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PAD -	Assign	ment 1
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Analysis of Vibrations.

$$m\frac{d^{2}x}{dt^{2}} + c\frac{dy}{dt} + Rx = F_{0}u(t)$$

$$m\left[s^{2}\bar{\chi}(s)-s\bar{\chi}(s)-\chi(s)\right]+cs\bar{\chi}(s)+k\bar{\chi}(s)=f_{u}(s)$$

$$\overline{x(s)} = F_0$$

$$\overline{u(s)} = ms^2 + cs + k$$

$$\frac{\overline{\chi}(\Delta)}{\overline{\chi}(\Delta)} = \frac{F_0/R}{R}$$

Comparing with the standard form:

$$\overline{\mathcal{A}}(\Delta) = \frac{K_b}{\nabla^2 \Delta^2 + 2\xi C \Delta + 1}$$

$$2\xi C = C/R$$

$$\xi = 2 R = C$$

$$2k m$$

$$2\sqrt{mR}$$

K	=	Fo/	K

Notural provided of oscillation = Z = \m/k

Domping coefficient = c 2/m/R

Steady state gain = Kp = Fo/k

Notural Period of Oscillation:

Period of Oscillation

 $7 = \frac{1}{2\pi} \left(\frac{2\pi z}{\sqrt{1 - \tilde{\xi}^2}} \right)$

for natural oscillation = = 0

Tn = 2

 $T_n = \sqrt{\frac{m}{n}}$

Laming coefficient:

 $\xi = c$ $2\sqrt{mk}$

Steady Grain:

Kp = Fo

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Transfer Function:

Now, substituting values,

$$\frac{m}{R}$$
 $\frac{c}{R}$ $\frac{c}{R}$ $\frac{c}{R}$ $\frac{c}{R}$ $\frac{c}{R}$



Underdomped, Overdamped & Critically damped:

$$\frac{m}{R}$$
 $\lambda^2 + \frac{C}{R}$ $\lambda + 1$

$$\frac{m}{k}$$
 $\frac{2}{R}$

$$s = -\frac{c}{k} + \sqrt{(9_k)^2 - 4(7_k)}$$

For underdamped case, nosts are complex conjugate

$$\left(\frac{c}{R}\right)^2$$

So,
$$\left(\frac{c}{R}\right)^2 - \frac{4(m)}{R} < 0$$

	For viitically damped,
	$\left(\frac{c}{R}\right)^2 - 4\left(\frac{m}{R}\right) = 0$
	$c = 2\sqrt{mk}$
	$\xi = 1$
	2 (E) e)
	For overdamped case,
	$\frac{\left(\frac{C}{R}\right)^2 - 4m_{1} + 0 + 0}{R}$
	c ² > 4mk (a) such 51
	2 /mk
	£>1 3
(4)	100 (10 to 100 (10 to 100 to 1
(d)	Response for step input
و بچ باند	W(s) = A/A Locustrible of
	For underdamped. $\overline{y}(\Delta) = 1$ $\int_{0}^{\infty} f_{0} dx$ $\int_{0}^{\infty} f_{0} dx$ $\int_{0}^{\infty} f_{0} dx$ $\int_{0}^{\infty} f_{0} dx$
	Δ τ ² Δ ² + 2ξτΔ+1
	$\widetilde{y}(\Delta) = AF_0 \cdot \frac{1}{k} \int_{-\infty}^{\infty} \frac{1}{\Delta} \frac{S + 2F/\tau}{\Delta^2 + 2F\Delta} = \frac{7\tau^2}{2}$
	R Z L S + 2E S + 1

Toking inverse laplace

$$Y(t) = AF_0 \left[1 - e^{\frac{-\xi t}{\zeta}} \left[\sqrt{-\xi^2 \cos\left(1 - \frac{\xi^2}{\zeta^2} t + \frac{\xi}{\zeta} \sin\left(1 - \frac{\xi}{\zeta} t + \frac{\xi}{\zeta} \sin\left(1$$

$$H = \sqrt{p^2 + q^2} \qquad \phi = \tan\left(\frac{p}{2}\right)$$

$$\frac{Y(t) = AF_0 \left[1 - \frac{\xi t}{\epsilon} \sin(\cot t + \phi) \right]}{R \left[\sqrt{1 - \xi^2} \sin(\cot t + \phi) \right]}$$

