

PROPOSAL OF A 3D CONSTITUTIVE MODEL BASED ON ELASTOPLASTICITY WITH DAMAGE FOR THE MODELING OF UNREINFORCED MASONRY INTERFACES

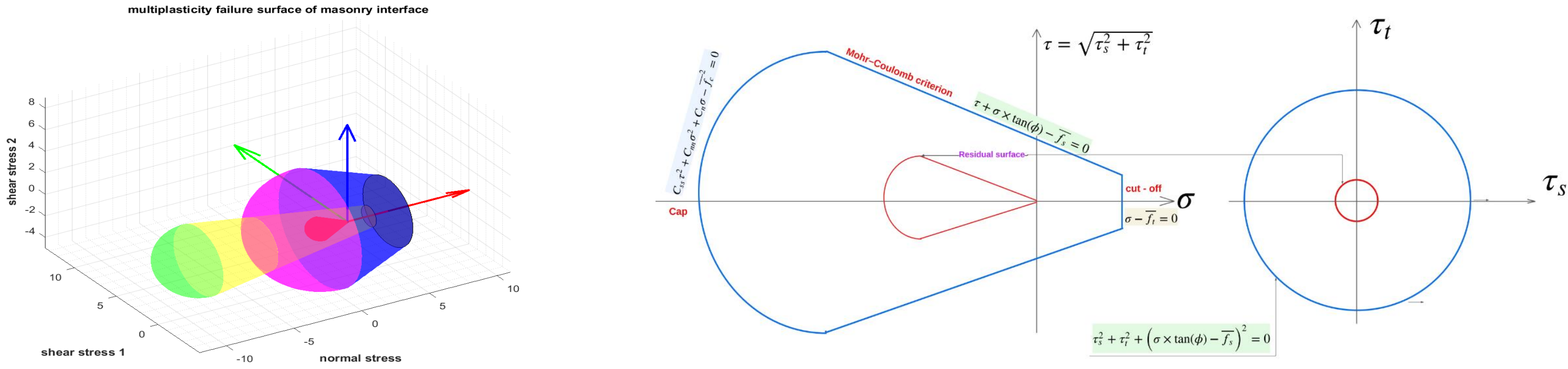
Introduction and objective

Masonry structures are composite structures made of brick and mortar. They were widely used in antiquity and are still relevant today because of the architectural aesthetics they offer. However, these structures are very vulnerable, especially when they are exposed to castle loads such as earthquakes and winds,...Therefore, understanding the mechanical handling of masonry is essential to prevent accidents but also to build more robust and economical structures. It is in this context that this project is part of the project, the aim of which is to set up a constitutive law based on elastoplasticity and damage to describe the behavior of the interface of these structures when subjected to the combined stresses of tension, shear and compression.

