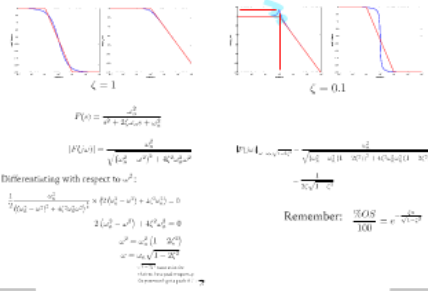


Bode Plots for Second Order Systems - Revisited

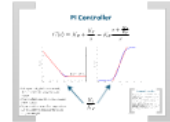


Frequency Response of PI

Consider a plant, $P(s)$, and controller, $C(s)$.
Open loop magnitude and phase responses are then:

$$20 \log_{10} |C(j\omega)P(j\omega)| = 20 \log_{10} |C(j\omega)| + 20 \log_{10} |P(j\omega)|$$

$$\angle C(j\omega)P(j\omega) = \angle C(j\omega) + \angle P(j\omega)$$



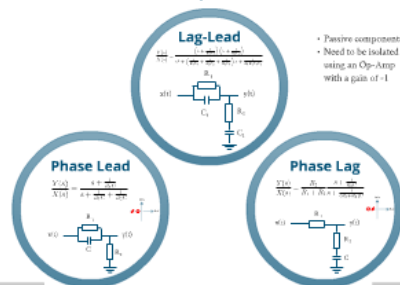
ELEC 207 Part B

Control Theory Lecture 13: Frequency Design (1)

Prof Simon Maskell
CHAD-G68
s.maskell@liverpool.ac.uk
0151 794 4573



Electronic Compensator Circuits



This lecture covers:
• Combining Controller and Process Frequency Response
• Frequency Response of PI
• Phase-lead and Phase-lag compensators

ELEC 207 Part B

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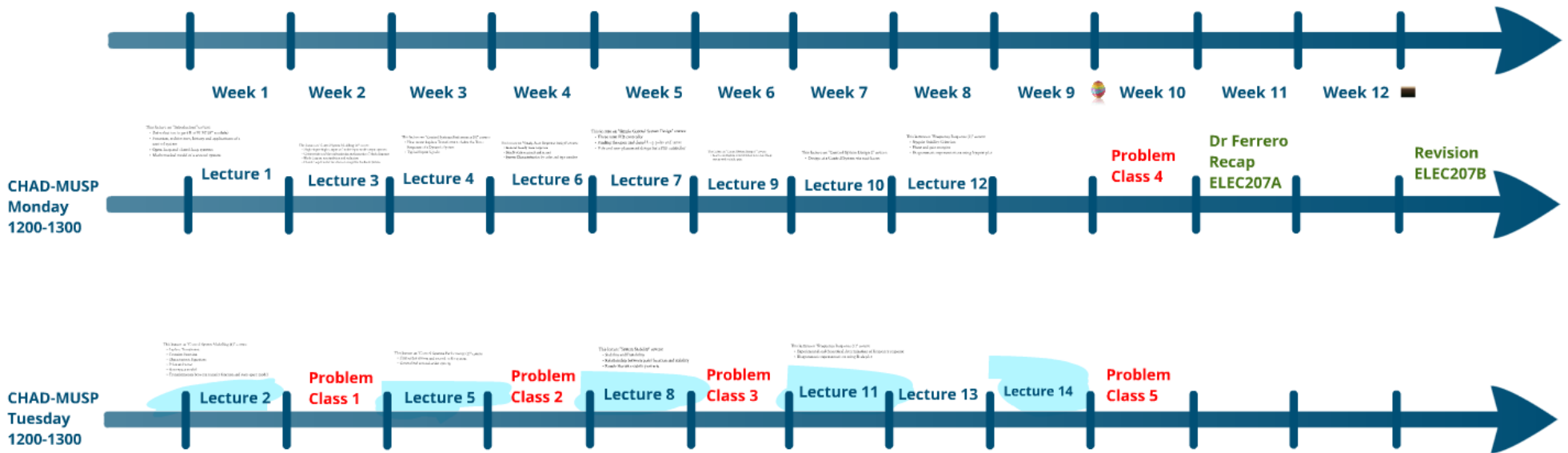
UNIVERSITY OF
LIVERPOOL

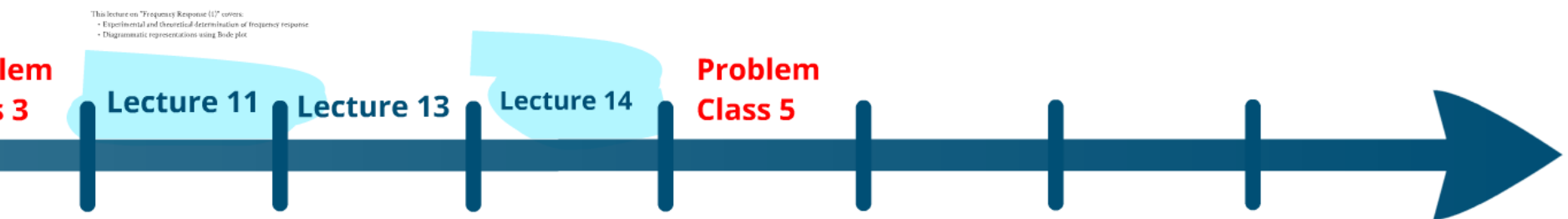
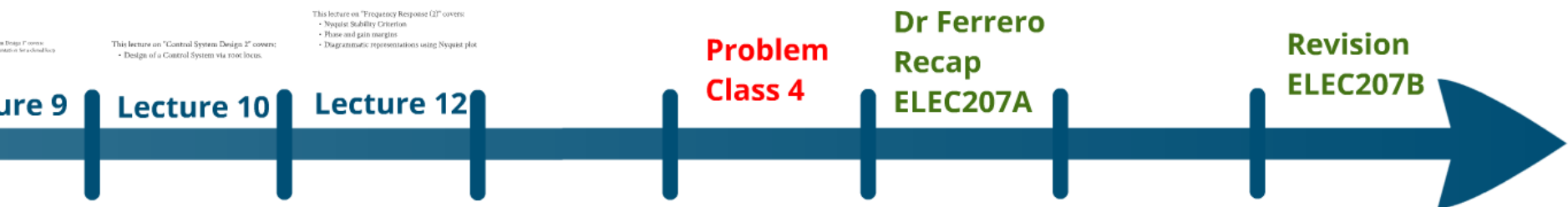
This lecture covers:

