

The closed-loop transfer function is  $T(s) = \frac{Y(s)}{X(s)}$ .  
 The closed-loop poles are the roots of the denominator polynomial  $1 + KG(s) = 0$ .  
 The closed-loop poles are the roots of the characteristic equation.

# ELEC 207 Part B

## Control Theory Lecture 9: Control System Design (1)

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## Root Locus

### Number of Branches

- A branch is the path that one pole traverses.
- There are as many branches as there are closed-loop poles.

### Start and End Points

$$1 + KG(s) = 0 \quad G(s) = \frac{N(s)}{D(s)}$$

$$P(s) + KZ(s) = 0$$

So, if we vary  $K$ , the closed-loop poles will move from the open-loop poles (at  $K=0$ ) to the open-loop zeros (at  $K=\infty$ ).

### Angles of Departure and Arrival

- Imagine a point on the root locus that is a tiny distance away from an open-loop pole. We know that the angle must add up to an odd multiple of  $180^\circ$ .
- We can solve for the angle between the point that is a tiny distance away from the open-loop pole. This enables us to find the angle of departure and arrival of complex poles and zeros.

### Symmetry

- If a pole has an imaginary part, there will be a complex conjugate pole. So, we know that the root locus is symmetric about the real axis.



$$\frac{Y(s)}{X(s)} = \frac{KG(s)}{1 + KG(s)}$$

### Imaginary Axis Crossings

- We know that poles in the RHP will cause instability. We can use the Routh-Hurwitz criteria to find  $K$ .
- We find a  $K$  that forces a zero in the Routh-Hurwitz table to be zero.
- The associated auxiliary equation can then be solved for  $s$ .

### Real-axis Segments

$$G(s) = \frac{N(s)}{D(s)} \quad N(s) = (s - z_1)(s - z_2) \dots (s - z_m) \quad D(s) = (s - p_1)(s - p_2) \dots (s - p_n)$$

$$1 + KG(s) = 0 \quad 1 + K \frac{N(s)}{D(s)} = 0 \quad D(s) + KN(s) = 0$$

$$\sum_{i=1}^m \frac{1}{s - z_i} - \sum_{j=1}^n \frac{1}{s - p_j} = 0$$

The real-axis segments are the segments of the real axis where the number of poles to the right of the point is odd.

### Infinite Zeros

The number of infinite zeros is the number of poles minus the number of zeros.

$$n_z = n_p - n_z$$

### Real-Axis Breakaway Points

- $K$  is a local maximum or minimum when the root locus breaks away from the real axis. So, we can differentiate  $K$  with  $s$ , set to zero and solve for  $s$ .

*This lecture covers:*  
• Root locus diagram representation for a closed loop system with variable gain.

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## Control Theory Lecture 9: Control System Design (1)

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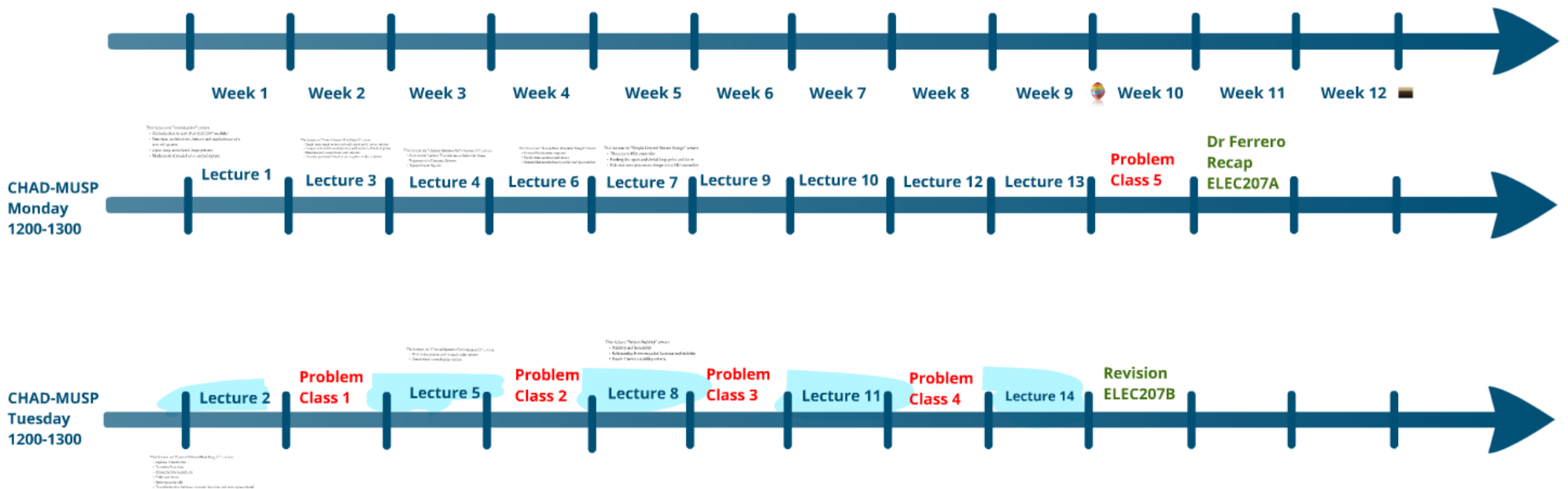
UNIVERSITY OF  
LIVERPOOL

This lecture covers:

- Root locus diagram representation for a closed loop system with variable gain.



# ELEC 207B: Timeline



This lecture covers:

- Root locus diagram representation for a closed loop system with variable gain.



# Root Locus

## Number of Branches

- A **branch** is the path that one pole traverses.
- There are as many branches as there are closed-loop poles.

## Start and End Points

$$1 + KG(s) = 0 \quad G(s) = \frac{Z(s)}{P(s)}$$

$$P(s) + KZ(s) = 0$$

- So, if we vary K, the closed-loop poles will move from the open-loop poles (at K=0) to the open-loop zeros (at K=∞).



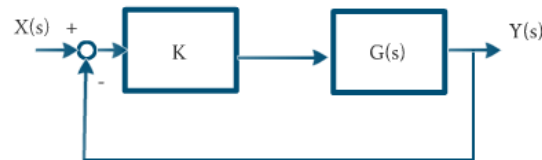
## Angles of Departure and Arrival

- Imagine a point on the root locus that is a tiny distance  $\epsilon$  away from an open-loop pole. We know that the angles must add up to an odd multiple of  $180^\circ$ .
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## Symmetry

- If a pole has an imaginary part, there will be a complex conjugate pole. So, we know that the root locus is symmetric about the real axis.



$$\frac{Y(s)}{X(s)} = \frac{KG(s)}{1 + KG(s)}$$

## Imaginary Axis Crossings

- We know that poles in the RHP will cause instability. We can use the Routh-Hurwitz criteria to find K.
- We find a K that forces a row in the Routh-Hurwitz table to be zero.
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## Real-axis Segments

$$KG(s) = -1 \quad \angle G(s) = -180 \pm k360$$

$$G(s) = K \frac{\prod_{i=1}^m (s - z_i)}{\prod_{j=1}^n (s - p_j)} \quad \angle(a \times b) = \angle a + \angle b$$

$$\angle G(s) = \angle Z(s) - \angle P(s)$$

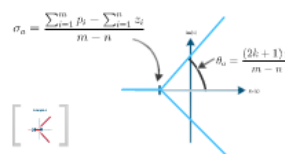
$$= \sum_{i=1}^m \angle(s - z_i) - \sum_{j=1}^n \angle(s - p_j) = -180 \pm k360$$

- For any point on the real axis, the contribution from any complex conjugate poles (or zeros) will cancel each other out.
- For two values of s on the real axis and either side of a zero or a pole, then they will have values of  $\angle G(s)$  that differ by  $180^\circ$ .
- More precisely, the root locus exists at s on the real-axis to the left of an odd total number of real-axis open-loop poles and open-loop zeros.



