

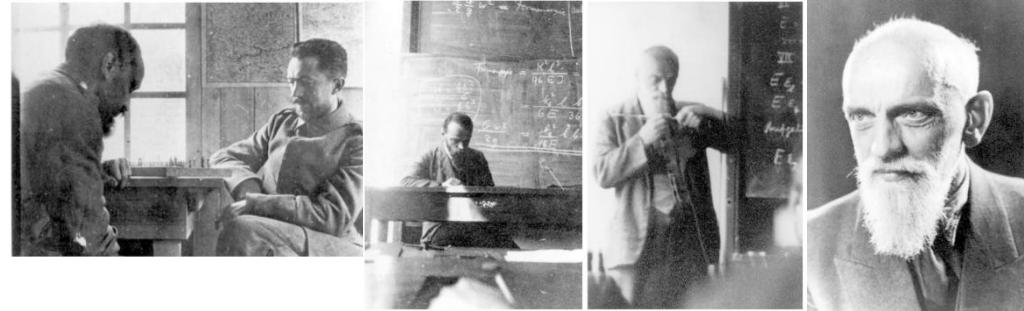
# Aerodynamics and Numerical Simulation Methods

Flat-Plate Boundary Layer (Blasius solution)



University of  
**BRISTOL**

# Blasius Solution



- For 2D, steady, incompressible flow along a flat plate, with no pressure gradients in the external flow, the boundary layer equations are reduced to:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2}$$

- With Boundary Conditions

$$u, v = 0$$

at the wall, and

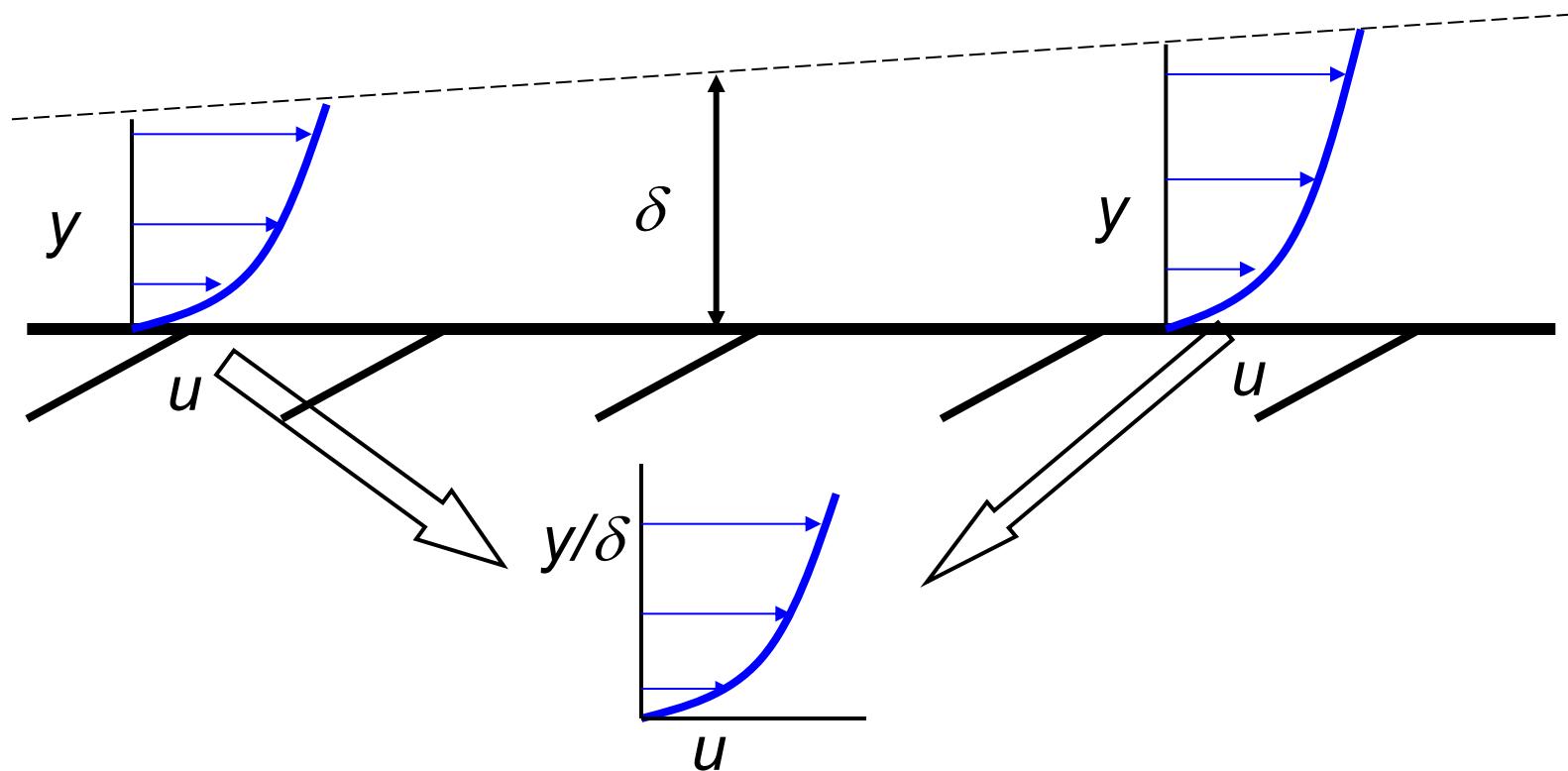
$$u = u_e, \frac{\partial u}{\partial y} = \frac{\partial^2 u}{\partial y^2} = \dots = 0$$