- Combining Controller and Process Frequency Response
- Frequency Response of PI
- Phase-lead and Phase-lag compensators



ELEC 207B: Timeline



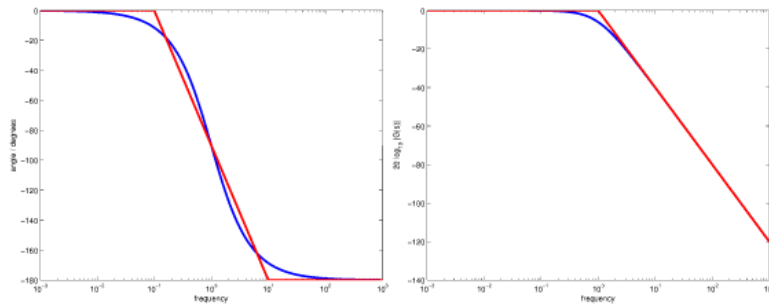


This lecture covers:

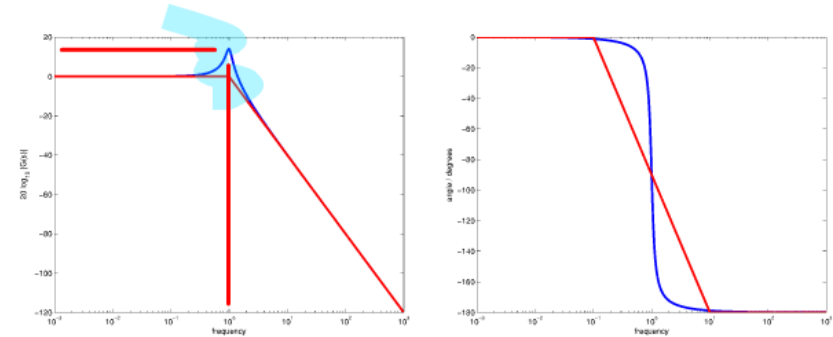
- Combining Controller and Process Frequency Response
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Bode Plots for Second Order Systems - Revisited



$$\zeta = 1$$



$$\zeta = 0.1$$

$$F(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$|F(j\omega)| = \frac{\omega_n^2}{\sqrt{(\omega_n^2 - \omega^2)^2 + 4\zeta^2\omega_n^2\omega^2}}$$

$$\begin{aligned} |F(j\omega)|_{\omega=\omega_n\sqrt{1-2\zeta^2}} &= \frac{\omega_n^2}{\sqrt{(\omega_n^2 - \omega_n^2(1-2\zeta^2))^2 + 4\zeta^2\omega_n^2\omega_n^2(1-2\zeta^2)}} \\ &= \frac{1}{2\zeta\sqrt{1-\zeta^2}} \end{aligned}$$

Differentiating with respect to ω^2 :

$$\frac{1}{2} \frac{\omega_n^2}{((\omega_n^2 - \omega^2)^2 + 4\zeta^2\omega_n^2\omega^2)^{\frac{3}{2}}} \times (2(\omega_n^2 - \omega^2) + 4\zeta^2\omega_n^2) = 0$$