## Infinite Zeros

- If  $n < m$  then there are more poles than there are (finite) zeros. The poles move from the open-loop poles to the open-loop zeros, so we have to think what happens when  $|s| \rightarrow \infty$ .
- As  $|s| \rightarrow \infty$ , the locus will asymptote to straight lines

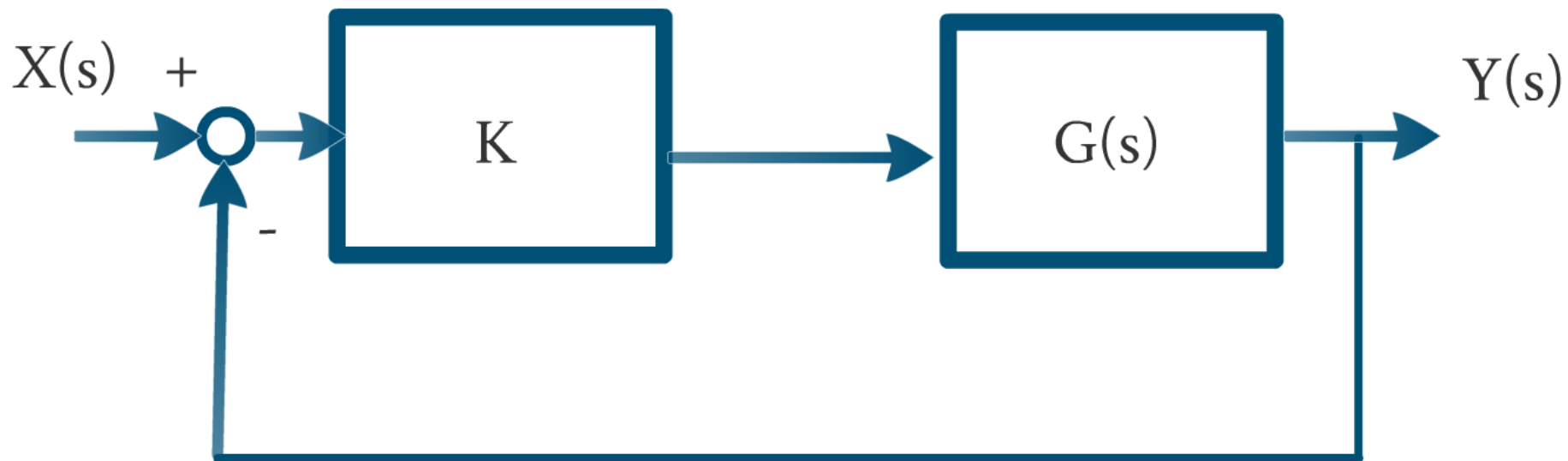


## Real-Axis Breakaway Points

$$K = \frac{1}{|G(s)|}$$

- K is a local maximum or minimum when the root locus breaks away from the real axis. So, we can differentiate K wrt s, set to zero and solve for  $\sigma$ .





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# Root Locus

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## Start and End Points

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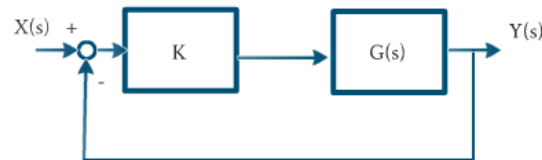
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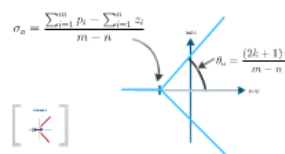
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## Infinite Zeros

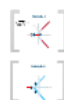
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- As  $|s| \rightarrow \infty$ , the locus will asymptote to straight lines



## Real-Axis Breakaway Points

$$K = \frac{1}{|G(s)|}$$

- K is a local maximum or minimum when the root locus breaks away from the real axis. So, we can differentiate K wrt s, set to zero and solve for  $\sigma$ .





# Start and End Points

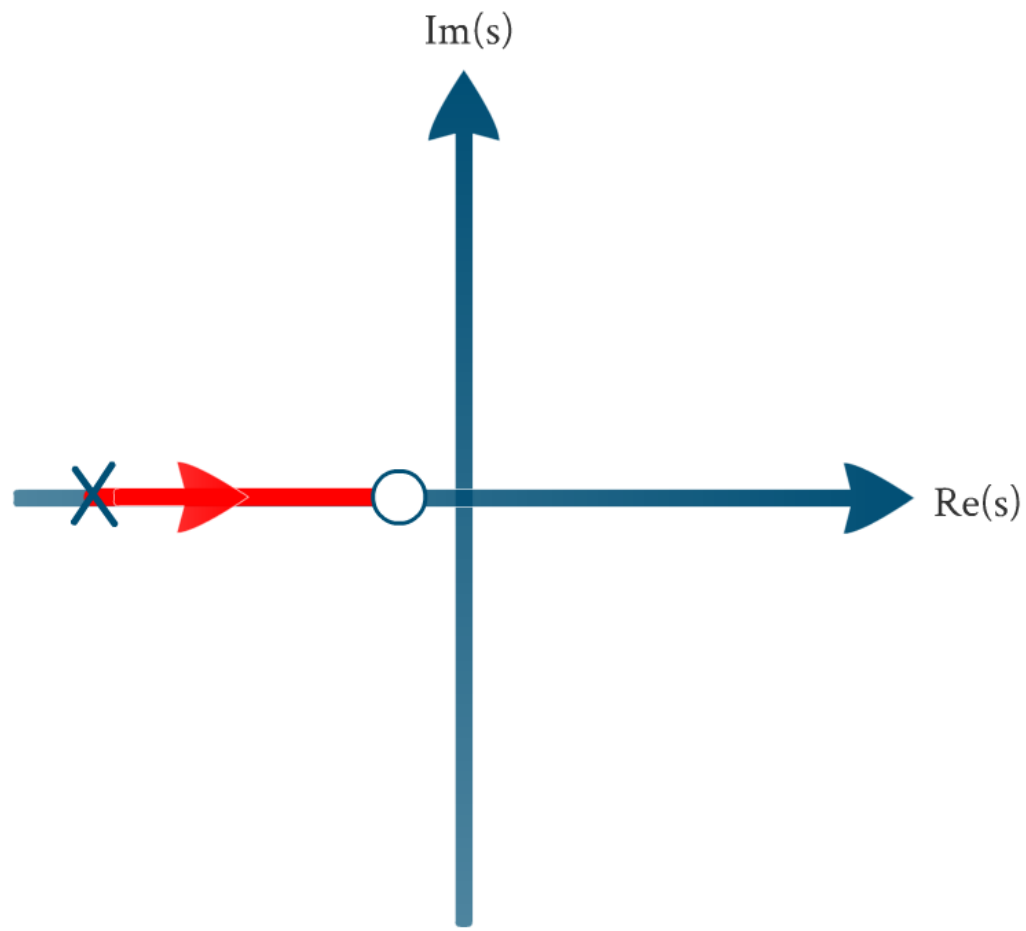
$$1 + K G(s) = 0 \qquad G(s) = \frac{Z(s)}{P(s)}$$

