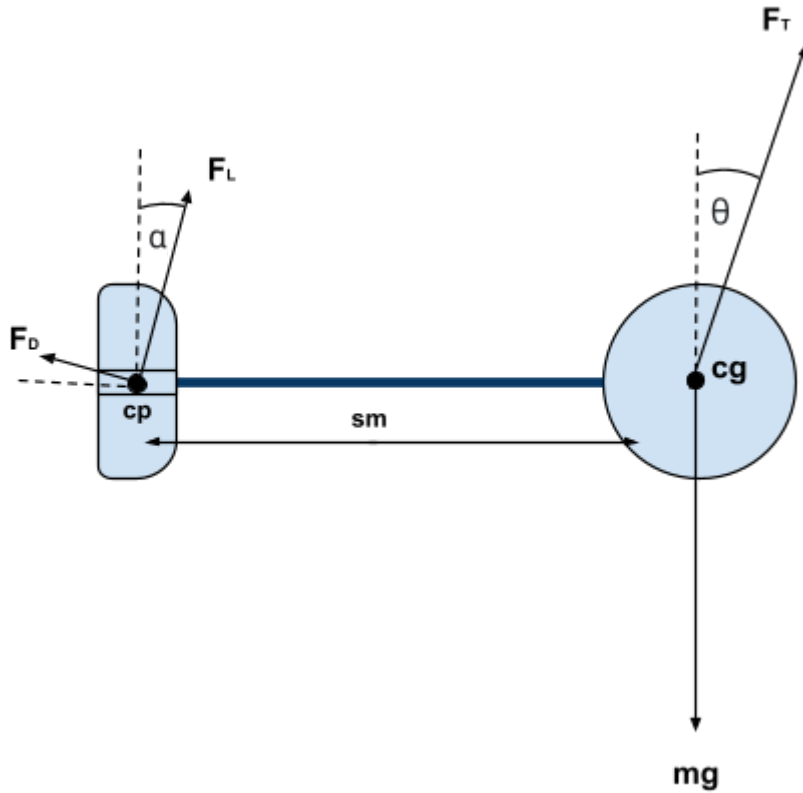


TOBIAS Pitch Axis Stability Analysis



Pitch axis stability equations about center of gravity:

$$\Sigma M_0: F_T \cos(\theta) d - F_D \sin(\alpha)(sm) - F_L \cos(\alpha)(sm) = 0$$

$$F_Y: F_T \cos(\theta) + F_D \sin(\alpha) + F_L \cos(\alpha) - mg = 0$$

$$F_X: F_T \sin(\theta) + F_L \sin(\alpha) - F_D \cos(\alpha) = 0$$

Rearrange moment equation & substitute for vertical component of tension using Y force balance:

$$d = \frac{F_D \sin(\alpha)(sm) + F_L \cos(\alpha)(sm)}{F_T \cos(\theta)} \Rightarrow d = \frac{F_D \sin(\alpha)(sm) + F_L \cos(\alpha)(sm)}{mg - F_D \sin(\alpha) - F_L \cos(\alpha)} = sm \frac{F_D \sin(\alpha) + F_L \cos(\alpha)}{mg - F_D \sin(\alpha) - F_L \cos(\alpha)}$$

Solving for d, method 1: Lift-to-drag ratio (approximation, as this assumes cruise condition)

$$d = (sm) \frac{F_L \left(\frac{\sin(\alpha)}{(L/D)} + \cos(\alpha) \right)}{mg - F_L \left(\frac{\sin(\alpha)}{(L/D)} - \cos(\alpha) \right)} = (sm) \frac{\left(\frac{1}{2} C_L \rho U_\infty^2 S \right) \left(\frac{\sin(\alpha)}{(L/D)} + \cos(\alpha) \right)}{mg - \left(\frac{1}{2} C_L \rho U_\infty^2 S \right) \left(\frac{\sin(\alpha)}{(L/D)} - \cos(\alpha) \right)}$$

Solving for d, method 2: Lift and Drag formulae

$$d = sm \frac{F_D \sin(\alpha) + F_L \cos(\alpha)}{mg - F_D \sin(\alpha) - F_L \cos(\alpha)} = sm \frac{(\frac{1}{2} \rho_{\infty} U_{\infty}^2 S_{wetted} C_f + \frac{2L^2}{e \rho_{\infty} U_{\infty}^2 \pi b^2}) \sin(\alpha) + (\frac{1}{2} C_L \rho U_{\infty}^2 S) \cos(\alpha)}{mg - (\frac{1}{2} \rho_{\infty} U_{\infty}^2 S_{wetted} C_f + \frac{2L^2}{e \rho_{\infty} U_{\infty}^2 \pi b^2}) \sin(\alpha) - (\frac{1}{2} C_L \rho U_{\infty}^2 S) \cos(\alpha)}$$

$$\Rightarrow d = sm \frac{(\rho_{\infty} U_{\infty}^2 S) (C_f + \frac{\frac{1}{2} (C_L \cos(\alpha)) (C_L S \cos(\alpha))}{e \pi b^2}) \sin(\alpha) + (\frac{1}{2} C_L) \cos(\alpha)}{mg - (\rho_{\infty} U_{\infty}^2 S) ((C_f + \frac{\frac{1}{2} (C_L \cos(\alpha)) (C_L S \cos(\alpha))}{e \pi b^2}) \sin(\alpha) + (\frac{1}{2} C_L) \cos(\alpha))}$$

Conclusion: the tether must attach to the towbody a distance d in front of the center of gravity, where d is of the form $sm \frac{aU_{\infty}^2}{b - aU_{\infty}^2}$. The faster the wind

speed, the further forward the tether attachment point. If we have any lift-generating surface behind the center of gravity, the tether attachment point must lie in front of the center of gravity, in order to balance the moments.

As the windspeed changes, we should shift the attachment point, the center of lift, or even the center of gravity - any of the three would resolve the moment imbalance.

Potential fix - a variable-sweep tail: Changing the sweep of the tail changes the magnitude of the lift, the position of the center of pressure, and slightly changes the position of the center of gravity.

Alternative fix proposed by Luis: a system that passively changes the attachment point as the windspeed changes.