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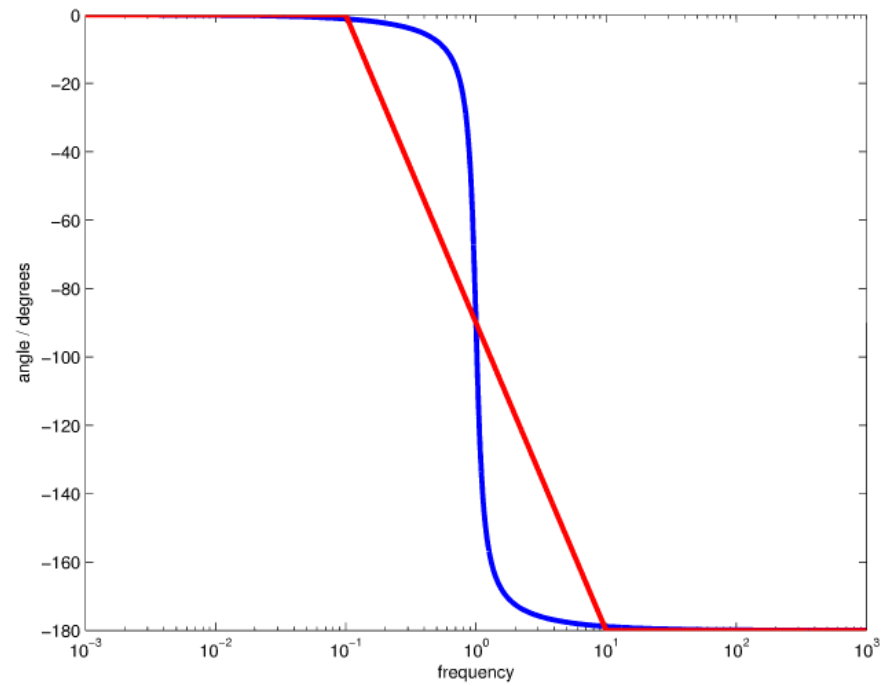
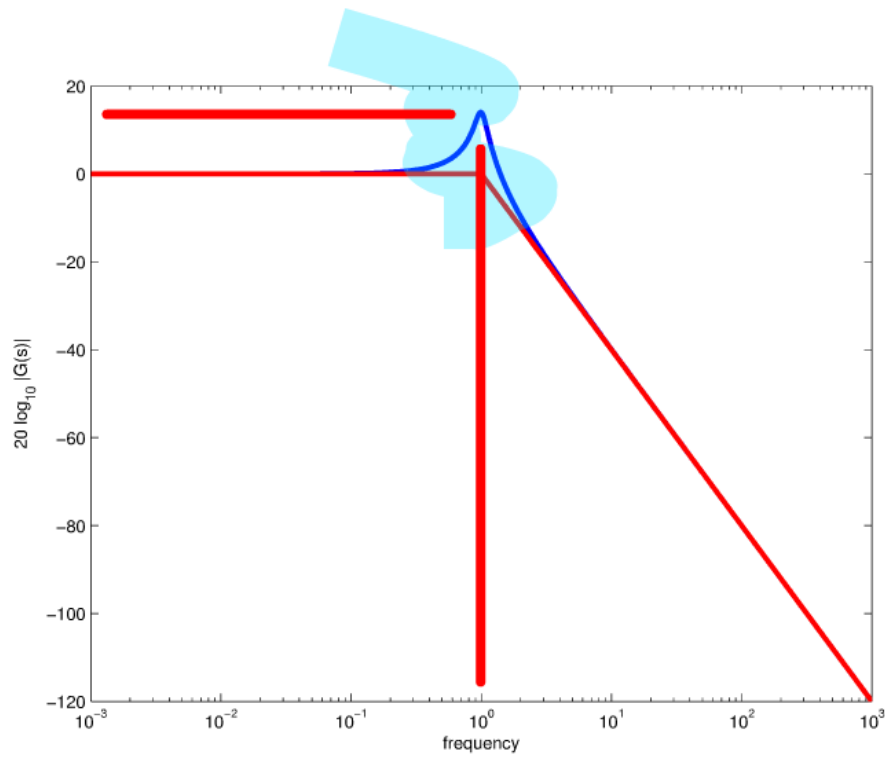
$$\omega^2 = \omega_n^2(1 - 2\zeta^2)$$

$$\omega = \omega_n\sqrt{1 - 2\zeta^2}$$

$\sqrt{1 - 2\zeta^2}$ must exist for
their to be a peak frequency
(ie you won't get a peak if $\zeta > \frac{1}{\sqrt{2}}$)

