

Straight Moss transfer

14=18

By material balance between O & @ we find of.

$$\frac{90000}{10^5}(1000-100) = \frac{900000}{55556}(C_{AI}-0)$$

or CAI = 50 mol/m3

Cat CAI

at equilibrium PA = HA CA - Or PA1 = 18x50 = 900

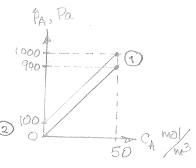
Now draw the pros Grangram. We see that the operating & equilibrium lines are parallel. Thus the rate of transfer is the some everywhere. So we find

$$-r_{A}^{""} = \frac{1}{k_{Ag}a} \frac{1}{k_{Ag}a} (p_{A} - p_{A}^{*}) = \frac{1}{0.36} + \frac{19}{72} (1000 - 900) = 38$$

 $V_r = \frac{f_g}{\pi} \left(\frac{d\rho_A}{-r_A^{(1)}} = \frac{90000(1000 - 100)}{105} = 24.5 \text{ m}^3 \right)$

3- 15-900 000 3-15 CA2=0

5=9000 N CA=?



24.5 By material balance find CBI (see diagram on right)

 $90000\left(\frac{0.01}{0.99} - \frac{0.001}{0.995}\right) = 900000\left(0.001 - X_{B1}\right)$

or CB1 = 5 mol/m3

We need to evaluate E: & MH

to find the rate

Fig 23.4 shows
$$M_{H} = \sqrt{\frac{D_{A} C_{B}}{k_{Ae}}} = 0.01$$

$$M_{A} = 0.01$$

$$M_{A}$$

$$\chi_{A2} = \frac{55.56}{55.556} = 10^3$$

24.5 continued Now determine the rate at top, bottom and intermediate point

At topQ $E_i = 1 + \frac{55.56 \times 10^5}{100} = 5.556 \times 10^4$ There I am goessing that all the resistance is in the gas film, so I put $P_{AZ}^* = P_{AZ}$

Because E; KMH we say that E=E; =5.556×104. Now to the rate

$$-\frac{1}{4} = \frac{1}{4} + \frac{1$$

At bottom, 0 E; = 1 + 55.56 × 105 = 501

To am again guessing that all resistance is in the gas film

$$-\Gamma_{A}^{IMI} = \frac{1}{1036 + 105} \cdot P_{A} = \frac{1}{1036 + 0.36} \cdot P_{A} = \frac{1}{0.36} \cdot P_{A} =$$

(I this chows that 50% of resistance is in the liquid film. This is not what we

Try ogain

Guess PAi = 500, repeat the procedure. We find E:=1001

and from the vare 1/3 of the resistance is in the gas film. Wrong gress

Try unce again

Guess Phi= 100, or 10% resistance in the gas film. Then E:= 5001 &

Herce

$$V = \frac{F_3}{m} \int \frac{d\rho_A}{-r_h''''} = \frac{90000}{10^5} \int \frac{d\rho_A}{0.345} = \frac{90000}{34500} \int_{10}^{10} = 6 \text{ m}^3$$
Gas film resistance is 9.1% of total, 9% is from liquid



First determine Coout -- see sketch at right

$$F_g(Y_{out} - Y_{in}) = F_e(X_{in} - X_{out})$$

$$90000\left(\frac{0.01-0.001}{0.99}-9000\left(\frac{5556}{5556}-\frac{CB_{OUT}}{55556}\right)\right)$$
 $C_{Bin}=5556$

in Gout = 500 mol/m3

Next determine the rate (note at the exit conditions)

$$M_{H} = \sqrt{\frac{D \, \text{LCB}}{k_{H}}} = \sqrt{\frac{3.6 \times 10^{5} (2.6 \times 10^{5})500}{0.72^{2}}} = 30$$

$$E_1 = 1 + \frac{c_8 H_A}{PAI} = 1 + \frac{500(10^5)}{100} = 5 \times 10^5$$
, or higher

Since E: > Mr. o. Fig 23.4 shows that E=MH = 30

$$-r_{A}^{(1)} = \frac{1}{k_{Ag}a} + \frac{1}{k_{A}a} + \frac{1}{k_{A}a} + \frac{1}{k_{B}} + \frac{1}{k_{B}} + \frac{1}{k_{B}} + \frac{1}{k_{B}} + \frac{1}{k_{A}a} + \frac{1}{k_$$

$$V = \frac{F_g}{\pi} \frac{\Delta \rho_A}{(-\Gamma_A^{(1)})} = \frac{90000(1000 - 100)}{105(0.041)100} = 197.6 \text{ m}^3$$

