

# Aerodynamics and Numerical Simulation Methods

Flat-Plate Boundary Layer (Blasius solution)



University of  
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# Blasius Solution



- For 2D, steady, incompressible flow along a flat plate, with no pressure gradients in the external flow, the boundary layer equations are reduced to:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2}$$

- With Boundary Conditions

$$u, v = 0$$

at the wall, and

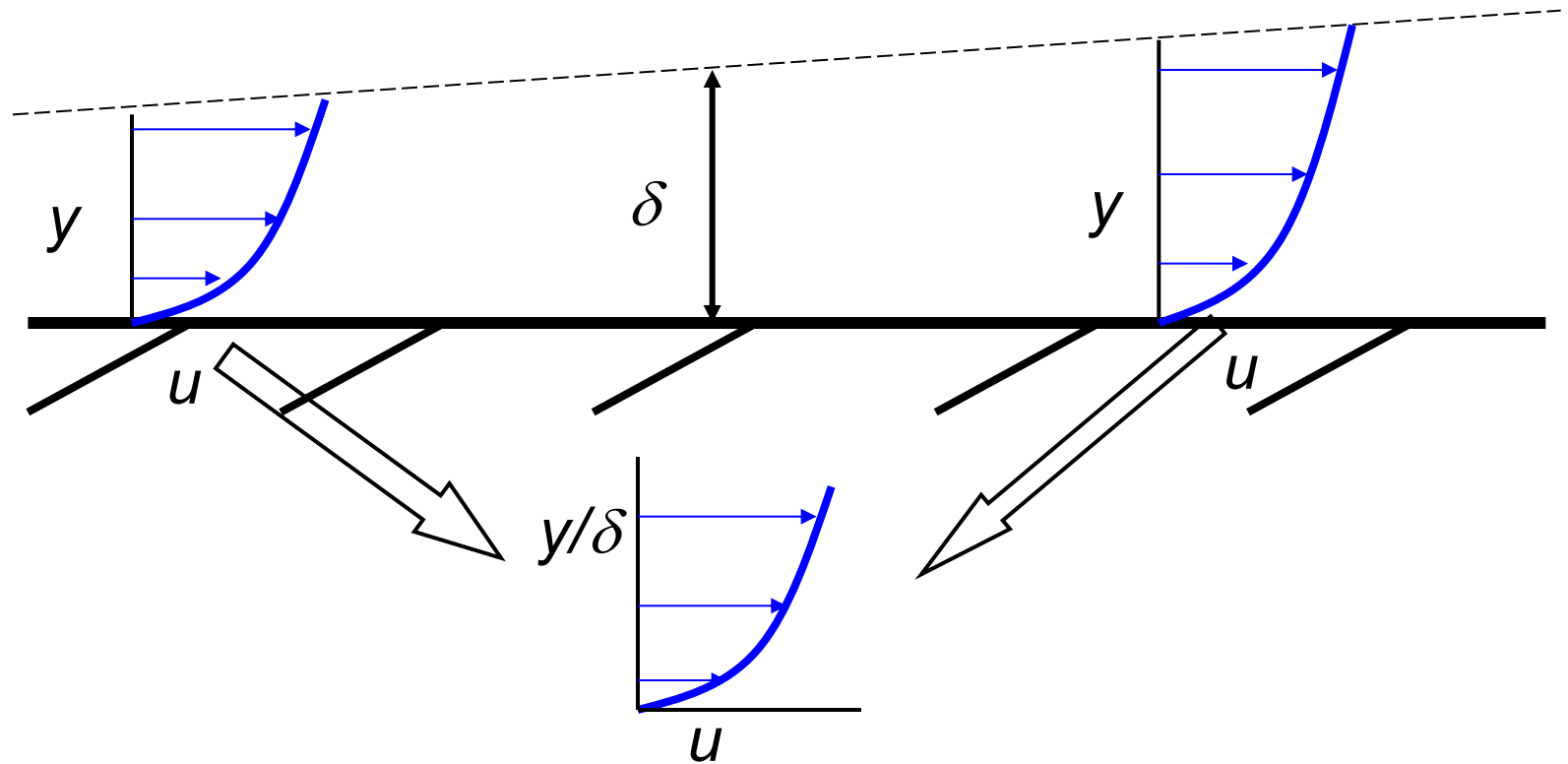
$$u = u_e, \frac{\partial u}{\partial y} = \frac{\partial^2 u}{\partial y^2} = \dots = 0$$

at the boundary  
layer edge

Kinematic  
viscosity

- Blasius goal: Reduce PDE to ODE!

