Heat Transfer

CH21004

Spatial effect

$$\frac{\partial^2 T}{\partial x^2} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$

$$T(x,0)=T_i$$

and the boundary conditions are

$$T = T(x, t, T_i, T_\infty, L, k, \alpha, h)$$

$$\theta^* \equiv \frac{\theta}{\theta_i} = \frac{T - T_{\infty}}{T_i - T_{\infty}} \qquad \frac{\partial^2 \theta^*}{\partial x^{*2}} = \frac{\partial \theta^*}{\partial F_O}$$

$$x^* \equiv \frac{X}{L}$$

$$t^* \equiv \frac{\alpha t}{L^2} \equiv Fo$$

$$\left. \frac{\partial T}{\partial x} \right|_{x=0} = 0$$

$$-k\frac{\partial T}{\partial x}\bigg|_{x=L} = h[T(L, t) - T_{\infty}]$$

$$\theta^*(x^*, 0) = 1$$

$$\left. \frac{\partial \theta^*}{\partial x^*} \right|_{x^*=0} = 0$$

$$\left. \frac{\partial \theta^*}{\partial x^*} \right|_{x^*=1} = -Bi \, \theta^*(1, t^*)$$

Spatial effect

$$\theta^* = f(x^*, Fo, Bi)$$

$$\theta^* = \sum_{n=1}^{\infty} C_n \exp(-\zeta_n^2 F_0) \cos(\zeta_n x^*)$$

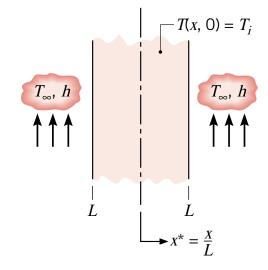
$$C_n = \frac{4\sin\zeta_n}{2\zeta_n + \sin(2\zeta_n)}$$

$$\zeta_n \tan \zeta_n = Bi$$

$$\frac{1}{\alpha} \frac{\partial T}{\partial t} = \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}$$

$$t = p \Delta t$$

$$\frac{\partial T}{\partial t}\Big|_{m, n} \approx \frac{T_{m, n}^{p+1} - T_{m, n}^{p}}{\Delta t}$$



$$\left. \frac{\partial T}{\partial t} \right|_{m, n} \approx \frac{T_{m, n}^{p+1} - T_{m, n}^{p}}{\Delta t}$$

$$\frac{1}{\alpha} \frac{\partial T}{\partial t} = \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}$$

$$\frac{1}{\alpha} \frac{T_{m,n}^{p+1} - T_{m,n}^p}{\Delta t} = \frac{T_{m+1,n}^p + T_{m-1,n}^p - 2T_{m,n}^p}{(\Delta x)^2} + \frac{T_{m,n+1}^p + T_{m,n-1}^p - 2T_{m,n}^p}{(\Delta y)^2}$$

$$T_{m,n}^{p+1} = Fo(T_{m+1,n}^p + T_{m-1,n}^p + T_{m,n+1}^p + T_{m,n-1}^p) + (1 - 4Fo)T_{m,n}^p$$

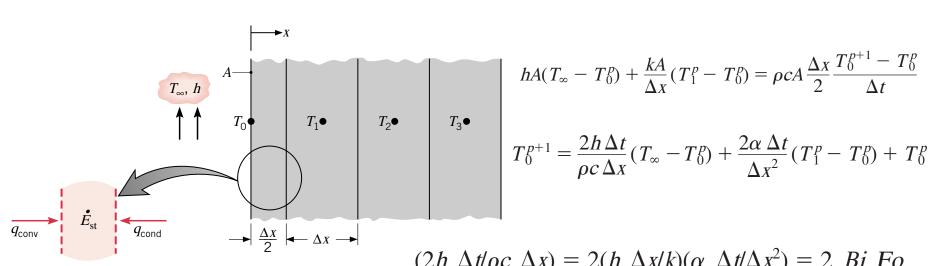
$$Fo = \frac{\alpha \, \Delta t}{(\Delta x)^2}$$

Explicit form

$$T_m^{p+1} = Fo(T_{m+1}^p + T_{m-1}^p) + (1 - 2Fo)T_m^p$$

$$(1 - 2Fo) \ge 0$$
, or $(1 - 4Fo) \ge 0$, or $Fo \le \frac{1}{4}$

$$\dot{E}_{\mathrm{in}} + \dot{E}_{\mathrm{g}} = \dot{E}_{\mathrm{st}}$$



$$hA(T_{\infty} - T_0^p) + \frac{kA}{\Delta x}(T_1^p - T_0^p) = \rho cA \frac{\Delta x}{2} \frac{T_0^{p+1} - T_0^p}{\Delta t}$$