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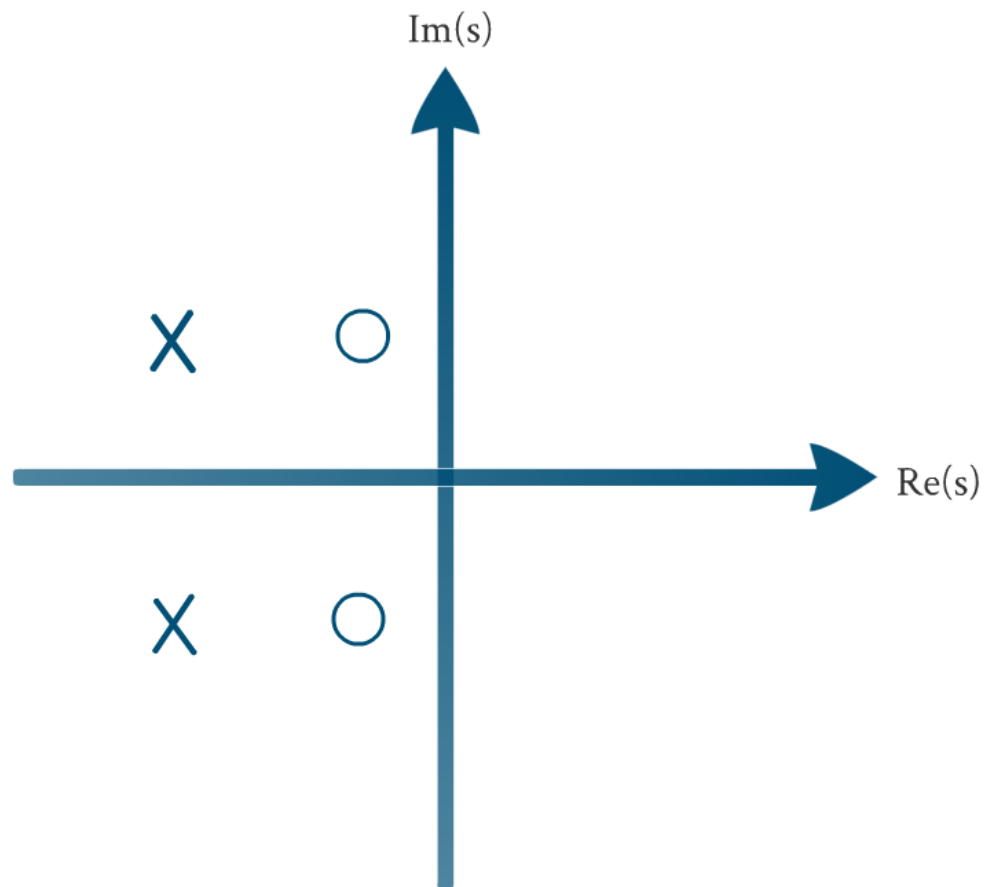
- So, if we vary K, the closed-loop poles will move from the open-loop poles (at K=0) to the open-loop zeros (at K=∞).



# Example 1



# Example 2



# Start and End Points

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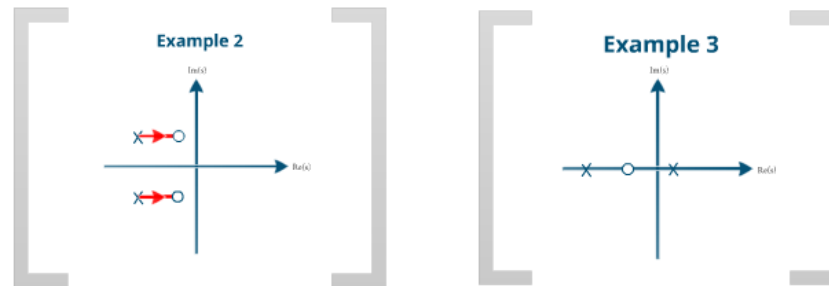


# Number of Branches

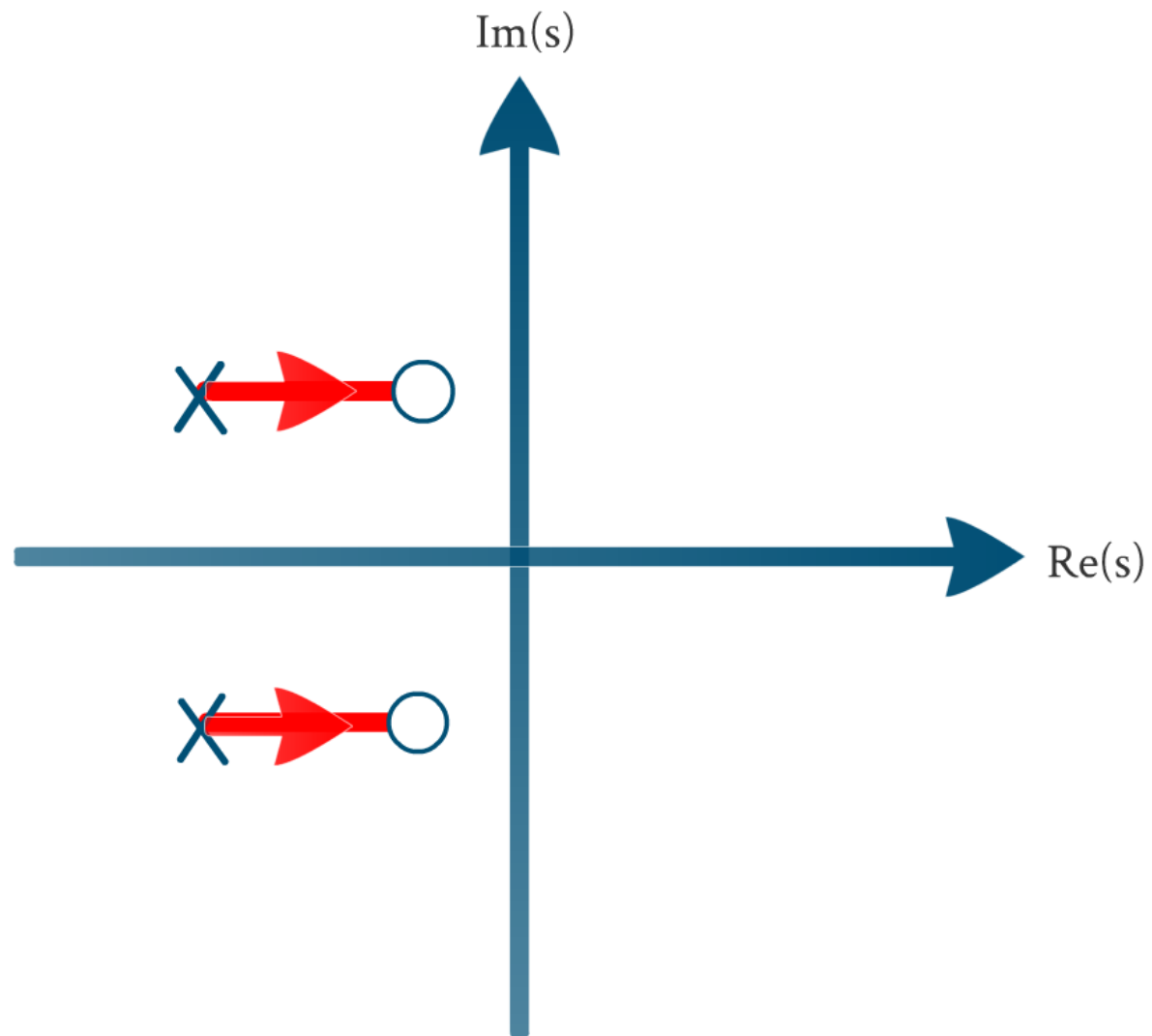
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# Symmetry

