

## ELEC 207 Part B

### Control Theory Lecture 11: Frequency Response (1)

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## Determination of Frequency Response

For a linear system, the output will be at the same frequency as the input.

### Experimental

Use a "wave analyser":

- Frequency of a sinusoidal input is varied
- Amplitude and relative phase of the output measured



### Theoretical

Laplace transform of a cos(wt) input

$$\frac{s}{s^2 + \omega^2} = \frac{s}{(s + j\omega)(s - j\omega)}$$

Output from a system with transfer function G(s)

$$\frac{s}{(s + j\omega)(s - j\omega)} G(s) = \frac{s}{(s + j\omega)(s - j\omega)} \left( \frac{A}{s + j\omega} + \frac{B}{s - j\omega} \right) + \frac{C}{s}$$

Partial fraction decomposition

$$= \frac{1}{(s + j\omega)} \left( \frac{A}{s + j\omega} + \frac{B}{s - j\omega} \right) + \frac{C}{s}$$

$$= \frac{1}{(s + j\omega)} \left( \frac{A}{s + j\omega} + \frac{B}{s - j\omega} \right) + \frac{C}{s}$$

Taking inverse Laplace Transforms

$$c = \frac{1}{s} \left( \frac{A}{s + j\omega} + \frac{B}{s - j\omega} \right) + \frac{C}{s}$$

So (relative to the input) the output has:

- Amplitude of  $|G(j\omega)|$
- Phase of  $\angle G(j\omega)$



This lecture covers:  
• Experimental and theoretical determination of frequency response  
• Diagrammatic representations using Bode plot

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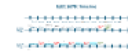
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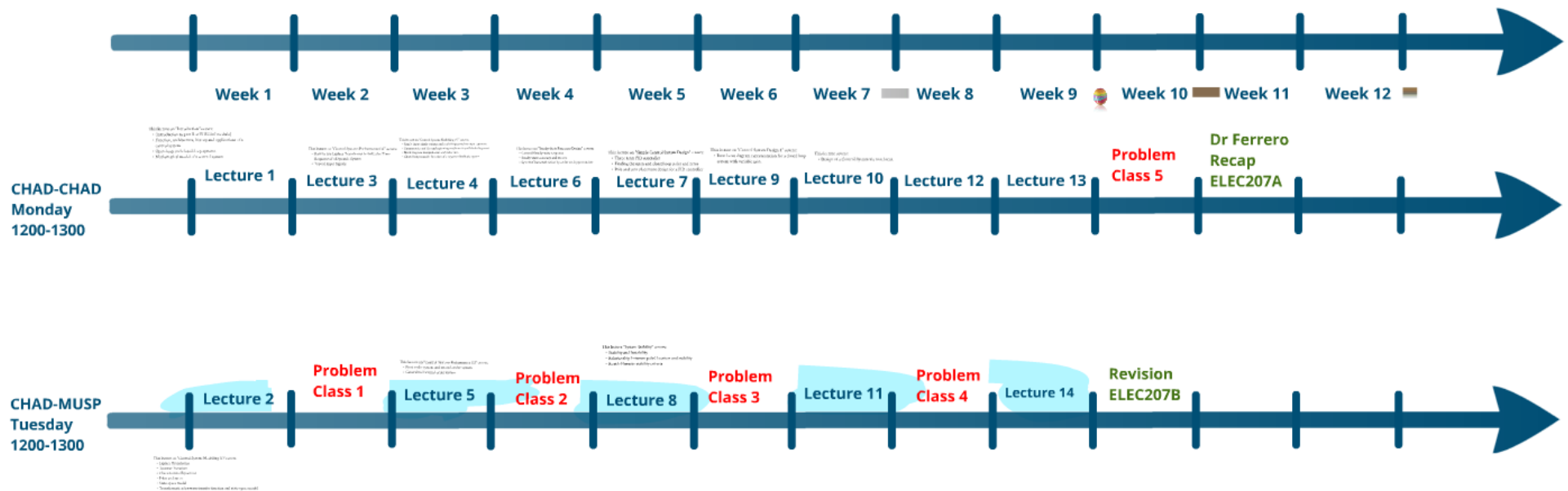
UNIVERSITY OF  
LIVERPOOL

This lecture covers:

- Experimental and theoretical determination of frequency response
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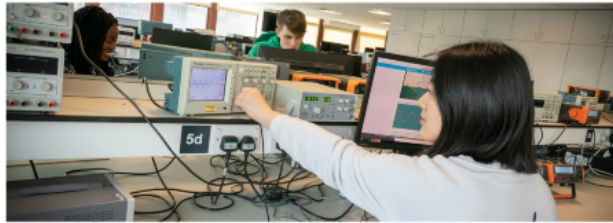


## ELEC 207B: Timeline





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We

Week 10



Week 11

Dr Corron

This lecture covers:

- Experimental and theoretical determination of frequency response
- Diagrammatic representations using Bode plot



# Determination of Frequency Response

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Laplace transform of a  $\cos(\omega t)$  input

$$\frac{s}{s^2 + \omega^2} = \frac{s}{(s + j\omega)(s - j\omega)}$$

Output from a system with transfer function  $G(s)$

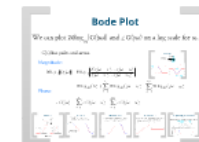
$$\begin{aligned} \frac{s}{(s + j\omega)(s - j\omega)} G(s) &= \frac{1}{(s + j\omega)} \left( \left. \frac{s}{s - j\omega} G(s) \right|_{s = -j\omega} \right) + \frac{1}{(s - j\omega)} \left( \left. \frac{s}{s + j\omega} G(s) \right|_{s = j\omega} \right) + \frac{T(s)}{s} \\ &\text{Steady-state Response} \\ &= \frac{1}{(s + j\omega)} \frac{1}{2} G(-j\omega) + \frac{1}{(s - j\omega)} \frac{1}{2} G(j\omega) + T(s) \\ &= \frac{|G(j\omega)|}{2} \left( e^{-j\angle G(j\omega)} \frac{1}{s + j\omega} + e^{j\angle G(j\omega)} \frac{1}{s - j\omega} \right) + T(s) \end{aligned}$$

Taking inverse Laplace Transforms

$$\mathcal{L}^{-1} \left[ \frac{|G(j\omega)|}{2} \left( e^{-j\angle G(j\omega)} \frac{1}{s + j\omega} + e^{j\angle G(j\omega)} \frac{1}{s - j\omega} \right) \right] = |G(j\omega)| \frac{e^{-j\omega t - j\angle G(j\omega)} + e^{j\omega t + j\angle G(j\omega)}}{2}$$

So (relative to the input) the output has:

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## Theoretical

Laplace transform of a  $\cos(\omega t)$  input

$$\frac{s}{s^2 + \omega^2} = \frac{s}{(s + j\omega)(s - j\omega)}$$

Output from a system with transfer function  $G(s)$

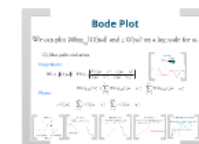
$$\begin{aligned} \frac{s}{(s + j\omega)(s - j\omega)} G(s) &= \frac{1}{(s + j\omega)} \left( \frac{s}{s - j\omega} G(s) \right) + \frac{1}{(s - j\omega)} \left( \frac{s}{s + j\omega} G(s) \right) + \frac{T(s)}{2} \\ &\text{Steady-state Response} \\ &= \frac{1}{(s + j\omega)} \frac{1}{2} G(-j\omega) + \frac{1}{(s - j\omega)} \frac{1}{2} G(j\omega) + T(s) \\ &= \frac{|G(j\omega)|}{2} \left( e^{-j\angle G(j\omega)} \frac{1}{s + j\omega} + e^{j\angle G(j\omega)} \frac{1}{s - j\omega} \right) + T(s) \end{aligned}$$

Taking inverse Laplace Transforms

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# Theoretical

Laplace transform of a  $\cos(\omega t)$  input

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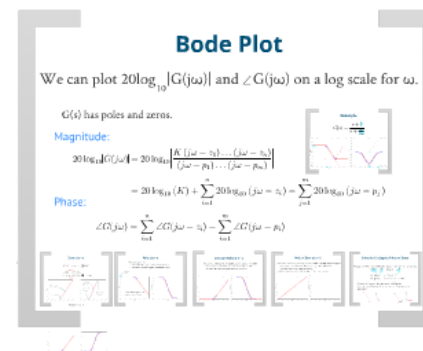
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So (relative to the input) the output has:

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# Theoretical

the transform of a  $\cos(\omega t)$  input

$$\frac{s}{s^2 + \omega^2} = \frac{s}{(s + j\omega)(s - j\omega)}$$

output from a system with transfer function  $G(s)$

$$\begin{aligned} \frac{s}{(s + j\omega)(s - j\omega)} G(s) &= \underbrace{\frac{1}{(s + j\omega)} \left( \frac{s}{s - j\omega} G(s) \right) \Big|_{s=-j\omega} + \frac{1}{(s - j\omega)} \left( \frac{s}{s + j\omega} G(s) \right) \Big|_{s=j\omega}}_{\text{Steady-state Response}} + \underbrace{T(s)}_{\text{Transient Response}} \\ &= \frac{1}{(s + j\omega)} \frac{1}{2} G(-j\omega) + \frac{1}{(s - j\omega)} \frac{1}{2} G(j\omega) + T(s) \\ &= \frac{|G(j\omega)|}{2} \left( e^{-j\angle G(j\omega)} \frac{1}{s + j\omega} + e^{j\angle G(j\omega)} \frac{1}{s - j\omega} \right) + T(s) \end{aligned}$$

finding inverse Laplace Transforms

$$\mathcal{L}^{-1} \left[ \frac{|G(j\omega)|}{2} \left( e^{-j\angle G(j\omega)} \frac{1}{s + j\omega} + e^{j\angle G(j\omega)} \frac{1}{s - j\omega} \right) \right] = |G(j\omega)| \frac{e^{-j\omega t - j\angle G(j\omega)} + e^{j\omega t + j\angle G(j\omega)}}{2}$$

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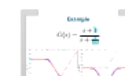
## Bode Plot

We can plot  $20\log_{10}|G(j\omega)|$  and  $\angle G(j\omega)$  on a log scale for  $\omega$ .

