim 1$

$$\Rightarrow \frac{u_e l_e}{\nu} \sim 1 \quad \Rightarrow \quad u_e \sim \nu / l_e$$

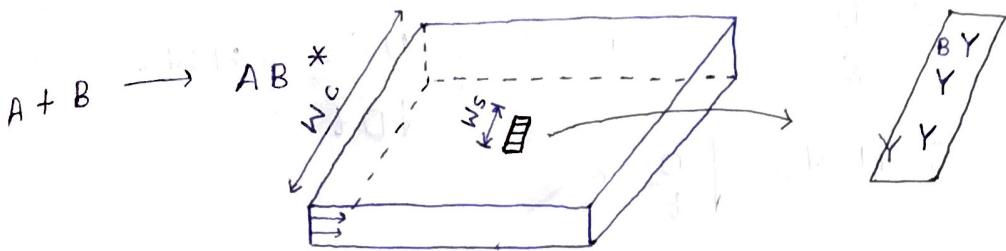
$$\therefore \dot{\epsilon} \sim \frac{\nu^3}{l_e^4}$$

$\dot{E} \sim \dot{\epsilon}$ (breaking of eddy occurs till this point)

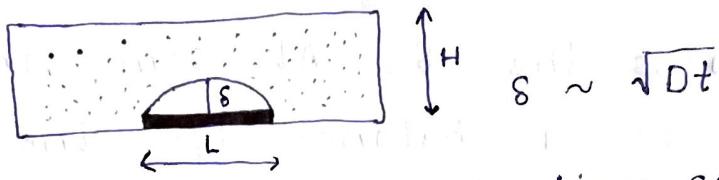
$$\frac{\bar{U}^3}{L} \sim \frac{\nu^3}{l_e^4}$$

$$l_e^4 \sim \frac{\nu^3 L}{\bar{U}^3}$$

$$I_e^4 \sim \left(\frac{L}{\frac{U_L}{2r}} \right)^3 L \Rightarrow I_e = L \left(\frac{1}{Re} \right)^{3/4}$$



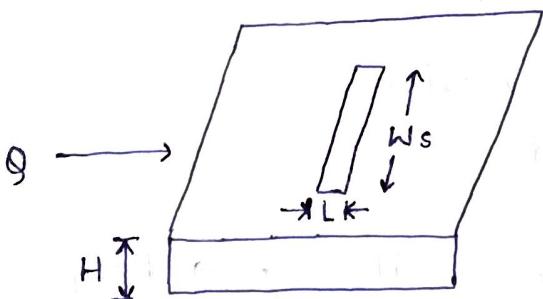
$A \xrightarrow{C_0}$ bulk flow \rightarrow Flux $j_D \sim D \frac{C_0}{8} \frac{s}{t}$



$$\tau_D = \frac{s^2}{D} \quad (\text{Diffusional time scale})$$

$$t \ll \frac{L^2}{D}, \quad s \ll H \quad t \ll \frac{H^2}{D}$$

$$J_D = j_D L W_s$$



A : Target molecule

B : Receptor

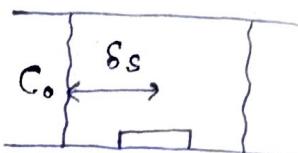
Reaction is instantaneous (transport l.t.d.)

C_0 : bulk concentration of A

$$J_D = D \frac{C_0}{s} L W_s = \frac{D C_0 L W_s}{\sqrt{Dt}} = C_0 L W_s \sqrt{\frac{D}{t}}$$

Early time, channel dimensions has no effect on J_D .

$$t \gg \frac{H^2}{D}$$



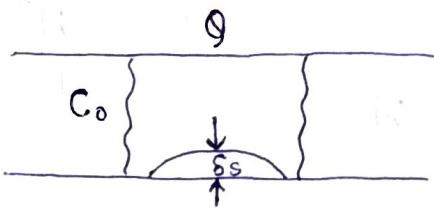
$$J_D = C_0 \frac{D}{\delta} ; \quad J_D = \left(\frac{DC_0}{\sqrt{Dt}} \right) HW_c$$

$$J_D \sim C_0 HW_c \sqrt{\frac{D}{t}}$$

• Flow is present : ($t \gg H^2/D$)

Diffusion increases the δ . Convection decreases the δ . At some instant, there is a balance b/w the two and δ will not change.

$$J_{\text{diffusion}} \sim \frac{DC_0 HW_c}{\delta s} \quad J_{\text{convection}} = C_0 \varphi$$



$$J_{\text{diffusion}} \approx J_{\text{convection}}$$

$$\frac{DC_0 HW_c}{\delta s} \approx \varphi \vartheta$$

$$\delta_s = \frac{DHW_c}{\vartheta} \sim \frac{H}{\left(\frac{\vartheta}{W_c D} \right)} \rightarrow Pe_H$$

$$Pe_H = \frac{\text{Diffusion time scale}}{\text{Convective time scale}} = \frac{H^2/D}{H/U}$$

$$Pe_H = \frac{H^2/D}{H/(U/HW_c)} = \frac{U}{DW_c}$$

$$\delta_s = \frac{H}{Pe_H}$$

(Valid for: $t \gg t_{\text{conv}}$)