

# **PowerInForwardFlight\_main\_tail\_rotor.m user guide**

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# 1 Introduction

## 1.1 Required power of main rotor in forward flight

The required power of main rotor in forward flight is calculated as:

$$P_{\text{request}} = P_i + P_0 + P_{\text{fus}}$$

Where:

$P_{\text{request}}$  is the power required;

$P_i$  is the induced power;

$P_0$  is the parasitic power;

$P_{\text{fus}}$  is the power absorbed by the fuselage.

$$P_0 = \pi \rho \frac{\sigma \bar{C}_d}{8} \Omega^3 R^5 [1 + k\mu^2] \quad \text{con} \quad \mu = \frac{V_\infty \cos \alpha}{\Omega R}$$

Assuming  $\alpha \cong 0$ :

$$P_i = T(V_\infty \sin \alpha + w) \cong Tw$$

Where, being in fast forward flight,  $T = W$ .

From Glauert's theory, that underly the rotor model in non-axial flow, it is derived that:

$$T = 2\dot{m}w = 2A\rho V'w$$

From the inversion of which we can derive  $w$ , then:

$$P_i = \frac{W^2}{2\rho AV'} \cong \frac{W^2}{2\rho AV_\infty}$$

In order to calculate the induced power more accurately, the equation describing the operating curve at constant-thrust of the rotor in forward flight is:

$$\tilde{P}_i = \tilde{V}_\infty \sin \alpha + \tilde{w} \cong \tilde{w}$$

We then solve axial induction by the equation:

$$(\tilde{V}_\infty \tilde{w} \sin \alpha + \tilde{w}^2)^2 + \tilde{V}_\infty^2 \tilde{w}^2 \cos^2 \alpha = 1$$

We go on to solve this second-degree equation in  $\tilde{w}$ , whose positive root is  $\tilde{w}$ . Then we obtain  $P_i$  from:

$$P_i = \tilde{P}_i P_h$$

Where  $P_h$  is the power under hovering conditions.

The parasitic power of the fuselage is given by:

$$P_{\text{fus}} = f \frac{1}{2} \rho_\infty V_\infty^3$$

Where the factor  $f$ , which has the size of a surface, is called the 'equivalent wet area'. A typical value is  $f/A \cong 0.007$ .

## 1.2 Required power of tail rotor in forward flight

The required power by the tail rotor is given by:

$$P_{rtail} = P_{indotta} + P_{parassita}$$

$P_{indotta}$  and  $P_{parassita}$  were calculated in the same way as was shown in the previous paragraph for the main rotor.

## 1.3 The complete helicopter system: the total required power

The total power required by the helicopter engines for forward flight is:

$$P_{tot} = [P_{rprincipal} + P_{rtail} + P_{aux}] \cdot \eta_t$$

Where  $P_{aux}$  is the power required by the on-board auxiliary systems. It assumes values between 10kW and 30kW.

$\eta_t$  is the coefficient that introduces transmission losses; it is assumed to be 1.03.

# 2 Inputs and outputs

## 2.1 Inputs

The function has the following inputs:

Altitude (h), asymptotic velocity vector ( $V_{inf}$ ), helicopter weight (W),

Main rotor's radius ( $v\_input(1)$ ), Main rotor's Area ( $v\_input(2)$ ), Main rotor's Solidity ( $v\_input(3)$ ), Main rotor's angular velocity ( $v\_input(4)$ ), Cd of main rotor's blade element ( $v\_input(5)$ ),

Tail rotor's radius ( $v\_input(6)$ ), Tail rotor's Area ( $v\_input(7)$ ), Tail rotor's solidity ( $v\_input(8)$ ), Tail rotor's angular velocity ( $v\_input(9)$ ), Cd of tail rotor's blade element ( $v\_input(10)$ ),

Distance between main rotor and tail rotor ( $v\_input(11)$ ), correction factor ( $v\_input(12)$ ), Auxiliary Power ( $v\_input(13)$ ), Coefficient due to transmission losses ( $v\_input(14)$ ), Available Power at sea level ( $v\_input(15)$ ).

## 2.2 Outputs

The function has the following outputs:

Induced Power, Parasitic Power and Required Power by the main rotor, Parasitic Power by the fuselage,

Induced Power, Parasitic Power and Required Power by the tail rotor,

Total Required Power, Available Power, Maximum Speed, Speed of maximum endurance and Speed of maximum Range.