$G(s)$  has poles and zeros.

Magnitude:

$$20\log_{10}|G(j\omega)| = 20\log_{10} |K(j\omega - z_1) \dots (j\omega - z_n)|$$



# Theoretical

Laplace transform of a  $\cos(\omega t)$  input

$$\frac{s}{s^2 + \omega^2} = \frac{s}{(s + j\omega)(s - j\omega)}$$

Output from a system with transfer function  $G(s)$

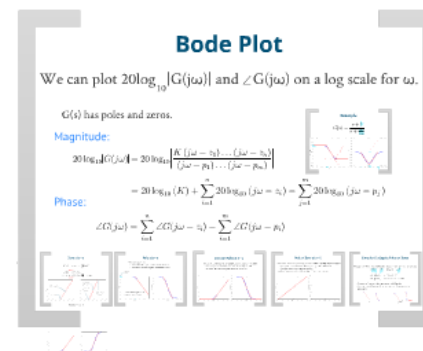
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$$\begin{aligned}
 \frac{s}{\omega(s-j\omega)} G(s) &= \underbrace{\frac{1}{(s+j\omega)} \left( \frac{s}{s-j\omega} G(s) \right) \Big|_{s=-j\omega}}_{\text{Steady-state Response}} + \frac{1}{(s-j\omega)} \left( \frac{s}{s+j\omega} G(s) \right) \Big|_{s=j\omega} + \underbrace{T(s)}_{\text{Transient Response}} \\
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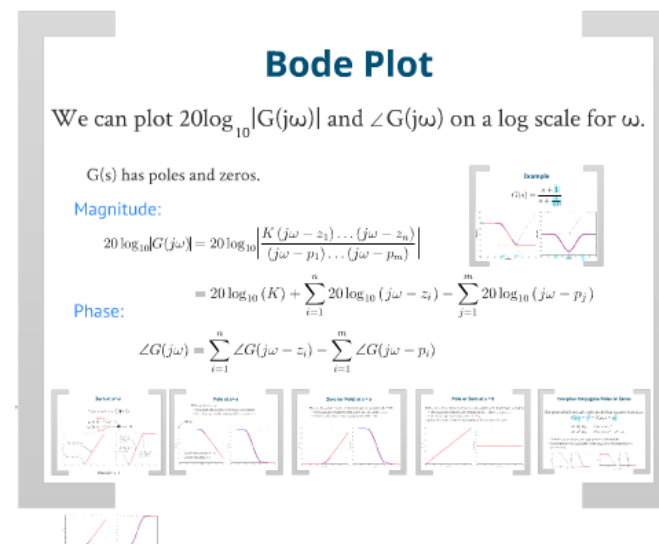
## Inverse Laplace Transforms

$$\mathcal{L}^{-1} \left[ \frac{|G(j\omega)|}{2} \left( e^{-j\angle G(j\omega)} \frac{1}{s+j\omega} + e^{j\angle G(j\omega)} \frac{1}{s-j\omega} \right) \right] = |G(j\omega)| \frac{e^{-j\omega t - j\angle G(j\omega)} + e^{j\omega t + j\angle G(j\omega)}}{2}$$

relative to the input) the output has:

Amplitude of  $|G(j\omega)|$

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Laplace transform of a  $\cos(\omega t)$  input

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Output from a system with transfer function  $G(s)$

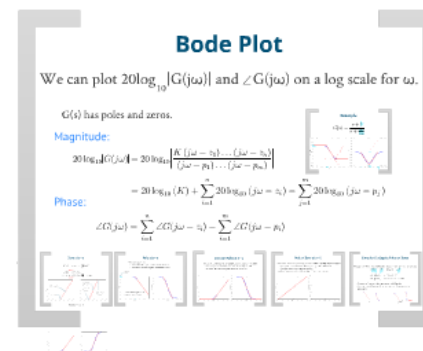
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# Bode Plot

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$G(s)$  has poles and zeros.

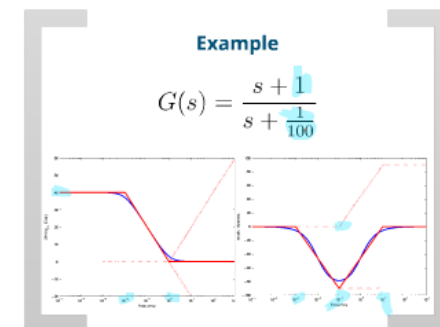
Magnitude:

$$20\log_{10}|G(j\omega)| = 20\log_{10}\left|\frac{K(j\omega - z_1)\dots(j\omega - z_n)}{(j\omega - p_1)\dots(j\omega - p_m)}\right|$$

$$= 20\log_{10}(K) + \sum_{i=1}^n 20\log_{10}(j\omega - z_i) - \sum_{j=1}^m 20\log_{10}(j\omega - p_j)$$

Phase:

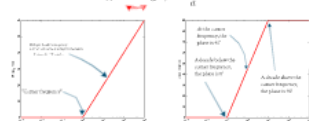
$$\angle G(j\omega) = \sum_{i=1}^n \angle G(j\omega - z_i) - \sum_{j=1}^m \angle G(j\omega - p_j)$$



**Zero at  $s=-a$**

$$G(s) = j\omega + a = a\left(j\frac{\omega}{a} + 1\right)$$

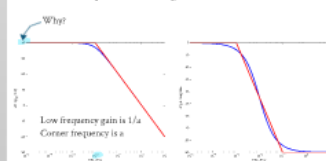
$\omega \approx 0 \quad G(j\omega) \approx a$   
 $\omega \gg a \quad G(j\omega) \approx a\frac{j\omega}{a} = j\omega \angle 90^\circ$



Example:  $a=1$

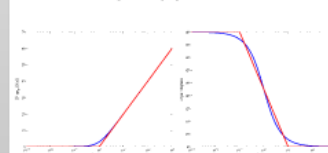
**Pole at  $s=-a$**

- With a pole at  $s=-a$ :
- The amplitude response is the negative of before
  - The phase is now the negative of that from before



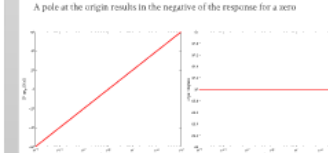
**Zero (or Pole) at  $s=a$**

- We can also consider a zero (or unstable open-loop) pole in the RHP.
- The magnitude response is identical to that for a pole at  $s=-a$ .
  - However, the phase now progresses from  $180^\circ$  to  $90^\circ$ .



**Pole or Zero at  $s=0$**

- With a zero at the origin, the response only consists of the high frequency regime.
- The magnitude response goes through  $20\log_{10}|G(j\omega)| = 0$  at  $\omega = 1$
  - The phase response is always  $90^\circ$  for all  $\omega$
- A pole at the origin results in the negative of the response for a zero



**Complex Conjugate Poles or Zeros**

The generalised second-order model has transfer function:

$$G(s) = \frac{s^2 + 2\zeta\omega_n s + \omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$\omega \ll \omega_n \quad G(j\omega) \approx (\omega_n)^2$$

$$\omega \gg \omega_n \quad G(j\omega) \approx (j\omega)^2 = -\omega^2 \angle 180^\circ$$

- However, as  $\zeta$  nears zero, the approximation fidelity falls
- The responses with a pair poles is the negative of the response for a pair of zeros.

