Controller Design based on State Space Model

Controllability

- A system is said to be *controllable* at time t_0 if it is possible by means of an *unconstrained* control vector to transfer the system from any initial state X_0 to any other state in a finite interval of time
- Controllability depends upon the system matrix
 A and the control influence matrix B

Condition for Controllability: (single input case)

System:

$$\dot{X} = AX + Bu$$

Solution:

$$X(t) = e^{At}X(0) + \int_0^t e^{A(t-\tau)}Bu(\tau) d\tau$$

Assuming $X(t_1) = 0$, $0 = e^{At_1}X(0) + \int_0^{t_1} e^{A(t_1 - \tau)}Bu(\tau)d\tau$

$$X(0) = -\int_{0}^{t_{1}} e^{-A\tau} Bu(\tau) d\tau$$

Condition for Controllability: (single input case)

$$e^{-A\tau} = \sum_{k=0}^{n-1} \alpha_k(\tau) A^k \quad \text{(Sylvester's formula)}$$

$$X(0) = -\int_0^{t_1} e^{-A\tau} Bu(\tau) d\tau = -\sum_{k=0}^{n-1} A^k B \int_0^{t_1} \alpha_k(\tau) u(\tau) d\tau$$

$$= -\sum_{k=0}^{n-1} A^k B \beta_k \quad \text{where} \quad \beta_k \triangleq \int_0^{t_1} \alpha_k(\tau) u(\tau) d\tau$$

$$= -\left[B \quad AB \quad \cdots \quad A^{n-1}B \right] \left[\beta_0 \quad \beta_1 \quad \cdots \quad \beta_{n-1} \right]^T$$

This system should have a non-trivial solution for $\begin{bmatrix} eta_0 & eta_1 & \cdots & eta_{n-1} \end{bmatrix}^T$

Condition for Controllability (multiple input case)

The result obtained for single input case can be easily extended for m-dimensional control input U.

System:
$$\dot{X} = AX + BU$$

$$X(0) = -\int_0^{t_1} e^{-A\tau} BU(\tau) d\tau$$

=
$$[B \ AB \ ... \ A^{n-1}B][\beta_0 \ \beta_1 \ ... \ \beta_{n-1}]^T$$

Condition for Controllability (multiple input case)

$$X(0) = [B \ AB \ ... \ A^{n-1}B][\boldsymbol{\beta_0} \ \boldsymbol{\beta_1} \ ... \ \boldsymbol{\beta_{n-1}}]^T$$

For completely state controllability, this equation must be satisfied. This requires the rank of

$$C_B = [B \ AB \ \dots \ A^{n-1}B]$$

Should be n.

Controllability

Result: If the rank of $C_B \triangleq \begin{bmatrix} B & AB & \cdots & A^{n-1}B \end{bmatrix}$ is n, then the system is controllable.

Example:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u$$

$$C_B = \begin{bmatrix} 2 \\ 1 \end{bmatrix} \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} 2 \\ 1 \end{bmatrix} = \begin{bmatrix} 2 & -2 \\ 1 & -2 \end{bmatrix}$$

 $rank(C_B) = 2$: The system is controllable.

Output Controllability

Result:
$$\dot{X} = AX + BU$$

$$Y = CX + DU$$

$$X \in \mathbb{R}^n$$
, $U \in \mathbb{R}^m$, $Y \in \mathbb{R}^p$

If the rank of $C_B \triangleq \begin{bmatrix} CB & CAB & \cdots & CA^{n-1}B & D \end{bmatrix}$ is p, then the system is output controllable.

Note: The presence of DU term in the output equation always helps to establish output controllability.

