ASSIGNMENT-2 F.M. 50

1 Mark

15 Marks

(0)  $G(S) = \frac{10}{S(S+5)} \Rightarrow G(S) = 2 \cdot \frac{1}{S} \cdot \frac{1}{0.2S+1}$ 

Amplitude ratio, AR = ARI: ARZ. ARZ

AR = 2. 1 . 1 . 1 . 1 . 1

 $\log AR = \log_2 + \log_3(\frac{1}{w}) + \log_3(\frac{1}{\sqrt{(0.2w)^2+1}})$   $\log AR = \log_2 - \log_3w - \frac{1}{2}\log_3\left[(0.2w)^2+1\right]$ 

Low frequency asymptote:  $\omega \rightarrow 0 \Rightarrow 0.2 \omega \rightarrow 0$ 

from O, [log AR = log 2 - log w] - (2) Slope = -1.

High frequency asymptote:

 $W \to \infty \rightarrow 0.2W \to \infty$ . from O, log AR = log 2 - log w - log [0.2 w]

log AR = 1-2 log w \_ 3

Slope =-2.

Corner frequency: Equating @ with 3

log 2 - log wr = 1 - 2 log wr

>> Wn = 5

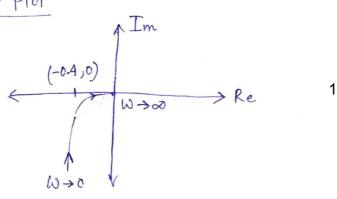
At Wh, AR = 0.4.

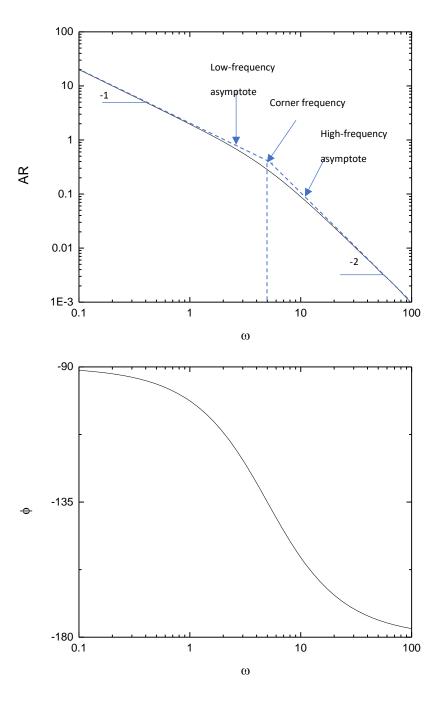
Phan Shift, P= \$1+\$2+\$3

\$ = 0+fan-1(-0) + fan-1(-0.2 w) \$ \$ = -90° + tan - (-0.2 w)

 $\omega \rightarrow 0 \Rightarrow 0.2\omega \rightarrow 0 \Rightarrow \phi \rightarrow -90$ W→N > 0.2W→N > p → -180

Nyquist Plot





1

 $G(S) = \frac{S+1}{S(S+5)} = \frac{0.2}{S(S+1)} \cdot \frac{1}{S(S+1)} \cdot \frac{1}{S(S+1)}$ Amplitude ratio, AR = AR1. AR2. AR3. AR4 AR = 0.2. \ \w^2+1. \ \w \ \ \(\sqrt{(0.2\omega)^2+1} log AR = log 0.2 + 1 log (w2+1) - log w - 1 log [0.20] We identify three regions on the frequency scale based on the cooker frequency of the constituent transfer functions. Vs Wolfagram Slope of the overall asymptote for the AR Slope of the Slope of the asymptotes of the individual framferfn. Frequency asymptote region 3 0.2 0.25 + 1 -1 0 05 W 51 0 1 15 W < 5 0 -1 0 5 5 W 4 00 Phan shift, \$= \$1 + \$2 + \$3 + \$4. \$ = 0 + tan-1(w) + tan-1(-0.2 iv) \$ = -90° + fam-1 (w) + tam-1 (-0.2w) W >0 > \$ > -90' W→8, > 0 -90' For finding omax: dø = 0 => 1 - 0.2 dw = 1+w2 - 1+0.04w2 Amax = A/w=vs = -48.2° Bode Plot Approximate plot using only the slopes of the asymptotes. 1

(c) 
$$G_1(s) = \frac{50}{(s+2)^2} = \frac{50 \cdot 1}{(s+2)} \cdot \frac{1}{(s+2)}$$
  
=  $\frac{12.5 \cdot 1}{(0.5.5+1)} \cdot \frac{1}{(0.5.5+1)}$ 

Amplitude ratio, 
$$AR = AR_1 \cdot AR_2 \cdot AR_3$$

$$AR = 12.5 \cdot \frac{1}{\sqrt{(0.5 \, \text{W})^2 + 1}} \cdot \frac{1}{\sqrt{(0.5 \, \text{W})^2 + 1}}$$

Low frequency asymptote

High frequency asymptote.