at the boundary layer edge

Kinematic viscosity

- Blasius goal: Reduce PDE to ODE!

Also, no external gradients, so flow is *similar*:



i.e. the velocity profiles are identical everywhere in terms of a fraction of boundary layer thickness

- This is because there are no gradients in  $x$  direction – No way for changes to occur, apart from b.l. thickness.

- If we introduce a new **auxiliary variable**  $\eta$  which scales with boundary layer height, then  $u$  for constant  $\eta$  is constant.

- What choice for  $\eta$ ? From dimensional analysis:

$$\delta \propto \frac{x}{\text{Re}_x^{\frac{1}{2}}}$$

$$\text{Re} = \frac{\rho u x}{\mu} = \frac{u x}{\nu}$$

$$\frac{x}{\text{Re}^{\frac{1}{2}}} = \frac{x \nu^{\frac{1}{2}}}{(u x)^{\frac{1}{2}}}$$

- So try:

$$\eta = \frac{1}{2} \frac{y}{\delta} = \frac{1}{2} \frac{y}{\frac{x}{\text{Re}^{\frac{1}{2}}}} = \frac{1}{2} \frac{y \text{Re}^{\frac{1}{2}}}{x} = \frac{1}{2} \frac{y}{x} \left( \frac{u_e x}{\nu} \right)^{\frac{1}{2}} = \frac{1}{2} y \left( \frac{u_e}{x \nu} \right)^{\frac{1}{2}}$$

Also, as we have incompressible flow, we know that the stream function exists (from continuity), i.e.

$$u = \frac{\partial \varphi}{\partial y}, \quad v = -\frac{\partial \varphi}{\partial x}$$

continuity:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = \frac{\partial^2 \varphi}{\partial x \partial y} - \frac{\partial^2 \varphi}{\partial y \partial x} \equiv 0$$

-Means we only need to find one variable, not two.

With these two ideas ( $\eta$ ,  $\varphi$ ), we define a **second auxiliary variable**:

$$\varphi = (u_e x \nu)^{\frac{1}{2}} \cdot F(\eta),$$

$$u = \frac{\partial \varphi}{\partial y}$$

Where  $F$  is some function. Then:

$$\Rightarrow \frac{\partial \varphi}{\partial y} = (u_e x \nu)^{\frac{1}{2}} \cdot F'(\eta) \frac{\partial \eta}{\partial y} + 0 \cdot F(\eta)$$

Also, from first auxiliary variable:

$$\eta = \frac{y}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}} \Rightarrow \frac{\partial \eta}{\partial y} = \frac{1}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}$$

Hence:  $u = (u_e x \nu)^{\frac{1}{2}} \frac{F' \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}}{2} = \frac{u_e F'}{2} \Rightarrow \boxed{\frac{u}{u_e} = \frac{F'}{2}}$

Similarly,

$$\varphi = (u_e x \nu)^{\frac{1}{2}} \cdot F(\eta)$$

Kinematic viscosity

$$\nu = -\frac{\partial \varphi}{\partial x}$$

Where  $F$  is some function. Then

$$\Rightarrow -\frac{\partial \varphi}{\partial x} = -(u_e x \nu)^{\frac{1}{2}} \cdot F'(\eta) \frac{\partial \eta}{\partial x} - \frac{1}{2} \left( \frac{u_e \nu}{x} \right)^{\frac{1}{2}} \cdot F(\eta)$$

