école: normalesupérieure

## WORKSHOP Année de Recherche Pré-doctorale à l'Etranger (A.R.P.E.)

Alexis Blaise TALLA SIMO alexis.talla\_simo@ens-paris-saclay.fr

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## PROPOSAL OF A 3D CONSTITUTIVE MODEL BASED ON ELASTOPLASTICITY WITH DAMAGE FOR THE MODELING

## OF UNREINFORCED MASONRY INTERFACES **Behavior curve of the model** Introduction and objective Masonry structures are composite structures made of brick and mortar. They were widely used in antiquity and are still relevant today because of the architectural aesthetics they offer. However, these structures are very vulnerable, especially to castle loads such as earthquakes and exposed winds,...Therefore, understanding the mechanical handling of masonry is essential to prevent accidents but also to build more robust and economical structures. It is Local and global algorigram **Internal variables** in this context that this project is part of the project, the aim of which is to set up tension and shear coupling tension and shear Local algorigram for the model a constitutive law based on elastoplasticity and damage to describe the behavior $\sigma_n$ $\tau_n$ $\dot{\kappa}_1 = \left| \Delta \dot{u}_n^p \right| = \dot{\lambda}_1$ $-\left(d_{n}^{n} d_{n}^{s}\right)$ of the interface of these structures when subjected to the combined stresses of $\dot{\kappa}_2 = \left| \Delta \dot{u}_S^p \right| = \dot{\lambda}_2$ $\overline{\tau}_n = \frac{\tau_n}{1 - d_n^s}$ compression tension, shear and compression. $\dot{\kappa}_3 = 2\dot{\lambda}_3 \sqrt{(\sigma_n)^2 + (C_{SS}\sigma_S)^2}$ Effective Stress sapce ( Multiplasticity surface for the model and plastic potential $\overline{\sigma}_{n+1}$ $\overline{\tau}_{n+1}$ ightharpoonup A criterion for tension failure (tension Cut – off) $F_T = Q_T = \sigma_n - \overline{f}_t(\kappa_3)$ > A Coulomb Criterion for Shear $F_S = \sqrt{(\sigma_s^2 + \sigma_s^2)} + \sigma_n \tan \phi - \overline{f_s}(\kappa_3)$ $Q_S = \sqrt{(\sigma_s^2 + \sigma_s^2)} + \sigma_n \tan \psi - c$ $-(d_{n+1}^n d_{n+1}^s)$ **Numerical implementation** $\sigma_{n+1} = \overline{\sigma}_{n+1} \left( 1 - d_{n+1}^n \right)$ $\tau_{n+1} = \overline{\tau}_{n+1} \left( 1 - d_{n+1}^{s} \right)$ General for of residual vector ightharpoonup A criterion for compression failure (cap): $F_C = Q_C = C_{nn}\sigma_n^2 + C_{ss}(\sigma_s^2 + \sigma_s^2) + C_n\sigma_n - (\overline{\sigma}(\kappa_3))^2$ $\left\{R^{j}\right\} = \left\{\begin{matrix} R^{j}_{\sigma} \\ R^{j}_{F} \end{matrix}\right\} = \left\{\begin{matrix} \{\sigma\}^{n+1} - \left\{\sigma^{trial}\right\}^{n+1} + \left[K_{1}\right] \sum_{i \in \{j_{ac}\}} \dot{\lambda}_{i}^{n+1} \left(\frac{\partial Q_{i}}{\partial \{\sigma\}}\right)^{n+1} \right\}$ Multi-plastic threshold surface in 3 and 2 dimensions $\left[\sigma^{trial}\right]^{n+1} = \left\{\sigma\right\}^n + \left[K^0\right]\left\{du\right\}$ computation of yield function $F_1 = C_{nn}(\sigma_{n+1}^{trial})^2 + C_{ss}(\tau_{n+1}^{trial})^2 - (f_c)^2$ **General form of Jacobian Matrix** $F_1 = \sigma_{n+1}^{trial} - f_t$ $F_2 = |\tau_{n+1}^{trial}| + \sigma_{n+1}^{trial} \times \tan \phi - f_s$ $au_{\scriptscriptstyle S}$ $F_1 < 0$ and $F_2 > 0$ $F_1 > 0$ and $F_2 >$ $F_1 < 0$ and $F_2 < 0$ $\tau_s^2 + \tau_t^2 + \left(\sigma \times \tan(\phi) - \overline{f_s}\right)^2 = 0$ $\sigma^{n+1} - \sigma_{trial}^{n+1} + k_n \ d\lambda_1 \frac{\partial Q_1}{\partial \sigma_{n+1}} = 0$ $\sigma_{n+1} = \sigma_n^{trial}$ $\tau_{n+1} = \tau_n^{trial}$ **Consistent tangent operator** $\sigma^{n+1} - \sigma_{trial}^{n+1} + k_n \, d\lambda_1 \frac{\partial Q_2}{\partial \sigma_{rel}} = 0$ Material level validation of the model $\tau^{n+1} - \tau_{trial}^{n+1} + k_s \, d\lambda_1 \frac{\partial Q_1}{\partial \tau_{n+1}} = 0 \quad F_1 = 0$ $\tau^{n+1} - \tau_{trial}^{n+1} + k_s \ d\lambda_1 \frac{\partial Q_2}{\partial \tau_{n+1}} = 0 \quad F_2 = 0$ $\left[\mathbb{L}_{n+1}^{i}\right] = \frac{\partial \sigma_{n+1}^{i}}{\partial \varepsilon_{n+1}^{i}} = H - \frac{H \frac{\partial Q}{\partial \sigma} \gamma^{T} H}{h + \gamma^{T} H \frac{\partial Q}{\partial \sigma}}$ Proposed model - - - Lourenço model $\sigma_{n+1}^{\cdot}$ $\tau_{n+1}^{\cdot}$ $\sigma_{n+1}^{\cdot}$ $\tau_{n+1}^{\cdot}$ Lourenço model $\left(\kappa_1^{n+1}\right)^{\cdot} \quad \left(\kappa_2^{n+1}\right)^{\cdot} = \kappa_2^n$ $\left(\kappa_2^{n+1}\right)^{\cdot} \quad \left(\kappa_1^{n+1}\right)^{\cdot} = \kappa_1^n$ $\sigma$ = - 0.86 MPa $F_2\left(\sigma_{n+1},\tau_{n+1},\left(\kappa_2^n\right)^{\cdot}\right)\leq 0$ $F_2\left(\sigma_{n+1},\tau_{n+1},\left(\kappa_2^n\right)^{\cdot}\right)\leq 0$ $F_1 = 0$ $F_2 = 0$ $\sigma$ = - 0.43 MPa $\triangleright$ tan $\phi$ Internal coefficient of friction $\triangleright$ tan $\psi$ dilatancy $\sigma$ = 0.00 MPa $\sigma_{n+1}$ $\tau_{n+1}$ $\sigma_{n+1} = \sigma_{n+1}^{\cdot} \quad \tau_{n+1} = \tau_{n+1}^{\cdot}$ $\sigma_{n+1} = \sigma_{n+1}$ $\tau_{n+1} = \tau_{n+1}$ 2.5 0.35 > c cohesion $\kappa_1^{n+1} = (\kappa_1^n)^{\cdot} \quad \kappa_2^{n+1} = (\kappa_2^n)^{\cdot}$ Displacement (dn) mm $\kappa_1^{n+1} = (\kappa_1^n)^{\cdot} \quad \kappa_2^{n+1} = (\kappa_2^n)^{\cdot}$ $\triangleright f_t$ tensile strength Global algorigram for FEM $\triangleright$ $f_c$ compressive strength i = i + 1 $\Delta U_i$ $\epsilon_i^{n+1}$ et $\Delta \epsilon_{i+1}^{n+1}$ $\triangleright [K_1] = (\mathbb{I} - [D])[K]$ Interface elasticity matrix $\triangleright$ { $\sigma$ } Vector of interface stress $F_i^{n+1}$ à partir de $\,\sigma_i^{n+1}$ $R_i^{n+1} = KU - F$ $R_i^{n+1}$ and $K_i^{n+1}$ $K^{n+1}$ à partir de $L_{ an}$ $\triangleright \lambda_i$ plastic multiplier $\succ C_{ss}$ , $C_{nn}$ and $C_n$ paterial parameters of cap



