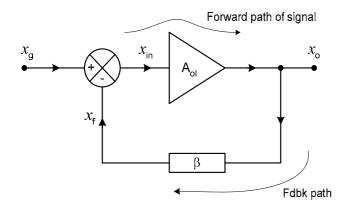
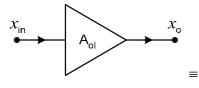
### **PART 13: Theoretical Matters**

Consider block diagram of a negative feedback amplifier system

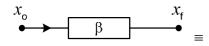


Arrows indicate signal flow direction NOT current!

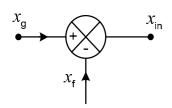
Note also that  $A_{OL}$  and  $\beta$  can  $\underline{transform}$  a signal from one type into another so the signal can be changed as it passes through different parts of the system. e.g.  $x_0$  may be a voltage whilst  $x_g$ ,  $x_f$  and  $x_{in}$  are currents, whilst in a control system,  $x_o$  might be displacement and  $x_g$ ,  $x_f$  and  $x_{in}$  a voltage.



<u>High gain amp</u> with "open loop gain"  $A_{0l} = \frac{x_0}{x_{in}}$ 



Feedback network with a "feedback fraction"  $\beta = \frac{x_f}{x_0}$ 



Input "summer"  $x_{in} = x_g - x_f$ 

Note: we use "x" because the quantities can be EITHER a voltage or a current

e.g.  $x_o$  is either  $i_o$  or  $v_o$ 

 $x_g$  is either  $i_g$  or  $v_g$   $x_{in}$  is either  $i_{in}$  or  $v_{in}$  $x_f$  is either  $i_f$  or  $v_f$ 

### Analysis - derivation of the feedback equation

$$x_{o} = A_{ol} \ x_{in}$$

$$x_{in} = x_{g} - x_{f}$$

$$= x_{g} - \beta x_{o}$$

$$\therefore x_{o} = A_{ol} \ (x_{g} - \beta x_{o}) = A_{ol} \ x_{g} - A_{ol} \ \beta x_{o}$$

$$\therefore x_{o} + A_{ol} \ \beta x_{o} = A_{ol} \ x_{g}$$

$$x_{o} = A_{ol} \ x_{g}$$
Forward path of signal

 $\therefore \frac{x_o}{x_o} = \frac{A_{ol}}{1 + A_{ol}\beta} = A_f \leftarrow \text{the "overall gain" also known as the 'closed loop gain'}$ 

$$A_f = \frac{A_{ol}}{1 + A_{ol}\beta}$$

This is the classic equation of negative feedback theory

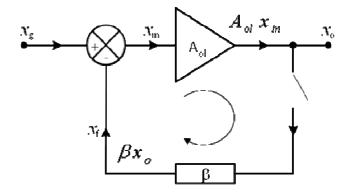
Note that the loop being referred to is the feedback loop

If the loop is broken (anywhere) then the gain given by simply going round the loop once = 'loop gain' =  $-\beta A_{ol}$  Note the negative sign is because it is negative feedback

The <u>closed loop gain</u> is the gain of the whole system when the loop is closed =  $A_{ol}$ 

The open loop gain is the gain of the system when the loop is open (i.e. no with feedback applied) =  $A_{ol}$ 

In practice, it is important that the bias conditions on the amplifier etc are not disturbed when the loop is broken. Some corrective action may be needed to compensate this.



## **Application**

Suppose we change transistors in an amplifier

Then  $A_{ol}$  will change to  $A_{ol} + \Delta A_{ol}$ And  $A_f$  will change to  $A_f + \Delta A_f$  How big is  $\Delta A_f$ ??

# **Proof:** Change in $A_f$ due to a change in $A_{ol}$

We know that 
$$A_f = \frac{A_{ol}}{1 + A_{ol}\beta}$$

Suppose change in  $A_{ol}$  is  $\Delta A_{ol}$ , what is change in  $A_f$ ?

Problem can be solved using a bit of calculus provided  $\Delta A_{ol}$  is small. (an alternative method is shown in problem 5).

First take logs of both sides:-

$$\ln(A_f) = \ln(A_{ol}) - \ln(1 + A_{ol} \beta)$$

Then differentiate both sides with respect to  $A_{ol}$  -since we are interested in the effects of changing  $A_{ol}$ , and remembering  $\beta$  is a constant gives:

$$\frac{1}{A_f} \frac{dA_f}{dA_{ol}} = \frac{1}{A_{ol}} - \frac{\beta}{1 + A_{ol}\beta} = \frac{1}{(1 + A_{ol}\beta)A_{ol}}$$

Letting  $\Delta A_{ol}$  approximate to  $dA_{ol}$  and  $\Delta A_{f}$  approximate to  $dA_{f}(OK \text{ if they are small!})$ , gives

$$\boxed{\frac{\Delta A_f}{A_f} = \frac{1}{1 + A_{ol}\beta} \frac{\Delta A_{ol}}{A_{ol}}}$$

ie % change in  $A_f$  is smaller than % change in  $A_{ol}$ ! by a factor  $1 + A_{ol}\beta$ 

**Example** Let  $A_{ol} = 10^3$  and  $\beta = 0.05$ 

Then 
$$A_f = \frac{A_{ol}}{1 + A_{ol} \beta} = \frac{10^3}{1 + 10^3 \times 0.05} = 19.61$$

Assume  $A_{ol}$  changes to 1100, so  $\Delta A_{ol} = 100$ 

Then formula gives 
$$\frac{\Delta A_f}{19.61} = \frac{1}{1+10^3 \times 0.05} \times \frac{100}{10^3}$$
  $\therefore \Delta A_f = 0.04$ 

So when  $A_{ol}$  changes from 1000  $\rightarrow$ 1100,  $A_f$  changes from 19.61 $\rightarrow$ 19.65

ie only **0.2%** increase in  $A_f$ , while  $A_{ol}$  change was 10%!!

- Negative feedback has stabilised the overall gain of the amplifier against changes in component values of amplifier itself.

### **Alternative Picture**

We can write 
$$A_f = \frac{A_{ol}}{1 + A_{ol}\beta}$$

As 
$$A_f = \frac{1}{\beta} \frac{A_{ol} \beta}{1 + A_{ol} \beta}$$

Provided 
$$A_{ol} \beta > 100$$
, then  $\frac{A_{ol} \beta}{1 + A_{ol}} \approx 1$  to <1%

$$A_f = \frac{1}{\beta} \text{ to } < 1\%$$

# **Important Conclusion**

Equation 
$$A_f \cong \frac{1}{\beta}$$

means that:

- 1. <u>closed loop gain</u> is practically <u>independent</u> of amplifier open loop gain  $A_{ol}$  provided  $A_{ol}$   $\beta$  is big
- 2.  $A_f$  is determined solely by feedback network only (since this controls  $\beta$ ).

Important quantity  $A_{ol} \beta$  is called the **loop gain** and we often write it as 'T'

It's worth thinking about the relation,  $T = A_{ol}\beta$ . In op-amps we have VERY high open-loop gain  $(A_{ol})$  so we can 'afford' to throw some of it away by feedback  $(\beta)$  because we can still usually maintain a large enough 'T' to make our simple approximation valid.

#### **Exercises**

You will find a set of exercises entitled 'S2 Problems 1' on VITAL, together with worked solutions. You are encouraged to attempt these questions which start with simply substituting numbers into equations to build familiarity with concepts. Later questions require a little more thought but should not take you much time.

It is very important you work through this problems sheet, which forms an integral part of the module.