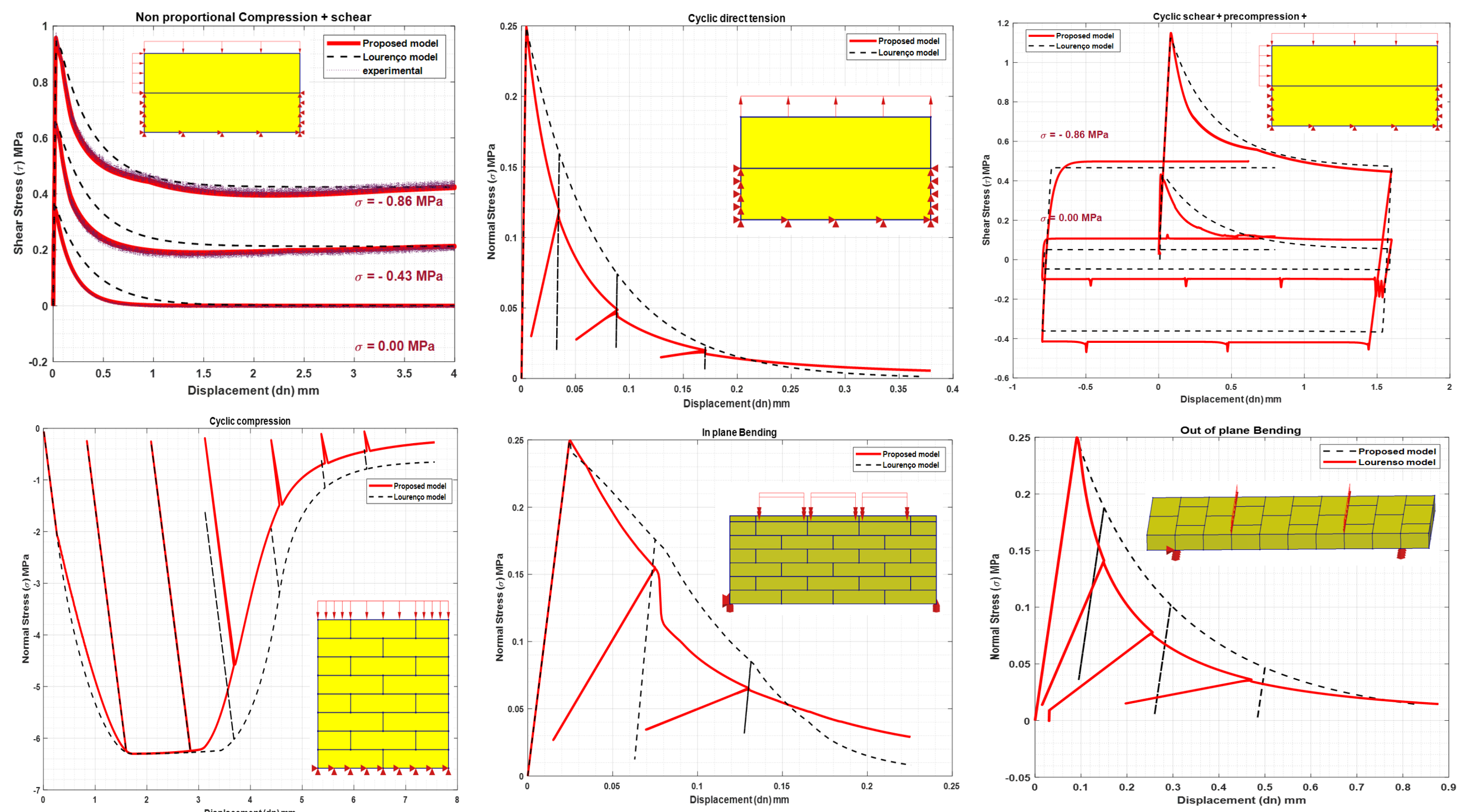
Multiplasticity surface for the model and plastic potential

- A criterion for tension failure (tension Cut – off) $F_T = Q_T = \sigma_n - \bar{f}_t(\kappa_3)$
- A Coulomb Criterion for Shear $F_S = \sqrt{(\sigma_s^2 + \sigma_t^2)} + \sigma_n \tan \phi - \bar{f}_s(\kappa_3)$ $Q_S = \sqrt{(\sigma_s^2 + \sigma_t^2)} + \sigma_n \tan \psi - c$
- A criterion for compression failure (cap) : $F_C = Q_C = C_{nn}\sigma_n^2 + C_{ss}(\sigma_s^2 + \sigma_t^2) + C_n\sigma_n - (\bar{\sigma}(\kappa_3))^2$