Also, from first auxiliary variable  $\eta = \frac{y}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}} \Rightarrow \frac{\partial \eta}{\partial x} = -\frac{1}{2x} \frac{y}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}} = -\frac{\eta}{2x}$

Hence:

$$\nu = (u_e x \nu)^{\frac{1}{2}} \frac{\eta}{2x} F' - \frac{1}{2} \left( \frac{u_e \nu}{x} \right)^{\frac{1}{2}} \cdot F$$

Kinematic viscosity

$$\Rightarrow \boxed{\nu = \frac{1}{2} \left( \frac{u_e \nu}{x} \right)^{\frac{1}{2}} (F' \eta - F)}$$

# Take a deep breath and let's recap

- We want to solve the boundary layer equations for a 2D, steady, incompressible flow along a flat plate

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2}$$

- We introduced 2 auxiliary variables

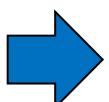
$$\eta = \frac{1}{2} \frac{y}{\delta} = \frac{1}{2} y \left( \frac{u_e}{x\nu} \right)^{1/2}$$

$$\varphi = (u_e x \nu)^{\frac{1}{2}} \cdot F(\eta)$$

Kinematic viscosity

- We solved for  $u$  and  $v$  using the stream functions

$$u = \frac{\partial \varphi}{\partial y}, \quad v = -\frac{\partial \varphi}{\partial x}$$



$$\frac{u}{u_e} = \frac{F'}{2}$$

$$v = \frac{1}{2} \left( \frac{u_e v}{x} \right)^{\frac{1}{2}} (F' \eta - F)$$

- We still need to solve for derivatives of u and v...

In the same way, we can differentiate u w.r.t, x, y & y again (try it yourself – this is examinable!):

$$\frac{\partial u}{\partial x} = -\frac{u_e}{2} F'' \frac{y}{4x} \left( \frac{u_e}{vx} \right)^{\frac{1}{2}}$$

$$\frac{\partial u}{\partial y} = u_e \frac{F'''}{4} \left( \frac{u_e}{vx} \right)^{\frac{1}{2}}$$

$$\frac{\partial^2 u}{\partial y^2} = \frac{u_e^2 F''''}{8vx}$$

Kinematic  
viscosity

We can then insert these into the x momentum equation:

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2}$$

First term of x-momentum equation:

$$u = \frac{u_e F'}{2}, \quad \frac{\partial u}{\partial x} = -\frac{u_e}{2} F'' \frac{y}{4x} \left( \frac{u_e}{vx} \right)^{\frac{1}{2}}$$

Hence

$$\begin{aligned} u \frac{\partial u}{\partial x} &= -\frac{u_e F'}{2} \frac{u_e F''}{2} \frac{y}{4x} \left( \frac{u_e}{vx} \right)^{\frac{1}{2}} \\ &= -\frac{y}{2} \left( \frac{u_e}{vx} \right)^{\frac{1}{2}} \left( \frac{u_e^2 F' F''}{8x} \right) \\ &= -\left( \frac{\eta u_e^2}{8x} \right) F' F'' \end{aligned}$$

Kinematic viscosity

## Second term of x-momentum equation:

$$\nu = \frac{1}{2} \left( \frac{u_e v}{x} \right)^{\frac{1}{2}} (F' \eta - F) \quad \frac{\partial u}{\partial y} = u_e \frac{F''}{4} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}$$

Hence

$$\nu \frac{\partial u}{\partial y} = \frac{1}{2} \left( \frac{u_e v}{x} \right)^{\frac{1}{2}} (F' \eta - F) u_e \frac{F''}{4} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}$$

$$= \frac{u_e^2 \eta}{8x} F' F'' - \frac{u_e^2}{8x} F F''$$

$$= \left( \frac{u_e^2 F''}{8x} \right) (F' \eta - F)$$

Kinematic viscosity

## RHS of x-momentum equation:

$$\nu \frac{\partial^2 u}{\partial y^2} = \nu \frac{u_e^2 F'''}{8vx} = \frac{u_e^2 F'''}{8x}$$

Kinematic viscosity

All the terms derived thus far have a common factor  $u_e^2/8x$ , so we divide by this, and add up the terms, giving:

$$u \frac{\partial u}{\partial x} + \nu \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2}$$