Also, no external gradients, so flow is *similar*:



*i.e.* the velocity profiles are identical everywhere in terms of a fraction of boundary layer thickness

- This is because there are no gradients in  $x$  direction – No way for changes to occur, apart from b.l. thickness.
- If we introduce a new **auxiliary variable**  $\eta$  which scales with boundary layer height, then  $u$  for constant  $\eta$  is constant.
- What choice for  $\eta$ ? From dimensional analysis:

$$\delta \propto \frac{x}{\text{Re}_x^{\frac{1}{2}}}$$

$$\text{Re} = \frac{\rho u x}{\mu} = \frac{u x}{\nu}$$

$$\frac{x}{\text{Re}^{\frac{1}{2}}} = \frac{x \nu^{\frac{1}{2}}}{(u x)^{\frac{1}{2}}}$$

Kinematic  
viscosity

- So try:

$$\eta = \frac{1}{2} \frac{y}{\delta} = \frac{1}{2} \frac{y}{\frac{x}{\text{Re}_x^{\frac{1}{2}}}} = \frac{1}{2} \frac{y \text{Re}_x^{\frac{1}{2}}}{x} = \frac{1}{2} \frac{y}{x} \left( \frac{u_e x}{\nu} \right)^{\frac{1}{2}} = \frac{1}{2} y \left( \frac{u_e}{x \nu} \right)^{\frac{1}{2}}$$

Kinematic  
viscosity

Also, as we have incompressible flow, we know that the stream function exists (from continuity), i.e.

$$u = \frac{\partial \phi}{\partial y}, \quad v = -\frac{\partial \phi}{\partial x}$$

continuity:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = \frac{\partial^2 \phi}{\partial x \partial y} - \frac{\partial^2 \phi}{\partial y \partial x} \equiv 0$$

-Means we only need to find one variable, not two.

With these two ideas ( $\eta$ ,  $\varphi$ ), we define a **second auxiliary variable**:

$$\varphi = (u_e x \nu)^{\frac{1}{2}} . F(\eta),$$

$$u = \frac{\partial \varphi}{\partial y}$$

Where  $F$  is some function. Then:

Kinematic  
viscosity

$$\Rightarrow \frac{\partial \varphi}{\partial y} = (u_e x \nu)^{\frac{1}{2}} . F'(\eta) \frac{\partial \eta}{\partial y} + 0 . F(\eta)$$

Also, from  
first auxiliary  
variable:

$$\eta = \frac{y}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}} \Rightarrow \frac{\partial \eta}{\partial y} = \frac{1}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}$$

Kinematic  
viscosity

Hence: 
$$u = (u_e x \nu)^{\frac{1}{2}} \frac{F'(\eta)}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}} = \frac{u_e F'}{2} \Rightarrow \boxed{\frac{u}{u_e} = \frac{F'}{2}}$$

Similarly,

$$\varphi = (u_e x \nu)^{\frac{1}{2}} \cdot F(\eta)$$

Where  $F$  is some function. Then

$$\Rightarrow -\frac{\partial \varphi}{\partial x} = -(u_e x \nu)^{\frac{1}{2}} \cdot F'(\eta) \frac{\partial \eta}{\partial x} - \frac{1}{2} \left( \frac{u_e \nu}{x} \right)^{\frac{1}{2}} \cdot F(\eta)$$

$$\nu = -\frac{\partial \varphi}{\partial x}$$

Also, from first auxiliary variable:

$$\eta = \frac{y}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}} \Rightarrow \frac{\partial \eta}{\partial x} = -\frac{1}{2x} \frac{y}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}} = -\frac{\eta}{2x}$$

Hence:

$$\nu = (u_e x \nu)^{\frac{1}{2}} \frac{\eta}{2x} F' - \frac{1}{2} \left( \frac{u_e \nu}{x} \right)^{\frac{1}{2}} \cdot F$$

$$\Rightarrow \boxed{\nu = \frac{1}{2} \left( \frac{u_e \nu}{x} \right)^{\frac{1}{2}} (F' \eta - F)}$$