Liquid film contributes 94.3% of the resistance



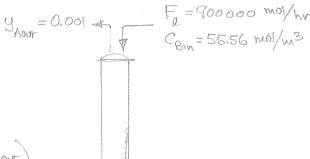
24.9

First defermine (Bout

by a material balance

$$90000\left(\frac{0.01}{0.99} - \frac{0.001}{0.992}\right) = \frac{900000}{55556}\left(55.56 - CBOUF\right)$$

From which



At top
$$M_H = \sqrt{\frac{9 \, \text{kCB}}{k_{AL}}} = \sqrt{\frac{3.6 \times 10^{-6} (2.6 \times 10^7) 55.56}{0.72^2}} = 100$$

$$- \frac{1}{1} = \frac{1}{1 + \frac{1}{1} + \frac{1$$

At bottom
$$M_{H} = \frac{3.6 \times 10^{-6} (2.6 \times 10^{7})5}{(0.72)^{2}} = 30$$

$$E_1 = 1 + \frac{5(10^5)}{1000} = 501 >> M_H - 30 = M_H = 30$$

Near the middle where CB=30.56. A mat balance then gives YA=547 Pa

$$M_{H} = \frac{3.6 \times 10^{-6} (2.6 \times 10^{7}) 30.56}{(0.72)^{2}} = 74$$

$$E_{1} = lavge$$

$$E_{2} = lavge$$

About 1/4 from the top where Px = 300 Pa & CB = 44.4 we fund My = 89.5, E: = very large, so E= My = 89.5 & - 5/1"=16.4

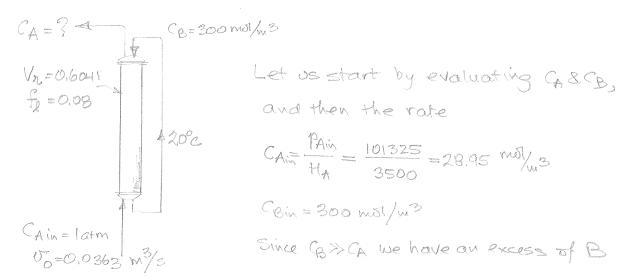
So now to the performance of the reactor

1000

$$V_{R} = \frac{F_{0}}{\Omega} \int \frac{d\rho_{A}}{-\Gamma_{A}^{(0)}} = \frac{90000}{10^{5}} (area) = \frac{90000}{10^{5}} (55) = 49.5 \text{ m}^{3}$$

Liquid frlm resistance dominates, 93~94%

24.11



$$C_{A,=} \frac{P_{A,m}}{H_A} = \frac{101325}{3500} = 28.95 \text{ mal}_{M3}$$

Since (B>> CA we have an excess of B

So we can take Ca = constant = 300

Now to the rate of 1x

$$M_{H} = \sqrt{\frac{1.4 \times 10^{7} (0.433)300}{0.25/120}} = 2.05$$
 since $E_{c} > 5 M_{H}$ we have $E_{c} = 1\frac{300(3500)}{100325} = 11.36$ $E = M_{H} = 2.05$

50

$$\frac{7}{4}''' = \frac{3500}{0.025(2.05)} + \frac{3500}{0.433(300)0.08} = \frac{9}{0.025(2.05)} + \frac{1.457 \times 10^{-5}}{0.433(300)0.08}$$

$$= \frac{9}{0.025(2.05)} + \frac{1.457 \times 10^{-5}}{0.433(300)0.08} = \frac{1.4764}{0.468292 + 337}$$
(pure Co₂ at 1 atm,
$$\frac{99.5}{0.05} + \frac{1.457 \times 10^{-5}}{0.05} = \frac{1.4764}{0.05}$$
(pure Co₂ at 1 atm,
$$\frac{1.457 \times 10^{-5}}{0.05} = \frac{1.4764}{0.05}$$

From Eq 15
$$\frac{V_n}{F_{Ao}} = \begin{cases} x_A & F \times x_A \\ -Y_A'''' & F_{Ao} \end{cases}$$
because $-T_K''' = \text{constant}$

24.13 Here we have a batch agitated tank k=2.6×105 th= 105

At the beginning
$$C_8 = 555.6$$
 $M_{H} = \frac{\sqrt{3.6 \times 10^{-6} (2.6 \times 10^{5}) 555.6}}{144/100} = 15.84$
 $E_{i} = 1 + \frac{555.6 (10^{5})}{103} = 55561$

Figures this or something smaller

Phont Batch

 $C_{80} = 555.6$
 $F_{g} = 9000 \text{ mol/w}$
 $C_{80} = 555.6$
 $F_{g} = 9000 \text{ mol/w}$
 $C_{80} = 555.6$

PAIN = 1000 Pa

whatever we guess makes no d'Alevence

Now My < Ei so E = My = 15.84.