Observability

- A system is said to be *observable* at time t_0 if, with the system in state $X(t_0)$, it is possible to determine this state from the observation of the output over a finite interval of time
- Observability depends upon the system matrix A and the output matrix C

Condition for Observability

System:
$$\dot{X} = AX$$

$$Y = CX$$

Output:
$$Y(t) = Ce^{At}X(0)$$

Sylvester Formula:
$$e^{At} = \sum_{k=0}^{n-1} \alpha_k(t) A^k$$

So,
$$Y(t) = \sum_{k=0}^{n-1} \alpha_k(t) CA^k X(0)$$

Condition for Observability

Expanding,

$$Y(t) = \alpha_0(t)CX(0) + \alpha_1(t)CAX(0) + \dots + \alpha_{n-1}(t)CA^{n-1}X(0)$$

If the system is completely observable, then given Y(t) over a time interval $0 \le t \le t_1$, X(0) should be determined from above equation. This requires the following $[np \ x \ n]$ matrix,

$$O_B = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix} = \begin{bmatrix} C^T & A^TC^T & \dots & (A^T)^{n-1}C^T \end{bmatrix}$$

must have rank n

Observability

Result: If the rank of $O_B \triangleq \begin{bmatrix} C^T & A^T C^T & \cdots & (A^T)^{n-1} & C^T \end{bmatrix}$ is n, then the system is observable.

Example:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u \qquad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$O_B = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 & -1 \\ 0 & 0 \end{bmatrix}$$

 $rank(O_B) = 1 \neq 2$: The system is NOT observable.

Discuss State controllability of
$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} -3 & 1 \\ -2 & 1.5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 4 \end{bmatrix} \mathbf{u}$$

Discuss State controllability of

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} -3 & 1 \\ -2 & 1.5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 4 \end{bmatrix} \mathbf{u}$$

So,
$$A = \begin{bmatrix} -3 & 1 \\ -2 & 1.5 \end{bmatrix}$$
; $B = \begin{bmatrix} 1 \\ 4 \end{bmatrix}$;

$$M = M = \begin{bmatrix} B & AB \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 4 & 4 \end{bmatrix}$$
. So rank(M) = 1

The system is not controllable. Why?

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The system is not controllable. Why?

$$\frac{X_1(s)}{U(s)} = \frac{s + 2.5}{(s + 2.5)(s - 1)}$$

So, Pole-Zero cancellation occurs.

Discuss controllability & observability of

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -0.4 & -1.3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u \qquad y = \begin{bmatrix} 0.8 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

Discuss controllability & observability of

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -0.4 & -1.3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \mathbf{u} \qquad y = \begin{bmatrix} 0.8 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

So,
$$A = \begin{bmatrix} 0 & 1 \\ -0.4 & -1.3 \end{bmatrix}$$
; $B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$;

$$M = \begin{bmatrix} B & AB \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 1 & -1.3 \end{bmatrix}$$
. So rank(M) = 2 The system is controllable.

$$N = \begin{bmatrix} C^T & A^T C^T \end{bmatrix} = \begin{bmatrix} 0.8 & -0.4 \\ 1 & -0.5 \end{bmatrix}$$
. So rank(N) = 1 The system is not observable

If we write the system in observable canonical form then, The system is observable but not controllable. Why? Discuss controllability & observability of

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -0.4 & -1.3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \mathbf{u} \qquad y = \begin{bmatrix} 0.8 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

So,
$$A = \begin{bmatrix} 0 & 1 \\ -0.4 & -1.3 \end{bmatrix}$$
; $B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$;

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. So rank(N) = 1 The system is not observable

If we write the system in observable canonical form then, The system is observable but not controllable. Why?

$$\frac{X_1(s)}{U(s)} = \frac{s + 0.8}{(s + 0.8)(s + 0.5)}$$

So, Pole-Zero cancellation occurs.

Controllability and Observability in Transfer Function Domain

 The system is both controllable and observable if there is no Pole-Zero cancellation.