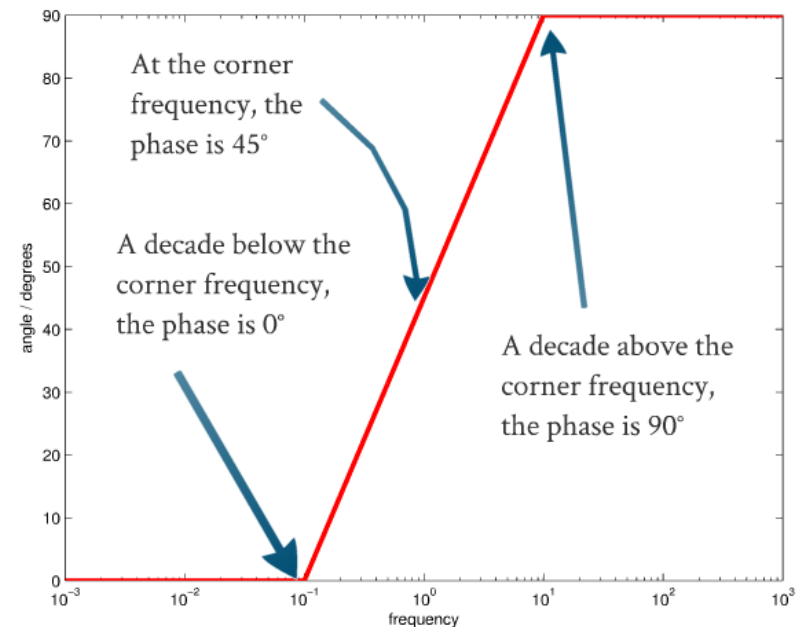
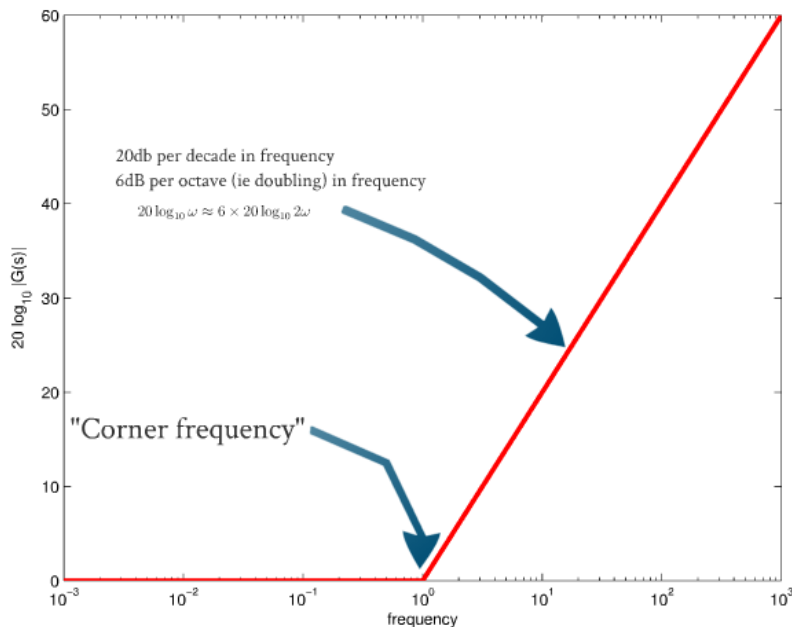




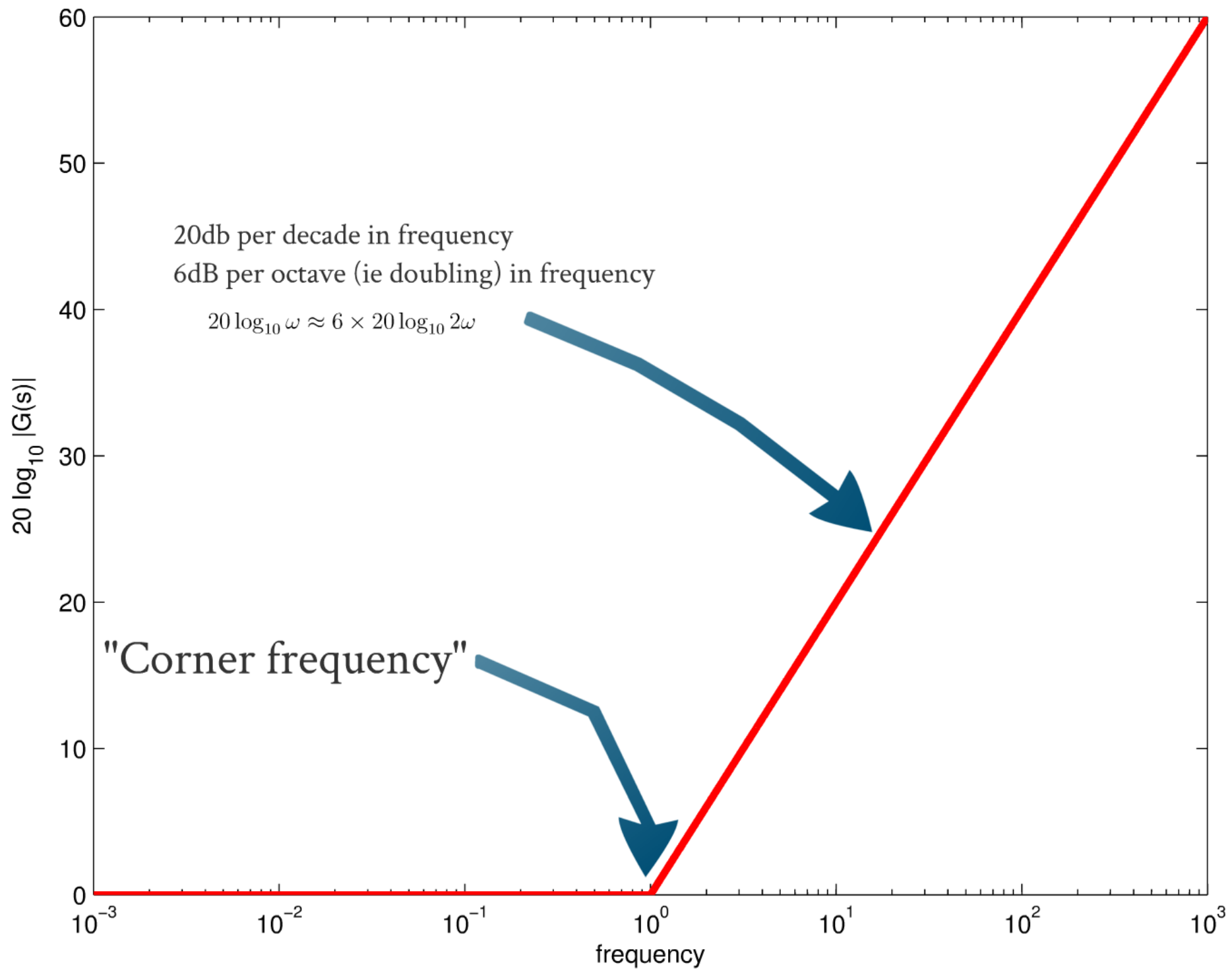
# Zero at $s=-a$

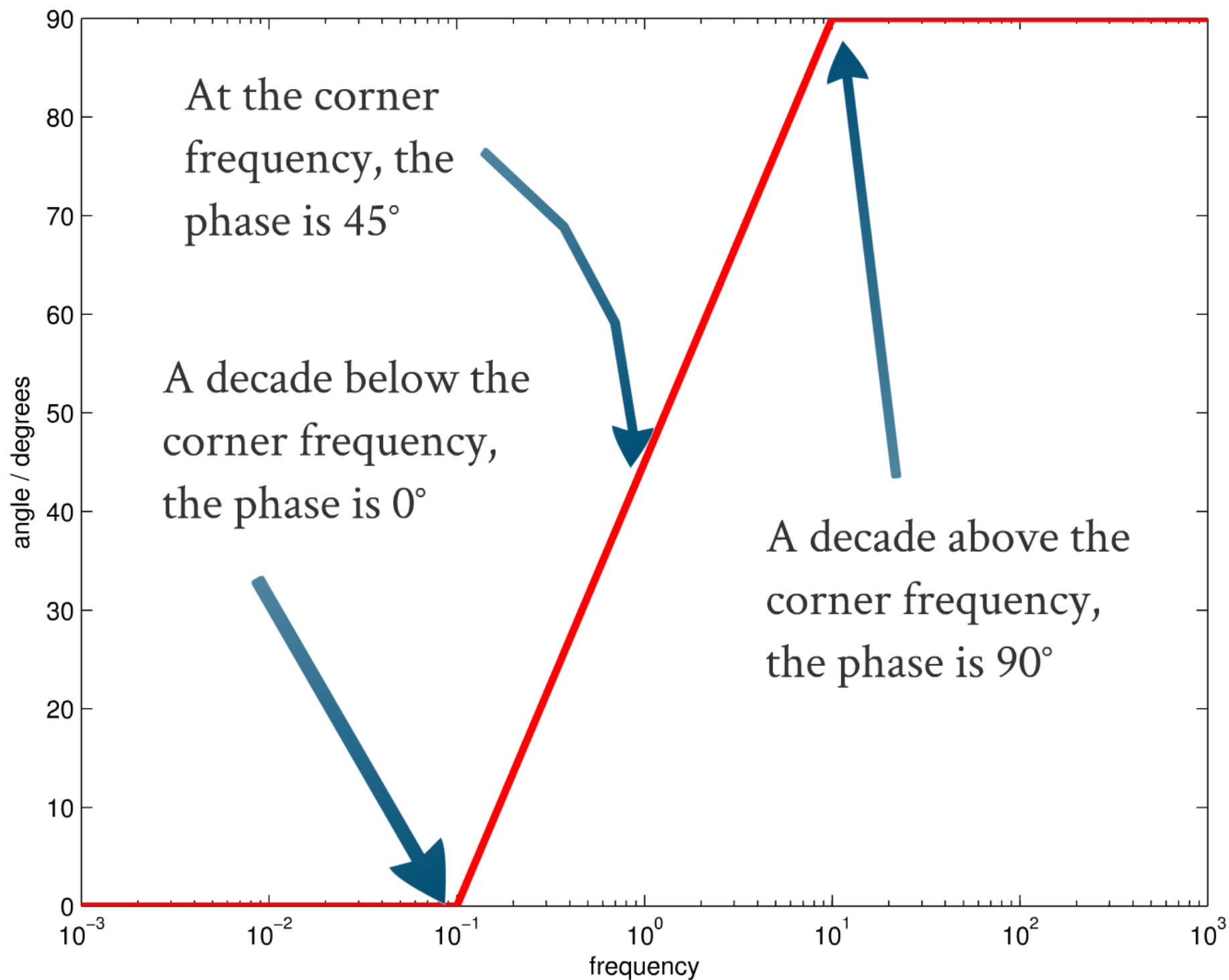
$$G(j\omega) = j\omega + a = a \left( j\frac{\omega}{a} + 1 \right)$$

$$\begin{aligned} \omega \approx 0 & \quad G(j\omega) \approx a \\ \omega \gg a & \quad G(j\omega) \approx a \frac{j\omega}{a} = \omega \angle 90^\circ \end{aligned}$$