Remember: $\frac{\%OS}{100} = e^{-\frac{\zeta\pi}{\sqrt{1-\zeta^2}}}$

Order Systems - Revisited



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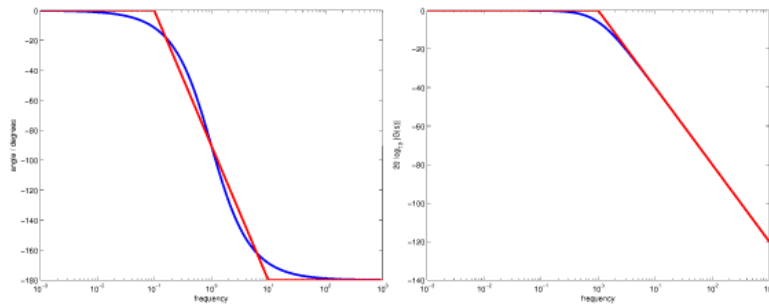
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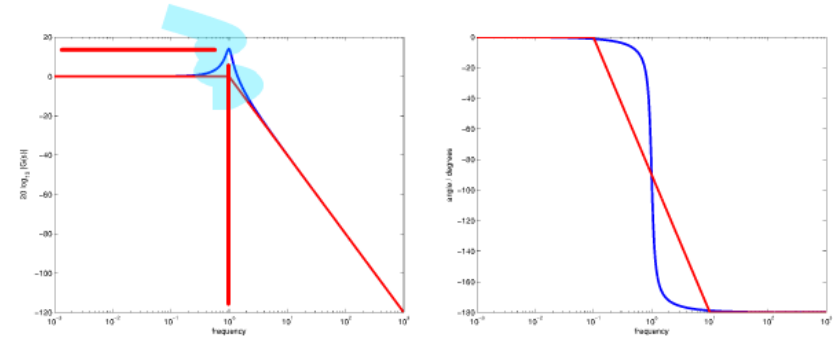
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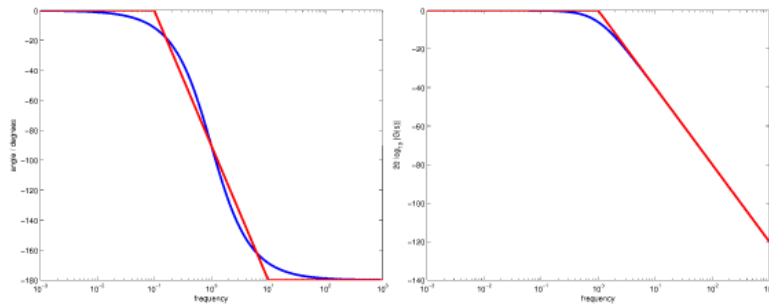
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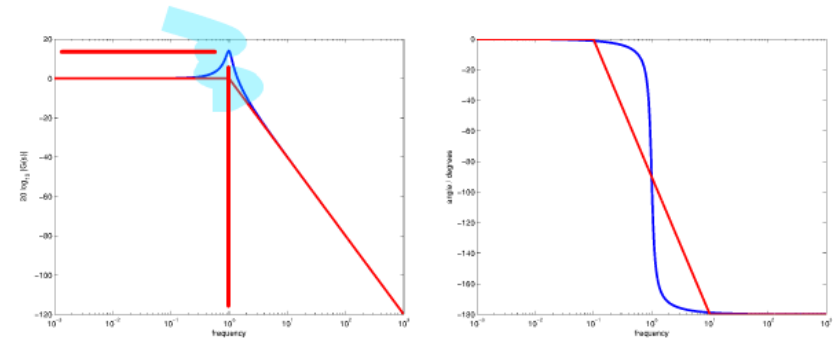
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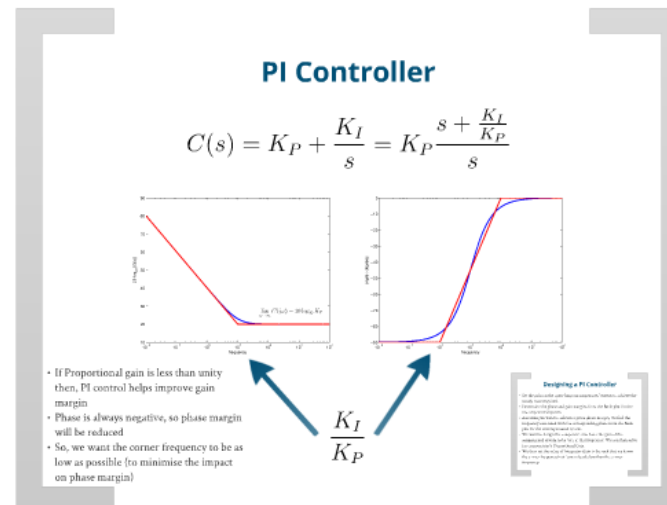
Frequency Response of PI

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Open loop magnitude and phase responses are then:

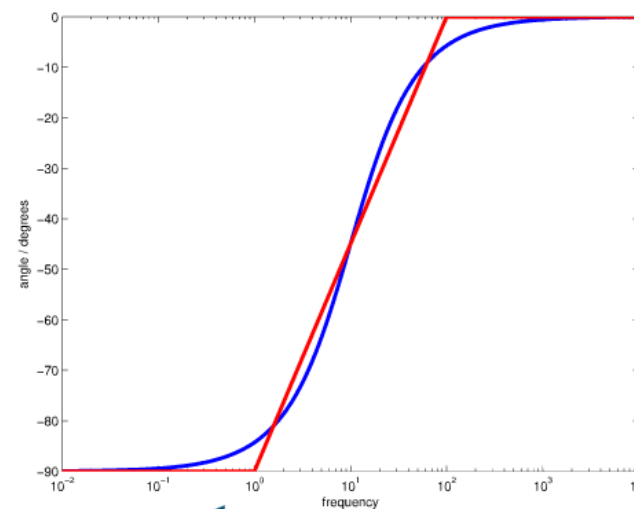
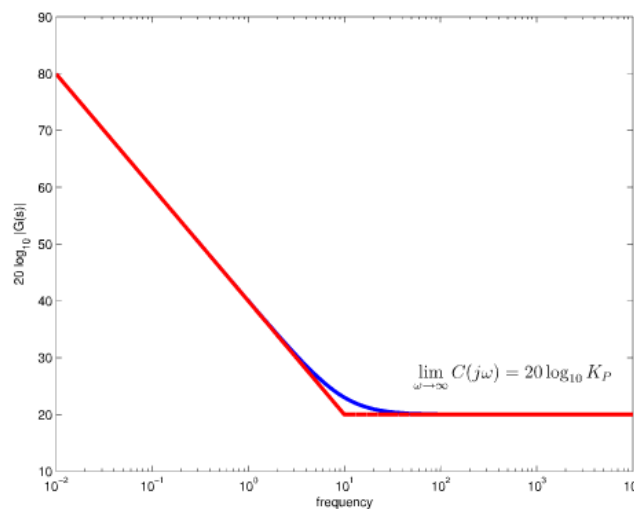
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PI Controller

