

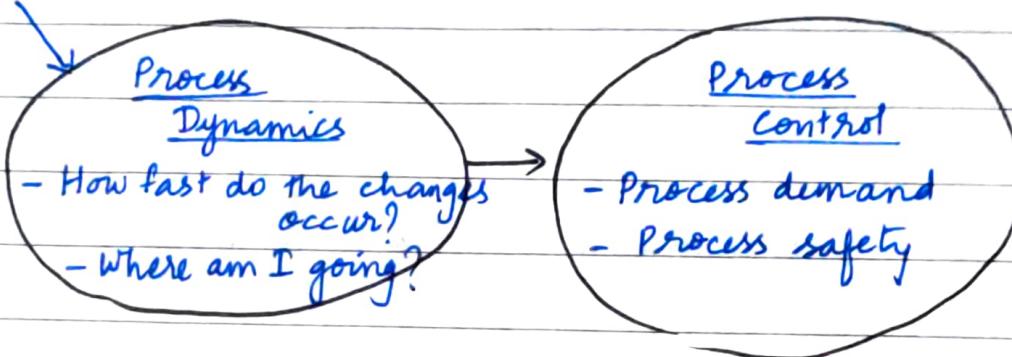
- References:
1. Bacquette
  2. Oggunaike
  3. Stephanopoulos

PAD

08.01.21

## Process Dynamics (and Control)

Process Modeling  
Math. eqs. and assumptions



Bosch Haber process: Synthesis of  $\text{NH}_3$  from  $\text{N}_2$  and  $\text{H}_2$

$\sim 500 \text{ bar}, 650^\circ\text{C} + \text{catalyst} \rightarrow \text{process demand}$

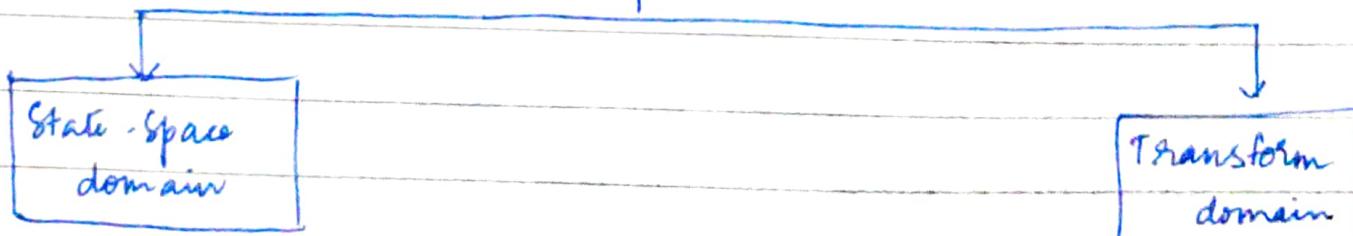
The importance of process dynamics is to identify the extremities of the system.

For example, in the above case, the two extremes are -

1. T and P fall -  $T = 27^\circ\text{C}$ ,  $P = 1 \text{ atm}$  → against process demand
2. Reactor blows up → against process safety

We won't focus on modeling. Model eqs. will be provided.

### Process Dynamics



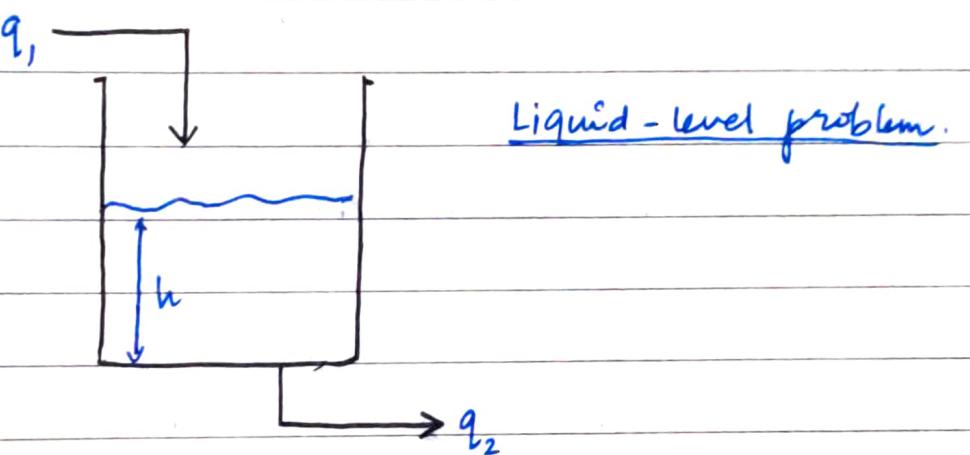
Tells everything that can happen in the system - all extremities.

B/w two states - how to reach a state from another.

CLASSMATE

We always start from the state-space domain to understand the possibilities and then move to transform domain to reach goals.

Dynamical System - Has at least one variable which varies in time.



Consider a tank

$q_1, q_2 \rightarrow$  volumetric flow rates

$h \rightarrow$  level of liq.

$A \rightarrow$  const. cross-section area.

Mass Conservation -

Input - output = Accumulation + Time rate of change (+/-) generation.

$$q_1 - q_2 = A \frac{dh}{dt}$$

$$\Rightarrow \frac{dh}{dt} = \frac{q_1 - q_2}{A} \rightarrow \text{model eq.}$$

Here, the dynamical variable is  $h$ .

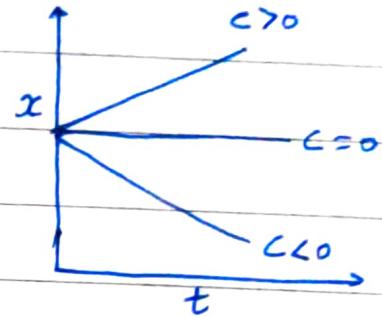
## State - space representation of a dynamical system

Case 1:  $q_1 = \text{constant} = c_1$ ,

$q_2 = \text{constant} = c_2$

$$\therefore \frac{dx}{dt} = \frac{c_1 - c_2}{A} = \text{constant} = c, \text{ where } x = h(t)$$

Consider 3 cases.  
 $c > 0; c = 0, c < 0$



What happens as  $t \rightarrow \infty$ ? - Depends on  $c$ .

Case 2:  $q_2 = f(h) \rightarrow \text{gravity driven flow}$

$q_1 = \text{constant} = c$

$$\frac{dx}{dt} = \frac{c - f(h)}{A}$$

$$\Rightarrow \frac{dx}{dt} + \frac{1}{A} f(h) = \frac{c}{A} \rightarrow \text{can be solved using I.F.}$$

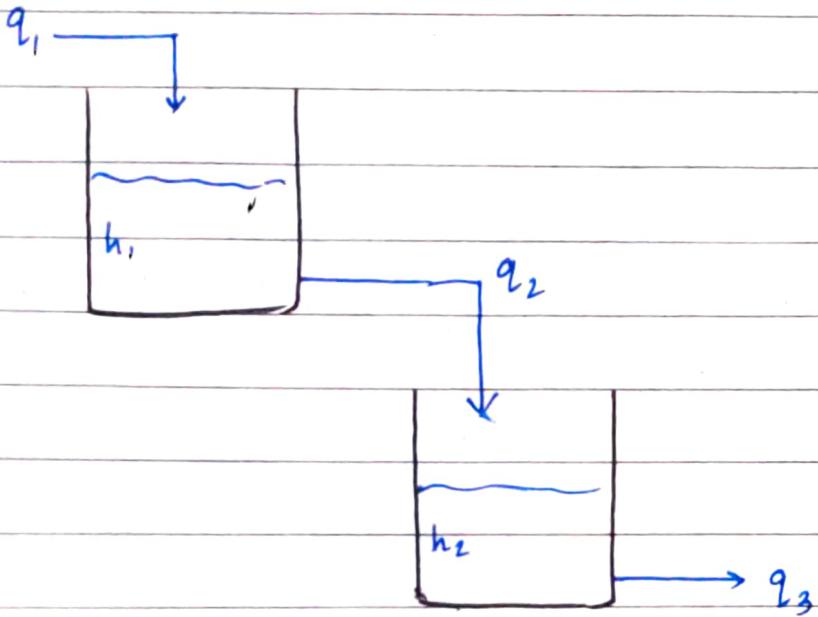
Case 3:  $q_2 = g(h) \rightarrow q_2 \text{ altered by placing a valve}$

$q_1 = f(t) \rightarrow q_1 \text{ altered as function of time by placing a pump.}$

$$\frac{dx}{dt} = \frac{-g(x) + f(t)}{A}$$

$$\frac{dx}{dt} + \frac{g(x)}{A} = \frac{f(t)}{A}$$

Now, let's complicate it more.



Here, there are 2 dynamical variables  $h_1$  and  $h_2$ .

The state of the system is described by a "vector": state vector

$$[h_1 \ h_2]^T$$

hence, State space domain

$$A_1 \frac{dh_1}{dt} = q_1 - q_2 \quad ; \quad A_2 \frac{dh_2}{dt} = q_2 - q_3$$

Cases:

1.  $q_1, q_2, q_3 \rightarrow \text{const.}$

2.  $q_1 = f(t)$ ,  $q_2 = f(h_1)$ ,  $q_3 = f(h_2)$

3.  $q_1 = f(h_1)$ ,  $q_2 = f(h_1, h_2)$ ,  $q_3 = f(h_2)$

What is the "order" of the two-tank liquid level system?

$$\frac{dh_1}{dt} = \frac{q_1 - q_2}{A} ; \quad \frac{dh_2}{dt} = \frac{q_2 - q_3}{A}$$

Order of a system is equal to the number of 1<sup>st</sup> order ODEs used to model the system.

$$a_2 \frac{d^2x}{dt^2} + a_1 \frac{dx}{dt} + a_0 x = b \rightarrow \text{II order.}$$

$$\text{Let } \frac{dx}{dt} = y \Rightarrow a_2 \frac{dy}{dt} + a_1 y + a_0 x = b$$

Hence,

$$\left\{ \begin{array}{l} \frac{dy}{dt} = \frac{b}{a_2} - \frac{a_0}{a_2} x - \frac{a_1}{a_2} y \quad \text{and} \\ \frac{dx}{dt} = y \end{array} \right. \rightarrow \text{I order.}$$

Together, a II order system.