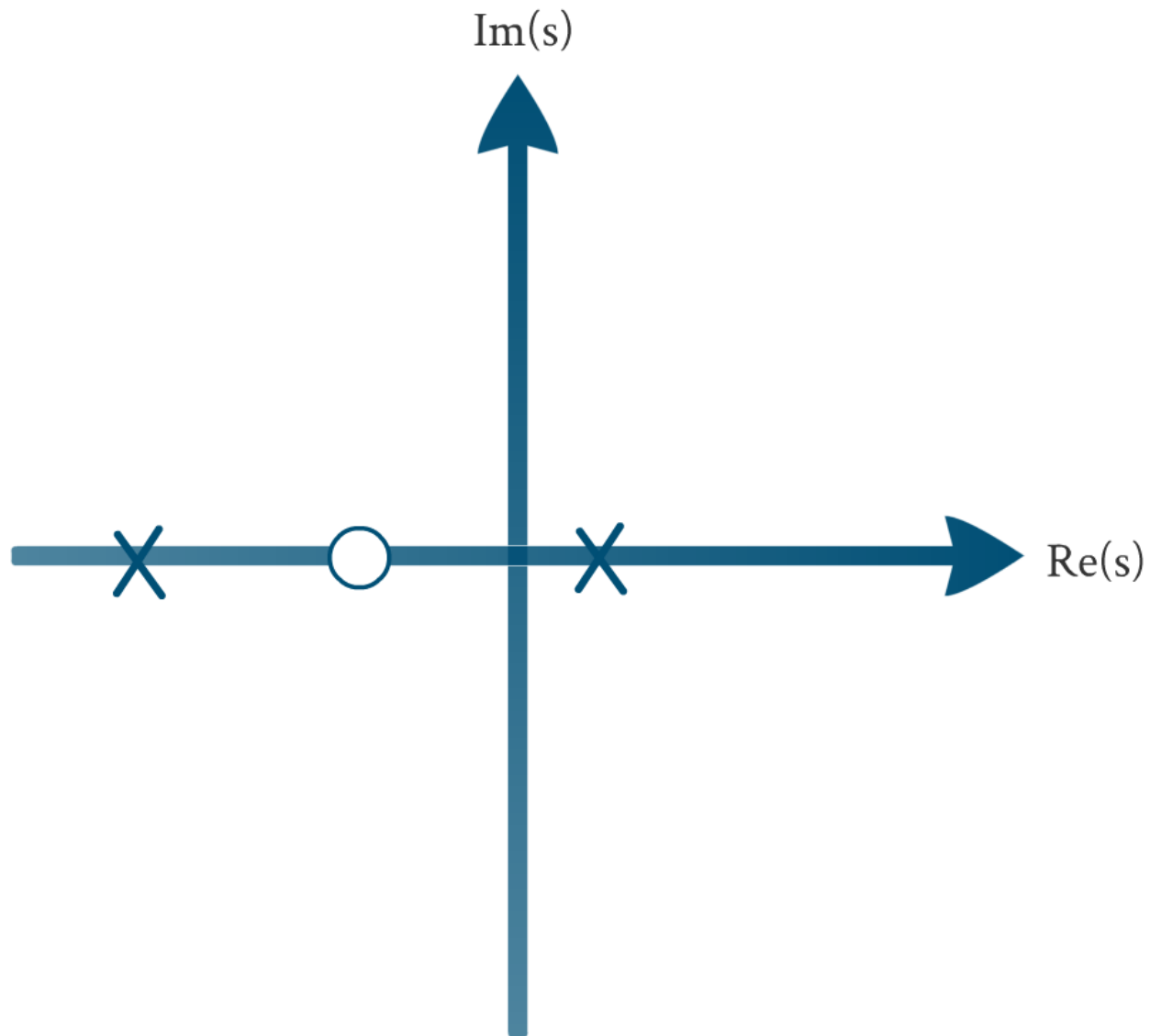
- If a pole has an imaginary part, there will be a complex conjugate pole. So, we know that the root locus is symmetric about the real axis.



## Example 2



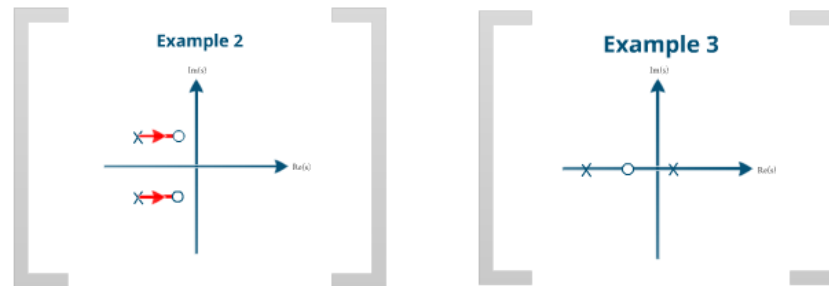
# Example 3





# Symmetry

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# Real-axis Segments

$$KG(s) = -1$$

$$\angle G(s) = -180 \pm k360$$

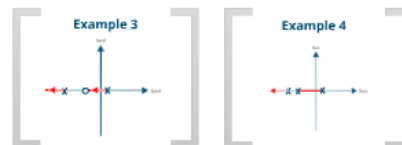
$$G(s) = K_G \frac{\prod_{i=1}^m (s - z_i)}{\prod_{j=1}^n (s - p_j)}$$

$$\angle (a \times b) = \angle a + \angle b$$

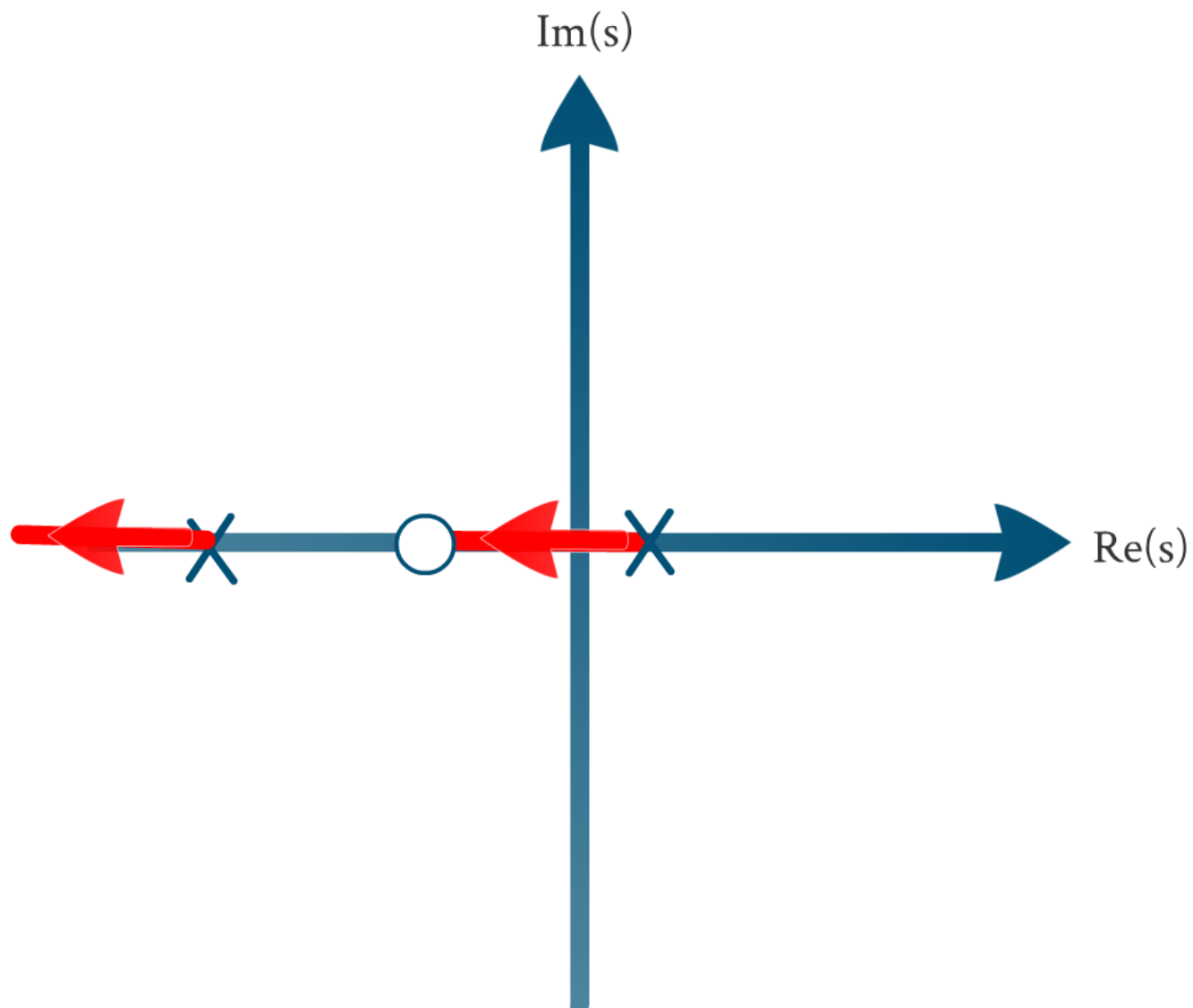
$$\angle G(s) = \angle Z(s) - \angle P(s)$$

$$= \sum_{i=1}^m \angle(s - z_i) - \sum_{i=1}^n \angle(s - p_i) = -180 \pm k360$$

