

INDIAN INSTITUTE OF TECHNOLOGY, KHARAGPUR Mid-Autumn Semester 2018-19

Date of Examination: 24-09-2018 Session (FN/AN) AN	Duration 2 hrs
Subject No.: CH20001 Subject Name: Fluid Mechanics	
Department/Center/School: Chemical Engineering	
Specific charts, graph paper, log book etc., required: No	
Special Instructions (if any): Assume any data you feel are missing	
Q1. A hot water tank is 28°C hotter at the top than at the bottom. A thermostat rebottom of the tank at 60°C, with temperature changing linearly with height. The	tank is 1.5 m tan, and vented
at the top. Assume that the density varies according to the relationship: $\frac{\rho(T)}{\rho(T_B)} = \frac{\rho(T)}{\rho(T_B)}$	kg/m³ Find
T and T_B are the temperatures in Kelvin. The density of water at 60° C is 983.21 (i) the pressure distribution in the tank as a function of height (ii) the pressure distribution in the tank if the entire tank is held at 60° C.	2+1=3 Marks
(ii) the pressure distribution in the tank it the entire tank is not a	(3)
<u>02.</u> For the velocity field, $\vec{V} = ax\hat{\imath} + ay\hat{\jmath} - 2az\hat{k}$, calculate i) acceleration	())
ii) the position of a particle at time t, if the coordinates of the particle was (x_0, y_0) iii) Vorticity	(y_0, z_0) at $t = 0$. 1+1+1=3 Marks
Q3. For the velocity field, $\vec{V} = \frac{1}{t_0 + t} x \hat{\imath} + v_0 \hat{\jmath}$, write the equation for streamline passing through (x_0, y_0) at time t	
write the equation for streamline passing through (x_0, y_0) at time t	
ii) write the equation for pathline of the fluid element that was at the position iii) show that the pathline forms a tangent to the streamline at (x_0, y_0)	2+2+1=5 Marks
Q4. The viscosity of a body fluid is found to be 6.5 cp at shear rate of 10 s ⁻¹ , ar What is the viscosity of the fluid when it is subjected to a shear stress of 100 dy follow a) Power law, b) Bingham plastic model?	μ (2) τ and 4.7 cp at shear rate of 80 s ⁻¹ . μ yne / cm ² assuming the fluid to μ 2+2=4 Marks
$\underline{O5.}$ The lower plate of a lubricated thrust bearing moves to the right at velocity V_O . The stop at the right prevents any liquid flow	Plate of weight W
beyond that point. Find the weight W that can be supported by the	L Stop
so that the end effects can be neglected. It can be assumed rather that the end if two unequal pressures act at the two ends (x=0 and	2 b Liquid (No Flow
x=L) of the plate it will not topple and the whole plate can be assumed to be acted on by an average of the two pressures at the two ends. 8 Marks	$ V_0$
Q6. A wetted wall column is used to measure mass transfer	5 2
coefficients. A liquid of density ρ and viscosity μ flows down the inside of a troof radius R, as shown in the figure. After an initial region, the flow becomes for developed and the thickness of the liquid layer is constant and equal to h. Simplify the Navier-Stokes and continuity equations to obtain $v_z(r)$ for lamin flow in the film.	ar Air h
	, ,2

.....continued

$$[\partial \rho/\partial t + (\nabla \cdot \rho \mathbf{v}) = 0]$$

Cartesian coordinates (x, y, z).