So, a general n<sup>th</sup> order system is represented as-

$$\left. \begin{array}{l} \frac{dx_1}{dt} = a_{11}x_1 + a_{12}x_2 + \dots + a_{1n}x_n \\ \frac{dx_2}{dt} = a_{21}x_1 + a_{22}x_2 + \dots + a_{2n}x_n \\ \vdots \\ \frac{dx_N}{dt} = a_{N1}x_1 + a_{N2}x_2 + \dots + a_{NN}x_N \end{array} \right\} \text{N 1}^{\text{st}} \text{ order systems.}$$

This is equivalent to,

$$\frac{d}{dx} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_N \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} & \cdots & a_{1N} \\ \vdots & \ddots & & \vdots \\ \vdots & & \ddots & \vdots \\ a_{N1} & \cdots & a_{NN} & \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_N \end{bmatrix}$$

Eigen value problem

state vector  
whose variation with  
time is of interest.

Example:

Consider a fluid reservoir at  $T = T_\infty$ , in which an object of temperature  $T_0$  is immersed at  $t=0$ . The time rate of change of temp. of object is governed by Newton's law of cooling, according to which rate of change of temp of a body is proportional to the diff. in temp of the body and the surroundings. Hence,

$$\frac{dT}{dt} = -h(T - T_\infty)$$

Determine the equilibrium temperature(s) of the system.

$$\text{Given, } \frac{dT}{dt} = -h(T - T_{\infty})$$

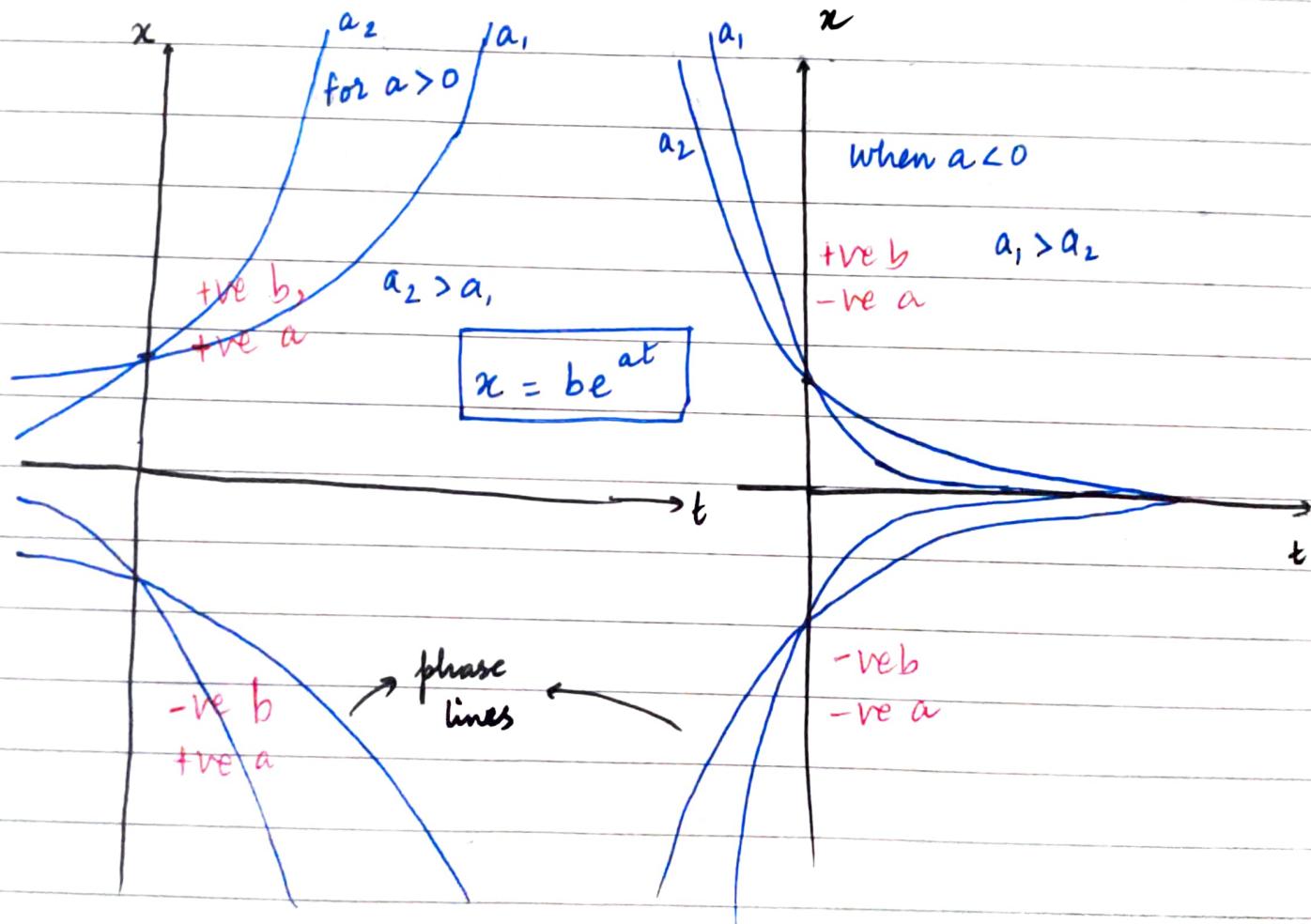
Let us consider the simplest 1<sup>st</sup> order system modelled as -

$$\frac{dx}{dt} = ax$$

$$\Rightarrow x(t) = x(0) \cdot e^{at}$$

Initial condition.

$$\text{Let } x(0) = 1; \text{ then } x(t) = e^{at}$$



Phase portrait. — Collection of solutions of system that represents all possibilities.

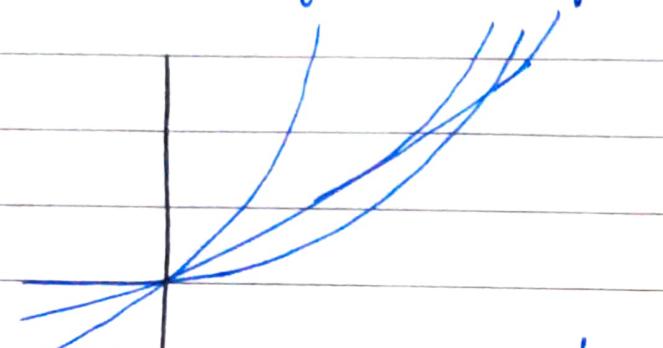
Q: What is the effect of 'a' on the system?

→ Large 'a' means quicker dynamics.

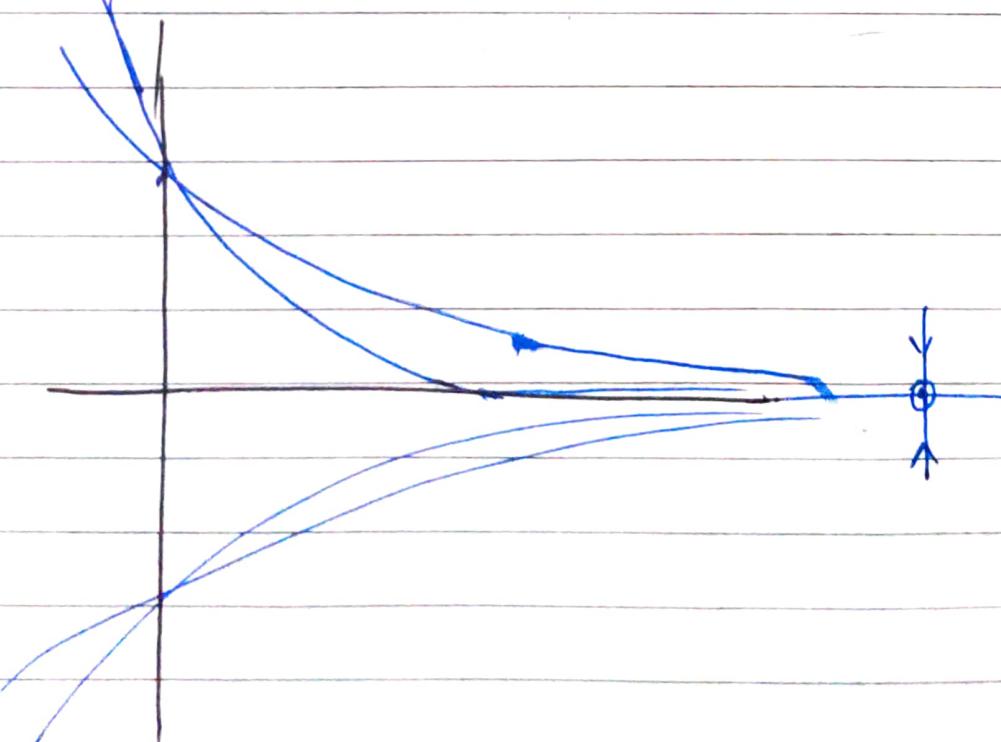
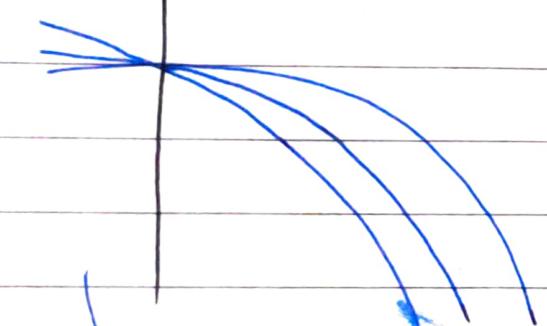
Q: What is the fate of the system? (a) What happens to the system as  $t \rightarrow \infty$ ?