### 3 Function description

```
function [ Pind_B, Ppar_rp, Pfus, P_tot_rp, ...
          Pind_rc, Ppar_rc, P_tot_rc, Ptot_req, Pdisp, ...
          V_NE, V_BE, V_BR] = PowerInForwardFlight_main_tail_rotor(h, Vinf, W, v_input)
% Required Power by the main rotor in forward flight
[~, ~, ~, rho] = atmosisa(h);
[~, ~, ~, rho_sl] = atmosisa(0);
```

The Available power varies with altitude:

$$P_{available} = P_{availableSL} \frac{\rho}{\rho_{SL}}$$

```
Pdisp = v_input(15)*rho/rho_sl;

%Total power of the main rotor
%Parasitic Power
mu_rp = Vinf./(v_input(4)*v_input(1));
Ppar_rp = (v_input(3)*v_input(5)/8.*(1+4.7*mu_rp.^2)).*...
          (pi*rho*v_input(4)^3*v_input(1)^5); % Rotor BEMT
          % obs: k=4.7 for radial speeds

T = W; % Hp small alpha, in forward flight
%Induced Power

%Impulsive Theory
Pind_A = W^2./(2*rho*v_input(2).*Vinf); %Glauert Theory

w_hov = 1/sqrt(2*rho)*sqrt(T/v_input(2));
Vinf_tilde = Vinf./w_hov;
w_tilde = sqrt((- (Vinf_tilde.^2)./2 + sqrt(((Vinf_tilde.^2)./2).^2+1)));
w_rotore = w_tilde*w_hov;
Pi_tilde = w_tilde; %Pi_tilde = Vinf_tilde*sin(alpha) + w = w because sin(alpha)=0
          % Hp: T constant
P_hov = T*w_hov;

Pind_B = Pi_tilde*P_hov;

%Fuselage Power
f = 0.007*v_input(2); % f: equivalent wet area
Pfus = 0.5*rho.*Vinf.^3*f;
%real main rotor's request Power

P_tot_rp = v_input(12)*Pind_B + Ppar_rp + Pfus;

%Total Power of the tail rotor

mu_rc = Vinf./(v_input(9)*v_input(6));

% Induced Power
Q_rot_main = P_tot_rp./(v_input(4));
T_tail_required = Q_rot_main/v_input(11);
whov_rc = 1/sqrt(2*rho).*sqrt(T_tail_required./v_input(7)); % Impulsive Theory
Vinf_tilde_rc = Vinf./whov_rc;
```

```

w_tilde_rc = sqrt((- (Vinf_tilde_rc.^2)./2 +...
    sqrt(((Vinf_tilde_rc.^2)./2).^2+1)));
w_rotor_rc = w_tilde_rc.*whov_rc;

Pind_rc = T_tail_required.*w_rotor_rc;

%Parasitic Power
Ppar_rc = (v_input(8)*v_input(10)/8.*(1+4.7*mu_rc.^2)).*...
    pi*rho*v_input(9)^3*v_input(6)^5;
% Total power of the tail rotor
P_tot_rc = v_input(12)*Pind_rc + Ppar_rc;

% Total power required by total helicopter system
% in forward flight

v_P_au = v_input(13)*ones(1,length(Vinf));
Ptot_req = (P_tot_rp+P_tot_rc+v_P_au)*v_input(14);

```

Maximum Speed in forward flight is determined by comparing the available Power with the total required Power. It corresponds to the value of the speed for which the available power is equal to the total required power.

The speed of maximum endurance is obtained at the minimum value of required power.

The speed of maximum range is obtained at the minimum value of the  $\frac{\text{required power}}{\text{speed}}$  ratio.

```

% Maximum speed in forward flight
for f=(length(Vinf)/2):length(Vinf)
    if (Pdisp>=Ptot_req(f-1) && Pdisp<Ptot_req(f))
        V_NE = (Vinf(f)+Vinf(f-1))/2;
    end
end

% Speed of maximum endurance
for f=1:length(Vinf)
    if (Ptot_req(f)==min(Ptot_req))
        V_BE = Vinf(f);
    end
end

% Speed of maximum Range
for f=1:length(Vinf)
    if (Ptot_req(f)/Vinf(f) == min(Ptot_req./Vinf))
        V_BR = Vinf(f);
    end
end
end