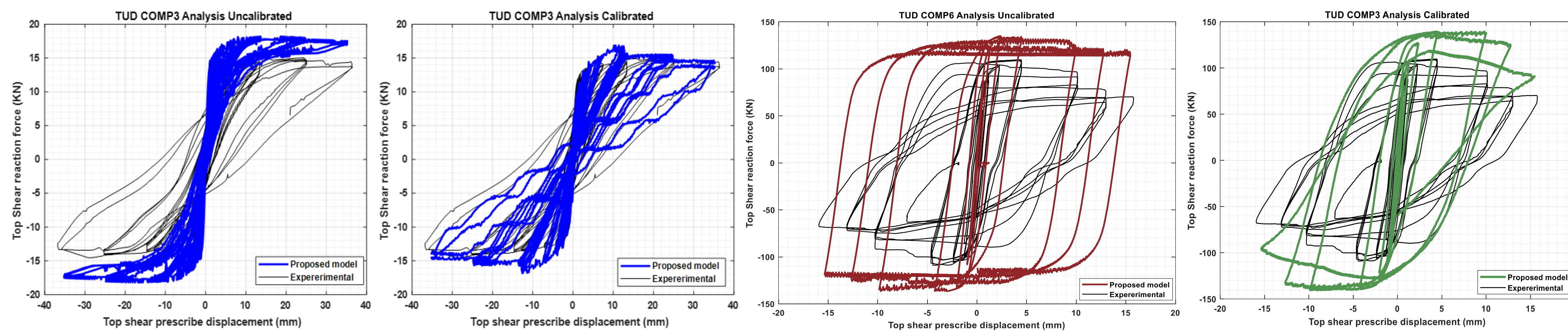
Multi-plastic threshold surface in 3 and 2 dimensions