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} (\rho v_x) + \frac{\partial}{\partial y} (\rho v_y) + \frac{\dot{o}}{\partial z} (\rho v_z) = 0$$
 (B.4-1)

Cylindrical coordinates (r, 0, z)

$$\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r} (\rho r v_s) + \frac{1}{r} \frac{\partial}{\partial \theta} (\rho v_g) + \frac{\partial}{\partial z} (\rho v_z) = 0$$
 (B.4-2)

Spherical coordinates (r, θ, φ):

$$\frac{\partial \rho}{\partial t} + \frac{1}{r^2} \frac{\partial}{\partial r} (\rho r^2 v_i) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\rho v_\theta \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} (\rho v_\phi) = 0$$
 (B.4-3)

§B.6 EQUATION OF MOTION FOR A NEWTONIAN FLUID WITH CONSTANT ρ AND μ

$$[\rho D\mathbf{v}/Dt = -\nabla p + \mu \nabla^2 \mathbf{v} + \rho \mathbf{g}]$$

Cartesian coordinates (x, y, z):

$$\rho \left(\frac{\partial v_x}{\partial t} + v_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} + v_t \frac{\partial v_x}{\partial z} \right) = -\frac{\partial p}{\partial x} + \mu \left[\frac{\partial^2 v_x}{\partial x^2} + \frac{\partial^2 v_x}{\partial y^2} + \frac{\partial^2 v_x}{\partial z^2} \right] + \rho g_x \qquad (B.6-1)$$

$$\rho\left(\frac{\partial v_{y}}{\partial t}+v_{z}\frac{\partial v_{y}}{\partial x}+v_{y}\frac{\partial v_{y}}{\partial y}+v_{z}\frac{\partial v_{y}}{\partial z}\right)=-\frac{\partial p}{\partial y}+\mu\left[\frac{\partial^{2} v_{y}}{\partial x^{2}}+\frac{\partial^{2} v_{y}}{\partial y^{2}}+\frac{\partial^{2} v_{y}}{\partial z^{2}}\right]+\rho g_{y} \qquad (B.6-2)$$

$$\rho \left(\frac{\partial v_z}{\partial t} + v_x \frac{\partial v_z}{\partial x} + v_y \frac{\partial v_z}{\partial y} + v_z \frac{\partial v_z}{\partial z} \right) = -\frac{\partial p}{\partial z} + \mu \left[\frac{\partial^2 v_z}{\partial x^2} + \frac{\partial^2 v_z}{\partial y^2} + \frac{\partial^2 v_z}{\partial z^2} \right] + \rho g_z \qquad (B.6-3)$$

Cylindrical coordinates (r, 0, z):

$$\rho\left(\frac{\partial v_r}{\partial t} + v_r \frac{\partial v_r}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_r}{\partial \theta} + v_z \frac{\partial v_r}{\partial z} - \frac{v_\theta^2}{r^2}\right) = -\frac{\partial p}{\partial r} + \mu \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial}{\partial r} (rv_r)\right) + \frac{1}{r^2} \frac{\partial^2 v_r}{\partial \theta^2} + \frac{\partial^2 v_r}{\partial z^2} - \frac{2}{r^2} \frac{\partial v_\theta}{\partial \theta}\right] + \rho g_r$$
(B.6-4)

$$\rho \left(\frac{\partial v_{\theta}}{\partial t} + v_{r} \frac{\partial v_{\theta}}{\partial r} + \frac{v_{\theta}}{r} \frac{\partial v_{\theta}}{\partial \theta} + v_{z} \frac{\partial v_{\theta}}{\partial z} + \frac{v_{z}v_{\theta}}{r} \right) = -\frac{1}{r} \frac{\partial p}{\partial \theta} + \mu \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial}{\partial r} (rv_{\theta}) \right) + \frac{1}{r^{2}} \frac{\partial^{2} v_{\theta}}{\partial \theta^{2}} + \frac{\partial^{2} v_{\theta}}{\partial z^{2}} + \frac{2}{r^{2}} \frac{\partial v_{r}}{\partial \theta} \right] + \rho g_{\theta}$$
 (B.6-5)

$$\rho \left(\frac{\partial v_z}{\partial t} + v_r \frac{\partial v_z}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_z}{\partial \theta} + v_z \frac{\partial v_z}{\partial z} \right) = -\frac{\partial p}{\partial z} + \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_z}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_z}{\partial \theta^2} + \frac{\partial^2 v_z}{\partial z^2} \right] + \rho g_s$$
(B.6-6)