 Note: The cancelled pole-zero pair suppresses part of the information about the system

Principle of Duality

System
$$S_1$$
: $\dot{X} = AX + BU$ $C_B = \begin{bmatrix} B & AB & A^2B & \cdots & A^{n-1}B \end{bmatrix}$ $Y_1 = CX$ $O_B = \begin{bmatrix} C^T & A^TC^T & A^{T^2}C^T & \cdots & A^{T^{n-1}}C^T \end{bmatrix}$ System S_2 : $\dot{Z} = A^TZ + C^TV$ $C_B = \begin{bmatrix} C^T & A^TC^T & A^{T^2}C^T & \cdots & A^{T^{n-1}}C^T \end{bmatrix}$

System **S₂:**
$$\dot{Z} = A^T Z + C^T V$$
 $C_B = \begin{bmatrix} C^T & A^T C^T & A^{T^2} C^T & \cdots & A^{T^{n-1}} C^T \end{bmatrix}$ $Y_2 = B^T Z$ $O_B = \begin{bmatrix} B & AB & A^2 B & \cdots & A^{n-1}B \end{bmatrix}$

The principle of duality states that the system S_1 is controllable if and only if system S_2 is observable; and vice-versa!

Hence, the problem of observer design for a system is actually a problem of control design for its dual system.

Stabilizability and Detectability

 Stabilizable system: Uncontrollable system in which uncontrollable part is stable

 Detectable system: Unobservable system in which the unobservable subsystem is stable

State Space Controller Design

System:
$$\dot{X} = AX + BU$$
 $X \in \mathbb{R}^n, U \in \mathbb{R}^m$

$$Y = CX + DU \qquad Y \in \mathbb{R}^p$$

Controllability:

State: Rank of $C_B = [B AB ... A^{n-1}B]$ is n

Output: Rank of $C_B = [CB \ CAB \ ... \ CA^{n-1}B \ D]$ is p

Observability:

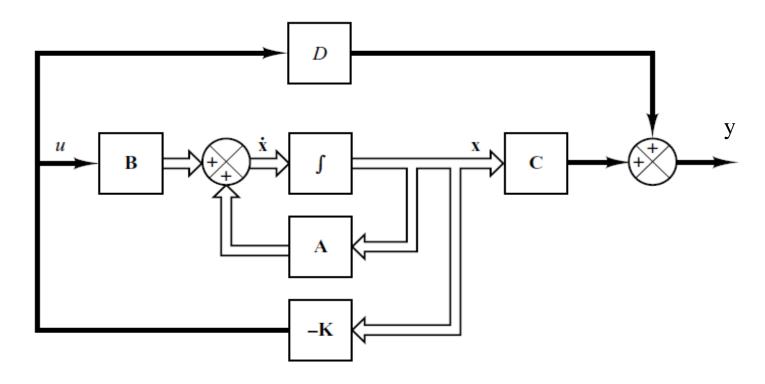
Rank of
$$O_B = \begin{bmatrix} C^T & A^T C^T & \dots & A^{T(n-1)} C^T \end{bmatrix}$$
 is n

State Feedback Controller

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System: \dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}
                         y = \mathbf{C}\mathbf{x} + Du
            where \mathbf{x} = \text{state vector}(n\text{-vector})
                         y = \text{output signal (scalar)}
                        u = \text{control signal (scalar)}
                        \mathbf{A} = n \times n constant matrix
                        \mathbf{R} = n \times 1 constant matrix
                        \mathbf{C} = 1 \times n constant matrix
                        D = constant (scalar)
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Control signal: $u = -\mathbf{K}\mathbf{x}$ where, $\mathbf{K} = 1$ x n matrix This means u is determined from instantaneous state.

Block Diagram



- This scheme is called state feedback and **K** matrix is called state feedback gain matrix.
- Non-zero output will be returned to zero reference input because of the state feedback scheme

Closed loop system

- System State equation: $\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$
- State feedback Control: u = -Kx
- Closed loop system: $\dot{\mathbf{x}}(t) = (\mathbf{A} \mathbf{B}\mathbf{K})\mathbf{x}(t)$
- Solution is: $\mathbf{x}(t) = e^{(\mathbf{A} \mathbf{B}\mathbf{K})t}\mathbf{x}(0)$