Kinematic  
viscosity

Kinematic  
viscosity

## Take a deep breath and let's recap

- We want to solve the boundary layer equations for a 2D, steady, incompressible flow along a flat plate

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2}$$

- We introduced 2 auxiliary variables

$$\eta = \frac{1}{2} \frac{y}{\delta} = \frac{1}{2} y \left( \frac{u_e}{x\nu} \right)^{1/2}$$

$$\varphi = (u_e x \nu)^{1/2} F(\eta)$$

Kinematic  
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- We solved for u and v using the stream functions

$$u = \frac{\partial \varphi}{\partial y}, \quad v = -\frac{\partial \varphi}{\partial x} \quad \Rightarrow \quad \boxed{\frac{u}{u_e} = \frac{F'}{2}} \quad \boxed{v = \frac{1}{2} \left( \frac{u_e \nu}{x} \right)^{1/2} (F' \eta - F)}$$



- We still need to solve for derivatives of  $u$  and  $v$ ...

In the same way, we can differentiate  $u$  w.r.t,  $x$ ,  $y$  &  $y$  again (try it yourself – this is examinable!):

$$\frac{\partial u}{\partial x} = -\frac{u_e}{2} F'' \frac{y}{4x} \left( \frac{u_e}{vx} \right)^{\frac{1}{2}} \quad \frac{\partial u}{\partial y} = u_e \frac{F''}{4} \left( \frac{u_e}{vx} \right)^{\frac{1}{2}}$$

$$\frac{\partial^2 u}{\partial y^2} = \frac{u_e^2 F'''}{8vx}$$

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We can then insert these into the x momentum equation:

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2}$$

First term of x-momentum equation:

$$u = \frac{u_e F'}{2}, \quad \frac{\partial u}{\partial x} = -\frac{u_e}{2} F'' \frac{y}{4x} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}$$

Hence

$$\begin{aligned} u \frac{\partial u}{\partial x} &= -\frac{u_e F'}{2} \frac{u_e F''}{2} \frac{y}{4x} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}} \\ &= -\frac{y}{2} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}} \left( \frac{u_e^2 F' F''}{8x} \right) \\ &= -\left( \frac{\eta u_e^2}{8x} \right) F' F'' \end{aligned}$$

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Second term of x-momentum equation:

$$v = \frac{1}{2} \left( \frac{u_e v}{x} \right)^{\frac{1}{2}} (F' \eta - F) \quad \frac{\partial u}{\partial y} = u_e \frac{F''}{4} \left( \frac{u_e}{v x} \right)^{\frac{1}{2}}$$

Hence

$$\begin{aligned} v \frac{\partial u}{\partial y} &= \frac{1}{2} \left( \frac{u_e v}{x} \right)^{\frac{1}{2}} (F' \eta - F) u_e \frac{F''}{4} \left( \frac{u_e}{v x} \right)^{\frac{1}{2}} \\ &= \frac{u_e^2 \eta}{8x} F' F'' - \frac{u_e^2}{8x} F F'' \\ &= \left( \frac{u_e^2 F''}{8x} \right) (F' \eta - F) \end{aligned}$$

Kinematic viscosity

RHS of x-momentum equation:

$$\nu \frac{\partial^2 u}{\partial y^2} = \nu \frac{u_e^2 F'''}{8\nu x} = \frac{u_e^2 F'''}{8x}$$

Kinematic viscosity

All the terms derived thus far have a common factor  $u_e^2/8x$ , so we divide by this, and add up the terms, giving:

$$u \frac{\partial u}{\partial x} + \nu \frac{\partial u}{\partial y} = \nu \frac{\partial^2 u}{\partial y^2}$$

Kinematic viscosity

$$\Rightarrow -\eta F' F'' + \eta F' F'' - FF'' = F'''$$

i.e.

$$FF'' + F''' = 0$$

$$FF'' + F''' = 0$$

- i.e. we want a function that when multiplied by its second derivative w.r.t.  $\eta$ , is the negative of its third derivative.
- The form of this ODE can change depending on your initial choice of the definition of  $\eta$ .
- This ODE can be solved numerically and is quite simple on today's computers. Can even be done by hand.
- The first to do so was Blasius (a student of Prandtl's), hence it is named after him. It may be considered *exact* for incompressible, steady, 2D flow over a flat plate