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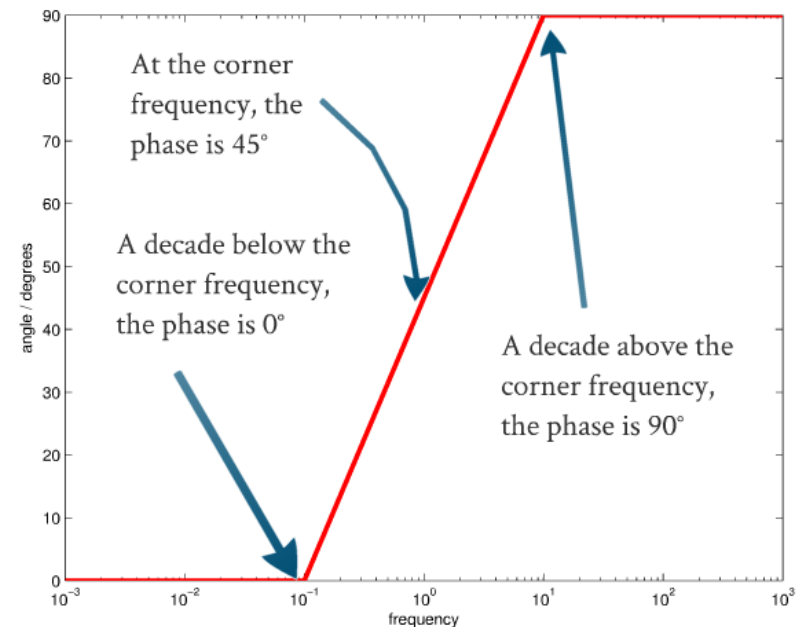
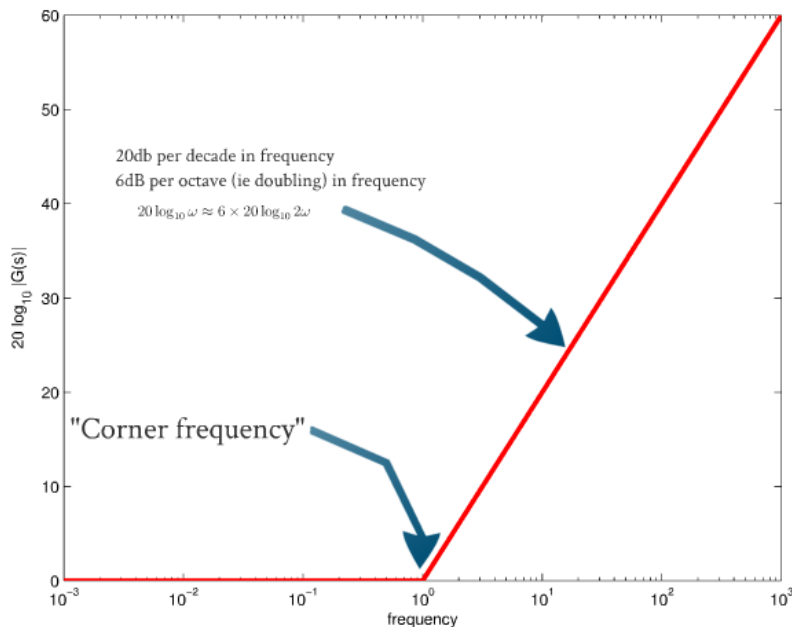




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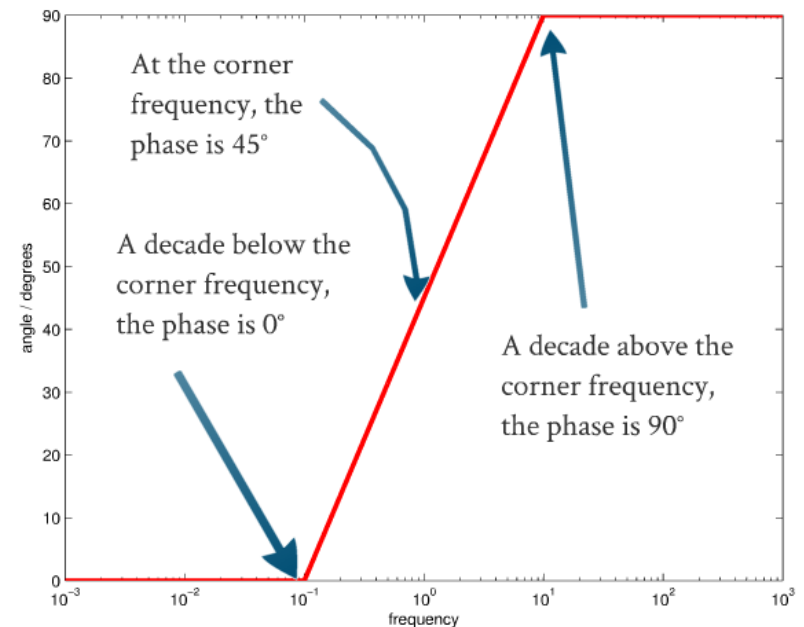
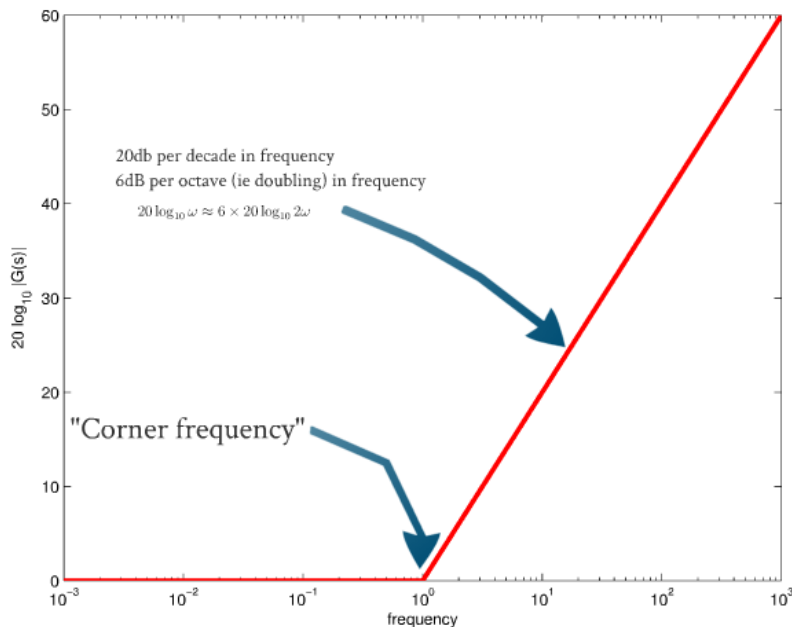