```

## 4 Test Case

A test case was performed in order to validate the function.

```
% DATA

% 1) Aircraft
Wto      = 9979.03*9.81;      % [N]
Pd_sl    = 2110000;           % [W]
h         = 0;                % [m]

T0       = 288; % K
mu0      = 1.79e-5; % Kg/(ms)
[Temp, a0, P0, rho] = atmosisa(h);
mu_viscoso = mu0*(Temp/T0)^1.5*(T0+110)/(Temp+110); % Sutherland's law

% 2) Main rotor                                % Tail rotor
N         = 4;                                N_rc    = 4;
R_rp      = 8.18;                             R_rc      = 1.7; % [m]
A_rp      = pi*R_rp^2;                         A_rc      = pi*R_rc^2; % [m^2]
c         = 0.53;                             c_rc      = 0.2; % [m]
sigma_rp  = 0.082;                           sigma_rc  = 0.188;
Vtip      = 220.98;                          Vtip_rc   = 208.79; % [m/s]
Omega_rp  = Vtip/R_rp;                        Omega_rc  = Vtip_rc/R_rc;
n         = Omega_rp/(2*pi);                  n_rc     = Omega_rc/(2*pi);

b = 10.73; % [m]

thetal_rp = -18;                             thetal_rc = -17; % [deg]
Num        = 10;
r_rp       = linspace(0.05,R_rp,Num); r_rc    = linspace(0.05,R_rc,Num);
r_adim_rp  = r_rp/R_rp;                     r_adim_rc = r_rc./R_rc;

Cd_rc=0.01;
Cd_rp=0.01;

k = 1.15;

%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
Forward Flight-Required Power at different altitudes and weights
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

numero    = 120;
Vinf      = linspace(0,120,numero);
P_aus     = 25000; % [W]
P_ausil   = P_aus*ones(1,length(Vinf));
eta_rc    = 1.03;

%Available Power

v_h = linspace(0, 1800, length(Vinf));

[~, ~, ~, rho_sl] = atmosisa(0);

for j = 1:length(v_h)
    [a,b,c,density] = atmosisa(v_h(j));
    v_Pdisponibile(j)= Pd_sl*density/rho_sl;
end
figure
plot(v_h,v_Pdisponibile, 'k');
xlabel('h [m]'); ylabel('P_a_v_a_i [W]'); title('Available power at different h');
```

```

grid on;

%Total Power at different altitudes and weights

v_WTO = [0.75*Wto,0.90*Wto, Wto];

h = [0,1000,1800];

v_input = [R_rp, A_rp, sigma_rp, Omega_rp, Cd_rp, ...
            R_rc, A_rc, sigma_rc, Omega_rc, Cd_rc, ...
            braccio, k, P_aus, eta_rc, Pd_sl];

for i = 1:length(h)
    for j = 1:length(v_WTO)

        [Pindotta_B, Pparassita_rp,Pfus,Ptot_rp,...
         Pindotta_rc, Pparassita_rc, Ptot_rc,Ptot_richiesta(j,:),Pdisp,...
         V_NE,V_BE, V_BR] = PowerInForwardFlight_main_tail_rotor(h(i), Vinf, v_WTO(j),...
         v_input);

        Pdisponibile(j,:) = Pdisp*ones(1,length(Vinf));

        if (h(i) == 0 && v_WTO(j) == Wto)

% Plot
        figure
        plot(Vinf,Pindotta_B,'k-.',Vinf,Pparassita_rp,'k--',Vinf,Pfus,'k:',Vinf,Ptot_rp,'k-
',Vinf,Pdisponibile(j,:),'.-k');
        hold on;
        assey = linspace(0,Ptot_rp(end),numero);
        xlabel('V_∞ [m/s]'); ylabel('P [W]'); title('Required power of the main rotor in
forward flight');
        subtitle(['altitude h = ',num2str(h(i)), 'm']);
        legend('P_i_n_d','P_p_a_r','P_f_u_s_o_l_a_g_e','P_t_o_t','P_a_v_a_i');
        grid on

        figure
        plot(Vinf,Pparassita_rc,'k-.',Vinf,Pindotta_rc,'k--',Vinf,Ptot_rc,'k-');
        title('Powers of the tail rotor'); xlabel('V_∞ [m/s]'); ylabel('P [W]');
        subtitle(['altitude h = ',num2str(h(i)), 'm']);
        legend('P_p_a_r','P_i_n_d','P_t_o_t');
        grid on;

        figure
        plot(Vinf,Ptot_rp,'k-.',Vinf,Ptot_rc,'k--
',Vinf,P_ausil,'k:',Vinf,Ptot_richiesta(j,:),'k-',Vinf,Pdisponibile(j,:),'.-k');
        hold on;
        xlabel('V_∞ [m/s]'); ylabel('P [W]'); title('Total required power in forward
flight');
        subtitle(['altitude h = ',num2str(h(i)), 'm']);
        legend('P_m_a_i_n_r_o_t_o_r','P_t_a_i_l_r_o_t_o_r','P_a_u_x','P_t_o_t',
'P_a_v_a_i');
        grid on

    end
end

figure
plot(Vinf,Ptot_richiesta(j,:),'.-k');
xlabel('V_∞ [m/s]'); ylabel('P [W]');
subtitle(['altitude h = ',num2str(h(i)), 'm']);
hold on;
plot(Vinf,Pdisponibile(j,:),'k');
assey = linspace(0,Ptot_richiesta(end),numero);