# Quick refresher on solving ODEs...

## Example 1

Solve:  $\frac{dx}{dt} = 5x - 3$

$$\frac{dx}{5x - 3} = dt$$

$$\int \frac{dx}{5x - 3} = \int dt$$

$$x(t) = Ce^{5t} + \frac{3}{5}$$

## Example 2

Solve:  $\frac{dy}{dx} = 7y^2x^3$  with  
initial condition  $y(2) = 3$

$$\int y^{-2} dy = \int 7x^3 dx$$

$$y(x) = -\frac{1}{\frac{7}{4}x^4 + C}$$

Solve for C using I.C.

$$y(x) = -\frac{1}{\frac{7}{4}x^4 - \frac{85}{3}}$$

How to solve?

$$FF'' + F''' = 0$$

- We know  $F(\eta)$  and  $\eta(x, y) = \frac{y}{2\delta}$
- Boundary conditions are key to solving the ODE
- At the wall,  $u=v=0$  (no-slip, no-flux)

- $F'(\eta = 0) = 0$  (u equation)
- $F(\eta = 0) = 0$  (v equation)

- At edge of boundary layer,  $u=u_e$

- $F'(\eta \rightarrow \infty) = 2$

$$\frac{u}{u_e} = \frac{F'}{2}$$

Kinematic  
viscosity

$$v = \frac{1}{2} \left( \frac{u_e \nu}{x} \right)^{\frac{1}{2}} (F' \eta - F)$$

- This is still very difficult to solve analytically... Blasius did it using an analytical series solution technique
- We have computers now – let's solve it numerically

## Shooting method

$$FF'' + F''' = 0$$

- Cast the third order ODE as three coupled **first order** ODE:

$$F'(\eta) = G(\eta)$$

$$G'(\eta) = F''(\eta) = H(\eta)$$

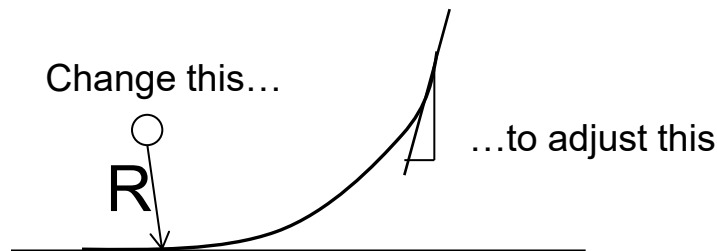
$$H'(\eta) = F'''(\eta) = -F(\eta)F''(\eta) = -F(\eta)H(\eta)$$

- B.C. gives us  $F(0) = F'(0) = G(0) = 0$
- Still stuck because we don't have a value for  $H(\eta = 0)$
- Employ an iterative approach known as the shooting method
- ODEs integrated numerically using Euler Predictor-Corrector method, solve by the shooting method