$$C(s) = K_P + \frac{K_I}{s} = K_P \frac{s + \frac{K_I}{K_P}}{s}$$

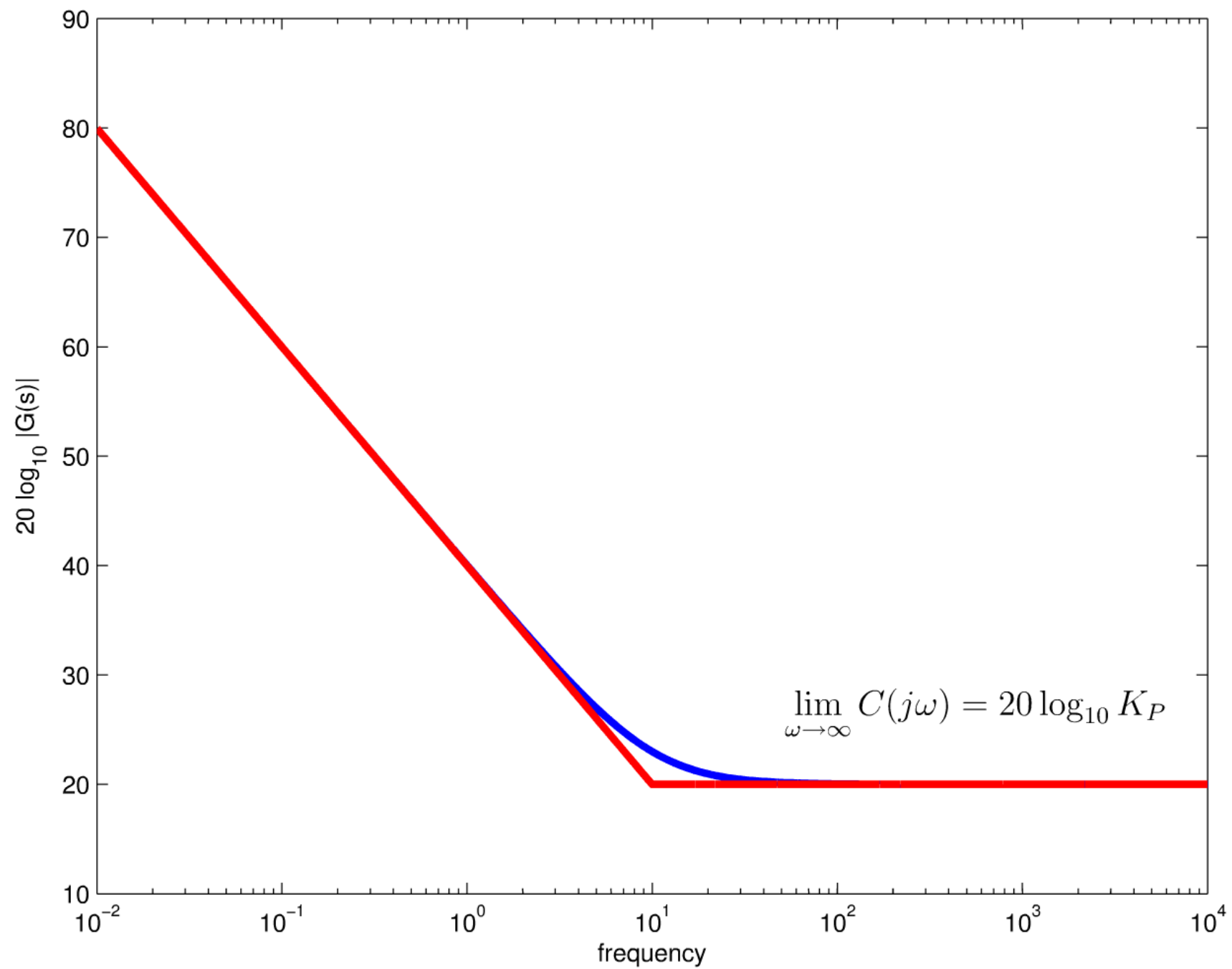



- If Proportional gain is less than unity then, PI control helps improve gain margin
- Phase is always negative, so phase margin will be reduced
- So, we want the corner frequency to be as low as possible (to minimise the impact on phase margin)

$$\frac{K_I}{K_P}$$

Designing a PI Controller

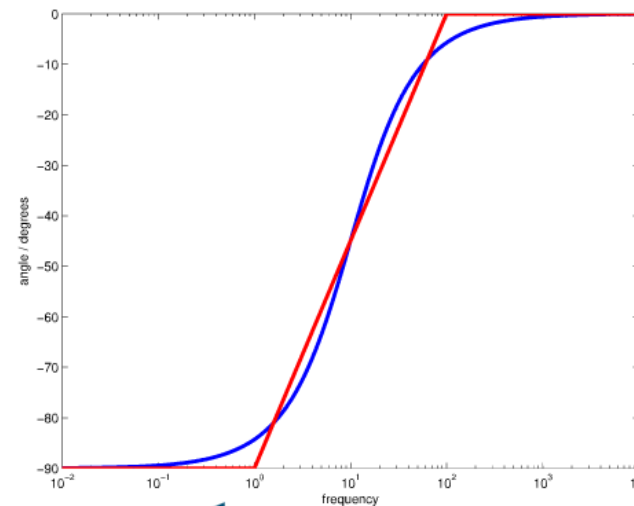
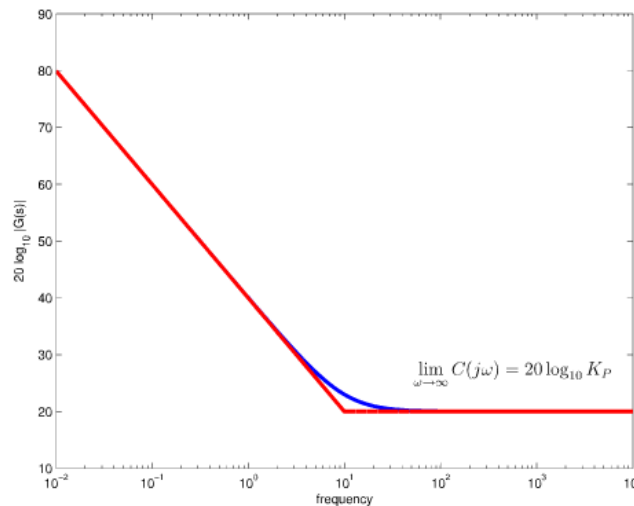
- Set the gain on the open-loop uncompensated system to achieve the steady-state required.
- Determine the phase and gain margins from the Bode plot for the uncompensated system.
- Assuming we want to achieve a given phase margin, we find the frequency associated with the corresponding phase from the Bode plot for the uncompensated system.
- We want to design the compensator to force the gain of the compensated system to be zero at that frequency. We can then solve for compensator's Proportional Gain
- We then set the value of Integrator Gain to be such that we know the corner frequency is at least a decade less than the corner frequency



