

$$\text{Vessel Height} = 25 \text{ m}$$

$$\text{Vessel ID} = 2 \text{ m}$$

$$\text{Max Op. Press} = 2 \text{ MPa}$$

$$\therefore \text{Design Press} = 1.05 \times 2 \text{ MPa} = 2.1 \text{ MPa} = p$$

$$\text{Skirt height} = 5 \text{ m}$$

$$f = 100 \text{ MPa}$$

$$C_s = \frac{0.04}{T}$$

$$\text{Wind Vel}_1 = 130 \text{ km/hr}$$

$$t = \frac{p D_i}{2 f T - p} = \frac{2.1 \times 10^6 \times 2}{2 \times 100 \times 10^6 \times 0.85 - 2.1 \times 10^6}$$

$$= 25.01 \text{ mm}$$

$$t_r = t + t_c (2 \text{ mm})$$
$$= 27.01 \text{ mm}$$

$$\text{Next Available Thickness} = 28 \text{ mm}$$

$$\text{Corroded Shell Thickness} = t - c$$

$$= 28 - 2 \text{ mm}$$

$$= 26 \text{ mm}$$

Axial stress due to pressure :

$$\begin{aligned}\sigma_{zp} &= \frac{p D_i^2}{4t (D_i + t)} \approx \frac{p D_o}{4t} \\ &= \frac{2.1 \times 10^6 \times 2}{4 \times 26 \times 10^{-3}} \\ &= 40.38 \text{ MPa}\end{aligned}$$

Axial stress due to dead load :

W_s = Weight of shell for X m length

$$= \pi D t X \gamma_s$$

$$= \pi \times 2 \times 26 \times 10^{-3} \times 7.7 \times 10^{-4} \times X$$

$$= 0.01257 X \text{ MN}$$

$$\sigma_{zs} = \frac{W_s}{\pi t D} = \gamma_s X \text{ N/m}^2$$

$$= 0.077 X \text{ MPa}$$

Weight of liquid supported for distance X m from top:

$$= \frac{\pi D^2 \rho g X}{4}$$

$$= \frac{\pi \times 2^2 \times 1000 \times 4.81 \times 10^{-6}}{4} \text{ MN}$$

$$= 0.0308 \times \text{MN}$$

$$\sigma_{z1} = \frac{W_L}{\pi D t} = \frac{0.0308 \times \text{MN}}{\pi \times 2 \times 26 \times 10^{-3}}$$

$$= 0.1886 \times \text{MPa}$$

$$\sigma_{zw} = \sigma_{zs} + \sigma_{z1}$$

$$= (0.077 + 0.1886) \times \text{MPa}$$

$$= 0.2656 \times \text{MPa}$$

Time period

$$\begin{aligned} T &= 6.35 \times 10^{-5} \left(\frac{H}{D} \right)^{3/2} \left(\frac{W}{t} \right)^{1/2} \\ &= 6.35 \times 10^{-5} \left(\frac{25+5}{2} \right)^{3/2} \left(\frac{0.0134}{26 \times 10^{-3}} \right)^{1/2} \\ &= 0.75 \text{ s} \end{aligned}$$

$$\begin{aligned} P_w &= k_1 k_2 (0.05 V_w^2) D_0 \\ &= 0.7 \times 2 \times 0.05 \times (130)^2 \times 2.056 \\ &= 3238.2 \text{ N} \end{aligned}$$

$$\begin{aligned} M_w &= P_w \frac{x}{2} J \\ &= 1614.1 \times^2 J \end{aligned}$$

$$\sigma_{Z_{w.m}} = \frac{4 M_w}{\pi D^2 t} = \frac{4 \times 1614.1 \times^2 J}{\pi \times (2.056)^2 \times 26 \times 10^{-3}}$$

$$= 0.0198x^2 \text{ MPa}$$

$$M_s = \frac{C_s W x (3H - x)}{3H^2}$$

$$= \frac{0.04 \times W \times H \times 2H}{T \times 3H^2} \quad \{x = H\}$$

$$= 0.041 \times MN$$

$$\sigma_{zsm} = \frac{4M_s}{\pi t (D_i + t) D_i}$$

$$= \frac{4 \times 1.035 \times 10^6}{\pi \times 26 \times 10^{-3} \times 2.036 \times 2}$$

$$= 0.47 \times \text{MPa}$$

$$\sigma_z (\text{tensile}) = \sigma_{zp} - \sigma_{zw} + \sigma_{zwm} + \sigma_{zsm} = fJ$$

$$= 40.38 - 0.2856x + 0.0198x^2 + 0.47x$$

$$\Rightarrow 0.0198x^2 + 0.2044x + 40.38 = 100 \times 0.85 = 85$$

$$\Rightarrow 0.0198x^2 + 0.2077x - 99.62 = 0$$

$$\Rightarrow x = 43$$

$$\sigma_z (\text{compression}) = \sigma_{zw} - \sigma_{zp} + \sigma_{zwm} + \sigma_{zsm}$$

$$= 0.125 \frac{E_t}{D_0}$$

$$\Rightarrow 0.26x - 10.38 + 0.0198x^2 + 0.17x$$

$$= 0.125 \times 2 \times 10^5 \times \frac{0.026}{2.056}$$

$$= 316.76 \text{ MPa}$$

$$0.0198x^2 + 0.73x - 357.14 = 0$$

$$x = 117.13 \text{ m}$$

$\therefore x > H$, The design is OK,