# Shooting method

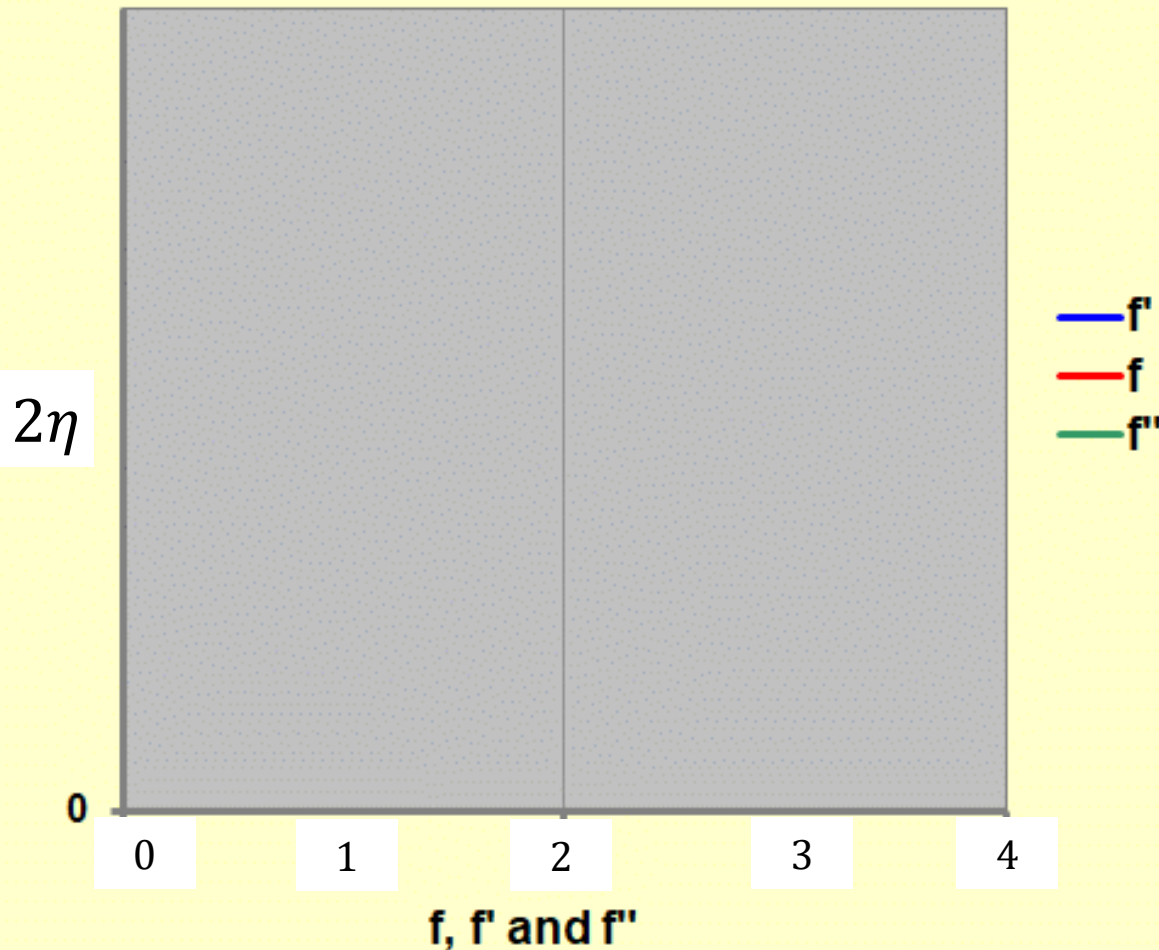
- Find solutions to the initial value problem by changing the initial conditions until we find the solution that also satisfies the boundary conditions of the original boundary value problem
1. Guess  $F''(0) = H(0)$  and see if the trajectory allows us to find the correct  $F'(\eta \rightarrow \infty) = 2$  at the edge
  2. Check the value of  $F'$  at the edge and adjust  $F''$
  3. Repeat process with new value of  $F''(0)$
  4. This is equivalent to iterating on the wall shear stress



$$\frac{\partial u}{\partial y} = u_e \frac{F''}{4} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}$$

Kinematic viscosity

## Blasius Equation Using Shooting



$$\frac{u}{u_e} = \frac{F'}{2}$$

$$\frac{\partial u}{\partial y} = u_e \frac{F''}{4} \left( \frac{u_e}{\nu x} \right)^{\frac{1}{2}}$$