→ If  $a > 0$ ,  $x \rightarrow \infty$ ; If  $a < 0$ ,  $x \rightarrow 0$  irrespective of magnitude of a. classmate P.T.O.

→ splits into 2.  
And, the system has bifurcation at  $a = 0$ .



Solutions diverging from this point. } called  
Source solution



Solutions converging called  
Sink solution.

$$\frac{dT}{dt} = -h(T - T_{\infty})$$

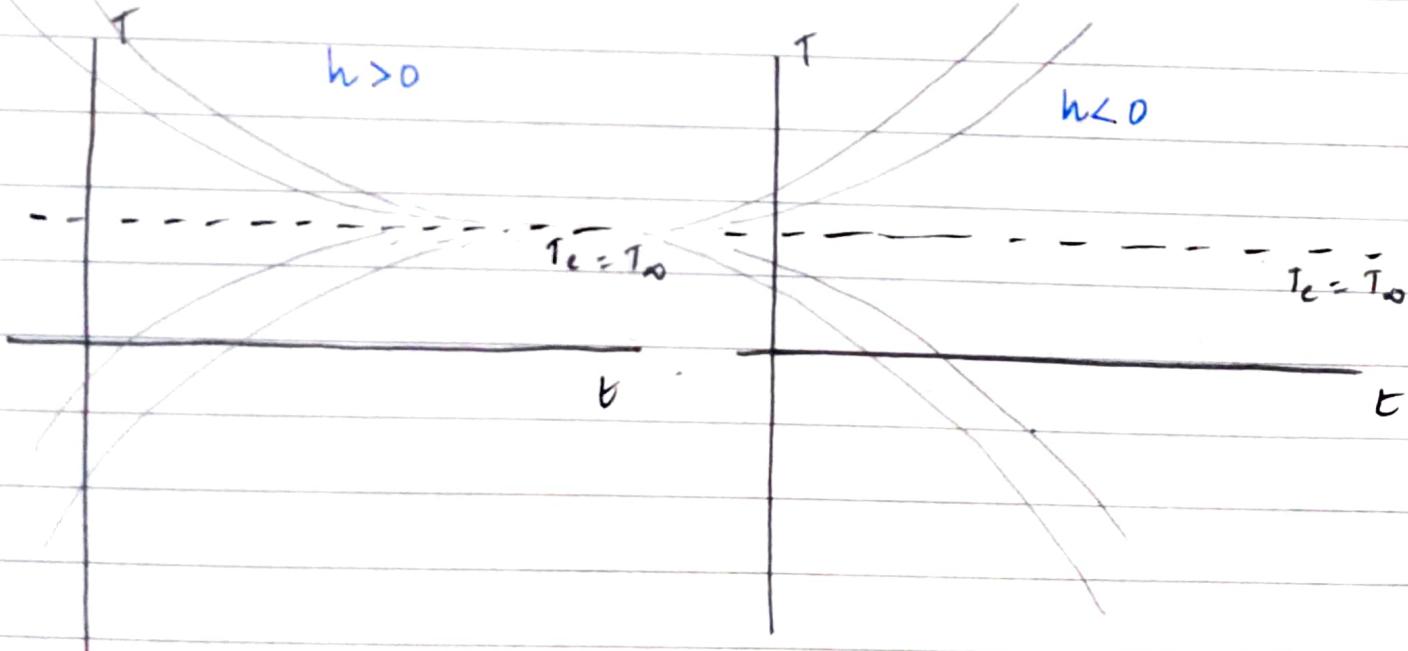
$$\text{Let } T - T_{\infty} = T^*$$

$$\frac{dT^*}{dt} = -hT^*$$

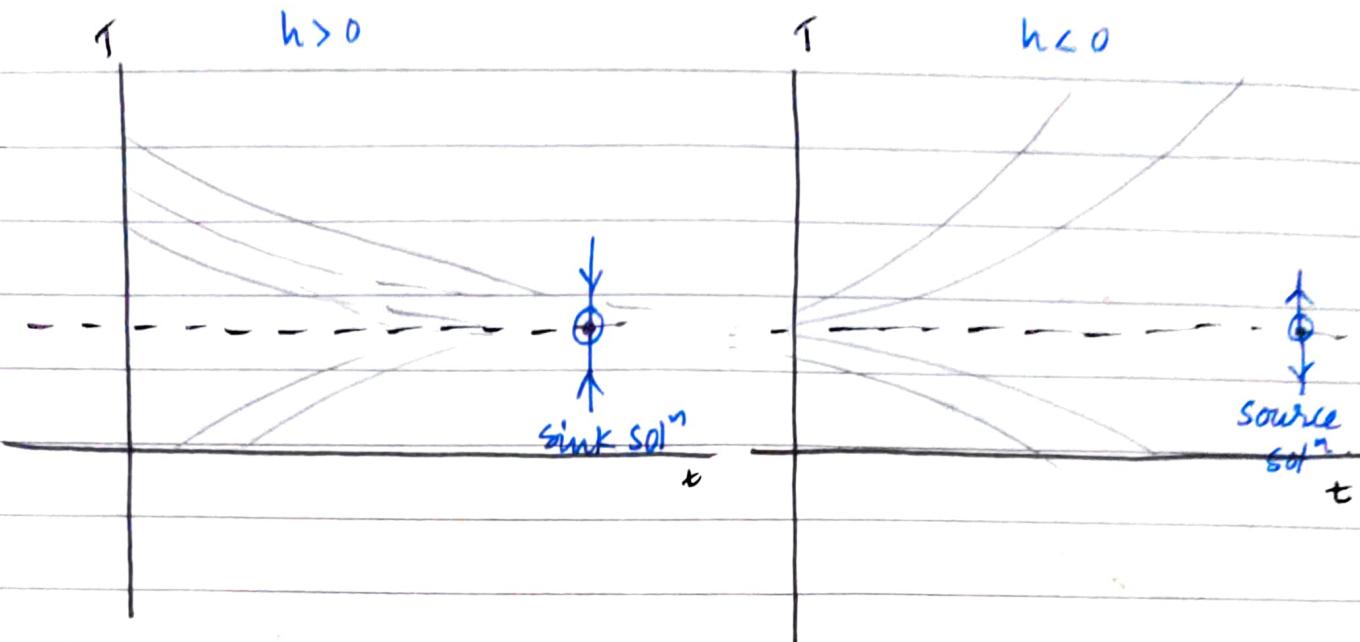
$$T^* = T(0) \cdot e^{-ht}$$

$$T = T_{\infty} + (T_0 - T_{\infty}) e^{-ht} \quad \left| \begin{array}{l} \rightarrow \text{At } t \rightarrow \infty, T = T_{\infty} \rightarrow \text{eq. condition} \\ \downarrow \\ \text{initial condition of } T^* \end{array} \right.$$

Phase portrait for this solution looks like -



How to reach phase portrait without the analytical solution? - PTO



Start from eq. solution.

$$\frac{dT}{dt} = -h(T - T_{\infty}) = 0 \Rightarrow T = T_{\infty} \rightarrow \text{equilibrium sol.}$$

For  $h > 0$

When  $T > T_{\infty}$ ,  $\frac{dT}{dt} < 0$  and when  $T < T_{\infty}$ ,  $\frac{dT}{dt} > 0$

For  $h < 0$ ,

when  $T < T_{\infty}$ ,  $\frac{dT}{dt} < 0$  and when  $T > T_{\infty}$ ,  $\frac{dT}{dt} > 0$ .

Consider a case when reservoir temp. is a function of time ( $T_{\infty} = f(t)$ ). Analyse dynamics of the system for -

- 1) Linear decay ;  $T_{\infty} = a - bt$
- 2) Linear rise ;  $T_{\infty} = a + bt$
- 3) Exponential decay ;  $T_{\infty} = ae^{-bt}$
- 4) Exponential rise ;  $T_{\infty} = ae^{bt}$

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## Dynamics of higher order systems

A governing eq. which is an ODE of  $n^{\text{th}}$  order can be converted to a system of  $n$  1<sup>st</sup> order ODEs.

First order:  $\frac{dx}{dt} = ax$  where,  $x \rightarrow$  dynamical variable  
 $a \rightarrow$  parameter.