```

```

plot(V_NE*ones(1,numero),assey,'k-.');
plot(V_BE*ones(1,numero),assey,'k--');
plot(V_BR*ones(1,numero),assey,'k');
legend('P_t_o_t','P_d_i_s_p','V_N_E','V_B_E','V_B_R');

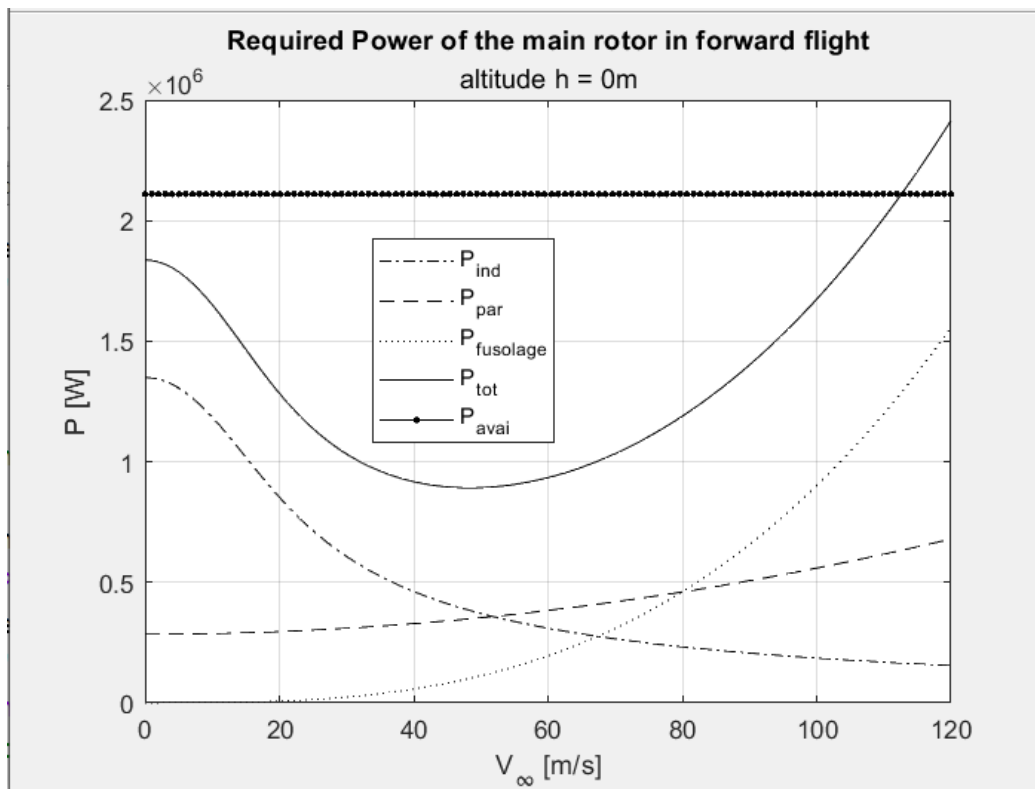
figure
plot(Vinf, Ptot_richiesta(1,:), 'k- ',...
Vinf, Ptot_richiesta(2,:), 'k--',...
Vinf, Ptot_richiesta(3,:), 'k-.',...
Vinf, Pdisponibile(j,:), '.-k ');

title('Total required power in forward flight at different W_T_O')
subtitle(['altitude h = ',num2str(h(i)), 'm']);
xlabel('V_∞ [m/s]'); ylabel('P [W]');
legend('75% WTO',...
'90% WTO',...
'WTO',...
'P_a_v_a_i_l_a_b_l_e');

grid on;

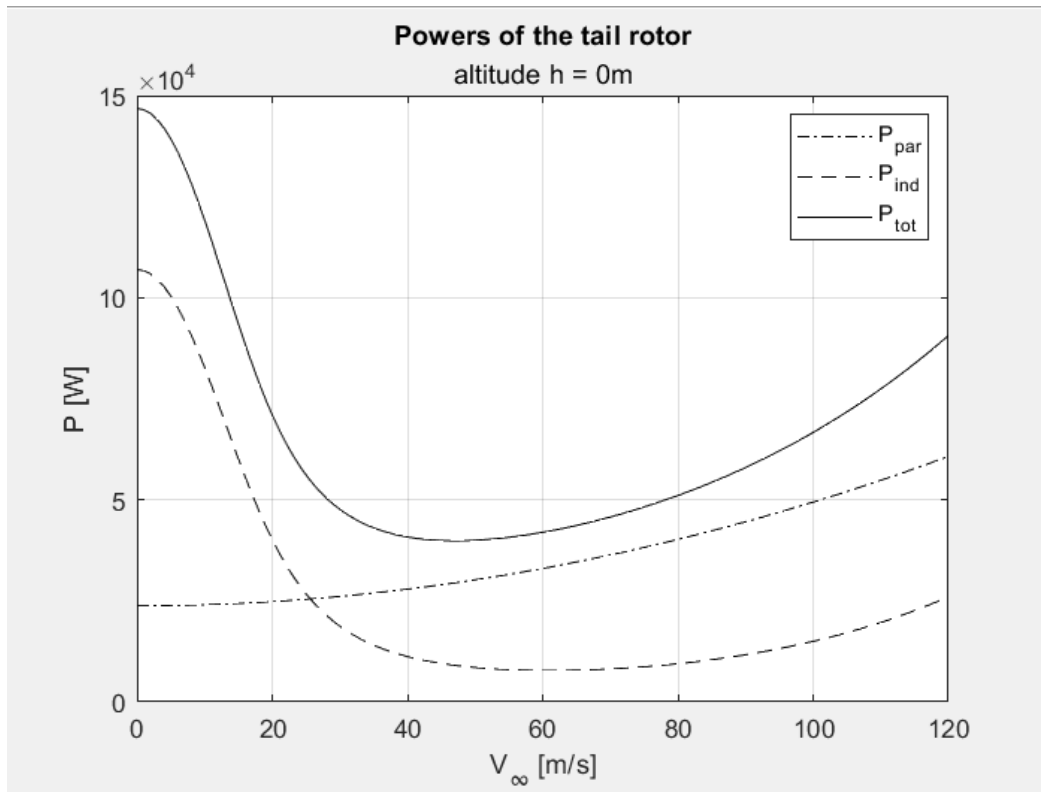
end