Example:  $a=1$

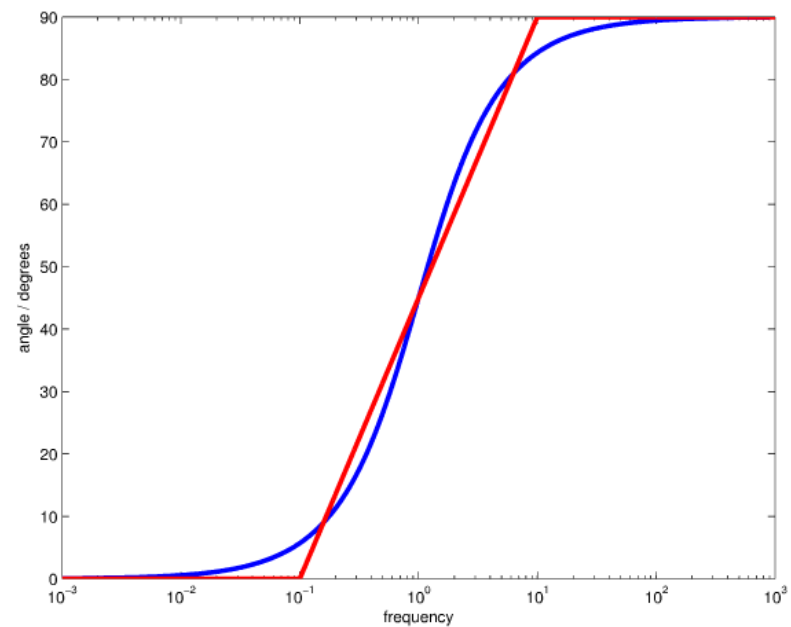
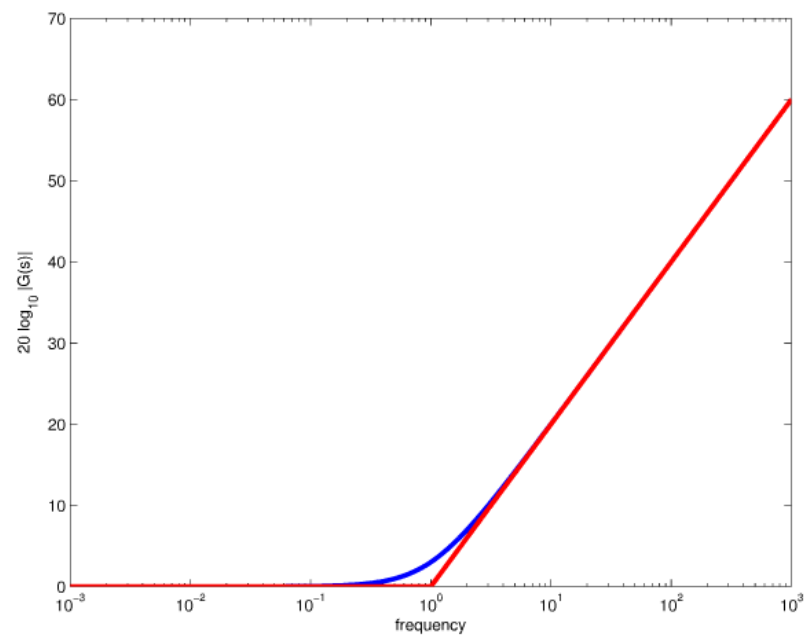
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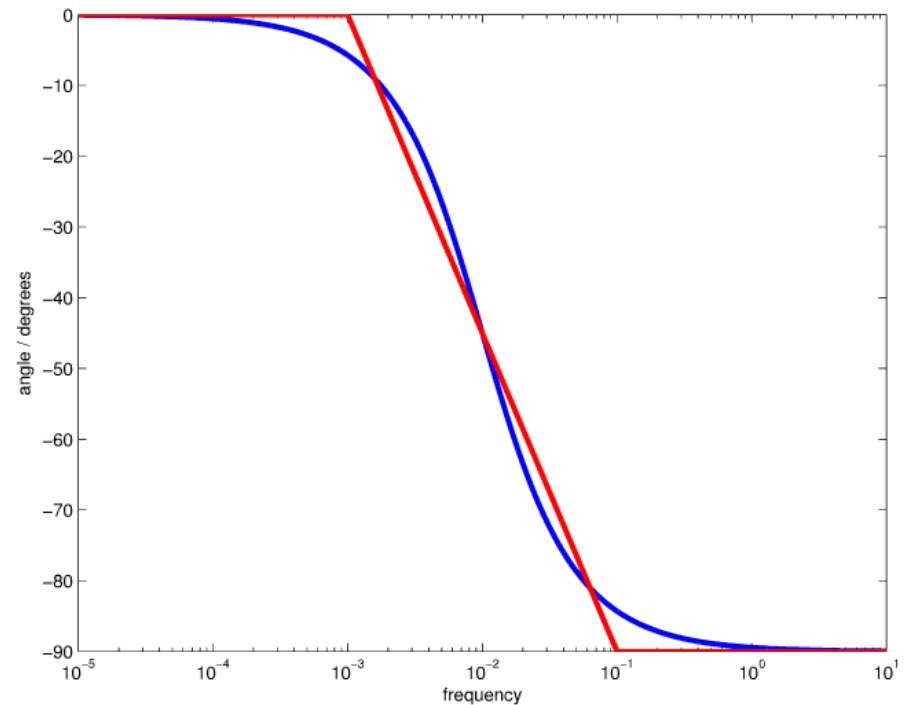
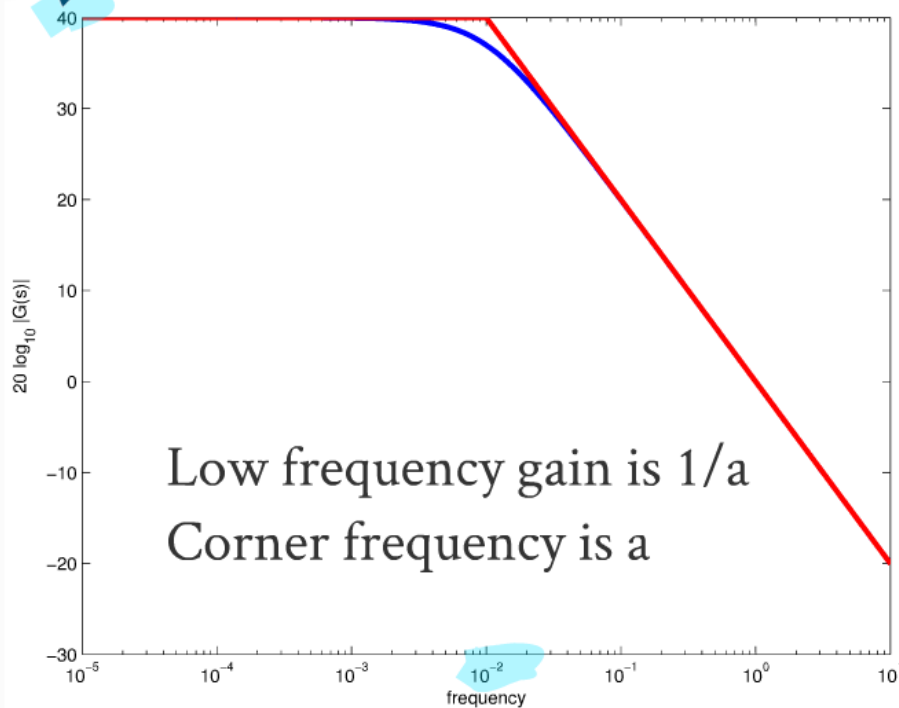


# Pole at $s=-a$

With a pole at  $s = -a$ :

- The amplitude response is the negative of before
- The phase is now the negative of that from before

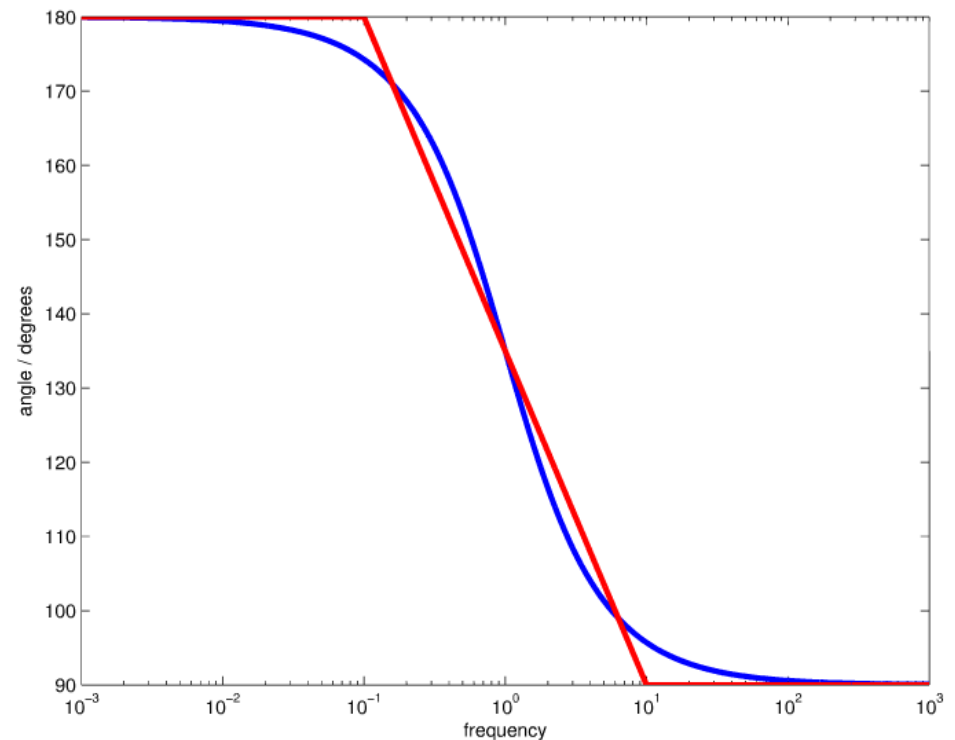
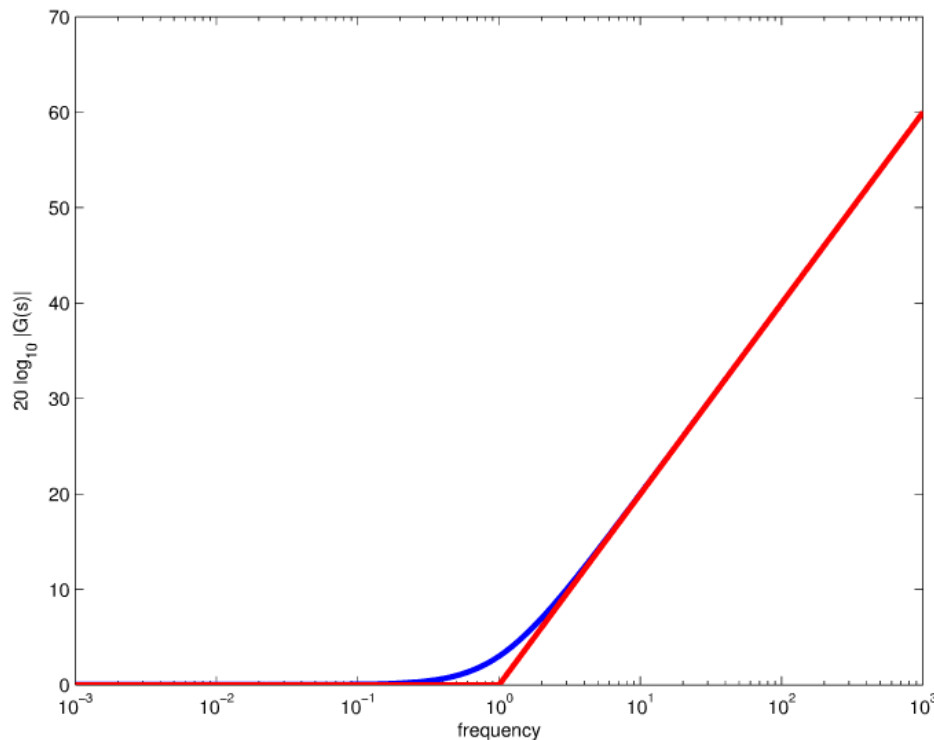
Why?