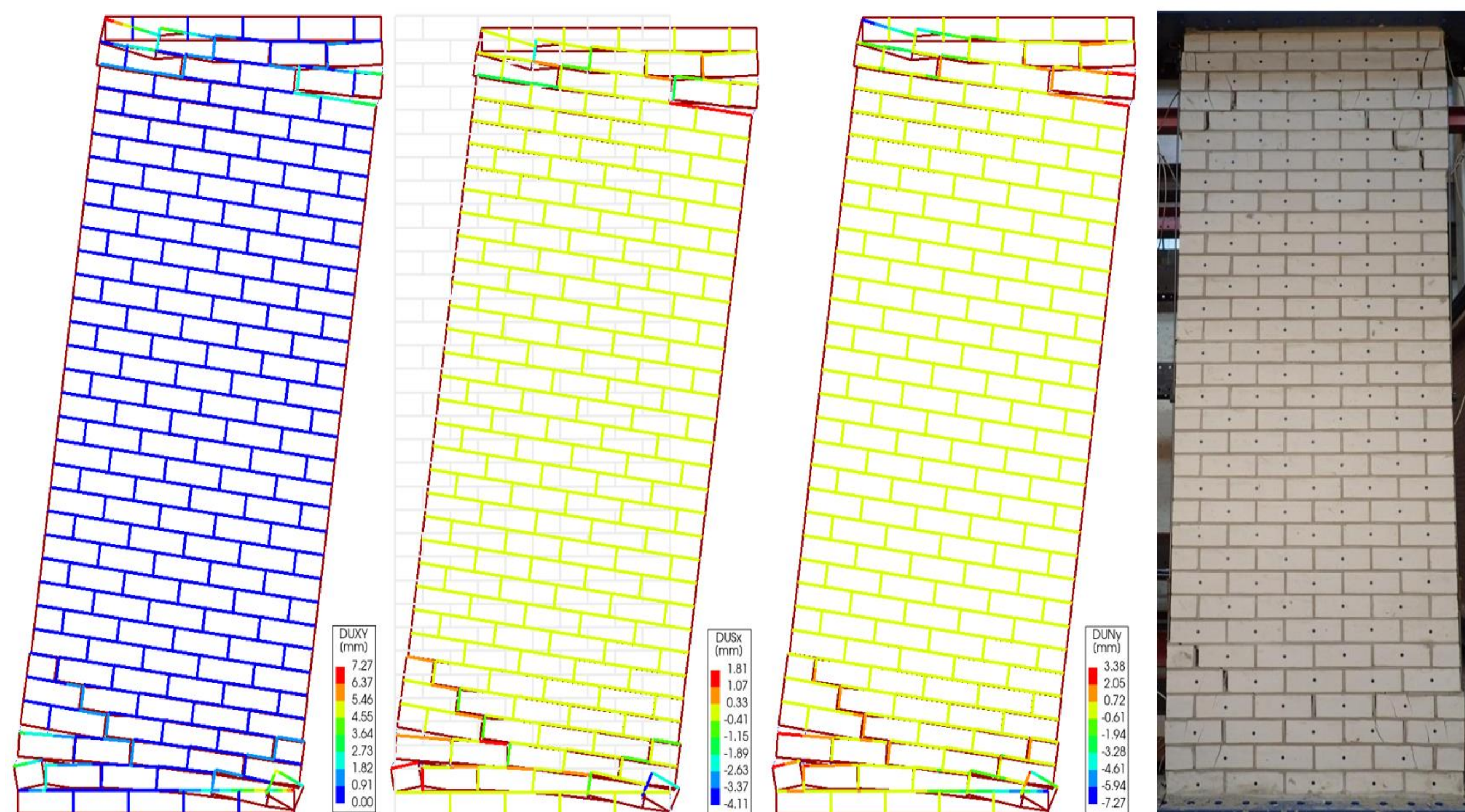
Material level validation of the model



