

PROBLEMS I

1. An amplifier has a feedback fraction β equal to 0.1. Calculate the overall gain with feedback, A_f , if the open loop gain A_{ol} has the following values (a) 10; (b) 50; (c) 100; (d) 500; (e) 1000. From these results what would you guess the limiting value of A_f would be as A_{ol} tends to infinity? Compare this guess with the value of $1/\beta$.

$$\beta=0.1$$

A_{ol}	$A_f = \frac{A_{ol}}{1+A_{ol}\beta}, \beta=0.1$
10	5
50	8.33
100	9.09
500	9.8
1000	9.9
∞	10

$A_{ol}\beta = T$ is the LOOP GAIN, if T very large $A_f \cong \frac{1}{\beta}$.

2. An amplifier with an open loop gain A_{ol} of 2500 can have the following possible β values (a) 0.2; (b) 0.4; (c) 0.8; (d) 1.0. Calculate the values of the overall gain with feedback A_f in each case and compare with the limiting values of A_f when A_{ol} tends to infinity (i.e. $1/\beta$).

$$A_{ol}=2500, A_f=?$$

β	$A_f = \frac{A_{ol}}{1+A_{ol}\beta}$, for $A_{ol}=2500$	$A_f = \frac{A_{ol}}{1+A_{ol}\beta}$, for $A_{ol}=\infty$
0.2	4.99	5
0.4	2.498	2.5
0.8	1.25	1.25
1	1	1

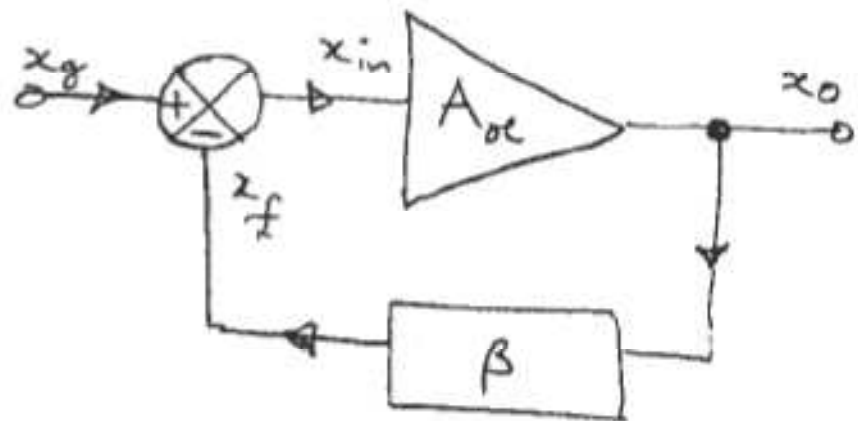
$A_{ol}\beta = T$ is the LOOP GAIN, if T is very large

$$A_f \cong \frac{1}{\beta}.$$

Closed loop gain is practically independent of amplifier open loop gain, A_{ol} , provided $A_{ol}\beta$ is big.

3. Calculate the value of x_{in} for the circuit shown in fig.P3.1 when $x_g = 1$, if $A_{ol} = 1000$, $\beta = 0.1$. Has the feedback increased or decreased x_{in} ? (Without feedback $x_{in} = x_g$). What would the limiting value of x_{in} be as A_{ol} tends to infinity?

Fig. P3.1



$$x_{in} = x_g - x_f = x_g - \beta x_o = x_g - \beta A_{ol} x_{in}$$

$$x_g = (1 + \beta A_{ol}) x_{in}$$

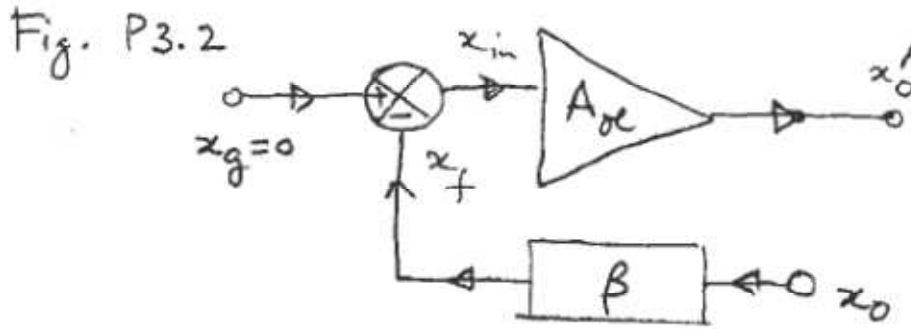
$$x_{in} = \frac{x_g}{1 + \beta A_{ol}} = 0.0099$$

The feedback reduces x_{in} !