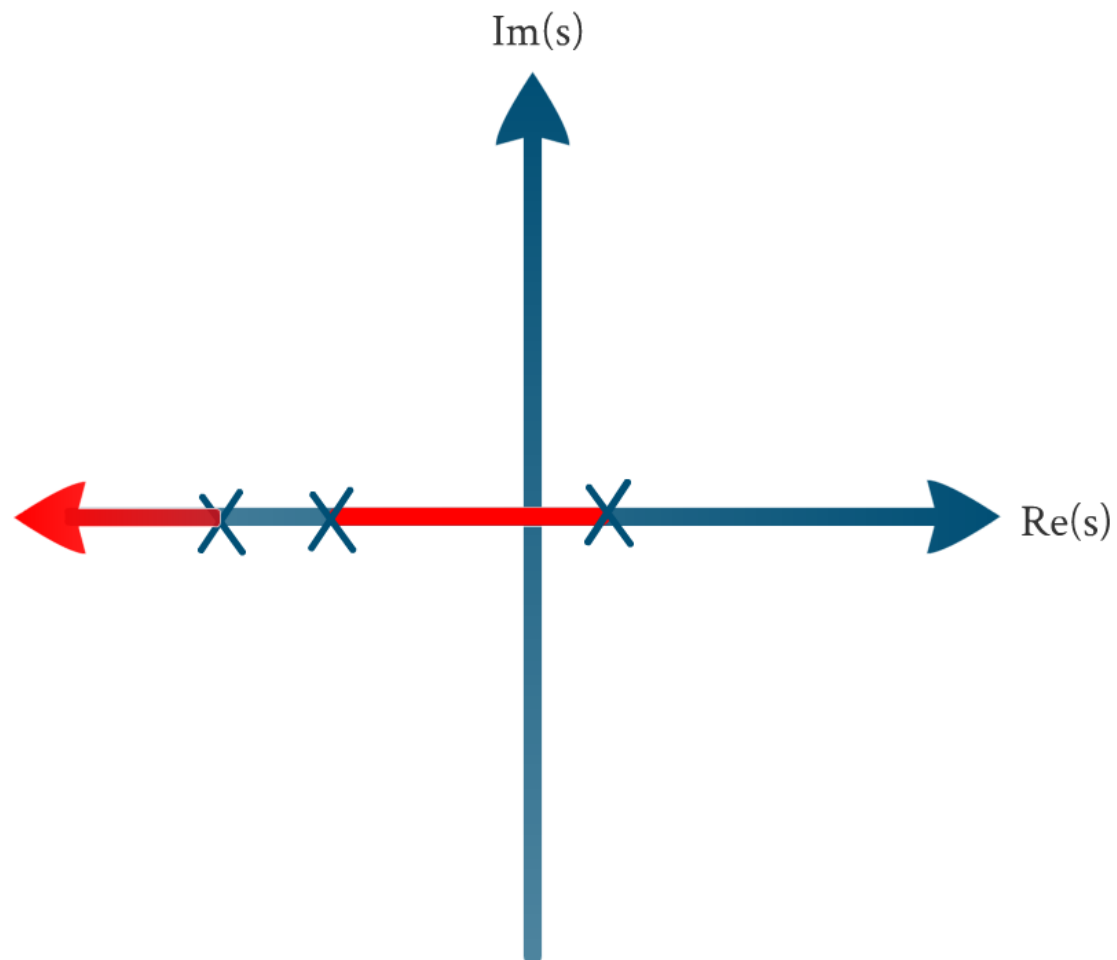
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# Example 3



# Example 4



# Real-axis Segments

$$KG(s) = -1$$

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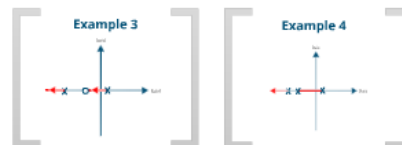
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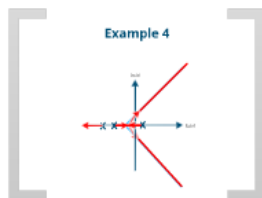
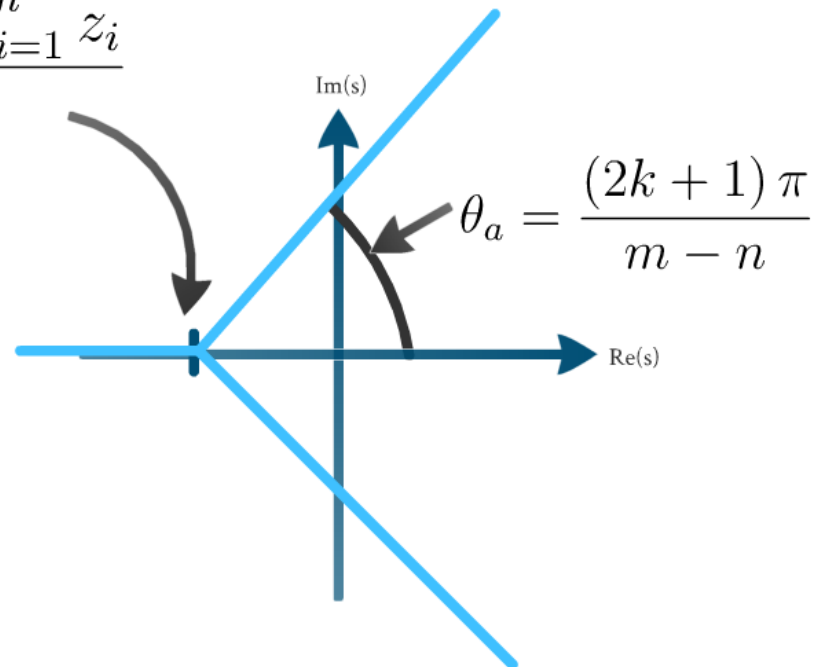
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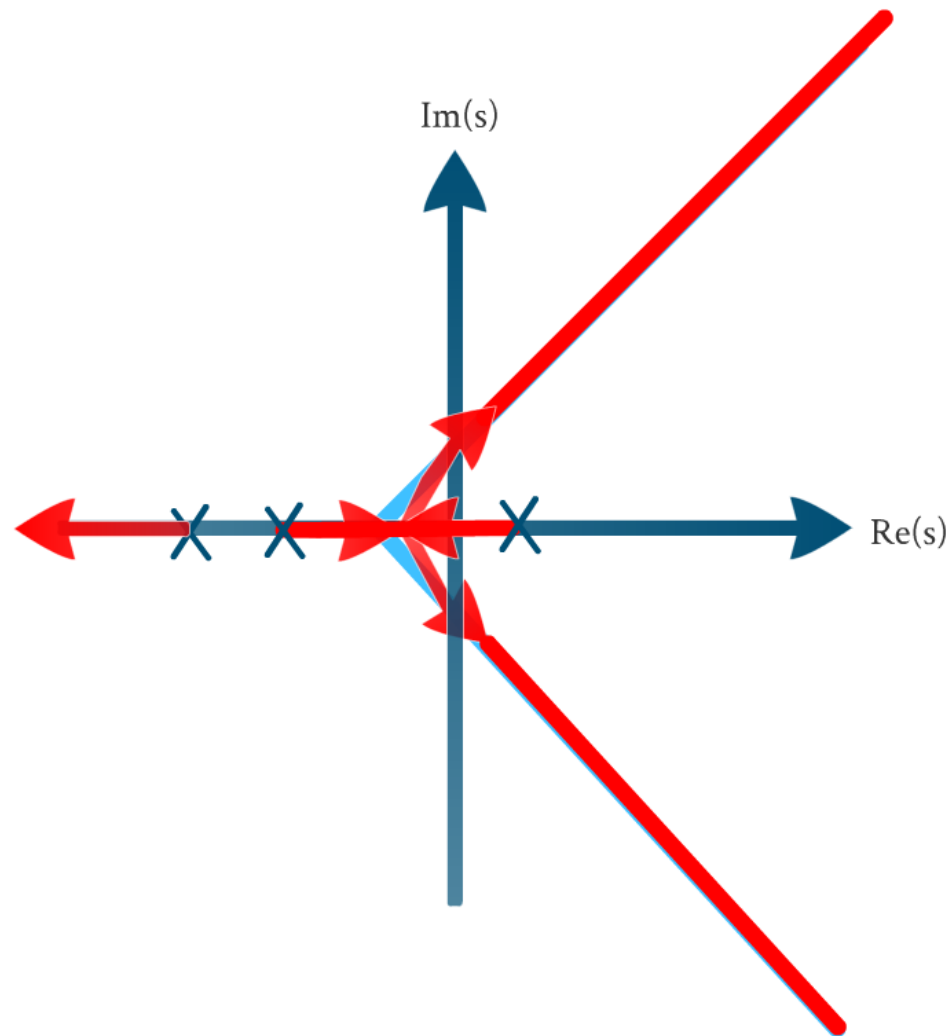
# Infinite Zeros