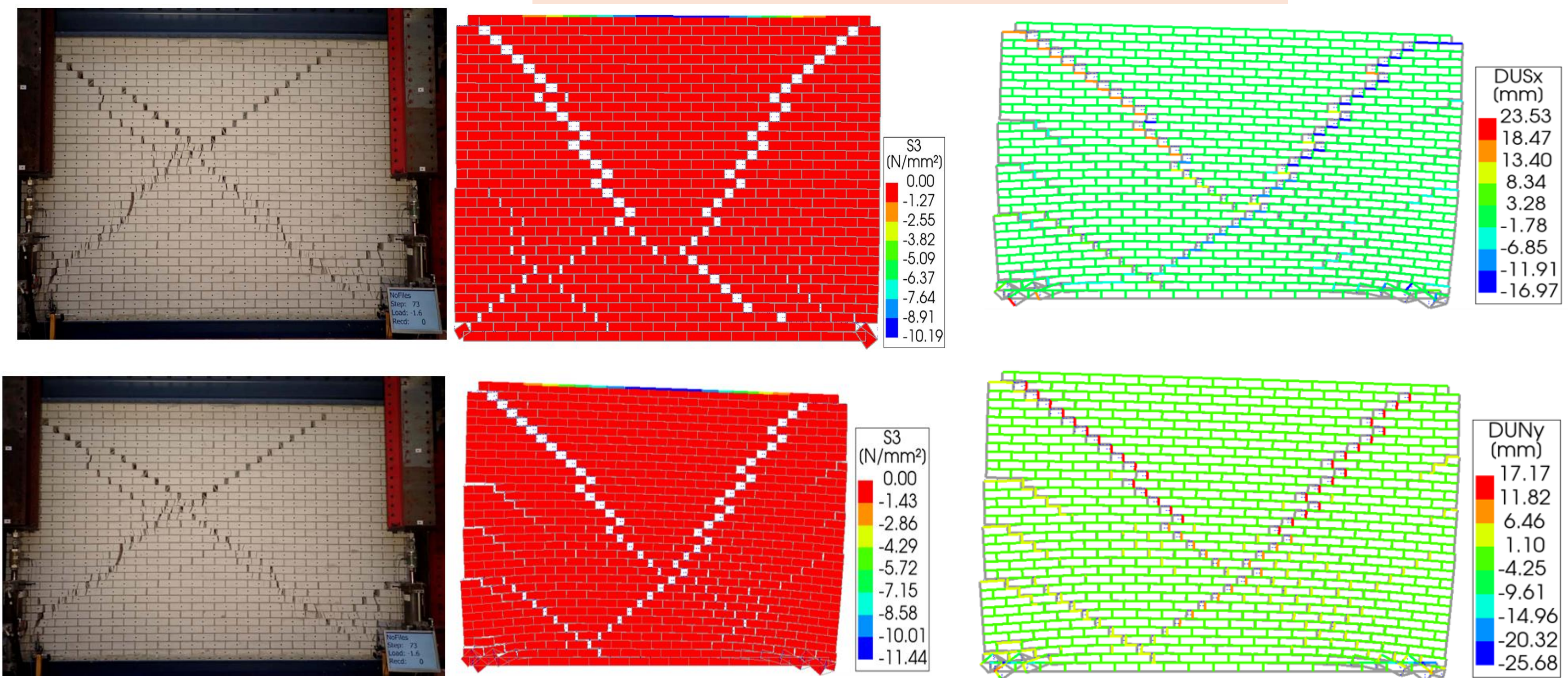
Structural level validation of the model