Next, since E=MH and PAKT we can use the shortcut j'ust above Eq 19 to explude the vate. So

$$\frac{1}{20 + 1.3889 + 43.8417 + 0.0008 \cdot 1000 \cdot = 15.33}$$

$$\frac{1}{1000} = 0.06523$$
main resistances \(\text{regligible} \)

At the end of the run 18=55.56

$$M_{H} = 5.01$$

$$E_{i} = 1 + \frac{586(105)}{103} = 5561$$

$$= 586(105)$$

$$= 3889 + \frac{1}{1000} = 6.25$$

$$= 6.25$$

$$= \frac{1}{138.61} = 0.16$$

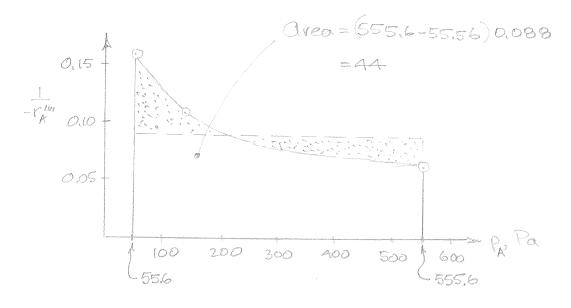
At some informediate condition, say at
$$C_{e} = \frac{555.6}{4} = 138.9$$

$$M_{H} = \frac{15.84}{2} = 7.92$$

$$E_{i} = 55561/_{4} = 13890$$

$$E = M_{H} = 7.92$$

$$\frac{1}{20 + 1.5959 + \frac{10^{5}}{144(7.92)^{500}} - 1000 = 9.168}$$



The length of time that we have to bubble gas through the houd is

$$t = \frac{g_0}{f_0} \int \frac{dg_0}{f_0} = f_0 \text{ (avea)} = 0.9(44) = 39.6 \text{ hr}$$

The minimum time needed if all the A reacts with B is

time = Ve (GBO-GBF) = 1.62 (SSS.6-SS.56) = 8.91 hr

Fa (PA/(TT-PA) 9000 (1000/99000) = 0000

5° Sefficiency of use of
$$A = \frac{8.91}{39.6} = 22.5\%$$

QH.15 Here we have a batch agitated tank with £=2.6×103 Hz=105

At the beginning CB=555.6 mol/m3

$$M_{H} = \frac{\sqrt{2.6 \times 10^{3} (3.6 \times 10^{-6}) 555.6}}{144 / 100} = 1.584$$

$$E_{1} = 1 + \frac{555.6 (105)}{103} = 55561$$

$$E_{2} = 1 + \frac{555.6 (105)}{103} = 55561$$

Use the shortcut formula just above Eq 19, thus

$$= \frac{1}{(1.62/0.9) \cdot 10^{5} + 1} \cdot \frac{1}{0.72} \cdot \frac{10^{5}}{144(1.584)} + \frac{10^{5}}{2.6 \times 10^{3}(555.6)} \cdot \frac{1000}{0.72}$$

At the end of the run CB=55.56

$$M_{H} = 1.584 / \sqrt{10} = 0.5$$
 $E_{1} = 1+ \frac{55.56(105)}{200} = \log \alpha \log \alpha$

Shortcot 2 (or smaller)

- [A"] = 20+1.3889+438.9 (10) + 20 (10) = 0.7096

24.15 At some intermediate condition, say CB = 555.6/4=138.9

$$M_{H} = 1.584/4 = 0.792$$
 $E_{i} = 1 + \frac{555.6(105)}{103} = 6ig$
 $E_{i} = 1 + \frac{M_{i}^{2}}{3} = 1.2$

$$60 - r_A^{(1)} = \frac{1}{20 + 13889 + 10^5/144(1.2)} \cdot 1000 = 1.666$$

The length of time needed to bubble gas through the reactor is

$$t = \frac{f_0}{f_0} \int \frac{dc_0}{-r_A'''} = f_0(\text{orea}) = 0.9(265) = 238.5 \text{ hr}$$
(a)

