

Dynamics of First-order systems.

Definition: A first-order system is one whose output $y(t)$ is modeled by a first-order differential equation

✓ Linear (or linearized) system

$$a_1 \frac{dy}{dt} + a_0 y = b f(t)$$

$y \rightarrow$ output
 $f \rightarrow$ input/forcing function
|
 \rightarrow both derivation variables

case 1. $a_0 \neq 0$

$$\frac{a_1}{a_0} \frac{dy}{dt} + y = \frac{b}{a_0} f(t)$$

$$\tau_p \frac{dy}{dt} + y = K_p f(t)$$

where,

$$\frac{a_1}{a_0} = \tau_p = \text{time constant of the process (Unit} \equiv \text{time)}$$

$$\frac{b}{a_0} = K_p = \text{steady-state/static gain } \left(= \frac{\Delta y}{\Delta f} \right)_{ss}$$

Taking L-transform and rearranging,

$$G(s) = \frac{\bar{y}(s)}{\bar{f}(s)} = \frac{K_p}{\tau_p s + 1} \quad \text{--- TF}$$

(1st-order lag / linear lag)

case 2. $a_0 = 0$

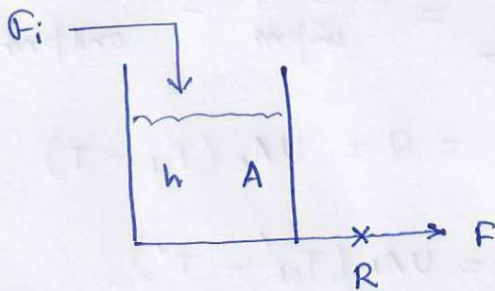
$$a_1 \frac{dy}{dt} = b f(t)$$

$$\frac{dy}{dt} = \frac{b}{a_0} f(t) = K_p' f(t)$$

$$G(s) = \frac{\bar{y}(s)}{\bar{f}(s)} = \frac{K_p'}{s} \quad \dots \quad \text{TF}$$

(purely capacitive / pure integrator)

Ex.1. First-order system (mass storage).



$$F = \frac{h}{R} = \frac{\text{driving force}}{\text{resistance}}$$

$$\text{Model: } A \frac{dh}{dt} = F_i - F = F_i - \frac{h}{R}$$

$$AR \frac{dh}{dt} + h = R F_i$$

$$\tau_p \frac{dh'}{dt} + h' = K_p F_i' \quad \dots \quad \text{in terms of deviation variables}$$

where,

$$\tau_p = AR \quad \text{unit?}$$

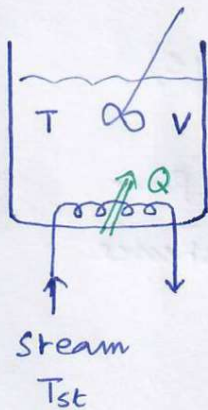
$$K_p = R \quad \text{unit?}$$

$$G(s) = \frac{\bar{h}'(s)}{\bar{F}_i'(s)} = \frac{K_p}{\tau_p s + 1}$$

time const $\tau_p = AR = \text{storage capacitance} \times \text{resistance to flow}$

$\uparrow A$ $\uparrow R$
 capacity to store mass
 is measured by A

Ex 2. First-order system (energy storage).



✓ Energy bal.

Rate of accumulation = Rate of input - Rate of output

$$V\rho C_p \frac{dT}{dt} = Q = UA_t (T_{st} - T)$$

$$V\rho C_p \frac{dT'}{dt} = UA_t (T_{st}' - T')$$

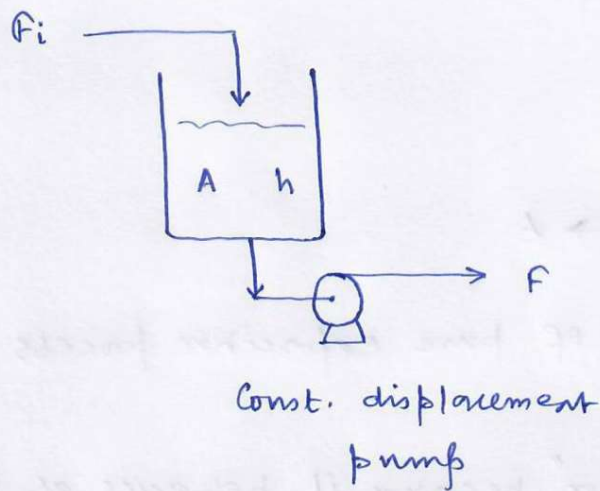
$$\checkmark G(s) = \frac{\bar{T}'(s)}{\bar{T}_{st}'(s)} = \frac{UA_t}{V\rho C_p s + UA_t} = \frac{1}{\frac{V\rho C_p}{UA_t} s + 1} = \frac{K_p}{\tau_p s + 1}$$