$N^{\text{th}}$  order:  $\frac{dx_1}{dt} = a_{11}x_1 + a_{12}x_2 + \dots + a_{1N}x_N$

$$\frac{dx_2}{dt} = a_{21}x_1 + a_{22}x_2 + \dots + a_{2N}x_N$$

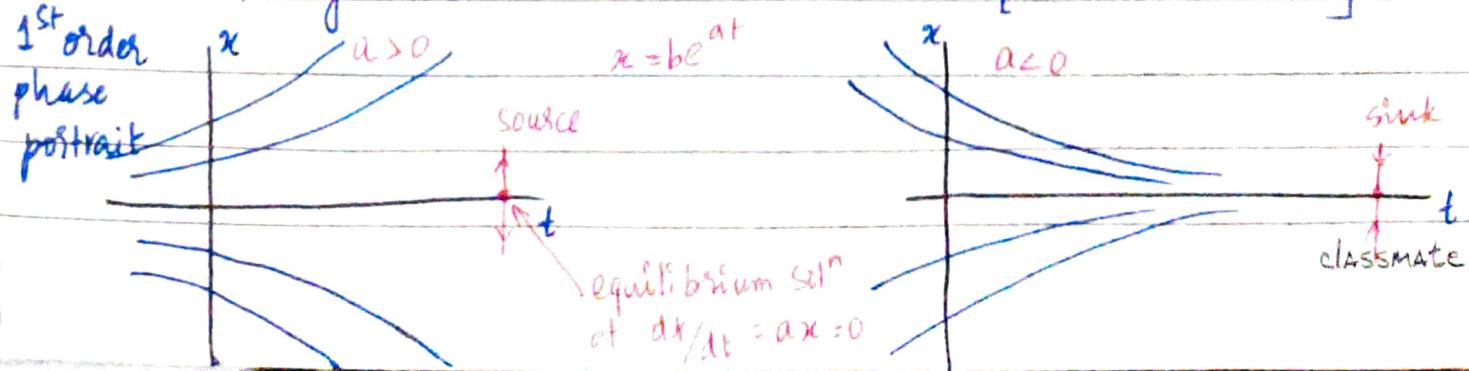
⋮

$$\frac{dx_N}{dt} = a_{N1}x_1 + a_{N2}x_2 + \dots + a_{NN}x_N$$

This dynamical eq. can be represented as a matrix eq. as -

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_N \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} & \dots & a_{1N} \\ a_{21} & \ddots & \dots & a_{2N} \\ \vdots & & \ddots & \vdots \\ a_{N1} & \dots & \dots & a_{NN} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_N \end{bmatrix}$$

Here, dynamical variable is a vector  $\rightarrow [x_1 \ x_2 \ \dots \ x_N]^T$



In 1<sup>st</sup> order systems as shown in the above phase diagram, the fate of the system and its dynamics depended on the value of 'a'.

For an  $n^{\text{th}}$  N<sup>th</sup> order system, the dynamics of the system depend on the  $N \times N$  coefficient matrix, particularly on the eigen values of this matrix.

In  $\frac{dx}{dt} = ax$ ;  $a$  is the eigen value of the differential operator  $d/dx$ , with  $x$  as the eigen function.

What is the solution to the system of equations  $\frac{d}{dt} \underline{x} = \underline{A} \underline{x}$ ?  
 (Eigen value problem)

If  $\lambda_i$ 's are the eigen values of  $\underline{A}$  with corresponding eigen vectors as  $\underline{v}_i$ 's, then the solution is given as

$$\underline{x} = \sum_{i=1}^N c_i e^{\lambda_i t} \underline{v}_i \quad \rightarrow \star$$

Consider a second order system given by -

$$\frac{dx_1}{dt} = a_{11}x_1 + a_{12}x_2 \quad ; \quad \frac{dx_2}{dt} = a_{21}x_1 + a_{22}x_2$$

$\therefore$  Dynamical variable :  $[x_1 \ x_2]^T$

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \quad \underline{A} \quad \underline{x}$$

So, it is req. to analyse the eigen values of  $\underline{A}$

$$\underline{\text{Case I: } A = \begin{bmatrix} a & 0 \\ 0 & b \end{bmatrix}}$$

$$\text{Then } \lambda_1 = a; \lambda_2 = b$$

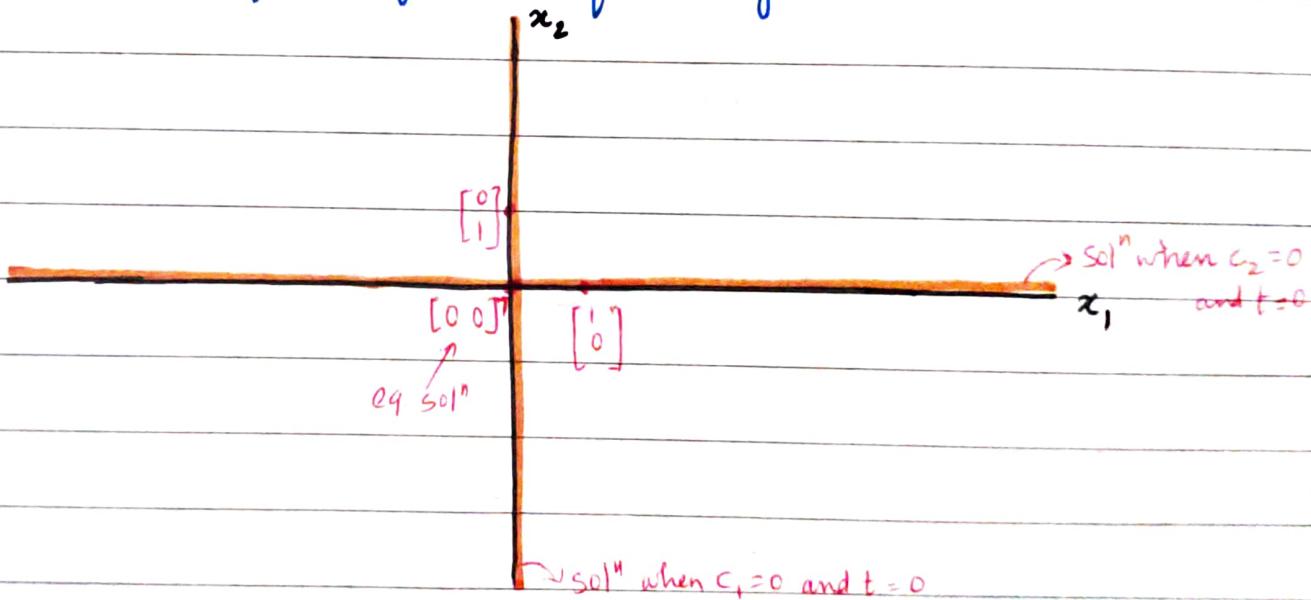
$$V_1 = \begin{bmatrix} 1 \\ 0 \end{bmatrix}; V_2 = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$\left\{ \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = c_1 e^{at} \begin{bmatrix} 1 \\ 0 \end{bmatrix} + c_2 e^{bt} \begin{bmatrix} 0 \\ 1 \end{bmatrix} \right.$$

from eq ①

In this solution, if i)  $c_1=1; c_2=0$  and  $t=0$ ;  $[x_1 x_2]^T = [1 \ 0]^T$   
 ii)  $c_1=0; c_2=1$  and  $t=0$ ;  $[x_1 x_2]^T = [0 \ 1]^T$

Now, the aim is to be able to draw the phase portrait, i.e., determine the fate/dynamics of the system.



The equilibrium solutions are obtained by setting

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = 0 = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

\* That is, equilibrium solutions will lie in the "null space" of  $A$  or

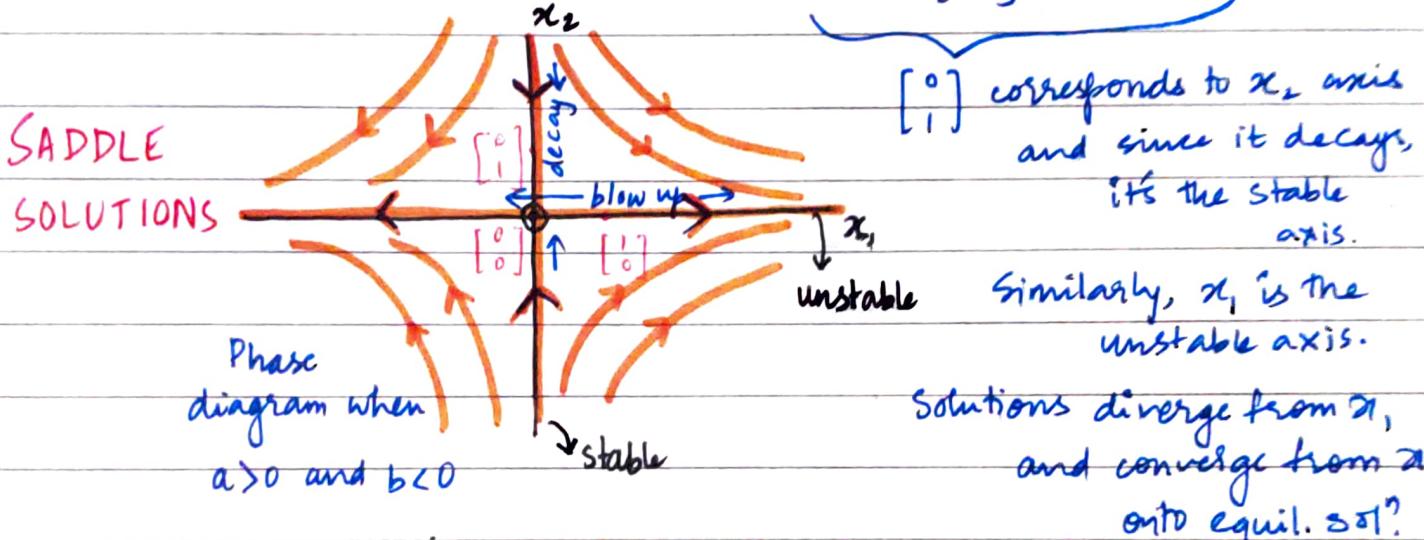
$$A \underline{x} = \underline{0} ; \text{i.e.} ; \begin{bmatrix} a & 0 \\ 0 & b \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \Rightarrow \boxed{\begin{array}{l} x_1 = 0 \\ x_2 = 0 \end{array}}$$

$\therefore [0 \ 0]^T$  is the eq. solution.