Oritically damped (Q=1)

$$y(s) = A \frac{50/R}{s}$$

$$y(s) = AF_0 \int_{\mathcal{R}} \frac{1}{\zeta^2 \left[s \left(s + V_{\zeta} \right)^2 \right]}$$

By partial fraction,

By Inverse Laplace

$$Y(t) = AF_{R} \left[1 - e^{-\frac{t}{2}} \left(1 + \frac{t}{2} \right) \right]$$

Overdamped Reponse (\$>1)

$$\overline{y}(s) = \frac{A(F_o)(\frac{1}{\zeta^2})}{S(R)(\frac{1}{\zeta^2})} \frac{1}{(\lambda^2 + 2\xi_s + \frac{1}{\zeta^2})}$$

$$\overline{y}(\Delta) = \left(\frac{AF_o}{R}\right) \left[\frac{1}{\Delta} \frac{\Delta + \overline{F}/c}{\Delta} - \frac{\overline{F}/c}{\overline{F}^2 - 1} \frac{\overline{F}^2 - 1}{\overline{F}^2 - 1} \frac{\overline{F}^2}{\overline{F}^2 - 1} \frac{\overline{F}^2 - 1}{\overline{F}^2 -$$

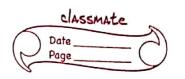
Taking Inverse Laplace

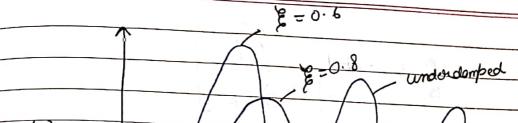
$$Y(t) = AF_0 \left[1 - e^{\frac{t}{E}t/E} \cosh \left(\frac{t^2-1}{E^2} + \frac{t}{E} \sinh \left(\frac{t^2-1}{E^2} + \frac{t}{E} \right) \right]$$

- * For underdomped system, decreasing & mokes the response more oscillatory
- * For Critically system, newponse reaches steady state move quickly without oscillations
- * For averdamped system, as & increases, me response becomes more sluggish.

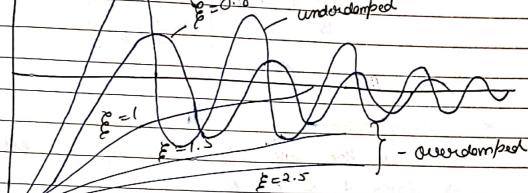
E & 1

speed of response

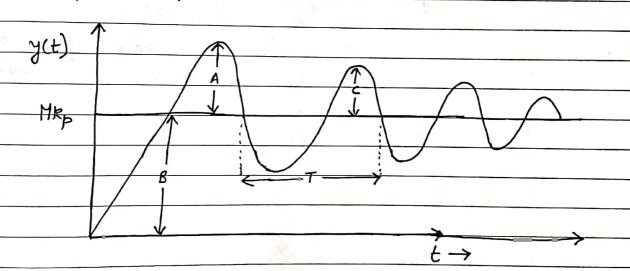








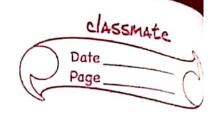
(e) Underdamped Response



avushoot:

Ratio of A/B

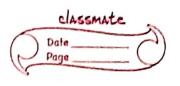
Overshoot =
$$\frac{A}{B} = \exp\left[-\frac{x\xi}{\sqrt{1-\xi^2}}\right]$$