```

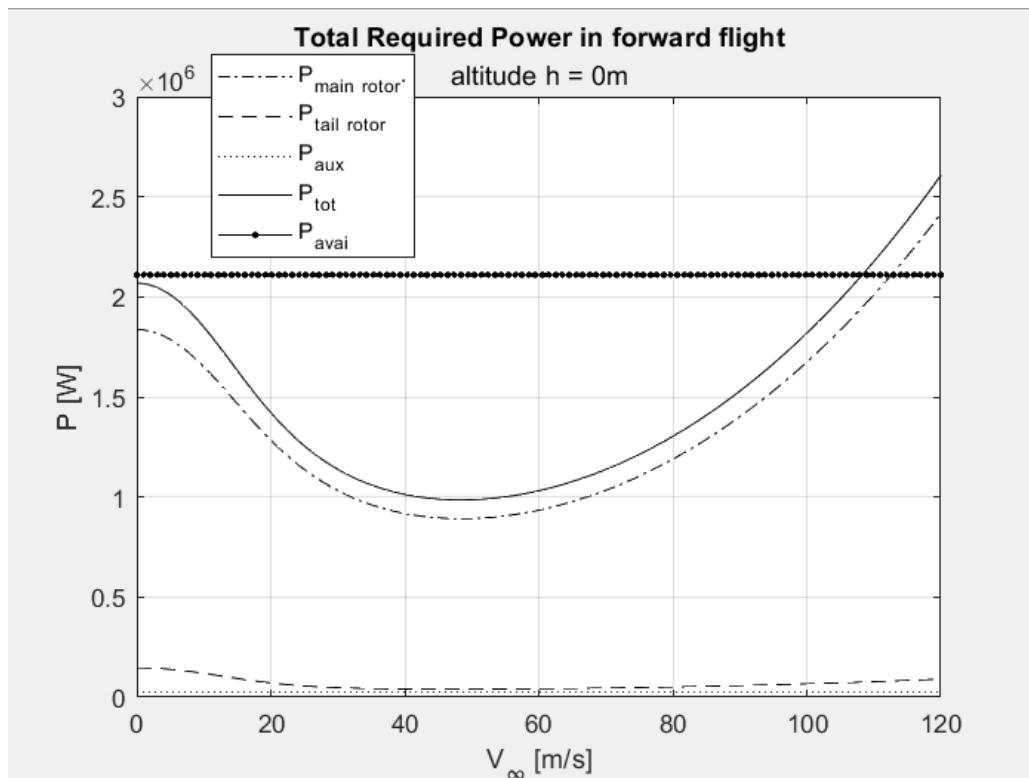


**Figure 4.1:** Powers of the main rotor in forward flight at Sea level.