$K_p = \text{static gain} = 1$

$$\tau_p = \frac{V\rho C_p}{UA_t} = (\text{storage capacitance}) \times \text{resistance to heat flow}$$

$\uparrow V\rho C_p$ $\uparrow \frac{1}{UA_t}$
 capacity to store thermal
 energy is measured by $V\rho C_p$

Ex 3. Pure Integrator



Mass bal.

$$A \frac{dh}{dt} = F_i - F$$

or yields:

$$A \frac{dh'}{dt} = F_i' \quad \text{Since } F = \text{const}$$

$$G(s) = \frac{\bar{h}'(s)}{\bar{F}_i'(s)} = \frac{1}{As} = \frac{1/A}{s} = \frac{K_p'}{s} \quad \frac{1}{s} \equiv \text{integrator}$$

✓ Dynamic response

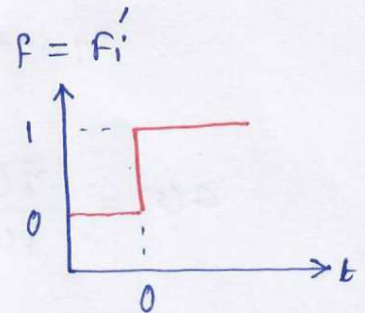
$$\bar{h}'(s) = \frac{K_p'}{s} \cdot \bar{F}_i'(s)$$

Introduce a unit step change in the input / forcing function F_i'

$$\bar{y} = \frac{K_p'}{s} \cdot \frac{1}{s}$$

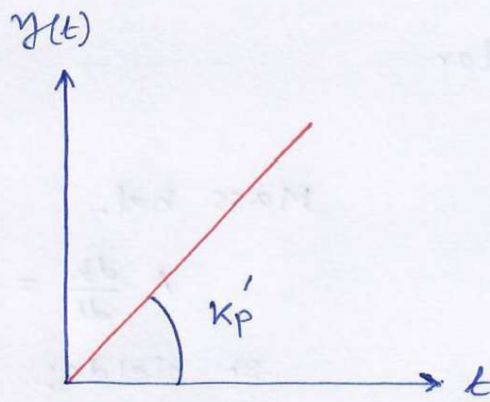
Taking inverse of L-transform:

$$y(t) = K_p' t = K_p' t$$



$$\bar{y} = \bar{h}'$$

$f(t) = 1$	-- time
$\bar{f}(s) = \frac{1}{s}$	-- Laplace



Unbounded response of pure capacitive process

- It is called "pure integrator" because it behaves as if there were an integrator betⁿ input and output.
- It is non-self-regulating system. As $F_i \uparrow$, y consistently \uparrow without attaining any ss.

Dynamic response of first-order lag system.

$$G(s) = \frac{\bar{y}(s)}{\bar{f}(s)} = \frac{K_p}{\tau_p s + 1} \quad \dots \text{derived before}$$