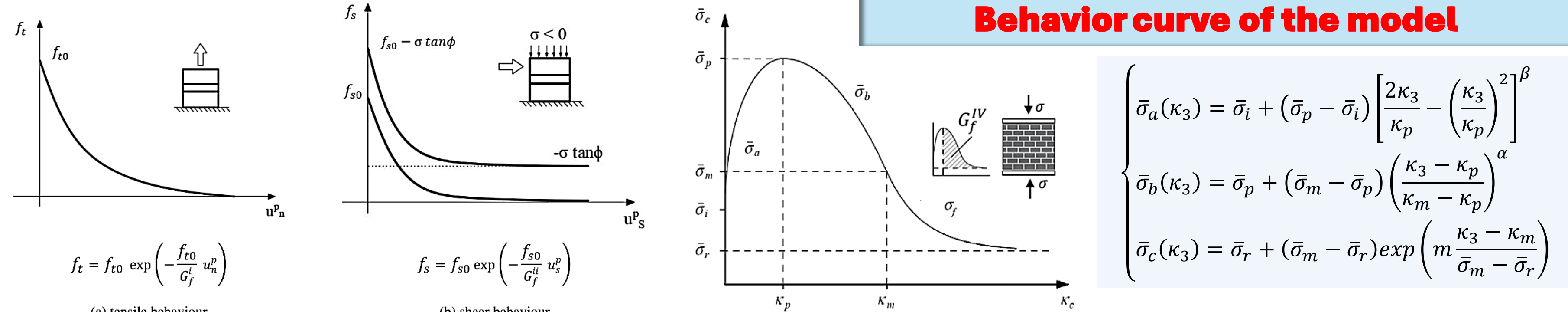
Crack pattern of the TUD_COMP3 wall



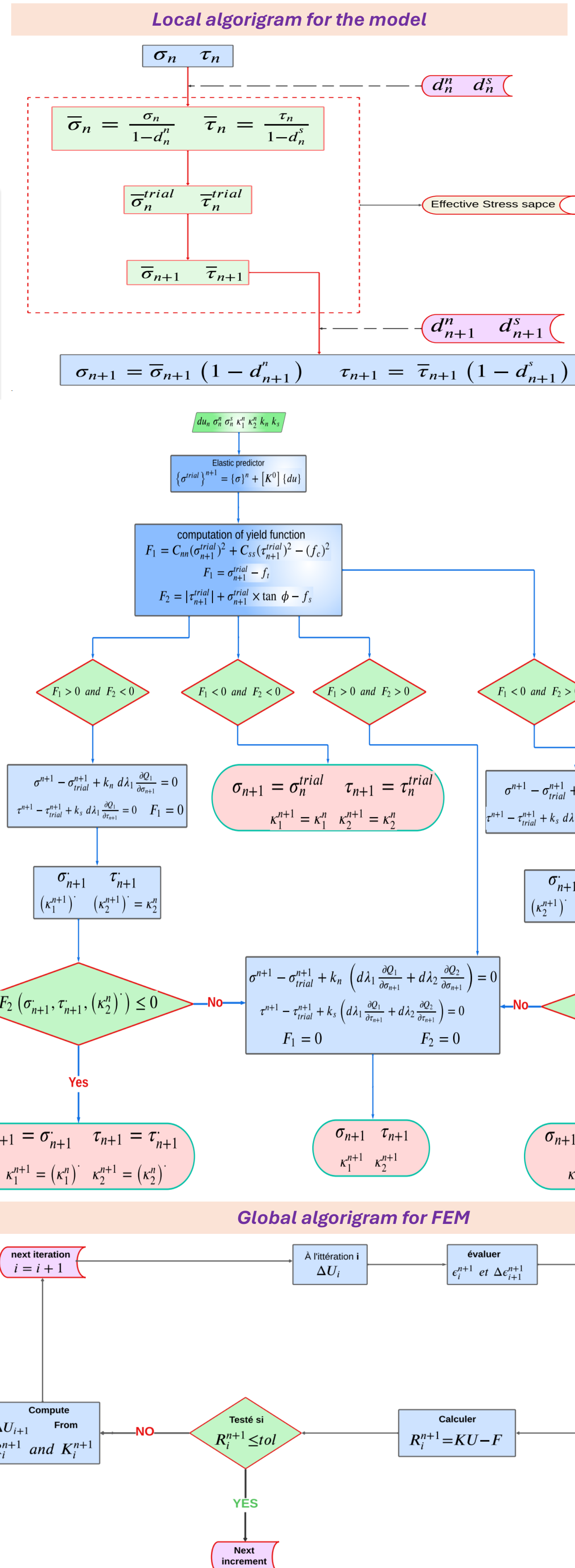
Crack pattern of the TUD_COMP6 wall



Behavior curve of the model



Local and global algorithm



Internal variables

tension and shear	coupling tension and shear
$\kappa_1 = \Delta u_n^p = \lambda_1$	$d\kappa_1 = \sqrt{\lambda_1^2 + \frac{G_f^2}{G_f^2} \frac{c^2}{f_t^2} \lambda_2^2}$
$\kappa_2 = \Delta u_s^p = \lambda_2$	$d\kappa_2 = \sqrt{\lambda_2^2 + \frac{G_f^2}{G_f^2} \frac{f_t^2}{c^2} \lambda_1^2}$
compression	
$\kappa_3 = 2\lambda_3\sqrt{(\sigma_n)^2 + (C_{ss}\sigma_s)^2}$	

Numerical implementation

General form of residual vector

$$\{R^j\} = \begin{Bmatrix} R_\sigma^j \\ R_f^j \end{Bmatrix} = \begin{Bmatrix} \{\sigma\}^{n+1} - \{\sigma^{trial}\}^{n+1} + [K_1] \sum_{i \in J_{ac}} \lambda_i^{n+1} \left(\frac{\partial Q_i}{\partial \{\sigma\}} \right)^{n+1} \\ F_i^j \end{Bmatrix}$$

General form of Jacobian Matrix

$$[J] = \frac{\partial R(\psi^j)}{\partial \psi^j} = \begin{bmatrix} [I] + \sum_{i \in J_{ac}} \lambda_i^{n+1} [K_1] \frac{\partial^2 Q_i}{\partial \{\sigma\}^2} & [K_1] \frac{\partial Q_i}{\partial \{\sigma\}} \\ \left(\frac{\partial F_i}{\partial \{\sigma\}} \right)^T & \left(\frac{\partial F_i}{\partial \lambda_i} \right)^T \end{bmatrix}$$

Consistent tangent operator

$$[\mathbb{L}_{n+1}^i] = \frac{\partial \sigma_{n+1}^i}{\partial \epsilon_{n+1}^i} = H - \frac{H \frac{\partial Q}{\partial \sigma} \gamma^T H}{h + \gamma^T H \frac{\partial Q}{\partial \sigma}}$$

Legend

- $\tan \phi$ Internal coefficient of friction
- $\tan \psi$ dilatancy
- c cohesion
- f_t tensile strength
- f_c compressive strength
- $[K_1] = (\mathbb{I} - [D])[K]$ Interface elasticity matrix
- $\{\sigma\}$ Vector of interface stress
- λ_i plastic multiplier
- C_{ss}, C_{nn} and C_n material parameters of cap

Wall geometry and load history