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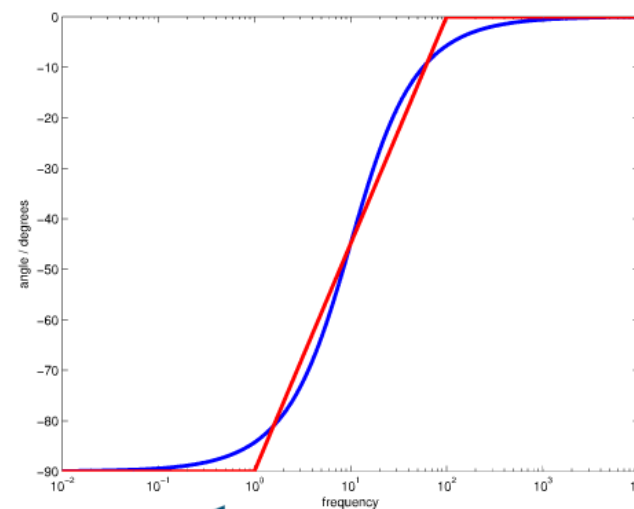
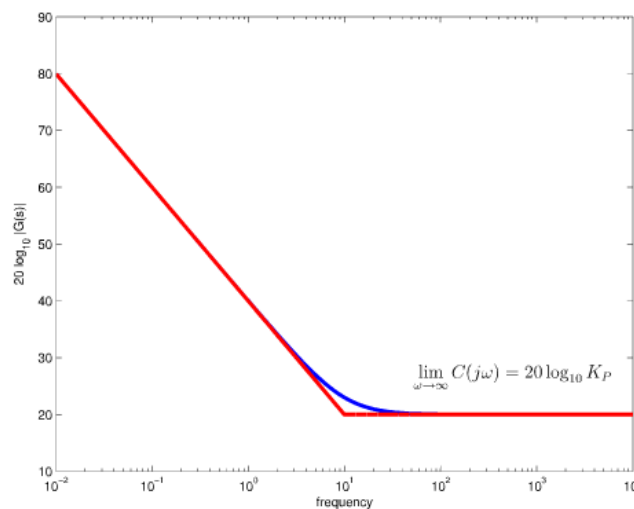
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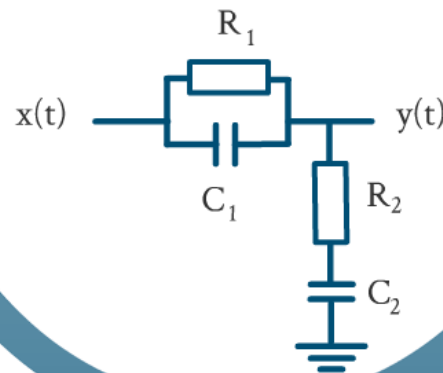
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Electronic Compensator Circuits

Lag-Lead

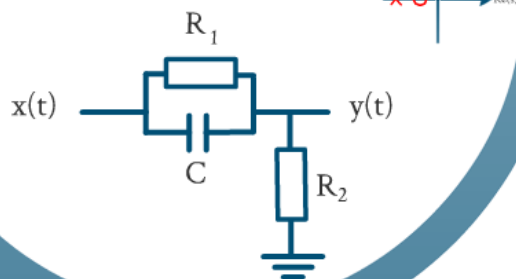
$$\frac{Y(s)}{X(s)} = \frac{\left(s + \frac{1}{R_1 C_1}\right) \left(s + \frac{1}{R_2 C_2}\right)}{s^2 + \left(\frac{1}{R_1 C_1} + \frac{1}{R_2 C_2} + \frac{1}{R_2 C_1}\right) s + \frac{1}{R_1 R_2 C_1 C_2}}$$