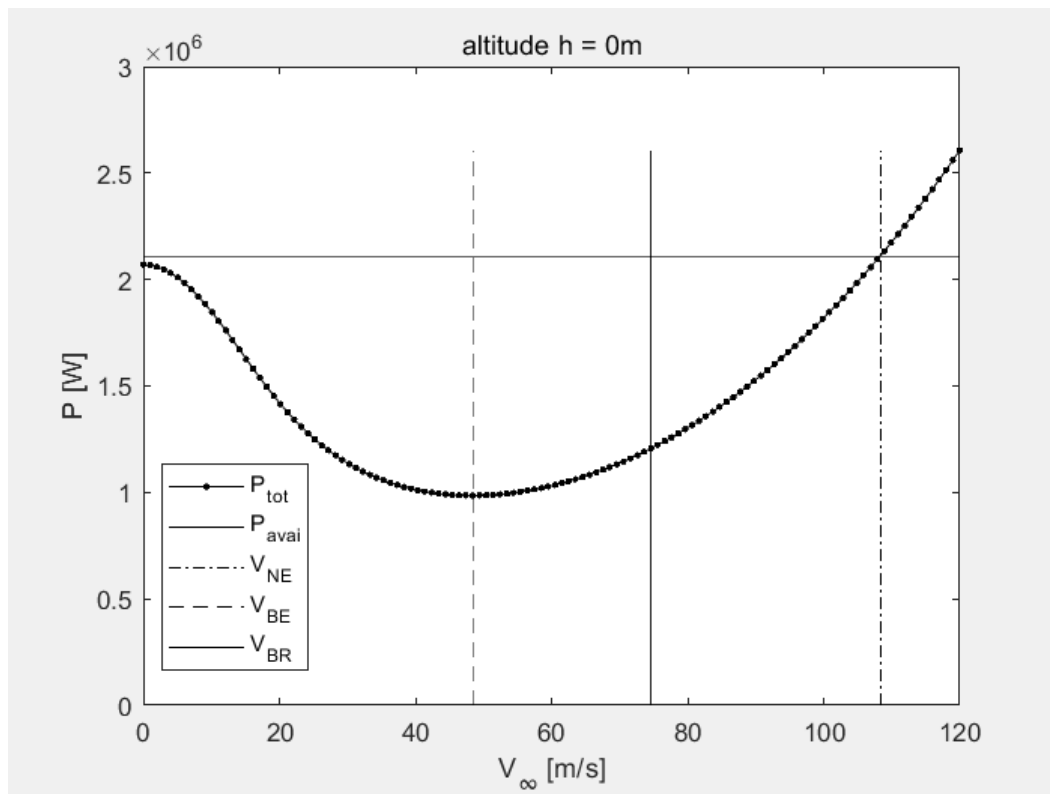




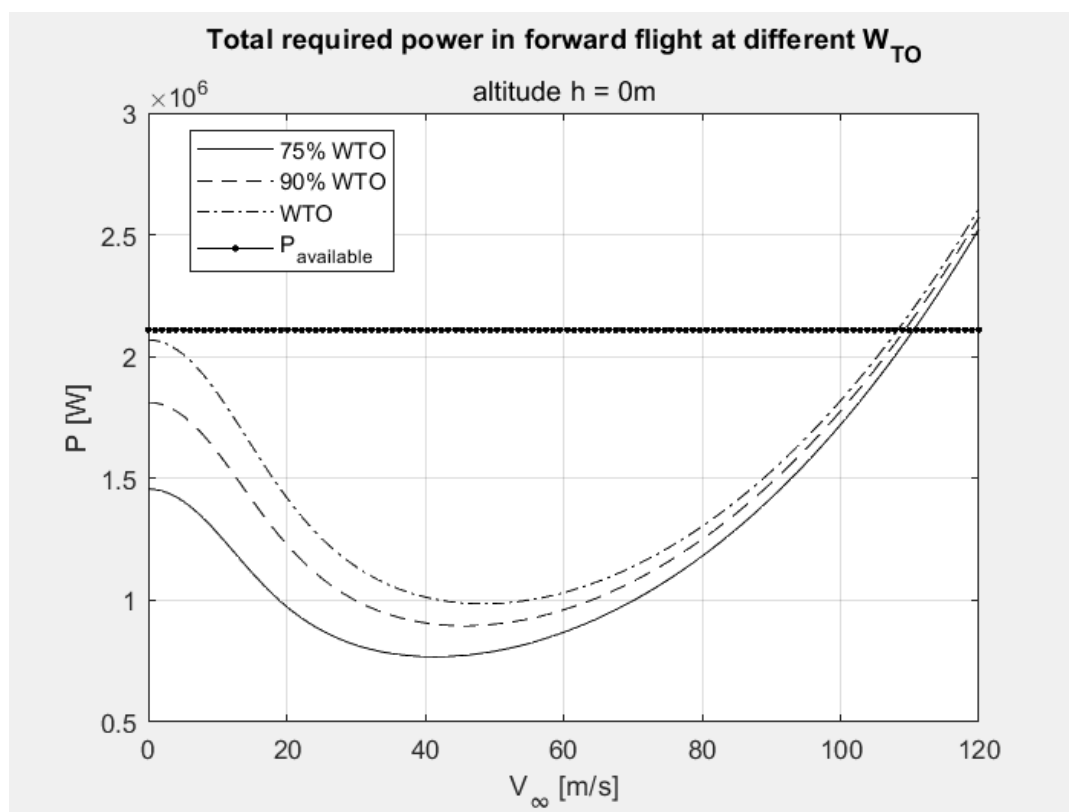
**Figure 4.2:** Powers of the tail rotor in forward flight at Sea level.



