

Process Dynamics and Control (CH 61016)

SNEH LATA SINGH
181E33006

2.

$$A = \begin{bmatrix} a & 0.15 & b & -0.09 \\ -0.01 & c & 0.29 & x \\ d & 3.31 & 0.27 & e \\ 0.22 & f & g & 1.84 \end{bmatrix}$$

RGA matrix (Relative gain array) has a property by which
sum of each row = 1
sum of each column = 1.

as if $x = 1.15$, then

→ for 2nd row

$$-0.01 + c + 0.29 + 1.15 = 1$$

$$\Rightarrow c = -0.43$$

→ for 2nd column

$$0.15 + c + 3.31 + f = 1$$

$$(c = -0.43)$$

$$\Rightarrow f = -2.03$$

→ for 4th row

$$0.22 + f + g + 1.84 = 1$$

$$\Rightarrow g = 0.97$$

→ for 3rd column

$$b + 0.29 + 0.27 + g = 1 \quad (g = 0.97)$$

$$\Rightarrow b = -0.53$$

→ for 1st row

$$a + 0.15 + b + (-0.09) = 1$$

$$\Rightarrow a = 1.47$$

→ for 4th column

$$-0.09 + 1.15 + e + 1.84 = 1$$

$$\Rightarrow e = -1.9$$

→ for 3rd row

$$d + 3.31 + 0.27 + e = 1$$

$$\Rightarrow d = -0.68$$

So values are

$$a = 1.47, \quad b = -0.53, \quad c = -0.43$$

$$d = -0.68, \quad e = -1.9, \quad f = -2.03$$

So, final RGA matrix

$$\begin{bmatrix} 1.47 & 0.15 & -0.53 & -0.09 \\ -0.01 & -0.43 & 0.29 & 1.15 \\ -0.68 & 3.31 & 0.27 & -1.9 \\ 0.22 & -2.03 & 0.97 & 1.84 \end{bmatrix}$$

b.) No, we cannot complete the RGA if α is not known.

$$5). \quad a_1 \frac{dy}{dt} + a_0 y = b u(t)$$

Taking Laplace transform on both sides,
using the initial boundary condition $y(t=0)=0$
 $= \frac{dy}{dt}(t=0),$

$$a_1 s \bar{y}(s) + a_0 \bar{y}(s) = b \bar{u}(s)$$

$$\bar{y}(s) = \frac{b \bar{u}(s)}{a_1 s + a_0}$$

for sinusoidal input, $u(t) = A \sin \omega t$

Taking Laplace transform, $\bar{u}(s) = \frac{A \omega}{s^2 + \omega^2}$

$$\therefore \bar{y}(s) = \frac{b}{a_1 s + a_0} \frac{A \omega}{s^2 + \omega^2} = \frac{A \omega s}{(a_1 s + a_0)(s + i\omega)(s - i\omega)}$$

$$\therefore A_1 (s + i\omega)(s - i\omega) + A_2 (a_1 s + a_0)(s - i\omega) + A_3 (a_1 s + a_0)(s + i\omega) = 1$$

$$\Rightarrow s = i\omega \Rightarrow A_3 (i\omega a_1 + a_0) 2i\omega = 1$$

$$\Rightarrow A_3 = \frac{1}{2i\omega (i\omega a_1 + a_0)}$$

$$\Rightarrow s = -i\omega \Rightarrow A_2 (-i\omega a_1 + a_0) (-2i\omega) = 1$$

$$\Rightarrow A_2 = \frac{1}{2i\omega (i\omega a_1 - a_0)}$$

$$\Rightarrow s = -\frac{a_0}{a_1} \Rightarrow A_1 \left(-\frac{a_0}{a_1} + i\omega \right) \left(-\frac{a_0}{a_1} - i\omega \right) = 1$$

$$\Rightarrow A_1 = \frac{1}{\left(\frac{a_0}{a_1} \right)^2 + \omega^2} = \frac{a_1^2}{a_0^2 + a_1^2 \omega^2}$$