We saw that  $\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = c_1 e^{at} \begin{bmatrix} 1 \\ 0 \end{bmatrix} + c_2 e^{bt} \begin{bmatrix} 0 \\ 1 \end{bmatrix}$  is the solution with equilibrium at  $\begin{bmatrix} 0 \\ 0 \end{bmatrix}$ .

case i)  $a > 0, b < 0$

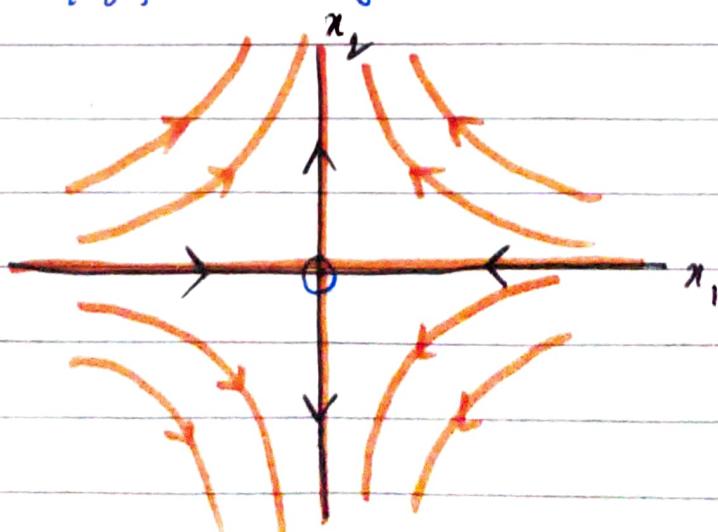
Then  $c_1 e^{at} \begin{bmatrix} 1 \\ 0 \end{bmatrix}$  will blow up and  $c_2 e^{bt} \begin{bmatrix} 0 \\ 1 \end{bmatrix}$  will decay.



This solution <sup>is</sup> called a 'saddle solution'.

case ii)  $a < 0, b > 0$

Then  $c_1 e^{at} \begin{bmatrix} 1 \\ 0 \end{bmatrix}$  will decay ( $x_1 \rightarrow$  stable) and  $c_2 e^{bt} \begin{bmatrix} 0 \\ 1 \end{bmatrix}$  will blow up ( $x_2 \rightarrow$  unstable)

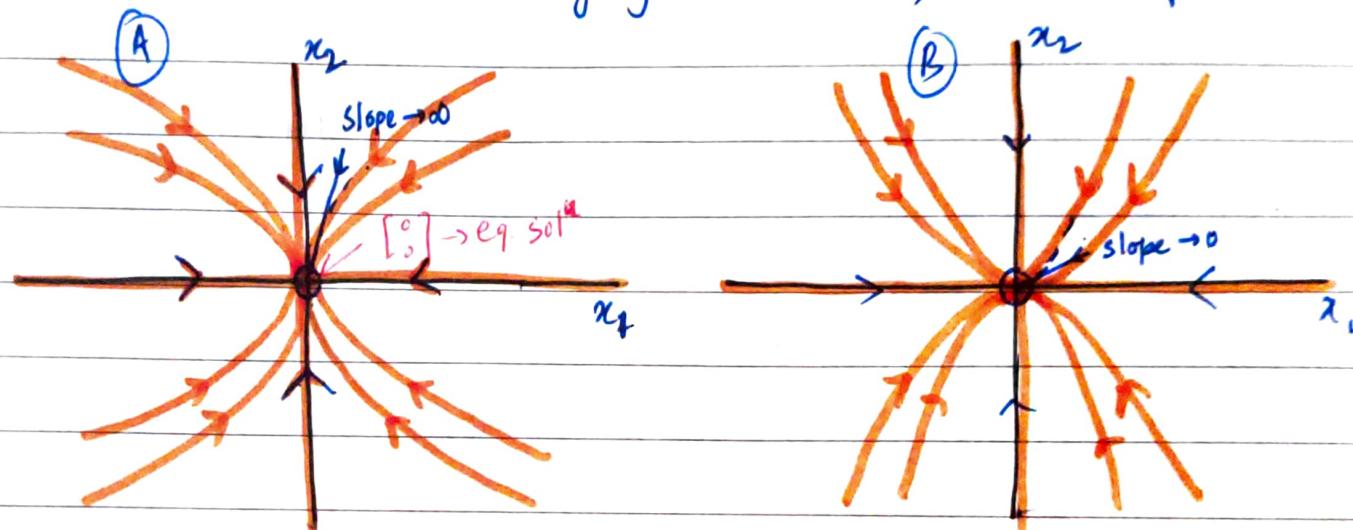


This is also a saddle solutions.

Both case (i) and (ii) lead to unstable solutions as at least one of (a, b) is ' $> 0$ ' and the solution eventually blows up as  $t \rightarrow \infty$ .

Case (iii):  $a < 0, b < 0$

Both  $x_1 e^{at} \begin{bmatrix} 1 \\ 0 \end{bmatrix}$  and  $x_2 e^{bt} \begin{bmatrix} 0 \\ 1 \end{bmatrix}$  will decay. So both axes are stable and both axes are converging. In this case, there are 2 possibilities.



Every solution converges to equilibrium solution, that is  $\begin{bmatrix} 0 \\ 0 \end{bmatrix}$  unlike in the previous cases. But, how do we determine which is the correct phase portrait, A or B? For that, we need to find -

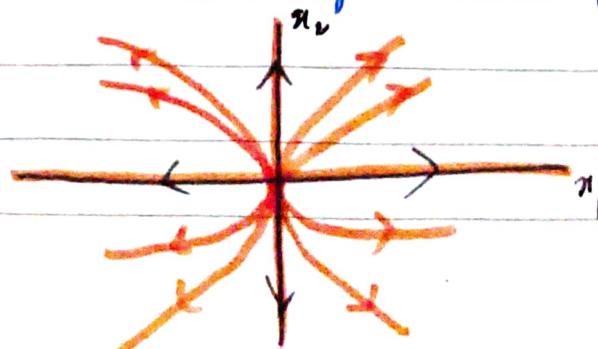
$$x_1 = x_{10} e^{at} \text{ and } x_2 = x_{20} e^{bt}$$

$$\therefore \frac{dx_2}{dx_1} = \frac{x_{20}b}{x_{10}a} \cdot e^{(b-a)t} \quad \left. \begin{array}{l} \text{when } b > a ; \frac{dx_2}{dx_1} \rightarrow \infty \text{ as } t \rightarrow \infty \\ \text{when } b < a ; \frac{dx_2}{dx_1} \rightarrow 0 \text{ as } t \rightarrow \infty \end{array} \right\} \text{ (A)}$$

$$\text{when } b < a ; \frac{dx_2}{dx_1} \rightarrow 0 \text{ as } t \rightarrow \infty \quad \text{(B)}$$

Case (iv):  $a > 0, b > 0$

both axes are unstable. System blows up as  $t \rightarrow \infty$ .



Case II:  $\underline{A} = \begin{bmatrix} 0 & a \\ -a & 0 \end{bmatrix}$

Then  $\lambda_1 = ia$  and  $v_1 = [1 \ i]^T$

$$\therefore \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = e^{iat} \begin{bmatrix} 1 \\ i \end{bmatrix} \quad \text{Put } e^{iat} = \cos at + i \sin at.$$

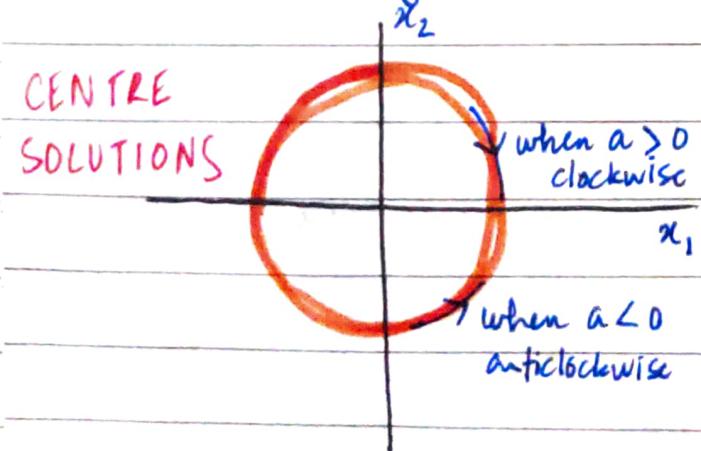
$$\therefore \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} \cos at + i \sin at \\ -\sin at + i \cos at \end{bmatrix} = \begin{bmatrix} \cos at \\ -\sin at \end{bmatrix} + i \begin{bmatrix} \sin at \\ \cos at \end{bmatrix}$$

Real part.      Imaginary part

Therefore,  $\text{Re}$  and  $\text{Im}$  are individually the solutions.

$$\therefore \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = c_1 \begin{bmatrix} \cos at \\ -\sin at \end{bmatrix} + c_2 \begin{bmatrix} \sin at \\ \cos at \end{bmatrix} = \begin{bmatrix} c_1 \cos at + c_2 \sin at \\ -c_1 \sin at + c_2 \cos at \end{bmatrix}$$

Upon plotting  $(c_1 \cos at + c_2 \sin at, -c_1 \sin at + c_2 \cos at)$  on [www.desmos.com](http://www.desmos.com), you'll see that it is a circle, whose radius changes with change in  $c_1$  or  $c_2$ .