Consider a unit step change in f ,

$$f(t) = 1 \quad \& \quad \bar{f}(s) = \frac{1}{s}$$

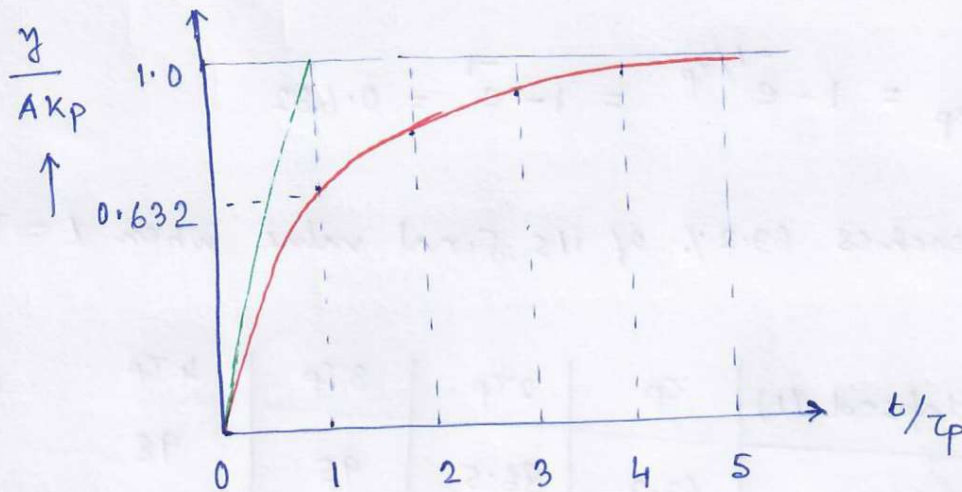
$$\bar{y}(s) = \frac{K_p}{s(\tau_p s + 1)} = \frac{K_p}{s} - \frac{K_p \tau_p}{\tau_p s + 1}$$

Inverting ,

$$y(t) = K_p (1 - e^{-t/\tau_p})$$

$$y(t) = K_p (1 - e^{-t/\tau_p}) \quad \dots \text{Unit step change}$$

$$y(t) = A K_p (1 - e^{-t/\tau_p}) \quad \dots \text{step change with magnitude } A$$

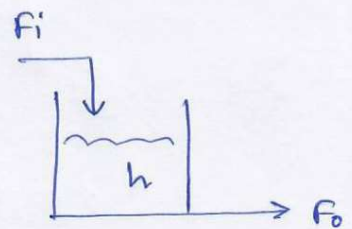


Dimensionless response y/AK_p vs. t/τ_p

Features.

1. First-order lag system is self-regulating (a) reaches a new ss. \Downarrow

If $F_i \uparrow \Rightarrow h \uparrow \Rightarrow \text{hydrostatic } p \uparrow \Rightarrow F_o \uparrow$



2. slope of response at $t=0$ is 1

$$\frac{d[y/AK_p]}{d(t/\tau_p)} \bigg|_{t=0} = \frac{e^{-t/\tau_p}}{1} \bigg|_{t=0} = 1$$

It implies that 'if the initial rate of change of $y(t)$ were to be maintained, the response would reach its final value in one time constant'.

$$t/\tau_p = 1$$

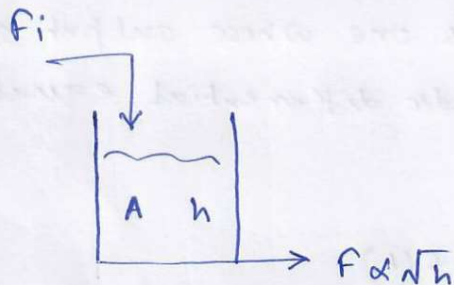
3. $y/A_{kp} = 1 - e^{-t/\tau_p} = 1 - e^{-1} = 0.632$

$y(t)$ reaches 63.2% of its final value when $t = \tau_p$.

Time elapsed (t)	τ_p	$2\tau_p$	$3\tau_p$	$4\tau_p$
% y/A_{kp}	63.2	86.5	95	98

4. As $t \rightarrow \infty$, $y/A_{kp} = 1$ = ultimate value of the response

Variable time const (τ_p) and gain (K_p)



$$\text{Model : } A \frac{dh}{dt} = F_i - F$$

$$A \frac{dh}{dt} + \alpha \sqrt{h} = F_i \quad \dots \text{nonlinear model}$$

$$A \frac{dh'}{dt} + \frac{\alpha}{2\sqrt{h_s}} h' = F_i' \quad \dots \text{linearized model}$$

$$\tau_p \frac{dh'}{dt} + h' = K_p F_i'$$

$$\text{where, } \tau_p = \frac{2A\sqrt{h_s}}{\alpha}, \quad K_p = \frac{2\sqrt{h_s}}{\alpha}$$

value of h_s can vary by varying F_{is} . so, τ_p and K_p also vary accordingly.