$$\frac{A}{B} = \exp \left[\frac{-\chi c}{2\sqrt{mk}} \right]$$

1	Rupense of a body towards changes in neservoir temperature
200	given Equation
	$\frac{dT = -h(7 - T_{\infty})}{dt}$
	and the second s
	Too -> reservoir lamp
	$T_0 \rightarrow at t=0$
	(3 - 1 / 2 (- 1)
	dT = -hT + hTm
	$\frac{dT}{dt} = -hT + hT_{\infty}$
	$dT + hT = hT\infty$
	ð t
	$\frac{1 \cdot dT}{h} + T = T_{00} \longrightarrow (i)$
	For, 1 croder system
	$z \cdot dy + y = \chi(t) \cdot K_{p} \rightarrow (ii)$
-	Comparing (i) & (ii)
1	Time constant Steady state gain
\dashv	
4	$G(8) = 1$ $(\frac{1}{2})s+1$
4	
4	
9)	Step input of magnifude A
1	$T'(S) = T(t) - T_S$
	$G_1(A) = T'(A) = 1$ I_{A+1}
	$\frac{T_{oo}'(\lambda)}{T_{oo}'(\lambda)} = \frac{1}{D} \frac{\lambda+1}{D} \qquad \qquad T_{oo}'(\lambda) = \frac{1}{D} \frac{\lambda}{D} \frac{\lambda}{D} = \frac{1}{$
1	100(0) = 100(0)
1	
1	
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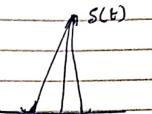
ment of	William of an or friends town or more
	$T_{\infty}'(s) = A/s$ $c = 1/h$
	$T'(s) = A \begin{pmatrix} 1 \\ -1 \\ s \end{pmatrix} \qquad k=1$
	$S(\frac{1}{h}S+1)$
	-ht
	$T(t) = T_s + A(1 - e^{-ht})$
. 2	
(d)	Pulse function:
	S = \$ 1/A 0 = E = A
	0 otherwise
	u(t)
	$T_{\infty}^{\prime}(b) = 1 \left(1 - e^{-Ab}\right)$
	A S
	AND
	$T'(s) = (1-e^{-As}) \begin{pmatrix} 1 \\ \frac{1}{p}s+1 \end{pmatrix}.$
	$As \left(\frac{1}{p}s+1\right)$
	By partial fraction
	11/ = 2/
	$T'(\Delta) = I\left(\frac{1}{\Delta} \frac{1}{\Delta + h}\right) \cdot \left(\frac{1}{\Delta} \frac{1}{\Delta + h}\right) = A\Delta$
	Inverse laplace LAIR
	14567
	$T = T_{k} + \frac{1}{A} \left(1 - e^{-ht} \right) - \left(1 - e^{-h(t-A)} \right) u(t-A)$
	AL A sharfings on the during not
10	Impulse function:
	1 -311 - 151 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
	Impulse function = 8(t)
A	$T_{\omega}(\lambda) = 1$
	T'(b) = 1
	1/8+1



inverse laplace

$$T'(t) = he^{-ht}$$

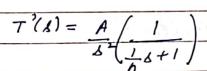
$$C = \frac{1}{h}$$

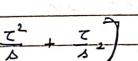


Ramp Function:

$$u(t) = At$$

 $T(t) = T_b + he^{-ht}$





By loplace inverse

where
$$z = \frac{1}{2}$$

For sinouidad response

 $T'(s) = A \int_{C} z^{2} + \frac{1}{3+1/2}$

$$T_{os}(\Delta) = A\omega$$

$$\Delta^2 + \omega^2$$

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1-15	By partial fraction
	$T'(\Delta) = A\omega \left[\frac{\zeta^2}{(1+\zeta^2\omega^2)(\lambda+\frac{1}{\zeta})} \frac{\zeta^2}{(1+\zeta^2\omega^2)(\lambda^2+\omega^2)} \frac{1}{(1+\zeta^2\omega^2)(\lambda^2+\omega^2)} \frac{\zeta^2}{(1+\zeta^2\omega^2)(\lambda^2+\omega^2)} \frac{1}{(1+\zeta^2\omega^2)(\lambda^2+\omega^2)} \frac{\zeta^2}{(1+\zeta^2\omega^2)(\lambda^2+\omega^2)} \frac{1}{(1+\zeta^2\omega^2)(\lambda^2+\omega^2)} \frac{1}{(1+\zeta^2\omega^2)} \frac{1}{(1$
	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
	Taking laplace inverse.
	$T(t) = A\omega t e^{-t/c} = -A\omega t \omega \omega t + A \sin \omega t$ $1 + t^2\omega^2 \qquad 1 + t^2\omega^2 \qquad 1 + t^2\omega^2$
	$1+c^2\omega^2 \qquad 1+c^2\omega^2 \qquad 1+c^2\omega^2$
	Trigonometry Identity
	$a\cos\theta + b\sin\theta = A\sin(\theta + 4)$
1	N=
	For this case $y = A$ $\phi = \tan^{-1}(\omega z)$
	$\sqrt{1+z^2\omega^2}$
	7(1) + 1 -42
	$T(t) = T_{s} + A\omega ce^{-4c} + A \omega ce^{-4c} + A \omega ce^{-4c}$ $1 + c^{2}\omega^{2} + \sqrt{1 + c^{2}\omega^{2}}$
\	
1	7 = 1/h
	Effect of Time constant burden landing
	C -> very small time constant
	D -> extremely large time constant
(ì)	For step input large z -> response
	For step input large z -> response
	A Small z - response
1	fast
	large z