- Passive components
- Need to be isolated using an Op-Amp with a gain of -1

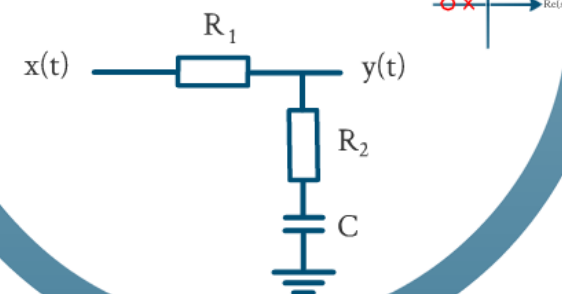
Phase Lead

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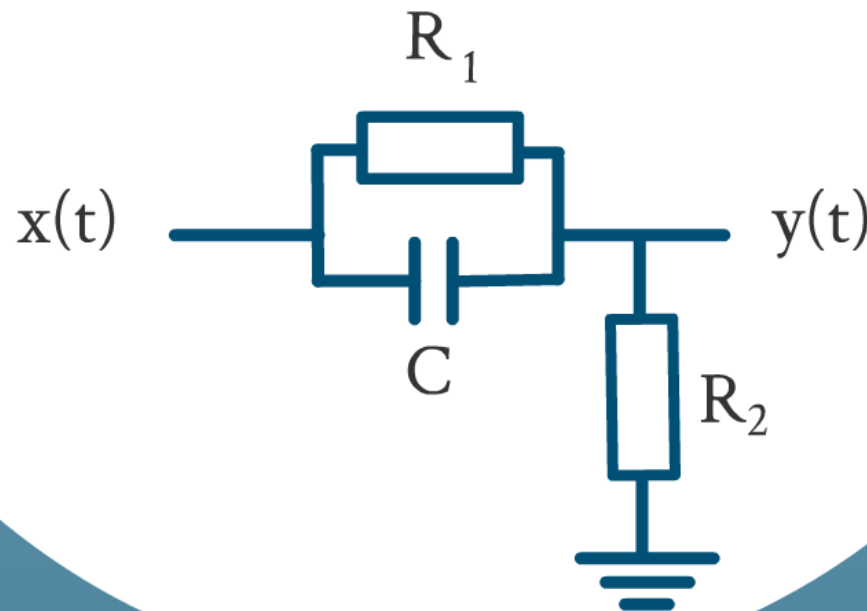
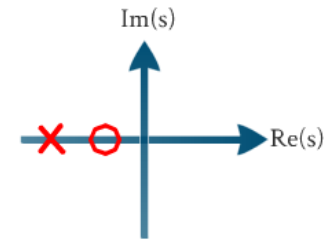
Phase Lag

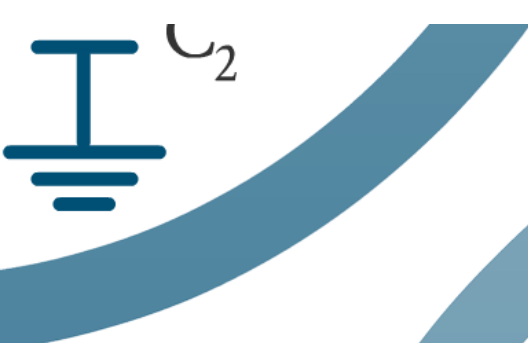
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Phase Lead

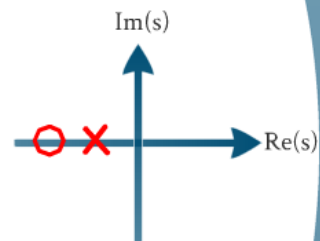
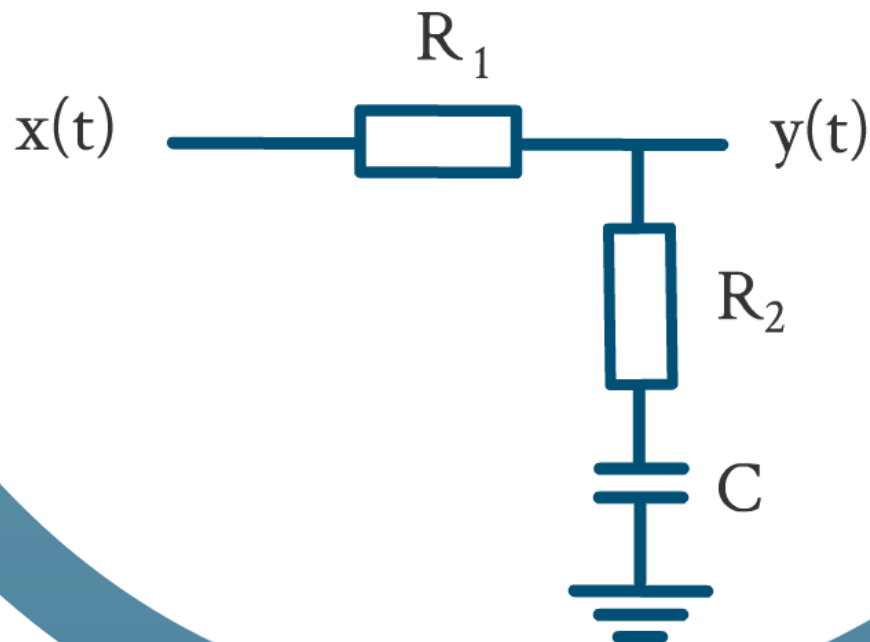
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Phase Lag