Making Laplace Inverse,

$$y(t) = A\omega_s \left[\frac{A_1}{a_1} \exp\left(-\frac{a_0}{a_1} t\right) + A_2 \exp(-i\omega t) + A_3 \exp(i\omega t) \right]$$

$$= A\omega_s \left[\frac{A_1}{a_1} \exp\left(-\frac{a_0}{a_1} t\right) + (A_2 + A_3) \cos \omega t + i(A_3 - A_2) \sin \omega t \right]$$

using $a_0 \rightarrow 0$

$$y(t) = \frac{AA_1}{a_1}$$

$$y(t) = \frac{Ab}{a_1 \omega} - \frac{Ab}{a_1 \omega} \cos(\omega t)$$

$$y(t) = \frac{Ab}{a_1 \omega} (1 - \cos(\omega t))$$

\therefore Difference b/w time period of oscillation,

$$\text{Input } T = \frac{2\pi}{\omega}$$

$$\text{Response } T = \frac{2\pi}{\omega}$$

$$\therefore \text{Input } T - \text{Response } T = \frac{2\pi}{\omega} - \frac{2\pi}{\omega} = 0$$

3. Transfer function model of a process

$$\begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} \frac{1.318 e^{-3s}}{20s+1} & \frac{-e^{-s}}{36} \\ \frac{0.38 (19s+1) e^{-2s}}{(27s+1)(10s+1)} & \frac{0.36}{s} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

a) Steady-state gain matrix.

$$\begin{bmatrix} \Delta y_1 \\ \Delta y_2 \end{bmatrix} = \begin{bmatrix} 1.318 & -1/3 \\ 0.38 & 0.36 \end{bmatrix} \begin{bmatrix} \Delta u_1 \\ \Delta u_2 \end{bmatrix}$$

$$\Lambda_{st} = \frac{1}{1 - \frac{k_{12} k_{21}}{k_{11} k_{22}}} = \frac{1}{1 - \frac{(-1/3)(0.36)}{1.318 \times 0.36}} = 0.7893$$

\therefore RGA matrix for the system:

$$\Lambda = \begin{bmatrix} \Lambda & 1-\Lambda \\ 1-\Lambda & \Lambda \end{bmatrix} = \begin{bmatrix} 0.7893 & 0.2107 \\ 0.2107 & 0.7893 \end{bmatrix}$$

b) $G_R = \text{diag}(G(s))$

$$= \begin{bmatrix} \frac{1.318 e^{-3s}}{20s+1} & 0 \\ 0 & \frac{0.36}{s} \end{bmatrix}$$

$$G^{-1} = \frac{1}{g_{11}g_{22} - g_{12}g_{21}} \begin{bmatrix} \frac{0.36}{s} & \frac{e^{-s}}{3s} \\ -\frac{0.38(18s+1)e^{-2s}}{(27s+1)(10s+1)} & \frac{1.318e^{-3s}}{20s+1} \end{bmatrix}$$

$$G_L = G^{-1} G_K$$

$$= \frac{1}{g_{11}g_{22} - g_{12}g_{21}} \begin{bmatrix} \frac{1.318 \times 0.36 e^{-3s}}{s(20s+1)} & \frac{0.36 e^{-s}}{3s^2} \\ -\frac{0.38 \times 1.318 (18s+1) e^{-5s}}{(20s+1)(27s+1)(10s+1)} & \frac{1.318 \times 0.36 e^{-3s}}{s(20s+1)} \end{bmatrix}$$

$$\begin{bmatrix} U_1 \\ U_2 \end{bmatrix} = G_L \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