Kinematic viscosity

$$\Rightarrow -\eta F' F'' + \eta F' F'' - FF'' = F'''$$

i.e.

$$FF'' + F''' = 0$$

$$FF'' + F''' = 0$$

- i.e. we want a function that when multiplied by its second derivative w.r.t.  $\eta$ , is the negative of its third derivative.
- The form of this ODE can change depending on your initial choice of the definition of  $\eta$ .
- This ODE can be solved numerically and is quite simple on today's computers. Can even be done by hand.
- The first to do so was Blasius (a student of Prandtl's), hence it is named after him. It may be considered exact for incompressible, steady, 2D flow over a flat plate

# Quick refresher on solving ODEs...

## Example 1

Solve:  $\frac{dx}{dt} = 5x - 3$

$$\frac{dx}{5x - 3} = dt$$

$$\int \frac{dx}{5x - 3} = \int dt$$

$$x(t) = Ce^{5t} + \frac{3}{5}$$

## Example 2

Solve:  $\frac{dy}{dx} = 7y^2x^3$  with initial condition  $y(2) = 3$

$$\int y^{-2} dy = \int 7x^3 dx$$

$$y(x) = -\frac{1}{\frac{7}{4}x^4 + C}$$

Solve for C using I.C.

$$y(x) = -\frac{1}{\frac{7}{4}x^4 - \frac{85}{3}}$$

## How to solve?

$$FF'' + F''' = 0$$

- We know  $F(\eta)$  and  $\eta(x, y) = \frac{y}{2\delta}$
- Boundary conditions are key to solving the ODE
- At the wall,  $u=v=0$  (no-slip, no-flux)
  - $F'(\eta = 0) = 0$  ( $u$  equation)
  - $F(\eta = 0) = 0$  ( $v$  equation)
- At edge of boundary layer,  $u=u_e$ 
  - $F'(\eta \rightarrow \infty) = 2$
- This is still very difficult to solve analytically... Blasius did it using an analytical series solution technique
- We have computers now – let's solve it numerically

$$\frac{u}{u_e} = \frac{F'}{2}$$

Kinematic  
viscosity

$$\nu = \frac{1}{2} \left( \frac{u_e \nu}{x} \right)^{\frac{1}{2}} (F' \eta - F)$$

## Shooting method

$$FF'' + F''' = 0$$

- Cast the third order ODE as three coupled **first order ODE**:

$$\mathbf{F}'(\eta) = \mathbf{G}(\eta)$$

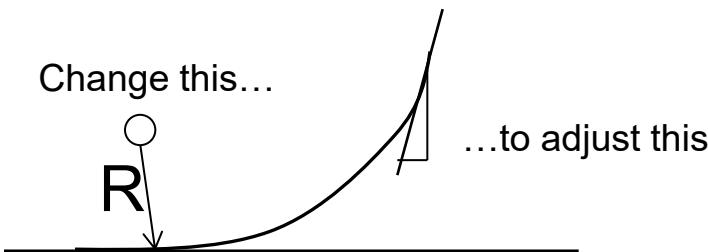
$$\mathbf{G}'(\eta) = F''(\eta) = \mathbf{H}(\eta)$$

$$\mathbf{H}'(\eta) = F'''(\eta) = -F(\eta)F''(\eta) = -\mathbf{F}(\eta)\mathbf{H}(\eta)$$

- B.C. gives us  $F(0) = F'(0) = G(0) = 0$
- Still stuck because we don't have a value for  $H(\eta = 0)$
- Employ an iterative approach known as the shooting method
- ODEs integrated numerically using Euler Predictor-Corrector method, solve by the shooting method