Kinematic  
viscosity

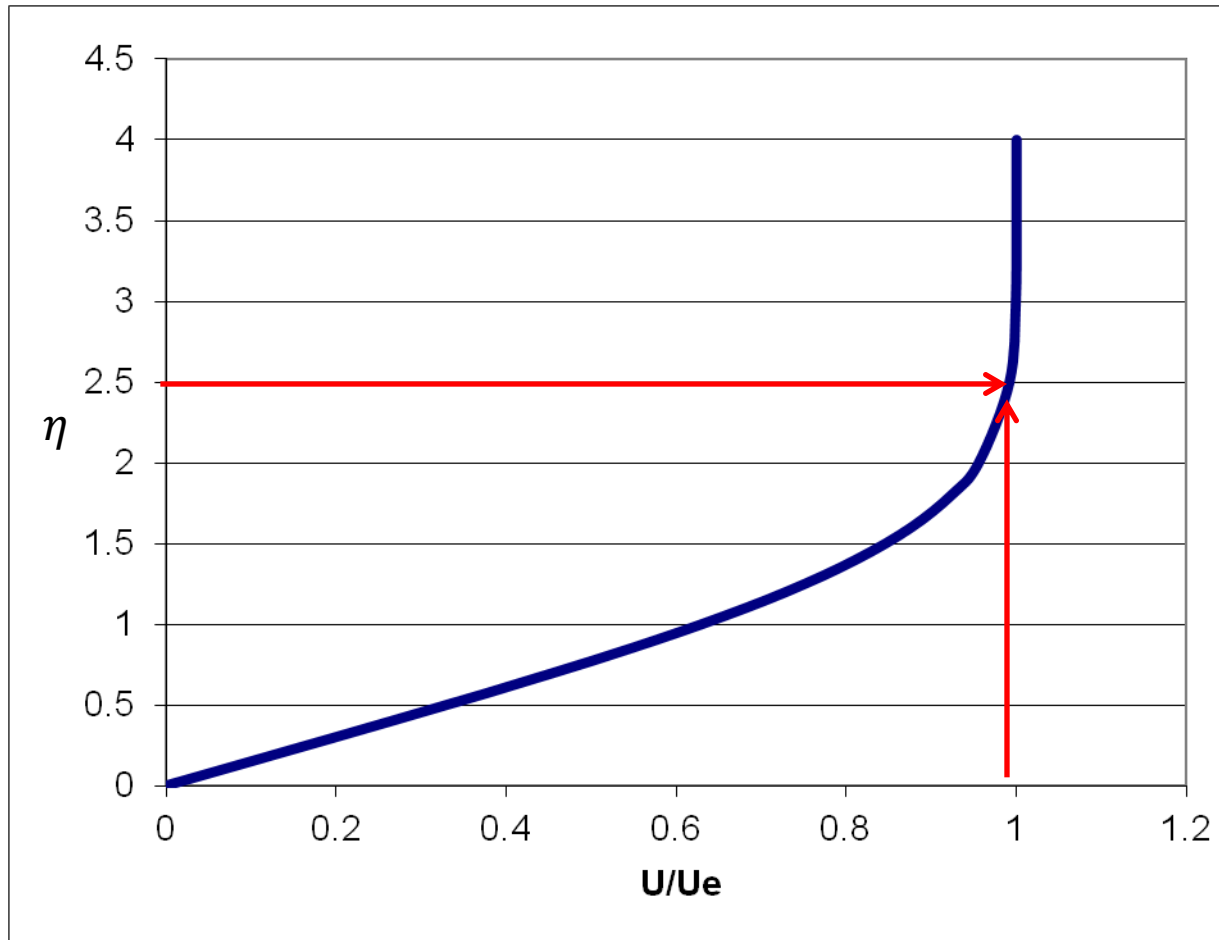
$$\frac{\partial^2 u}{\partial y^2} = \frac{u_e^2 F'''}{8\nu x}$$

$$F'(\eta \rightarrow \infty) = 2$$

$$F'(\eta = 0) = 0$$

$$F(\eta = 0) = 0$$

Adapted from: <https://www.robertribando.com/xls/fluid-mechanics/solution-of-blasius-equation/>



$$\frac{u}{u_e} = \frac{F'}{2}$$

$$\eta = \frac{1}{2} \frac{y}{\delta} = \frac{1}{2} y \left( \frac{u_e}{x\nu} \right)^{1/2} \quad \rightarrow \quad 2.5 = \frac{1}{2} \delta \left( \frac{u_e}{\nu x} \right)^{1/2} = \frac{1}{2} \frac{\delta}{x} \left( \frac{u_e x}{\nu} \right)^{1/2}$$

From last time (slide 16)...  $\frac{\delta}{x} = 5 \left( \frac{u_e x}{\nu} \right)^{-1/2}$

Kinematic viscosity

This profile can be numerically integrated using definitions of momentum and displacement thickness (slide 21/22) to give:

$$\frac{\delta^*}{x} = \frac{1.721}{\text{Re}_x^{\frac{1}{2}}} \qquad \frac{\theta}{x} = \frac{0.664}{\text{Re}_x^{\frac{1}{2}}}$$

Friction coefficient can be computed as:

$$c_f = \frac{\tau_w}{\frac{1}{2} \rho_e u_e^2} = \frac{0.664}{\text{Re}_x^{1/2}} = \frac{\theta}{x} \qquad \tau = \mu \frac{\partial U}{\partial y}$$

Drag coefficient on a (one-sided) plate of length  $x$ :

$$c_d = 2c_f = \frac{1.328}{\text{Re}_x^{1/2}}$$