4). State space Model of drug concentration in blood and tissue as

$$\frac{dx_1}{dt} = 0.4x_1 + 0.09x_2 + 0.005x_3 + 0.14$$

$$\frac{dx_2}{dt} = 0.2x_1 - 0.2x_2$$

$$\frac{dx_3}{dt} = 0.4x_1 - 0.005x_3$$

$$y = x_1$$

9) \Rightarrow state space Model has been determined,

$$\frac{dx_1}{dt} = -0.4x_1 + 0.09x_2 + 0.005x_3 + 0.14$$

$$\frac{dx_2}{dt} = 0.2x_1 + 0.2x_2$$

$$\frac{dx_3}{dt} = 0.4x_1 - 0.005x_3$$

$$y = x_1$$

$$\dot{x} = Ax + Bu$$

$$\dot{x} = \begin{bmatrix} -0.4 & 0.09 & 0.005 \\ 0.2 & -0.2 & 0 \\ 0.4 & 0 & -0.005 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0.14 \\ 0 \\ 0 \end{bmatrix} u$$

Since we have been given pole location

$$[-0.5, -0.15, -0.1]$$

we have to define a gain matrix

$$K = [K_1, K_2, K_3]$$

& Now, we have to equate

$$|sI - A + BK| =$$

$$|sI - A| = \begin{bmatrix} s & 0 & 0 \\ 0 & s & 0 \\ 0 & 0 & s \end{bmatrix} - \begin{bmatrix} -0.4 & 0.09 & 0.005 \\ 0.2 & -0.2 & 0 \\ 0.04 & 0 & -0.005 \end{bmatrix}$$

$$= \begin{bmatrix} s-0.4 & -0.09 & -0.005 \\ -0.2 & s+0.2 & 0 \\ -0.04 & 0 & s+0.005 \end{bmatrix}$$

$$|sI - A + BK|$$

$$= \begin{bmatrix} s-0.4 & -0.09 & -0.005 \\ -0.2 & s+0.2 & 0 \\ -0.04 & 0 & s+0.5 \end{bmatrix} + \begin{bmatrix} 0.1 \\ 0 \\ 0 \end{bmatrix} [K_1 \ K_2 \ K_3] \quad \text{--- ①}$$

Equating the constants with the help

$$(s+0.5)(s+0.15)(s+0.1) = 0 \quad \text{--- ②}$$

Now solving & Equating with ① & ②

Now we can get

$$K = \begin{bmatrix} 1.45 & 0.5154 & 8.7918 \end{bmatrix}$$

$$\boxed{K = \begin{bmatrix} 1.45 & 0.5154 & 8.7918 \end{bmatrix}}$$

4. b)

$$\frac{dx_1}{dt} = 0.2x_1 - 0.2x_2$$

$$\frac{dx_3}{dt} = 0.04x_1 - 0.005x_3$$

$$Ax + Bu$$

$$= \begin{bmatrix} 0.2 & 0 \\ 0 & -0.005 \end{bmatrix} x + \begin{bmatrix} 0 \\ 0 \end{bmatrix} u$$

reduced system has been mentioned.

Now, we have been given the pole placement as $[-0.05, -0.5]$

using ackermann's approach.

$$K = [0 \ 0] [B^T, AB] \phi(A) \quad \text{--- (1)}$$

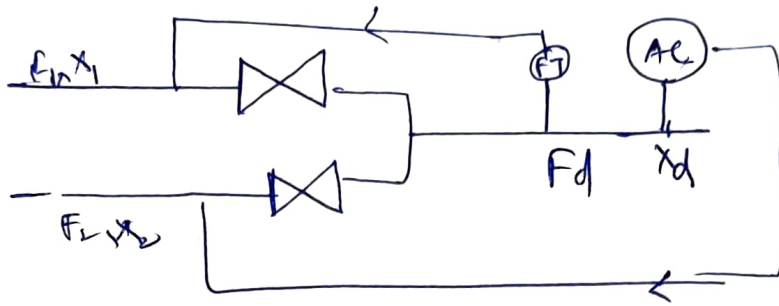
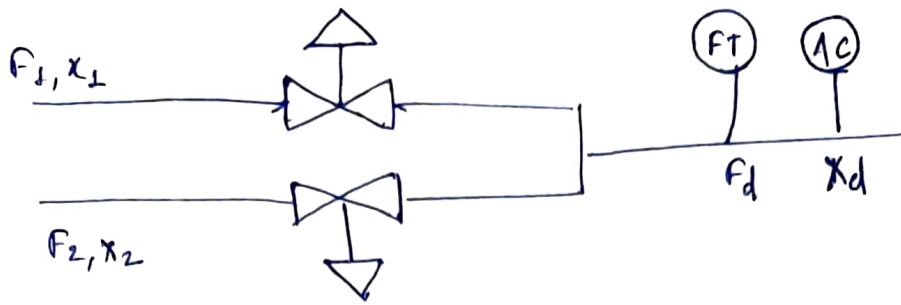
\therefore characteristic equation is given by.