# Shooting method

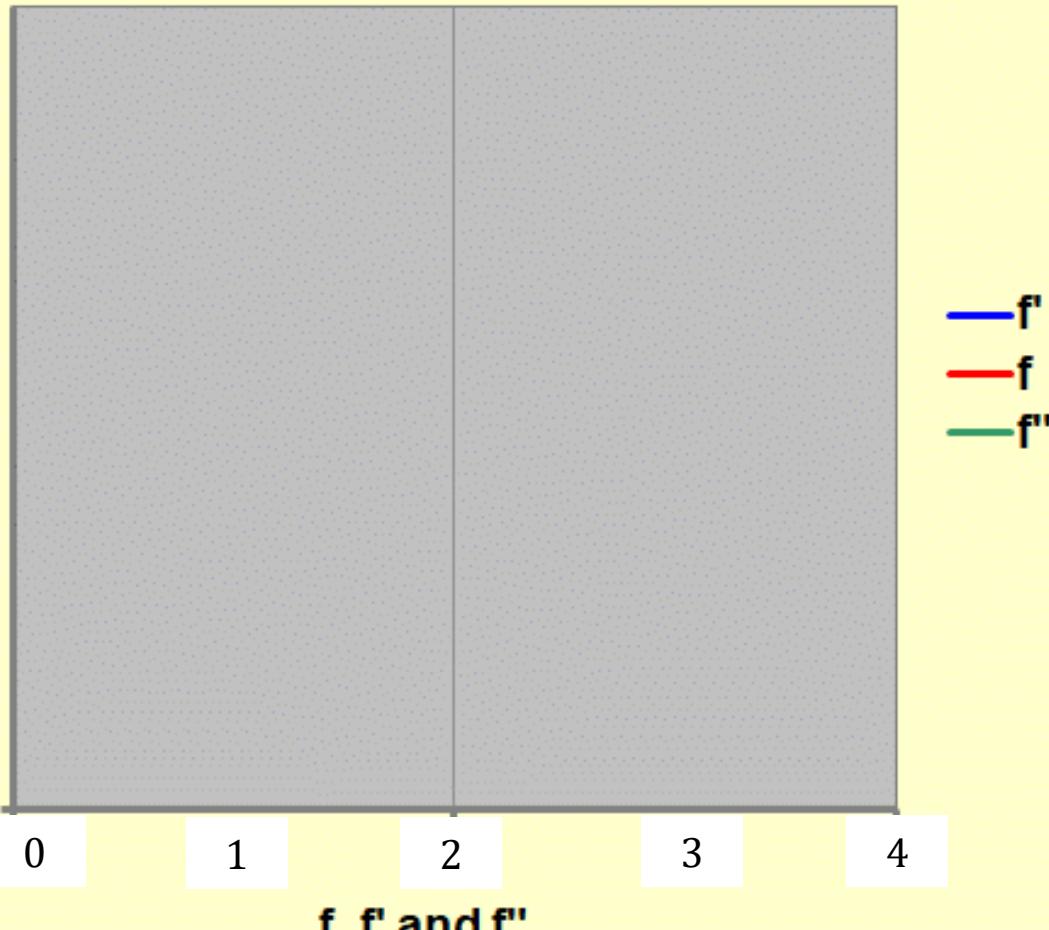
- Find solutions to the initial value problem by changing the initial conditions until we find the solution that also satisfies the boundary conditions of the original boundary value problem
- Guess  $F''(0) = H(0)$  and see if the trajectory allows us to find the correct  $F'(\eta \rightarrow \infty) = 2$  at the edge
  - Check the value of  $F'$  at the edge and adjust  $F''$
  - Repeat process with new value of  $F''(0)$
  - This is equivalent to iterating on the wall shear stress



$$\frac{\partial u}{\partial y} = u_e \frac{F''}{4} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}$$

Kinematic viscosity

## Blasius Equation Using Shooting



$$\frac{u}{u_e} = \frac{F'}{2}$$

$$\frac{\partial u}{\partial y} = u_e \frac{F''}{4} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}$$