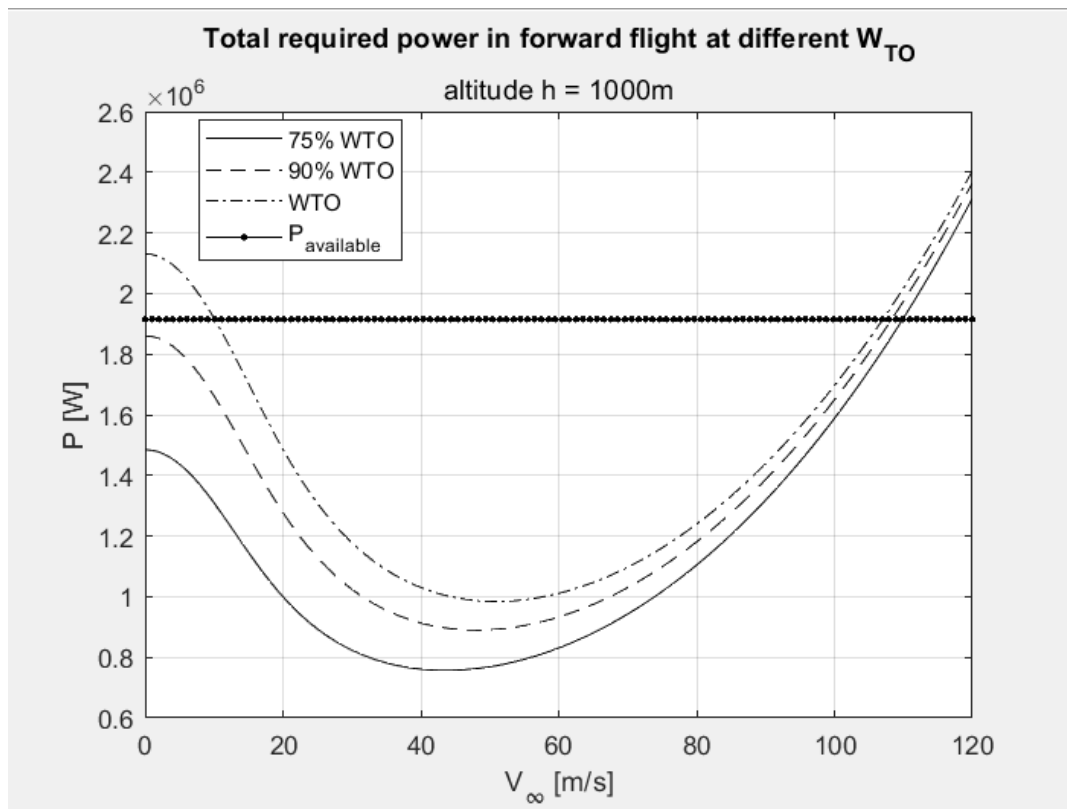
**Figure 4.3:** Total required powers in forward flight at Sea level.