- If  $n < m$  then there are more poles than there are (finite) zeros. The poles move from the open-loop poles to the open-loop zeros, so we have to think what happens when  $|s| = \infty$ .
- As  $|s| \rightarrow \infty$ , the locus will asymptote to straight lines

$$\sigma_a = \frac{\sum_{i=1}^m p_i - \sum_{i=1}^n z_i}{m - n}$$



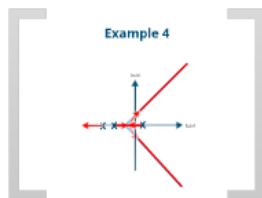
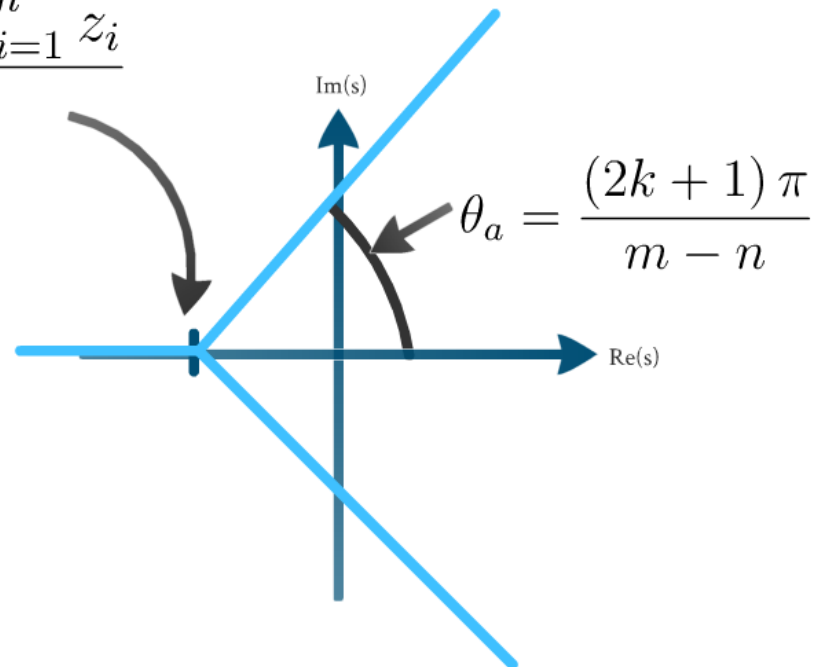
# Example 4



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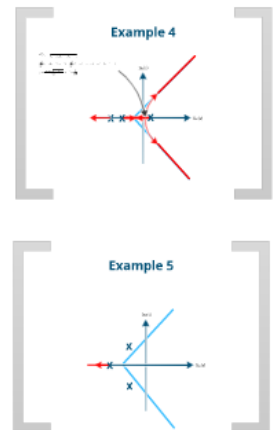




# Real-Axis Breakaway Points

$$K = \frac{1}{|G(s)|}$$

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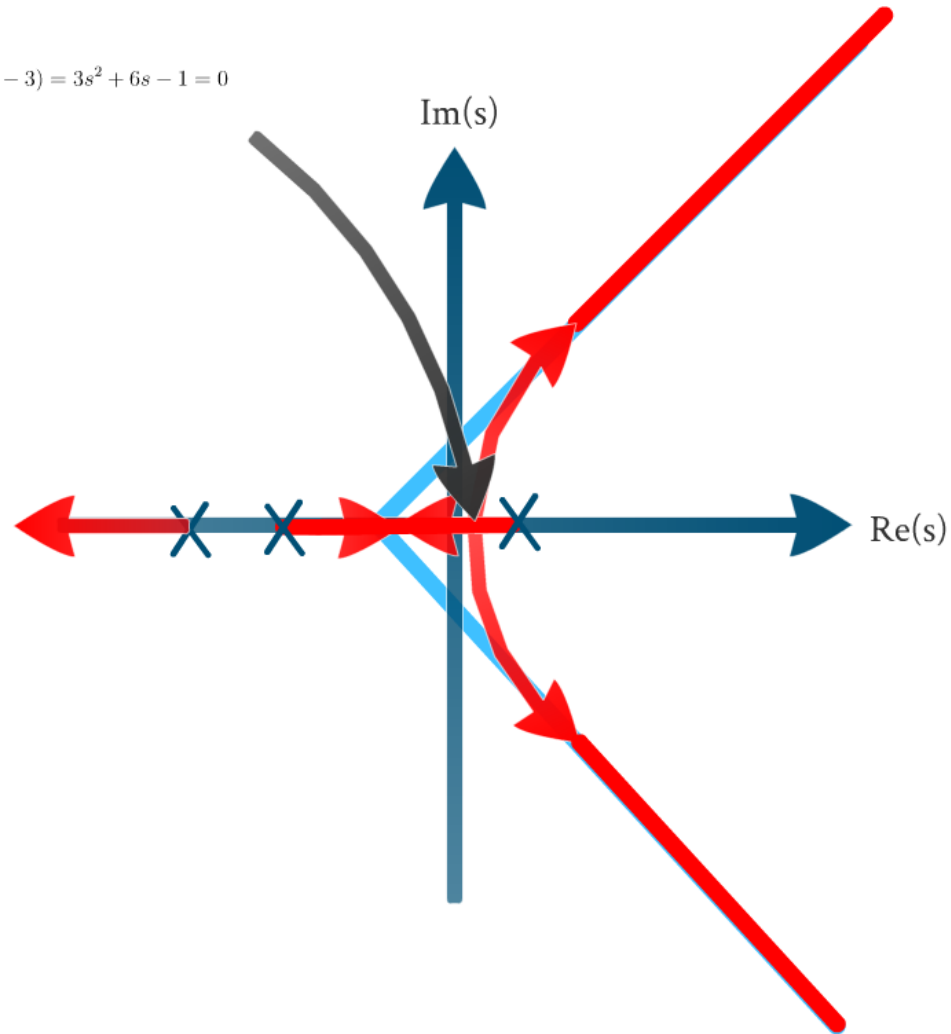