# Zero (or Pole) at $s = a$

We can also consider a zero or (unstable open-loop) pole in the RHP.

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- However, the phase now progresses from  $180^\circ$  to  $90^\circ$ .



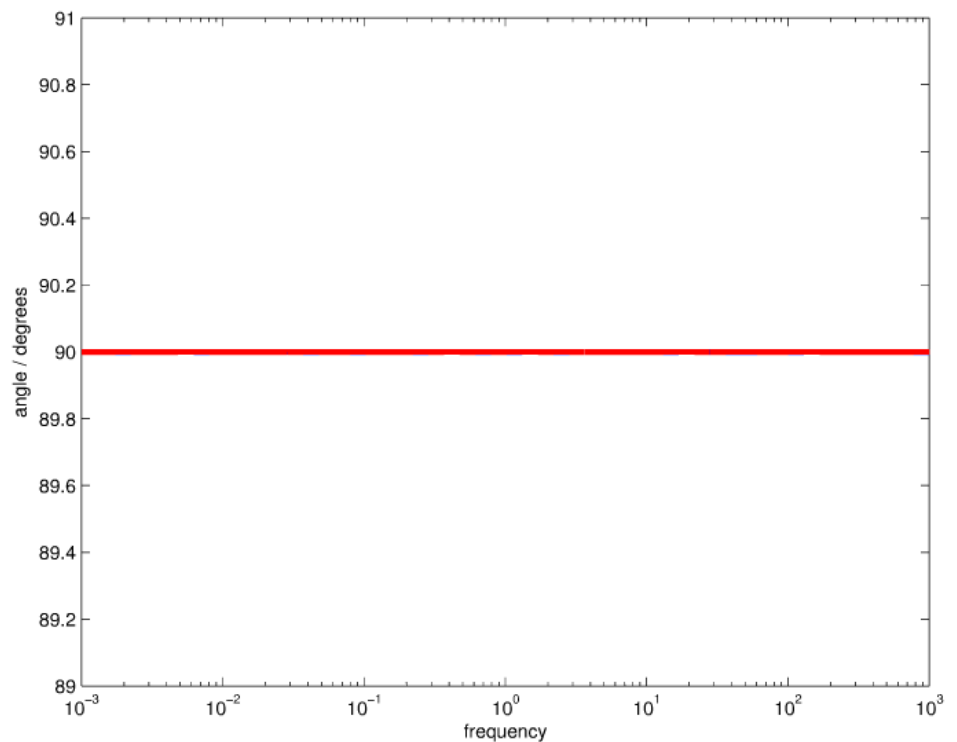
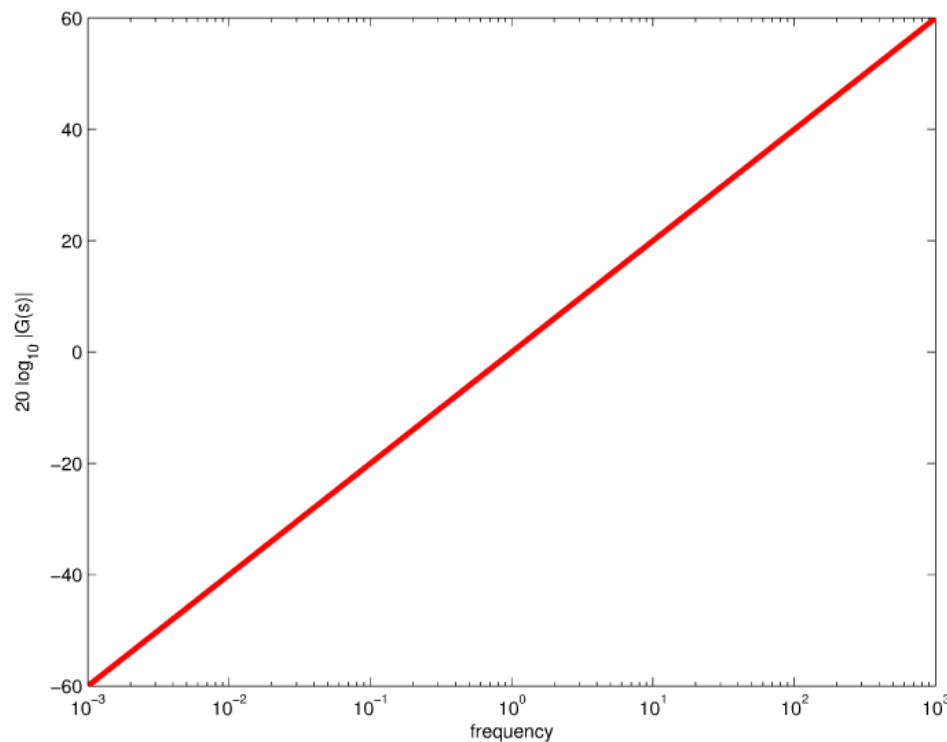


# Pole or Zero at $s = 0$

With a zero at the origin, the response only consists of the high frequency regime.

- The magnitude response goes through  $20 \log_{10} |G(j\omega)| = 0$  at  $\omega = 1$
- The phase response is always  $90^\circ$  for all  $\omega$

A pole at the origin results in the negative of the response for a zero



# Complex Conjugate Poles or Zeros

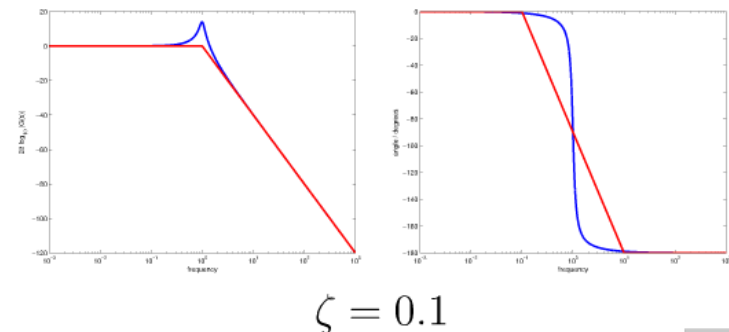
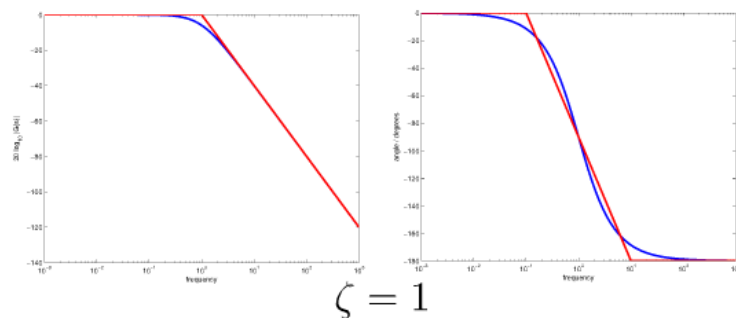
The generalised second-order model has transfer function:

$$G(s) = s^2 + 2\zeta\omega_n s + \omega_n^2$$

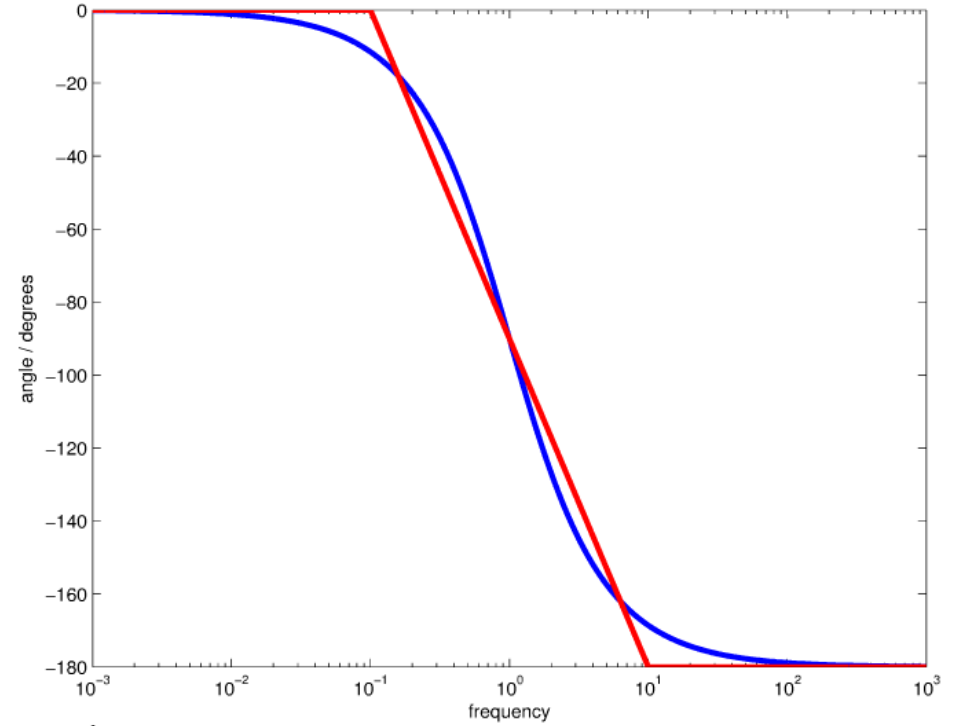
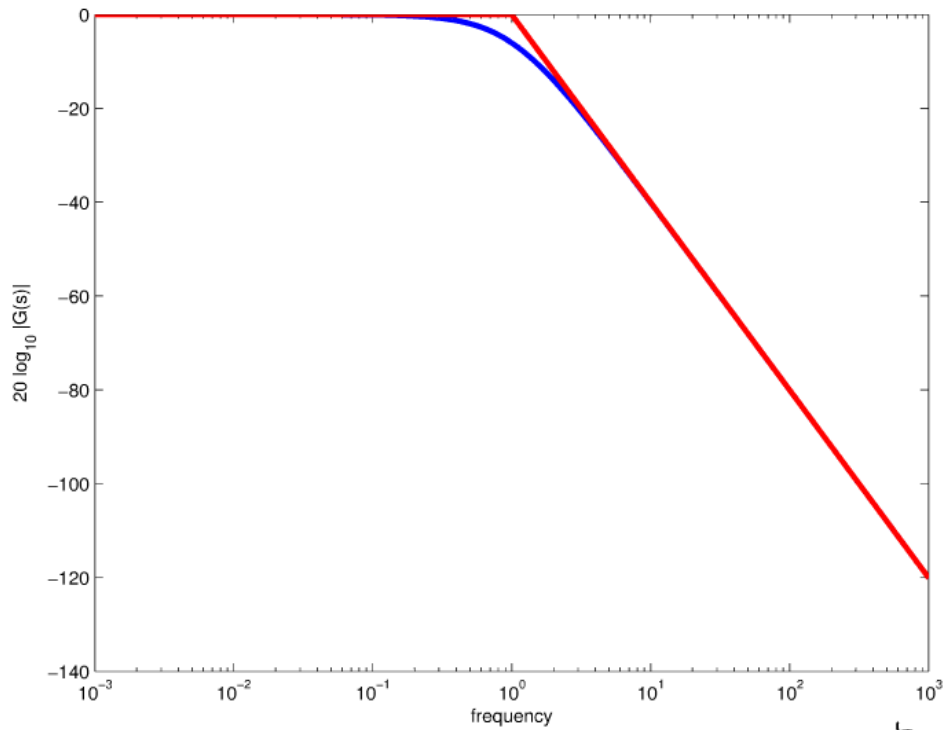
$$\omega \ll \omega_n \quad G(j\omega) \approx (\omega_n)^2$$

$$\omega \gg \omega_n \quad G(j\omega) \approx (j\omega)^2 = \omega^2 \angle 180$$

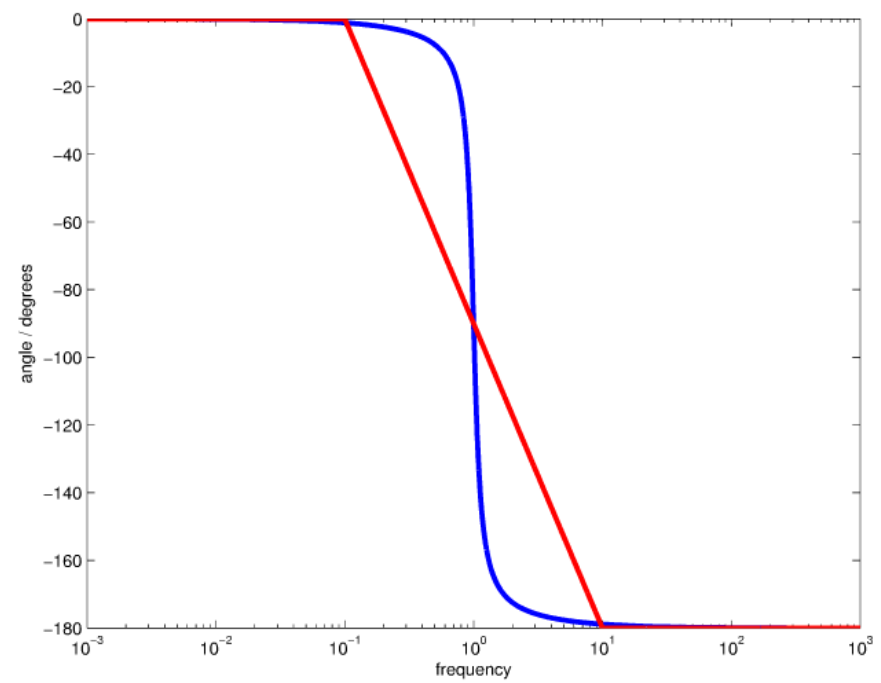
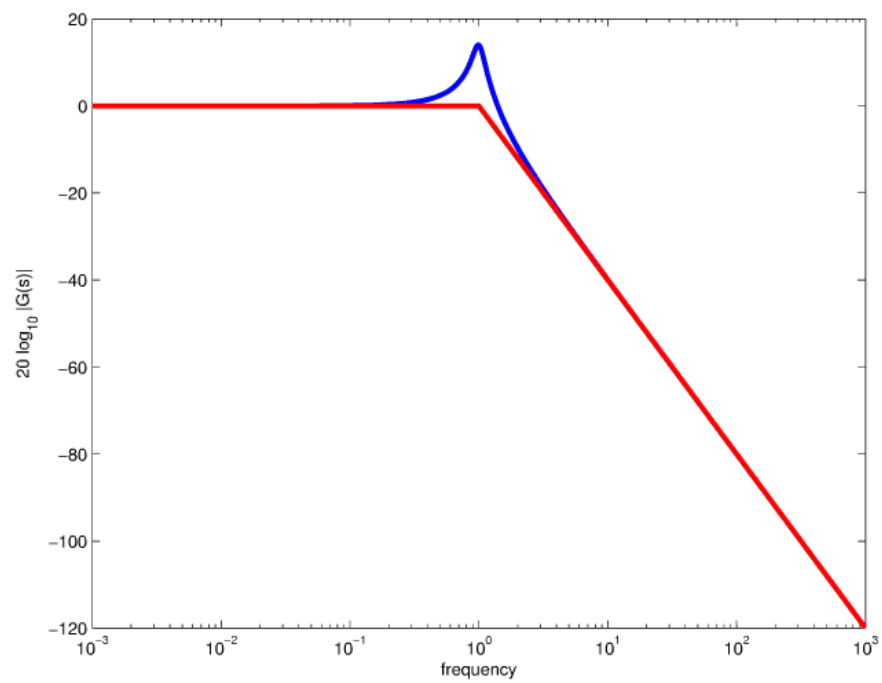
- However, as  $\zeta$  nears zero, the approximation fidelity falls
- The responses with a pair poles is the negative of the response for a pair of zeros.



# pair of zeros.



$$\zeta = 1$$



$$\zeta = 0.1$$

# Complex Conjugate Poles or Zeros

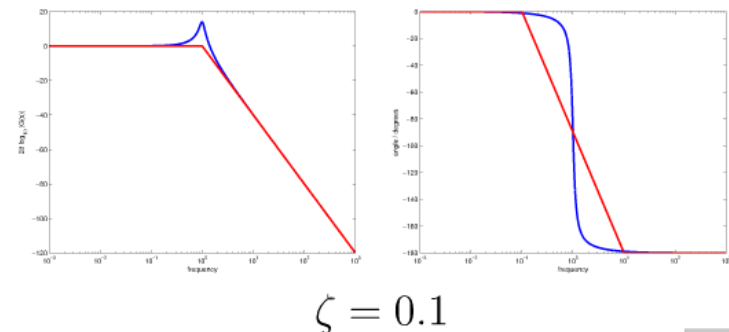
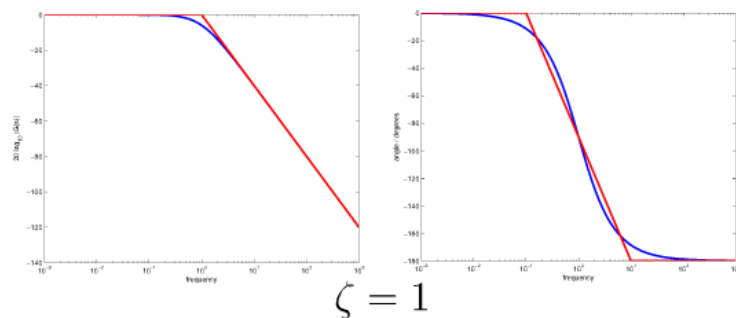
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# Bode Plot

We can plot  $20\log_{10}|G(j\omega)|$  and  $\angle G(j\omega)$  on a log scale for  $\omega$ .

