

ECE 697 Modeling and High-Performance Control of Electric Machines
HW 3 Solutions
Spring 2022

Problem 16 *A Two-Phase Four-Pole Generator*

(a) Using an outward normal for the flux surface ($\hat{\mathbf{n}} = \hat{\mathbf{r}}$), the flux linkage in stator loop $a - a'$ due to the rotor's magnetic field is

$$\begin{aligned}
 \lambda_a &= \int_0^{\ell_1} \int_{-\pi/2}^0 B_{R\max} \cos(n_p(\theta - \theta_R)) \hat{\mathbf{r}} \cdot (r_S d\theta d\ell \hat{\mathbf{r}}) + \int_0^{\ell_1} \int_{\pi/2}^{\pi} B_{R\max} \cos(n_p(\theta - \theta_R)) \hat{\mathbf{r}} \cdot (r_S d\theta d\ell \hat{\mathbf{r}}) \\
 &= \frac{r_S \ell_1 B_{R\max}}{n_p} \sin(n_p(\theta - \theta_R)) \Big|_{-\pi/2}^0 + \frac{r_S \ell_1 B_{R\max}}{n_p} \sin(n_p(\theta - \theta_R)) \Big|_{\pi/2}^{\pi} \\
 &= \frac{r_S \ell_1 B_{R\max}}{n_p} \left(-\sin(n_p \theta_R) + \sin(n_p(\pi/2 + \theta_R)) + \sin(n_p(\pi - \theta_R)) - \sin(n_p(\pi/2 - \theta_R)) \right) \\
 &= \frac{r_S \ell_1 B_{R\max}}{2} \left(-\sin(2\theta_R) + \sin(2(\pi/2 + \theta_R)) + \sin(2(\pi - \theta_R)) - \sin(2(\pi/2 - \theta_R)) \right) \\
 &= \frac{r_S \ell_1 B_{R\max}}{2} (-4 \sin(2\theta_R)) \\
 &= -2r_S \ell_1 B_{R\max} \sin(2\theta_R).
 \end{aligned}$$

(b) Does the positive direction of travel around each of the two flux surfaces of phase a coincide with the positive direction of current? **Yes**

(c)

$$\xi_{a-a'} = -\frac{d\lambda_a}{dt} = 4r_S \ell_1 B_{R\max} \omega_R \cos(2\theta_R) = 4r_S \ell_1 B_{R\max} \omega_R \cos(2\omega_R t)$$

(d) Similarly ($n_p = 2$)

$$\begin{aligned}
 \lambda_b(\theta_R) &= \int_0^{\ell_1} \int_{-\pi/4}^{+\pi/4} B_{R\max} \cos(n_p(\theta - \theta_R)) \hat{\mathbf{r}} \cdot (r_S d\theta d\ell \hat{\mathbf{r}}) + \int_0^{\ell_1} \int_{3\pi/4}^{5\pi/4} B_{R\max} \cos(n_p(\theta - \theta_R)) \hat{\mathbf{r}} \cdot (r_S d\theta d\ell \hat{\mathbf{r}}) \\
 &= \frac{r_S \ell_1 B_{R\max}}{n_p} \sin(n_p(\theta - \theta_R)) \Big|_{-\pi/4}^{+\pi/4} + \frac{r_S \ell_1 B_{R\max}}{n_p} \sin(n_p(\theta - \theta_R)) \Big|_{3\pi/4}^{5\pi/4} \\
 &= \frac{r_S \ell_1 B_{R\max}}{n_p} \left(\sin(2(\pi/4) - 2\theta_R) - \sin(2(-\pi/4) - 2\theta_R) + \sin(2(5\pi/4) - 2\theta_R) - \sin(2(3\pi/4) - 2\theta_R) \right) \\
 &= \frac{r_S \ell_1 B_{R\max}}{2} \left(\cos(2\theta_R) + \cos(2\theta_R) + \cos(2\theta_R) + \cos(2\theta_R) \right) \\
 &= \frac{r_S \ell_1 B_{R\max}}{2} (4 \cos(2\theta_R)) \\
 &= 2r_S \ell_1 B_{R\max} \cos(2\theta_R).
 \end{aligned}$$

Note that

$$\lambda_b(\theta_R) = \lambda_a(\theta_R - \pi/4) = -2r_S \ell_1 B_{R\max} \sin(2(\theta_R - \pi/4)) = 2r_S \ell_1 B_{R\max} \cos(2\theta_R).$$

The induced voltage in phase $b - b'$ is

$$\xi_{b-b'} = -d\lambda_b/dt = 4r_S \ell_1 B_{R\max} \omega_R \sin(2\theta_R) = 4r_S \ell_1 B_{R\max} \omega_R \sin(2\omega_R t).$$

(e) With the electric field given by

$$\vec{\mathbf{E}}(\theta - \theta_R) = \omega_R B_{R\max} r_S \cos(n_p(\theta - \theta_R)) \hat{\mathbf{z}}$$

the voltage in phase $a - a'$ is computed as

$$\begin{aligned}
\xi_{a-a'} &= \int_{a'}^a \vec{\mathbf{E}}(\theta - \theta_R) \cdot d\vec{\ell} \\
&= \int_{side\ a'_1} (\omega_R B_{R\max} r_S \cos(n_p(-\pi/2 - \theta_R)) \hat{\mathbf{z}}) \cdot (-d\ell \hat{\mathbf{z}}) + \int_{side\ a_1} (\omega_R B_{R\max} r_S \cos(n_p(0 - \theta_R)) \hat{\mathbf{z}}) \cdot (d\ell \hat{\mathbf{z}}) \\
&\quad + \int_{side\ a'_2} (\omega_R B_{R\max} r_S \cos(n_p(\pi/2 - \theta_R)) \hat{\mathbf{z}}) \cdot (-d\ell \hat{\mathbf{z}}) + \int_{side\ a_2} (\omega_R B_{R\max} r_S \cos(n_p(\pi - \theta_R)) \hat{\mathbf{z}}) \cdot (d\ell \hat{\mathbf{z}}) \\
&= \omega_R B_{R\max} r_S \ell_1 \left(-\cos(2(-\pi/2 - \theta_R)) + \cos(2\theta_R) - \cos(2(\pi/2 - \theta_R)) + \cos(2(\pi - \theta_R)) \right) \\
&= \omega_R B_{R\max} r_S \ell_1 \left(-\cos(\pi + 2\theta_R) + \cos(2\theta_R) - \cos(\pi - 2\theta_R) + \cos(2\theta_R) \right) \\
&= 4r_S \ell_1 B_{R\max} \omega_R \cos(2\theta_R) \\
&= 4r_S \ell_1 B_{R\max} \omega_R \cos(2\omega_R t)
\end{aligned}$$

which is the same result as using Faraday's law in part (c).