$$(s+0.05)(s+0.5)=0$$

$$\text{Now, } \phi(A) = (A+0.5)(A+0.05)$$

Now eqⁿ two eqⁿ with the help of eqⁿ (3) & doing the Matrix OP in MATLAB, we get the values of K .

1.



consider $F_1, F_2 \rightarrow$ input
 $F_d, x_d \rightarrow$ output

let F_1 is ~~control~~ control to F_d and
 F_2 is control to x_d

equation are as follow

$$F_d = F_1 + F_2 \quad \text{--- (1)}$$

$$x_d = \frac{x_1 F_1 + x_2 F_2}{F_d} \quad \text{--- (2)}$$

for open loop

$$\frac{dF_d}{dF_1} = 1 \quad \left| \begin{array}{l} \text{open loop} \end{array} \right.$$

now closed $F_2 - x_d$ loop and open $F_d - F_1$ loop

eq ② become

$$0.5 F_d = 0.8 F_1 + 0.1 F_2$$
$$\therefore F_2 = 5 F_d - 8 F_1 \quad \text{--- ③}$$

put ③ in eq ①

$$F_1 + (5 F_d - 8 F_1) = F_d$$

$$4 F_d = 7 F_1$$

$$\therefore \frac{d F_d}{d F_1} = \frac{7}{4} \quad \left| \text{closed loop} \right.$$

Relative gain is given by

$$\lambda = \frac{1}{\frac{7}{4}} = \frac{4}{7}$$

Relative gain array is given by

$$RGA = \begin{bmatrix} \lambda & 1-\lambda \\ 1-\lambda & \lambda \end{bmatrix}$$

$$\begin{bmatrix} F_1 \\ F_2 \end{bmatrix} = \begin{bmatrix} 4/7 & 3/7 \\ 3/7 & 4/7 \end{bmatrix} \begin{bmatrix} F_d \\ X_d \end{bmatrix}$$

$$RGA = \begin{bmatrix} \boxed{0.571} & 0.42857 \\ 0.42857 & \boxed{0.571} \end{bmatrix}$$

From above RGA array it can be seen that best pair is $F_1 - F_d$ and $F_2 - X_d$.

= 6. Let the transfer function be

$$\frac{\bar{y}(s)}{\bar{u}(s)} = \frac{k (x_1 s + 1) (x_2 s + 1) \dots (x_q s + 1)}{(z_{p_1} s + 1) (z_{p_2} s + 1) \dots (z_p s + 1)}$$

This is for order (p, q)

$$\frac{\bar{y}(s)}{\bar{u}(s)} = \frac{k (x_1 s + 1) \dots (x_q s + 1)}{(z_{p_1} s + 1) \dots (z_p s + 1)}$$

Now, $\bar{u}(s) = \frac{A}{s}$ for step input

$$\therefore \bar{y}(s) = \frac{k (x_1 s + 1) \dots (x_q s + 1)}{(z_{p_1} s + 1) \dots (z_p s + 1)} \cdot \frac{A}{s}$$

Here, poles are roots of denominator, &
zeros are roots of numerator,

At poles, $\bar{y}(s)$ goes to infinity.
whereas at zeroes, $\bar{y}(s)$ goes to 0.

Therefore stability depends on $\bar{y}(s)$.