The moment you have imaginary eigen values (can happen even for real), your system shows oscillations that are periodic in nature. The combination of  $x_1$  and  $x_2$  will keep on repeating.

The solutions won't decay or blow up. But they'll keep oscillating about the same value. Such solutions are called "center solutions".

Case III:  $A = \begin{bmatrix} a & b \\ -b & a \end{bmatrix}$

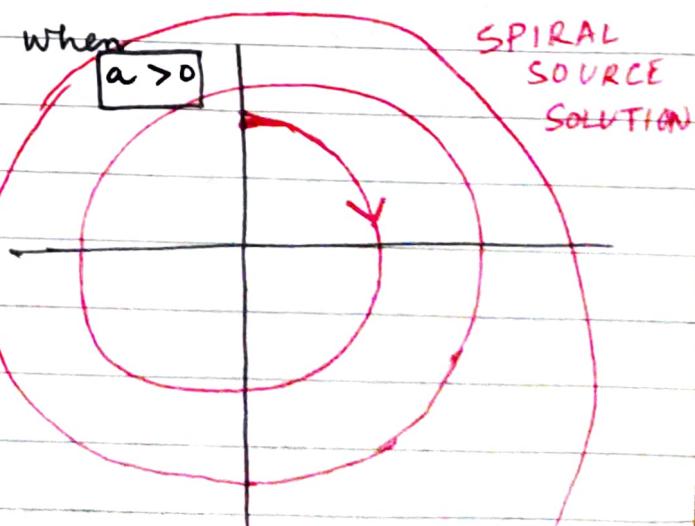
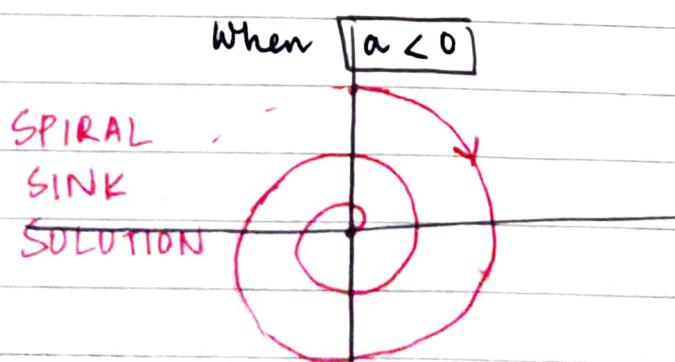
$\lambda_1 = (a+ib)$  and  $v_1 = [1 i]^T$

$$\begin{aligned} \therefore \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} &= e^{(a+ib)t} \begin{bmatrix} 1 \\ i \end{bmatrix} = e^{at} \cdot e^{ibt} \begin{bmatrix} 1 \\ i \end{bmatrix} \\ &= e^{at} \left[ \begin{bmatrix} \cos bt \\ -\sin bt \end{bmatrix} + i \begin{bmatrix} \sin bt \\ \cos bt \end{bmatrix} \right] \\ &\quad \text{Real} \qquad \qquad \qquad \text{Imaginary} \end{aligned}$$

Therefore, Re and Im parts are individually the solns.

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = C_1 e^{at} \begin{bmatrix} \cos bt \\ -\sin bt \end{bmatrix} + C_2 e^{at} \begin{bmatrix} \sin bt \\ \cos bt \end{bmatrix}$$

$$= \begin{bmatrix} e^{at} (C_1 \cos bt + C_2 \sin bt) \\ e^{at} (-C_1 \sin bt + C_2 \cos bt) \end{bmatrix} \rightarrow \text{How does this phase diagram look?}$$



Solutions oscillate but their values could be decaying or blowing up with every oscillation based on the value (sign) of ' $a$ '.

## \* So, conclusions:

- First order systems are monotonous. They either decay ~~to zero~~ or blow up monotonously.

- Higher order systems introduce complexity. HO systems with complexity (imaginary terms) oscillate. Whether the oscillations die out, sustain or blow up depends on the eigen value.

If eigen value is purely imaginary, then oscillations sustain without change in magnitude. If eigen value is complex with real part  $> 0$ , then oscillations blow up. If real part  $< 0$  then oscillations decay.

Example: Consider system of elementary reactions in series -

$A \rightarrow B \rightarrow C$ . The kinetics are given by -

$$\left. \begin{array}{l} \frac{dC_A}{dt} = -k_1 C_A \\ \frac{dC_B}{dt} = k_1 C_A - k_2 C_B \\ \frac{dC_C}{dt} = k_2 C_B \end{array} \right\} \text{III order system}$$

The reactions are carried out in batch reactor with initial cones as  $C_{A0}, C_{B0}, C_{C0}$ .

- a) By sequentially solving the three eqs, determine expressions for the time evolutions of  $C_A, C_B, C_C$  and their concentrations as  $t \rightarrow \infty$

$$\frac{dC_A}{dt} = -k_1 C_A \Rightarrow C_A = C_{A0} e^{-k_1 t}$$

$$\frac{dC_B}{dt} + k_2 C_B = k_1 C_{A0} e^{-k_1 t} \rightarrow \text{solved using I.F. method.}$$

Similarly,  $C_C$  can be found by substituting  $C_B$  into the ODE.

b) Convert the above system of eqs to a matrix equation and solve for the concentrations. Check if the solutions match the ones obtained from (a).

$$\frac{d}{dt} \begin{bmatrix} C_A \\ C_B \\ C_C \end{bmatrix} = \begin{bmatrix} -k_1 & 0 & 0 \\ k_1 & -k_2 & 0 \\ 0 & k_2 & 0 \end{bmatrix} \begin{bmatrix} C_A \\ C_B \\ C_C \end{bmatrix}$$

$$X = \sum_{i=1}^N c_i e^{\lambda_i t} v_i \rightarrow \text{We need to find eigen values \& vectors}$$

Using Wolfram alpha; we get;

$$\lambda_1 = 0 ; \quad v_1 = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix}^T$$

$$\lambda_2 = -k_1 ; \quad v_2 = \begin{bmatrix} \left(\frac{k_1 - k_2}{k_2}\right) & -\frac{k_1}{k_2} & 1 \end{bmatrix}^T$$

$$\lambda_3 = -k_2 ; \quad v_3 = \begin{bmatrix} 0 & -1 & 1 \end{bmatrix}^T$$

$$\therefore \begin{bmatrix} C_A \\ C_B \\ C_C \end{bmatrix} = C_1 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} + C_2 e^{-k_1 t} \begin{bmatrix} \left(-\frac{k_1 + k_2}{k_2}\right) \\ -\frac{k_1}{k_2} \\ 1 \end{bmatrix} + C_3 e^{-k_2 t} \begin{bmatrix} 0 \\ -1 \\ 1 \end{bmatrix}$$

$$\therefore C_A = C_2 \left( \frac{-k_2 + k_1}{k_2} \right) e^{-k_1 t} \approx C_{A0} \rightarrow \text{same result} \rightarrow \text{decay (monotonous)}$$

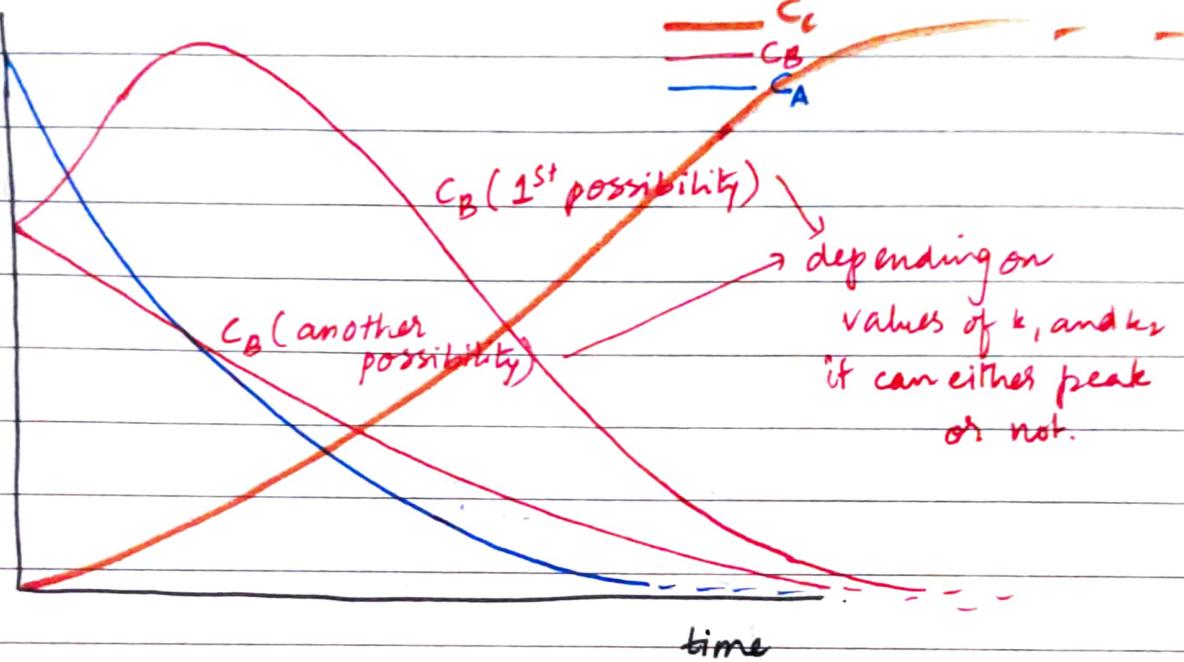
$$C_B = C_2 \left( \frac{k_1 - k_1}{k_2} \right) e^{-k_1 t} - C_3 e^{-k_2 t}$$

$$C_C = C_1 + C_2 e^{-k_1 t} + C_3 e^{-k_2 t}$$

$$\text{We got } C_B = C_2 \left( -\frac{k_1}{k_2} \right) e^{-k_1 t} - C_3 e^{k_2 t}$$

$C_B = A e^{-k_1 t} + B e^{k_2 t} \rightarrow \text{what are its dynamics?}$

cont.



c) Determine the equilibrium solutions.