$$T_0^{p+1} = \frac{2h\Delta t}{\rho c \Delta x} (T_{\infty} - T_0^p) + \frac{2\alpha \Delta t}{\Delta x^2} (T_1^p - T_0^p) + T_0^p$$

$$(2h \ \Delta t/\rho c \ \Delta x) = 2(h \ \Delta x/k)(\alpha \ \Delta t/\Delta x^2) = 2 \ Bi \ Fo$$

$$Bi = \frac{h \, \Delta x}{k}$$

$$T_0^{p+1} = 2Fo(T_1^p + Bi T_{\infty}) + (1 - 2Fo - 2Bi Fo)T_0^p$$

$$1 - 2Fo - 2BiFo \ge 0$$

$$Fo(1+Bi) \le \frac{1}{2}$$

$$\frac{1}{\alpha} \frac{\partial T}{\partial t} = \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2}$$

$$\frac{1}{\alpha} \frac{T_{m,n}^{p+1} - T_{m,n}^{p}}{\Delta t} = \frac{T_{m+1,n}^{p+1} + T_{m-1,n}^{p+1} - 2T_{m,n}^{p+1}}{(\Delta x)^{2}} + \frac{T_{m,n+1}^{p+1} + T_{m,n-1}^{p+1} - 2T_{m,n}^{p+1}}{(\Delta y)^{2}}$$

$$(1 + 4Fo)T_{m,n}^{p+1} - Fo(T_{m+1,n}^{p+1} + T_{m-1,n}^{p+1} + T_{m,n+1}^{p+1} + T_{m,n-1}^{p+1}) = T_{m,n}^{p}$$

Implicit form

TABLE 5.3 Transient, two-dimensional finite-difference equations $(\Delta x = \Delta y)$

(a) Explicit Method Configuration **Finite-Difference Equation Stability Criterion** (b) Implicit Method $T_{m,n}^{p+1} = Fo(T_{m+1,n}^p + T_{m-1,n}^p)$ $(1+4Fo)T_{m,n}^{p+1} - Fo(T_{m+1,n}^{p+1} + T_{m-1,n}^{p+1})$ $+ T_{m\,n+1}^p + T_{m\,n-1}^p$ $Fo \leq \frac{1}{4}$ $+ T_{m,n+1}^{p+1} + T_{m,n-1}^{p+1}) = T_{m,n}^{p}$ (5.92) $+(1-4Fo)T_{mn}^{p}$ (5.76)1. Interior node $T_{m,n}^{p+1} = \frac{2}{3} Fo(T_{m+1,n}^p + 2T_{m-1,n}^p)$ $(1 + 4Fo(1 + \frac{1}{3}Bi))T_{mn}^{p+1} - \frac{2}{3}Fo$. $Fo(3 + Bi) \le \frac{3}{4}$ (5.86) $(T_{m+1,n}^{p+1} + 2T_{m-1,n}^{p+1} + 2T_{m,n+1}^{p+1} + T_{m,n-1}^{p+1})$ $+2T_{m\,n+1}^{p}+T_{m\,n-1}^{p}+2Bi\,T_{\infty}$ $= T_{mn}^p + \frac{4}{3}BiFoT_{\infty}$ $+ (1 - 4Fo - \frac{4}{3}BiFo)T_{mn}^{p}$ (5.85)2. Node at interior corner with convection $T_{m,n}^{p+1} = Fo(2T_{m-1,n}^p + T_{m,n+1}^p)$ $(1 + 2Fo(2 + Bi))T_{mn}^{p+1}$ $Fo(2 + Bi) \le \frac{1}{2}$ (5.88) $-Fo(2T_{m-1,n}^{p+1} + T_{m,n+1}^{p+1} + T_{m,n-1}^{p+1})$ $+ T_{m\,n-1}^p + 2Bi\,T_{\infty}$ $+ (1 - 4Fo - 2BiFo)T_{mn}^{p}$ (5.87) $= T_{mn}^p + 2BiFoT_{\infty}$ (5.96)3. Node at plane surface with convection^a $T_{m,n}^{p+1} = 2Fo(T_{m-1,n}^p + T_{m,n-1}^p + 2BiT_{\infty}) + (1 - 4Fo - 4BiFo)T_{m,n}^p$ (5.89) $Fo(1 + Bi) \le \frac{1}{4}$ (5.90) $(1 + 4Fo(1 + Bi))T_{m,n}^{p+1} - 2Fo(T_{m-1,n}^{p+1} + T_{m,n-1}^{p+1})$ $= T_{mn}^p + 4Bi Fo T_{\infty}$ (5.97)4. Node at exterior corner with convection

^aTo obtain the finite-difference equation and/or stability criterion for an adiabatic surface (or surface of symmetry), simply set Bi equal to zero.