$G(s)$  has poles and zeros.

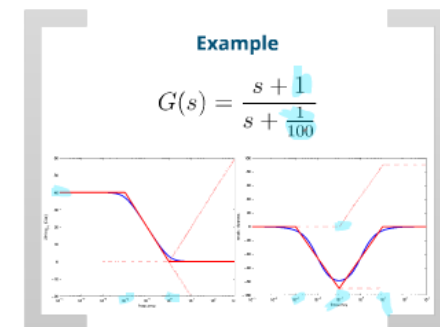
Magnitude:

$$20\log_{10}|G(j\omega)| = 20\log_{10}\left|\frac{K(j\omega - z_1)\dots(j\omega - z_n)}{(j\omega - p_1)\dots(j\omega - p_m)}\right|$$

$$= 20\log_{10}(K) + \sum_{i=1}^n 20\log_{10}(j\omega - z_i) - \sum_{j=1}^m 20\log_{10}(j\omega - p_j)$$

Phase:

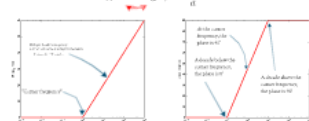
$$\angle G(j\omega) = \sum_{i=1}^n \angle G(j\omega - z_i) - \sum_{j=1}^m \angle G(j\omega - p_j)$$



**Zero at  $s=-a$**

$$G(s) = j\omega + a = a\left(j\frac{\omega}{a} + 1\right)$$

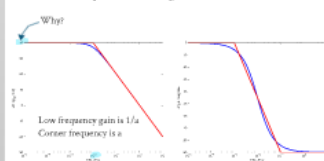
$\omega \approx 0 \quad |G(j\omega)| \approx a$   
 $\omega \gg a \quad |G(j\omega)| \approx a\frac{\omega}{a} = \omega \angle 90^\circ$



Example:  $a=1$

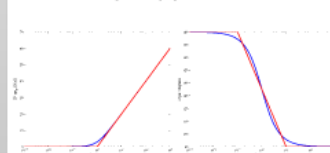
**Pole at  $s=-a$**

- With a pole at  $s=-a$ :
- The amplitude response is the negative of before
  - The phase is now the negative of that from before



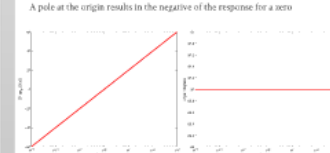
**Zero (or Pole) at  $s=a$**

- We can also consider a zero (or unstable open-loop) pole in the RHP.
- The magnitude response is identical to that for a pole at  $s=-a$ .
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**Pole or Zero at  $s=0$**

- With a zero at the origin, the response only consists of the high frequency regime.
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**Complex Conjugate Poles or Zeros**

The generalised second-order model has transfer function:

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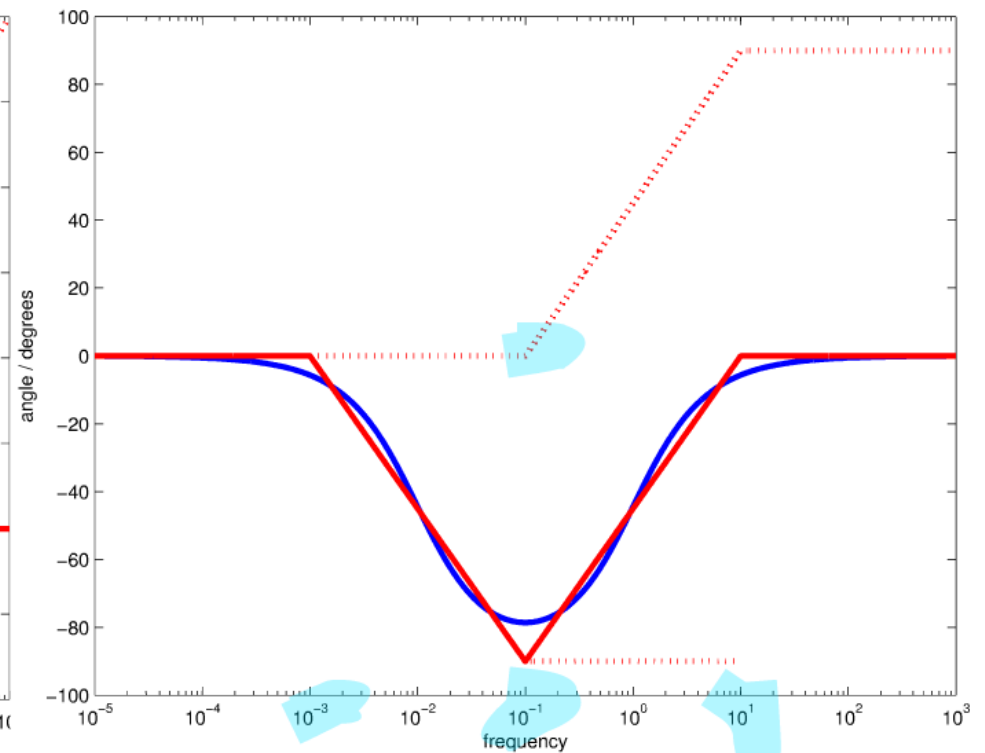
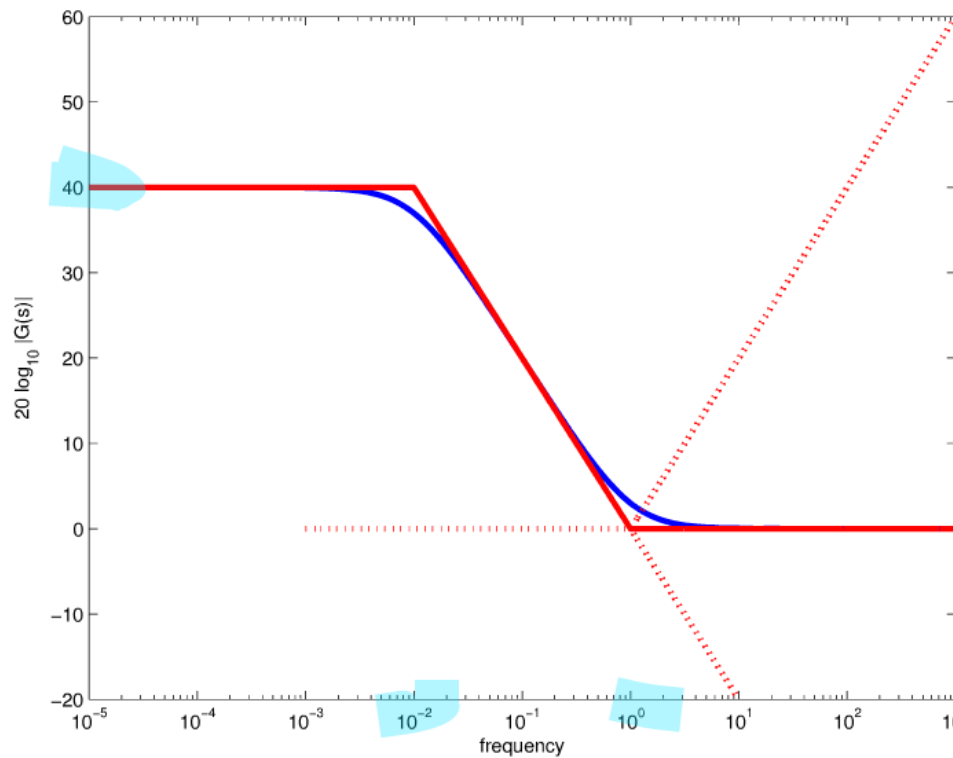
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# Example

$$G(s) = \frac{s + 1}{s + \frac{1}{100}}$$



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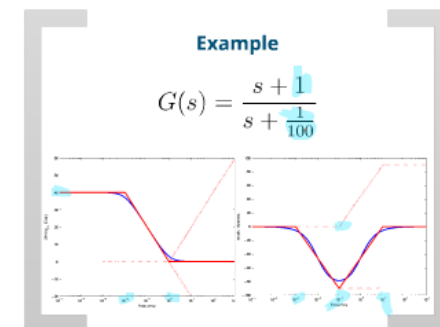
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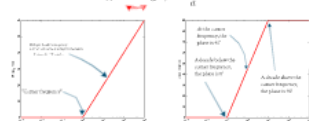
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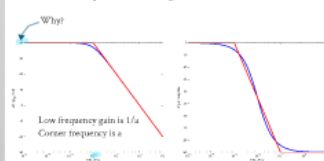
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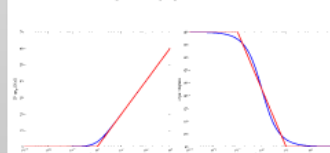
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Low frequency gain is  $1/a$   
Corner frequency is  $a$

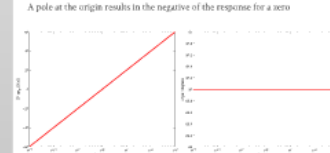
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This lecture covers:

- Experimental and theoretical determination of frequency response
- Diagrammatic representations using Bode plot