Equilibrium sol'n's lie in the null space of  $\underline{A}$   $\Rightarrow \underline{A}\underline{x} = 0$

$$\underline{A} = \begin{bmatrix} -k_1 & 0 & 0 \\ k_1 & -k_2 & 0 \\ 0 & k_2 & 0 \end{bmatrix} \rightarrow \begin{bmatrix} -k_1 & 0 & 0 \\ k_1 & -k_2 & 0 \\ 0 & 0 & 0 \end{bmatrix} \rightarrow \begin{bmatrix} -k_1 & 0 & 0 \\ 0 & -k_2 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

Row-reduced form (Step 1)

Step 2: Convert matrix to equations

$$\left. \begin{array}{l} -k_1 C_A = 0 \\ -k_2 C_B = 0 \end{array} \right\} \text{from } \underline{A}\underline{x} = 0$$

$$\therefore C_A e = C_B e = 0$$

There is no constraint for  $C_C \rightarrow$  It means that, whatever amount of  $A$  and  $B$  were in the system determines  $C_C$ .

d) Comment on the stability of the solutions. Analyse your comment in reference to the mag. and signs of  $k_i$ 's.

Stability is governed by eigen values. They were 0, - $k$ , and - $k_L$ .

When eigen values are +ve, ~~are~~ unstable and vice versa.

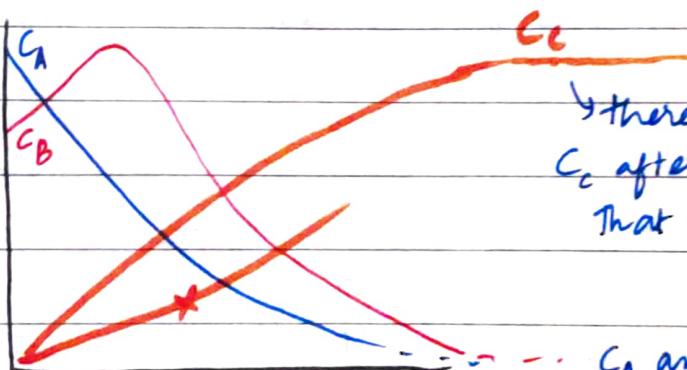
$\lambda_1 = 0, \lambda_2 < 0, \lambda_3 < 0 \rightarrow$  System is stable as none of the eigen values are  $> 0$ .  
 what does this mean?

Physically, this means that the system won't blow up; i.e., concentrations won't blow up to  $\infty$ .

-ve eigen value means system squeezes or decays.

+ve eigen value means system expands or blows up.

'0' eigen value means system is rigid.

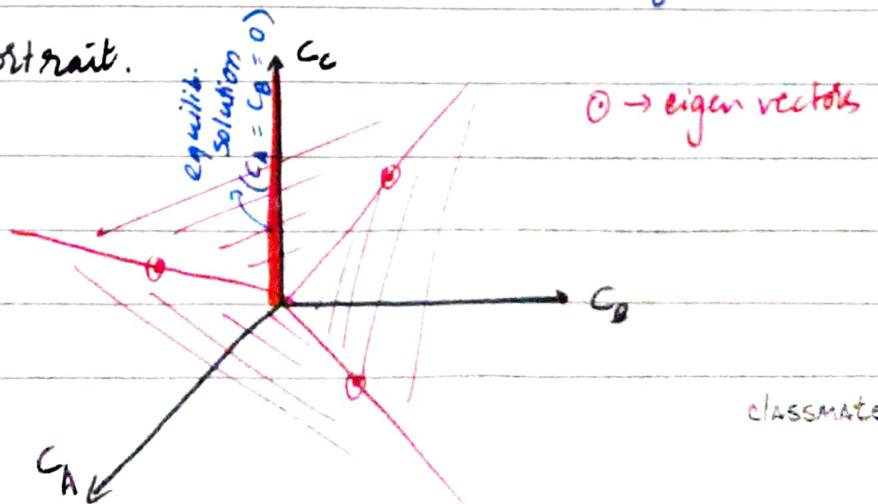


→ there is no dynamics of  $C_C$  after it reaches this phase. That is the significance of  $\lambda_1 = 0$  here.

...  $C_A$  and  $C_B \rightarrow 0$  as  $t \rightarrow \infty$

Similarly,  $C_C$  becomes equal to  $C_{final}$  and it remains there. Of course there are minor changes due to small changes in A and B; but there is no dynamic in C.

e) Draw the phase portrait.



22.01.21

Consider the case of a single linear spring of spring constant  $k$  with mass  $m$  attached to it such that the motion is confined along spring axis. The following questions govern the dynamics of the system.

Once disturbed, you leave the spring alone. No persistent external force.

Free undamped system:

$$(A) : m \frac{d^2x}{dt^2} + kx = 0$$

$$\Rightarrow \frac{d^2x}{dt^2} + \omega^2 x = 0 ; \quad \omega^2 = \frac{k}{m} \rightarrow \text{always positive}$$

Solution 1  $\Rightarrow x(t) = c_1 \sin \omega t + c_2 \cos \omega t$  - sinusoidal undamped

As  $\omega$  increases, the time period of oscillations changes but amplitude is the same.

①

Oscillatory solution

The system has bifurcation about  $\omega'$ . (Check recording). As  $c_1/c_2$  change, the initial values and amplitude change.

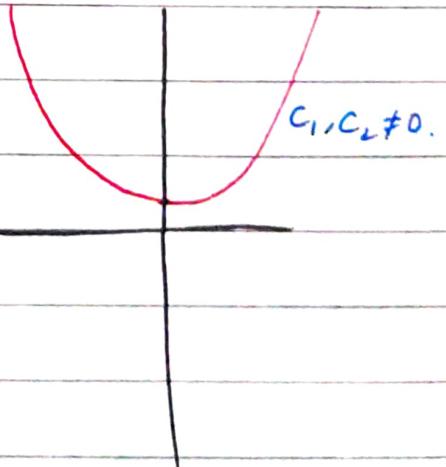
$$\text{Solution 2} \Rightarrow x(t) = c_1 e^{at} + c_2 e^{-at}$$

If  $c_1 = 0$ ; decay behaviour

②

$c_2 = 0$ ; blows up monotonously

$c_1, c_2 \neq 0$ ; blows up eventually



Free vibration with damping:

$$(B) : m \frac{d^2x}{dt^2} + c \frac{dx}{dt} + kx = 0$$

$$\Rightarrow \frac{d^2x}{dt^2} + \frac{c}{m} \frac{dx}{dt} + \frac{k}{m} x = 0 ; \quad a = \frac{c}{m}, \quad b = \frac{k}{m}$$

classmate

$$D^2 + aD + b = 0$$

$$\Rightarrow D = \frac{-a \pm \sqrt{a^2 - 4b}}{2}$$

$$x(t) = c_1 \exp\left(\frac{-a + \sqrt{a^2 - 4b}}{2} t\right) + c_2 \exp\left(\frac{(-a - \sqrt{a^2 - 4b})}{2} t\right)$$

• When  $\sqrt{a^2 - 4b}$  is real and is equal to  $c$ :

$$x(t) = c_1 \exp\left(\frac{-a+c}{2} t\right) + c_2 \exp\left(\frac{-a-c}{2} t\right)$$

oscillatory solution

Same as the solution of free undamped system;

solution 2. The decay/rise will happen like  
in the previous case. Qualitatively same as eq ①

• When  $\sqrt{a^2 - 4b}$  is imaginary and is equal to  $ic$ :

$$x(t) = c_1 \exp\left(\frac{-a+ic}{2} t\right) + c_2 \exp\left(\frac{-a-ic}{2} t\right)$$

$$= e^{-\frac{at}{2}} \left[ c_1 \exp^{ict/2} + c_2 \exp^{-ict/2} \right]$$

$$= e^{-at/2} \left[ c_1 \cos\left(\frac{ct}{2}\right) + c_2 \cos\left(\frac{ct}{2}\right) + i[c_1 \sin\left(\frac{ct}{2}\right) - c_2 \sin\left(\frac{ct}{2}\right)] \right]$$

$$= e^{-at/2} \left[ \underbrace{\cos\left(\frac{ct}{2}\right)}_{\alpha} \cdot (c_1 + c_2) + i \underbrace{\sin\left(\frac{ct}{2}\right)}_{\beta} \cdot (c_1 - c_2) \right]$$

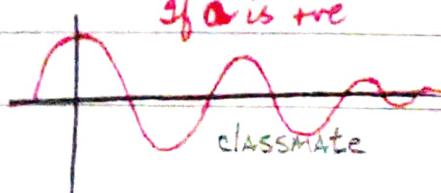
$$x(t) = e^{-at/2} \left[ \alpha \cos\frac{ct}{2} + i\beta \sin\frac{ct}{2} \right] \rightarrow \text{Re} + i\text{Im}$$