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Corner frequency:

from ② and ③

$$log 12.5 = log 12.5 - 2 log (0.5 w)$$
 $log 0.5 wn = 1 >> wn = 2$ .

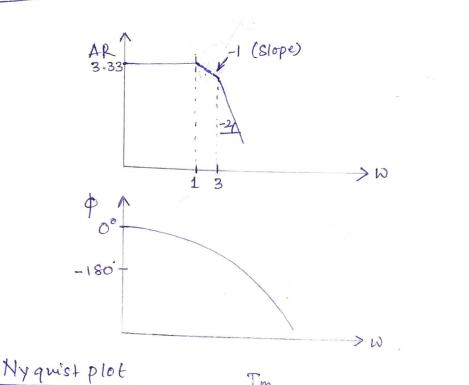
AR | Wn=2 = 12.5

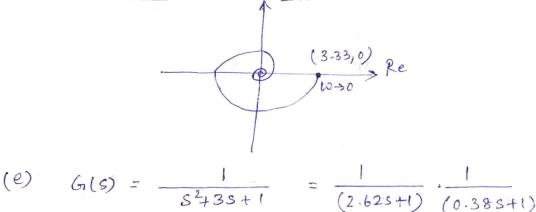
Phan Shift 
$$\phi = \phi_1 + \phi_2 + \phi_3$$
  
 $\phi = 0 + \tan^{-1}(-0.5 \text{W}) + \tan^{-1}(-0.5 \text{W})$ 

$$N \rightarrow 0 \rightarrow 0$$
 $N \rightarrow 0 \rightarrow -180$ 

Bode plot Nyquist plot  $6n(s) = \frac{10e^{-S}}{(S+1)(S+3)}$ (d) Amplifude ratio, AR = AR1. AR2. AR3. AR4  $AR = 3.33 \cdot \frac{1}{\sqrt{W^2+1}} \cdot \frac{1}{\sqrt{(0.33W)^2+1}}$ log AR = log 3.33 - 1 log [w2+1] - 1 log [(0.3320]+1]+0 We identify three regions on the frequency scale based on corner frequency of the constituent transfer functions Slope of the overall asymptote for the AR VS Wodiagram Slope of tere Slope of the asymptote of the individual transfer on overall asymptote. Frequency region 0.335+1 3.33 0 0 0 06 W < 1 0 -1 0 -1 15 W < 3 0 -2. -1 0 34640 Phase shift,  $\phi = \phi_1 + \phi_2 + \phi_3 + \phi_4$ Φ= 0 + fan-1(-ω) + fan-1 (-0.33 ω) -1 × 180° × ω tan-1 (-w) + tan-1 (-0.33w) - 57.32° xw

## Bode Plot





1

1

S435+1 (2.625+1) (0.385+ Amplifude vatio, AR = AR, AR2.

log AR = - 1 log [ (2-62 W)2+1] - 1 log [ (0.38 W)2+1]

we identify three regions on the frequency scale based on their corner frequencies.

Slope of the	overall asymp	tote for the AR	VS W diagram.
Frequency	Slope of asympto	ofe of individual er function	Slope of the overall anywork
	2.625+1	0.385+1	
04 W 60.38	0	0	O
0.38 5 W 6 2.	62 -	-1	-2.
2.62 5 W C	∞ -1		

Phase Shiff, 
$$\phi = \phi_1 + \phi_2$$
 $\phi = + \tan^{-1}(-0.38\omega) + \tan^{-1}(-2.62\omega)$ 
 $\omega \Rightarrow 0 \Rightarrow \phi = -180^{\circ}$ 

Bode Plot

AR

Nyquist Plot

Nyq

2.

Low frequency asymptote: 10 → 0 ⇒ log AR = 0 = 0 AR=1 ; slope = 0. High frequency asymptote War a logAR = - logW Corner frequency: from @ and 3 -log w= 0 = Wn=1. AR | Wn=1 = 1 = 0.707. Phase shift Φ = tan-1(w) - x x 180° w→0 >> \$ -180° ロコスカカ >-900  $W \rightarrow W_{n}=1 \quad \phi \rightarrow -135$ Bode Plots. Weo > Cross over frequency: Frequency when the phase lag is 180 AR | we = 1 = The system lies on the Stability limit Bode criterion leads to rigorous conclusions only when AR and of the corresponding open loop transfer functions durease continuously as wincrease. As phan shift (4) is not a monotonically deceasing

As phan shift (\$) is not a monotonically dura function of w, Bode Stability criterion may lead to errollous conclusions.

AP | we = 1 1 ... The System dies on the Stability limit

0.5

3. (a) Gol = 
$$\frac{1}{S-1}$$

From problem 2(a)

Af | we = 1 = M

Grain Margin =  $\frac{1}{M} = 1$ 

Phase Margin =  $\frac{1}{80}$  -  $\frac{1}{9}$  |

 $\frac{1}{9}$  | phase lag at the frequency for which AR = 1.