Where $\mathbf{X}(0)$ is the initial state

- eigenvalues of **A-BK** are called regulator poles
- Placement of regulator poles in left half of s-plane ensure
 x(t) approaches 0 as t tending to ∞
- Problem of placing regulator poles at desired location is called Pole Placement Problem

Arbitrary pole placement of a given system is possible if and only if the system is completely state controllable

Proof:

Suppose the system is not fully state controllable i.e,

rank [**P**] = rank [**B** | **AB** | ... |
$$A^{n-1}B$$
] = $q < n$

Let us write

$$P = [f_1 | f_2 | ... | f_q | v_{q+1} | v_{q+2} | ... | v_n]$$
 of rank n.

Where $\mathbf{f_i}$ (i = 1,q) are q linearly independent column vectors and $\mathbf{v_j}$ (j = q+1, n) are n-q additional chosen vectors to make rank [**P**] = n.

• By using **P** as transformation matrix for A and B,

•
$$\mathbf{A} \mathbf{P} = \mathbf{P} \hat{\mathbf{A}}$$
 or $[\mathbf{A} \mathbf{f}_1 \mid \mathbf{A} \mathbf{f}_2 \mid \cdots \mid \mathbf{A} \mathbf{f}_q \mid \mathbf{A} \mathbf{v}_{q+1} \mid \cdots \mid \mathbf{A} \mathbf{v}_n]$
= $[\mathbf{f}_1 \mid \mathbf{f}_2 \mid \cdots \mid \mathbf{f}_q \mid \mathbf{v}_{q+1} \mid \cdots \mid \mathbf{v}_n] \hat{\mathbf{A}}$

• Using Cauly-Hamilton's theorem to express Af_1 , Af_2 , ... Af_q

$$\mathbf{Af}_{1} = a_{11} \mathbf{f}_{1} + a_{21} \mathbf{f}_{2} + \dots + a_{q1} \mathbf{f}_{q}
\mathbf{Af}_{2} = a_{12} \mathbf{f}_{1} + a_{22} \mathbf{f}_{2} + \dots + a_{q2} \mathbf{f}_{q}
\cdot
\cdot
\mathbf{Af}_{q} = a_{1q} \mathbf{f}_{1} + a_{2q} \mathbf{f}_{2} + \dots + a_{qq} \mathbf{f}_{q}$$

• Hence,

$$[\mathbf{Af}_{1} \mid \mathbf{Af}_{2} \mid \cdots \mid \mathbf{Af}_{q} \mid \mathbf{Av}_{q+1} \mid \cdots \mid \mathbf{Av}_{n}]$$

$$= [\mathbf{f}_{1} \mid \mathbf{f}_{2} \mid \cdots \mid \mathbf{f}_{q} \mid \mathbf{v}_{q+1} \mid \cdots \mid \mathbf{v}_{n}]$$

$$= \begin{bmatrix} \mathbf{a}_{11} & \cdots & a_{1q} & a_{1q+1} & \cdots & a_{1n} \\ a_{21} & \cdots & a_{2q} & a_{2q+1} & \cdots & a_{2n} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ a_{q1} & \cdots & a_{qq} & a_{qq+1} & \cdots & a_{qn} \end{bmatrix}$$

$$0 & \cdots & 0 & a_{q+1q+1} & \cdots & a_{q+1n} \\ \vdots & \vdots & \ddots & \vdots & \ddots & \vdots \\ 0 & \cdots & 0 & a_{nq+1} & \cdots & a_{nn} \end{bmatrix}$$

• Hence,

$$\begin{bmatrix} \mathbf{A}\mathbf{f}_1 & \mathbf{A}\mathbf{f}_2 & \cdots & \mathbf{A}\mathbf{f}_q & \mathbf{A}\mathbf{v}_{q+1} & \cdots & \mathbf{A}\mathbf{v}_n \end{bmatrix}$$

$$= \begin{bmatrix} \mathbf{f}_1 & \mathbf{f}_2 & \cdots & \mathbf{f}_q & \mathbf{v}_{q+1} & \cdots & \mathbf{v}_n \end{bmatrix} \begin{bmatrix} \mathbf{A}_{11} & \mathbf{A}_{12} \\ \mathbf{0} & \mathbf{A}_{22} \end{bmatrix}$$