Re and Im are itself sol's

$$\therefore x(t) = c_1 e^{-at} \cos\left(\frac{ct}{2}\right) + c_2 e^{-at} \sin\left(\frac{ct}{2}\right)$$

individually.

$$x(t) = e^{-at} \left[ c_1 \cos\left(\frac{ct}{2}\right) + c_2 \sin\left(\frac{ct}{2}\right) \right]$$



if  $a$  is +ve

CLASSMATE

so, in a general 2nd order system; three things can happen -

- exponential decay
- exponential growth
- oscillatory
  - constant amplitude
  - decaying amplitude
  - growing amplitude

Forced vibration without damping:

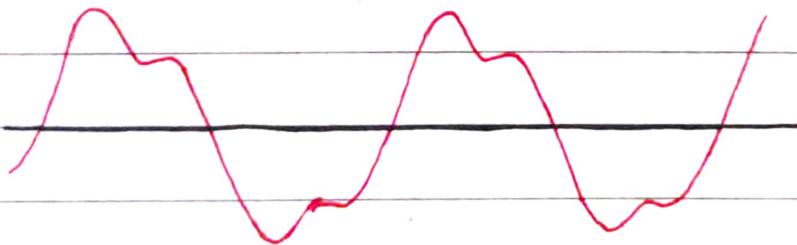
$$\textcircled{1}: m \frac{d^2x}{dt^2} + kx = F_0 \sin \omega t \rightarrow \text{external force}$$

Solve using wolfram alpha

$$\Rightarrow \frac{d^2x}{dt^2} + a^2 x = b \sin \omega t ; \quad a^2 = k/m \quad \& \quad b = F_0/m$$

We get  $x(t) = e^{j\omega_0 t} + c_1 \cos(\omega t) + c_2 \sin(\omega t) + \frac{b \sin(\omega t)}{a^2 - \omega^2}$

Plot on desmos.



Inherent dynamics  
( $c_1 \cos \omega t + c_2 \sin \omega t$ )  
are being superposed  
by forcing function ( $b \sin \omega t$ )

If we analyse forced vibration with damping, we would get

$$x(t) = (e^{-ct}) \left( c_1 \cos \omega t + c_2 \sin \omega t + \frac{b \sin(\omega t)}{a^2 - \omega^2} \right)$$

will cause damping.

a) Solve (A) using the matrix method, phase diagram. Find equilibrium solutions.

$$m \frac{d^2x}{dt^2} + kx = 0$$

$$\frac{d^2x}{dt^2} + \frac{k}{m}x = 0 ; a = \frac{k}{m}$$

$$\text{Let } \frac{dx}{dt} = y \Rightarrow \frac{dy}{dt} = -ax.$$

$$\therefore \frac{d}{dt} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -a & 0 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix}$$

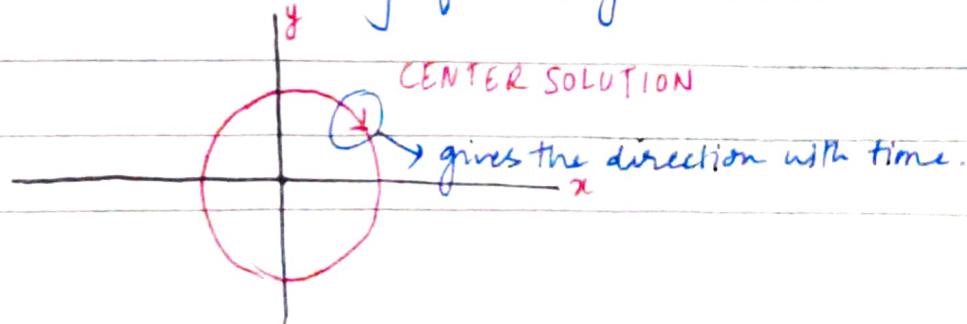
$$\text{We get, } \lambda_1 = -i\sqrt{a} ; v_1 = \begin{bmatrix} i/\sqrt{a} & 1 \end{bmatrix}^T$$

$$\lambda_2 = +i\sqrt{a} ; v_2 = \begin{bmatrix} -i/\sqrt{a} & 1 \end{bmatrix}^T$$

$$\therefore x = c_1 e^{-i\sqrt{a}t} \begin{bmatrix} i/\sqrt{a} \\ 1 \end{bmatrix} + c_2 e^{i\sqrt{a}t} \begin{bmatrix} -i/\sqrt{a} \\ 1 \end{bmatrix}$$

$$x = c_1 \begin{bmatrix} \frac{i}{\sqrt{a}} \cos(\sqrt{a}t) + \frac{1}{\sqrt{a}} \sin(\sqrt{a}t) \\ \cos(\sqrt{a}t) - i \sin(\sqrt{a}t) \end{bmatrix} + c_2 \begin{bmatrix} -\frac{i}{\sqrt{a}} \cos(\sqrt{a}t) + \frac{1}{\sqrt{a}} \sin(\sqrt{a}t) \\ \cos(\sqrt{a}t) + i \sin(\sqrt{a}t) \end{bmatrix}$$

Observations: Eigen values are purely imaginary. Oscillations with center solution are sustained. Eigen vectors only give magnitude of solutions. Everything we need to know qualitatively about the solutions and phase portrait can be obtained from just an understanding of the eigen values.



Equilibrium solutions:  $\underline{A} \underline{x} = 0$

$$\underline{Ax} = \begin{bmatrix} 0 & 1 \\ -a & 0 \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$y = 0 \text{ and } -ax = 0$$

$\therefore x = 0$  and  $y = 0$  are equilibrium solutions.

The above solution holds for  $k > 0, m > 0$ ; i.e.;  $a > 0$

Consider for any hypothetical scenario,  $a < 0$ . Then,

$$\begin{aligned} \lambda_1 &= -\sqrt{a} \\ \lambda_2 &= \sqrt{a} \end{aligned} \quad ? \quad \text{we get saddle solutions.} \quad \text{??}$$

b) Solve ③ using matrix

$$\frac{d^2x}{dt^2} + a \frac{dx}{dt} + bx = 0$$

$$\frac{dx}{dt} = y ; \quad \frac{dy}{dt} + ay + bx = 0$$

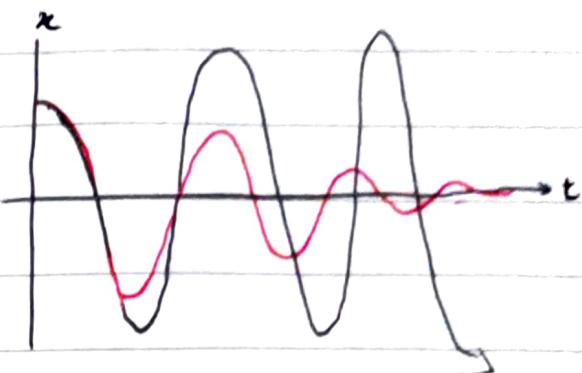
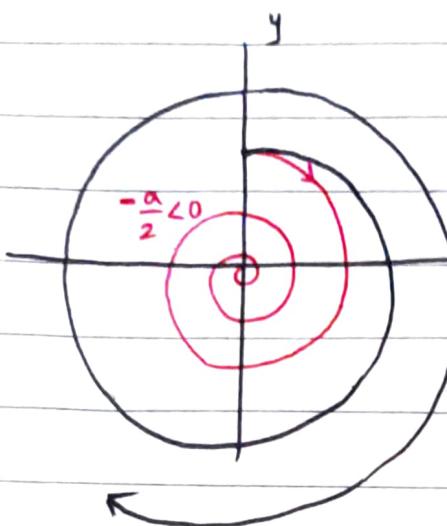
$$\frac{d}{dt} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -b & -a \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} \rightarrow \begin{aligned} \lambda_1 &= \frac{1}{2}(-\sqrt{a^2-4b}-a) \\ \lambda_2 &= \frac{1}{2}(\sqrt{a^2-4b}-a) \end{aligned}$$

If  $\sqrt{a^2-4b}$  is real,  $\lambda_1$  is real &  $\lambda_2$  is real  
Saddle solutions.

If  $\sqrt{a^2-4b}$  is imaginary,  $\lambda_1$  and  $\lambda_2$  would be complex.  
Solution would be oscillatory. It might be centre or spiral  
based upon the value of  $-a/2$ ; the real part. If  $a=0$ , then  
centre solutions. If  $-a/2 < 0$ , then spiral sink.  
If  $-a/2 > 0$ , then spiral source.

Quiz 1: Jan 31, Sunday 9:00 - 10:00 pm  
Pen & paper test → scan to PDF → email.

Topic: Linear dynamics - Topic 1, 2, 3



c) Solve forced damping.

$$\frac{d^2x}{dt^2} + a \frac{dx}{dt} + bx = c \sin \omega t$$

$$\Rightarrow \frac{dx}{dt} = y ; \quad \frac{dy}{dt} + ay + bx = c \sin \omega t.$$

$$\Rightarrow \frac{d}{dt} \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -b & -a \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} + \begin{bmatrix} 0 \\ c \sin \omega t \end{bmatrix}$$

$$\Rightarrow \frac{d \underline{x}}{dt} = \underline{A} \underline{x} + \underline{b} \quad \rightarrow \text{How to solve this?}$$

↓  
Refer to class notes.

Last 10 mins of  
the class.