# Example 4

$$G(s) = \frac{1}{(s+3)(s+1)(s-1)}$$

$$\frac{d}{ds}(s+3)(s+1)(s-1) = \frac{d}{ds}(s^3 + 3s^2 - s - 3) = 3s^2 + 6s - 1 = 0$$

$$s = \frac{-6 \pm \sqrt{6^2 + 4.3.1}}{2.3} = -1 \pm \frac{2}{\sqrt{3}}$$





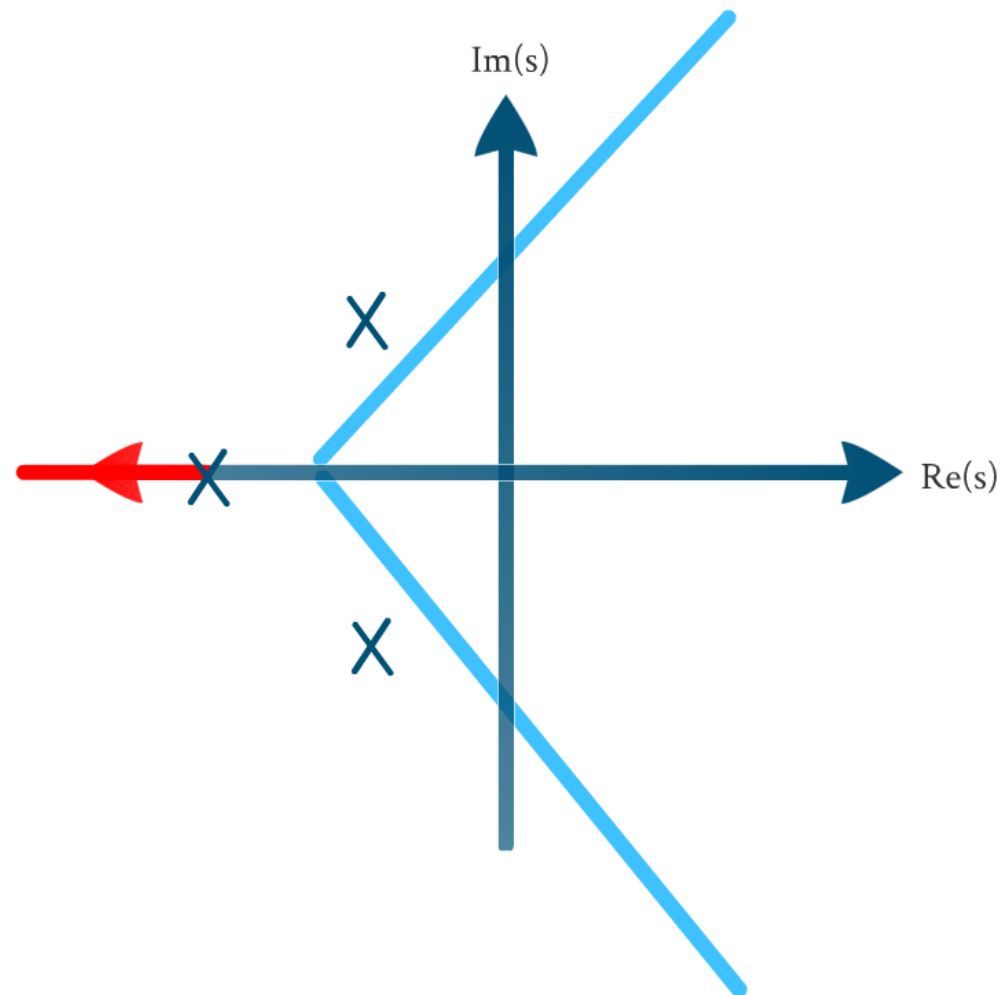
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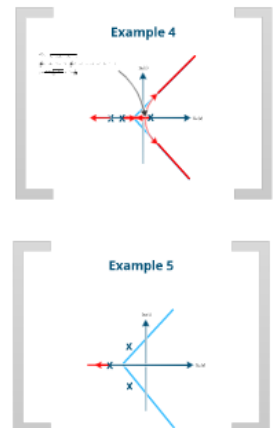
# Example 5



# Real-Axis Breakaway Points

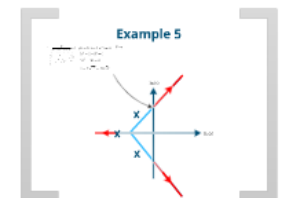
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# Example 5

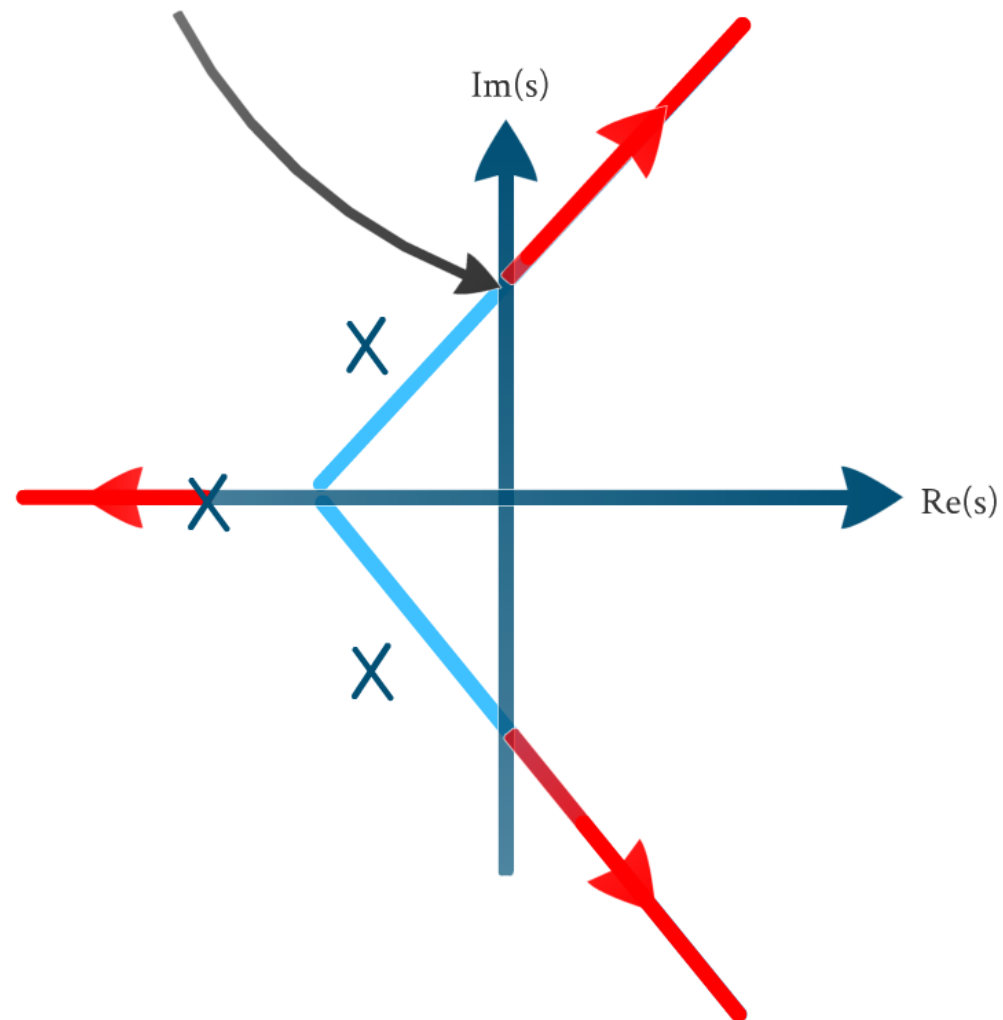
$$1 + \frac{K}{s^3 + 5s^2 + 8s + 6} = 0 \quad (6 + K) - 8 \times 5 = 0 \quad K=34$$