(without feedback, $x_{in} = x_g = 1$).

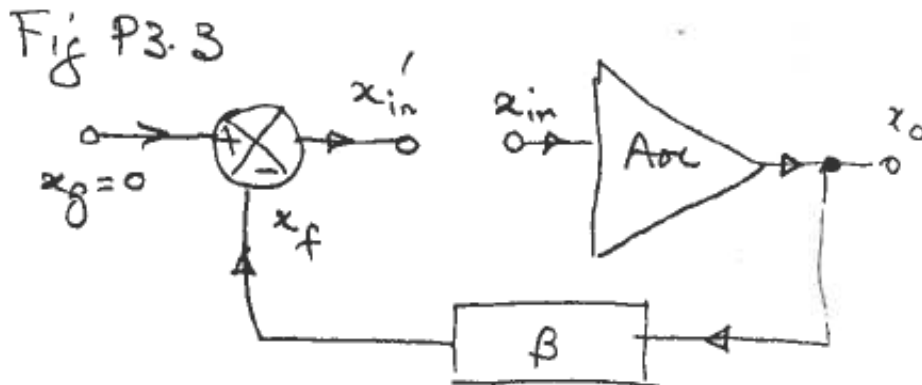
If $A_{ol} \rightarrow \infty$, $x_{in} \rightarrow 0$.

4. Consider the circuit shown in fig. P3.2, in which the input signal x_o has been reduced to zero and the feedback path is broken at the output. Calculate the ratio x'_o/x_o . Now consider the circuit shown in fig. P3.3, in which the connection between the summing junction and the amplifier input has been broken. Calculate x'_{in}/x_{in} . [In both cases, the answer is $-A_{ol}\beta$. I hope you can now see why this quantity, (without the negative sign) is called the *loop gain*.]



$$x'_o = A_{ol}x_{in} = A_{ol}(0 - x_f) = -A_{ol}\beta x_o$$

$$\frac{x'_o}{x_o} = -\beta A_{ol}$$



$$x'_{in} = (0 - x_f) = 0 - \beta x_o = -\beta A_{ol}x_{in}$$

$$\frac{x'_{in}}{x_{in}} = -\beta A_{ol}$$

$\beta A_{ol} = \text{LOOP GAIN}$ (same all the way round/ the loop).

5. An amplifier has an open loop gain of 2400 when the transistors used in its construction have a common emitter gain of 100. If the feedback fraction is $1/21$, calculate the overall gain with feedback, A_{f1} . (You will need to express your answer to 3 decimal places). If now the transistors are replaced, so that the open loop gain rises to 2600, calculate the new gain with feedback, A_{f2} . Hence calculate the fractional change in overall gain given by

$$\frac{\Delta A_f}{A_f} = \frac{A_{f2} - A_{f1}}{A_{f1}}$$

Compare this result with that using the equation given in the lecture.

$$A_{f1} = \frac{A_{ol1}}{1 + \beta A_{ol1}} = \frac{2400}{1 + \left(\frac{1}{21}\right) 2400} = 20.818$$

$$A_{f2} = \frac{A_{ol2}}{1 + \beta A_{ol2}} = \frac{2600}{1 + \left(\frac{1}{21}\right) 2600} = 20.832$$

$$\frac{\Delta A_f}{A_f} = \frac{20.832 - 20.818}{20.818} = 6.7 \cdot 10^{-4}$$

Using the formula from the lecture:

$$\frac{\Delta A_f}{A_{f1}} = \frac{1}{1 + \beta A_{ol1}} \frac{\Delta A_{ol}}{A_{ol1}} = \frac{1}{1 + 2400(\frac{1}{21})} \frac{200}{2400} \\ = 7.23 \cdot 10^{-4}$$