• Thus,
$$\mathbf{AP} = \mathbf{P} \begin{bmatrix} \mathbf{A}_{11} & \mathbf{A}_{12} \\ \hline \mathbf{0} & \mathbf{A}_{22} \end{bmatrix}$$

$$\mathbf{P}^{-1}\mathbf{A}\mathbf{P} = \hat{\mathbf{A}} = \begin{bmatrix} \mathbf{A}_{11} & \mathbf{A}_{12} \\ \mathbf{0} & \mathbf{A}_{22} \end{bmatrix}$$

• Similarly, $\mathbf{B} = \mathbf{P}\mathbf{\hat{B}}$

$$\mathbf{B} = \begin{bmatrix} \mathbf{f}_1 & \mathbf{f}_2 & \cdots & \mathbf{f}_q & \mathbf{v}_{q+1} & \cdots & \mathbf{v}_n \end{bmatrix} \hat{\mathbf{B}}$$

• So,

$$b_{11}\mathbf{f}_{1} + b_{21}\mathbf{f}_{2} + \dots + b_{q1}\mathbf{f}_{q} = \begin{bmatrix} \mathbf{f}_{1} \mid \mathbf{f}_{2} \mid \dots \mid \mathbf{f}_{q} \mid \mathbf{v}_{q+1} \mid \dots \mid \mathbf{v}_{n} \end{bmatrix} \begin{bmatrix} \cdot \\ \cdot \\ \cdot \\ b_{q1} \\ 0 \\ \cdot \end{bmatrix}$$

Where **B** can be written in terms of independent q column vectors

$$\mathbf{B} = b_{11} \, \mathbf{f}_1 + b_{21} \, \mathbf{f}_2 + \dots + b_{q1} \, \mathbf{f}_q$$

$$\hat{\mathbf{B}} = \left[\frac{\mathbf{B}_{11}}{\mathbf{0}} \right]$$

- Now define, $\hat{\mathbf{K}} = \mathbf{KP} = \begin{bmatrix} \mathbf{k}_1 & \mathbf{k}_2 \end{bmatrix}$
- Then we have,

$$|s\mathbf{I} - \mathbf{A} + \mathbf{B}\mathbf{K}| = |\mathbf{P}^{-1}(s\mathbf{I} - \mathbf{A} + \mathbf{B}\mathbf{K})\mathbf{P}|$$

$$= |s\mathbf{I} - \mathbf{P}^{-1}\mathbf{A}\mathbf{P} + \mathbf{P}^{-1}\mathbf{B}\mathbf{K}\mathbf{P}|$$

$$= |s\mathbf{I} - \hat{\mathbf{A}} + \hat{\mathbf{B}}\hat{\mathbf{K}}|$$

$$= |s\mathbf{I} - \left[\frac{\mathbf{A}_{11} | \mathbf{A}_{12}}{\mathbf{0} | \mathbf{A}_{22}}\right] + \left[\frac{\mathbf{B}_{11}}{\mathbf{0}}\right] [\mathbf{k}_1 | \mathbf{k}_2]$$

$$= |s\mathbf{I}_q - \mathbf{A}_{11} + \mathbf{B}_{11}\mathbf{k}_1 - \mathbf{A}_{12} + \mathbf{B}_{11}\mathbf{k}_2|$$

$$= |s\mathbf{I}_q - \mathbf{A}_{11} + \mathbf{B}_{11}\mathbf{k}_1| \cdot |s\mathbf{I}_{n-q} - \mathbf{A}_{22}| = 0$$

• Notice that the eigenvalues of A_{22} do not depend on K. Thus if the system is not completely state controllable, then there are eigenvalues of A that cannot be arbitrarily placed.