Spherical coordinates (r, θ, ϕ) :

$$\rho \left(\frac{\partial v_r}{\partial t} + v_r \frac{\partial v_r}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_r}{\partial \theta} + \frac{v_\phi}{r \sin \theta} \frac{\partial v_r}{\partial \phi} - \frac{v_\theta^2 + v_\phi^2}{r} \right) = -\frac{\partial p}{\partial r} + \mu \left[\frac{1}{r^2} \frac{\partial^2}{\partial r^2} (r^2 v_r) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial v_r}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 v_r}{\partial \phi^2} \right] + \rho g, \tag{B.6.7}$$

$$\rho\left(\frac{\partial v_{\theta}}{\partial t} + v, \frac{\partial v_{\theta}}{\partial r} + \frac{v_{\theta}}{r} \frac{\partial v_{\theta}}{\partial \theta} + \frac{v_{\theta}}{r \sin \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{v_{r}v_{\theta} - v_{\phi}^{2} \cot \theta}{r}\right) = \frac{1}{r} \frac{\partial p}{\partial \theta} + \frac{1}{r^{2} \sin^{2} \theta} \frac{\partial v_{\theta}}{\partial r} + \frac{1}{r^{2} \sin^{2} \theta} \frac{\partial v_{\theta}}{\partial \theta} + \frac{1}{r^{2} \sin^{2} \theta} \frac{\partial v_{\theta}}{\partial \phi^{2}} + \frac{1}{r^{2} \sin^{2} \theta} \frac{\partial v_{\theta}}{\partial \theta} - \frac{1}{r^{2} \sin \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin^{2} \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin^{2} \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin^{2} \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1}{r^{2} \sin^{2} \theta} \frac{\partial v_{\theta}}{\partial \phi} + \frac{1$$

$$\rho \left(\frac{\partial v_{\phi}}{\partial t} + v_{r} \frac{\partial v_{\phi}}{\partial r} + \frac{v_{\phi}}{r} \frac{\partial v_{\phi}}{\partial \theta} + \frac{v_{\phi}}{r} \frac{\partial v_{\phi}}{\partial \theta} + \frac{v_{\phi}v_{r} + v_{\theta}v_{\phi} \cot \theta}{r} \right) = \frac{1}{r \sin \theta} \frac{\partial p}{\partial \phi} + \frac{1}{r \sin \theta} \frac{\partial v_{\phi}}{\partial r} + \frac{1}{r^{2}} \frac{\partial}{\partial \theta} \left(\frac{1}{\sin \theta} \frac{\partial}{\partial \theta} (v_{\phi} \sin \theta) \right) + \frac{1}{r^{2}} \frac{\partial^{2}v_{\phi}}{\sin^{2}\theta} \frac{2}{\partial \phi^{2}} + \frac{2}{r^{2}} \frac{\partial v_{r}}{\sin \theta} \frac{2}{\partial \phi} + \frac{2}{r^{2}} \frac{\partial v_{\phi}}{\sin \theta} \frac{2}{\partial \phi} \frac{2}{\partial \phi} + \frac{2}{r^{2}} \frac{\partial v_{\phi}}{\sin \theta} \frac{2}{\partial \phi} \frac{2}{\partial \phi} + \frac{2}{r^{2}} \frac{\partial v_{\phi}}{\sin \theta} \frac{2}{\partial \phi} \frac{2}{\partial \phi} \frac{2}{\partial \phi} \frac{2}{\partial \phi} \frac{2}{r^{2}} \frac{\partial v_{\phi}}{\partial \phi} \frac{2}{\partial \phi} \frac{2}$$

When the fluid is assumed to have constant mass density ρ , the equation simplifies to $(\nabla \cdot \mathbf{v}) = 0$.