$$\frac{\Delta A_f}{A_{f2}} = \frac{1}{1 + \beta A_{ol2}} \frac{\Delta A_{ol}}{A_{ol2}} = \frac{1}{1 + 2600(\frac{1}{21})} \frac{200}{2600} \\ = 6.16 \cdot 10^{-4}$$

$$\frac{\Delta A_f}{A_f} = \frac{1}{2} \left(\frac{\Delta A_f}{A_{f1}} + \frac{\Delta A_f}{A_{f2}} \right) = 6.7 \cdot 10^{-4}$$

6. We found that A_f can be approximated by $1/\beta$. The error made in making this assumption can be defined as the *fractional gain error (FGE)*:

$$FGE = \frac{\left(\frac{1}{\beta} - \frac{A_{ol}}{(1 + A_{ol} \cdot \beta)}\right)}{\frac{A_{ol}}{(1 + A_{ol} \cdot \beta)}}$$

Calculate the FGE if $\beta = 1/21$ and $A_{ol} = 2400$ as a percentage.

$$FGE = 0.874\%$$

7. The feedback network is normally made up of resistors. These will have a finite tolerance, for example 1%. As a result, the value of β will be unknown to some tolerance as well. Suppose β lies in the range 0.100 ± 0.002 . What is the range of A_f expected if A_{ol} is 1600. Can you use calculus to find the answer?

$$A_{f+} = \frac{1600}{1 + 1600 \cdot 0.102} = 9.744$$

$$A_{f-} = \frac{1600}{1 + 1600 \cdot 0.098} = 10.139$$

$$A_f = \frac{1600}{1 + 1600 \cdot 0.100} = 9.94$$

Thus, $9.744 < A_f < 10.139$, i.e. $A_f = 9.94 \pm 0.1975$

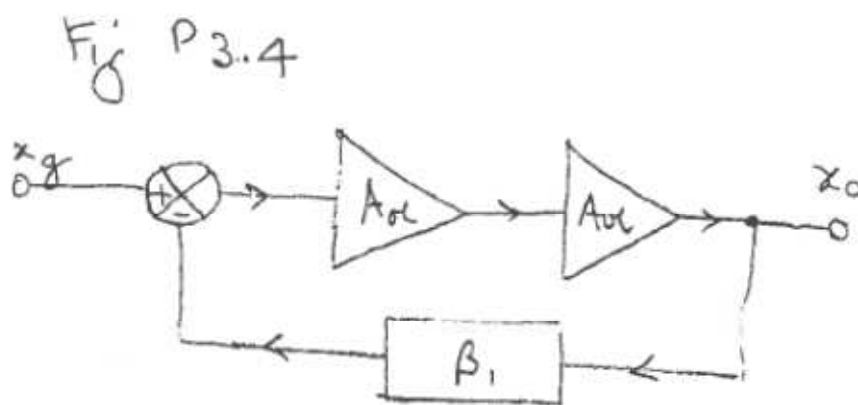
$$\frac{\Delta A_f}{A_f} = \frac{\pm 0.1975}{9.9415} \cdot 100\% = \pm 1.99\%$$

$$\frac{\Delta \beta}{\beta} = \frac{\pm 0.002}{0.1} \cdot 100\% = \pm 2\%$$

8. Calculate the overall gains with feedback x_o/x_g for the circuits shown in fig. P3.4. Show that if the overall gains of these circuits are to be the same, then

$$\beta_1 = \frac{2\beta_2}{A_{ol}} + \beta_2^2$$

Now calculate the overall gains on the assumption that A_{ol} is extremely large. Show that with this approximation the gains are equal when $\beta_1 \approx (\beta_2)^2$. If the overall gain of both circuits is to be 10 with $A_{ol} = 100$, calculate suitable values for β_1 and β_2 .



