flappingangles

This script evaluates a rotor blade's flapping angles as a function of the azimuth angle, and its derivative. In this scope, the first harmonic flapping motion has been determined with the assumptions of small flapping angles and linear aerodynamics. [1]

$$\beta = \beta_0 + \beta_{1c}\cos(\psi) + \beta_{1s}\sin(\psi) \tag{1}$$

syntax

The default syntax of the function is shown below; all inputs are scalar values.

Where:

INPUT

V Airspeed [m/s]

alpha Angle of attack [deg]

W Helicopter (Rotor) weight [N]

gamma Rotor Lock number

sigma Rotor solidity

theta_tw Rotor blade twist (Assumed linear) [deg]

cla Rotor blade airfoil lift curve slope [1/rad]

omegaR Rotor blade tip speed ΩR [m/s]

eR Adimensional flapping hinge eccentricity e/R

R Rotor blade radius [m]

OUTPUT

psi Azimuth angles [deg]

beta Rotor blade flapping angle [deg]

beta_dot Rotor blade flapping angle derivative $\frac{d\beta}{dy}$

By default ψ is an array of 200 equally spaced points from 0° to 360° . The user may also choose to specify the query points through the 'sample' keyword.

```
[~,beta,beta_dot] = flappingangles(V,alpha,W,gamma,sigma,theta_tw,cla,omegaR,eR,R,'sample',psi)
```

By adding 'output','coefficients' to the function call, the output will change to the flapping angle coefficients used in 1. That is, respectively:

beta_0 Rotor blade coning [deg]

beta_1c Rotor blade longitudinal flapping [deg]

beta_1s Rotor blade lateral flapping [deg] $\frac{d\beta}{dab}$

[beta_0,beta_1c,beta_1s] = flappingangles(V,alpha,W,gamma,sigma,theta_tw,cla, omegaR,eR,R,'output','coefficients') A test case for the function is shown below, where it is called multiple times in a cylce in order to obtain the flapping coefficients β_0 , β_{1c} and β_{1s} as functions of the advance ratio μ .

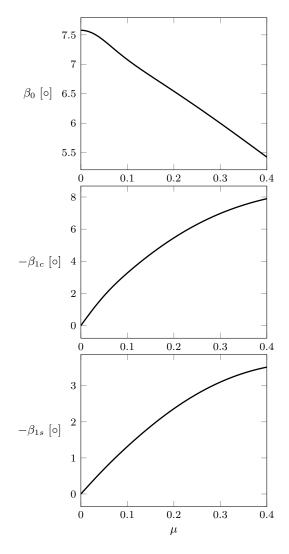


Figure 1: Flapping coefficients as functions of advance ratio [2]

References

- [1] Raymond W. Prouty. *Helicopter Performance, Stability and Control.* 1986, pp. 467–469.
- [2] Wayne Johnson. Helicopter Theory. 1980, pp. 194–197.

```
function [varargout] = flappingangles(V,alpha,W,gamma,...
sigma,theta_tw,cla,omegaR,eR,R,options)
% Argument validation
arguments
          (1,1) {mustBeNumeric,mustBeReal}
          (1,1) {mustBeNumeric,mustBeReal}
alpha
          (1,1) {mustBeNumeric,mustBeNonnegative}
W
gamma
          (1,1) {mustBeNumeric,mustBeNonnegative}
sigma
          (1,1) {mustBeNumeric,mustBeNonnegative}
theta_tw (1,1) {mustBeNumeric,mustBeReal}
cla (1,1) {mustBeNumeric,mustBeReal}
omegaR
          (1,1) {mustBeNumeric,mustBeNonnegative}
          (1,1) {mustBeNumeric,mustBeNonnegative}
(1,1) {mustBeNumeric,mustBeNonnegative}
eR
options.output (1,1) string {mustBeMember(options.output,{'angles','
    coefficients'})} = 'angles'
options.sample (:,1) {mustBeNumeric,mustBeReal} = linspace(0,360,200)'
%% Preliminary calculations
% Converting to radians
theta_tw = theta_tw*pi/180;
% Thrust coefficient
Tc = W/(1.225*omegaR^2*pi*R^2);
% Advance ratio
mi = V*cosd(alpha)/omegaR;
% Adimensional inflow
lambda_i = sqrt(-.5*V.^2+.5*sqrt(V.^4+4*(W/(2*1.225*pi*R^2)).^2))/omegaR;
        = mi.*tand(alpha)+ lambda_i;
% Collective pitch
theta_0 = 6*Tc./(sigma*cla*(1+3/2*mi.^2)*(1-eR))...
-3/4*theta_tw*(1+mi.^2)./(1+3/2*mi.^2)+1.5*lambda./(1+3/2*mi.^2);
%% Flapping coefficients
% Coning
beta_0 = 1/6*gamma*(3/4*theta_0.*(1+mi.^2)+theta_tw*(3/5+mi.^2/2)-lambda)
*(1-eR)^2;
% Longitudinal flapping
beta_1c = -2*mi.*(4/3*theta_0+theta_tw-lambda)./(1-mi.^2/2)...
-12*eR./(gamma*(1-eR)^3*(1+mi.^4/4)).*(4/3*Tc/sigma*...
(2/3*mi*gamma/(cla*(1+3/2*eR))));
% Lateral flapping
beta_1s = -4/3*mi.*beta_0.*(1+eR/2)./((1+mi.^2/2)*(1-eR)^2)...
-12*eR*(1+eR/2)./(gamma*(1-eR)^3*(1+mi.^4/4))*...
2.*mi.*(4/3*theta_0+theta_tw—lambda);
% Output
if strcmpi(options.output,'coefficients')
varargout = {beta_0*180/pi,beta_1c*180/pi,beta_1s*180/pi};
else
psi
        = options.sample;
beta = (beta_0 + beta_1c.*cosd(psi) + beta_1s.*sind(psi))*180/pi;
beta_dot = ( -beta_1c.*sind(psi) + beta_1s.*cosd(psi))*180/pi;
varargout = {psi,beta,beta_dot};
end
end
```