$s^3$		1		8
$s^2$		5		$6 + K$
$s^1$	$-\frac{1}{5}$	$\frac{1}{5}$	8	0
$s^0$				

$$5s^2 + 6 + K = 0$$

$$5s^2 + 40 = 0$$

$$s = \pm\sqrt{-8} = \pm 2\sqrt{2}j$$



# Ex

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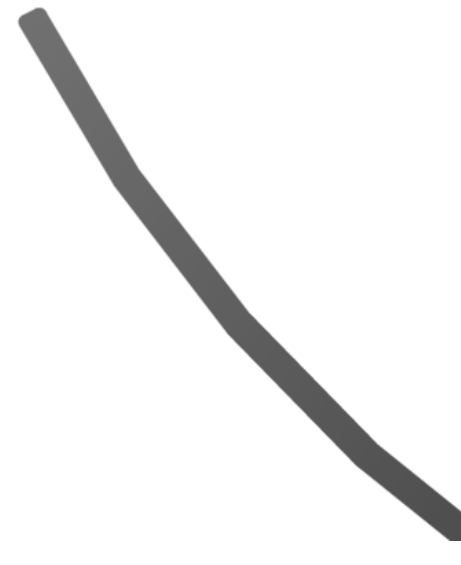
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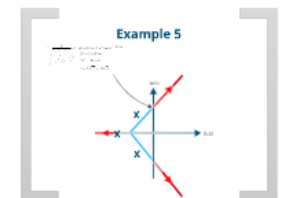
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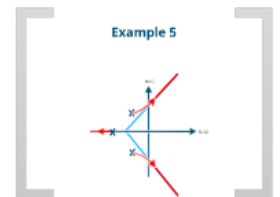
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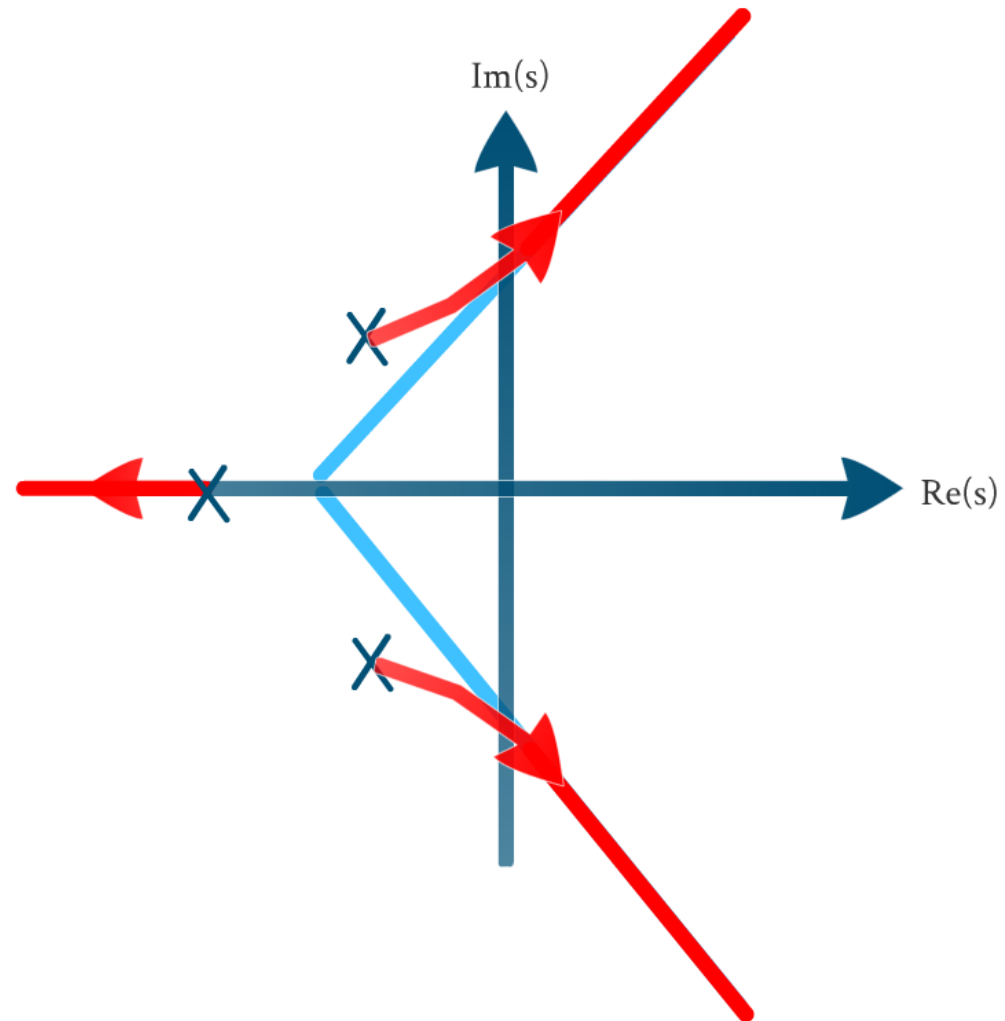


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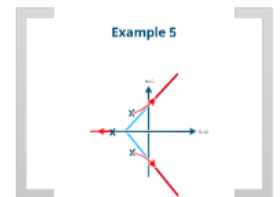


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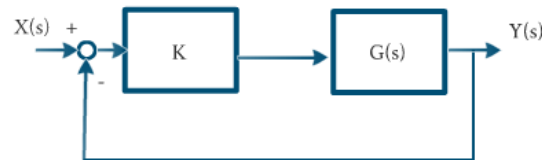
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- We know that poles in the RHP will cause instability. We can use the Routh-Hurwitz criteria to find K.
- We find a K that forces a row in the Routh-Hurwitz table to be zero.
- The associated auxiliary equation can then be solved for s.



## Real-axis Segments

$$KG(s) = -1 \quad \angle G(s) = -180 \pm k360$$

$$G(s) = K \frac{\prod_{i=1}^m (s - z_i)}{\prod_{j=1}^n (s - p_j)} \quad \angle(a \times b) = \angle a + \angle b$$

$$\angle G(s) = \angle Z(s) - \angle P(s)$$

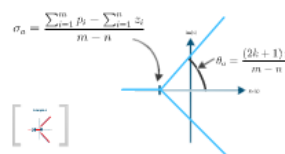
$$= \sum_{i=1}^m \angle(s - z_i) - \sum_{j=1}^n \angle(s - p_j) = -180 \pm k360$$

- For any point on the real axis, the contribution from any complex conjugate poles (or zeros) will cancel each other out.
- For two values of s on the real axis and either side of a zero or a pole, then they will have values of  $\angle G(s)$  that differ by  $180^\circ$ .
- More precisely, the root locus exists at s on the real-axis to the left of an odd total number of real-axis open-loop poles and open-loop zeros.



## Infinite Zeros

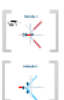
- If  $n < m$  then there are more poles than there are (finite) zeros. The poles move from the open-loop poles to the open-loop zeros, so we have to think what happens when  $|s| \rightarrow \infty$ .
- As  $|s| \rightarrow \infty$ , the locus will asymptote to straight lines



## Real-Axis Breakaway Points

$$K = \frac{1}{|G(s)|}$$

- K is a local maximum or minimum when the root locus breaks away from the real axis. So, we can differentiate K wrt s, set to zero and solve for  $\sigma$ .



This lecture covers:

- Root locus diagram representation for a closed loop system with variable gain.