$$x_o = A_{ol}x'_{in} = A_{ol} \cdot A_{ol}x_{in} = A_{ol}^2x_{in} \quad (1)$$

$$x_{in} = x_g - x_f = x_g - \beta_1x_o \quad (2)$$

Substituting (2) in (1),

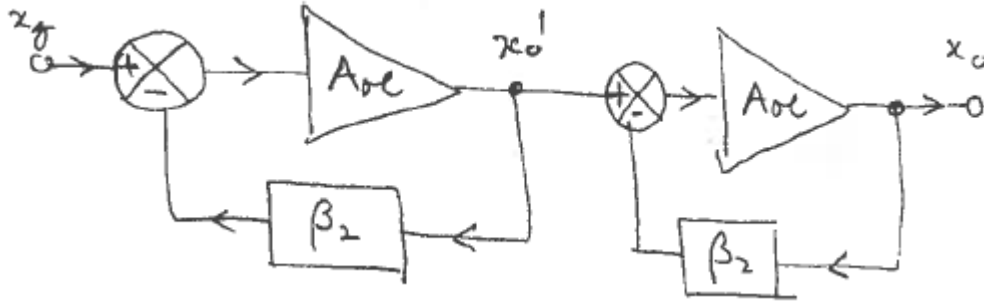
$$x_o = A_{ol}^2 \cdot [x_g - \beta_1x_o]$$

and rearranging:

$$\frac{x_o}{x_g} = \frac{A_{ol}^2}{1 + \beta_1 A_{ol}^2} \quad (3)$$

If $A_{ol} \rightarrow \infty$, then $\frac{x_o}{x_g} = \frac{1}{\beta_1}$.

Now, let's look at the 2nd circuit:



$$x_o = A_{ol}x_{in2} = A_{ol}[x_o' - \beta_2x_o] \quad (4)$$

$$x_{in2} = x_o' - \beta_2x_o \quad (5)$$

$$x_o' = A_{ol}x_{in1} \quad (6)$$

$$x_{in1} = x_g - \beta_2x_o' \quad (7)$$

Substituting (7) in (6) gives:

$$x_o' = \frac{A_{ol}}{1+\beta_2A_{ol}}x_g \quad (8)$$

Substituting (8) in (4) gives:

$$\frac{x_o}{x_g} = \frac{A_{ol}^2}{(1+\beta_2A_{ol})^2} \quad (9)$$

If $A_{ol} \rightarrow \infty$, then $\frac{x_o}{x_g} = \frac{1}{\beta_2^2}$

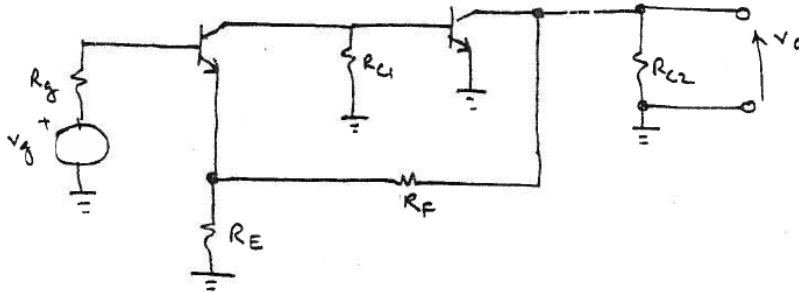
By equating (3) and (9), the following relation is obtained:

$$\beta_1 = \frac{2\beta_2}{A_{ol}} + \beta_2^2$$

For given values from Eq. (3): $\beta_1=0.1$, and from Eq. (9) $\beta_2=0.306$.

PROBLEMS II

- ③. The partial a.c equivalent circuit of an amplifier is shown below:



Calculate the overall gain (closed loop gain) $\frac{v_o}{v_g}$ assuming loop gain is very large.