Kinematic viscosity

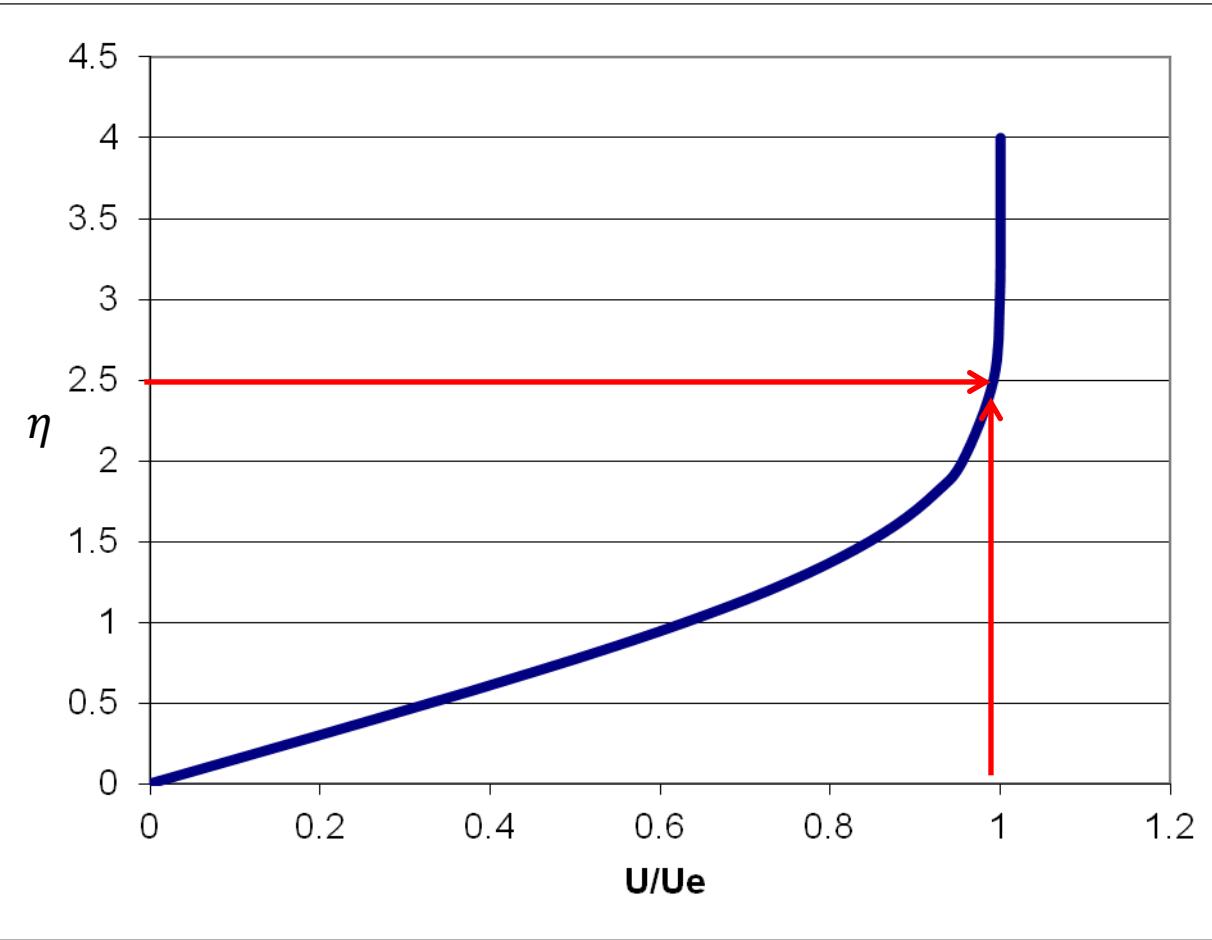
$$\frac{\partial^2 u}{\partial y^2} = \frac{u_e^2 F'''}{8\nu x}$$

$$F'(\eta \rightarrow \infty) = 2$$

$$F'(\eta = 0) = 0$$

$$F(\eta = 0) = 0$$

Adapted from: <https://www.robertribando.com/xls/fluid-mechanics/solution-of-blasius-equation/>



$$\frac{u}{u_e} = \frac{F'}{2}$$

$$\eta = \frac{1}{2} \frac{y}{\delta} = \frac{1}{2} y \left( \frac{u_e}{x \nu} \right)^{1/2} \quad \rightarrow \quad 2.5 = \frac{1}{2} \delta \left( \frac{u_e}{\nu x} \right)^{1/2} = \frac{1}{2} \frac{\delta}{x} \left( \frac{u_e x}{\nu} \right)^{1/2}$$

From last time (slide 16)...

$$\frac{\delta}{x} = 5 \left( \frac{u_e x}{\nu} \right)^{1/2}$$

Kinematic viscosity

This profile can be numerically integrated using definitions of momentum and displacement thickness (slide 21/22) to give:

$$\frac{\delta^*}{x} = \frac{1.721}{\text{Re}_x^{1/2}} \quad \frac{\theta}{x} = \frac{0.664}{\text{Re}_x^{1/2}}$$

Friction coefficient can be computed as:

$$c_f = \frac{\tau_w}{\frac{1}{2} \rho_e u_e^2} = \frac{0.664}{\text{Re}_x^{1/2}} = \frac{\theta}{x} \quad \tau = \mu \frac{\partial U}{\partial y}$$

Drag coefficient on a (one-sided) plate of length x:

$$c_d = 2c_f = \frac{1.328}{\text{Re}_x^{1/2}}$$