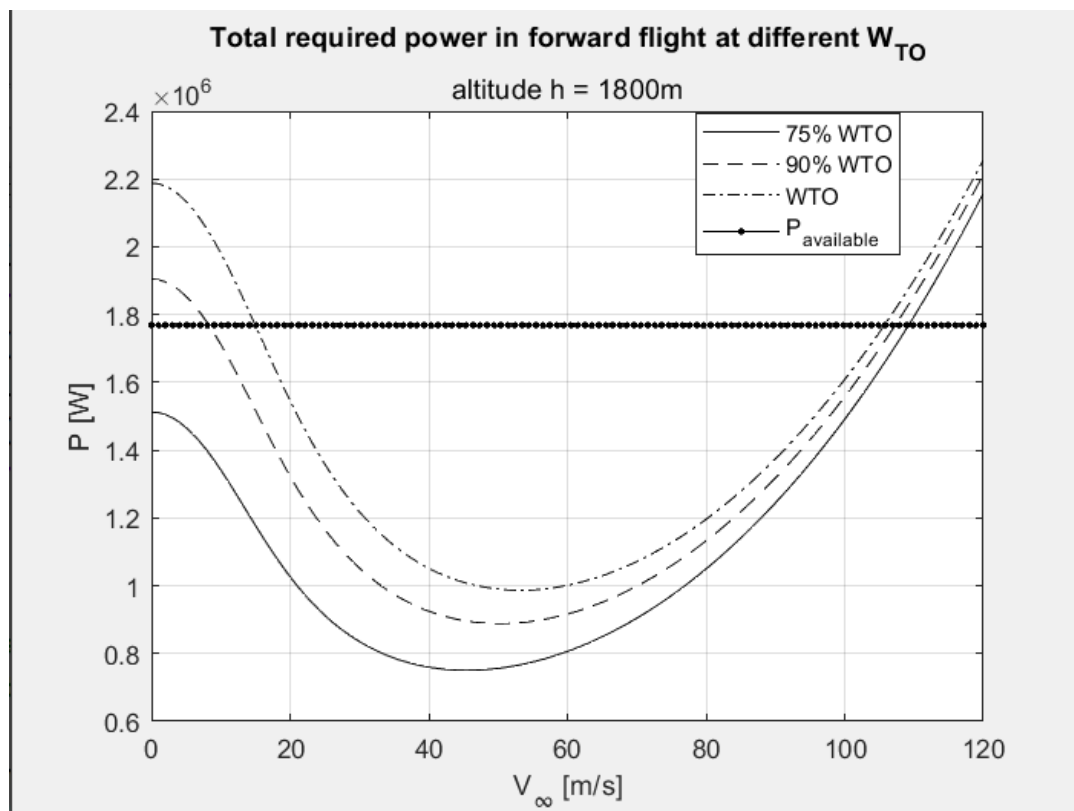
**Figure 4.4:** Maximum speed, speed of maximum endurance and speed of maximum range at Sea level.



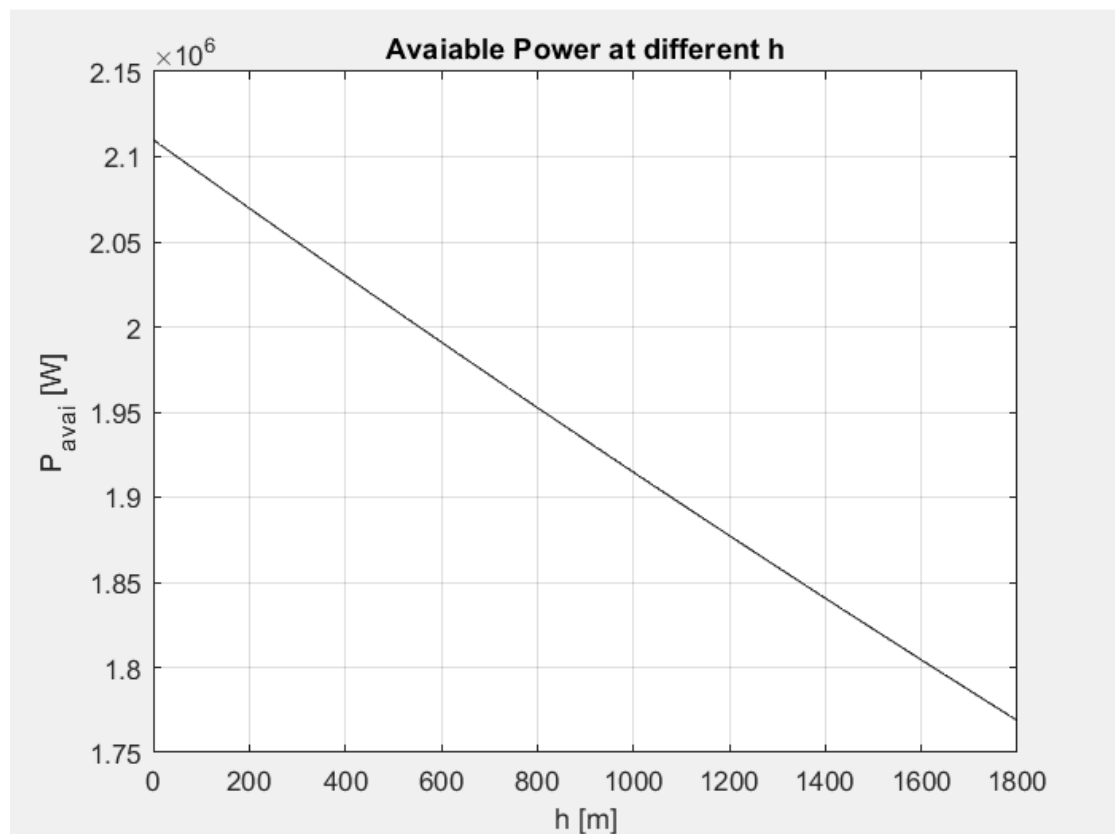
**Figure 4.5:** Total required power at different weights at Sea Level.



**Figure 4.6:** Total required power at different weights at 1000m.



**Figure 4.7:** Total required power at different weights 1800m.



**Figura 4.8:** Available Power at different altitudes.