A_{ol} is very large, thus $T = \beta A_{ol}$ is very large and the closed loop gain is

$$A_v \sim \frac{1}{\beta_v}$$

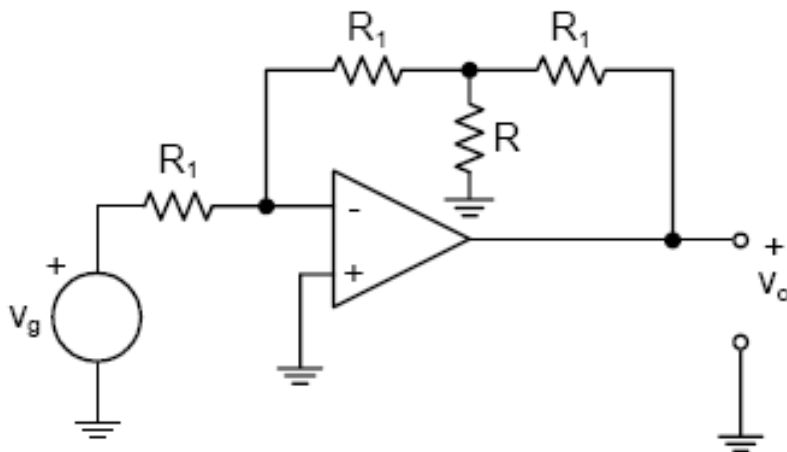
So, we need to find the feedback fraction $\beta_v = v_f/v_o$.

$$v_f = v_o \frac{R_E}{R_E + R_F}$$

$$A_v \cong \frac{R_E + R_F}{R_E}$$

PROBLEMS III

6. Find R such that $\frac{v_o}{v_g} = -100$ when $R_1 = 10k$



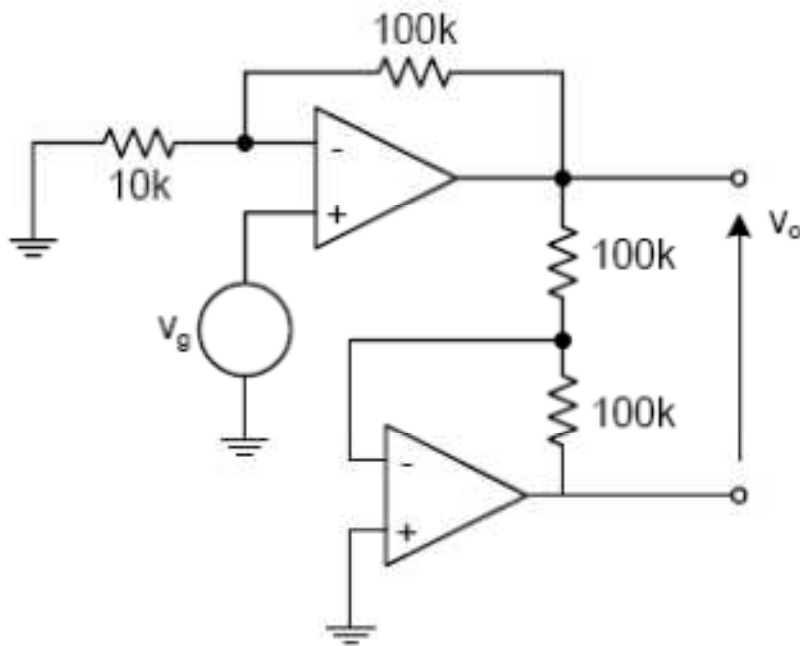
$$\frac{V_g - 0}{R_1} = \frac{0 - V}{R_1} \quad \text{so} \quad V = -V_g \quad (1)$$

$$\frac{0 - V}{R_1} = \frac{V}{R} + \frac{V - V_o}{R_1}$$

$$\frac{V_o}{V_g} = -\left(2 + \frac{R_1}{R}\right)$$

Hence $R = 102 \, \Omega$.

7. Find $\frac{v_o}{v_g}$ for



Label o/p of top op-amp as v and bottom as v'

Then $v_o = v - v'$. Also, for top op-amp, $v_n = v_p = v_g$

Then, for top op-amp: $\frac{0 - v_g}{10k} = \frac{v_g - v}{100k}$ giving $\frac{v}{v_g} = 11$

For bottom op-amp, $v_n = v_p = 0$

so $\frac{v - 0}{100k} = \frac{0 - v'}{100k}$ giving $v = -v'$

so, $v_o = v + v = 2v = 22v_g$ giving $\frac{v_o}{v_g} = 22$

*Note that $\frac{v'}{v_g} = -11$