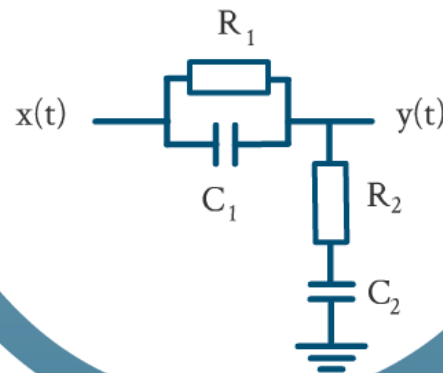
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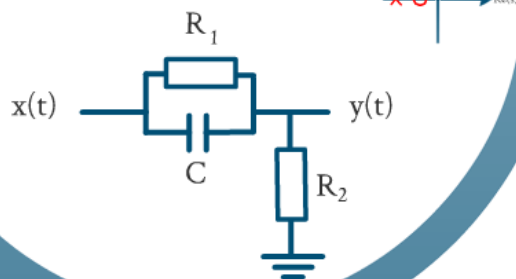
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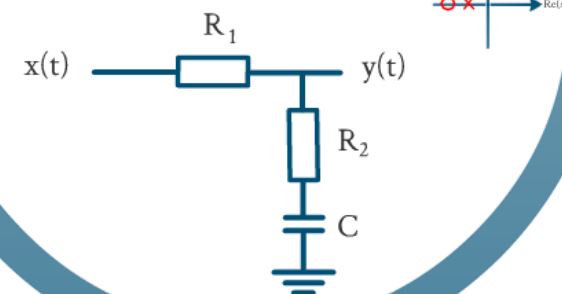
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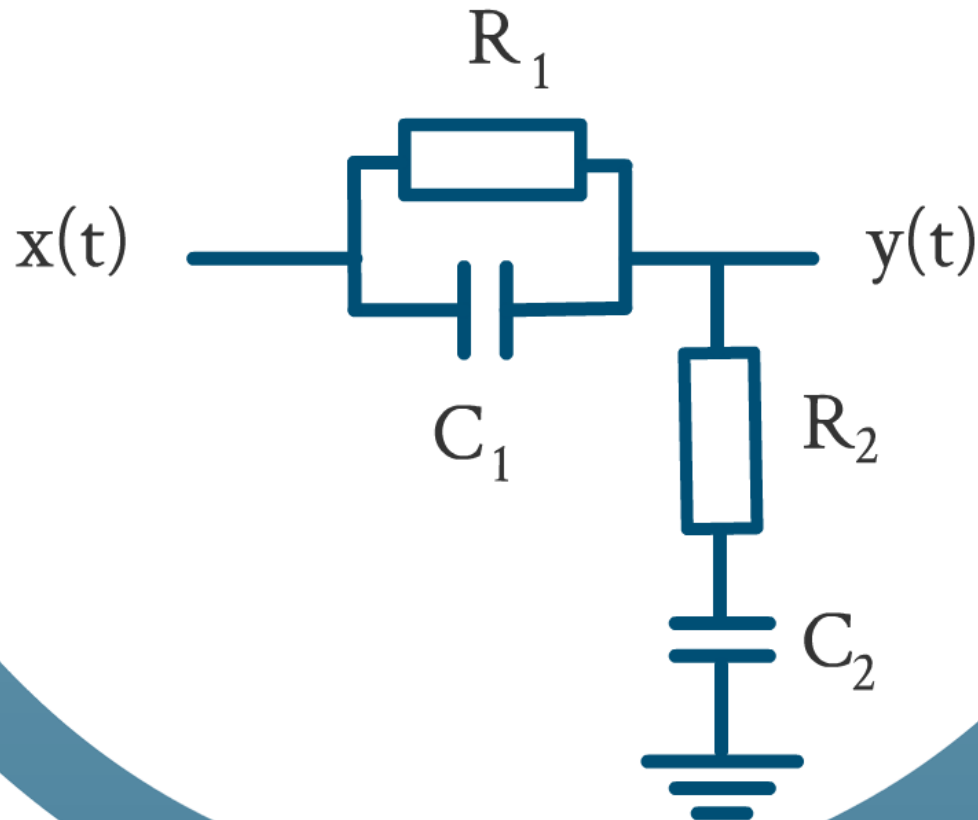
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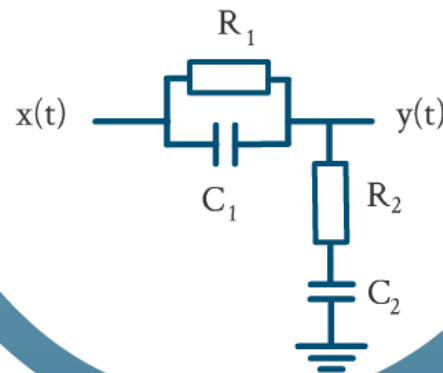


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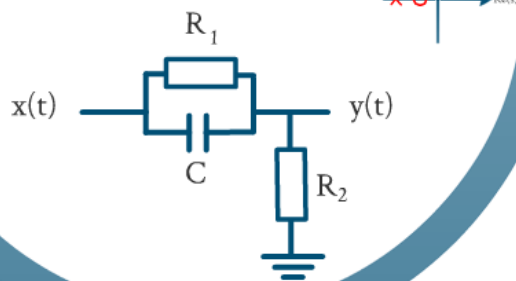
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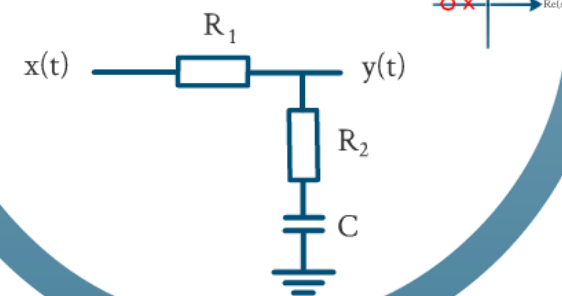
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