AR = 1 at  $W = Wco$ 

Phase Nargin =  $0^{\circ}$  -  $0$  1

From 0 and 0

The system lies on the stability limit 0.5

(b)  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |

Grain Margin =  $\frac{1}{M} = \frac{1}{3.59}$  |

 $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac{1}{9}$  |  $\frac$ 

(c) 
$$C_{101} = \frac{5e^{-55}}{(25+1)(5+1)}$$

From problem 2(c)

AR | we = 3.57 = M

Gain Margin :  $\frac{1}{1} = \frac{1}{3.57}$ 

Gain Margin (1. — ①

AR =  $\frac{5}{\sqrt{910^{4}+1}}\sqrt{10^{4}+1} = 40^{4}+40^{2}+10^{4}+1$ 
 $\Rightarrow 25 = (40^{4}+1)(10^{4}+1) = 40^{4}+40^{2}+10^{4}+1$ 
 $\Rightarrow 40^{4}+50^{2}-24=0$ 
 $\Rightarrow 1.38 \text{ rad/min}$ 

AR =  $\frac{1}{100} = 1.38 \text{ rad/min}$ 

AR =  $\frac{1}{100} = 1.38 \text{ rad/min}$ 
 $= -519.5$ 

Phase margin =  $\frac{1}{100} = 1.38 \text{ rad/min}$ 

From ① and ②

The system is unstable . 0.5

(d)  $G_{01} = \frac{1}{0.25^{2}+0.85-1}$ 

From problem 2(d)

AP | we =  $\frac{1}{100} = \frac{1}{100}$ 

Gain Margin =  $\frac{1}{100} = \frac{1}{100}$ 

AR =  $\frac{1}{100} = \frac{1}{100}$ 

Phase margin = 0 1

From ① and ②

The system lies on Stability limit 0.5

GoL = 
$$\frac{1}{s-1}$$
  
From problem 2(a)  
 $AR = \frac{1}{\sqrt{1+\omega^2}}$   
 $\phi = +on^{-1}(\omega) - \pi \times 180'$   
 $A+\omega = 0$ ,  $AR = 1$ ,  $\phi = -180'$   
 $A+\omega \Rightarrow \infty$ ,  $AR \Rightarrow 0$ ,  $\phi \Rightarrow -90'$   
 $A+\omega \Rightarrow -\infty$ ,  $AR \Rightarrow 0$ ,  $\phi \Rightarrow -270'$ 

1

0.5

1

The point (-1,0) lies on the Nyquist plot. The system is on Stability limit

(-1,0) W>00

(b)

The system is on Stability limit

Got = 
$$\frac{10e^{-S}}{4S+1}$$

From problem 2(b)

 $AR = \frac{10}{\sqrt{(4w)^2+1}}$   $\phi = \frac{10}{\sqrt{(4w)^2+1}}$   $A = \frac{10}{\sqrt{(-4w)}} - \frac{3w \cdot 180}{\sqrt{x}}$   $A = \frac{10}{\sqrt{x}}$   $AR = \frac{10}{\sqrt{x}}$   $AR = \frac{10}{\sqrt{x}}$   $AR = \frac{10}{\sqrt{x}}$   $AR = \frac{10}{\sqrt{x}}$ 

At 
$$\phi = -180^{\circ}$$
,  $W = ? \Rightarrow W = W = 0$   
 $+ am^{-1} (-4W) - 3W \cdot \frac{180}{\pi} = -180$   
 $W = 0.65$   
At  $W = W = 0.65$   
 $W = 0.65$ ,  $AR = 3.59$ ,  $\phi = -180^{\circ} = 3$   
 $W \rightarrow -\infty$   $AR \rightarrow 0$ ,  $\phi \rightarrow \infty$   $Q$ 

(d) GoL = 
$$\frac{1}{0.2s_{+}^{2}0.8s_{-1}}$$
  
from problem 2(c),  
AR =  $\sqrt{(-1-0.2w_{-}^{2})^{2}+(0.8w_{-}^{2})^{2}}$   
 $\phi = -\pi + \tan^{-1}\left(\frac{0.8w_{-}^{2}}{1+0.2w_{-}^{2}}\right)$ 

At 
$$W=0$$
,  $AR=1$ ,  $\phi=-180^{\circ}$ 
 $W\to\infty$ ,  $AR\to0$ ,  $\phi\to-180$ 
 $W\to-\infty$ ,  $AR\to0$ ,  $\phi\to-180$ 

Im

$$W=0$$
 $(-1,0)$ 
 $W\to\infty$ 

$$(-1,0)$$
 $W\to\infty$ 

$$(-1,0)$$

$$(-1,0)$$
 $W\to\infty$ 

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5 Marks

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